# Supplementary information for an interlaboratory study of additively manufactured nickel alloy (IN625) tensile specimens 

Christopher U. Brown
Gregor Jacob
Mark Stoudt
Antonio Possolo
Shawn Moylan
Alkan Donmez

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National Institute of Standards and Technology
U.S. Department of Commerce

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Christopher U. Brown<br>Systems Integration Division<br>Engineering Laboratory

Gregor Jacob
Intelligent Systems Division
Engineering Laboratory
Mark Stoudt
Materials Science and Engineering Division Material Measurement Laboratory

Antonio Possolo<br>Statistical Engineering Division Information Technology Laboratory<br>Shawn Moylan<br>Intelligent Systems Division<br>Engineering Laboratory<br>Alkan Donmez<br>Intelligent Systems Division<br>Engineering Laboratory

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U.S. Department of Commerce Penny Pritzker, Secretary

National Institute of Standards and Technology

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## 1. INTRODUCTION

In fiscal year 2014, National Institute of Standards and Technology (NIST) conducted a round robin study to investigate the variation of mechanical properties of nickel alloy (IN 625) tensile specimens fabricated on six different laser-based powder bed fusion (LPBF) machines from the same machine vendor by six different institutions. The study results were summarized in a journal paper [1]. This report provides the supplementary information generated during planning and execution of the study. This supplementary information includes: (1) the manufacturing plan and blank process control document sent to the participants, (2) a description of the build programs sent to the participants, (3) engineering drawings with build instructions, (4) powder size distribution analysis of the powder sent to the participants, and (5) results obtained from a different LPBF machine. Copies of the process control documents received from the participants are provided in the Appendix.

During this study, the round robin coordinator identified a willing participant who had a LPBF machine from a different vendor. To obtain an additional data point for future comparative studies, this participant was invited to fabricate tensile specimens using the same powder and manufacturing plan with the process settings provided to the other participants. This participant was also sent the same individual tessellated and slice files to duplicate the process and fabricate the tensile bars. Upon receiving the build platform with the tensile specimens attached, NIST followed the same post processing procedures to heat treat them, extract the specimens, and prepare the specimens for the tension tests. This report ${ }^{1}$ also provides a comparison of tension test results and fracture analysis

[^0]between the results obtained from the main group of participants and the participant with a different LPBF machine (section 6).

## 2. MANUFACTURING PLAN AND BLANK PROCESS CONTROL DOCUMENT SENT TO PARTICIPANTS

NIST sent the following manufacturing plan and blank Process Control Document (PCD) to each participant before fabricating the specimens. The manufacturing plan consists of a detailed list of steps for each participant to follow in order to fabricate the build. NIST requested that the participants track the machine parameters used for the build in the Process Control Document (PCD). Participants returned the completed process control document back to NIST.

## Manufacturing Plan, NIST IN625 RR

The Manufacturing Plan defines the requirements to complete the desired work that is agreed upon by the supplier and purchaser. The Process Control Document is a procedure to ensure the requirements of the Manufacturing Plan are met. Together, the Manufacturing Plan and PCD tightly control and fully document the fabrication of test coupons for generating material property data.
0. Scope and Purpose of Study

Starting in May of 2014, NIST will conduct a round robin test to 1) further refine test protocols and analysis methods that will be used in future, more extensive round robin tests that will result in certification of AM materials, and 2) assess the variability in the tensile properties of additively made nickel alloy (Inconel 625) tension specimens from different institutions. The focus will be the Direct Metal Laser Sintering (DMLS) EOS M270/M280 process.

NIST will distribute virgin nickel chrome (IN625) powder and build plates for the participants. Before distribution, NIST will sample the various powder lots for subsequent powder analysis. Each participant will follow a NIST-provided manufacturing plan to make one single build of eight (8) tensile bars, using a NIST-provided build file. (In the cases where the NIST-provided EOS job file is not compatible, NIST will provide the necessary information for the participant to construct the job file.). Inability to comply with the manufacturing plan should be raised by the participant and approved by the study coordinator.

Each participant will send the tensile bars, still on the NIST-provided build plate, to NIST. NIST will coordinate the heat treatment, removal from the build plates, and testing the bars. NIST statistical experts will then perform the data analysis and make recommendations for test protocols and analysis methods for future round robins that lead to certification of AM materials. All results will be shared with the participants and may be published as well. The specific results from individual participants will not be publically attributed. All participants may keep any unused powder for their own future use.

## 1. Part Description

1.1. Engineering Drawing (the final geometry of the tensile specimen conforms to ASTM E8/E8M [2], dimensions are in mm's) :


Please note - the following revised drawing sent to the participants by email within the build files reflects the actual build design in the study. The original image in the manufacturing plan was an earlier version of the build design which was modified slightly. Dimensions are in mm's.

1.2. STL file: to be sent by email from study coordinator
1.3. EOSJOB file: to be sent by email from study coordinator
2. Machine Requirements
2.1. System
2.1.1.Process: Laser Powder Bed Fusion
2.1.2.Manufacturer: EOS
2.1.3.Model: EOSINT M270
2.1.4.Laser System: 200 W maximum power, $1060 \mathrm{~nm}-1100 \mathrm{~nm}$ wavelength (preferred IPG YLR-SM-200)
2.2. Software: EOS M270 Operating Software Version: PSW 3.5 rev 71 or newer preferred, not required.
2.3. Maintenance: All maintenance of the system must be current and documented.

Preventative maintenance must have been completed within 6 months of building the test specimens.
2.4. System Calibrations: All system calibrations shall be current and documented. Some of these calibrations should be completed as part of regular preventative maintenance (e.g., laser power, skywriting, etc.). Others should be performed by the individual users (e.g., beam offset, $x$ and $y$ scaling).
3. Powder Requirements
3.1. Powder shall be supplied to the participants by the study coordinator for use in this study.

The subsections below document the powder as procured by the study coordinator. Samples have been extracted from each powder container for further evaluation.
3.2. Chemistry (mass fraction):

Ni (balance $\geq 58.00 \mathrm{wt}-\%$ )
Cr (20.00-23.00wt - \%)

Mo (8.00-10.00 wt - \%)
Nb (3.15-4.15 wt - \%)
Fe ( $\leq 5.00 w t-\%)$
Ti ( $\leq 0.40 w t-\%)$
Al ( $\leq 0.40 \mathrm{wt}-\%$ )
Co ( $\leq 1.0$ wt - \%)
C ( $\leq 0.10$ wt - \%)
Ta ( $\leq 0.05 \mathrm{wt}-\%)$
$\mathrm{Si}, \mathrm{Mn}$ (each $\leq 0.50 \mathrm{wt}-\%)$
P, S (each $\leq 0.015$ wt - \%)
3.3. Powder Size and Distribution: mean diameter $=37.8 \mu \mathrm{~m} \pm 12.4 \mu \mathrm{~m}$. $\mathrm{D}(0.7)=40 \mu \mathrm{~m}$.
3.4. Recycling of Powder: Only virgin (per ASTM 2924) powder may be used to produce the components.

## 4. Process Set-Up Requirements

4.1. Platform: Build platforms can be provided to participants upon request. If a participant would prefer to use their own build platform, it should conform to the specifications below. An individual participant's build plate will be returned upon completion of the study.
4.1.1.Material: Platform must be AISI 1045 steel.
4.1.2.Thickness: Platform must be $20 \mathrm{~mm} \pm 2 \mathrm{~mm}$ thick.
4.1.3.Condition: Platform should be ground flat to a roughness of $R_{z}=10 \mu \mathrm{~m}$ or better. The platform demagnetized after grinding. The platform shall be thoroughly cleaned of machining lubricants prior to installation into the system. Once installed, the build platform surface shall be cleaned with alcohol using a lint free cloth and gloved hands.
4.1.4.Preheat: Platform shall be preheated to a temperature of $80^{\circ} \mathrm{C}$.
4.2. Recoater Blade: The blade shall be ceramic (EOS part HSS 2200-4073) and within the manufacturers specified useful lifetime and or original specification. The blade shall be maintained and cleaned according to manufacturer's guidelines.
4.3. Process Parameters: The study coordinator will provide, via email, an EOSJOB file with process parameters preset. Participants should check and document correct settings of all process parameters. All process parameters below are to be explicitly followed and reported. The process parameters are to be defined in the default job file and held constant throughout all builds unless otherwise agreed upon. Any changes in the default parameter set from build to build must be documented and carried forward in all reporting. All parameter sets are to be disclosed. Each job file will be saved and archived upon completion of the build for each and every build. All parameters that are unique to each system and that are not saved in the job file shall also be documented. A list of all process parameters shall be created and reported. The process parameter list shall
include all key parameters, system settings and machine conditions including but not limited to:
4.3.1.Base Parameter Set: The EOS MP1 (Cobalt-Chrome) parameter set for an EOS M270 with 200W laser machine using the layer thickness in 4.3 .2 shall be used.
4.3.2.Layer Thickness: $20 \mu \mathrm{~m}$ layers
4.3.3.Material Specific Settings
4.3.3.1. Material Dependent Scaling Factors (to be set at each machine for each machine). Scaling Factors may be determined from the EOS certification part and fine tuning spreadsheet

| X | Y | Z(0) | Z(200) |
| :--- | :--- | :--- | :--- |
| TBD by <br> participant | TBD by <br> participant | TBD by <br> participant | TBD by <br> participant |

4.3.3.2. Beam Offset (mm): May be determined from EOS certification part
4.3.3.3. Beam Expander Setting: 1
4.3.4.Adjust Tab
4.3.4.1. Groups: All individual parts shall be contained in their own group with the same exposure setting (4.3.5). The position and rotation of the group shall not be modified from 2.1.
4.3.4.2. $\quad$ Sorting: Sorting of parts by $X / Y / Z$ by smallest point.
4.3.5. Exposure Parameters
4.3.5.1. Pre exposure type: PreContour
4.3.5.1.1. First Contour

|  | Standard | OnPart | Downskin |
| :--- | :--- | :--- | :--- |
| Speed (mm/s): | 900.0 | 800.0 | 1600.0 |
| Power (W): | 100.0 | 100.0 | 100.0 |


| Beam Offset <br> (mm): | 0.000 |  | Contour | Yes (checked) |
| :--- | :--- | :--- | :--- | :--- |
| Thickness <br> (mm): | 0.040 |  | Post <br> Contour | No <br> (unchecked) |
| Corridor <br> $(\mathrm{mm}):$ | 0.040 |  |  |  |

4.3.5.1.2. Second Contour (Turned Off)

|  | Standard | OnPart | Downskin |
| :--- | :--- | :--- | :--- |
| Speed (mm/s): | - | - | - |
| Power (W): | - | - | - |


| Beam Offset <br> $(\mathrm{mm}):$ | - |  | Contour | No <br> (unchecked) |
| :--- | :--- | :--- | :--- | :--- |
| Thickness <br> $(\mathrm{mm}):$ | - |  | Post Contour | No <br> (unchecked) |


| Corridor <br> $(\mathrm{mm}):$ | - |  |  |  |
| :--- | :--- | :--- | :--- | :--- |

4.3.5.1.3. Edges (Turned Off)

| Edge factor | - |  | Edges | No <br> (unchecked) |
| :--- | :--- | :--- | :--- | :--- |
| Threshold: | - |  | Post Edge | No <br> (unchecked) |
| Minimum <br> radius factor: | - |  |  |  |
| Beam offset <br> (mm): | - |  |  |  |
| Speed <br> (mm/s): | - |  |  |  |
| Power (W): | - |  |  |  |

### 4.3.5.2. Skin exposure type: OuterSkin

4.3.5.2.1. Stripes

| Distance <br> $(\mathrm{mm}):$ | 0.10 |  | Stripe width <br> $(\mathrm{mm}):$ | 4.00 |
| :--- | :--- | :--- | :--- | :--- |
| Speed <br> $(\mathrm{mm} / \mathrm{s}):$ | 800.0 | Stripes overlap <br> $(\mathrm{mm}):$ | 0.10 |  |
| Power (W): | 195.0 | Skywriting: | Yes (checked) |  |
| Beam offset <br> (mm) | 0.030 | Offset: | Yes (checked) |  |
| Hatching, X | Yes (checked) |  | Alternating: | Yes (checked) |
| Hatching, Y | Yes (checked) |  | Rotating: | Yes (checked) |
|  |  | Rotated Angle | $67^{\circ}$ |  |

