## NATIONAL BUREAU OF STANDARDS

The National Bureau of Standards ' was established by an act of Congress March 3, 1901. Today, in addition to serving as the Nation's central measurement laboratory, the Bureau is a principal focal point in the Federal Government for assuring maximum application of the physical and engineering sciences to the advancement of technology in industry and commerce. To this end the Bureau conducts research and provides central national services in four broad program areas. These are: (1) basic measurements and standards, (2) materials measurements and standards, (3) technological measurements and standards, and (4) transfer of technology.
The Bureau comprises the Institute for Basic Standards, the Institute for Materials Research, the Institute for Applied Technology, the Center for Radiation Research, the Center for Computer Sciences and Technology, and the Office for Information Programs.
THE INSTITUTE FOR BASIC STANDARDS provides the central basis within the United States of a complete and consistent system of physical measurement; coordinates that system with measurement systems of other nations; and furnishes essential services leading to accurate and uniform physical measurements throughout the Nation's scientific community, industry, and commerce. The Institute consists of an Office of Measurement Services and the following technical divisions:

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Office of Standard Reference Data-Clearinghouse for Federal Scientific and Technical Information 3-Office of Technical Information and Publications-Library-Office of Public Information-Office of International Relations.

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# HANDBOOK H28 (1969) SCREW-THREAD STANDARDS FOR FEDERAL SERVICES 

PART I<br>UNIFIED UNJ<br>UNIFIED MINIATURE SCREW THREADS

NBS Handbook H28 (1969)
Superseding H28 (1957) Part I and that applicable to Part I in the 1963 Supplement to H28
Nat. Bur. Stand. (U.S.), Handb. 28, 237 pages (Dec. 1969)

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## Foreword

The Interdepartmental Screw Thread Committee (ISTC) was established to promote uniformity in screw-thread standards in the Department of Defense (including the Departments of the Army, Navy, and Air Force) and the Department of Commerce. The organization and functions of the ISTC are shown in its charter.

The ISTC shall be responsible for (1) recommending to appropriate activities research and development efforts relating to screw threads; (2) developing standards for screw threads; (3) participating in the development of standards for gages, dies, taps, and other items associated with the manufacture and use of interchangeable threaded parts employed by Government agencies; and (4) providing advisory services on science, technology, and standards of practice as these relate to screw threads.

The standards developed by the ISTC, on approval by the participating Departments and Agencies, are published in Handbook H28. The standards in Handbook H28 are revised as deemed necessary by the ISTC.

This 1969 issue of Part I is being published essentially to incorporate the changes in Part I made by the 1963 Supplement and to revise the sections on Nomenclature, and Gages and Gaging to be in general agreement with USA B1.7-1965 and USA B1.2-1966.

Handbook H28 is issued in 3 parts. This Part, Part I, contains information on Unified and Unified miniature screw threads. Part II contains information on pipe threads, including dryseal pipe threads; gas cylinder valve threads; hose coupling, including fire-hose coupling threads; and hose connections for welding and cutting equipment. Part III contains information on Acme, Stub-Acme, Buttress, and miscellaneous threads.

At this time, the latest issues of Parts II and III are those of 1957 identified by a block on the cover stating "Reprinted December 1966 with corrections". These two parts include the changes to the respective parts listed in the 1963 Supplement to H28.

In this 1969 issue of Part I, sections are being designated by arabic instead of roman numerals. Appendixes are designated by an arabic number preceded by A. To allow insertion of section 4 on UNJ threads, section I, Introduction, of the 1957 issue is included but without a section designation. Former sections II, III, and IV have been renumbered as sections 1,2 , and 3 .

In this 1969 issue of Part I, when designating tables and figures, a number is only used once. For example, if a figure is designated figure 2.1, there will be no table 2.1.

In 1966, the American Standards Association (ASA) changed its name to the United States of America Standards Institute (USASI). In October 1969, USASI changed its name to the American National Standards Institute (ANSI).

All references to USASI herein will apply to the American National Standards Institute (ANSI). Preparation for printing of Handbook H28 has progressed too far to make the changes in name throughout the Handbook.

Arthur G. Strang, Chairman,<br>Interdepartmental Screw Thread Committee

## Metric Translation of Screw Thread Specifications

To facilitate and encourage the use of these unified screw thread standards in metric countries most of the specifications given in this document have been translated into metric language under the sponsorship of ASME and SAE. This translation appears as USA standard B1.1a-1968. The detailed specifications in metric language of the unified screw threads given in B1.1a-1968 is more extensive than is presently available for the ISO metric series of screw threads. Copies of USA standard B1.1a can be obtained for $\$ 3.00$ from the American National Standards Institute, 1430 Broadway, New York, New York 10018.

# Declaration of Accord 

with respect to the

## unification of Screw Threads

3 is herebu declared that the undersigned，representatives of their Government and Industry Bodies，charged with the development of standards for screw threads，Agree that the standards for the Unified Secrete Threads given in the publications of the Committees of the British Standards Institution，Canadian Standards Association，American Standards Association and of the Interde－ partmental Screw Thread Committee fulfil all of the basic requirements for general interchangeability of threaded products made in accordance with anu of these standards．

$\mathbb{T}_{1}$he Bodies noted above will maintain continuous cooperation in the further development and extension of these standards．

Signed in washington，包．©．，this 18th day of November，1948，at the Rational Bureau of Standards of the $\mathfrak{Z n i t e d} \mathfrak{S t a t e s}$ ．

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Canadian Standards Association
zetinistry of Supply，Wanted Ring dom
British Standards $\mathfrak{g n s t i t u t i o n ~}$
Representative of British $\mathfrak{F n d u s t r y}$
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American Standards Association
The American Society of $\mathfrak{\text { mechanical Engineers }}$ Society of Automotive engineers
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APPROVAL BY

THE DEPARTMENTS OF DEFENSE AND COMMERCE
The accompanying Handbook H28 (1969), Part I, on Screw-Thread
Standards for Federal Services, submitted by the Interdepartmental Screw Thread Committee, is hereby approved for use by the Departments of Defense and Commerce.

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## Contents <br> Part I



The purpose of Handbook H 28 is to present complete dimensional data for the threads on the threaded products procured by the Federal Services. So far as practicable, these data are intended to conform to generally accepted commercial practice, although certain special requirements of the Federal Services necessitate the inclusion of some standards not generally applicable outside of the Government. References are cited throughout the text to the standards promulgated by the United States of America Standards Institute (USASI) and to such other published standards as are in agreement with the specifications herein.

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USA Standards Committees are:
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# UNITED STATES DEPARTMENT OF COMMERCE <br> NATIONAL BUREAU OF STANDARDS 

## HANDBOOK H28

SCREW-THREAD STANDARDS

FOR FEDERAL SERVICES

## SECTION 1

1969

## NOMENCLATURE, DEFINITIONS, AND LETTER SYMBOLS FOR SCREW THREADS

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This section is in general agreement with United States of America Standards Institute Standard USA B1.7, Nomenclature, Definitions, and Letter Symbols for Screw Threads, published by The American Society of Mechanical Engineers, United Engineering Center, 345 East 47th Street, New York, N.Y. 10017. The latest revision should be consulted when referring to this USA standard. As of date of issue of this section, USA B1.7-1965 is the latest revision. For further related definitions, see USA B18.12, Glossary of Terms for Mechanical Fasteners.

## 1. GENERAL

1.1. The purpose of this section is to establish uniform practices with regard to: (1) Screw-thread nomenclature, and (2) letter symbols for designating dimensions of screw threads for use on drawings, in tables of dimensions which set forth dimensional standards, and in other records, and for expressing mathematical relationships.
1.2. This section consists of a glossary of terms, tables of screw-thread dimensional symbols, illustrations showing the application of dimensional symbols, tables of thread series and dimensional designations, and an index.
1.3. Typography.-In accordance with the usual practice in published text, letter symbols and letter subscripts, whether upper or lower case, should be printed in italic type. An exception is Greek letters; Greek capital letters are always vertical, and lower case always resembles italics. In manuscripts this is indicated by underlining each symbol to be italicized. Coefficients, numeral subscripts, and exponents should be printed in vertical Arabic numerals. Standard mathematical notation should be followed.

## 2. DEFINITIONS OF TERMS

2.1. The terms commonly applied to screw threads may be classified in four general groups, namely, those relating to: (1) types of screw threads, (2) size and fit of mechanical parts in general, (3) geometrical elements of both straight and taper screw threads, and (4) dimensions of screw threads.

The definitions presented herein apply generally to theoretically correct leads and thread forms but also reflect practical considerations relative to production, gaging, and measurement of threads. With a few obvious exceptions the definitions apply generally to all forms of thread.

## 3. TERMS RELATING TO TYPES OF SCREW THREADS

3.1. Screw threads and the terms generally applied to designate the types of screw threads, are defined as follows:
3.2. Screw Thread.-A screw thread (hereinafter referred to as a thread), is a ridge, usually of uniform section and produced by forming a groove in the form of a helix on the external or internal surface of a cylinder, or in the form of a conical spiral on the external or internal surface
of a cone or frustum of a cone. A screw thread formed on a cylinder is known as a straight or parallel thread, to distinguish it from a taper thread which is formed on a cone or frustum of a cone.
3.3. Thread.-A thread is a portion of a screw thread encompassed by one pitch. On a single-start thread it is equal to one turn. (See par. 6.5 Threads per Inch and par. 6.6 Turns per Inch.)
3.4. Single-Start Thread.-A single-start thread is one having the lead equal to the pitch. (See par. 6.2 Pitch and par. 6.3 Lead.)
3.5. Multiple-Start Thread.-A multiple-start thread is one in which the lead is an integral multiple (other than one) of the pitch.
3.6. External Thread.-An external thread is one on a cylindrical or conical external surface.
3.7. Internal Thread.-An internal thread is one on a cylindrical or conical internal surface.
3.8. Right-Hand Thread.-A thread is a righthand thread if, when viewed axially, it winds in a clockwise and receding direction. A thread is considered to be right-hand unless specifically indicated otherwise.
3.9. Left-Hand Thread.-A thread is a left-hand thread if, when viewed axially, it winds in a counterclockwise and receding direction. All left-hand threads are designated $L H$.
3.10. Complete Thread.-The complete or full form thread is that cross section of a threaded length having full form at crest and root. (See par. 3.14 Effective Thread, par. 6.26 Length of Complete Thread.)
NOTE: Formerly in pipe thread terminology this was referred to as "the perfect thread" but that is no longer considered desirable.
3.11. Incomplete Thread.-An incomplete thread is a threaded profile having either crests or roots, or both crests and roots, not fully formed, resulting from their intersection with the cylindrical or end surface of the work or the vanish cone. It may occur at either end of the thread.
NOTE: Formerly in pipe thread terminology this was referred to as "the imperfect thread" but that is no longer considered desirable.
3.12. Lead-Thread.-The lead-thread is that portion of the incomplete thread that is fully formed at root but not fully formed at crest which occurs at the entering end of either external or internal threads. (See note at par. 6.26.)
3.13. Vanish Thread.-(Partial Thread, Washout Thread, or Thread Run-out.) A vanish thread is that portion of the incomplete thread which is not fully formed at root or at crest and root. It is produced by the chamfer at the starting end of the thread forming tool. (See par. 5.28 Vanish Cone.)

[^1]3.14. Effective Thread.-The effective (or useful) thread includes the complete thread, and those
portions of the incomplete thread which are fully formed at the root but not at the crest (in taper pipe threads this includes the so-called black crest threads); thus excluding the vanish thread.
3.15. Total Thread.-The total thread includes the complete and all of the incomplete thread; thus including the vanish thread.
3.16. Classes of Threads.-Classes of threads are distinguished from each other by the amounts of tolerance or tolerance and allowance specified.
3.17. Thread Series.-Thread series are groups of diameter/pitch combinations distinguished from each other by the number of threads per inch applied to specific diameters.
3.18. Structural Thread.-A structural thread is intended to develop a significant amount of the core strength of the externally threaded member before breaking the core of that member or stripping the external or internal threads of a threaded connection. A structural thread is not intended for, but may be used for attaching purposes. (UNC and UNF thread series are examples of Structural Threads with tolerance calculations based on a length of engagement equal to one diameter.)
3.19. Attaching-Purpose Thread (also sometimes referred to as constructional or retaining threads).-An attaching-purpose thread is not intended to develop a significant amount of core strength of the externally or internally threaded member of a threaded connection. An attachingpurpose thread is not normally intended for structural purposes. ( 12 UN and 16 UN uniform pitch thread series are examples of Attaching-Purpose Threads with tolerance calculations based on a length of engagement equal to nine pitches.)

## 4. TERMS RELATING TO SIZE AND FIT

(These are definitions applying to mechanical parts, generally.)
4.1. Terms relating to the size and fit of parts, which are generally applicable to mechanical parts, including threads, are defined as follows:
4.2. Dimension.-A dimension is a geometrical characteristic such as diameter, length, angle, or center distance.
4.3. Size.-Size is a designation of magnitude. When a value is assigned to a dimension it is referred to hereinafter as the size of that dimension.

NOTE: It is recognized that the words "dimension" and "size" are both used at times to convey the meaning of magnitude.
4.4. Nominal Size.-The nominal size is the designation which is used for the purpose of general identification.
4.5. Basic Size.-The basic size is that size from which the limits of size are derived by the application of allowances and tolerances.
4.6. Reference Size.-A reference size is a size without tolerance used only for information purposes and does not govern manufacturing or inspection operations.
4.7. Design Size.-The design size is the basic size with allowance applied, from which the limits of size are derived by the application of tolerances. If there is no allowance the design size is the same as the basic size.
4.8. Actual Size.-An actual size is a measured size.
4.9. Limits of Size.-The limits of size are the applicable maximum and minimum sizes. (See par. 4.14.)
4.10. Maximum-Material-Limit.-A maximum-material-limit is that limit of size that provides the maximum amount of material for the part. Normally it is the maximum limit of size of an external dimension or the minimum limit of size of an internal dimension.
4.11. Minimum-Material-Limit.-A minimum-material-limit is that limit of size that provides the minimum amount of material for the part. Normally it is the minimum limit of size of an external dimension or the maximum limit of size of an internal dimension.

NOTE: Examples of exceptions are; an exterior corner radius where the maximum radius is the minimum-material-limit and the minimum radius is the maximum-material-limit.
4.12. Allowance.-An allowance is a prescribed difference between the maximum-material-limits of mating parts. It is the minimum clearance (positive allowance) or maximum interference (negative allowance) between such parts. (See par. 4.17 Fit.)
4.13. Tolerance.-A tolerance is the total permissible variation of a size. The tolerance is the difference between the limits of size.
4.14. Tolerance Limit.-A tolerance limit is the variation, positive or negative, by which a size is permitted to depart from the design size. (See par. 4.9.)
4.15. Unilateral Tolerance.-A unilateral tolerance is a tolerance in which variation is permitted only in one direction from the design size.
4.16. Bilateral Tolerance.-A bilateral tolerance is a tolerance in which variation is permitted in both directions from the design size.
4.17. Fit.-Fit is the general term used to signify the range of tightness or looseness which may result from the application of a specific combination of allowances and tolerances in the design of mating parts.
4.18. Actual Fit.-The actual fit between two mating parts is the relation existing between them with respect to the amount of clearance or interference that is present when they are assembled.

NOTE: Fits are of three general types: clearance, transition, and interference.
4.19. Clearance Fit.-A clearance fit has limits of size so prescribed that a clearance always results when mating parts are assembled.
4.20. Interference Fit.-An interference fit has limits of size so prescribed that an interference always results when mating parts are assembled.
4.21. Transition Fit.-A transition fit has limits
of size so prescribed that either a clearance or an interference may result when mating parts are assembled.
4.22. Unilateral Tolerance System.-A design plan which uses only unilateral tolerances is known as a unilateral tolerance system.
4.23. Bilateral Tolerance System.-A design plan which uses only bilateral tolerances is known as a bilateral tolerance system.
4.24. Basic Hole System.-A basic hole system is a system of fits in which the design size of the hole is the basic size and the allowance, if any, is applied to the shaft.
4.25. Basic Shaft System.-A basic shaft system is a system of fits in which the design size of the shaft is the basic size and the allowance, if any, is applied to the hole.

## 5. TERMS RELATING TO GEOMETRICAL ELEMEN'S OF SCREW THREADS

5.1. Terms relating to geometrical elements of both straight and taper threads are defined as follows:
5.2. Thread Axis.-The thread axis is the axis of its pitch cylinder or cone. (See par. 7.2.)
5.3. Major Cylinder.-The major cylinder bounds the crests of an external straight thread or the roots of an internal straight thread.
5.4. Sharp Major Cylinder.-The sharp major cylinder bounds the sharp crests of an external straight thread or the sharp roots of an internal straight thread.
5.5. Major Cone.-The major cone bounds the crests of an external taper thread or the roots of an internal taper thread.
5.6. Sharp Major Cone.-The sharp major cone has an apex angle equal to that of the pitch cone, the surface of which bounds the sharp crests of an external taper thread or the sharp roots of an internal taper thread.
5.7. Рitch Cylinder.-The pitch cylinder is one of such diameter and location of its axis that its surface would pass through a straight thread in such a manner as to make the widths of the thread ridge and the thread groove equal and, therefore, is located equidistantly between the sharp major and minor cylinders of a given thread form. On a theoretically perfect thread these widths are equal to one-half of the basic pitch. (See par. 5.2 Axis of Thread, par. 6.21 Pitch Diameter.)
5.8. Рitch Cone.-The pitch cone is one of such apex angle and location of its vertex and axis that its surface would pass through a taper thread in such a manner as to make the widths of the thread ridge and the thread groove equal and, therefore, is located equidistantly between the sharp major and minor cones of a given thread form. On a theoretically perfect taper thread these widths are equal to one-half of the basic pitch. (See par. 5.2 Axis of Thread and par. 6.21 Pitch Diameter.)
5.9. Minor Cylinder.-The minor cylinder
bounds the roots of an external straight thread or the crests of an internal straight thread.
5.10. Sharp Minor Cylinder.-The sharp minor cylinder bounds the sharp roots of an external straight thread or the sharp crests of an internal straight thread.
5.11. Minor Cone.-The minor cone bounds the roots of an external taper thread or the crests of an internal taper thread.
5.12. Sharp Minor Cone.-The sharp minor cone has an apex angle equal to that of the pitch cone, the surface of which bounds the sharp roots of an external taper thread or the sharp crests of an internal taper thread.
5.13. Pitch Line.-The pitch line is a generator of the cylinder or cone specified in the definitions of par. 5.7 Pitch Cylinder and par. 5.8 Pitch Cone.
5.14. Thread Form.-The thread form is the thread profile in an axial plane for a length of one pitch of the complete thread.
5.1.5. Basic Thread Form.-The basic thread form is the theoretical thread profile for a length of one pitch in an axial plane, from which the design thread forms for both the external and internal threads are developed.
5.16. Design Thread Form.-The design thread form is the maximum material form permitted for the extennal or internal thread. In practice, however, the form of root is an indeterminate contour not encroaching on the maximum material form of the mating thread when assembled.
5.17. Fundamental Triangle.-The fundamental triangle is the triangle whose corners coincide with three consecutive intersections of the extended flanks of the basic thread form.
5.18. Flank.-The flank (or side) of a thread is either surface connecting the crest with the root. The flank surface intersection with an axial plane is theoretically a straight line.
5.19. Leading Flank.-When a thread is about to be assembled with a mating thread, the leading flank of the thread faces the mating thread.
5.20. Following Flank.-The following flank of a thread faces the leading flank.
5.21. Load Flank.-The load flank takes the externally applied axial load in an assembly. The term is used particularly in relation to buttress and other similar threads.
5.22. Clearance Flank.-The clearance flank faces the load flank.
5.23 . Crest.-The crest is that surface of the thread which joins the flanks of the thread and is farthest from the cylinder or cone from which the thread projects.
5.24. Rоот.-The root is that surface of the thread which joins the flanks of adjacent thread forms and is identical with or immediately adjacent to the cylinder or cone from which the thread projects.
5.25. Sharp Crest (Crest Apex).-The sharp crest is the apex formed by the intersection of the flanks of a thread when extended, if necessary, beyond the crest.
5.26. Sharp Root (Root Apex).-The sharp root is the apex formed by the intersection of the ajdacent flanks of adjacent threads when extended, if necessary, beyond the root.
5.27. Base.-The base of a thread section coincides with the cylindrical or conical surface from which the thread projects.
5.28. Vanish Cone.-The surface of the vanish cone bounds the roots of the vanish thread formed by the lead or chamfer of the threading tool. (See fig. 1.2 and par. 3.13 Vanish Thread.)
5.29. Plane of Vanish Point.-The plane of vanish point of an external thread is the intersection of generators of the vanish cone with generators of the cylinder of the largest major diameter of the thread. (See fig. 1.5.)
5.30. Blunt Start or Blunt End Thread."Blunt start" or "blunt end" designates the removal of the incomplete thread at the end of the thread. This is a feature of threaded parts that are repeatedly assembled by hand, such as hose couplings and thread plug gages, to prevent cutting of hands and crossing of threads, and which was formerly known as a Higbee cut. (See fig. 1.1.)


Figure 1.1. Blunt start
5.31. Gimlet Point.-A gimlet point is a threaded cone point at the entering end of an external thread.
5.32. Chamfer.-A chamfer is a conical surface at the end of a thread or shaft.
5.33. Countersink.-A countersink is a bevel or flare at the end of a hole.
5.34. Вотtom of Chamfer.-On a chamfered internal taper thread, the bottom of the chamfer is defined as the intersection of the chamfer cone and the pitch cone of the thread.

## 6. TERMS RELATING TO DIMENSIONS OF SCREW THREADS

6.1. Terms relating to dimensions of both straight and taper threads are defined as follows:
6.2. Ретсн.-The pitch of a thread having uniform spacing is the distance, measured parallel to its axis, between corresponding points on adjacent
thread forms in the same axial plane and on the same side of the axis. The basic pitch is equal to the lead divided by the number of thread starts. (See par. 6.4 Helix Variation, par. 7.4.)
6.3. Lead.-When a threaded part is rotated about its axis with respect to a fixed mating thread, the lead is the axial distance moved by the part in relation to the amount of angular rotation. The basic lead is commonly specified as the distance to be moved in one complete rotation. It is necessary to distinguish measurement of lead from measurement of pitch, as uniformity of pitch measurements does not assure uniformity of lead. Variations in either lead or pitch cause the functional diameter of thread to differ from the pitch diameter. (See par. 7.5.)
6.4. Helix Variation.-Helix variation of a thread is a wavy deviation from true helical advancement. The "helical path" includes the helix with its superimposed variation and is measured either as the maximum deviation from the true helix or as the "cumulative pitch." The cumulative pitch is the distance measured parallel to the axis of the thread between corresponding points on any two thread forms whether or not they are in the same axial plane. (See par. 7.5.)
6.5. Threads per Inch.-The number of threads per inch is the reciprocal of the pitch in inches.
6.6. Turns per Inch.-The number of turns per inch is the reciprocal of the lead in inches.
6.7. Included Angle.-The included angle of a thread (or angle of thread) is the angle between the flanks of the thread measured in an axial plane.
6.8. Flank Angle.-The flank angle is the angle between the flank and the perpendicular to the axis of the thread, measured in an axial plane. A flank angle of a symmetrical thread is commonly termed the half-angle of thread. (See par. 7.3.)
6.9. Lead Angle.-On a straight thread, the lead angle is the angle made by the helix of the thread at the pitch line with a plane perpendicular to the axis. On a taper thread, the lead angle at a given axial position is the angle made by the conical spiral of the thread with the plane perpendicular to the axis, at the pitch line. (See fig. 1.2.)
6.10. Helix Angle.-On a straight thread, the helix angle is the angle made by the helix of the thread at the pitch line with the axis. On a taper thread, the helix angle at a given axial position is the angle made by the conical spiral of the thread with the axis at the pitch line. The helix angle is the complement of the lead angle. (See fig. 1.2.)

NOTE: The helix angle was formerly defined in accordance with the present definition of lead angle. (See par. 6.9.)
6.11. Thread Ridge Thickness.-The thread ridge thickness is the distance between the flanks of one thread ridge, normally measured parallel to the axis at the specified pitch radius. The thread ridge thickness may be specified and measured parallel to the axis at any other specified radius.
NOTE: The pitch radius is equal to one-half of the pitch diameter.
6.12. Thread Groove Width.-The thread groove width is the distance between the flanks of adjacent thread ridges normally measured parallel to the axis at the specified pitch radius. The thread groove width may be specified and measured parallel to the axis at any other specified radius.
6.13. Fundamental Triangle Height.-The fundamental triangle height of a thread, that is, the height of a sharp-V thread, is the distance, measured radially, between the sharp major and minor cylinders or cones.
6.14. Thread Height.-The thread height (or depth) is the distance measured radially between the major and minor cylinders or cones.
NOTE: In American practice the thread height is often expressed as a percentage of three-fourths of the fundamental triangle height.
6.15. Addendum.-The addendum of an external thread is the radial distance between the major and pitch cylinders or cones. The addendum of an internal thread is the radial distance between the minor and pitch cylinders or cones.
6.16. Dedendum.-The dedendum of an external thread is the radial distance between the pitch and minor cylinders or cones. The dedendum of an internal thread is the radial distance between the major and pitch cylinders or cones.
6.17. Crest Truncation.-The crest truncation of a thread is the radial distance between the sharp crest (crest apex) and the cylinder or cone that would bound the crest.
6.18. Root Truncation.-The root truncation of a thread is the radial distance between the sharp root (root apex) and the cylinder or cone that would bound the root.
6.19. Major Diameter.-On a straight thread the major diameter is that of the major cylinder. On a taper thread the major diameter at a given position on the thread axis is that of the major cone at that position. (See par. 5.3 Major Cylinder and par. 5.5 Major Cone.)
6.20. Minor Diameter.-On a straight thread the minor diameter is that of the minor cylinder. On a taper thread the minor diameter at a given position on the thread axis is that of the minor cone at that position. (See par. 5.9 Minor Cylinder and par. 5.11 Minor Cone.)
6.21. Pitch Diameter.-On a straight thread the pitch diameter is the diameter of the pitch cylinder. (See par. 5.7.) On a taper thread, the pitch diameter at a given position on the thread axis is the diameter of the pitch cone at that position. (See par. 5.8.) On a single-start thread of perfect form and lead, it is also the length between intercepts of a line which is perpendicular to the thread axis and intersects thread flanks on opposite sides of the thread axis. (See par. 7.6.)

[^2]NOTE: Pitch diameter on the buttress casing thread is defined by the American Petroleum Institute in API Standard 5B, as being midway between the major and minor diameters.
6.22. Thread Groove Diameter (Simple Effective Diameter).-On a straight thread the thread groove diameter is the diameter of the coaxial cylinder, the surface of which would pass through the thread profiles at such points as to make the width of the thread groove equal to one-half of the basic pitch. It is the diameter yielded by measuring over or under cylinders (wires) or spheres (balls) inserted in the thread groove on opposite sides of the axis and computing the thread groove diameter as thus defined.

On a taper thread the thread groove diameter is the diameter at a given position on the thread axis of the coaxial cone, the surface of which would pass through the thread profiles at such points as to make the width of the thread groove (measured parallel to the axis) equal to one-half of the basic pitch. It is the diameter yielded by measuring over or under cylinders (wires) or spheres (balls) inserted in the thread groove on opposite sides of the axis and computing the thread groove diameter as thus defined. (See par. 7.6.)
6.23. Thread Ridge Diameter.-On a straight thread the thread ridge diameter is the diameter of the coaxial cylinder, the surface of which would pass through the thread profiles at such points as to make the thickness of the thread ridge equal to one-half of the basic pitch.

On a taper thread the thread ridge diameter is the diameter at a given position on the thread axis of the coaxial cone, the surface of which would pass through the thread profiles at such points as to make the thickness of the thread ridge (measured parallel to the axis) equal to one-half of the basic pitch. (See par. 7.6.)
6.24. Functional (Virtual) Diameter.-The functional diameter of an external or internal thread is the pitch diameter of the enveloping thread of perfect pitch, lead, and flank angles, having full depth of engagement but clear at crests and roots, and of a specified length of engagement. It may be derived by adding to the pitch diameter in the case of an external thread, or subtracting from the pitch diameter in the case of an internal thread, the cumulative effects of deviations from specified profile, including variations in lead and flank angle over a specified length of engagement. The effects of taper, out-of-roundness, and surface defects may be positive or negative on either external or internal threads. (A perfect GO thread plug or ring gage, having a pitch diameter equal to that specified for the maximum-material-limit and having clearance at crest and root, is the enveloping thread corresponding to that limit.) (See par. 7.6.)

[^3]6.25. Form Diameter.-The form diameter is the diameter at the point nearest the root from which the flank is required to be straight.
6.26. Length of Complete Thread.-The length of complete thread is the axial length of a part where the thread section has full form at both
crest and root; that is, the vanish threads are not included. However, on commercial fasteners where there are unfilled crests at the start of rolled threads or a chamfer at the start of a thread, not exceeding two pitches in length, this is traditionally included in the specified thread length. (See par. 3.10 Complete Thread, par. 3.12 Lead Thread and par. 3.14 Effective Thread.)

Note: When designing threaded products, it is necessary to take cognizance of: (1) Such permissible length of chamfer and (2) the first threads which by virtue of gaging practice may exceed or be less than the product limits and which may be included within the length of complete thread. However, when the application is such as to require a minimum or maximum number, or length, of complete threads the specification shall so state. Similar specification is required for a definite length of engagement.
6.27. Length of Thread Engagement.-The length of thread engagement of two mating threads is the axial distance over which two mating threads are designed to contact. (See par. 6.26 Length of Complete Thread.)
6.28. Depth of Thread Engagement.-The depth (or height) of thread engagement between two coaxially assembled mating threads is the radial distance by which their thread forms overlap each other.
6.29. Major Clearance.-The major clearance is the radial distance between the root of the internal thread and the crest of the external thread of the coaxially assembled design forms of mating threads.
6.30. Minor Clearance.-The minor clearance is the radial distance between the crest of the internal thread and the root of the external thread of the coaxially assembled design forms of mating threads.
6.31. Tensile Stress Area.-The tensile stress area of an externally threaded part is the circular cross-sectional area, normal to the axis, of a theoretical circular cylinder which would fail under tension at the same load at which the threaded part fails, if the materials of both have the same mechanical properties.
6.32. Thread Shear Area.-The thread shear area of the external thread is the effective area in shear at a specified diameter of the mated internal thread. The thread shear area of the internal thread is the effective area in shear at a specified diameter of the mated external thread.
NOTE: The specified diameters are usually the maximum minor diameter of the mated internal thread and the minimum major diameter of the mated external thread.
6.33. Standoff.-The standoff is the axial distance between specified reference points on external and internal taper threaded members or gages, when assembled with a specified torque or under other specified conditions.

## 7. SCREW THREAD DEFINITIONS IN RELATION TO GAGING AND MEASUREMENT

7.1. The meanings of certain definitions, as given previously, require some explanation in regard to
their practical application and the values or results obtained in gaging or measurement of threads. The terms involved are: thread axis, flank angle, pitch, lead, and pitch diameter.
7.2. Thread Axis.-The thread axis is the axis of the pitch cylinder or cone. The pitch cylinder is one of such diameter and location of its axis that its surface would pass through a straight thread in such a manner as to make the widths of the thread ridge and the thread groove equal. The pitch cone is one of such apex angle and locations of its vertex and axis that its surface would pass through a taper thread in such a manner as to make the widths of the thread ridge and the thread groove equal.

It is required that measurements of pitch, lead, and flank angle of a thread gage be made in an axial plane, making it necessary that the direction or location of the axis be accurately known. To locate this axis accurately is relatively difficult. Normally the major cylinder or cone of an external thread, or the minor cylinder or cone of an internal thread, may be used as the reference surface, provided that it is round and concentric with the pitch cylinder or cone. The amount of eccentricity of such a surface, if any, may be determined at various points along and around the thread, by measuring the distance from the crest to the top of a cylinder (wire) or sphere (ball) laid in the thread. Also, the axis may be established by conical centers in the ends of a thread plug gage, with respect to which the thread was originally generated.
7.3. Flank Angle.-The flank angle is the angle between the flank and the perpendicular to the axis of the thread, measured in an axial plane. A flank angle of a symmetrical thread is commonly termed the half-angle of thread.

A flank angle is generally measured with respect to a reference surface, such surface being an end surface of a thread plug or ring gage or the major or minor cylinder or cone. Prior to using such a surface as a reference it is necessary to determine its actual relationship to the thread axis. The flank angle may also be measured with respect to an axis established by conical centers at the ends of a thread plug gage, with respect to which the thread was originally generated.
7.4. Pitch.- The pitch of a thread is the distance, measured parallel to its axis, between corresponding points on adjacent thread forms in the same axial plane and on the same side of the axis.

Measurements of pitch are commonly made from thread groove to thread groove in an axial plane using a ball contact piece to touch both flanks simultaneously. Such measurements establish the number of threads per unit of length (per inch) when the pitch is uniform, or the variations from the nominal pitch when the pitch is either uniform or periodic throughout the measured length of thread. (See par. 6.2.)
7.5. Lead and Helix Variations.-When a threaded part is rotated about its axis with respect to a fixed contact piece inserted in a thread groove, the lead is the axial distance moved by the part in
relation to the amount of angular rotation. Lead is commonly specified as the distance moved in one complete rotation. It is necessary to distinguish measurement of lead from measurement of pitch, as uniformity of pitch measurements does not assure uniformity of lead. Variations in either lead or pitch cause the functional diameter of a thread to differ from the pitch diameter.

Helix variation is a wavy deviation from true helical advancement.

Accordingly, it is necessary to measure lead or helix variation throughout one or more turns of a thread, in addition to measurements of pitch, in order to obtain full information regarding the dimensional deviations of the thread. (See pars. 6.3, 6.4.)
7.6. Pitch Diameter, Functional (Virtual) Diameter, Thread Ridge Diameter, and Thread Groove Diameter.-(As the definitions of these terms are rather lengthy they are not repeated here, but reference should be made to pars. 6.21 to 6.24 , inclusive. For threads of perfect form and lead the numerical value of the diameter defined by any one of these terms is equal to the pitch diameter.)
7.6.1. Because of the nearly perfect flank angles and lead of a thread plug gage, the measurement yielded by employing the three-wire system is considered to be the pitch diameter.
7.6.2. On threads of imperfect form or lead it is generally impracticable to determine accurately the pitch diameter as defined; the result obtained in measuring or gaging the thread is an approximation of either the pitch diameter or the functional (virtual) diameter. This approximation may be regarded as a pitch diameter, functional diameter, thread groove diameter, or thread ridge diameter, as related to respective types of equipment and conditions of verifying or measuring a thread. When a thread size is verified by means of a GO thread plug or ring gage, which is within specified gage limits or tolerances and engages the thread throughout a specified length of engagement, a determination is made by the method of attributes that the functional (virtual) diameter does not exceed the maximum-materiallimit. The size limit thus verified may be designated the "GO Functional Diameter." The GO thread plug or thread ring gage is the accepted criterion for verification of threaded product for GO functional diameter. However, various indicating type thread gages or thread snap gages having gaging elements which engage the thread over a length and flank engagement approximately equivalent to that of the GO thread plug or thread ring gage should give comparable results, and when properly correlated with the GO thread plug or thread ring gage may serve satisfactorily to give assurance that the functional diameter does not exceed the specified maximum-material-limit.
7.6.3. When a thread size is verified by means of a HI thread plug gage or LO thread ring gage, which is within specified gage limits or tolerances and enters or is entered with a drag over the length of thread specified, a determination is made that
the functional diameter lies within the minimum-material-limit. The size limit thus verified may be designated the "HI Functional Diameter" or the "LO Functional Diameter." The HI thread plug or the LO thread ring gage is the accepted criterion for verification of the HI and LO functional diameters of classes $1 \mathrm{~A}, 2 \mathrm{~A}, 1 \mathrm{~B}, 2 \mathrm{~B}$, and 3 B threads. However, various types of thread snap gages or indicating type thread gages with thread gaging elements which engage the thread over a length and flank engagement approximately equivalent to that of a HI thread plug gage or a LO thread ring gage should give comparable results, and when properly correlated with the HI thread plug or LO thread ring gage may serve satisfactorily to give assurance that the functional diameter is within the minimum-material-limit.
7.6.4. Gaging practice approximating pitch diameter measurement has been termed "LO Mini-mum-Material-Limit Gaging" and is the accepted criterion for verifying the minimum-material-limit of class 3A external threads. Such verification is accomplished by means of a limit type thread snap or indicating type thread gage with gaging elements having a thread form equivalent to that of the LO thread ring gage. Many thread snap and indicating type thread gages having gaging elements which contact the thread over a length of approximately two pitches are currently in use for determining the minimum-material-limit of various classes of screw threads. However, optimum results for verification of conformance to specifications utilizing differential analysis require a determination of pitch diameter, and this is achieved by means of gaging elements which contact the thread over a maximum length of one pitch. The size limit thus verified may be designated the "Min Single Element PD."
7.6.5. Indicating type thread gages may serve as suitable alternates for gaging the minimum single element PD. A gage having two gaging elements is preferred for detecting an elliptical condition, while a gage having three gaging elements is preferred for detecting the multi-lobed condition.
7.6.6. Gaging practices employing indicating type thread gages with thread forms of gaging elements suitable for approximating pitch diameter measurement, should give comparable results and serve satisfactorily to give assurance that the pitch diameter lies within the minimum-material-limit. Thread forms of gaging elements such as the cone and vee with radius contacts for pitch diameter or radius rolls (simulating the best wire) for thread groove diameter are employed in these instances, and, dependent on design and length of engagement, approximate pitch diameter measurement. The choice as to a cone and vee arrangement compared to radius rolls is a matter of individual preference, in consideration of including or excluding either flank angle or pitch deviations in the measurement. In general, it may be stated that a minimum length of engagement coupled with minimum flank contact results in the closest approximation of pitch diameter.

Conversely it may be stated that by increasing the length of engagement and the flank contact, the gaging tends toward the LO functional diameter. In practice, the length of engagement varies from less than one to approximately three pitches for various designs of gaging elements.
7.6.7. In order to determine that the deviations in lead or flank angle do not exceed the equivalent of one-half of the pitch diameter tolerance, indicating type thread gages may be employed to indicate the differential between the GO functional diameter and the pitch diameter. When the differential exceeds the equivalent of one-half of the pitch diameter tolerance, it is necessary to make a further analysis to determine whether or not any individual thread element exceeds the equivalent of the allowable specified percentage of the pitch diameter tolerance. Deviations from specified size and profile include variations in lead, uniformity of helix, flank angle, and taper; also out-of-roundness, and surface defects. Indicating type thread gages for determining diameter equivalents of lead deviations have gaging elements of the specified form and length of the GO thread gage, by which a differential reading can be obtained between the measured functional diameter and the first-full-thread pitch diameter measured by a single ridge of the GO gaging element, excluding taper, if any. Indicating type thread gages for determining diameter equivalents of flank angle deviations are those by which a differential reading can be obtained between the first-full-thread pitch diameter determined by a single ridge of the GO gaging element and that determined by the indicating type thread gage for pitch diameter having radius-type gaging elements.
7.6.8. When a thread size of a taper thread is verified by means of a taper thread plug or ring gage, or equivalent, having a basic gaging notch or surface, or limit notches, and which is within specified gage limits or tolerances, a determination is made that the functional diameter throughout the specified
length of hand engagement lies within specified size limits. The thread size thus verified may be designated the "Taper Thread Functional Diameter."

## 8. LETTER SYMBOLS AND DESIGNATIONS

8.1. Symbols associated with screw threads are of two kinds: (1) Letter symbols for designating dimensions of screw threads and threaded products; and (2) abbreviations used as designations for various standard thread forms and thread series.
8.2. Dimensional Symbols.
8.2.1. Standard letter symbols to designate the dimensions of screw threads in text and formulas are given in tables 1.4 and 1.6. General symbols are given in table 1.4 and pipe-thread symbols in table 1.6. The application of general symbols is illustrated in figures 1.2 and 1.3, and pipe-thread symbols in figure 1.5.
8.2.2. ISO symbols to designate screw thread dimensions are given in table 1.7. These symbols are commonly applied in Recommendations for Screw Threads of the International Standardization Organization (ISO).
8.3. Thread Designations.
8.3.1. Thread series designations are capital letter abbreviations of names used on drawings, in tables, and otherwise to designate various forms of thread and thread series, and commonly consist of combinations of such abbreviations. Assembled in tables 1.8 and 1.8 a are the names and abbreviations which are now in use, together with references to standards in which they occur, for various standard threads.
8.3.2. Thread element designations are capital letter abbreviations based on names of various thread dimensions in thread designations. Such abbreviations are for use on drawings and are shown in table 1.9.


Figure 1.2. General screw thread symbols (see table 1.4).


## EXTERNAL THREAD

Figure 1.3. General screw thread symbols (see table 1.4).
NOTE: These diagrams are not intended to show standard forms but illustrate only the applications of symbols.

Table 1.4. General Symbols (see figs. 1.2 and 1.3)

| Symbol | Dimensiou | Symbol | Dimension |
| :---: | :---: | :---: | :---: |
| D | Major diameter ${ }^{\text {a }}$, ${ }^{\text {b }}$ | G | Allowance at major, pitch, and minor |
| E | Pitch diameter. ${ }^{\text {b }}$ |  | diameters of external thread. |
| K | Minor diameter. ${ }^{\text {b }}$ | $L_{\text {Ls }}$ | Length of complete external thread. |
| $p$ | Pitch (Equals 1/n). | $L_{\text {tn }}$ | Length of complete internal thread |
| $L$ | Lead (Equals 1/N). |  | including chamfer. |
| $n$ | Number of threads (pitches) per unit of length (per inch) (tpi) (Equals $1 / p$ ). | $L_{w}{ }^{\text {c }}$ | Length of thread engagement. Diameter of measuring wires. |
| $N$ | Number of turns per unit of | $M_{w}$ | Measurement over wires. |
|  | length (per inch) (Equals $1 / L$ ). | $\stackrel{T}{T}$ | Measurement under wires. |
| ${ }^{\text {H }}$ | Fundamental triangle height. |  | Correction to measurement |
| $h$ | Thread height (or depth). ${ }^{\text {b }}$ |  | over wires to give pitch diameter, |
| ${ }_{h_{a}}$ | Addendum. |  | ${ }_{C}^{C}=w_{w}(1+\operatorname{cosec} \alpha)-\left(\cot ^{*} \alpha\right) / 2 n$. |
| $h_{b}$ | Symmetrical thread height.c | P | Correction to measurement |
| $h_{\text {e }}$ | Depth of thread engagement. |  | under wires to give pitch diameter, |
| $\alpha$ | Half-angle of symmetrical thread. |  | W. $P=(p \cot \alpha) / 2-(\operatorname{cosec} \alpha-1) w$. |
| $\alpha_{1}$ | Angle between leading flank of thread and normal to thread axis. | $\begin{aligned} & \lambda^{\prime} \\ & c \end{aligned}$ | Wire angle. Wire angle correction. ${ }^{e}$ |
| $\alpha_{2}$ | Angle between following flank of thread and normal to thread axis. | $\delta$ | Dcviation in any dimension. |
| $\lambda$ | Lead angle ( $\tan \lambda=L / \pi E)$. |  | Examples: Deviation in |
| $\psi$ | Helix angle ( $\cot \psi=L / \pi E)$. |  | pitch, $\delta p$; deviation in flank |
| $r_{\text {cs }}$ | Radius of rounding at: Crest of external thread |  | Pitch-diameter equivalent of |
| $r_{r s}$ | Root of external thread |  | deviations in flank half-angle. |
| $r_{\text {cn }}$ | Crest of internal thread | $\Delta E_{p}$ |  |
| $r_{r n}$ | Root of internal thread. |  | deviation in pitch. |
|  | Radial distance from apex of fundamental triangle to: |  |  |
|  | Rounded crest of external thread. ${ }^{\text {d }}$ |  |  |
| $f_{c s}$ | Flat at crest of external thread. ${ }^{\text {a }}$ |  |  |
|  | Width of: |  |  |
| $F_{c s}$ | Flat at crest of external thread. ${ }^{\text {d }}$ |  |  |

${ }^{a}$ Exception: $B$ is used for basic major diameter when this differs from the nominal major diameter.
${ }^{b}$ Subscripts $s$ (for screw) or $n$ (for nut) designating external and internal thread, respectively, may be used if necessary.
${ }^{c}$ For $60^{\circ}$ Unified thread this equals $0.75 \mathrm{H}=100$ percent thread height.
${ }^{d}$ In addition to the symbol with subscript $c s$, symbols with subscripts $r s, c n$, and $r n$ are also applicable as in the $r_{c s}$, etc., symbols above.
-See National Physical Laboratory "Gauging and Measuring Screw Threads," 1951, p. 23; Appendix A4 of H28.

| GREEK ALPHABET |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A $\boldsymbol{\alpha}$ Alpha | $\Delta \delta$ Delta | H $\eta$ Eta | K к Kappa | $\mathrm{N} \nu \mathrm{Nu}$ | $\Pi \pi \mathrm{Pi}$ | T $\tau$ Tau | X $\chi$ Chi |
| B $\beta$ Beta | E $\in$ Epsilon | $\theta \theta$ Theta | $\Lambda \lambda$ Lambda | E $\xi \mathrm{Xi}$ | P $\rho$ R Ro | $\Upsilon \cup$ Upsilon | $\Psi \psi \mathrm{Psi}$ |
| 「 $\gamma$ Gamma | Z $\zeta$ Zeta | I 1 Iota | M $\mu \mathrm{Mu}$ | $\bigcirc$ O Omicron | $\Sigma \sigma$ Sigma | $\Phi \phi$ Phi | $\Omega \omega$ Omega |



Figure 1.5. Pipe and pipe thread symbols (see table 1.6).

Table 1.6. Pipe-thread symbols (see fig. 1.5)

| Symbol | Dimension | Symbol | Dimension |
| :---: | :---: | :---: | :---: |
| D | Outside diameter of pipe. |  | Length from center line of soupling, face of |
| d | Inside diameter of pipe. |  | flange, or bottom of internsl thread chamber' |
| $t$ | Wall thickness of pipe. |  | to face of fitting. |
| $D_{x}$ | Major diameter. ${ }^{\text {d }}$ ( |  | Width of bearing face on coupling. |
| $E_{x}$ | Pitch diameter. See footnotes a and b | $\tau$ (tau) | Angle of chamfer at bottom of recess or counter- |
| $K_{x}$ | Minor diameter. |  | bore measured from the axis. |
|  | Length of thread from plane of pipe end to plane containing basic diameter $D_{x}, E_{x}$, or $K_{x}$. | $\begin{aligned} & \epsilon(\text { epsilon }) \\ & J \\ & \hline \end{aligned}$ | Half apex angle of vanish cone. <br> Length from center line of coupling, face of |
| $V$ | Length of vanish cone (washout) threads. |  | flange, or bottom of internal thread chamber |
| $\beta$ (beta) | Half apex angle of pitch cone of taper thread. |  | to end of pipe, wrenched engagement. |
| $\gamma$ (gamma) -- | Angle of chamfer at end of pipe measured from a plane normal to the axis. |  | (1) Length of straight full thread (see table 1.4). |
| A | Handtight standoff of face of coupling from a plane containing vanish point on pipe. |  | (2) Length from plane of handtight engagement to small end of full internal taper |
| M | Length from plane of handtight engagement to the face of coupling on internally threaded member. |  | thread. <br> Diameter of recess or counterbore in fitting. Depth of recess or counterbore in fitting. |
|  | Distance of gaging step of plug gage from face of ring gage for handtight engagement. Standoff. |  | Outside diameter of coupling or hab of fitting. |

${ }^{\text {a }}$ Subscript $x$ denotes plane containing the diameter. For axial positions of planes see below.
${ }^{5}$ Subscripts $s$ (for screw) or $n$ (for nut) designating external and internal threads, respectively, may also be used if necessary

## DEFINITIONS OF PLANES DENOTED BY SUBSCRIPT $x$

| $x=0$ |
| :--- |
| $x=1$ |


| Plane of pipe end. |
| :--- |
| $x=2$ |


| Plane of handtight engagement or plane at mouth of coupling (excluding recess, if present). |
| :--- |
| On British pipe threads this is designated the "gauge plane" and the major diameter in this plane is designated the |
| "gauge diameter." |


| Plane at which vanish threads on pipe commence. |
| :--- |

$x=4$

$x=5$ | Plane in coupling reached by end of pipe in wrenched condition. ( $L_{3}$ is measured from plane containing pipe end in |
| :--- |
| plane containing vanish point of thread on pipe. |

Table 1.7 ISO symbols

| Symbol | Dimension |
| :---: | :---: |
| $d$ | Basic major diameter of bolt thread. |
| $d_{2}$ | Basic pitch (effective) diameter of bolt thread. |
| $d_{1}$ | Basic minor diameter of bolt thread. |
| D | Basic major diameter of nut thread. |
| $D_{1}$ | Basic minor diameter of nut thread. |
| $D_{2}$ | Basic pitch (effective) diameter of nut thread. |
| $P$ | Pitch. |
|  | Number of threads per inch. |
| $R$. | Radius of root of bolt thread. |
| $\mathrm{H}_{1}$ | Depth of thread engagement. |
| $n_{\text {e }}$ | Number of threads in engagement. |
| S | Designation for thread engagement group Short. |
| $N$ | Desiguation for thread engagement group Normal. |
| $L$ | Designation for thread engagement group Long. |
| $T$ | Tolerance. |
| $\begin{gathered} T_{d}, T_{d 2}, T_{d 1} \\ T_{D 1}, T_{D 2} \end{gathered}$ | Tolerance for major diameter of bolt thread, for pitch (effective) diameter of bolt thread, etc. |
| $e i, E I$ | Lower deviation. |
| es, $E S$ | Upper deviation. |
|  | Allowance. |

Table 1.8. Thread series designations ${ }^{\text {a, }} \mathrm{b}$

${ }^{\text {a }}$ Methods of designating multiple threads are shown in USA B1.5, Acme screw threads, and Part III of Handbook H28.
${ }^{\text {b }}$ All threads, except NGO, are right hand unless otherwise designated. For NGO threads, designations "RH" or "LH" are required.

Table 1.8a. Designations for $U N, U N J, N, N R$ thread series

| Basic thread series | External thread root | $\underset{\text { pitch }}{\text { Constant }}$ | Coarse | Fine | Extra fine | Special diameters, pitches, or lengths of engagement | Reference |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  | United States of America (USA) Standard | H28 |
| UN | With optional radius root on external thread. | UN | UNC | UNF | UNEF | UNS | $\begin{aligned} & \text { B1.1 } \\ & \text { B1.1 } \end{aligned}$ | Section 2 <br> Section 3 |
| UNJ | With 0.15011 p to 0.18042 p mandatory radius root on external thread. | UNJ | UNJC | UNJF | UNJEF | UNJS |  | Section 4 |
| $\mathrm{Na}^{\mathbf{4}}$ |  | N | NC | NF | NEF | NS |  | Appendix A1 |
| NR |  | NR |  |  |  |  | M IL-B-7838 |  |

[^4]Table 1.9 Dimensional designations for use on drawings

| Designation | Dimension | Designation | $\because$. Dimension |
| :---: | :---: | :---: | :---: |
| CR | Crest radius. | RR | Root radius. |
| DR | Differential reading. | T | Tolerance. |
| FD | Functional diameter. | TGD | Thread groove diameter. |
| G | Allowance. | TGW | Thread groove width. |
| L | Lead. | TPI | Threads per inch. |
| ${ }_{\text {L }}$ | Length of thread engagement. | TRD | Thread ridge diameter. |
| $\mathrm{P} \mathbf{D}$ | Pitch diameter. | TRT | Thread ricge thickness. |

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# UNITED STATES DEPARTMENT OF COMMERCE <br> NATIONAL BUREAU OF STANDARDS 

# HANDBOOK H28 

## SCREW-THREAD STANDARDS

FOR FEDERAL SERVICES

SECTION 2
1969
UNIFIED THREAD FORM AND THREAD SERIES FOR BOLTS, SCREWS, NUTS, TAPPED HOLES, AND GENERAL APPLICATIONS

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## 1. INTRODUCTION

The Unified thread standards shown in this section are in agreement with International Standardization Organization (ISO) Recommendations:

R68 Screw Threads (That part dealing with the ISO Basic Thread Profile), and
R263 ISO Inch Screw Threads, General Plan and Selection for Screws, Bolts, and Nuts (diameter range 0.06 to 6 inch).
This section is in general agreement with United States of America Standard USA B1.1, Unified Screw Threads, published by The American Society of Mechanical Engineers, 345 East 47th Street, New York, N.Y. 10017; also with CSA B1.1, Standard for Unified and American Screw Threads, published by the Canadian Standards Association, Ottawa, Canada; and with British Standard 1580, Unified Screw Threads, published by the British Standards Institution, 2 Park Street, London, W.1. The latest revision should be consulted when referring to such standards. As of date of issue of this section of H28, USA B1.1-1960 is the latest revision of B1.1.

The Unified screw thread standards shown in this section constitute the basic thread standards used in the United States for the screw threads used on threaded fasteners. Unified screw threads are a complete and integrated system of threads for fastening purposes in mechanisms and structures. Their outstanding characteristic is general interchangeability of threads achievcd through the standardization of thread form, diameter-pitch combinations, and limits of size.

The standards have as their original basis the work done about a century ago by William Sellers in the United States and Sir Joseph Whitworth in Great Britain. Throughout the intervening years there have been many further developments and revisions, culminating in the system of Unified Threads approved and adopted for use by all inch-using countries.

Unification of screw thread standards received its impetus from the need for interchangeability among the billions of fasteners used in the complex equipment of modern warfare which equipment was, and continues to be, made in different countries. Equally important, however, are international trade in mechanisms of all kinds and the servicing of transportation equipment which moves from country to country. These have made unification not only highly advantageous but practically essential.

Unified screw threads had their origin in an Accord signed at Washington, D.C., on November 18, 1948, by representatives of Standardizing Bodies of Canada, the United Kingdom, and the United States. The Unified standard threads generally supersede the American standard threads. Threads are classed as Unified if they have the basic Unified thread form and have limits of size and tolerances based on the Unified formulations. Such threads are identified by the letter combination "UN" in the thread symbol.

In relation to previous American practice, Unified threads have substantially the same thread form and are mechanically interchangeable with American National threads of the same diameter and pitch.

The principal differences between the two systems relate to the application of allowances, the variation of tolerances with sizc, difference in amount of pitch diameter tolerance on external and internal threads, and differences in thread designations. Under the Unified system, an allowance is provided on both the classes 1A and 2A external threads, whereas under the American National system only the class 1 external thread has an allowancc. Under the Unified system, the pitch diameter tolerance of an internal thread is 30 percent greater than that of the external thread, but such tolerances are equal under the American National system. Since the tolerances differ, the letter " A " is used in the thread symbol to denote an external thread and the letter " B " is used to denote an internal thread. Unified tolerances and allowances for both standard and special diameter-pitch combinations are derived from the same formula, but American National tolerances for special threads have a different basis from that for some standard threads.

## 2. UNIFIED THREAD FORM

2.1. Basic Thread Form.--The Unified thread form is the basis of all thread dimensions given in this section. The formulas for its proportions are given in table 2.1, together with figure 2.2, showing the basic profile from which the design forms are derived. Both the ISO basic profile and the American (U.S.) concept of the basic Unified thread form are shown. These are essentially alike except that in the second illustration the position of the basic minor diameter provides for the long established practice in the U . S. of considering 100 percent thread height as being cqual to 0.75 H measured from the basic major diameter.
2.1(a) Angle of thread.-The basic angle of thread between the flanks of the thread, measured in an axial plane, is $60^{\circ}$. The line bisecting this $60^{\circ}$ angle is perpendicular to the axis of the screw thread.
2.1(b) Form of crest. - The form of the crest of external threads is flat. The crest of the basic thread form of the external thread shall be truncated from the sharp crest an amount equal to $0.125 H$, where $H$ is the depth of the fundamental triangle. The form of the crest of internal threads is flat and the crest shall be truncated from the sharp crest an amount equal to 0.25 H .
2.1(c) Rounded root forms.-The crest clearances allowed are such as to permit rounded root forms in both the external and internal threads. Rounded roots are required in some applications and are made by tools that are purposely rounded. Otherwise, rounded roots may be the result of tool wear.
2.1(d) Clearance at minor diameter.-A clearance is provided at the minor diameter of the internal thread by truncating from the sharp crest an amount equal to 0.25 H .
Table 2.1. Thread data, Unified thread form (see fig. 2.4.)

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline Threads per inch, \& Pitch,

$p=1 / n$ \& Flat at internal thread crest,

$$
\begin{aligned}
& F_{c n}= \\
& p / 4= \\
& 0.25 / n
\end{aligned}
$$ \& Flat at internal thread root and

external thread $\stackrel{\text { crest, }}{F_{r n}}=$ $r_{c s}=$
$F_{c s}=$ $p / 8=$ $0.125 / n$ \& Height of sharp v-thread,

$$
H=
$$

$$
.8660254 / n
$$ \& Twice min truncation of internal thread root,

$$
\begin{gathered}
2 f_{r n}= \\
H / 12= \\
0.0721688 / n
\end{gathered}
$$ \& Max truncation of internal thread root and external thread crest, $f_{r n}=$ $f_{c s}=$ $H / 8=$ $0.108253 / n$ \& Truncation of exterual thread rounded root,

$$
\begin{gathered}
s_{r s}= \\
H / 6= \\
0.144338 / n
\end{gathered}
$$ \& Half

addendum
of external

thread, \& | Addendum of internal thread and truncation of intcinal thread crest, $h_{a n}=$ $f_{c n}=$ |
| :--- |
| $H / 4=$ |
| $0.216506 / n$ | \& Dedendum of internal thread and addendum of external thread,

$$
\begin{aligned}
& h_{d n}= \\
& h_{a s}=
\end{aligned}
$$

$$
3 H / 8=
$$

$$
0.324759 / n
$$ \& Height of internal thread and depth of thread engagement,

\[
$$
\begin{gathered}
h_{n}= \\
h_{e}= \\
5 H / 8= \\
0.541266 / n
\end{gathered}
$$

\] \& | ifeight of external thread and max height of internal thread, |
| :--- |
| $h_{s}=$ $17 \mathrm{H} / 24=$ $0.613435 / n$ | \& | ${ }^{(a)}$ |
| :--- |
| Twice the external thread addendum, $\begin{gathered} h_{b}= \\ 2 h_{\text {as }}= \\ 3 H / 4= \\ 0.649519 / n \end{gathered}$ | \& Thread

height
from basic
flat crest
to sharp
root, \& Difference between max major and pitch diameters of internal thread,

$$
\begin{aligned}
& 11 \mathrm{H} / 12= \\
& 0.793857 / n
\end{aligned}
$$ \& Double height of internal thread,

$$
\begin{gathered}
2 h_{n}= \\
5 H / 4= \\
1.082532 / n
\end{gathered}
$$ \& Double height of external thread,

$$
\begin{aligned}
& 17 \mathrm{H} / 12= \\
& 1.226868 / n
\end{aligned}
$$ <br>

\hline 1 \& 2 \& 3 \& 4 \& 5 \& 6 \& 7 \& 8 \& 9 \& 10 \& 11 \& 12 \& 13 \& 14 \& 15 \& 16 \& 17 \& 18 <br>

\hline \& $$
\underset{i n}{i n}
$$ \& \[

\stackrel{i n}{0.00312}
\] \& ${ }_{\text {in }}^{\text {in }}$ \& ${ }_{\text {in }}^{\text {in }}$ \& in ${ }^{\text {in }}$ \& in \& in \& in \& in \& in \& in \& in \& in \& in \& in \& in \& in <br>

\hline 72 \& . 013889 \& . 00347 \& . 00174 \& . 012028 \& . 00100 \& . 00150 \& . 00200 \& -0.0226 \& ${ }^{0.00301}$ \& . 00451 \& 0.000752 \& 0.00767 \& 0.008192 \& 0.00947 \& . 01103 \& . 01504 \& 0.01534 <br>
\hline 64 \& . 0156250 \& . 00391 \& . $00195+$ \& . 013532 \& . 00113 \& . 00169 \& . 00226 \& . 00254 \& . 00338 \& . 00507 \& . 00846 \& . 00958 \& . 010149 \& . 01184 \& . 01240 \& . 01691 \& . 01917 <br>
\hline 56 \& . 017857 \& . 00446 \& . 00223 \& .015465- \& . 00129 \& . 00193 \& . 00258 \& . 00290 \& . 00387 \& . 00580 \& . 00967 \& .01095+ \& . 011599 \& . 01353 \& . 01418 \& . 01933 \& . 02191 <br>
\hline 48 \& . 020833 \& . 00521 \& . 00260 \& . 018042 \& . 00150 \& . 00226 \& . 00301 \& . 00338 \& . 00451 \& . 00677 \& . 01128 \& . 01278 \& . 013532 \& . 01579 \& . 01654 \& . $02255+$ \& . 02556 <br>
\hline 44 \& . 022727 \& . 00568 \& . 00284 \& . 019682 \& . 00164 \& . 00246 \& . 00328 \& . 00369 \& . 00492 \& . 00738 \& . 01230 \& . 01394 \& . 014762 \& . 01722 \& . 01804 \& . 02460 \& . 02788 <br>
\hline 40 \& . 025000 \& . 006250 \& . 00312 \& . 021651 \& . 00180 \& . 00271 \& . 00361 \& . 00406 \& . 00541 \& . 00812 \& . 01353 \& . 01534 \& . 016238 \& . 01894 \& . $01985-$ \& . 02706 \& . 03067 <br>
\hline 36 \& . 027778 \& . 006694 \& . 00347 \& . 024056 \& . 00200 \& . 00301 \& . 00401 \& . 00451 \& . 00601 \& . 00902 \& . 01504 \& . 01704 \& . 018042 \& . $02105-$ \& . $02205+$ \& . 03007 \& . 034108 <br>
\hline 32 \& . 031250 \& . 00781 \& . 00391 \& . 027063 \& . 00226 \& . 00338 \& . 00451 \& . 00507 \& . 00677 \& .01015- \& . 01691 \& . 01917 \& . 020297 \& . 02368 \& . 02481 \& . 03383 \& . 03834 <br>
\hline 28 \& . 035714 \& . 00893 \& . 00446 \& . 030929 \& . 00258 \& ,00387 \& . $00515+$ \& . 00580 \& . 00773 \& . 01160 \& . 01933 \& . 02191 \& . 023197 \& . 02706 \& . $02835+$ \& . 03866 \& . 04382 <br>
\hline 27 \& . 037037 \& . 00926 \& . 00463 \& $.032075+$ \& . 00267 \& . 00401 \& .00535- \& . 00601 \& . 00802 \& . 01203 \& .02005- \& . 02272 \& . 024056 \& . 02807 \& . 02940 \& . 04009 \& . 04544 <br>
\hline 24 \& . 041667 \& . 01042 \& . 00521 \& . 036084 \& . 00301 \& . 00451 \& . 00601 \& . 00677 \& . 00902 \& . 01353 \& . $02255+$ \& . 02556 \& . 027063 \& . 03157 \& . 03308 \& . 04511 \& . 05112 <br>
\hline 20 \& . 050000 \& . 01250 \& . 006250 \& . 043301 \& . 00361 \& . 00541 \& . 00722 \& . 00812 \& . 01083 \& . 01624 \& . 02706 \& . 03067 \& . 032476 \& . 03789 \& . 03969 \& . 05413 \& . 06134 <br>
\hline 18 \& . 055556 \& . 01389 \& . 00694 \& . 048113 \& . 00401 \& . 00601 \& . 00802 \& . 00902 \& . 01203 \& . 01804 \& . 03007 \& . 03408 \& . 036084 \& . 04210 \& . 04410 \& . 06014 \& . 06816 <br>
\hline 16 \& . 062500 \& . 01562 \& . 00781 \& . 054127 \& . 00451 \& . 00677 \& . 00902 \& .01015- \& . 01353 \& . 02030 \& . 03383 \& . 03834 \& .040595- \& . 04736 \& . 04962 \& . 06766 \& . 07668 <br>
\hline 14 \& . 071429 \& . 01786 \& . 00893 \& . 061859 \& . $00515+$ \& . 00773 \& . 01031 \& . 01160 \& . 01546 \& . 02320 \& . 03866 \& . 04382 \& . 046394 \& . 05413 \& . 05670 \& . 07732 \& . 08763 <br>
\hline 13 \& . 076923 \& . 01923 \& . 00962 \& . 0666617 \& . $00555+$ \& . 00833 \& . 01110 \& . 01249 \& . $01665+$ \& . 02498 \& . 04164 \& . 04719 \& . 049963 \& . 05829 \& . 06107 \& . 08327 \& . 09437 <br>
\hline 12 \& . 083333 \& . 02083 \& . 01042 \& . 072169 \& . 00601 \& . 00902 \& . 01203 \& . 01353 \& . 01804 \& . 02706 \& . 04511 \& . 05112 \& . 054127 \& .06315- \& . $06615+$ \& . 09021 \& . 10224 <br>
\hline 11.5 \& . 086957 \& . 02174 \& . 01087 \& . 075307 \& . 00628 \& . 00941 \& .01255+ \& . 01412 \& . 01883 \& . 02824 \& . 04707 \& . 05334 \& . 056480 \& . 06589 \& . 06903 \& . 09413 \& . 10668 <br>
\hline 11 \& . 090909 \& . 02273 \& . 01136 \& . 078730 \& . 00656 \& . 00984 \& . 01312 \& . 01476 \& . 01968 \& . 02952 \& . 04921 \& . 05577 \& . 059047 \& . 06889 \& . 07217 \& . 09841 \& . 11153 <br>
\hline 10 \& . 100000 \& . 02500 \& . 01250 \& . 086603 \& . 00722 \& . 01083 \& . 01443 \& . 01624 \& .02165+ \& . 03248 \& . 05413 \& . 06134 \& . 064952 \& . 07578 \& . 07939 \& .10825+ \& . 12269 <br>
\hline 9 \& . 111111 \& . 02778 \& .01389 \& . $096225+$ \& . 00802 \& . 01203 \& . 01604 \& . 01804 \& . 02406 \& . 03608 \& . 06014 \& . 06816 \& . 072169 \& . 08420 \& . 08821 \& . 12028 \& . 13632 <br>
\hline 8 \& .125000 \& . 031250 \& . 01568 \& . 108253 \& . 00902 \& . 01353 \& . 01804 \& . 02030 \& . 02706 \& . 04059 \& . 06766 \& . 07668 \& .081190 \& . 09472 \& . 09923 \& . 13532 \& . 15336 <br>
\hline 7 \& . 142857 \& . 03571 \& . 01788 \& . 123718 \& . 01031 \& . 01546 \& . 02062 \& . 02320 \& . 03093 \& . 04639 \& . 07732 \& . 08763 \& . 092788 \& . $10825+$ \& . 11341 \& .15465- \& . 17527 <br>
\hline 6 \& . 166667 \& . 04167 \& . 02083 \& . 144338 \& . 01203 \& . 01804 \& . 02406 \& . 02706 \& . 03608 \& . 05413 \& . 09021 \& . 10224 \& . 108253 \& . 12630 \& . 13231 \& . 18042 \& . 20448 <br>
\hline 5 \& . 200000 \& . 05000 \& . 02500 \& $.173205+$ \& . 01443 \& . $02165+$ \& . 02887 \& . 03248 \& . 04330 \& . $06495+$ \& . $10825+$ \& . 12269 \& . 129904 \& . $15155+$ \& . 15877 \& . 21651 \& . 24537 <br>
\hline 4.5 \& . 222222 \& . 05555 \& . 02778 \& . 192450 \& . 01604 \& . 02406 \& . 03208 \& . 03608 \& . 04811 \& . 07217 \& . 12028 \& . 13632 \& . 144338 \& . 16839 \& . 17641 \& . 24056 \& . 27264 <br>
\hline 4 \& . 250000 \& . 06250 \& . 031250 \& . 216506 \& . 01804 \& . 02706 \& . 03608 \& . 04059 \& . 05413 \& . 08119 \& . 13532 \& . 15336 \& . 162380 \& . 18944 \& . 19846 \& . 27063 \& . 30672 <br>
\hline
\end{tabular}

${ }^{\text {a }}$ This is taken as 100 percent thread height and is now known as a symmetrical thread form. It is equivalent to the "basic height" $h$ of the original American National form.


Figure 2.2. Basic unified thread form; ISO basic profile and American (U.S.) symmetrical thread form.
2.1(e) Clearance at major diameter.-A clearance is provided at the major diameter of the internal thread by making the thread form at the root such that its width is less than $0.125 p$.
2.2. Design Form Of External Thread.-The design form for an external Unified thread, i.e., the form of an external thread in its maximum material condition, shown in figure 2.3, is derived from the fundamental triangle. It is truncated at the major diameter to 0.125 H . In practice, due to providing for tool crest wear at the thread roots, i.e., the minor diameter, the roots are shown as a rounded contour and cleared beyond the flat width of $0.25 p$ for the minimum minor diameter of the internal thread. Also, in practice, the crests of the external threads may be rounded within the confines established by the major diameter tolerance.
2.3. Design Form Of Internal Thread.-The design form for an internal Unified thread, i.e., the form of an internal thread in its maximum material condition, shown in figure 2.3, is derived from the fundamental triangle. It is similar to the basic form except that the truncation at the minor diameter is an amount equal to one-quarter of the fundamental triangle height ( $0.25 H$ ). In practice, due to providing for tool crest wear at the thread roots, i.e., the major diameter, the roots are shown as a rounded contour and cleared beyond the flat width of $0.125 p$ for the maximum major diameter of the internal thread.
2.4. Basic Thread Data.-The basic thread data for all standard pitches of the Unified form of thread are given in table 2.1.

## 3. THREAD SERIES, ORDER OF SELECTION, AND SUGGESTED APPLICATIONS

### 3.1. Thread Series Definition.-Thread series

 are groups of diameter-pitch combinations distinguished from each other by the number of threads per inch applied to series of specific diameters. The various diameter-pitch combinations of three series with graded pitches and 8 series with constant pitches are given in table 2.7, p. 2.08. The symbols for designating the various thread series are shown in table 2.7. In table 2.21, p. 2.26, the limits of size of the series in table 2.7 are given but the full range is not covered in the case of the $4 \mathrm{UN}, 6 \mathrm{UN}$, and 8UN series. (See par. 11 Limits of Size, p. 2.25.)3.2. Order Of Selection.-Whenever possible, selection should be made from table 2.21, p. 2.26, Standard series limits of size-Unified screw threads, preference being given to the coarse-thread and fine-thread series. If threads in the standard series do not meet the requirements of design, reference should be made to the selected combinations in table 3.1. The third expedient is to compute the limits of size for a special diameter-pitch combination in accordance with table 3.11. The fourth and last resort is calculation by the formulas in section 3.
3.3. UNC, Coarse-Thread Series.-This series is generally utilized for the bulk production of bolts, screws, nuts, and other general engineering applications. It is used in general applications for threading into lower tensile strength materials such as cast iron, mild steel, and softer materials to obtain the optimum resistance to stripping of the internal


Figure 2.3. Unified internal and external screw thread design forms (maximum material condition).
NOTE: See table 2.1 for numerical values. In practice the crests of external threads may be rounded.
thread. It is applicable for rapid assembly or disassembly, or if corrosion or slight damage is possible. The basic dimensions and limits of size for this series are shown in tables 2.8 and 2.21.
3.4. UNF, Fine-Thread Series.-This series is suitable for the production of bolts, screws, nuts, and other applications where the coarse series is not applicable. External threads of this series have greater tensile stress area than comparable sizes of the coarse series. The fine series is suitable when the resistance to stripping of both external and mating internal threads equals or exceeds the tensile load carrying capacity of the externally threaded
member. It is also used where the length of engagement is short, where a smaller lead angle is desired, or where the wall thickness demands a fine pitch. It may also be used for threading into lower strength materials where maximum strength of the external thread is not required, otherwise, the length of engagement must be selected to meet the above required strength conditions.

Fine threads up to and including 1 in size are suitable for screw, bolt, and nut, and other threaded fastener applications. Sizes over 1 in may not be suitable unless the mating materials are compatible as outlined above. The basic dimensions and limits of


Figure 2.4. Symbols for thread data in table 2.1.
size for this series are shown in tables 2.9 and 2.21 .
3.5. UNEF, Extra-Fine Thread Series.-This series is applicable where even finer pitches of threads are desirable for short lengths of engagement and for thin-walled tubes, nuts, ferrules, or couplings. It is also generally applicable under the conditions stated above for the fine threads. The basic dimensions and limits of size for this series are shown in tables 2.10 and 2.21 .
3.6. UN, Constant Pitch Series.-The various constant-pitch series with $4,6,8,12,16,20,28$, and 32 threads per inch, given in table 2.7, offer a comprehensive range of diameter-pitch combinations for those purposes where the threads in the UNC, UNF, and UNEF series do not meet the particular requirements of the design. The constant pitch series have application on parts that are repeatedly as-
sembled and disassembled or where it might be advantageous to rethread oversize to recondition the threaded portions of the parts. Whenever a thread in a constant-pitch series also appears in the UNC, UNF, or UNEF series, the symbols, tolerances, and limits of size of those standard series are applicable. When selecting threads from these constant-pitch series, preference should be given whenever possible to those tabulated in the 8-, 12-, or 16 -thread series. The basic dimensions for the $4-$, 6 -, 20-, 28 -, and 32 -thread series are shown in tables 2.11, 2.12, 2.16, 2.17, and 2.18.
3.6 (a) $8 U N, 8$-thread series.-The 8UN series is a uniform-pitch series for large diameters or for use as a compromise between the coarse- and finethread series. Although originally intended for high-pressure-joint bolts and nuts, it is now widely used as a substitute for the coarse-thread series for diameters larger than 1 in . The basic dimensions for this series are shown in table 2.13 .
3.6(b) 12UN, 12-thread series.-The 12UN series is a uniform-pitch series for large diameters requiring threads of medium-fine pitch. Although originally intended for boiler practice, it is now used as a continuation of the fine-thread series for diameters larger than 1.5 in . The basic dimensions for this series are shown in table 2.14.
3.6(c) $16 U N, 16$-thread series.-The 16 UN series is a uniform-pitch series for large diameters requiring fine-pitch threads. It is suitable for adjusting collars and retaining nuts, and also serves as a continutation of the extra-fine-thread series for diameters larger than 1.6875 in. The basic dimensions for this series are shown in table 2.15 .
3.7. High-Temperature, High-Strength Ap-plications.-For these applications the coarsethread series is recommended in sizes from 0.25 to 1 in and the 8 -thread series in sizes over 1 in . Limits of size are given in table 2.21. Some high-temperature applications involving special physical characteristics or conditions may require modification of thread dimensions. See italicized part in par. 4.2, p. 2.19, and par. 10.5, p. 2.24.
3.8. Selected Combinations of UNS Threads. -These data are tabulated in table 3.1 for some selected combinations of diameter and pitch of Unified special screw threads, designated UNS, with pitch diameter tolerances based on a length of thread engagement of 9 times the pitch. The pitch diameter limits are applicable to a length of engagement of from 5 to 15 times the pitch. (This should not be confused with the length of thread on mating parts, as it may exceed the length of engagement by a considerable amount.)
3.9. Fine Threads for Thin-Wall Tubing.The limits of size for a 27 -thread series, ranging from 0.25 to 1 in nominal size, are included in table 3.1. These threads are recommended for general use on thin-wall tubing. For more detailed information see part II of Handbook H28.
3.10. Threads Of Special Diameters, Pitches, And Lengths Of Engagement.-For information on special threads, see section 3.


Figure 2.5. Disposition of tolerances, allowances, and crests clearances for classes 1A, 2A, 1B, and 2B.
NOTE: "Nominal minor diameter of external thread" is that specified in tables.


Figure 2.6. Disposition of tolerances and crest clearances for classes $3 A$ and $3 B$.
NOTE: "Nominal minor diameter of external thread" is that specified in tables.

Table 2.7. Unified standard screw thread series

| Nominal size and basic major diameter |  | Threads per inch |  |  |  |  |  |  |  |  |  |  | Nominal size and basic major diameter |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Series with graded pitches |  |  | Series with constant pitches |  |  |  |  |  |  |  |  |
| Primary | Secondary | Coarse UNC | $\begin{aligned} & \text { Fine } \\ & \text { UNF } \end{aligned}$ | $\begin{aligned} & \text { Extra fine } \\ & \text { UNEF } \end{aligned}$ | 4UN | 6UN | 8UN | 12UN | 16UN | 20UN | 28 UN | 32 UN |  |
| in <br> . 060 | in |  | 80 |  |  |  |  |  |  |  |  |  | in .060 |
| . 086 | . 073 | 64 56 | 72 | -------- |  |  |  |  |  |  |  |  | . 073 |
|  | . 099 | 48 | 56 |  |  |  |  |  |  |  |  |  | . 099 |
| . 112 |  | 40 | 48 |  |  |  |  |  |  |  |  |  | . 112 |
| . 125 |  | 40 | 44 |  |  |  |  |  |  |  |  |  | . 125 |
| . 138 |  | 32 32 | 40 36 |  |  |  |  |  |  |  |  | UNC | .138 .164 |
| . 190 |  | 24 | 32 |  |  |  |  |  |  |  |  | UNF | . 190 |
|  | .216 | 24 | 28 | 32 |  |  |  |  |  |  | UNF | UNEF | . 216 |
| .250 | ---------- | 20 | 28 | 32 |  |  |  |  |  | UNC | UNF | UNEF | .250 |
| . 375 |  | 18 16 | $\stackrel{24}{24}$ | 32 |  |  |  |  | UNC̄ | 20 20 | $\xrightarrow{28}$ | UNEF | . 3125 |
| . 4375 |  | 14 | 20 | 28 |  |  |  |  | 16 | UNF | UNEF | 32 | . 4375 |
| .500 .5625 |  | 13 | 20 18 | 28 |  |  |  |  | 16 | UNF | UNEF | 32 | . 500 |
| . 625 |  | 11 | 18 | 24 |  |  |  | 12 | 16 | 20 | 28 | 32 | . 625 |
|  | . 6875 |  |  | 24 |  |  |  | 12 | 16 | 20 | 28 | 32 | . 6875 |
| . 750 |  | 10 | 16 | 20 |  |  |  | 12 | UNF | UNEF | 28 | 32 | . 750 |
|  | . 8125 |  |  | 20 |  |  |  | 12 | 16 | UNEF | 28 | 32 | . 8125 |
| . 875 |  | 9 | 14 | 20 |  |  |  | 12 | 16 | UNEF | $\stackrel{28}{ }$ | 32 | . 875 |
|  | . 9375 |  |  | 20 |  |  |  | 12 | 16 | UNEF | 28 | 32 | . 9375 |
| 1.000 | 1.0625 | 8 | 12 | 20 18 |  |  | UNC | UNF | 16 16 | ${ }_{20}^{\text {UNEF }}$ | 28 28 | 32 | 1.000 1.0625 |
| 1.125 |  | 7 | 12 | 18 |  |  | 8 | UNF | 16 | 20 | 28 |  | 1.125 |
|  | 1.1875 |  |  | 18 |  |  | 8 | 12 | 16 | 20 | 28 |  | 1.1875 |
| 1.250 |  | 7 | 12 | 18 |  |  | 8 | UNF | 16 | 20 | 28 |  | 1.250 |
|  | 1.3125 |  |  | 18 |  |  | 8 | 12 | 16 | 20 | 28 |  | 1.3125 |
| 1.375 | ---7.4375 | 6 | 12 | 18 18 |  | UNC | 8 | UNF | 16 16 | 20 20 | 28 28 | ------ | 1.375 1.4375 |
| 1.500 |  | 6 | 12 | 18 |  | UNC | 8 | UNF | 16 | 20 | 28 |  | 1.500 |
| 1.625 | 1.5625 |  |  | 18 |  | 6 | 8 | 12 | 16 | 20 |  |  | 1.5625 |
| 1.625 | 1.6875 |  |  | 18 |  | 6 | 8 | 12 | 16 | 20 |  |  | 1.6875 |
| 1.750 |  | 5 |  |  |  | 6 | 8 | 12 | 16 | 20 | ----- |  | 1.750 |
|  | 1.8125 | ------- | --- | ------ |  | 6 | 8 | 12 | 16 | 20 |  |  | 1.8125 |
| 1.875 | 1.9375 |  |  |  |  | 6 | 8 | 12 12 | 16 16 | 20 20 |  |  | 1.875 1.9375 |
| 2.000 |  | 4.5 |  |  |  | 6 | 8 | 12 | 16 | 20 |  |  | 2.000 |
|  | 2.125 |  |  |  |  | 6 | 8 | 12 | 16 | 20 |  |  | 2.125 |
| 2.250 | -----375-- | 4.5 |  |  |  | 6 | 8 | 12 | 16 16 | 20 20 | ---- |  | 2.250 2.375 |
| 2.500 |  | 4 |  |  | UNC | 6 | 8 | 12 | 16 | 20 | ---10 |  | 2.500 |
|  | 2.625 |  |  |  | $\stackrel{4}{4}$ | 6 | 8 | 12 | 16 | 20 |  |  | 2.625 |
| 2.750 | -----875-- | 4 |  |  | ${ }_{4}^{\text {UNC }}$ | 6 6 | 8 | 12 | 16 16 | 20 20 |  |  | 2.750 2.875 |
| 3.000 |  | 4 |  |  | UNC | 6 | 8 | 12 | 16 | 20 |  |  | 3.000 |
| 3.250 |  | 4 |  |  | $\stackrel{4}{4}$ | 6 6 | 8 | 12 | 16 16 | ----- |  |  | 3.125 |
|  | 3.375 |  |  |  | 4 | 6 | 8 | 12 | 16 | - |  |  | 3.375 |
| 3.500 |  | 4 |  |  | UNC | 6 | 8 | 12 | 16 | ------ |  |  | 3.500 |
|  | 3.625 |  |  |  | 4 | 6 | 8 | 12 | 16 | ------ |  |  | 3.625 |
| 3.750 | -----8.--- | 4 |  |  | UNC | 6 6 | 8 | 12 | 16 | - |  |  | 3.750 |
| 4.000 |  | 4 |  |  | UNC | 6 | 8 |  |  |  |  |  |  |
|  | 4.125 |  |  |  | 4 | 6 | 8 | 12 | 16 | -------- |  |  | 4.125 |
| 4.250 |  | ------- |  |  | 4 | 6 | 8 | 12 | 16 | - |  |  | 4.250 |
|  | 4.375 |  |  |  | 4 | 6 | 8 | 12 | 16 |  |  |  | 4.375 |
| 4.500 |  |  |  |  | 4 | 6 | 8 | 12 | 16 |  |  |  |  |
|  | 4.625 |  |  |  | 4 | 6 | 8 | 12 | 16 |  |  |  | 4.625 |
| 4.750 | 4.875 |  |  |  | 4 | 6 | 8 | 12 | 16 |  |  |  | 4.750 |
|  |  |  |  |  |  |  |  |  | 1 |  | --- | ---- | 4.875 |
| 5.000 |  |  |  |  | 4 | 6 | 8 | 12 | 16 |  |  |  |  |
| 5.250 | 5.125 | ------- |  |  | 4 | 6 | 8 | 12 | 16 |  |  |  | 5.125 |
|  | 5.375-- |  |  |  | 4 | 6 | 8 | 12 | 16 | ---- |  |  | 5.250 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5.500 |  |  |  |  | 4 | 6 | 8 | 12 | 16 |  |  |  |  |
| 5.750 | 5.625 |  |  |  |  | 6 | 8 | 12 | 16 |  |  |  | 5.625 |
|  | 5.875 |  |  |  | 4 | 6 | 8 | 12 | 16 | - |  |  | 5.750 |
| 6.000 |  |  |  |  | 4 | 6 | 8 | 12 | 16 16 |  |  |  | 5.875 |
|  |  |  |  |  |  |  |  |  |  |  |  |  | 6.000 |

Table 2.8. Coarse thread series, basic dimensions, UNC

| Nominal size and basic major diameter, $D$ |  | Threads per inch, $n$ | Basic pitch diameter, E | Minora diameter, external threads, $K_{s}$ | Minor ${ }^{\text {a }}$ diameter, internal threads, $K_{n}$ |  | Lead angle at basic pitch diameter, $\lambda$ | Sectional area at minor diameter at $D-2 h_{b}$ | Tensile stressb$\pi\left(\frac{E}{2}-\frac{3 H}{16}\right)^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Primary | Secondary |  |  |  |  |  |  |  |  |
| in | in |  | in | in | in | deg | $\min$ | $i n^{2}$ | in ${ }^{2}$ |
|  | . 073 | 64 | 0.0629 | 0.0538 | 0.0561 | 4 | 31 | 0.00218 | 0.00263 |
| . 086 |  | 56 | . 0744 | . 0641 | . 0667 | 4 | 22 | . 00310 | . 00370 |
|  | . 099 | 48 | . 0855 | . 0734 | . 0764 | 4 | 26 | . 00406 | . 00487 |
| . 112 |  | 40 | . 0958 | . 0813 | . 0849 | 4 | 45 | . 00496 | . 00604 |
| . 125 |  | 40 | . 1088 | . 0943 | . 0979 | 4 | 11 | . 00672 | . 00796 |
| . 138 |  | 32 | . 1177 | . 0997 | . 1042 |  | 50 | . 00745 | . 00909 |
| . 164 |  | 32 | . 1437 | . 1257 | . 1302 | 3 | 58 | . 01126 | . 0140 |
| . 190 |  | 24 | . 1829 | . 1389 | . 1449 | 4 | 39 | . 01450 | . 0175 |
|  | . 216 | 24 | . 1889 | . 1649 | . 1709 | 4 | 1 | . 0206 | . 0242 |
| . 250 |  | 20 | . 2175 | . 1887 | . 1959 | 4 | 11 | . 0269 | . 0318 |
| . 3125 |  | 18 | . 2764 | . 2443 | . 2524 | 3 | 40 | . 0454 | . 0524 |
| .375 .4375 |  | 116 | . 33344 | . 24983 | . 38073 | 3 | 24 20 | . 06778 | . 0775 |
| . 4375 |  | 14 | . 3911 | . 3499 | . 3802 | 3 | 20 | . 0933 | . 1063 |
| . 500 |  | 13 | . 4500 | . 4056 | . 4167 | 3 | 7 | . 1257 | . 1419 |
| . 5625 |  | 12 | . 5084 | . 4603 | . 4723 | 2 | 59 | . 162 | . 182 |
| . 625 |  | 11 | . 5660 | . 5135 | . 5266 | 2 | 56 | . 202 | . 226 |
| . 875 |  | 9 | . 8028 | . 7387 | . 7547 | 2 | 31 | . 419 | . 462 |
| 1.000 |  | 8 | . 9188 | . 8466 | . 8647 | 2 | 29 | . 551 | . 606 |
| 1.125 |  | 7 | 1.0322 | . 9497 | . 9704 | 2 | 31 | . 693 | . 763 |
| 1.250 |  | 7 | 1.1572 | 1.0747 | 1.0954 | 2 | 15 | . 890 | . 969 |
| 1.375 |  | 6 | 1.2667 | 1.1705 | 1.1946 | 2 | 24 | 1.054 | 1.155 |
| 1.500 | ---------- | 6 | 1.3917 | 1.2955 | 1.3196 | 2 | 11 | 1.294 | 1.405 |
| 1.750 |  | 5 | 1.6201 | 1.5046 | 1.5335 | 2 | 15 | 1.74 | 1.90 |
| 2.000 |  | 4.5 | 1.8557 | 1.7274 | 1.7594 | 2 | 11 | 2.30 | 2.50 |
| 2.250 |  | 4.5 | 2.1057 | 1.9774 | 2.0094 | 1 | 55 | 3.02 | 3.25 |
| 2.500 |  | 4 | 2.3376 | 2.1933 | 2.2294 | 1 | 57 | 3.72 | 4.00 |
| 2.750 |  | 4 | 2.5876 | 2.4433 | 2.4794 | 1 | 46 | 4.62 | 4.93 |
| 3.000 |  | 4 | 2.8376 | 2.6933 | 2.7294 | 1 | 36 | 5.62 | 5.97 |
| 3.250 |  | 4 | 3.0876 | 2.9433 | 2.9794 | 1 | 29 | 6.72 | 7.10 |
| 3.500 |  | 4 | 3.3376 | 3.1933 | 3.2294 | 1 | 22 | 7.92 | 8.33 |
| 3.750 |  | 4 | 3.5876 | 3.4433 | 3.4794 | 1 | 16 | 9.21 | 9.66 |
| 4.000 |  | 4 | 3.8376 | 3.6933 | 3.7294 | 1 | 11 | 10.61 | 11.08 |

${ }^{\text {a }}$ Design form. See fig. 2.3.
${ }^{\mathrm{b}}$ See formula under definition of tensile stress area in appendix A5.

Table 2.9. Fine thread series, basic dimensions, UNF


[^5]Table 2.10. Extra-fine thread series, basic dimensions, UNEF

| Nominal sizea and basic major diameter, $D$ |  | Threads per inch, n | Basic pitch diameter, E | Minor ${ }^{\text {b }}$ diameter, external threads, $K_{s}$ | Minorb diameter, internal threads, $K_{n}$ |  | Lead angle at basic pitch diameter, $\lambda$ | Sectional area at minor diameter at $D-2 h_{b}$ | $\begin{gathered} \text { Tensile stresso } \\ \text { area, } \\ \pi\left(\frac{E}{2}-\frac{3 H}{16}\right)^{2} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Primary | Secondary |  |  |  |  |  |  |  |  |
| in | in |  | in | in | in | deg | min | $i n^{2}$ | $i{ }^{2}$ |
|  | . 216 | 32 | 0.1957 | 0.1777 | 0.1822 | 2 | 55 | 0.0242 | 0.0270 |
| . 250 |  | 32 | . 2297 | . 2117 | . 2162 | 2 | 29 | . 0344 | . 0379 |
| . 3125 |  | 32 | . 2922 | . 2742 | . 2787 | 1 | $\stackrel{57}{ }$ | . 0581 | . 0625 |
| . 375 |  | 32 28 | .3547 .4143 | . 33937 | . 34128 | 1 | 36 34 | . 087201 | . 0932 |
| $\begin{aligned} & .500 \\ & .5625 \\ & .625 \end{aligned}$ |  | 28 | . 4768 | . 4562 | . 4613 | 1 | 22 | . 162 | . 170 |
|  |  | 24 | . 5354 | . 5114 | . 5174 | 1 | 25 | . 203 | . 214 |
|  |  | 24 | . 5979 | . 5739 | . 5799 | 1 | 16 | . 256 | . 268 |
|  | . 6875 | 24 | . 6604 | . 6364 | . 6424 | 1 | 9 | . 315 | . 329 |
| . 750 |  | 20 | . 7175 | . 6887 | . 6959 | 1 | 16 | . 369 | . 386 |
|  | . 8125 | 20 | . 7800 | . 7512 | . 7584 | 1 | 10 | . 439 | . 458 |
| . 875 |  | 20 | . 8425 | . 8137 | . 8209 | 1 | 5 | . 515 | . 536 |
|  | . 9375 | 20 | . 9050 | . 8762 | . 8834 | 1 | 0 | . 598 | . 620 |
| 1.000 |  | 20 | . 9675 | . 9387 | . 9459 | 0 | 57 | . 687 | . 711 |
|  | 1.0625 | 18 | 1.0264 | . 9943 | 1.0024 | 0 | 59 | . 770 | . 799 |
| 1.125 |  | 18 | 1.0889 | 1.0568 | 1.0649 | 0 | 56 | . 871 | . 901 |
|  | 1.1875 | 18 | 1.1514 | 1.1193 | 1.1274 | 0 | 53 | . 977 | 1.009 |
| 1.250 |  | 18 | 1.2139 | 1.1818 | 1.1899 | 0 | 50 | 1.090 | 1.123 |
|  | 1.3125 | 18 | 1.2764 | 1.2443 | 1.2524 | 0 | 48 | 1.208 | 1.244 |
| 1.375 |  | 18 | 1.3389 | 1.3068 | 1.3149 | 0 | 48 | 1.333 | 1.370 |
|  | 1.4375 | 18 | 1.4014 | 1.3693 | 1.3774 | 0 | 43 | 1.464 | 1.503 |
| 1.500 |  | 18 | 1.4639 | 1.4318 | 1.4399 | 0 | 42 | 1.60 | 1.64 |
|  | 1.5625 | 18 | 1.5264 | 1.4943 | 1.5024 | 0 | 40 | 1.74 | 1.79 |
| 1.625 |  | 18 | 1.5889 | 1.5568 | 1.5649 | 0 | 38 37 | $\xrightarrow{1.89}$ | 1.94 |
|  | 1.6875 | 18 | 1.6514 | 1.6193 | 1.6274 | 0 | 37 | 2.05 | 2.10 |

${ }^{\mathrm{a}} \mathrm{b}$ For sizes larger than 1.6875 in, use 16 -thread series. See table 2.15 .
${ }^{6}$ Design form. See fig. 2.3.
${ }^{\text {- }}$ See formula under definition of tensile stress area in appendix A5.

Table 2.11. 4-thread series, basic dimensions, $4 U N$

| Nominal size and basic major diameter, $D$ |  | Basic pitch diameter, $E$ | Minor ${ }^{\text {b }}$ diameter, external threads, $K_{g}$ | Minor ${ }^{\text {b }}$ <br> diameter, internal threads, $K_{n}$ |  | Lead angle at basic pitch diameter, $\lambda$ | Sectional area at minor diameter at D $-2 h_{b}$ | $\begin{gathered} \text { Tensile stress } \\ \text { area, } \\ \pi\left(\frac{E}{2}-\frac{3 H}{16}\right)^{2} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Primary | Secondary |  |  |  |  |  |  |  |
| $i_{2}$ | in | in | in | in | deg | $\min$ | $\mathrm{in}^{2}$ | $i n^{2}$ |
|  |  | 2.3376 | 2.1933 | 2.2294 | 1 | 57 | 3.72 | 4.00 |
|  | 2.625 | 2.4626 | 2.3183 | 2.3544 | 1 | 51 | 4.16 | 4.45 |
| $2.750^{\text {a }}$ |  | 2.5876 | 2.4433 | 2.4794 | 1 | 46 | 4.62 | 4.93 |
|  | 2.875 | 2.7126 |  | 2.6044 | 1 | 41 | 5.11 | 5.44 |
| $3.000^{\text {a }}$ |  | 2.8376 | 2.6933 | 2.7294 | 1 | 36 | 5.62 | 5.97 |
|  | 3.125 | 2.9626 | 2.8183 | 2.8544 | 1 | 32 | 6.16 | 6.52 |
| $3.250{ }^{\text {a }}$ |  | 3.0876 | 2.9433 | 2.9794 | 1 | $\stackrel{29}{ }$ | 6.72 | 7.10 |
|  | 3.375 | 3.2126 | 3.0683 | 3.1044 |  |  |  |  |
| $3.500^{\text {a }}$ |  | 3.3376 | 3.1933 | 3.2294 | 1 | 22 | 7.92 | 8.33 |
|  | 3.625 | 3.4626 | 3.3183 | 3.3544 | 1 | 19 | 8.55 | 9.00 |
| $3.750^{\text {a }}$ |  | 3.5876 | 3.4433 | 3.4794 | 1 | 16 | 9.21 | 9.66 |
|  | 3.875 | 3.7126 | 3.5683 | 3.6044 |  |  | 9.90 | 10.36 |
| $4.000^{\text {a }}$ |  | 3.8376 | 3.6933 | 3.7294 | 1 | 11 | 10.61 | 11.08 |
|  | 4.125 | 3.9626 | 3.8183 | 3.8544 | 1 | 9 | 11.34 | 11.83 |
| 4.250 | -----7.375 | 4.0876 4.2126 | 3.9433 4.0683 | 3.9794 4.1044 | 1 | 7 5 | 12.10 12.88 | 12.61 13.41 |
| 4.500 |  | 4.3376 | 4.1933 | 4.2294 | 1 | 3 | 13.69 |  |
|  | 4.625 | 4.4626 | 4.3183 | 4.3544 | 1 | 1 | 14.52 | 15.1 |
| 4.750 |  | 4.5876 | 4.4433 | 4.4794 | 1 | 0 | 15.4 | 15.9 |
|  | 4.875 | 4.7126 | 4.5683 | 4.6044 | 0 | 58 | 16.3 | 16.5 |
| 5.000 |  | 4.8376 | 4.6933 | 4.7294 | 0 | 57 |  |  |
|  | 5.125 | 4.9626 | 4.8183 | 4.8544 | 0 | 55 | 18.1 | 18.7 |
| 5.250 |  | 5.0876 | 4.9423 | 4.9794 | 0 | 54 | 19.1 | 19.7 |
|  | 5.375 | 5.2126 | 5.0683 | 5.1044 | 0 | 52 | 20.0 | 20.7 |
| 5.500 |  | 5.3376 | 5.1933 | 5.2294 | 0 | 51 | 21.0 | 21.7 |
|  | 5.625 | 5.4626 | 5.3183 | 5.3544 | 0 | 50 | 22.1 | 22.7 |
| 5.750 |  | 5.5876 | 5.4433 | 5.4794 | 0 | 49 | 23.1 | 23.8 |
| 6.000 | 5.875 | 5.7126 5.8376 | 5.5683 5.6933 | 5.6044 5.7294 | 0 0 | 48 47 | 24.2 25.3 | 24.9 26.0 |

[^6]Table 2.12. 6-thread series, basic dimensions, 6UN

| Nominal size and basic major diameter, $D$ |  | Basic pitch diameter, $E$ | Minor ${ }^{\text {b }}$ diameter, external threads, $K_{s}$ | $\begin{array}{r} \text { Minorb } \\ \text { diameter, } \\ \text { internal } \\ \text { threads, } K_{n} \end{array}$ |  | Lead angle at basic pitch diameter, $\lambda$ | Sectional area at minor diameter at $D-2 h_{b}$ | $\begin{gathered} \text { Tensile stresse } \\ \text { area, } \\ \pi\left(\frac{E}{2}-\frac{3 H}{16}\right)^{2} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Primary | Secondary |  |  |  |  |  |  |  |
| $\operatorname{in}_{1.375^{\mathrm{a}}}$ | in | in | in | in | deg | min | $i n^{2}$ | $i n^{2}$ |
|  | 1.4375 | 1.2667 | 1.1705 | 1.1946 | 2 | 24 | 1.054 | 1.155 |
|  | 1.4375 |  |  |  | 2 |  | 1.171 | 1.277 |
| $1.500^{\text {a }}$ |  | 1.3917 | 1.2955 | 1.3196 | 2 | 11 | 1.294 | 1.405 |
|  | 1.5625 | 1.4542 | 1.3580 | 1.3821 | $\stackrel{2}{2}$ | 5 | 1.423 | 1.54 |
| 1.625 | 1.6875 | 1.5167 1.5792 | 1.4205 1.4830 | 1.4446 1.5071 | $\stackrel{2}{1}$ | 0 55 | 1.56 1.70 | 1.68 1.83 |
| 1.750 |  | 1.6417 | 1.5455 | 1.5696 | 1 | 51 | 1.85 | 1.98 |
|  | 1.8125 | 1.7042 | 1.6080 | 1.6321 |  | 47 | 2.00 | 2.14 |
| 1.875 | 1.9375 | 1.7667 1.8292 | 1.6705 1.7330 | 1.6946 1.7571 | 1 | 43 40 | 2.16 2.33 | 2.30 2.47 |
| 2.000 |  | 1.8917 | 1.7955 | 1.8196 | 1 | 36 | 2.50 | 2.65 |
|  | 2.125 | 2.0167 | 1.9205 | 1.9446 | 1 | 30 | 2.86 | 3.05 |
| 2.250 |  | 2.1417 | 20455 | 2.0696 | 1 | 25 | 3.25 | 3.42 |
|  | 2.375 | 2.2667 | 2.1705 | 2.1946 | 1 | 20 | 3.66 | 3.85 |
| 2.500 |  | 2.3917 | 2.2955 | 2.3196 | 1 | 16 | 4.10 | 4.29 |
|  | 2.625 | 2.5167 | 2.4205 | 2.4446 | 1 | 12 | 4.56 | 4.76 |
| 2.750 | 2.-875--- | 2.6417 2.7667 | 2.5455 2.6705 | 2.5696 2.6946 | 1 | 9 6 | 5.04 5.55 | 5.26 5.78 |
| 3.000 |  | 2.8917 | 2.7955 | 2.8196 | 1 | 3 | 6.09 |  |
|  | 3.125 | 3.0167 | 2.9205 | 2.9446 | 1 | 0 | 6.64 | 6.89 |
| 3.250 |  | 3.1417 | 3.0455 | 3.0696 | 0 | 58 | 7.23 | 7.49 |
|  | 3.375 | 3.2667 | 3.1705 | 3.1946 | 0 | 56 | 7.84 | 8.11 |
| 3.500 |  | 3.3917 | 3.2955 | 3.3196 | 0 | 54 | 8.47 | 8.75 |
|  | 3.625 | 3.5167 | 3.4205 | 3.4446 | 0 | 52 |  | 9.42 |
| 3.750 |  | 3.6417 3.7667 | 3.5455 | 3.5696 | 0 | 50 | 9.81 | 10.11 |
|  | 3.875 | 3.7667 | 3.6705 | 3.6946 | 0 | 48 | 10.51 | 10.83 |
| 4.000 |  | 3.8917 | 3.7955 | 3.8196 | 0 | 47 | 11.24 | 11.57 |
|  | 4.125 | 4.0167 | 3.9205 | 3.9446 | 0 | 45 | 12.00 | 32.33 |
| 4.250 |  | 4.1417 4.2667 | 4.0455 | 4.0696 | 0 | 44 | 12.78 | 13.12 |
|  | 4.375 | 4.2667 | 4.1705 | 4.1946 |  | 43 | 13.58 |  |
| 4.500 |  | 4.3917 | 4.2955 | 4.3196 |  | 42 |  | 14.78 |
|  | 4.625 | 4.5167 | 4.4205 | 4.4446 | 0 | 40 | 15.3 | 15.6 |
| 4.750 |  | 4.6417 4.7667 | 4.5455 4.6705 | 4.5696 | 0 | 39 | 16.1 | 16.5 |
|  | 4.875 | 4.7667 | 4.6705 | 4.6946 |  | 38 | 17.0 | 17.5 |
| 5.000 |  |  |  |  |  | 37 | 18.0 | 18.4 |
|  | 5.125 | 5.0167 | 4.9205 | 4.9446 | 0 | 36 | 18.9 | 19.3 |
| 5.250 |  | 5.1417 5.2667 | 5.0455 5.1705 | 5.0696 5.1946 | 0 | 35 | 19.9 | 20.3 |
|  | 5.375 | 5.2667 | 5.1705 | 5.1846 |  | 35 | 20.9 | 21.3 |
| 5.500 |  | 5.3917 |  |  |  | 34 | 21.9 | 22.4 |
|  | 5.625 | 5.5167 | 5.4205 | 5.4446 | 0 | 33 | 23.0 | 23.4 |
| 5.750 | 5.875 | 5.6417 5.7667 | 5.5455 5.6705 | 5.5696 5.6946 | 0 | 32 | 24.0 25.1 | 24.5 25.6 |
| 6.000 |  | 5.8917 | 5.7955 | 5.8196 | 0 | 31 | 26.3 | 26.8 |

${ }^{\mathrm{a}}$ These are standard sizes of the UNC series.
${ }^{\mathrm{b}}$ Design form. See fig. 2.3.
${ }^{\text {c }}$ See formula under definition of tensile stress area in appendix A5.

