NIST Technical Note 2131

Fire Hazards of Dry Versus Watered Christmas Trees

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Abstract

These experiments were designed to examine the difference in fire hazard between a dry Christmas tree and a watered Christmas tree for fire safety awareness. One dry tree (no water after harvesting) and one watered tree was tested with no replicates.

The test specimens were approximately 2.1 m (7 ft.) tall Douglas fir trees cut fresh from a local Maryland tree farm approximately four weeks prior to testing. The watered tree was placed in a bucket of water within 3 hours of being harvested and a fresh cut was made approximately 50 mm (2 in.) from the base of the trunk prior to placement in the water. Both the dry tree and watered tree were stored indoors until the day of the test.

For fire testing, each tree was placed in a mockup of a corner of a living room constructed to provide background for video recording and not to replicate a specific or typical living room. The ignition source was a book of matches with the match heads wrapped with a thin nickel-chromium wire that heats, igniting the matchbook, when electricity is applied.

Three attempts were made to ignite the watered tree during which the ignition source and position of fuel adjacent to the ignition source were varied, however, no sustained ignition of the tree was achieved. For the dry tree, ignition of the tree was achieved on the first attempt and a peak heat release rate of 7362 kW was reached 31 s after ignition.

Data and video from these experiments are available in the Fire Calorimetry Database [1].

Key words

Christmas Tree; Holiday Fire Safety; Fire Calorimetry Database

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1. Scope and Objectives

According to the National Fire Protection Association (NFPA), between 2014 and 2018 fire departments in the United States responded to an average of 160 home fires each year started with a Christmas tree [2]. Although Christmas tree fires are infrequent, when they occur, they can be dangerous and costly. These fires cause an annual average of 2 civilian deaths, 14 civilian injuries, and \$10.3 million in property damage [3] in the United States.

Previous experimental studies conducted at the National Institute of Standards and Technology (NIST) have focused on the characterization of fires in specific species of trees [4] and the numerical modeling of these fires [5]. Additionally, numerous institutions conduct tree burns to promote holiday fire safety; e.g. [6]–[8].

The experiments presented in this report were designed by staff at the NIST National Fire Research Laboratory (NFRL) and Public Affairs Office (PAO) to examine the difference in fire hazard between a properly maintained (watered) Christmas tree and dry Christmas tree for fire safety awareness. One watered tree and one dry tree (no water after harvesting) was tested with no test replicates. For fire testing, each tree was placed in a mockup of a corner of a living room constructed to provide background for video recording and not to replicate a specific or typical living room. The fire behavior of artificial trees was not considered.

2. Test Setup and Procedure

2.1. Tree specimens and conditioning

Four approximately 2.1 m (7 ft.) tall Douglas fir trees were cut fresh from a local Maryland tree farm on October 5th, 2017; approximately four weeks prior to testing (Fig. 1). The trees were transported to the NFRL and stored indoors until the day of the test. Two trees were placed in buckets of water within 3 hours of harvesting and a fresh cut was made approximately 50 mm (2 in.) from the base of the trunk prior to placement in the water (Fig. 2a). The water in the buckets was refilled regularly until the day of the fire test; i.e., the trees always had water. The other two trees were nailed to plywood bases and not given water (Fig. 2b). Four trees were harvested to have backups in case of problems during conditioning or testing, however, only one dry and one watered tree were fire tested. The mass and dimensions of the trees were not measured.



Fig. 1. Photograph of the trees shortly after they were cut.



Fig. 2. Photograph of conditioning of the trees prior to testing: (a) watered and (b) dry.

2.2. Room corner mockup

The trees were tested in a mockup of a corner of a living room designed to provide background for video recording (Fig. 3). The ceiling height was approximately 2.4 m (8 ft.). The setup was constructed without a soffit to allow combustion products (smoke) to rise to the exhaust hood more easily with less obscuration of the video. The room corner was rebuilt for each test using identical furnishings including an upholstered wing chair, a wood table, a shelf with miscellaneous objects, a carpet, and a painting. The laboratory floor was covered with 16 mm (5/8 in.) thick Type X gypsum boards to limit heat transfer to the concrete. The mass and location of the furnishings were not measured.



Fig. 3. Photograph of room corner test setup.

2.3. Ignition scenario

The ignition source was a book of matches with the match heads wrapped with a thin nickelchromium wire that heats when electricity is applied allowing safe, remote ignition of the tree. This is often referred to as an "electric match." The electric match was placed in the branches in the lower third of the tree. After the first unsuccessful attempt to ignite the watered tree, two books of matches were used to create a larger source as seen in Fig. 4 for the remainder of the ignitions for both the watered and dry tree.



Fig. 4. Photographs of fire ignition source (electric match) with two match books.

2.4. Instrumentation

The instrumentation used in these experiments was limited to data acquired using the NIST 20 MW calorimetry measurement system and video cameras. A digital timer with a large (red) light emitting diode (LED) display was placed in view of the cameras. The display showed seconds and deci-seconds for the first 60 s and then switched to minutes and seconds. For example, the photograph of "ignition" for the watered tree in Section 3 shows 00:58 (or 580 ms). The digital timer was used with the video to confirm the times reported by the calorimeter data acquisition system. Slight discrepancies (< 2 s) between the calorimeter event time and image clock time may exist due to lack of synchronization of the clocks.