*may not be available for specification

### 4.3.5.2.2. UpDown

|  | Upskin | Downskin |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Distance <br> (mm): | 0.05 | 0.05 |  | Overlap <br> with inskin <br> (mm): | 0.10 |
| Speed <br> (mm/s): | 800.0 | 3000.0 |  | Min. length <br> (mm): | 2.00 |
| Power (W): | 195.0 | 195.0 |  |  |  |
| Thickness <br> (mm): | 0.00 | 0.04 |  |  |  |
| X: | Yes <br> (checked) | Yes <br> (checked) |  |  |  |
| Y: | Yes <br> (checked) | Yes <br> (checked) |  |  |  |
| Alternating | No <br> (unchecked) | No <br> (unchecked) |  | Skywriting | Yes <br> (checked) |

4.3.5.2.3. Skip layer

| Skipped layers: | 0 |
| :--- | :--- |
| Offset layers: | 0 |
| Expose first layer: | Yes (checked) |

4.3.5.3. Core exposure type: InnerSkin
4.3.5.3.1. Chess

|  | Squares | Gap |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Distance <br> (mm): | 0.10 | 0.10 |  | Square <br> width (mm): | 8.00 |
| Speed <br> (mm/s): | 800.0 | 800.0 |  | Gap width <br> (mm): | 0.00 |
| Power (W): | 195.0 | 195.0 |  | Overlap <br> (mm): | 0.08 |
|  |  |  |  | Alternating: | Yes <br> (checked) |
| Beam <br> offset: | -0.050 |  |  | Rotated: | Yes <br> (checked) |
| Hatching: | X=Yes <br> (checked) | Y = Yes <br> (checked) |  | Offset: | Yes <br> (checked) |
| Skywriting: | No <br> (unchecked) |  |  |  |  |

4.3.5.3.2. Skip layer

| Skipped layers: | 0 |
| :--- | :--- |
| Offset layers: | 0 |
| Expose first layer: | Yes (checked) |

### 4.3.5.4. Post exposure type: Postcontour

4.3.5.4.1. First Contour

|  | Standard | OnPart | Downskin |
| :--- | :--- | :--- | :--- |
| Speed $(\mathrm{mm} / \mathrm{s}):$ | 900.0 | 800.0 | 1600.0 |
| Power $(\mathrm{W}):$ | 120.0 | 120.0 | 120.0 |


| Beam Offset <br> $(\mathrm{mm}):$ | 0.015 |  | Contour | Yes (checked) |
| :--- | :--- | :--- | :--- | :--- |
| Thickness <br> $(\mathrm{mm}):$ | 0.040 |  | Post Contour | Yes (checked) |
| Corridor <br> $(\mathrm{mm}):$ | 0.040 |  |  |  |

4.3.5.4.2. Second Contour (Turned Off)

|  | Standard | OnPart | Downskin |
| :--- | :--- | :--- | :--- |
| Speed $(\mathrm{mm} / \mathrm{s}):$ | - | - | - |
| Power $(\mathrm{W}):$ | - | - | - |


| Beam Offset <br> $(\mathrm{mm}):$ | - |  | Contour | No <br> (unchecked) |
| :--- | :--- | :--- | :--- | :--- |
| Thickness <br> $(\mathrm{mm}):$ | - |  | Post Contour | No <br> (unchecked) |
| Corridor <br> $(\mathrm{mm}):$ | - |  |  |  |

4.3.5.4.3.

Edges

| Edge factor | 2.00 |  | Edges | Yes (checked) |
| :--- | :--- | :--- | :--- | :--- |
| Threshold: | 3.0 |  | Post Edge | Yes (checked) |
| Minimum <br> radius factor: | 0.00 |  |  |  |
| Beam offset <br> (mm): | 0.000 |  |  |  |
| Speed <br> (mm/s): | 900.0 |  |  |  |
| Power (W): | 100.0 |  |  |  |

4.3.5.5. Skin Thickness (x/y): 3.00 mm
4.3.5.6. $\quad$ Skin Thickness (z): 3.00 mm
4.3.5.7. Base radius: 0.00 mm
4.3.5.8. Core open to platform: No (unchecked)
4.3.5.9. Skin/Core: Yes (checked)
4.3.6.Setting
4.3.6.1. Part Specific Scaling: $0 \%$ in $X$ and $Y$
4.3.6.2. Material Dependent Scaling $0 \%$ in $X$ and $Y$
4.3.6.3. Part Specific Undersize/Oversize: 0 mm
4.3.7.Building
4.3.7.1. Start Height: 0.02 mm
4.3.7.2. Final Height: the height of the tallest part in 1.2 ( 4.18 mm )
4.3.7.3. Layer Thickness: See 4.3.2
4.3.8.DMLS
4.3.8.1. DMLS: DMLS shall be unchecked
4.3.8.2. Pre-exposure: Pre-exposure shall be set to 0.06 mm (3 layers).
4.3.9.Recoating.
4.3.9.1. Minimum charge amount: 150 \%
4.3.9.2. Maximum charge amount: $200 \%$
4.3.9.3. Dosing boost amount: 300 \%
4.3.9.4. Recoater speed 1: $500 \mathrm{~mm} / \mathrm{s}$
4.3.9.5. Recoater speed 2: $80 \mathrm{~mm} / \mathrm{s}$
4.3.9.6. Lower dispenser platform: 1.00 mm
4.3.9.7. Contact-free outward travel: yes (checked)
4.4. Build Chamber Environment
4.4.1.Purge Gas: For the purpose of this study, nitrogen will be used as the inert gas within the process chamber. Nitrogen 'sourced' from a nitrogen generator, bottle, or dewar is allowable. If the Nitrogen is from a bottle or dewar, user should report the nominal gas purity.
4.4.2.Flow Rates: Flow rates set within manufacturers' specification.
4.4.2.1. Flow Meters set on the front of the machine ( 5 meters)
4.4.2.2. Flow meter set (voltage) on the filtration unit
4.4.3.Filtration: Filtration must be enabled. Filter maintenance must be current per manufacturer guidelines
4.4.4.Oxygen Level: Oxygen level must be less than 1.3 \% oxygen (15000 ppm) maximum.

### 4.5. Required Quality Control Checks at Build Start

The following Quality Control Checks are required to be performed sequentially before beginning the build.
4.5.1.System Maintenance and Cleaning: All system maintenance must be performed and the interior of the chamber, including optical components, powder hoppers, recoater blade, shall be cleaned per manufacturer guidelines.
4.5.2.Laser Power: The laser power shall be measured (if possible) using a laser power meter within calibration at all power levels prescribed in 4.3 and fall within $10 \%$ of the prescribed value. Each measurement is to be reported as setpoint, displayed and measured value. If any value is outside the prescribed value, the individual measurement shall be repeated and if the average of 3 measurements exceeds the power range, corrective action should be taken which includes laser maintenance and adjusting the setpoint value to achieve the desired delivered laser power.
4.5.3.Installation of Platform: Platform may be installed after completion requirements in 4.5.1 and 4.5.2. The build platform shall be parallel to the recoating blade and recoating arm motion to within $50 \mu \mathrm{~m}$. Preferred method of levelling to recoating blade uses feeler gage/ shims between build platform and recoating blade. Preferred method of levelling to recoating arm motion uses dial indicator mounted to recoating arm. After installation and levelling of the platform, it shall be cleaned in a manner described in 4.1.3.
4.5.4.Powder Loading: New powder, directly from containers, must be loaded into the dispenser per manufacturer guidelines (sieving not necessary). Sufficient quantities shall be loaded to achieve a complete build without the need to refill. Any devices used to stab, pack or tamp the powder must be stainless steel and cleaned using acetone and wiped with a lint free cloth prior to inserting into the powder.
4.5.5.First layer: Once the build platform is leveled and the powder is loaded, railed, packed and smoothed, the first layer shall be created. The recoating arm should be past the dispenser platform. The build platform should be brought up to the level of the recoating blade,
then lowered by the distance equal to one layer thickness. The dispenser platform shall be raised to a height to expose enough powder to deposit one layer as well as fill any gaps, holes, crevices, etc. between the dispenser platform and the collector bin. The recoating arm shall then be moved across the dispenser platform and build platform (to the home position) at the speed described in 4.3.9.5.
4.5.6.Platform Temperature: The platform temperature must be within $5{ }^{\circ} \mathrm{C}$ of the value prescribed in 4.1.4. Record the platform temperature at the start of the build.
4.5.7.Oxygen Level: The oxygen level must be less than the level prescribed in 4.4.4. Record the oxygen level at the start of the build process.

## 5. In Process Requirements

### 5.1. Limits

5.1.1.Environment: If during processing the oxygen level in the build chamber exceeds the level prescribed in 4.4.4, the build shall be stopped.
5.2. Build Pause/Interruption
5.2.1. No planned interruption of the build is required.
5.2.2.Any interruption to the continuous build cycle must be recorded with a description of the reason for the interruption and corrective action.
5.2.3. Prior to opening the build chamber, the oxygen level and platform temperature must be recorded.
5.2.4.Upon continuation of the build, the requirements of 4.5.6 and 4.5.7 must be met and preferably be within $10 \%$ of the values recorded in 5.2.3.
6. Process Completion Requirements
6.1. Removal from System
6.1.1.The build shall be allowed to cool inside the build chamber submerged in powder under protective environment until the temperature drops below $30^{\circ} \mathrm{C}$.
6.1.2. The temperature and oxygen level shall be recorded prior to opening the build chamber.
6.1.3.The build and platform shall be removed from the chamber and cleaned of loose powder using a non-metallic brush.
6.1.4.The build and platform may be further cleaned by using a metallic brush or other means to remove partially sintered powder particles.
6.1.5.Laser Power: The laser power shall be measured (if possible) using a laser power meter within calibration at all power levels prescribed in 4.3. Each measurement is to be reported as setpoint, displayed and measured value.
6.1.6.Cleaning: The system may be cleaned at this point following manufacturer guidelines.