Table 2.13. 8-thread series, basic dimensions, 8UN

| Nominal size and basic major diameter, $D$ |  | Basic pitch diameter, $E$ | Minorb diameter, external threads, $K_{s}$ | Minorb diameter, internal threads, $K_{r}$ |  | Lead angle at basic pitch diameter, $\lambda$ | Sectional area at minor diameter at $D-2 h_{b}$ | Tensile stresso$\pi\left(\frac{E}{2}-\frac{3 H}{16}\right)^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Primary | Secondary |  |  |  |  |  |  |  |
| $\begin{gathered} i n \\ 1.000^{\mathrm{a}} \end{gathered}$ | in | in | in | ${ }^{\text {in }}$ | deg | min | $i^{2}{ }^{2}$ | $i n^{2}$ |
|  |  | 0.9188 | 0.8466 | 0.8647 | 2 | 29 | 0.551 | 0.606 |
|  | 1.0625 | . 9813 | . 9091 | . 9272 | 2 | 19 | . 636 | - 695 |
| 1.125 |  | 1.0438 | . 9716 | . 9897 | 2 | 11 | . 728 | . 790 |
|  | 1.1875 | 1.1063 | 1.0341 | 1.0522 | 2 |  | . 825 | . 892 |
| 1.250 |  | 1.1688 | 1.0966 | 1.1147 | 1 | 57 | . 929 | 1.000 |
|  | 1.3125 | 1.2313 | 1.1591 | 1.1772 | , | 51 | 1.039 | 1.114 |
| 1.375 | 1.4375 | 1.2938 1.3563 | 1.2216 1.2841 | 1.2397 1.3022 | 1 | 46 41 | 1.155 | 1.233 1.360 |
| 1.500 |  | 1.4188 | 1.3466 | 1.3647 | 1 | 36 | 1.405 | 1.492 |
|  | 1.5625 | 1.4813 | 1.4091 | 1.4272 | 1 | 32 | 1.54 | 1.63 |
| 1.625 |  | 1.5438 | 1.4716 | 1.4897 | 1 | 29 | 1.68 | 1.78 |
|  | 1.6875 | 1.6063 | 1.5341 | 1.5522 | 1 | 25 | 1.83 | 1.93 |
| 1.750 |  | 1.6688 | 1.5966 | 1.6147 | 1 | 22 | 1.98 | 2.08 |
|  | 1.8125 | 1.7313 | 1.6591 | 1.6772 | 1 | 19 | 2.14 | 2.25 |
| 1.875 |  | 1.7938 | 1.7216 | 1.7397 | 1 | 16 | 2.30 | 2.41 |
|  | 1.9375 | 1.8563 | 1.7841 | 1.8022 | 1 | 14 | 2.47 | 2.59 |
| 2.000 |  | 1.9188 | 1.8466 | 1.8647 | 1 | 11 | 2.65 |  |
|  | 2.125 | 2.0438 | 1.9716 | 1.9897 | 1 | 7 | 3.03 | 3.15 |
| 2.250 |  | 2.1688 | 2.0966 | 2.1147 | 1 | 3 | 3.42 3.85 | 3.56 |
|  | 2.375 | 2.2938 | 2.2216 | 2.2397 |  | 0 | 3.85 | 3.99 |
| 2.500 |  | 2.4188 | 2.3466 | 2.3647 | 0 | 57 | 4.29 | 4.44 |
|  | 2.625 | 2.5438 | 2.4716 | 2.4897 | 0 | 54 | 4.76 | 4.92 |
| 2.750 |  | 2.6688 2.7938 | 2.5966 2.7216 | 2.6147 2.7397 | 0 0 | 51 49 | 5.26 5.78 | 5.43 5.95 |
|  | 2.875 | 2.7938 | 2.7216 | 2.7397 | 0 | 49 | 5.78 |  |
| 3.000 |  | 2.9188 | 2.8466 | 2.8647 | 0 | 47 | 6.32 | 6.51 |
|  | 3.125 | 3.0438 | 2.9716 | 2.9897 | 0 | 45 | 6.89 | 7.08 |
| 3.250 |  | 3.1688 | 3.0966 | 3.1147 | 0 | 43 | 7.49 | 7.69 |
|  | 3.375 | 3.2938 | 3.2216 | 3.2397 | 0 | 42 | 8.11 | 8.31 |
| 3.500 |  | 3.4188 | 3.3466 | 3.3647 | 0 | 40 | 8.75 | 8.96 |
|  | 3.625 | 3.5438 | 3.4716 | 3.4897 | 0 | 39 | 9.42 | 9.64 |
| 3.750 |  | 3.6688 | 3.5966 | 3.6147 | 0 | 37 | 10.11 | 10.34 |
|  | 3.875 | 3.7938 | 3.7216 | 3.7397 | 0 | 36 | 10.83 | 11.06 |
| 4.000 |  | 3.9188 | 3.8466 | 3.8647 | 0 | 35 | 11.57 | 11.81 |
|  | 4.125 | 4.0438 | 3.9716 | 3.9897 | 0 | 34 | 12.34 | 12.59 |
| 4.250 |  | 4.1688 | 4.0966 | 4.1147 | 0 | 33 | 13.12 | 13.38 |
|  | 4.375 | 4.2938 | 4.2216 | 4.2397 | 0 | 32 | 13.94 | 14.21 |
| 4.500 |  | 4.4188 | 4.3466 | 4.3647 | 0 | 31 | 14.78 | 15.1 |
|  | 4.625 | 4.5438 | 4.4716 | 4.4897 | 0 | 30 | 15.6 | 15.9 |
| 4.750 |  | 4.6688 | 4.5966 | 4.6147 | 0 | 29 | 16.5 | 16.8 |
|  | 4.875 | 4.7938 | 4.7216 | 4.7397 | 0 | 29 | 17.4 | 17.7 |
| 5.000 |  | 4.9188 | 4.8466 | 4.8647 | 0 | 28 | 18.4 | 18.7 |
|  | 5.125 | 5.0438 | 4.9716 | 4.9897 | 0 | 27 | 19.3 | 19.7 |
| 5.250 |  | 5.1688 | 5.0966 | 5.1147 | 0 | 26 | 20.3 | 20.7 |
|  | 5.375 | 5.2938 | 5.2216 | 5.2397 | 0 | 26 | 21.3 | 21.7 |
| 5.500 |  | 5.4188 | 5.3466 | 5.3647 | 0 | 25 | 22.4 | 22.7 |
|  | 5.625 | 5.5438 | 5.4716 | 5.4897 | 0 | 25 | 23.4 | 23.8 |
| 5.750 | 5.875 | 5.6688 | 5.5966 | 5.6147 | 0 | 24 | 24.5 | 24.9 |
| $6.001)$ | 5.875 | 5.7938 5.9188 | 5.7216 5.8466 | 5.7397 5.8647 | 0 | 24 | 25.6 26.8 | 26.0 27.1 |
|  |  | 5.0188 | 5.8466 | 5.8647 | 0 | 23 | 26.8 | 27.1 |

${ }^{\text {a }}$ This is a standard size of the UNC series.
${ }^{\mathrm{b}}$ Design form. See fig. 2.3.
e See formula under definition of tensile stress area in appendix A5.

Table 2.14. 12-thread series, basic dimensions, 12UN

| Nominal size and basic major diameter, $D$ |  | Basic pitch diameter, $E$ | Minorb diameter, external threads, $K_{s}$ | Minorb diameter, internal threads, $K_{n}$ |  | Lead angle at basic pitch diameter, $\lambda$ | Sectional area at minor diameter at $D-2 h_{b}$ | $\begin{gathered} \text { Tensile stress॰ } \\ \text { area, } \\ \pi\left(\frac{E}{2}-\frac{3 H}{16}\right)^{2} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Primary | Secondary |  |  |  |  |  |  |  |
| $\begin{aligned} & i n \\ & .5625^{\mathrm{a}} \\ & .625 \end{aligned}$ | in | ${ }^{\text {in }}$ | in | in | deg | $\min$ | in ${ }^{2}$ | in ${ }^{2}$ |
|  |  | 0.5084 | 0.4603 | 0.4723 | 2 | 59 | 0.162 | 0.182 |
|  |  | . 5709 | . 52228 | . 53478 | $\stackrel{2}{2}$ | 40 | . 210 | . 232 |
|  | . 6875 | 6334 | . 5853 | . 5973 | 2 | 24 | . 264 | . 289 |
| . 750 |  | . 6959 | . 6478 | . 6598 | 2 | 11 | . 323 | . 351 |
|  | . 8125 | . 7584 | . 7103 | . 7223 | 2 | 0 | . 390 | . 420 |
| . 875 | .9375 | .8209 .8834 | .7728 | . 78488 | 1 | 51 43 | . 540 | . 495 |
| $1.000^{\text {a }}$ |  | . 9459 | . 8978 | . 9098 | 1 | 36 | . 625 | . 663 |
|  | 1.0625 | 1.0084 | . 9603 | . 9723 |  | 30 | . 715 | . 756 |
| 1.125 ${ }^{\text {a }}$ |  | 1.0709 | 1.0228 | 1.0348 | 1 | 25 | . 812 | . 856 |
|  | 1.1875 | 1.1334 | 1.0853 | 1.0973 | 1 | 20 | . 915 | . 961 |
| $1.250{ }^{\text {a }}$ |  | 1.1959 | 1.1478 | 1.1598 | 1 | 16 | 1.024 | 1.073 |
|  | 1.3125 | 1.2584 | 1.2103 | 1.2223 | 1 | 12 | 1.139 | 1.191 |
| $1.375^{\text {a }}$ |  | 1.3209 | 1.2728 | 1.2848 | 1 | 9 | 1.260 | 1.315 |
|  | 1.4375 | 1.3834 | 1.3353 | 1.3473 | 1 | 6 | 1.388 | 1.445 |
| $1.500^{\text {a }}$ |  | 1.4459 | 1.3978 | 1.4098 | 1 | 3 | 1.52 | 1.58 |
|  | 1.5625 | 1.5084 | 1.4603 | 1.4723 | 1 | 0 | 1.66 | 1.72 |
| 1.625 |  | 1.5709 | 1.5228 | 1.5348 | 0 | 58 | 1.81 | 1.87 |
|  | 1.6875 | 1.6334 | 1.5853 | 1.5973 | 0 | 56 | 1.96 | 2.03 |
| 1.750 |  | 1.6959 | 1.6478 | 1.6598 | 0 | 54 | 2.12 | 2.19 |
|  | 1.8125 | 1.7584 | 1.7103 | 1.7223 | 0 | 52 | 2.28 | 2.35 |
| 1.875 |  | 1.8209 | 1.7728 | 1.7848 | 0 | 50 | 2.45 | 2.53 |
|  | 1.9375 | 1.8834 | 1.8353 | 1.8473 | 0 | 48 | 2.63 | 2.71 |
| 2.000 |  | 1.9459 | 1.8978 | 1.9098 | 0 | 47 | 2.81 | 2.89 |
|  | 2.125 | 2.0709 | 2.0228 | 2.0348 | 0 | 44 | 3.19 | 3.28 |
| 2.250 |  | 2.1959 | 2.1478 | 2.1598 | 0 | 42 | 3.60 | 3.69 |
|  | 2.375 | 2.3209 | 2.2728 | 2.2848 | 0 | 39 | 4.04 | 4.13 |
| 2.500 |  | 2.4459 | 2.3978 | 2.4098 | 0 | 37 | 4.49 | 4.60 |
|  | 2.625 | 2.5709 | 2.5228 | 2.5348 | 0 | 35 | 4.97 | 5.08 |
| 2.750 |  | 2.6959 | 2.6478 | 2.6598 | 0 | 34 | 5.48 | 5.59 |
|  | 2.875 | 2.8209 | 2.7728 | 2.7848 | 0 | 32 | 6.01 | 6.13 |
| 3.000 |  | 2.9459 | 2.8978 | 2.9098 | 0 | 31 | 6.57 | 6.69 |
|  | 3.125 | 3.0709 | 3.0228 | 3.0348 | 0 | 30 | 7.15 | 7.28 |
| 3.250 |  | 3.1959 | 3.1478 | 3.1598 | 0 | $\stackrel{29}{ }$ | 7.75 | 7.89 |
|  | 3.375 | 3.3209 | 3.2728 | 3.2848 | 0 | 27 | 8.38 | 8.52 |
| 3.500 |  | 3.4459 | 3.3978 | 3.4098 | 0 | 26 | 9.03 | 9.18 |
|  | 3.625 | 3.5709 | 3.5228 | 3.5348 | 0 | 26 | 9.71 | 9.86 |
| 3.750 |  | 3.6959 | 3.6478 | 3.6598 | 0 | 25 | 10.42 | 10.57 |
|  | 3.875 | 3.8209 | 3.7728 | 3.7848 | 0 | 24 | 11.14 | 11.30 |
| 4.000 |  | 3.9459 | 3.8978 | 3.9098 | 0 | 23 | 11.90 | 12.06 |
|  | 4.125 | 4.0709 | 4.0228 | 4.0348 | 0 | 22 | 12.67 | 12.84 |
| 4.250 |  | 4.1959 | 4.1478 | 4.1598 | 0 | 22 | 13.47 | 13.65 |
|  | 4.375 | 4.3209 | 4.2728 | 4.2848 | 0 | 21 | 14.30 | 14.48 |
| 4.500 |  | 4.4459 | 4.3978 | 4.4098 | 0 | 21 | 15.1 | 15.3 |
|  | 4.625 | 4.5709 | 4.5228 | 4.5348 | 0 | 20 | 16.0 | 16.2 |
| 4.750 |  | 4.6959 | 4.6478 | 4.6598 | 0 | 19 | 16.9 | 17.1 |
|  | 4.875 | 4.8209 | 4.7728 | 4.7848 | 0 | 19 | 17.8 | 18.0 |
| 5.000 |  | 4.9459 | 4.8978 | 4.9098 | 0 | 18 | 18.8 | 19.0 |
|  | 5.125 | 5.0709 | 5.0228 | 5.0348 | 0 | 18 | 19.8 | 20.0 |
| 5.250 |  | 5.1959 | 5.1478 | 5.1598 | 0 | 18 | 20.8 | 21.0 |
|  | 5.375 | 5.3209 | 5.2728 | 5.2848 | 0 | 17 | 21.8 | 22.0 |
| 5.500 |  | 5.4459 | 5.3978 | 5.4098 | 0 | 17 | 22.8 | 23.1 |
|  | 5.625 | 5.5709 | 5.5228 | 5.5348 | 0 | 16 | 23.9 | 24.1 |
| 5.750 |  | 5.6959 | 5.6478 | 5.6598 | 0 | 16 | 25.0 | 25.2 |
|  | 5.875 | 5.8209 | 5.7728 | 5.7848 | 0 | 16 | 26.1 | 26.4 |
| 6.000 |  | 5.9459 | 5.8978 | 5.9098 | 0 | 15 | 27.3 | 27.5 |

${ }^{\text {a }}$ These are standard sizes of the UNC or UNF series.
${ }^{\mathrm{b}}$ Design form. See fig. 2.3.
${ }^{\mathbf{c}}$ See formula under definition of tensile stress area in appendix A5.

Table 2.15. 16-thread series, basic dimensions, 16 UN

| Nominal size and basic major diameter, $D$ |  | Basic pitch diameter, $E$ | Miner ${ }^{\text {b }}$ diameter, external threads, $K_{s}$ | Minorb <br> diameter, internal threads, $K_{n}$ |  | Lead angle at basic pitch diameter, $\lambda$ | Sectional area at minor diameter at$D-2 h_{b}$ | Tensile stresso$\pi\left(\frac{E}{\text { area, }}-\frac{3 H}{16}\right)^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Primary | Secondary |  |  |  |  |  |  |  |
| $\begin{gathered} i n \\ .375^{a} \\ .4375 \end{gathered}$ | in | in 0.3344 .3969 | in 0.2983 .3608 | in 0.3073 .3698 | deg 3 2 | $\min$ 24 52 | in ${ }^{2}$ 0.0678 .0997 | $i n^{2}$ <br> 0.0775 <br> . 1114 |
| $\begin{aligned} & .500 \\ & .5625 \\ & .625 \end{aligned}$ |  | . 4594 | . 4233 | . 4323 | 2 | 29 | . 1378 | . 151 |
|  |  | . 5219 | . 4858 | . 4948 | 2 | 11 | . 182 | . 198 |
|  |  | . 5844 | . 5483 | . 5573 | 1 | 57 | . 232 | . 250 |
|  | . 6875 | . 6469 | . 6108 | . 6198 | 1 | 46 | . 289 | . 308 |
| .750 ${ }^{\text {a }}$ |  | . 7094 | . 6733 | . 6823 | 1 | 36 | . 351 | . 373 |
|  | . 8125 | . 7719 | . 7358 | . 7448 | 1 | 29 | . 420 | . 444 |
| . 875 |  | . 8344 | . 7983 | . 8073 | 1 | 22 | . 495 | . 521 |
|  | . 9375 | . 8969 | . 8608 | . 8698 | 1 | 16 | . 576 | . 604 |
| 1.000 |  | . 9594 | . 9233 | . 9323 | 1 | 11 | . 663 | . 693 |
|  | 1.0625 | 1.0219 | . 9858 | . 9948 | 1 | 7 | . 756 | . 788 |
| 1.125 |  | 1.0844 | 1.0483 | 1.0573 | 1 | 3 | . 856 | . 889 |
|  | 1.1875 | 1.1469 | 1.1108 | 1.1198 | 1 | 0 | . 961 | . 997 |
| 1.250 |  | 1.2094 | 1.1733 | 1.1823 | 0 | 57 | 1.073 | 1.111 |
|  | 1.3125 | 1.2719 | 1.2358 | 1.2448 | 0 | 54 | 1.191 | 1.230 |
| 1.375 | 1.485 | 1.3344 1.3969 | 1.2983 1.3608 | 1.3073 1.3698 | 0 | 51 49 | 1.315 1.445 | 1.356 1.488 |
| 1.500 |  |  |  |  |  |  |  |  |
|  |  | 1.4594 | 1.4233 | 1.4323 | 0 | 47 | 1.58 | 1.63 |
|  | 1.5625 | 1.5219 | 1.4858 | 1.4948 | 0 | 45 | 1.72 | 1.77 |
| 1.625 |  | 1.5844 | 1.5483 | 1.5573 | 0 | 43 | 1.87 | 1.92 |
|  | 1.6875 | 1.6469 | 1.6108 | 1.6198 |  |  | 2.03 | 2.08 |
| 1.750 |  | 1. 7094 | 1.6733 | 1. 6823 | 0 | 40 | 2.19 | 2.24 |
|  | 1.8125 | i. 7719 | 1.7358 | 1.7448 | 0 | 39 | 2.35 | 2.41 |
| 1.875 |  | 1.8344 | 1.7983 | 1. 8073 | 0 | 37 | 2.53 | 2.58 |
|  | 1.9375 | 1.8969 | 1.8608 | 1.8698 | 0 | 36 | 2.71 | 2.77 |
| 2.000 |  | 3.0594 | 1.9233 | 1.9323 | 0 | 35 | 2.89 | 2.95 |
|  | 2.125 | 2.0594 | 2.0483 | 2.0573 | 0 | 33 | 3.28 | 3.35 |
| 2.250 | 2.375 | 2.2094 2.3344 | 2.1733 2.2983 | 2.1823 2.3073 | 0 | 31 29 | 3.69 4.13 | 3.76 4.21 |
| 2.500 |  | 2.4594 | 2.4233 | 2.4323 | 0 | 28 | 4.60 | 4.67 |
|  | 2.625 | 2.5844 | 2.5483 | 2.5573 | 0 | 26 | 5.08 | 5.16 |
| 2.750 |  | 2.7094 | 2.6733 | 2.6823 | 0 | 25 | 5.59 | 5.68 |
|  | 2.875 | 2.8344 | 2.7983 | 2.8073 | 0 | 24 | 6.13 | 6.22 |
| 3.000 |  | 2.9594 | 2.923 | 2.9323 | 0 | 23 | 6.69 |  |
|  | 3.125 | 3.0844 | 3.0483 | 3.0573 | 0 | 22 | 7.28 | 7.37 |
| 3.250 |  | 3.2094 3.3344 | 3.1733 3.2983 | 3.1823 3.3073 | 0 0 | 21 21 | 7.89 8.52 | 7.99 8.63 |
|  | 3.375 | 3.3344 | 3.2983 | 3.3073 | 0 | 21 | 8.52 | 8.63 |
| 3.500 |  | 3.4594 | 3.4233 | 3.4323 | 0 | 20 | 9.18 | 9.29 |
|  | 3.625 | 3.5844 | 3.5483 | 3.5573 | 0 | 19 | 9.86 | 9.98 |
| 3.750 | 3.875 | 3.7094 3.8344 | 3.6733 3.7983 | 3.6823 3.8073 | 0 | 18 18 | 10.57 11.30 | 10.69 11.43 |
| 4.000 |  | 3.9594 | 3.9233 | 3.9323 | 0 | 17 | 12.06 | 12.19 |
|  | 4.125 | 4.0844 | 4.0483 | 4.0573 | 0 | 17 | 12.84 | 12.97 |
| 4.250 |  | 4.2094 | 4.1733 | 4.1823 | 0 | 16 | 13.65 | 13.78 |
|  | 4.375 | 4.3344 | 4.2983 | 4.3073 | 0 | 16 | 14.48 | 14.62 |
| 4.500 |  | 4.4594 | 4.4233 | 4.4323 | 0 | 15 | 15.34 | 15.5 |
|  | 4.625 | 4.5844 | 4.5483 | 4.5573 | 0 | 15 | 16.2 | 16.4 |
| 4.750 |  | 4.7094 | 4.6733 | 4.6823 | 0 | 15 | 17.1 | 17.3 |
|  | 4.875 | 4.8344 | 4.7983 | 4.8073 | 0 | 14 | 18.0 | 18.2 |
| 5.000 |  | 4.9594 | 4.9233 | 4.9323 | 0 | 14 | 19.0 | 19.2 |
|  | 5. 125 | 5.0844 | 5.0483 | 5.0573 | 0 | 13 | 20.0 | 20.1 |
| 5.250 |  | 5.2094 | 5.1733 | 5.1823 | 0 | 13 | 21.0 | 21.1 |
|  | 5.375 | 5.3344 | 5.2983 | 5.3073 | 0 | 13 | 22.0 | 22.2 |
| 5.500 |  | 5.4594 | 5.4233 | 5.4323 | 0 | 13 | 23.1 | 23.2 |
|  | 5.625 | 5.5844 | 5.5483 | 5.5573 | 0 | 12 | 24.1 | 24.3 |
| 5.750 | 5.875 | 5.7094 | 5. 6733 | 5. 6823 | 0 | 12 | 25.2 | 25.4 |
| 6.000 | 5.875 | 5.8344 5.9594 | 5.7983 5.9233 | 5.8073 5.9323 | 0 | 12 11 | 26.4 27.5 | 26.5 27.7 |
|  |  | 5.9594 | 5.9233 | 5.9323 | 0 | 11 | 27.5 | 27.7 |

[^7]Table 2.16. 20-thread series, basic dimensions, 20UN

| Nominal size and basic major diameter, $D$ |  | Basic pitch diameter, $E$ | Minor ${ }^{\text {b }}$ diameter, external threads, $K_{s}$ | Minor ${ }^{\text {b }}$ diameter, internal threads. $K_{n}$ |  | Lead angle at basic pitch diameter, $\lambda$ | Sectional area at minor diameter at$D-2 h_{b}$ | Tensile stress area,$\pi\left(\frac{E}{2}-\frac{3 H}{16}\right)^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Primary | Secondary |  |  |  |  |  |  |  |
| in | in | ${ }^{\text {in }}$ | in | $\mathrm{in}^{\text {in }}$ | deg | min | $i^{2}{ }^{2}$ | $\mathrm{in}^{2}$ |
| $.250^{\text {a }}$ |  | 0.2175 | 0.1887 | 0.1959 | 4 | 11 | 0.0269 | 0.0318 |
| . 3125 |  | .2800 .3425 | . 25137 | .2584 .3209 | 3 | 15 | . 0481 | . 0547 |
| . 37375 |  | . 34050 | . 3137 | . 3209 | 2 2 | 40 15 | .0755 .1090 | .0836 .1187 |
| . $500^{\text {a }}$ |  | . 4675 | . 4387 | . 4459 | 1 | 57 | . 1486 | . 160 |
| . 5625 |  | . 5300 | . 5012 | . 5084 | 1 | 43 | . 194 | . 207 |
| . 625 |  | . 5925 | . 5637 | . 5709 | 1 | 32 | . 246 | . 261 |
|  | . 6875 | . 6550 | . 6262 | . 6334 | 1 | 24 | . 304 | . 320 |
| $.750^{\text {a }}$ |  | . 7175 | . 6887 | . 6959 | 1 | 16 | . 369 | . 386 |
|  | .8125 ${ }^{\text {a }}$ | . 7800 | . 7512 | . 7584 | 1 | 10 | . 439 | . 458 |
| . $875^{\text {a }}$ |  | . 8425 | . 8137 | . 8209 | 1 | 5 | . 515 | . 536 |
|  | $.9375^{\text {a }}$ | . 9050 | . 8762 | . 8834 | 1 | 0 | . 598 | . 620 |
| $1.000^{8}$ |  | . 9675 | . 9387 | . 9459 | 0 | 57 | . 687 | . 711 |
|  | 1.0825 | 1.0300 | 1.0012 | 1.0084 | 0 | 53 | . 782 | . 807 |
| 1.125 |  | 1.0925 | 1.0637 | 1.0709 | 0 | 50 | . 882 | . 910 |
|  | 1.1875 | 1.1550 | 1.1262 | 1.1334 | 0 | 47 | . 980 | 1.018 |
| 1.250 |  | 1.2175 | 1.1887 | 1.1959 | 0 | 45 | 1.103 | 1.133 |
|  | 1.3125 | 1.2800 | 1.2512 | 1.2584 | 0 | 43 | 1.222 | 1.254 |
| 1.375 |  | 1.3425 | 1.3137 | 1.3209 | 0 | 41 | 1.348 | 1.382 |
|  | 1.4375 | 1.4050 | 1.3762 | 1.3834 | 0 | 39 | 1.479 | 1.51 |
| 1.500 |  | 1.4675 | 1.4387 | 1.4459 | 0 | 37 | 1.62 | 1.65 |
|  | 1.5625 | 1.5300 | 1.5012 | 1.5084 | 0 | 36 | 1.76 | 1.80 |
| 1.625 |  | 1.5925 | 1.5637 | 1.5709 | 0 | 34 | 1.91 | 1.95 |
|  | 1.6875 | 1.6550 | 1.6262 | 1.6334 | 0 | 33 | 2.07 | 2.11 |
| 1.750 |  | 1.7175 | 1.6887 | 1.6959 | 0 | 32 | 2.23 | 2.27 |
|  | 1.8125 | 1.7800 | 1.7512 | 1.7584 | 0 | 31 | 2.40 | 2.44 |
| 1.875 |  | 1. 8425 | 1.8137 | 1.8209 | 0 | 30 | 2.57 | 2.62 |
|  | 1.9375 | 1.8050 | 1.8762 | 1.8834 | 0 | 29 | 2.75 | 2.80 |
| 2.000 |  | 1.9675 | 1.9387 | 1.9459 | 0 | 28 | 2.94 | 2.99 |
|  | 2.125 | 2.0925 | 2.0637 | 2.0709 | 0 | 26 | 3.33 | 3.38 |
| 2. 250 |  | 2.2175 | 2.1887 | 2.1959 | 0 | 25 | 3.75 | 3.81 |
|  | 2.375 | 2.3425 | 2.3137 | 2.3209 | 0 | 23 | 4.19 | 4.25 |
| 2.500 |  | 2.4675 | 2.4387 | 2.4459 | 0 | 22 | 4.66 | 4.72 |
|  | 2.625 | 2.5925 | 2.5637 | 2.5709 | 0 | 21 | 5.15 | 5.21 |
| 2.750 |  | 2.7175 | 2.6887 | 2.6959 | 0 | 20 | 5.66 | 5.73 |
|  | 2.875 | 2.8425 | 2.8137 | 2.8209 | 0 | 19 | ${ }^{6.20}$ | 6.27 |
| 3.000 |  | 2.9675 | 2.9387 | 2.9459 | 0 | 18 | 6.77 | 6.84 |

a These are standard sizes of the UNC, UNF, or UNEF series.
b Design form. Sea fi. 2.3.
${ }^{6}$ Deaign form. See fig. 2.3.

- See formula under definition of tensile stress area in appendix A5.

Table 2.17. 28-thread series, basic dimensions, 28UN

| Nominal size and basic major diameter, $D$ |  | Basic pitch diameter, $E$ | Minor ${ }^{\text {b }}$ diameter, external threads, $K_{s}$ | Minorb diameter, internal threads, $K_{n}$ |  | Lead angle at basic pitch diameter, $\lambda$ | Sectional area at minor diameter at $D-2 h_{b}$ | Tensile stress ${ }^{\circ}$$\pi\left(\frac{E^{\text {area }}}{2}-\frac{3 H}{16}\right)^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Primary | Secondury |  |  |  |  |  |  |  |
| in |  | $\begin{gathered} \quad i n \\ 0.1928 \end{gathered}$ | $\stackrel{i n}{0.1722}$ | $\mathrm{in}^{\text {in }}$ | ${ }_{3}^{\text {deg }}$ | $\min _{22}$ | $\begin{gathered} i n^{2} \\ 0.0226 \end{gathered}$ | $\begin{gathered} i n^{2} \\ 0.0258 \end{gathered}$ |
| . $250^{\text {a }}$ |  | . 2268 | . 2062 | . 2113 | 2 | 52 | . 0326 | . 0364 |
| . 3125 |  | .2893 | . 2687 | . 2738 | 2 | 15 | . 0556 | . 0606 |
| . 375 |  | . 3518 | . 3312 | . 3363 | 1 | 51 | . 0848 | . 0909 |
| . $4375^{\text {8 }}$ |  | . 4143 | . 3937 | . 3988 | 1 | 34 | . 1201 | . 1274 |
| . $500^{\text {a }}$ |  | . 4768 | . 4562 | . 4613 | 1 | 22 | . 162 | . 170 |
| . 5625 |  | . 5393 | . 5187 | . 5238 | 1 | 12 | . 209 | . 219 |
| . 625 |  | . 6018 | . 5812 | . 5863 | 1 | 5 | . 263 | . 274 |
|  | . 6875 | . 6643 | . 6437 | . 6488 | 0 | 59 | . 323 | . 335 |
| . 750 |  | . 7268 | . 7062 | . 7113 | 0 | 54 | . 389 | . 402 |
|  | . 8125 | . 7893 | . 7687 | . 7738 | 0 | 50 | . 461 | . 475 |
| . 875 | , 275 | . 8518 | . 8312 | . 8363 | 0 | 46 | . 539 | . 554 |
|  | . 9375 | . 9143 | . 8937 | . 8988 | 0 | 43 | . 624 | . 640 |
| 1.000 |  | . 9768 | . 9562 | . 9613 | 0 | 40 | . 714 | . 732 |
|  | 1.0625 | 1.0393 | 1.0187 | 1.0238 | 0 | 38 | . 811 | . 830 |
| 1.125 |  | 1.1018 | 1.0812 | 1.0863 1.1488 | 0 0 | 35 34 | .914 1.023 | . 933 |
|  | 1.1875 | 1.1643 | 1.1437 | 1.1488 | 0 | 34 | 1.023 | 1.044 |
| 1. 250 |  | 1.2268 | 1.2062 | 1.2113 | 0 | 32 | 1.138 | 1.160 |
|  | 1.3125 | 1.2893 | 1.2687 | 1.2738 | 0 | 30 | 1.259 | 1.282 |
| 1.375 |  | 1.3518 | 1.3312 | 1.3363 | 0 | $\stackrel{29}{ }$ | 1.386 | 1.411 |
|  | 1.4375 | 1.4143 | 1.3937 | 1.3988 | 0 | 28 | 1.52 | 1.55 |
| 1.500 |  | 1.4768 | 1.4562 | 1.4613 | 0 | 26 | 1.66 | 1.69 |

${ }^{\text {a }}$ These are standard sizes of the UNF or UNEF series.
b Design form. See fig. 2.3.

- See formula under definition of tensile stress area in appendix A5.

Table 2.18. 32-thread series, basic dimensions, 32UN

| Nominal size and basic major diameter, $D$ |  | Basic pitch diameter, $E$ | Minor ${ }^{\text {b }}$ diameter, external threads, $K_{s}$ | Minor ${ }^{\text {b }}$ diameter, internal threads, $K_{n}$ |  | Lead angle at basic pitch diameter, $\lambda$ | Sectional area at minor diameter at $D-2 h_{b}$ | $\begin{gathered} \text { Tensile stress } \\ \text { area, } \\ \pi\left(\frac{E}{2}-\frac{3 H}{16}\right)^{2} \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Primary | Secondary |  |  |  |  |  |  |  |
| in | in | in | in | in | deg | min | $\mathrm{in}^{2}$ | $i^{2}$ |
| . $138^{\text {a }}$ |  | 0.1177 | 0.0997 | 0.1042 | 4 | 50 | 0.00745 | 0.00909 |
| .164a |  | . 1437 | . 1257 | . 1302 | 3 | 58 | . 01196 | . 0140 |
| . $180{ }^{\text {a }}$ |  | . 1697 | . 1517 | . 1562 | 3 | 21 | . 01750 | . 0200 |
|  | $.216^{\text {a }}$ | . 1957 | . 1777 | . 1822 | 2 | 55 | . 242 | . 0270 |
| . $250{ }^{\text {a }}$ | ----- | . 2297 | . 2117 | . 2162 | 2 | 29 | . 0344 | . 0379 |
| . $3125^{8}$ |  | . 2922 | . 2742 | . 2787 | 1 | 57 | . 0581 | . 0625 |
| . $375{ }^{\text {a }}$ |  | . 3547 | . 3367 | . 3412 | 1 | 36 | . 0878 | . 0932 |
| . 4375 |  | . 4172 | . 3992 | . 4037 | 1 | 22 | . 1237 | . 1301 |
| . 500 |  | . 4797 | . 4617 | . 4662 | 1 | 11 | . 166 | . 173 |
| . 5625 |  | . 5422 | . 5242 | . 5287 | 1 | 3 | . 214 | . 222 |
| . 625 |  | . 6047 | . 5867 | . 5912 | 0 | 57 | . 268 | . 278 |
|  | . 6875 | . 6672 | . 6492 | . 6537 | 0 | 51 | . 329 | . 339 |
| . 750 |  | . 7297 | . 7117 | . 7162 | 0 | 47 | . 395 | . 407 |
|  | . 8125 | . 7922 | . 7742 | . 7787 | 0 | 43 | . 488 | . 480 |
| . 875 |  | . 8547 | . 8367 | . 8412 | 0 | 40 | . 547 | . 560 |
|  | . 9375 | . 9172 | . 8992 | . 9037 | 0 | 37 | . 632 | . 646 |
| 1.000 |  | . 9797 | . 9617 | . 9662 | 0 | 35 | . 723 | . 738 |

[^8]
## 4. THREAD CLASSES

Thread classes are distinguished from each other by the amounts of tolerance and allowance. The function of these classes is to assure the interchangeability of threaded parts. Six distinct classes of screw threads have been established for general use. These classes are: $1 \mathrm{~A}, 2 \mathrm{~A}$, and 3 A (for external threads only) and $1 \mathrm{~B}, 2 \mathrm{~B}$, and 3 B (for internal threads only). The disposition of the tolerances, allowances, and crest clearances for the various classes is illustrated in figures 2.5 and 2.6, p. 2.06.

The requirements for a screw-thread fit for a specific application can be met by specifying the proper combination of classes for the components. For example, an external thread made to class 2 A limits can be used with an internal thread made to classes 1B, 2B, or 3B limits for specific applications. It is not the purpose of this standard to limit applications of the various standard classes.
4.1. Classes 1A and 1B Threads.-Classes 1A and 1 B threads replace class 1 for new designs. These classes are intended for ordnance and other special uses. They are used on threaded components where quick and easy assembly is necessary and where a liberal allowance is required to permit ready assembly, even with slightly bruised or dirty threads.

Maximum diameters of class 1A (external) threads are less than basic by the amount of the same allowance as applied to class 2A. For the intended applications in American practice the allowance is not available for plating or coating. Where the thread is plated or coated, special provisions are necessary." The minimum diameters of class 1B (internal) threads, whether or not plated or coated, are basic, affording no allowance or clearance for assembly with maximum material external thread components having maximum diameters which are basic.

Allowances and tolerances for the respective thread series are specified in tables and their application is shown in figure 2.5.
4.2. Classes 2A And 2B Threads.-Class 2A for external threads and 2 B for internal threads are the most commonly used thread standards for general applications, including production of bolts, screws, nuts, and similar threaded fasteners.

The maximum diameters of class 2A (external) uncoated threads are less than basic by the amount of the allowance. The allowance minimizes galling and seizing in high-cycle wrench assembly, or it can be used to accommodate plated finishes or other coating. However, for threads with additive finish, the maximum diameters of class 2A may be exceeded by the amount of the allowance; i.e., the 2 A maximum diameters apply to an unplated part or to a part before plating whereas the basic diameters (the 2 A maximum diameter plus allowance) apply to a part after plating. The minimum diameters of class 2B (internal) threads, whether or not plated or coated, are basic, affording no allowance or clearance in assembly at maximum material limits. See par. 3.7, p. 2.05.

Certain applications require an allowance to permit application of the proper lubricant when making up the assembly, particularly with pressure vessels and steel pipe flanges, fittings, and valves for high-temperature, high-pressure service. For such applications class 2A, which has an allowance, and class 2B are rècommended, replacing class 7 which was previously established for such applications but which has been discontinued as a standard. See par. 3.7. In this application, when the thread is coated, the 2A allowance may not be consumed by such coating.

Allowances and tolerances for the respective thread series are specified in the tables and their application is shown in figure 2.5 .
4.3. Classes 3A And 3B Threads.-Class 3A for external threads and class 3 B for internal threads provide for applications where closeness of fit and accuracy of lead and angle of thread are important. They are obtainable consistently only by the use of high quality production equipment supported by a very efficient system of gaging and inspection. The maximum diameters of class 3A (external) threads and the minimum diameters of class 3 B (internal) threads, whether or not plated or coated, are basic, affording no allowance or clearance for assembly of maximum-material components.

No allowance is provided, but since the tolerances on GO gages are within the limits of size of the product, the gages will assure a slight clearance between product made to the maximum material limits. Tolerances for the respective thread series are specified in tables and their application is shown in figure 2.6.

## 5. ALLOWANCES

The allowance is minus and is applied from the basic size to below basic size. Allowance is applied only to the classes 1 A and 2 A external threads. Values of the allowance for these two classes are obtained by use of a $C$ factor of 0.3 in the formula shown in par. 6.1.

## 6. TOLERANCES

The internal thread tolerance is plus and is applied from the basic size to above the basic size for all three thread classes.

The external thread tolerance is minus and is applied:

1. from the basic size to below the basic size for class 3A (see fig. 2.6),
2. from the design size (basic size minus allowance) to below design size for classes 1 A and 2 A (see fig. 2.5).

The tolerances specified represent the extreme variations permitted on the product.
6.1. Pitch Diameter Tolerances.-The basic formula for pitch diameter tolerance is composed of the following increments:
P.D. Tolerance
$=C\left(0.0015 \sqrt[3]{D}+0.0015 \sqrt[3]{L_{e}}+0.015 \sqrt[3]{p^{2}}\right)$,
Table 2.19. Increments in pitch diameter tolerance formula ${ }^{a}$
[PD tolerance $\left.=C\left(0.0015 \sqrt[3]{D}+0.0015 \sqrt{L_{e}}+0.015 \sqrt[3]{p^{2}}\right)\right]$

| Diameter increments |  |  |  | Length of engagement increments |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D | $0.0015 \sqrt[3]{D}$ | D | $0.0015 \sqrt[3]{D}$ | Based on ${ }^{\text {b }}$ |  |  | $L_{e}$ | $\stackrel{0.0015}{\sqrt{L_{e}}} \times$ | Based on ${ }^{\text {b }}$ |  |  | $L_{e}$ | $\sqrt[0.0015]{\sqrt{\overline{L_{e}}} \times}$ | Based on ${ }^{\text {b }}$ |  | $L_{e}$ | $\sqrt[0.0015]{\sqrt{L_{e}}}$ |
|  |  |  |  | $1 D \text { for }$ sizes | $\begin{aligned} & 9 p \\ & \text { for } \\ & \text { tpi } \end{aligned}$ | $\begin{aligned} & 20 p \\ & \text { for } \\ & \text { tpi } \end{aligned}$ |  |  | $\begin{aligned} & 1 D \text { for } \\ & \text { sizes } \end{aligned}$ | $\begin{gathered} 9 p \\ \text { for } \\ \text { tpi } \end{gathered}$ | $\begin{aligned} & 20 p \\ & \text { for } \\ & \text { tpi } \end{aligned}$ |  |  | $1 D$ for sizes | $\begin{aligned} & 20 p \\ & \text { for } \\ & \text { tpi } \end{aligned}$ |  |  |
| in | in | in | in | in |  |  | in | in | in |  |  | in | in | in |  |  |  |
| 0.0600 | 0.000587 | 1.9375 | 0.001870 | . 060 |  |  | 0.0600 | 0.000367 | . 500 | 18 | 40 | 0.5000 | 0.001061 | 2.375 |  | 2.3750 | 0.002312 |
| . 0625 | . 000595 | 2.0000 | . 001890 | . 0625 |  |  | . 0625 | . 000375 | . 5556 |  | 36 | . 5556 | . 001118 | 2.500 | 8 | 2.5000 | . 0023372 |
| . 0730 | . 000627 | 2.1250 | . 001928 | . 073 |  |  | . 0730 | . 000405 | . 5625 | 16 |  | . 5625 | . 001125 | 2.625 |  | 2.6250 | . 002430 |
| . 0860 | . 000662 | 2.2500 | . 001966 | . 0781 |  |  | . 0781 | . 000419 | .625 .6429 | 14 | 32 | . 62429 | . 001186 | 2.750 2.851 | 7 | 2.7500 2.8571 | . 0024857 |
| . 0938 | . 000682 | 2.3750 | . 002001 | . 086 |  |  | . 0860 | . 000440 |  | 14 |  | . 6429 | . 001203 | 2.8571 | 7 | 2.8571 | . 002535 |
| . 0990 | . 000694 | 2.5000 | . 002036 | . 0938 |  |  | . 0938 | . 000459 | . 6875 |  |  | . 6875 | . 001244 | 2.875 |  | 2.8750 | . 002543 |
| . 1120 | . 000723 | 2.6250 | . 002069 | . 099 |  |  | . 0990 | . 000472 | . 6923 | 13 |  | . 6923 | . 001248 | 3.000 |  | 3.0000 3.1250 | . 00225958 |
| . 1250 | . 000750 | 2.7500 | . 002102 | . 1094 |  |  | . 1094 | . 000496 | . 7143 |  | 28 | . 7143 | . 0001268 | 3.125 |  | 3.12500 | . 0027024 |
| .1380 .1640 | . 0000775 | 2.8750 3.0000 | . 0002133 | . 11125 | 80 |  | . 11125 | . 0000502 | . 7450 | 12 | 27 | .7407 .7500 | . 0001299 | 3.2333 | 6 | ${ }_{3.3333}$ | . 002739 |
| . 1875 | . 000859 | 3.1250 | . 002193 | . 125 | 72 |  | . 1250 | . 000530 | . 7826 | 11.5 |  | . 7826 | . 001327 | 3.375 |  | 3.3750 | . 002756 |
| . 1900 | . 000862 | 3.2500 | . 002222 | . 138 |  |  | . 1380 | . 000557 | . 8125 |  |  | . 8125 | . 001352 | 3.500 |  | 3.5000 | . 002806 |
| . 2160 | . 000900 | 3.3750 | . 002250 | . 1406 | 64 |  | . 1406 | . 000562 | . 8182 | 11 |  | . 8182 | . 001357 | 3.625 |  | 3.6250 | . 002856 |
| . 2500 | . 000945 | 3.5000 | . 002277 | . 1562 |  |  | . 1562 | . 000593 | . 8333 |  | 24 | . 8333 | . 001369 | 3.750 |  | 3.7500 | . 0022905 |
| . 3125 | . 001018 | 3.6250 | . 002304 | . 1607 | 56 |  | . 1607 | . 000601 | . 875 |  |  | . 8750 | . 001403 | 3.875 |  | 3.8750 | . 002953 |
| . 3750 | . 001082 | 3.7500 | . 002330 | . 164 |  | -- | . 1640 | . 000607 | . 900 | 10 |  | . 9000 | . 001423 | 4.000 | 5 | 4.0000 | . 003000 |
| . 4375 | . 001139 | 3.8750 | . 002356 | . 1719 |  |  | . 1719 | . 0006622 | . 9375 |  |  | . 9375 | . 001452 | 4.125 |  | 4.1250 | . 00304097 |
| . 5600 | . 0001191 | 4.0000 4.1250 | . 002381 | ${ }^{.1} 1875$ | 48 |  | . 1875 | . 0000655 | 1.000 | 9 | 20 | 1.0000 | . 001500 | 4.250 |  | 4.2500 4.3750 | . 00303137 |
| . 6875 | . 001324 | 4.3750 | . 002453 | . 2045 | 44 |  | . 2045 | . 000678 | 1.125 | 8 |  | 1.1250 | . 001591 | 4.500 |  | 4.5000 | . 003182 |
| . 7500 | . 001363 | 4.5000 | . 002476 | . 216 |  |  | . 2160 | . 000697 | 1.1875 |  |  | 1.1875 | . 001635 | 4.625 |  | 4.6250 | . 003226 |
| . 8125 | . 001400 | 4.6250 | . 002499 | . 2188 |  |  | . 2188 | . 000702 | 1.250 |  | 16 | 1.2500 | . 001677 | 4.750 |  | 4.7500 | . 003269 |
| . 8750 | . 001435 | 4.7500 | . 002521 | . 225 | 40 |  | . 2250 | . 000712 | 1.2857 | 7 |  | 1.2857 | . 001701 | 4.875 |  | 4.8750 | . 003312 |
| . 9375 | . 001468 | 4.8750 | . 002543 | . 2344 |  |  | . 2344 | . 000726 | 1.3125 |  |  | 1.3125 | . 001718 | 5.000 | 4 | 5.0000 | . 003354 |
| 1.0000 | . 001500 | 5.0000 | . 002565 | . 250 | 36 | 80 | . 2500 | . 000750 | 1.375 |  |  | 1.3750 | . 001759 | 5.125 |  | 5.1250 | . 003396 |
| 1.0625 | . 001531 | 5.1250 | . 002586 | . 2656 |  |  | . 2656 | . 000773 | 1.4286 |  | 14 | 1.4286 | . 001793 | 5.250 |  | 5.2500 | . 0033437 |
| 1.1250 | . 001560 | 5.2500 | . 002607 | . 2778 |  | 72 | . 2778 | . 0000791 | 1.4375 |  |  | 1.4375 | . 0001798 | 5.375 5.500 |  | 5.3750 5.5000 | . 0003478 |
| 1.1875 1.2500 | . 001588 | 5.3750 | . 002628 | . 2812 | 32 |  | .2812 .2969 | .000795 .000817 | 1.500 1.5385 | 6 |  | 1.5000 1.5385 | . 000183781 | 5.500 5.625 |  | 5.5000 5.6250 | . 00035588 |
| 1.2500 | . 001616 | 5.5000 | . 002648 | . 2969 |  |  | . 2969 | . 000817 | 1.5385 |  | 13 | 1.5385 | . 001861 | 5.625 |  |  |  |
| 1.3125 | . 001642 | 5.6250 | . 002668 | . 3125 |  | 64 | . 3125 | . 000839 | 1.5625 |  |  | 1.5625 | . 001875 | 5.750 |  | 5.7500 | . 0035397 |
| 1.3750 | . 001668 | 5.7500 | . 002687 | . 3214 | 28 |  | . 3214 | . 000850 | 1.625 |  |  | 1.6250 | . 001912 | 5.875 |  | 5.8750 | . 003636 |
| 1.4375 | . 001693 | 5.8750 | . 002707 | . 3281 |  |  | . 3281 | . 000859 | 1.6667 |  | 12 | 1.6667 | . 001936 | ${ }_{6}^{6.000}$ |  | 6.0000 6.5000 | . 0033674 |
| 1.5625 | . 001741 | 7.0000 | . 002869 | . 3438 |  |  | . 3438 | . 000880 | 1.7391 |  | 11.5 | 1.7391 | . 001978 | 7.000 |  | 7.0000 |  |
| 1.6250 | . 001764 | 8.0000 | . 003000 | . 3571 |  | 56 | . 3571 | . 000896 | 1.750 |  |  | 1.7500 | . 001984 | 7.500 |  | 7.5000 | . 004108 |
| 1.6875 | . 001786 | 9.0000 | . 003120 | . 3594 |  |  | . 3594 | . 000899 | 1.800 | 5 |  | 1.8000 | . 002012 | 8.000 |  | 8.0000 | . 0004243 |
| 1.7500 | . 001808 | 10.0000 | . 003232 | . 375 | 24 |  | . 3750 | . 000919 | 1.8125 |  |  | 1.8125 | . 002019 | 8.500 |  | 8.5000 | . 0004373 |
| 1.8125 | . 001829 | 12.0000 | . 003434 | . 3906 |  |  | . 3906 | . 000937 | 1.8182 |  | 11 | 1.8182 | . 002023 | 9.000 |  | 9.0000 9.5000 | . 0004500 |
| 1.8750 | . 001850 | 14.0000 | . 003615 | . 4062 |  |  | . 4062 | . 000956 | 1.875 |  |  | 1.8750 | . 002054 | 9.500 |  | 9.5000 |  |
|  |  | 16.0000 | . 003780 | . 4167 |  | 48 | . 4167 | . 000968 | 1.9375 |  |  | 1.9375 | . 002088 | 10.000 |  | 10.0000 | . 004743 |
|  |  | 18.0000 | . 003931 | . 4219 |  |  | . 4219 | . 000974 | 2.000 | 4.5 | 10 | 2.0000 | . 002121 | 10.500 |  | 10.5000 | . 0048481 |
|  |  | 20.0000 | . 004072 | . 4375 |  |  | . 4375 | . 0009992 | 2.125 |  |  | 2.1250 | . 002187 | 11.000 |  | 11.0000 | . 004975 |
|  |  | 24.0000 | . 004327 | . 450 | 20 | 44 | . 4500 | . .001006 | 2.2222 2.250 | $4{ }^{--}$ | 9 | 2.2222 2.2500 | . 0022250 | 11.000 |  | 12.0000 | . 005196 |


| Pitch increments |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Threads per inc | $0.015 \sqrt[3]{p^{2}}$ | Threads per inc | $0.015 \sqrt[3]{p^{2}}$ | $\underset{\substack{\text { Threads } \\ \text { per } \\ \text { inch }}}{ }$ | $(0.015) \sqrt[3]{p^{2}}$ | $\begin{gathered} \text { Threads } \\ \text { per } \\ \text { inch } \end{gathered}$ | $0.015 \sqrt[3]{p^{2}}$ | $\begin{aligned} & \text { Threads } \\ & \text { per } \\ & \text { inch } \end{aligned}$ | $0.015 \sqrt[3]{p^{2}}$ | $\begin{aligned} & \text { Threads } \\ & \text { per } \\ & \text { inch } \end{aligned}$ | $0.015 \sqrt[3]{p^{2}}$ | Threads per inch | $0.015 \sqrt[3]{p^{2}}$ |
| $\begin{aligned} & 80 \\ & 72 \\ & 64 \\ & 60 \\ & 56 \end{aligned}$ | in 0.000808 .0080867 .000938 .00979 .001025 | 50 48 44 42 40 | in 0.001105 O . 001136 .001204 .001241 .001282 | 36 34 34 32 30 28 | in 0.001376 0.001429 .004888 .001554 .001627 | $\begin{aligned} & 27 \\ & 26 \\ & 24 \\ & 22 \\ & 20 \end{aligned}$ | in 0.001667 .001709 .001709 .001910 .002036 | $\begin{aligned} & 18 \\ & 16 \\ & 14 \\ & 13 \\ & 12 \end{aligned}$ | in 0.002184 .002362 .002382 .002713 $\therefore 002862$ | $\begin{gathered} 11.5 \\ 11 \\ 10 \\ 9 \\ 8 \end{gathered}$ |  | 7 7 6.5 5.5 4.5 4 4 | in <br> 0.004099 . 004543 .004814 .005130 .005953 |

a For class $2 \mathrm{~A}, C$
$\mathrm{~b}_{\text {For }}=1$. For other classes, values of $C$ are given in the table on p. 2.20.
$\boldsymbol{L}_{c}=0.5000$ is equivalent to one diameter for the .500 inch size, 9 pitches for 18 threads per inch, and 20 pitches for 40 threads per inch.
where
$C=$ a factor which differs for each class,
$D=$ basic major (nominal) diameter of thread,
$L_{e}=$ length of thread engagement,
$p=$ pitch of thread.
The values of the factor $C$ for the various thread classes are:

| Class | Factor $C$ | Class | Factor $C$ |
| :---: | :---: | :--- | :--- |
| 1A | 1.5 | 1 B | 1.95 |
| 2 A | 1.0 | 2B | 1.30 |
| 3 A | 0.75 | 3B | 0.975 |

The incremental values of the above formula are shown in table 2.19. The P. D. tolerances obtained by the use of the formulas are shown in table 2.21. The length of thread engagement ( $L_{e}$ ) used in the formula is $1 D$ (diameter) or 9 pitches, depending on the series. (See par. 7, Length of engagement, p. 2.21, for the $L_{e}$ for the various standard series of Unified threads.)

The factor $C$ is 30 percent greater for internal than for external threads of a given class on account of the greater difficulties encountered in the manufacture of internal threads.
6.2. Major Diameter Tolerances.-The class 1A major diameter tolerance is $0.090 \sqrt[3]{p^{2}}$ and that for classes 2 A and 3 A is $0.060 \sqrt[3]{p^{2}}$. The tolerance for class 2 A coarse and the 8 -thread series threads of unfinished, hot-rolled material is $0.090 \sqrt[3]{p^{2}}$.

The internal thread major diameter tolerance for all classes is $H / 6$ plus the pitch diameter tolerance of the class of thread involved. The maximum major
diameter of the internal thread may be determined by adding $0.793857 p(=11 H / 12$, table 2.1 , p. 2.02) to the maximum pitch diameter of the internal thread. In dimensioning internal threads the maximum major diameter is not specified, being established by the crest of an unworn tool. In practice, the major diameter of an internal thread is satisfactory when accepted by a gage or gaging method that represents the maximum material condition of an external thread which has no allowance.
6.3. Minor Diameter Tolerances.--External thread minor diameter tolerances are for reference only. At the nominal minor diameter, that is, at the intersection of the rounded root with its center line (see fig. 2.3, p. 2.04):

$$
\text { tolerance }=\text { P.D. tolerance }+H / 12
$$

and applies only when the rounded root is a design requirement. Otherwise:

$$
\text { tolerance }=\text { P.D. tolerance }+0.25 H
$$

The external thread minimum minor diameter is:

$$
\begin{aligned}
& \text { ext. thread min. P.D. }-0.649519 p . \\
& (0.649519 p=0.75 H \text {; see table 2.1.) }
\end{aligned}
$$

In dimensioning external threads, the minimum minor diameter is not specified, being established by the crest of an unworn tool. In practice, the minor diameter of an external thread is satisfactory when accepted by a gage or gaging method that represents the maximum material condition of the internal thread less the allowance, if any. Internal thread minor diameter tolerances are as shown in table 2.20.

Table 2.20. Minor diameter tolerances for internal threads

| Nominal Size (diameter) | Internal thread minor diameter tolerances for all standard thread series |  |
| :---: | :---: | :---: |
|  | Classes 1B and 2B | Class 3B (all sizes) |
| in <br> Less than 0.25 | $0.05 \sqrt[3]{\overline{p^{2}}}+0.03 p / D-0.002 \mathrm{in}$ <br> EXCEPT: <br> Tolerances shall not exceed $0.394 p$ <br> Tolerances shall not be less than $0.25 p-0.4 p^{2}$ - | $0.05 \sqrt[3]{p^{2}}+0.03 p / D-0.002 \mathrm{in}$. |
| 0.25 and larger | $0.25 p-0.4 p^{2}$ <br> EXCEPT: <br> The formula is not applicable to threads coarser than 4 tpi. For such threads the tolerance is 0.1 .5 p | EXCEPT: <br> Tolerances shall not exceed $0.394 p$. <br> Tolerances shall not be less than, For 80 to 13 tpi, inclusive: $0.23-1.5 p^{2}$ <br> For 12 tpi and coarser: $0.120 p$. |

The tolerance of $0.394 p$ corresponds to 53 percent of the basic thread height and applies in the range of the smallest sizes of the UNC and UNF thread series.

The tolerance of $0.120 p$ corresponds to 74 percent of the basic thread height.
The formulas are suitable for general applications having lengths of engagement up to $1.5 D$. However, some thread applications require lengths of engagement which are greater than $1.5 D$ or less than $D$. For such applications it may be advantageous to increase or decrease tolerances, as explained in section 3, or to use recommended hole size limits for different lengths of engagement as specified in appendix A3.

## 7. LENGTH OF ENGAGEMENT

The pitch diameter tolerances specified in table 2.21 for the UNC, UNF, 4UN, 6UN, and 8UN series are based on a length of engagement equal to the basic major (nominal) diameter and are applicable for lengths of engagement up to 1.5 diameters.

Where the length of engagement exceeds that for which these tolerances are applicable, the pitch diameter tolerances should be computed from the formula (table 2.21) values for the standard lengths of engagement of one diameter, as follows: for lengths of engagement over 1.5 to 3 diameters, the pitch diameter tolerances are 125 percent of the formula values; and for lengths of engagement over 3 diameters, the tolerances are 150 percent of the formula values.

The pitch diameter tolerances specified in table 2.21 for the UNEF, 12UN, 16UN, 20UN, 28UN, and 32UN series are based on a length of engagement of 9 pitches and are applicable for lengths of engagement up to 15 pitches.

Where the length of engagement exceeds that for which these tolerances are applicable, the pitch diameter tolerances should be computed from the formula (table 2.21) values for the standard lengths of engagement of 9 pitches, as follows: for lengths of engagement over 15 to 30 pitches, the pitch diameter tolerances are 125 percent of the formula values; and for lengths of engagement over 30 pitches, the tolerances are 150 percent of the formula values.

## 8. LIMITS OF SIZE

(For aeronautical applications, practices may deviate from those here specified. See Military Specification MIL-S-7742.)

With respect to the pitch diameter limits of size, it is intended, except as hereinafter qualified, that no portion of the complete thread be permitted to project beyond the envelope defined by the maxi-mum-material limits on the one hand, or beyond that defined by the minimum-material limits on the other, and thus be outside of the tolerance zone as illustrated in figures 2.5 and 2.6.
Note: The full tolerance cannot, therefore, be used on pitch diameter unless deviations in all other thread elements are zero.

Diameter equivalents of variations in lead, uniformity of helix, and flank angle are in the direction toward maximum material. Also included in pitchdiameter limits are other variations from size and profile, such as taper, out-of-round, and surface defects. Thus the maximum-material pitch diameter limits are a limitation of the virtual diameter (effective size) and are so specified herein for all thread classes. It is intended that diameter equivalents of deviations in any given element except pitch diameter should not exceed 0.5 of the pitchdiameter tolerance. Values are given in table 2.22 for deviations in lead and half-angle equivalent to
0.5 of pitch diameter tolerances. Flank angle equivalents should be based on a depth of thread engagement of 0.625 H .

Variations in taper and roundness of the pitch diameter, together with variations of the pitch diameter as a whole, may be in the direction of minimum material and thus the minimum-material pitch diameter limit may be specified as a limitation of the pitch diameter as a single element. However, in view of the interrelation of the pitch diameter, variations in lead and flank angle, etc., together with practical considerations relating to established production processes, product application and inspection procedures, except for class 3 A , for fasteners and some custom threaded parts, it is customary to base acceptance at the minimum-material condition (minimum pitch diameter of the external thread and maximum pitch diameter of the internal thread) on threaded plug and ring gaging, with gages to the thread form and length specified in section 6. See paragraph on Dimensional acceptability of threads in section 6 .
8.1. Diameter Equivalent of Angle Devia-tion.-The general formula expressing the relation between deviation in the half angle of thread and its diameter equivalent-that is, the amount of the pitch diameter tolerance absorbed by such a devia-tion-is:

$$
\cot \delta \alpha=\frac{h_{e}}{\delta E \sin \alpha \cos \alpha} \pm \cot \alpha
$$

in which

$$
\begin{aligned}
& \delta E=\text { pitch diameter increment due to deviation } \\
& \text { in half angle } \\
& h_{e}=\text { depth of thread engagement } \\
& \alpha=\text { basic half angle of thread } \\
& \delta \alpha=\text { deviation in half angle of thread. }
\end{aligned}
$$

In solving for $\delta E$ the average value of $\delta \alpha$ for two sides of the thread, regardless of their sign, should be taken. The sign of $\cot \alpha$ is plus when the half angle of thread is less than basic, minus when the half angle is greater than basic. By omitting $\pm \cot \alpha$ from the formula an approximate mean value for $\delta \alpha$ or $\delta E$ is obtained which differs very little from either extreme value. The Committee has, therefore, adopted for general use the formula

$$
\cot \delta \alpha=\frac{h_{e}}{\delta E \sin \alpha \cos \alpha} .
$$

For threads of Unified, American, or American National form, where $h_{e}=0.625 H$, this formula reduces to

$$
\cot \delta \alpha=\frac{5 p}{4 \delta E} \text { or } \delta E=1.25 p \tan \delta \alpha
$$

8.2. Diameter Equivalent of Lead Deviation. -The formula expressing the relation between lead deviation between any two threads within the length of engagement, and its diameter equivalent is as follows:

$$
\delta E=( \pm \delta p) \cot \alpha,
$$

in which

$$
\begin{aligned}
& \delta E=\text { pitch diameter increment due to lead } \\
& \text { deviation } \\
& \delta p=\text { the maximum pitch deviation between any } \\
& \text { two of the threads engaged } \\
& \alpha=\text { half angle of thread. }
\end{aligned}
$$

The quantity $\delta E$ is always added to the measured pitch diameter in the case of an external thread, and it is always subtracted in the case of an internal thread, regardless of the sign introduced by the lead deviation $\delta p$.

For threads of Unified, American, or American National form, the above formula reduces to

$$
\delta E=1.7321 \delta p
$$

## 9. COATED THREADS

It is not within the scope of this standard to make recommendations for thickness of, or to specify limits for, coatings. However, it will aid mechanical interchangeability if certain principles are followed whenever conditions permit.

It is desirable that the finished threads be within the limits of size established herein. To that end, external threads should not exceed the basic size after coating and internal threads should not be below the basic size after coating. However, it is recognized that there are some commonly used processes, such as hot-dip galvanizing, which are firmly established, and threads coated by such processes do not fall within the scope of this recommendation.
9.1. Guide For Relieving External Threads. -(This does not apply to extremes of diameter, length, and pitch.) Class 2A provides both a tolerance and an allowance. Many requirements are such as those for coatings deposited by electroplating processes. In general the 2 A allowance provides adequate relief for coatings up to a minimum thickness ${ }^{1}$ of one-sixth of the 2 A pitch diameter allowance, inasmuch as there are variables in thickness of coating and symmetry of coating resulting from commercial processes. See par. 4.2, p. 2.17. It should be stressed that threads after coating should be accepted by a basic size GO thread ring gage or equivalent functional gage.

Class 1A provides an allowance, but in this case the allowance is maintained for both coated and uncoated product. Special provisions before coating are necessary where (1) the design requires that the class 2A allowance be available after coating, or (2) the design requires that an allowance be provided for class 3A threads, or (3) the thickness of coating is too great to be accomodated by the class 2 A al-

[^9]lowance. In these cases it is recommended that the limits of size before coating be reduced by the amount of the 2 A allowance whenever that allowance is adequate, or that the maximum limits of the major and pitch diameters be decreased by an amount equal to six times the minimum coating thickness and the minimum limits be decreased by an amount equal to four times the minimum coating thickness.
9.2. Relief Of Internal Threads.-No provision is made for relieving internal threads as coatings on such threads are not generally required. Further, it is very difficult to deposit a significant thickness of coating on the flanks of internal threads. However, where a specific thickness of coating is required in an internal thread, it is suggested that the thread be relieved so that the thread after coating will be accepted by a GO thread plug gage of basic size. It is recommended that (1) the limits of size before coating be increased by the amount of the 2 A allowance whenever that allowance is adequate, or (2) the minimum limits of the minor and pitch diameters be increased by an amount equal to six times the minimum coating thickness and the maximum limits be increased by an amount equal to four times the minimum coating thickness.

## 10. METHOD OF DESIGNATING SCREW THREADS

The basic method of designating screw threads is used when the standard tolerances or limits of size based on the standard length of engagement are applicable as indicated in par. 7, Length of engagement, p. 2.21. The designation specifies in sequence the nominal size in decimals, number of threads per inch, thread series symbol, and thread class symbol. The nominal size is the basic major diameter. The nominal size shall be shown in four place decimals unless there is a cipher in the fourth place. A cipher in the fourth place shall be omitted.

The thread series symbol is UNC, UNF, UNEF, or UN for any of the series shown in table 2.7 and UNS for any other diameter-pitch combination having tolerances to Unified formulation.

The thread class symbol is $1 \mathrm{~A}, 1 \mathrm{~B}, 2 \mathrm{~A}, 2 \mathrm{AG}, 2 \mathrm{~B}$, 3 A , or 3 B in which the suffixes A and B relate to external and internal threads, respectively. Suffix G in the 2 AG symbol indicates that the 2 A dimensions are to be met after coating.

## Examples:

Nominal size (basic major diameter in decimals)
Number of threads per inch
Thread series symbol (see dimensional tables)
Thread class symbol (see par. 4 Thread
| classes, p. 2.17.)

For uncoated standard series threads (table 2.7) these designations may optionally be supplemented by the addition of the pitch diameter limits of size.

Example: (PD limits are those in table 2.21 for class 2A.)
.250-20 UNC-2A
PD .2164-2127 (Optional for uncoated threads).
UNS threads and threads having special length of engagement require certain additional information as shown on the following pages.
10.1. Designating Coated (Or Plated) Threads.-Specification on drawings of the before and after coating dimensions for screw threads is sometimes dictated by an engineering or production consideration that the size before and after coating be controlled. This results from coated screw threads having two stages of design: the before coating stage and the after coating stage. The threaded product may be produced by a supplier and coated by a user. In this case, it is necessary that a clear understanding of the coating requirements and the allowance for coating buildup be agreed upon by both supplier and user.

The before coating dimensions have a definite bearing on the strength of the screw threads. The after coating dimensions must allow the threads to assemble with their mating threads, as intended.

Recommended methods for designating coated threads under various conditions are described below:

For coated (or plated) class 1A external threads the max major and max pitch diameters may optionally be given followed by the words "AFTER COATING," thereby indicating that the thread before coating must have special provisions to allow for coating thickness. The major and pitch diameter limits of size before coating (calculated in accordance with footnote $1, \mathrm{p} .2 .22$, shall be given followed by the words "BEFORE COATING."

Example: (Major and PD limits are those in table 2.21 for class 1A for AFTER COATING and for class 1A minus allowance for BEFORE COATING.)

```
.250-20 UNC-1A
MAJOR DIA . }2489\mathrm{ MAX\AFTER COATING
PD . 2164 MAX
MAJOR DIA .2478-.2356 SPL BEFORE
PD .2153-.2097 SPL
```

For coated (or plated) class 2 A external threads the basic (max) major and basic (max) pitch diameters shall be given followed by the words "AFTER COATING." The major and pitch diameter limits of size before coating shall also be given followed by the words "BEFORE COATING."

Example: ${ }^{2}$ (Major and PD limits are those in table 2.21 for class 3 A (basic) for AFTER COATING and for class 2A for BEFORE COATING.)

[^10]750-10 UNC-2A
MAJOR DIA . 7500 MAX
PD . 6850 MAX
MAJOR DIA .7482-.7353
PD .6832-. 6773 BEFORE COATING

Certain applications require an allowance for rapid assembly to permit application of the proper lubricant or for residual growth due to high temperature expansion. In these applications, when the thread is coated and the 2A allowance is not permitted to be consumed by such coating, the thread class symbol is qualified by the addition of the letter G (symbol for allowance) following the class symbol and the max major and max pitch diameters are reduced below basic size by the amount of the 2A allowance and followed by the words "AFTER COATING," thereby ensuring that the allowance is maintained. The thread before coating must have special provisions to allow for coating thickness. The major and pitch diameter limits of size before coating (calculated in accordance with par 9, p. 2.22) shall also be given followed by the words "BEFORE COATING."
Example: (Major and PD limits are those in table 2.21 for class 2 A for AFTER COATING and for class 2A minus the allowance for BEFORE COATING.)

750-10 UNC-2AG
MAJOR DIA . 7482 MAX ${ }_{\text {PD }} 6832$ AFTER COATING MAJOR DIA .7464-. 7335 SPL $\backslash$ BEFORE
PD .6814-. 6755 SPL /COATING

For coated (or plated) class 3A external threads, the max major and max pitch diameters may optionally be given followed by the words "AFTER COATING," thereby indicating that the thread before coating must have special provisions to allow for coating thickness. The major and pitch diameter limits of size before coating (calculated in accordance with par. 9, p. 2.22) shall be given followed by the words "BEFORE COATING."
Example: (Major and PD limits for AFTER COATING are those in table 2.21 for class 3A.)

## 250-28 UNF-3A

MAJOR DIA. . 2500 MAX $\backslash$ AFTER COATING PD . 2268 MAX f (Optional) MAJOR DIA .2488-. 2427 SPL $\backslash$ BEFORE PD .2256-. 2235 SPL COATING

For coated (or plated) class 1B, 2B, or 3B internal threads the min minor diameter and min pitch diameter may optionally be given followed by the words "AFTER COATING." The minor and pitch diameter limits of size before coating (calculated in accordance with par. 9, p. 2.22) shall be given followed by the words "BEFORE COATING."

Examples: (The after coating limits for all of the examples given are the minor and PD limits in table 2.21 for the respective class of thread. The before coating limits for all of the examples are calculated using the 2 A allowance where it is suitable for a minimum coating (or plating) thickness of 0.0002 in. on the thread flanks.)

```
.250-20 UNC-1B
MINOR DIA . 196 MIN\AFTER COATING
PD .2175 MIN f(Optional)
MINOR DIA .197-.208 SPL/BEFORE
PD .2186-.2259 SPL /COATING
.750-10 UNC-2B
MINOR DIA .642 MIN\AFTER COATING
PD .6850 MIN \(Optional)
MINOR DIA .644-.665 SPL\BEFORE
PD .6868-.6945 SPL /COATING
.250-28 UNF-3B
MINOR DIA . 2110 MIN |AFTER COATING PD . 2268 MIN \(\int\) (Optional)
MINOR DIA .2122-. 2198 SPL\BEFORE
PD .2280-. 2308 SPL
JCOATING
```

10.2. Designating Left Hand Threads.-Unless otherwise specified, threads are right-hand; a left-hand thread shall be designated LH as follows:

## .250-20 UNC-3A-LH

10.3. Designating UNS Threads (With Unified Tolerance Formulations).-UNS threads have the basic form of designation set out above, supplemented always by the limits of size.

Examples:

```
.250-24 UNS-3A
MAJOR DIA .2500-.2428
PD .2229-.2201
.495-20 UNS-3A
MAJOR DIA .4950-.4869
PD .4625-.4593
1.200-10 UNS-2B
MINOR DIA 1.092-1.113
PD 1.1350-1.1432
```

10.4. Designating Threads Having Special Length Of Engagement.-When a standard series thread has a special length of engagement differing from that for which the standard pitch diameter tolerances are applicable, as indicated in par. 7, Length of engagement, p. 2.21, the thread class symbol is qualified by the addition of the letters SE (special engagement) preceding the class symbol. The specification of the special pitch diameter limits of size and the length of engagement (LE) rounded to a two-place decimal are a requirement.

Examples

```
.500-13 UNC-SE2A
PD .4485-.4431
LE 1.00
```

.250-24 UNS-SE3A
MAJOR DIA .2500-. 2428
PD .2229-. 2198
LE . 88
10.5. Designating Threads Having Modified Crests.-It is occasionally necessary to modify the limits of size of the major diameter of an external thread or the minor diameter of an internal thread to fit a specific application but without change in class of thread or pitch diameter limits. (It should be noted that standard pitch diameter gages may be used to accept such threads). Such threads shall be specified with the established thread designation followed by the designation "MOD" and a statement of the modified diameter limits.

Examples:

```
.375-24 UNF-3A MOD
MAJOR DIA . 3720-. }3648\mathrm{ MOD
1.500-10 UNS-3B MOD
MINOR DIA 1.398-1.409 MOD
PD 1.4350-1.4412
```

10.6. Designating Threads For Acceptance By Other Than General Practice.-Threads to be accepted by gaging practices deviating from those outlined in section 6 require additional notes in the thread designation. The recommended methods of designating these threads are described in the following:
10.6.1. Designating class 3A threads for LO functional (virtual) diameters.-When it is desired to gage the minimum pitch diameter limits of class 3 A external threads as functional (virtual) diameter, instead of as specified in section 6, the words "LO FUNCTIONAL DIAMETER" following the pitch diameter limits should be included in addition to the information normally given, as follows:
.375-24 UNF-3A
PD .3468-. 3430
LO FUNCTIONAL DIAMETER
10.6.2. Designating class 2A threads for LO pitch diameters.-When it is desired to gage the minimum pitch diameter limits of class 2A external threads as a single element instead of as specified in section 6, the words "LO PITCH DIAMETER" following the pitch diameter limits should be included in addition to the information normally given, as follows:

```
.375-16 UNC-2A
PD .3331-.3287
LO PITCH DIAMETER
```

10.7. Designating Other Threads.-Threads having tolerances that do not conform to Unified formulation, and threads having multiple starts or special form, also require additional data in the thread designation. The recommended methods of designating these threads are described in the following:
10.7.1. Designating threads having tolerances not to Unified formulation.-If a standard series thread is altered in any respect other than revised pitch diameter limits for a special length of engagement, the modification of crests or the adjustment of the limits of size to accommodate coating, as shown previously, it is designated in accordance with the following examples:

```
.500-13 UNIFIED FORM SPECIAL-INT
MINOR DIA .424-.434 SPL
PD .4500-.4580 SPL
LE .50
```

.4375-24 UNIFIED FORM SPECIAL-EXT
MAJOR DIA . $4340-.4280$ SPL
PD . $4065-.4025 \mathrm{SPL}$
LE . 38
10.7.2. Designating multiple-start threads.-If a thread is required with a multiple start, it is designated by specifying sequentially in decimals the nominal size, pitch, and lead as follows: (The number of starts is obtained by dividing the lead by the pitch.)

```
.75-.0625P-.1875L-(3 START)-UNIFIED
FORM SPECIAL-EXT
MAJOR DIA .7485-.7391
PD .7079-:7003 SPL
LE . }7
```

10.7.3. Designating special form threads.-If a thread for design considerations requires a deviation from Unified standard thread contour and is not covered by another recognized standard, such as when the detail of the root differs from that for the standard thread form, the designation shall neither include the letters "UN" nor the word "UNIFIED" but shall be as follows:
.875-18 SPECIAL FORM-EXT
THREAD ANGLE $60^{\circ}$
MAJOR DIA .8750-. 8668
PD .8384-. 8343
MAX MINOR DIA . 8068 (as gaged)
LE . 69

Note. The "as gaged" diameter describes the maximum minor diameter of the GO thread ring gage.
10.7.4. Designating threads with long lengths of engagement.- In the assembly of threads in mating parts, the length of engagement varies according to the design requirements. It should be noted that the length of engagement is not necessarily the same as the full thread length provided on the part, but is the length of assembled thread in the mating parts.

In some instances, the length of engagement may be longer than that which is applicable to the tolerances for the standard length of engagement and additional precautions are necessary to assure proper assembly. In the case of custom parts, this may be taken into consideration when designing the parts. The proper pitch diameter tolerance may be obtained from the step tables in section 3 or computed from the formulas. The length of engagement shall be included in the designation as specified previously.

## 11. LIMITS OF SIZE FOR UNIFIED STANDARD SCREW THREAD SERIES

The limits of size, allowances, and pitch diameter tolerances for the Unified standard screw thread series are given in table 2.21. The sizes listed in table 2.21 are those shown in table 2.7 except for the omission of the secondary sizes over 2.5 in nominal size in the 4UN series, all sizes over 5 in . in the 6UN series, and all sizes over 4 in . in the 8UN series. However, the basic dimensions for these sizes omitted from table 2.21 are given in tables 2.11, 2.12, and 2.13.

The maximum-material pitch diameter limits (maximum external and minimum internal threads) are a limitation of the virtual diameter (effective size) for all thread classes. The minimum-material pitch diameter limits are to be interpreted in accordance with par. 8 Limits of size, p. 2.21.

Concerning class 2A threads with an additive finish, footnote b of table 2.21 on p. 2.37 should be specifically noted.

## 12. GAGES

Threads covered by this section shall be gaged in accordance with section 6 .

Table 2.21. Standard series limits of size-Unified screw threads


See footnotes at end of table.

Table 2.21. Standard series limits of size-Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Externala |  |  |  |  |  |  |  |  | Internala |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Allowance | Major diameter limits |  |  | Pitch diameter limits |  |  | Minor diameter ${ }^{\text {d }}$ | Class | Minor diameter limits |  | Pitch diameter limits |  |  | Major diameter <br> Min |
|  |  |  |  | Max ${ }^{\text {b }}$ | Min | Min ${ }^{\text {c }}$ | Max ${ }^{\text {b }}$ | Min | Tolerance |  |  | Min | Max | Min | Max | Tolerance |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| . $3125-32$ | UNEF | 2 A | $\begin{gathered} i n \\ 0.0010 \\ .0000 \end{gathered}$ | $\begin{aligned} & \text { in } \\ & 0.3115 \\ & .3125 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & 0.3055 \\ & .3065 \end{aligned}$ | in | in 0.2912 .2922 | in 0.2880 .2898 | in 0.0032 .0024 | $i n$ 0.2732 .2742 | 2B | in 0.279 .2790 | in 0.286 .2847 | in 0.2922 .2922 | in 0.2964 .2953 | in 0.0042 .0031 | in 0.3125 .3125 |
| .375-16 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0013 .0013 .0000 | .3737 .3737 .3750 | $\begin{array}{r} .3595 \\ .3643 \\ .3656 \end{array}$ | 0.3595 | .3331 .3331 .3344 | .3266 .3287 .3311 | .0065 .0044 .0033 | .2970 .2970 .2983 | 18 28 3 B | .307 .307 .3070 | .321 .321 .3182 | .3344 .3344 .3344 | .3429 .3401 .3387 | .0085 .0057 .0043 | .3750 .3750 .3750 |
| . $375-20$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 00012 | .3738 .3750 | $\begin{array}{r} .3657 \\ .3669 \end{array}$ |  | . 3413 | .3372 .3394 | . 00041 | .3125 .3137 | 2B 3 3 | .321 .3210 | .332 .3297 | .3425 .3425 | .3479 .3465 | . 0054 | .3750 .3750 |
| . $375-24$ | UNF | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0011 .0011 .0000 | .3739 .3739 .3750 | .3631 .3667 .3678 |  | .3468 .3468 .3479 | .3411 .3430 .3450 | .0057 .0038 .0029 | .3228 .3228 .3239 | 1B 2B 3 B | .330 .330 .3300 | .340 .340 .3372 | .3479 .3479 .3479 | .3553 .3528 .3516 | .0074 .0049 .0037 | $\begin{aligned} & .3750 \\ & .3750 \\ & .3750 \end{aligned}$ |
| . $375-28$ | UN | 2A | .0011 .0000 | .3739 .3750 | .3674 .3685 |  | . 3507 | .3471 .3491 | . 0036 | .3301 .3312 | 2B | .336 .3360 | . 345 | .3518 <br> .3518 | . 3564 | .0046 .0035 | .3750 .3750 |
| . $375-32$ | UNEF | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0010 .0000 | .3740 .3750 | .3680 .3690 |  | .3547 .3547 | .3503 .3522 | .0034 .0025 | .3357 .3367 | ${ }_{3 \mathrm{~B}}^{2 \mathrm{~B}}$ | .341 .3410 | .349 .3469 | .3547 <br> .3547 | .3591 .3580 | .0044 .0033 | .3750 .3750 |
| . 4375 -14 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0014 .0014 .0000 | .4361 .4361 .4375 | .4206 .4258 .4272 | . 4206 | .3897 .3897 .3911 | .3826 .3850 .3876 | .0071 .0047 .0035 | .3485 .3485 .3499 | 1B 2 B 3 B | .360 .360 .3600 | .376 .376 .3717 | .3911 .3911 .3911 | .4003 .3972 .3957 | .0092 .0061 .0046 | .4375 .4375 .4375 |
| .4375-16 | UN | 2 A | . 0014 | .4361 .4375 | . 4268 |  | .3955 .3969 | .3909 .3935 | .0046 .0034 | .3594 .3608 | $2 \mathrm{3B}$ | .370 <br> .3700 | .384 .3800 | .3969 .3969 | . 4028 | .0059 .0045 | . 4375 |
| . $4375-20$ | UNF | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0013 \\ & .0013 \\ & .0000 \end{aligned}$ | .4362 .4362 .4375 | .4240 .4281 .4294 |  | .4037 .4037 .4050 | .3974 .3995 .4019 | .0063 .0042 .0031 | .3749 .3749 .3762 | 18 2 B 3 B | .383 .383 .3830 | .395 .395 .3916 | .4050 .4050 .4050 | .4131 .4104 .4091 | .0081 .0054 .0041 | .4375 .4375 .4375 |
| . $4375-28$ | UNEF | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 00011 | .4364 .4375 | . 4299 |  | .4132 .4143 | .4096 .4116 | .0036 .0027 | .3926 .3937 | $2 \mathrm{3B}$ | . 3999 | . 407051 | . 4143 | .4189 .4178 | .0046 .0035 | .4375 .4375 |
| .4375-32 | UN | 2A | .0010 .0000 | .4365 .4375 | .4305 .4315 |  | . 4162 | .4128 .4147 | .0034 .0025 | .3982 .3992 | 2B 3 B | . 404 | . 4111 | .4172 .4172 | .4216 .4205 | . 0044 | .4375 .4375 |
| .500-13 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0015 .0015 .0000 | .4985 .4985 .5000 | .4822 .4876 .4891 | . 4822 | .4485 .4485 .4500 | .4411 .4435 .4463 | .0074 .0050 .0037 | .4041 .4041 .4056 | 18 28 3 B | .417 .417 .4170 | .434 .434 .4284 | .4500 .4500 .4500 | .4597 .4565 .4548 | .0097 .0065 .0048 | .5000 .5000 .5000 |
| .500-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0014 .0000 | .4986 .5000 | .4892 .4906 |  | .4580 .4594 | .4533 .4559 | .0047 .0035 | .4219 .4233 | 2B 3 3 | $\begin{aligned} & .432 \\ & .4320 \end{aligned}$ | . 44419 | . 4.4594 | .4655 .4640 | . 0061 | .5000 .5000 |
| .500-20 | UNF | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0013 .0013 .0000 | .4987 .4987 .5000 | .4865 .4906 .4919 |  | .4662 .4662 .4675 | .4598 .4619 .4643 | .0064 .0043 .0032 | .4374 .4374 .4387 | 18 28 3 B | .446 .446 .4460 | .457 .457 .4537 | .4675 .4675 .4675 | .4759 .4731 .4717 | .0084 .0056 .0042 | .5000 .5000 .5000 |
| . $500-28$ | UNEF | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{gathered} .0011 \\ .0000 \end{gathered}$ | .4989 .5000 | $\begin{array}{r} .4924 \\ .4935 \end{array}$ |  | .4757 .4768 | .4720 .4740 | . 0037 | . 4551 | ${ }_{3}^{2 B}$ | $.461$ | . 47076 | .4768 .4768 | .4816 .4804 | . 0048 | .5000 .5000 |
| . $500-32$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0010 .0000 | .4990 .5000 | $\begin{array}{r} .4930 \\ .4940 \end{array}$ |  | .4787 .4797 | .4752 .4771 | .0035 .0026 | . 46078 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .466 \\ & .4660 \end{aligned}$ | .474 .4719 | . 4797 | .4842 .4831 | . 0045 | .5000 .5000 |
| .5625-12 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0016 .0016 .0000 | .5609 .5609 .5625 | .5437 .5495 .5511 | . 5437 | .5068 .5068 .5084 | .4990 .5016 .5045 | .0078 .0052 .0039 | .4587 .4587 .4603 | 1B 2 B 3 B | .472 .472 .4720 | .490 .490 .4843 | .5084 .5084 .5084 | .5186 .5152 .5135 | .0102 .0068 .0051 | .5625 .5625 .5625 |
| . $5625-16$ | UN | 2 A 3 A | .0014 .0000 | $\begin{array}{r} .5611 \\ .5625 \end{array}$ | $.5517$ |  | $\begin{aligned} & .5205 \\ & .5219 \end{aligned}$ | .5158 .5184 | .0047 .0035 | . 484848 | 2 B 3 B | . 495 | .509 .5040 | .5219 .5219 | .5280 .5265 | . 00661 | .5625 .5625 |
| . $5625-18$ | UNF | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} .0014 \\ .0014 \\ .0000 \end{array}$ | $\begin{aligned} & .5611 \\ & .5611 \\ & .5625 \end{aligned}$ | $\begin{array}{r} .5480 \\ .5524 \\ .5538 \end{array}$ |  | $\begin{array}{r} .5250 \\ .5250 \\ .5264 \end{array}$ | $\begin{array}{r} .5182 \\ .5205 \\ .5230 \end{array}$ | .0068 .0045 .0034 | .4929 .4929 .4943 | $\begin{aligned} & 1 \mathrm{~B} \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .502 .502 .5020 | .515 .515 .5106 | .5264 .5264 .5664 | .5353 .5323 .5308 | .0089 .0059 .0044 | .5625 .5625 .5625 |
| . $5625-20$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0013 \\ & .0000 \end{aligned}$ | $\begin{aligned} & .5612 \\ & .5625 \end{aligned}$ | $\begin{aligned} & .5531 \\ & .5544 \end{aligned}$ |  | . 52887 | .5245 .5268 | . 0042 | . 4999 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .508 \\ & .5080 \end{aligned}$ | . 520 | .5300 .5300 | .5355 .5341 | . 0055 | .5625 .5625 |
| . $5625-24$ | UNEF | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0012 .0000 | $\begin{aligned} & .5613 \\ & .5625 \end{aligned}$ | $\begin{aligned} & .5541 \\ & .5553 \end{aligned}$ |  | $\begin{aligned} & .5342 \\ & .5354 \end{aligned}$ | $\begin{array}{r} .5303 \\ .5325 \end{array}$ | $\begin{array}{r} .0039 \\ .0029 \end{array}$ | $\begin{aligned} & .5102 \\ & .5114 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .517 \\ & .5170 \end{aligned}$ | .527 .5244 | $\begin{aligned} & .5354 \\ & .5354 \end{aligned}$ | .5405 .5392 | .0051 .0038 | .5625 .5625 |
| .5625-28 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0011 \\ & .0000 \end{aligned}$ | $\begin{array}{r} .5614 \\ .5625 \end{array}$ | $\begin{aligned} & .5549 \\ & .5560 \end{aligned}$ |  | $\begin{aligned} & .5382 \\ & .5393 \end{aligned}$ | $\begin{array}{r} .5345 \\ .5365 \end{array}$ | . 00037 | .5176 .5187 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .524 \\ & .5240 \end{aligned}$ | . 53321 | .5393 .5393 | .5441 .5429 | $\begin{aligned} & .0048 \\ & .0036 \end{aligned}$ | $\begin{aligned} & .5625 \\ & .5625 \end{aligned}$ |
| .5625-32 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 00010 | $\begin{aligned} & .5615 \\ & .5625 \end{aligned}$ | $\begin{aligned} & .5555 \\ & .5565 \end{aligned}$ |  | .5412 .5422 | $\begin{array}{r} .5377 \\ .5396 \end{array}$ | $\begin{aligned} & .0035 \\ & .0026 \end{aligned}$ | $\begin{aligned} & .5232 \\ & .5242 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .529 \\ & .5290 \end{aligned}$ | $\begin{aligned} & .536 \\ & .5344 \end{aligned}$ | . 5422 | .5467 .5456 | $\begin{aligned} & .0045 \\ & .0034 \end{aligned}$ | $\begin{aligned} & .5625 \\ & .5625 \end{aligned}$ |
| . 625-11 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0016 .0016 .0000 | $\begin{aligned} & .6234 \\ & .6234 \\ & .6250 \end{aligned}$ | $\begin{aligned} & .6052 \\ & .6113 \\ & .6129 \end{aligned}$ | . 6052 | $\begin{aligned} & .5644 \\ & .5644 \\ & .5660 \end{aligned}$ | $\begin{array}{r} .5561 \\ .5589 \\ .5619 \end{array}$ | $\begin{aligned} & .0083 \\ & .0055 \\ & .0041 \end{aligned}$ | .5119 .5119 .5135 | $\begin{aligned} & 1 \mathrm{~B} \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .527 \\ & .527 \\ & .5270 \end{aligned}$ | .546 .546 .5391 | .5660 .5660 .5660 | .5767 .5732 .5714 | $\begin{array}{r} .0107 \\ .0072 \\ .0054 \end{array}$ | .6250 .6250 .6250 |
| .625-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0016 \\ & .0000 \end{aligned}$ | $\begin{array}{r} .6234 \\ .6250 \end{array}$ | $\begin{array}{r} .6120 \\ .6136 \end{array}$ |  | $\begin{aligned} & .5693 \\ & .5709 \end{aligned}$ | $\begin{aligned} & .5639 \\ & .5668 \end{aligned}$ | $\begin{aligned} & .0054 \\ & .0041 \end{aligned}$ | $\begin{array}{r} .5112 \\ .5228 \end{array}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .535 \\ & .5350 \end{aligned}$ | $\begin{aligned} & .553 \\ & .5463 \end{aligned}$ | $\begin{aligned} & .5709 \\ & .5709 \end{aligned}$ | $\begin{aligned} & .5780 \\ & .5762 \end{aligned}$ | $\begin{aligned} & .0071 \\ & .0053 \end{aligned}$ | $\begin{array}{r} .6250 \\ .6250 \end{array}$ |

See footnotes at end of table.

Table 2.21. Standard series limits of size-Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Externala |  |  |  |  |  |  |  |  | Internala ${ }^{\text {a }}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Allowance | Major diameter limits |  |  | Pitch diameter limits |  |  | Minor diameter ${ }^{\text {d }}$ | Class | Minor diameter limits |  | Pitch diameter limits |  |  | Major diameter <br> Min |
|  |  |  |  | Max ${ }^{\text {b }}$ | Min | Minc | Max ${ }^{\text {b }}$ | Min | Tolerance |  |  | Min | Max | Min | Max | Tolerance |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| . 625-16 | UN | 2A | in 0.0014 .0000 | in 0.6236 .6250 | $\begin{gathered} i n \\ 0.6142 \\ .6156 \end{gathered}$ | in | in 0.5830 .5844 | in 0.5782 .5808 | in 0.0048 .0036 | $\begin{gathered} \text { in } \\ 0.5469 \\ .5483 \end{gathered}$ | 2B | in 0.557 .5570 | in 0.571 .5662 | $\begin{gathered} \text { in } \\ 0.5844 \\ .5844 \end{gathered}$ | $\begin{aligned} & \text { in } \\ & 0.5906 \\ & .5890 \end{aligned}$ | $i n$ 0.0062 .0046 | $\begin{aligned} & i n \\ & 0.6250 \\ & .6250 \end{aligned}$ |
| . $625-18$ | UNF | 1 A 2 A 3 A | .0014 .0014 .0000 | .6236 .6236 .6250 | .6105 .6149 .6163 |  | .5875 .5875 .5889 | .5805 .5828 .5854 | .0070 .0047 .0035 | .5554 .5554 .5568 | 1 B 2 B 3 B | .565 .565 .5650 | .578 .578 .5730 | .5889 .5889 .5889 | .5980 .5949 .5934 | .0091 .0060 .0045 | .6250 .6250 .6250 |
| . $625-20$ | UN | ${ }_{3}^{2 A}$ | .0013 .0000 | .6237 .6250 | .6156 .6169 |  | .5912 .5925 | .5869 .5893 | . 0043 | . 5624 | 2 B 3 B | . 571 | .582 .5787 | .5925 .5925 | .5981 .5967 | .0056 | .6250 .6250 |
| . $625-24$ | UNEF | 2A | .0012 .0000 | .6238 .6250 | .6166 .6178 |  | .5967 .5979 | .5927 .5949 | .0040 .0030 | .5727 .5739 | 2B 3 B | .580 .5800 | . 5980 | .5979 .5879 | . 60318 | . 00052 | .6250 .6250 |
| . 625-28 | UN | 2 AA | . 00011 | .6239 .6250 | .6174 .6185 |  | .6007 .6018 | .5969 .5990 | . 00038 | .5801 .5812 | 2B | .586 .5860 | .595 .5926 | .6018 .6018 | $\begin{array}{r}.6067 \\ .6055 \\ \hline\end{array}$ | . 0049 | .6250 .6250 |
| .625-32 | UN | 2 A | . 00011 | .6239 .6250 | .6179 .6190 |  | .6036 .6047 | .6000 .6020 | .0036 | .5856 .5867 | 2B ${ }_{3}$ | .591 .5910 | .599 .5969 | .6047 .6047 | .6093 .6082 | .0046 .0035 | .6250 .6250 |
| . 6875-12 | UN | 2A | .0016 .0000 | .6859 .6875 | .6745 .6761 |  | 6318 .6334 | .6264 .6293 | .0054 .0041 | .5837 .5853 | 2B 3 B | .597 .5970 | . 615 | .6334 .6334 | .6405 .6387 | . 00071 | .6875 .6875 |
| . $6875-16$ | UN | 2 A | . 00014 | . 68681 | .6767 .6781 |  | .6455 .6469 | .6407 .6433 | .0048 .0036 | .6094 .6108 | 2B 3 B | .620 .6200 | .634 .6284 | .6469 .6469 | .6531 .6515 | . 00062 | .6875 .6875 |
| . $6875-20$ | UN | ${ }_{3}^{2 A}$ | .0013 .0000 | .6862 .6875 | .6781 .6794 |  | .6537 .6550 | .6494 .6518 | . 00043 | .6249 .6262 | 2B 3 B | $\begin{aligned} & .633 \\ & .6330 \end{aligned}$ | .645 .6412 | .6550 .6550 | .6606 .6592 | .0056 .0042 | .6875 .6875 |
| .6875-24 | UNEF | 2 A | . 00012 | .6863 .6875 | .6791 .6803 |  | .6592 .6604 | .6552 .6574 | .0040 .0030 | .6352 .6364 | 2B ${ }_{3}$ | . 642 | . 6542 | .6604 .6604 | .6656 .6643 | .0052 .0039 | . 68875 |
| . 6875-28 | UN | 2 A | .0011 .0000 | . 6864 | .6799 .6810 |  | .6632 .6643 | .6594 .6615 | . 00038 | .6426 .6437 | 2B 3 B | .649 .6490 | . 6557 | .6643 .6643 | .6692 .6680 | . 0049 | .6875 .6875 |
| . $6875-32$ | UN | 2 A | . 00011 | .6864 .6875 | .6804 .6815 |  | .6661 .6672 | .6625 .6645 | .0036 .0027 | .6481 .6492 | 2B | .654 .6540 | .661 .6594 | .6672 .6672 | .6718 .6707 | .0046 .0035 | .6875 .6875 |
| .750-10 | UNC | 1 A 2 A 3 A | .0018 .0018 .0000 | .7482 .7482 .7500 | .7288 .7353 .7371 | 0.7288 | .6832 .6832 .6850 | .6744 .6773 .6806 | .0088 .0059 .0044 | .6255 .6255 .6273 | 1B 2B 3 B | .642 .642 .6420 | .663 .663 .6545 | .6850 .6850 .6850 | .6965 .6927 .6907 | .0115 .0077 .0057 | .7500 .7500 .7500 |
| . $750-12$ | UN | 2A | .0017 .0000 | .7483 .7500 | .7369 .7386 |  | .6942 .6959 | .6887 .6918 | .0055 | .6461 .6478 | 2B | . 66600 | . 6787 | .6959 .6959 | .7031 .7013 | .0072 | .7500 .7500 |
| . $750-16$ | UNF | 1 A 2 A 3 A | .0015 .0015 .0000 | .7485 .7485 .7500 | .7343 .7391 .7406 |  | .7079 .7079 .7094 | .7004 .7029 .7056 | .0075 .0050 .0038 | .6718 .6718 .6733 | 18 28 38 | .682 .682 .6820 | .696 .696 .6908 | .7094 .7094 .7094 | .7192 .7159 .7143 | .0098 .0065 .0049 | .7500 .7500 .7500 |
| . $750-20$ | UNEF | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0013 \\ & .0000 \end{aligned}$ | $\begin{aligned} & .7487 \\ & .7500 \end{aligned}$ | $\begin{aligned} & .7406 \\ & .7419 \end{aligned}$ |  | $\begin{aligned} & .7162 \\ & .7175 \end{aligned}$ | $\begin{array}{r} .7118 \\ .7142 \end{array}$ | . 00044 | .6874 .6887 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .696 \\ & .6960 \end{aligned}$ | $.707$ | $\begin{aligned} & .7175 \\ & .7175 \end{aligned}$ | .7232 .7218 | . 00057 | .7500 .7500 |
| .750-28 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0012 \\ & .0000 \end{aligned}$ | $\begin{aligned} & .7488 \\ & .7500 \end{aligned}$ | $\begin{aligned} & .7423 \\ & .7435 \end{aligned}$ |  | .7256 .7268 | .7218 .7239 | .0038 .0029 | .7050 .7062 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .711 \\ & .7110 \end{aligned}$ | $\begin{aligned} & .720 \\ & .7176 \end{aligned}$ | .7268 .7268 | $\begin{aligned} & .7318 \\ & .7305 \end{aligned}$ | .0050 | .7500 .7500 |
| .750-32 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{gathered} .0011 \\ .0000 \end{gathered}$ | .7489 .7500 | .7429 .7440 |  | .7286 .7297 | .7250 .7270 | $\begin{aligned} & .0036 \\ & .0027 \end{aligned}$ | $\begin{array}{r} .7106 \\ .7117 \end{array}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .716 \\ & .7160 \end{aligned}$ | $\begin{aligned} & .724 \\ & .7219 \end{aligned}$ | $\begin{aligned} & .7297 \\ & .7297 \end{aligned}$ | $\begin{aligned} & .7344 \\ & .7333 \end{aligned}$ | .0047 .0036 | .7500 .7500 |
| .8125-12 | UN | 2 A | $\begin{array}{r} .0017 \\ .0000 \end{array}$ | $\begin{aligned} & .8108 \\ & .8125 \end{aligned}$ | $\begin{aligned} & .7994 \\ & .8011 \end{aligned}$ |  | $\begin{aligned} & .7567 \\ & .7584 \end{aligned}$ | .7512 .7543 | . 00055 | $\begin{aligned} & .7086 \\ & .7103 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .722 \\ & .7220 \end{aligned}$ | $\begin{aligned} & .740 \\ & .7329 \end{aligned}$ | .7584 .7584 | .7656 .7638 | . 0072 | .8125 .8125 |
| . $8125-16$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0015 \\ & .0000 \end{aligned}$ | .8110 | .8016 .8031 |  | $\begin{aligned} & .7704 \\ & .7719 \end{aligned}$ | .7655 .7683 | .0049 | .7343 .7358 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .745 \\ & .7450 \end{aligned}$ | $.759$ | .7719 .7719 | .7782 .7766 | .0063 | .8125 .8125 |
| . $8125-20$ | UNEF | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 00013 | .81125 | .8031 .8044 |  | $\begin{aligned} & .7787 \\ & .7800 \end{aligned}$ | $\begin{aligned} & .7743 \\ & .7767 \end{aligned}$ | $.0044$ | $\begin{array}{r} .7499 \\ .7512 \end{array}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $.758$ | $\begin{aligned} & .770 \\ & .7662 \end{aligned}$ | $\begin{aligned} & .7800 \\ & .7800 \end{aligned}$ | .7857 .7843 | .0057 | .8125 .8125 |
| . $8125-28$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0012 \\ & .0000 \end{aligned}$ | $\begin{aligned} & .8113 \\ & .8125 \end{aligned}$ | $\begin{array}{r} .8048 \\ 8060 \end{array}$ |  | $\begin{aligned} & .7881 \\ & .7893 \end{aligned}$ | $\begin{aligned} & .7843 \\ & .7864 \end{aligned}$ | $\begin{aligned} & .0038 \\ & .0029 \end{aligned}$ | .7675 .7687 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .774 \\ & .7740 \end{aligned}$ | $\begin{aligned} & .782 \\ & .7801 \end{aligned}$ | $\begin{aligned} & .7893 \\ & .7893 \end{aligned}$ | $\begin{array}{r} .7943 \\ .7930 \end{array}$ | .0050 | .8125 |
| .8125-32 | UN | ${ }_{3 \mathrm{~A}}^{\mathrm{A}}$ | . 00011 | .8114 | . 8054 |  | .7911 .7922 | .7875 .7895 | .0036 | .7731 .7742 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .779 .7790 | $\begin{aligned} & .786 \\ & .78 \pm 4 \end{aligned}$ | .7922 .7922 | .7969 .7958 | . 0047 | .8125 .8125 |
| .875-9 | UNC | 1 A 2 A 3 A | .0019 .0019 .0000 | .8731 .8731 .8750 | .8523 .8592 .8611 | . 8523 | .8009 .8009 .8028 | .7914 .7946 .7981 | $\begin{array}{r} .0095 \\ .0063 \\ .0047 \end{array}$ | .7368 .7368 .7387 | $\begin{aligned} & 1 \mathrm{~B} \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .755 \\ & .755 \\ & .7550 \end{aligned}$ | .778 .778 .7681 | .8028 .8028 .8028 | .8151 .8110 .8089 | .0123 .0082 .0061 | .8750 .8750 .8750 |
| . $875-12$ | UN | ${ }_{3} \mathbf{2 A}$ | . 0017 | $\begin{aligned} & .8733 \\ & .8750 \end{aligned}$ | $\begin{array}{r} .8619 \\ .8636 \end{array}$ |  | .8192 .8209 | $.8137$ | $\begin{aligned} & .0055 \\ & .0041 \end{aligned}$ | $.7711$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .785 \\ & .7850 \end{aligned}$ | $\begin{aligned} & .803 \\ & .7952 \end{aligned}$ | $\begin{array}{r} .8209 \\ .8209 \end{array}$ | $.8281$ | $\begin{aligned} & .0072 \\ & .0054 \end{aligned}$ | .8750 |
| . $875-14$ | UNF | 1 A 2 A 3 A | $\begin{aligned} & .0016 \\ & .0016 \\ & .0000 \end{aligned}$ | .8734 .8734 .8750 | $\begin{aligned} & .8579 \\ & .8631 \\ & .8647 \end{aligned}$ |  | .8270 .8270 .8286 | $\begin{aligned} & .8189 \\ & .8216 \\ & .8245 \end{aligned}$ | $\begin{aligned} & .0081 \\ & .0054 \\ & .0041 \end{aligned}$ | $\begin{array}{r} .7858 \\ .7858 \\ .7874 \end{array}$ | $\begin{aligned} & 1 \mathrm{~B} \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .798 \\ & .798 \\ & .7980 \end{aligned}$ | $\begin{aligned} & .814 \\ & .814 \\ & .8068 \end{aligned}$ | $\begin{array}{r} .8286 \\ .8286 \\ .8286 \end{array}$ | $\begin{aligned} & .8392 \\ & .8356 \\ & .8339 \end{aligned}$ | .0106 .0070 .0053 | .8750 .8750 .8750 |

See footnotes at end of table.