2.4.1. Fire calorimetry

The calorimetry measurement system at the NFRL allows for measurement of heat release by 1) the principle of oxygen consumption calorimetry and 2) the principle of fuel consumption calorimetry (consumption of natural gas). The NFRL utilizes large canopy exhaust hoods to capture fire effluents for quantification of the heat release as a function of time. The system

includes an emissions control system (ECS) to treat smoke particulates and combustion gases to comply with local environmental requirements. The facility has four canopy hoods, each denoted by its maximum fire capacity: 0.5 MW ($3.1 \text{ m} \times 3.2 \text{ m}$), 3 MW ($6.1 \text{ m} \times 6.1 \text{ m}$), 10 MW ($8.4 \text{ m} \times 12.4 \text{ m}$), and 20 MW ($13.8 \text{ m} \times 15.4 \text{ m}$). The average expanded uncertainty in the normal operating range for each hood for generic combustible fuel is 7.9 %, 6.8 %, 8.7 %, and 9.8 %, respectively. This uncertainty is valid for near steady state fires. Transient events (less than 30 s) may have larger uncertainty because of system response time. The range of expanded uncertainty for the natural gas (fuel consumption) verification burners is 1.4 % to 1.8 %. Detailed information on the NFRL calorimetry measurement system is provided by Bryant and Bundy [9].

These experiments utilize only oxygen consumption calorimetry on the 6 m hood with an exhaust flow rate of approximately 21 kg/s. This exhaust flow rate is sufficient to capture all the combustion products for this experiment due to the short duration of the peak burning.

2.4.2. Video cameras

High-definition video of the experiments was captured using several digital video cameras at a large stand-off from the room corner (Fig. 5). Close up video footage of the tree was captured using a waterproof sports action camera placed in a water-filled glass globe on the table directly in front of the tree (Fig. 6). The water served the dual purposes of cooling the camera and filtering out the infrared thermal radiation produced by the fire that would otherwise damage the camera's imaging sensor. This concept was later developed to house 360° cameras as described by Hoehler [10].



Fig. 5. Photograph of the video camera setup.



Fig. 6. Photograph of the setup used for the water-cooled video camera.

2.5. Test procedure

The following procedure was used:

- 1. Pre-test
 - a. Call the NIST Fire Department to deactivate automatic fire suppression.
 - b. Turn on exhaust fans and open makeup air dampers.
 - c. Verify that area carbon monoxide detectors and alarms are functioning.
 - d. Turn on measurement systems and verify that they are functioning.
 - e. Turn on lighting and verify camera settings.
 - f. Prepare the ignition source.
- 2. Test Director conducts Safety Briefing and completes safety checklist.
- 3. Start data acquisition and turn on video cameras and audio recording.
- 4. Acquire background data for Heat Release Rate.
- 5. Ignite fire using electric match.
- 6. Collect experimental data and video.
- 7. Stop data acquisition: The test will proceed until total fuel burnout unless the Test Director, in consultation with the Safety Officer, decide to suppress the fire.
- 8. Post-test/Tear-down:
 - a. Safety Officer calls NIST fire department to reactivate automatic fire suppression systems.
 - b. Debris and material are properly stored or discarded by NFRL staff.

3. Results

Downloadable data and video from these experiments are available in the <u>NIST Fire Calorimetry Database</u> [1]. Behind the scenes photos and the final videos from the NIST Public Affairs Office are available at <u>https://www.nist.gov/topics/fire/why-you-should-water-your-christmas-tree</u>. Due to the limited number of tests conducted and because the room corner was not designed to replicate real conditions, these results should not be extrapolated.

Three attempts were made to ignite the watered tree; however, no sustained ignition of the tree was achieved. After the first attempt, a second match book was added to the electric match to create a larger fire source. For the third attempt, two match books were used, and the electric match was placed in an area of the tree with the most significant drying of the needles. In the third attempt, the fire initially grew as the needles adjacent to the matches ignited, however the fire then self-extinguished. The measured heat release rate (HRR) for the third attempt is shown in Fig. 7. A peak heat release rate of 6.7 kW was reached 71 s after ignition. This fire size is well below the normal operating range and outside the range of confirmation tests with the reference burner. The peak heat release rate is at the limit of detection for this calorimeter and not well quantified. A sequence of images associated with key events is provide in Table 1.

For the dry tree, ignition of the tree was achieved on the first attempt and the fire grew rapidly. The measured heat release rate is shown in Fig. 8. A peak heat release rate of 7362 kW was reached 31 s after ignition. A sequence of images for key events is provide in Table 2.



Fig. 7. Plot of Heat Release Rate data with event markers and error bars (combined expanded uncertainty) shown at peak for the watered tree.

Event #	Time (min)	Description	Video Snapshot Image
1	0	Ignition of Electric Match	
peak	1.18	Peak HRR	
2	4.05	Fire Out	

 Table 1. Summary of observed test events for the watered tree.



Fig. 8. Plot of Heat Release Rate data with event markers and error bars (combined expanded uncertainty) shown at peak for the dry tree.

Event #	Time (min)	Description	Video Snapshot Image
1	0	Ignition of Electric Match	
peak	0.52	Peak HRR	
2	12.02	Suppression	
3	16.55	Fire Out	

 Table 2. Summary of observed test events for the dry tree.

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