### 6.2. Powder Recovery

6.2.1.Excess, loose powder removed from the build platform through the completion of 6.1.3 shall be collected and stored in appropriately marked containers indicating that it is USED.
6.2.2.Any partially sintered material is not allowable for reuse and should be disposed of properly.
6.2.3.Participants may keep any unused powder for their own use.
7. Post Process Requirements
7.1. Heat treat
7.2. Machine samples
7.2.1. Mill top surface
7.2.2. Remove samples by electric discharge machining (EDM)
7.2.3.EDM gage section
7.2.4.Grind remaining surfaces
8. Reporting
8.1. Part Technical Data
8.2. Machine Technical Data
8.3. Powder Technical Data
8.4. Process Setup Technical Data
8.5. In Process Technical Data
8.6. Process Completion Technical Data
8.7. Post Process Technical Data
8.8. Testing Technical Data

## Process Control Document

Technical Data (section numbers refer to Manufacturing Plan)
Part Manufacturing Technical Data
Completed by the part manufacturer

|  | Value | Requirement <br> Section | Approval |
| :--- | :--- | :---: | :---: |
| Job Number |  |  |  |
| Build File Name: |  | 1.2 |  |
| Process |  | 2.1 .1 |  |
| Equipment <br> Manufacturer and <br> Model: |  | 2.1 .2 |  |
| Equipment Serial <br> Number: |  | 2.1 .4 |  |
| Laser Manufacturer <br> and Model: |  |  |  |
| Laser Serial Number: |  | 2.2 |  |
| Software Version: |  |  |  |


| Date of last preventative maintenance |  | 2.3 |  |
| :---: | :---: | :---: | :---: |
| System Calibration Current |  | 2.4 |  |
| Material <br> Requirements |  |  |  |
| Verify Powder <br> Heat/Lot Loaded <br> Matches Feedstock <br> Technical Data |  |  |  |
| Material Condition (Virgin/Recycled) |  | 3.4 |  |
| Process Setup Requirements |  |  |  |
| Build Platform Material |  | 4.1.1 |  |
| Build Platform <br> Thickness |  | 4.1.2 |  |
| Build Platform Condition |  | 4.1.3 |  |
| Build Platform <br> Preheat, ${ }^{\circ} \mathrm{C}$ |  | 4.1.4 |  |
| Recoater Blade <br> Material/Part Number |  | 4.2 |  |
| Process Parameter Settings |  |  |  |
| Base Parameter Set |  | 4.3.1 |  |
| Base Parameter Filename |  |  |  |
| Layer Thickness, $\mu \mathrm{m}$ |  | 4.3.2 |  |
|  |  |  |  |
| Sort Parts Method: |  | 4.3.4.2 |  |
| Exposure Parameters | Complete Exposure Parameters Table Below | 4.3.5 |  |
| Pre Contour Type |  | 4.3.5.1 |  |
| Skin Exposure Type |  | 4.3.5.2 |  |
| Core Exposure Type |  | 4.3.5.3 |  |
| Post Contour Type |  | 4.3.5.4 |  |
| Skin Thickness (x/y), mm |  | 4.3.5.5 |  |
| Skin Thickness (z), mm |  | 4.3.5.6 |  |
| Base Radius: |  | 4.3.5.7 |  |
| Core open to platform?: |  | 4.3.5.8 |  |
| Skin/Core: |  | 4.3.5.9 |  |
| Scaling and Offset |  |  |  |




## Exposure Parameters

Completed by the part manufacturer

|  | Value | Requirement <br> Section | Approval |
| :--- | :---: | :---: | :---: |


| Job Number |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Build File Name: |  |  |  |  |  |  |
| Pre Exposure |  |  |  |  |  |  |
| Pre Exposure Type |  |  |  |  | 4.3.5.1 |  |
| First Contour |  | Standard | OnPart | Downskin | 4.3.5.1.1 |  |
|  | $\begin{gathered} \hline \text { Speed } \\ (\mathrm{mm} / \mathrm{s}) \text { : } \end{gathered}$ |  |  |  |  |  |
|  | Power (W): |  |  |  |  |  |
|  | Beam Offset (mm): |  | Contour |  |  |  |
|  | Thickness ( mm ): |  | Post <br> Contour |  |  |  |
|  | Corridor (mm): |  |  |  |  |  |
| Second Contour |  | Standard | OnPart | Downskin | 4.3.5.1.2 |  |
|  | $\begin{gathered} \hline \text { Speed } \\ (\mathrm{mm} / \mathrm{s}) \text { : } \end{gathered}$ |  |  |  |  |  |
|  | Power (W): |  |  |  |  |  |
|  | Beam Offset (mm): |  | Contour |  |  |  |
|  | Thickness (mm): |  | Post Contour |  |  |  |
|  | Corridor ( mm ): |  |  |  |  |  |
| Edges | Edge factor |  | Edges |  | 4.3.5.1.3 |  |
|  | Threshold: |  | Post Edge |  |  |  |
|  | Minimum radius factor: |  |  |  |  |  |
|  | Beam offset (mm): |  |  |  |  |  |
|  | Speed ( $\mathrm{mm} / \mathrm{s}$ ): |  |  |  |  |  |
|  | Power (W): |  |  |  |  |  |
| Skin Exposure |  |  |  |  |  |  |
| Skin Exposure Type |  |  |  |  | 4.3.5.2 |  |
| Stripes | Distance (mm): |  | Stripe width (mm): |  | 4.3.5.2.1 |  |


|  | $\begin{gathered} \text { Speed } \\ (\mathrm{mm} / \mathrm{s}) \text { : } \end{gathered}$ |  | Stripes overlap (mm): |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Power (W): |  | Skywriting: |  |  |  |
|  | $\begin{gathered} \text { Beam } \\ \text { offset (mm) } \end{gathered}$ |  | Offset: |  |  |  |
|  | Hatching, $X$ |  | Alternating: |  |  |  |
|  | Hatching, Y |  | Rotating: |  |  |  |
| UpDown |  | Upskin | Downskin |  | 4.3.5.2.2 |  |
|  | Distance (mm): |  |  |  |  |  |
|  | $\begin{aligned} & \text { Speed } \\ & (\mathrm{mm}) \text { : } \end{aligned}$ |  |  |  |  |  |
|  | Power (W): |  |  |  |  |  |
|  | Thickness (mm): |  |  |  |  |  |
|  | X : |  |  |  |  |  |
|  | $Y$ : |  |  |  |  |  |
|  | Alternating: |  | Overlap with inskin(mm): |  |  |  |
|  | Skywriting: |  | $\begin{aligned} & \text { Min. length } \\ & (\mathrm{mm}) \end{aligned}$ |  |  |  |
| Skip Layer | Skipped Layers |  |  |  | 4.3.5.2.3 |  |
|  | Offset layers: |  |  |  |  |  |
|  | Expose first layer: |  |  |  |  |  |
|  |  |  | ore Exposure |  |  |  |
| Core Exposure Type |  |  |  |  | 4.3.5.3 |  |
| Chess |  | Squares | Gap |  |  |  |
|  | Distance (mm): |  |  |  |  |  |
|  | $\begin{aligned} & \text { Speed } \\ & (\mathrm{mm} / \mathrm{s}) \text { : } \end{aligned}$ |  |  |  |  |  |
|  | Power (W): |  |  |  |  |  |
|  | Width (mm): |  |  |  |  |  |
|  | $\begin{gathered} \text { Beam } \\ \text { offset (mm) } \end{gathered}$ |  | Overlap: |  |  |  |
|  | Hatching, X: |  | Alternating: |  |  |  |



## 3. BUILD FILES SENT TO THE PARTICIPANTS

Figure 1 shows a block diagram of the process of developing build files from the initial computer solid models using various software modules. NIST sent the computer files to all the participants.

## Round Robin 2014 Build File Management



Figure 1. Block diagram of the process of developing the build files.

Material setting: "MP1_020_100_Surface" (default)

NIST generated the following build files and distributed them to the participants:

- Six STL files, named: "RR_IN625_tensile_x.stl" where $x=1$ to 6 for each of the 6 tensile bars
- Six CLI support structure related files, named: RR_IN625_tensile_x_Om. cli where $x=1$ to 6
- One Magics file, named: "AM_Round Robin IN625_tensile specimens.magics"
- six part related slice files named: "RR_IN625_tensile_x_p.sli" where $x=1$ to 6
- six support structure related slice files named: "RR_IN625_tensile_x_Om.sli" where $x=1$ to 6 for each of the 6 tensile bars
- One EOS build file, named: "AM_Round Robin_Inconel 625.eosjob"


## 4. ENGINEERING DRAWINGS WITH BUILD INSTRUCTIONS SENT TO PARTICIPANTS

Engineering drawings of the build with post processing directions.






Engineering drawing of the final tensile specimens:


## 5. ANALYSIS OF PARTICLE SIZE DISTRIBUTION OF THE POWDERS SENT TO PARTICIPANTS

## IN625 powder size distribution as determined using sieves

ASTM B214 [3] was followed to perform the sieve analysis for each of the 15 buckets of IN625 powder sent to the participants. Originally two buckets were distributed to each of the 7 participants; however, one bucket was misplaced and therefore a fifteenth, replacement bucket, was issued. All 15 buckets were from the same manufacturing lot (M111201). Seven sieves were chosen based on the expected maximum size of the powder. The chosen US Standard sieve sizes were: $230(75 \mu \mathrm{~m}>63 \mu \mathrm{~m})$, $270(63 \mu \mathrm{~m}>53 \mu \mathrm{~m}), 325(53 \mu \mathrm{~m}>45 \mu \mathrm{~m}), 400(45 \mu \mathrm{~m}>38 \mu \mathrm{~m}), 450(38 \mu \mathrm{~m}>32 \mu \mathrm{~m}), 500(32 \mu \mathrm{~m}>$ $25 \mu \mathrm{~m}), 635(25 \mu \mathrm{~m}>20 \mu \mathrm{~m})$, and pan (> $20 \mu \mathrm{~m}$ ). According to the powder's mill certificate, $98 \%$ of the powder was expected to be $53 \mu \mathrm{~m}$ or smaller, therefore one sieve size larger than $53 \mu \mathrm{~m}$ was used, sieve 230 (US Standard size).

The powder in each sieve was determined using a mass balance and the cumulative mass percent was calculated for each sieve. Figure 2 is an example plot from one of the powder samples. The data was used to approximate the powder diameter at cumulating mass percentages of $10 \%$ (D10), 50 \% (D50), and 90 \% (D90). In other words, the D50 for a given powder as determined by sieving indicates $50 \%$ of the powder mass has this diameter size or smaller.


Figure 2. Cumulative mass (\%) versus powder size ( $\mu \mathrm{m}$ ) versus for one of the IN625 powder samples. The data in this plot was used to approximate the powder diameter at the cumulative mass percentages of $10 \%, 50 \%$, and $90 \%$ for each powder bucket (see ASTM E11 for sieve variation [4]).

A line was chosen to connect the data points however it is possible that the actual powder size distribution between the sieves does not follow a straight line. To report the diameter at the cumulative mass percent at $10 \%, 50 \%$, and $90 \%$, linear interpolation was chosen to approximate the powder diameter at these percentages. Thus the D50 for the distribution in Figure 2 is $35 \mu \mathrm{~m}$, or in other words, $50 \%$ of the powder mass has a diameter of $35 \mu \mathrm{~m}$ or smaller. Table 1 lists the powder diameter for each bucket as determined by sieving.

Table 1. The powder diameter determined by sieving for each of the 15 participant buckets of IN625.

The $10 \%, 50 \%$, and $90 \%$ cumulative mass percentages are shown along with the average and standard deviation.

| Bucket \# | D10 | D50 | D90 |
| :---: | :---: | :---: | :---: |
| 1 | 20.32 | 34.85 | 50.54 |
| 2 | 14.59 | 34.68 | 49.82 |
| 3 | 10.59 | 30.84 | 48.3 |
| 4 | 22.28 | 35.4 | 50.36 |
| 5 | 21.03 | 36.36 | 51.5 |
| 6 | 22.15 | 36.41 | 51.18 |
| 7 | 16.68 | 33.29 | 48.88 |
| 8 | 19.65 | 33.98 | 49.33 |
| 9 | 21.14 | 34.37 | 49.66 |
| 10 | 14.08 | 32.28 | 48.89 |
| 11 | 21.95 | 36.57 | 51.48 |
| 12 | 16.12 | 33.22 | 48.79 |
| 13 | 13.99 | 31.79 | 48.86 |
| 14 | 20.67 | 35.47 | 50.98 |
| 15 | 21.69 | 35.29 | 50.72 |
|  |  |  |  |
| Average $=$ | 18.46 | 34.32 | 49.95 |
| St D $=$ | 3.77 | 1.74 | 1.08 |

## IN625 powder size distribution as determined using laser diffraction

Table 2 lists the particle size distribution measured using laser diffraction of the 15 buckets of IN625 that were distributed to the participants. The technique involves using isopropanol (IPA) to suspend the powder. The D10, D50, and D90 values are based on a cumulative volume percentage, rather than a cumulative mass percent as is used for sieve analysis. In other words, the D50 for a given powder as determined by laser diffraction indicates $50 \%$ of the powder volume has this diameter size or
smaller. The average powder diameter ( $\mu \mathrm{m}$ ) for D10, D50, and D90 are shown at the bottom along with the corresponding standard deviation.

Table 2. Powder distribution as determined using laser diffraction for each of the 15 participant buckets of IN625. The diameter at the $10 \%, 50 \%$ and $90 \%$ cumulative volume percentages are shown for each bucket along with the average and standard deviation.