Table 2.21. Standard series limits of size-Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Externala |  |  |  |  |  |  |  |  | Internala |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Allowance | Major dianeter limits |  |  | Pitch diameter limits |  |  | Minor diam. eter ${ }^{\text {d }}$ | Class | Minor diameter limits |  | Pitch diameter limits |  |  | Major diameter Min |
|  |  |  |  | Max ${ }^{\text {b }}$ | Min | Minc | Max ${ }^{\text {b }}$ | Min | Tolerance |  |  | Min | Max | Min | Max | Tolerance |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| .875-16 | UN | 2 A 3 A | in 0.0015 .0000 | in 0.8735 .8750 | in 0.8641 .8656 | in | in 0.8329 .8344 | in 0.8280 .8308 | in 0.0049 .0036 | $\begin{gathered} \text { in } \\ 0.7968 \\ .7983 \end{gathered}$ | 2B ${ }^{\text {B }}$ | in 0.807 .8070 | in 0.821 .8158 | in 0.8344 .8344 | in 0.8807 .8391 | $\begin{gathered} \text { in } \\ 0.0063 \\ .0047 \end{gathered}$ | $\begin{aligned} & \text { in } \\ & 0.8750 \\ & .8750 \end{aligned}$ |
| .875-20 | UNEF | 2 A | .0013 .0000 | .8737 .8750 | .8656 .8669 |  | . 8412 | .8368 .8392 | . 00044 | .8124 .8137 | $2 \mathrm{3B}$ | . 821 | .832 | .8425 .8425 | .8482 .8468 | . 0057 | $\begin{aligned} & .8750 \\ & .8750 \end{aligned}$ |
| . $875-28$ | UN | 2A | . 0012 | .8738 .8750 | .8673 .8685 |  | .8506 .8518 | .8468 .8489 | .0038 .0029 | .8300 .8312 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .836 | .845 | .8518 <br> .8518 | .8568 .8555 | . 0050 | $\begin{aligned} & .8750 \\ & .8750 \end{aligned}$ |
| . $875-32$ | UN | 2 A 3 A | .0011 .0000 | .8739 .8750 | .8679 .8690 |  | .8536 .8547 | .8500 .8520 | . 00036 | .8356 | 2B 3 B | . 8411 | . 849 | .8547 .8547 | .8594 .8583 | .0047 .0036 | . 8750 |
| .9375-12 | UN | 2 AA | .0017 .0000 | .9358 .9375 | $\begin{aligned} & .9244 \\ & .9261 \end{aligned}$ |  | . 88817 | .8760 .8792 | . 00057 | . 83336 | $\begin{aligned} & \text { 2B } \\ & 3 \mathrm{~B} \end{aligned}$ | $.847$ | .865 | .8834 .8834 | $\begin{aligned} & .8908 \\ & .8889 \end{aligned}$ | $\begin{aligned} & .0074 \\ & .0055 \end{aligned}$ | .9375 .9375 |
| .9375-16 | UN | $2{ }_{3}^{2 A}$ | .0015 .0000 | .9360 <br> .9375 | . 92686 |  | . 89594 | .8904 | .0050 | .8593 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 87800 | . 8878 | . 898969 | .9034 .9018 | . 0065 | $\begin{aligned} & .9375 \\ & .9375 \end{aligned}$ |
| . $9375-20$ | UNEF | 2 A 3 A | .0014 .0000 | .9361 .9375 | . 9288 |  | .9036 <br> .9050 | .8991 .9016 | .0045 .0034 | .8748 .8762 | $2 \mathrm{3B}$ | . 88830 | .895 .8912 | .9050 .9050 | . 9109 | .0059 .0044 | . 9375 |
| .9375-28 | UN | 2A | .0012 <br> .0000 | .9363 <br> .9375 | . 929810 |  | .9131 .9143 | . 9091 | .0040 | . 89825 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .899 .8990 | . 907 | .9143 .9143 | . 9195 | . 0052 | $\begin{array}{r} .9375 \\ .9375 \end{array}$ |
| . $9375-32$ | UN | 2 A | . 0011 | .9364 .9375 | .9304 .9315 |  | .9161 .9172 | .9123 .9144 | .0038 | . 89881 | 2B | . 904 | . 911 | .9172 .9172 | . 92201 | . 0049 | .9375 .9375 |
| 1.000-8 | UNC | 14 24 34 | .0020 .0020 .0000 | .9980 .9980 1.0000 | .9755 .9830 .9850 | 0.9755 | .9168 .9168 .9188 | .9067 .9100 .9137 | .0101 .0068 .0051 | .8446 .8446 .8466 | $\begin{aligned} & 1 \mathrm{~B} \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .865 .865 .8650 | .890 .890 .8797 | .9188 .9188 .9188 | .9320 .9276 .9254 | .0132 .0088 .0066 | 1.0000 1.0000 1.0000 |
| 1.000-12 | UNF | 1 A 2 A 3 A | .0018 .0018 .0000 | .9982 .9982 1.0000 | .9810 .9868 .9886 |  | .9441 .9441 .9459 | .9353 .9382 .9415 | .0088 .0059 .0044 | .8960 .8960 .8978 | $\begin{aligned} & 1 \mathrm{~B} \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .910 .910 .9100 | .928 .928 .9198 | .9459 .9459 .9459 | .9573 .9535 .9516 | .0114 .0076 .0057 | 1.0000 1.0000 1.0000 |
| $1.000-16$ | UN | 2 A | . 0015 | .9985 1.0000 | .9891 .9906 |  | .9579 .9594 | . 9529 | .0050 .0037 | . 92218 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 932 | .946 .9408 | .9594 .9594 | . 9659 | .0065 .0049 | 1.0000 1.0000 |
| 1.000-20 | UNEF | 2 A | $\begin{gathered} .0014 \\ .0000 \end{gathered}$ | $\begin{array}{r} .9986 \\ 1.0000 \end{array}$ | $\begin{aligned} & .9905 \\ & .9919 \end{aligned}$ |  | . 96661 | . 9616 | .0045 .0034 | .9373 .9387 | $2 \mathrm{3B}$ | .946 .9460 | . 957 | .9675 .9675 | .9734 .9719 | . 0059 | 1.0000 1.0000 |
| 1.000-28 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 0012 | $\begin{array}{r} .9988 \\ 1.0000 \end{array}$ | $\begin{array}{r} .9923 \\ .9935 \end{array}$ |  | $\begin{aligned} & .9756 \\ & .9768 \end{aligned}$ | $\begin{aligned} & .9716 \\ & .9738 \end{aligned}$ | . 0040 | .9550 .9562 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .961 \\ & .9610 \end{aligned}$ | .970 .9676 | . 97688 | . 98800 | . 0052 | $\begin{aligned} & 1.0000 \\ & 1.0000 \end{aligned}$ |
| 1.000-32 | UN | 2 A | . 0011 | .9989 1.0000 | . 9929 |  | .9786 .9797 | .9748 .9769 | .0038 .0028 | .9606 .9617 | 2B | . 9666 | . 974 | .9797 .9797 | . 9846 | .0049 .0037 | 1.0000 1.0000 |
| 1.0625-8 | UN | $\underset{3 \mathrm{~A}}{2 \mathrm{~A}}$ | $\begin{aligned} & .0020 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.0605 \\ & 1.0625 \end{aligned}$ | $\begin{aligned} & 1.0455 \\ & 1.0475 \end{aligned}$ |  | $\begin{aligned} & .9793 \\ & .9813 \end{aligned}$ | $\begin{array}{r} .9725 \\ .9762 \end{array}$ | $\begin{aligned} & .0068 \\ & .0051 \end{aligned}$ | $\begin{array}{r} .9071 \\ .9091 \end{array}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $.927$ | $\begin{aligned} & .952 \\ & .9422 \end{aligned}$ | $\begin{aligned} & .9813 \\ & .9813 \end{aligned}$ | . 99802 | $\begin{aligned} & .0089 \\ & .0067 \end{aligned}$ | $\begin{aligned} & 1.0625 \\ & 1.0625 \end{aligned}$ |
| $1.0625-12$ | UN | ${ }_{3}^{2 A}$ | . 00017 | 1.0608 1.0625 | $\begin{aligned} & 1.0494 \\ & 1.0511 \end{aligned}$ |  | 1.0067 | 1.0010 1.0042 | .0057 | .9586 .9603 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .972 .9720 | $.990$ | 1.0084 | 1.0158 1.0139 | .0074 | $\begin{aligned} & 1.0625 \\ & 1.0625 \end{aligned}$ |
| 1.0625-16 | UN | 2 A | $\begin{aligned} & .0015 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.0610 \\ & 1.0625 \end{aligned}$ | $\begin{aligned} & 1.0516 \\ & 1.0531 \end{aligned}$ |  | 1.0204 | $\begin{aligned} & 1.0154 \\ & 1.0182 \end{aligned}$ | $\begin{gathered} .0050 \\ .0037 \end{gathered}$ | $\begin{aligned} & .9843 \\ & .9858 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .995 \\ & .9950 \end{aligned}$ | $\begin{aligned} & 1.009 \\ & 1.0033 \end{aligned}$ | $\begin{aligned} & 1.0219 \\ & 1.0219 \end{aligned}$ | $\begin{aligned} & 1.0284 \\ & 1.0268 \end{aligned}$ | .0065 | $\begin{aligned} & 1.0625 \\ & 1.0625 \end{aligned}$ |
| $1.0625-18$ | UNEF | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | . 0014 | $\begin{aligned} & 1.0611 \\ & 1.0625 \end{aligned}$ | $\begin{aligned} & 1.0524 \\ & 1.0538 \end{aligned}$ |  | 1.0250 | 1.0203 1.0228 | .0047 | .9929 .9943 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.002 \\ & 1.0020 \end{aligned}$ | $\begin{aligned} & 1.015 \\ & 1.0105 \end{aligned}$ | 1.0264 | $\begin{aligned} & 1.0326 \\ & 1.0310 \end{aligned}$ | .0062 | $\begin{aligned} & 1.0625 \\ & 1.0625 \end{aligned}$ |
| 1.0625-20 | UN | 2 A 3 A | . 00014 | 1.0611 1.0625 | 1.0530 1.0544 |  | 1.0286 1.0300 | 1.0241 1.0266 | .0045 .0034 | .9998 1.0012 | $2 \mathrm{3B}$ | 1.008 1.0080 | 1.020 1.0162 | 1.0300 1.0300 | 1.0359 1.0344 | .0059 | 1.0625 1.0625 |
| 1.0625-28 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0012 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.0613 \\ & 1.0625 \end{aligned}$ | $\begin{aligned} & 1.0548 \\ & 1.0560 \end{aligned}$ |  | 1.0381 | 1.0341 1.0363 | .0040 | $\begin{aligned} & 1.0175 \\ & 1.0187 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.024 \\ & 1.0240 \end{aligned}$ | $\begin{aligned} & 1.032 \\ & 1.0301 \end{aligned}$ | $\begin{aligned} & 1.0393 \\ & 1.0393 \end{aligned}$ | 1.0445 1.0432 | . 00532 | $\begin{aligned} & 1.0625 \\ & 1.0625 \end{aligned}$ |
| 1.125-7 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0022 .0022 .0000 | 1.1228 1.1228 1.1250 | 1.0982 1.1064 1.1086 | 1.0982 | 1.0300 1.0300 1.0322 | 1.0191 1.0228 1.0268 | .0109 .0072 .0054 | .9475 .9475 .9497 | $\begin{aligned} & 1 \mathrm{~B} \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 0.970 .970 .9700 | 0.998 .998 .9875 | 1.0322 1.0322 1.0322 | 1.0463 1.0416 1.0393 | .0141 .0094 .0071 | $\begin{aligned} & 1.1250 \\ & 1.1250 \\ & 1.1250 \end{aligned}$ |
| 1.125-8 | UN | $2{ }_{3}^{2 A}$ | . 0021 | 1.1229 1.1250 | 1.1079 1.1100 | 1.1004 | 1.0417 1.0438 | 1.0348 1.0386 | .0069 .0052 | .9695 .9716 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 990 | 1.015 1.0047 | 1.0438 1.0438 | 1.0528 1.0505 | .0090 .0067 | 1.1250 1.1250 |
| 1.125-12 | UNF | 1 A 2 A 3 A | .0018 .0018 .0000 | 1.1232 1.1232 1.1250 | $\begin{aligned} & 1.1060 \\ & 1.1118 \\ & 1.1136 \end{aligned}$ |  | 1.0691 1.0691 1.0709 | 1.0601 1.0631 1.0664 | .0090 .0060 .0045 | $\begin{aligned} & 1.0210 \\ & 1.0210 \\ & 1.0228 \end{aligned}$ | $\begin{aligned} & 1 \mathrm{~B} \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.035 \\ & 1.035 \\ & 1.0350 \end{aligned}$ | 1.053 1.053 1.0448 | 1.0709 1.0709 1.0709 | 1.0826 1.0787 1.0768 | .0117 .0078 .0059 | 1.1250 1.1250 1.1250 |
| 1.125-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0015 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.1235 \\ & 1.1250 \end{aligned}$ | $\begin{aligned} & 1.1141 \\ & 1.1156 \end{aligned}$ |  | 1.0829 | 1.0779 1.0807 | . 00050 | 1.0468 1.0483 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.057 \\ & 1.0570 \end{aligned}$ | $\begin{aligned} & 1.071 \\ & 1.0658 \end{aligned}$ | $\begin{aligned} & 1.0844 \\ & 1.0844 \end{aligned}$ | 1.0909 1.0893 | . 0065 | 1.1250 1.1250 |
| 1.125-18 | UNEF | $\underset{3 \mathbf{A}}{2 \mathbf{A}}$ | $\begin{aligned} & .0014 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.1236 \\ & 1.1250 \end{aligned}$ | $\begin{aligned} & 1.1149 \\ & 1.1163 \end{aligned}$ |  | $\begin{aligned} & 1.0875 \\ & 1.0889 \end{aligned}$ | $\begin{aligned} & 1.0828 \\ & 1.0853 \end{aligned}$ | $\begin{aligned} & .0047 \\ & .0036 \end{aligned}$ | $\begin{aligned} & 1.0554 \\ & 1.0568 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.065 \\ & 1.0650 \end{aligned}$ | $\begin{aligned} & 1.078 \\ & 1.0730 \end{aligned}$ | $\begin{aligned} & 1.0889 \\ & 1.0889 \end{aligned}$ | $\begin{aligned} & 1.0951 \\ & 1.0935 \end{aligned}$ | . 0062 | 1.1250 1.1250 |
| 1.125-20 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathbf{A} \end{aligned}$ | $\begin{aligned} & .0014 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.1236 \\ & 1.1250 \end{aligned}$ | $\begin{aligned} & 1.1155 \\ & 1.1169 \end{aligned}$ | --- | $\begin{aligned} & 1.0911 \\ & 1.0925 \end{aligned}$ | $\begin{aligned} & 1.0866 \\ & 1.0891 \end{aligned}$ | $\begin{aligned} & .0045 \\ & .0034 \end{aligned}$ | $\begin{aligned} & 1.0623 \\ & 1.0637 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.071 \\ & 1.0710 \end{aligned}$ | $\begin{aligned} & 1.082 \\ & 1.0787 \end{aligned}$ | $\begin{aligned} & 1.0925 \\ & 1.0925 \end{aligned}$ | $\begin{aligned} & 1.0984 \\ & 1.0969 \end{aligned}$ | $\begin{aligned} & .0059 \\ & .0044 \end{aligned}$ | $\begin{aligned} & 1.1250 \\ & 1.1250 \end{aligned}$ |

see footnotes at end of table.

Table 2.21. Standard series limits of size-Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Externala |  |  |  |  |  |  |  |  | Internal ${ }^{\text {a }}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Allowance | Major diameter limits |  |  | Piteh diameter limits |  |  | Minor diameter ${ }^{\text {d }}$ | Class | Minor diameter limits |  | Piteh diameter limits |  |  | Major diameter |
|  |  |  |  | Max ${ }^{\text {b }}$ | Min | Min ${ }^{\circ}$ | Max ${ }^{\text {b }}$ | Min | Tolerance |  |  | Min | Max | Min | Max | Tolerance |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | . 13 | 14 | 15 | 16 | 17 | 18 |
| 1.125-28 | UN | 2A | $\begin{aligned} & \text { in } \\ & 0.0012 \\ & .0000 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & 1.1238 \\ & 1.1250 \end{aligned}$ | $\begin{gathered} i n \\ 1.1173 \\ 1.1185 \end{gathered}$ | in | $\begin{gathered} i n \\ 1.1006 \\ 1.1018 \end{gathered}$ | $\begin{aligned} & \text { in } \\ & 1.0966 \\ & 1.0988 \end{aligned}$ | $\begin{gathered} i \mathrm{n} \\ 0.0040 \\ .0030 \end{gathered}$ | $\begin{aligned} & i n \\ & 1.0800 \\ & 1.0812 \end{aligned}$ | ${ }_{3}^{2 \mathrm{~B}}$ | $\begin{aligned} & \text { in } \\ & 1.086 \\ & 1.0860 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & 1.095 \\ & 1.0926 \end{aligned}$ | $\begin{aligned} & i_{\mathrm{n}} \\ & 1.1018 \\ & 1.1018 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & 1.1070 \\ & 1.1057 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & 0.0052 \\ & .0039 \end{aligned}$ | 1.1250 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.1875-8 | UN | 2A | $\begin{aligned} & .0021 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.1854 \\ & 1.1875 \end{aligned}$ | $\begin{aligned} & 1.1704 \\ & 1.1725 \end{aligned}$ |  | 1.10421.1063 | $\begin{aligned} & 1.0972 \\ & 1.1011 \end{aligned}$ | $\begin{aligned} & .0070 \\ & .0052 \end{aligned}$ | 1.0320 | 2 B3 B | $\begin{aligned} & 1.052 \\ & 1.0520 \end{aligned}$ | $\begin{aligned} & 1.077 \\ & 1.0672 \end{aligned}$ | 1.10631.1063 | 1.11541.1131 | . 0091 | $\begin{aligned} & 1.1875 \\ & 1.1875 \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | . 0068 |  |
| 1.1875-12 | UN | 2 A | $\begin{aligned} & .0017 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.1858 \\ & 1.1875 \end{aligned}$ | $\begin{aligned} & 1.1744 \\ & 1.1761 \end{aligned}$ |  | 1.1317 | $\begin{aligned} & 1.1259 \\ & 1.1291 \end{aligned}$ | $\begin{aligned} & .0058 \\ & .0043 \end{aligned}$ | $\begin{aligned} & 1.0836 \\ & 1.0853 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.097 \\ & 1.0970 \end{aligned}$ | $\begin{aligned} & 1.115 \\ & 1.1073 \end{aligned}$ | $\begin{aligned} & 1.1334 \\ & 1.1334 \end{aligned}$ | 1.14091.1390 | .0075.0056 | $\begin{aligned} & 1.1875 \\ & 1.1875 \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.1875-16 | UN | 2 A3 A | $\begin{aligned} & .0015 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.1860 \\ & 1.1875 \end{aligned}$ | $\begin{aligned} & 1.1766 \\ & 1.1781 \end{aligned}$ |  | 1.14541.1469 | $\begin{aligned} & 1.1403 \\ & 1.1431 \end{aligned}$ | $\begin{aligned} & .0051 \\ & .0038 \end{aligned}$ | $\begin{aligned} & 1.1093 \\ & 1.1108 \end{aligned}$ | 2B3 B | $\begin{aligned} & 1.120 \\ & 1.1200 \end{aligned}$ | $\begin{array}{\|l} 1.134 \\ 1.1283 \end{array}$ | $\begin{aligned} & 1.1469 \\ & 1.1469 \end{aligned}$ | 1.15351.1519 | . 00050 | 1.18751.1875 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.1875-18 | UNEF | 2A | .0015.0000 | $\begin{aligned} & 1.1860 \\ & 1.1875 \end{aligned}$ | $\begin{aligned} & 1.1773 \\ & 1.1788 \end{aligned}$ |  | 1.1514 | $\begin{aligned} & 1.1450 \\ & 1.1478 \end{aligned}$ | $\begin{array}{r} .0049 \\ .0036 \end{array}$ | $\begin{aligned} & 1.1178 \\ & 1.1193 \end{aligned}$ | 2B 3 3 | $\begin{aligned} & 1.127 \\ & 1.1270 \end{aligned}$ | $\begin{aligned} & 1.140 \\ & 1.1355 \end{aligned}$ | $\begin{array}{\|l\|} 1.1514 \\ 1.1514 \end{array}$ | $\begin{array}{\|l} 1.1577 \\ 1.1561 \end{array}$ | . 00063 | 1.18751.1875 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.1875-20 | UN | 2 A | $\begin{aligned} & .0014 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.1861 \\ & 1.1875 \end{aligned}$ | $\begin{aligned} & 1.1780 \\ & 1.1794 \end{aligned}$ |  | 1.15361.1550 | $\begin{aligned} & 1.1489 \\ & 1.1515 \end{aligned}$ | $\begin{aligned} & .0047 \\ & .0035 \end{aligned}$ | $\begin{aligned} & 1.1248 \\ & 1.1262 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.133 \\ & 1.1330 \end{aligned}$ | $\begin{array}{\|l\|} \hline 1.145 \\ 1.1412 \end{array}$ | $\begin{aligned} & 1.1550 \\ & 1.1550 \end{aligned}$ | $\begin{aligned} & 1.1611 \\ & 1.1595 \end{aligned}$ | $\begin{aligned} & .0061 \\ & .0045 \end{aligned}$ | $\begin{aligned} & 1.1875 \\ & 1.1875 \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.1875-28 | UN | 2 A | .0012.0000 | $\begin{aligned} & 1.1863 \\ & 1.1875 \end{aligned}$ | $\begin{aligned} & 1.1798 \\ & 1.1810 \end{aligned}$ |  | 1.1631 | $\begin{aligned} & 1.1590 \\ & 1.1612 \end{aligned}$ | $.0041$ | 1.14251.1437 | 2B 3 3 | 1.1491.1490 | $\begin{array}{\|l\|} \hline 1.157 \\ 1.1551 \\ \hline \end{array}$ | 1.1643 | 1.16961.1683 | .0053.0040 | 1.18751.1875 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.250-7 | UNC | 1 A | . 0022 | 1.2478 | $\begin{aligned} & 1.2232 \\ & 1.2314 \\ & 1.2336 \end{aligned}$ |  | 1.1550 | 1.1439 | . 0111 | 1.0725 | 1B | 1.095 | 1.1231.1231.1125 | $\begin{aligned} & 1.1572 \\ & 1.1572 \\ & 1.1572 \end{aligned}$ | $\begin{aligned} & 1.1716 \\ & 1.1668 \\ & 1.1644 \end{aligned}$ | $\begin{array}{r} .0144 \\ .0096 \\ .0072 \end{array}$ | $\begin{aligned} & 1.2500 \\ & 1.2500 \\ & 1.2500 \end{aligned}$ |
|  |  | 2 A | $\begin{array}{r} .0022 \\ .0000 \end{array}$ | $\begin{aligned} & 1.2778 \\ & 1.278 \\ & 1.2500 \end{aligned}$ |  | 1.2232 | $\begin{aligned} & 1.1550 \\ & 1.1572 \end{aligned}$ | $\begin{aligned} & 1.1476 \\ & 1.1517 \end{aligned}$ | $\begin{gathered} .0074 \\ .0055 \end{gathered}$ | $\begin{aligned} & 1.0725 \\ & 1.0747 \end{aligned}$ | 2B | $\begin{aligned} & 1.095 \\ & 1.0950 \end{aligned}$ |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.250-8 | UN | 2A3 A | $\begin{aligned} & .0021 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.2479 \\ & 1.2500 \end{aligned}$ | $\begin{aligned} & 1.2329 \\ & 1.2350 \end{aligned}$ | 1.2254 | 1.16671.1688 | 1.15971.1635 | $\begin{array}{r} .0070 \\ .0053 \end{array}$ | 1.0945 | 2B | 1.115 | 1.140 | 1.1688 | 1.1780 | . 0092 | 1.2500 |
|  |  |  |  |  |  |  |  |  |  | 1.0966 | 3B | 1.1150 | 1.1297 | 1.1688 | 1.1757 | . 0069 | 1.2500 |
|  |  | 1 A | . 0018 | 1.2482 | 1.2310 |  | 1.1941 | 1.1849 | . 0092 | 1.1460 | 1B | 1.160 | 1.178 | 1.1959 | 1.2079 | . 0120 | 1.2500 |
| 1.250-12 | UNF | 2A | . 0018 | 1.2482 | 1.2368 |  | 1.1941 | 1.1879 | . 0062 | 1.1460 | 2B | 1.160 | 1.178 | 1.1959 | 1.2039 | . 0080 | 1.2500 |
|  |  | 3A | . 0000 | 1.2500 | 1.2386 |  | 1.1959 | 1.1913 | . 0046 | 1.1478 | 3B | 1.1600 | 1.1698 | 1.1959 | 1.2019 | . 0060 | 1.2500 |
| 1.250-16 | UN | 2 A | . 0015 | 1.2485 | 1.2391 |  | 1.2079 | 1.2028 | . 0051 | 1.1718 | 2B | 1.182 | 1.196 | 1.2094 | 1.2160 | . 0066 | 1.2500 |
|  |  | 3A | . 0000 | 1.2500 | 1.2406 |  | 1.2094 | 1.2056 | . 0038 | 1.1733 | 3B | 1.1820 | 1.1908 | 1.2094 | 1.2144 | . 0050 | 1.2500 |
| 1.250-18 | UNEF | 2 A | . 0015 | 1.2485 | 1.2398 |  | 1.2124 | 1.2075 | . 0049 | 1.1803 | 2 B | 1.190 | 1.203 | 1.2139 | 1.2202 | . 0063 | 1.2500 |
|  |  | 3A | . 0000 | 1.2500 | 1.2413 |  | 1.2139 | 1.2103 | . 0036 | 1.1818 | 3B | 1.1990 | 1.1980 | 1.2139 | 1.2186 | . 0047 | 1.2500 |
| 1.250-20 | UN | 2 A | . 0014 | 1.2486 | 1.2405 |  | 1.2161 | 1.2114 | . 0047 | 1.1873 | 2B | 1.196 | 1.207 | 1.2175 | 1.2236 | . 0061 | 1.2500 |
|  |  | 3A | . 0000 | 1.2500 | 1.2419 |  | 1.2175 | 1.2140 | . 0035 | 1.1887 | 3B | 1.1960 | 1.2037 | 1.2175 | 1.2220 | . 0045 | 1.2500 |
| 1.250-28 | UN | 2 A | . 0012 | 1.2488 | 1.2423 |  | 1.2256 | 1.2215 | . 0041 | 1.2050 | 2B | 1.211 | 1.220 | 1.2268 | 1.2321 | . 0053 | 1.2500 |
|  |  | 3A | . 0000 | 1.2500 | 1.2435 |  | 1.2268 | 1.2237 | . 0031 | 1.2062 | 3B | 1.2110 | 1.2176 | 1.2268 | 1.2308 | . 0040 | 1.2500 |
| 1.3125-8 | UN | 2 A | . 0021 | 1.3104 | 1.2954 |  | 1.2292 | 1.2221 | . 0071 | 1.1570 | 2B | 1.177 | 1.202 | 1.2313 | 1.2405 | . 0092 | 1.3125 |
|  |  | 3A | . 0000 | 1.3125 | 1.2975 |  | 1.2313 | 1.2260 | . 0053 | 1.1591 | 3B | 1.1770 | 1.1922 | 1.2313 | 1.2382 | . 0069 | 1.3125 |
| 1.3125-12 | UN | 2A | . 0017 | 1.3108 | 1.2994 |  | 1.2567 | 1.2509 | . 0058 | 1.2086 | 2B | 1.222 | 1.240 | 1.2584 | 1.2659 | . 0075 | 1.3125 |
|  |  | 3A | . 0000 | 1.3125 | 1.3011 |  | 1.2584 | 1.2541 | . 0043 | 1.2103 | 3B | 1.2220 | 1.2323 | 1.2584 | 1.2640 | . 0056 | 1.3125 |
| 1.3125-16 | UN | 2A | . 0015 | 1.3110 | 1.3016 |  | 1.2704 | 1.2653 | . 0051 | 1.2343 | 2B | 1.245 | 1.259 | 1.2719 | 1.2785 | . 0066 | 1.3125 |
|  |  | 3A | . 0000 | 1.3125 | 1.3031 |  | 1.2719 | 1.2681 | . 0038 | 1.2358 | 3B | 1.2450 | 1.2533 | 1.2719 | 1.2769 | . 0050 | 1.3125 |
| 1.3125-18 | UNEF | 2 A | . 0015 | 1.3110 | 1.3023 |  | 1.2749 | 1.2700 | . 0049 | 1.2428 | 2 B | 1.252 | 1.265 | 1.2764 | 1.2827 | . 0063 | 1.3125 |
|  |  | 3A | . 0000 | 1.3125 | 1.3038 |  | 1.2764 | 1.2728 | . 0036 | 1.2443 | 3B | 1.2520 | 1.2605 | 1.2764 | 1.2811 | . 0047 | 1.3125 |
| 1.3125-20 | UN | 2 A | . 0014 | 1.3111 | 1.3030 |  | 1.2786 | 1.2739 | . 0047 | 1.2498 | 2B | 1.258 | 1.270 | 1.2800 | 1.2861 | . 0061 |  |
|  |  | 3A | . 0000 | 1.3125 | 1.3044 |  | 1.2800 | 1.2765 | . 0035 | 1.2512 | 3B | 1.2580 | 1.2662 | 1.2800 | 1.2845 | . 0045 | 1.3125 |
| 1.3125-28 | UN | 2 A | . 0012 | 1.3113 | 1.3048 |  | 1.2881 | 1.2840 | . 0041 | 1.2675 | 2 B | 1.274 | 1.282 | 1.2893 | 1.2946 | . 0053 | 1.3125 |
|  |  | 3A | . 0000 | 1.3125 | 1.3060 |  | 1.2893 | 1.2862 | . 0031 | 1.2687 | 3B | 1.2740 | 1.2801 | 1.2893 | 1.2933 | . 0040 | 1.3125 |
|  |  | 1A | . 0024 | 1.3726 | 1.3453 |  | 1.2643 | 1.2523 | . 0120 | 1.1681 | 1B | 1.195 | 1.225 | 1.2667 | 1.2822 | . 0155 | 1.3750 |
| 1.375-6 | UNC | 2 A | . 0024 | 1.3726 | 1.3544 | 1.3453 | 1.2643 | 1.2563 | . 0080 | 1.1681 | 2B | 1.195 | 1.225 | 1.2667 | 1.2771 | . 0104 | 1.3750 |
|  |  | 3A | . 0000 | 1.3750 | 1.3568 |  | 1.2667 | 1.2607 | . 0060 | 1.1705 | 3B | 1.1950 | 1.2146 | 1.2667 | 1.2745 | . 0078 | 1.3750 |
| 1.375-8 | UN | 2 A | . 0022 | 1.3728 | 1.3578 | 1.3503 | 1.2916 | 1.2844 | . 0072 | 1.2194 | 2B | 1.240 | 1.265 | 1.2938 | 1.3031 | . 0093 | 1.3750 |
|  |  | 3 A | . 0000 | 1.3750 | 1.3600 |  | 1.2938 | 1.2884 | . 0054 | 1.2216 | 3B | 1.2400 | 1.2547 | 1.2938 | 1.3008 | . 0070 | 1.3750 |
|  |  | 1A | . 0019 | 1.3731 | 1.3559 |  | 1.3190 | 1.3096 | . 0094 | 1.2709 | 1B | 1.285 | 1.303 | 1.3209 | 1.3332 | . 0123 | 1.3750 |
| 1.375-12 | UNF | 2 A | . 0019 | 1.3731 | 1.3617 |  | 1.3190 | 1.3127 | . 0063 | 1.2709 | 2 B | 1.285 | 1.303 | 1.3209 | 1.3291 | . 0082 | 1.3750 |
|  |  | 3A | . 0000 | 1.3750 | 1.3636 |  | 1.3209 | 1.3162 | . 0047 | 1.2728 | 3B | 1.2850 | 1.2948 | 1.3209 | 1.3270 | . 0061 | 1.3750 |
| 1.375-16 | UN | 2 A | . 0015 | 1.3735 | 1.3641 |  | 1.3329 | 1.3278 | . 0051 | 1.2968 | 2B | 1.307 | 1.321 | 1.3344 | 1.3410 | . 0066 | 1.3750 |
|  |  | 3A | . 0000 | 1.3750 | 1.3656 |  | 1.3344 | 1.3306 | . 0038 | 1.2983 | 3B | 1.3070 | 1.3158 | 1.3344 | 1.3394 | . 0050 | 1.3750 |
| 1.375-18 | UNEF | 2 A | . 0015 | 1.3735 | 1.3648 |  | 1.3374 | 1.3325 | . 0049 | 1.3053 | 2 B | 1.315 | 1.328 | 1.3389 | 1.3452 | . 0063 | 1.3750 |
|  |  | 3A | . 0000 | 1.3750 | 1.3663 |  | 1.3389 | 1.3353 | . 0036 | 1.3068 | 3B | 1.3150 | 1.3230 | 1.3389 | 1.3436 | . 0047 | 1.3750 |
| 1.375-20 | UN | 2 A | . 0014 | 1.3736 | 1.3655 |  | 1.3411 | 1.3364 | . 0047 | 1.3123 | 2B | 1.321 | 1.332 | 1.3425 | 1.3486 | . 0061 |  |
|  |  | 3A | . 0000 | 1.3750 | 1.3669 |  | 1.3425 | 1.3390 | . 0035 | 1.3137 | 3B | 1.3210 | 1.3287 | 1.3425 | 1.3470 | . 0045 | 1.3750 |

See footnotes at end of table.

Table 2.21. Standard series limits of size-Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Externala |  |  |  |  |  |  |  |  | Internala ${ }^{\text {a }}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Allowance | Major diameter limits |  |  | Pitch diameter limits |  |  | Minor diameter ${ }^{\mathrm{d}}$ | Class | Minor diameter limits |  | Pitch diameter limits |  |  | Major <br> diam- <br> eter <br> Min |
|  |  |  |  | Max ${ }^{\text {b }}$ | Min | Min ${ }^{\text {c }}$ | Max ${ }^{\text {b }}$ | Min | Tolerance |  |  | Min | Max | Min | Max | Tolerance |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| 1.375-28 | UN | 243 A | $\begin{gathered} \text { in } \\ 0.0012 \\ .0000 \end{gathered}$ | $\begin{gathered} i n \\ 1.3738 \\ 1.3750 \end{gathered}$ | $\begin{gathered} i n \\ 1.3673 \\ 1.3685 \end{gathered}$ | in | $\begin{aligned} & i n \\ & 1.3506 \\ & 1.3518 \end{aligned}$ | $\begin{aligned} & i n \\ & 1.3465 \\ & 1.3487 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & 0.0041 \\ & .0031 \end{aligned}$ | $\begin{aligned} & i n \\ & 1.3300 \\ & 1.3312 \end{aligned}$ | $\begin{aligned} & { }_{3 B}^{2 B} \\ & 3 \end{aligned}$ | $\begin{aligned} & i n \\ & 1.336 \\ & 1.3360 \end{aligned}$ | $\begin{aligned} & i n \\ & 1.345 \\ & 1.3426 \end{aligned}$ | $\begin{aligned} & i n \\ & 1.3518 \\ & 1.3518 \end{aligned}$ | $\stackrel{\text { in }}{1.3571}$ | ${ }_{\text {in }}^{\text {in }}$ | ${ }_{1.3750}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | 1.3558 | . 0040 | 1.3750 |
| 1.4375-6 | UN | ${ }_{3}^{2 A}$ | $\begin{aligned} & .0024 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.4351 \\ & 1.4375 \end{aligned}$ | $\begin{aligned} & 1.4169 \\ & 1.4193 \end{aligned}$ |  | $\begin{aligned} & 1.3268 \\ & 1.3292 \end{aligned}$ | $\begin{aligned} & 1.3188 \\ & 1.3232 \end{aligned}$ | $\begin{aligned} & .0080 \\ & .0060 \end{aligned}$ | 1.2306 1.2330 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.257 \\ & 1.2570 \end{aligned}$ | 1.288 1.2771 | 1.3292 1.3292 | $\begin{aligned} & 1.3396 \\ & 1.3370 \end{aligned}$ | .0104 .0078 | $\begin{aligned} & 1.4375 \\ & 1.4375 \end{aligned}$ |
| 1.4375-8 | UN | 2 A | $\begin{aligned} & .0022 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.4353 \\ & 1.4375 \end{aligned}$ | $\begin{aligned} & 1.4203 \\ & 1.4225 \end{aligned}$ |  | $\begin{aligned} & 1.3541 \\ & 1.3563 \end{aligned}$ | $\begin{aligned} & 1.3469 \\ & 1.3509 \end{aligned}$ | $\begin{aligned} & .0072 \\ & .0054 \end{aligned}$ | $\begin{aligned} & 1.2819 \\ & 1.2841 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.302 \\ & 1.3020 \end{aligned}$ | $\begin{aligned} & 1.327 \\ & 1.3172 \end{aligned}$ | $\begin{aligned} & 1.3563 \\ & 1.3563 \end{aligned}$ | $\begin{aligned} & 1.3657 \\ & 1.3634 \end{aligned}$ | $\begin{aligned} & .0094 \\ & .0071 \end{aligned}$ | $\begin{aligned} & 1.4375 \\ & 1.4375 \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.4375-12 | UN | 2 A | $\begin{aligned} & .0018 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.4357 \\ & 1.4375 \end{aligned}$ | $\begin{aligned} & 1.4243 \\ & 1.4261 \end{aligned}$ |  | 1.3834 | $\begin{aligned} & 1.3757 \\ & 1.3790 \end{aligned}$ | $\begin{aligned} & .0059 \\ & .0044 \end{aligned}$ | $\begin{aligned} & 1.3335 \\ & 1.3353 \end{aligned}$ | $\begin{aligned} & 2 B \\ & 3 B \end{aligned}$ | $\begin{aligned} & 1.347 \\ & 1.3470 \end{aligned}$ | $\begin{aligned} & 1.365 \\ & 1.3573 \end{aligned}$ | 1.3834 | $\begin{aligned} & 1.3910 \\ & 1.3891 \end{aligned}$ | $\begin{aligned} & .0076 \\ & .0057 \end{aligned}$ | $\begin{aligned} & 1.4375 \\ & 1.4375 \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.4375-16 | UN | 2 A | $\begin{aligned} & .0016 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.4359 \\ & 1.4375 \end{aligned}$ | $\begin{aligned} & 1.4265 \\ & 1.4281 \end{aligned}$ |  | 1.39531.3969 | $\begin{aligned} & 1.3901 \\ & 1.3930 \end{aligned}$ | $\begin{aligned} & .0052 \\ & .0039 \end{aligned}$ | $\begin{aligned} & 1.3592 \\ & 1.3608 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.370 \\ & 1.3700 \end{aligned}$ | $\begin{aligned} & 1.384 \\ & 1.3783 \end{aligned}$ | $\begin{aligned} & 1.3969 \\ & 1.3969 \end{aligned}$ | $\begin{aligned} & 1.4037 \\ & 1.4020 \end{aligned}$ | $\begin{aligned} & .0068 \\ & .0051 \end{aligned}$ | $\begin{aligned} & 1.4375 \\ & 1.4375 \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.4375-18 | UNEF | 2 A | $\begin{aligned} & .0015 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.4360 \\ & 1.4375 \end{aligned}$ | $\begin{aligned} & 1.4273 \\ & 1.4288 \end{aligned}$ |  | 1.39991.4014 | $\begin{aligned} & 1.3949 \\ & 1.3977 \end{aligned}$ | $\begin{array}{r} .0050 \\ .0037 \end{array}$ | $\begin{aligned} & 1.3678 \\ & 1.3693 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.377 \\ & 1.3770 \end{aligned}$ | $\begin{aligned} & 1.390 \\ & 1.3855 \end{aligned}$ | $\begin{aligned} & 1.4014 \\ & 1.4014 \end{aligned}$ | $\begin{aligned} & 1.4079 \\ & 1.4062 \end{aligned}$ | $\begin{aligned} & .0065 \\ & .0048 \end{aligned}$ | $\begin{aligned} & 1.4375 \\ & 1.4375 \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.4375-20 | UN | 2 A | $\begin{aligned} & .0014 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.4361 \\ & 1.4375 \end{aligned}$ | $\begin{aligned} & 1.4280 \\ & 1.4294 \end{aligned}$ |  | 1.40361.4050 | $\begin{aligned} & 1.3998 \\ & 1.4014 \end{aligned}$ | $\begin{aligned} & .0048 \\ & .0036 \end{aligned}$ | $\begin{aligned} & 1.3748 \\ & 1.3762 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.383 \\ & 1.3830 \end{aligned}$ | $\begin{array}{\|l\|} \hline 1.395 \\ 1.3912 \end{array}$ | $\begin{aligned} & 1.4050 \\ & 1.4050 \end{aligned}$ | $\begin{aligned} & 1.4112 \\ & 1.4096 \end{aligned}$ | $\begin{aligned} & .0062 \\ & .0046 \end{aligned}$ | $\begin{aligned} & 1.4375 \\ & 1.4375 \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.4375-28 | UN | $3{ }_{3}{ }^{\text {A }}$ | $\begin{aligned} & .0013 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.4362 \\ & 1.4375 \end{aligned}$ | $\begin{aligned} & 1.4297 \\ & 1.4310 \end{aligned}$ |  | 1.41301.4143 | $\begin{aligned} & 1.4088 \\ & 1.4112 \end{aligned}$ | $\begin{aligned} & .0042 \\ & .0031 \end{aligned}$ | $\begin{aligned} & 1.3924 \\ & 1.3937 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.399 \\ & 1.3990 \end{aligned}$ | $\begin{aligned} & 1.407 \\ & 1.4051 \end{aligned}$ | $\begin{aligned} & 1.4143 \\ & 1.4143 \end{aligned}$ | $\begin{aligned} & 1.4198 \\ & 1.4184 \end{aligned}$ | $\begin{aligned} & .0055 \\ & .0041 \end{aligned}$ | $\begin{aligned} & 1.4375 \\ & 1.4375 \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1.500-6 | UNC | 1A | $\begin{gathered} .0024 \\ .0024 \\ .0000 \end{gathered}$ | $\begin{aligned} & 1.4976 \\ & 1.4976 \\ & 1.5000 \end{aligned}$ | $\begin{aligned} & 1.4703 \\ & 1.4794 \\ & 1.4818 \end{aligned}$ | --4703 | 1.3893 | $\begin{aligned} & 1.3812 \\ & 1.3856 \end{aligned}$ | $\begin{aligned} & .0121 \\ & .0081 \\ & .0061 \end{aligned}$ | $\begin{aligned} & 1.2931 \\ & 1.2931 \\ & 1.2955 \end{aligned}$ | 1B2B3 B | 1.320 | 1.350 | 1.3917 | 1.4075 | . 0158 | 1.5000 |
|  |  | 243 A |  |  |  |  | $\begin{aligned} & 1.3893 \\ & 1.3893 \\ & 1.3917 \end{aligned}$ |  |  |  |  | 1.320 | 1.350 | 1.3917 | 1.4022 | . 0105 | 1.5000 |
|  |  |  |  |  |  |  |  |  |  |  |  | 1.3200 | 1.3396 | 1.3917 | 1.3996 | . 0079 | 1.5000 |
| 1.500-8 | UN | 2 A | . 0022 | 1.4978 | 1.4828 | 1.4753 | 1.4166 | 1.4093 | . 0073 | 1.3444 | 2B | 1.365 | 1.390 | 1.4188 | 1.4283 | . 0095 | 1.5000 |
|  |  | 3 A | . 0000 | 1.5000 | 1.4850 |  | 1.4188 | 1.4133 | . 0055 | 1.3466 | 3 B | 1.3650 | 1.3797 | 1.4188 | 1.4259 | . 0071 | 1.5000 |
|  |  | 1A | . 0019 | 1.4981 | 1.4809 |  | 1.4440 | 1.4344 | . 0096 | 1.3959 | 1B | 1.410 | 1.428 | 1.4459 | 1.4584 | . 0125 | 1.5000 |
| 1.500-12 | UNF | 2 A | . 0019 | 1.4981 | 1.4867 |  | 1.4440 | 1.4376 | . 0064 | 1.3959 | 2 B | 1.410 | 1.428 | 1.4459 | 1.4542 | . 0083 | 1.5000 |
|  |  | 3 A | . 0000 | 1.5000 | 1.4886 |  | 1.4459 | 1.4411 | . 0048 | 1.3978 | 3B | 1.4100 | 1.4198 | 1.4459 | 1.4522 | . 0063 | 1.5000 |
| 1.500-16 | UN | 2 A | . 0016 | 1.4984 | 1.4890 |  | 1.4578 | 1.4526 | . 0052 | 1.4217 | 2B | 1.432 | 1.446 | 1.4594 | 1.4662 | . 0068 | 1.5000 |
|  |  | 3 A | . 0000 | 1.5000 | 1.4906 |  | 1.4594 | 1.4555 | . 0039 | 1.4233 | 3B | 1.4320 | 1.4408 | 1.4594 | 1.4645 | . 0051 | 1.5000 |
| 1.500-18 | UNEF | 2 A | . 0015 | 1.4985 | 1.4898 |  | 1.4624 | 1.4574 | . 0050 | 1.4303 | 2 B | 1.440 | 1.452 | 1.4639 | 1.4704 | . 0065 | 1.5000 |
|  |  | 3 A | . 0000 | 1.5000 | 1.4913 |  | 1.4639 | 1.4602 | . 0037 | 1.4318 | 3B | 1.4400 | 1.4480 | 1.4639 | 1.4687 | . 0048 | 1.5000 |
| 1.500-20 | UN | 2 A | . 0014 | 1.4986 | 1.4905 |  | 1.4661 | 1.4613 | . 0048 | 1.4373 | 2B | 1.446 | 1.457 | 1.4675 | 1.4737 | . 0062 | 1.5000 |
|  |  | 3 A | . 0000 | 1.5000 | 1.4919 |  | 1.4675 | 1.4639 | . 0036 | 1.4387 | 3B | 1.4460 | 1.4537 | 1.4675 | 1.4721 | . 0046 | 1.5000 |
| 1.500-28 | UN | 2A | . 0013 | 1.4987 | 1.4922 |  | 1.4755 | 1.4713 | . 0042 | 1.4549 | 2B | 1.461 | 1.470 | 1.4768 | 1.4823 | . 0055 | 1.5000 |
|  |  | 3 A | . 0000 | 1.5000 | 1.4935 |  | 1.4768 | 1.4737 | . 0031 | 1.4562 | 3B | 1.4610 | 1.4676 | 1.4768 | 1.4809 | . 0041 | 1.5000 |
| 1.5625-6 | UN | 2A | . 0024 | 1.5601 | 1.5419 |  | 1.4518 | 1.4436 | . 0082 | 1.3556 | 2 B | 1.382 | 1.413 | 1.4542 | 1.4648 | . 0106 | 1.5625 |
|  |  | 3A | . 0000 | 1.5625 | 1.5143 |  | 1.4542 | 1.4481 | . 0061 | 1.3580 | 3B | 1.3820 | 1.4021 | 1.4542 | 1.4622 | . 0080 | 1.5625 |
| 1.5625-8 | UN | 2A | . 0022 | 1.5603 | 1.5453 |  | 1.4791 | 1.4717 | . 0074 | 1.4069 | 2 B | 1.427 | 1.452 | 1.4813 | 1.4909 | . 0096 | 1.5625 |
|  |  | 3A | . 0000 | 1.5625 | 1.5475 |  | 1.4813 | 1.4758 | . 0055 | 1.4091 | 3B | 1.4270 | 1.4422 | 1.4813 | 1.4885 | . 0072 | 1.5625 |
| 1.5625-12 | UN | 2 A | . 0018 | 1.5607 | 1.5493 |  | 1.5066 | 1.5007 | . 0059 | 1.4585 | 2 B | 1.472 | 1.490 | 1.5084 | 1.5160 | . 0076 | 1.5625 |
|  |  | 3A | . 0000 | 1.5625 | 1.5511 |  | 1.5084 | 1.5040 | . 0044 | 1.4603 | 3 B | 1.4720 | 1.4823 | 1.5084 | 1.5141 | . 0057 | 1.5625 |
| 1.5625-16 | UN | 2A | . 0016 | 1.5609 | 1.5515 |  | 1.5203 | 1.5151 | . 0052 | 1.4842 | 2B | 1.495 | 1.509 | 1.5219 | 1.5287 | . 0068 | 1.5625 |
|  |  | 3A | . 0000 | 1.5625 | 1.5531 |  | 1.5219 | 1.5180 | . 0039 | 1.4858 | 3B | 1.4950 | 1.5033 | 1.5219 | 1.5270 | . 0051 | 1.5625 |
| 1.5625-18 | UNEF | 2A | . 0015 | 1.5610 | 1.5523 |  | 1.5249 | 1.5199 | . 0050 | 1.4928 | 2B | 1.502 | 1.515 | 1.5264 | 1.5329 | . 0065 | 1.5625 |
|  |  | 3 A | . 0000 | 1.5625 | 1.5538 |  | 1.5264 | 1.5227 | . 0037 | 1.4943 | 3B | 1.5020 | 1.5105 | 1.5264 | 1.5312 | . 0048 | 1.5625 |
| 1.5625-20 | UN | 2 A | . 0014 | 1.5611 | 1.5530 |  | 1.5286 | 1.5238 | . 0048 | 1.4998 | 2B | 1.508 | 1.520 | 1.5300 | 1.5362 | . 0062 | 1.5625 |
|  |  | 3 A | . 0000 | 1.5625 | 1.5544 |  | 1.5300 | 1.5264 | . 0036 | 1.5012 | 3B | 1.5080 | 1.5162 | 1.5300 | 1.5346 | . 0046 | 1.5625 |
| 1.625-6 | UN | 2A | . 0025 | 1.6225 | 1.6043 |  | 1.5142 | 1.5060 | . 0082 | 1.4180 | 2B | 1.445 | 1.475 | 1.5167 | 1.5274 | . 0107 | 1.6250 |
|  |  | 3 A | . 0000 | 1.6250 | 1.5068 |  | 1.5167 | 1.5105 | . 0062 | 1.4205 | 3B | 1.4450 | 1.4646 | 1.5167 | 1.5247 | . 0080 | 1.6250 |
| 1.625-8 | UN | 2 A | . 0022 | 1.6228 | 1.6078 | 1.6003 | 1.5416 | 1.5342 | . 0074 | 1.4694 | 2 B | 1.490 | 1.515 | 1.5438 | 1.5535 | . 0097 | 1.6250 |
|  |  | 3A | . 0000 | 1.6250 | 1.6100 |  | 1.5438 | 1.5382 | . 0056 | 1.4716 | 3B | 1.4900 | 1,5047 | 1.5438 | 1.5510 | . 0072 | 1.6250 |
| 1.625-12 | UN | 2A | . 0018 | 1.6232 | 1.6118 |  | 1.5691 | 1.5632 | . 0059 | 1.5210 | 2B | 1.535 | 1.553 | 1.5709 | 1.5785 | . 0076 | 1.6250 |
|  |  | 3 A | . 0000 | 1.6250 | 1.6136 |  | 1.5709 | 1.5665 | . 0044 | 1.5228 | 3B | 1.5350 | 1.5448 | 1.5709 | 1.5766 | . 0057 | 1.6250 |
| 1.625-16 | UN | 2A | . 0016 | 1.6234 | 1.6140 |  | 1.5828 | 1.5776 | . 0052 | 1.5467 | 2 B | 1.557 | 1.571 | 1.5844 | 1.5912 | . 0068 | 1.6250 |
|  |  | 3A | . 0000 | 1.6250 | 1.6156 |  | 1.5844 | 1.5805 | . 0039 | 1.5483 | 3 B | 1.5570 | 1.5658 | 1.5844 | 1.5895 | . 0051 | 1.6250 |
| 1.625-18 | UNEF | 2 A | . 0015 | 1.6235 | 1.6148 |  | 1.5874 | 1.5824 | . 0050 | 1.5553 | 2B | 1.565 | 1.578 | 1.5889 | 1.5954 | . 0065 | 1.6250 |
|  |  | 3 A | . 0000 | 1.6250 | 1.6163 |  | 1.5889 | 1.5852 | . 0037 | 1.5568 | 3 B | 1.5650 | 1.5730 | 1.5889 | 1.5937 | . 0048 | 1.6250 |
| 1.625-20 | UN | 2 A | . 0014 | 1.6236 | 1.6155 |  | 1.5911 | 1.5863 | . 0048 | 1.5623 | 2 B | 1.571 | 1.582 | 1.5925 | 1.5987 | . 0062 | 1.6250 |
|  |  | 3A | . 0000 | 1.6250 | 1.6169 |  | 1.5925 | 1.5889 | . 0036 | 1.5637 | 3 B | 1.5710 | 1.5787 | 1.5925 | 1.5971 | . 0046 | 1.6250 |

See footnotes at end of table.

Table 2.21. Standard series limits of size-Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Exterual ${ }^{\text {a }}$ |  |  |  |  |  |  |  |  | Internala |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Allowance | Major diameter limits |  |  | Pitch diameter limits |  |  | Minor diameter ${ }^{\text {d }}$ | Class | Minor diameter limits |  | Pitch diameter limits |  |  | Major diameter Min |
|  |  |  |  | Max ${ }^{\text {b }}$ | Mill | Minc | Max ${ }^{\text {b }}$ | Min | Tolerance |  |  | Min | Max | Min | Max | Toleranee |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| 1.6875-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & i n \\ & .0025 \\ & .0000 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & \text { 1.6850 } \\ & 1.6875 \end{aligned}$ | $\begin{aligned} & i n \\ & 1.6668 \\ & 1.6693 \end{aligned}$ | in | $\begin{aligned} & i n \\ & 1.5767 \\ & 1.5792 \end{aligned}$ | $\begin{aligned} & i n \\ & 1.5684 \\ & 1.5730 \end{aligned}$ | $\begin{gathered} \text { in } \\ 0.0083 \\ .0062 \end{gathered}$ | $\begin{aligned} & i n \\ & 1.4805 \\ & 1.4830 \end{aligned}$ | 2 B | $\begin{aligned} & i n \\ & 1.507 \\ & 1.5070 \end{aligned}$ | $\begin{gathered} \text { in } \\ 1.538 \\ 1.5271 \end{gathered}$ | $\begin{aligned} & 1.5792 \\ & 1.5792 \end{aligned}$ | $\begin{aligned} & i n \\ & 1.5900 \\ & 1.5873 \end{aligned}$ | $\begin{gathered} i n \\ 0.0108 \\ .0081 \end{gathered}$ | $\begin{aligned} & \text { in } \\ & 1.6875 \\ & 1.6875 \end{aligned}$ |
| 1.6875-8 | UN | 2 A | . 0022 | 1.6853 1.6875 | $\begin{aligned} & 1.6703 \\ & 1.6725 \end{aligned}$ |  | 1.6041 1.6063 | 1.5966 1.6007 | . 0075 | 1.5319 1.5341 | 2B | 1.552 1.5520 | 1.577 1.5672 | 1.6063 1.6063 | 1.6160 1.6136 | $\begin{aligned} & .0097 \\ & .0073 \end{aligned}$ | $\begin{aligned} & 1.6875 \\ & 1.6875 \end{aligned}$ |
| 1.6875-12 | UN | 2 A | . 0018 | 1.6857 1.6875 | $\begin{aligned} & 1.6743 \\ & 1.6761 \end{aligned}$ |  | 1.6316 1.6334 | 1.6256 1.6289 | . 0060 | 1.5835 1.5853 | 2B | 1.597 1.5970 | 1.615 1.6073 | 1.6334 1.6334 | 1.6412 1.6392 | .0078 .0058 | $\begin{aligned} & 1.6875 \\ & 1.6875 \end{aligned}$ |
| 1.6875-16 | UN | 2 A | $\begin{aligned} & .0016 \\ & .0000 \end{aligned}$ | 1.6859 1.6875 | $\begin{aligned} & 1.6765 \\ & 1.6781 \end{aligned}$ |  | 1.6453 1.6469 | 1.6400 1.6429 | . 00053 | 1.6092 1.6108 | 2B | 1.620 1.6200 | 1.634 1.6283 | 1.6469 1.6469 | 1.6538 1.6521 | $\begin{array}{r} .0069 \\ .0052 \end{array}$ | $\begin{aligned} & 1.6875 \\ & 1.6875 \end{aligned}$ |
| 1.6875-18 | UNEF | ${ }_{3}^{2 A}$ | . 0015 | 1.6860 1.6875 | 1.6773 1.6788 |  | 1.6499 1.6514 | 1.6448 1.6476 | . 00051 | 1.6178 1.6193 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 1.627 1.6270 | 1.640 1.6355 | 1.6514 1.6514 | 1.6580 1.6563 | . 00666 | $\begin{aligned} & 1.6875 \\ & 1.6875 \end{aligned}$ |
| 1.6875-20 | UN | ${ }_{3}^{2} \mathrm{~A}$ | . 0015 | 1.6860 1.6875 | $\begin{aligned} & 1.6779 \\ & 1.6794 \end{aligned}$ |  | 1.6535 1.6550 | 1.6487 1.6514 | . 0048 | 1.6247 1.6262 | 2B | 1.633 1.6330 | 1.645 1.6412 | 1.6550 1.6550 | 1.6613 1.6597 | . 0063 | 1.6875 1.6875 |
| 1.750-5 | UNC | 1 A 2 A 3 A | $\begin{aligned} & .0027 \\ & .0027 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.7473 \\ & 1.7473 \\ & 1.7500 \end{aligned}$ | $\begin{aligned} & 1.7165 \\ & 1.7268 \\ & 1.7295 \end{aligned}$ | 1.7165 | 1.6174 1.6174 1.6201 | 1.6040 1.6085 1.6134 | .0134 .0089 .0067 | 1.5019 1.5019 1.5046 | 1 B 2 B 3 B | 1.534 1.534 1.5340 | 1.568 1.568 1.5575 | 1.6201 1.6201 1.6201 | 1.6375 1.6317 1.6288 | .0174 .0116 .0087 | 1.7500 1.7500 1.7500 |
| 1.750-6 | UN | 2 A | $\begin{aligned} & .0025 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.7475 \\ & 1.7500 \end{aligned}$ | $\begin{aligned} & 1.7293 \\ & 1.7318 \end{aligned}$ |  | 1.6392 | 1.6309 1.6354 | . 0083 | 1.5430 1.5455 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.570 \\ & 1.5700 \end{aligned}$ | $\begin{aligned} & 1.600 \\ & 1.5896 \end{aligned}$ | $\begin{aligned} & 1.6417 \\ & 1.6417 \end{aligned}$ | 1.6525 1.6498 | . 010081 | $\begin{aligned} & 1.7500 \\ & 1.7500 \end{aligned}$ |
| 1.750-8 | UN | 2 A | . 0023 | 1.7477 1.7500 | $\begin{aligned} & 1.7327 \\ & 1.7350 \end{aligned}$ | 1.7252 | 1.6665 | 1.6590 1.6631 | . 0075 | 1.5943 1.5966 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 1.615 1.6150 | 1.640 1.6297 | 1.6688 1.6688 | 1.6786 1.6762 | . 00098 | 1.7500 1.7500 |
| 1.750-12 | UN | 2 A | . 0018 | 1.7482 1.7500 | $\begin{aligned} & 1.7368 \\ & 1.7386 \end{aligned}$ |  | 1.6941 | 1.6881 | . 0060 | 1.6460 1.6478 | 2B | 1.660 1.6600 | 1.678 1.6698 | 1.6959 1.6959 | 1.7037 1.7017 | .0078 .0058 | $\begin{aligned} & 1.7500 \\ & 1.7500 \end{aligned}$ |
| 1.750-16 | UN | ${ }_{3}{ }_{3} \mathrm{~A}$ | $\begin{array}{r} .0016 \\ .0000 \end{array}$ | $\begin{aligned} & 1.7484 \\ & 1.7500 \end{aligned}$ | $\begin{aligned} & 1.7390 \\ & 1.7406 \end{aligned}$ |  | 1.7078 1.7094 | 1.7025 1.7054 | .0053 .0040 | 1.6717 1.6733 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.682 \\ & 1.6820 \end{aligned}$ | 1.696 1.6908 | $\begin{aligned} & 1.7094 \\ & 1.7094 \end{aligned}$ | $\begin{aligned} & 1.7163 \\ & 1.7146 \end{aligned}$ | . 0069 | $\begin{aligned} & 1.7500 \\ & 1.7500 \end{aligned}$ |
| 1.750-20 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0015 .0000 | 1.7485 1.7500 | 1.7404 1.7419 |  | 1.7160 1.7175 | 1.7112 1.7139 | . 0048 | 1.6872 1.6887 | 2B 3 | 1.696 1.6960 | 1.707 1.7037 | 1.7175 1.7175 | 1.7238 1.7222 | . 00063 | 1.7500 1.7500 |
| 1.8125-6 | UN | 2 A | . 0025 | $\begin{aligned} & 1.8100 \\ & 1.8125 \end{aligned}$ | $\begin{aligned} & 1.7918 \\ & 1.7943 \end{aligned}$ |  | 1.7017 1.7042 | 1.6933 1.6979 | . 0084 | 1.6055 1.6080 | 2 B | 1.632 1.6320 | 1.663 1.6521 | 1.7042 1.7042 | 1.7151 1.7124 | . 01009 | $\begin{aligned} & 1.8125 \\ & 1.8125 \end{aligned}$ |
| 1.8125-8 | UN | ${ }_{3}{ }^{\text {A }}$ | . 0023 | $\begin{aligned} & 1.8102 \\ & 1.8125 \end{aligned}$ | $\begin{aligned} & 1.7952 \\ & 1.7975 \end{aligned}$ |  | 1.7290 1.7313 | 1.7214 1.7256 | . 0076 | 1.6568 1.6591 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 1.677 1.6770 | 1.702 1.6922 | 1.7313 1.7313 | 1.7412 1.7387 | $\begin{aligned} & .0099 \\ & .0074 \end{aligned}$ | $\begin{aligned} & 1.8125 \\ & 1.8125 \end{aligned}$ |
| 1.8125-12 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | . 00018 | $\begin{aligned} & 1.8107 \\ & 1.8125 \end{aligned}$ | 1.7993 1.8011 |  | 1.7566 1.7584 | 1.7506 1.7539 | . 0060 | 1.7085 1.7103 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 1.722 1.7220 | 1.740 1.7323 | 1.7584 1.7584 | 1.7662 1.7642 | . 0078 | 1.8125 1.8125 |
| 1.8125-16 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | . 00016 | $\begin{aligned} & 1.8109 \\ & 1.8125 \end{aligned}$ | 1.8015 1.8031 |  | 1.7703 1.7719 | 1.7650 1.7679 | . 00053 | 1.7342 1.7358 | 2B 3 B | 1.745 1.7450 | $\begin{aligned} & 1.759 \\ & 1.7533 \end{aligned}$ | $\begin{aligned} & 1.7719 \\ & 1.7719 \end{aligned}$ | $\begin{aligned} & 1.7788 \\ & 1.7771 \end{aligned}$ | .0069 .0052 | $\begin{aligned} & 1.8125 \\ & 1.8125 \end{aligned}$ |
| 1.8125-20 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0015 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.8110 \\ & 1.8125 \end{aligned}$ | $\begin{aligned} & 1.8029 \\ & 1.8044 \end{aligned}$ |  | $\begin{aligned} & 1.7785 \\ & 1.7800 \end{aligned}$ | $\begin{aligned} & 1.7737 \\ & 1.7764 \end{aligned}$ | $\begin{aligned} & .0048 \\ & .0036 \end{aligned}$ | $\begin{aligned} & 1.7497 \\ & 1.7512 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.758 \\ & 1.7580 \end{aligned}$ | 1.770 1.7662 | $\begin{aligned} & 1.7800 \\ & 1.7800 \end{aligned}$ | $\begin{aligned} & 1.7863 \\ & 1.7847 \end{aligned}$ | . 0063 | $\begin{aligned} & 1.8125 \\ & 1.8125 \end{aligned}$ |
| 1.875-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0025 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.8725 \\ & 1.8750 \end{aligned}$ | $\begin{aligned} & 1.8543 \\ & 1.8568 \end{aligned}$ |  | $\begin{aligned} & 1.7642 \\ & 1.7667 \end{aligned}$ | $\begin{aligned} & 1.7558 \\ & 1.7604 \end{aligned}$ | . 00084 | 1.6680 1.6705 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.695 \\ & \mathrm{i} .6950 \end{aligned}$ | 1.725 1.7146 | 1.7667 1.7667 | 1.7777 1.7749 | . 0110 | $\begin{aligned} & 1.8750 \\ & 1.8750 \end{aligned}$ |
| 1.875-8 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | . 0023 | 1.8727 1.8750 | $\begin{aligned} & 1.8577 \\ & 1.8600 \end{aligned}$ | 1.8502 | 1.7915 1.7938 | 1.7838 1.7881 | . 0077 | 1.7193 1.7216 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.740 \\ & 1.7400 \end{aligned}$ | $\begin{aligned} & 1.765 \\ & 1.7547 \end{aligned}$ | $\begin{aligned} & 1.7938 \\ & 1.7938 \end{aligned}$ | $\begin{aligned} & 1.8038 \\ & 1.8013 \end{aligned}$ | $\begin{aligned} & .0100 \\ & .0075 \end{aligned}$ | $\begin{aligned} & 1.8750 \\ & 1.8750 \end{aligned}$ |
| 1.875-12 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{array}{r} .0018 \\ .0000 \end{array}$ | $\begin{aligned} & 1.8732 \\ & 1.8750 \end{aligned}$ | $\begin{aligned} & 1.8618 \\ & 1.8636 \end{aligned}$ |  | $\begin{aligned} & 1.8191 \\ & 1.8209 \end{aligned}$ | 1.8131 1.8164 | . 0060 | 1.7710 1.7728 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.785 \\ & 1.7850 \end{aligned}$ | $\begin{aligned} & 1.803 \\ & 1.7948 \end{aligned}$ | $\begin{aligned} & 1.8209 \\ & 1.8209 \end{aligned}$ | $\begin{aligned} & 1.8287 \\ & 1.8267 \end{aligned}$ | . 00078 | $\begin{aligned} & 1.8750 \\ & 1.8750 \end{aligned}$ |
| 1.875-16 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{aligned} & .0016 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.8734 \\ & 1.8750 \end{aligned}$ | $\begin{aligned} & 1.8640 \\ & 1.8656 \end{aligned}$ |  | $\begin{aligned} & 1.8328 \\ & 1.8344 \end{aligned}$ | 1.8275 1.8304 | . 0053 | 1.7967 1.7983 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 1.807 1.8070 | 1.821 1.8158 | 1.8344 1.8344 | 1.8413 1.8396 | .0069 .0052 | $\begin{aligned} & 1.8750 \\ & 1.8750 \end{aligned}$ |
| 1.875-20 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} .0015 \\ .0000 \end{array}$ | $\begin{aligned} & 1.8735 \\ & 1.8750 \end{aligned}$ | $\begin{aligned} & 1.8654 \\ & 1.8669 \end{aligned}$ |  | 1.8410 1.8425 | 1.8362 1.8389 | $\begin{aligned} & .0048 \\ & .0036 \end{aligned}$ | 1.8122 1.8137 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.821 \\ & 1.8210 \end{aligned}$ | $\begin{aligned} & 1.832 \\ & 1.8287 \end{aligned}$ | 1.8425 1.8425 | $\begin{aligned} & 1.8488 \\ & 1.8472 \end{aligned}$ | $\begin{aligned} & .0063 \\ & .0047 \end{aligned}$ | $\begin{aligned} & 1.8750 \\ & 1.8750 \end{aligned}$ |
| 1.9375-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0026 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.9349 \\ & 1.9375 \end{aligned}$ | $\begin{aligned} & 1.9167 \\ & 1.9193 \end{aligned}$ |  | $\begin{aligned} & 1.8266 \\ & 1.8292 \end{aligned}$ | $\begin{aligned} & 1.8181 \\ & 1.8228 \end{aligned}$ | $\begin{aligned} & .0085 \\ & .0064 \end{aligned}$ | $\begin{aligned} & 1.7304 \\ & 1.7330 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.757 \\ & 1.7570 \end{aligned}$ | $\begin{aligned} & 1.788 \\ & 1.7771 \end{aligned}$ | $\begin{aligned} & 1.8292 \\ & 1.8292 \end{aligned}$ | $\begin{aligned} & 1.8403 \\ & 1.8375 \end{aligned}$ | $\begin{aligned} & .0111 \\ & .0083 \end{aligned}$ | $\begin{aligned} & 1.9375 \\ & 1.9375 \end{aligned}$ |
| 1.9375-8 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0023 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.9352 \\ & 1.9375 \end{aligned}$ | $\begin{aligned} & 1.9202 \\ & 1.9225 \end{aligned}$ |  | $\begin{aligned} & 1.8510 \\ & 1.8563 \end{aligned}$ | 1.8463 1.8505 | $\begin{aligned} & .0077 \\ & .0058 \end{aligned}$ | 1.7818 1.7841 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.802 \\ & 1.8020 \end{aligned}$ | $\begin{aligned} & 1.827 \\ & 1.8172 \end{aligned}$ | 1.8563 1.8563 | 1.8663 1.8638 | .0100 .0075 | 1.9375 1.9375 |
| 1.9375-12 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{aligned} & .0018 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.9357 \\ & 1.9375 \end{aligned}$ | $\begin{aligned} & 1.9243 \\ & 1.9261 \end{aligned}$ |  | $\begin{aligned} & 1.8816 \\ & 1.8834 \end{aligned}$ | $\begin{aligned} & 1.8755 \\ & 1.8789 \end{aligned}$ | $\begin{aligned} & .0061 \\ & .0045 \end{aligned}$ | 1.8335 1.8353 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.847 \\ & 1.8470 \end{aligned}$ | $\begin{aligned} & 1.865 \\ & 1.8573 \end{aligned}$ | $\begin{aligned} & 1.8834 \\ & 1.8834 \end{aligned}$ | $\begin{aligned} & 1.8913 \\ & 1.8893 \end{aligned}$ | $\begin{aligned} & .0079 \\ & .0059 \end{aligned}$ | $\begin{aligned} & 1.9375 \\ & 1.9375 \end{aligned}$ |
| 1.9375-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} .0016 \\ .0000 \end{array}$ | $\begin{aligned} & 1.9359 \\ & 1.9375 \end{aligned}$ | $\begin{aligned} & 1.9265 \\ & 1.9281 \end{aligned}$ |  | $\begin{aligned} & 1.8953 \\ & 1.8969 \end{aligned}$ | $\begin{aligned} & 1.8899 \\ & 1.8929 \end{aligned}$ | $\begin{aligned} & .0054 \\ & .0040 \end{aligned}$ | $\begin{aligned} & 1.8592 \\ & 1.8608 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.870 \\ & 1.8700 \end{aligned}$ | $\begin{aligned} & 1.884 \\ & 1.8783 \end{aligned}$ | $\begin{aligned} & \text { 1. } 8969 \\ & 1.8969 \end{aligned}$ | $\begin{aligned} & 1.9039 \\ & 1.9021 \end{aligned}$ | $\begin{aligned} & .0070 \\ & .0052 \end{aligned}$ | $\begin{aligned} & 1.9375 \\ & 1.9375 \end{aligned}$ |
| 1.9375-20 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0015 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 1.9360 \\ & 1.9375 \end{aligned}$ | $\begin{aligned} & 1.9279 \\ & 1.9294 \end{aligned}$ |  | $\begin{aligned} & 1.9035 \\ & 1.9050 \end{aligned}$ | $\begin{aligned} & 1.8986 \\ & 1.9013 \end{aligned}$ | $\begin{aligned} & .0049 \\ & .0037 \end{aligned}$ | $\begin{aligned} & 1.8747 \\ & 1.8762 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.883 \\ & 1.8830 \end{aligned}$ | $\begin{aligned} & 1.895 \\ & 1.8912 \end{aligned}$ | $\begin{aligned} & 1.9050 \\ & 1.9050 \end{aligned}$ | 1.9114 1.9098 | . 0064 | $\begin{aligned} & 1.9375 \\ & 1.9375 \end{aligned}$ |

See footnotes at end of table.

Table 2.21. Standard series limits of size-Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | External ${ }^{\text {a }}$ |  |  |  |  |  |  |  |  | Internala |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Allowance | Major diameter limits |  |  | Pitch diameter limits |  |  | Minor diameter ${ }^{\mathrm{d}}$ | Class | Minor diameter limits |  | Pitch diameter limits |  |  | Major diameter |
|  |  |  |  | Max ${ }^{\text {b }}$ | Min | Min ${ }^{\text {c }}$ | Max ${ }^{\text {b }}$ | Min | Tolerance |  |  | Min | Max | Min | Max | Tolerance |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| 2.000-4.5 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | ${ }_{0}^{\text {in }}$ .0029 0000 | $\begin{gathered} i n \\ 1.9971 \\ 1.9971 \\ 2.0000 \end{gathered}$ | $\begin{gathered} \text { in } \\ 1.9641 \\ 1.9751 \\ 1.9780 \end{gathered}$ | in | in 1.8528 1.8528 1.8557 | in 1.8385 1.8433 1.8486 | $\begin{gathered} \text { in } \\ 0.0143 \\ .0095 \\ .0071 \end{gathered}$ | in 1.7245 1.7245 1.7274 | 18 2 B 3 B | in 1.759 1.759 1.7590 | $\quad i n$ 1.795 1.795 1.7861 | in 1.8557 1.8557 1.8557 | in 1.8743 1.8681 1.8650 | in 0.0186 .0124 .0093 | in <br> 2.0000 2.0000 <br> 2.0000 |
| 2.000-6 | UN | 2 A | .0026 .0000 | 1.9974 2.0000 | $\begin{aligned} & 1.9792 \\ & 1.9818 \end{aligned}$ |  | 1.8891 1.8917 | 1.8805 1.8853 | . 0086 | $\begin{aligned} & 1.7929 \\ & 1.7955 \end{aligned}$ | 2B ${ }_{3}$ | $\begin{aligned} & 1.820 \\ & 1.8200 \end{aligned}$ | $\begin{aligned} & 1.850 \\ & 1.8396 \end{aligned}$ | $\begin{aligned} & 1.8917 \\ & 1.8917 \end{aligned}$ | $\begin{aligned} & 1.9028 \\ & 1.9000^{\circ} \end{aligned}$ | . 0111 | $\begin{aligned} & 2.0000 \\ & 2.0000 \end{aligned}$ |
| 2.000-8 | UN | 2 A | .0023 .0000 | 1.9977 2.0000 | 1.9827 1.9850 | 1.9752 | 1.9165 1.9188 | 1.9087 1.9130 | .0078 .0058 | 1.8443 1.8466 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 1.865 \\ & 1.8650 \end{aligned}$ | $\begin{aligned} & 1.890 \\ & 1.8797 \end{aligned}$ | 1.9188 1.9188 | $\begin{aligned} & 1.9289 \\ & 1.9264 \end{aligned}$ | .0101 .0076 | $\begin{aligned} & 2.0000 \\ & 2.0000 \end{aligned}$ |
| 2.000-12 | UN | 2A | . 0018 | $\begin{aligned} & 1.9982 \\ & 2.0000 \end{aligned}$ | $\begin{aligned} & 1.9868 \\ & 1.9886 \end{aligned}$ |  | 1.9441 1.9459 | 1.9380 1.9414 | . 00615 | 1.8960 1.8978 | 2 B | $\begin{aligned} & 1.910 \\ & 1.9100 \end{aligned}$ | $\begin{aligned} & 1.928 \\ & 1.9198 \end{aligned}$ | 1.9459 1.9459 | 1.9538 1.9518 | . 0079 | $\begin{aligned} & 2.0000 \\ & 2.0000 \end{aligned}$ |
| 2.000-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathbf{A} \end{aligned}$ | .0016 .0000 | 1.9984 2.0000 | 1.9890 1.9906 |  | 1.9578 1.9594 | 1.9524 | . 0054 | 1.9217 1.9233 | 2 B 3 B | 1.932 1.9320 | 1.946 1.9408 | 1.9594 1.9594 | 1.9664 1.9646 | . 0070 | $\begin{aligned} & 2.0000 \\ & 2.0000 \end{aligned}$ |
| 2.000-20 | UN | 2 A A | .0015 .0000 | $\begin{aligned} & 1.9985 \\ & 2.0000 \end{aligned}$ | $\begin{aligned} & 1.9904 \\ & 1.9919 \end{aligned}$ |  | 1.9660 1.9675 | 1.9611 1.9638 | .0049 .0037 | 1.9372 1.9387 | 2B 3 B | 1.946 1.9460 | 1.957 1.9537 | 1.9675 1.9675 | 1.9739 1.9723 | . 0064 | 2.0000 2.0000 |
| 2.125-6 | UN | 2 A | .0026 .0000 | $\begin{aligned} & 2.1224 \\ & 2.1250 \end{aligned}$ | $\begin{aligned} & 2.1042 \\ & 2.1068 \end{aligned}$ |  | 2.0141 2.0167 | 2.0054 2.0102 | $\begin{aligned} & .0087 \\ & .0065 \end{aligned}$ | $\begin{aligned} & 1.9179 \\ & 1.9205 \end{aligned}$ | ${ }_{3}^{2 B}$ | $\begin{aligned} & 1.945 \\ & 1.9450 \end{aligned}$ | $\begin{aligned} & 1.975 \\ & 1.9646 \end{aligned}$ | $\begin{aligned} & 2.0167 \\ & 2.0167 \end{aligned}$ | $\begin{aligned} & 2.0280 \\ & 2.0251 \end{aligned}$ | $\begin{gathered} .0113 \\ .0084 \end{gathered}$ | $\begin{aligned} & 2.1250 \\ & 2.1250 \end{aligned}$ |
| 2.125-8 | UN | $\begin{aligned} & 2 A \\ & 3 A \end{aligned}$ | .0024 .0000 | 2.1226 2.1250 | $\begin{aligned} & 2.1076 \\ & 2.1100 \end{aligned}$ | 2.1001 | 2.0414 2.0438 | 2.0335 2.0379 | .0079 .0059 | 1.9692 1.9716 | 2 B | 1.990 1.9900 | 2.015 2.0047 | 2.0438 2.0438 | 2.0540 2.0515 | . 0102 | 2.1250 2.1250 |
| 2.125-12 | UN | 2 A | $\begin{aligned} & .0018 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.1232 \\ & 2.1250 \end{aligned}$ | $\begin{aligned} & 2.1118 \\ & 2.1136 \end{aligned}$ |  | 2.0691 2.0709 | $\begin{aligned} & 2.0630 \\ & 2.0664 \end{aligned}$ | . 00641 | 2.0210 2.0228 | 2B 3 | $\begin{aligned} & 2.035 \\ & 2.0350 \end{aligned}$ | $\begin{aligned} & 2.053 \\ & 2.0448 \end{aligned}$ | $\begin{aligned} & 2.0709 \\ & 2.0709 \end{aligned}$ | 2.0788 2.0768 | $\begin{array}{r} .0079 \\ .0059 \end{array}$ | $\begin{aligned} & 2.1250 \\ & 2.1250 \end{aligned}$ |
| 2.125-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0016 .0000 | $\begin{aligned} & 2.1234 \\ & 2.1250 \end{aligned}$ | $\begin{aligned} & 2.1140 \\ & 2.1156 \end{aligned}$ |  | 2.0828 2.0844 | 2.0774 2.0804 | .0054 .0040 | 2.0467 2.0483 | 2B 3 B | $\begin{aligned} & 2.057 \\ & 2.0570 \end{aligned}$ | $\begin{aligned} & 2.071 \\ & 2.0658 \end{aligned}$ | $\begin{aligned} & 2.0844 \\ & 2.0844 \end{aligned}$ | 2.0914 2.0896 | .0070 .0052 | $\begin{aligned} & 2.1250 \\ & 2.1250 \end{aligned}$ |
| 2.125-20 | UN | 2 A | . 0015 | 2.1235 2.1250 | 2.1154 2.1169 |  | 2.0910 2.0925 | 2.0861 2.0888 | . 0049 | 2.0622 2.0637 | 2B 3 3 | $\xrightarrow[2.071]{2.0710}$ | 2.082 2.0787 | 2.0925 2.0925 | 2.0989 2.0973 | .0064 .0048 | $\begin{aligned} & 2.1250 \\ & 2.1250 \end{aligned}$ |
| 2.250-4.5 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} .0029 \\ .0029 \\ .0000 \end{array}$ | $\begin{aligned} & 2.2471 \\ & 2.2471 \\ & 2.2500 \end{aligned}$ | $\begin{aligned} & 2.2141 \\ & 2.2251 \\ & 2.2280 \end{aligned}$ | 2.2141 | 2.1028 2.1028 2.1057 | $\begin{aligned} & 2.0882 \\ & 2.0931 \\ & 2.0984 \end{aligned}$ | $\begin{aligned} & .0146 \\ & .0097 \\ & .0073 \end{aligned}$ | 1.9745 1.9745 1.9774 | 18 2 B 3 B | 2.009 2.009 2.0090 | 2.045 2.045 2.0361 | 2.1057 2.1057 2.1057 | 2.1247 2.1183 2.1152 | .0190 .0126 .0095 | $\begin{aligned} & 2.2500 \\ & 2.2500 \\ & 2.2500 \end{aligned}$ |
| 2.250-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 0026 | $\begin{aligned} & 2.2474 \\ & 2.2500 \end{aligned}$ | $\begin{aligned} & 2.2292 \\ & 2.2318 \end{aligned}$ |  | 2.1391 2.1417 | 2.1303 2.1351 | .0088 .0066 | 2.0429 2.0455 | 2 B 3 B | $\begin{aligned} & 2.070 \\ & 2.0700 \end{aligned}$ | 2.100 2.0896 | 2.1417 2.1417 | 2.1531 2.1502 | . 0114 | $\begin{array}{r} 2.2500 \\ 2.2500 \end{array}$ |
| 2.250-8 | UN | 2A | . 0024 | 2.2476 2.2500 | 2.2326 2.2350 | 2.2251 | 2.1664 2.1688 | 2.1584 2.1628 | .0080 .0060 | 2.0942 2.0966 | 2 B | $\xrightarrow[2.115]{2.1150}$ | 2.140 2.1297 | 2.1688 2.1688 | 2.1792 2.1766 | .0104 .0078 | $\begin{aligned} & 2.2500 \\ & 2.2500 \end{aligned}$ |
| 2.250-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0018 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.2482 \\ & 2.2500 \end{aligned}$ | $\begin{aligned} & 2.2368 \\ & 2.2386 \end{aligned}$ |  | 2.1941 2.1959 | 2.1880 2.1914 | . 0061 | $\begin{aligned} & 2.1460 \\ & 2.1478 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.160 \\ & 2.1600 \end{aligned}$ | $\begin{aligned} & 2.178 \\ & 2.1698 \end{aligned}$ | $\begin{aligned} & 2.1959 \\ & 2.1959 \end{aligned}$ | $\begin{aligned} & 2.2038 \\ & 2.2018 \end{aligned}$ | .0079 .0059 | $\begin{aligned} & 2.2500 \\ & 2.2500 \end{aligned}$ |
| 2.250-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 0016 | $\begin{aligned} & 2.2484 \\ & 2.2500 \end{aligned}$ | $\begin{aligned} & 2.2390 \\ & 2.2406 \end{aligned}$ |  | 2.2078 2.2094 | 2.2024 2.2054 | .0054 .0040 | 2.1717 2.1733 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 2.182 2.1820 | 2.196 2.1908 | 2.2094 2.2094 | 2.2164 2.2146 | . 0070 | $\begin{aligned} & 2.2500 \\ & 2.2500 \end{aligned}$ |
| 2.250-20 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0015 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.2485 \\ & 2.2500 \end{aligned}$ | $\begin{aligned} & 2.2404 \\ & 2.2419 \end{aligned}$ |  | 2.2160 2.2175 | $\begin{aligned} & 2.2111 \\ & 2.2138 \end{aligned}$ | $\begin{array}{r} .0049 \\ .0037 \end{array}$ | $\begin{aligned} & 2.1872 \\ & 2.1887 \end{aligned}$ | 2B 3 B | $\begin{aligned} & 2.196 \\ & 2.1960 \end{aligned}$ | $\begin{aligned} & 2.207 \\ & 2.2037 \end{aligned}$ | $\begin{aligned} & 2.2175 \\ & 2.2175 \end{aligned}$ | $\begin{aligned} & 2.2239 \\ & 2.2223 \end{aligned}$ | . 00644 | $\begin{aligned} & 2.2500 \\ & 2.2500 \end{aligned}$ |
| 2.375-6 | UN | $\underset{3 \mathrm{~A}}{2 \mathrm{~A}}$ | $\begin{array}{r} .0027 \\ .0000 \end{array}$ | $\begin{aligned} & 2.3723 \\ & 2.3750 \end{aligned}$ | $\begin{aligned} & 2.3541 \\ & 2.3568 \end{aligned}$ |  | 2.2640 2.2667 | $\begin{aligned} & 2.2551 \\ & 2.2601 \end{aligned}$ | .0089 .0066 | $\begin{aligned} & 2.1678 \\ & 2.1705 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.195 \\ & 2.1950 \end{aligned}$ | $\begin{aligned} & 2.226 \\ & 2.2146 \end{aligned}$ | $\begin{aligned} & 2.2667 \\ & 2.2667 \end{aligned}$ | $\begin{aligned} & 2.2782 \\ & 2.2753 \end{aligned}$ | $\begin{array}{r} .0115 \\ .0086 \end{array}$ | $\begin{array}{r} 2.3750 \\ 2.3750 \end{array}$ |
| 2.375-8 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 A \end{aligned}$ | $\begin{aligned} & .0024 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.3726 \\ & 2.3750 \end{aligned}$ | $\begin{aligned} & 2.3576 \\ & 2.3600 \end{aligned}$ |  | 2.2914 2.2938 | 2.2833 2.2878 | .0081 .0060 | 2.2192 2.2216 | $\begin{aligned} & { }_{3 \mathrm{~B}}^{2 \mathrm{~B}} \end{aligned}$ | 2.240 2.2400 | 2.265 2.2547 | 2.2938 2.2938 | 2.3043 2.3017 | .0105 .0079 | $\begin{aligned} & 2.3750 \\ & 2.3750 \end{aligned}$ |
| 2.375-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0019 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.3731 \\ & 2.3750 \end{aligned}$ | $\begin{aligned} & 2.3617 \\ & 2.3636 \end{aligned}$ |  | $\begin{aligned} & 2.3190 \\ & 2.3209 \end{aligned}$ | $\begin{aligned} & 2.3128 \\ & 2.3163 \end{aligned}$ | $\begin{aligned} & .0062 \\ & .0046 \end{aligned}$ | $\begin{aligned} & 2.2709 \\ & 2.2728 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.285 \\ & 2.2850 \end{aligned}$ | $\begin{aligned} & 2.303 \\ & 2.2948 \end{aligned}$ | $\begin{aligned} & 2.3209 \\ & 2.3209 \end{aligned}$ | $\begin{aligned} & 2.3290 \\ & 2.3269 \end{aligned}$ | $\begin{aligned} & .0081 \\ & .0060 \end{aligned}$ | $\begin{aligned} & 2.3750 \\ & 2.3750 \end{aligned}$ |
| 2.375-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0017 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.3733 \\ & 2.3750 \end{aligned}$ | $\begin{aligned} & 2.3639 \\ & 2.3656 \end{aligned}$ |  | 2.3327 2.3344 | 2.3272 2.3303 | . 0055 | 2.2966 2.2983 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 2.307 2.3070 | $\begin{aligned} & 2.321 \\ & 2.3158 \end{aligned}$ | 2.3344 2.3344 | 2.3416 2.3398 | . 0072 | $\begin{aligned} & 2.3750 \\ & 2.3750 \end{aligned}$ |
| 2.375-20 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0015 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.3735 \\ & 2.3750 \end{aligned}$ | $\begin{aligned} & 2.3654 \\ & 2.3669 \end{aligned}$ |  | 2.3410 2.3425 | $\begin{aligned} & 2.3359 \\ & 2.3387 \end{aligned}$ | $\begin{aligned} & .0051 \\ & .0038 \end{aligned}$ | $\begin{aligned} & 2.3122 \\ & 2.3137 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.321 \\ & 2.3210 \end{aligned}$ | $\begin{aligned} & 2.332 \\ & 2.3287 \end{aligned}$ | $\begin{aligned} & 2.3425 \\ & 2.3425 \end{aligned}$ | $\begin{aligned} & 2.3491 \\ & 2.3475 \end{aligned}$ | .0066 .0050 | $\begin{array}{r} 2.3750 \\ 2.3750 \end{array}$ |
| 2.500-4 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} .0031 \\ .0031 \\ .0000 \end{array}$ | $\begin{aligned} & 2.4969 \\ & 2.4969 \\ & 2.5000 \end{aligned}$ | $\begin{aligned} & 2.4612 \\ & 2.4731 \\ & 2.4762 \end{aligned}$ | 2.4612 | $\begin{aligned} & 2.3345 \\ & 2.33+5 \\ & 2.3376 \end{aligned}$ | $\begin{aligned} & 2.3100 \\ & 2.3241 \\ & 2.3298 \end{aligned}$ | $\begin{aligned} & .0155 \\ & .0104 \\ & .0078 \end{aligned}$ | $\begin{aligned} & 2.1902 \\ & 2.1902 \\ & 2.1933 \end{aligned}$ | $\begin{aligned} & 1 \mathrm{~B} \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.229 \\ & 2.229 \\ & 2.2290 \end{aligned}$ | $\begin{aligned} & 2.267 \\ & 2.267 \\ & 2.2594 \end{aligned}$ | $\begin{aligned} & 2.3376 \\ & 2.3376 \\ & 2.3376 \end{aligned}$ | $\begin{aligned} & 2.3578 \\ & 2.3511 \\ & 2.3477 \end{aligned}$ | .0202 .0135 .0101 | $\begin{aligned} & 2.5000 \\ & 2.5000 \\ & 2.5000 \end{aligned}$ |
| 2.500-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0027 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.4973 \\ & 2.5000 \end{aligned}$ | $\begin{aligned} & 2.4791 \\ & 2.4818 \end{aligned}$ |  | 2.3890 2.3917 | $\begin{aligned} & 2.3800 \\ & 2.3850 \end{aligned}$ | . 0090 | $\begin{aligned} & 2.2928 \\ & 2.2955 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.320 \\ & 2.3200 \end{aligned}$ | $\begin{aligned} & 2.350 \\ & 2.3396 \end{aligned}$ | $\begin{aligned} & 2.3917 \\ & 2.3917 \end{aligned}$ | 2.4033 2.4004 | . 0116 | $\begin{aligned} & 2.5000 \\ & 2.5000 \end{aligned}$ |
| 2.500-8 | UN | 2 A | $\begin{aligned} & .0024 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.4976 \\ & 2.5000 \end{aligned}$ | $\begin{aligned} & 2.4826 \\ & 2.4850 \end{aligned}$ | 2.4751 | $\begin{aligned} & 2.4164 \\ & 2.4188 \end{aligned}$ | $\begin{aligned} & 2.4082 \\ & 2.4127 \end{aligned}$ | $\begin{aligned} & .0082 \\ & .0061 \end{aligned}$ | $\begin{aligned} & 2.3442 \\ & 2.3466 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.365 \\ & 2.3650 \end{aligned}$ | $\begin{aligned} & 2.390 \\ & 2.3797 \end{aligned}$ | $\begin{aligned} & 2.4188 \\ & 2.4188 \end{aligned}$ | $\begin{aligned} & 2.4294 \\ & 2.4268 \end{aligned}$ | $\begin{array}{r} .0106 \\ .0080 \end{array}$ | $\begin{aligned} & 2.5000 \\ & 2.5000 \end{aligned}$ |
| 2.500-12 | UN | ${ }_{3}^{2 A}$ | $\begin{aligned} & .0019 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.4981 \\ & 2.5000 \end{aligned}$ | $\begin{aligned} & 2.4867 \\ & 2.4886 \end{aligned}$ |  | $\begin{aligned} & 2.4440 \\ & 2.4459 \end{aligned}$ | $\begin{aligned} & 2.4378 \\ & 2.4413 \end{aligned}$ | $\begin{aligned} & .0062 \\ & .0046 \end{aligned}$ | $\begin{aligned} & 2.3959 \\ & 2.3978 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.410 \\ & 2.4100 \end{aligned}$ | $\begin{aligned} & 2.428 \\ & 2.4198 \end{aligned}$ | $\begin{aligned} & 2.4459 \\ & 2.4459 \end{aligned}$ | $\begin{aligned} & 2.4540 \\ & 2.4519 \end{aligned}$ | $\begin{aligned} & .0081 \\ & .0060 \end{aligned}$ | $\begin{aligned} & 2.5000 \\ & 2.5000 \end{aligned}$ |
| 2.500-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0017 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.4983 \\ & 2.5000 \end{aligned}$ | $\begin{aligned} & 2.4889 \\ & 2.4906 \end{aligned}$ |  | $\begin{aligned} & 2.4577 \\ & 2.4594 \end{aligned}$ | $\begin{aligned} & 2.4522 \\ & 2.4553 \end{aligned}$ | $\begin{aligned} & .0055 \\ & .0041 \end{aligned}$ | $\begin{aligned} & 2.4216 \\ & 2.4233 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.432 \\ & 2.4320 \end{aligned}$ | $\begin{aligned} & 2.446 \\ & 2.4408 \end{aligned}$ | $\begin{aligned} & 2.4594 \\ & 2.4594 \end{aligned}$ | $\begin{aligned} & 2.4666 \\ & 2.4648 \end{aligned}$ | $\begin{array}{r} .0072 \\ .0054 \end{array}$ | $\begin{aligned} & 2.5000 \\ & 2.5000 \end{aligned}$ |

See footnotes at end of table.