IN625
Bucket

| $\#$ | Label | $\underline{\text { D10 }}$ | $\underline{\text { D50 }}$ | $\underline{\text { D90 }}$ |
| :---: | :---: | :---: | :---: | :---: |
| 1 | A | 16.122 | 28.293 | 49.243 |
| 2 | B | 14.609 | 24.723 | 42.127 |
| 3 | C | 15.752 | 26.51 | 44.861 |
| 4 | D | 14.645 | 25.224 | 43.875 |
| 5 | E | 14.895 | 24.908 | 41.779 |
| 6 | F | 15.321 | 25.972 | 43.797 |
| 7 | G | 15.696 | 27.623 | 48.657 |
| 8 | H | 15.362 | 26.554 | 45.823 |
| 9 | I | 15.642 | 26.605 | 45.047 |
| 10 | J | 15.561 | 27.962 | 50.103 |
| 11 | K | 17.389 | 28.396 | 45.749 |
| 12 | L | 15.39 | 26.589 | 45.748 |
| 13 | M | 15.251 | 26.063 | 44.773 |
| 14 | N | 15.065 | 26.152 | 45.634 |
| 15 | P | 15.336 | 26.009 | 44.718 |


| Average | 15.469 | 26.506 | 45.462 |
| :---: | ---: | ---: | ---: |
| St Dev | 0.671 | 1.146 | 2.359 |

Figure 3 shows the volume percent versus particle size ( $\mu \mathrm{m}$ ) as determined by laser diffraction for all 15 powder samples.


Figure 3. Volume percent versus powder diameter for all 15 samples of IN625 powder. The legend shows a different symbol for each of the 15 buckets.

## Comments on the size distribution results

Although the main goal of this study was not comparing the results of different size distribution techniques, we did want to understand the size distribution of our powder used by the participants. The vendor powder specification reported $98 \%$ of the powder mass should have a diameter of $53 \mu \mathrm{~m}$ or smaller. Our sieve results showed that $98 \%$ of the powder mass had a diameter of $58.02 \mu \mathrm{~m} \pm 2.72 \mu \mathrm{~m}$ or smaller.

## 6. TENSION SPECIMENS FABRICATED ON A DIFFERENT LPBF MACHINE

During this study, the round robin coordinator identified a willing participant who had a LPBF machine from a different vendor. NIST sent this participant the same powder and the same individual tessellated and slice files to fabricate the parts as sent to the other participants. This participant used the manufacturing plan and the files to duplicate the process parameters in their machine. Upon receiving the build platform with the tensile specimens attached, NIST followed the same post processing procedures to heat treat, extract the specimens, and prepare the specimens for the tension tests. The statistical analysis was conducted on the tension test results, including the specimens from the different LPBF machine.

## Statistical analysis

The yield strength (YS), ultimate tensile strength (UTS), elongation after fracture (A), and Young's modulus (E), were measured for 6 test specimens produced by each participant. Figure 4 shows summaries of these results, in the form of boxplots. Each rectangular box comprises the middlemost 50 \% of the data, the thick horizontal line within the box marks the median, and the whiskers, if present, extend to the extreme data points. Circles indicate potential outliers: values that lie farther than 1.5 times the inter-quartile range from either the top or bottom sides of a box. As seen in these plots, the tensile properties of the specimens from the last participant (with a different LPBF machine) are clearly different than the properties obtained from the specimens fabricated on the other participants' machines. Therefore, the results from participant \#7 were not included in the following statistical analysis.


Figure 4. Boxplots of tension test results of the specimens received from all participants. Box plots of measured mechanical properties from all participants including Lab 7. The data from Labs 1 through 6 were used in the statistical analysis. Results from the additional participant, Lab 7, that used a different LPBF machine, are also shown.

Values of the following covariates were also reported by almost all participants: energy density, volume rate, layer thickness, and skin power. However, these attributes had only two or three different values, and their values varied between some of the laboratories, but never within a laboratory.

The statistical model for the value $x_{i, j}$ of each of the four measurands (YS, UTS, A and E) measured on test coupon $i$ produced by laboratory $j$ expresses it as an additive superposition of three different effects, $x_{i, j}=\mu+\alpha+b_{j}+e_{i, j}$. This is called a mixed effects model [5] because $\mu$ and $\alpha$ are treated
as fixed effects, and the $b_{j}$ and $e_{i, j}$ are treated as random effects. For YS , for example, $\mu$ denotes the true value of the yield strength for this material that results from this manufacturing process, $\alpha$ is the effect of a particular covariate (for example, energy density), $b_{j}$ is the effect of laboratory $j$, and $e_{i, j}$ is the effect of this particular coupon, all for $j=1, \ldots, n$, with $n=6$ participants, and $i=1, \ldots, m_{j}$, where $m_{j}=6$ denotes the number of coupons from participant $j$ that were used in the analysis.

The fact that the covariates take constant values within laboratories, and that often they take the same values also between laboratories, prevents studying their effects other than one at a time. This is an important weakness of the study that should be avoided in future studies.

The $\left\{b_{j}\right\}$ are modeled as independent, Gaussian random variables with mean of 0 and standard deviation $\tau$, which characterizes the between-laboratory dispersion of values; and the $\left\{e_{1, j}, \ldots, e_{m j, j}\right\}$ are modeled as independent, Gaussian random variables with mean of 0 and standard deviation $\sigma_{j}$, which characterizes the dispersion of values within laboratory $j$, and may vary between laboratories. These models were fitted using function lme from the package nlme for the $R$ environment for statistical computing and graphics $[6,7]$. Their fit to the data was evaluated via graphical examination of the corresponding estimates of the laboratory and coupon effects. The heterogeneity of the results from the different laboratories may be evaluated in greater detail by applying Cochran's $Q$-test to determine whether the standard deviation of the laboratory effects $\tau$ is zero [8].

Table 3 summarizes the results that may be relevant to the design of future, more ambitious interlaboratory studies of additive manufacturing. The between-laboratory range of values, expressed relative to the estimate of the measurand, listed in the column labeled $\hat{\tau} / \hat{\mu}(\%)$, is a modest $1.3 \%$ to 4.1 \%. The between-laboratory variability is substantially (up to 4 times) larger than the typical withinlaboratory variability, listed in the column labeled $\hat{\tau} /$ median $\left(\left\{\hat{\sigma}_{j}\right\}\right)$, for all measurands except for elongation, whose values are surprisingly uniform across laboratories.

Considered one at a time, none of the four covariates (energy density, volume rate, layer thickness, and skin power) had effects significantly different from zero, once the differences between laboratories were taken into account. An analysis based on summary data (averages and standard errors of these averages), where the same mixed effects model was fitted using a different statistical procedure [9], implemented in function rma defined in R package meta for Viechtbauer [10] revealed the following:

- For yield strength (YS), ultimate tensile strength (UTS), and Young's modulus (E), there is significant between-lab heterogeneity (that is, the standard deviation $\tau$ of the laboratory effects is significantly greater than 0 ), but not for elongation after fracture (A), as judged by Cochran's $Q$-test.
- Only for yield strength is there a slight indication of possible significance of energy density upon mechanical performance, with higher values of the energy density (coefficient of corresponding effect is positive, 0.66 , with associated standard uncertainty 0.28 ) tending to produce greater yield strength.

Table 3. Selected results from fitting mixed effects models to the experimental data. The values in the last two columns are the same for all the covariates (to within the number of significant digits quoted) because the variability in the covariates was insufficient to impact the variability of the measured values of the mechanical properties.

|  | Estimate | Effect | $\hat{\tau} / \hat{\mu}(\%)$ | $\hat{\tau} /$ median (\{ $\hat{\sigma}\}\})$ |
| :--- | :---: | :---: | :---: | :---: |
| Energy Density | 701 | 0.66 | 2.4 | 3.2 |
| Yield Strength (MPa) | 1044 | 0.25 | 2.0 | 4.9 |
| Ultimate Tensile Strength (MPa) | 36.3 | -0.01 | 1.3 | 0.4 |
| Elongation (\%) | 203 | -0.17 | 3.3 | 1.5 |
| Young's Modulus (GPa) |  |  |  |  |
|  |  |  |  |  |
| Volume Rate | 802 | -13 | 2.1 | 3.2 |
| Yield Strength (MPa) | 1081 | -5 | 1.9 | 4.9 |
| Ultimate Tensile Strength (MPa) | 35.1 | 0.15 | 1.4 | 0.4 |
| Elongation (\%) | 177 | 3.4 | 3.8 | 1.5 |
| Young's Modulus (GPa) |  |  |  |  |
|  |  |  |  |  |
| Layer Thickness | 816 | -1.7 | 2.1 | 3.2 |
| Yield Strength (MPa) | 1086 | -0.64 | 1.9 | 4.9 |
| Ultimate Tensile Strength (MPa) | 35 | 0.02 | 1.4 | 0.4 |
| Elongation (\%) | 174 | 0.44 | 3.9 | 1.5 |
| Young's Modulus (GPa) |  |  |  |  |
|  |  |  |  |  |
| Skin Power | 852 | -0.36 | 2.0 | 3.2 |
| Yield Strength (MPa) | 1100 | -0.14 | 1.9 | 4.9 |
| Ultimate Tensile Strength (MPa) | 34.6 | 0.00 | 1.4 | 0.4 |
| Elongation (\%) | 164 | 0.09 | 4.1 | 1.5 |
| Young's Modulus (GPa) |  |  |  |  |

## Fractography analysis

Fractography analysis of these specimens was also carried out to understand the differences seen in the tensile test results. A series of scanning electron micrographs were taken of the fracture surface from tensile bar 5 from participant 7. The tensile bar in the following images was stress-relief
heat-treated following the same heat treatment followed for the other 6 participants [1]. The build platform was heated to $840^{\circ} \mathrm{C}$ in 6 h and temperature held at $840^{\circ} \mathrm{C}$ for 1 h . For comparison purposes, micrographs from a specimen made on the LPBF machine of the other 6 participants are included at the end of this section (Figure 22 to Figure 27).

The nature of the fracture surface morphology in the following images showed significant differences compared to a specimen made on the LPBF machine of the other 6 participants [1] (Figure 22 to Figure 27). The surface shows several secondary cracks, some quite large, that appear to be the result of the variability in the LPBF process. The small secondary cracks appear to have initiated near an unmelted powder particle (or other microstructural anomaly) and propagated a short distance into the bulk of the sample (i.e., perpendicular to the primary fracture plane) and arrested. These cracks may be the result of translating a manufacturing plan developed for one LPBF machine for use on a different vendor's LPBF machine. The translation of the manufacturing plan may have resulted in the suboptimum build producing lower mechanical properties and the observed fracture surface.

Figure 5 is a low-magnification view of the surface showing a large flaw in the lower left corner of the tensile specimen cross-section. This flaw appears to be a pore caused by trapped gas and is the most likely initiation point of the primary fracture. At higher magnification (Figure 6 and Figure 7), this area shows that the pore may have originated during the solidification process as unmelted and partially melted powder are clearly observable within.

The fracture surface has a number of large secondary cracks aligned in the build direction (Figure 5). During the build, the powder was applied in layers in a horizontal plane. The horizontal secondary cracks may have initiated as interlayer cracks that pulled apart during the tensile loading. However since these cracks appear to be open, it may suggest that they are build related rather than the result of loading. Higher magnification images also show smaller secondary cracks that are in various directions along the surface as well (Figure 8 and Figure 13).


Figure 5. Overview of the fracture surface (x23) showing a large flaw in the lower left corner of the specimen and large secondary cracks parallel to build layers. The white box is the region magnified in Figure 8.


Figure 6. A low magnification view (x100) of the lower
left corner of the specimen showing the flaw (1) and what appears to be a short crack that initiated to the


Figure 7. A higher magnification image (x250)
showing unmelted and partially melted particles (1) of various sizes trapped within the flaw (2). right of a large particle (2).


Figure 8. Higher magnification (x110) of the white box in Figure 5 with secondary cracks (1) and dimple-like microvoids (2). Some cracks are aligned in the build direction while others are not.


Figure 9. Higher magnification (x500) of Figure 8
showing similar features to Figure 13. Fine dendritic
segregation (1), microvoids (2), a small secondary crack (3), and an unmelted powder particle within the crack (4). The white box is the region magnified in

Figure 10.


Figure 10. Higher magnification (x1000) of Figure 9
showing a portion of the small crack (1) (labeled 3 in Figure 9) and a microvoid (2) from Figure 9. The fine scaled dendrites can easily be seen across the surface.


Figure 12. This area of the fracture surface shows areas of very consistent dendrite orientation.

Figure 11. Another high magnification image (x1500) of the fracture surface showing dendrites. In the center of this image there is a cube shaped formation (1) that appears to be a different nature then the surrounding material and could be crystallographic.


Figure 13. A small secondary crack (3) is surrounded by fine dendritic segregation (1) and microvoids (2). An unmelted particle is within the crack (4). While the microvoids reflect the ductility observed in the mechanical data, the crack may have contributed to lower overall ductility in this specimen as compared to the specimen representing the other 6 participants.

Fine-scaled dendrites, resulting from micro-segregation during the solidification process, are exhibited at region 1 in Figure 13 and these are the most prevalent features on the fracture surface
overall. Microvoids, or dimple-like features, are also visible on the surface and they are noted in Figure 13 as region 2. Numerous voids were observed and they ranged in size from extremely fine to quite large. Since many of the observed microvoids are smaller than the diameter of an unmelted powder particle, it is possible these formed around an unmelted powder or contaminate particle during solidification. Microvoids typically form during final fracture (i.e., after necking has initiated in the sample) and indicate ductile failure, which is consistent with the mechanical test data for this specimen. While lower than the results from the other 6 participants, this specimen did demonstrate significant ductility prior to failure.

Figure 13 also shows a small secondary crack (region 3). Several secondary cracks, also ranging in size were observed on the fracture surface of this specimen. Most exhibited small, unmelted powder particles near the mouth of the crack, which can be seen in Figure 13 (region 4). These cracks were most likely produced by local variability in the layered solidification process and may have contributed to the reduced strength. Another example of a secondary crack is shown in Figure 14 through Figure 17.

The powder particles were examined further and Figure 18 and Figure 20 are high magnification images of partially melted powder from Figure 17. Some evidence of decohesion can be seen between the unmelted powder particle and the surrounding matrix (decohesion at region 2 in Figure 18), which is also consistent with the reduced mechanical properties for this specimen. The particle morphology was relatively spherical. Some evidence of grain structure and fine-scale dendrites is also observable at extremely high magnification (Figure 19 and Figure 21).


Figure 14. Figure 5, a low magnification overview (x23) of the fracture surface. The white box is the region magnified in Figure 15. Note the area for Figure 15 with relation to the flaw.


Figure 16. Higher magnification (x200) of Figure 15
showing secondary cracks with unmelted or partially


Figure 15. Higher magnification (x85) of Figure 14 showing secondary cracks, one with unmelted or partially melted powder particles trapped inside. Note the thin horizontal crack passing through the white box extends from the flaw across most of this image.

The white box is the region magnified in Figure 16.


Figure 17. A higher magnification view (x400) of the mouth of a secondary crack showing unmelted or
melted powder trapped in the mouth of the crack.

The thin horizontal crack noted in Figure 15 that extends from the flaw is easier to see. The white box
is the region magnified for Figure 17.


Figure 18. Partially melted powder at a higher magnification (x2500) from Figure 17. The rough texture on the particle surfaces is produced by rapid solidification during the atomization process (1).

There is evidence of decohesion between the unmelted powder particle and the surrounding matrix
partially melted powder particles trapped inside. The white box is the region magnified for Figure 18.


Figure 19. A high magnification image (x15000) of Figure 18 showing the surface of an unmelted powder particle. The brighter regions are likely second phase precipitates (1) decorating extremely fine grain boundaries (2).
(2).


Figure 20. Partially melted powder within the secondary crack at a high magnification (x2500) from Figure 17. The rough texture on the particles surface is produced by rapid solidification during the atomization process.


Figure 21 . The melted region between two partially melted powder particles (x5000) shown in Figure
18. The brighter regions are likely second phase participates decorating extremely fine grain boundaries.

The above images represent the microstructure and associated fracture patterns of a specimen fabricated on a different LPBF machine then the other 6 participants. The nature of the fracture surface morphology in these images showed significant differences compared to a specimen made on the LPBF machine of the other 6 participants [1]. The difference in the facture pattern may be the result of translating a manufacturing plan developed for one LPBF machine for use on a different vendor's LPBF machine. The translation of the manufacturing plan may have resulted in the sub-optimum build results exhibited in the above images and in the lower mechanical properties. Figure 22 through Figure 27 show the fractography results from a specimen made using the LPBF machine of the 6 participants.


Figure 22. A region of fracture zone ( x 100 ) that does not appear to have horizontal secondary cracks related to the build layer but rather localized transgranular cracking in various directions.


Figure 25. A different area of the fracture surface (x250). Large TCL facet is in the middle of the
image and the top of the facet was chosen to magnify in Figure 26.


Figure 26. Dendrites are evident around a secondary crack (x1500).

Figure 27. A high magnification image (x3000) of the fracture surface shows primarily dendrites with a transgranular cleavage-like feature.

## 7. SUMMARY

Conducting a round robin study involving a large number of variables requires significant effort to identify and control most, if not all, of these variables. Additive manufacturing processes are examples of such processes with very large, on the order of hundred, number of variable process parameters. Therefore, careful planning is needed to determine the manufacturing plan and collect all necessary information to be able to draw conclusions from the resulting tests.

This report presented all the information and documentation shared between the study coordinator (NIST) and each participant during execution of this study. This report also provided an example of using some fixed process parameters on different LPBF machines, which are not intended to necessarily use the same parameters. The test results from the specimens fabricated on a different
vendor's LPBF machine showed significant differences both in mechanical properties as well as fracture and microstructure characteristics. These differences are most likely the result of translating a manufacturing plan developed for one LPBF machine for use on a different vendor's machine. The translation of the manufacturing plan may have resulted in the sub-optimum build results. Future studies will take these results into account when setting and applying fixed parameters on different AM platforms.

The results indicate that differences between laboratories, even between those that have used the very same parent material and manufacturing process (the only ones considered in the analyses that produced the results summarized in Table 3), generally are considerably more important than differences between coupons manufactured in the same laboratory. This fact suggests that there is more to be gained by increasing the number of participating laboratories, than by increasing the number of coupons manufactured by each laboratory.

Future experiments will be designed to enable investigation of the effects that process variables (the covariates considered above and others) have upon the mechanical properties of the resulting parts. To achieve this goal, settings of key process variables should be varied deliberately, over practically significant ranges, both within laboratories and between laboratories, in a suitably designed experiment. For example, one may choose at a minimum two different values for the energy density, but then ensure that the two levels are used in different runs in each laboratory.

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## APPENDIX

COPY OF THE 7 PROCESS CONTROL DOCUMENTS RETURNED BY THE PARTICIPANTS

## Participant 1 PCD

## Process Control Document

## Technical Data

Part Manufacturing Technical Data
Completed by the part manufacturer

|  | Value | Requirement Section | Approval |
| :---: | :---: | :---: | :---: |
| Job Number |  |  |  |
| Build File Name: | AM_Round Robin_Inconel 625 | 1.2 |  |
| Process | Laser Powder Bed Fusion | 2.1.1 |  |
| Equipment Manufacturer and Model: | $\begin{gathered} \text { EOS } \\ \text { EOSINT M270D } \end{gathered}$ | 2.1.2 |  |
| Equipment Serial Number: | S1978 |  |  |
| Laser Manufacturer and Model: | H0911286 | 2.1.4 |  |
| Laser Serial Number: | 1212-0163 |  |  |
| Software Version: | PSW Version 3.5 (Build 64) | 2.2 |  |
| Date of last preventative maintenance | 02/04/14 | 2.3 |  |
| System Calibration Current | yes | 2.4 |  |
| Material Requirements |  |  |  |
| Verify Powder Heat/Lot Loaded Matches Feedstock Technical Data | Containers \#2 and \#15 |  |  |
| Material Condition (Virgin/Recycled) | Virgin | 3.4 |  |
| Process Setup Requirements |  |  |  |
| Build Platform Material | $\begin{gathered} \text { New Plate } \\ \text { PN: 2200-4372 } \end{gathered}$ | 4.1.1 |  |





## Exposure Parameters

Completed by the part manufacturer

|  | Value |  |  |  | Requirement | Approval |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Job <br> Number |  |  |  |  |  |  |
| Build File <br> Name: | AM_Round Robin_Inconel 625 |  |  |  |  |  |
| Pre Exposure |  |  |  |  |  |  |
| Pre Exposure Type | NIST_RR_IN625_PreContour |  |  |  | 4.3.5.1 |  |
| First Contour |  | Standard | OnPart | Downskin | 4.3.5.1.1 |  |
|  | $\begin{gathered} \text { Speed } \\ (\mathrm{mm} / \mathrm{s}) \text { : } \end{gathered}$ | 900.0 | 800.0 | 1600.0 |  |  |
|  | Power (W): | 100.0 | 100.0 | 100.0 |  |  |
|  | Beam Offset (mm): | 0.000 | Contour | Yes (checked) |  |  |


|  | Thickness ( mm ): | 0.040 | Post Contour | No <br> (unchecked) |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Corridor (mm): | 0.040 |  |  |  |  |
| Second Contour |  | Standard | OnPart | Downskin | 4.3.5.1.2 |  |
|  | $\begin{gathered} \hline \text { Speed } \\ (\mathrm{mm} / \mathrm{s}): \end{gathered}$ | - |  | - |  |  |
|  | Power (W): | - | - | - |  |  |
|  | Beam Offset (mm): | - | Contour | No <br> (unchecked) |  |  |
|  | Thickness (mm): | - | Post Contour | $\begin{gathered} \text { No } \\ \text { (unchecked) } \end{gathered}$ |  |  |
|  | Corridor ( mm ): | - |  |  |  |  |
| Edges | Edge factor | - | Edges | No(unchecked) | 4.3.5.1.3 |  |
|  | Threshold: | - | Post Edge | No(unchecked) |  |  |
|  | Minimum radius factor: | - |  |  |  |  |
|  | Beam offset (mm): | - |  |  |  |  |
|  | $\begin{gathered} \text { Speed } \\ (\mathrm{mm} / \mathrm{s}) \text { : } \end{gathered}$ | - |  |  |  |  |
|  | Power (W): | - |  |  |  |  |
| Skin Exposure |  |  |  |  |  |  |
| Skin <br> Exposure Type | NIST_RR_IN625_OuterSkin |  |  |  | $4.3 .5 .2$ |  |
| Stripes | Distance (mm): | 0.10 | Stripe width (mm): | 4.00 | 4.3.5.2.1 |  |
|  | $\begin{gathered} \text { Speed } \\ (\mathrm{mm} / \mathrm{s}) \text { : } \end{gathered}$ | 800.0 | Stripes overlap (mm): | 0.10 |  |  |
|  | Power (W): | 195.0 | Skywriting: | Yes(checked) |  |  |
|  | $\begin{gathered} \text { Beam } \\ \text { offset (mm) } \end{gathered}$ | 0.030 | Offset: | Yes(checked) |  |  |
|  | Hatching, $X$ | Yes(checked) | Alternating: | Yes(checked) |  |  |
|  | Hatching, Y | Yes(checked) | Rotating: | Yes(checked) |  |  |
| UpDown |  | Upskin | Downskin |  | 4.3.5.2.2 |  |
|  | Distance (mm): | 0.05 | 0.05 |  |  |  |
|  | $\begin{aligned} & \text { Speed } \\ & (\mathrm{mm}) \text { : } \end{aligned}$ | 800.0 | 3000.0 |  |  |  |