Table 2.21. Standard series limits of size-Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Externala |  |  |  |  |  |  |  |  | Internal ${ }^{\text {a }}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Allowance | Major diameter limits |  |  | Pitch diameter limits |  |  | Minor diameter ${ }^{\text {d }}$ | Class | Minor diameter limits |  | Pitch diameter limits |  |  | Major diameter <br> Min |
|  |  |  |  | Max ${ }^{\text {b }}$ | Min | Minc | Max ${ }^{\text {b }}$ | Min | Tolerance |  |  | Min | Max | Min | Max | Tolerance |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| 2.500-20 | UN | 2 A 3 A | in 0.0015 .0000 | $\begin{aligned} & i n \\ & \mathbf{2 . 4 9 8 5} \\ & \mathbf{2 . 5 0 0 0} \end{aligned}$ | $\begin{gathered} \text { in } \\ 2.4904 \\ \mathbf{2 . 4 9 1 9} \end{gathered}$ | in | in 2.4660 2.6675 | in 2.4609 2.4637 | $\begin{gathered} \text { in } \\ 0.0051 \\ .0038 \end{gathered}$ | in 2.4372 2.4387 | ${ }_{3}^{2 B}$ | $\begin{gathered} \text { in } \\ 2.446 \\ 2.4460 \end{gathered}$ | $\begin{aligned} & i n \\ & 2.457 \\ & 2.4537 \end{aligned}$ | $\begin{gathered} i n \\ 2.4675 \\ 2.4675 \end{gathered}$ | $\begin{aligned} & i n \\ & 2.4741 \\ & 2.4725 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & 0.0066 \\ & .0050 \end{aligned}$ | in <br> 2.5000 <br> 2.5000 |
| 2.625-6 | UN | 2 A | . 00000 | 2.6223 2.6250 | 2.6041 2.6068 |  | 2.5140 2.5167 | 2.5050 2.5099 | . 00090 | 2.4178 2.4205 | ${ }_{3}^{2 B}$ | 2.445 2.4450 | $\begin{aligned} & 2.475 \\ & 2.4616 \end{aligned}$ | 2.5167 2.5167 | 2.5285 2.5255 | . 0118 | $\begin{aligned} & 2.6250 \\ & 2.6250 \end{aligned}$ |
| 2.625-8 | UN | 2 A | . 00025 | $\begin{aligned} & 2.6225 \\ & 2.6250 \end{aligned}$ | $\begin{aligned} & 2.6075 \\ & 2.6100 \end{aligned}$ |  | 2.5413 2.5438 | 2.5331 2.5376 | . 00082 | 2.4691 2.4716 | $2 \mathrm{3B}$ | 2.490 2.4900 | 2.515 2.5047 | 2.5438 2.5438 | 2.5545 2.5518 | . 0107 | $\begin{aligned} & 2.6250 \\ & 2.6250 \end{aligned}$ |
| 2.625-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0019 .0000 | $\begin{aligned} & 2.6231 \\ & 2.6250 \end{aligned}$ | $\begin{aligned} & 2.6117 \\ & 2.6136 \end{aligned}$ |  | 2.5690 2.5709 | 2.5628 2.5663 | . 00062 | 2.5209 2.5228 | 2 B | 2.535 2.5350 | $\begin{aligned} & 2.553 \\ & 2.5448 \end{aligned}$ | 2.5709 2.5709 | 2.5790 2.5769 | $\begin{array}{r} .0081 \\ .0060 \end{array}$ | $\begin{aligned} & 2.6250 \\ & 2.6250 \end{aligned}$ |
| 2.625-16 | UN | 2A | . 0017 | 2.6233 2.6250 | 2.6139 2.6156 |  | 2.5827 2.5844 | 2.5772 2.5803 | . 00055 | 2.5466 2.5483 | 2B | 2.557 2.5570 | 2.571 2.5658 | 2.5844 2.5844 | 2.5916 2.5898 | . 0072 | $\begin{aligned} & 2.6250 \\ & 2.6250 \end{aligned}$ |
| 2.625-20 | UN | 2 A | . 00015 | $\begin{aligned} & 2.6235 \\ & 2.6250 \end{aligned}$ | $\begin{aligned} & 2.6154 \\ & 2.6169 \end{aligned}$ |  | 2.5910 | 2.5859 2.5887 | .0051 | 2.5622 2.5637 | 2 BB | ${ }_{2}^{2.571}$ | 2.582 2.5787 | 2.5925 2.5925 | 2.5991 2.5975 | . 00666 | $\begin{aligned} & 2.6250 \\ & 2.6250 \end{aligned}$ |
| 2.750-4 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0032 .0032 .0000 | $\begin{aligned} & 2.7468 \\ & 2.7468 \\ & 2.7500 \end{aligned}$ | $\begin{aligned} & 2.7111 \\ & 2.7230 \\ & 2.7262 \end{aligned}$ | 2.7111 | 2.5844 2.5844 2.5876 | 2.5686 2.5739 2.5797 | $\begin{array}{r} .0158 \\ .0105 \\ .0079 \end{array}$ | 2.4401 2.4401 2.4433 | $\begin{aligned} & 1 \mathrm{~B} \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.479 \\ & 2.479 \\ & 2.4790 \end{aligned}$ | $\begin{aligned} & 2.517 \\ & 2.517 \\ & 2.5094 \end{aligned}$ | $\begin{aligned} & 2.5876 \\ & 2.5876 \\ & 2.5876 \end{aligned}$ | $\begin{aligned} & 2.6082 \\ & 2.6013 \\ & 2.5979 \end{aligned}$ | $\begin{array}{r} .0206 \\ .0137 \\ .0103 \end{array}$ | $\begin{aligned} & 2.7500 \\ & 2.7500 \\ & 2.7500 \end{aligned}$ |
| 2.750-6 | UN | 2 A | . 00027 | 2.7473 2.7500 | ${ }_{2.7291}^{2.7318}$ |  | 2.6390 | 2.6299 2.6349 | .0091 | 2.5428 2.5455 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 2.570 2.5700 | $\begin{aligned} & 2.600 \\ & 2.5896 \end{aligned}$ | $\begin{aligned} & 2.6417 \\ & 2.6417 \end{aligned}$ | 2.6536 2.6506 | . 0119 | 2.7500 2.7500 |
| 2.750-8 | UN | 2 A | . 00025 | 2.7475 2.7500 | $\begin{aligned} & 2.7325 \\ & 2.7350 \end{aligned}$ | 2.7250 | 2.6663 2.6688 | 2.6580 2.6625 | . 00083 | 2.5941 2.5966 | 2B 3 B | 2.615 2.6150 | 2.640 2.6297 | 2.6688 2.6688 | 2.6796 2.6769 | . 0108 | $\begin{aligned} & 2.7500 \\ & 2.7500 \end{aligned}$ |
| 2.750-12 | UN | 2 A 3 A | $\begin{gathered} .0019 \\ .0000 \end{gathered}$ | $\begin{aligned} & 2.7481 \\ & 2.7500 \end{aligned}$ | $\begin{aligned} & 2.7367 \\ & 2.7386 \end{aligned}$ |  | 2.6940 2.6959 | $\begin{aligned} & 2.6878 \\ & 2.6913 \end{aligned}$ | . 00642 | $\begin{aligned} & 2.6459 \\ & 2.6478 \end{aligned}$ | 2B 3 | $\begin{aligned} & 2.660 \\ & 2.6600 \end{aligned}$ | $\begin{aligned} & 2.678 \\ & 2.6698 \end{aligned}$ | $\begin{aligned} & 2.6959 \\ & 2.6959 \end{aligned}$ | 2.7040 2.7019 | $\begin{aligned} & .0081 \\ & .0060 \end{aligned}$ | $\begin{array}{r} 2.7500 \\ 2.7500 \end{array}$ |
| 2.750-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 00017 | 2.7483 2.7500 | $\begin{aligned} & 2.7389 \\ & 2.7106 \end{aligned}$ |  | 2.7077 2.7094 | 2.7022 2.7053 | . 00055 | 2.6716 2.6733 | $2 \mathrm{3B}$ | $\xrightarrow{2.682}$ | 2.696 2.6908 | 2.7094 2.7094 | 2.7166 2.7148 | . 00072 | 2.7500 2.7500 |
| 2.750-20 | UN | 2 A | . 00015 | 2.7485 2.7500 | $\begin{aligned} & 2.7404 \\ & 2.7419 \end{aligned}$ |  | 2.7160 2.7175 | 2.7109 2.7137 | .0051 .0038 | 2.6872 2.6887 | $\stackrel{2 B}{3 B}$ | 2.696 2.6960 | 2.707 2.7037 | 2.7175 2.7175 | 2.7241 2.7225 | $\begin{aligned} & .0066 \\ & .0050 \end{aligned}$ | $\begin{aligned} & 2.7500 \\ & 2.7500 \end{aligned}$ |
| 2.875-6 | UN | $\underset{3 \mathrm{~A}}{2 \mathrm{~A}}$ | $\begin{aligned} & .0028 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.8722 \\ & 2.8750 \end{aligned}$ | $\begin{aligned} & 2.8540 \\ & 2.8568 \end{aligned}$ |  | $\begin{aligned} & 2.7639 \\ & 2.7667 \end{aligned}$ | $\begin{aligned} & 2.7547 \\ & 2.7598 \end{aligned}$ | . 00092 | $\begin{aligned} & 2.6677 \\ & 2.6705 \end{aligned}$ | $\begin{aligned} & { }_{3 B}^{2 B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.695 \\ & 2.6950 \end{aligned}$ | $\begin{aligned} & 2.725 \\ & 2.7146 \end{aligned}$ | $\begin{aligned} & 2.7667 \\ & 2.7667 \end{aligned}$ | $\begin{aligned} & 2.7787 \\ & 2.7757 \end{aligned}$ | $\begin{array}{r} .0120 \\ .0090 \end{array}$ | $\begin{aligned} & 2.8750 \\ & 2.8750 \end{aligned}$ |
| 2.875-8 | UN | 2 A | . 00025 | 2.8725 2.8750 | $\begin{aligned} & 2.8575 \\ & 2.8600 \end{aligned}$ |  | 2.7913 2.7938 | 2.7829 2.7875 | . 00084 | 2.7191 2.7216 | $\begin{aligned} & { }_{3 \mathrm{~B}}^{2 \mathrm{~B}} \end{aligned}$ | 2.740 2.7400 | 2.765 2.7547 | 2.7938 2.7938 | 2.8048 2.8020 | . 0110 | 2.8750 2.8750 |
| 2.875-12 | UN | 2 A | $\begin{aligned} & .0019 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.8731 \\ & 2.8750 \end{aligned}$ | $\begin{aligned} & 2.8617 \\ & 2.8636 \end{aligned}$ |  | 2.8190 2.8209 | 2.8127 2.8162 | $\begin{aligned} & .0063 \\ & .0047 \end{aligned}$ | 2.7709 2.7728 | 2 B | $\begin{aligned} & 2.785 \\ & 2.7850 \end{aligned}$ | $\begin{aligned} & 2.803 \\ & 2.7948 \end{aligned}$ | $\begin{aligned} & 2.8209 \\ & 2.8209 \end{aligned}$ | $\begin{aligned} & 2.8291 \\ & 2.8271 \end{aligned}$ | $\begin{gathered} .0082 \\ .0062 \end{gathered}$ | $\begin{aligned} & 2.8750 \\ & 2.8750 \end{aligned}$ |
| 2.875-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0017 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.8733 \\ & 2.8750 \end{aligned}$ | $\begin{aligned} & 2.8639 \\ & 2.8656 \end{aligned}$ |  | $\begin{aligned} & 2.8327 \\ & 2.8344 \end{aligned}$ | 2.8271 2.8302 | .0056 .0042 | $\begin{aligned} & 2.7966 \\ & 2.7983 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.807 \\ & 2.8070 \end{aligned}$ | $\begin{aligned} & 2.821 \\ & 2.8158 \end{aligned}$ | $\begin{aligned} & 2.8344 \\ & 2.8344 \end{aligned}$ | $\begin{aligned} & 2.8417 \\ & 2.8399 \end{aligned}$ | . 0073 | $\begin{aligned} & 2.8750 \\ & 2.8750 \end{aligned}$ |
| 2.875-20 | UN | 2 A | . 0016 | 2.8734 2.8750 | $\begin{aligned} & 2.8653 \\ & 2.8669 \end{aligned}$ |  | 2.8409 2.8425 | ${ }_{2}^{2.8357}$ | .0052 .0039 | $\stackrel{2.8121}{2.8137}$ | $2 \mathrm{3B}$ | 2.821 2.8210 | 2.832 2.8287 | 2.8425 2.8425 | 2.8493 2.8476 | . 00688 | $\begin{aligned} & 2.8750 \\ & 2.8750 \end{aligned}$ |
| 3.000-4 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0032 \\ & .0032 \\ & .0000 \end{aligned}$ | 2.9968 2.9968 3.0000 | $\begin{aligned} & 2.9611 \\ & 2.9730 \\ & 2.9762 \end{aligned}$ | 2.9611 | 2.8344 2.8344 2.8376 | 2.8183 2.8237 2.8296 | .0161 .0107 .0080 | 2.6901 2.6901 2.6933 | 1 B 2 B 3 B | 2.729 2.729 2.7290 | 2.767 2.767 2.7594 | 2.8376 2.8376 2.8376 | 2.8585 2.8515 2.8480 | .0209 .0139 .0104 | 3.0000 3.0000 3.0000 |
| 3.000-6 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{array}{r} .0028 \\ .0000 \end{array}$ | $\begin{aligned} & 2.9972 \\ & 3.0000 \end{aligned}$ | $\begin{aligned} & 2.9790 \\ & 2.9818 \end{aligned}$ |  | $\begin{aligned} & 2.8889 \\ & 2.8917 \end{aligned}$ | $\begin{aligned} & 2.8796 \\ & 2.8847 \end{aligned}$ | $\begin{aligned} & .0093 \\ & .0070 \end{aligned}$ | $\begin{aligned} & 2.7927 \\ & 2.7955 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.820 \\ & 2.8200 \end{aligned}$ | $\begin{aligned} & 2.850 \\ & 2.8396 \end{aligned}$ | $\begin{aligned} & 2.8917 \\ & 2.8917 \end{aligned}$ | $\begin{aligned} & 2.9038 \\ & 2.9008 \end{aligned}$ | $\begin{aligned} & .0121 \\ & .0091 \end{aligned}$ | $\begin{aligned} & 3.0000 \\ & 3.0000 \end{aligned}$ |
| 3.000-8 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0026 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.9974 \\ & 3.0000 \end{aligned}$ | $\begin{aligned} & 2.9824 \\ & 2.9850 \end{aligned}$ | 2.9749 | $\begin{aligned} & 2.9162 \\ & 2.9188 \end{aligned}$ | $\begin{aligned} & 2.9077 \\ & 2.9124 \end{aligned}$ | $\begin{aligned} & .0085 \\ & .0064 \end{aligned}$ | $\begin{aligned} & 2.8440 \\ & 2.8466 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.865 \\ & 2.8650 \end{aligned}$ | $\begin{aligned} & 2.890 \\ & 2.8797 \end{aligned}$ | $\begin{aligned} & 2.9188 \\ & 2.9188 \end{aligned}$ | $\begin{aligned} & 2.9299 \\ & 2.9271 \end{aligned}$ | $\begin{aligned} & .0111 \\ & .0083 \end{aligned}$ | $\begin{aligned} & 3.0000 \\ & 3.0000 \end{aligned}$ |
| 3.000-12 | UN | 2 A | . 0019 | 2.9981 3.0000 | ${ }_{2.9886}^{2.986}$ |  | 2.9440 2.9459 | 2.9377 2.9412 | $\begin{aligned} & .0063 \\ & .0047 \end{aligned}$ | 2.8959 2.8978 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.910 \\ & 2.9100 \end{aligned}$ | $\begin{aligned} & 2.928 \\ & 2.9198 \end{aligned}$ | $\begin{aligned} & 2.9459 \\ & 2.9459 \end{aligned}$ | 2.9541 2.9521 | $\begin{aligned} & .0082 \\ & .0062 \end{aligned}$ | $\begin{aligned} & 3.0000 \\ & 3.0000 \end{aligned}$ |
| 3.000-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0017 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.9983 \\ & 3.0000 \end{aligned}$ | $\begin{aligned} & 2.9889 \\ & 2.9906 \end{aligned}$ |  | $\begin{aligned} & 2.9577 \\ & 2.9594 \end{aligned}$ | $\begin{array}{r} 2.9521 \\ -2.9552 \end{array}$ | $\begin{aligned} & .0056 \\ & .0042 \end{aligned}$ | $\begin{aligned} & 2.9216 \\ & 2.9233 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.932 \\ & 2.9320 \end{aligned}$ | $\begin{aligned} & 2.946 \\ & 2.9408 \end{aligned}$ | $\begin{aligned} & 2.9594 \\ & 2.9594 \end{aligned}$ | $\begin{aligned} & 2.9667 \\ & 2.9649 \end{aligned}$ | $\begin{array}{r} .0073 \\ .0055 \end{array}$ | $\begin{aligned} & 3.0000 \\ & 3.0000 \end{aligned}$ |
| 3.000-20 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0016 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.9984 \\ & 3.0000 \end{aligned}$ | $\begin{aligned} & 2.9903 \\ & 2.9919 \end{aligned}$ |  | $\begin{aligned} & 2.9659 \\ & 2.9675 \end{aligned}$ | $\begin{aligned} & 2.9607 \\ & 2.9636 \end{aligned}$ | .0052 .0039 | ${ }_{2}^{2.93787}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 2.946 2.9460 | $\begin{aligned} & 2.957 \\ & 2.9537 \end{aligned}$ | 2.9675 2.9675 | 2.9743 2.9726 | . 00058 | $\begin{aligned} & 3.0000 \\ & 3.0000 \end{aligned}$ |
| 3.125-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0028 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 3.1222 \\ & 3.1250 \end{aligned}$ | $\begin{aligned} & 3.1040 \\ & 3.1068 \end{aligned}$ |  | $\begin{aligned} & 3.0139 \\ & 3.0167 \end{aligned}$ | $\begin{aligned} & 3.0045 \\ & 3.0097 \end{aligned}$ | $\begin{aligned} & .0094 \\ & .0070 \end{aligned}$ | 2.9177 2.9205 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.945 \\ & 2.9450 \end{aligned}$ | $\begin{aligned} & 2.975 \\ & 2.9646 \end{aligned}$ | $\begin{aligned} & 3.0167 \\ & 3.0167 \end{aligned}$ | $\begin{aligned} & 3.0289 \\ & 3.0259 \end{aligned}$ | $\begin{aligned} & .0122 \\ & .0092 \end{aligned}$ | $\begin{aligned} & 3.1250 \\ & 3.1250 \end{aligned}$ |
| 3.125-8 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{aligned} & .0026 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 3.1224 \\ & 3.1250 \end{aligned}$ | $\begin{aligned} & 3.1074 \\ & 3.1100 \end{aligned}$ |  | $\begin{aligned} & 3.0412 \\ & 3.0438 \end{aligned}$ | $\begin{aligned} & 3.0326 \\ & 3.0374 \end{aligned}$ | $\begin{aligned} & .0086 \\ & .0064 \end{aligned}$ | $\begin{aligned} & 2.9690 \\ & 2.9716 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.990 \\ & 2.9900 \end{aligned}$ | $\begin{aligned} & 3.015 \\ & 3.0047 \end{aligned}$ | $\begin{aligned} & 3.0438 \\ & 3.0438 \end{aligned}$ | $\begin{aligned} & 3.0550 \\ & 3.0522 \end{aligned}$ | $\begin{array}{r} .0112 \\ .0084 \end{array}$ | $\begin{aligned} & 3.1250 \\ & 3.1250 \end{aligned}$ |
| 3.125-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{gathered} .0019 \\ .0000 \end{gathered}$ | $\begin{aligned} & 3.1231 \\ & 3.1250 \end{aligned}$ | $\begin{aligned} & 3.1117 \\ & 3.1136 \end{aligned}$ |  | $\begin{aligned} & 3.0690 \\ & 3.0709 \end{aligned}$ | $\begin{aligned} & 3.0627 \\ & 3.0662 \end{aligned}$ | $\begin{aligned} & .0063 \\ & .0047 \end{aligned}$ | $\begin{aligned} & 3.0209 \\ & 3.0228 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.035 \\ & 3.0350 \end{aligned}$ | $\begin{aligned} & 3.053 \\ & 3.0448 \end{aligned}$ | $\begin{aligned} & 3.0709 \\ & 3.0709 \end{aligned}$ | $\begin{aligned} & 3.0791 \\ & 3.0771 \end{aligned}$ | $\begin{gathered} .0082 \\ .0062 \end{gathered}$ | $\begin{gathered} 3.1250 \\ 3.1250 \end{gathered}$ |
| 3.125-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $.0017$ | $\begin{aligned} & 3.1233 \\ & 3.1250 \end{aligned}$ | $\begin{aligned} & 3.1139 \\ & 3.1156 \end{aligned}$ |  | $\begin{aligned} & 3.0827 \\ & 3.0844 \end{aligned}$ | $\begin{aligned} & 3.0771 \\ & 3.0802 \end{aligned}$ | $\begin{aligned} & .0056 \\ & .0042 \end{aligned}$ | $\begin{aligned} & 3.0466 \\ & 3.0483 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.057 \\ & 3.0570 \end{aligned}$ | $\begin{aligned} & 3.071 \\ & 3.0658 \end{aligned}$ | $\begin{aligned} & 3.0844 \\ & 3.0844 \end{aligned}$ | $\begin{aligned} & 3.0917 \\ & 3.0899 \end{aligned}$ | $\begin{array}{r} .0073 \\ .0055 \end{array}$ | $\begin{aligned} & 3.1250 \\ & 3.1250 \end{aligned}$ |

See footnotes at end of table.

| Nominal size and threads per inch | Series designation | External ${ }^{\text {a }}$ |  |  |  |  |  |  |  |  | Internal ${ }^{\text {a }}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Allowance | Major diameter limits |  |  | Pitch diameter limits |  |  | Minor diameter ${ }^{\text {d }}$ | Class | Minor diameter limits |  | Pitch diameter limits |  |  | $\begin{gathered} \begin{array}{c} \text { Major } \\ \text { diam- } \\ \text { eter } \end{array} \\ \hline \text { Min } \end{gathered}$ |
|  |  |  |  | Max ${ }^{\text {b }}$ | Min | Minc | Max ${ }^{\text {b }}$ | Min | Tolerance |  |  | Min | Max | Min | Max | Tolerance |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| 3.250-1 | UNC | 14 24 3 A |  | in 3.2467 3.2467 3.2500 | $\begin{gathered} \text { in } \\ 3.2110 \\ 3.2229 \\ 3.2262 \end{gathered}$ | in | in 3.0843 3.0843 3.0876 | in 3.0680 3.0734 3.0794 | in 0.0163 .0109 .0082 | in 2.9400 2.9400 2.9433 | 1 B 2 B 3 B | $\quad$ in 2.979 2.979 2.9790 | $\quad$ in 3.017 3.017 3.0094 | in 3.0876 3.0876 3.0876 | in 3.1088 3.1017 3.0982 | in 0.0212 .0141 .0106 | $\begin{aligned} & i n \\ & 3.2500 \\ & 3.2500 \\ & 3.2500 \end{aligned}$ |
| 3.250-6 | UN | 2A | $\begin{aligned} & .0028 \\ & .0000 \end{aligned}$ | 3.2472 3.2500 | $\begin{aligned} & 3.2290 \\ & 3.2318 \end{aligned}$ |  | 3.1389 3.1417 | 3.1294 3.1346 | . 0095 | 3.0427 3.0455 | $2 \mathrm{3B}$ | $\begin{aligned} & 3.070 \\ & 3.0700 \end{aligned}$ | $\begin{aligned} & 3.100 \\ & 3.0896 \end{aligned}$ | 3.1417 3.1417 | $\begin{aligned} & 3.1540^{\circ} \\ & 3.1509 \end{aligned}$ | $\begin{aligned} & .0123 \\ & .0092 \end{aligned}$ | $\begin{aligned} & 3.2500 \\ & 3.2500 \end{aligned}$ |
| $3.250-8$ | UN | 2 A | .0026 .0000 | 3.2474 3.2500 | $\begin{aligned} & 3.2324 \\ & 3.2350 \end{aligned}$ | 3.2249 | 3.1662 3.1688 | 3.1575 3.1623 | . 0087 | 3.0940 3.0966 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.115 \\ & 3.1150 \end{aligned}$ | $\begin{aligned} & 3.140 \\ & 3.1297 \end{aligned}$ | 3.1688 3.1688 | 3.1801 3.1773 | .0113 .0085 | $\begin{aligned} & 3.2500 \\ & 3.2500 \end{aligned}$ |
| 3.250-12 | UN | 2 A | .0019 .0000 | 3.2481 3.2500 | $\begin{aligned} & 3.2367 \\ & 3.2386 \end{aligned}$ |  | 3.1940 3.1959 | 3.1877 3.1912 | . 0063 | 3.1459 3.1478 | ${ }_{3}^{2 B}$ | 3.160 3.1600 | 3.178 <br> 3.1698 | 3.1959 3.1959 | 3.2041 3.2021 | $\begin{aligned} & .0082 \\ & .0062 \end{aligned}$ | $\begin{aligned} & 3.2500 \\ & 3.2500 \end{aligned}$ |
| 3.250-16 | UN | 2A | $\begin{aligned} & .0017 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 3.2483 \\ & 3.2500 \end{aligned}$ | $\begin{aligned} & 3.2389 \\ & 3.2406 \end{aligned}$ |  | 3.2077 3.2094 | 3.2021 3.2052 | .0056 .0042 | $\begin{aligned} & 3.1716 \\ & 3.1733 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.182 \\ & 3.1820 \end{aligned}$ | $\begin{aligned} & 3.196 \\ & 3.1908 \end{aligned}$ | $\begin{aligned} & 3.2094 \\ & 3.2094 \end{aligned}$ | $\begin{aligned} & 3.2167 \\ & 3.2149 \end{aligned}$ | $\begin{aligned} & .0073 \\ & .0055 \end{aligned}$ | $\begin{aligned} & 3.2500 \\ & 3.2500 \end{aligned}$ |
| 3.375-6 | UN | 2A | . 0029 | 3.3721 3.3750 | 3.3539 3.3568 |  | 3.2638 3.2667 | 3.2543 3.2595 | . 0095 | 3.1676 3.1705 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 3.195 3.1950 | $\begin{aligned} & 3.225 \\ & 3.2146 \end{aligned}$ | 3.2667 3.2667 | 3.2791 3.2760 | . 0124 | 3.3750 3.3750 |
| 3.375-8 | UN | 2 A | . 0026 | $\begin{aligned} & 3.3724 \\ & 3.3750 \end{aligned}$ | $\begin{aligned} & 3.3574 \\ & 3.3600 \end{aligned}$ |  | 3.2912 3.2938 | 3.2824 3.2872 | . 0088 | 3.2190 3.2216 | 2 B 3 B | $\begin{aligned} & 3.240 \\ & 3.2400 \end{aligned}$ | $\begin{aligned} & 3.265 \\ & 3.2547 \end{aligned}$ | $\begin{aligned} & 3.2938 \\ & 3.2938 \end{aligned}$ | $\begin{aligned} & 3.3052 \\ & 3.3023 \end{aligned}$ | $\begin{aligned} & .0114 \\ & .0085 \end{aligned}$ | $\begin{aligned} & 3.3750 \\ & 3.3750 \end{aligned}$ |
| 3.375-12 | UN | 2 A | . 0019 | 3.3731 3.3750 | 3.3617 3.3636 |  | 3.3190 3.3209 | 3.3126 3.3161 | . 0064 | 3.2709 3.2728 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.285 \\ & 3.2850 \end{aligned}$ | $\begin{aligned} & 3.303 \\ & 3.2948 \end{aligned}$ | 3.3209 3.3209 | 3.3293 3.3272 | . 0084 | $\begin{aligned} & 3.3750 \\ & 3.3750 \end{aligned}$ |
| 3.375-16 | UN | 2 A | .0017 .0000 | 3.3733 3.3750 | $\begin{aligned} & 3.3639 \\ & 3.3656 \end{aligned}$ |  | 3.3327 3.3344 | 3.3269 3.3301 | . 0058 | 3.2966 3.2983 | ${ }_{3}^{2 B}$ | 3.307 3.3070 | 3.321 3.3158 3. | 3.3344 3.3344 | 3.3419 3.3400 | . 0075 | 3.3750 3.3750 |
| 3.500-4 | UNC | 1 A 2 A 3 A | .0033 .0033 .0000 | $\begin{aligned} & 3.4967 \\ & 3.4967 \\ & 3.5000 \end{aligned}$ | $\begin{aligned} & 3.4610 \\ & 3.4729 \\ & 3.4762 \end{aligned}$ | 3.4610 | 3.3343 3.3334 3.3376 | $\begin{aligned} & 3.3177 \\ & 3.3233 \\ & 3.3293 \end{aligned}$ | .0166 .0110 .0083 | 3.1900 3.1900 3.1933 | 1 B 2 B 3 B | 3.229 3.229 3.2290 | 3.267 3.267 3.2594 | $\begin{aligned} & 3.3376 \\ & 3.3376 \\ & 3.3376 \end{aligned}$ | $\begin{aligned} & 3.3591 \\ & 3.3519 \\ & 3.3484 \end{aligned}$ | $\begin{aligned} & .0215 \\ & .0143 \\ & .0108 \end{aligned}$ | $\begin{aligned} & 3.5000 \\ & 3.5000 \\ & 3.5000 \end{aligned}$ |
| $3.500-6$ | UN | 2 A | . 0029 | 3.4971 3.5000 | $\begin{aligned} & 3.4789 \\ & 3.4818 \end{aligned}$ |  | 3.3888 3.3917 | 3.3792 3.3845 | . 0096 | 3.2926 3.2955 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 3.320 3.3200 | 3.350 3.3396 | 3.3917 3.3917 | 3.4042 3.4011 | . 0125 | $\begin{aligned} & 3.5000 \\ & 3.5000 \end{aligned}$ |
| 3.500-8 | UN | 2 A | . 0026 | $\begin{aligned} & 3.4974 \\ & 3.5000 \end{aligned}$ | $\begin{aligned} & 3.4824 \\ & 3.4850 \end{aligned}$ | 3.4749 | 3.4162 3.4188 | 3.4074 3.4122 | . 00888 | 3.3440 3.3466 | ${ }_{3}^{2 B}$ | $\begin{aligned} & 3.365 \\ & 3.3650 \end{aligned}$ | 3.390 3.3797 | 3.4188 3.4188 | 3.4303 3.4274 | . 0115 | $\begin{aligned} & 3.5000 \\ & 3.5000 \end{aligned}$ |
| 3.500-12 | UN | 2A | $\begin{array}{r} .0019 \\ .0000 \end{array}$ | $\begin{aligned} & 3.4981 \\ & 3.5000 \end{aligned}$ | $\begin{aligned} & 3.4867 \\ & 3.4886 \end{aligned}$ |  | 3.4440 3.4459 | 3.4376 3.4411 | . 0064 | 3.3959 3.3978 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.410 \\ & 3.4100 \end{aligned}$ | $\begin{aligned} & 3.428 \\ & 3.4198 \end{aligned}$ | $\begin{aligned} & 3.4459 \\ & 3.4459 \end{aligned}$ | $\begin{aligned} & 3.4543 \\ & 3.4522 \end{aligned}$ | . 00084 | $\begin{aligned} & 3.5000 \\ & 3.5000 \end{aligned}$ |
| 3.500-16 | UN | 2 A | . 00017 | 3.4983 3.5000 | $\begin{aligned} & 3.4889 \\ & 3.4906 \end{aligned}$ |  | 3.4577 3.4594 | 3.4519 3.4551 | . 0058 | 3.4216 3.4233 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 3.432 3.4320 | 3.446 3.4408 | 3.4594 3.4594 | 3.4669 3.4650 | . 0075 | $\begin{aligned} & 3.5000 \\ & 3.5000 \end{aligned}$ |
| 3.625-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{gathered} .0029 \\ .0000 \end{gathered}$ | $\begin{aligned} & 3.6221 \\ & 3.6250 \end{aligned}$ | $\begin{aligned} & 3.6039 \\ & 3.6068 \end{aligned}$ |  | 3.5138 3.5167 | 3.5041 3.5094 | $\begin{aligned} & .0097 \\ & .0073 \end{aligned}$ | $\begin{aligned} & 3.4176 \\ & 3.4205 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.445 \\ & 3.4450 \end{aligned}$ | $\begin{aligned} & 3.475 \\ & 3.4646 \end{aligned}$ | $\begin{aligned} & 3.5167 \\ & 3.5167 \end{aligned}$ | $\begin{aligned} & 4.5293 \\ & 3.5262 \end{aligned}$ | $\begin{aligned} & .0126 \\ & .0095 \end{aligned}$ | $\begin{aligned} & 3.6250 \\ & 3.6250 \end{aligned}$ |
| 3.625-8 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0027 .0000 | 3.6223 3.6250 | $\begin{aligned} & 3.6073 \\ & 3.6100 \end{aligned}$ |  | 3.5411 3.5438 | 3.5322 3.5371 | . 00089 | 3.4689 3.4716 | $\begin{aligned} & { }_{3 B}^{2 B} \\ & 3 \end{aligned}$ | $\begin{aligned} & 3.490 \\ & 3.4900 \end{aligned}$ | 3.515 3.5047 | $\begin{aligned} & 3.5438 \\ & 3.5438 \end{aligned}$ | 3.5554 3.5525 | . 0116 | $\begin{aligned} & 3.6250 \\ & 3.6250 \end{aligned}$ |
| 3.625-12 | UN | 2 A | $\begin{array}{r} .0019 \\ .0000 \end{array}$ | $\begin{aligned} & 3.6231 \\ & 3.6250 \end{aligned}$ | $\begin{aligned} & 3.6117 \\ & 3.6136 \end{aligned}$ |  | $\begin{aligned} & 3.5690 \\ & 3.5709 \end{aligned}$ | 3.5626 3.5661 | $\begin{aligned} & .0064 \\ & .0048 \end{aligned}$ | $\begin{aligned} & 3.5209 \\ & 3.5228 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.535 \\ & 3.5350 \end{aligned}$ | $\begin{aligned} & 3.553 \\ & 3.5448 \end{aligned}$ | $\begin{aligned} & 3.5709 \\ & 3.5709 \end{aligned}$ | $\begin{aligned} & 3.5793 \\ & 3.5772 \end{aligned}$ | $\begin{aligned} & .0084 \\ & .0063 \end{aligned}$ | $\begin{aligned} & 3.6250 \\ & 3.6250 \end{aligned}$ |
| 3.625-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0017 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 3.6233 \\ & 3.6250 \end{aligned}$ | $\begin{aligned} & 3.6139 \\ & 3.6156 \end{aligned}$ |  | 3.5827 3.5844 | $\begin{aligned} & 3.5769 \\ & 3.5801 \end{aligned}$ | . 0058 | $\begin{aligned} & 3.5466 \\ & 3.5483 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.557 \\ & 3.5570 \end{aligned}$ | $\begin{aligned} & 3.571 \\ & 3.5658 \end{aligned}$ | $\begin{aligned} & 3.5844 \\ & 3.5844 \end{aligned}$ | $\begin{aligned} & 3.5919 \\ & 3.5900 \end{aligned}$ | $\begin{aligned} & .0075 \\ & .0056 \end{aligned}$ | $\begin{aligned} & 3.6250 \\ & 3.6250 \end{aligned}$ |
| 3.750-4 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0034 .0034 .0000 | $\begin{aligned} & 3.7466 \\ & 3.7466 \\ & 3.7500 \end{aligned}$ | $\begin{aligned} & 3.7109 \\ & 3.7228 \\ & 3.7262 \end{aligned}$ | 3.7109 | 3.5842 3.5842 3.5876 | 3.5674 3.5730 3.5792 | .0168 .0112 .0084 | 3.4399 3.4399 3.4433 | $\begin{aligned} & 1 \mathrm{~B} \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 3.479 3.479 3.4790 | 3.517 3.517 3.5094 | $\begin{aligned} & 3.5876 \\ & 3.5876 \\ & 3.5876 \end{aligned}$ | $\begin{aligned} & 3.6094 \\ & 3.6021 \\ & 3.5985 \end{aligned}$ | .0218 .0145 .0109 | $\begin{aligned} & 3.7500 \\ & 3.7500 \\ & 3.7500 \end{aligned}$ |
| 3.750-6 | UN | 2 A | $\begin{array}{r} .0029 \\ .0000 \end{array}$ | $\begin{aligned} & 3.7 \pm 71 \\ & 3.7500 \end{aligned}$ | $\begin{aligned} & 3.7289 \\ & 3.7318 \end{aligned}$ |  | $\begin{aligned} & 3.6388 \\ & 3.6417 \end{aligned}$ | $\begin{aligned} & 3.6290 \\ & 3.6344 \end{aligned}$ | $\begin{aligned} & .0098 \\ & .0073 \end{aligned}$ | $\begin{aligned} & 3.5426 \\ & 3.5455 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.570 \\ & 3.5700 \end{aligned}$ | $\begin{aligned} & 3.600 \\ & 3.5896 \end{aligned}$ | $\begin{aligned} & 3.6417 \\ & 3.6417 \end{aligned}$ | $\begin{aligned} & 3.6544 \\ & 3.6512 \end{aligned}$ | $\begin{aligned} & .0127 \\ & .0095 \end{aligned}$ | $\begin{aligned} & 3.7500 \\ & 3.7500 \end{aligned}$ |
| $3.750-8$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0027 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 3.7473 \\ & 3.7500 \end{aligned}$ | $\begin{aligned} & 3.7323 \\ & 3.7350 \end{aligned}$ | 3.7248 | $\begin{aligned} & 3.6661 \\ & 3.6688 \end{aligned}$ | $\begin{aligned} & 3.6571 \\ & 3.6621 \end{aligned}$ | $\begin{aligned} & .0090 \\ & .0067 \end{aligned}$ | $\begin{aligned} & 3.5939 \\ & 3.5966 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.615 \\ & 3.6150 \end{aligned}$ | $\begin{aligned} & 3.640 \\ & 3.6297 \end{aligned}$ | $\begin{aligned} & 3.6688 \\ & 3.6688 \end{aligned}$ | $\begin{aligned} & 3.6805 \\ & 3.6776 \end{aligned}$ | . 0117 | $\begin{aligned} & 3.7500 \\ & 3.7500 \end{aligned}$ |
| $3.750-12$ | UN | ${ }_{3}^{2 A}$ | . 00019 | 3.7481 3.7500 | $\begin{aligned} & 3.7367 \\ & 3.7386 \end{aligned}$ |  | $\begin{aligned} & 3.6940 \\ & 3.6959 \end{aligned}$ | 3.6876 3.6911 | $.0064$ | 3.6459 3.6478 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.660 \\ & 3.6600 \end{aligned}$ | $\begin{aligned} & 3.678 \\ & 3.6698 \end{aligned}$ | $\begin{aligned} & 3.6959 \\ & 3.6959 \end{aligned}$ | $\begin{aligned} & 3.7043 \\ & 3.7022 \end{aligned}$ | . 0084 | $\begin{aligned} & 3.7500 \\ & 3.7500 \end{aligned}$ |
| 3.750-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0017 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 3.7483 \\ & 3.7500 \end{aligned}$ | $\begin{aligned} & 3.7389 \\ & 3.7406 \end{aligned}$ |  | $\begin{aligned} & 3.7077 \\ & 3.7094 \end{aligned}$ | $\begin{aligned} & 3.7019 \\ & 3.7051 \end{aligned}$ | $\begin{aligned} & .0058 \\ & .0043 \end{aligned}$ | $\begin{aligned} & 3.6716 \\ & 3.6733 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.682 \\ & 3.6820 \end{aligned}$ | $\begin{aligned} & 3.696 \\ & 3.6908 \end{aligned}$ | $\begin{aligned} & 3.7094 \\ & 3.7094 \end{aligned}$ | $\begin{aligned} & 3.7169 \\ & 3.7150 \end{aligned}$ | $\begin{aligned} & .0075 \\ & .0056 \end{aligned}$ | $\begin{aligned} & 3.7500 \\ & 3.7500 \end{aligned}$ |
| 3.875-6 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | . 00030 | $\begin{aligned} & 3.8720 \\ & 3.8750 \end{aligned}$ | $\begin{aligned} & 3.8538 \\ & 3.8568 \end{aligned}$ |  | $\begin{aligned} & 3.7637 \\ & 3.7667 \end{aligned}$ | $\begin{aligned} & 3.7538 \\ & 3.7593 \end{aligned}$ | $\begin{aligned} & .0099 \\ & .0074 \end{aligned}$ | $\begin{aligned} & 3.6675 \\ & 3.6705 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.695 \\ & 3.6950 \end{aligned}$ | $\begin{aligned} & 3.725 \\ & 3.7146 \end{aligned}$ | $\begin{aligned} & 3.7667 \\ & 3.7667 \end{aligned}$ | $\begin{aligned} & 3.7795 \\ & 3.7763 \end{aligned}$ | $\begin{aligned} & .0128 \\ & .0096 \end{aligned}$ | $\begin{aligned} & 3.8750 \\ & 3.8750 \end{aligned}$ |
| 3.875-8 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0027 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 3.8723 \\ & 3.8750 \end{aligned}$ | $\begin{aligned} & 3.8573 \\ & 3.8600 \end{aligned}$ |  | $\begin{aligned} & 3.7911 \\ & 3.7938 \end{aligned}$ | $\begin{aligned} & 3.7820 \\ & 3.7870 \end{aligned}$ | $\begin{array}{r} .0091 \\ .0068 \end{array}$ | $\begin{aligned} & 3.7189 \\ & 3.7216 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.740 \\ & 3.7400 \end{aligned}$ | $\begin{aligned} & 3.765 \\ & 3.7517 \end{aligned}$ | $\begin{aligned} & 3.7938 \\ & 3.7938 \end{aligned}$ | $\begin{aligned} & 3.8056 \\ & 3.8026 \end{aligned}$ | $\begin{aligned} & .0118 \\ & .0088 \end{aligned}$ | $\begin{aligned} & 3.8750 \\ & 3.8750 \end{aligned}$ |
| 3.875-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0020 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 3.8730 \\ & 3.8750 \end{aligned}$ | $\begin{aligned} & 3.8616 \\ & 3.8636 \end{aligned}$ |  | $\begin{aligned} & 3.8189 \\ & 3.8209 \end{aligned}$ | $\begin{aligned} & 3.8124 \\ & 3.8160 \end{aligned}$ | $\begin{aligned} & .0065 \\ & .0049 \end{aligned}$ | $\begin{aligned} & 3.7708 \\ & 3.7728 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.785 \\ & 3.7850 \end{aligned}$ | $\begin{aligned} & 3.803, \\ & 3.7948 \end{aligned}$ | $\begin{aligned} & 3.8209 \\ & 3.8209 \end{aligned}$ | $\begin{aligned} & 3.8294 \\ & 3.8273 \end{aligned}$ | $\begin{aligned} & .0085 \\ & .0064 \end{aligned}$ | $\begin{aligned} & 3.8750 \\ & 3.8750 \end{aligned}$ |
| 3.875-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0018 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 3.8732 \\ & 3.8750 \end{aligned}$ | $\begin{aligned} & 3.8638 \\ & 3.8656 \end{aligned}$ |  | $\begin{aligned} & 3.8326 \\ & 3.8344 \end{aligned}$ | $\begin{aligned} & 3.8267 \\ & 3.8300 \end{aligned}$ | $\begin{aligned} & .0059 \\ & .0044 \end{aligned}$ | $\begin{aligned} & 3.7965 \\ & 3.7983 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 3.807 \\ & 3.8070 \end{aligned}$ | $\begin{aligned} & 3.821 \\ & 3.8158 \end{aligned}$ | $\begin{aligned} & 3.8344 \\ & 3.8344 \end{aligned}$ | $\begin{aligned} & 3.8420 \\ & 3.8401 \end{aligned}$ | $\begin{aligned} & .0076 \\ & .0057 \end{aligned}$ | $\begin{aligned} & 3.8750 \\ & 3.8750 \end{aligned}$ |

See footnotes at end of table.

Table 2.21. Standard series limits of size-Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Externala |  |  |  |  |  |  |  |  | Internala |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Allowance | Major diameter limits |  |  | Pitch diameter limits |  |  | Minor diameter ${ }^{\text {d }}$ | Class | Minor diameter limits |  | Pitch diameter limits |  |  | Major <br> diameter <br> Min |
|  |  |  |  | Max ${ }^{\text {b }}$ | Min | Min ${ }^{\text {c }}$ | Max ${ }^{\text {b }}$ | Mill | Tolerance |  |  | Min | Max | Min | Max | Tolerance |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| 4.000-4 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ |  |  | $i n$ 3.9609 3.9728 3.9762 | in |  |  | in 0.0170 .0113 .0085 | in 3.6899 3.6899 3.6933 | 1B 2B 3 B | in 3.729 3.729 3.7290 | $\quad i n$ <br> 3.767 <br> 3.767 <br> 3.7594 <br>  <br>  <br>  | in 3.8376 3.8376 3.8376 | in 3.8597 3.8523 3.8487 | $\begin{gathered} \text { in } \\ 0.0221 \\ .0147 \\ .0111 \end{gathered}$ | $\begin{aligned} & \text { in } \\ & 4.0000 \\ & 4.0000 \\ & 4.0000 \end{aligned}$ |
| 4.000-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0030 .0000 | 3.9970 4.0000 | $\begin{aligned} & 3.9788 \\ & 3.9818 \end{aligned}$ |  | 3.8887 3.8917 | 3.8788 3.8843 | $\begin{aligned} & .0099 \\ & .0074 \end{aligned}$ | 3.7925 3.7955 | 2B 3 B | 3.820 3.8200 | 3.850 3.8396 | 3.8917 3.8917 | 3.9046 3.9014 | $\begin{array}{r} .0129 \\ .0097 \end{array}$ | $\begin{aligned} & 4.0000 \\ & 4.0000 \end{aligned}$ |
| $4.000-8$ | UN | 2A | .0027 .0000 | 3.9973 4.0000 | 3.9823 3.9850 | 3.9748 | 3.9161 3.9188 | 3.9070 3.9120 | . 00991 | 3.8439 3.8466 | 2B ${ }^{\text {B }}$ | 3.865 3.8650 | 3.890 3.8798 | 3.9188 3.9188 | 3.9307 3.9277 | .0119 .0089 | 4.0000 4.0000 |
| 4.000-12 | UN | 2A | .0020 .0000 | $\begin{aligned} & 3.9980 \\ & 4.0000 \end{aligned}$ | $\begin{aligned} & 3.9866 \\ & 3.9886 \end{aligned}$ |  | 3.9439 3.9459 | 3.9374 3.9410 | . 0065 | 3.8958 3.8978 | $2 \mathrm{3B}$ | 3.910 3.9100 | 3.928 3.9198 | 3.9459 3.9459 | 3.9544 3.9523 | . 00085 | $\begin{aligned} & 4.0000 \\ & 4.0000 \end{aligned}$ |
| 4.000-16 | UN | 2A | . 00018 | 3.9982 4.0000 | $\begin{aligned} & 3.9888 \\ & 3.9906 \end{aligned}$ |  | 3.9576 3.9594 | 3.9517 3.9550 | . 00059 | 3.9215 3.9233 | ${ }_{3}^{2 B}$ | 3.932 3.9320 | 3.946 <br> 3.9408 | 3.9594 3.9594 | 3.9670 3.9651 | $\begin{aligned} & .0076 \\ & .0057 \end{aligned}$ | $\begin{aligned} & 4.0000 \\ & 4.0000 \end{aligned}$ |
| 4.125-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0030 .0000 | 4.1220 4.1250 | $\begin{aligned} & 4.1038 \\ & 4.1068 \end{aligned}$ |  | 4.0137 4.0167 | 4.0037 4.0092 | .0100 .0075 | 3.9175 3.9205 | $2 \mathrm{3B}$ | 3.945 3.9450 | 3.975 3.9646 | 4.0167 4.0167 | 4.0297 4.0264 | .0130 .0097 | 4.1250 4.1250 |
| 4.125-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0020 .0000 | $\begin{aligned} & 4.1230 \\ & 4.1250 \end{aligned}$ | $\begin{aligned} & 4.1116 \\ & 4.1136 \end{aligned}$ |  | 4.0689 4.0709 | 4.0624 4.0660 | $\begin{aligned} & .0065 \\ & .0049 \end{aligned}$ | $\begin{aligned} & 4.0208 \\ & 4.0228 \end{aligned}$ | 2B ${ }_{3}$ | 4.035 4.0350 | 4.053 4.0448 | 4.0709 4.0709 | 4.0794 4.0773 | . 0085 | $\begin{aligned} & 4.1250 \\ & 4.1250 \end{aligned}$ |
| 4.125-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 0018 | 4.1232 4.1250 | $\begin{aligned} & 4.1138 \\ & 4.1156 \end{aligned}$ |  | 4.0826 4.0844 | 4.0767 4.0800 | . 00059 | 4.0465 4.0483 | 2B | 4.057 4.0570 | $\begin{aligned} & 4.071 \\ & 4.0658 \end{aligned}$ | 4.0844 4.0844 | 4.0920 4.0901 | .0076 .0057 | $\begin{aligned} & 4.1250 \\ & 4.1250 \end{aligned}$ |
| 4.250-4 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0034 .0000 | 4.2466 4.2500 | $\begin{aligned} & 4.2228 \\ & 4.2262 \end{aligned}$ |  | 4.0842 4.0876 | 4.0727 4.0790 | . 0115 | 3.9399 3.9433 | 2B 3 | 3.979 3.9790 | 4.017 4.0094 | 4.0876 4.0876 | 4.1025 4.0988 | . 0149 | $\begin{aligned} & 4.2500 \\ & 4.2500 \end{aligned}$ |
| 4.250-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0030 .0000 | $\begin{aligned} & 4.2470 \\ & 4.2500 \end{aligned}$ | $\begin{aligned} & 4.2288 \\ & 4.2318 \end{aligned}$ |  | 4.1387 4.1417 | 4.1286 4.1342 | .0101 .0075 | 4.0425 4.0455 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 4.070 4.0700 | $\begin{aligned} & 4.100 \\ & 4.0896 \end{aligned}$ | $\begin{aligned} & 4.1417 \\ & 4.1417 \end{aligned}$ | 4.1548 4.1515 | .0131 .0098 | $\begin{aligned} & 4.2500 \\ & 4.2500 \end{aligned}$ |
| 4. 250-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0020 .0000 | 4.2480 4.2500 | $\begin{aligned} & 4.2366 \\ & 4.2386 \end{aligned}$ |  | 4.1939 4.1959 | 4.1874 4.1910 | . 0065 | 4.1458 4.1478 | 2B ${ }_{3}$ | 4.160 4.1600 | 4.178 4.1698 | 4.1959 4.1959 | 4.2044 4.2023 | . 00085 | 4.2500 4.2500 |
| 4.250-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0018 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 4.2482 \\ & 4.2500 \end{aligned}$ | $\begin{aligned} & 4.2388 \\ & 4.2406 \end{aligned}$ |  | 4.2076 4.2094 | 4.2017 4.2050 | .0059 .0044 | 4.1715 4.1733 | 2B ${ }^{\text {B }}$ | $\begin{aligned} & 4.182 \\ & 4.1820 \end{aligned}$ | $\begin{aligned} & 4.196 \\ & 4.1908 \end{aligned}$ | $\begin{aligned} & 4.2094 \\ & 4.2094 \end{aligned}$ | 4.2170 4.2151 | .0076 .0057 | 4.2500 4.2500 |
| 4.375-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0030 .0000 | $\begin{aligned} & 4.3720 \\ & 4.3750 \end{aligned}$ | $\begin{aligned} & 4.3538 \\ & 4.3568 \end{aligned}$ |  | 4.2637 4.2667 | 4.2536 4.2591 | . 0101 | 4.1675 4.1705 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 4.195 4.1950 | 4.225 4.2146 | $\begin{aligned} & 4.2667 \\ & 4.2667 \end{aligned}$ | $\begin{aligned} & 4.2799 \\ & 4.2766 \end{aligned}$ | .0132 .0099 | 4.3750 4.3750 |
| 4.375-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0020 .0000 | 4.3730 4.3750 | $\begin{aligned} & 4.3616 \\ & 4.3636 \end{aligned}$ |  | 4.3189 4.3209 | 4.3124 4.3160 | .0065 .0049 | 4.2708 4.2728 | ${ }_{3}^{2 B}$ | 4.285 4.2850 | 4.303 4.2948 | 4.3209 4.3209 | 4.3294 4.3273 | .0085 .0064 | 4.3750 4.3750 |
| 4.375-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0018 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 4.3732 \\ & 4.3750 \end{aligned}$ | $\begin{aligned} & 4.3638 \\ & 4.3656 \end{aligned}$ |  | 4.3326 4.3344 | $\begin{aligned} & 4.3267 \\ & 4.3300 \end{aligned}$ | $\begin{array}{r} .0059 \\ .0044 \end{array}$ | $\begin{aligned} & 4.2965 \\ & 4.2983 \end{aligned}$ | $2 \mathrm{3B}$ | $\begin{aligned} & 4.307 \\ & 4.3070 \end{aligned}$ | $\begin{aligned} & 4.321 \\ & 4.3158 \end{aligned}$ | $\begin{aligned} & 4.3344 \\ & 4.3344 \end{aligned}$ | $\begin{aligned} & 4.3420 \\ & 4.3401 \end{aligned}$ | . 00076 | $\begin{aligned} & 4.3750 \\ & 4.3750 \end{aligned}$ |
| 4.500-4 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0035 .0000 | $\begin{aligned} & 4.4965 \\ & 4.5000 \end{aligned}$ | $\begin{aligned} & 4.4727 \\ & 4.4762 \end{aligned}$ |  | 4.3341 4.3376 | 4.3225 4.3289 | . 0116 | $\begin{aligned} & 4.1898 \\ & 4.1933 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 4.229 \\ & 4.2290 \end{aligned}$ | $\begin{aligned} & 4.267 \\ & 4.2594 \end{aligned}$ | $\begin{aligned} & 4.3376 \\ & 4.3376 \end{aligned}$ | 4.3527 4.3489 | . 0151 | 4.5000 4.5000 |
| 4.500-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0031 .0000 | $\begin{aligned} & 4.4969 \\ & 4.5600 \end{aligned}$ | $\begin{aligned} & 4.4787 \\ & 4.4818 \end{aligned}$ |  | 4.3886 4.3917 | 4.3784 4.3840 | .0102 .0077 | 4.2924 4.2955 | 2B ${ }^{\text {B }}$ | 4.320 4.3200 | $\begin{aligned} & 4.350 \\ & 4.3396 \end{aligned}$ | $\begin{aligned} & 4.3917 \\ & 4.3917 \end{aligned}$ | $\begin{aligned} & 4.4050 \\ & 4.4016 \end{aligned}$ | .0133 .0099 | 4.5000 4.5000 |
| 4.500-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0020 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 4.4980 \\ & 4.5000 \end{aligned}$ | $\begin{aligned} & 4.4866 \\ & 4.4886 \end{aligned}$ |  | $\begin{aligned} & 4.4439 \\ & 4.4459 \end{aligned}$ | $\begin{aligned} & 4.4374 \\ & 4.4410 \end{aligned}$ | $\begin{aligned} & .0065 \\ & .0049 \end{aligned}$ | $\begin{aligned} & 4.3958 \\ & 4.3978 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 4.410 \\ & 4.4100 \end{aligned}$ | $\begin{aligned} & 4.428 \\ & 4.4198 \end{aligned}$ | $\begin{aligned} & 4.4459 \\ & 4.4459 \end{aligned}$ | $\begin{aligned} & 4.4544 \\ & 4.4523 \end{aligned}$ | $\begin{aligned} & .0085 \\ & .0064 \end{aligned}$ | $\begin{aligned} & 4.5000 \\ & 4.5000 \end{aligned}$ |
| 4.500-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\text { . } 0018$ | $\begin{aligned} & 4.4982 \\ & 4.5000 \end{aligned}$ | $\begin{aligned} & 4.4888 \\ & 4.4906 \end{aligned}$ |  | $\begin{aligned} & 4.4576 \\ & 4.4594 \end{aligned}$ | $\begin{aligned} & 4.4517 \\ & 4.4550 \end{aligned}$ | . 0059 | 4.4215 4.4233 | $\begin{aligned} & \text { 2B } \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 4.432 \\ & 4.4320 \end{aligned}$ | $\begin{aligned} & 4.446 \\ & 4.4408 \end{aligned}$ | $\begin{aligned} & 4.4594 \\ & 4.4594 \end{aligned}$ | $\begin{aligned} & 4.4670 \\ & 4.4651 \end{aligned}$ | . 00076 | $\begin{aligned} & 4.5000 \\ & 4.5000 \end{aligned}$ |
| 4.625-6 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | .0031 .0000 | $\begin{aligned} & 4.6219 \\ & 4.6250 \end{aligned}$ | $\begin{aligned} & 4.6037 \\ & 4.6068 \end{aligned}$ |  | $\begin{aligned} & 4.5136 \\ & 4.5167 \end{aligned}$ | $\begin{aligned} & 4.5033 \\ & 4.5090 \end{aligned}$ | $\begin{array}{r} .0103 \\ .0077 \end{array}$ | 4.4174 4.4205 | ${ }^{2 B}$ 3B | $\begin{aligned} & 4.445 \\ & 4.4450 \end{aligned}$ | $\begin{aligned} & 4.475 \\ & 4.4646 \end{aligned}$ | 4.5167 4.5167 | $\begin{aligned} & 4.5300 \\ & 4.5267 \end{aligned}$ | .0133 .0100 | $\begin{aligned} & 4.6250 \\ & 4.6250 \end{aligned}$ |
| 4.625-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{gathered} .0020 \\ .0000 \end{gathered}$ | $\begin{aligned} & 4.6230 \\ & 4.6250 \end{aligned}$ | $\begin{aligned} & 4.6116 \\ & 4.6136 \end{aligned}$ |  | $\begin{aligned} & 4.5689 \\ & 4.5709 \end{aligned}$ | $\begin{aligned} & 4.5622 \\ & 4.5659 \end{aligned}$ | $\begin{gathered} .0067 \\ .0050 \end{gathered}$ | $\begin{aligned} & 4.5208 \\ & 4.5228 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 4.535 \\ & 4.5350 \end{aligned}$ | $\begin{aligned} & 4.553 \\ & 4.5448 \end{aligned}$ | $\begin{aligned} & 4.5709 \\ & 4.5709 \end{aligned}$ | $\begin{aligned} & 4.5796 \\ & 4.5775 \end{aligned}$ | $\begin{aligned} & .0087 \\ & .0066 \end{aligned}$ | $\begin{aligned} & 4.6250 \\ & 4.6250 \end{aligned}$ |
| 4.625-16 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | . 00018 | $\begin{aligned} & 4.6232 \\ & 4.6250 \end{aligned}$ | $\begin{aligned} & 4.6138 \\ & 4.6156 \end{aligned}$ |  | $\begin{aligned} & 4.5826 \\ & 4.5844 \end{aligned}$ | $\begin{aligned} & 4.5765 \\ & 4.5799 \end{aligned}$ | . 0061 | 4.5465 4.5483 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 4.557 \\ & 4.5570 \end{aligned}$ | $\begin{aligned} & 4.571 \\ & 4.5658 \end{aligned}$ | $\begin{aligned} & 4.5844 \\ & 4.5844 \end{aligned}$ | $\begin{aligned} & 4.5923 \\ & 4.5903 \end{aligned}$ | $\begin{aligned} & .0079 \\ & .0059 \end{aligned}$ | $\begin{aligned} & 4.6250 \\ & 4.6250 \end{aligned}$ |
| 4.750-4 | UN | $\underset{3 \mathrm{~A}}{2 \mathrm{~A}}$ | $\begin{array}{r} .0035 \\ .0000 \end{array}$ | $\begin{aligned} & 4.7465 \\ & 4.7500 \end{aligned}$ | $\begin{aligned} & 4.7227 \\ & 4.7262 \end{aligned}$ |  | $\begin{aligned} & 4.5841 \\ & 4.5876 \end{aligned}$ | $\begin{aligned} & 4.5724 \\ & 4.5788 \end{aligned}$ | $\begin{array}{r} .0117 \\ .0088 \end{array}$ | $\begin{aligned} & 4.4398 \\ & 4.4433 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 4.479 \\ & 4.4790 \end{aligned}$ | $\begin{aligned} & 4.517 \\ & 4.5094 \end{aligned}$ | $\begin{aligned} & 4.5876 \\ & 4.5876 \end{aligned}$ | $\begin{aligned} & 4.6029 \\ & 4.5990 \end{aligned}$ | . 0153 | $\begin{aligned} & 4.7500 \\ & 4.7500 \end{aligned}$ |
| 4.750-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0031 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 4.7469 \\ & 4.7500 \end{aligned}$ | $\begin{aligned} & 4.7287 \\ & 4.7318 \end{aligned}$ |  | $\begin{aligned} & 4.6386 \\ & 4.6417 \end{aligned}$ | $\begin{aligned} & 4.6283 \\ & 4.6340 \end{aligned}$ | $\begin{array}{r} .0103 \\ .0077 \end{array}$ | $\begin{aligned} & 4.5424 \\ & 4.5455 \end{aligned}$ | $\begin{aligned} & \text { 2B } \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 4.570 \\ & 4.5700 \end{aligned}$ | $\begin{aligned} & 4.600 \\ & 4.5896 \end{aligned}$ | $\begin{aligned} & 4.6417 \\ & 4.6417 \end{aligned}$ | $\begin{aligned} & 4.6551 \\ & 4.6518 \end{aligned}$ | .0134 .0101 | $\begin{aligned} & 4.7500 \\ & 4.7500 \end{aligned}$ |
| 4.750-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0020 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 4.7480 \\ & 4.7500 \end{aligned}$ | $\begin{array}{r} 4.7366 \\ 4.7386 \end{array}$ |  | $\begin{aligned} & 4.6939 \\ & 4.6959 \end{aligned}$ | $\begin{aligned} & 4.6872 \\ & 4.6909 \end{aligned}$ | $\begin{aligned} & .0067 \\ & .0050 \end{aligned}$ | $\begin{aligned} & 4.6458 \\ & 4.6478 \end{aligned}$ | $\begin{aligned} & \text { 2B } \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 4.660 \\ & 4.6600 \end{aligned}$ | $\begin{aligned} & 4.678 \\ & 4.6698 \end{aligned}$ | $\begin{aligned} & 4.6959 \\ & 4.6959 \end{aligned}$ | $\begin{aligned} & 4.7046 \\ & 4.7025 \end{aligned}$ | $\begin{aligned} & .0087 \\ & .0066 \end{aligned}$ | $\begin{aligned} & 4.7500 \\ & 4.7500 \end{aligned}$ |
| 4.750-16 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{aligned} & .0018 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 4.7482 \\ & 4.7500 \end{aligned}$ | $\begin{aligned} & 4.7388 \\ & 4.7406 \end{aligned}$ |  | $\begin{aligned} & 4.7076 \\ & 4.7094 \end{aligned}$ | $\begin{aligned} & 4.7015 \\ & 4.7049 \end{aligned}$ | $\begin{aligned} & .0061 \\ & .0045 \end{aligned}$ | $\begin{aligned} & 4.6715 \\ & 4.6733 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 4.682 \\ & 4.6820 \end{aligned}$ | $\begin{aligned} & 4.696 \\ & 4.6908 \end{aligned}$ | $\begin{aligned} & 4.7094 \\ & 4.7094 \end{aligned}$ | $\begin{aligned} & 4.7173 \\ & 4.7153 \end{aligned}$ | $\begin{aligned} & .0079 \\ & .0059 \end{aligned}$ | $\begin{aligned} & 4.7500 \\ & 4.7500 \end{aligned}$ |
| 4.875-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0031 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 4.8719 \\ & 4.8750 \end{aligned}$ | $\begin{aligned} & 4.8537 \\ & 4.8568 \end{aligned}$ |  | $\begin{aligned} & 4.7636 \\ & 4.7667 \end{aligned}$ | $\begin{aligned} & 4.7532 \\ & 4.7589 \end{aligned}$ | $\begin{aligned} & .0104 \\ & .0078 \end{aligned}$ | $\begin{aligned} & 4.6674 \\ & 4.6705 \end{aligned}$ | $\begin{aligned} & \text { 2B } \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 4.695 \\ & 4.6950 \end{aligned}$ | $\begin{aligned} & 4.725 \\ & 4.7146 \end{aligned}$ | $\begin{aligned} & 4.7667 \\ & 4.7667 \end{aligned}$ | $\begin{aligned} & 4.7802 \\ & 4.7768 \end{aligned}$ | $\begin{aligned} & .0135 \\ & .0101 \end{aligned}$ | $\begin{aligned} & 4.8750 \\ & 4.8750 \end{aligned}$ |
| 4.875-12 | UN | ${ }_{3 A}^{2 A}$ | $\begin{aligned} & .0020 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 4.8730 \\ & 4.8750 \end{aligned}$ | $\begin{aligned} & 4.8616 \\ & 4.8636 \end{aligned}$ |  | $\begin{aligned} & 4.8189 \\ & 4.8209 \end{aligned}$ | $\begin{aligned} & 4.8122 \\ & 4.8159 \end{aligned}$ | $\begin{array}{r} .0067 \\ .0050 \end{array}$ | $\begin{aligned} & 4.7708 \\ & 4.7728 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 4.785 \\ & 4.7850 \end{aligned}$ | $\begin{aligned} & 4.803 \\ & 4.7948 \end{aligned}$ | $\begin{aligned} & 4.8209 \\ & 4.8209 \end{aligned}$ | $\begin{aligned} & 4.8296 \\ & 4.8275 \end{aligned}$ | $\begin{aligned} & .0087 \\ & .0066 \end{aligned}$ | $\begin{aligned} & 4.8750 \\ & 4.8750 \end{aligned}$ |

See footnotes at end of table.

Table 2.21. Standard series limits of size-Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | External ${ }^{\text {a }}$ |  |  |  |  |  |  |  |  | Internal ${ }^{\text {a }}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Allowance | Major diameter limits |  |  | Pitch diameter limits |  |  | Minor diameter ${ }^{\text {d }}$ | Class | Minor diameter limits |  | Pitch diameter limits |  |  | Major <br> diam- <br> eter <br> Min |
|  |  |  |  | Max ${ }^{\text {b }}$ | Min | Min ${ }^{\circ}$ | Max ${ }^{\text {b }}$ | Min | Tolerance |  |  | Min | Max | Min | Max | Tolerance |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 |
| 4.875-16 | UN | ${ }_{3}^{2 A}$ | in 0.0018 .0000 | in 4.8732 4.8750 | in 4.8638 4.8656 | in | in 4.8366 4.8344 | in 4.8265 4.8299 | in 0.0061 .0045 | in 4.7965 4.7983 | 2 BB | $\begin{aligned} & i n \\ & 4.807 \\ & 4.8070 \end{aligned}$ | $\begin{gathered} \text { in } \\ 4.821 \\ 4.8158 \end{gathered}$ | $\begin{aligned} & i n \\ & 4.8344 \\ & 4.8344 \end{aligned}$ | $\begin{gathered} \text { in } \\ 4.8423 \\ 4.8403 \end{gathered}$ | $\begin{gathered} \text { in } \\ 0.0079 \\ .0059 \end{gathered}$ | $\begin{aligned} & \text { in } \\ & 4.8750 \\ & 4.8750 \end{aligned}$ |
| 5.000-4 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0036 .0000 | 4.9964 5.0000 | $\begin{aligned} & 4.9726 \\ & 4.9762 \end{aligned}$ |  | 4.8340 4.8376 | 4.8221 4.8287 | . 0119 | 4.6897 4.6933 | 2 B 3 B | $\begin{aligned} & 4.729 \\ & 4.7290 \end{aligned}$ | $\begin{aligned} & 4.767 \\ & 4.7594 \end{aligned}$ | $\begin{aligned} & 4.8376 \\ & 4.8376 \end{aligned}$ | $\begin{aligned} & 4.8530 \\ & 4.8492 \end{aligned}$ | .0154 .0116 | $\begin{aligned} & 5.0000 \\ & 5.0000 \end{aligned}$ |
| 5.000-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0031 .0000 | 4.9969 5.0000 | $\begin{aligned} & 4.9787 \\ & 4.9818 \end{aligned}$ |  | 4.8886 4.8917 | 4.8781 4.8839 | . 0105 | 4.7924 4.7955 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 4.820 \\ & 4.8200 \end{aligned}$ | $\begin{aligned} & 4.850 \\ & 4.8396 \end{aligned}$ | $\begin{aligned} & 4.8917 \\ & 4.8917 \end{aligned}$ | $\begin{aligned} & 4.9053 \\ & 4.9019 \end{aligned}$ | $\begin{aligned} & .0136 \\ & .0102 \end{aligned}$ | 5.0000 <br> 5.0000 |
| 5.000-12 | UN | 2 A | .0020 .0000 | 4.9980 5.0000 | $\begin{aligned} & 4.9866 \\ & 4.9886 \end{aligned}$ |  | 4.9439 4.9459 | 4.9372 4.9409 | .0067 .0050 | 4.8958 4.8978 | $2 \mathrm{2B}$ | 4.910 4.9100 | 4.928 4.9198 | 4.9459 4.9459 | 4.9546 4.9525 | .0087 .0066 | 5.0000 <br> 5.0000 |
| 5.000-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 00018 | 4.9982 5.0000 | $\begin{aligned} & 4.9888 \\ & 4.9906 \end{aligned}$ |  | 4.9576 4.9594 | 4.9515 4.9549 | . 0061 | 4.9215 4.9233 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 4.932 \\ & 4.9320 \end{aligned}$ | $\begin{aligned} & 4.946 \\ & 4.9408 \end{aligned}$ | $\begin{aligned} & 4.9594 \\ & 4.9594 \end{aligned}$ | 4.9673 4.9653 | $\begin{array}{r} .0079 \\ .0059 \end{array}$ | 5.0000 <br> 5.0000 |
| 5.125-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 0020 | 5.1230 5.1250 | 5.1116 5.1136 |  | 5.0689 5.0709 | 5.0622 5.0659 | .0067 .0050 | 5.0208 5.0228 | ${ }_{3}^{2} \mathrm{~B}$ | 5.035 5.0350 | 5.053 5.0448 | 5.0709 5.0709 | 5.0796 5.0775 | . 0087 | 5.1250 5.1250 |
| 5.125-16 | UN | 2 A | . 00018 | 5.1232 5.1250 | $\begin{aligned} & 5.1138 \\ & 5.1156 \end{aligned}$ |  | 5.0826 5.0844 | 5.0765 5.0799 | . 00661 | 5.0465 5.0483 | ${ }_{3}^{2 B}$ | $\begin{aligned} & 5.057 \\ & 5.0570 \end{aligned}$ | 5.071 5.0658 | 5.0844 4.0844 | $\begin{aligned} & 5.0923 \\ & 5.0903 \end{aligned}$ | $\begin{aligned} & .0079 \\ & .0059 \end{aligned}$ | $\begin{array}{r} 5.1250 \\ 5.1250 \end{array}$ |
| 5.250-4 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 0036 | 5.2464 5.2500 | $\begin{aligned} & 5.2226 \\ & 5.2262 \end{aligned}$ |  | 5.0840 5.0876 | 5.0720 5.0786 | .0120 .0090 | 4.9397 4.9433 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | 4.979 4.9790 | $\begin{aligned} & 5.017 \\ & 5.0094 \end{aligned}$ | $\begin{aligned} & 5.0876 \\ & 5.0876 \end{aligned}$ | 5.1032 5.0993 | . 0156 | $\begin{aligned} & 5.2500 \\ & 5.2500 \end{aligned}$ |
| 5.250-12 | UN | 2 A 3 A | . 0020 | 5.2480 5.2500 | 5.2366 5.2386 |  | 5.1939 5.1959 | 5.1872 5.1909 | .0067 | 5.1458 5.1478 | 2B | 5.160 $\mathbf{5 . 1 6 0 0}$ | 5.178 5.1698 | 5.1959 5.1959 | 5.2046 5.2025 | .0087 .0066 | 5.2500 5.2500 |
| 5.250-16 | UN | ${ }_{3}^{2 A}$ | . 0018 | 5.2482 5.2500 | $\begin{aligned} & 5.2388 \\ & 5.2406 \end{aligned}$ |  | 5.2076 5.2094 | 5.2015 5.2049 | . 0061 | 5.1715 5.1733 | ${ }_{3}^{2 B}$ | $\begin{aligned} & 5.182 \\ & 5.1820 \end{aligned}$ | $\begin{aligned} & 5.196 \\ & 5.1908 \end{aligned}$ | $\begin{aligned} & 5.2094 \\ & 5.2094 \end{aligned}$ | 5.2173 5.2153 | .0079 .0059 | $\begin{aligned} & 5.2500 \\ & 5.2500 \end{aligned}$ |
| 5.375-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0020 | 5.3730 5.3750 | 5.3616 5.3636 |  | 5.3189 5.3209 | 5.3122 5.3159 | . 0067 | 5.2708 5.2728 | ${ }_{3}^{2} \mathrm{~B}$ | 5.285 5.2850 | 5.303 5.2948 | 5.3209 5.3209 | 5.3296 5.3275 | . 0087 | 5.3750 5.3750 |
| 5.375-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 00018 | 5.3732 5.3750 | $\begin{aligned} & 5.3638 \\ & 5.3656 \end{aligned}$ |  | 5.3326 5.3344 | 5.3265 5.3299 | .0061 | 5.2965 5.2983 | 2B | $\begin{aligned} & 5.307 \\ & 5.3070 \end{aligned}$ | $\begin{aligned} & 5.321 \\ & 5.3158 \end{aligned}$ | 5.3344 5.3344 | 5.3423 5.3403 | .0079 | 5.3750 5.3750 |
| 5.500-4 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 0036 | 5.4964 5.5000 | $\begin{aligned} & 5.4726 \\ & 5.4762 \end{aligned}$ |  | 5.3340 5.3376 | 5.3219 5.3285 | . 0121 | 5.1897 5.1933 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 5.229 \\ & 5.2290 \end{aligned}$ | $\begin{aligned} & 5.267 \\ & 5.2594 \end{aligned}$ | 5.3376 5.3376 | 5.3534 5.3494 | .0158 .0118 | $\begin{aligned} & 5.5000 \\ & 5.5000 \end{aligned}$ |
| 5.500-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0020 | 5.4980 5.5000 | 5.4866 5.4886 |  | 5.4439 5.4459 | 5.4372 5.4409 | . 0067 | 5.3958 5.3978 | 2B | 5.410 5.4100 | 5.428 5.4198 | 5.4459 5.4459 | 5.4546 5.4525 | .0087 .0066 | $\begin{aligned} & 5.5000 \\ & 5.5000 \end{aligned}$ |
| 5.500-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0018 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 5.4982 \\ & 5.5000 \end{aligned}$ | $\begin{aligned} & 5.4888 \\ & 5.4906 \end{aligned}$ |  | $\begin{aligned} & 5.4576 \\ & 5.4594 \end{aligned}$ | 5.4515 5.4549 | .0061 | $\begin{aligned} & 5.4215 \\ & 5.4233 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 5.432 \\ & 5.4320 \end{aligned}$ | $\begin{aligned} & 5.446 \\ & 5.4408 \end{aligned}$ | $\begin{aligned} & 5.4594 \\ & 5.4594 \end{aligned}$ | $\begin{aligned} & 5.4673 \\ & 5.4653 \end{aligned}$ | .0079 | 5.5000 <br> 5.5000 |
| 5.625-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 0021 | $\begin{aligned} & 5.6229 \\ & 5.6250 \end{aligned}$ | $\begin{aligned} & 5.6115 \\ & 5.6136 \end{aligned}$ |  | 5.5688 5.5709 | 5.5619 5.5657 | .0069 | 5.5207 5.5228 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 5.535 \\ & 5.5350 \end{aligned}$ | 5.553 5.5448 | 5.5709 5.5709 | 5.5799 5.5776 | .0090 .0067 | $\begin{array}{r} 5.6250 \\ 5.6250 \end{array}$ |
| 5.625-16 | UN | 2 A | .0019 | $\begin{aligned} & 5.6231 \\ & 5.6250 \end{aligned}$ | $\begin{aligned} & 5.6137 \\ & 5.6156 \end{aligned}$ |  | 5.5825 5.5844 | 5.5763 5.5797 | . 0062 | $\begin{aligned} & 5.5464 \\ & \mathbf{5 . 5 4 8 3} \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 2 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 5.557 \\ & 5.5570 \end{aligned}$ | $\begin{aligned} & 5.571 \\ & 5.5658 \end{aligned}$ | $\begin{aligned} & 5.5844 \\ & 5.5844 \end{aligned}$ | $\begin{aligned} & 5.5925 \\ & 5.5905 \end{aligned}$ | .0081 .0061 | $\begin{aligned} & 5.6250 \\ & 5.6250 \end{aligned}$ |
| 5.750-4 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0037 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 5.7463 \\ & 5.7500 \end{aligned}$ | $\begin{aligned} & 5.7225 \\ & 5.7262 \end{aligned}$ |  | $\begin{aligned} & 5.5839 \\ & 5.5876 \end{aligned}$ | $\begin{aligned} & 5.5717 \\ & 5.5784 \end{aligned}$ | . 0122 | $\begin{aligned} & 5.4396 \\ & 5.4433 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 5.479 \\ & 5.4790 \end{aligned}$ | $\begin{aligned} & 5.517 \\ & 5.5094 \end{aligned}$ | $\begin{aligned} & \mathbf{5 . 5 8 7 6} \\ & \mathbf{5 . 5 8 7 6} \end{aligned}$ | $\begin{aligned} & 5.6035 \\ & 5.5995 \end{aligned}$ | .0159 .0119 | $\begin{aligned} & 5.7500 \\ & 5.7500 \end{aligned}$ |
| 5.750-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 0021 | $\begin{aligned} & 5.7479 \\ & 5.7500 \end{aligned}$ | $\begin{aligned} & 5.7365 \\ & 5.7386 \end{aligned}$ |  | 5.6938 5.6959 | 5.6869 5.6907 | . 0069 | 5.6457 5.6478 | ${ }_{3}^{2 B}$ | $\begin{aligned} & 5.660 \\ & 5.6600 \end{aligned}$ | $\begin{aligned} & 5.678 \\ & 5.6698 \end{aligned}$ | 5.6959 5.6959 | 5.7049 5.7026 | .0090 | $\begin{aligned} & 5.7500 \\ & 5.7500 \end{aligned}$ |
| 5.750-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0019 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 5.7481 \\ & 5.7500 \end{aligned}$ | $\begin{aligned} & 5.7387 \\ & 5.7406 \end{aligned}$ |  | $\begin{aligned} & 5.7075 \\ & 5.7094 \end{aligned}$ | $\begin{aligned} & 5.7013 \\ & 5.7047 \end{aligned}$ | $\begin{aligned} & .0062 \\ & .0047 \end{aligned}$ | $\begin{aligned} & 5.6714 \\ & 5.6733 \end{aligned}$ | $\begin{aligned} & \text { 2B } \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 5.682 \\ & 5.6820 \end{aligned}$ | $\begin{aligned} & 5.696 \\ & 5.6908 \end{aligned}$ | $\begin{aligned} & 5.7094 \\ & 5.7094 \end{aligned}$ | $\begin{aligned} & 5.7175 \\ & 5.7155 \end{aligned}$ | . 00081 | $\begin{array}{r} 5.7500 \\ 5.7500 \end{array}$ |
| 5.875-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0021 | 5.8729 5.8750 | 5.8615 5.8636 |  | 5.8188 5.8209 | 5.8119 5.8157 | . 0069 | 5.7707 5.7728 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 5.785 \\ & 5.7850 \end{aligned}$ | $\begin{aligned} & 5.803 \\ & 5.7948 \end{aligned}$ | $\begin{aligned} & 5.8209 \\ & 5.8200 \end{aligned}$ | 5.8299 5.8276 | .0090 .0067 | $\begin{array}{r} 5.8750 \\ 5.8750 \end{array}$ |
| 5.875-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .0019 .0000 | $\begin{aligned} & 5.8731 \\ & 5.8750 \end{aligned}$ | $\begin{aligned} & 5.8637 \\ & 5.8656 \end{aligned}$ |  | 5.8325 5.8344 | $\begin{aligned} & 5.8263 \\ & 5.8297 \end{aligned}$ | $\begin{aligned} & .0062 \\ & .0047 \end{aligned}$ | $\begin{aligned} & 5.7964 \\ & 5.7983 \end{aligned}$ | $\begin{aligned} & \text { 2B } \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 5.807 \\ & 5.8070 \end{aligned}$ | $\begin{aligned} & 5.821 \\ & 5.8158 \end{aligned}$ | $\begin{aligned} & 5.8344 \\ & 5.8344 \end{aligned}$ | 5.8425 5.8405 | .0081 .0061 | $\begin{aligned} & 5.8750 \\ & 5.8750 \end{aligned}$ |
| 6.000-4 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0037 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 5.9963 \\ & 6.0000 \end{aligned}$ | $\begin{aligned} & 5.9725 \\ & 5.9762 \end{aligned}$ |  | 5.8338 5.8376 | 5.8215 5.8283 | . 0124 | 5.6896 5.6933 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 5.729 \\ & 5.7290 \end{aligned}$ | $\begin{aligned} & 5.767 \\ & 5.7594 \end{aligned}$ | $\begin{aligned} & 5.8376 \\ & 5.8376 \end{aligned}$ | $\begin{aligned} & 5.8537 \\ & 5.8496 \end{aligned}$ | . 0161 | $\begin{aligned} & 6.0000 \\ & 6.0000 \end{aligned}$ |
| 6.000-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0021 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 5.9979 \\ & 6.0000 \end{aligned}$ | $\begin{aligned} & 5.9865 \\ & 5.9886 \end{aligned}$ |  | 5.9438 5.9459 | $\begin{aligned} & 5.9369 \\ & 5.9407 \end{aligned}$ | $\begin{aligned} & .0069 \\ & .0052 \end{aligned}$ | $\begin{aligned} & 5.8957 \\ & 5.8978 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 5.910 \\ & 5.9100 \end{aligned}$ | $\begin{aligned} & 5.928 \\ & 5.9198 \end{aligned}$ | $\begin{aligned} & 5.9459 \\ & 5.9459 \end{aligned}$ | $\begin{aligned} & 5.9549 \\ & 5.9526 \end{aligned}$ | . 00090 | $\begin{aligned} & 6.0000 \\ & 6.0000 \end{aligned}$ |
| 6.000-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0019 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 5.9981 \\ & 6.0000 \end{aligned}$ | $\begin{aligned} & 5.9887 \\ & 5.9906 \end{aligned}$ | ----- | $\begin{aligned} & 5.9575 \\ & 5.9594 \end{aligned}$ | $\begin{aligned} & 5.9513 \\ & 5.9547 \end{aligned}$ | . 00662 | $\begin{aligned} & 5.9214 \\ & 5.9233 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 5.932 \\ & 5.9320 \end{aligned}$ | $\begin{aligned} & 5.946 \\ & 5.9408 \end{aligned}$ | $\begin{aligned} & 5.9594 \\ & 5.9594 \end{aligned}$ | $\begin{aligned} & 5.9675 \\ & 5.9655 \end{aligned}$ | $\begin{aligned} & .0081 \\ & .0061 \end{aligned}$ | $\begin{aligned} & 6.0000 \\ & 6.0000 \end{aligned}$ |

${ }^{\text {a }}$ Regarding combinations of thread classes, see par. 4, Thread classes, p. 2.17.
b For class 2 A threads having an additive fnish the maximum is increased to the basic size, the value being the same as for class 3 A shown in this column. See par.
4.2, p. 2.17, and par. 9. p. 2.22 .

- For unfinished hot-rolled material.
${ }^{\mathrm{d}}$ See figs. 2.3, 2.5, and 2.6.
Note: See par. 11 Limits of Size, p. 2.25.

Table 2.22. Deviations in lead and half-angle equivalent to one-half of pitch diameter tolerances, Unified screw threads

| Nominal size and threads per inch | Series designation | External |  |  |  |  | Internal |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  |
| 1 | 2 | 3 | 4 | 5 |  |  | 7 | 8 | 9 |  |  |
| .060-80 | UNF | 2 A | $\begin{gathered} i n \\ 0.00090 \\ .00065 \end{gathered}$ | $\begin{gathered} i n \\ 0.00052 \\ .00038 \end{gathered}$ | deg 3 2 | min 18 23 | 2B | $\begin{gathered} \text { in } \\ 0.00115 \\ .00085 \end{gathered}$ | $\begin{gathered} i n \\ 0.00066 \\ .00049 \end{gathered}$ | deg 4 3 | $\min$ 13 7 |
| .073-64 | UNC | 2 A | .00100 .00075 | $\begin{aligned} & .00058 \\ & .00043 \end{aligned}$ | 2 2 | 56 12 | 2B | .00130 .00095 | . 00075 | $\begin{aligned} & 3 \\ & 2 \end{aligned}$ | 48 |
| .073-72 | UNF | 2 A | .00095 .00070 | .00055 .00040 | 3 2 | 8 19 | $2 \mathrm{3B}$ | .00125 .00095 | .00072 .00055 | 4 | 7 8 |
| .086-56 | UNC | 2A | .00105 .00080 | .00061 .00046 | 2 2 | 42 | 2B | .00140 .00105 | . 000081 | 3 2 | 35 42 |
| .086-64 | UNF | 2 A | .00100 .00075 | . 00058 | 2 2 | 56 12 | 2 B | .00135 .00100 | .00078 .00058 | $\begin{aligned} & 3 \\ & 2 \end{aligned}$ | 57 56 |
| .099-48 | UNC | 2A | . 00115 | .00066 .00049 | 1 | 32 52 | 2B | .00150 .00110 | . 000087 | 3 2 | 18 25 |
| .099-56 | UNF | 2A | . 000110 | .00064 .00046 | 2 | 49 3 | 2B | .00140 .00105 | . 000081 | 3 | 35 |
| .112-40 | UNC | 2A | .00125 .00095 | .00072 .00055 | 2 | 17 44 | $2 \mathrm{3B}$ | .00165 .00120 | .00095 .00069 | $\begin{aligned} & 3 \\ & 2 \end{aligned}$ | 12 |
| .112-48 | UNF | 2A | .00120 .00090 | .00069 .00052 | 2 | 38 59 | 2 BB | . 00155 | .00089 .00066 | 3 2 | 24 32 |
| . 125-40 | UNC | 2 A | .00130 .00095 | . 000075 | 2 1 | 23 44 | 2B | .00165 .00125 | . 000095 | $\begin{aligned} & 3 \\ & 2 \end{aligned}$ | 17 |
| .125-44 | UNF | 2 A | . 000125 | .00072 .00055 | 1 | 31 55 | 2 B 3 B | .00160 .00120 | . 000092 | $\begin{aligned} & 3 \\ & 2 \end{aligned}$ | 13 25 |
| . 138-32 | UNC | 2A | .00140 .00105 | . 000081 | 2 1 | 3 32 | 2B | .00185 .00135 | .00107 .00078 | 2 | 43 59 |
| . 138-40 | UNF | 2A | .00130 .00100 | .00075 .00058 | 2 | 23 50 | $2 \mathrm{3B}$ | .00170 .00125 | . 000098 | $\begin{aligned} & 3 \\ & 2 \end{aligned}$ | $\begin{array}{r}7 \\ \hline\end{array}$ |
| . $164-32$ | UNC | 2 A | .00145 .00110 | . 000084 | 2 | 8 37 | 2 B 3 B | .00190 .00140 | .00110 .00081 | 2 | 47 3 |
| . 164 -36 | UNF | 2A | .00140 .00105 | . 000081 | $\stackrel{2}{1}$ | 19 44 | 2B ${ }_{3}$ | .00180 .00135 | .00104 .00078 | 2 | 58 14 |
| .190-24 | UNC | 2 A | .00165 .00125 | .00095 .00072 | 1 | 49 22 | 2 B 3 B | . 00215 | . 000124 | 2 1 | 22 46 |
| . 190-32 | UNF | 2 A | .00150 .00115 | . 000087 | 2 | 12 | 2 B | .00195 .00145 | .00113 .00084 | 2 2 | 51 8 |
| .216-24 | UNC | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00170 .00130 | . 000098 | 1 | 52 26 | ${ }_{3}^{2 B}$ | .00220 .00165 | .00127 .00095 | 2 1 | 25 49 |
| .216-28 | UNF | 2 A | .00160 .00120 | .00092 .00069 | 2 1 | 3 32 | 2B | . 00210 | . 000121 | 2 1 | 42 59 |
| .216-32 | UNEF | 2A | .00155 .00120 | $\begin{aligned} & .00089 \\ & .00069 \end{aligned}$ | 2 1 | 16 46 | 2B | .00205 .00155 | . 00118 | 3 2 | 0 |
| . $250-20$ | UNC | 1 A 2 A 3 A | .00280 .00185 .00140 | .00162 .00107 .00081 | 2 1 1 | 34 42 17 | 1B 2B 3 B | .00365 .00245 .00180 | .00211 .00141 .00104 | 3 2 1 | 21 15 39 |
| . 250-28 | UNF | 1 A 2 A 3 A | .00250 .00165 .00125 | .00144 .00095 .00072 | 3 2 1 | 12 7 36 | 1 B 2 B 3 B | .00325 .00215 .00160 | .00188 .00124 .00092 | 4 2 2 | 10 45 3 |
| .250-32 | UNEF | 2A | .00160 .00120 | .00092 .00069 | 2 | 21 46 | 2B ${ }_{3}$ | .00210 .00155 | . 000121 | 3 2 | 5 16 |
| .3125-18 | UNC | 1 A 2 A 3 A | .00305 .00200 .00150 | .00176 .00115 .00087 | 2 1 1 | 31 39 14 | 1 B 2 B 3 B | .00395 .00265 .00195 | .00228 .00153 .00113 | 3 2 1 | 15 11 37 |
| . $3125-20$ | UN | 2 A | $\begin{aligned} & .00200 \\ & .00150 \end{aligned}$ | $\begin{aligned} & .00115 \\ & .00087 \end{aligned}$ | 1 | 50 22 | 2B | .00260 .00195 | . 000150 | $\stackrel{2}{1}$ | 23 47 |
| .3125-24 | UNF | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00275 \\ & .00185 \\ & .00135 \end{aligned}$ | .00159 .00107 .00078 | 3 2 1 | 1 2 29 | 1 B 2 B 3 B | .00355 .00240 .00180 | .00205 .00139 .00104 | 3 2 1 | 54 38 59 |
| .3125-28 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} .00170 \\ .00130 \end{array}$ | $\begin{aligned} & .00098 \\ & .00075 \end{aligned}$ | $\stackrel{2}{1}$ | 11 40 | ${ }_{3}^{2 B}$ | .00220 .00165 | . 000127 | 2 2 | 49 7 |

Table 2.22. Deviations in lead and half-angle equivalent to one-half of pitch diamter tolerances, Unified screw threads-Continued

| Nominal size and threads per inch | Series desighation | External |  |  |  |  | Internal |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Half of pitch tolerance | Equivalent deviation in lead | Equivalent deviation in half-sngle |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  |
| 1 | 2 | 3 | 4 | 5 |  |  | 7 | 8 | 9 | 10 |  |
| .3125-32 | UNEF | ${ }_{3}^{2 A}$ | $\begin{gathered} \text { in } \\ .00160 \\ .00120 \end{gathered}$ | $\begin{gathered} i n \\ .00092 \\ .00069 \end{gathered}$ | deg 2 1 | $\begin{aligned} & \min \\ & 21 \\ & 46 \end{aligned}$ | ${ }_{3 B}^{2 B}$ | in .00210 .00155 | in .00021 .00089 | deg 3 2 | min 5 5 16 |
| .375-16 | UNC | 1 A 2 A 3 A | $\begin{aligned} & .00325 \\ & .0020 \\ & .00165 \end{aligned}$ | .00188 .00127 .00095 | $\begin{aligned} & 2 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 23 \\ & 37 \\ & 13 \end{aligned}$ | 18 2 B 3 B | .00425 .00285 .00215 | .00245 .00165 .00124 | 3 2 1 1 | 7 5 35 |
| . $375-20$ | UN | ${ }_{3}^{2 A}$ | . 002205 | . 00118 | 1 | 53 25 | ${ }_{3 \mathrm{~B}}^{2 \mathrm{~B}}$ | .00270 | .00156 | ${ }_{1}^{2}$ | 28 50 |
| . $375-24$ | UNF | 1 A 2 A 3 A | .00285 .000190 .00145 | .00165 .00110 .00084 | 3 2 1 1 | 8 5 36 | 18 2 B 3 B | .00370 .00245 .00185 | .00214 .00141 .0107 | 4 2 2 2 | 4 4 42 2 |
| . $375-28$ | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | . 000180 | . 000078 | ${ }_{1}$ | 19 44 | ${ }_{3 \mathrm{~B}}^{2 \mathrm{~B}}$ | . 000230 | . 000133 | ${ }_{2}^{2}$ | 57 15 |
| .375-32 | UNEF | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | . 000170 | .00098 | 2 | $\begin{aligned} & 30 \\ & 50 \end{aligned}$ | ${ }_{3 B}^{2 B}$ | . 002200 | $\begin{aligned} & .00127 \\ & .00095 \end{aligned}$ | 3 2 | 13 25 |
| .4375-14 | UNC | 1 A 2 A 3 A | .00355 .00235 .00175 | .00205 .00136 .00101 | 2 1 1 | 17 30 7 | 18 <br> 28 <br> 3 B | .00460 .00305 .00230 | .00266 .00176 .00133 | 2 1 1 | 57 57 59 29 |
| .4375-16 | UN | ${ }_{3 \mathrm{~A}}{ }^{\text {A }}$ | . 000230 | . 0001338 | 1 | 41 15 | ${ }_{3 B}^{2 B}$ | . 002295 | $\begin{gathered} .00170 \\ .00130 \end{gathered}$ | $\stackrel{2}{1}$ | 10 39 |
| .4375-20 | UNF | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00315 .00210 .00155 | .00182 .00121 .00089 | 2 1 1 | $\begin{aligned} & 53 \\ & 55 \\ & 25 \end{aligned}$ | 18 28 3 B | .00405 .00270 .00205 | .00234 .00156 .00118 | 3 2 1 | 42 28 53 |
| . $4375-28$ | UNEF | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{aligned} & .00180 \\ & .00135 \end{aligned}$ | $\begin{aligned} & .00104 \\ & .00078 \end{aligned}$ | ${ }_{1}^{2}$ | 19 44 | ${ }_{3 B}^{2 B}$ | . 000230 | $\begin{aligned} & .00133 \\ & .00101 \end{aligned}$ | ${ }_{2}^{2}$ | 57 15 |
| .4375-32 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | . 000170 | $\begin{array}{r} .00098 \\ .00072 \end{array}$ | ${ }^{2}$ | 30 50 | ${ }_{3 B}^{2 B}$ | . 002200 | . 000127 | 3 2 | 13 25 |
| .500-13 | UNC | 1A 2 2 A 3 | .00370 .00250 .00185 | .00214 .00144 .00107 | 2 1 1 | 12 29 6 | 1B 2 B 3 B | .00485 .00325 .00240 | .00280 .00188 .00139 | 2 1 1 | 53 <br> 56 <br> 56 <br> 6 |
| .500-16 | UN | ${ }_{3 \mathrm{~A}}{ }^{\text {A }}$ | . 000235 | .00136 .00101 | 1 | 43 <br> 17 | ${ }_{3 B}^{2 B}$ | . 0030230 | . 000176 | 1 | 14 41 |
| .500-20 | UNF | 1A 2 2 A 3 A | .00320 .00215 .00160 | .00185 .00124 .00092 | 2 1 1 | $\begin{aligned} & 56 \\ & 58 \\ & 28 \end{aligned}$ | 18 2 B 3 B | .00420 .00280 .00210 | .00242 .00162 .00121 | 3 2 1 | 51 34 55 |
| .500-28 | UNEF | ${ }_{3}^{2 A}$ | . 000185 | . 000107 | ${ }_{2}$ | 22 48 | ${ }_{3 \mathrm{~B}}^{2 \mathrm{~B}}$ | . 000240 | . 000139 | 3 2 | 5 19 |
| . $500-32$ | UN | ${ }_{3}^{2 A}$ | . 000175 | . 000075 | ${ }_{1}^{2}$ | $\begin{aligned} & 34 \\ & 54 \end{aligned}$ | ${ }_{3 B}^{2 B}$ | . 000225 | . 000130 | 3 <br> 2 | 18 30 |
| . $5625-12$ | UNC | 1A 2 A 3 A | .00390 .00260 .00195 | .00225 .00150 .00113 | 2 1 1 | 9 26 4 | 18 28 38 | .00510 .00340 .00255 | .00294 .000196 .00147 | 2 1 1 | 48 52 24 |
| . $5625-16$ | UN | ${ }_{3}^{2 A}$ | $\begin{aligned} & .00235 \\ & .00175 \end{aligned}$ | $\begin{aligned} & .00136 \\ & .00101 \end{aligned}$ | 1 | $\begin{aligned} & 43 \\ & 17 \end{aligned}$ | ${ }_{3 B}{ }^{\text {B }}$ | $\begin{aligned} & .00305 \\ & .00230 \end{aligned}$ | $\begin{aligned} & .00176 \\ & .00133 \end{aligned}$ | ${ }_{1}^{2}$ | 14 41 |
| . $5625-18$ | UNF | 1 A 2 A 3 A | .00340 .00225 .00170 | .00196 .00130 .00098 | 2 1 1 | 48 51 24 24 | 1B 2 B 3 B | .00445 .00295 .00220 | .00257 .00170 .00127 | 3 2 1 1 | 40 26 49 |
| . $5625-20$ | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | . 002160 | $\begin{aligned} & .00121 \\ & .00092 \end{aligned}$ | 1 | $\begin{aligned} & 55 \\ & 28 \end{aligned}$ | ${ }_{3 \mathrm{~B}}^{2 \mathrm{~B}}$ | $\begin{aligned} & .00275 \\ & .00205 \end{aligned}$ | $.00159$ | ${ }_{1}^{2}$ | 31 53 |
| . $5625-24$ | UNEF | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | . 000195 | . 000113 | 1 | 9 <br> 36 | ${ }_{3 \mathrm{~B}}^{2 \mathrm{~B}}$ | . 00255 | . 000147 | 2 | 48 5 |
| . $5625-28$ | UN | ${ }_{3 \mathrm{~A}}$ | $\begin{aligned} & .00185 \\ & .00140 \end{aligned}$ | $\begin{aligned} & .00107 \\ & .00081 \end{aligned}$ | 1 | $\begin{aligned} & 22 \\ & 48 \end{aligned}$ | ${ }_{3}^{2 B}$ | $\begin{aligned} & .00240 \\ & .00180 \end{aligned}$ | $\begin{aligned} & .00139 \\ & .00104 \end{aligned}$ | 3 2 | 5 19 |
| . $5625-32$ | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{array}{r} .00175 \\ .00130 \end{array}$ | $\begin{aligned} & .00101 \\ & .00075 \end{aligned}$ | ${ }_{1}^{2}$ | $\begin{aligned} & 34 \\ & 54 \end{aligned}$ | ${ }_{3 \mathrm{~B}}^{2 \mathrm{~B}}$ | $\begin{aligned} & .00225 \\ & .00170 \end{aligned}$ | $\begin{array}{r} .00130 \\ .00098 \end{array}$ | 3 2 | ${ }_{30}^{18}$ |
| .625-11 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & \begin{array}{l} 2 \mathrm{~A} \\ 3 \mathrm{~A} \end{array} \end{aligned}$ | $\begin{aligned} & .00415 \\ & .00275 \\ & .00205 \end{aligned}$ | $\begin{aligned} & .00240 \\ & .00159 \\ & .00118 \end{aligned}$ | 2 1 1 | 5 23 23 | 18 28 38 | $\begin{aligned} & .00535 \\ & .00360 \\ & .00270 \end{aligned}$ | $\begin{aligned} & .00309 \\ & .00208 \\ & .00156 \end{aligned}$ | 2 1 1 | 42 49 29 |
| . $625-12$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00270 \\ & .00205 \end{aligned}$ | $\begin{aligned} & .00156 \\ & .00118 \end{aligned}$ |  | $\begin{array}{r} 29 \\ 8 \end{array}$ | ${ }_{3 \mathrm{~B}}^{2 \mathrm{~B}}$ | $\begin{aligned} & .00355 \\ & .00265 \end{aligned}$ | $\begin{aligned} & .00205 \\ & .00153 \end{aligned}$ | 1 | 57 27 |