|  | Power (W): | 195.0 | 195.0 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Thickness ( mm ): | 0.00 | 0.04 |  |  |  |
|  | X: | Yes(checked) | Yes(checked) |  |  |  |
|  | Y: | Yes(checked) | Yes(checked) |  |  |  |
|  | Alternating: | No <br> (unchecked) | Overlap with inskin(mm): | 0.10 |  |  |
|  | Skywriting: | $\begin{gathered} \text { Yes } \\ \text { (checked) } \end{gathered}$ | $\begin{aligned} & \hline \text { Min. length } \\ & (\mathrm{mm}) \end{aligned}$ | 2.00 |  |  |
| Skip Layer | Skipped Layers | 0 |  |  | 4.3.5.2.3 |  |
|  | Offset layers: | 0 |  |  |  |  |
|  | Expose first layer: | Yes (checked) |  |  |  |  |
| Core Exposure |  |  |  |  |  |  |
| Core <br> Exposure <br> Type | NIST_RR_IN625_InnerSkin |  |  |  | 4.3.5.3 |  |
| Chess |  | Squares | Gap |  |  |  |
|  | Distance (mm): | 0.10 | 0.10 |  |  |  |
|  | $\begin{gathered} \text { Speed } \\ (\mathrm{mm} / \mathrm{s}): \end{gathered}$ | 800.0 | 800.0 |  |  |  |
|  | Power (W): | 195.0 | 195.0 |  |  |  |
|  | Width (mm): | 8.00 | 0.00 |  |  |  |
|  | Beam offset (mm) | -0.050 | Overlap: | 0.08 |  |  |
|  | Hatching, X: | Yes (checked) | Alternating: | Yes (checked) |  |  |
|  | Hatching, Y: | Yes (checked) | Rotating: | Yes (checked) |  |  |
|  | Skywriting: | No (unchecked) | Rotated Angle: | - |  |  |
|  | Offset: | Yes(checked) |  |  |  |  |
| Post Exposure |  |  |  |  |  |  |
| Post <br> Exposure <br> Type | NIST_RR_IN625_Postcontour |  |  |  | 4.3.5.4 |  |
| First Contour |  | Standard | OnPart | Downskin | 4.3.5.4.1 |  |
|  | $\begin{gathered} \hline \text { Speed } \\ (\mathrm{mm} / \mathrm{s}) \text { : } \end{gathered}$ | 900.0 | 800.0 | 1600.0 |  |  |
|  | Power (W): | 120.0 | 120.0 | 120.0 |  |  |


|  | Beam Offset (mm): | 0.015 | Contour | Yes (checked) |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Thickness (mm): | 0.040 | Post Contour | Yes (checked) |  |
|  | Corridor (mm): | 0.040 |  |  |  |
| Second Contour |  | Standard | OnPart | Downskin | 4.3.5.4.2 |
|  | $\begin{gathered} \text { Speed } \\ (\mathrm{mm} / \mathrm{s}) \text { : } \end{gathered}$ | - | - | - |  |
|  | Power (W): | - | - | - |  |
|  | Beam Offset (mm): | - | Contour | No (unchecked) |  |
|  | Thickness (mm): | - | Post Contour | No (unchecked) |  |
|  | Corridor (mm): | - |  |  |  |
| Edges | Edge factor | 2.00 | Edges | Yes(checked) | 4.3.5.4.3 |
|  | Threshold: | 3.0 | Post Edge | Yes(checked) |  |
|  | Minimum radius factor: | 0.00 |  |  |  |
|  | Beam offset (mm): | 0.000 |  |  |  |
|  | $\begin{gathered} \text { Speed } \\ (\mathrm{mm} / \mathrm{s}) \text { : } \end{gathered}$ | 900.0 |  |  |  |
|  | Power (W): | 100.0 |  |  |  |

## Participant 2 PCD

## Process Control Document

## Technical Data

Part Manufacturing Technical Data
Completed by the part manufacturer

|  | value | Requirement Section | Approval |
| :---: | :---: | :---: | :---: |
| Job Number |  |  |  |
| Build file Name： | Nist Plate | 1.2 | 33 |
| Process | DmLs | ${ }^{2.1 .1}$ |  |
| Equipment Manufacturer and | EOS m280 | 2．1．2 | 砥 |
| Equipment Serial <br> Number | 511469 |  | B3 |
| Laser Manufacturer and Model | IPG $\quad 4 / R-400-5 M$ | ${ }^{2.1 .4}$ | B弓 |
| Laser Serial Number： | can not find |  | $B B$ |
| Sotware Version： | 3.6 Buid 32 | 0 |  |
| Date of last preventative | 6／24／2014 | ${ }^{2.3}$ | 万B |
| $\begin{aligned} & \text { System Calibration } \\ & \text { Current } \\ & \hline \end{aligned}$ | Yes－checked／$/ 24 / 2014$ | ${ }^{2.4}$ | B3 |
| Material |  |  |  |
| Verify Powde Heat／Lot Loade Matches Feedsto | Cans $3+11$ <br> lot M1112012 |  | SB |
| Material Condition （Virgin／Recycled） | Virgin | ${ }^{3.4}$ | BS |
| Process Setup Requirements |  |  |  |
| Build Platform <br> Materia | Steel－Provided | 4.1 .1 | $B B$ |
| Build Platform Thicknes | No provided | 4．1．2 | $B B$ |
| Build Platform <br> Condition | Machined－cheneed oy IPA | 4.1 .3 | $B B$ |
| Build Platform | 80 | 4．1．4 | $\cdots B$ |
| Recoater lide | Ceramic | 0 | B3 |


| Material/Part Number | IN 625 |  |  | $D B$ |
| :---: | :---: | :---: | :---: | :---: |
| Process Parameter Settings |  |  |  |  |
| Base Parameter Set | MPI -040-101 Performance |  | 4.3.1 | 813 |
| Base Parameter Filename | same $T$ |  |  | Bア |
| Layer Thickness, $\mu \mathrm{m}$ | 40 |  | 4.3.2 | 85 |
| Sort Parts Method: |  |  | 4.3.4.2 |  |
| Exposure Parameters | Complete Exposure Parameters Table Below |  | 4.3.5 |  |
| Pre Contour Type | No exposule |  | 4.3.5.1 |  |
| Skin Exposure Type | - Defanlt-Owtersein - Direct Part |  | 4.3.5.2 |  |
| Core Exposure Type | No exposure |  | 4.3.5.3 |  |
| Post Contour Type | - Defant - Pogt conton-s |  | 4.3.5.4 |  |
| Skin Thickness ( $\mathrm{x} / \mathrm{y}$ ), mm | 200.00 | mm | 4.3.5.5 |  |
| Skin Thickness (z), mm | 200.00 | mm | 4.3.5.6 |  |
| Base Radius: | 0.00 cmm |  | 4.3.5.7 |  |
| Core open to platform?: | NO |  | 4.3.5.8 |  |
| Skin/Core: | Yes |  | 4.3.5.9 |  |
| Scaling and Offset | (3) $0.000 \%$ for both K, Y |  |  |  |
| Material Specific Scaling | $0.122 \% x^{x, \%} 0.153 \% y$ |  |  | Y, \% |
| Part Specific Undersize/Oversize Beam Offset, mm | $\begin{aligned} & 4.3 .6 .3 \\ & 0.800 \end{aligned}$ | $\mathrm{mm}$ | 4.3.6.1 |  |
|  |  |  | 4.3.6.2 |  |
| Building Screen |  |  |  |  |
| Start Height (mm): | 0.020 |  | 4.3.7.1 |  |
| Final Height (mm) : | 9.200 |  | 4.3.7.2 |  |
| Layer Thickness | 0.040 nm ( 40 mm ) |  | 4.3.2 |  |
| DMLS Settings |  |  |  |  |
| DMLS | Off $\checkmark$ |  | 0.00 | Range, <br> (mm) |
| Pre-exposure |  |  | 0.04 | $\begin{aligned} & \text { Range, } \\ & (\mathrm{mm}) \end{aligned}$ |
|  |  |  | 4.3.8.1 |  |
|  |  |  | 4.3.8.2 |  |
| Recoating Screen |  |  |  |  |
| Minimum Charge, \% | $150 \%$ |  | BR |  |
| Maximum Charge, \% | 200 \% |  | तै |  |
| Dosing Boost, \% | $300 \%$ |  | $B \beta$ |  |
| Recoating Speeds $(\mathrm{mm} / \mathrm{s})$ | Recoating Speed 1 |  | Recoating Speed 2 | $\begin{aligned} & \hline \text { 4.3.9.4, } \\ & \text { 4.3.9.5 } \end{aligned}$ |
| Bosing beort | $500 \mathrm{~mm} / \mathrm{s}$ |  | $150 \mathrm{~mm} / \mathrm{s}$ |  |




Exposure Parameters
Completed by the part manufacturer

|  | Value |  |  |  | Requirement | Approval |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Job Number |  |  |  |  |  |  |
| Build File Name: | Nist Plates |  |  |  |  |  |
| Pre Exposure |  |  |  |  |  |  |
| Pre Exposure Type | No Exposure |  |  |  | 4.3.5.1 |  |
| First Contour |  | Standard | OnPart | Downskin | 4.3.5.1.1 |  |
|  | Speed ( $\mathrm{mm} / \mathrm{s}$ ): |  |  |  |  |  |
|  | Power (W): |  |  |  |  |  |
|  | Beam Offset (mm): |  | Contour |  |  |  |
|  | Thickness (mm): |  | Post Contour |  |  |  |
|  | Corridor (mm): |  |  |  |  |  |
| Second Contour |  | Standard | OnPart | Downskin | 4.3.5.1.2 |  |
|  | $\begin{gathered} \text { Speed } \\ (\mathrm{mm} / \mathrm{s}): \\ \hline \end{gathered}$ |  |  |  |  |  |
|  | Power (W): |  |  |  |  |  |
|  | Beam Offset (mm): |  | Contour |  |  |  |





Results from Firetaning job:

$$
\begin{aligned}
& x \text { scaling: } 6.122 \% \\
& y \text { scaling: } 0.153 \%
\end{aligned}
$$

New Beam offset: 0.027

## Participant 3 PCD:

## Process Control Document

Technical Data
Part Manufacturing Technical Data
Completed by the part manufacturer

|  | Value | Requirement Section | Approval |
| :---: | :---: | :---: | :---: |
| Job Number |  |  |  |
| Build File Name: | NIST-1.625 | 1.2 |  |
| Process |  | 2.1.1 |  |
| Equipment <br> Manufacturer and <br> Model: | EOSINT M 270 | 2.1.2 |  |
| Equipment Serial Number: |  |  |  |
| Laser Manufacturer and Model: | IPG Y/R-200-5M | 2.1.4 |  |
| Laser Serial Number: | 11102522 |  |  |
| Software Version: | PSW 3.4 | 0 |  |
| Date of last preventative maintenance | 6-5-14 | 2.3 |  |
| System Calibration Current |  | 2.4 |  |
| Material Requirements |  |  |  |
| Verify Powder Heat/Lot Loaded Matches Feedstock Technical Data | $\ln 625$ Contanes $7+13$ M1112012 |  |  |
| Material Condition (Virgin/Recycled) | Virgin | 3.4 |  |
| Process Setup Requirements |  |  |  |
| Build Platform Material | NIST prouided Cosplate Charge-Nr:26 2200-4372 | 4.1.1 |  |
| Build Platform Thickness | 22.13 mm | 4.1.2 |  |
| Build Platform Condition | New | 4.1.3 |  |
| Build Platform Preheat, ${ }^{\circ} \mathrm{C}$ | 80 | 4.1.4 |  |
| Recoater Blade |  | 0 |  |




| Chamber Oxygen Prior <br> to Opening | $0.03 \%$ |  | 6.1 .2 |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Recovered Powder <br> Labeling |  |  |  |  |  |
| Post Build Laser <br> Power Measurement | Setpoint |  |  | 6.2 |  |
| Pre Contour |  |  |  | Display | Measure <br> d |
| Stripes |  |  |  |  |  |
| Up Skin |  |  |  | 6.1 .5 |  |
| Down Skin |  |  |  |  |  |
| Post Contour |  |  |  |  |  |
| Edges |  |  |  |  |  |
|  |  |  |  |  |  |
|  |  |  |  |  |  |

Exposure Parameters
Completed by the part manufacturer

|  | Value |  |  |  | Requirement Section | Approval |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Job Number |  |  |  |  |  |  |
| Build File Name: |  |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Pre Exposure |  |  |  |  |  |  |
| Pre Exposure Type |  |  |  |  | 4.3.5.1 |  |
| First Contour |  | Standard | OnPart | Downskin | 4.3.5.1.1 |  |
|  | Speed <br> ( $\mathrm{mm} / \mathrm{s}$ ): | 900 | 800 | 1600 |  |  |
|  | Power (W): | 100 | 100 | 100 |  |  |
|  | Beam Offset (mm): | $\bigcirc$ | Contour | yes |  |  |
|  | Thickness (mm): | 0.040 | Post Contour | 10 |  |  |
|  | Corridor (mm): | 0,0\% |  |  |  |  |
| Second Contour |  | Standard | OnPart | Downskin | 4.3.5.1.2 |  |
|  | Speed ( $\mathrm{mm} / \mathrm{s}$ ): | - | - | - |  |  |
|  | Power (W): | - | - | - |  |  |
|  | Beam Offset (mm): | - | Contour | off |  |  |


|  | Thickness (mm): | - | Post <br> Contour | off | 4.3.5.1.3 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Corridor (mm): | - |  |  |  |  |
| Edges | Edge factor | - | Edges | No |  |  |
|  | Threshold: | - | Post Edge | $N_{3}$ |  |  |
|  | Minimum radius factor: | - |  |  |  |  |
|  | Beam offset (mm): | - |  |  |  |  |
|  | $\begin{aligned} & \text { Speed } \\ & (\mathrm{mm} / \mathrm{s}): \end{aligned}$ | - |  |  |  |  |
|  | Power (W): | - |  |  |  |  |
|  | Skin Exposure |  |  |  |  |  |
| Skin Exposure Type |  |  |  |  | 4.3.5.2 |  |
| Stripes | Distance (mm): | 0.1 | Stripe width (mm): | 4.0 | 4.3.5.2.1 |  |
|  | Speed ( $\mathrm{mm} / \mathrm{s}$ ): | 800 | Stripes overlap $(\mathrm{mm}):$ | $0.1$ |  |  |
|  | Power (W): | 195 | Skywriting: | yes |  |  |
|  | Beam offset (mm) | 0,03 | Offset: | yes |  |  |
|  | Hatching, $X$ | yes | Alternating: | yes |  |  |
|  | Hatching, $Y$ | yes | Rotating: | yes |  |  |
| UpDown |  | Upskin | Downskin |  | 4.3.5.2.2 |  |
|  | Distance (mm): | 0.05 | 0.05 |  |  |  |
|  | Speed <br> (mm): | 800 | 3000 |  |  |  |
|  | Power (W): | 195 | 195 |  |  |  |
|  | Thickness (mm): | 0 | 0.04 |  |  |  |
|  | X : | Yes | yes |  |  |  |
|  | $Y$ : | yes | yes |  |  |  |
|  | Alternating: | ペ | ```Overlap with inskin(mm):``` | 0.1 |  |  |
|  | Skywriting: | Yes | Min. length (mm) | 2.0 |  |  |
| Skip Layer | Skipped | $\bigcirc$ |  |  | 4.3.5.2.3 |  |


|  | Layers |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Offset layers: | $\bigcirc$ |  |  |  |  |
|  | Expose first layer: | yes |  |  |  |  |
| Core Exposure |  |  |  |  |  |  |
| Core Exposure Type |  |  |  |  | 4.3.5.3 |  |
| Chess |  | Squares | Gap |  |  |  |
|  | Distance (mm): | 0.1 | 0,1 |  |  |  |
|  | Speed ( $\mathrm{mm} / \mathrm{s}$ ): | 800 | 800 |  |  |  |
|  | Power (W): | 195 | 195 |  |  |  |
|  | Width (mm): | 8.0 | 0 |  |  |  |
|  | $\begin{gathered} \text { Beam } \\ \text { offset (mm) } \end{gathered}$ | -0.05 | Overlap: | 0,08 |  |  |
|  | Hatching, X : | yes | Alternating: | yes |  |  |
|  | Hatching, $\qquad$ Y: | yes | Rotating: | yes |  |  |
|  | Skywriting: | no | Rotated Angle: | - |  |  |
|  | Offset: | yes |  |  |  |  |
| Post Exposure |  |  |  |  |  |  |
| Post Exposure Type |  |  |  |  | 4.3.5.4 |  |
| First Contour |  | Standard | OnPart | Downskin | 4.3.5.4.1 |  |
|  | Speed ( $\mathrm{mm} / \mathrm{s}$ ): | 900 | 800 | 1600 |  |  |
|  | Power (W): | 120 | 120 | 120 |  |  |
|  | Beam Offset (mm): | 0.015 | Contour | Yes |  |  |
|  | Thickness ( mm ): | 0,040 | Post Contour | yes |  |  |
|  | Corridor (mm): | 0.040 |  |  |  |  |
| Second Contour |  | Standard | OnPart | Downskin | 4.3.5.4.2 |  |
|  | $\begin{gathered} \text { Speed } \\ (\mathrm{mm} / \mathrm{s}): \end{gathered}$ | - | - | - |  |  |
|  | Power (W): | - | - | - |  |  |
|  | Beam Offset (mm): | - | Contour | no |  |  |



Participant 4 PCD:

## Process Control Document

## Technical Data

Part Manufacturing Technical Data
Completed by the part manufacturer

|  | Value | Requirement Section | Approval |
| :---: | :---: | :---: | :---: |
| Job Number | 8-11-2014 |  |  |
| Build File Name: | IN625NISTROUNDROBIN.eosjob | 1.2 |  |
| Process | DMLS | 2.1.1 |  |
| Equipment Manufacturer and Model: | EOSINT M270 | 2.1.2 |  |
| Equipment Serial Number: | SI 987 |  |  |
| Laser Manufacturer and Model: |  | 2.1.4 |  |
| Laser Serial Number: |  |  |  |
| Software Version: | PSW 3.6 | 2.2 |  |
| Date of last preventative maintenance | May 28 | 2.3 |  |
| System Calibration Current | May 28 | 2.4 |  |
| Material Requirements |  |  |  |
| Verify Powder Heat/Lot Loaded Matches Feedstock Technical Data | Use SEM with EDS to verify the powder met specification |  |  |
| Material Condition (Virgin/Recycled) | Virgin | 3.4 |  |
| Process Setup Requirements |  |  |  |
| Build Platform Material | 1045 steel | 4.1.1 |  |
| Build Platform Thickness | $\sim 20 \mathrm{~mm}$ | 4.1.2 |  |
| Build Platform Condition | Good | 4.1.3 |  |




| Platform Temperature at Time of Chamber Opening |  | 6.1.1,6.1.2 |  |
| :---: | :---: | :---: | :---: |
| Chamber Oxygen Prior to Opening | The chamber was opened several hours after build was completed | 6.1.2 |  |
| Recovered Powder Labeling |  | 6.2 |  |
| Post Build Laser <br> Power Measurement | Setpoint | Display | $\begin{gathered} \hline \text { Measure } \\ \mathrm{d} \\ \hline \end{gathered}$ |
| Pre Contour |  |  |  |
| Stripes |  | 6.1.5 |  |
| Up Skin |  |  |  |
| Down Skin |  |  |  |
| Post Contour |  |  |  |
| Edges |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |

## Exposure Parameters

Completed by the part manufacturer

| Value |  |  |  |  | Requirement <br> Section | Approval |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Job Number | Standard |  |  |  |  |  |
| Build File Name: | OnPart |  |  |  | Downskin | 4.3 .5 .1 .1 |





## Participant 5 PCD

## Process Control Document

## Technical Data

Part Manufacturing Technical Data
Completed by the part manufacturer:

|  | Value | Requirement Section | Approval |
| :---: | :---: | :---: | :---: |
| Job Number |  |  |  |
| Build File Name: | AM_Round Robin_Inconel 625 | 1.2 | GJ |
| Process | Laser Powder Bed Fusion | 2.1.1 | GJ |
| Equipment <br> Manufacturer and Model: | EOS M270, year of production: 2010 | 2.1.2 | GJ |
| Equipment Serial Number: | 992 |  | GJ |
| Laser Manufacturer and Model: | IPG, YLR-200-SM-EOS | 2.1.4 | GJ |
| Laser Serial Number: | 10061428 |  | GJ |
| Software Version: | PSW, Version 3.5 (Build 71) | 2.2 | GJ |
| Date of last preventative maintenance | June $2^{\text {nd }}$ unit June $6^{\text {th }} 2014$ performed by Mr. Jay Thornburg | 2.3 | GJ |
| System Calibration Current | August 22 ${ }^{\text {nd }} 2014$ | 2.4 | GJ |
| Material Requirements |  |  |  |
| Verify Powder <br> Heat/Lot Loaded <br> Matches Feedstock <br> Technical Data | ```EOS_IN625 Lot. No.: 1112012 Buckets: #4 and #12``` |  | GJ |
| Material Condition (Virgin/Recycled) | virgin | 3.4 | GJ |
| Process Setup Requirements |  |  |  |
| Build Platform Material | AlSi 1045 steel, charge no.: 2200-4372 | 4.1.1 | GJ |
| Build Platform <br> Thickness | 22.4 mm | 4.1.2 | GJ |
| Build Platform Condition | Virgin, unused | 4.1.3 | GJ |
| Build Platform Preheat, ${ }^{\circ} \mathrm{C}$ | 80 | 4.1.4 | GJ |




| Recovered Powder <br> Labeling | Yes |  | 6.2 | GJ |
| :--- | :---: | :---: | :---: | :---: |
| Post Build Laser <br> Power Measurement | Setpoint <br> (After the was finished and the lens untouched) |  |  | Display |
| Pre Contour | 100 | 20 sec. |  | Measured <br> Sep. $18^{\text {th }}$ |
| Stripes | 195 | 20 sec. |  | 6.1 .5 |
| Up Skin | 195 | 20 sec. |  | 190.8 W |
| Down Skin | 195 | 20 sec. |  |  |
| Post Contour | 120 | 20 sec. |  |  |
| Edges | 100 | 20 sec. |  |  |
|  |  |  |  |  |
|  |  |  |  | 195.8 W |
|  |  |  |  |  |