Table 2.22. Deviations in lead and half-angle equivalent to one-half of pitch diameter tolerances, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | External |  |  |  |  | Internal |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivaleut deviation in half-angle |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  |
| 1 | 2 | 3 | 4 | 5 |  |  | 7 | 8 | 9 |  |  |
| .625-16 | UN | 2 A 3 A | in .00240 .00180 | in .00139 .00104 | deg 1 1 | min 46 19 | 2B | in .00310 .00230 | in .00179 .00133 | deg 2 1 1 | min 16 41 |
| . $625-18$ | UNF | 1 A 2 A 3 A | .00350 .00235 .00175 | .00202 .00136 .00101 | 2 1 1 | 53 56 27 | 18 2 B 3 B | .00455 .00300 .00225 | .00263 .00173 .00130 | 3 2 1 | 45 28 51 |
| . $625-20$ | UN | 2 A | . 00215 | . 000124 | 1 | 58 28 28 | $2 B$ $3 B$ | .00280 .00210 | . 00162 | ${ }_{1}^{2}$ | 34 55 |
| .625-24 | UNEF | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00200 .00150 | .00115 .00087 | 2 1 | 12 39 | 2B 3 B | .00260 .00195 | . 00150 | $\stackrel{2}{2}$ | 51 9 |
| .625-28 | UN | 2 A | .00190 .00140 | . 000110 | 1 | 26 48 | ${ }_{3}^{2 B}$ | . 00245 | . 000141 | 3 2 | 8 22 |
| . $625-32$ | UN | 2 A | .00180 .00135 | .00104 .00078 | 2 1 | 38 59 | 2 B 3 B | .00230 .00175 | .00133 .00101 | 3 2 | 22 34 |
| . $6875-12$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 000270 | .00156 .00118 | 1 | 29 8 | 2B ${ }^{\text {B }}$ | .00355 .00265 | . 00205 | 1 | 57 27 |
| .6875-16 | UN | 2 A | .00240 .00180 | . 000139 | 1 | 46 19 | 2B 3 B | .00310 .00230 | .00179 .00133 | 2 1 | 16 41 |
| . $6875-20$ | UN | 2A ${ }^{\text {A }}$ | .00215 .00160 | .00124 .00092 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 58 28 | $2 B$ 3 B | .00280 .00210 | . 00162 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | 34 55 |
| .6875-24 | UNEF | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00200 .00150 | . 000115 | 2 1 | 12 39 | 2B ${ }^{\text {B }}$ | .00260 .00195 | . 000150 | 2 2 | 51 9 |
| . $6875-28$ | UN | $2{ }_{3}{ }^{\text {A }}$ | .00190 .00140 | . 000110 | ${ }_{1}^{2}$ | 26 48 | 2B 3 B | . 000245 | . 00141 | 3 2 | 8 22 |
| .6875-32 | UN | 2 A | .00180 .00135 | . 000104 | 2 1 | $\begin{aligned} & 38 \\ & 59 \end{aligned}$ | 2 B 3 B | . 00230 | . 000133 | 3 2 | $\stackrel{22}{34}$ |
| .750-10 | UNC | 1 A 2 A 3 A | .00440 .00295 .00220 | .00254 .00170 .00127 | 2 1 1 | 1 21 0 | 1 B 2 B 3 B | .00575 .00385 .00285 | .00332 .00222 .00165 | 2 1 1 | 38 46 18 |
| .750-12 | UN | 2 A | . 000275 | . 000159 | 1 | 31 8 | 2 B 3 B | .00360 .00270 | .00208 .00156 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 59 29 |
| .750-16 | UNF | 1 A 2 A 3 A | .00375 .00250 .00190 | .00217 .00144 .00110 | 2 1 1 | 45 50 24 | 1B 2B 3 B | .00490 .00325 .00245 | .00283 .00188 .00141 | 3 2 1 | 35 23 48 |
| .750-20 | UNEF | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00220 .00165 | . 000127 | 2 1 | 31 | 2B ${ }_{3}$ | .00285 .00215 | . 000165 | 2 1 | 37 |
| . $750-28$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00190 .00145 | . 000110 | 2 1 | 26 52 | ${ }_{3}^{2 B}$ | .00250 .00185 | .00144 .00107 | 3 2 | 12 |
| .750-32 | UN | 2 A | .00180 .00135 | .00104 .00078 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{aligned} & 38 \\ & 59 \end{aligned}$ | 2B 3 B | . 00235 | .00136 .00104 | 3 2 | 27 38 |
| . $8125-12$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00275 \\ & .00205 \end{aligned}$ | .00159 .00118 | 1 | 31 8 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00360 .00270 | .00208 .00156 | 1 | 59 29 |
| .8125-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 00245 | $.00141$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 48 \\ & 19 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 000315 | . 000182 | 2 1 | 19 43 |
| .8125-20 | UNEF | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 0002205 | . 000127 | 2 1 | 31 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 000285 | . 00165 | 2 1 | 37 58 |
| .8125-28 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00190 .00145 | . 000110 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{aligned} & 26 \\ & 52 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00250 .00185 | .00144 .00107 | 3 2 | 12 22 |
| .8125-32 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00180 \\ & .00135 \end{aligned}$ | $\begin{aligned} & .00104 \\ & .00078 \end{aligned}$ | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{aligned} & 38 \\ & 59 \end{aligned}$ | $\begin{aligned} & \text { 2B } \\ & 3 \mathrm{~B} \end{aligned}$ | .00235 .00180 | . 000136 | 3 2 | 27 38 |
| .875-9 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00475 .00315 .00235 | .00274 .00182 .00136 | $\begin{aligned} & 1 \\ & 1 \\ & 0 \end{aligned}$ | $\begin{aligned} & 58 \\ & 18 \\ & 58 \end{aligned}$ | $\begin{aligned} & 1 \mathrm{~B} \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00615 .00410 .00305 | .00355 .00237 .00176 | 2 1 1 | 32 41 15 |
| . $875-12$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 000275 | $.00159$ | 1 | 31 8 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00360 .00270 | .00208 .00156 | 1 | 59 29 |
| .875-14 | UNF | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00405 \\ & .00270 \\ & .00205 \end{aligned}$ | $\begin{aligned} & .00234 \\ & .00156 \\ & .00118 \end{aligned}$ | 2 1 1 | $\begin{aligned} & 36 \\ & 44 \\ & 19 \end{aligned}$ | $\begin{aligned} & 1 \mathrm{~B} \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00530 .00350 .00265 | .00306 .00202 .00153 | 3 2 1 | 24 15 42 |
| .875-16 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{aligned} & .00245 \\ & .00180 \end{aligned}$ | $\text { . } 00141 .$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 48 \\ & 19 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .00315 \\ & .00235 \end{aligned}$ | $\begin{aligned} & .00182 \\ & .00136 \end{aligned}$ | 2 1 | 19 43 |

Table 2.22. Deviations in lead and half-angle equivalent to one-half of pitch diameter tolerances, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | External |  |  |  |  | Internal |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  |
| 1 | 2 | 3 | 4 | 5 |  |  | 7 | 8 | 9 |  |  |
| .875-20 | UNEF | ${ }_{3}^{2 A}$ | in .00220 .00165 | in .00127 .00095 | deg 2 1 | min 1 31 | 2B | $\begin{gathered} \text { in } \\ .00285 \\ .00215 \end{gathered}$ | $\begin{aligned} & i n \\ & .00165 \\ & .00124 \end{aligned}$ | deg 2 1 | min 37 58 |
| .875-28 | UN | 2 A | .00190 .00145 | . 000110 | 2 1 | 26 52 | 2B ${ }_{3}$ | .00250 .00185 | . 00144 | 3 2 | 12 22 |
| . $875-32$ | UN | 2 A | .00180 .00135 | . 00104 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | 38 59 | 2 B 3 B | .00235 .00180 | .00136 .00104 | 3 2 | 27 38 |
| . $9375-12$ | UN | 2 A | .00285 .00210 | . 00165 | 1 | 34 9 | ${ }_{3}^{2 B}$ | .00370 .00275 | .00214 .00159 | 1 | 31 |
| .9375-16 | UN | 2 AA | .00250 .00185 | . 000144 | 1 | 50 21 | 2 B 3 B | .00325 .00245 | . 00188 | 2 1 | 23 48 |
| . 9375 -20 | UNEF | 2 A | .00225 .00170 | .00130 .00098 | 2 1 | 4 33 | ${ }_{3}^{2} \mathrm{~B}$ | .00295 .00220 | .00170 .00127 | $\stackrel{2}{2}$ | 42 1 |
| .9375-28 | UN | 2 A | .00200 .00150 | .00115 .00087 | $\stackrel{2}{1}$ | 34 55 | $2 \mathrm{3B}$ | .00260 .00195 | .00150 .00113 | 3 2 | 20 30 |
| . $9375-32$ | UN | 2 A 3 A | .00190 .00140 | .00110 .00081 | $\stackrel{2}{2}$ | 47 3 | 2 B 3 B | .00245 .00185 | . 00141 | 3 2 | 35 43 |
| 1.000-8 | UNC | 1 A 2 A 3 A | .00505 .00340 .00255 | .00292 .00196 .00147 | 1 1 0 | 51 15 56 | 18 28 38 | .00660 .00440 .00330 | .00381 .00259 .00191 | 2 1 1 | 25 37 13 |
| 1.000-12 | UNF | 1 A 2 A 3 A | .00440 .00295 .00220 | .00254 .00170 .00127 | 2 1 1 | 25 37 13 | 1 B 2 B 3 B | .00570 .00380 .00285 | .00329 .00219 .00165 | 3 2 1 | 8 5 34 |
| 1.000-16 | UN | 2 A | .00250 .00185 | . 000144 | 1 | 50 21 | 2B ${ }_{3}$ | . 00325 | . 00188 | $\stackrel{2}{1}$ | 23 48 |
| 1.000-20 | UNEF | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00225 .00170 | .00130 .00098 | 2 1 | 4 33 | $2 \mathrm{3B}$ | .00295 .00220 | .00170 .00127 | 2 | 42 1 |
| 1.000-28 | UN | $2 A$ $3 A$ | .00200 .00150 | . 00115 | 2 1 | 34 55 | 2 B 3 B | .00260 .00195 | . 00150 | 3 2 | 20 30 |
| 1.000-32 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00190 .00140 | . 00110 | $\begin{aligned} & 2 \\ & 2 \end{aligned}$ | 47 3 | 2 B 3 B | .00245 .00185 | . 00141 | 3 2 | 35 43 |
| 1.0625-8 | UN | 2 A 3 A | . 00340 | .00196 .00147 | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | 15 56 | ${ }_{3}^{2 B}$ | .00445 .00335 | . 00257 | 1 | 38 14 |
| 1.0625-12 | UN | 2 A | .00285 .00210 | .00165 .00121 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 34 9 | ${ }_{3}^{2} \mathrm{~B}$ | .00370 .00275 | .00214 .00159 | 2 1 | $\stackrel{2}{31}$ |
| 1.0625-16 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | .00250 .00185 | . 000144 | 1 | 50 21 | 2B | .00325 .00245 | . 00188 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | 23 48 |
| 1.0625-18 | UNEF | 2 A | .00235 .00180 | .00136 .00104 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 56 29 | 2B 3 B | .00310 .00230 | .00179 .00133 | 2 | 33 54 |
| 1.0625-20 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00225 .00170 | .00130 .00098 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | 4 33 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00295 .00220 | $\begin{aligned} & .00170 \\ & .00127 \end{aligned}$ | $\begin{aligned} & 2 \\ & 2 \end{aligned}$ | 42 1 |
| 1.0625-28 | UN | 2 A 3 A | .00200 .00150 | . 000115 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | 34 55 | 2 B 3 B | . 002600 | . 00150 | 3 2 | 20 30 |
| 1.125-7 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathbf{A} \end{aligned}$ | .00545 .00360 .00270 | .00315 .00208 .00156 | $\begin{aligned} & 1 \\ & 1 \\ & 0 \end{aligned}$ | $\begin{array}{r} 45 \\ 9 \\ 52 \end{array}$ | 1 B 2 B 3 B | .00705 .00470 .00355 | .00407 .00271 .00205 | 2 1 1 | 16 30 8 |
| 1.125-8 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00345 .00260 | .00199 .00150 | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | $\begin{aligned} & 16 \\ & 57 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 00450 | .00260 .00193 | 1 | 39 14 |
| 1.125-12 | UNF | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00450 .00300 .00225 | .00260 .00173 .00130 | 2 1 1 | 28 39 14 | 1 B 2 B 3 B | .00585 .00390 .00295 | .00338 .00225 .00170 | 3 2 1 | 13 9 37 |
| 1.125-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00250 \\ & .00185 \end{aligned}$ | $\begin{aligned} & .00144 \\ & .00107 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 50 \\ & 21 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 000325 | .00188 .00141 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{aligned} & 23 \\ & 48 \end{aligned}$ |
| 1.125-18 | UNEF | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00235 \\ & .00180 \end{aligned}$ | $\begin{aligned} & .00136 \\ & .00104 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 56 \\ & 29 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .00310 \\ & .00230 \end{aligned}$ | $\begin{aligned} & .00179 \\ & .00133 \end{aligned}$ | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{aligned} & 33 \\ & 54 \end{aligned}$ |
| 1.125-20 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00225 \\ & .00170 \end{aligned}$ | $\begin{aligned} & .00130 \\ & .00098 \end{aligned}$ | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{array}{r} 4 \\ 33 \end{array}$ | $\begin{aligned} & \text { 2B } \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{array}{r} .00295 \\ .00220 \end{array}$ | $\begin{aligned} & .00170 \\ & .00127 \end{aligned}$ | $\stackrel{2}{2}$ | 42 1 |

Table 2.22. Deviations in lead and half-angle equivalent to one-half of pitch diameter tolerances, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | External |  |  |  |  | Internal |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  |
| 1 | 2 | 3 | 4 | 5 |  |  | 7 | 8 | 9 |  |  |
| 1.125-28 | UN | ${ }_{3}^{2 A}$ | in .00200 .00150 | in .00015 .00087 | $\begin{gathered} \operatorname{deg} \\ 2 \\ 1 \end{gathered}$ | $\begin{aligned} & \min \\ & 34 \\ & 55 \end{aligned}$ | ${ }_{3 \mathrm{~B}}^{2 \mathrm{~B}}$ | $\begin{gathered} \text { in } \\ .00260 \\ .00195 \end{gathered}$ | $\begin{gathered} \text { in } \\ .00150 \\ .001113 \end{gathered}$ | deg 3 3 2 | $\begin{aligned} & \min \\ & 20 \\ & 30 \end{aligned}$ |
| 1.1875-8 | UN | ${ }_{3}^{2 A}$ | . 000350 | . 000202 | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | 17 <br> 57 | ${ }_{3 B}^{2 B}$ | . 004535 | $\begin{aligned} & .00263 \\ & .00196 \end{aligned}$ | 1 | 40 15 |
| 1.1875-12 | UN | ${ }_{3}^{2 \mathrm{~A}}$ | . 002929 | $\begin{array}{r} .00167 \\ .00124 \end{array}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 36 \\ & 11 \end{aligned}$ | $\begin{aligned} & { }_{3 B}^{2 B} \end{aligned}$ | $\begin{array}{r} .00375 \\ .00280 \end{array}$ | $\begin{aligned} & .00217 \\ & .00162 \end{aligned}$ | ${ }_{1}^{2}$ | 4 3 |
| 1.1875-16 | UN | ${ }_{3}^{2 A}$ | $\begin{aligned} & .00255 \\ & .00190 \end{aligned}$ | $\begin{aligned} & .00147 \\ & .00110 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 52 \\ & 24 \end{aligned}$ | ${ }_{3 B}^{2 B}$ | $\begin{aligned} & .0033030 \\ & .0 \end{aligned}$ | $\begin{aligned} & .00191 \\ & .00144 \end{aligned}$ | 2 | 25 50 |
| 1.1875-18 | UNEF | ${ }_{3}^{2 \mathrm{~A}}$ | . 000245 | . 000141 | ${ }_{1}^{2}$ | 1 29 | ${ }_{3 \mathrm{~B}}^{2 \mathrm{~B}}$ | . 000315 | . 00182 | ${ }_{1}^{2}$ | 36 56 |
| 1.1875-20 | UN | ${ }_{3}^{2 A}$ | . 000235 | . 000136 | 2 | 9 <br> 36 | ${ }_{3 \mathrm{~B}}^{2 \mathrm{~B}}$ | . 000225 | . 000176 | ${ }_{2}^{2}$ | 48 4 |
| 1.1875-28 | UN | ${ }_{3}^{2 A}$ | . 000205 | . 0000118 | ${ }_{1}^{2}$ | $\begin{aligned} & 38 \\ & 59 \end{aligned}$ | ${ }_{3 \mathrm{~B}}^{2 \mathrm{~B}}$ | $\begin{aligned} & .00265 \\ & .00200 \end{aligned}$ | $\begin{aligned} & .00153 \\ & .00115 \end{aligned}$ | 3 2 2 | ${ }_{34}^{24}$ |
| 1.250-7 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00555 .00370 .00275 | .00320 .00214 .00159 | $\begin{aligned} & 1 \\ & 1 \\ & 0 \end{aligned}$ | $\begin{aligned} & 47 \\ & 11 \\ & 53 \end{aligned}$ | 18 2 B 3 B | .00720 .00480 .00360 | $\begin{array}{r} .00416 \\ .00277 \\ .00208 \end{array}$ | 1 | 19 32 9 |
| 1.250-8 | UN | 2 A 3 A | $\begin{aligned} & .00350 \\ & .00265 \end{aligned}$ | $\begin{aligned} & .00202 \\ & .00153 \end{aligned}$ | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | $\begin{aligned} & 17 \\ & 58 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{array}{r} .00460 \\ .00345 \end{array}$ | $\begin{aligned} & .00266 \\ & .00199 \end{aligned}$ | ${ }_{1}^{1}$ | 41 16 |
| 1.250-12 | UNF | 1 A ${ }_{2} \mathrm{~A}$ 3 A | .00460 .00310 .00230 | .00266 .00179 .00133 | $\begin{aligned} & 2 \\ & 1 \\ & 1 \end{aligned}$ | 32 42 46 16 | 18 2 B 3 B | .00600 .00400 .00300 | .00346 .00231 .00173 | 3 2 1 1 | 18 12 39 |
| 1.250-16 | UN | ${ }_{3 A}^{2 A}$ | . 000255 | . 000147 | 1 | ${ }_{24}^{52}$ | ${ }_{3 \mathrm{~B}}^{2 \mathrm{~B}}$ | . 0003350 | . 0001914 | 2 | 25 50 |
| 1.250-18 | UNEF | ${ }_{3}^{2 A}$ | . 000245 | . 000141 | $\stackrel{2}{1}$ | 1 29 | 2B | $\begin{aligned} & .00315 \\ & .00235 \end{aligned}$ | $\begin{aligned} & .00182 \\ & .00136 \end{aligned}$ | $\stackrel{2}{1}$ | 36 56 |
| 1.250-20 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00235 \\ & .00175 \end{aligned}$ | . 000136 | ${ }_{1}^{2}$ | 98 <br> 38 | 2B | $\begin{aligned} & .00305 \\ & .00225 \end{aligned}$ | $\begin{aligned} & .00176 \\ & .00130 \end{aligned}$ | ${ }_{2}^{2}$ | 48 4 |
| 1.250-28 | UN | ${ }_{3}^{2 A}$ | .00205 .00155 | . 000118 | ${ }_{1}^{2}$ | 38 59 | 28 3 B | .00265 .00200 | . 000153 | 3 2 | ${ }_{34}^{24}$ |
| 1.3125-8 | UN | 2 A 3 A | . 0002655 | $\begin{aligned} & .00205 \\ & .00153 \end{aligned}$ | 1 | 18 58 | ${ }_{3 B}^{2 B}$ | . 0046445 | . 0002669 | 1 | 41 16 |
| 1.3125-12 | UN | ${ }_{3}^{2 A}$ | . 002290 | . 000167 | $\frac{1}{1}$ | 36 11 | ${ }_{3 B}^{2 B}$ | . 000375 | $\begin{aligned} & .00217 \\ & .00162 \end{aligned}$ | ${ }_{1}^{2}$ | ${ }_{32}^{4}$ |
| 1.3125-16 | UN | $\begin{aligned} & 2 A \\ & 3 A \end{aligned}$ | $\begin{aligned} & .00255 \\ & .00190 \end{aligned}$ | $\begin{aligned} & .00147 \\ & .00110 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 52 \\ & 24 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .00330 \\ & .00250 \end{aligned}$ | $\begin{aligned} & .00191 \\ & .00144 \end{aligned}$ | ${ }_{1}^{2}$ | 25 50 |
| 1.3125-18 | UNEF | ${ }_{3}^{2 A}$ | . 000245 | . 000141 | ${ }_{1}^{2}$ | 1 29 | ${ }_{3 \mathrm{~B}}^{2 \mathrm{~B}}$ | .00315 .00235 | . 000182 | 2 | 36 56 |
| 1.3125-20 | UN | ${ }_{3}^{2 A}$ | . 000235 | . 000136 | ${ }_{1}^{2}$ | 9 36 | 2B ${ }_{3}$ | . 000225 | $\text { . } 000136$ | 3 2 2 | 48 4 |
| 1.3125-28 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} .00205 \\ .00155 \end{array}$ | .00118 .00089 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | 38 59 | ${ }_{3 \mathrm{~B}}^{2 \mathrm{~B}}$ | .00265 .00200 | $\text { .00153 } .00115$ | $\begin{array}{r}3 \\ 2 \\ \hline\end{array}$ | ${ }_{34}^{24}$ |
| 1.375-6 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} .00600 \\ .00400 \\ .00300 \end{array}$ | .00346 .00231 .00173 | $\begin{aligned} & 1 \\ & 1 \\ & 0 \end{aligned}$ | 39 50 50 | 18 2 B 3 B | .00775 .00520 .00390 | $\begin{array}{r} .00447 \\ .00300 \\ .00225 \end{array}$ | 1 | 8 <br> 26 <br> 4 |
| 1.375-8 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{aligned} & .00360 \\ & .00270 \end{aligned}$ | $\begin{aligned} & .00208 \\ & .00156 \end{aligned}$ | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | $\begin{aligned} & 19 \\ & 59 \end{aligned}$ | $\begin{aligned} & { }_{3 \mathrm{~B}}^{2 \mathrm{~B}} \end{aligned}$ | $\begin{array}{r} .00465 \\ .00350 \end{array}$ | $\begin{aligned} & .00268 \\ & .00202 \end{aligned}$ | 1 | 42 17 |
| 1.375-12 | UNF | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00470 \\ & .00315 \\ & .00235 \end{aligned}$ | $\begin{aligned} & .00271 \\ & .00182 \\ & .00136 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 35 \\ & 44 \\ & 18 \end{aligned}$ | $\begin{aligned} & 1 \mathrm{~B} \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .00615 \\ & .00410 \\ & .00305 \end{aligned}$ | $\begin{aligned} & .00365 \\ & .00237 \\ & .00176 \end{aligned}$ | 3 2 1 | 23 15 41 |
| 1.375-16 | UN | ${ }_{3 A}$ | $\begin{array}{r} .00255 \\ .00190 \end{array}$ | $\begin{array}{r} .00147 \\ .00110 \end{array}$ | 1 | $\begin{aligned} & 52 \\ & 24 \end{aligned}$ | $\begin{aligned} & { }_{3}^{2 \mathrm{~B}} \\ & { }_{3} \end{aligned}$ | $\begin{aligned} & .00330 \\ & .00250 \end{aligned}$ | $\begin{array}{r} .00191 \\ .00144 \end{array}$ | ${ }_{1}^{2}$ | 25 50 |
| 1.375-18 | UNEF | ${ }_{3 \mathrm{~A}}{ }^{\text {A }}$ | $\begin{aligned} & .0024545 \\ & .00180 \end{aligned}$ | $\begin{aligned} & .00141 \\ & .00104 \end{aligned}$ | ${ }_{1}^{2}$ | 1 29 | ${ }_{3 B}^{2 B}$ | $.00315$ | $\begin{aligned} & .00182 \\ & .00136 \end{aligned}$ | ${ }_{1}^{2}$ | 36 56 |

Table 2.22. Deviations in lead and half-angle equivalent to one-half of pitch diameter tolerances, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | External |  |  |  |  | Internal |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  | Class | Half of pitch diameter tolerance | Equivaleut deviation in lead | Equivalent deviation in half-angle |  |
| 1 | 2 | 3 | 4 | 5 |  |  | 7 | 8 | 9 |  |  |
| 1.375-20 | UN | 2 A 3 A | $\begin{gathered} i n \\ .00235 \\ .00175 \end{gathered}$ | $\begin{aligned} & i n \\ & .00136 \\ & .00101 \end{aligned}$ | deg 2 1 | min 9 96 | 2B 3 B | in .00305 .00225 | $\begin{gathered} i n \\ .00176 \\ .00130 \end{gathered}$ | deg 2 2 | min 48 4 |
| 1.375-28 | UN | 2 A | .00205 .00155 | .00118 .00089 | 2 1 | $\begin{aligned} & 38 \\ & 59 \end{aligned}$ | 2B | . 00265 | .00153 .00115 | 3 2 | 24 |
| 1.4375-6 | UN | 2 A | .00400 .00300 | . 00231 | 1 | 6 50 | 2 B 3 B | .00520 .00390 | .00300 .00225 | 1 | 26 4 |
| 1.4375-8 | UN | $\underset{3 \mathrm{~A}}{2 \mathrm{~A}}$ | .00360 .00270 | .00208 .00156 | 1 | 19 59 | ${ }^{2} \mathbf{3 B}$ | .00470 .00355 | .00271 .00205 | 1 | 43 18 |
| 1.4375-12 | UN | 2 A | .00295 .00220 | .00170 .00127 | 1 | 37 13 | 28 3 B | .00380 .00285 | .00219 .00165 | 2 1 | 5 34 |
| 1.4375-16 | UN | 2A | . 00260 | . 000150 | 1 | 54 26 | 2B | .00340 .00255 | .00196 .00147 | $\stackrel{2}{1}$ | 30 52 |
| 1.4375-18 | UNEF | 2A | .00250 .00185 | . 000144 | 2 1 | 4 32 | 2B | . 00325 | .00188 .00139 | $\stackrel{2}{1}$ | 41 59 |
| 1.4375-20 | UN | $2 \mathrm{3A}$ | .00240 .00180 | .00139 .00104 | 2 1 | 12 39 | 2B | .00310 .00230 | .00179 .00133 | $\stackrel{2}{2}$ | 50 6 |
| 1.4375-28 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00210 .00155 | .00121 .00089 | 2 1 | 42 59 | ${ }_{3}^{2 B}$ | .00275 .00205 | .00159 .00118 | 3 2 | 31 38 |
| 1.500-6 | UNC | 1 A 2 A 3 A | .00605 .00405 .00305 | .00349 .00234 .00176 | 1 1 0 | 40 7 50 | 18 $2 B$ 3 B | .00790 .00525 .00395 | .00456 .00303 .00288 | 2 1 1 | 10 27 5 |
| 1.500-8 | UN | 2 A | . 00365 | . 00211 | 1 | 20 | 2B | .00475 .00355 | . 000274 | 1 1 | 44 18 |
| 1.500-12 | UNF | 14 2 A 3 A | .00480 .00320 .00240 | .00277 .00185 .00139 | 2 1 1 | 38 46 19 | 18 28 3 B | .00625 .00415 .00315 | .00361 .00240 .00182 | 3 2 1 | 26 17 44 |
| 1.500-16 | UN | $\begin{array}{r}24 \\ 3 \\ \hline\end{array}$ | .00260 .00195 | .00150 .00113 | 1 | $\begin{aligned} & 54 \\ & 26 \end{aligned}$ | 2B ${ }^{\text {3B }}$ | .00340 .00255 | .00196 .00147 | 2 1 | 30 52 |
| 1.500-18 | UNEF | $\stackrel{2 \mathrm{~A}}{3 \mathrm{~A}}$ | . 00250 | . 000144 | 2 1 | 4 32 | 2 B 3 B | .00325 .00240 | .00188 .00139 | 2 1 | 41 59 |
| 1.500-20 | UN | $\underset{3 \mathrm{~A}}{2 \mathrm{~A}}$ | .00240 .00180 | .00139 .00104 | $\stackrel{2}{1}$ | 12 39 | ${ }_{3}^{2 B}$ | .00310 .00230 | .00179 .00133 | 2 2 | 50 6 |
| 1.500-28 | UN | 2 A | . 00210 | . 00121 | 2 1 | 42 59 | 2B | .00275 .00205 | . 00159 | 3 2 | 31 38 |
| 1.5625-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00410 .00305 | .00237 .00176 | 1 | 8 50 | 2 B 3 B | .00530 .00400 | . 003026 | 1 | 27 6 |
| 1.5625-8 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00370 .00275 | .00214 .00159 | 1 | 21 | ${ }_{3}^{2 B}$ | .00480 .00360 | . 00277 | 1 | 46 19 |
| 1.5625-12 | UN | 2 A | $\begin{array}{r} .00295 \\ .00220 \end{array}$ | .00170 .00127 | 1 | 37 13 | 2B ${ }_{3}$ | .00380 .00285 | .00219 .00165 | 2 1 | 5 34 |
| 1.5625-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00260 .00195 | . 000150 | 1 | $\begin{aligned} & 54 \\ & 26 \end{aligned}$ | ${ }_{3}^{2 B}$ | . 000340 | . 000196 | $\stackrel{2}{1}$ | 30 52 |
| 1. 5625-18 | UNEF | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00250 \\ & .00185 \end{aligned}$ | . 00144 | 2 1 | 4 32 | 2B | .00325 .00240 | .00188 .00139 | 2 | 41 59 |
| 1.5625-20 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00240 \\ & .00180 \end{aligned}$ | .00139 .00104 | 2 1 | 12 39 | $2 B$ 3 B | $\begin{array}{r} .00310 \\ .00230 \end{array}$ | $\begin{array}{r} .00179 \\ .00133 \end{array}$ | $\stackrel{2}{2}$ | 50 6 |
| 1.625-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00410 .00310 | $\begin{array}{r} .00237 \\ .00179 \end{array}$ | 1 0 | $\begin{array}{r} 8 \\ 51 \end{array}$ | $\begin{aligned} & \text { 2B } \\ & 3 \mathrm{~B} \end{aligned}$ | .00535 .00400 | .00309 .00231 | 1 | 28 6 |
| 1.625-8 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{aligned} & .00370 \\ & .00280 \end{aligned}$ | $\begin{aligned} & .00214 \\ & .00162 \end{aligned}$ | 1 | 21 2 | $2 B$ 3 B | $\begin{array}{r} .00485 \\ .00360 \end{array}$ | . 002880 | 1 | 47 19 |
| 1.625-12 | UN | $\begin{aligned} & \text { 2A } \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} .00295 \\ .00220 \end{array}$ | $\begin{aligned} & .00170 \\ & .00127 \end{aligned}$ | 1 | $\begin{aligned} & 37 \\ & 13 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{array}{r} .00380 \\ .00285 \end{array}$ | .00219 .00165 | $\stackrel{2}{1}$ | 5 34 |
| 1.625-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00260 \\ & .00195 \end{aligned}$ | $\begin{aligned} & .00150 \\ & .00113 \end{aligned}$ | 1 | $\begin{aligned} & 54 \\ & 26 \end{aligned}$ | $\begin{aligned} & \text { 2B } \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{array}{r} .00340 \\ .00255 \end{array}$ | $\begin{aligned} & .00196 \\ & .00147 \end{aligned}$ | 1 | 30 52 |
| 1.625-18 | UNEF | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} .00250 \\ .00185 \end{array}$ | $\begin{aligned} & .00144 \\ & .00107 \end{aligned}$ | $\stackrel{2}{1}$ | $\begin{array}{r} 4 \\ 32 \end{array}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{array}{r} .00325 \\ .00240 \end{array}$ | $\begin{aligned} & .00188 \\ & .00139 \end{aligned}$ | 2 1 | 41 59 |

Table 2.22. Deviations in lead and half-angle equivalent to one-half of pitch diameter tolerances, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Exterual |  |  |  |  | Internal |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  |
| 1 | 2 | 3 | 4 | 5 |  |  | 7 | 8 | 9 |  |  |
| 1.625-20 | UN | 2 A | $\begin{gathered} i n \\ .00240 \\ .00180 \end{gathered}$ | $\begin{gathered} \text { in } \\ .00139 \\ .00104 \end{gathered}$ | deg 2 1 | $\begin{aligned} & \min \\ & 12 \\ & 39 \end{aligned}$ | ${ }_{3}^{2 B}$ | $\begin{gathered} i n \\ .00310 \\ .00230 \end{gathered}$ | $\begin{gathered} i n \\ .00179 \\ .00133 \end{gathered}$ | deg 2 2 | $\min$ 50 6 |
| 1.6875-6 | UN | 2 A | .00415 .00310 | .00240 .00179 | 1 | 8 51 | 2 B 3 B | .00540 .00405 | $\begin{aligned} & .00312 \\ & .00234 \end{aligned}$ | 1 | 29 7 |
| 1.6875-8 | UN | 2 A | $\begin{aligned} & .00375 \\ & .00280 \end{aligned}$ | . 00217 | 1 | 22 2 | ${ }_{3}^{2 B}$ | . 00485 | . 00280 | 1 | 47 20 |
| 1.6875-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00300 .00225 | .00173 .00130 | 1 | $\begin{aligned} & 39 \\ & 14 \end{aligned}$ | 2B ${ }_{3}$ | .00390 .00290 | . 00225 | 2 | 9 36 |
| 1.6875-16 | UN | 2 A | . 00265 | . 00153 | 1 | 57 28 | 2B 3 3 | .00345 .00260 | .00199 .00150 | 2 1 | 32 54 |
| 1.6875-18 | UNEF | 2 A | .00255 .00190 | .00147 .00110 | 2 | $\begin{array}{r} 6 \\ 34 \end{array}$ | 2B 3 B | .00330 .00245 | . 000191 | $\stackrel{2}{2}$ | 43 1 |
| 1.6875-20 | UN | 2 A | .00240 .00180 | .00139 .00104 | 2 | $\begin{aligned} & 12 \\ & 39 \end{aligned}$ | 2B 3 B | . 000315 | .00182 .00136 | 2 | 53 9 |
| 1.750-5 | UNC | 1 A 2 A 3 A | .00670 .00445 .00335 | .00387 .00257 .00193 | 1 1 0 | $\begin{array}{r} 32 \\ 1 \\ 46 \end{array}$ | 1B 2B 3 B | .00870 .00580 .00435 | .00502 .00335 .00251 | 2 1 1 | 0 20 0 |
| 1.750-6 | UN | 2 A | . 00415 | . 00240 | 1 | 8 52 | 2 B | .00540 .00405 | .00312 .00234 | 1 | 29 7 |
| 1.750-8 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00375 .00285 | . 000217 | 1 | 22 3 | 2B ${ }^{\text {B }}$ | .00490 .00370 | .00283 .00214 | 1 | 48 21 |
| 1.750-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00300 .00225 | .00173 .00130 | 1 | 39 14 | 2B 3 B | . 000390 | . 00225 | 2 | 9 36 |
| 1.750-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00265 .00200 | . 00153 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 57 \\ & 28 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00345 .00260 | .00199 .00150 | 2 1 | 32 54 |
| 1.750-20 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00240 .00180 | .00139 .00104 | $\stackrel{2}{1}$ | 12 39 | 2B ${ }^{\text {B }}$ | .00315 .00235 | .00182 .00136 | $\stackrel{2}{2}$ | 53 9 |
| 1.8125-6 | UN | 2 A | .00420 .00315 | .00242 .00182 | 1 0 | 9 52 | 2B | . 00545 | .00315 .00237 | 1 | 30 8 |
| 1.8125-8 | UN | 2 A | .00380 .00285 | .00219 .00165 | 1 | 24 3 | 2B 3 B | .00495 .00370 | .00286 .00214 | 1 | 49 21 |
| 1.8125-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00300 \\ & .00225 \end{aligned}$ | .00173 .00130 | 1 | 39 14 | ${ }_{3 \mathrm{~B}}^{2 \mathrm{~B}}$ | .00390 .00290 | .00225 .00167 | 1 | 9 36 |
| 1.8125-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00265 \\ & .00200 \end{aligned}$ | . 00153 | 1 | 57 28 | 2B ${ }^{\text {B }}$ | .00345 .00260 | .00199 .00150 | 2 1 | 32 54 |
| 1.8125-20 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & \mathrm{~A}^{\mathrm{A}} \end{aligned}$ | .00240 .00180 | $\begin{aligned} & .00139 \\ & .00104 \end{aligned}$ | $\stackrel{2}{1}$ | $\begin{aligned} & 12 \\ & 39 \end{aligned}$ | 2B ${ }^{\text {B }}$ | .00315 .00235 | .00182 .00136 | $\stackrel{2}{2}$ | 53 9 |
| 1.875-6 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{aligned} & .00420 \\ & .00315 \end{aligned}$ | $\begin{array}{r} .00242 \\ .00182 \end{array}$ | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | $\begin{array}{r} 9 \\ 52 \end{array}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 000550 | .00318 .00237 | 1 | 31 8 |
| 1.875-8 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & \end{aligned}$ | $\begin{aligned} & .00385 \\ & .00285 \end{aligned}$ | .00222 .00165 | 1 | 25 3 | ${ }_{2}^{2 B}$ | .00500 .00375 | .00289 .00217 | 1 | 50 22 |
| 1.875-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & \hline \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00300 \\ & .00225 \end{aligned}$ | .00173 .00130 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 39 \\ & 14 \end{aligned}$ | $\begin{aligned} & \text { 2B } \\ & 3 \mathrm{~B} \end{aligned}$ | .00390 .00290 | .00225 .00167 | $\stackrel{2}{1}$ | 9 36 |
| 1.875-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00265 \\ & .00200 \end{aligned}$ | $\begin{aligned} & .00153 \\ & .00115 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 57 \\ & 28 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00345 .00260 | .00199 .00150 | 1 | 32 54 |
| 1.875-20 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00240 \\ & .00180 \end{aligned}$ | .00139 .00104 | 2 | $\begin{aligned} & 12 \\ & 39 \end{aligned}$ | 2B 3 3 | .00315 .00235 | .00182 .00136 | $\stackrel{2}{2}$ | 53 9 |
| 1.9375-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} .00425 \\ .00320 \end{array}$ | . 00245 | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | $\begin{aligned} & 10 \\ & 53 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 000555 | .00320 .00240 | 1 | 32 8 |
| 1.9375-8 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00385 \\ & .00290 \end{aligned}$ | . 000222 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{array}{r} 25 \\ 4 \end{array}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 000500 | .00289 .00217 | 1 | 50 22 |
| 1.9375-12 | UN | $\underset{3 \mathrm{~A}}{2 \mathrm{~A}}$ | $\begin{aligned} & .00305 \\ & .00225 \end{aligned}$ | $\begin{aligned} & .00176 \\ & .00130 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 41 \\ & 14 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00395 .00295 | .00228 .00170 | $\stackrel{2}{1}$ | 10 37 |
| 1.9375-16 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{aligned} & .00270 \\ & .00200 \end{aligned}$ | $\begin{aligned} & .00156 \\ & .00115 \end{aligned}$ | 1 | $\begin{aligned} & 59 \\ & 28 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{array}{r} .00350 \\ .00260 \end{array}$ | $\begin{aligned} & .00202 \\ & .00150 \end{aligned}$ | 2 1 | $\begin{aligned} & 34 \\ & 54 \end{aligned}$ |
| 1.9375-20 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{aligned} & .00245 \\ & .00185 \end{aligned}$ | $\begin{aligned} & .00141 \\ & .00107 \end{aligned}$ | $\stackrel{2}{1}$ | $\begin{aligned} & 15 \\ & 42 \end{aligned}$ | $\begin{aligned} & \text { 2B } \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .00320 \\ & .00240 \end{aligned}$ | .00185 .00139 | 2 2 | $\begin{aligned} & 56 \\ & 12 \end{aligned}$ |

Table 2.22. Deviations in lead and half-angle equivalent to one-half of pitch diameter tolerances, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | External |  |  |  |  | Internal |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  |
| 1 | 2 | 3 | 4 | 5 |  |  | 7 | 8 | 9 |  |  |
| 2.000-4.5 | UNC | 14 24 3 A | in .00715 .00475 .00355 | in .00413 .00274 .00205 | $\begin{gathered} \operatorname{deg} \\ 1 \\ 0 \\ 0 \end{gathered}$ | $\begin{aligned} & \min \\ & 28 \\ & 59 \\ & 44 \end{aligned}$ | $\begin{aligned} & \text { 1B } \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | in .00930 .00620 .00465 | in .00537 .00358 .00268 | deg 1 1 0 | min 55 17 58 |
| 2.000-6 | UN | 2 A | .00430 .00320 | .00248 .00185 | 1 | $\begin{aligned} & 11 \\ & 53 \end{aligned}$ | 2 B 3 B | . 000555 | .00320 .00240 | 1 | 32 8 |
| 2.000-8 | UN | 2 A | . 00390 | .00225 .00167 | 1 | 26 4 | $2 B$ 3 B | .00505 .00380 | .00292 .00219 | 1 | 51 24 |
| 2.000-12 | UN | 2 A | .00305 .00225 | .00176 .00130 | 1 | 41 14 | $2 B$ 3 B | .00395 .00295 | .00228 .00170 | $\stackrel{2}{1}$ | 10 37 |
| 2.000-16 | UN | 2 A | .00270 .00200 | .00156 .00115 | 1 | 59 28 | 2B 3 B | .00350 .00260 | .00202 .00150 | 2 1 | 34 54 |
| 2.000-20 | UN | 2 A 3 | .00245 .00185 | . 00141 | 2 1 | 15 42 | 2 B 3 B | .00320 .00240 | .00185 .00139 | $\stackrel{2}{2}$ | 56 12 |
| 2.125-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00435 .00325 | .00251 .00188 | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | $\begin{aligned} & 12 \\ & 54 \end{aligned}$ | 2 B 3 B | .00565 .00420 | .00326 .00242 | 1 | 33 9 |
| 2.125-8 | UN | 2A | .00395 .00295 | .00228 .00170 | 1 | 27 5 | 2 B 3 B | .00510 .00385 | .00294 .00222 | 1 | 52 25 |
| 2.125-12 | UN | 2A | .00305 .00225 | .00176 .00130 | 1 | 41 | ${ }_{3}^{2 B}$ | .00395 .00295 | .00228 .00170 | 2 1 | 10 37 |
| 2.125-16 | UN | $2{ }_{3}{ }^{\text {A }}$ | .00270 .00200 | .00156 .00115 | 1 | 59 28 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 00350 | . 00202 | 2 1 | 34 54 |
| 2.125-20 | UN | $2 \mathrm{3A}$ | .00245 .00185 | .00141 .00107 | 2 1 | 15 42 | $2 B$ 3 B | .00320 .00240 | .00185 .00139 | 2 2 | 56 12 |
| 2.250-4.5 | UNC | 1 A 2 A 3 A | .00730 .00485 .00365 | .00421 .00280 .00211 | $\begin{aligned} & 1 \\ & 1 \\ & 0 \end{aligned}$ | $\begin{array}{r} 30 \\ 0 \\ 45 \end{array}$ | $\begin{aligned} & 1 \mathrm{~B} \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00950 .00630 .00475 | .00548 .00364 .00274 | 1 1 0 | 58 18 59 |
| 2.250-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 00440 | . 000254 | 1 | $\begin{aligned} & 13 \\ & 54 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00570 .00425 | . 00329 | 1 1 | 34 10 |
| 2.250-8 | UN | 2A | .00400 .00300 | . 00231 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 28 6 | $2 B$ $3 B$ | . 00520 | .00300 .00225 | 1 1 | 54 26 |
| 2. 250-12 | UN | $\underset{3 \mathrm{~A}}{2 \mathrm{~A}}$ | .00305 .00225 | .00176 .00130 | 1 | 41 14 | ${ }_{3}^{2 B}$ | .00395 .00295 | . 00228 | 2 1 | 10 37 |
| 2.250-16 | UN | 2 A | .00270 .00200 | . 00156 | 1 | 59 28 | 2B 3 B | .00350 .00260 | .00202 .00150 | $\stackrel{2}{1}$ | 34 54 |
| 2.250-20 | UN | 2 A | .00245 .00185 | .00141 .00107 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{aligned} & 15 \\ & 42 \end{aligned}$ | 28 3 B | .00320 .00240 | .00185 .00139 | $\stackrel{2}{2}$ | 56 12 |
| 2.375-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00445 .00330 | .00257 .00191 | 1 | $\begin{aligned} & 13 \\ & 54 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00575 .00430 | .00332 .00248 | 1 1 | 35 11 |
| 2.375-8 | UN | 2 A | $\begin{aligned} & .00405 \\ & .00300 \end{aligned}$ | $\begin{aligned} & .00234 \\ & .00173 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 29 6 | $2 B$ 3 B | .00525 .00395 | .00303 .00228 | 1 1 | 55 27 |
| 2.375-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} .00310 \\ .00230 \end{array}$ | .00179 .00133 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 42 \\ & 16 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .00405 \\ & .00300 \end{aligned}$ | .00234 .00173 | 2 1 | 14 39 |
| 2.375-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00275 .00205 | .00159 .00118 | 2 1 | $\begin{array}{r} 1 \\ 30 \end{array}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .00360 \\ & .00270 \end{aligned}$ | $\begin{aligned} & .00208 \\ & .00156 \end{aligned}$ | 2 1 | 38 59 |
| 2.375-20 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00255 \\ & .00190 \end{aligned}$ | .00147 .00110 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{aligned} & 20 \\ & 44 \end{aligned}$ | 2 B 3 B | .00330 .00250 | . 00191 | 3 2 | 17 |
| 2.500-4 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00775 \\ & .00520 \\ & .00390 \end{aligned}$ | .00447 .00300 .00225 | $\begin{aligned} & 1 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 25 \\ & 57 \\ & 43 \end{aligned}$ | $\begin{aligned} & \text { 1B } \\ & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .01010 .00675 .00505 | .00583 .00390 .00292 | 1 1 0 | 51 14 56 |
| 2.500-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} .00450 \\ .00335 \end{array}$ | .00260 .00193 | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | $\begin{aligned} & 14 \\ & 55 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00580 .00435 | .00335 .00251 | 1 1 | 36 12 |
| 2.500-8 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00410 \\ & .00305 \end{aligned}$ | $\begin{array}{r} .00237 \\ .00176 \end{array}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{array}{r} 30 \\ 7 \end{array}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .00530 \\ & .00400 \end{aligned}$ | $\begin{aligned} & .00306 \\ & .00231 \end{aligned}$ | 1 | 57 28 |
| 2.500-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00310 \\ & .00230 \end{aligned}$ | $\begin{aligned} & .00179 \\ & .00133 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 42 \\ & 16 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .00405 \\ & .00300 \end{aligned}$ | $\begin{aligned} & .00234 \\ & .00173 \end{aligned}$ | 2 1 | 14 39 |
| 2.500-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00275 \\ & .00205 \end{aligned}$ | $\begin{aligned} & .00159 \\ & .00118 \end{aligned}$ | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{array}{r} 1 \\ 30 \end{array}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{array}{r} .00360 \\ .00270 \end{array}$ | $\begin{aligned} & .00208 \\ & .00156 \end{aligned}$ | 2 1 | $\begin{aligned} & 38 \\ & 59 \end{aligned}$ |

Table 2.22. Deviations in lead and half-angle equivalent to one-half of pitch diameter tolerances, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | External |  |  |  |  | Internal |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead |  |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  |
| 1 | 2 | 3 | 4 | 5 |  |  | 7 | 8 | 9 |  |  |
| 2.500-20 | UN | 2 A | in .00255 .00190 | in .00147 .00110 | deg 2 1 | min 20 44 | 23B | in .00330 .00250 | in .00191 .00144 | deg 3 2 | $\min$ 1 17 |
| 2.625-6 | UN | 2 A 3 A | .00450 .00340 | .00260 .00196 | 1 | 14 56 | 2B | .00590 .00440 | . 00341 | 1 | 37 13 |
| 2.625-8 | UN | 3 A | .00410 .00310 | .00237 .00179 | 1 | 30 8 | 2B ${ }_{3}$ | .00535 .00400 | .00309 .00231 | 1 | 58 28 |
| 2.625-12 | UN | 3 AA | . 00310 | .00179 .00133 | 1 | 42 16 | $2 B$ $3 B$ | .00405 .00300 | . 00234 | $\stackrel{2}{1}$ | 14 39 |
| 2.625-16 | UN | 2 A | .00275 .00205 | .00159 .00118 | 2 1 | 1 30 | 2B ${ }_{3}$ | .00360 .00270 | .00208 .00156 | 2 1 | 38 59 |
| 2.625-20 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | .00255 .00190 | . 00147 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{aligned} & 20 \\ & 44 \end{aligned}$ | 2B ${ }^{\text {B }}$ | .00330 .00250 | . 000191 | 3 2 | 17 |
| 2.750-4 | UNC | 1 A 2 A 3 A | .00790 .00525 .00395 | .00456 .00303 .00228 | $\begin{aligned} & 1 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 27 \\ & 58 \\ & 43 \end{aligned}$ | 1B 2 B 3 B | .01030 .00685 .00515 | .00595 .00395 .00297 | 1 1 0 | 53 15 57 |
| 2.750-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00455 .00340 | .00263 .00196 | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | 15 56 | ${ }_{3}^{2 B}$ | .00595 .00445 | . 000344 | 1 | 38 13 |
| 2.750-8 | UN | ${ }_{3}^{2 A}$ | . .00415 | .00240 .00182 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 31 9 | 2B ${ }^{\text {B }}$ | .00540 .00405 | . 000312 | 1 | 59 29 |
| 2.750-12 | UN | $\stackrel{2}{\text { A }}$ | .00310 .00230 | .00179 .00133 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 42 16 | 2 BB | .00405 .00300 | . 000234 | 2 1 | 14 39 |
| 2.750-16 | UN | ${ }_{3}^{2 A}$ | . 00275 | .00159 .00118 | 2 1 | 1 30 | 2B | .00360 .00270 | .00208 .00156 | 2 1 | 38 59 |
| 2.750-20 | UN | 2 A | .00255 .00190 | . 000147 | 2 1 | $\begin{aligned} & 20 \\ & 44 \end{aligned}$ | 2B ${ }_{3}$ | .00330 .00250 | . 000191 | 3 2 | 17 |
| 2.875-6 | UN | 2 A 3 A | .00460 .00345 | .00266 .00199 | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | $\begin{aligned} & 16 \\ & 57 \end{aligned}$ | 2B 3 B | .00600 .00450 | .00346 .00260 | 1 | 39 14 |
| 2.875-8 | UN | ${ }_{3 A}^{2 A}$ | .00420 .00315 | .00242 .00182 | 1 | 32 9 | 2B ${ }^{\text {B }}$ | .00550 .00410 | . 00318 | 2 1 | ${ }_{30}^{1}$ |
| 2.875-12 | UN | 2 A 3 A | .00315 .00235 | .00182 .00136 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 44 18 | 2B ${ }^{\text {B }}$ | . 000410 | . 00237 | $\stackrel{2}{1}$ | 15 42 |
| 2.875-16 | UN | 2 A 3 A | . 002880 | .00162 .00121 | 2 1 | 3 32 | 2B | .00365 .00275 | .00211 .00159 | $\stackrel{2}{2}$ | 40 1 |
| 2.875-20 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | .00260 .00195 | .00150 .00113 | 1 | 23 47 | ${ }_{3}^{2 B}$ | . 00340 | . 00196 | 3 2 | 7 20 |
| 3.000-4 | UNC | 1 A 2 A 3 A | .00805 .00535 .00400 | .00465 .00309 .00231 | $\begin{aligned} & 1 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & 29 \\ & 59 \\ & 44 \end{aligned}$ | 1B 2B 3 B | .01045 .00695 .00520 | .00603 .00401 .00300 | 1 1 0 | 55 16 57 |
| 3.000-6 | UN | ${ }_{3 A}^{2 A}$ | . 00465 | .00268 .00202 | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | $\begin{aligned} & 17 \\ & 58 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00605 .00455 | . 00349 | 1 | 40 15 |
| 3.000-8 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & \hline \mathrm{~A} \end{aligned}$ | .00425 .00320 | . 00245 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 33 \\ & 10 \end{aligned}$ | 2 B 3 B | .00555 .00415 | .00320 .00240 | 2 1 | ${ }_{31}^{2}$ |
| 3.000-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00315 .00235 | .00182 .00136 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 44 \\ & 18 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00410 .00310 | .00237 .00179 | 2 1 | 15 |
| $3.000-16$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00280 \\ & .00210 \end{aligned}$ | . 00162 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{array}{r} 3 \\ 32 \end{array}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 00365 | . 00211 | $\stackrel{2}{2}$ | 40 1 |
| 3.000-20 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | .00260 .00195 | .00150 .00113 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{aligned} & 23 \\ & 47 \end{aligned}$ | 2B ${ }_{3}$ | .00340 .00255 | .00196 .00147 | 3 2 | 7 20 |
| 3.125-6 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{aligned} & .00470 \\ & .00350 \end{aligned}$ | .00271 .00202 | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | $\begin{aligned} & 18 \\ & 58 \end{aligned}$ | 2B ${ }^{\text {B }}$ | $\begin{aligned} & .00610 \\ & .00460 \end{aligned}$ | $\begin{aligned} & .00352 \\ & .00266 \end{aligned}$ | 1 | 41 16 |
| 3.125-8 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{array}{r} .00430 \\ .00320 \end{array}$ | . 00248 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 35 \\ & 10 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .00560 \\ & .00420 \end{aligned}$ | $\begin{aligned} & .00323 \\ & .00242 \end{aligned}$ | 2 1 | 3 32 |
| 3.125-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00315 .00235 | $\begin{aligned} & .00182 \\ & .00136 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 44 \\ & 18 \end{aligned}$ | 2B 3 B | $\begin{aligned} & .00410 \\ & .00310 \end{aligned}$ | $\begin{array}{r} .00237 \\ .00179 \end{array}$ | 2 1 | 15 |
| 3.125-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00280 \\ & .00210 \end{aligned}$ | $\begin{aligned} & .00162 \\ & .00121 \end{aligned}$ | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{array}{r} 3 \\ 32 \end{array}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .00365 \\ & .00275 \end{aligned}$ | $\begin{aligned} & .00211 \\ & .00159 \end{aligned}$ | $2_{2}^{-}$ | 40 1 |

Table 2.22. Deviations in lead and half-angle equivalent to one-half of pitch diameter tolerances, Unified screw threads-Continued

| Nominal size and threads per inch | Series des ignation | External |  |  |  |  | Internal |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  |
| 1 | 2 | 3 | 4 | 5 |  |  | 7 | 8 | 9 |  |  |
| 3.250-4 | UNC | 1 A 2 A 3 A | in .00815 .00545 .00410 | in .00471 .00315 .00237 | deg 1 1 0 | $\min$ 30 0 45 | 18 2B 3B | in .01060 .00705 .00530 | in .00612 .00407 .00306 | deg 1 1 0 | min 57 18 58 |
| 3.250-6 | UN | 2 A | .00475 .00355 | .00274 .00205 | 1 | 18 59 | 2 B 3 B | .00615 .00460 | . 00355 | 1 | 41 16 |
| 3.250-8 | UN | 2A | .00435 .00325 | . 00251 | 1 | 36 11 | 2B | .00565 .00425 | .00326 .00245 | 1 | 4 3 |
| 3.250-12 | UN | 2A | .00315 .00235 | .00182 .00136 | 1 | 44 18 | 2B | . 000410 | .00237 .00179 | 2 1 | 15 42 |
| 3.250-16 | UN | 2A | .00280 .00210 | .00162 .00121 | 2 1 | 3 32 | 2B | .00365 .00275 | .00211 .00159 | $\stackrel{2}{2}$ | 40 1 |
| 3.375-6 | UN | 2 A | .00475 .00360 | .00274 .00208 | 1 | 18 59 | 2B ${ }_{3}$ | .00620 .00465 | .00358 .00268 | 1 | 42 17 |
| 3.375-8 | UN | 2 A | .00440 .00330 | . 00254 | 1 | 37 13 | 2B 3 B | . 00570 | .00329 .00245 | $\stackrel{2}{1}$ | 5 33 |
| 3.375-12 | UN | 2 A | .00320 .00242 | .00185 .00139 | 1 | 46 19 | 2B ${ }_{3}$ | . 00420 | .00242 .00182 | $\stackrel{2}{1}$ | 19 44 |
| 3.375-16 | UN | 2A | .00290 .00215 | .00167 .00124 | 2 1 | 8 35 | 2B ${ }_{3}$ | .00375 .00280 | . 00217 | 2 2 | 45 3 |
| 3.500-4 | UNC | 1 A 2 A 3 A | .00830 .00550 .00415 | .00479 .00318 .00240 | $\begin{aligned} & 1 \\ & 1 \\ & 0 \end{aligned}$ | 31 0 46 | 1B 2B 3B | .01075 .00755 .00540 | .00621 .00413 .00312 | 1 1 0 | 58 19 59 |
| 3.500-6 | UN | 2A | .00480 .00360 | . 00277 | 0 | 19 59 | 2B | .00625 .00470 | . 00361 | 1 | 43 18 |
| 3.500-8 | UN | 2 A | . 004440 | .00254 .00191 | $\begin{aligned} & \mathbf{1} \\ & 1 \end{aligned}$ | 37 13 | 2B | . 00575 | .00332 .00248 | 2 1 | 6 35 |
| 3.500-12 | UN | 2A | .00320 .00240 | .00185 .00139 | 1 | 46 19 | 2B | . 00420 | . 00242 | 2 1 | 19 44 |
| 3.500-16 | UN | 2 A | .00290 .00215 | .00167 .00124 | 2 1 | 8 35 | 2B ${ }_{3}$ | .00375 .00280 | .00217 .00162 | $\stackrel{2}{2}$ | 45 3 |
| 3.625-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00485 .00365 | .00280 .00211 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 20 0 | 2B 3 B | .00630 .00475 | .00364 .00274 | 1 | $\begin{aligned} & 44 \\ & 18 \end{aligned}$ |
| 3.625-8 | UN | 2A | .00445 .00335 | . 00257 | 1 | 38 14 | 2B ${ }^{\text {B }}$ | .00580 .00435 | .00335 .00251 | ${ }_{1}^{2}$ | 8 36 |
| 3.625-12 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | .00320 .00240 | .00185 .00139 | 1 | 46 19 | 2B ${ }^{\text {B }}$ | .00420 .00315 | .00242 .00182 | $\stackrel{2}{1}$ | 19 44 |
| 3.625-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00290 .00215 | .00167 .00124 | 2 1 | 8 35 | ${ }_{3}^{2 B}$ | .00375 .00280 | .00217 .00162 | $\stackrel{2}{2}$ | 45 3 |
| 3.750-4 | UNC | 1 A 2 A 3 A | .00840 .00560 .00420 | .00485 .00323 .00242 | $\begin{aligned} & 1 \\ & 1 \\ & 0 \end{aligned}$ | $\begin{array}{r} 32 \\ 2 \\ 46 \end{array}$ | 1B 2 B 3 B | .01090 .00725 .00545 | .00629 .00419 .00315 | 2 1 1 | 0 20 0 |
| 3.750-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00490 .00365 | .00283 .00211 | 1 | 21 0 | 2B ${ }^{\text {3B }}$ | . 006635 | .00367 .00274 | 1 | 45 18 |
| 3.750-8 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00450 .00335 | $\begin{aligned} & .00260 \\ & .00193 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 39 \\ & 14 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00585 .00440 | . 000338 | 2 1 | 9 37 |
| $3.750-12$ | UN | 2 A | $\begin{array}{r} .00320 \\ .00240 \end{array}$ | $\begin{aligned} & .00185 \\ & .00139 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 46 \\ & 19 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 00420 | .00242 .00182 | 2 | 19 44 |
| $3.750-16$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00290 \\ & .00215 \end{aligned}$ | $\begin{aligned} & .00167 \\ & .00124 \end{aligned}$ | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{array}{r} 8 \\ 35 \end{array}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .00375 \\ & .00280 \end{aligned}$ | $\begin{aligned} & .00217 \\ & .00162 \end{aligned}$ | $\stackrel{2}{2}$ | 45 3 |
| 3.875-6 | UN | 2 A | $\begin{aligned} & .00495 \\ & .00370 \end{aligned}$ | $\begin{aligned} & .00286 \\ & .00214 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 22 1 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{array}{r} .00640 \\ .00480 \end{array}$ | $\begin{aligned} & .00369 \\ & .00277 \end{aligned}$ | 1 | 46 19 |
| 3.875-8 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00455 \\ & .00340 \end{aligned}$ | $\begin{aligned} & .00263 \\ & .00196 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 40 \\ & 15 \end{aligned}$ | $\begin{aligned} & \text { 2B } \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .00590 \\ & .00440 \end{aligned}$ | $\begin{array}{r} .00341 \\ .00254 \end{array}$ | 2 1 | 10 37 |
| 3.875-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00325 \\ & .00245 \end{aligned}$ | $\begin{aligned} & .00188 \\ & .00141 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 47 \\ & 21 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .00425 \\ & .00320 \end{aligned}$ | .00245 .00185 | 2 1 | 20 46 |
| 3.875-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00295 \\ & .00220 \end{aligned}$ | $\begin{aligned} & .00170 \\ & .00127 \end{aligned}$ | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{aligned} & 10 \\ & 37 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{array}{r} .00380 \\ .00285 \end{array}$ | $\begin{aligned} & .00219 \\ & .00165 \end{aligned}$ | $\stackrel{2}{2}$ | 47 5 |

Table 2.22. Deviations in lead and half-angle equivalent to one-half of pitch diameler tolerances, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | External |  |  |  |  | Internal |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead |  |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  |
| 1 | 2 | 3 | 4 | 5 |  |  | 7 | 8 | 9 |  |  |
|  |  |  | in | in |  | min |  | in | in | deg | min |
| 4.000-4 | UNC | 1 A 2 A 3 A | .00850 .00565 .00425 | .00491 .00326 .00245 | 1 1 0 | 33 2 47 | 1 B 2 B 3 B | .01105 .00755 .00555 | .00638 .00424 .00320 | 2 1 1 | 2 21 1 |
| 4.000-6 | UN | 2 A 3 A | .00495 .00370 | .00286 .00214 | 1 | 22 1 | 2B ${ }^{3}$ | .00645 .00485 | .00372 .00280 | 1 | $\begin{aligned} & 46 \\ & 20 \end{aligned}$ |
| 4.000-8 | UN | 2 A | .00455 .00340 | .00263 .00196 | 1 | 40 15 | 2B 3 B | .00595 .00445 | . 000344 | 2 1 | 11 38 |
| 4.000-12 | UN | 2A | .00325 .00245 | .00188 .00141 | 1 | 47 21 | ${ }_{3}^{2 B}$ | .00425 .00320 | .00245 .00185 | $\stackrel{2}{1}$ | 20 46 |
| 4.000-16 | UN | 2 A | .00295 .00220 | .00170 .00127 | 2 1 | 10 37 | 2B ${ }_{3}$ | .00380 .00285 | .00219 .00165 | $\stackrel{2}{2}$ | 47 5 |
| 4.125-6 | UN | 2 A | .00500 .00375 | . 00289 | 1 | 22 2 | 2 B 3 B | .00650 .00485 | .00375 .00280 | 1 | 47 20 |
| 4.125-12 | UN | 2 A | .00325 .00245 | .00188 .00141 | 1 | 47 21 | ${ }_{3}^{2 B}$ | .00425 .00320 | .00245 .00185 | 2 1 | 20 |
| 4.125-16 | UN | 2 A | $\begin{aligned} & .00295 \\ & .00220 \end{aligned}$ | .00170 .00127 | 2 | 10 37 | 2B 3 B | .00380 .00285 | .00219 .00165 | $\stackrel{2}{2}$ | 47 5 |
| 4.250-4 | UN | 2 A | .00575 .00430 | .00332 .00248 | 1 | 3 47 | 2B ${ }^{\text {3B }}$ | .00745 .00560 | .00430 .00323 | 1 | 22 |
| 4.250-6 | UN | 2 A | .00505 .00375 | . 00292 | 1 | 23 2 | 2B ${ }^{\text {B }}$ | .00655 .00490 | .00378 .00283 | 1 | 48 21 |
| 4.250-12 | UN | 2 A 3 A | .00325 .00245 | .00188 .00141 | 1 | 47 21 | 2B 3 B | .00425 .00320 | .00245 .00185 | 2 1 | 20 46 |
| 4.250-16 | UN | 2 A | .00295 .00220 | .00170 .00127 | 2 1 | 10 37 | 2B 3 B | .00380 .00285 | . 00219 | 2 2 | 47 5 |
| 4.375-6 | UN | 2 A | .00505 .00380 | .00292 .00219 | 1 | 23 3 | 2B | . 006660 | .00381 .00286 | 1 | 49 22 |
| 4.375-12 | UN | 2 A | .00325 .00245 | . 00188 | 1 | 47 21 | 2B 3 B | .00425 .00320 | .00245 .00185 | 2 1 | 20 |
| 4.375-16 | UN | 2A | .00295 .00220 | . 00170 | 1 | 10 37 | 2B 3 B | .00380 .00285 | . 00219 | 2 2 | 47 5 |
| 4.500-4 | UN | 2A | .00580 .00435 | . 00335 | 1 | 4 48 | 2B 3 B | .00755 .00565 | .00436 .00326 | 1 | 23 2 |
| 4.500-6 | UN | $2 A$ $3 A$ | .00510 .00385 | .00294 .00222 | 1 | 24 | 2B | .00665 .00495 | .00384 .00286 | 1 | 50 22 |
| 4.500-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | . 00325 | . 00188 | 1 | 47 21 | ${ }_{3}^{2 B}$ | .00425 .00320 | . 00245 | 2 1 | 20 46 |
| 4.500-16 | UN | 2 A 3 A | . 002295 | .00170 .00127 | $\stackrel{2}{1}$ | 10 37 | 2B ${ }^{\text {B }}$ | .00380 .00285 | .00219 .00165 | $\stackrel{2}{2}$ | 47 5 |
| 4. 625-6 | UN | 2 A 3 A | .00515 .00385 | .00297 .00222 | 1 | 25 4 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00665 .00500 | .00384 .00289 | 1 | 50 22 |
| 4.625-12 | UN | 2 A 3 A | .00335 .00250 | .00193 .00144 | 1 | 51 22 | 2 B 3 B | .00435 .00330 | . 00251 | $\stackrel{2}{1}$ | $\begin{aligned} & 23 \\ & 49 \end{aligned}$ |
| 4.625-16 | UN | 2 A 3 | .00305 .00225 | .00176 .00130 | $\stackrel{2}{1}$ | $\begin{aligned} & 14 \\ & 39 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .00395 \\ & .00295 \end{aligned}$ | .00228 .00170 | 2 2 | 54 10 |
| 4.750-4 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00585 \\ & .00440 \end{aligned}$ | .00338 .00254 | 1 | 4 48 | 2 B 3 B | $\begin{aligned} & .00765 \\ & .00570 \end{aligned}$ | .00442 .00329 | 1 | 24 3 |
| 4.750-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00515 .00385 | $\begin{aligned} & .00297 \\ & .00222 \end{aligned}$ | 1 | 25 4 | 2B ${ }_{3}$ | $\begin{aligned} & .00670 \\ & .00505 \end{aligned}$ | $\begin{array}{r} .00387 \\ .00292 \end{array}$ | 1 | 51 23 |
| 4.750-12 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | $\begin{array}{r} .00335 \\ .00250 \end{array}$ | .00193 .00144 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 51 \\ & 22 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{array}{r} .00435 \\ .00330 \end{array}$ | $\begin{array}{r} .00251 \\ .00191 \end{array}$ | 2 1 | 23 49 |
| 4.750-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00305 \\ & .00225 \end{aligned}$ | $\begin{aligned} & .00176 \\ & .00130 \end{aligned}$ | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{aligned} & 14 \\ & 29 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & .00395 \\ & .00295 \end{aligned}$ | $\begin{array}{r} .00228 \\ .00170 \end{array}$ | 2 2 | $\begin{aligned} & 54 \\ & 10 \end{aligned}$ |
| 4.875-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00520 \\ & .00390 \end{aligned}$ | $\begin{aligned} & .00300 \\ & .00225 \end{aligned}$ | 1 | 26 4 | 2B 3B | $\begin{aligned} & .00675 \\ & .00505 \end{aligned}$ | $\begin{aligned} & .00390 \\ & .00292 \end{aligned}$ | 1 | $\begin{aligned} & 51 \\ & 23 \end{aligned}$ |

Table 2.22. Deviations in lead and half-angle cquivalent to onc-half of pitch diameter tolerances, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | External |  |  |  |  | Internal |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  | Class | Half of pitch diameter tolerance | Equivalent deviation in lead | Equivalent deviation in half-angle |  |
| 1 | 2 | 3 | 4 | 5 |  |  | 7 | 8 | 9 |  |  |
| 4.875-12 | UN | 2 A 3 A | $\begin{gathered} \text { in } \\ .00335 \\ .00250 \end{gathered}$ | $\begin{gathered} i n \\ .00193 \\ .00144 \end{gathered}$ | deg 1 1 | $\min$ 51 22 | 2B | in .00435 .00330 | $\begin{aligned} & \text { in } \\ & .00251 \\ & .00101 \end{aligned}$ | deg 1 1 | min 23 49 |
| 4.875-16 | UN | 2 A | . 00305 | .00176 .00130 | 2 1 | 14 39 | 2 B | .00395 .00295 | .00228 .00170 | $\stackrel{2}{2}$ | $\begin{aligned} & 54 \\ & 10 \end{aligned}$ |
| 5.000-4 | UN | 2 A 3 | . 00595 | . 00344 | 1 | 5 49 | $2 \mathrm{3B}$ | .00770 .00580 | . 00445 | 1 | 25 4 |
| 5.000-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00525 .00390 | .00303 .00225 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 27 4 | 2B ${ }^{\text {3B }}$ | .00680 .00510 | . 00393 | 1 | 52 24 |
| 5.000-12 | UN | 2A | .00335 .00250 | .00193 .00144 | 1 | 51 22 | $2 \mathrm{3B}$ | .00435 .00330 | . 00251 | $\stackrel{2}{1}$ | 23 49 |
| 5.000-16 | UN | 2A | .00305 .00225 | .00176 .00130 | 2 1 | 14 39 | 2B ${ }_{3}$ | .00395 .60295 | .00228 .00170 | $\stackrel{2}{2}$ | 54 10 |
| 5.125-12 | UN | 2 A | .00335 .00250 | . 000193 | 1 | 51 22 | ${ }_{2}^{2 B}$ | .00435 .00330 | . 00251 | $\stackrel{2}{1}$ | 23 49 |
| 5.125-16 | UN | 2 A | .00305 .00225 | .00176 .00130 | 2 1 | 14 39 | ${ }_{3}^{2 B}$ | .00395 .00295 | . 00228 | $\stackrel{2}{2}$ | 54 10 |
| 5. 250-4 | UN | 2 A | .00600 .00450 | .00346 .00260 | 1 | 50 | 2 BB | .00780 .00585 | .00450 .00338 | 1 | 26 4 |
| 5.250-12 | UN | 2 A | .00335 .00250 | .00193 .00144 | 1 | 51 22 | ${ }_{3}^{2 B}$ | . 00435 | . 00251 | 2 1 | 23 49 |
| 5. 250-16 | UN | 2 A | .00305 .00225 | .00176 .00130 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | 14 39 | 2B | .00395 .00295 | .00228 .00170 | $\stackrel{2}{2}$ | 54 10 |
| 5.375-12 | UN | 2 A | . 00335 | .00193 .00144 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 51 22 | ${ }_{3}^{2 B}$ | . 00435 | . 00251 | 2 1 | 23 49 |
| 5.375-16 | UN | 2 A | .00305 .00225 | .00176 .00130 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{aligned} & 14 \\ & 39 \end{aligned}$ | ${ }_{3}^{2 B}$ | .00395 .00295 | . 00228 | $\stackrel{2}{2}$ | 54 10 |
| 5.500-4 | UN | 2 A | . 00605 | . 000349 | 10 | 7 50 | ${ }_{3}^{2 B}$ | .00790 .00590 | .00456 .00341 | 1 1 | 27 5 |
| 5.500-12 | UN | $2 \mathrm{2A}$ | .00335 .00250 | .00193 .00144 | 1 | 51 22 | 23 ${ }_{3}$ | . 00435 | .00251 .00191 | ${ }_{1}^{2}$ | 23 49 |
| 5.500-16 | UN | 2 A | .00305 .00225 | .00176 .00130 | 2 1 | 14 39 | 2B | .00395 .00295 | .00228 .00170 | $\stackrel{2}{2}$ | 54 10 |
| 5.625-12 | UN | 2 A | . 000345 | .00199 .00150 | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | 54 26 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00450 .00335 | .00260 .00193 | $\stackrel{2}{1}$ | 28 51 |
| 5.625-16 | UN | 2A | .00310 .00235 | .00179 .00136 | 2 1 | 16 43 | ${ }_{3}^{2 B}$ | .00405 .00305 | .00234 .00176 | $\stackrel{2}{2}$ | 58 14 |
| 5.750-4 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} .00610 \\ .00460 \end{array}$ | $\begin{array}{r} .00352 \\ .00266 \end{array}$ | 1 0 | 7 51 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00795 .00595 | . 000459 | 1 | 27 5 |
| 5.750-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00345 .00260 | .00199 .00150 | 1 | 54 26 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 00450 | . 00260 | 2 | 28 51 |
| 5.750-16 | UN | ${ }_{3 \mathrm{~A}}^{2 \mathrm{~A}}$ | . 00310 | .00179 .00136 | 2 1 | 16 43 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 00405 | .00234 .00176 | 2 | 58 14 |
| 5.875-12 | UN | $\underset{3 A}{2 A}$ | . 000345 | $\begin{array}{r} .00199 \\ .00150 \end{array}$ | $\begin{aligned} & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 54 \\ & 26 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 00450 | .00260 .00193 | 2 1 | 28 |
| 5.875-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00310 .00235 | .00179 .00136 | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{aligned} & 16 \\ & 43 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00405 .00305 | .00234 .00176 | $\stackrel{2}{2}$ | 58 14 |
| 6.000-4 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .00620 .00465 | .00358 .00268 | $\begin{aligned} & 1 \\ & 0 \end{aligned}$ | 8 51 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{array}{r} .00805 \\ .00600 \end{array}$ | . 00465 | 1 | 29 6 |
| 6.000-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} .00345 \\ .00260 \end{array}$ | $\begin{aligned} & .00199 \\ & .00150 \end{aligned}$ | 1 | 54 26 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | . 000450 | . 00260 | 2 1 | 28 51 |
| 6.000-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .00310 \\ & .00235 \end{aligned}$ | $\begin{array}{r} .00179 \\ .00136 \end{array}$ | $\begin{aligned} & 2 \\ & 1 \end{aligned}$ | $\begin{aligned} & 16 \\ & 43 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | .00405 .00305 | $\begin{aligned} & .00234 \\ & .00176 \end{aligned}$ | 2 2 | 58 14 |

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# UNITED STATES DEPARTMENT OF COMMERCE National bureau of standards 

## HANDBOOK H28

SCREW-THREAD STANDARDS
FOR FEDERAL SERVICES
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1969

## UNIFIED THREADS OF SPECIAL DIAMETERS, PITCHES, AND LENGTHS OF ENGAGEMENT

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## 1. INTRODUCTION

The thread series, tolerances, and allowances specified in section 2 of H28 apply in general to bolts, nuts, and tapped holes of standard pitches and diameters. In addition, there are large quantities of threaded parts produced where the relations of diameter to pitch are necessarily different from those of the standard thread series, and the lengths of engagement either shorter or longer than for bolt and nut practice. Such threads are designated "threads of special diameters, pitches, and lengths of engagement". Selected combinations of Unified special screw threads are listed in table 3.1. Pitch diameter tolerances in this table are based on a length of thread engagement of 9 times the pitch. The pitch diameter limits are applicable to a length of engagement of from 5 to 15 times the pitch. (This should not be confused with the length of thread on mating parts, as it may exceed the length of engagement by a considerable amount.)

## 2. TYPES OF SPECIAL THREADS

There are various degrees of specialization in the design of special threads that may be classified as follows:
(1) A standard thread that is modified by the inclusion of some nonstandard feature as discussed in section 2,
(2) A thread of a standard diameter such as is found in one or more of the thread series in section 2 associated with a standard pitch listed in table 2.1 forming a diameter-pitch combination that is not in a standard thread series; for example, 1.000-10 UNS,
(3) A diameter of odd size such as 1.137 in . associated with a standard pitch,
(4) A thread of either standard or nonstandard diameter associated with a nonstandard pitch; for example, 1.000-15 UNS or .895-26 UNS,
(5) A thread of any of the first four degrees of specialization to which special tolerances are applied,
(6) A completely special thread that deviates from the standard Unified thread form.

In the interest of economy, the designer should adhere to standard threads or to thread features conforming as closely as possible to established standards. It should be remembered that special threads entail the design and manufacture of special threading tools and gages with consequent greater costs, increase in inventories, and difficulties in procuring spare parts when replacements are necessary.

In this section, standards for special threads are presented, including thread form, selected combinations of Unified special screw threads (table 3.1), allowances and tolerances, and detailed directions for specifying special threads on drawings. A discussion of factors affecting the design of special threads is presented in appendix A5.

## 3. UNIFIED FORM OF THREAD

The Unified form of thread profile as specified in section 2 shall be used.

## 4. PREFERRED DIAMETERS AND PITCHES

The use, whenever possible, of the standard series of screw threads listed in table 2.7 is recommended for all applications. Whenever sizes and pitches in table 2.7 are not suitable, the designer should, if possible, choose a thread from table 3.1 which lists selected combinations of Unified special screw threads. If a selection cannot be made from either table 2.7 or 3.1 , consideration should be given to the following paragraphs in a choice of thread.
4.1. Preferred Diameters.-Whenever possible, the basic diameter should be selected from series of diameter increments as follows:

| Range | Diameter increments |  |
| :---: | :---: | :---: |
|  | First choice | Second choice |
| in | in | in |
| 0.25 to 0.6 | 0.05 |  |
| above 0.6 to 1.5 | 0.1 | 0.05 |
| above 1.5 to 6.0 | 0.25 | 0.1 |
| above 6 to 16 | 0.5 | 0.25 |
| above 16 to 24 | 1.0 | 0.5 |

It is recommended that diameters less than 0.25 in conform to the standard sizes of screws under 0.25 in. as there is virtually no necessity for the selection of a diameter not included in those sizes. Furthermore, the coarse and fine thread series provide ample choice as to diameter-pitch combinations.
4.2. Preferred Pitches.-Whenever possible, the pitch should be selected from the series 40,36 , $32,28,24,20,16,12,10,8,6$, and 4 threads per inch. Intermediate pitches should be used only when absolutely necessary. Pitches coarser than 4 threads per inch are not recommended.

There are practical limits to both the largest and smallest diameters suitable for any pitch. The curves on the chart for determining minimum length of thread engagement in Appendix A5 stop at such limits.
4.3. Basic Thread Data.--Basic thread data for standard pitches are given in table 2.1. These data are to be used in conjunction with the directions for specifying special threads on drawings as given in par. 5.4, p. 3.02.

## 5. THREAD CLASSES

Thread classes are distinguished from each other by the amounts of tolerance and allowance. The function of these classes is to assure the interchangeability of threaded parts. Six distinct classes of screw threads have been established for general use. These classes are: 1A, 2A, and 3A (for external threads only) and $1 \mathrm{~B}, 2 \mathrm{~B}$, and 3 B (for internal threads only).

Class 1AR (for external threads only, 16 threads per inch and coarser) is also included for special use. Class 1AR is produced by combining the American National class 1 allowances with class 1A tolerances.

The disposition of the tolerances, allowances, and crest clearances for the six general use classes is illustrated in figures 2.5 and 2.6.

The requirements for a screw thread fit for a specific application can be met by specifying the proper combination of classes for the components. For example, an external thread made to class 2A limits can be used with an internal thread made to classes 1B, 2B, or 3B limits for specific applications.
5.1. Classes 1A, 1AR, and 1B.-The combinations of classes 1 A or 1 AR and 1 B are intended to cover the manufacture of threaded parts where quick and easy assembly is necessary, and where an allowance is required to permit ready assembly, even when the threads are slightly bruised or dirty.

Maximum diameters of class 1A (external) threads are less than basic by the amount of the same allowance as applied to class 2A. For the intended applications in American practice the allowance is not available for plating or coating. Where the thread is plated or coated, special provisions are necessary. The minimum diameters of class 1B (internal) threads, whether or not plated or coated, are basic, affording no allowance or clearance for assembly with maximum material external thread components having maximum diameters which are basic.

Allowances for all diameters and pitch diameter tolerances are specified in tables 3.2, 3.3, and 3.6. Their application is shown in figure 2.5.
5.2. Classes 2A and 2B.-Classes 2A for external threads and 2 B for internal threads are designed for general use. A moderate allowance is provided for class 2A threads.

The maximum diameters of class 2A (external) uncoated threads are less than basic by the amount of the allowance. The allowance minimizes galling and seizing in high-cycle wrench assembly, or it can be used to accommodate plated finishes or other coating. However, for threads with additive finish, the maximum diameters of class 2 A may be exceeded by the amount of the allowance; i.e., the 2 A maximum diameters apply to an unplated part or to a part before plating, whereas the basic diameters (the 2A maximum diameter plus allowance) apply to a part after plating. The minimum diameters of class 2B (internal) threads, whether or not plated or
coated, are basic, affording no allowance or clearance in assembly at maximum material limits.

Allowances for all diameters and pitch diameter tolerances are specified in tables 3.2, 3.4, and 3.7. Their application is shown in figure 2.5.
5.3. Classes 3A and 3B.-Classes 3A for external threads and 3 B for internal threads provides for applications where closeness of fit and accuracy of lead and angle of thread are important. They are obtainable consistently only by the use of high quality production equipment supported by a very efficient system of gaging and inspection. The maximum diameters of class 3A (external) threads and the minimum diameters of class 3 B (internal) threads, whether or not plated or coated, are basic, affording no allowance or clearance for assembly of maximum material components

No allowance is provided, but since the tolerances on GO gages are within the limits of size of the product, the gages will assure a slight clearance between product made to the maximum-material limits. Pitch diameter tolerances are specified in tables 3.5 and 3.8. Their application is shown in figure 2.6.
5.4. Selection of Class of Thread.-Consideration should first be given to the use of a class 2 A external thread with a class 2B internal thread since these classes are designed for general use. The use of class 2 A provides that there will always be a small clearance between maximum-material parts except when the external thread is plated. Plated parts are intended to be gaged with basic-size GO gages. In either case, it is expected that parts will assemble readily without galling or seizing. Tolerances are sufficiently large so that ordinary production methods are generally applicable.

Past experience with similar designs may indicate that a more accurately made or closer fitting thread is required than that which is permitted by classes 2A and 2B tolerances. In such cases consideration should be given to the use of classes 3A and 3B. The necessary increase in cost should not be overlooked.

In some designs there may be advantages in providing for greater average looseness of fit than that obtained with classes 2A and 2B. Such greater average looseness is provided by classes 1 A and 1 B or the assembly of class 1 A external threads with class 2B internal threads. The minimum looseness, however, is the same as for classes 2 A and 2 B except that a positive allowance is provided for plated parts. When a greater minimum looseness is requisite to provide for adverse conditions of assembly, class 1 AR is available, which is not a Unified class and is based on the American National class 1 allowance combined with class 1A tolerance. These classes also provide larger tolerances to the manufacturer, which may be of advantage if the thread is difficult to produce.

It should be noted that any class of external thread may be associated with any class of internal thread, there being no requirement to combine classes of like number.

## 6. ALLOWANCES

The allowance is minus and is applied from the basic size to below basic size. Allowance is applied only to the classes $1 \mathrm{~A}, 1 \mathrm{AR}$, and 2 A external threads. Values of the allowance for classes 1 A and 2 A are obtained by use of a $C$ factor of 0.3 in the formula shown in paragraph 7.3. Numerical values of classes 1 A and 2 A allowances for the commonly used pitches are listed in table 3.2.

The formula in paragraph 7.3 is not applicable to class 1AR as this class is produced by combining the American National class 1 allowances with class 1A tolerances. These allowances are larger than those for classes 1 A and 2 A and provide for ready assembly under adverse conditions.

Numerical values of class 1 AR allowances are:

| Threads per inch (tpi), $n$ | Class 1AR allowance |
| :---: | :---: |
|  | in |
| 16 | 0.0018 |
| 14 | .0021 |
| 12 | .0024 |
| 10 | .0038 |
| 8 | .0044 |
| 6 | .0064 |

(Class 1AR allowances apply only to external threads, 16 tpi and coarser.)

## 7. TOLERANCES

The following general specifications apply to all classes specified for applications of the Unified form of thread.
7.1. Uniform Minimum Internal Thread.The minimum major, pitch, and minor diameters of the internal thread are, respectively, the same for classes $1 \mathrm{~B}, 2 \mathrm{~B}$, and 3 B .
7.2. Direction and Scope of Tolerances.-
(a) The tolerance on the internal thread is plus, and is applied from the basic size to above basic size.
(b) The tolerance on the external thread is minus and is applied from the maximum (or design) size to below the maximum size.
(c) The tolerances specified represent the extreme variations permitted on the product.
7.3. Pitch Diameter Tolerances.-The basic formula for pitch diameter tolerance is composed of the following increments:

## P.D. Tolerance

$$
=C\left(0.0015 \sqrt[3]{D}+0.0015 \sqrt{L_{e}}+0.015 \sqrt[3]{p^{2}}\right)
$$

where

$$
\begin{aligned}
C & =\text { a factor which differs for each class } \\
D & =\text { basic major diameter } \\
L_{e} & =\text { length of engagement } \\
p & =\text { pitch. }
\end{aligned}
$$

This formula is based on the accuracy of present day threading practice, and is applicable to all reasonable combinations of diameter, pitch, and length of engagement. Numerical values of the increments in the formula for standard diameters, pitches, and lengths of engagement are given in table 2.19. The values of factor $C$ for pitch diameter tolerances are as follows:

| Class | Factor $C$ |
| :---: | :---: |
| 1A and |  |
| 1 AR | 1.500 |
| 1 B | 1.950 |
| 2 A | 1.000 |
| 2 B | 1.300 |
| 3 A | 0.750 |
| 3 B | .975 |

It will be noted that the factor $C$ is 30 percent greater for internal than for external threads of a given class number on account of the relative difficulties of manufacture.

Numerical values of pitch diameter tolerances for classes $1 \mathrm{~A}, 1 \mathrm{AR}, 1 \mathrm{~B}, 2 \mathrm{~A}, 2 \mathrm{~B}, 3 \mathrm{~A}$, and 3 B are given in tables 3.3 through 3.8. Two sets of tolerances are given: Those for 5 to 15 pitches length of engagement, based on lengths of 9 pitches, and those for 16 to 30 pitches length of engagement, which are 1.25 times the 9 -pitch values. For lengths of engagement over 30 pitches, it is recommended that pitch diameter tolerances 1.5 times the 9 -pitch values be used. If excessively small or large lengths of engagement are encountered, the thread tolerances may be calculated from the formulas, if considered advisable. Also, for threads per inch not included in the tables, tolerances should be calculated by applying the formulas.
7.4. Major Diameter Tolerances.- (a) External threads.-The tolerance on major diameter for special threads is not specified, as it must be determined in relation to the requirements of a given design in accordance with the procedure outlined in appendix A5. Preferred tolerances equal to $0.060 \sqrt[3]{p^{2}}$ for classes 2 A and 3 A , and equal to $0.090 \sqrt[3]{p^{2}}$ for classes 1 A and 1 AR are as follows:

| Threads per inch | Major diameter tolerance |  |
| :---: | :---: | :---: |
|  | Classes 1A and <br> $1 \mathrm{AR}, 0.090 \sqrt[3]{p^{2}}$ | Classes 2A and $3 \mathrm{~A}, 0.060 \sqrt[3]{p^{2}}$ |
| 80 | in | $\begin{gathered} \stackrel{i n}{0.0032} \end{gathered}$ |
| 72 |  | . 0035 |
| 64 |  | . 0038 |
| 56 |  | . 0041 |
| 48 |  | . 0045 |
| 44 |  | . 0048 |
| 40 | 0.0077 | . 0051 |
| 36 | . 0083 | . 0055 |
| 32 | . 0089 | . 0060 |
| 28 | . 0098 | . 0065 |
| 27 | . 0100 | . 0067 |
| 24 | . 0108 | . 0072 |
| 20 | . 0122 | . 0081 |
| 18 | . 0131 | . 0087 |
| 16 | . 0142 | . 0094 |
| 14 | . 0155 | . 0103 |
| 12 | . 0172 | . 0114 |
| 10 | . 0194 | . 0129 |
| 8 | . 0225 | . 0150 |
| 6 | . 0273 | . 0182 |
| 4 | . 0357 | . 0238 |

(b) Internal threads.-The tolerance on major diameter is for reference only. It is equal to $H / 6$ plus the pitch diameter tolerance of the class of thread involved. The maximum major diameter of the internal thread may be determined by adding $0.793857 p(=11 H / 12$, table 2.1) to the maximum pitch diameter of the internal thread. However, this diameter shall not result in a root flat width less than $p / 24$. In dimensioning internal threads the maximum major diameter is not specified, being established by the crest of an unworn tool. In practice, the major diameter of an internal thread is satisfactory when accepted by a gage or gaging method that represents the maximum material condition of an external thread which has no allowance.
7.5. Minor Diameter Tolerances.-(a) External threads.-The tolerance on minor diameter of external threads is for reference only. At the nominal minor diameter, that is, at the intersection of the rounded root with its center line (see fig. 2.3) it equals the pitch diameter tolerance plus $H / 12$ and applies only where the rounded root is a requirement of the design. Otherwise the tolerance shall be $H / 4$ plus the pitch diameter tolerance. The minimum minor diameter of the external thread may be determined by subtracting $0.649519 p$ ( $=0.75 H$, table 2.1) from the minimum pitch diameter of the external thread. However, this diameter shall not result in a root flat width less than $p / 8$. In dimensioning external threads the minimum minor diameter is not specified, being established by the crest of an unworn tool. In practice, the minor diameter of an external thread is satisfactory when accepted by
a gage or gaging method that represents the maxi-mum-material condition of the internal thread less the allowances, if any.
(b) Internal threads.-Formulas for the internal thread minor diameter tolerances are shown in table 2.20. Numerical values for the tolerances are shown in tables 3.9 and 3.10 . To reduce the number of minor diameter tolerances to a practical minimum, tolerances are shown in these tables for selected pitches and diameters. In these tables, the tolerances are as follows:

| Length of <br> engagement | Percent of <br> formula value | Tolerance <br> ratio |
| :--- | :---: | :---: |
|  | $50 \%$ | 0.5 |
| Less than 0.33D | $75 \%$ | 0.75 |
| From 0.33D to 0.67D | $100 \%$ | 1.0 |
| Over 0.67D to 1.5D | $125 \%$ | 1.25 |
| Over 1.5D |  |  |

When the tolerance value so computed is more than $0.394 p$, which corresponds to a resulting minimum thread height of 53 percent, the value is adjusted to equal $0.394 p$.

## 8. LENGTH OF ENGAGEMENT

The values in tables 3.9 and 3.10 for lengths of engagement from $0.67 D$ to $1.5 D$, are suitable for general applications.

Some thread applications have lengths of engagement which are greater than 1.5 diameters or less than 0.67 D. For applications having shorter or longer lengths of engagement it may be advantageous to decrease or increase the internal thread minor diameter tolerance as explained below.

The principal practical factors that govern these tolerances are tapping difficulties, particularly tap breakage in the small sizes, availability of standard drill sizes in the medium and large sizes, and depth of engagement. Depth of engagement correlates with the stripping strength of the thread assembly, and thus also with the length of engagement. It also correlates with the tendency toward disengagement of the threads on one side when assembly is eccentric. The amount of possible eccentricity is one half of the sum of the pitch diameter allowance and tolerance on both mating threads. For a given pitch or height of thread this sum increases with the diameter, and accordingly this factor would require a decrease in minor diameter tolerance with increase in diameter. However, such decrease in tolerance often is not feasible without requiring special drill sizes; therefore, to be able to use as many as possible of the available standard drill sizes listed in USA B5.12, the minor diameter tolerance for classes $1 B$ and $2 B$ of a given pitch for 0.25 in. diameter and larger is constant, in accordance with the formula:

$$
0.25 p-0.4 p^{2}
$$

There may be applications where the lengths of engagement of the mating threads or the combination of materials used for mating threads are such that the maximum tolerance may not provide the desired strength of the fastening. Experience has shown that for lengths of engagements less than $0.67 D$ (the minimum thickness of standard nuts) the minor diameter tolerance may be reduced without causing tapping difficulties.

In other applications, the length of engagement of mating threads may be long because of design considerations or the combination of materials used for mating threads. As the threads engaged increase in number, their depth of engagement may be shallower and still develop stripping strength greater than the external thread breaking strength. In these cases the maximum tolerance should be increased to reduce the possibility of tapping difficulties.

Recommended internal thread minor diameter tolerances for various lengths of engagement are shown in tables 3.9 and 3.10. Recommended hole size limits before threading for different lengths of engagement are shown in appendix A3.

## 9. LIMITS OF SIZE

With respect to the pitch diameter limits of size, it is intended, except as hereinafter qualified, that no portion of the complete thread be permitted to project beyond the envelope defined by the maxi-mum-material limits on the one hand, or beyond that defined by the minimum-material limits on the other, and thus be outside of the tolerance zone as illustrated in figures 2.5 and 2.6. The full tolerance cannot therefore, be used on pitch diameter unless deviations in other thread elements are zero.

Diameter equivalents of variations in lead, uniformity of helix, and flank angle are in the direction toward maximum material. Also included in pitchdiameter limits are other variations from size and profile, such as taper, out-of-round, and surface defects. Thus the maximum-material pitch diameter limits are a limitation of the virtual diameter (effective size) and are so specified herein for all thread classes. It is intended that diameter equivalents of deviations in any given element except pitch diameter should not exceed one-half of the pitch-diameter tolerance. Values are given in table 2.22 for deviations in lead and half-angle equivalent to one-half of pitch diameter tolerances. Flank angle equivalents should be based on a depth of thread engagement of 0.625 H .

Variations in taper and roundness of the pitch diameter, together with variations of the pitch diameter as a whole, may be in the direction of minimum material and thus the minimum-material pitch diameter limit may be specified as a limitation of the pitch diameter as a single element. However, in view of the interrelation of the pitch diameter, variations in lead and flank angle, etc., together with practical considerations relating to established production processes, product application and inspection procedures, except for class 3 A , for
fasteners and some custom threaded parts, it is customary to base acceptance at the minimummaterial condition (minimum pitch diameter of the external thread and maximum pitch diameter of the internal thread) on threaded plug and ring gaging, with gages to the thread form and length specified in section 6. See Dimensional acceptability of threads in that section.

## 10. METHOD OF DESIGNATING SPECIAL SCREW THREADS

For the method of designating threads of special diameters, pitches, and lengths of engagement, and UNS threads (threads with Unified tolerance formulations), see also section 2.
The symbol "UNS" is applicable to any thread,
(1) having the basic Unified thread form,
(2) with limits based on Unified formulations, and
(3) which is not listed in table 2.7.

Selected combinations of UNS threads are listed in table 3.1.

## 11. DIRECTIONS FOR DETERMINING LIMITS OF SIZE OF SPECIAL THREADS

The following directions are intended to simplify the task of the designer or specification writer in preparing the specification for a special thread:

The procedure to be followed in determining values for the essential thread elements (as shown in fig. 3.12) and the associated tolerances, is outlined in table 3.11. The application of this and other tables is illustrated by the following example:

Internal thread, $2.500-28 \mathrm{UNS}-2 \mathrm{~B}$
Length of engagement, 1 in .

$$
\begin{aligned}
\text { Min major diameter } & =2.5000 \text { in. } \\
\text { Min pitch diameter } & =\text { basic major diameter }- \\
& 0.75 H \text { (table } 2.1) \\
& =2.5000-0.0232= \\
& 2.4768 \\
\text { Max pitch diameter } & =\text { min pitch diameter } \\
& \text { tolerance (table } 3.7) \\
& =2.4768+0.0064= \\
& 2.4832 \\
\text { Min minor diameter } & =\text { basic major diameter }- \\
& 1.25 H \text { (table } 2.1) \\
& =2.500-0.0387=2.461 \\
\text { Max minor diameter } & =\text { min minor diameter }+ \\
& \text { tolerance (table } 3.9) \\
& =2.4613+0.0063=2.468 .
\end{aligned}
$$

The dimensions of the above internal thread may be stated on the drawing as follows:

Major diameter: 2.5000 min
Pitch diameter: $2.4768+0.0064$
$-0.0000$
Minor diameter: $2.461+0.0063$
-0.0000 .

| Threads per inch | Major diameter tolerance |  |
| :---: | :---: | :---: |
|  | Classes 1A and <br> $1 \mathrm{AR}, 0.090 \sqrt[3]{p^{2}}$ | Classes 2A and $3 \mathrm{~A}, 0.060 \sqrt[3]{p^{2}}$ |
| 80 | in | $\stackrel{i n}{0.0032}$ |
| 72 |  | . 0035 |
| 64 |  | . 0038 |
| 56 |  | . 0041 |
| 48 |  | . 0045 |
| 44 | --------- | . 0048 |
| 40 | 0.0077 | . 0051 |
| 36 | . 0083 | . 0055 |
| 32 | . 0089 | . 0060 |
| 28 | . 0098 | . 0065 |
| 27 | . 0100 | . 0067 |
| 24 | . 0108 | . 0072 |
| 20 | . 0122 | . 0081 |
| 18 | . 0131 | . 0087 |
| 16 | . 0142 | . 0094 |
| 14 | . 0155 | . 0103 |
| 12 | . 0172 | . 0114 |
| 10 | . 0194 | . 0129 |
| 8 | . 0225 | . 0150 |
| 6 | . 0273 | . 0182 |
| 4 | . 0357 | . 0238 |

(b) Internal threads.-The tolerance on major diameter is for reference only. It is equal to $H / 6$ plus the pitch diameter tolerance of the class of thread involved. The maximum major diameter of the internal thread may be determined by adding $0.793857 p(=11 H / 12$, table 2.1) to the maximum pitch diameter of the internal thread. However, this diameter shall not result in a root flat width less than $p / 24$. In dimensioning internal threads the maximum major diameter is not specified, being established by the crest of an unworn tool. In practice, the major diameter of an internal thread is satisfactory when accepted by a gage or gaging method that represents the maximum material condition of an external thread which has no allowance.
7.5. Minor Diameter Tolerances.-(a) External threads.-The tolerance on minor diameter of external threads is for reference only. At the nominal minor diameter, that is, at the intersection of the rounded root with its center line (see fig. 2.3) it equals the pitch diameter tolerance plus $H / 12$ and applies only where the rounded root is a requirement of the design. Otherwise the tolerance shall be $H / 4$ plus the pitch diameter tolerance. The minimum minor diameter of the external thread may be determined by subtracting $0.649519 p$ ( $=0.75 H$, table 2.1) from the minimum pitch diameter of the external thread. However, this diameter shall not result in a root flat width less than $p / 8$. In dimensioning external threads the minimum minor diameter is not specified, being established by the crest of an unworn tool. In practice, the minor diameter of an external thread is satisfactory when accepted by
a gage or gaging method that represents the maxi-mum-material condition of the internal thread less the allowances, if any.
(b) Internal threads.-Formulas for the internal thread minor diameter tolerances are shown in table 2.20. Numerical values for the tolerances are shown in tables 3.9 and 3.10. To reduce the number of minor diameter tolerances to a practical minimum, tolerances are shown in these tables for selected pitches and diameters. In these tables, the tolerances are as follows:

| Length of <br> engagement | Percent of <br> formula value | Tolerance <br> ratio |
| :--- | :---: | :---: |
| Less than 0.33D | $50 \%$ | 0.5 |
| From 0.33D to 0.67D_ | $75 \%$ | 0.75 |
| Over 0.67D to 1.5D | $100 \%$ | 1.0 |
| Over 1.5D | $125 \%$ | 1.25 |

When the tolerance value so computed is more than $0.394 p$, which corresponds to a resulting minimum thread height of 53 percent, the value is adjusted to equal $0.394 p$.