## Exposure Parameters

Completed by the part manufacturer:
September $16^{\text {th }} 2014$

|  | Value |  |  |  | Requirement | Approval |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Job Number | --- |  |  |  |  |  |
| Build File Name: | AM_Round Robin_Inconel 625.eosjob |  |  |  |  |  |
| Pre Exposure |  |  |  |  |  |  |
| Pre Exposure Type | NIST_PreContour_RR_IN625 |  |  |  | 4.3.5.1 |  |
| First Contour |  | Standard | OnPart | Downskin | 4.3.5.1.1 |  |
|  | $\begin{gathered} \hline \text { Speed } \\ (\mathrm{mm} / \mathrm{s}) \text { : } \end{gathered}$ | 900.0 | 800.0 | 1600.0 |  |  |
|  | Power (W): | 100.0 | 100.0 | 100.0 |  |  |
|  | Beam Offset (mm): | 0.000 | Contour | Yes |  |  |
|  | Thickness (mm): | 0.040 | Post Contour | No |  |  |
|  | Corridor (mm): | 0.040 |  |  |  |  |
| Second Contour |  | Standard | OnPart | Downskin | 4.3.5.1.2 |  |
|  | $\begin{gathered} \hline \text { Speed } \\ (\mathrm{mm} / \mathrm{s}) \text { : } \end{gathered}$ | 50 | 50 | 50 |  |  |
|  | Power (W): | 0 | 0 | 0 |  |  |
|  | Beam Offset (mm): | 0.000 | Contour | No |  |  |
|  | Thickness (mm): | 0.040 | Post Contour | No |  |  |


|  | Corridor ( mm ): | 0.040 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Edges | Edge factor | 2.0 | Edges | No | 4.3.5.1.3 |  |
|  | Threshold: | 3.0 | Post Edge | No |  |  |
|  | Minimum radius factor: | 0.000 |  |  |  |  |
|  | Beam offset (mm): | 0.000 |  |  |  |  |
|  | $\begin{gathered} \text { Speed } \\ (\mathrm{mm} / \mathrm{s}): \end{gathered}$ | 50 |  |  |  |  |
|  | Power (W): | 0 |  |  |  |  |
|  |  |  |  |  |  |  |
| Skin Exposure Type |  | NIST_Out | Skin_RR_IN62 |  | 4.3.5.2 |  |
| Stripes | Distance (mm): | 0.10 | Stripe width (mm): | 4.00 |  |  |
|  | Speed ( $\mathrm{mm} / \mathrm{s}$ ): | 800.0 | Stripes overlap (mm): | 0.10 |  |  |
|  | Power (W): | 195 | Skywriting: | Yes | 4.3.5.2.1 |  |
|  | $\begin{gathered} \text { Beam } \\ \text { offset (mm) } \\ \hline \end{gathered}$ | 0.030 | Offset: | Yes |  |  |
|  | Hatching, X | Yes | Alternating: | Yes |  |  |
|  | Hatching, Y | Yes | Rotating: | Yes |  |  |
|  |  |  | Rot. Angle: | $67^{\circ}$ |  |  |
| UpDown |  | Upskin | Downskin |  |  |  |
|  | Distance (mm): | 0.05 | 0.05 |  |  |  |
|  | $\begin{aligned} & \text { Speed } \\ & (\mathrm{mm}) \text { : } \end{aligned}$ | 800.0 | 3000.0 |  |  |  |
|  | Power (W): | 195.0 | 195.0 |  |  |  |
|  | Thickness (mm): | 0.00 | 0.04 |  | 4.3.5.2.2 |  |
|  | X : | Yes | Yes |  |  |  |
|  | $Y$ : | Yes | Yes |  |  |  |
|  | Alternating: | No | Overlap with inskin(mm): | 0.10 |  |  |
|  | Skywriting: | Yes | $\begin{aligned} & \text { Min. length } \\ & (\mathrm{mm}) \end{aligned}$ | 2.00 |  |  |
| Skip Layer | Skipped Layers | 0 |  |  | 4.3.5.2.3 |  |


|  | Offset <br> layers: | 0 |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Expose first <br> layer: | Yes |  |  |  |  |


| Core Exposure Type | NIST_InnterSkin_RR_IN625 |  |  |  | 4.3.5.3 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Chess |  | Squares | Gap |  | 4.3.5.3.1 |  |
|  | Distance (mm): | 0.10 | 0.10 |  |  |  |
|  | $\begin{gathered} \text { Speed } \\ (\mathrm{mm} / \mathrm{s}): \end{gathered}$ | 800.0 | 800.0 |  |  |  |
|  | Power (W): | 195.0 | 195.0 |  |  |  |
|  | $\begin{aligned} & \text { Width } \\ & (\mathrm{mm}) \text { : } \end{aligned}$ | 8.00 | 0.00 |  |  |  |
|  | Beam offset (mm) | -0.050 | Overlap: | 0.08 |  |  |
|  | Hatching, X: | Yes | Alternating: | Yes |  |  |
|  | Hatching, Y: | Yes | Rotating: | Yes |  |  |
|  | Skywriting: | No | Rotated Angle: | $67^{\circ}$ |  |  |
|  | Offset: | Yes |  |  |  |  |
| Skip Layer | Skipped Layers | 1 |  |  |  |  |
|  | Offset layers: | 0 |  |  | 4.3.5.3.2 |  |
|  | Expose first layer: | Yes |  |  |  |  |


| Post Exposure <br> Type | NIST_PreContour_RR_IN625 |  |  |  | 4.3 .5 .4 |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| First Contour |  | Standard | OnPart | Downskin |  |  |
|  | Speed <br> $(\mathrm{mm} / \mathrm{s}):$ | 900.0 | 800.0 | 1600.0 |  |  |
|  | Power (W): | 120.0 | 120.0 | 120.0 |  | 4.3 .5 .4 .1 |



## Participant 6 PCD:

## Process Control Document

## Technical Data

Part Manufacturing Technical Data
Completed by the part manufacturer

|  | Value | Requirement Section | Approval |
| :---: | :---: | :---: | :---: |
| Job Number |  |  |  |
| Build File Name: | NIST_RoundRobbin_IN625 | 1.2 |  |
| Process |  | 2.1.1 |  |
| Equipment Manufacturer and Model: | EOS INT M270D | 2.1.2 |  |
| Equipment Serial Number: | 1088 |  |  |
| Laser Manufacturer and Model: | IPG Laser YLR-200-SM | 2.1.4 |  |
| Laser Serial Number: |  |  |  |
| Software Version: | PSW 3.5 (71) | 2.2 |  |
| Date of last preventative maintenance | September 2014 | 2.3 |  |
| System Calibration Current | yes | 2.4 |  |
| Material Requirements |  |  |  |
| Verify Powder Heat/Lot Loaded Matches Feedstock Technical Data | EOS Nickel Alloy IN 625 LOT M111201-2 Bucket \#1 and \#10 |  |  |
| Material Condition (Virgin/Recycled) | Virgin | 3.4 |  |
| Process Setup Requirements |  |  |  |
| Build Platform Material | NIST provided | 4.1.1 |  |
| Build Platform Thickness |  | 4.1.2 |  |
| Build Platform Condition |  | 4.1.3 |  |





## Exposure Parameters

Completed by the part manufacturer

|  | Value |  |  |  | Requirement | Approval |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Job Number |  |  |  |  |  |  |
| Build File Name: |  |  |  |  |  |  |
| Pre Exposure |  |  |  |  |  |  |
| Pre Exposure Type |  |  |  |  | 4.3.5.1 |  |
| First Contour |  | Standard | OnPart | Downskin | 4.3.5.1.1 |  |
|  | Speed $(\mathrm{mm} / \mathrm{s})$ $(\mathrm{mm} / \mathrm{s}):$ |  |  |  |  |  |
|  | Power (W): |  |  |  |  |  |
|  | Beam Offset (mm): |  | Contour |  |  |  |
|  | Thickness (mm): |  | Post Contour |  |  |  |
|  | Corridor (mm): |  |  |  |  |  |
| Second Contour |  | Standard | OnPart | Downskin | 4.3.5.1.2 |  |
|  | $\begin{gathered} \text { Speed } \\ (\mathrm{mm} / \mathrm{s}) \text { : } \end{gathered}$ |  |  |  |  |  |


|  | Power (W): |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Beam Offset (mm): |  | Contour |  |  |  |
|  | Thickness ( mm ): |  | Post Contour |  |  |  |
|  | Corridor (mm): |  |  |  |  |  |
| Edges | Edge factor |  | Edges |  | 4.3.5.1.3 |  |
|  | Threshold: |  | Post Edge |  |  |  |
|  | Minimum radius factor: |  |  |  |  |  |
|  | Beam offset (mm): |  |  |  |  |  |
|  | $\begin{gathered} \text { Speed } \\ (\mathrm{mm} / \mathrm{s}) \text { : } \end{gathered}$ |  |  |  |  |  |
|  | Power (W): |  |  |  |  |  |
| Skin Exposure |  |  |  |  |  |  |
| Skin Exposure Type |  |  |  |  | 4.3.5.2 |  |
| Type <br> Stripes | Distance (mm): |  | Stripe width (mm): |  | 4.3.5.2.1 |  |
|  | Speed ( $\mathrm{mm} / \mathrm{s}$ ): |  | Stripes overlap (mm): |  |  |  |
|  | Power (W): |  | Skywriting: |  |  |  |
|  | Beam offset (mm) |  | Offset: |  |  |  |
|  | Hatching, X |  | Alternating: |  |  |  |
|  | Hatching, Y |  | Rotating: |  |  |  |
| UpDown |  | Upskin | Downskin |  | 4.3.5.2.2 |  |
|  | Distance (mm): |  |  |  |  |  |
|  | $\begin{aligned} & \text { Speed } \\ & (\mathrm{mm}) \text { : } \end{aligned}$ |  |  |  |  |  |
|  | Power (W): |  |  |  |  |  |
|  | ```Thickness (mm):``` |  |  |  |  |  |
|  | X : |  |  |  |  |  |
|  | $Y$ : |  |  |  |  |  |




Participant 7 PCD

## Process Control Document

## Technical Data

Part Manufacturing Technical Data
Completed by the part manufacturer

|  | Value | Requirement Section | Approval |
| :---: | :---: | :---: | :---: |
| Job Number |  |  |  |
| Build File Name: |  | 1.2 |  |
| Process |  | 2.1.1 |  |
| Equipment Manufacturer and Model: |  | 2.1.2 |  |
| Equipment Serial Number: |  |  |  |
| Laser Manufacturer and Model: |  | 2.1.4 |  |
| Laser Serial Number: |  |  |  |
| Software Version: |  | 2.2 |  |
| Date of last preventative maintenance |  | 2.3 |  |
| System Calibration Current |  | 2.4 |  |
| Material Requirements |  |  |  |
| Verify Powder Heat/Lot Loaded Matches Feedstock Technical Data |  |  |  |
| Material Condition (Virgin/Recycled) |  | 3.4 |  |
| Process Setup Requirements |  |  |  |
| Build Platform Material |  | 4.1.1 |  |
| Build Platform <br> Thickness |  | 4.1.2 |  |
| Build Platform Condition |  | 4.1.3 |  |




| Platform Temperature at Time of Chamber Opening |  | 6.1.1,6.1.2 |  |
| :---: | :---: | :---: | :---: |
| Chamber Oxygen Prior to Opening |  | 6.1.2 |  |
| Recovered Powder Labeling |  | 6.2 |  |
| Post Build Laser <br> Power Measurement | Setpoint | Display | Measure <br> d |
| Pre Contour |  |  |  |
| Stripes |  | 6.1.5 |  |
| Up Skin |  |  |  |
| Down Skin |  |  |  |
| Post Contour |  |  |  |
| Edges |  |  |  |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |

## Exposure Parameters

Completed by the part manufacturer

|  | Value |  |  |  | Requirement Section | Approval |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Job Number |  |  |  |  |  |  |
| Build File Name: | 20140916.SLM |  |  |  |  |  |
| Pre Exposure |  |  |  |  |  |  |
| Pre Exposure Type |  |  |  |  | 4.3.5.1 |  |
| First Contour (Volume Border) |  | Standard | OnPart | Downskin | 4.3.5.1.1 |  |
|  | Speed $(\mathrm{mm} / \mathrm{s})$ : | 400 |  |  |  |  |
|  | Power (W): | 125 |  |  |  |  |
|  | Beam Offset (mm): | 3.0 | Contour |  |  |  |
|  | Thickness (mm): | . 05 | Post Contour |  |  |  |
|  | Corridor (mm): |  |  |  |  |  |
| Second Contour |  | Standard | OnPart | Downskin | 4.3.5.1.2 |  |
|  | $\begin{gathered} \text { Speed } \\ (\mathrm{mm} / \mathrm{s}): \\ \hline \end{gathered}$ |  |  |  |  |  |
|  | Power (W): |  |  |  |  |  |






[^0]:    ${ }^{1}$ Certain commercial entities, equipment, or materials may be identified in this document in order to describe an experimental procedure or concept adequately. Such identification is not intended to imply recommendation or endorsement by the National Institute of Standards and Technology, nor is it intended to imply that the entities, materials, or equipment are necessarily the best available for the purpose.