## 8. LENGTH OF ENGAGEMENT

The values in tables 3.9 and 3.10 for lengths of engagement from $0.67 D$ to $1.5 D$, are suitable for general applications.

Some thread applications have lengths of engagement which are greater than 1.5 diameters or less than $0.67 D$. For applications having shorter or longer lengths of engagement it may be advantageous to decrease or increase the internal thread minor diameter tolerance as explained below.

The principal practical factors that govern these tolerances are tapping difficulties, particularly tap breakage in the small sizes, availability of standard drill sizes in the medium and large sizes, and depth of engagement. Depth of engagement correlates with the stripping strength of the thread assembly, and thus also with the length of engagement. It also correlates with the tendency toward disengagement of the threads on one side when assembly is eccentric. The amount of possible eccentricity is one half of the sum of the pitch diameter allowance and tolerance on both mating threads. For a given pitch or height of thread this sum increases with the diameter, and accordingly this factor would require a decrease in minor diameter tolerance with increase in diameter. However, such decrease in tolerance often is not feasible without requiring special drill sizes; therefore, to be able to use as many as possible of the available standard drill sizes listed in USA B5.12, the minor diameter tolerance for classes 1 B and 2 B of a given pitch for 0.25 in. diameter and larger is constant, in accordance with the formula:

$$
0.25 p-0.4 p^{2}
$$

There may be applications where the lengths of engagement of the mating threads or the combination of materials used for mating threads are such that the maximum tolerance may not provide the desired strength of the fastening. Experience has shown that for lengths of engagements less than $0.67 D$ (the minimum thickness of standard nuts) the minor diameter tolerance may be reduced without causing tapping difficulties.

In other applications, the length of engagement of mating threads may be long because of design considerations or the combination of materials used for mating threads. As the threads engaged increase in number, their depth of engagement may be shallower and still develop stripping strength greater than the external thread breaking strength. In these cases the maximum tolerance should be increased to reduce the possibility of tapping difficulties.

Recommended internal thread minor diameter tolerances for various lengths of engagement are shown in tables 3.9 and 3.10. Recommended hole size limits before threading for different lengths of engagement are shown in appendix A3.

## 9. LIMITS OF SIZE

With respect to the pitch diameter limits of size, it is intended, except as hereinafter qualified, that no portion of the complete thread be permitted to project beyond the envelope defined by the maxi-mum-material limits on the one hand, or beyond that defined by the minimum-material limits on the other, and thus be outside of the tolerance zone as illustrated in figures 2.5 and 2.6. The full tolerance cannot therefore, be used on pitch diameter unless deviations in other thread elements are zero.

Diameter equivalents of variations in lead, uniformity of helix, and flank angle are in the direction toward maximum material. Also included in pitchdiameter limits are other variations from size and profile, such as taper, out-of-round, and surface defects. Thus the maximum-material pitch diameter limits are a limitation of the virtual diameter (effective size) and are so specified herein for all thread classes. It is intended that diameter equivalents of deviations in any given element except pitch diameter should not exceed one-half of the pitch-diameter tolerance. Values are given in table 2.22 for deviations in lead and half-angle equivalent to one-half of pitch diameter tolerances. Flank angle equivalents should be based on a depth of thread engagement of $0.625 H$.

Variations in taper and roundness of the pitch diameter, together with variations of the pitch diameter as a whole, may be in the direction of minimum material and thus the minimum-material pitch diameter limit may be specified as a limitation of the pitch diameter as a single element. However, in view of the interrelation of the pitch diameter, variations in lead and flank angle, etc., together with practical considerations relating to established production processes, product application and inspection procedures, except for class 3 A , for
fasteners and some custom threaded parts, it is customary to base acceptance at the minimummaterial condition (minimum pitch diameter of the external thread and maximum pitch diameter of the internal thread) on threaded plug and ring gaging, with gages to the thread form and length specified in section 6. See Dimensional acceptability of threads in that section.

## 10. METHOD OF DESIGNATING SPECIAL SCREW THREADS

For the method of designating threads of special diameters, pitches, and lengths of engagement, and UNS threads (threads with Unified tolerance formulations), see also section 2.
The symbol "UNS" is applicable to any thread,
(1) having the basic Unified thread form,
(2) with limits based on Unified formulations, and
(3) which is not listed in table 2.7.

Selected combinations of UNS threads are listed in table 3.1.

## 11. DIRECTIONS FOR DETERMINING LIMITS OF SIZE OF SPECIAL THREADS

The following directions are intended to simplify the task of the designer or specification writer in preparing the specification for a special thread:

The procedure to be followed in determining values for the essential thread elements (as shown in fig. 3.12) and the associated tolerances, is outlined in table 3.11. The application of this and other tables is illustrated by the following example:

Internal thread, $2.500-28$ UNS-2B
Length of engagement, 1 in .

$$
\begin{aligned}
\text { Min major diameter } & =2.5000 \text { in. } \\
\text { Min pitch diameter } & =\text { basic major diameter }- \\
& 0.75 H \text { (table 2.1) } \\
& =2.5000-0.0232= \\
& 2.4768 \\
\text { Max pitch diameter } & =\text { min pitch diameter } \\
& \text { tolerance (table } 3.7) \\
& =2.4768+0.0064= \\
& 2.4832 \\
\text { Min minor diameter } & =\text { basic major diameter }- \\
& 1.25 H \text { (table 2.1) } \\
& =2.500-0.0387=2.461 \\
\text { Max minor diameter } & =\text { min minor diameter } \\
& \text { tolerance (table } 3.9) \\
& =2.4613+0.0063=2.468 .
\end{aligned}
$$

The dimensions of the above internal thread may be stated on the drawing as follows:

Major diameter: 2.5000 min
Pitch diameter: $2.4768+0.0064$
$-0.0000$
Minor diameter: $2.461+0.0063$
-0.0000 .

External thread, 2.500-28UNS-2A (To mate with the above thread)
Max major diameter $=$ basic major diameter allowance (table 3.2)
$=2.5000-0.0014=2.4986$
Min major diameter $=\max$ major diameter tolerance (tabulated on p. 3.04)
$=2.4986-0.0065=2.4921$
Max pitch diameter $=\max$ major diameter $0.75 H$ (table 2.1)
$=2.4986-0.0232=2.4754$
Min pitch diameter $=$ max pitch diameter - tolerance (table 3.4)
$=2.4754-0.0049=2.4705$
Nom minor diameter $=\max$ ma; diameter $17 \mathrm{H} / 12$ ( 1.4167 H ) (table 2.1)
$=2.4986-0.0438=2.4548$.
The dimensions of the above external thread may
be stated on the drawing as follows:
Major diameter: $2.4986+0.0000$

- 0.0065

Pitch diameter: $2.4754+0.0000$

- 0.0049

Minor diameter: 2.4548, nominal.
The design of a special thread usually requires that consideration be given to various factors in order that the thread assembly will function properly. These factors are discussed in appendix A5. It is to be noted particularly that deviations from the preferred tolerances for major diameter of the external thread and for minor diameter of the internal thread may be necessary in order to arrive at the optimum design.

## 12. GAGES

The specifications for gages, including marking, as presented in section 6 apply also to gages for special threads.

Table 3.1. Selected combinations, Cnified special screw threads, l'NS

| Nominal size and threads per inch | External ${ }^{\text {a }}$ |  |  |  |  |  |  |  | Internal ${ }^{\text {a }}$ |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Class | Allowance | Major diameter |  | Pitch diameter |  |  | (c) <br> Minor diameter | Class | Minor diameter |  | Pitch diameter |  |  | Major diameter <br> Min |
|  |  |  | Max ${ }^{\text {b }}$ | Min | Max ${ }^{\text {b }}$ | Min | Tolerance |  |  | Min | Max | Min | Max | Tolerance |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| .190-28 | 2A | $\begin{aligned} & i n \\ & 0.0010 \end{aligned}$ | $\begin{gathered} i n \\ 0.1890 \end{gathered}$ | $\begin{gathered} i n \\ 0.1825 \end{gathered}$ | ${\underset{\sim}{i n}}_{0.1658}$ | $i_{i n}$ | $\begin{aligned} & \text { in } \\ & 0.0033 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & 0.1452 \end{aligned}$ | 2B | $\stackrel{i n}{0.151}$ | $\operatorname{in}_{0.160}$ | $\begin{aligned} & \text { in } \\ & 0.1668 \end{aligned}$ | $\begin{gathered} \text { in } \\ 0.1711 \end{gathered}$ | $\begin{aligned} & \text { in } \\ & 0.0043 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & 0.1900 \end{aligned}$ |
| .190-36 | 2A | . 0009 | . 1891 | . 1836 | . 1711 | . 1681 | . 0030 | . 1550 | 2B | . 160 | . 166 | . 1720 | . 1759 | . 0039 | . 1900 |
| . 190-40 | 2A | . 0009 | . 1891 | . 1840 | . 1729 | . 1700 | . 0029 | . 1584 | 2B | . 163 | . 169 | . 1738 | . 1775 | . 0037 | . 1900 |
| . 190-48 | 2A | . 0008 | . 1892 | . 1847 | . 1757 | . 1731 | . 0026 | . 1636 | 2B | . 167 | . 172 | . 1765 | . 1799 | . 0034 | . 1900 |
| .190-56 | 2A | . 0007 | . 1893 | . 1852 | . 1777 | . 1752 | . 0025 | . 1674 | 2B | . 171 | . 175 | . 1784 | . 1816 | . 0032 | . 1900 |
| .216-36 | 2A | . 0009 | . 2151 | . 2096 | . 1971 | . 1941 | . 0030 | . 1810 | 2B | . 186 | . 192 | . 1980 | . 2019 | . 0039 | . 2160 |
| .216-40 | 2A | . 0009 | . 2151 | . 2100 | . 1989 | . 1960 | . 0029 | . 1844 | 2B | . 189 | . 195 | . 1998 | . 2035 | . 0037 | . 2160 |
| .216-48 | 2A | . 0008 | . 2152 | . 2107 | . 2017 | . 1991 | . 0026 | . 1896 | 2 B | . 193 | . 198 | . 2025 | . 2059 | . 0034 | . 2160 |
| .216-56 | 2A | . 0007 | . 2153 | . 2112 | . 2037 | . 2012 | . 0025 | . 1934 | 2B | . 197 | . 201 | . 2044 | . 2076 | . 0032 | . 2160 |
| .250-24 | 2A | . 0011 | . 2489 | . 2417 | . 2218 | . 2181 | . 0037 | . 1978 | 2B | . 205 | . 215 | . 2229 | . 2277 | . 0048 | . 2500 |
| .250-27 | 2A | . 0010 | . 2490 | . 2423 | . 2249 | . 2214 | . 0035 | . 2036 | 2B | . 210 | . 219 | . 2259 | . 2304 | . 0045 | . 2500 |
| . 250-36 | 2A | . 0009 | . 2491 | . 2436 | . 2311 | . 2280 | . 0031 | . 2150 | 2B | . 220 | . 226 | . 2320 | . 2360 | . 0040 | . 2500 |
| . $250-40$ | 2A | . 0009 | . 2491 | . 2440 | . 2329 | . 2300 | . 0029 | . 2184 | 2B | . 223 | . 229 | . 2338 | . 2376 | . 0038 | . 2500 |
| .250-48 | 2A | . 0008 | . 2492 | . 2447 | . 2357 | . 2330 | . 0027 | . 2236 | 2B | . 227 | . 232 | . 2365 | . 2401 | . 0036 | . 2500 |
| .250-56 | 2A | . 0008 | . 2492 | . 2451 | . 2376 | . 2350 | . 0026 | . 2273 | 2B | . 231 | . 235 | . 2384 | . 2417 | . 0033 | . 2500 |
| . $3125-27$ | 2A | . 0010 | . 3115 | . 3048 | . 2874 | . 2839 | . 0035 | . 2661 | 2B | . 272 | . 281 | . 2884 | . 2929 | . 0045 | . 3125 |
| . $3125-36$ | 2A | . 0009 | . 3116 | . 3061 | . 2936 | . 2905 | . 0031 | . 2775 | 2B | . 282 | . 289 | . 2945 | . 2985 | . 0040 | . 3125 |
| . $3125-40$ | 2A | . 0009 | . 3116 | . 3065 | . 2954 | . 2925 | . 0029 | . 2809 | 2B | . 285 | . 291 | . 2963 | . 3001 | . 0038 | . 3125 |
| . $3125-48$ | 2A | . 0008 | . 3117 | . 3072 | . 2982 | . 2955 | . 0027 | . 2861 | 2B | . 290 | . 295 | . 2990 | . 3026 | . 0036 | . 3125 |
| . $375-18$ | 2A | . 0013 | . 3737 | . 3650 | . 3376 | . 3333 | . 0043 | . 3055 | 2 B | . 315 | . 328 | . 3389 | . 3445 | . 0056 | . 3750 |
| . $375-27$ | 2A | . 0011 | . 3739 | . 3672 | . 3498 | . 3462 | . 0036 | . 3285 | 2B | . 335 | . 344 | . 3509 | . 3556 | . 0047 | . 3750 |
| . $375-36$ | 2A | . 0010 | . 3740 | . 3685 | . 3560 | . 3528 | . 0032 | . 3399 | 2B | . 345 | . 352 | . 3570 | . 3612 | . 0042 | . 3750 |
| . $375-40$ | 2A | . 0009 | . 3741 | . 3690 | . 3579 | . 3548 | . 0031 | . 3434 | 2 B | . 348 | . 354 | . 3588 | . 3628 | . 0040 | . 3750 |
| . $390-27$ | 2A | . 0011 | . 3889 | . 3822 | . 3648 | . 3612 | . 0036 | . 3435 | 2B | . 350 | . 359 | . 3659 | . 3706 | . 0047 | . 3900 |
| .4375-18 | 2 A | . 0013 | . 4362 | . 4275 | . 4001 | . 3958 | . 0043 | . 3680 | 2B | . 377 | . 390 | . 4014 | . 4070 | . 0056 | . 4375 |
| .4375-24 | 2 A | . 0011 | . 4364 | . 4292 | . 4093 | . 4055 | . 0038 | . 3853 | 2B | . 392 | . 402 | . 4104 | . 4153 | . 0049 | . 4375 |
| .4375-27 | 2 A | . 0011 | . 4364 | . 4297 | . 4123 | . 4087 | . 0036 | . 3910 | 2B | . 397 | . 406 | . 4134 | . 4181 | . 0047 | . 4375 |
| . $4375-36$ | 2 A | . 0011 | . 4365 | . 4310 | . 4185 | . 4153 | . 0032 | . 4024 | 2B | . 407 | . 414 | . 4195 | . 4237 | . 0042 | . 4375 |
| .4375-40 | 2A | . 0009 | . 4366 | . 4315 | . 4204 | . 4173 | . 0031 | . 4059 | 2B | . 410 | . 416 | . 4213 | . 4253 | . 0040 | . 4375 |
| . $500-12$ | 2A | $\begin{aligned} & .0016 \\ & .0000 \end{aligned}$ | $\begin{aligned} & .4984 \\ & .5000 \end{aligned}$ | $\begin{array}{r} .4870 \\ .4886 \end{array}$ | $\begin{array}{r} .4443 \\ .4459 \end{array}$ | $\begin{array}{r} .4389 \\ .4419 \end{array}$ | . 0054 | .3962 .3978 | ${ }_{3}^{2 B}$ | $\begin{aligned} & .410 \\ & .4100 \end{aligned}$ | $\begin{aligned} & .428 \\ & .4223 \end{aligned}$ | $\begin{array}{r} .4459 \\ .4459 \end{array}$ | .4529 .4511 | .0070 .0052 | $\begin{aligned} & .5000 \\ & .5000 \end{aligned}$ |
| . $500-14$ | 2 A | . 0015 | . 4985 | . 4882 | . 4521 | . 4471 | . 0050 | .4109 | 2B | . 423 | . 438 | . 4536 | . 4601 | . 0065 | . 5000 |
| .500-18 | 2A | . 0013 | . 4987 | . 4900 | . 4626 | . 4582 | . 0044 | . 4305 | 2B | . 440 | . 453 | . 4639 | . 4697 | . 0058 | . 5000 |
| .500-24 | 2A | . 0012 | . 4988 | . 4916 | . 4717 | . 4678 | . 0039 | . 4477 | 2B | . 455 | . 465 | . 4729 | . 4780 | . 0051 | . 5000 |
| . $500-27$ | 2 A | . 0011 | . 4989 | . 4922 | . 4748 | . 4711 | . 0037 | . 4535 | 2B | . 460 | . 469 | . 4759 | . 4807 | . 0048 | . 5000 |
| .500-36 | 2A | . 0010 | . 4990 | . 4935 | . 4810 | . 4777 | . 0033 | . 4649 | 2B | . 470 | . 476 | . 4820 | . 4863 | . 0043 | . 5000 |
| . $500-40$ | 2A | . 0010 | . 4990 | . 4939 | . 4828 | . 4796 | . 0032 | . 4683 | 2B | . 473 | . 479 | . 4838 | . 4879 | . 0041 | . 5000 |
| .5625-14 | 2A | . 0015 | . 5610 | . 5507 | . 5146 | . 5096 | . 0050 | . 4734 | 2B | . 485 | . 501 | . 5161 | . 5226 | . 0065 | . 5625 |
| .5625-27 | 2 A | . 0011 | . 5614 | . 5547 | . 5373 | . 5336 | . 0037 | . 5160 | 2B | . 522 | . 531 | . 5384 | . 5432 | . 0048 | . 5625 |
| .5625-36 | 2 A | . 0010 | . 5615 | . 5560 | . 5435 | . 5402 | . 0033 | . 5274 | 2 B | . 532 | . 539 | . 5445 | . 5488 | . 0043 | . 5625 |
| . $5625-40$ | 2 A | . 0010 | . 5615 | . 5564 | . 5453 | . 5421 | . 0032 | . 5308 | 2B | . 535 | . 541 | . 5463 | . 5504 | . 0041 | . 5625 |
| . $625-14$ | 2A | . 0015 | . 6235 | . 6132 | . 5771 | . 5720 | . 0051 | . 5359 | 2B | . 548 | . 564 | . 5786 | . 5852 | . 0066 | . 6250 |

[^11]Table 3.1. Selected combinations, Unified special screw thrcads, $l N S$-Continued

| Nominal size and threads per inch | Externala |  |  |  |  |  |  |  | Internala |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Class | Allowance | Major diameter |  | Pitch diameter |  |  | (c) Minor diameter | Class | Minor diameter |  | Pitch diameter |  |  | Major diameter <br> Min |
|  |  |  | Max ${ }^{\text {b }}$ | Min | Max ${ }^{\text {b }}$ | Min | Tolerance |  |  | Min | Max | Min | Max | Tolerance |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| . $625-27$ | 2A | $\begin{aligned} & \text { in } \\ & .0011 \end{aligned}$ | $\begin{aligned} & i n \\ & .6239 \end{aligned}$ | $\begin{aligned} & i n \\ & .6172 \end{aligned}$ | $\begin{aligned} & i n \\ & .5998 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & .5960 \end{aligned}$ | in <br> . 0038 | in . 5785 | 2B | $\begin{gathered} i n \\ .585 \end{gathered}$ | $\begin{aligned} & i n \\ & .594 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & .6009 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & .6059 \end{aligned}$ | $\begin{aligned} & i n \\ & .0050 \end{aligned}$ | ${ }^{i n} .6250$ |
| . $625-36$ | 2A | . 0010 | . 6240 | . 6185 | . 6060 | . 6026 | . 0034 | . 5899 | 2B | . 595 | . 602 | . 6070 | . 6114 | . 0044 | . 6250 |
| . $625-40$ | 2A | . 0010 | . 6240 | . 6189 | . 6078 | . 6045 | . 0033 | . 5933 | 2B | . 598 | . 604 | . 6088 | . 6131 | . 0043 | . 6250 |
| .750-14 | 2 A | . 0015 | . 7485 | . 7382 | . 7021 | . 6970 | . 0051 | . 6609 | 2 B | . 673 | . 688 | . 7036 | . 7103 | . 0067 | . 7500 |
| .750-18 | 2 A | . 0014 | . 7486 | . 7399 | . 7125 | . 7079 | . 0046 | . 6804 | 2 B | . 690 | . 703 | . 7139 | . 7199 | . 0060 | . 7500 |
| .750-24 | 2 A | . 0012 | . 7488 | . 7416 | . 7217 | . 7176 | . 0041 | . 6977 | 213 | . 705 | . 715 | . 7229 | . 7282 | . 0053 | . 7500 |
| .750-27 | 2 A | . 0012 | . 7488 | . 7421 | . 7247 | . 7208 | . 0039 | . 7034 | 2B | . 710 | . 719 | . 7259 | . 7310 | . 0051 | . 7500 |
| .750-36 | 2 A | . 0010 | . 7490 | . 7435 | . 7310 | . 7275 | . 0035 | . 7149 | 2B | . 720 | . 726 | . 7320 | . 7365 | . 0045 | . 7500 |
| .750-40 | 2 A | . 0010 | . 7490 | . 7439 | . 7328 | . 7294 | . 0034 | . 7183 | 2B | . 723 | . 729 | . 7338 | . 7382 | . 0044 | . 7500 |
| .875-10 | 2 A | . 0018 | . 8732 | . 8603 | . 8082 | . 8022 | . 0060 | . 7505 | 2B | . 767 | . 788 | . 8100 | . 8178 | . 0078 | . 8750 |
| .875-18 | 2 A | . 0014 | . 8736 | . 8649 | . 8375 | . 8329 | . 0046 | . 8054 | 2B | . 815 | . 828 | . 8389 | . 8449 | . 0060 | . 8750 |
| .875-24 | 2 A | . 0012 | . 8738 | . 8666 | . 8467 | . 8426 | . 0041 | . 8227 | 2B | . 830 | . 840 | . 8479 | . 8532 | . 0053 | . 8750 |
| .875-27 | 2 A | . 0012 | . 8738 | . 8671 | . 8197 | . 8458 | . 0039 | . 8284 | 2B | . 835 | . 844 | . 8509 | . 8560 | . 0051 | . 8750 |
| .875-36 | 2 A | . 0010 | . 8740 | . 8685 | . 8560 | . 8525 | . 0035 | . 8399 | 2B | . 845 | . 852 | . 8570 | . 8615 | . 0045 | . 8750 |
| . 875-40 | 2 A | . 0010 | . 8740 | . 8689 | . 8578 | . 8544 | . 0034 | . 8433 | 2B | . 848 | . 854 | . 8588 | . 8632 | . 0044 | . 8750 |
| 1.000-10 | 2A | . 0018 | . 9982 | . 9853 | . 9332 | . 9270 | . 0062 | . 8755 | 2B | . 892 | . 913 | . 9350 | . 9430 | . 0080 | 1.0000 |
| $1.000-14^{\text {d }}$ | 1 A | . 0017 | . 9983 | .9828 .9880 | .9519 .9519 | .9435 .9463 | . 0084 | .9107 <br> .9107 | ${ }_{1}^{1 B}$ | .923 .923 | .938 .938 | .9536 .9536 | . 9645 | .0109 .0073 | 1.0000 1.0000 |
|  | 3 A | . 0000 | 1.0000 | . 9897 | . 9536 | . 9494 | . 0042 | . 9124 | 3B | . 9230 | . 9315 | . 9536 | . 9590 | . 0054 | 1.0000 |
| 1.000-18 | 2 A | . 0014 | . 9986 | . 9899 | . 9625 | . 9578 | . 0047 | . 9304 | 2B | . 940 | . 953 | . 9639 | . 9701 | . 0062 | 1.0000 |
| 1.000-24 | 2 A | . 0013 | . 9987 | . 9915 | . 9716 | . 9674 | . 0042 | . 9476 | 2B | . 955 | . 965 | . 9729 | . 9784 | . 0055 | 1.0000 |
| 1.000-27 | 2 A | . 0012 | . 9988 | . 9921 | . 9747 | . 9707 | . 0040 | . 9534 | 2B | . 960 | . 969 | . 9759 | . 9811 | . 0052 | 1.0000 |
| 1.000-36 | 2 A | . 0011 | . 9989 | . 9934 | . 9809 | . 9773 | . 0036 | . 9648 | 2B | . 970 | . 976 | . 9820 | . 9867 | . 0047 | 1.0000 |
| 1.000-40 | 2 A | . 0010 | . 9990 | . 9939 | . 9828 | . 9793 | . 0035 | . 9683 | 2B | . 973 | . 979 | . 9838 | . 9883 | . 0045 | 1.0000 |
| 1.125-10 | 2 A | . 0018 | 1.1232 | 1.1103 | 1.0582 | 1.0520 | . 0062 | 1.0005 | 2B | 1.017 | 1.038 | 1.0600 | 1.0680 | . 0080 | 1.1250 |
| 1.125-14 | 2 A | . 0016 | 1.1234 | 1.1131 | 1.0770 | 1.0717 | . 0053 | 1.0358 | 2B | 1.048 | 1.064 | 1.0786 | 1.0855 | . 0069 | 1.1250 |
| 1.125-24 | 2 A | . 0013 | 1.1237 | 1.1165 | 1.0966 | 1.0924 | . 0042 | 1.0726 | 2B | 1.080 | 1.090 | 1.0979 | 1.1034 | . 0055 | 1.1250 |
| 1.250-10 | 2 A | . 0019 | 1.2481 | 1.2352 | 1.1831 | 1.1768 | . 0063 | 1.1254 | 2 B | 1.142 | 1.163 | 1.1850 | 1.1932 | . 0082 | 1.2500 |
| 1.250-14 | 2 A | . 0016 | 1.2484 | 1.2381 | 1.2020 | 1.1966 | . 0054 | 1.1608 | 2B | 1.173 | 1.188 | 1.2036 | 1.2106 | . 0070 | 1.2500 |
| 1.250-24 | 2 A | . 0013 | 1.2487 | 1.2415 | 1.2216 | 1.2173 | . 0043 | 1.1976 | 2B | 1.205 | 1.215 | 1.2229 | 1.2285 | . 0056 | 1.2500 |
| 1.375-10 | 2 A | . 0019 | 1.3731 | 1.3602 | 1.3081 | 1.3018 | . 0063 | 1.2504 | 2B | 1.267 | 1.288 | 1.3100 | 1.3182 | . 0082 | 1.3750 |
| 1.375-14 | 2 A | . 0016 | 1.3734 | 1.3631 | 1.3270 | 1.3216 | . 0054 | 1.2858 | 2 B | 1.298 | 1.314 | 1.3286 | 1.3356 | . 0070 | 1.3750 |
| 1.375-24 | 2A | . 0013 | 1.3737 | 1.3665 | 1.3466 | 1.3423 | . 0043 | 1.3226 | 2B | 1.330 | 1.340 | 1.3479 | 1.3535 | . 0056 | 1.3750 |
| 1.500-10 | 2 A | . 0019 | 1.4981 | 1.4852 | 1.4331 | 1.4267 | . 0064 | 1.3754 | 2B | 1.392 | 1.413 | 1.4350 | 1.4433 | . 0083 | 1.5000 |
| 1.500-14 | 2A | . 0017 | 1.4983 | 1.4880 | 1.4519 | 1.4464 | . 0055 | 1.4107 | 2B | 1.423 | 1.438 | 1.4536 | 1.4608 | . 0072 | 1.5000 |
| 1.500-24 | 2 A | . 0013 | 1.4987 | 1.4915 | 1.4716 | 1.4672 | . 0044 | 1.4476 | 2B | 1.455 | 1.465 | 1.4729 | 1.4787 | . 0058 | 1.5000 |
| 1.625-10 | 2 A | . 0019 | 1.6231 | 1.6102 | 1.5581 | 1.5517 | . 0064 | 1.5004 | 2B | 1.517 | 1.538 | 1.5600 | 1.5683 | . 0083 | 1.6250 |
| 1.625-14 | 2 A | . 0017 | 1.6233 | 1.6130 | 1.5769 | 1.5714 | . 0055 | 1.5357 | 2B | 1.548 | 1.564 | 1.5786 | 1.5858 | . 0072 | 1.6250 |
| 1.625-24 | 2 A | . 0013 | 1.6237 | 1.6165 | 1.5966 | 1.5922 | . 0044 | 1.5726 | 2B | 1.580 | 1.590 | 1.5979 | 1.6037 | . 0058 | 1.6250 |
| 1.750-10 | 2 A | . 0019 | 1.7481 | 1.7352 | 1.6831 | 1.6766 | . 0065 | 1.6254 | 2 B | 1.642 | 1.663 | 1.6850 | 1.6934 | . 0084 | 1.7500 |
| 1.750-14 | 2A | . 0017 | 1.7483 | 1.7380 | 1.7019 | 1.6963 | . 0056 | 1.6607 | 2 B | 1.673 | 1.688 | 1.7036 | 1.7109 | . 0073 | 1.7500 |

Sce footnotes at end of table.

Table 3.1. Selected combinations, Unified special screw threads, UNS-Continued

| Nominal size and threads per inch | External ${ }^{\text {a }}$ |  |  |  |  |  |  |  | Internal: |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Class | Allowance | Major diameter |  | Pitch diameter |  |  | (c) <br> Minor diameter | Class | Minor diameter |  | Pitch diameter |  |  | Major diameter <br> Min |
|  |  |  | Max ${ }^{\text {b }}$ | Min | Max ${ }^{\text {b }}$ | Min | Tolerance |  |  | Min | Max | Min | Max | Tolerance |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| 1.750-18 | 2A | $\begin{aligned} & \text { in } \\ & .0015 \end{aligned}$ | $\operatorname{in}_{1.7485}$ | $\stackrel{i n}{1.7398}$ | $\stackrel{i n}{1.7124}$ | $\stackrel{i n}{1.7073}$ | $\begin{aligned} & i n \\ & .0051 \end{aligned}$ | $\stackrel{i n}{1 n}_{1.6803}$ | 2 B | ${ }_{1.690}^{i n}$ | $\stackrel{i n}{1.703}$ | $\stackrel{i n}{1.7139}$ | $\stackrel{i n}{1.7205}$ | in | 1.7500 |
| 1.875-10 | 2 A | . 0019 | 1.8731 | 1.8602 | 1.8081 | 1.8016 | . 0065 | 1.7504 | 2 B | 1.767 | 1.788 | 1.8100 | 1.8184 | . 0084 | 1.8750 |
| 1.875-14 | 2A | . 0017 | 1.8733 | 1.8630 | 1.8269 | 1.8213 | . 0056 | 1.7857 | 2B | 1.798 | 1.814 | 1.8286 | 1.8359 | . 0073 | 1.8750 |
| 1.875-18 | 2 A | . 0015 | 1.8735 | 1.8648 | 1.8374 | 1.8323 | . 0051 | 1.8053 | 2B | 1.815 | 1.828 | 1.8389 | 1.8455 | . 0066 | $\begin{aligned} & 1.8750 \\ & 2.0000 \end{aligned}$ |
| 2.000-10 | 2 A | . 0020 | 1.9980 | 1.9851 | 1.9330 | 1.9265 | . 0065 | 1.8753 | 2B | 1.892 | 1.913 | 1.9350 | 1.9435 | . 0085 |  |
| 2.000-14 | 2 A | . 0017 | 1.9983 | 1.9880 | 1.9519 | 1.9462 | . 0057 | 1.9107 | 2B | 1.923 | 1.938 | 1.9536 | 1.9610 | . 0074 | 2.0000 |
| 2.000-18 | 2 A | . 0015 | 1.9985 | 1.9898 | 1.9624 | 1.9573 | . 0051 | 1.9303 | 2B | 1.940 | 1.953 | 1.9639 | 1.9706 | . 0067 | 2.0000 |
| 2.0625-16 | 2 A | $\begin{aligned} & .0016 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.0609 \\ & 2.0625 \end{aligned}$ | $\begin{aligned} & 2.0515 \\ & 2.0531 \end{aligned}$ | $\begin{aligned} & 2.0203 \\ & 2.0219 \end{aligned}$ | $\begin{array}{r} 2.0149 \\ 2.0179 \end{array}$ | . 0040 | 1.9842 | 2 B | 1.995 | 2.009 | 2.0219 | 2.0289 | . 0070 | 2.0625 |
|  |  |  |  |  |  |  |  | 1.9858 | 3 B | 1.9950 | 2.0033 | 2.0219 | 2.0271 | . 0052 | 2.0625 |
| 2.1875-16 | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & .0016 \\ & .0000 \end{aligned}$ | $\begin{aligned} & 2.1859 \\ & 2.1875 \end{aligned}$ | $\begin{aligned} & 2.1765 \\ & 2.1781 \end{aligned}$ | $\begin{aligned} & 2.1453 \\ & 2.1469 \end{aligned}$ | $\begin{aligned} & 2.1399 \\ & 2.1428 \end{aligned}$ | $\begin{aligned} & .0054 \\ & .0041 \end{aligned}$ | $\begin{aligned} & 2.1092 \\ & 2.1108 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 2.120 \\ & 2.1200 \end{aligned}$ | $\begin{aligned} & 2.134 \\ & 2.1283 \end{aligned}$ | $\begin{aligned} & 2.1469 \\ & 2.1469 \end{aligned}$ | $\begin{aligned} & 2.1539 \\ & 2.1521 \end{aligned}$ | $\begin{aligned} & .0070 \\ & .0052 \end{aligned}$ | $\begin{aligned} & 2.1875 \\ & 2.1875 \end{aligned}$ |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2.250-10 | 2A | . 0020 | 2.2480 | 2.2351 | 2.1830 | 2.1765 | . 0065 | 2.1253 | 2B | 2.142 | 2.163 | 2.1850 | 2.1935 | . 0085 | 2.2500 |
| 2.250-14 | 2 A | . 0017 | 2.2483 | 2.2380 | 2.2019 | 2.1962 | . 0057 | 2.1607 | 2B | 2.173 | 2.188 | 2.2036 | 2.2110 | . 0074 | 2.2500 |
| 2.250-18 | 2A | . 0015 | 2.2485 | 2.2398 | 2.2124 | 2.2073 | . 0051 | 2.1803 | 2B | 2.190 | 2.203 | 2.2139 | 2.2206 | . 0067 | 2.2500 |
| 2.3125-16 | 2 A | . 0017 | 2.3108 | 2.3014 | 2.2702 | 2.2647 | . 0055 | 2.2341 | 2 B | 2.245 | 2.259 | 2.2719 | 2.2791 | . 0072 | 2.3125 |
|  | 3A | . 0000 | 2.3125 | 2.3031 | 2.2719 | 2.2678 | . 0041 | 2.2358 | 3B | 2.2450 | 2.2533 | 2.2719 | 2.2773 | . 0054 | 2.3125 |
| 2.4375-16 | 2 A | . 0017 | 2.4358 | 2.4264 | 2.3952 | 2.3897 | . 0055 | 2.3591 | 2 B | 2.370 | 2.384 | 2.3969 | 2.4041 | . 0072 | 2.4375 |
|  | 3A | . 0000 | 2.4375 | 2.4281 | 2.3969 | 2.3928 | . 0041 | 2.3608 | 3B | 2.3700 | 2.3783 | 2.3969 | 2.4023 | . 0054 | 2.4375 |
| 2.500-10 | 2 A | . 0020 | 2.4980 | 2.4851 | 2.4330 | 2.4263 | . 0067 | 2.3753 | 2B | 2.392 | 2.413 | 2.4350 | 2.4437 | . 0087 | 2.5000 |
| 2.500-14 | 2 A | . 0017 | 2.4983 | 2.4880 | 2.4519 | 2.4461 | . 0058 | 2.4107 | 2B | 2.423 | 2.438 | 2.4536 | 2.4612 | . 0076 | 2.5000 |
| 2.500-18 | 2A | . 0016 | 2.4984 | 2.4897 | 2.4623 | 2.4570 | . 0053 | 2.4302 | 2B | 2.440 | 2.453 | 2.4639 | 2.4708 | . 0069 | 2.5000 |
| 2.750-10 | 2A | . 0020 | 2.7480 | 2.7351 | 2.6830 | 2.6763 | . 0067 | 2.6253 | 2B | 2.642 | 2.663 | 2.6850 | 2.6937 | . 0087 | 2.7500 |
| 2.750-14 | 2A | . 0017 | 2.7483 | 2.7380 | 2.7019 | 2.6961 | . 0058 | 2.6607 | 2B | 2.673 | 2.688 | 2.7036 | 2.7112 | . 0076 | 2.7500 |
| 2.750-18 | 2 A | . 0016 | 2.7484 | 2.7397 | 2.7123 | 2.7070 | . 0053 | 2.6802 | 2B | 2.690 | 2.703 | 2.7139 | 2.7208 | . 0069 | 2.7500 |
| 3.000-10 | 2 A | . 0020 | 2.9980 | 2.9851 | 2.9330 | 2.9262 | . 0068 | 2.8753 | 2B | 2.892 | 2.913 | 2.9350 | 2.9439 | . 0089 | 3.0000 |
| 3.000-14 | 2 A | . 0018 | 2.9982 | 2.9879 | 2.9518 | 2.9459 | . 0059 | 2.9106 | 2B | 2.923 | 2.938 | 2.9536 | 2.9613 | . 0077 | 3.0000 |
| 3.000-18 | 2 A | . 0016 | 2.9984 | 2.9897 | 2.9623 | 2.9569 | . 0054 | 2.9302 | 2 B | 2.940 | 2.953 | 2.9639 | 2.9709 | . 0070 | 3.0000 |
| 3.250-10 | 2A | . 0020 | 3.2480 | 3.2351 | 3.1830 | 3.1762 | . 0068 | 3.1253 | 2B | 3.142 | 3.163 | 3.1850 | 3.1939 | . 0089 | 3.2500 |
| 3.250-14 | 2 A | . 0018 | 3.2482 | 3.2379 | 3.2018 | 3.1959 | . 0059 | 3.1606 | 2B | 3.173 | 3.188 | 3.2036 | 3.2113 | . 0077 | 3.2500 |
| 3.250-18 | 2A | . 0016 | 3.2484 | 3.2397 | 3.2123 | 3.2069 | . 0054 | 3.1802 | 2B | 3.190 | 3.203 | 3.2139 | 3.2209 | . 0070 | 3.2500 |
| 3.500-10 | 2A | . 0021 | 3.4979 | 3.4850 | 3.4329 | 3.4260 | . 0069 | 3.3752 | 2B | 3.392 | 3.413 | 3.4350 | 3.4440 | . 0090 | 3.5000 |
| 3.500-14 | 2A | . 0018 | 3.4982 | 3.4879 | 3.4518 | 3.4457 | . 0061 | 3.4106 | 2B | 3.423 | 3.438 | 3.4536 | 3.4615 | . 0079 | 3.5000 |
| 3.500-18 | 2A | . 0017 | 3.4983 | 3.4896 | 3.4622 | 3.4567 | . 0055 | 3.4301 | 2B | 3.440 | 3.453 | 3.4639 | 3.4711 | . 0072 | 3.5000 |
| 3.750-10 | 2 A | . 0021 | 3.7479 | 3.7350 | 3.6829 | 3.6760 | . 0069 | 3.6252 | 2B | 3.642 | 3.663 | 3.6850 | 3.6940 | . 0090 | 3.7500 |
| 3.750-14 | 2A | . 0018 | 3.7482 | 3.7379 | 3.7018 | 3.6957 | . 0061 | 3.6606 | 2B | 3.673 | 3.688 | 3.7036 | 3.7115 | . 0079 | 3.7500 |
| 3.750-18 | 2A | . 0017 | 3.7483 | 3.7396 | 3.7122 | 3.7067 | . 0055 | 3.6801 | 2B | 3.690 | 3.703 | 3.7139 | 3.7211 | . 0072 | 3.7500 |
| 4.000-10 | 2 A | . 0021 | 3.9979 | 3.9850 | 3.9329 | 3.9259 | . 0070 | 3.8752 | 2B | 3.892 | 3.913 | 3.9350 | 3.9441 | . 0091 | 4.0000 |
| 4.000-14 | 2A | . 0018 | 3.9982 | 3.9879 | 3.9518 | 3.9456 | . 0062 | 3.9106 | 2B | 3.923 | 3.938 | 3.9536 | 3.9616 | . 0080 | 4.0000 |
| 4.250-10 | 2A | . 0021 | 4.2479 | 4.2350 | 4.1829 | 4.1759 | . 0070 | 4.1252 | 2B | 4.142 | 4.163 | 4.1850 | 4.1941 | . 0091 | 4.2500 |
| 4.250-14 | 2A | . 0018 | 4.2482 | 4.2379 | 4.2018 | 4.1956 | . 0062 | 4.1606 | 2B | 4.173 | 4.188 | 4.2036 | 4.2116 | . 0080 | 4.2500 |
| 4.500-10 | 2A | . 0021 | 4.4979 | 4.4850 | 4.4329 | 4.4259 | . 0070 | 4.3752 | 2B | 4.392 | 4.413 | 4.4350 | 4.4441 | . 0091 | 4.5000 |

See footnotes at end of table.

Table 3.1. Selected combinations, Unified special screw threads, UNS-Continued

| Nominal size and threads per inch | External ${ }^{\text {a }}$ |  |  |  |  |  |  |  | Internala |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Class | Allowance | Major diameter |  | Pitch diameter |  |  | (c) <br> Minor diameter | Class | Minor diameter |  | Pitch diameter |  |  | $\frac{$ Major  <br>  diameter }{ Min } |
|  |  |  | Max ${ }^{\text {b }}$ | Min | Max ${ }^{\text {b }}$ | Min | Tolerance |  |  | Min | Max | Min | Max | Tolerance |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
| 4.500-14 | 2A | in . 0018 | $\operatorname{in}_{4.4982}$ | $\operatorname{in}_{4.4879}$ | $\operatorname{in}_{4.4518}$ | $\stackrel{i n}{4.4456}$ | in . 0062 | $\operatorname{in}_{4.4106}$ | 2B | $\operatorname{in}_{4.423}$ | $\stackrel{i n}{4.438}$ | $\operatorname{in}_{4.4536}$ | ${ }_{4.4616}$ | $\begin{aligned} & \text { in } \\ & .0080 \end{aligned}$ | $\begin{aligned} & i n \\ & 4.5000 \end{aligned}$ |
| 4.750-10 | 2 A | . 0022 | 4.7478 | 4.7349 | 4.6828 | 4.6756 | . 0072 | 4.6251 | 2B | 4.642 | 4.663 | 4.6850 | 4.6944 | . 0094 | 4.7500 |
| 4.750-14 | 2 A | . 0019 | 4.7481 | 4.7378 | 4.7017 | 4.6953 | . 0064 | 4.6605 | 2B | 4.673 | 4.688 | 4.7036 | 4.7119 | . 0083 | 4.7500 |
| 5.000-10 | 2 A | . 0022 | 4.9978 | 4.9849 | 4.9328 | 4.9256 | . 0072 | 4.8751 | 2B | 4.892 | 4.913 | 4.9350 | 4.9444 | . 0094 | 5.0000 |
| 5.000-14 | 2A | . 0019 | 4.9981 | 4.9878 | 4.9517 | 4.9453 | . 0064 | 4.9105 | 2B | 4.923 | 4.938 | 4.9536 | 4.9619 | . 0083 | 5.0000 |
| 5.250-10 | 2A | . 0022 | 5.2478 | 5.2349 | 5.1828 | 5.1756 | . 0072 | 5.1251 | 2 B | 5.142 | 5.163 | 5.1850 | 5.1944 | . 0094 | 5.2500 |
| 5.250-14 | 2 A | . 0019 | 5.2481 | 5.2378 | 5.2017 | 5.1953 | . 0064 | 5.1605 | 2B | 5.173 | 5.188 | 5.2036 | 5.2119 | . 0083 | 5.2500 |
| 5.500-10 | 2 A | . 0022 | 5.4978 | 5.4849 | 5.4328 | 5.4256 | . 0072 | 5.3751 | 2B | 5.392 | 5.413 | 5.4350 | 5.4444 | . 0094 | 5.5000 |
| 5.500-14 | 2A | . 0019 | 5.4981 | 5.4878 | 5.4517 | 5.4453 | . 0064 | 5.4105 | 2 B | 5.423 | 5.438 | 5.4536 | 5.4619 | . 0083 | 5.5000 |
| 5.750-10 | 2 A | . 0022 | 5.7478 | 5.7349 | 5.6828 | 5.6754 | . 0074 | 5.6251 | 2B | 5.642 | 5.663 | 5.6850 | 5.6946 | . 0096 | 5.7500 |
| 5.750-14 | 2A | . 0020 | 5.7480 | 5.7377 | 5.7016 | 5.6951 | . 0065 | 5.6604 | 2B | 5.673 | 5.688 | 5.7036 | 5.7121 | . 0085 | 5.7500 |
| 6.000-10 | 2 A | . 0022 | 5.9978 | 5.9849 | 5.9328 | 5.9254 | . 0074 | 5.8751 | 2B | 5.392 | 5.913 | 5.9350 | 5.9446 | . 0696 | 6.0000 |
| 6.000-14 | 2A | . 0020 | 5.9980 | 5.9877 | 5.9516 | 5.9451 | . 0065 | 5.9104 | 2B | 5.923 | 5.938 | 5.9536 | 5.9621 | . 0085 | 6.0000 |

[^12]Table 3.2 Allowances for external threads of special diameters and pitches, classes $1 A$ and 2As
(UNS threads. See par. 10, p. 3.05.)


- Class 1AR allowances are tabulated on p. 3.03.

CLASSES 1A, 2A ALLOWANCES

Table 3.3. Pitch diameter tolerances for external threads of special diameters, pitches, and lengths of engagement, classes 1 A and 1 AR (UNS threads. See par. 7.3, p. 3.03; par. 10, p. 3.05.)


1A, 1AR P.D. TOLERANCES

Table 3.3 Pitch diameter tolerances for external threads of special diameters, pitches, and lengths of engagement, classes $1 A$ and $1 A R$-Con.


## LEGENDS

1. These values do not agree with and shall not be used in place of any tabulated values for the UNC, UNF, and 8UN thread series in table 2.21 .
2. Classes 1 A and 1 AR tolerances in this table for 5 to 15 pitches are based on 9 pitches and are obtained by multiplying the class 2 A (external thread) tolerances for 9 pitches taken to six decimal places (see table 2.19) by a factor of 1.5 .
3. Classes 1 A and 1 AR tolerances in this table for 16 to 30 pitches are obtained by multiplying the class 2 A (external thread) tolerances for 9 pitches taken to six decimal places (see table 2.19) by a factor of 1.875 (obtained by multiplying the 1.5 factor by 1.25). For lengths of engagement not tabulated, see par. 7.3, p. 3.03 .
4. Pitches listed are those used most commonly and are recommended. Where intermediate pitches are specified, the formula in par. 7.3, p. 3.03, should be applied.
5. Tolerances are tabulated only for combinations of diameter, pitch, and length of engagement which are considered to be generally used. For other combinations encountered, see Design of Special Threads in appendix A5.


1A, 1AR P.D. TOLERANCES
'Table 3.4 Pitch diameter tolerances for external threads of special diameters, pitches, and lengths of engagement, class $2 A$
(UNS threads. See par. 7.3, p. 3.03; par. 10, p. 3.05.)

| Tolerance based on diameter of $\rightarrow$ |  |  | 0.0625 | 0.09375 | 0.125 | 0.1875 | 0.25 | 0.375 | 0.5 | 0.625 | 0.75 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| For diameter range Above $\rightarrow$ |  |  | 0.0470 | 0.0781 | 0.1094 | 0.1562 | 0.2188 | 0.3125 | 0.4375 | 0.5625 | 0.6875 | 0.875 |
| To and including $\rightarrow$ |  |  | 0.0781 | 0.1094 | 0.1562 | 0.2188 | 0.3125 | 0.4375 | 0.5625 | 0.6875 | 0.875 | 1.125 |
| Threads per inch | Length of engagement |  | Pitch diameter tolerances |  |  |  |  |  |  |  |  |  |
|  | Number of pitches | Inches |  |  |  |  |  |  |  |  |  |  |
| 80 | 5 to 15 16 to 30 | 0.06 to 0.19 0.191 to 0.38 | in 0.0019 .0024 | in 0.0020 .0025 | in 0.0021 .0026 | in 0.0022 .0027 | in 0.0023 .0028 | in | in | in | in | in |
| 72 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.07 to 0.21 0.211 to 0.42 | .0020 .0025 | .0021 .0026 | . 00021 | .0023 .0028 | .0023 .0029 | 0.0025 .0031 |  |  |  |  |
| 64 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.08 to 0.23 0.231 to 0.46 | . 0021 | .0022 | . 00022 | .0024 .0029 | . 00024 | . 00026 | $\begin{array}{r} 0.0027 \\ .0034 \end{array}$ |  |  |  |
| 56 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.09 0.271 to 0.27 0.54 |  | .0023 .0029 | . 00024 | . 00025 | . 00026 | . 00027 | . 00288 | 0.0029 .0036 | 0.0030 .0037 |  |
| 48 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.10 to 0.31 0.311 to 0.62 |  | . 0025 | . 00025 | . 0026 | . 00027 | . 0029 | . 00030 | . 00031 | . 0031 |  |
| 44 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.11 \text { to } 0.34 \\ & 0.341 \text { to } 0.68 \end{aligned}$ |  | . 0026 | . 00026 | . 0027 | . 00288 | . .0030 | . 00031 | . 00032 | . 00032 | $\begin{array}{r} 0.0034 \\ .0042 \end{array}$ |
| 40 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.12 to 0.38 0.381 to 0.76 |  |  | .0027 .0034 | .0029 .0036 | .0029 .0037 | . 00031 | .0032 .0040 | . 00033 | .0034 .0042 | $\begin{aligned} & .0035 \\ & .0044 \end{aligned}$ |
| 36 | 5 to 15 16 to 30 | $\begin{aligned} & 0.14 \text { to } 0.42 \\ & 0.421 \text { to } 0.84 \end{aligned}$ |  |  | .0029 .0036 | .0030 .0037 | . 0031 | . .0032 | .0033 .0041 | . 0034 | . 00035 | . .0036 |
| 32 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.16 \text { to } 0.47 \\ & 0.471 \text { to } 0.94 \end{aligned}$ |  |  | .0030 .0038 | .0031 .0039 | . 0032 | . .0034 | . 00035 | .0036 .0045 | .0036 .0046 | . 00388 |
| 28 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.18 to 0.54 0.541 to 1.08 |  |  |  | .0033 .0042 | . 00034 | .0036 .0044 | .0037 .0046 | .0038 .0047 | .0038 .0048 | .0040 .0050 |
| 27 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.19 \text { to } 0.56 \\ & 0.561 \text { to } 1.12 \end{aligned}$ |  |  |  | .0034 .0042 | .0035 .0043 | . 00036 | . 00037 | .0038 .0048 | . 0039 | . 0040 |
| 24 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.21 \text { to } 0.62 \\ & 0.621 \text { to } 1.24 \end{aligned}$ |  |  |  | .0036 .0045 | . 00037 | . 00038 | . 00039 | .0040 | .0041 | . 00042 |
| 20 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.25 \text { to } 0.75 \\ & 0.751 \text { to } 1.50 \end{aligned}$ | --------- | ------- |  |  | . 0040 | . 00041 | . 00042 | .0043 .0054 | . 00044 | . 0045 |
| 18 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.28 \text { to } 0.83 \\ & 0.831 \text { to } 1.66 \end{aligned}$ |  |  |  |  |  | . 0043 | . 00044 | . 00045 | .0046 .0058 | $\begin{aligned} & .0047 \\ & .0059 \end{aligned}$ |
| 16 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.31 \text { to } 0.94 \\ & 0.941 \text { to } 1.88 \end{aligned}$ |  |  |  |  |  | . 0046 | .0047 .0058 | . 00048 | .0049 .0061 | $\begin{aligned} & .0050 \\ & .0062 \end{aligned}$ |
| 14 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.36 \text { to } 1.07 \\ & 1.071 \text { to } 2.14 \end{aligned}$ |  |  |  |  |  |  | . 00050 | . 00061 | .0051 | $\begin{aligned} & .0053 \\ & .0066 \end{aligned}$ |
| 12 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.42 \text { to } 1.25 \\ & 1.251 \text { to } 2.50 \end{aligned}$ |  |  |  |  |  |  | $\begin{aligned} & .0054 \\ & .0067 \end{aligned}$ | . 00054 | .0055 .0069 | $\begin{aligned} & .0057 \\ & .0071 \end{aligned}$ |
| 10 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.50 \text { to } 1.50 \\ & 1.501 \text { to } 3.00 \end{aligned}$ |  |  |  |  |  |  |  |  | .0060 .0075 | $\begin{aligned} & .0062 \\ & .0077 \end{aligned}$ |
| 8 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.62 \text { to } 1.88 \\ & 1.881 \text { to } 3.76 \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{aligned} & .0068 \\ & .0086 \end{aligned}$ |
| 6 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.83 \text { to } 2.50 \\ & 2.501 \text { to } 5.00 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |
| 4 | $\left\{\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \\ \hline \end{array}\right.$ | $\begin{aligned} & 1.25 \text { to } 3.75 \\ & 3.751 \text { to } 7.50 \\ & \hline \end{aligned}$ | ---- |  | -- |  |  |  |  |  |  | ------ |

Table 3.4. Pitch diameter tolerances for external threads of special diameters, pitches, and lengths of engagement, class 2A-Con

| 1.25 | 1.5 | 1.75 | 2 | 2.5 | 3 | 3.5 | 4 | 5 | 6 | 8 | 10 | 12 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.125 | 1.375 | 1.625 | 1.875 | 2.25 | 2.75 | 3.25 | 3.75 | 4.5 | 5.5 | 7 | 9 | 11 |
| 1.375 | 1.625 | 1.875 | 2.25 | 2.75 | 3.25 | 3.75 | 4.5 | 5.5 | 7 | 9 | 11 | 13 |

Pitch diameter tolerances
Threads

LEGENDS

1. These values do not agree with and shall not be used in place of any tabulated values for the UNC, UNF, and 8UN thread series in table 2.21 .
2. Formula:

Class 2A tolerances $=0.0015 \sqrt[3]{D}+0.0015 \sqrt{L_{e}}+0.015 \sqrt[3]{p^{2}}$ where
$D=$ basic major diameter
$L_{p}=$ length of engagement
3. Length of engagement increments included in the tabulated tolerances for lengths of engagement of from 5 to 15 pitches are based on lengths of 9 pitches; those for lengths of engagement greater than 15 to 30 pitches are obtained by multiplying the 9 -pitch values taken to six decimal places (see table 2.19) by 1.25. For lengths of engagement not tabulated, the formula in legend 2 should be applied except as modified by par. 7.3, p. 3.03.
4. Pitches listed are those used most commonly and are recommended. When intermediate pitches are specified, the formula in legend 2 should be applied.
5. Tolerances are tabulated only for combinations of diameter, pitch and length of engagement which are considered to be generally used. For other combinations encountered, see Design of Special Threads in appendix A5.

| in | in | in | in | in | in | in | in | in | in | in | in | in | 40 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} 0.0037 \\ .0047 \end{array}$ | 0.0038 .0048 |  |  |  |  |  |  |  |  |  |  |  | 36 |
| . 0039 | . 0040 | 0.0041 | 0.0042 | 0.0043 | 0.0044 |  |  |  |  |  |  |  | 32 |
| . 0049 | . 0050 | . 0051 | . 0052 | . 0054 | . 0056 |  |  |  |  |  |  |  |  |
| . 0041 | . 0042 | . 0043 | . 0044 | . 0045 | . 0046 | 0.0048 | 0.0049 |  |  |  |  |  | 28 |
| . 0041 | . 0042 | . 0043 | . 0044 | . 0046 | . 0047 | . 0048 | . 0049 | 0.0051 | 0.0053 |  |  |  | 27 |
| . 0052 | . 0053 | . 0054 | . 0055 | . 0057 | . 0059 | . 0060 | . 0061 | . 0064 | . 0066 |  |  |  |  |
| . 0043 | . 0044 | . 0045 | . 0046 | . 0048 | . 0049 | . 0050 | . 0051 | . 0053 | . 0054 |  |  |  | 24 |
| . 0054 | . 0055 | . 0057 | . 0058 | . 0059 | . 0061 | . 0062 | . 0064 | . 0066 | . 0068 |  |  |  |  |
| . 0047 | . 0048 | . 0048 | . 0049 | . 0051 | . 0052 | . 0053 | . 0054 | . 0056 | . 0058 |  |  |  | 20 |
| . 0058 | . 0059 | . 0061 | . 0062 | . 0063 | . 0065 | . 0066 | . 0068 | . 0070 | . 0072 |  |  |  |  |
| . 0049 | . 0050 | . 0051 | . 0051 | . 0053 | . 0054 | . 0055 | . 0056 | . 0058 | . 0060 | 0.0062 |  |  | 18 |
| . 0061 | . 0062 | . 0063 | . 0064 | . 0066 | . 0068 | . 0069 | . 0070 | . 0073 | . 0075 | . 0078 |  |  |  |
| . 0051 | . 0052 | . 0053 | . 0054 | . 0055 | . 0056 | . 0058 | . 0059 | . 0061 | . 0062 | . 0065 | 0.0067 |  | 16 |
| . 0064 | . 0065 | . 0066 | . 0067 | . 0069 | . 0071 | . 0072 | . 0073 | . 0076 | . 0078 | . 0081 | . 0084 |  |  |
| . 0054 | . 0055 | . 0056 | . 0057 | . 0058 | . 0059 | . 0061 | . 0062 | . 0064 | . 0065 | . 0068 | . 0070 | 0.0072 | 14 |
| . 0068 | . 0069 | . 0070 | . 0071 | . 0073 | . 0074 | . 0076 | . 0077 | . 0079 | . 0081 | . 0085 | . 0088 | . 0090 |  |
| . 0058 | . 0059 | . 0060 | . 0061 | . 0062 | . 0063 | . 0064 | . 0065 | . 0067 | . 0069 | . 0072 | . 0074 | . 0076 | 12 |
| . 0072 | . 0073 | . 0075 | . 0076 | . 0077 | . 0079 | . 0080 | . 0082 | . 0084 | . 0086 | . 0090 | . 0092 | . 0095 |  |
| . 0063 | . 0064 | . 0065 | . 0065 | . 0067 | . 0068 | . 0069 | . 0070 | . 0072 | . 0074 | . 0077 | . 0079 |  | 10 |
| . 0078 | . 0080 | . 0081 | . 0082 | . 0084 | . 0085 | . 0087 | . 0088 | . 0090 | . 0092 | . 0096 | . 0099 | . 0101 |  |
| . 0070 | . 0071 | . 0071 | . 0072 | . 0074 | . 0075 | . 0076 | . 0077 | . 0079 | . 0081 | . 0083 | . 0086 | . 0088 | 8 |
| . 0087 | . 0088 | . 0089 | . 0090 | . 0092 | . 0094 | . 0095 | . 0097 | . 0099 | . 0101 | . 0104 | . 0107 | . 0110 |  |
|  | . 0081 | . 0082 | . 0083 | . 0084 | . 0085 | . 0087 | . 0088 | . 0089 | . 0091 | . 0094 | . 0096 | . 0098 | 6 |
|  | . 0101 | . 0102 | . 0103 | . 0105 | . 0107 | . 0108 | . 0110 | . 0112 | . 0114 | . 0117 | . 0120 | . 0123 |  |
|  |  |  | . 0101 | . 0102 | . 0104 | . 0105 | . 0106 | . 0108 | . 0109 | . 0112 | . 0114 | . 0116 | 4 |
|  |  |  | . 0126 | . 0128 | . 0130 | . 0131 | . 0132 | . 0135 | . 0137 | . 0140 | . 0143 | . 0145 |  |

2A P.D. TOLERANCES

Table 3.5 Pitch diameter tolerances for external threads of special diameters, pitches, and lengths of engagement, class 3 A (UNS threads. See par. 7.3, p. 3.03; par. 10, p. 3.05.)

| Tolerance based on diameter of $\rightarrow$ |  |  | 0.0625 | 0.09375 | 0.125 | 0.1875 | 0.25 | 0.375 | 0.5 | 0.625 | 0.75 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| For diameter range Above $\rightarrow$ |  |  | 0.0470 | 0.0781 | 0.1094 | 0.1562 | 0.2188 | 0.3125 | 0.4375 | 0.5625 | 0.6875 | 0.875 |
| To and including $\rightarrow$ |  |  | 0.0781 | 0.1094 | 0.1562 | 0.2188 | 0.3125 | 0.4375 | 0.5625 | 0.6875 | 0.875 | 1.125 |
| Threads per inch | Length of engagement |  | Pitch diameter tolerances |  |  |  |  |  |  |  |  |  |
|  | Number of pitches | Inches |  |  |  |  |  |  |  |  |  |  |
| 80 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.06 to 0.19 0.191 to 0.38 | in 0.0014 .0018 | in 0.0015 .0019 | $\begin{aligned} & \text { in } \\ & 0.0015 \\ & .0019 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & 0.0016 \\ & .0020 \end{aligned}$ | in 0.0017 .0021 | in | in | in | in | in |
| 72 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.07 to 0.21 0.211 to 0.42 | . 0015 | . 0016 | .0016 .0020 | . 0017 | . 0018 | 0.0019 .0023 |  |  |  |  |
| 64 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.08 to 0.23 0.231 to 0.46 | . 0016 | . 00026 | . 0017 | . 0018 | . 0018 | . 00019 | 0.0020 .0025 |  |  |  |
| 56 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.09 to 0.27 0.271 to 0.54 |  | . 0017 | . 0018 | . 0019 | .0019 .0024 | .0020 .0025 | . 0021 | 0.0022 .0027 | 0.0022 .0028 |  |
| 48 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.10 \text { to } 0.31 \\ & 0.311 \text { to } 0.62 \end{aligned}$ |  | . 00019 | .0019 .0024 | . 0020 | . 0020 | . 00022 | . 0022 | . 0023 | . 0024 |  |
| 44 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.11 to 0.34 0.341 to 0.68 |  | . 0019 | . 0020 | . 0021 | . 0021 | . 0022 | .0023 .0029 | . 0024 | . 0024 | 0.0025 .0032 |
| 40 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.12 to 0.38 9.381 |  |  | . 0021 | . 0021 | . 0022 | . 0023 | . 0024 | . 0025 | . 0025 | . 0026 |
| 36 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.14 \text { to } 0.42 \\ & 0.421 \text { to } 0.84 \end{aligned}$ |  |  | . 0022 | . 0022 | . 0023 | . 0024 | .0025 .0031 | . 0026 | . 0026 | . 0027 |
| 32 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.16 to 0.47 0.471 to 0.94 |  |  | . 0023 | .0024 | .0024 | . 0025 | . 0026 | . 0027 | . 0027 | . 00028 |
| 28 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.18 \text { to } 0.54 \\ & 0.541 \text { to } 1.08 \end{aligned}$ |  |  |  | . 0025 | . 00236 | . 00027 | . 00028 | . 0028 | . 0029 | . 00030 |
| 27 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.19 \text { to } 0.56 \\ & 0.561 \text { to } 1.12 \end{aligned}$ |  |  |  | . 0025 | .0026 .0033 | . 0027 | . 0028 | .0029 .0036 | .0029 .0037 | $\begin{aligned} & .0030 \\ & .0038 \end{aligned}$ |
| 24 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.21 \text { to } 0.62 \\ & 0.621 \text { to } 1.24 \end{aligned}$ |  |  |  | .0027 .0034 | . 0028 | .0029 .0036 | . 0029 | . 0030 | .0031 .0038 | .0032 .0040 |
| 20 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.25 \text { to } 0.75 \\ & 0.751 \text { to } 1.50 \end{aligned}$ |  |  |  |  | . 0030 | . 00031 | . 00032 | . 0032 | . 00033 | . 0034 |
| 18 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.28 to 0.83 0.831 to 1.66 |  |  |  |  |  | . 00032 | . 0033 | . 0034 | .0035 .0043 | $\begin{aligned} & .0036 \\ & .0044 \end{aligned}$ |
| 16 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.31 \text { to } 0.94 \\ & 0.941 \text { to } 1.88 \end{aligned}$ |  |  |  |  |  | . 00034 | . 0035 | . 0036 | . 0036 | . 00037 |
| 14 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.36 \text { to } 1.07 \\ & 1.071 \text { to } 2.14 \end{aligned}$ |  |  |  |  |  |  | . 00037 | . 00388 | .0039 .0048 | . 0040 |
| 12 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.42 \text { to } 1.25 \\ & 1.251 \text { to } 2.50 \end{aligned}$ |  |  |  |  |  |  | . 00040 | . 0041 | . 0041 | $\begin{aligned} & .0042 \\ & .0053 \end{aligned}$ |
| 10 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.50 \text { to } 1.50 \\ & 1.501 \text { to } 3.00 \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{aligned} & .0045 \\ & .0056 \end{aligned}$ | $\begin{array}{r} .0046 \\ .0058 \end{array}$ |
| 8 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.62 \text { to } 1.88 \\ & 1.881 \text { to } 3.76 \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{aligned} & .0051 \\ & .0064 \end{aligned}$ |
| 6 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.83 \text { to } 2.50 \\ & 2.501 \text { to } 5.00 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |
| 4 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 1.25 \text { to } 3.75 \\ & 3.751 \text { to } 7.50 \end{aligned}$ |  | --- |  |  |  |  |  |  |  |  |

3A P.D. TOLERANCES

Table 3.5 Pitch diameter tolerances for external threads of special diameters, pitches, and lengths of engagement, class 3A-Con

| 1.25 | 1.5 | 1.75 | 2 | 2.5 | 3 | 3.5 | 4 | 5 | 6 | 8 | 10 | 12 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.125 | 1.375 | 1.625 | 1.875 | 2.25 | 2.75 | 3.25 | 3.75 | 4.5 | 5.5 | 7 | 9 | 11 |
| 1.375 | 1.625 | 1.875 | 2.25 | 2.75 | 3.25 | 3.75 | 4.5 | 5.5 | 7 | 9 | 11 | 13 |

## LEGENDS

1. These values do not agree with and shall not be used in place of any tabulated values for the UNC, UNF, and 8UN thread series in table 2.21 .
2. Class 3A tolerances in this table for 5 to 15 pitches are based on 9 pitches and are obtained by multiplying the class 2 A (external thread) tolerences for 9 pitches taken to six decimal places by a factor of 0.75 . (See table 2.19).
3. Class 3 A tolerances in this table for 16 to 30 pitches are obtained by multiplying the class 2 A (external thread) tolerances for 9 pitches taken to six decimal places by a factor of 0.9375 (obtained by multiplying the 0.75 factor by 1.25.) (See table 2.19.) For lengths of engagement not tabulated, see par. 7.3, p. 3.03.
4. Pitches listed are those used most commonly and are recommended. Where intermediate pitches are specified, the formula in par. 7.3, p. 3.03 , should be applied.
5. Tolerances are tabulated only for combinations of diameter, pitch, and length of engagement which are considered to be generally used. For other combinations encountered, see Design of Special Threads in appendix A5.


3A P.D. TOLERANCES

Table 3.6. Pitch diameter tolerances for internal threads of special diameters, pitches, and lengths of engagement, class $1 B$ (UNS threads. See par. 7.3, p. 3.03; par. 10, p. 3.05.)

| Tolerance based on diameter of $\rightarrow$ |  |  | 0.0625 | 0.09375 | 0.125 | 0.1875 | 0.25 | 0.375 | 0.5 | 0.625 | 0.75 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| For diameter range Above $\rightarrow$ |  |  | 0.0470 | 0.0781 | 0.1094 | 0.1562 | 0.2188 | 0.3125 | 0.4375 | 0.5625 | 0.6875 | 0.875 |
| To and including $\rightarrow$ |  |  | 0.0781 | 0.1094 | 0.1562 | 0.2188 | 0.3125 | 0.4375 | 0.5625 | 0.6875 | 0.875 | 1.125 |
| Threads per inch | Length of engagement |  | Pitch diameter tolerances |  |  |  |  |  |  |  |  |  |
|  | Number of pitches | Inches |  |  |  |  |  |  |  |  |  |  |
| 80 | 5 to 15 | $\begin{aligned} & 0.06 \text { to } 0.19 \\ & 0.191 \text { to } 0.38 \end{aligned}$ | in | in | in | in | in | in | in | in | in | in |
| 72 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.07 \text { to } 0.21 \\ & 0.211 \text { to } 0.42 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |
| 64 | $\left\{\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}\right.$ | $\begin{aligned} & 0.08 \text { to } 0.23 \\ & 0.231 \text { to } 0.46 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |
| 56 | $\left\{\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}\right.$ | $\begin{aligned} & 0.09 \text { to } 0.27 \\ & 0.271 \text { to } 0.54 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |
| 48 | $\left\{\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}\right.$ | $\begin{aligned} & 0.10 \text { to } 0.31 \\ & 0.311 \text { to } 0.62 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |
| 4 | $\left\{\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}\right.$ | $\begin{aligned} & 0.11 \text { to } 0.34 \\ & 0.341 \text { to } 0.68 \end{aligned}$ |  | $\begin{array}{r} 0.0050 \\ .0066 \end{array}$ | $\begin{gathered} 0.0051 \\ .0064 \end{gathered}$ | $\begin{array}{r} 0.0053 \\ .0067 \end{array}$ | $\begin{array}{r} 0.0055 \\ .0069 \end{array}$ | $\begin{array}{r} 0.0058 \\ .0072 \end{array}$ | $\begin{array}{r} 0.0060 \\ .0075 \end{array}$ | $\begin{array}{r} 0.0062 \\ .0077 \end{array}$ | $\begin{array}{r} 0.0063 \\ .0079 \end{array}$ | 0.0066 .0082 |
| 40 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.12 \text { to } 0.38 \\ & 0.381 \text { to } 0.76 \end{aligned}$ |  |  | $\begin{aligned} & .005 \pm \\ & .0067 \end{aligned}$ | $\begin{aligned} & .0056 \\ & .0070 \end{aligned}$ | $.0057$ | $\begin{aligned} & .0060 \\ & .0075 \end{aligned}$ | $\begin{aligned} & .0062 \\ & .0078 \end{aligned}$ | $\begin{aligned} & .0064 \\ & .0080 \end{aligned}$ | $\begin{aligned} & .0065 \\ & .0082 \end{aligned}$ | . 00688 |
| 36 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.14 \text { to } 0.42 \\ & 0.421 \text { to } 0.84 \end{aligned}$ |  |  | $\begin{aligned} & .0056 \\ & .0070 \end{aligned}$ | . 00058 | . 00060 | . 00063 | $.0065$ | . .00663 | . 00068 | . 0071 |
| 32 | $\left\{\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}\right.$ | $\begin{aligned} & 0.16 \text { to } 0.47 \\ & 0.471 \text { to } 0.94 \end{aligned}$ |  |  | $.0059$ | . 00671 | . 00063 | $\begin{aligned} & .0066 \\ & .0082 \end{aligned}$ | $\begin{aligned} & .0068 \\ & .0085 \end{aligned}$ | . .0070 | $.0071$ | .0074 |
| 28 | $\left\{\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}\right.$ | $\begin{aligned} & 0.18 \text { to } 0.54 \\ & 0.541 \text { to } 1.08 \end{aligned}$ |  |  |  | $.0065$ | $.0067$ | $\begin{aligned} & .0069 \\ & .0087 \end{aligned}$ | . .0072 | $\begin{aligned} & .0073 \\ & .0092 \end{aligned}$ | . 00075 | . 00078 |
| 27 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.19 \text { to } 0.56 \\ & 0.561 \text { to } 1.12 \end{aligned}$ |  |  |  | .0066 .0083 | $.0068$ | $\begin{aligned} & .0070 \\ & .0088 \end{aligned}$ | $\begin{aligned} & .0073 \\ & .0091 \end{aligned}$ | $\begin{aligned} & .0074 \\ & .0093 \end{aligned}$ | . 0076 | . 0079 |
| 24 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.21 \text { to } 0.62 \\ & 0.621 \text { to } 1.24 \end{aligned}$ |  |  |  | $\begin{aligned} & .0070 \\ & .0087 \end{aligned}$ | $.0072$ | . .0074 | . 0076 | . 0078 | . 0080 | . 00082 |
| 20 | $\left\{\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}\right.$ | $\begin{aligned} & 0.25 \text { to } 0.75 \\ & 0.751 \text { to } 1.50 \end{aligned}$ |  |  |  |  | $.0078$ | .0080 .0101 | . 0083 | . 00084 | . 0086 | . 0089 |
| 18 | $\left\{\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}\right.$ | $\begin{aligned} & 0.28 \text { to } 0.83 \\ & 0.831 \text { to } 1.66 \end{aligned}$ |  |  |  |  |  | . 00084 | $\begin{aligned} & .0087 \\ & .0108 \end{aligned}$ | . 0088 | . 00912 | . 00093 |
| 16 | $\left\{\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}\right.$ | $\begin{aligned} & 0.31 \text { to } 0.94 \\ & 0.941 \text { to } 1.88 \end{aligned}$ |  |  |  |  |  | $\begin{aligned} & .0089 \\ & .0111 \end{aligned}$ | $\begin{aligned} & .0091 \\ & .0114 \end{aligned}$ | . 00093 | . 00095 | . 00097 |
| 14 | $\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}$ | $\begin{aligned} & 0.36 \text { to } 1.07 \\ & 1.071 \text { to } 2.14 \end{aligned}$ |  |  |  |  |  |  | $\begin{aligned} & .0097 \\ & .0121 \end{aligned}$ | . 0099 | .0100 <br> .0125 | . 010129 |
| 12 | $\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}$ | $\begin{aligned} & 0.42 \text { to } 1.25 \\ & 1.251 \text { to } 2.50 \end{aligned}$ |  |  |  |  |  |  | $.0104$ | . 010136 | . 0108 | . 01110 |
| 10 | $\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}$ | $\begin{aligned} & 0.50 \text { to } 1.50 \\ & 1.501 \text { to } 3.00 \end{aligned}$ |  |  |  |  |  |  |  |  | . 0117 | . 0120 |
| 8 | $\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}$ | $\begin{aligned} & 0.62 \text { to } 1.88 \\ & 1.881 \text { to } 3.76 \end{aligned}$ | ----- |  |  |  |  |  |  |  |  | . 01338 |
| 6 | 5 to 15 16 to 30 | $\begin{aligned} & 0.83 \text { to } 2.50 \\ & 2.501 \text { to } 5.00 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |
| 4 | $\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}$ | $\begin{aligned} & 1.25 \text { to } 3.75 \\ & 3.751 \text { to } 7.50 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |

1B P.D. TOLERANCES

Table 3.6. Pitch diameter tolerances for internal threads of special diameters, pitches, and lengths of engagement, class $1 B$-.Con

| 1.25 | 1.5 | 1.75 | 2 | 2.5 | 3 | 3.5 | 4 | 5 | 6 | 8 | 10 | 12 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.125 | 1.375 | 1.625 | 1.875 | 2.25 | 2.75 | 3.25 | 3.75 | 4.5 | 5.5 | 7 | 9 | 11 |
| 1.375 | 1.625 | 1.875 | 2.25 | 2.75 | 3.25 | 3.75 | 4.5 | 5.5 | 7 | 9 | 11 | 13 |

## LEGENDS

1. These values do not agree with and shall not be used in place of any tabulated values for the UNC, UNF. and 8UN thread series in table 2.21 .
2. Class 1B (internal thread) tolerances in this table for 5 to 15 pitches are based on 9 pitches and are obtained by multiplying the class 2 A (external thread) tolerances for 9 pitches taken to six decimal places by a factor of 1.95 . (See table 2.19.)
3. Class 1 B tolerances in this table for 16 to 30 pitches are obtained by multiplying the class 2 A (external thread) tolerances for 9 pitches taken to six decimal places by a factor of 2.4375 (obtained by multiplying the 1.95 factor by 1.25.) (See table 2.19.) For lengths of engagement not tabulated, see par. 7.3, p. 3.03.
4. Pitches listed are those used most commonly and are recommended. Where intermediate pitches are specified, the formula in par. 7.3, p. 3.03 , should be applied.
5. Tolerances are tabulated only for combinations of diameter, pitch, and length of engagement which are considered to be generally used. For other combinations eulcountered, see Design of Special Threads in appendix A5.


1B P.D. TOLERANCES

TABLE 3.7. Pitch diameter tolerances for internal threads of special diameters, pitches, and lengths of engagement, class $2 B$ (UNS threads. See par. 7.3, p. 3.03 ; par. 10, p. 3.05.)

| Tolerance based on diameter of $\rightarrow$ |  |  | 0.0625 | 0.09375 | 0.125 | 0.1875 | 0.25 | 0.375 | 0.5 | 0.625 | 0.75 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| For diameter range Above $\rightarrow$ |  |  | 0.0470 | 0.0781 | 0.1094 | 0.1562 | 0.2188 | 0.3125 | 0.4375 | 0.5625 | 0.6875 | 0.875 |
| To and including $\rightarrow$ |  |  | 0.0781 | 0. 1094 | 0.1562 | 0.2188 | 0.3125 | 0.4375 | 0.5625 | 0.6875 | 0.875 | 1.125 |
| Threads per inch | Length of engagement |  | Pitch diameter tolerances |  |  |  |  |  |  |  |  |  |
|  | Number of pitches | Inches |  |  |  |  |  |  |  |  |  |  |
| 80 | 5 to 15 16 to 30 | 0.06 to 0.19 0.191 | in 0.0025 .0031 | in 0.0026 .0032 | in 0.0027 .0033 | $\begin{aligned} & i n \\ & 0.0028 \\ & .0035 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & 0.0029 \\ & .0037 \end{aligned}$ | in | in | in | in | in |
| 72 | 5 to 15 16 to 30 | 0.07 to 0.21 0.211 | $\begin{aligned} & .0026 \\ & .0032 \end{aligned}$ | . 00027 | $\begin{aligned} & .0028 \\ & .0035 \end{aligned}$ | $\begin{aligned} & .0029 \\ & .0037 \end{aligned}$ | . 00030 | $\begin{array}{r} 0.0032 \\ .0040 \end{array}$ |  |  |  |  |
| 64 | 5 to 15 16 to 30 | 0.08 to 0.23 0.231 | . 0027 | .0028 .0035 | $\begin{aligned} & .0029 \\ & .0037 \end{aligned}$ | . 0031 | . 00032 | .0034 .0042 | $\begin{array}{r} 0.0035 \\ .0044 \end{array}$ |  |  |  |
| 56 | 5 to 15 16 to 30 | 0.09 0.271 to 0.27 |  | .0030 .0037 | . 0031 | . 00332 | . 00033 | .0035 .0044 | .0037 .0046 | 0.0038 .0047 | 0.0039 .0049 |  |
| 48 | 5 to 15 16 to 30 | 0.10 0.311 to 0.31 |  | .0032 .0040 | .0033 .0041 | . 0034 | . 00036 | . 00037 | .0039 .0048 | .0040 .0050 | . 00041 |  |
| 44 | 5 to 15 16 to 30 | 0.11 to 0.34 0.341 to 0.68 |  | .0033 .0042 | .0034 .0043 | . 0036 | .0037 .0046 | .0039 .0048 | .0040 .0050 | . 0041 | .0042 .0053 | 0.0044 .0055 |
| 40 | 5 to 15 16 to 30 | 0.12 to 0.38 0.381 to 0.76 |  |  | . 0036 | . 0037 | . 00038 | . 0040 | . 0041 | . 00043 | .0044 | . 00045 |
| 36 | 5 to 15 16 to 30 | $\begin{aligned} & 0.14 \text { to } 0.42 \\ & 0.421 \text { to } 0.84 \end{aligned}$ |  |  | . 00037 | . 00039 | .0040 .0050 | . 0042 | . 0043 | . 0044 | .0045 .0057 | $\begin{array}{r} .0047 \\ .0059 \end{array}$ |
| 32 | 5 to 15 16 to 30 | $\begin{aligned} & 0.16 \text { to } 0.47 \\ & 0.471 \text { to } 0.94 \end{aligned}$ |  |  | .0030 .0049 | . 0041 | .0042 .0052 | . 00044 | .0045 .0056 | .0046 .0058 | .0047 .0059 | . 00049 |
| 28 | 5 to 15 16 to 30 | $\begin{aligned} & 0.18 \text { to } 0.54 \\ & 0.541 \text { to } 1.08 \end{aligned}$ |  |  |  | . 0043 | . 00044 | . 0046 | .0048 .0060 | . 0049 | . 00050 | . 00052 |
| 27 | 5 to 15 16 to 30 | $\begin{aligned} & 0.19 \text { to } 0.56 \\ & 0.561 \text { to } 1.12 \end{aligned}$ |  |  |  | . 0044 | . 0045 | . 0047 | . 00048 | . 0050 | . 00051 | . 00052 |
| 24 | 5 to 15 16 to 30 | $\begin{aligned} & 0.21 \text { to } 0.62 \\ & 0.621 \text { to } 1.24 \end{aligned}$ |  |  |  | $\begin{aligned} & .0047 \\ & .0058 \end{aligned}$ | . 0048 | . 0049 | . 00051 | . 0052 | . 00053 | . 00055 |
| 20 | 5 to 15 16 to 30 | $\begin{aligned} & 0.25 \text { to } 0.75 \\ & 0.751 \text { to } 1.50 \end{aligned}$ |  |  |  |  | . 00052 | . 00054 | .0055 .0069 | .0056 .0070 | .0057 .0072 | . 0059 |
| 18 | $\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}$ | $\begin{aligned} & 0.28 \text { to } 0.83 \\ & 0.831 \text { to } 1.66 \end{aligned}$ |  |  |  |  |  | .0056 .0070 | .0058 .0072 | . 0059 | .0060 .0075 | . 00062 |
| 16 | $\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}$ | $\begin{aligned} & 0.31 \text { to } 0.94 \\ & 0.941 \text { to } 1.88 \end{aligned}$ |  |  |  |  |  | . 00059 | .0061 .0076 | .0062 | . 00638 | . 00085 |
| 14 | 5 to 15 <br> 16 to 30 | $\begin{aligned} & 0.36 \text { to } 1.07 \\ & 1.071 \text { to } 2.14 \end{aligned}$ |  |  |  |  |  |  | .0065 .0081 | . 00666 | . 00067 | $\begin{array}{r} .0069 \\ .0086 \end{array}$ |
| 12 | $\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}$ | $\begin{aligned} & 0.42 \text { to } 1.25 \\ & 1.251 \text { to } 2.50 \end{aligned}$ |  |  |  |  |  |  | . 0070 | . 0071 | .0072 .0090 | . 00074 |
| 10 | $\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}$ | $\begin{aligned} & 0.50 \text { to } 1.50 \\ & 1.501 \text { to } 3.00 \end{aligned}$ |  |  |  |  |  |  |  |  | $\begin{aligned} & .0078 \\ & .0098 \end{aligned}$ | . 0080 |
| 8 | 5 to 15 16 to 30 | $\begin{aligned} & 0.62 \text { to } 1.88 \\ & 1.881 \text { to } 3.76 \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{aligned} & .0089 \\ & .0111 \end{aligned}$ |
| 6 | 5 to 15 16 to 30 | $\begin{aligned} & 0.83 \text { to } 2.50 \\ & 2.501 \text { to } 5.00 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |
| 4 | 5 to 15 16 to 30 | $\begin{aligned} & 1.25 \text { to } 3.75 \\ & 3.751 \text { to } 7.50 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |

Table 3.7 Pitch diameter tolerances for internal threads of special diameters, pitches, and lengths of engagement. class $2 B-$ Con

| 1.25 | 1.5 | 1.75 | 2 | 2.5 | 3 | 3.5 | 4 | 5 | 6 | 8 | 10 | 12 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.125 | 1.375 | 1.625 | 1.875 | 2.25 | 2.75 | 3.25 | 3.75 | 4.5 | 5.5 | 7 | 9 | 11 |
| 1.375 | 1.625 | 1.875 | 2.25 | 2.75 | 3.25 | 3.75 | 4.5 | 5.5 | 7 | 9 | 11 | 13 |

## LEGENDS

1. These values do not agree with and shall not be used in place of any tabulated values for the UNC, UNF, and 8UN thread series in table 2.21 .
2. Class 2 B (internal thread) tolerances in this table for 5 to 15 pitches are based on 9 pitches and are obtained by multiplying the class 2 A (external thread) tolerances for 9 pitches taken to six decimal places by a factor of 1.3. (See table 2.19.)
3. Class 2B tolerances in this table for 16 to 30 pitches are obtained by multiplying the class 2 A (external thread) tolerances for 9 pitches taken to six decimal places by a factor of 1.625 (obtained by multiplying the 1.3 factor by 1.25 .) (See table 2.19.) For lengths of engagement not tabulated, see par. 7.3, p. 3.03.
4. Pitches listed are those used most commonly and are recommended. Where intermediate pitches are specified, the formula in par. 7.3 , p. 3.03, should be applied.
5. Tolerances are tabulated only for combinations of diameter, pitch, and length of engagement which are considered to be generally used. For other combinations encountered, see Design of Special Threads in appendix A5.

| in | in | in | in | in | in | in | in | in | in | in | in | in |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} 0.0049 \\ .0061 \end{array}$ | $\begin{array}{r} 0.0050 \\ .0062 \end{array}$ |  |  |  |  |  |  |  |  |  |  |  | 36 |
| . 0051 | . 0052 | 0.0053 .0066 |  |  | 0.0058 .0072 |  |  |  |  |  |  |  | 32 |
| . 0053 | .0055 .0068 | .0056 .0070 | . 0057 | .0059 .0073 | .0060 .0075 | 0.0062 .0077 | $0.0063$ |  |  |  |  |  | 23 |
| .0053 | $\begin{array}{r} .0055 \\ .0069 \end{array}$ | .0056 .0071 | . 00057 | .0059 .0074 | .0061 .0076 | .0063 .0078 | .0064 .0080 | 0.0066 .0083 | 0.0068 .0085 |  |  |  | 27 |
| .0056 .0070 | . 00058 | .0059 .0074 | .0060 .0075 | . 00062 | .0064 .0079 | .0065 .0081 | .0066 .0083 | .0069 .0086 | .0071 .0089 |  |  |  | 24 |
| . 0061 | . 0062 | . 0063 | . 0064 | . 0066 | . 0068 | . 0069 | . 0070 | . 0073 | . 0075 |  |  |  | 20 |
| . 0076 | . 0077 | . 0079 | . 0080 | . 0083 | . 0085 | . 0086 | . 0088 | . 0091 | . 0094 |  |  |  | 2 |
| $\begin{aligned} & .0063 \\ & .0079 \end{aligned}$ | . 0065 | $\begin{aligned} & .0066 \\ & .0082 \end{aligned}$ | . 00067 | .0069 .0086 | .0070 .0088 | .0072 .0090 | . 00073 | .0076 .0094 | .0078 .0097 | 0.0081 .0101 |  |  | 18 |
| $\begin{array}{r} .0070 \\ .0088 \end{array}$ | .0072 .0089 | $\begin{array}{r} .0073 \\ .0091 \end{array}$ | . 00074 | .0076 .0095 | . 0077 | .0079 .0099 | . 0080 | .0083 .0103 | . 0085 | .0088 .0110 | . 0091 | 0.0094 .0117 | 14 |
| . 0075 | .0076 .0096 | .0078 .0097 | .0079 .0098 | .0081 .0101 | .0082 .0103 | .0084 .0105 | . 0085 | .0087 .0109 | .0090 .0112 | .0093 .0116 | .0096 .0120 | .0099 .0123 | 12 |
| . 0082 | . 0083 | . 0084 | . 0085 | . 0087 | . 0089 | . 0090 | . 0091 | . 0094 | . 00096 | . 0100 | . 0103 | . 0105 | 10 |
| . 0102 | . 0104 | . 0105 | . 0106 | . 0109 | . 0111 | . 0113 | . 0114 | . 0117 | . 0120 | . 0124 | . 0128 | . 0131 | 10 |
| $\begin{aligned} & .0090 \\ & .0113 \end{aligned}$ | . 0092 | .0093 .0116 | . 00094 | .0096 .0120 | .0098 .0122 | .0099 .0124 | .0100 .0125 | .0103 .0128 | .0105 .0131 | .0108 .0136 | . 01111 | . 0114 | 8 |
|  | $\begin{aligned} & .0105 \\ & .0132 \end{aligned}$ | $\begin{aligned} & .0106 \\ & .0133 \end{aligned}$ | $\begin{aligned} & .0108 \\ & .0134 \end{aligned}$ | .0109 .0137 | . 0111 | . 0113 | . 0114 | . 0116 | . 0118 | . 0122 | . 0125 | . 0128 | 6 |
|  |  |  | . 0131 | . 0133 | .0135 .0168 | .0136 .0170 | .0138 .0172 | . 0140 | . 0142 | .0146 .0182 | . 0149 | . 0151 | 4 |

Table 3.8 Pitch diameter tolerances for internal threads of special diameters, pitches, and lengths of engagement, class 3B
(UNS threads. See par. 7.3, p. 3.03; par. 10, p. 3.05.)

| Tolerance based on diameter of $\rightarrow$ |  |  | 0.0625 | 0.09375 | 0.125 | 0.1875 | 0.25 | 0.375 | 0.5 | 0.625 | 0.75 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| For diameter range Above $\rightarrow$ |  |  | 0.0470 | 0.0781 | 0.1094 | 0.1562 | 0.2188 | 0.3125 | 0.4375 | 0.5625 | 0.6875 | 0.875 |
| To and including $\rightarrow$ |  |  | 0.0781 | 0.1094 | 0.1562 | 0.2188 | 0.3125 | 0.4375 | 0.5625 | 0.6875 | 0.875 | 1.125 |
| Threads per inch | Length of engagement |  | Pitch diameter tolerances |  |  |  |  |  |  |  |  |  |
|  | Number of pitches | Inches |  |  |  |  |  |  |  |  |  |  |
| 80 | 5 to 15 16 to 30 | 0.06 to 0.19 0.191 to 0.38 | in 0.0019 .0023 | in 0.0019 .0024 | in 0.0020 .0025 | in 0.0021 .0026 | in 0.0022 .0027 | in | in | in | in | in |
| 72 | \| $\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}$ | 0.07 to 0.21 0.211 to 0.42 | .0019 .0024 | . 0020 | .0021 .0026 | . 00022 | .0023 .0029 | 0.0024 .0030 |  |  |  |  |
| 64 | $\left\{\begin{array}{r} 5 \text { to } 15 \\ 16 \text { to } 30 \end{array}\right.$ | 0.08 to 0.23 0.231 to 0.46 | . 0020 | . 00021 | . 0022 | .0023 .0029 | .0024 .0030 | . 0025 | 0.0026 .0033 |  |  |  |
| 56 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.09 0.271 to 0.27 |  | . 0023 | . 0023 | . 00024 | . 00025 | . 0026 | . 0027 | 0.0028 .0035 | 0.0029 .0036 |  |
| 48 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.10 to 0.31 0.311 to 0.62 |  | . 0024 | . 0025 | . 00026 | .0027 .0033 | .0028 .0035 | .0029 .0036 | . 00030 | . 00031 |  |
|  | f 5 to 15 | 0.11 to 0.34 |  | . 0025 | . 0026 | . 0027 | . 0028 | . 0029 | . 0030 | . 0031 | . 0032 | 0.0033 |
| 4 | - 16 to 30 | 0.341 to 0.68 |  | . 0031 | . 0032 | . 0033 | . 0034 | . 0036 | . 0037 | . 0039 | . 0040 | . 0041 |
| 40 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16.030\end{array}\right.$ | 0.12 to 0.38 |  |  | . 0027 | . 0028 | . 0029 | . 00330 | . 0031 | . 00342 | . 0033 | . 00034 |
| 36 | ¢ 5 to 15 | 0.14 to 0.42 |  |  | . 0028 | . 0029 | . 0030 | . 0031 | . 0032 | . 0033 | . 0034 | . 0035 |
| 30 | ( 16 to 30 | 0.421 to 0.84 |  |  | . 0035 | . 0036 | . 0037 | . 0039 | . 0040 | . 0042 | . 0043 | . 0044 |
| 32 | $\{\quad 5$ to 15 | 0.16 to 0.47 |  |  | . 0030 | . 0031 | . 0031 | . 0033 | . 0034 | . 0035 | . 0036 | . 0037 |
|  | - 16 to 30 | 0.471 to 0.94 |  |  | . 0037 | . 0038 | . 0039 | . 0041 | . 0042 | . 0043 | . 0044 | . 0046 |
| 28 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | 0.18 to 0.54 0.541 to 1.08 |  |  |  | .0033 .0041 | .0033 .0042 | .0035 .0043 | . 0036 | . 00037 | . 00037 | .0039 .0048 |
|  | \} 5 to 15 | 0.19 to 0.56 |  |  |  | . 0033 | . 0034 | . 0035 | . 0036 | . 0037 | . 0038 | . 0039 |
| 27 | - 16 to 30 | 0.561 to 1.12 |  |  |  | . 0041 | . 0042 | . 0044 | . 0045 | . 0046 | . 0047 | . 0049 |
| 24 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.21 \text { to } 0.62 \\ & 0.621 \text { to } 1.24 \end{aligned}$ |  |  |  | .0035 .0044 | .0036 .0045 | .0037 .0046 | . 0038 | . 0039 | .0040 .0050 | .0041 .0051 |
| 20 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.25 \text { to } 0.75 \\ & 0.751 \text { to } 1.50 \end{aligned}$ |  |  |  |  | .0039 .0049 | .0040 .0050 | . 0041 | . 0042 | .0043 .0054 | . 00044 |
| 18 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.28 \text { to } 0.83 \\ & 0.831 \text { to } 1.66 \end{aligned}$ |  |  |  |  |  | .0042 .0053 | . 00053 | . 00054 | .0045 .0056 | .0046 .0058 |
| 16 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.31 \text { to } 0.94 \\ & 0.941 \text { to } 1.88 \end{aligned}$ |  |  |  |  |  | .0045 .0056 | . 0046 | . 0046 | . 00047 | .0049 .0061 |
| 14 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.36 \text { to } 1.07 \\ & 1.071 \text { to } 2.14 \end{aligned}$ |  |  |  |  |  |  | . 0049 | . 0049 | . 00050 | . 00052 |
| 12 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.42 \text { to } 1.25 \\ & 1.251 \text { to } 2.50 \end{aligned}$ |  |  |  |  |  |  | . 0052 | . 0053 | .0054 | $\begin{array}{r} .0055 \\ .0069 \end{array}$ |
| 10 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.50 \text { to } 1.50 \\ & 1.501 \text { to } 3.00 \end{aligned}$ |  |  |  |  |  |  |  |  | .0059 .0073 | $\begin{aligned} & .0060 \\ & .0075 \end{aligned}$ |
| 8 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.62 \text { to } 1.88 \\ & 1.881 \text { to } 3.76 \end{aligned}$ |  |  |  |  |  |  |  |  |  | $\begin{gathered} .0067 \\ .0083 \end{gathered}$ |
| 6 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 0.83 \text { to } 2.50 \\ & 2.501 \text { to } 5.00 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |
| 4 | $\left\{\begin{array}{r}5 \text { to } 15 \\ 16 \text { to } 30\end{array}\right.$ | $\begin{aligned} & 1.25 \text { to } 3.75 \\ & 3.751 \text { to } 7.50 \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |

3B P.D. TOLERANCES

Table 3.8 Pitch diameter tolerances for internal threads of special diameters, pitches, and lengths of engagement, class 3B-Con

| 1.25 | 1.5 | 1.75 | 2 | 2.5 | 3 | 3.5 | 4 | 5 | 6 | 8 | 10 | 12 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.125 | 1.375 | 1.625 | 1.875 | 2.25 | 2.75 | 3.25 | 3.75 | 4.5 | 5.5 | 7 | 9 | 11 |
| 1.375 | 1.625 | 1.875 | 2.25 | 2.75 | 3.25 | 3.75 | 4.5 | 5.5 | 7 | 9 | 11 | 13 |

## LEGENDS

1. These values do not agree with and shall not be used in place of any tabulated values for the UNC, UNF, and 8 UN thread series in table 2.21 .
2. Class 3 B (internal thread) tolerances in this table for 5 to 15 pitches are based on 9 pitches and are obtained by multiplying the class 2 A (extcrnal thrcad) tolcrances for 9 pitches taken to six decimal places by a factor of 0.975 . (See table 2.19.)
3. Class 3B tolerances in this table for 16 to 30 pitches are obtained by multiplying the class 2 A (external thread) tolerances for 9 pitches taken to six decimal places by a factor of 1.21875 (obtained by multiplying the 0.975 factor by 1.25 .) (See table 2.19.) For lengths of engagement not tabulated, see par. 7.3, p. 3.03.
4. Pitches listed are those used most commonly and are recommended. Where intermediate pitches are specified, the formula in par. 7.3, p. 3.03, should be applied.
5. Tolerances are tabulated only for combinations of diameter, pitch, and length of engagement which are considered to be generally used. For other combinations encountered, see Design of Special Threads in appendix A5.


Table 3.9. Minor diameter tols rances for internal special screw threads, classes $1 B$ and 2B
(UNS threads, see par. 10, p. 3.05.)

| Tolerance based on basic major diameter of $\rightarrow$ |  |  |  | 0.060 | 0.073 | 0.086 | 0.099 | 0.112 | 0.125 | 0.138 | 0.164 | 0.190 | 0.216 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| For diameter range Above $\rightarrow$ |  |  |  | 0.053 | 0.066 | 0.079 | 0.092 | 0.105 | 0.118 | 0.131 | 0.151 | 0.177 | 0.203 | All larger diameters |
| To and including $\rightarrow$ |  |  |  | 0.066 | 0.079 | 0.092 | 0.105 | 0.118 | 0.131 | 0.151 | 0.177 | 0.203 | 0.233 |  |
| Threads per inch | Tolerance ratios | Length of engagement in terms of diameter ${ }^{3}$ |  |  |  | B, 2B |  | Minor diam | tolcrance |  | $1 \mathrm{~B}, 2 \mathrm{~B}$ |  |  |  |
|  |  | Above | to and including |  |  |  |  |  |  |  |  |  |  |  |
| 80 |  |  |  | in | in | in | in | in | in | in | in | in | in | in |
|  | 0.5 | 0 | 0.33 D | 0.0035 | 0.0029 | 0.0025 | 0.0022 | 0.0020 | 0.0018 | 0.0017 | 0.0016 | 0.0016 | 0.0016 | 0.0016 |
|  | 0.75 | 0.33 D | 0.67 D | . 0049 | . 0044 | . 0038 | . 0034 | . 0030 | . 0028 | . 0026 | . 0023 | . 0023 | . 0023 | . 0023 |
|  | 1.0 | 0.67 D | 1.5 D | . 0049 | . 0049 | . 0049 | . 0045 | . 0040 | . 0037 | . 0034 | . 0031 | . 0031 | . 0031 | . 0031 |
|  | 11.25 | 1.5 D | 3 D | . 0049 | . 0049 | . 0049 | . 0049 | . 0049 | . 0046 | . 0043 | . 0039 | . 0039 | . 0039 | . 0039 |
| 72 | 0.5 | 0 | 0.33 D | . 0039 | . 0033 | . 0029 | . 0026 | . 0023 | . 0021 | . 0020 | . 0017 | . 0017 | . 0017 | . 0017 |
|  | 0.75 | 0.33 D | ${ }_{0} 0.67 \mathrm{D}$ | . 0055 | . 0049 | . 0043 | . 0038 | . 0035 | . 0032 | . 0029 | . 00226 | . 0026 | . 0026 | . 0026 |
|  | 1.0 1.25 | 0.67 D 1.5 D | ${ }_{3} 1.5 \mathrm{D}$ | . 0055 | . 00055 | . 0055 | . 0051 | . 0046 | . 0042 | .0039 .0049 | . 00044 | . 0034 | .0034 .0042 | . 00034 |
| 64 |  |  | 0.33 D | . 0045 | . 0038 | . 0033 | . 0029 | . 0027 | . 0024 | . 0023 | . 0020 | . 0019 | . 0019 | . 0019 |
|  | 0.75 | 0.33 D | 0.67 D | . 0062 | . 0057 | . 0049 | . 0044 | . 0040 | . 0037 | . 0034 | . 0030 | . 0028 | . 0028 | . 0028 |
|  | 1.0 | 0.67 D | 1.5 D | . 0062 | . 0062 | . 0062 | . 0059 | . 0053 | . 0049 | . 0045 | . 0040 | . 0038 | . 0038 | . 0038 |
|  | 11.25 | 1.5 D | $3 D$ | . 0062 | . 0062 | . 0062 | . 0062 | . 0062 | . 0061 | . 0057 | . 0050 | . 0048 | . 0048 | . 0048 |
| 56 | 0.5 | 0 | 0.33 D |  | . 0044 | . 0038 | . 0034 | . 0031 | . 0029 | . 0026 | . 0023 | . 0022 | . 0022 | . 0022 |
|  | 0.75 | 0.33 D | 0.67 D |  | . 0066 | . 0057 | . 0051 | . 0046 | . 0043 | . 0040 | . 0035 | . 0032 | . 0032 | . 0032 |
|  | - 1.0 | ${ }_{0}^{0.67 D}$ | ${ }_{3}^{1.5 D}$ |  | . 0070 | . 00070 | . 00068 | . 00672 | . 0057 | . 0053 | . 0047 | . 0043 | . 0043 | . 0043 |
|  | 11.25 | 1.5 D | $3 D$ |  | . 0070 | . 0070 | . 0070 | . 0070 | . 0070 | . 0066 | . 0059 | . 0054 | . 0054 | . 0054 |
| 48 | $\int 0.5$ | 0 | 0.33 D |  |  | . 0045 | . 0040 | . 0037 | . 0034 | . 0032 | . 0028 | . 0025 | . 0025 | . 0025 |
|  | ${ }_{1}^{0.75}$ | ${ }_{0} 0.33 \mathrm{D}$ | 0.67 D |  |  | . 00068 | . 00061 | . 0055 | . 0051 | . 0047 | . 0042 | . 0038 | . 0038 | . 0038 |
|  | \| 1.0 | 0.67 D 1.5 D | 1.50 |  |  | . 00082 | . 0081 | .0074 .0082 | . 0068 | .0063 .0079 | . 0056 | . 0051 | . 00050 | .0050 .0062 |
| 44 |  | 0 | 0.33 D |  |  | . 0050 | . 0044 | . 0040 | . 0037 | . 0035 | . 0031 | . 0028 | . 0028 | . 0028 |
|  | 0.75 | 0.33 D | 0.67 D |  |  | . 0075 | . 0067 | . 0061 | . 0056 | . 0052 | . 0046 | . 0042 | . 0041 | . 0041 |
|  | 1.0 | 0.67 D | 1.5 D |  |  | . 0090 | . 0089 | . 0081 | . 0075 | . 0070 | . 0062 | . 0056 | . 0055 | . 0055 |
|  | 1.25 | 1.5 D | 3 D |  |  | . 0090 | . 0090 | . 0090 | . 0090 | . 0087 | . 0077 | . 0070 | .C069 | . 0069 |
| 40 | 0.5 | 0 | 0.33 D |  |  |  | . 0049 | . 0045 | . 0041 | . 0039 | . 0034 | . 0031 | . 0030 | . 0030 |
|  | 0.75 | 0.33 D | 0.67 D |  |  |  | . 0074 | . 0067 | . 0062 | . 0058 | . 0051 | . 0047 | . 0045 | . 0045 |
|  | 1.0 | 0.67 D | 1.5 D |  |  |  | . 0098 | . 0090 | . 0083 | . 0077 | . 0068 | . 0062 | . 0060 | . 0060 |
|  | 1.25 | 1.5 D | $3 D$ |  |  |  | . 0098 | . 0098 | . 0098 | . 0096 | . 0086 | . 0078 | . 0075 | . 0075 |
| 36 | 0.5 | 0 | 0.33 D |  |  |  |  | . 0050 | . 0046 | . 0043 | . 0038 | . 0035 | . 0033 | . 0033 |
|  | 0.75 | 0.33 D | 0.67 D |  |  |  |  | . 0075 | . 0069 | . 0065 | . 0058 | . 0052 | . 0050 | . 0050 |
|  | 1.0 | 0.67 D | 1.5 D |  |  |  |  | . 0100 | . 0093 | . 0086 | . 0077 | . 0070 | . 0066 | . 0066 |
|  | 1.25 | 1.5 D | 3 D |  |  |  |  | . 0109 | . 0109 | . 0108 | . 0096 | . 0087 | . 0082 | . 0082 |
| 32 | 0.5 | 0 | 0.33 D |  |  |  |  |  |  | . 0049 | . 0043 | . 0039 | . 0037 | . 0037 |
|  | 0.75 | 0.33 D | 0.67 D |  |  |  |  |  |  | . 0073 | . 0065 | . 0059 | . 0056 | . 0056 |
|  | 1.0 | 0.67 D | 1.5 D |  |  |  |  |  |  | . 0098 | . 0087 | . 0079 | . 0074 | . 0074 |
|  | 1.25 | 1.5 D | $3 D$ |  |  |  | - |  |  | . 0122 | . 0108 | . 0099 | . 0092 | . 0092 |
| 28 | 0.5 |  | 0.33 D |  |  |  |  |  |  |  |  | . 0045 | . 0042 | . 0042 |
|  | 0.75 | 0.33 D | 0.67 D |  |  | Tole | ces in th | range |  |  |  | . 0068 | . 0063 | . 0063 |
|  | 1.0 1.25 | ${ }^{0.67 D}$ | ${ }_{3 D}^{1.5 D}$ |  |  |  |  |  |  | $\longrightarrow$ |  | . 0091 | . 0084 | . 0084 |
|  | 1.25 | 1.5 D | $3 D$ |  |  |  | ply to threads. |  |  |  |  | . 0113 | . 0105 | . 0105 |
| 27 | 0.5 |  | 0.33 D |  |  |  |  |  |  |  |  | . 0047 | . 0044 | . 0044 |
|  | 0.75 1.0 | 0.33 D | 0.67 D |  |  |  |  |  |  |  |  | . 0071 | . 0065 | . 0065 |
|  | 1.05 | 0.67 D $1.5 D$ | ${ }_{3 D}^{1.5 D}$ |  |  |  |  |  |  |  |  | . 00994 | . 0087 | .0087 .0109 |
| 24 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | ${ }_{0}^{0.33 D}$ |  |  |  |  |  |  |  |  | . 0053 | . 0049 | . 0048 |
|  | 1.0 | ${ }_{0.67 \mathrm{D}}$ | 1.5 D |  |  |  |  |  |  |  |  | . 0106 | . 0009 | . 00073 |
|  | 1.25 | 1.5 D | $3 D$ |  |  |  |  |  |  |  |  | . 0132 | . 0122 | . 0121 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |


| Tolerance ratios | Length of engagement in terms of diameter |  | Minor diameter tolerances <br> (Not applicable to diameters less than 0.25 in ) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | A bove | to and including | $\begin{aligned} & 20 \\ & \text { tpi } \end{aligned}$ | $\begin{aligned} & 18 \\ & \text { tpi } \end{aligned}$ | $\begin{aligned} & 16 \\ & \text { tpi } \end{aligned}$ | $\begin{aligned} & 14 \\ & \text { tpi } \end{aligned}$ | $\begin{aligned} & 13 \\ & \text { tpi } \end{aligned}$ | $\frac{12}{\text { tpi }}$ | $\begin{aligned} & 11 \\ & \text { tpi } \end{aligned}$ | $\begin{aligned} & 10 \\ & \text { tpi } \end{aligned}$ | $\stackrel{9}{\text { tpi }}$ | $\stackrel{8}{\text { tpi }}$ | ${ }_{\text {tpi }}^{7}$ | $\stackrel{6}{\text { tpi }}$ | $\stackrel{5}{\text { tpi }}$ | $\begin{aligned} & 4.5 \\ & \text { tpi } \end{aligned}$ | $\stackrel{4}{\operatorname{tpi}}$ |
| 0.5 | 0 | 0.33 D | in 0.0058 | ${ }_{\text {in }}^{\text {in }}$ | ${ }_{\text {in }}^{\text {in }}$ | in 0.0079 | in 0.0085 | in 0.0090 | ${ }_{0}^{\text {in }}$ | $\xrightarrow{\text { in }}$ | ${ }_{0}^{\text {in }}$ | ${ }_{0}^{\text {in }}$ | ${ }_{\text {in }}$ | ${ }_{0}^{\text {in }}$ | ${ }_{0}^{\text {in }}$ | in 0.0179 | in 0.0188 |
| 0.75 | 0.33 D | 0.67 D | 0.0086 | 0.0095 | 0.0106 | 0.0118 | 0.0128 | 0.0135 | 0.0146 | 0.0158 | 0.0171 | 0.0188 | 0.0207 | 0.0230 | 0.0255 | 0.0268 | 0.0281 |
| 1.0 | 0.67 D | 1.5 D | 0.0115 | 0.0127 | 0.0141 | 0.0158 | 0.0170 | 0.0180 | 0.0194 | 0.0210 | 0.0228 | 0.0250 | 0.0276 | 0.0306 | 0.0340 | 0.0358 | 0.0375 |
| 1.25 | 1.5 D | 3 D | 0.0144 | 0.0159 | 0.0176 | 0.0198 | 0.0213 | 0.0225 | 0.0242 | 0.0262 | 0.0286 | 0.0312 | 0.0344 | 0.0382 | 0.0425 | 0.0448 | 0.0469 |

[^13]If the minor diameter tolerance as selected from this table is less than the pitch diameter tolerance, use the latter. See Design of Special Threads in appendix A5.

Table 3.10. Minor diameter tolerances for internal special screw threads, class SB
(UNS threads, see par. 10, p. 3.05.)


[^14]Table 3.10. Minor diameter tolerances for internal special screw threads, class 3B-Continued
(UNS threads, see par. 10, p. 3.05.)


[^15]Table 3.11. Consolidated method for the calculation of dimensions of special threads

| External thread |  |  |  |  | Internal thread |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Thread element | Class 1A | Class 1ar | Class 2A | Class 3A | Class 1B | Class 2B | Class 3B | Thread element |
| Max major dia | Nominal size minus allowance |  |  | Nominal size | Nominal size |  |  | Min major dia |
|  | Table 3.2 | Tabulated on p. 3.03 | Table 3.2 |  |  |  |  |  |
| Tolerance on major dia | Use values tabulated on $\mathfrak{p} .3 .04$ or compute in accordance with directions for designing special threads in appendix A5. APPLY MINUS. |  |  |  | $H / 6(0.1667 H)$, table 2.1 , col. 8 APPLY PLUS. |  |  | Tolerance on major dia |
| Max pitch dia | Subtract 0.75 H , table 2.1 , col. 14 , from maximum major diameter shown above. |  |  |  | Subtract 0.75 H , table 2.1, col. 14 , from minimum major diameter shown above. |  |  | Min pitch dia |
| Tolerance on pitch dia | Table 3.3 APPLY MINUS | Table 3.3 APPLY MINUS | Table 3.4 APPLY MINUS | Table 3.5 <br> APPLY MINUS | Table 3.6 APPLY PLUS | Table 3.7 <br> APPLY PLUS | Table 3.8 <br> APPLY PLUS | Tolerance on pitch dia |
| Max minor dia | Subtract $17 H / 12(1.4167 H)$, table 2.1 , col. 18 , from maximum major diameter. This is a reference dimen sion only. |  |  |  | Subtract 1.25 H , table 2.1 , col. 17 . from the basic major diameter and round off to the nearest 0.001 in for sizes 0.138 in and larger. For class 3B a cipher is added to yield four decimal places. |  |  | Min minor dia |
| Tolerance on minor dia | $H / 12(0.0833 H)$, table 2.1 , col. 6. APPLY MINUS |  |  |  | For general applications use value for $0.67 D$ to $1.5 D$ length of engagement from table 3.9 or 3.10 . For specific applications use values for applicable length of engagement or compute in accordance with directions for design-ing special threads in appendix A5. APPLY PLUS to four-place value of min minor diameter and round off for classes 1 B and 2 B values to the nearest 0.001 in for sizes 0.138 in and larger; class 3 B values are to be rounded off to the nearest 0.0001 in . |  |  | Tolerance on minor dia |



Figure 3.12. Thread dimensions to be determined for a special thread.

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# UNITED STATES DEPARTMENT OF COMMERCE NATIONAL BUREAU OF STANDARDS 

## HANDBOOK H28

SCREW-THREAD STANDARDS<br>FOR FEDERAL SERVICES

$$
\begin{gathered}
\text { SECTION } 4 \\
1969 \\
\text { CONTROLLED RADIUS ROOT SCREW THREADS } \\
\text { UNJ SYMBOL }
\end{gathered}
$$

This section of Handbook H28 has not as yet been fully coordinated. As soon as coordination has been completed, it will be issued as a separate document.

Section 4 will be in general agreement with Military Specification MIL-S-8879, Screw Threads, Controlled Radius Root with Increased Minor Diameter; General Specification for.

Also in process of coordination is USAS B1.15 which is the industry standard for the UNJ thread.

# UNITED STATES DEPARTMENT OF COMMERCE National bureau of standards 

## HANDBOOK H28

## SCREW-THREAD STANDARDS

FOR FEDERAL SERVICES
SECTION 5
1969
UNIFIED MINIATURE SCREW THREADS

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## 1. INTRODUCTION

This section is in general agreement with United States of America Standards Institute (USASI) Standard USA B1.10, Unified Miniature Screw Threads, published by The American Society of Mechanical Engineers, United Engineering Center, 345 East 47th Street, New York, N.Y. 10017. The latest revision should be consulted when referring to this USA standard. As of date of issue of this part of H28, USA B1.10-1958 is the latest revision.

The thread sizes shown in this section are those endorsed by the American-British-Canadain Conference as the basis for a Unified standard among the inch-using countries.

This section presents a thread series known as Unified Miniature Screw Threads and is intended for general purpose fastening screws and similar uses in watches, instruments, and miniature mechanisms. The series covers a diameter range from 0.30 to 1.40 mm ( 0.0118 to 0.0551 in ) and thus supplements the Unified thread series that begin at 0.060 in.

The 14 sizes are systematically distributed, providing a uniformly proportioned selection over the entire range. They are alternately separated into two categories. The primary sizes are selections made in the interest of simplification and are those to which it is recommended that usage be confined whenever the
circumstances of design permit. For more restrictive conditions, the secondary sizes are available.

The diameter-pitch combinations have been determined to provide both maximum strength against stripping and optimum conditions for manufacture on an interchangeable basis.

The values of all dimensions are supplied in both metric and inch units. The standard being basically metric, only the metric values of the nominal diameters and pitches are rational. Consequently, metric units are stipulated for all formulas and the inch dimensions derived by conversion of the unrounded metric values, using the conversion factor $25.4 \mathrm{~mm} / \mathrm{in}$.

Use of this series is recommended on all new products in place of the many improvised and unsystematized sizes now in existence that have never arrived at broad acceptance nor recognition by any standardization bodies.

## 2. THREAD FORM

2.1. Basic Thread Form-The theoretical profile on which the design forms of the threads covered by this section are based is, except for one element, the Unified basic thread form as specified in section 2 and shown in figure 5.1. In exception is thread height, for which a basic value of $0.48 p$ is used instead of


Figure 5.1. Basic thread form, Unified Miniature threads, UNM.
$0.54127 p(=5 H / 8)$. Selection of this value is based on the extensive simplification that it affords throughout the calculations for this standard. Resulting coefficients in the formulas for many of the other thread dimensions derived from this property thereby become simple, finite multiples of the lowest common denominator (40) of the fractional equivalents of all but two of the metric pitches, thus yielding values for the majority of metric dimensions that are finite within the decimal place limits of the tables. Also, the calculation of inch equivalents from the terminal metric values is thereby simplified and discrepancies between the metric and inch tables kept to a minimum. This modification will not affect interchangeability with product made to any other standards retaining $0.54127 p$, as the resulting difference is negligible and completely offset by practical considerations in tapping, full internal thread heights being invariably avoided in these small sizes to escape excessive tap breakage.
2.2. Design Forms of Threads.-The design forms (maximum material condition) of external and internal Unified Miniature threads are shown in figure 5.2.
2.3. Basic Thread Data.-The formulas for the various features of the thread form are as follows:


| Design thread form |  |  |
| :---: | :---: | :---: |
| Addendum of external thread | $h_{u s}$ | $0.32476 p$. |
| Height of external thread_ | $h_{s}$ | $0.56 p$ |
| Flat at crest of external thread | $F_{c s}$ |  |
| Radius at root of external thread | $r_{r s}$ | $0.158 p$ (approx.). |
| Depth of thread engagement | $h_{e}=h_{b}$ | $0.48 p$. |
| Height of internal thread | $h_{n}$ | $0.516 p$. |
| Flat at crest of internal thread_ | $F_{c n}$ | $0.32074 p$. |
| Radius at root of internal thread | $r_{r n}$ | $0.072 p$ (approx.). |

${ }^{a}$ The formulas are applied to the metric values of $p$. Tabulated inch dimensions are derived from the unrounded metric dimensions.
${ }^{b}$ This item is listed for reference only. For the present standard all dependent details of thread form and dimensions are based on a height of $0.48 p$.
The corresponding thread data for the various standard pitches are shown in table 5.3. The formulas for basic and design thread sizes are as follows:

| Dimension | Symbol | Formula |
| :---: | :---: | :---: |
| Major diameter, nominal and basic. | D |  |
| Major diameter of external thread. | $D_{s}$ | D. |
| Major diameter of internal thread. | $D_{n}$ | $\begin{gathered} D-2 h_{b}+2 h_{n}= \\ D+0.072 p . \end{gathered}$ |
| Pitch diameter, basic | $E$ | $\begin{aligned} & D-2 h_{a b}= \\ & D-0.64952 p \end{aligned}$ |
| Pitch diameter of external thread. | $E_{s}$ | $E$. |
| Pitch diameter of internal thread. | $E_{n}$ | $E$. |
| Minor diameter, basic | $K$ | $D-2 h_{b}=D-0.96 p$. |
| Minor diameter of external thread. | $K_{s}$ | $D-2 h_{s}=D-1.12 p$ |
| Minor diameter of internal thread. | $K_{n}$ | $K$. |



Figure 5.2. Unified Miniature internal and external screw thread design forms (maximum-material condition).

Table 5.3. Thread form data, Unified Miniature screw threads, UNM

a In all subsequent tables these values are rounded to the nearest whole number.

Table 5.4. Basic and design sizes, Unified Miniature thread series, UNM

| Size designation |  | Pitch, p | $\begin{gathered} \text { Basic } \\ \text { major } \\ \text { diameter, } \\ D \end{gathered}$ | Basic pitch diameter, $E=$ $D=0.64952 p$ | Minor diameter external threads, $K_{\mathrm{s}}=$ $D-1.12 p$ | $\begin{aligned} & \begin{array}{c} \text { Minor diameter } \\ \text { internal } \end{array} \\ & \text { threads, } K_{n}= \\ & K=D-0.96 p \end{aligned}$ | Major diameter internal threads, $D_{n}=$ $D+0.072 p$ | Lead angle at basic pitch diameter, $\lambda$ |  | Sectional area at minor diameter at D-1.28p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Primary | Secondary |  |  |  |  |  |  |  |  |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  | 10 |
| .30UNM |  | $m m$  <br>   <br> .080  <br> .090  <br> .100  <br>   <br>   <br> 100  <br> .125  | mm | mm | mm | mm | mm | deg | min | $\mathrm{mm}^{2}$ |
|  |  |  | mm 0.300 | 0.248 | 0.210 | 0.223 | 0.306 | 5 | 52 |  |
|  | .35UNM |  | . 350 | .292 <br> .335 | . 250 | .264.304.304 | .356 <br> .407 | $5 \quad 37$ |  | 0.0307 .0433 |
| . 40 UNM |  |  | . 400 |  | . 288 |  |  | 5 | 37 <br> 26 <br> 6 | . 0581 |
| .50UNM | .45UNM |  | . 450 | . 385 | . 338 | . 354 | . 509 | 4 | 26 | . 0814 |
|  |  |  | . 500 | . 419 | . 360 | . 380 |  | 5 |  | . 0908 |
| .60UNM | .55UNM | .125.150 | $\begin{array}{r}.550 \\ 600 \\ \hline\end{array}$ | . 469 | . 410 | . 430 | . 559 | $4 \quad 51$ |  | .1195.1307 |
|  |  |  | .600.700 | . 503 | . 432 | . 456 | . 611 | $5 \quad 26$ |  |  |
|  | .70UNM | . 175 |  | . 586 | . 504 | . 532 | . 713 | 5 | 26 | .1307 .1780 |
| .80UNM | .90UNM | $\begin{aligned} & .200 \\ & .225 \end{aligned}$ | $\begin{array}{r} .800 \\ .900 \end{array}$ | . 670 |  |  | . 814 | $5 \quad 26$ |  | . 232 |
| 1.00UNM |  | . 250 | 1.000 | . 838 | . 720 | . 760 | 1.018 | 5 | 26 | . 363 |
|  | 1.10UNM | $\begin{array}{r} .250 \\ .250 \\ .300 \end{array}$ | 1.100 | . 938 | . 820 | . 860 | 1.118 | 4 | 51 | . 478 |
| 1.20UNM |  |  | $\begin{aligned} & 1.200 \\ & 1.400 \end{aligned}$ | $\begin{aligned} & 1.038 \\ & 1.205 \end{aligned}$ | . 920 | . 960 | 1.218 | 4 | 23 | . 608 |
|  | 1.40UNM |  |  |  | 1.064 | 1.112 | 1.422 | 432 |  | . 811 |
|  |  | threads per inch |  |  |  |  |  |  |  |  |  |
|  |  | 318 | $\stackrel{i n}{0}_{0.0118}$ | in | in | in | in | deg | $\min$ | sq in $\times 10^{-4}$ |
| .30UNM |  |  |  | 0.0098 | 0.0083 | 0.0088 | 0.0120 | 5 |  |  |
|  | . 35 UNM | 282 | . 0138 | . 0115 | . 0098 | . 0104 | . 0160 | 55 |  | .671.901 |
| $.50 \mathrm{UNM}$ |  | 254 | . 0157 | .0132.0152.0165 | . 0133 | . 0120 |  | 5 | 2644 |  |
|  | .45UNM | 254203 | $\begin{aligned} & .0177 \\ & .0197 \end{aligned}$ |  |  | . 0139 | . 0200 | 4 |  | 1.2621.407 |
|  |  |  |  |  |  | . 0150 |  | $5 \quad 26$ |  |  |
| . 60 UNM | .55UNM | 203 | . 0217 | . 0185 | . 0161 | . 0169 | . 0220 | $4 \quad 51$ |  | 1.8522.032.763.604.56 |
|  |  | 169 | . 02236 |  | . 0170 |  | . 0240 | 5 | 26 |  |
|  | .70UNM | 145 | . 0276 | . 0231 | . 0198 | . 0209 | . 0281 | 5 | 26 |  |
| .80UNM | .-90UNM | 127 113 | . 0315 | .0264 | .0227 | . 02369 | . 0321 | 5 5 | 26 26 |  |
| 1.00UNM <br> 1.20UNM |  | $\begin{array}{r} 102 \\ 102 \\ 102 \\ 85 \end{array}$ | $\begin{aligned} & .0394 \\ & .0433 \\ & .0472 \\ & .0551 \end{aligned}$ | $\begin{array}{r} .0330 \\ .0369 \\ .0409 \\ .0474 \end{array}$ | $\begin{array}{r} .0283 \\ .0323 \\ .0362 \\ .0419 \end{array}$ | $\begin{aligned} & .0299 \\ & .0339 \\ & .0378 \\ & .0438 \end{aligned}$ | $\begin{array}{r} .0401 \\ .0440 \\ .0480 \\ .0560 \end{array}$ | 5444 | 26512332 | 5.637.419.4312.57 |
|  | 1.10UNM |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
|  | 1.40UNM |  |  |  |  |  |  |  |  |  |

Table 5.5. Limits of size and tolerances, Unified Miniature thread series, UNM

| Size designation |  | Pitch | External threads |  |  |  |  |  |  |  | Internal threads |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Major diameter limits | Pitch diameter limits |  |  | Minor diameter limits |  | Minor diameter limits |  |  | Pitch diameter limits |  |  | Major diameter limits |  |
| Primary | Secondary |  | Max. | Min. | Tol. | Max. | Min. | Tol. | Max. ${ }^{\text {a }}$ | Min. ${ }^{\text {b }}$ | Min. | Max. | Tol. | Min. | Max. | Tol. | Min.e | Max. ${ }^{\text {b }}$ |
| 1 | 2 |  | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 |
| .30UNM |  | $m m$0.080 | $m m$0.300 | mm | mm | mm | ${ }_{0}^{m m}$ | ${ }_{0}^{m m}$ | mm0.210 | mm ${ }^{\text {m }}$ | ${ }_{0}^{m m}$ | $m m$ | ${ }^{72 m}$ | mm | mm | ${ }_{0}^{m m} 0.014$ | mm0.306 | mm |
|  |  |  |  | 0.284 | 0.016 | 0.248 |  |  |  | 0.189.228 |  | 0.260.305 | 0.037 | 0.248 | 0.262 |  |  | 0.327 |
|  | .35UNM | . 090 | . 350 | . 333 | . 017 | . 292 | . 277 | . 015 | . 250 |  | $\begin{array}{r}0.223 \\ .264 \\ \hline\end{array}$ |  | . 041 |  |  | . 015 | . 356 | . 380 |
| .40UNM | . 45 UNM | . 100 | . 450 | . 432 | . 018 | . 385 | . 369 | . 016 | . 338 | . 314 | . 354 | . 398 | . 044 | $\begin{aligned} & .292 \\ & .335 \end{aligned}$ | $\begin{array}{llll}.351 & .016 & .407 & .432 \\ .401 & .016 & .457 & .482\end{array}$ |  | . 407 |  |
| .50UNM |  | . 125 | . 500 | . 479 | . 021 | .385 .419 | . 401 | . 018 | . 360 | . 332 | . 380 | . 432 | . 052 | .419 . 437 . 018 . 509 . 538 |  | . 018 | . 509 |  |
|  | .55UNM | .125.150 | . 550 | . 529 | . 021 | . 469 | . 483 | . 020 | . 432 |  |  |  | . 052 | . 469 | . 487 | . 018 |  | . 5888 |
| .60UNM |  |  | . 600 | . 576 | . 024 | . 503 |  |  |  | . 400 | . 456 | . 516 | . 060 | . 503 | . 523 | . 020 | . 611 |  |
|  | .70UNM | .200.225 | . 700 | . 673 | . 027 | . 586 | . 5644 | . 0222 | . 5046 | . 536 | . 608 | . 684 | . 076 | . 670 | . 694 | . 024 | . 814 | .856.962 |
| .80UNM | .90UNM |  | . 900 | . 867 | . 033 | . 754 | . 728 | . 026 | . 648 | . 604 | . 684 | . 768 | . 084 | . 754 | . 780 | . 026 | . 916 |  |
| $\begin{aligned} & 1.00 \mathrm{UNM} \\ & 1.20 \mathrm{UNM} \end{aligned}$ |  | $\begin{aligned} & .250 \\ & .250 \\ & .250 \\ & .300 \end{aligned}$ | 1.000 | . 964 | . 036 | . 838 | . 810 | . 028 | . 720 | . 672 | . 760 | . 852 | . 092 | . 838 | . 866 | . 028 | 1.018 | $\begin{aligned} & 1.068 \\ & 1.168 \\ & 1.268 \\ & 1.480 \end{aligned}$ |
|  | 1.10UNM |  | 1.100 | 1.064 | . 036 | . 938 | . 910 | . 028 | . 820 | . 772 | . 860 | . 952 | . 092 | . 938 | . 966 | . 028 | 1.118 |  |
|  | 1.40UNM |  | 1.200 1.400 | 1.164 1.358 | . 036 | 1.038 1.205 | 1.010 1.173 | . 0238 | 1. 92064 | .872 1.008 | . 1.112 | 1.052 1.220 | .092 .108 | 1.038 1.205 | 1.066 1.237 | . 028 | 1.218 1.422 |  |
|  |  | threads per in | ${ }_{0}^{\text {in }} 0.0118$ | in 0.0112 |  | in0.0098 | ${ }_{0}^{\text {in }} 0.0092$ | in0.0006 |  | ${ }_{0}^{\text {in }} 0.0074$ | in0.0088 | in0.0102 | in0.0014 | in0.0098 | ${ }_{0}^{\text {in }} 0.0104$ | ${ }_{0}^{\text {in }}$ | in0.0120 | in ${ }_{0}$ |
| .30UNM |  | 318282 |  |  | 0.0006 |  |  |  | in 0.0083 |  |  |  |  |  |  |  |  |  |
| $.40 \mathrm{UNM}$ | .35UNM |  | . 0138 | $\begin{array}{r} .0131 \\ .0150 \end{array}$ | . 0007 | $\begin{array}{r} .0115 \\ .0132 \end{array}$ | $\begin{array}{r} .0109 \\ .0126 \end{array}$ | $\begin{aligned} & .0006 \\ & .0006 \end{aligned}$ | $\begin{array}{r} .0098 \\ .0113 \end{array}$ | $\begin{array}{r} .0090 \\ .0104 \end{array}$ | $\begin{aligned} & .0104 \\ & .0120 \end{aligned}$ | $\begin{array}{r} .0120 \\ .0137 \end{array}$ | $.0016$ | $\begin{array}{r} .0115 \\ .0132 \end{array}$ | $\begin{array}{r} .0121 \\ .0138 \\ \hline \end{array}$ | . 00006 | $\begin{array}{ll}.0140 & .0149 \\ .0160 & .0170\end{array}$ |  |
|  |  | 254 | . 0157 |  | . 0007 |  |  |  |  |  |  |  |  |  |  | . 0006 |  |  |  |
|  | .45UNM | 254 203 | . 0177 | .0170 .0189 | . 00007 | . 0152 | .0145 .0158 | . .00007 | .0133 .0142 | . 0124 | .0139 .0150 | . 0170 | . 0020 | . 010165 | .0158 | . 00006 | . 0180 | . .01912 |
| $\begin{aligned} & .60 \mathrm{UNM} \\ & .80 \mathrm{UNM} \end{aligned}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  | $\begin{aligned} & .0007 \\ & .0008 \\ & .0009 \\ & .0009 \\ & .010 \end{aligned}$ |  |  |
|  | .55UNM | $\begin{aligned} & 203 \\ & 169 \\ & 145 \\ & 127 \\ & 113 \end{aligned}$ | . 0217 | $\begin{aligned} & .0208 \\ & .0227 \\ & .0265 \\ & .0303 \\ & .0341 \end{aligned}$ | . 00009 | $\begin{aligned} & .0185 \\ & .0198 \\ & .0231 \\ & .0264 \\ & .0297 \end{aligned}$ | $\begin{aligned} & .0177 \\ & .0190 \\ & .0222 \\ & .0254 \\ & .0287 \end{aligned}$ | $\begin{aligned} & .0008 \\ & .0008 \\ & .0009 \\ & .0010 \\ & .0010 \end{aligned}$ | $\begin{aligned} & .0161 \\ & .0170 \\ & .0198 \\ & .0227 \\ & .0255 \end{aligned}$ | $\begin{aligned} & .0150 \\ & .0157 \\ & .0181 \\ & .02211 \\ & .0238 \end{aligned}$ | $\begin{aligned} & .0169 \\ & .0180 \\ & .0209 \\ & .0239 \\ & .0269 \end{aligned}$ | $\begin{aligned} & .0190 \\ & .0203 \\ & .0236 \\ & .0269 \\ & .0302 \end{aligned}$ | $\begin{aligned} & .0021 \\ & .0023 \\ & .0027 \\ & .0930 \\ & .0033 \end{aligned}$ | $\begin{aligned} & .0185 \\ & .0198 \\ & .0231 \\ & .0264 \\ & .0297 \end{aligned}$ | $\begin{aligned} & .0192 \\ & .0206 \\ & .0240 \\ & .0233 \\ & .0307 \end{aligned}$ |  | . 02220 | . 0231 |
|  | .70UNM |  | . 02786 |  | . 00011 |  |  |  |  |  |  |  |  |  |  |  | . 0281 | . 0295 |
|  |  |  | . 0315 |  | . 0012 |  |  |  |  |  |  |  |  |  |  |  | . 0321 | . 0337 |
|  | .90UNM |  | . 0354 |  | . 0013 |  |  |  |  |  |  |  |  |  |  |  | . 0361 | . 0379 |
| 1.00UNM |  | 102 | . 0394 | . 0380 | . 0014 | . 0330 | . 0319 | . 0011 | . 0283 | . 0265 | . 0299 | . 0335 | . 0036 | . 0330 | . 0341 | . 0011 | . 0401 | . 0420 |
|  | 1.10UNM | 102 | . 0433 | . 0419 | . 0014 | . 0369 | . 0358 | . 0011 | . 0323 | . 0304 | . 0339 | . 0375 | . 0036 | . 0369 | . 0380 | . 0011 | . 0440 | . 0460 |
| 1.20UNM | 1.40UNM | 102 85 | . 0472 | . 04588 | . 00014 | . .04097 | . 039462 | . 00012 | .0362 .0419 | . 03438 | .0378 .0438 | . 04184 | . 00036 | .0409 .0472 | . 042487 | .0011 | . 04860 | .0499 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

 b This limit is provided for reference only. In practice, the form of the threading tool is relied upon for this limit. Control by gaging is not imposed.
e This limit is provided for reference only, and is not gaged. For gaging, the maximum major diameter of the external lhread is applied.


## 3. UNIFIED MINIATURE THREAD SERIES

The diameter-pitch eombinations which constitute the Unified Miniature thread series, and the design sizes, are those shown in table 5.4. All threads are of the single (single-start) type.

## 4. CLASSIFICATION AND TOLERANCES

4.1. Classification.-There is established herein only one class of thread, with zero allowance on all diameters.
4.2. Tolerances,-All tolerances governing limits of size are based on functions of the pitch only and apply to lengths of engagement from 0.67 to 1.5 times the nominal diameter. (See note, table 5.5.) The limits of size resulting from the application of the speeified tolerances are illustrated in figure 5.6. Length of engagement and nominal diameter have not been incorporated in any of the tolerance formulas in view of the following: (1) In the small thread sizes covered by this standard, lengths of engagement appreciably below or above the range covered by the formulas are seldom employed. (2) Funetional fitness in these small sizes is dependent principally upon the properties of the thread rather than the size of the threaded member. (3) Total tolerances are too small to permit the imposition of minor order modifications.

Tolerances are tabulated in table 5.5 and are based on the following formulas:

|  | External thread ${ }^{d}$ | Internal thread $^{b}$ |
| :--- | :---: | :---: |
| Major diameter_-- | $0.12 p+0.006$ | $0.168 p+0.008^{d}$ |
| Pitch diameter_-- | $0.08 p+0.008$ | $0.08 p+0.008$ |
| Minor diameter_-- | $0.16 p+0.008^{c}$ | $0.32 p+0.012$ |

NOTE: Metric units (millimeters) apply in these formulas. Inch tolerances are not derived by direct conversions of the metric values but are the differences between the rounded-off limits of size in inch units.
${ }^{a}$ Tolerances on external threads are applied to the design sizes in the minus direction.
${ }^{b}$ Tolerances on internal threads are applied to the design sizes in the plus direction.
c This formula is for reference only. In practice, the form of the threading tool is relied upon for controling the minimura minor diameter, and this limit is not gaged, except in confirming new tools.
${ }^{d}$ This formula is for reference only and is comprised of the pitch diameter tolerance and an extension of the thread form of $0.08 p$ beyond the basic major diameter. In practice, this limit is applied to the threading tool (tap) and is not gaged on the product.

## 5. COA'TED THREADS

It is not within the scope of this standard to make recommendations for thicknesses of, or to specify limits for, coatings. However, it is obvious that in these small sizes any eoatings applicd must be kept thin because of the smallness of the threads. Generally, the coatings employed in praetiee are confined to those of the elcetroplated or oxide types and are limited to a flash thickness. For applieations where these eoatings are inadequate the produet is usually made of a corrosion-resistant material, thereby avoiding the problems attendant to providing for heavier coatings. However, where coatings of a measurable thiekness are required, it is essential that they be included within the maximum-material limits sinee no allowance is provided between these limits of the external and internal thread. In other words, the maximum material limits given in this standard apply to both uneoated and coated threads.

## 6. THREAD DESIGNATIONS

Screw threads of this series shall be designated on engincering drawings, in specifieations, and on tools and gages (when space permits) by the size designations shown in columns 1 and 2 of table 5.4 in which the symbol UNM designates the Unified Miniature series. To these designations may be affixed, in parentheses, the ineh equivalent of the basie major diameter, but this addition is optional. Thus, for example, the thread size identified by the designation . 80 UNM may also be designated .80UNM (.0315).

## 7. LIMITS OF SIZE

The limits of size of both external and internal threads, resulting from the applieation of the specified tolcrances, are given in table 5.5 in both the metric and English systems and are illustrated in figure 5.6. For hole size limits before tapping, see appendix A3.

## 8. GAGES AND GAGING

The development of a gaging standard for Unified Miniature threads is anticipated after the aecumulation of more experienee with this standard. The following procedures are at present being suecessfully used by some producers:

1. Gaging Of External Threads.--The major diameter of the external thread is inspected by either contact gaging or optieal projection. All other dimensions, sueh as pitch diameter, lead, thread form, and minor diameter are inspected by optieal projection methods. There is presented in figure 5.7 an illustration of a chart which has been found very satisfactory for the optieal projeetion method of


Figure 5.6. Disposition of tolerances and crest clearances, Lnified Miniature threads, ITM.


## . 80 UNM EXTERNAL THREAD

100 x


Figure 5.7. Suggested chart for projection inspection of external Unified Miniature threads, UNM.
inspection of external threads. Inspection at a magnification of 100 is recommended and at this scale the charts should be accurate to within $\pm 0.01$ in on all diameters and on pitches cumulatively up to five.
2. Gaging Of Internal Threads.-The minor diameter of the internal thread is gaged with GO and NOT GO plain cylindrical plug gages. All other elements are checked only for assembleability limits
by means of a GO thread plug gage. For the mini-mum-material limit of the internal thread the accuracy and performance of the tap is relied upon. This implies that the major and pitch diameters of the tap do not exceed the maximum internal thread limits for these elements and disregards overcutting, which is rarely incurred because of the flexibility of these small taps and the manner in which they are generally fluted.

## 9. WIRE MEASUREMENT OF PITCH DIATETER

For information concerning the wire measurement of pitch diameter, see appendix A4.

# UNITED STATES DEPARTMENT OF COMMERCE <br> NATIONAL BUREAU OF STANDARDS <br> HANDBOOK H28 

SCREW-THREAD STANDARDS
FOR FEDERAL SERVICES

SECTION 6
1969

GAGES AND GAGING FOR UNIFIED SCREW THREADS

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This section is in general agreement with United States of America Standards Institute (USASI) Standard USA B1.2 Gages and Gaging for Unified Screw Threads, published by The American Society of Mechanical Engineers, United Engineering Center, 345 East 47 th Street, New York, N.Y. 10017. The latest revision should be consulted when referring to this USA Standard. As of date of issue of this part of H28, USA B1.2-1966 is the latest revision.

A related standard is Commercial Standard CS8, Gage Blanks which is for sale by the Superintendent of Documents, U.S. Government Printing Office, Washington, D.C. 20402. The Industry standard for Gage Blanks is USA B47.1, published by The American Society of Mechanical Engineers. The latest revision should be consulted when referring to these standards. As of date of issue of this part of H28, CS8-61 and USA B47.1-1962 are the latest revisions.

## 1. INTRODUCTION

Gaging of screw threads is the process of investigating or determining the extent to which they conform dimensionally to prescribed limits of size. Dimensional gages are the means applied for that purpose.
This section for gages and gaging practice is supplementary to sections 2 and 3 and is intended to facilitate adherence to the limits of size specified therein without in any sense restricting the requirements more severely than those specified. Adherence to the gaging principles laid down, which have been tested by many years of practical use, will assure interchangeable assembly of product threads, the acceptance of satisfactory threads, and the rejection of threads that are outside of prescribed limitations.

This section covers gaging methods for final conformance and provides the essential specifications for the applicable gages required in line with the provisions of par. 5.1, p. 6.17.

It is not the intent to preclude the use of other gaging systems or dimensional control systems provided they are properly correlated by the user to this section and yield comparable results with respect to conformance within specified limits.

This section includes specifications for the following gages used for product inspection:

For Product Internal Thread:
(a) GO Thread Plug Gage for functional (virtual) diameter maximum-material limit.
(b) HI Thread Plug Gage for HI functional diameter minimum-material limit.
(c) GO and NOT GO Plain Plug Gages for minimum and maximum limits of the minor diameter.

For Product External Thread:
(a) GO Thread Ring Gage for functional (virtual) diameter maximum-material limit.
(b) LO Thread Ring Gage for LO functional diameter minimum-material limit.
(c) Indicating Thread Gages to establish numerical values for determining Functional Differential Reading for use in verifying conformance of the thread elements.
(d) LO Limit Thread Snap or Indicating Gages for LO minimum-material limit.
(e) GO and LO Thread Setting Plug Gages for (a) through (d) above.
( $f$ ) Plain Gages for minimum and maximum limits of the major diameter.

## 2. BASIC PRINCIPLES

2.1. Gage Classification.-The limits of size of the threads to be produced should be represented in: (1) Gages used in checking the threads as they are produced, known as "working gages"; (2) gages for use in the acceptance of the product, known as "inspection gages"; and (3) gages used to determine the accuracy of the two preceding classes of gages known as "master" and "setting gages."
2.2. Gages For Reference.-(a) Master gage.The master gage is a thread plug gage which represents the physical dimensions of the basic size of
the part. It clearly establishes the minimum size of the internal thread and the maximum size of the external thread at the point at which interference between mating parts begins when no allowance is provided. A master gage shall be accompanied by a record of its measurement.
(b) Setting gage (check gage).-Threaded setting gages.-A setting gage is a thread plug gage to which adjustable thread ring gages, thread snap gages, and other thread comparators are set to size. Threaded setting plug gages are of two standard designs which are designated as "basic-crest setting plugs" and "truncated setting plugs."

The basic-crest setting plug is one having a width of flat at the crest equal to $0.125 p$. It is frequently used for setting thread snap gages and indicating type gages. See par. 5.2, p. 6.18 .

The truncated setting plug of standard design, as shown in CS8 or B47.1, is similar to the basic-crest setting plug except that the crest of the thread is truncated for half the length of the gage, giving a full-form portion and a truncated portion, as specificd in par. 4.6.3, p. 6.16. In setting thread gages to size, the truncated portion controls the pitch diameter, and the full-form portion assures that proper clearance is provided at the major diameter of the ring gage. Also, the use of the full-form portion in conjunction with the truncated portion checks, to some degree, the flank angle of the thread gage.

Plain cylindrical plug acceptance check gages.-GO and NOT GO plain cylindrical plug acceptance check gages are required to check the minor diameter limits of thread ring gages of the smaller sizes, after the gage has been properly set to the thread setting plug gage. Standard measuring equipment is usually employed in lieu of plain cylindrical plug gages for minor diameters larger than 0.375 in .
2.3. Limit Gages.-Limit gages are of two categories: (1) maximum-material-limit gages, designated GO gages and (2) minimum-material-limit gages, designated low limit ( LO ) gages for the functional diameter of external threads and high limit (HI) gages for internal threads. ${ }^{1}$
(a) Maximum-material-limit or GO gages.-The maximum-material-limit or GO gages, check or control the extent of the tolerance, as applied to a specific screw thread, in the direction of the limit of maximum material and represent the maximum limit of external threads and the minimum limit of internal threads. The ideal maximum-material-limit or GO gage is a threaded counterpart of the thread, made exactly to its prescribed maximum-material limits and, in length, equal to the length of engagement of the thread with its mating thread. Such gages would most nearty duplicate the assembly conditions of threads. They control the virtual diameter (or effective size) at the maximum-material limit. See par. 5.1, p. 6.17.
(b) Minimum-material-limit or HI/LO gages.The minimum-material-limit gages control the ex-

[^16]tent of the tolerance in the direction of the limit of minimum material and represent the minimum limit of external threads and the maximum limit of internal threads. The minimum-material pitch diameter limits are necessarily a limitation of the pitch diameter as a single thread element. Also, it is a principle of limit gaging that each element or dimension can be checked only singly by a minimum-material-limit gage. Accordingly, separate gages are required to check pitch, major, and minor diameters at minimum-material limits. That is, for external threads two gages are necessary: one to check the major diameter and another to check the pitch diameter; internal threads require a gage to check the pitch diameter and another to check the minor diameter. A third factor in minimum-material-limit gaging is nontechnical but of practical importance, namely, the economics of the gaging means and procedures, as thorough checking of a thread requires several individual gaging operations along and around the thread. It is not feasible, therefore, to establish an ideal gage design for gaging pitch diameter and approach that ideal closely in practice, as is done for maximum-material-limit gages.

As a result, two distinct gaging practices are widely used, as follows:
(1) The use of minimum-material-limit thread plug and ring gages provides a satisfactory means of gaging when proper functioning of the thread assembly only requires control of the virtual diameter (or effective size) of the threads at the minimummaterial limits. The use of such gages is referred to as "virtual diameter (or effective size) gaging , ractice." See par. 5.1, p. 6.17.
(2) The use of minimum-material-limit thread snap or indicating gages conforming to the thread length requirements stated in paragraphs 4.4.2.2, p. 6.07, and 4.5.2.2, p. 6.12, controls to a close degree the pitch diameter at the minimum-material limit as a single element. Thus, without further checking, their use provides an economical means of control over such other variables as lead, uniformity of helix, flank angle, taper, roundness, and surface condition. The use of such gages, however, is referred to as "single element gaging practice." See par. 5.1, p. 6.17.
2.4. Final Conformance Gaging.-The object of final conformance gaging of product threads is to determine the extent they conform dimensionally to prescribed limits of size, and to segregate or reject product threads that are outside of prescribed limitations.

There are two general methods of approach to dimensional inspection of product threads, namely, inspection by attributes and inspection by variables.

Inspection by attributes involves the application of limit gages to assure that the product threads are within prescribed limits of size. Inspection by attributes forms the basis of final conformance gaging except as noted in the next paragraph.

Inspection by variables forms the basis of final conformance gaging where it is required by supplemental specifications that individual elements of
product threads be controlled. Dimensional Inspection by variables is most useful in the control of manufacturing tools and processes and to collect manufacturing data for the analysis of product thread deviations. Inspection by variables involves the application of indicating gages or measuring instruments (optical, mechanical, pneumatic, or electrical) to determine the extent of deviations of product threads and their individual elements relative to prescribed limits.
2.5. Screw Thread Conformance.-Final dimensional acceptance of product threads shall be in accordance with the limits of size as determined by the final conformance gages outlined in par. 5.1, p. 6.17. It is important that the method of final conformance gaging be understood by both the producer and user. See par. 3.2, p. 6.04.

Thread plug gages are controlled by direct measuring methods. Thread ring, thread snap limit gages, and indicating thread gages are controlled by reference to the appropriate setting plugs.
2.6. Limitations Of Gaging.-Product threads accepted by a gage of one type may be verified by other types. It is possible, however, that parts which are near either rejection limit may be accepted by one type and rejected by another. Also, it is possiblc for two individual limit gages of the same type to be at the opposite extremes of the gage tolerances permitted, and borderline product threads accepted by one gage could be rejected by another. See under par. 3 which follows.

Large product external and internal threads may present additional problems for technical and economic reasons. In these instances, verification may be based on use of gages or measurement of thread elements. Various types of gages or measuring devices in addition to those defined in this section are available and acceptable when properly correlated to this section. It is essential to achieve agreement between producer and consumer with respect to method and equipment used.
2.7. Surveillance Of Gages.-Periodic rechecking and surveillance of gages is a necessary precaution to assure satisfactory product thread conformance.
2.8. Measurement Of Gages.
2.8.1. Determining Pitch Diameter.-The threewire method of determining pitch diameter of thread plug gages is standard for gages in this section. Sizes of ring thread gages are determined by their fit on their respective setting plugs so measured. Other thread gages for product external threads are controlled by reference to appropriate setting plugs so measured. See appendix A4.
2.8.2. Standard Temperature.-The standard temperature used internationally for linear measurements is $68^{\circ} \mathrm{F}\left(20^{\circ} \mathrm{C}\right)$. Nominal dimensions of gages and product, as specified, and actual dimensions, as measured, shall be within specified limits at this temperature.

As product threads are frequently checked at temperatures which are not controlled, it is desirable that the coefficient of thermal expansion of gages
be the same as that of the product on which they are used. Inasmuch as the majority of threaded product consists of iron or stecl, and screw-thread gages are ordinarily made of hardened steel, this condition is usually fulfilled without special attention. When the materials of the product thread and the gage are dissimilar, the differing thermal coefficients can cause serious complications and must be taken into account.
2.8.3. Measuring Force for Wire Measurements of 60 Degree Threads.- In measuring the pitch diameter of screw thread gages by means of wires, the following measuring forces shall be used:

Threads per Inch 20 or less
Above 20 to and including 40
Above 40 to and including 80

Measuring Force in
Pounds ( $\pm 10 \%$ ) 2.5 1 0.5

The thread wires should be calibrated by the procedure specified in appendix A4.

## 3. GAGING AND VERIFICATION OF PRODUCT THREADS

Gages are classified as to type and use, together with specific details of gaging practice applicable to each type, in the following paragraphs.

GO thread gages check the maximum-material size, to assure interchangcable assembly. HI and LO thread gages check the minimum-matcrial size.

The thread form of GO thread gages corresponds to maximum product thread depth of engagement to assure clearance at the major diameter of the product internal thread or the minor diameter of the product external thread.

GO and NOT GO plain cylindrical plug gages, snap, or indicating gages, check the limits of size of the minor diameter of product internal threads and the major diameter of product cxternal threads, respectively.

At the product thread maximum-material limit, the gages used for final conformance gaging arc within the extreme limits of size of the product thread. At the product thread minimum-material limit the usual practice for gages used for final conformance gaging is to have the gage tolerance within the extremc limits of size of the product thread. However, to assure that usable product thread at the cxtreme limit of size (minimum-material limit) is not rejected, in border-line cases, the consumer may elect to use HI/LO gages having pitch diameter tolerances outside the product thread limits.
3.1. Use Of Gages.
3.1.1. Threaded and Plain Gages for Verification of Product Internal Threads:

Unless otherwise specified, all thread gages which directly check the product thread shall be $X$ tolerance for all classes.

GO Thread Plug Gages. GO thread plug gages must enter the full threaded length of the product
freely. The GO thread plug gage is a cumulative check of all thread elements except the minor diameter.

HI Thread Plug Gages. HI thread plug gages when applied to the product internal thread may engage only the end threads (which may not be represcntative of the complete thread). Entering threads on product are incompletc and permit gage to start. Starting threads on HI plugs are subject to greater wear than the remaining thrcads. Such wear in combination with the incomplete product threads permit further entry of the gage. Surveillance facilities ordinarily available in the field are often inadequate for fully determining such gage wear. Also, it is not practical to control nor limit the torque applied by operators, nor that utilized by a specific operator at various times and under varying conditions. For these reasons the following standard practice has been adopted with respect to permissible entry. Threads are acceptable when the HI thread plug gage is applicd to the product internal thread if: (a) it does not cnter, or if (b) all complete product threads can be entered, provided that a definite drag from contact with the product material results on or before the third turn of entry. The gage should not be forced after the drag is definitc. Special requirements such as exceptionally thin or ductile material, or small number of threads, may necessitate modification of this practice.

GO and NOT GO Plain Plug Gages for Minor Diameter of Product Internal Thread. GO plain plug gages must completely enter the product internal thread to assure that the minor diameter does not exceed the maximum-material limit. NOT GO plain plug gages must not enter the product internal thread to provide adequate assurance that the minor diameter does not exceed the minimummaterial limit.
3.1.2. Thread Setting Plug Gages.

GO and LO Truncated Setting Plugs. W tolerance truncated setting plugs are recommended for setting adjustable thread ring gages up to and including 6.25 inches nominal size and may be used for setting thread snap gages and indicating thread gages. Above 6.25 in . nominal size, the difference in feel between the full form and truncated sections in setting thread ring gages is insignificant, and the basic crest setting plug may be used.

When setting adjustable thread ring gages to size, the truncated portion of the setting plug controls the functional size, and the full form portion assures that adequate clearance is provided at the major diameter of the ring gagc. The full form portion, in conjunction with the truncated portion, chceksto some degree - the half-angle accuracy of the gage. The same procedure may be applicd to detect uneven angle wear of ring gages in use.

GO and LO Basic-crest (Full Form) Setting Plugs. W tolerance basic crest setting plugs are frequently used for setting thread snap limit gages and indicating thread gages. They may also be used for setting large adjustable thread ring gages, especially
those above 6.25 inches nominal size. When they are so used it may be desirable to take a cast of the ring gage thread form to check the half-angle and profile. See par. 5.2.1.1, p. 6.18.

GO and NOT GO Plain Plug Acceptance Check Gages for Checking Minor Diameter of Thread Ring Gages. The GO plain plug gage is made to the minimum minor diameter specified for the thread ring gage (GO or LO), while the NOT GO gage is made to maximum minor diameter specified for the thread ring gage (GO or LO). After the adjustable thread ring gages have been set to the applicable thread setting plugs, the GO and NOT GO plain plug acceptance check gages are applied to check the minor diameter of the ring gage to assure that it is within the specified limits. An alternate method for checking minor diameter of thread ring gages is by the use of measuring equipment.
3.1.3. Threaded and Plain Ring, Suap, and Indicating Thread Gages for Verification of Product External Thread.

GO Thread Ring Gages. GO thread ring gages must be set to the applicable $W$ tolerance setting plugs to assure they are within specified limits. The product thread must freely enter the GO thread ring gage for the entire length of the threaded portion. The GO thread ring gage is a cumulative check of all thread elements except the major diameter.

LO Thread Ring Cages. LO Thread ring gages must be set to the applicable $W$ tolerance setting plugs to assure that they are within specified limits. LO thread ring gages when applied to the product external thread may engage only the end threads (which may not be representative of the complete product thread). Starting threads on LO rings are subject to greater wear than the remaining threads. Such wear in combination with the incomplete threads at the end of the product thread permit further entry in the gage. Surveillance facilities ordinarily a vailable in the ficld are often inadequate for fully determining such gage wear. Also, it is not practical to control nor limit the torque applied by operators, nor that utilized by a specific operator at various times and under varying conditions. For these reasons the following standard practice has been adopted with respect to permissible entry. Threads are acceptable when the LO thread ring gage is applied to the product external thread if (a) it is not entered, or if (b) all complete product threads can be entered provided that a definite drag from contact with the product material results on or before the third turn of entry. The gage should not be forced after the drag is definite. Special requirements such as exceptionally thin or ductile material, small number of threads, etc., may necessitate modification of this practice.

LO Thread Snap Limit Gages or Indicating Thread Gages. LO thread snap limit gages (or indicating thread gages) check Class 3 A product external thread LO minimum-material limit. The gages must be set to the applicable $W$ tolerance setting plugs.

The gage is then applied to the product thread at various points around the circumference and over the entire length of complete product thread. In applying the thread snap limit gage, threads are dimensionally acceptable when the gaging elements do not pass over the product thread or just pass over the product thread with perceptible drag from contact with the product material and the gage. Indicating thread gages provide a numerical value for the product thread size. Product external threads are dimensionally acceptable when the value derived in applying the gage (as described above) is not less than the specified minimum-material limit.
3.1.4. Check of Effect of Lead and Flank Angle Deviations on Product Thread. When this check is specified, there are two general methods available for the inspection procedures involved, as follows:

Direct Measurement of Deviations. The lead and flank angle of the product thread may be measured by means of available measuring equipment such as projection comparators, measuring microscopes, graduated cone points, lead measuring machines, helix variation measuring machines, and thread flank charting equipment. Formulas for obtaining the diameter equivalents of lead and flank angle deviations are given in subsection "Limits of size" in section 2. Sce also table 2.22 for such deviations equivalent to half the pitch diameter tolerances for Standard Unified Threads.

Differential gaging utilizing indicating thread gages with appropriate gaging elements as outlined under par. 5.4, p. 6.21, and par. 6, p. 6.27, may be used.
3.1.5. GO and NOT GO Plain Rings and Adjustable Snap Limit and Indicating Gages for Checking Major Diameter of Product External Thread. The GO gage must completely receive or pass over the major diameter of the product external thread to assure that the major diameter does not exceed the maximum-material limit. The NOT GO gage must not pass over the major diameter of the product external thread to assure that the major diameter is not less than the minimum-material limit.
3.2. Limitations.

Product threads accepted by a gage of one type may be verified by other types. It is possible, however, that parts which are near either rejection limit may be accepted by one type and rejected by another. Also, it is possible for two individual limit gages of the same type to be at the opposite extremes of the gage tolerances permitted and borderline product threads accepted by one gage could be rejected by another. In such instances (except when LO limit snap or indicating thread gages are specified) limit plug and ring thread gages that approximate as closely as practicable the extreme maxi-mum-material product-limit and minimum-material product-limit shall be used to determine whether or not the product threads under inspection are within the specified limits of size.

Large product external and internal threads above 6.25 in. nominal size may present additional problems
for technical and cconomic reasons. In these instances verification may bc based on use of gages or measurement of thread elements. Various types of indicating thread gages are shown under par. 6, p.6.27. Producer and user should agree on the method and equipment used.

### 3.3. Surveillance.

Gages are subject to wear and/or damage from normal usage. Periodic rechecking and surveillance is a necessary precaution to assure product thread conformance.

## 4. SPECIFICATIONS FOR GAGES

### 4.1. General Design.

The design of gages is specified herein only to the extent that it affects the results obtained in the gaging of product threads. Moreover, to serve their intended purposes satisfactorily, thread gages should be produced by the latest and best manufacturing techniques. The type of steel or wear-resistant material selected, together with the heat-treating and stabilization processes, should provide wear life and dimensional stability. Thread gaging elements should be precisely manufactured to assure adequate refinement of surface texture, prevention or eliminaton of amorphous or smear metal, and uniformity of thread form over the entire length of the gaging member. Precision lapping of thread flanks of thread plug and ring gages is a commonly used practice in manufacture.

### 4.2. Design Of Gage Blanks.

Designs of standard blanks for thread plug and ring gages, setting plug gages, plain cylindrical plug and ring gages, and plain snap gages have been developed by the American Gage Design Committce. The designs have proved satisfactory in many years of use and have been published in CS8 and B47.1, Gage Blanks. Also see tables 6.11 and 6.12 .

GO gage blanks should theoretically approximate the length of engagement of the product thread with its mating thread, while HI/LO blanks may be shorter.

Where indicating thread gages are uscd, the length of GO gaging elements should approximate the length of the corresponding GO thread gage.

4 3. Specific Design Requirements.
4.3.1. Thread Form. The specifications for thread form of thread gages applicable to both external and internal threads are stated below for each particular type gage. These specifications for thread form apply over the entire circumference and threaded length of the gaging element.
4.3.2 Limits of Size. The specifications and format for tables of limits of size of thread gages and setting plugs are summarized in tables 6.6 and 6.7. Constants for the various standard thread pitches which are required to determine gage dimensions are tabulated in table 6.5.
4.3.3. Standard Gage Tolerances. Standard tolerances for thread plug and ring gages and thread setting plugs are: (1) W tolerances, shown in table 6.9 , which represent the highest commercial grade
of accuracy and workmanship, and are specified for truncated setting plugs; (2) X tolerances, shown in table 6.8 are larger than $W$ tolerances.
4.3.3.1. Application of Tolerances. Thread Setting Plugs. Regardless of product thread class, all thread setting plugs for final conformance gaging shall be to $W$ tolerances. For other than final conformance gaging, see par. 5.3.2, p. 6.20 .

Thread Gages. Final conformance gages which directly check the product thread shall be to X tolerances for all classes unless otherwise specified.
4.3.3.2. Direction of Tolerances on Gages. At the maximum-material limit (GO), the dimensions of all gages used for final conformance gaging are within the extreme limits of size of the product thread. At the minimum-material limit (HI/LO), the usual practice for gages used for final conformance gaging, unless otherwise specified, is to have the gage tolerance within the cxtreme limits of size of the product thread. Dimensions for such gages are listed in columns 6 and 15 of table 6.19, p. 6.30 , and col. 9 of table 6.20. However in order to assure that usable product thread at the extreme limit of sizc is not rejected, the consumer may elect to use (HI/LO) gages having pitch diameter tolerances outside of the product thread limit. Dimensions for such gages are listed in columns 7 and 16 of table 6.19, p. 6.30 , and col. 10 of table 6.20 .

Direction of Tolerances for Individual Gage Elemonts. The direction of tolerances for the individual elements of the various types of gages arc specified in tables 6.6 and 6.7.
4.3.3.3. Tolerance on Lead (cumulative effect of progressive or erratic helix variation and thick-end or thin-end thread deviations) is specified as an allowable variation between any two threads not farther apart than the length of the standard taperlock or trilock gage as shown in CS8 or B47.1, Gage Blanks. In the case of setting plugs, the specificd tolerance shall be applicable to the thread length in the mating ring gage or 9 pitches, whichever is smaller. *The tolerancc on lead establishes the width of a zone, measured parallel to the axis of the thread, within which the actual helical path must lie for the specified length of the thread. Measurements will be taken from a fixed reference point located at the start of the first full thread to a sufficient number of positions along the entire helix to detect all types of lead deviations. The amounts that these positions deviate from their basic (theoretical) positions will be recorded with due respect to sign. The greatest deviation in each direction ( + and - ) will bc selected and the sum of their values, disregarding sign, shall not exceed the specified tolerance. If the deviations are all in one direction, the maximum

[^17]value governs conformance. In the casc of truncated setting plugs, the lead deviations present on the full-form portion and the truncated portion of an individual gage shall not differ from each other by more than 0.0001 in . over any portion equivalent to the length of the thread ring gage, or nine pitches, whichever is smaller.
4.3.3.4. Tolerances on Half-Angle. Tolerances are specified for the half-angle rather than the included angle to assure that the bisector of the included angle will be perpendicular to the axis of the thread within proper limits. The equivalent of the deviation from the true thread form caused by such irregularities as convex or concave flanks, rounded crests, or slight projections on the thread form, shall not exceed the tolerance permitted on half-angle.
4.3.3.5. Interpretation of Tolerances. Tolerances on lead, half-angle, and pitch diameter are deviations which may be taken independently for each of these elements and may be taken to the full extent allowed by respective tabulated tolerances. The tabulated tolerance on any one element must not be exceeded even though deviations in the other two elements are smaller than the respective tabulated tolerances.
4.3.3.6. Tolerances for Plain Gages. Standard tolerances for plain plug gages for checking minor diameter of product internal threads and for gages for checking major diameter of product external threads are $Z$ tolerances, as shown in table 6.10.
4.3.4. Identification. Each gage shall be plainly and permanently marked with the minimum marking essential for positive identification.

For multi-piece gages it may be desirable to identify individual components and handles or frames.

When it is impracticable to identify the gaging elements, due to size and/or lack of suitable space for marking, and they are packaged separately, it is suggested that identification be accomplished by a tag suitably attached or by marking the container.
4.4. Specifications For Gages Applicable To Product Internal Threads.
4.4.1. GO Thread Plug Gages.
4.4.1.1. Purpose. The GO thread plug gage checks the limit of tolerance of product internal thread in the direction of maximum material. The GO thread plug gage represents the minimum size limit of the product internal thread and its purpose is to achieve interchangeable assembly of maximum material mating parts. (See par. 4.4.3, p. 6.09, for gaging of minor diameter.) For gaging practice, see par. 3.1.1, p. 6.03.
4.4.1.2. Basic Design. Ideally, the maximum-material-limit or GO thread plug gage should be made to the prescribed maximum-material limit of the product internal thread, and, in length, be at least equal to the length of engagement of the mating product thread.

Gage Blanks. For practical and economic reasons, the design and lengths of the gaging members and handles have been standardized for various size
ranges and pitches. (See CS8 or B47.1 and table 6.11.)
4.4.1.3. Thread Form. The specifications for thread form are stated in detail below and are summarized in table 6.6 and figure 6.1.

Thread Crests. The major diameter of the GO thread plug gage shall be the same as the minimum (basic) major diameter of the product internal thread, with a plus gage tolerance. The thread crests shall be flat in an axial section and parallel to the axis.

Thread Roots. The minor diameter of the GO thread plug gage shall be cleared beyond a $p / 8$ width of flat either by an extension of the sides of the thread toward a sharp V or by an undercut no greater than $p / 8$ maximum width and approximately central. (See fig. 6.1.)

Concentricity of Pitch and Major Cylinders. The pitch and major cylinders of GO thread plug gages should be concentric as stated hereafter. On thread plug gages, an eccentric condition produces an oversize effective major diameter, having a width of flat less than $p / 8$, which may encroach on the minimum permissible limit for the root profile of the product internal thread. The permissible maximum effective major diameter, as determined by measurement of runout (total indicator variation) with respect to the pitch cylinder, shall not exceed the maximum major diameter specified.

Pitch Cylinder. The pitch cylinder shall be round and straight within the gage pitch diameter limits specified.
4.4.1.4. Lead and Half-Angle Deviations. Lead and half-angle deviations shall be within the limits specified. (See table 2.22.)
4.4.1.5. End Threads. The feather edge at both ends of the threaded section of the gaging member shall be removed. On pitches coarser than 28 threads per inch, not more than one complete turn of the end threads shall be removed to obtain a full thread form blunt start. See figure 6.4. On pitches 28 threads per inch and fince a $60^{\circ}$ chamfer from the axis of the gage is acceptable in lieu of the blunt start.
4.4.1.6. Chip Grooves. Each GO thread plug gage, except in sizes No. $8(0.164)$ and smaller, shall be provided with a chip groove at the entering end. On reversible gages, a chip groove shall be provided at each end. Chip grooves are acceptable that are in accordance with commercial practice, such as a groove cut at an angle with the axis or a longitudinal groove cut parallel with the axis and extending the complete length of the gaging member. The groove shall be located circumferentially at the start of the full thread, and in all cases the depth shall extend below the root of the first full thread. The distance from the major diameter of the thread plug to the crest of the convolution rise in front of the chip groove, due to the radius of the convoluting tool, shall be a minimum of $H / 2$ as shown in figure 6.4. The beginning of the first thread shall be of full form. The recommended widths for chip grooves are as follows:

| Nominal diameter (inches) | Chip groove width (inches) |  |
| :---: | :---: | :---: |
|  | Max | Min |
| . 164 and smaller | No chip groove required |  |
| Above . 164 to and including .216 | 0.036 | 0.026 |
| Above .216 to and including . 375 | 0.052 | 0.042 |
| Above . 375 to and including . 500 | 0.067 | 0.057 |
| Above . 500 to and including 1.000 | 0.083 | 0.067 |
| Above 1.000 to and including 1.750 | 0.130 | 0.067 |
| Above 1.750-. | 0.193 | 0.067 |

4.4.1.7. Identification. The GO thread plug gage is basic and common to all classes of thread for any particular nominal size and series. Accordingly, it is recommended that the gage be identified by nominal size, threads per inch, series, and GO pitch diameter.

## Example:

.250-20 (or 1/4-20) UNC GO PD . 2175 .190-32 (or 10-32) UNF GO PD . 1697

### 4.4.2. HI Thread Plug Gages.

4.4.2.1. Purpose. The HI thread plug gage checks the limit of tolerance of a product internal thread in the direction of minimum-material. The HI thread plug gage represents the maximum size limit of the product internal thread and provides a satisfactory method of gaging the functional diameter at the minimum-material limit. For gaging practice, see par. 3.1.1, p. 6.03.
4.4.2.2. Basic Design. In order that the HI thread plug gage may effectively check the minimummaterial functional diameter, the half-angle contact should be reduced by truncating the major diameter and the length of the gaging element, where practical, should be less than that of the GO gage.

Gage Blanks. For practical and economic reasons the designs and lengths of the gaging members and handles have been standardized for various size


See paras. 4.4.1.3, 4.4.2.3, 4.5.1.3, 4.5.2.3 relative root clearance.
Figure 6.1. Thread forms of gages for product external and internal threads.
ranges and pitches. (See CS8 or B47.1 and table 6.11.)
4.4.2.3. Thread Form. The specifications for thread form are stated in detail below and are summarized in table 6.6 and figure 6.1.

Thread Crests. The maximum major diameter of the HI thread plug gage shall be equal to the maximum pitch diameter of the product internal thread plus $H / 2$ with the gage tolerance minus. This corresponds to a width of flat at the crest of the gage equal to $p / 4$. However, the maximum major diameter of the HI thread plug gage shall not exceed the minimum major diameter of the product internal thread minus $0.0375 H$ or $0.05 h_{b}$. (See col. 16 of table 6.5.)

Thread Roots. The minor diameter of the HI thread plug gage shall be cleared beyond a $p / 4$ width of flat by an extension toward a sharp $V$ of
the sides of the thread from the position corresponding to this approximate width or by an undercut to any dimension no wider than the width resulting from $p / 8$ maximum width either side of and approximately central with the center line of the thread groove.

Concentricity of Pitch and Major Cylinders. The pitch and major cylinders of HI thread plug gages shall be concentric as stated hereafter. On thread plug gages an eccentric condition produces an oversize effective major diameter, having a width of flat less than $p / 4$. The permissible maximum effective major diameter, as determined by measurements of runout (total indicator variation) with respect to the pitch cylinder, shall not exceed the maximum major diameter specified.
Pitch Cylinder. The pitch cylinder shall be round and straight within the gage pitch diameter limits specified.


See paras. 4.4.1.3, 4.4.2.3, 4.6.3.3 relative root clearance.
See col. 13 of table 6.7 relative crest of full portion of LO thread gage.
Figure 6.2. Thread form of truncated thread setting plug gages.


See paras. 4.4.1.2, 4.4.2.2, 4.6.3.3 relative root clearance.
See col. 13 of table 6.7 relative crest of LO thread gage.
Figure 6.3. Thread forms of basic crest thread setting plug gages.


Figure 6.4. Removal of partial thread and chip groove.
4.4.2.4. Lead and Half-Angle Deviations. Lead and half-angle deviations shall be within the limits specified. See table 2.22.
4.4.2.5. End Threads. The feather edge at both ends of the threaded section of the gaging member shall be removed. On pitches coarser than 28 threads per inch, not more than onc complete turn of the end threads shall be removed to obtain a full thread blunt start. On pitches 28 threads per inch and finer, a $60^{\circ}$ chamfer from the axis of the gage is acceptable in lieu of the blunt start.
4.4.2.6. Identification. The HI thread plug gage should be marked with the nominal size, threads per inch, thread series, class, HI, and pitch diameter.

Example:

$$
\begin{aligned}
& .250-20 \text { UNC-2B HI PD } .2224 \\
& .190-32 \text { UNF-2B HI PD } .1736
\end{aligned}
$$

4.4.3. Plain Plug Gages for Minor Diameters.
4.4.3.1. Purpose and Basic Design. The GO and HI thread plug gages are cleared at the root and do not check the minor diameter of the product internal thread. Accordingly, GO and NOT GO plain plug gages are necessary to check the maximummaterial and minimum-material limits at the minor diameter. For gaging practice, see par. 3.1.1, p. 6.03.

Gage Blanks. The designs of the gaging elements and handles have been standardized. (See CS8 or B47.1, Gage Blanks.)

Table 6.5. Constants for computing thread gage dimensions

| Threads per inch, $n$ | $\begin{gathered} \text { Pitch, } \\ p \end{gathered}$ | $\begin{gathered} 3 / 4 p= \\ 0.75 p \end{gathered}$ | $\begin{aligned} & p / 4= \\ & 0.25 p \end{aligned}$ | $\begin{gathered} p / 8= \\ 0.125 p \end{gathered}$ | 0.067p | $0.10048 p$ | $0.060 \sqrt[3]{p^{2}}$ | $0.017 p$ | $\begin{gathered} 0.060 \sqrt[3]{p^{2}} \\ +0.017 p \end{gathered}$ | Height of sharp Vthread, $H=$ $0.866025 p$ | $\begin{gathered} 3 / 4 H= \\ 0.649519 p \end{gathered}$ | $\begin{gathered} H / 2= \\ 0.43301 p \end{gathered}$ | $\begin{gathered} H / 4= \\ 0.21651 p \end{gathered}$ | $\begin{gathered} 0.13395 \mathrm{H} \\ =0.116 p \\ =(2 \times \\ 0.058 p) \end{gathered}$ | $\begin{gathered} 0.0375 H \\ =0.05 h_{b} \\ =0.03248 p \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 |
|  | $\begin{gathered} i n \\ 0.012500 \end{gathered}$ | $\stackrel{i n}{0.00938}$ | $\begin{gathered} \stackrel{i n}{ } \\ 0.00312 \end{gathered}$ | $\begin{gathered} i n \\ 0.00156 \end{gathered}$ | $\stackrel{i n}{0.00084}$ | $\begin{gathered} \quad \text { in } \\ 0.00126 \end{gathered}$ | $\begin{gathered} \quad \text { in } \\ 0.00323 \end{gathered}$ | $\begin{gathered} i n \\ 0.00021 \end{gathered}$ | $\begin{aligned} & i n \\ & 0.0034 \end{aligned}$ | $\begin{gathered} i n \\ 0.010825 \end{gathered}$ | $\stackrel{i n}{n}_{0.008119}$ | $\stackrel{i n}{0.00541}$ | $\begin{gathered} \stackrel{i n}{ } \\ 0.00271 \end{gathered}$ | $\begin{gathered} \stackrel{i n}{0.00145} \end{gathered}$ | $\begin{aligned} & \text { in } \\ & 0.00041 \end{aligned}$ |
| 72 | . 013889 | . 01042 | . 00347 | . 00174 | . 00093 | . 00140 | . 00347 | . 00024 | . 0037 | . 012028 | . 009021 | . 00601 | . 00301 | . 00161 | . 00045 |
| 64 | 015625 | . 01172 | . 00391 | . 00195 | . 00105 | . 00157 | 00375 | . 00027 | 0040 | . 013532 | . 010149 | . 00677 | . 00338 | . 00181 | . 00051 |
| 56 | 017857 | . 01339 | . 00446 | . 00223 | . 00120 | . 00179 | . 00410 | . 00030 | . 0044 | . 015465 | . 011599 | . 00773 | . 00387 | . 00207 | . 00058 |
| 48 | . 020833 | . 01562 | . 00521 | . 00260 | . 00140 | . 00209 | . 00454 | . 00035 | . 0049 | . 018042 | . 013532 | . 00902 | . 00451 | . 00242 | . 00068 |
| 44 | . 022727 | . 01705 | . 00568 | . 00284 | . 00152 | . 00228 | . 00482 | . 00039 | . 0052 | . 019682 | . 014762 | . 00984 | . 00492 | . 00264 | . 00074 |
| 40 | . 025000 | . 01875 | . 00625 | . 00312 | . 00168 | . 00251 | . 00513 | . 00042 | . 0056 | . 021651 | . 016238 | . 01083 | . 00541 | . 00290 | . 00081 |
| 36 | . 027778 | . 02083 | . 00694 | . 00347 | . 00186 | . 00279 | . 00550 | . 00047 | . 0060 | . 024056 | . 018042 | . 01203 | . 00601 | . 00322 | . 00090 |
| 32 | . 031250 | . 02344 | . 00781 | . 00391 | . 00209 | . 00314 | . 00595 | . 00053 | . 0065 | . 027063 | . 020297 | . 01353 | . 00677 | . 00362 | . 00101 |
| 28 | . 035714 | . 02679 | . 00893 | . 00446 | . 00239 | . 00359 | . 00651 | . 00061 | . 0071 | . 030929 | . 023197 | . 01546 | . 00773 | . 00414 | . 00116 |
| 27 | . 037037 | . 02778 | . 00926 | . 00463 | . 00248 | . 00372 | . 00667 | . 00063 | . 0073 | . 032075 | . 024056 | . 01604 | . 00802 | . 00430 | . 00120 |
| 24 | . 041667 | . 03125 | . 01042 | . 00521 | . 00279 | . 00419 | . 00721 | . 00071 | . 0079 | . 036084 | . 027063 | . 01804 | . 00902 | . 00483 | . 00135 |
| 20 | . 050000 | . 03750 | . 01250 | . 00625 | . 00335 | . 00502 | . 00814 | . 00085 | . 0090 | . 043301 | . 032476 | . 02165 | . 01083 | . 00580 | . 00162 |
| 18 | . 055556 | . 04167 | . 01389 | . 00694 | . 00372 | . 00558 | . 00874 | . 00094 | . 0097 | . 048113 | . 036084 | . 02406 | . 01203 | . 00644 | . 00180 |
| 16 | . 062500 | . 04688 | . 01562 | . 00781 | . 00419 | . 00628 | . 00945 | . 00106 | . 0105 | . 054127 | . 040595 | . 02706 | . 01353 | . 00725 | . 00203 |
| 14 | . 071429 | . 05357 | . 01786 | . 00893 | . 00479 | . 00718 | . 01033 | . 00121 | . 0115 | . 061859 | . 046394 | . 03093 | . 01546 | . 00829 | . 00232 |
| 13 | . 076923 | . 05769 | . 01923 | . 00962 | . 00515 | . 00773 | . 01085 | . 00131 | . 0122 | . 066617 | . 049963 | . 03331 | . 01665 | . 00892 | . 00250 |
| 12 | . 083333 | . 06250 | . 02083 | . 01042 | . 00558 | . 00837 | . 01145 | . 00142 | . 0129 | . 072169 | . 054127 | . 03608 | . 01804 | . 00967 | . 00271 |
| 11.5 | . 086957 | . 06522 | . 02174 | . 01087 | . 00583 | . 00874 | . 01178 | . 00148 | . 0133 | . 075307 | . 056480 | . 03765 | . 01883 | . 01009 | . 00282 |
| 11 | . 090909 | . 06818 | . 02273 | . 01136 | . 00609 | . 00913 | . 01213 | . 00155 | . 0137 | . 078730 | . 059047 | . 03936 | . 01968 | . 01055 | . 00295 |
| 10 | . 100000 | . 07500 | . 02500 | . 01250 | . 00670 | . 01005 | . 01293 | . 00170 | . 0146 | . 086603 | . 064952 | . 04330 | . 02165 | . 01160 | . 00325 |
| 9 | . 111111 | . 08333 | . 02778 | . 01389 | . 00744 | . 01116 | . 01387 | . 00189 | . 0158 | . 096225 | . 072169 | . 04811 | . 02406 | . 01289 | . 00361 |
| 8 | . 125000 | . 09375 | . 03125 | . 01562 | . 00838 | . 01256 | . 01500 | . 00212 | . 0171 | . 108253 | . 081190 | . 05413 | . 02706 | . 01450 | . 00406 |
| 7 | . 142857 | . 10714 | . 03571 | . 01786 | . 00957 | . 01435 | . 01640 | . 00243 | . 0188 | . 123718 | . 092788 | . 06186 | . 03093 | . 01657 | . 00464 |
| 6 | . 166666 | . 12500 | . 04167 | . 02083 | . 01117 | . 01675 | . 01817 | . 00283 | . 0210 | . 144338 | . 108253 | . 07217 | . 03608 | . 01933 | . 00541 |
| 5 | . 200000 | . 15000 | . 05000 | . 02500 | . 01340 | . 02010 | . 02052 | . 00340 | . 0239 | . 173205 | . 129904 | . 08660 | . 04330 | . 02320 | . 00650 |
| 4.5 | . 222222 | . 16667 | . 05556 | . 02778 | . 01489 | . 02233 | . 02201 | . 00378 | . 0258 | . 192450 | 144338 | . 09623 | . 04811 | . 02578 | . 00722 |
| 4 | . 250000 | . 18750 | . 06250 | . 03125 | . 01675 | . 02512 | . 02381 | . 00425 | . 0281 | . 216506 | . 162380 | . 10825 | . 05413 | . 02900 | . 00812 |

4.4.3.2. Identification. The GO plain plug gage members for Unified threads are common to all classes of Unified threads, and as such should be marked with: Nominal size, threads per inch,thread designation, GO, and minor diameter.

Example:

## .250-20 UNC GO . 1960

The NOT GO plain plug gage members are not common to all classes, and should be marked with: Nominal size, threads per inch, thread designation, tolerance, class, NOT GO, and minor diameter. Example:

## .250-20 UNC-3B NOT GO . 2067.

4.5. Specifications For Gages Applicable To Product External Threads.
4.5.1. GO Thread Ring Gages.
4.5.1.1. Purpose. The GO thread ring gage checks the limit of tolerance of a product external thread in the direction of maximum material. The GO thread ring gage, when properly set on its respective thread setting plug, represents the maximum size limit of the product external thread and its purpose is to achieve intcrchangeable asscmbly of maximum material mating parts. For gaging practice, see par. 3.1.3, p. 6.04. See par. 4.5.5, p. 6.16, for gaging of major diameter.
4.5.1.2. Basic Design. Ideally, the maximum-material-limit or GO thread ring gage should be
made to the prescribed maximum-material limit of the product external thread and, in length, equal to the length of engagement of the mating product thread.

Gage Blanks. For practical and economic reasons, the designs and thicknesses of thread ring gages have been standardized for various size ranges and pitches. (See CS8 or B47.1 and table 6.12.) The AGD (American Gage Design Standard) thread ring gage is adjustable to facilitate manufacturing and setting.
4.5.1.3. Thread Form. The specifications for thread form are stated in detail below and are summarized in table 6.6 and figure 6.1.

Thread Crests. The minor diameter of the GO thread ring gage shall be equal to the maximum pitch diameter of the product external thread minus $H / 2$ with a minus gage tolerance. This corresponds to a width of flat of $p / 4$. The thread crests shall be flat in an axial section and parallel to the axis.

Thread Roots. The major diameter of the GO thread ring gage shall be clcarcd by a clearance cut of substantially $p / 8$ width and approximately central. The root clearance must be such that the maximum major diameter of the full form section of the thread setting plug gage is cleared after the gage has been properly set to sizc.

Concentricity of Pitch and Minor Cylinders. The pitch and minor cylinders of the GO thread ring gage shall be concentric as stated hereinafter. On thread ring gages an eccentric condition results in

| Nominal size and threads per inch | Series desig－ nation | Class | Gages for external threads |  |  |  |  |  |  |  | Gages for internal threads |  |  |  |  |  |  | Class | Series desig－ nation | Nominal size and threads per inch |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Thread gages |  |  |  |  | Plain gages for major diameter |  |  | Thread gages |  |  |  |  | Plain gages for minor diameter |  |  |  |  |
|  |  |  | GO |  | LO |  |  | GO | NOT GO＊ |  | GO |  | HI |  |  |  |  |  |  |  |
|  |  |  | Pitch diameter | Minor diameter | Piteh diameter |  | Minor diameter |  | Semi－ finished | Unfinished hot－rolled material | Major diameter | Piteh diameter | Major diameter | Piteh diameter |  |  |  |  |  |  |
|  |  |  |  |  | Plus tol．gage | Minus tol．gage |  |  |  |  |  |  |  | Minus <br> tol．gage | Plus tol．gage |  |  |  |  |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |



Table 6．7．Spccifications and format for tables of limits of size of threaded setting plug gages for Unified，external threads

| Nominal size and threads per inch | Series desig－ nation | Class | Truncated setting plugs |  |  |  |  |  |  | Basic－crest setting plugs |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Plug for GO |  |  | Plug for LO |  |  |  | Plug for GO |  | Plug for LO |  |  |
|  |  |  | Major diameter |  | Pitch diameter | Major diameter |  | Pitch diameter |  | Major diame－ ter | Pitch diame－ ter | Major diameter | Pitch diameter |  |
|  |  |  | Truncated | Full－ form |  | Trun－ cated | Full－ form | Plus tol． gage． | Minus tol． gage． |  |  |  | Plustol． gage | Minus tol．gage |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
|  |  |  | ． 2 亿合 <br>  <br>  <br>  <br>  ざも ज゙영 がす。 ․․․ 느야웅云 ${ }^{3}$ ？ 748 ．電资 <br>  |  |  |  |  |  |  |  |  |  |  |  |

an undersize effective minor diameter having a width of flat less than $p / 4$ ，which may encroach on the maximum permissible limit for the root profile of the product external thread．The permissible minimum effective minor diameter，as determined by measurements of runout（total indicator vari－ ation）with respect to the pitch cylinder，shall not be less than the specified minimum minor diameter minus the sum of the gage tolerances for the pitch and minor diameters．

Pitch Cylinder，Lead，and Half－Angle．Satisfactory conformance of these elements is normally deter－ mined by the setting of the thread ring gage to the applicable truncated setting plug gage．

4．5．1．4．End Threads．The feather edge at both ends of the thread ring gage shall be removed． On gages larger than 0.5 in．nominal size or on those having less than 20 threads per inch，from half to one pitch of the partially formed thread at each end shall be removed to obtain a full thread blunt start．On gages 0.5 in ．nominal size and smaller or on those having 20 or more threads per inch，a $60^{\circ}$ chamfer on the end threads from the axis of the gage to a depth of half to one pitch is acceptable in lieu of the blunt start．

4．5．1．5．Chip Grooves．GO thread ring gages of the adjustable type（AGD standard）do not require chip grooves as the adjusting slots serve this purpose．

4．5．1．6．Identification．The GO Thread Ring Gage for Class 3A is basic，and also is applicable for
acceptance of Class 2A after coating．Accordingly， it is recommended that the gage be identified by nominal size，threads per inch，series，and GO pitch diameter．Example：

## $.250-20$ UNC GO PD ． 2175.

The GO gages for Classes 1A and 2A are below basic size，having a common allowance．Accordingly， it is recommended that the gage be identified by nominal size，threads per inch，series，class，and GO pitch diameter．Example：

## $.250-20$ UNC 1A－2A GO PD ． 2164.

## 4．5．2．LO Thread Ring Gages．

4．5．2．1．Purpose．The LO thread ring gage checks the limit of tolerance of a product external thread in the direction of minimum material．The LO thread ring gage when properly set on its re－ spective set plug represents the minimum size limit of the product external thread and provides a satis－ factory method of gaging the functional diameter at the minimum－material limit．For Gaging Practice， see par．3．1．3，p．6．04．

4．5．2．2．Basic Design．In order that the LO thread ring gage may effectively check the minimum－ material functional diameter，the half－angle contact should be less than that of the GO gage and the length of the gaging element，where practical，should be less than that of the GO gage．

Gage Blanks．For practical and economic reasons， the thicknesses of thread ring gages have been standardized for various size ranges and pitches． （See CS8 or B47．1 and table 6．12．）

Table 6.8. $X$ Tolerances for $G O, H I$, and LO Thread Gages

| Threads per inch | Tolerance on lead ${ }^{\text {a }}$ | Tolerance on halfangle of thread | Tolerancc on major or minor diameters |  | Tolerance on pitch diameter |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | To and including 4 in dia | Above 4 in dia | To and including 1.5 in dia | $\begin{gathered} \text { Above } \\ 1.5 \text { to } 4 \\ \text { in dia } \end{gathered}$ | Above 4 to 8 in dia | $\begin{aligned} & \text { Above } \\ & 8 \text { to } 12 \\ & \text { in } \\ & \text { dia } b \end{aligned}$ |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
|  | in | deg $\min$ | in | in | in | in | in | in |
| 80 | 0.0002 | $0 \quad 30$ | 0.0003 |  | 0.0002 |  |  |  |
| 72 | . 0002 | $0 \quad 30$ | . 0003 |  | . 0002 |  |  |  |
| 64 | . 0002 | $0 \quad 30$ | . 0004 |  | . 0002 |  |  |  |
| 56 | . 0002 | 030 | . 0004 |  | . 0002 | 0.0003 |  |  |
| 48 | . 0002 | 030 | . 0004 |  | . 0002 | . 0003 |  |  |
| 44 | . 0002 | $0 \quad 20$ | . 0004 |  | . 0002 | . 0003 |  |  |
| 40 | . 0002 | $0 \quad 20$ | . 0004 |  | . 0002 | . 0003 |  |  |
| 36 | . 0002 | 020 | . 0004 |  | . 0002 | . 0003 |  |  |
| 32 | . 0003 | $0 \quad 15$ | . 0005 | 0.0007 | . 0003 | . 0004 | 0.0005 | 0.0006 |
| 28 | . 0003 | $0 \quad 15$ | . 0005 | . 0007 | . 0003 | . 0004 | . 0005 | . 0006 |
| 27 | . 0003 | $0 \quad 15$ | . 0005 | . 0007 | . 0003 | . 0004 | . 0005 | . 0006 |
| 24 | . 0003 | $0 \quad 15$ | . 0005 | . 0007 | . 0003 | . 0004 | . 0005 | . 0006 |
| 20 | . 0003 | $0 \quad 15$ | . 0005 | . 0007 | . 0003 | . 0004 | . 0005 | . 0006 |
| 18 | . 0003 | 010 | . 0005 | . 0007 | . 0003 | . 0004 | . 0005 | . 0006 |
| 16 | . 0003 | 010 | . 0006 | . 0009 | . 0003 | . 0004 | . 0006 | . 0008 |
| 14 | . 0003 | 010 | . 0006 | . 0009 | . 0003 | . 0004 | . 0006 | . 0008 |
| 13 | . 0003 | $0 \quad 10$ | . 0006 | . 0009 | . 0003 | . 0004 | . 0006 | . 0008 |
| 12 | . 0003 | $0 \quad 10$ | . 0006 | . 0009 | . 0003 | . 0004 | . 0006 | . 0008 |
| 11.5 | . 0003 | $0 \quad 10$ | . 0006 | . 0009 | . 0003 | . 0004 | . 0006 | . 0008 |
| 11 | . 0003 | 010 | . 0006 | . 0009 | . 0003 | . 0004 | . 0006 | . 0008 |
| 10 | . 0003 | 010 | . 0006 | . 0009 | . 0003 | . 0004 | . 0006 | . 0008 |
| 9 | . 0003 | $0 \quad 10$ | . 0007 | . 0011 | . 0003 | . 0004 | . 0006 | . 0008 |
| 8 | . 0004 | 05 | . 0007 | . 0011 | . 0004 | . 0005 | . 0006 | . 0008 |
| 7 | . 0004 | 05 | . 0007 | . 0011 | . 0004 | . 0005 | . 0006 | . 0008 |
| 6 | . 0004 | 05 | . 0008 | . 0013 | . 0004 | . 0005 | . 0006 | . 0008 |
| 5 | . 0004 | 05 | . 0008 | . 0013 |  | . 0005 | . 0006 | . 0008 |
| 4.5 | . 0004 | 0 | . 0008 | . 0013 |  | . 0005 | . 0006 | . 0008 |
| 4 | . 0004 | 05 | . 0009 | . 0015 |  | . 0005 | . 0006 | . 0008 |

a Allowable variation in lead betwcen any two threads not farther apart than the length of the standard gage, shown in CS8 or B47.1.
It has been customary in the past to specify tolcrances on lead as plus or minus (土) values. Under the requirement established above, the widtb of the tolerance zone is the nominal tolerance value specified regardless of sign. In view of the preceding, the tolerance symbols, plus or minus ( $\pm$ ), should be removed in refcrencing lead tolcrances. The omission of the plus and minus does not change the total tolerance.
minus does not change the total tolerance. column 9 , in the ratio of the diameter to 12 in .
4.5.2.3. Thread Form. The specifications for thread form are stated in detail below and are summarized in table 6.6 and figure 6.1.

Thread Crests. The minimum minor diameter of the LO thread ring gage shall be equal to the minimum pitch diameter of the external thread minus 0.25 H . This corresponds to a width of flat at the crest of the gage equal to 0.375 p . However, the minimum minor diameter of the LO thread ring gage shall not be less than the minimum minor diameter of the GO thread ring gage plus $0.0375 H$ or $0.05 h_{b}$. See col. 16 of table 6.5 . This requirement is necessary to assure that the minor diameter of the gage is not less than the minor diameter of the GO thread ring gage which may occur with a $0.375 p$ flat on the LO ring thread crest when there is a pitch diameter allowance on the product external thread combined with a large pitch diameter tolerance.

Thread Roots. The major diameter of the LO thread ring gage shall be cleared by a clearance cut of substantially $0.25 p$ width, approximately central.

The LO thread ring gage shall clear the maximum major diameter of the product external thread or the maximum major diameter of the full-form portion of the truncated thread setting plug for the LO thread ring gage, whichever is the greater. Thus, contact of the thread gage can occur on the sides of the threads but not on the crest or root. Also, the effect of angle deviation on the fit of the gage with the product thread is minimized.

Concentricity of Pitch and Minor Diameter Cylinders. The pitch and minor cylinders of the LO thread ring gage shall be concentric as stated hereinafter. On thread ring gages, an eccentric condition results in an undersize effective minor diameter having a width of flat less than 0.375 p . The permissible minimum effective minor diameter as determined by runout (total indicator variation) with respect to the pitch cylinder shall not be less than the specified minimum minor diameter minus twice the sum of the gage tolerances for pitch and minor diameter.

Pitch Cylinder, Lead, and Half-Angle. Satisfactory conformance of these elements is normally determined by the setting of the thread ring gage to the applicable truncated setting plug gage.
4.5.2.4. End Threads. The feather edge at both ends of the thread ring gage shall be removed. On gages larger than 0.5 in . nominal size or on those having less than 20 threads per in., not more than one complete turn of the end threads shall be removed to obtain a full thread blunt start. On gages 0.5 in . nominal size and smaller or on those having 20 or more threads per inch, a $60^{\circ}$ chamfer on the end threads from the axis of the gage, is acceptable in lieu of the blunt start.
4.5.2.5. Identification. The LO thread ring gage should be identified by nominal size, threads per inch, series, class, and LO pitch diameter. Example:

## .250-20 UNC 2A LO PD . 2127.

4.5.3. Thread Snap Limit Gages or Indicating Thread Gages for LO Minimum-material limit.
4.5.3.1. Purpose. Thread snap limit gages or indicating thread gages having gaging elements as specified in par. 4.5.3.3, check Class 3 A LO minimummaterial limit. For gaging practices, see par. 3.1.3, p. 6.04 .
4.5.3.2. Basic Design. The design is specified only to the extent that it affects the results obtained in gaging. Design details, etc., are optional and not included herein.

Thread snap limit gages are adjustable, and the gaging elements are adjusted and set to setting plugs and locked in proper position. Indicating thread gages are adjusted and set with reference to the applicable thread setting plugs.
4.5.3.3. Gaging Elements. The gaging elements should engage the thread over a length of approximately two pitches. The profile of the gaging element should be that of the LO thread ring gage.
4.5.3.4. Identification. Where practicable, the gaging elements should be marked with the minimum marking essential for identification. When space available for marking is inadequate and the gages

Table 6.9. W Tolerances for GO, HI, and LO Thread Gages

| Threads per inch | Tolerance on lead ${ }^{3}$ |  | Toleranee on halfangle of thread | Tolerance on major or minor diameters |  |  | Tolerance on pitch diameter |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | To and including 0.5 in dia | Above 0.5 in dia |  | To and including 0.5 in dia | $\begin{aligned} & \text { A bove } 0.5 \\ & \text { in. to } 4 \text { in. } \\ & \text { dia } \end{aligned}$ | A bove 4 in. dia | To and ineluding 0.5 in dia | A bove 0.5 in. to 1.5 in dia | Above 1.5 <br> in. to 4 in . dia | Above 4 in. to 8 in. dia | $\begin{aligned} & \text { Above } 8 \\ & \text { in. to } 12 \text { in. } \\ & \text { dia } 6 \end{aligned}$ |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
|  | in | in | ${ }_{ \pm}^{\text {deg }} \min$ | in | in | in | in | in | in | in | in |
| 80 | 0. 00001 | 0.00015 | $\begin{array}{ll}0 & 20 \\ 0 & 20\end{array}$ | 0.0003 0003 | 0.0003 .0003 |  | 0.0001 0001 | 0. 000015 |  |  |  |
| 72 | .0001 .0001 | . 000015 | $\begin{array}{ll}0 & 20 \\ 0 & 20\end{array}$ | .0003 .0003 | . 0003 |  | .0001 .0001 | .00015 .00015 |  |  |  |
| 56 | . 0001 | . 00015 | $0 \quad 20$ | . 0003 | . 0004 |  | . 0001 | . 00015 | 0.0002 |  |  |
| 48 | . 0001 | . 00015 | $0 \quad 18$ | . 0003 | . 0004 |  | . 0001 | . 00015 | . 0002 |  |  |
| 44 | . 0001 | . 00015 | $0 \quad 15$ | . 0003 | . 0004 |  | . 0001 | . 00015 | . 0002 |  |  |
| 40 | . 0001 | . 00015 | $0 \quad 15$ | . 0003 | . 0004 |  | . 00001 | . 000015 | . 0002 |  |  |
| 36 | .0001 | . 000015 | $\begin{array}{ll}0 & 12 \\ 0 & 12\end{array}$ | .0003 .0003 | . 0004 | 0.0007 | .0001 .9001 | .00015 .00015 | .0002 .0002 |  |  |
| 28 | . 00015 | . 00015 | 08 | . 0005 | . 0005 | . 0007 | . 0001 | . 00015 | . 0002 | . 00025 | 0.0003 .0003 |
| 27 | . 00015 | . 00015 | $0 \quad 3$ | . 0005 | . 0005 | . 0007 | . 0001 | . 00015 | . 0002 | . 00025 | . 0003 |
| 24 | . 00015 | . 00015 | 08 | . 0005 | . 6005 | . 0007 | . 0001 | . 00015 | . 0002 | . 00025 | . 0003 |
| 20 | . 00015 | . 00015 | 08 | . 0005 | . 0005 | . 0007 | . 0001 | . 00015 | . 0002 | . 00025 | . 0003 |
| 18 | . 00015 | . 00015 | 0 8 | . 00006 | . 0005 | . 0007 | . 0001 | . 000015 | . 0002 | . 00025 | . 0003 |
| 16 | . 00015 | . 00015 | 08 | . 0006 | . 0006 | . 0009 | . 0001 | . 0002 | . 00025 | . 0003 | . 0004 |
| 14 | . 0002 | . 0002 | $0 \quad 6$ | . 0006 | . 0006 | . 0009 | . 00015 | . 0002 | . 00025 | . 0003 | . 0004 |
| 13 | . 0002 | . 0002 | ${ }^{0}{ }^{6}$ | . 0006 | . 0006 | . 0009 | . 00015 | . 0002 | . 00025 | . 0003 | . 0004 |
| 12 | . 0002 | . 0002 | $0 \quad 6$ | . 0006 | . 0006 | . 0009 | . 00015 | . 0002 | . 90025 | . 0003 | . 0004 |
| 11.5 | . 0002 | . 0002 | ${ }_{0}^{0} \quad 6$ | . 0006 | . 0006 | . 0009 | . 000015 | . 0002 | . 00025 | . 0003 | . 0004 |
| 11 | . 0002 | . 0002 | $0 \quad 6$ | . 0006 | . 0006 | 0009 | . 00015 | . 0002 | . 00025 | . 0003 | . 0004 |
| 10 |  | . 00025 | $0 \quad 6$ |  | . 0006 | . 0009 |  | . 0002 | . 00025 | . 0003 | . 0004 |
| 9 |  | . 00025 | $0 \quad 6$ |  | . 0007 | . 00011 |  | . 0002 | . 00025 | . 0003 | . 0004 |
| 8 |  | .00025 .0003 | $\begin{array}{ll}0 & 5 \\ 0 & 5\end{array}$ |  | .0007 .0007 | .0011 .0011 |  | .0002 .0002 | .00025 .00025 | .0003 .0003 | . 0004 |
| 6 |  | . 0003 | $0 \quad 5$ |  | . 0008 | . 0013 |  | . 0002 | . 00025 | . 0003 | . 0004 |
| 5 |  | . 0003 | $0 \quad 4$ |  | . 0008 | . 0013 |  |  | . 00025 | . 0003 | . 0004 |
| 4.5 |  | . 0003 | $0 \quad 4$ |  | . 0008 | . 0013 |  |  | . 00025 | . 0003 | . 0004 |
| 4 |  | . 0003 | $0 \quad 4$ |  | . 0009 | . 0015 |  |  | . 00025 | . 0003 | . 0004 |

[^18]Table 6.10. Tolerances for Plain Gages

| Size range |  | Tolerances |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| A bove- | To and in-cluding- | XX | X | Y | Z | ZZ |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| in | in | in | in | in. | in |  |
| 0.029 | 0.825 | 0.00002 | 0.00004 | 0. 00007 | 0.00010 | 0.00020 |
| . 825 | 1. 510 | . 00003 | . 00006 | . 00009 | . 00012 | . 00024 |
| 1.510 | 2. 510 | . 00004 | . 00008 | . 00012 | . 00016 | . 00032 |
| 2. 510 | 4.510 | . 00005 | . 00010 | . 00015 | . 00020 | . 00040 |
| 4.510 | 6.510 | . 000065 | . 00013 | . 00019 | . 00025 | . 00050 |
| 6.510 | 9.010 | . 00008 | . 00016 | . 00024 | . 00032 | . 00064 |
| 9. 010 | 12.010 | . 00010 | . 00020 | . 00030 | . 00040 | . 00080 |

Table 6.11. Lengths of AGD taperlock and trilock thread plug gage blanks selected from CS8 or B47.1


NOTE 1: For Trilock Plug Blanks above 0.760 to and including 1.510, see CS8 or B47.1.

NOTE 2: For Wire Type Plug Blanks in sizes below 0.760, see CS8 or B47.1.

Table 6.12. Lengths of AGD thread ring gage blanks and total thread lengths of standard truncated setting plug gage blanks selected from CS8 or B47.1

| Thread sizes |  | Thread lengths Thread ring gages |  |  | Total thread lengths of truncated thread setting plugs |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Decimal range |  |  |  |  |  |  |  |
| Above | To and including | Thin Ring | Thick Ring | Fine-pitch instrument ring | $\begin{aligned} & \text { For } \\ & \text { thin } \\ & \text { ring } \end{aligned}$ | For thick ring | For finepitch instrument ring |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| 0.059 | 0.090 | 0.09375 |  |  | 0.21875 |  |  |
| . 090 | . 150 | . 15675 |  |  | . 375 |  |  |
| . 150 | . 240 | . 1875 |  |  | . 40625 |  |  |
| . 240 | . 365 | . 34375 |  | . 25 | . 75 |  | 0.5625 |
| . 365 | . 510 | . 4375 |  | . 3125 | 1. |  | . 6875 |
| . 510 | . 825 | . 5625 | 0.75 | . 46875 | 1.25 | 1.875 |  |
| . 825 | 1.135 | . 6875 | . 9375 | . 53125 | 1.5 | 2.125 | 1.125 |
| 1.135 | 1.510 | . 75 | 1.125 | . 625 | 1.625 | 2.375 | 1.3125 |
| 1.510 | 2.010 | . 8125 | 1.25 | . 625 | 1.875 | 2.875 | 1.3125 |
| 2.010 2.510 | 2.510 3.010 | . 875 | 1.3125 | . 6875 | ${ }_{1}^{2.875}$ | 3. 3. | 2.4375 |
| 3.010 | 3.510 | .8375 | 1.4375 |  | 2. | 3.125 |  |
| 3.510 | 4.010 | . 9375 | 1.5 |  |  | 3.25 |  |
| 4.010 | 6.260 | 1. | 1.5 |  | 2.125 | 3.25 |  |

NOTE 3: For diameters 0.059 to 0.510 in, use thin blank for all pitches, recessing sides where applicable

Above 0.510 to 1.135 in, use thick blank for pitches coarser than 12 TPI , thin blank for pitches 12 to 28 TPI, and fine pitch instrument blank for pitches 30 and finer.

Above 1.135 to 6.260 in incl., use thick blank for pitches coarser than 10 TPI , thin blank for pitches 10 to 28 TPI, and fine pitch instrument blank for pitches 30 and finer.
and gaging elements are packaged separately, the containers should be suitably marked and/or the gaging elements suitably tagged.
4.5.4. Indieating Thread Gages for Differential Gaging.
4.5.4.1. Purpose. The purpose of indicating thread gages used in differential gaging within this standard is two-fold. The gages are used: (a) by consumers, but only where it is required by supplemental specifications to determine final conformance, (b) by manufacturers, to determine cumulative effect of deviations of product thread elements as an aid in control of manufacturing. For gaging practice, see par. 3.1.4, p. 6.04.
4.5.4.2. Basio Design. The design is specified only to the extent that it affects the results obtained in gaging. Other design details pertaining to frame construction, method of operation, readout, etc., are not included herein.
4.5.4.3. Gaging Elements. The gaging elements for functional differential reading to verify conformance of product thread elements shall be so designed that:
(a) The first set shall engage over a length which approximates the thickness of the GO thread ring blank. The thread form of the gaging elements shall be the same as that of the applicable GO thread ring gage.
(b) The second set shall engage over a length of approximately two pitches and contact the thread flanks $0.375 H$ (i.e. the same as that of the comparable LO thread snap gage).

NOTE: Some representative gaging elements in current use are shown in subsection 6, p. 6.27. See the fourth paragraph under subsection 1, p. 6.01 , par. 5.4, p. 6.21 , par. 5.5 , regarding use of gaging elements.
4.5.4.4. Identification. Where practicable, the gaging elements should be marked with the minimum marking essential for identification. When space available for marking is inadequate and the comparators and gaging elements are packaged separately, the containers should be suitably marked and/or the gaging elements suitably tagged.
4.5.5. Plain Gages for Major Diameter.
4.5.5.1. Purpose. The GO and LO thread ring gages clear the major diameter of the product external thread. To check the major diameter limits, plain ring, snap, or indicating gages are required. For gaging practice, see par. 3.1.5, p. 6.04.
4.5.5.2. Basic Design. To assure that the maxi-mum-material limit is not exceeded, a plain cylindrical ring gage is used for the GO gage while a snap or indicating gage is preferred to assure conformance within the minimum-material limit. Plain progressive snap or indicating gages may be used.

Gage Blanks. Plain cylindrical ring blanks and plain progressive adjustable snap gages have been standardized for various size ranges. See CS8 or B47.1.
4.5.5.3. Identification. Fixed limit gages for major diameter of product external threads are to be identified by GO and the major diameter as follows: GO . 2500 .

### 4.6. Thread Setting Plug Gages.

4.6.1. Purpose. Thread setting plug gages are used to set adjustable thread ring gages, thread snap limit gages, and indicating thread gages to specified size. Thread setting plug gages are also applied to detect wear on gages and gaging elements in use. GO thread setting plug gages are made to the maximum-material limit of the thread specification while LO thread setting plug gages are made to the minimum-material limit of the thread specification. For gaging practice, see par. 3.1.2, p. 6.03 .
4.6.2. Basic Design. Thread setting plug gages are of two standard designs which are designated as basic-crest (full form) and truncated setting plugs. The basic-crest GO setting plug is one having a width of flat at the crest equal to $0.125 p$. The truncated GO setting plug is the same as the basiccrest setting plug except that it is longer and the crest of the thread is truncated a greater amount for half the length of the gage giving a full form portion and a truncated portion.

Gage Blanks. For practical and economic reasons the lengths of setting plug gages have been standardized for various size ranges and pitches. See CS8 or B47.1 and table 6.12. The length of the full form and the length of the truncated sections are each at least equal in length to the thickness of the corresponding thread ring gage.
4.6.3. Thread Form. The specifications for thread form of setting plug gages are stated in detail below and are summarized in table 6.7 and figure 6.2.
4.6.3.1. Thread Crests of Truncated and BasicCrest Maximum-Material-Limit (GO) Thread Setting Plugs.

The major diameter of the basic-crest setting plug and of the full form portion of the truncated maxi-mum-material-limit (GO) thread setting plug is equal to the maximum major diameter of the product external thread.

The major diameter of the truncated portion of the truncated maximum-material-limit (GO) thread setting plug is equal to the maximum major diameter of the product external thread minus $\left(0.060 \sqrt[3]{p^{2}}+\right.$ $0.017 p$ ). See col. 10 of table 6.5 .
4.6.3.2. Thread Crests of Truncated and BasicCrest Minimum-Material-Limit (LO) Thread Setting Plugs.

The major diameter of the basic-crest setting plug and of the full form portion of the truncated mini-mum-material-limit (LO) thread setting plug is equal to the maximum major diameter of the product external thread. (Same as GO thread setting plug.) The maximum major diameter of the gage must correspond to a truncation that is not less than 0.067 H ( $0.067 p$ flat) or 0.0009 in . ( 0.001 in flat) whichever is the greatest truncation.

NOTE: Method of Computation. Select the smallest of following three values. (a) Maximum major diameter of the product external thread (Max pitch diameter of product external thread plus 0.75 H (b) Minimum pitch dimaeter of the product external thread plus ( $H-0.00173$ ) minus gage tolerance. (c) Minimum pitch diameter of the product external thread plus $0.75 p$.

The major diameter of the truncated portion of the truncated minimum-material-limit (LO) thread setting plug is equal to the minimum pitch diameter of the product external thread plus 0.5 H .
4.6.3.3. Thread Roots. The minor diameter of thread setting plug gages shall be cleared beyond a $0.125 p$ width of flat either by an extension of the sides of the thread toward a sharp $V$ or by an undercut no wider than $0.125 p$. See figures 6.2 and 6.3.
4.6.3.4. Pitch Diameter, Limitation of Taper. To effect proper setting of a thread gage, the maximum permissible taper over the entire length of the setting plug shall be within the following limits: For sizes to and including 1.50 in . nominal diameter, maximum taper cquals 0.0001 in ., except that for threads coarser than 16 threads per inch the maximum taper equals 0.00015 in . For sizes larger than 1.50 in . to and including 6.25 in . nominal-diameter, maximum taper equals 0.0002 in . The permissible taper shall be back taper (largest diameter at entering end) and shall be confined within the gage pitch diameter limits.
4.6.3.5. End Threads. The feather edge at both ends of the threaded section of the setting plug shall be removed. On pitches coarser than 28 threads per inch, not more than one complete turn of the end threads shall be removed to obtain a full thread blunt start. On pitches 28 threads per inch and finer, a $60^{\circ}$ chamfer from the axis of the gage is acceptable in lieu of the blunt start.
4.6.3.6. Lead Deviation. Deviation in lead shall be within the limits specified. See table 2.22 , par. 4.3.3.3, p. 6.05.
4.6.3.7. Half-Angle Deviations. Deviations in half-angle shall be within the limits specified. Sec table 2.22 .
4.6.4. Identification. The GO thread setting plug for Class 3A gage is basic and is applicable to Class 2A after coating. Accordingly, it is recommended that the gage be identified by set plug, nominal size, threads per inch, series, and GO pitch diameter.

Example:

## SET PLUG .250-20 UNC GO PD . 2175

The GO thread setting plug gages for Classes 1 A and 2 A are under basic, having a common allowance. Accordingly, it is recommended that the gage be identified by set plug, nominal size, threads per inch, series, class, and GO pitch diameter.

Example:
SET PLUG . $250-20$ UNC 1A-2A GO PD . 2164
The LO thread setting plug gage is different for each class and accordingly should be identified by set plug, nominal size, threads per inch, series, class, and LO pitch diameter.

Example:
SET PLUG .250-20 UNC-2A LO PD . 2127

### 4.7. Plain Plug Acceptance Check Gages.

4.7.1. Purpose. GO and NOT GO plain plug acceptance check gages verify the minor diameter limits of size of thread ring gages after the thread rings have been properly set with the applicable thread setting plug gages. For gaging practice, see par. 3.1.2, p. 6.03 .
4.7.2. Basic Design. The direction of the gage tolerances on plain plug acceptance check gages is reversed as follows: The GO plain plug gage is made to the minimum minor diameter of the thread ring gage with the tolerance taken minus. Sec table 6.10. The NOT GO plain plug gage is made to the maximum minor diameter of the thread ring gage with the tolerance taken plus.

Gage Blanks. For standardization and economic reasons the gaging members and handles have been standardized for various size ranges. See CS8 or B47.1.
4.7.3. Identification.

The GO and NOT GO plain plug acceptancc check gages for the GO thread ring gage should be identified as GO and NOT GO Acceptance Checks for GO Thread Ring Minor Dia XXXX-XXXX.

The GO and NOT GO plain plug acceptance check gages for the LO thread ring gage should be identified as GO and NOT GO Acceptance Checks for LO Thread Ring Minor Dia XXXX-XXXX.

## 5. RECOMMENDED GAGING PRACTICES

5.1. Dimensional Acceptability Of Threads. -General practice as to the dimensional acceptability of threads shall be based on the interpretations of pitch diameter limits of size in subscction on Limits of size in scetion 3 and the following specifications of gages and gaging practices:
(a) At maximum-material limits ${ }^{2}$ - For referec purposes, the dimensional acceptability of threads at the maximum-material limits shall be based on gaging with GO thread plug and ring gages conforming as closely as practicable to the limits of size of the thread and to the thread form and length specified for such gages. (See par. 2.3, p. 6.01.)
(b) At minimum-material limits.-Unless otherwise specified on the drawing or procurement document, dimensional acceptability at the minimummaterial pitch-diameter limits shall be based on the following accepted practices:
(1) Functional (virtual) diameter gaging practiceFunctional (virtual) diameter gaging practice, involving the use of thread plug gages and thread ring gages, conforming as closely as practicable to the limits of size of the thread and to the thread form and lengths specified in this section for such gages, is specified for the minimum-material limits of classes 1 A and 2 A external threads, and classes $1 \mathrm{~B}, 2 \mathrm{~B}$, and 3 B internal threads.

[^19](2) Single element gaging practice.-Single element gaging practice, involving the use of thread snap gages or indicating type gages having thread form in accordance with this section, or its equivalent, engaging the thread over a length of two pitches, is specified for the minimum-material limits of class 3A external threads.
5.2. Procedure In Setting Adjustable Limit And Indicating Thread Gages.-The size of adjustable limit or indicating thread gages is controlled by utilizing the applicable $W$ tolerance thread setting plugs. The observance of uniform setting procedures will aid in the proper setting and surveillance of the thread gages and facilitate correlation of gaging results.
5.2.1. Adjustable Thread Ring Gages.-In setting an $A G D$ adjustable thread ring gage, the sealing compound should be removed and the locking screw loosened. Turning the adjusting screw to the right enlarges the ring so that it turns freely onto the thread setting plug. Alternately adjusting the adjusting screw and tightening the locking screw, a firm fit on the smallest portion of the thread in the ring should result. While making the adjustment, the knurled outside diameter and both sides of the ring should be lightly tapped with a soft-tip or plastic hammer to permit the threads of the ring to wrap themselves around the threads of the setting plug.

Care should be taken to assure that there is no lateral displacement of the sectors comprising the ring gage that would produce a lead deviation beyond the prescribed tolerance zone. After satisfactory adjustment has been obtained, the ring is to be removed from the plug and the same procedure of tapping is repeated with slightly greater emphasis to the sides. If the thread ring gage possesses proper rigidity, the same feel should be still there when the setting gage again is turned into the ring. A tighter fit or inability to reenter the setting gage denotes a fault of the locking devjce, that should then be taken apart and checked for dimensional conformity to CS8 or B47.1. It is often advisable to do this before even attempting to adjust the thread ring gage. When proper adjustment has been obtained, the gage should be sealed.

In setting to a truncated setting plug, the ring gage may be set to either the full or the truncated portion. It is common practice to set slightly freer than a snug fit to the truncated portion and then to check the root clearance and wear of flank angle by screwing the ring onto the full portion. Extreme caution is required when this practice is followed to prevent damage to the thread crest of the setting plug. The opposite practice is to adjust and set the ring to the full portion and then determine the fit of the gage on the truncated portion. If the thread form of the ring gage is satisfactory, there will be slight or no change of fit. In the case of a worn thread ring gage, the presence of shake or play when on the truncated portion indicates that the sides of the thread are no longer straight near the root and the gage should be relapped or discarded.

In order to provide maximum wear life of a setting plug, the plug should be threaded into a ring as few times as possible. This will prevent uneven wear and a taper on the truncated end of the plug. When setting plugs are thus used properly they do not wear unevenly. However, when setting plugs are applied repeatedly to check thread ring gages, the criteria for acceptability will vary with the type and application of the ring. A LO ring, for example, should be a snug fit at full engagement and provide some resistance to turning at one or two turns engagement. GO thread ring gages should also be a snug fit at full engagement. When the length of the product thread permits engagement with the full length of the GO ring, the requirement as to partial engagement may be relaxed to permit a slightly freer fit. However, there should be no relaxation in the requirements when short product threads, that only partly engage the GO ring, are being engaged.

If a basic-crest setting plug is used to set a thread ring gage, root clearance of the thread in the ring should be determined by the procedure outlined below.

The ring gage should be given further inspection to determine whether or not the minor diameter is within the specified limits. The minor diameter may be inspected by means of GO and NOT GO plain cylindrical plug acceptance check gages or by direct measurement.
5.2.1.1. Procedure for Determining the Clearance in Thread Ring Gages.-The roots of threads of ring gages, particularly LO ring gages, frequently do not clear the maximum major diameter of the external thread. To assist the gage maker and gage inspector, the recommended procedure for determining the clearance at root of thread of ring gages is given to supplement, or substitute for, the use of truncated setting plugs described in par. 5.2.1. For this purpose an optical examination of a sulfurgraphite, plaster of Paris, copper-amalgam, or other suitable cast of the thread is made by means of a projection comparator, toolmaker's microscope, or universal measuring microscope. The actual magnification of the instrument as used must be known.
(a) Methods of making sulfur-graphite casts.-Sul-fur-graphite casts are made from a thorough mixture of finely powdered graphite and crushed lump sulfur which is heated in a ladle until the sulfur is completely melted and becomes viscous. This mixture may be used repeatedly by crushing and remelting. The graphite should constitute about 7 percent of the mixture by weight, although in the practice of various users, the proportion varies from 4 to 20 percent. The graphite is added to eliminate reflections that would be produced by a plain sulfur cast, and to reduce the tendency to shrink upon cooling.

The casting mold may be formed by holding the ring gage between thin plates in the jaws of a vise, the top edge of the plate on one side being well below the thread axis. For small sizes of threads, a convenient arrangement is to use a taper mandrel that is provided with a lengthwise groove having
smooth surfaces and an included angle of about $90^{\circ}$, into which the mixture is poured, and in which the cast is later mounted for examination. The bottom of the slot has a slight taper toward the axis at the small end. A square metal stop clamped in the groove serves as a wall in casting. The mandrel is also useful in making copper-amalgam casts, in which case the casting mixture is pressed in.

The sulfur-graphite casting mixture is poured into the mold when the temperature is from $260^{\circ}$ to $266^{\circ} \mathrm{F}$, and allowed to solidify with slow cooling. The cast may be marked with an identification number with a steel stylus. Sulfur-graphite casts warp considerably after a few hours.
(b) Method of making plaster of Paris casts.-A plaster of Paris cast is usually made to determine errors in thread angle, and this cast can usually be used to determine clearance. Such a cast is made by mixing 5 parts ( 28 g or 1 oz ) of a good grade of dental plaster of Paris with from 4 to 5 ( 26 ml ) parts by weight of potassium-bichromate solution made by dissolving 40 g in 1 liter of water. The potassium bichromate inhibits rusting of the gage. This mixture is applied to the threads inside a mold which may be fashioned from cardboard or a strip of copper, with modeling clay pressed in to the threads along the outside bottom edges of the mold. It should be allowed to harden completely before removal. Plaster of Paris casts have less shrinkage than sulfur-graphite, but do not retain dimensions over extended periods of time. They are difficult to remove from rough finish threads without damage.
(c) Determining clearance of GO thread ring gages.The flat at the crest of the naximum external thread is $0.125 p$, therefore, if the root of thread of the GO ring is relieved to a width of $0.125 p$, the ring threads clear the maximum major diameter of the thread. If the roots of the GO ring gage threads are not relieved, they must be to a sharp enough $V$ to clear a flat of $0.125 p$. The flanks of the thread should be straight to the point where the $0.125 p$ flat will make contact with the flanks of the thread. The width of flat on the chart or template used should be $0.125 p$ times the magnification of the comparator.
(d) Determining clearance of LO thread ring gages.The flat at the crest of a screw with maximum major diameter and minimum pitch diameter is determined by the formula:

$$
\text { Flat }=\frac{p}{2}-h^{\prime} \tan 30^{\circ}=\frac{p}{2}-0.57735 h^{\prime}
$$

for the Unified form of thread, where $h^{\prime}=$ maximum major diameter minus minimum pitch diameter.

If the LO ring gage has a relief of $0.25 p$ as recommended, it is necessary to determine whether or not the relief is deep enough. To do this, make a chart or template representing a $60^{\circ}$ thread with a flat at the crest cqual to the flat, as determined by the above formula, times the magnification of the comparator. This chart or template should fit the image of the thread and contact the flanks of the thread image without contacting in the relief. If the ring
threads are not relieved, they must be sharp enough to permit the chart or template to contact on the flanks of the image rather than in the root.
5.2.2. Thread Snap Gages.-The gaging clements of most types of thread snap gages are mounted on eccentric pins or studs which can be securely locked in position by means of locking screws or nuts. Since thread snap gages may be of different designs, the above description is used only to illustrate a general classification.
It is essential that proper setting procedures be utilized to assure uniform contact pressure between the gaging elements and their applicable thread setting plugs. The gaging elements should be adjusted so that the thread setting plug will have a minimum pcrceptible drag when passing it through the gaging elements. One method is to adjust the gage so that the pressure between the gaging elements and the thread setting plug will just support the weight of the thread snap gage and, as the setting plug is slowly rotated, the thread snap gage will drop off by its own weight.

In setting large diameter thread snap gages, it may be desirable to support the thread snap gage in a vise or other holding means. Care should be taken to a void deformation of the gage frame. Uniform gaging pressure can be attained by holding the gage frame in a vertical position and adjusting the gaging elements so that the thread setting plug will have perceptible drag and will just drop through the gaging elements by its own wcight.

Care should be taken not to use too much force when checking or setting thread snap gages so that deformation, brinelling, or permanent damage to the gaging elements, gage frame, or thread setting plug does not occur.

Standard AGD truncated or basic-crest thread setting plugs may be used for setting thread snap gages. Large diameter thread snap gages are sometimes adjusted and set to the proper pitch diameter by direct measurcment, size blocks, or various types of setting bars. Details of design and specific instructions covering the use of various types of setting means for large diameter thread snap gages are available directly from the gage manufacturer.
5.2.3. Indicating Thread Gages.-Indicating thread gages are of various designs but most of them are of the comparator type which compare and indicate the variation in size between a thread setting plug of known size and the size of the product thread being checked. Indicating thread gages provide an adjustable gaging force as an inherent part of the gage body construction. This gaging force may be varied according to the particular characteristics (i.e., weight, size, shape, etc.) of the product being checked. The accuracy of the setting and gaging is not normally influenced by variations in the gaging force as the gage is set and used with the same force applied in both instances. Care should be used in selecting the gaging force to be applied in relation to the deformability of product threads.

Usually the applicable GO and LO AGD trun-
cated or basic crest thread setting plugs are used to set the indicating thread gages. However, a thread setting plug of other than the applicable size is sometimes used and the tolerance zone for the product thread is established with reference to the size of the thread setting plug employed. This practice is advantageous as it eliminates the necessity for having applicable setting plugs for each of the various classes of thread as well as special limits. Modification of limits of size to provide allowance for coating and limits of size after coating may be readily established with reference to the size of a thread setting plug gage.

Gage manufacturers usually offer specific information regarding the operation, checking, setting, and surveillance to cover their particular designs of indicating type thread gages.
5.3. Limit Gages For Use In Manufacturing.
5.3.1. In the manufacture of product threads it is necessary to control the limits of size and the various individual thread elements so that the threads produced will be acceptable with final conformance gages. Adoption and use of specific manufacturing gages is the prerogative of individual organizations. If the producer uses gages other than those described in this section, he should evaluate the results obtained to assure correlation with the final conformance gages specified in this section and final conformance within the specifications in section 2.
5.3.2. Limit gages used in manufacturing checking may be of the same general design of thread plug and ring gages used in final conformance gaging. It is important, however, that thread plug and ring gages used in manufacturing checking have pitch diameter tolerances so applied as to be within the product limits of size: i.e., GO thread plugs with tolerance plus, HI thread plugs with tolerance minus, GO thread rings and GO setting plugs with tolerance minus, LO thread rings and LO setting plugs with tolerance plus. Whereas final conformance gages should be as close as practical to the extreme limits of size of the product threads, gages for manufacturing checking should be as far removed from those extremes as is practicable while still within X gage tolerances. When X pitch diameter tolerance is specified for setting plugs, it is recommended that W tolerances for lead and half-angle be specified. (See par. 4.3.3.1, p. 6.05.)
5.3.3. A practice sometimes utilized is to check the pitch diameter of new gages as received, to assign for final conformance gaging those closest to the extreme sizes of the product thread and to assign for manufacturing checking those farthest from the extreme limits of size of the product thread.
5.3.4. Periodic surveillance of both final conformance and manufacturing gages will disclose when the manufacturing gages, due to wear, approach approximately the same size as those used as final conformance gages. At such time either of two courses of action is suggested.
(a) Manufacturing gages (GO) may be transferred to the final conformance application, and be replaced
with new gages from the manufacturing gage stock, or
(b) Final conformance gages (HI/LO) may be transferred to the manufacturing gage application, and vice versa.

Perhaps the most difficult point to reconcile in such a program is that of deviations resulting from normal use. Starting threads of both plugs and rings bear the brunt of use when making an inspection. Wear is seldom uniformly distributed over the gaging length and the thread flanks, resulting in inaccuracies of flank angle and pitch diameter. It is important for the success of such a program that inspection and manufacturing personnel agree on the position for the pitch diameter check and the degree of taper which may be tolerated before that gage should be taken out of service. The HI/LO gaging practice which permits the minimum-ma-terial-limit gages to assemble for their entire length, provided a definite drag is achieved on or before the third thread of entry, has alleviated appreciably the problem of worn end threads.
5.3.5. There are a number of other styles of limit thread gages utilized as manufacturing gages for technical or economic reasons. Among these are caliper or snap gages using gaging elements of various configurations. Included are those utilizing rolls, segments, serrated anvils, wires, probes, and ball points. Whereas all of these would accept perfect threads with little or no appreciable difference, they may react quite differently on threads having acceptable deviations.
5.3.6. There is an additional problem, primarily stemming from economics, where a relatively few parts with threads are involved, when neither limit nor indicating gages are a vailable and it is economically impracticable to procure them. Such situations are daily problems in model shops, experimental and research departments, tool rooms, and job shops. A discussion of some commonly used practices follows:
5.3.7. Adequate means for determining accuracy of thread angle, thread form, and lead (both linear and helical) are essential. Optical projection or mechanical gages of a general nature are uscd frequently for such checking.
5.3.8. Numerical values for groove diameter may be determined by use of the three-wire method or for LO minimum-material limit by the use of thread micrometers. The accuracy of these values is affected by the following factors.
5.3.9. Values obtained from three-wire measurement are influenced by:

Deviation in geometry and pitch of product thread.
Product thread characteristics (cleanliness, surface texture, hardness, etc.).
Measuring force exerted over the wires.
Operating skill in handling part, wires, and micrometer.
5.3.10. Values obtained with thread micrometers are influenced by factors enumerated in par. 5.3.9, as applicable, and accuracy of the cone and vee contact elements.
5.3.11. To make use of the values covered in par. 5.3.8 (as applicable to the maximum-material limit, i.e., functional diameter), the diameter equivalents of deviations in lead and half-angle must be taken into account.
5.3.12. For use as a manufacturing check at minimum-material limit the values covered in par. 5.3.8 may be used without change. However, one must realize that these values may be more restrictive of pitch diameter limits than would be experienced with limit gages.
5.4. Differential Gaging.
5.4.1. Differential Gaging provides an economical method of checking for thread element deviations of product complete threads. The principle involved is the determination of values for two essential features or characteristics and by subtraction to determine the difference, i.e., the differential reading. This principle as utilized in checking Unified Screw Threads is a convenient and effective manner of evaluating the effect of deviations of the several elements and some other characteristics. It is helpful to the manufacturer in control of tools and processes. It is not intended that values determined for Differential Gaging be utilized for verification of size conformance.
5.4.2. The following differential readings determined thru the use of appropriate gaging elements are utilized for final conformance gaging of thread elements when specified. See par. 4.5.4.3, p. 6.16, and par. 5.5.
5.4.3. Functional Differential Reading Par. 4.5.4.3, p. 6.16, utilizes Gaging Elements 6.5(a), p. 6.27, for determination of GO functional size, and 6.5(b) for determination of LO minimum-material limit. When the difference between values so determined (Functional Differential Reading) exceeds the specified percentage of the applicable pitch diameter tolerance, it is necessary to make a further analysis to determine if either lead or flank angle exceeds the allowable tolerance. Functional Differential Reading may not be used in thread analysis. (See par. 5.5.)

NOTE 1: The numerical value determined for the Functional Differential Reading will not correlate with that determined by measurement, nor that determined in Thread Analysis except in the case of a perfect thread. Reason is that the contour of the gaging elements $6.5(\mathrm{~b})$, p. 6.27, engage a significant portion of the flank angle and approximately two pitches length of engagement. To be completely assured that no single element exceeds the specified tolerance, the Functional Differential Reading should not exceed one-half of the specified tolerance.
5.4.4. Cumulative Differential Reading.-The size (using gaging elements $6.5(\mathrm{~d})$, (f), (g), or (i) with ( j$)$, (k), (l), or (m), p. 6.28, profile) devoid of any effect from lead or angle deviations is subtracted from the value for functional size (using gaging elements 6.5(a)) to establish the CUMULATIVE DIFFERENTIAL READING. When this differential reading does not exceed the specified percentage of the applicable pitch diameter tolerance, the thread elements (lead and flank angle) are well within tolerance. If differential reading exceeds the
specified percentage of the applicable pitch diameter tolerance, it is necessary to make a further analysis of lead and flank angle separately. See pars. 5.4.5, 5.4.6, and 5.5. The values determined and utilized in Differential Gaging should not be used for verification of size conformance.
5.4.5. Lead Differential Reading.-Lead Deviation is evaluated using gaging elements as provided in subsection 6, p. 6.27. Gaging elements 6.5(a) engage the thread over approximately the normal length of engagement. Gaging elements 6.7 (n) engage the thread over a length not excecding one pitch. Both contact the thread with a flank engagement of $0.625 H$. Care must be taken to avoid any error in product thread cylindricity affecting the readings. The difference between the values is used to determine the LEAD DIFFERENTIAL READING. It is intended that this reading should not exceed the specified percentage of the applicable pitch diameter tolerance.
5.4.6. Flank Angle Differential Reading.-Flank Angle Deviation is evaluated using gaging elements as provided in subsection 6, p. 6.27. Gaging elements 6.5(c) engage the thread flank $0.375 H$ (i.e., that which is a vailable at minimum-material condition of the major diameter). Gaging elements 6.6(1) contact the gage flank with curved contacts, or contacts having a slight flat. Both gaging elements engage the thread not over one pitch in length. Care must be taken to avoid any effect of product thread cylindricity affecting the reading. The difference between the values so determined, multiplied by two, is the FLANK ANGLE DIFFERENTIAL READING. It is intended that this reading should not exceed the specified percentage of the applicable pitch diameter tolerance.
5.5. Thread Analysis Utilizing Indicating Thread Gages.
5.5.1. Differential Gaging provides an economical method of checking to verify conformance of thread elements of product complete threads. However, when a numerical value for deviations in each of the several elements is desired, more comprehensive Differential Gaging and Thread Analysis are utilized as covered in the following paragraphs.

The most effective manner by which to convey and understand Thread Analysis utilizing Indicating Thread Gages is to outline the procedures and interpretations. The following applies to gages for product external threads. Comparable techniques and procedures are utilized for checking product internal threads but are not covered in detail herein. Details of gaging elements are presented in subsection 6, p. 6.27.
5.5.2. Differential Gaging Procedures.-The value yielded for the product complete thread, when checked with an indicating thread gage utilizing gaging elements 6.5(a), p. 6.27, to determine Functional Diameter, should at no point along the thread exceed the specified maximum-material limit.

On a perfect thread, the reading obtained when utilizing applicable indicating thread gages would be identical for Functional, Pitch, Groove, and Ridge Diameters.

The deviation in any single thread element, such as lead and flank angle, may not exceed the diameter equivalent of the allowable specified percentage of the pitch diameter tolerance. This is interpreted to mean that no deviation in any single thread element may exceed the allowable specified percentage of the pitch diameter tolerance even though the size of the thread falls within the specified maximum and mini-mum-material limits.

Any deviations in lead and flank angle of product threads are reflected in the direction of maximum material. Thus, the numerical value for Functional Diameter will differ from the numerical values for LO Minimum-Material Size or Pitch Diameter, as applicable. This difference in numerical values is referred to as the Differential Reading of which there are four as covered in par. 5.4. These numerical values are affected by some features of the gaging elements and some conditions of the product threads which are overlooked all too frequently. The following examples in this category and explanations may be of assistance in evaluating and selecting the applicable gaging elements.

NOTE 1 : Pitch Diameter.-It ls recognized that numerical values determined by various gaging elements reflect deviations in pitch and flank angle. (See subsection 6, p. 6.27.)
When pitch and flank angle of product threads are within acceptable deviations (see par. 5.5.2.1) the difference in numerical values between gaging elements engaging in the groove or engaging both the thread ridge and groove is of negligible magnitude. A few examples are given below to illustrate the magnitude of this difference on product threads having maximum permissible progressive lead deviation for Unified Threads over a length of engagement comparable to the thickness of the applicable GO thread ring gage. See par. 4.5.4.3., p. 6.16. These values are yielded by the following formula:

$$
V=0.866 L T / N T R
$$

where: $V=$ Variation between pitch diameter and groove diameter values
$L T=$ max acceptable lead deviation in product thread $N T R=$ number of threads in thread ring gage.

|  | 1 A | 2 A | 3A |
| :---: | :---: | :---: | :---: |
| . $250-20$ UNC | 0.00021 | 0.00014 | 0.00010 |
| .250-28 UNF | . 00013 | . 00009 | . 00007 |
| . $250-32$ UNEF |  | . 00007 | . 00005 |
| . $750-10$ UNC | . 00029 | . 00020 | . 00015 |
| .750-16 UNF | . 00021 | . 00014 | . 00010 |
| .750-20 UNEF |  | . 00011 | . 00007 |

NOTE 2: Flank Angle
(a) Effect of engagement of gaging contacts on thread flanks. Functional Differential Reading utilizes 0.625 H and $0.375 H$ flank engagements for verifying conformance, whereas Cumulative Differential Reading utilizes $0.625 H$ and curved (or slight flat) contacts to determine a numerical value representative of the extent of the deviation. Values achieved are significantly different as illustrated by the formulas and tabulation which follow.

Formulas:

$$
\begin{aligned}
\text { Plus Angle }\left\{\begin{aligned}
A & =0.10825 p \tan 30^{\circ} \\
B & =A \cot (\alpha+) \\
\text { Variation } & =2(0.10825 p-B)
\end{aligned}\right. \\
\text { Minus Angle }\left\{\begin{aligned}
A & =0.10825 p \tan 30^{\circ} \\
B & =A \cot (\alpha-) \\
\text { Variation } & =4(B-0.10825 p)
\end{aligned}\right.
\end{aligned}
$$

|  | 1 A |  | 2 A |  | 3 A |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | + angle | - angle | + angle | - angle | + angle | - angle |
| . $250-20 \mathrm{UNC}$ | 0.00106 | 0.00240 | 0.00072 | 0.00164 | 0.00056 | 0.00112 |
| . $250-28$ UNF | . 00092 | . 00216 | . 00064 | . 00136 | . 00005 | . 00100 |
| . $250-32 \mathrm{UNEF}$ |  |  | . 00060 | . 00136 | . 00046 | . 00100 |
| .750-10 UNC | . 00166 | . 00372 | . 00104 | . 00244 | . 00086 | .00180 |
| .750-16 UNF | . 00142 | . 00370 | . 00098 | . 00204 | . 00076 | . 00156 |
| . $750-20 \mathrm{UNEF}$. |  |  | . 00082 | . 00184 | . 00064 | . 00156 |

(b) Effect of deviations in plus direction and minus direction. The dual formulas and sets of values in the table result from the unequal heights above and below the pitch line (addendum and dedendum). This complexity may be resolved by locating the curved (or slight flat) contacts above the pitch line as shown in $6.6(1)$ and (m), p. 6.29.
(c) Effect of deviations in major diameter. A specific deviation in flank angle yields significantly different values when the major diameter is at maximum and when it is at minimum when using $0.625 H$ and curved (or slight flat) contacts. This complexity may be resolved by using 6.5 (c), p.6.28, $(0.375 H)$ which bears on flank length and $6.5(\mathrm{~d}), 6.6(1)$, or (m) (curved or slight flat) contacts. Multiplying the resultant figure by two converts the reading to that which is applicable to the full 0.625 H length of flank.
5.5.2.1. When the Cumulative Differential Reading is not greater than the allowable specified percentage of the pitch diameter tolerance, the product thread is verified as well within the specification. (See par. 5.4.4, p. 6.21.) When the Cumulative Differential Reading is greater than the allowable specified percentage of the pitch diameter tolerance, the product thread must be analyzed further to assure that the diameter equivalent of the deviation of either lead or flank angle does not exceed the allowable percentage of the pitch diameter tolerance. Lead equivalent deviation, for practical purposes, applies over the length of the applicable GO thread ring blank in CS8 or B47.1.
5.5.3. Analysis of Deviations in Product Threads.
5.5.3.1. Deviation in Lead. Deviation in lead is especially important since it affects pitch diameter in the ratio of 1.732 to 1 in a $60^{\circ}$ thread. To check deviation in lead:
(a) Determine the straightness of the product thread by checking at different positions along the product thread using the $6.5(\mathrm{~d})$, (e), (g), or (i), p. 6.28, gaging elements and note the position of the first full thread.
(b) Determine and note the functional diameter of the product thread.
(c) Engage the product thread at the position of the first full product thread as determined in (a) with the first thread of the functional diameter gaging elements $6.5(\mathrm{a})$ or with $6.7(\mathrm{n})$ single rib gaging elements, and note the difference in readings. This is the Lead Differential Reading. If the difference is greater than the allowable percentage of pitch diameter tolerance, exclusive of taper, it signifies that the lead deviation is excessive.

NOTE 3: In steps (b) and (c) the results are not affected by deviation in flank angle since the length of flank angle contact in both steps is the same. The only difference in contact is in the length of engagement. Lead deviation may be wholly compensated for by taper deviation since the diameter equivalent of lead deviation will not influence the reading until it exceeds the taper deviation. The extent of taper deviation is known as measured in step (a). If the lead differential reading exceeds this taper deviation by more than the pitch diameter equivalent for lead deviation, the lead deviation is excessive. If the lead differential reading does not excecd the permissible taper deviation, it indicates that the pitch diameter equivalent for lead deviation is less than the maximum taper deviation. If the taper deviation is within the required percentage of pitch diameter tolerance, then it would follow that the lead deviation is also within the required percentage of pitch diameter tolerance and in conformance with specified tolerance.
5.5.3.2. Deviation in Flank Angle. Deviation in flank angle may be revealed by engaging the first full product thread with the $6.5(\mathrm{~d})$, (f), (g), or (i) gaging elements (see 6.5, p. 6.28) and then engaging the same thread with $6.7(\mathrm{n})$ single rib gaging elements or 6.5(a) gaging elements. If this Flank Angle Differential Reading exceeds the specified percentage of pitch diameter tolerance, it may be that the product thread has excessive flank angle deviation. (See Note 6.)

Analysis of Thread Flank Deviation. With the above types of elements, there are two product deviations which can affect the differential reading. These are: direction of angle deviation (Note 4) and actual major diameter of product thread (Note 5). To reduce these effects, the gaging elements may consist of $6.6(\mathrm{l})$ or (m) limited contact elements used in conjunction with 0.375 H LO single element profile elements 6.5 c . The difference between readings obtained using this combination of gaging elements, multiplied by two, is the diameter equivalent of flank angle variation present in that product thread.

NOTE 4: The reading for a plus angle deviation on the product thread checked, will be greater than that for a minus angle deviation of the same angular mangitude. This results from unequal height of profile, above and below the pitch line (addendum and dedendum) for Unified threads.

NOTE 5: The differential so obtained is greater for a product thread having maximum major diameter than for one having minimum major diameter.
5.5.3.3. Taper. Taper is determined by checking at several positions along and over the length of engagement of the product thread using the $6.5(\mathrm{~d})$, (e), (f), (g), or (i) gaging elements, p. 6.28.
5.5.3.4. Deviation in Minor Diameter or Root Fillet. Oversized minor diameter or root fillet may be revealed by engaging the first full product thread in the $6.5(\mathrm{~d})$, (f), (g), or (i) gaging elements and then engaging the same thread in the $6.7(\mathrm{n})$ single rib gaging elements or 6.5(a) gaging elements. If this Flank Angle Differential Reading exceeds the specified percentage of pitch diameter tolerance, it may be that the product thread has an oversized minor diameter or root fillet. (See Note 6.)

NOTE 6: For further analysis of product thread profile and control of threading tools, optical projection methods are suggested. They are particularly useful in checking thread form, flank angle, and pitch deviations of product threads and manufacturing tools.
5.5.3.5. Out-of-Round. Out-of-Round in a product thread may be elliptical, oval, egg-shaped, or lobed (frequently called clover leaf). Ovality is detected most effectively with two-point gaging contacts in an indicating thread gage. Lobing can be detected most effectively with three-point gaging contacts in an indicating thread gage. See figures $6.13,6.14$, and 6.15, p. 6.24 , and notes 7 and 8 .

NOTE 7: A gage having two gaging elements is preferred for detecting an elliptical condition, while a gage having three gaging elements is preferred for detecting the multi-lobed condition.

NOTE 8: Any helix variation (deviation in helical path or "drunkenness") may be reflected in the check for roundness. When an excessive deviation from roundness is detected, further analysis should be made utilizing equipment of a universal nature capable of differentiating and evaluating helix variation, or equipment especially made for evaluating helical path deviation. This check is applicable when the product thread call-out specifies control and inspection of thread elements.
5.5.4. Determining Allowances on Pitch Diameter to Compensate for Lead Deviation in Product Threads with Long Length of Engagement.
5.5.4.1. Determine the straightness of the product thread and note the location of the first full product thread with reference to the starting thread using the pitch diameter gaging elements with an indicating thread gage.
5.5.4.2. Determine and note the functional diameter of the product thread using the functional diameter indicating thread gage.
5.5.4.3. Engage the first full product thread (as determined in par. 5.5.4.1) in the first thread of the functional diameter gaging elements and note the size indication.
5.5.4.4. Subtract the first full product thread diameter numerical value (par. 5.5.4.3) from the functional diameter numerical value (par. 5.5.4.2). This difference in readings is the differential numerical value and represents the pitch diameter equivalent of the lead deviation in the product thread over a length equal to the length of the functional diameter gaging elements.


Figure 6.13. Out-of-round: elliptical, oval, or eqg-shaped. (Utilizing segments for gaging elements).


Figure 6.14. Out-of-round: elliptical, oval, or egg-shaped. (Utilizing rolls for gaging elements).


Figure 6.15. Out-of-round: Lobed. (Utilizing rolls for gaging elements).
5.5.4.5. Divide the length of engagement of the product thread by the length of the functional diameter gaging elements. This result is the Length Factor.
5.5.4.6. Multiply the differential reading (par. 5.5.4.4) by the length factor (par. 5.5.4.5). This result is the amount by which the specified maximummaterial functional diameter of that external product thread must be below the specified maximum-material limit. This will compensate for the lead deviation in that product thread and will assure acceptance over full length engagement with a mating product thread made to its specified maximummaterial size.
5.6. Gaging Functional Depth Limits Of Product Internal Threads.
5.6.1. The data herein represents current practice and should be helpful in specifying depth limit steps on thread plug gages. Specifications for the location of depth limit steps on GO thread plug gages, which are otherwise made in accordance with details in this section, are as follows.
5.6.2. Object of Depth Limit Steps. The object of depth limit steps on GO plug thread gages is to determine the extent a product functionally conforms to the specified thread depth.

Therc are two types of specifications referring to depth of internal threads. One type specifies minimum depth only and therefore requires only one depth limit step on the gage. The other type specifies minimum and maximum values for depth of thread and requires two depth limit stcps on the gage.
5.6.3. Use of Gages with Depth Limit Steps. The step limit GO thread plug gage is applied to the product as far as it will go without the application of significant force which would tend to deform the product material. The position of the limit steps in relation to the face of the product is noted to determine conformance.
5.6.4. Location of Limit Steps. Limit steps shall be located with reference to the front end face of the gage as shown in figures 6.16 and 6.17 and at a point on the circumference that will approximately bisect the crest flat of the gage.

The first full crest of the GO thread plug gage with a depth limit step shall start at a location $0.5 p$ from the front end face of the gage as shown in figures 6.16 and 6.18.

The limit step face shall be straight for the depth of thread and shall be ground at 90 degrees to the axis of the gage.

Reversible style thread gages are gencrally made with only one set of limit steps from one end of the gage in order to eliminate confusion and error from runout of onc set of steps running into steps from the other end.

The design of the depth step is based on the length from the centerline of the crest on the first full thread ridge (which is untouched by removal of the thread convolution or chamfer at the end of the thread plug gage). The length from the end of the thread gage to the depth step is calculated by adding $0.5 p$ to the functional depth of the full depth thread form required in the product.

When measuring the step length over the end of the gage, the step length tolerance will apply only if the


Figure 6.16. Depth limit thread plug gage.
exact $0.5 p$ length is held from the first full thread ridge centerline to the end. This dimension may vary without affecting the function, so long as the variation from $0.5 p$ is taken into account, when measuring the step length over the end of the thread plug gage. Variation of the $0.5 p$ dimension should be in a minus direction only and should not be of such magnitude as to infringe on the engaging flank of the first full thread ridge.


Figure 6.17. Location of depth step on gage (in plane which bisects crest flat).


Figure 6.18. Start of perfect thread on gage.

### 5.7. DETERMINATION OF LIMITS OF SIZE OF GAGES

An example of limits of size and tolerances of gages required for an external and an internal thread is presented below. A diameter/pitch size was chosen from table 3.1. All calculations were made from the specifications and formulas in tables $6.6,6.7,6.8$, and 6.9, p. 6.11.

Example: 2-18 UNS-2A

## GAGES FOR PRODUCT EXTERNAL THREADS

GO Thread Ring Gage

|  | Max |
| :--- | :--- |
| Major Dia | Cleared |
| Pitch Dia | 1.9624 |
| Minor Dia | 1.9383 |
| Truncated Setting Plug for GO Thread | Ring Gage | Major Dia:

-Truncated Portion
1.9888
1.9990
1.9883

Tolerance
Min

| 1.9620 | 0.0004 |
| :--- | :--- |
| 1.9378 | 0.0005 |

1.9985
1.9622

Cleared
Minor Dia
LO Thread Ring Gage
Major Dia
Pitch Dia:
-Tolerance plus
-Tolerance minus
Minor Dia
Truncated Setting Plug for LO Thread Ring Gage
Major Dia:
-Truncated Portion
-Full Portion
Pitch Dia:
-Tolerance plus
--Tolerance minus
Minor Dia
1.9814
1.9990
1.9575
1.9573
Cleared

Basic-Crest Setting Plug for GO Thread Snap Gage

| Major Dia | 1.9990 |
| :--- | :--- |
| Pitch Dia | 1.9624 |

Minor Dia
Cleared
Basic-Crest Setting Plug for LO Thread Snap Gage


GO Thread Plug Gage

Major Dia
Max
2.0005
1.9643

Cleared
Minor Dia
HI Thread Plug Gage
Major Dia
Pitch Dia:
-Tolerance minus
-Tolerance plus
Minor Dia
Cleared

GO Plain Plug Gage for Minor Diameter Diameter 1.94016

NOT GO Plain Plug Gage for Minor Diameter Diameter
1.95300

Min
2.0000
1.9639
1.9942
1.9702
0.0004
1.9706
1.94000
0.00016
1.95284

Tolerance
0.0005
0.0004
0.0005
0.0004
0.00016

## 6. INDICATING THREAD GAGES

6.1. Many types of indicating thread gages have been designed to meet specific needs in gaging both external and internal threads. The following descriptions apply to gages for checking external threads. Comparable techniques and principles are utilized for checking internal threads but are not covered in detail herein.
6.2. There were many factors which encouraged the development of indicating thread gages such as:
(1) A need for a numerical value for size to facilitate adjustments of manufacturing tools or processes.
(2) Means for a faster method of gaging.
(3) Flexibility in application to accommodate the several tolerance classes both before and after coating.
(4) Ability to determine numerical values for deviations in the essential thread elements to
serve more effectively the needs of statistical quality control techniques.
6.3. Practically all indicating thread gages utilize mechanisms which facilitate application of the gage to the product thread or application of the product thread to the gage. Gages are set to a thread setting plug or pair of thread setting plugs of known size. Deviations are read from a scale when utilizing mechanical, electronic, or pneumatic amplification, or from an enlarged image when utilizing optical projection.
6.4. It is generally impracticable to determine precisely the pitch diameter of product threads as defined because of variations in form and/or lead. However, the result obtained with many types of gages in gaging product threads is a close approximation of either pitch diameter or functional diameter. Certain types of gaging elements consisting of two or more rolls, segments, probes, or wires, with configurations as described and illustrated are in general use.

### 6.5. Some Representative Gaging Elements in Current Use.

(a) Gaging elements which, in length, approximate the width of the applicable GO thread ring gage blank and which, in contour, engage the product thread flank $0.625 H$ (approximating the flank contact of the GO thread ring gage) check Functional Diameter (Defined in section 1).
(b) Gaging elements which, in length, approximate two pitches and in contour, engage the product thread flank $0.375 H$ (approximating the flank contact of the LO thread ring gage) check LO MinimumMaterial Limit (Defined in section 1). (Deviation in product thread flank angle and lead affects this determination. See Notes 2 and 3 in par. 5.5, p. 6.21).
(c)

(d)

(e)

(f)

(g)

(i)

(c) Gaging elements which engage not over one pitch in length and in contour engage the product thread flank $0.375 H$ (approximating the flank contact of the LO thread ring gage) check Groove Diameter to yield LO Minimum-Material Size. (Deviation in product thread flank angle affects this determination. See Note 2 in par. 5.5, p. 6.21.)
(d) Gaging elements which engage not over one pitch in length and have a curved contact simulating best wire size or contacts having a slight flat, check Thread Groove Diameter (Defined in section 1) closely approximating pitch diameter. ${ }^{3}$ (See 6.6 j , $\mathrm{k}, \mathrm{l}$, or m$)$.
(e) Cone and vee ${ }^{4}$ gaging elements which engage not over one pitch in length and in contour engage the flank $0.375 H$ (approximating the flank contact of the LO thread ring gage) check groove and ridge diameter to yield LO Minimum-Material Size. (Deviation in product thread flank angle affects this determination. See Note 2 in par. 5.5, p. 6.21.)
(f) Cone and vee gaging elements which engage not over one pitch in length and have curved contacts simulating best wire size or contacts having a slight flat, check groove and ridge diameter closely approximating pitch diameter. (See $6.6 \mathrm{j}, \mathrm{k}, \mathrm{l}$, or m).
(g) Single radial probe contacting not more than one pitch, with ball point contact (simulating best size wire) checks Groove Diameter closely approximating pitch diameter. (See $6.6 \mathrm{k}, \mathrm{j}, \mathrm{l}$, or m ).
(h) Same as (g) except with angular cone contact of the LO ring thread gage. Checks Groove Diameter to yield LO Minimum-Material Size. (Deviation in product thread flank angle affects this determination. See Note 2 in par. 5.5, p. 6.21).
(i) Wire gaging contacts (simulating best size wire) check Groove Diameter closely approximating pitch diameter.

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6.6. Typical cross sections of limited contact gaging elements are as follows:
(j) Gaging elements with curved contacts simulating best wire size, designed to contact approximately at the pitch line.
(k) Gaging elements with short straight flank contacts, designed to straddle contact approximately at the pitch line.
(l) Gaging elements with curved contacts designed to contact above the pitch line approximately midway on available flank (i.e., that flank which is engaged when using 6.7 (o) gaging elements.)
(m) Gaging elements with short straight flank contacts, designed to straddle contact above the pitch line approximately midway on a vailable flank.
6.7. Cross sections of full and LO flank angle gaging elements are as follows:
(n) Gaging elements with full length flank contact, (approximating the flank contact of the GO thread ring gage) designed to contact for full depth of thread engagement.
(o) Gaging elements with LO ( 0.375 H ) flank contacts, (approximating the flank contact of the LO thread ring gage) designed to contact for partial depth of thread engagement.
6.8. The several designs of gages and multiplicity of gaging elements embrace developments over many years. Each was conceived to meet a specific need, and to the degree which that need was valid, and the gage filled it, that design has been utilized.
Table 6.19. Gages for standard thread series, Unified screw threads

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| $\frac{5}{2}$ | $\begin{aligned} & 0 \\ & 4 \\ & \hline \end{aligned}$ | $\stackrel{y}{5}$ | $\begin{aligned} & 0 \\ & 3 \\ & \vdots \end{aligned}$ | $\stackrel{y}{z}$ | $\begin{aligned} & 0 \\ & \text { 台 } \end{aligned}$ | $\stackrel{\text { E }}{\substack{2 \\ \hline}}$ | $\begin{aligned} & 0 \\ & \vdots \\ & \vdots \\ & \hline \end{aligned}$ | 花 | $\begin{aligned} & \text { 差 } \\ & \text { Z } \\ & \text { 2 } \end{aligned}$ | $\begin{aligned} & 0 \\ & Z \\ & Z \end{aligned}$ | $\stackrel{y}{z}$ | $\begin{aligned} & \text { 畄 } \\ & \text { 号 } \end{aligned}$ | 0 台 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $$ |  |  | $\begin{aligned} & \underset{\sim}{9} \\ & \vdots \\ & \vdots \end{aligned}$ | $\begin{aligned} & \stackrel{9}{9} \\ & \stackrel{\rightharpoonup}{6} \end{aligned}$ | $\begin{aligned} & \text { 筞 } \\ & \stackrel{\rightharpoonup}{9} \end{aligned}$ | $\begin{aligned} & \stackrel{\circ}{0} \\ & \stackrel{\Phi}{9} \end{aligned}$ |  | $\begin{aligned} & \infty \\ & \text { It } \\ & \text { Hal } \end{aligned}$ | $\begin{aligned} & \ddot{0} \\ & \stackrel{y}{4} \\ & \hline \end{aligned}$ |  | $$ |  | 号 |

Table 6．19．Gages for standard thread series，Unified screw threads－Continued

|  |  |  |  |  | ה | $\begin{aligned} & \text { ¢ } \\ & \text { ث } \\ & \stackrel{\text { Hen }}{6} \end{aligned}$ | $\begin{gathered} \text { N } \\ \text { Ni } \\ \text { Noల } \end{gathered}$ | $\begin{aligned} & \infty \\ & \underset{1}{1} \\ & \stackrel{1}{4} \\ & \end{aligned}$ | $\begin{aligned} & \stackrel{(0}{0} \\ & \stackrel{1}{*} \\ & \text { N} \end{aligned}$ | $\begin{aligned} & 0 \\ & 1 \\ & \stackrel{1}{6} \\ & 6.0 \end{aligned}$ | $\begin{aligned} & \text { H } \\ & \stackrel{1}{0} \\ & \stackrel{N}{0} \end{aligned}$ | $$ | $\begin{aligned} & \infty \\ & \stackrel{1}{1} \\ & \stackrel{0}{0} \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { N్ } \\ & \text { N } \\ & \text { مల } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | 2 | 台 | $\begin{aligned} & \text { 号 } \\ & \hline \end{aligned}$ | $\stackrel{\text { z }}{b}$ | $\begin{aligned} & \text { 䛼 } \\ & \underset{S}{2} \end{aligned}$ | $\begin{aligned} & 0 \\ & 2 \\ & b \end{aligned}$ | $\underset{b}{4}$ | $\stackrel{y}{4}$ | 分 | $\begin{aligned} & \text { 罡 } \\ & \vdots \\ & \hline \end{aligned}$ |
|  |  | $\begin{aligned} & \mathscr{0} \\ & \text { \% } \\ & 0 \end{aligned}$ |  |  | $\stackrel{9}{\sim}$ | ヘึ ค |  | $\cdots$ | 网 | $\Leftrightarrow$ ¢ ${ }_{\sim}^{\infty}$ | 内 | $\underset{\sim}{\sim}$ | ヘึ ¢ึ | N |
|  |  | $\begin{aligned} & \text { EiO } \\ & \text { B } \end{aligned}$ |  |  | $\stackrel{\infty}{\sim}$ |  | 옹옹뮹N ลNNNN | Bon |  | 이기궁№m | ి్ల్లిల్ల్ల్ల్ల్ల | ి్రి్ల్లి |  | S. |
|  |  | 8 |  |  | $\cong$ |  |  | 육ㅋㄲ규걱 <br> 内人た | 商灾灾灾 |  |  |  |  |  |
|  | $\text { sәรея sп!̣ реәлч7 } \mathrm{X}$ | 岩 |  |  | $\stackrel{\sim}{\sim}$ |  |  | NG: |  |  |  |  ๗లల్లగలల |  ๗लলల |  |
|  |  |  |  |  | $\sim$ |  | Ti్రㄱ్య <br>  | がでった స్సా్సా |  |  |  | ํํํNNN․ にల్ల్లొల్ల | 苦 $-{ }^{\circ} \mathrm{F}$ がల゙ゃ | $\sigma_{\infty}^{\infty} \infty$ ๗ొల్లో |
|  |  |  |  |  | $\pm$ | Bidisiz | 잉ㅇㅇㅇㅇㅇㅇ ల్ల్లాగ్ల్లా． | N్ల్ల్రీద్ల్ల్ల. |  | BUNTOM H <br>  |  |  స్లో స్లో | NiNe |  |
|  |  | $\bigcirc$ |  |  | $\cong$ |  |  Nద | \%oo ooo |  |  <br>  |  |  |  |  |
|  |  |  |  | 象是范 | ค |  |  | ヘ్లిల్ల్ల్లి | స్లిల్ల్ల్లి | 오우웅 స్లんかんた |  స్ల్లసた | NNNDNN | 人たへ్లో |  <br> స్లnస్ల |
|  | $\begin{gathered} \text { Z plain ring gages for major } \\ \text { diameter } \end{gathered}$ | $\begin{aligned} & 0 \\ & 0 \\ & E \\ & Z \\ & Z \end{aligned}$ |  |  | 7 | ※ $\begin{aligned} & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & \\ & 1\end{aligned}$ |  | （1） 1111 | （ $1: 11$ |  | （ 1 |  | 1 1 | 1 1 <br>  1 <br> 1  |
|  |  |  |  |  | 9 |  | 옹్ㅓ얘융 ్లా్లాగ్లిగ్లి |  |  ్ల్లా్ల户్ద |  గ్ల్లాల్ల | $\mathrm{H}_{6}^{\infty}$ ద్లాల్లా్ల | 下్ల్లీ： గ్లో | N上20 స్లొ్ల్ల్ల | 웅ㅇㅇㅇ웅 ్ల్ల్ల్ల |
|  |  |  | $\bigcirc$ |  | $\infty$ |  |  | Natiog |  |  たたがたがた | 無会会宗 ద్లో |  た | 유우윽 た స్లn | 유ㄱㅜㅠㅇ뮨 సだNた |
|  |  | $0$ |  |  | $\infty$ |  | 品ANㅓNA | N上尺： NANA | $\begin{aligned} & \text { NNo } \\ & \text { No } \\ & \text { Now } \end{aligned}$ |  |  |  |  |  |
|  |  |  | $\begin{aligned} & \text { 志 } \\ & \text { 券 } \\ & \text { 畀 } \end{aligned}$ |  | N |  | 今NかNNN |  かか | $\begin{aligned} & \text { BNo } \\ & \substack{\infty \\ \infty \\ \infty \\ \infty \\ \infty \\ \infty \\ \hline} \end{aligned}$ |  |  |  |  |  |
|  |  |  |  |  | $\bigcirc$ | \&NRN | $\infty$ がロ日웅ㅇㅇ <br>  |  |  |  | N్ల్లీస్ల్ల్ల్ల్ల |  | 두ㅇㅜㅜ우웅 |  స్ల్లగ |
|  |  | 0 |  |  | $\sim$ | $\begin{aligned} & \text { Hemm } \\ & \text { NAN } \\ & \text { N. } \end{aligned}$ | ఇompario <br>  | か～がm NNたた | NNron |  |  |  | N్ల్ల్ల్ల్ల్ల్ |  |
|  |  |  |  |  | $\pm$ |  |  <br>  | $\mathfrak{\infty} \mathscr{\infty}$ |  | శ్ల్లిల్ల్ల్ల్ల్ల్ల్ల్ల్ల |  |  |  | 5 దొలొల్ |
|  |  | $\begin{aligned} & \mathscr{0} \\ & \stackrel{0}{0} \\ & \tilde{O} \end{aligned}$ |  |  | ๓ | 允 | 【 ష | जू | से | 【 ふ | से | 【 | स द्य | द य |
|  |  |  |  |  | N | $\stackrel{Z}{\square}$ | $\stackrel{y}{4}$ | 台 | $\begin{aligned} & \text { 啡 } \\ & \vdots \\ & \hline \end{aligned}$ | $\begin{aligned} & 0 \\ & Z \\ & \hline \end{aligned}$ | 台 | $\stackrel{y}{4}$ | 台 | $\begin{aligned} & \text { 哇 } \\ & E \\ & Z \\ & D \end{aligned}$ |
|  |  |  |  |  | H | ¢ ¢ － | $\begin{aligned} & \text { ત্} \\ & \stackrel{\rightharpoonup}{N} \\ & \text { N} \end{aligned}$ | $\begin{aligned} & \infty \\ & \text { N } \\ & \text { А్ల } \end{aligned}$ |  | ¢ | ¢ | \＃ | ¢ | $\begin{aligned} & \text { Non } \\ & \text { N } \\ & \text { No } \end{aligned}$ |














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| 0 7 $\square$ | 2 | $\stackrel{y}{4}$ |  | 名 | 0 <br> 7 | 号 | 号 <br> 号 |  | ＇${ }^{\text {S }}$ | 0 7 $\square$ | 名 | E 又 号 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $$ | $\begin{gathered} 9 \\ \substack{4 \\ \underset{y}{4}} \end{gathered}$ |  | $\begin{aligned} & \stackrel{\infty}{1} \\ & \stackrel{1}{0} \\ & \stackrel{\rightharpoonup}{\circ} \\ & \end{aligned}$ | ¢ | $\begin{aligned} & \stackrel{9}{1} \\ & \stackrel{1}{8} \end{aligned}$ | $\begin{aligned} & 0 \\ & \underset{\sim}{1} \\ & \stackrel{1}{6} \end{aligned}$ | $\begin{aligned} & 8 \\ & 1 \\ & \frac{1}{5} \\ & \end{aligned}$ | $$ | $\begin{aligned} & \text { N } \\ & \text { O} \\ & \text { O} \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { a } \\ & \text { 10 } \\ & \text { is } \end{aligned}$ | $\begin{aligned} & 0 \\ & 1 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $$ |

Table 6.19. Gages for standard thread series, Unified screw threads-Continued











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| $\begin{aligned} & \text { 体 } \\ & \text { 名 } \\ & \text { S } \end{aligned}$ | $\underset{\square}{Z}$ | $\underset{b}{Z}$ | 㤐 | $\stackrel{7}{4}$ | 怠 |  | 乙 | 号 | 0 7 $\square$ | 々 | 信 | 宜 | 乙 | 各 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { N } \\ & \text { d } \\ & 0 \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & \infty \\ & 0 \\ & 1 \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \text { in } \\ & \text { No } \\ & \hline \end{aligned}$ | $\begin{aligned} & 0 \\ & 1 \\ & 16 \\ & 00 \\ & 00 \end{aligned}$ | 0 4 18 88 8 | 8 1 10 18 08 | 31 1 10 0 0 0 | $\infty$ 1 10 10 0 | 18 0 10 0 80 | $\begin{aligned} & 0 \\ & 1 \\ & 1 \\ & 10 \end{aligned}$ | $\begin{aligned} & 0 \\ & 1 \\ & 8 \\ & 5 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0 \\ & 1 \\ & 8 \\ & 9 \end{aligned}$ | $\begin{aligned} & 8 \\ & 8 \\ & 1 \\ & 15 \\ & \hline \end{aligned}$ | － | ¢ |


| Nominal size and threads per inch | Series designation | Class | Gages for external threads |  |  |  |  |  |  |  | Gages for internal threads |  |  |  |  |  |  | Class | $\begin{aligned} & \text { Series } \\ & \text { designa- } \\ & \text { tion } \end{aligned}$ | Nominal <br> size and <br> threads <br> per inch |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | X thread ring gages |  |  |  |  | Z plain ring gages for major diameter |  |  | X thread plug gages |  |  |  |  | Z plain plug gages for minor diameter |  |  |  |  |
|  |  |  | GO |  | LO |  |  | GO | NOT | GO |  |  |  | HI |  | GO | $\begin{aligned} & \text { NOT } \\ & \text { GO } \end{aligned}$ |  |  |  |
|  |  |  | Pitch diamcter | Minor diameter | Pitch diameter |  | Minor diam. eter |  | Semifinished | $\left\lvert\, \begin{gathered} \text { Un- } \\ \text { finished } \\ \text { hot- } \\ \text { rolled } \\ \text { material } \end{gathered}\right.$ | Major diameter | Pitch diameter | Major diameter | Pitch diameter |  |  |  |  |  |  |
|  |  |  |  |  | Plus tolerance gage | Minus tolerance gage |  |  |  |  |  |  |  | Minus tolerance gage | Plus tolerance gage |  |  |  |  |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 |
| . $8125-12$ | UN | 2 A 3 A | in 0.7567 .7564 .7584 .7581 | $\begin{gathered} i n \\ 0.7206 \\ .7200 \\ .7223 \\ .7217 \end{gathered}$ | $\begin{gathered} i n \\ 0.7512 \\ .7515 \\ .7543 \\ .7546 \end{gathered}$ | $\begin{gathered} i n \\ 0.7512 \\ .7509 \\ .7543 \\ .7540 \end{gathered}$ | $\begin{gathered} i n \\ 0.7332 \\ .7338 \\ .7363 \\ .7369 \end{gathered}$ | in 0.8108 .8107 .8125 .8124 | $i n$ 0.7994 .7995 .8011 .8012 | in | $\begin{gathered} i n \\ 0.8125 \\ .8131 \\ .8125 \\ .8131 \end{gathered}$ | $i n$ 0.7584 .7587 .7584 .7587 | $\begin{gathered} i n \\ 0.8017 \\ .8011 \\ .7999 \\ .7993 \end{gathered}$ | $\begin{gathered} i n \\ 0.7656 \\ .7653 \\ .7638 \\ .7635 \end{gathered}$ | $i n$ 0.7656 .7659 .7638 .7641 | $\begin{gathered} i n \\ 0.7220 \\ .7221 \\ .7220 \\ .7221 \end{gathered}$ | $\begin{gathered} i n \\ 0.7400 \\ .7399 \\ .7329 \\ .7328 \end{gathered}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | UN | . $8125-12$ |
| .8125-16 | UN | 2 A 3 A | .7704 .7701 .7719 .7716 | .7433 .7427 .7448 .7442 | .7655 .7658 .7683 .7686 | .7655 .7652 .7683 .7680 | .7520 .7526 .7548 .7554 | .8110 .8109 .8125 .8124 | .8016 .8017 .8031 .8032 | ------------------------- | .8125 .8131 .8125 .8131 | .7719 .7722 .7719 .7722 | .8053 .8047 .8037 .8031 | .7782 .7779 .7766 .7763 | .7782 .7785 .7766 .7769 | .7450 .7451 .7450 .7451 | .7590 .7589 .7533 .7532 | 2B 3 B | UN | .8125-16 |
| . $8125-20$ | UNEF | 2 A 3 A | .7787 .7784 .7800 .7797 | .7570 .7565 .7583 .7578 | .7743 .7746 .7767 .7770 | .7743 .7740 .7767 .7764 | .7635 .7640 .7659 .7664 | .8112 .8111 .8125 .8124 | .8031 .8032 .8044 .8045 | --------------- | .8125 .8130 .8125 .8130 | .7800 .7803 .7800 .7803 | .8074 .8069 .8060 .8055 | .7857 .7854 .7843 .7840 | .7857 .7860 .7843 .7846 | .7580 .7581 .7580 .7581 | .7700 .7699 .7662 .7661 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | UNEF | . $8125-20$ |
| . $8125-28$ | UN | 2 A 3 A | .7881 .7878 .7893 .7890 | .7726 .7771 .738 .7733 | .7843 .7846 .7864 .7867 | .7843 .7840 .7864 .7861 | .7766 .7771 .7787 .7792 | .8113 .8112 .8125 .8124 | .8048 .8049 .8060 .8061 | -------------------------- | .8125 .8130 .8125 .8130 | .7893 .7896 .7893 .7896 | .8098 .8093 .8085 .8080 | .7943 .7940 .7930 .7927 | .7943 .7946 .7930 .7933 | .7740 .7741 .7740 .7741 | .7820 .7819 .7801 .7800 | 2 B 3 B | UN | . $8125-28$ |
| .8125-32 | UN | 2 A 3 A | .7911 .7908 .7922 .7919 | .7776 .7771 .7878 .7782 | .7875 .7878 .7895 .7898 | .7875 .7872 .7895 .7892 | .7807 .7812 .7827 .7832 | .8114 .8113 .8125 .8124 | .8054 .8055 .8065 .8066 | ------------------------ | .8125 .8130 .8125 .8130 | .7922 .7925 .7922 .7925 | .8104 .8099 .8093 .8088 | .7969 .7966 .7958 .7955 | .7969 .7979 .7972 .7961 | .7790 .7791 .7790 .7791 | .7860 .7859 .7844 .7843 | 2 B 3 B | UN | . $8125-32$ |
| . 875-9 | UNC | 1 A 2A 3 A | .8009 .8006 .8009 .8006 .8028 .8025 | .7528 .7521 .7528 .7521 .7547 .7540 | .7914 .7917 .7946 .7949 .7981 .7984 | .7914 .7911 .7946 .7943 .7981 .7978 | .7673 .7680 .7705 .7712 .7740 .7747 | .87310 .87299 .8710 .87298 .87500 .87488 | .85230 .85242 .85920 .85932 .86110 .86122 | 0.85230 .85242 | .8750 .8757 .8750 .8757 .8750 .8757 | .8028 .8031 .8028 .8031 .8028 .8031 | .8632 .8625 .8591 .8584 .8570 .8563 | $\begin{aligned} & .8151 \\ & .8148 \\ & .8110 \\ & .8107 \\ & .8089 \\ & .8086 \end{aligned}$ | .8151 .8154 .8110 .8113 .8089 .8092 | .75500 .75512 .75500 .75512 .75500 .75512 | .77800 .7788 .77800 .77788 .76810 .76798 | 1 B 2B 3B | UNC | . $875-9$ |
| . 875-12 | UN | 2 A 3 A | .8192 .8189 .8209 .8206 | .7831 .7825 .7848 .7842 | .8137 .8140 .8168 .8171 | .8137 .8134 .8168 .8165 | .7957 .7963 .7988 .7994 | .87330 .87318 .87500 .87488 | .86190 .86202 .86360 .86372 | -------------- | .8750 .8756 .8750 .8756 | .8209 .8212 .8209 .8212 | .8642 .8636 .8624 .8618 | .8281 .8278 .8263 .8260 | .8281 .8284 .8263 .8266 | .78500 .78512 .78500 .78512 | .80300 .80288 .79550 .79508 | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | UN | . $875-12$ |
| .875-14 | UNF | 1 A 2A 3A | .8270 .8267 .8270 .8267 .8286 .8283 | .7961 .7955 .7961 .7955 .7977 .7971 | .8189 .8192 .8216 .8219 .8245 .8248 | .8189 .8186 .8216 .8213 .8245 .8242 | .8034 .8040 .8061 .8067 .8090 .8096 | .87340 .87328 .87340 .87328 .8700 .87488 | .85790 .85802 .86310 .86322 .86470 .86482 | --------------------------- | .8750 .8756 .8750 .8756 .8750 .8756 | .8286 .8289 .8286 .8289 .8286 .8289 | $\begin{aligned} & .8701 \\ & .8695 \\ & .8665 \\ & .8659 \\ & .8648 \\ & .8642 \end{aligned}$ | $\begin{array}{r} .8392 \\ .8389 \\ .8356 \\ .8353 \\ .8339 \\ .8336 \end{array}$ | .8392 .8395 .8356 .8359 .8339 .8342 | .79800 .79812 .79800 .79812 .79800 .79812 | .81400 .81888 .81400 .81388 .80680 .80668 | 1 B 2B 3B | UNF | . $875-14$ |
| .875-16 | - UN | 2 A 3 A | .8329 .8326 .8344 .8341 | .8058 .8052 .8073 .8067 | .8280 .8283 .8308 .8311 | .8280 .8277 .8308 .8305 | .8145 .8151 .8173 .8179 | .87350 .87338 .87500 .87489 | .86410 8642 .86560 .86572 |  | $\begin{aligned} & .8750 \\ & .8756 \\ & .8750 \\ & .8756 \end{aligned}$ | $\begin{aligned} & .8344 \\ & .8347 \\ & .8344 \\ & .8347 \end{aligned}$ | $\begin{aligned} & .8678 \\ & .8672 \\ & .8662 \\ & .8656 \end{aligned}$ | $\begin{array}{r} 8407 \\ .8404 \\ .8391 \\ .8388 \end{array}$ | .8407 .8410 .8391 .8394 | .80700 .80712 .80700 .80712 | $\begin{aligned} & .82100 \\ & .82088 \\ & .81580 \\ & .81568 \end{aligned}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | UN | .875-16 |
| .875-20 | UNEF | 2 A 3 A | .8412 .8409 .8425 .8422 | .8195 .8190 .8208 .8203 | .8368 .8371 .8392 .8395 | $\begin{aligned} & .8368 \\ & .8365 \\ & .8392 \\ & .8389 \end{aligned}$ | .8260 .8265 .8284 .8289 | $\begin{aligned} & .87370 \\ & .87358 \\ & .87500 \\ & .87488 \end{aligned}$ | .86560 .86572 .86690 .86702 |  | $\begin{aligned} & .8750 \\ & .8755 \\ & .8750 \\ & .8755 \end{aligned}$ | $\begin{aligned} & .8425 \\ & .8428 \\ & .8425 \\ & .8428 \end{aligned}$ | $\begin{aligned} & .8699 \\ & .8694 \\ & .8885 \\ & .8680 \end{aligned}$ | $\begin{aligned} & .8482 \\ & .8479 \\ & .8848 \\ & .8465 \end{aligned}$ | .8482 .8485 .8468 .8471 |  | $\begin{array}{r} .83200 \\ .83188 \\ .82870 \\ .82858 \end{array}$ | $\begin{aligned} & 2 \mathrm{~B} \\ & 3 \mathrm{~B} \end{aligned}$ | UNEF | . $875-2$ ) |


| $\begin{aligned} & \infty \\ & \underset{\sim}{1} \\ & \stackrel{1}{\infty} \\ & \hline \end{aligned}$ | $\begin{aligned} & \mathscr{e}_{0}^{2} \\ & \stackrel{1}{6} \\ & \infty \\ & \hline \end{aligned}$ | $\begin{aligned} & \frac{9}{1} \\ & 0 \\ & \hline \\ & \hline \end{aligned}$ | $\begin{aligned} & \stackrel{\varrho}{1} \\ & \stackrel{1}{6} \\ & \stackrel{5}{\circ} \end{aligned}$ |  | $\begin{aligned} & \infty \\ & 0 \\ & 1 \\ & \stackrel{1}{6} \\ & \stackrel{5}{\circ} . \end{aligned}$ |  | $\begin{aligned} & \infty \\ & 1 \\ & 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \frac{1}{8} \\ & -1 \end{aligned}$ | $\begin{aligned} & \text { o } \\ & \frac{1}{8} \\ & - \end{aligned}$ | $\begin{aligned} & \stackrel{1}{1} \\ & \stackrel{8}{8} \\ & - \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{1}{8} \\ & \stackrel{1}{8} \\ & - \end{aligned}$ | $\begin{aligned} & \text { O్ } \\ & \text { O} \\ & \hline 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{1}{6} \\ & \text { io } \\ & - \\ & -1 \end{aligned}$ |  |
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| $\begin{aligned} & 7 \\ & \hline \end{aligned}$ | 参 | 莈 | 高 |  | 台 | 台 | 0 7 3 | $\begin{aligned} & \text { 号 } \\ & \underset{D}{5} \end{aligned}$ | 台 |  | 言 | 号 | 高 | 育 |








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| $\underset{\square}{Z}$ | $\underset{b}{\text { Z }}$ | $\begin{aligned} & 7 \\ & \hline \end{aligned}$ | $\stackrel{2}{\square}$ |  | Z | $\begin{aligned} & Z \\ & \hline \end{aligned}$ | $\begin{aligned} & 0 \\ & Z \\ & b \end{aligned}$ | $\underset{\substack{\text { 号 } \\ \hline \\ \hline}}{ }$ | $\begin{aligned} & 7 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { 至 } \\ & \text { 又 } \\ & \text { 号 } \end{aligned}$ | $\underset{\Delta}{Z}$ | 台 | Z | 号 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \infty \\ & \underset{1}{1} \\ & \underset{\infty}{\infty} \\ & \hline \end{aligned}$ | $\begin{aligned} & 1 \\ & i \\ & 10 \\ & 10 \\ & \hline \infty \end{aligned}$ | $\begin{aligned} & \underset{7}{9} \\ & \text { N } \\ & \text { 8 } \end{aligned}$ | $\begin{aligned} & 0 \\ & 3 \\ & 10 \\ & 6 \\ & 6 \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \stackrel{1}{6} \\ & \stackrel{1}{\infty} \\ & \hline \end{aligned}$ | $\begin{aligned} & \infty \\ & \underset{N}{1} \\ & \stackrel{1}{6} \\ & \underset{\infty}{6} \end{aligned}$ | $\begin{aligned} & \mathbb{1} \\ & 1 \\ & 1 \\ & \text { N } \\ & \hline 8 \end{aligned}$ | $\begin{aligned} & \infty \\ & 8 \\ & 8 \\ & -8 \\ & -1 \end{aligned}$ | $\begin{aligned} & \text { N } \\ & \frac{1}{8} \\ & 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & 6 \\ & 1 \\ & 8 \\ & 8 \\ & -1 \end{aligned}$ | $\begin{aligned} & 8 \\ & \frac{1}{8} \\ & \frac{1}{8} \end{aligned}$ | $\begin{aligned} & \infty \\ & 1 \\ & 1 \\ & 8 \\ & 8 \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { N} \\ & \underset{8}{8} \\ & -1 \end{aligned}$ | $\begin{aligned} & \infty \\ & 1 \\ & 1 \\ & 0 \\ & 8 \\ & -1 \end{aligned}$ |  |

Table 6.19. Gages for standard thread series, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Class | Gages for external threads |  |  |  |  |  |  |  | Gages for internal threads |  |  |  |  |  |  | Class | $\begin{aligned} & \text { Series } \\ & \text { designa- } \\ & \text { tion } \end{aligned}$ | Nominal size and threads per inch |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | X thread ring gages |  |  |  |  | Z plain ring gages for major diameter |  |  | X thread plug gages |  |  |  |  | Z plain plug gages for minor diameter |  |  |  |  |
|  |  |  | GO |  | LO |  |  | GO | NOT G\% |  | GO |  | HI |  |  | GO |  |  |  |  |
|  |  |  | Pitch diameter | Minor diameter | Piteh diameter |  | Minor dianeter |  | Semifinished | Un-finishedhot-rolledmaterial | Major diameter | Piteh diameter | Major diameter | Piteh diameter |  |  | NOT |  |  |  |
|  |  |  |  |  | Plus <br> toler- <br> anee <br> gage | Minus tolerance gage |  |  |  |  |  |  |  | Minus tolerance gage | Plus tolerance gage |  |  |  |  |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 |
| 1. 6625-16 | UN | 2 A3 A | in | in | in | in | in | -in | in | in | in | in | in | in | in | in | in |  |  |  |
|  |  |  | 1. 0204 | . 9933 | 1. 0154 | 1. 0154 | 1. 0019 | 1.06100 | 1. 05160 |  | 1.0625 | 1. 0219 | 1.0555 | 1.0284 | 1. 0284 | . 99500 | 1.00900 | 2B |  |  |
|  |  |  | 1.0201 | . 9927 | 1.0157 | 1. 0151 | 1. 0025 | 1.06088 | 1.05172 |  | 1.0631 | 1.0222 | 1.0549 | 1.0281 | 1.0287 | . 99512 | 1. 00888 |  | UN | 1.0625-16 |
|  |  |  | 1. 0219 | . 9948 | 1. 0182 | 1. 0182 | 1. 0047 | 1.06250 | 1.05310 |  | 1. 0625 | 1. 0219 | 1. 0539 | 1.0268 | 1. 0268 | . 99500 | 1. 00330 | 3B |  |  |
|  |  |  | 1. 0216 | . 9942 | 1. 0185 | 1. 0179 | 1. 0053 | 1.06238 | 1.05322 |  | 1. 0631 | 1. 0222 | 1. 0533 | 1. 0265 | 1. 0271 | . 99512 | 1. 00318 |  |  |  |
| 1. $0625-18$ | UNEF | 2A | 1. 0250 | 1. 0009 | 1. 0203 | 1. 0203 | 1. 0083 | 1. 06110 | 1.05240 |  | 1.0625 | 1. 0264 | 1.0567 | 1. 0326 | 1.0326 | 1. 00200 | 1. 01500 | 2B |  |  |
|  |  | 3A | 1. 0247 | 1. 0004 | 1. 0206 | 1. 0200 | 1. 0088 | 1. 06098 | 1. 05252 |  | 1. 0630 | 1. 0267 | 1. 0562 | 1. 0323 | 1. 0329 | 1. 00212 | 1.01488 |  | UNEF | 1. $0625-18$ |
|  |  |  | 1. 0264 | 1. 0023 | 1. 0228 | 1. 0228 | 1. 0108 | 1. 06250 | 1.05380 |  | 1.0625 | 1. 0264 | 1.0551 | 1.0310 | 1. 0310 | 1.00200 | 1.01050 | 3B |  |  |
|  |  |  | 1. 0261 | 1.0018 | 1.0231 | 1. 0225 | 1. 0113 | 1.06238 | 1.05392 |  | 1.0630 | 1. 0267 | 1. 0546 | 1.0307 | 1. 0313 | 1. 00212 | 1. 01038 |  |  |  |
| 1. $0625-20$ | UN | 2 A3 A | 1. 0286 | 1. 0069 | 1. 0241 | 1. 0241 | 1. 0133 | 1. 06110 | 1. 05300 |  | 1. 0625 | 1. 0300 | 1.0576 | 1. 0359 | 1. 0359 | 1. 00800 | 1.02000 | 2B |  |  |
|  |  |  | 1.0283 | 1.0064 | 1. 0244 | 1. 0238 | 1. 0138 | 1.06098 | 1. 05312 |  | 1. 06330 | 1. 0303 | 1. 0571 | 1. 0356 | 1. 0362 | 1.00812 | 1. 01988 |  | UN | 1.0625-20 |
|  |  |  | 1.0297 | 1.0078 | 1.0269 | 1.0263 | 1.0163 | 1.06238 | 1.05452 |  | 1.0625 1.0630 | 1.0300 1.0303 | 1.0556 | 1.0341 | 1.0347 | 1.00812 | $\begin{aligned} & 1.01620 \\ & 1.01608 \end{aligned}$ | 3 B |  |  |
| 1. $0625-28$ | UN | 2 A | 1. 0381 | 1. 0226 | 1. 0341 | 1. 0341 | 1. 0264 | 1. 06130 | 1. 05480 |  | 1. 0625 | 1.0393 | 1. 0600 | 1. 0445 | 1. 0445 | 1. 02400 | 1. 03200 | 2B |  |  |
|  |  | 3 A | 1. 0378 | 1. 0221 | 1. 0344 | 1. 0338 | 1. 0269 | 1.06118 | 1.05492 |  | 1.0630 | 1. 0396 | 1.0595 | 1. 0442 | 1.0448 | 1.02412 | 1. 03188 |  | UN | 1.0625-28 |
|  |  |  | 1. 0393 | 1. 0238 | 1.0363 | 1. 0363 | 1. 0286 | 1.06250 | 1. 05600 |  | 1.0625 | 1.0393 | 1.0587 | 1.0432 | 1. 0432 | 1.02400 | 1.03010 | 3B |  |  |
|  |  |  | 1. 0390 | 1. 0233 | 1.0366 | 1. 0360 | 1. 0291 | 1.06238 | 1. 05612 |  | 1.0630 | 1.0396 | 1. 0582 | 1.0429 | 1.0435 | 1.02412 | 1. 02998 |  |  |  |
| 1. 125-7 | UNC | 1A | 1. 0300 | . 9681 | 1. 0191 | 1. 0191 | . 9882 | 1.12280 | 1. 09820 |  | 1. 1250 | 1.0322 | 1. 1082 | 1. 0463 | 1. 0463 | . 97000 | . 99800 | 1B |  |  |
|  |  | 2 A | 1. 0296 | . 9684 | 1.0195 | 1. 0187 | .9889 .9919 | 1.12268 1.12280 | 1. 09832 1.10640 | 1. 09820 | 1.1257 | 1.0326 | 1.1075 | 1.0459 1.0416 | 1.0467 1.0416 | .97012 .97000 | .99788 .99800 | 2B | UNC | 1.125~7 |
|  |  |  | 1. 0296 | . 9674 | 1. 0232 | 1. 0224 | . 9926 | 1.12268 | 1. 10652 | 1.09832 | 1. 1257 | 1. 0326 | 1.1028 | 1. 0412 | 1. 0420 | . 97012 | . 99788 |  |  |  |
|  |  | 3A | 1. 0322 | . 9703 | 1. 0268 | 1. 0268 | . 9959 | 1. 12500 | 1. 10860 |  | 1.1250 | 1. 0322 | 1.1012 | 1. 0393 | 1. 0393 | . 97000 | . 98750 | 3B |  |  |
|  |  |  | 1. 0318 | . 9696 | 1. 0272 | 1.0264 | . 9966 | 1.12488 | 1. 10872 |  | 1.1257 | 1. 0326 | 1.1005 | 1.0389 | 1. 0397 | . 97012 | . 98738 |  |  |  |
| 1.125-8 | UN | 2A | 1. 0417 | . 9876 | 1. 0348 | 1. 0348 | 1. 0077 | 1. 12290 | 1. 10790 | 1. 10040 | 1.1250 | 1. 0438 | 1. 1069 | 1.0528 | 1.0528 | . 99000 | 1. 01500 | 2B |  |  |
|  |  | 3A | 1. 0413 | . 98869 | 1.0352 1.0386 | 1. 0344 1. 0386 | 1. 1.0084 | 1.12278 | 1.10802 1.11000 | 1. 10052 | 1.1257 1.1250 | 1.0442 | 1. 1062 | 1.0524 1.0505 | 1.0532 1.0505 1.050 | .99012 .99000 | 1.01488 1.00470 | 3B | UN | 1.125-8 |
|  |  |  | I. 0434 | . 9890 | 1. 0390 | 1. 0382 | 1. 0122 | 1.12488 | 1.11012 |  | 1.1257 | 1. 0442 | 1. 1039 | 1.0501 | 1.0509 | . 99012 | 1. 00458 |  |  |  |
| 1.125-12 | UNF | 1A | 1. 0691 | 1. 0330 | 1. 0601 | 1. 0601 | 1. 0421 | 1. 12320 | 1. 10600 |  | 1.1250 | 1. 0709 | 1. 1187 | 1. 0826 | 1. 0826 | 1. 03500 | 1. 05300 | 1B |  |  |
|  |  |  | 1. 0688 | 1.0324 | 1. 0604 | 1. 0598 | 1. 0427 | 1.12308 | 1. 10612 |  | 1.1256 | 1.0712 | 1. 1181 | 1. 0823 | 1. 0829 | 1.03512 | 1.05288 |  |  |  |
|  |  | 2 A | 1. 0691 | 1.0330 | 1. 0631 | 1. 0631 | 1.0451 | 1. 12320 | 1.11180 |  | 1.1250 | 1.0709 | 1.1148 | 1.0787 | 1.0787 | 1.03500 | 1. 05300 | 2B | UNF | 1. $125-12$ |
|  |  |  | 1. 0688 | 1. 0324 | 1. 0634 | 1. 0628 | 1. 0457 | 1. 12308 | 1.11192 |  | 1.1256 | 1. 0712 | 1. 1142 | 1. 0784 | 1. 0790 | 1.03512 | 1. 05288 |  |  |  |
|  |  | 3A | 1.0709 1.0706 | 1.0348 1.0342 | 1. 06664 | 1. 0664 1. 0661 | 1. 1.0484 | 1.12500 1.12488 | 1.11360 1.11372 |  | 1. 1250 1.1256 | 1.0709 1.0712 | 1. 11129 | 1. 1.0768 1.0765 | 1. 0768 1. 0771 | 1.03500 1.03512 | 1.04480 1.04468 | 3B |  |  |
|  |  |  | 1.0706 |  |  |  |  |  | 1.11372 |  |  | 1.0712 | 1.1123 |  | 1.071 | 1.03512 | 1.04468 |  |  |  |
| 1. 125-16 | UN | 2A | 1. 0829 | 1. 0558 | 1. 0779 | 1. 0779 | 1. 0644 | 1. 12350 | 1. 11410 |  | 1.1250 | 1. 0844 | 1.1180 | 1. 0909 | 1. 0909 | 1.05700 | 1. 07100 | 2B |  |  |
|  |  |  | 1. 0826 | 1.0552 | 1. 0782 | 1. 0776 | 1. 0650 | 1.12338 | 1.11422 |  | 1.1256 | 1. 0847 | 1. 1174 | 1.0906 | 1. 0912 | 1. 05712 | 1. 07088 |  | UN | 1. 125-16 |
|  |  | 3A | 1. 0844 | 1. 0573 | 1. 0807 | 1.0807 | 1. 0672 | 1. 12500 | 1.11560 |  | 1. 1250 | 1. 0844 | 1. 1164 | 1.0893 | 1. 0893 | 1. 05700 | 1.06580 | 3B |  |  |
|  |  |  | 1.0841 | 1. 0567 | 1. 0810 | 1. 0804 | 1.0678 | 1. 12488 | 1.11572 |  | 1. 1256 | 1.0847 | 1.1158 | 1.0890 | 1.0896 | 1.05712 | 1.06568 |  |  |  |
| 1. 125-18 | UNEF | 2 A | 1.0875 | 1. 0634 | 1. 0828 | 1. 0828 | 1. 0708 | 1. 12360 | 1. 11490 |  | 1.1250 | 1. 0889 | 1. 1192 | 1.0951 | 1. 0951 | 1. 06500 | 1. 07800 | 2B |  |  |
|  |  |  | 1. 0872 1.0889 | 1. 06629 | 1. 0831 | 1. 0825 | 1. 0713 | 1.12348 | 1.11502 |  | 1.1255 | 1. 0892 1. 0889 | 1.1187 | 1.0948 | 1. 0954 | 1. 06512 | 1.07788 1.07300 1.0 |  | UNEF | 1. 125-18 |
|  |  | 3A | 1.0889 1.0886 | 1.0648 1.0643 | 1. 0853 1.0856 | 1. 0853 1.0850 | 1.0733 1.0738 | 1. 12500 1.12488 | 1.11630 1.11642 |  | 1.1250 1.1255 | 1. 0889 | 1. 1176 | 1. 1.0935 | $\begin{aligned} & 1.0935 \\ & 1.0938 \end{aligned}$ | $\begin{aligned} & 1.06500 \\ & 1.06512 \end{aligned}$ | 1.07300 1.07288 | 3B |  |  |
|  |  |  | 1.0886 | 1.0643 | 1.0850 | 1.0850 | 1.0738 |  |  |  | 1.1255 | 1.0892 | 1.117 | 1.0932 | 1.098 | 1.06512 | 1.07288 |  |  |  |
| 1.125-20 | UN | 2A | 1. 0911 | 1. 0694 | 1. 0866 | 1. 0866 | 1. 0758 | 1.12360 1.12348 | 1.11550 1.11562 |  | 1. 1250 | 1. 0925 | 1. 1201 | 1. 0984 | 1. 0984 | 1. 07100 | 1. 08200 | 2B |  |  |
|  |  | 3A | 1. 09008 1.0925 | 1.0689 1.0708 | 1. 0889 | 1. 08683 1.0891 | 1. 0763 | 1.12348 1.12500 | 1.11562 1.11690 |  | 1.1255 | 1. 0928 | 1.1196 | 1. 0981 1. 0969 | 1.0987 | 1.07112 1.07100 | 1.08188 1.07870 | 3B | UN | 1. $125-20$ |
|  |  |  | 1. 0922 | 1.0703 | 1.0894 | 1. 0888 | 1. 0788 | 1.12488 | 1.11702 |  | 1. 1255 | 1. 0928 | 1.1181 | 1. 0966 | 1.0972 | 1. 07112 | 1. 07858 |  |  |  |


| UN | $1.125-28$ |
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| UN | $1.1875-16$ |
| UNEF | $1.1875-18$ |
| UN | $1.1875-20$ |
| UN | $1.1875-28$ |
| UNC | $1.250-7$ |
| UN | $1.3125-8$ |
| UN | $1.250-8$ |
| UN | $1.250-28$ |
| UNF | $1.250-12$ |
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| $1.250-16$ |
| $1.250-18$ |
| $1.250-20$ |
| $1.3125-88$ |


| Nominal threads per inch | Seriesdesignation | Class | Gages for external threads |  |  |  |  |  |  |  | Gages for internal threads |  |  |  |  |  |  | Class | Seriesdesignation | Nominal threads per inch |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | X thread ring gages |  |  |  |  | Z plaln ring gages for major diameter |  |  | X thread plug gages |  |  |  |  | Z plain plug gages for minor diameter |  |  |  |  |
|  |  |  | GO |  | LO |  |  | GO | NOT GO |  | GO |  | HI |  |  | GO | $\underset{\text { NOT }}{\text { NOT }}$ |  |  |  |
|  |  |  | $\begin{aligned} & \text { Pitch } \\ & \text { diam- } \\ & \text { eter } \end{aligned}$ | $\begin{aligned} & \text { Minor } \\ & \text { diam- } \\ & \text { eter } \end{aligned}$ | Pitch diameter |  | Minor eter |  | Semi- |  | $\begin{aligned} & \text { Major } \\ & \text { diam- } \\ & \text { eter } \end{aligned}$ | $\begin{aligned} & \text { Pitch } \\ & \text { diam- } \\ & \text { eter } \end{aligned}$ | $\begin{aligned} & \text { Major } \\ & \text { diam- } \\ & \text { eter } \end{aligned}$ | Pitch diameter |  |  |  |  |  |  |
|  |  |  |  |  | $\begin{aligned} & \text { Plus } \\ & \text { toler- } \\ & \text { ance } \\ & \text { gage } \end{aligned}$ | Minus tolerance gage |  |  |  |  |  |  |  | Minus tolerance gage | Plus tolerance gage |  |  |  |  |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 |
| 1.3125-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | in | in | in | in | in | in | in | in | in | ${ }^{\text {in }}$ | in | in | in | in | in |  |  |  |
|  |  |  | 1.2567 | 1.2206 | 1.2509 | ${ }_{1}^{1.2509}$ | 1.2329 | 1.31080 | 1. 299940 |  | ${ }_{1}^{1.3125}$ | 1.2584 | 1.3020 1.3014 | 1. 2659 | 1. 2659 | 1.22200 | 1.24000 | 2 B |  | 13125-12 |
|  |  |  | 1.2584 | 1.2223 | 1.2541 | 1.2541 | 1. 2361 | 1. 31250 | 1. 30110 |  | 1.3125 | 1.2584 | 1. 3001 | 1. 2640 | 1.2640 | 1. 22200 | 1. 23230 | 3B | N | 1.3125-12 |
|  |  |  | 1. 2581 | 1. 2217 | 1. 2544 | 1.2538 | 1. 2367 | 1.31238 | 1.30122 |  | 1.3131 | 1. 2587 | 1. 2995 | 1. 2637 | 1. 2643 | 1.22212 | 1. 23218 |  |  |  |
| 1.3125-16 | UN | 2 A3 A | 1. 2704 | 1. 2433 | 1. 2653 | 1. 2653 | 1.2518 | 1.31100 | 1.30160 |  | 1. 3125 | 1. 2719 | 1. 3056 | 1. 2785 | 1. 2785 | 1. 24500 | 1. 25900 | 2B |  |  |
|  |  |  | 1.2719 | 1.2448 | 1.2688 | 1. 2681 | 1.2546 | 1.31250 | 1.30310 |  | 1.3125 | 1.2719 | 1. 3040 | 1. 2769 | 1.2769 | 1.24500 | 1.25330 | 3B | UN | 1.3125-16 |
|  |  |  | 1.2716 | 1.2442 | 1. 2684 | 1. 2678 | 1.2552 | 1.31238 | 1. 30322 |  | 1.3131 | 1.2722 | 1.3034 | 1. 2766 | 1. 2772 | 1. 24512 | 1.25318 |  |  |  |
| 1. 3125-18 | UNEF | 2 A3 A | 1. 2749 | 1. 2508 | 1. 2700 | 1. 2700 | 1. 2580 | 1.31100 | 1.30230 |  | 1.3125 | 1. 2764 | 1. 3068 | 1. 2827 | 1. 2827 | 1. 25200 | 1. 26500 | 2B |  |  |
|  |  |  | ${ }_{1}^{1.2764}$ | 1.2503 | 1. 2703 1.2728 | 1.2697 1.2728 | 1.2508 | 1.31088 | 1.30242 |  | 1.3130 | ${ }_{1}^{1.2767}$ | 1.3063 | 1.2824 | 1.2830 | 1. 2522212 | 1.26488 | 3B | UNE | 1. 3125-18 |
|  |  |  | 1. 2761 | 1.2518 | 1. 2731 | 1. 2725 | 1.2613 | 1.31238 | 1.30392 |  | 1.3130 | 1.2767 | 1.3047 | 1.2808 | 1. 2814 | 1. 25212 | 1.26038 |  |  |  |
| 1.3125-20 | UN | 2 A3 A | 1. 2786 | 1. 2569 | 1. 2739 | 1. 2739 | 1.2631 | 1.31110 | 1.30300 |  | 1. 3125 | 1. 2800 | 1. 3078 | 1. 2861 | 1. 2861 | 1.25800 | 1. 27000 | 2B |  |  |
|  |  |  | 1. 2783 1.2800 | 1.2564 1.2583 | 1.2742 | 1. 2736 1.2765 | 1.2636 | 1.31098 1.31250 | 1.30312 |  | l $\begin{aligned} & 1.3130 \\ & 1.3125\end{aligned}$ | 1.2803 1.2800 | 1.3073 | 1. 28845 | 1.2864 | 1.25812 1.25800 | 1.26988 | 3B | UN | 1.3125-20 |
|  |  |  | 1.2797 | 1.2578 | 1.2768 | 1.2762 | 1.2662 | 1.31238 | 1. 30452 |  | 1.3130 | 1.2803 | 1.3057 | 1.2842 | 1.2848 | 1. 25812 | 1. 26608 | ${ }^{\text {B }}$ |  |  |
| 1.3125-28 | UN | 2 A3 A | 1. 2881 | 1. 2726 | 1. 2840 | 1. 2840 | 1. 2763 | 1.31130 | 1. 30480 |  | 1.3125 | 1. 2893 | 1. 3101 | 1. 2946 | 1. 2946 | 1. 27400 | 1. 28200 | 2B |  |  |
|  |  |  | 1. 2878 1.2893 | 1. 2721 | 1.2843 | 1.2837 | 1.2768 | 1.31118 | 1.30492 | - | 1.3130 | 1.2896 1.2893 1 | 1.3096 | 1.2943 | 1.2949 | 1.27412 | 1.28188 1.28010 |  | UN | 1.3125-28 |
|  |  |  | 1. 2890 | 1. 2733 | 1. 2865 | 1. 2859 | 1.2790 | 1.31238 | 1. 30612 |  | 1. 3130 | 1.2896 | 1.3088 1.3083 | 1. 2933 | 1.2933 1.2936 | 1.27400 1.2742 | $\begin{aligned} & 1.28010 \\ & 1.27998 \end{aligned}$ | 3B |  |  |
| 1.375-6 | UNC | 1A | 1. 2643 | 1. 1921 | 1.2523 | 1. 2523 | 1. 2162 | 1.37260 | 1.34530 |  | 1. 3750 | 1.2667 | 1.3544 | 1. 2822 | 1. 2822 | 1.19500 | 1. 22500 | 1B |  |  |
|  |  | 2 A | 1. 2639 1.2643 1 | 1.1913 1.1921 | 1.2527 | 1.2519 | 1.2170 | 1.37248 1.37260 | 1.34542 | 1.34530 | 1.3758 | 1.2671 1.2667 | 1.3536 1.3493 | 1.2818 1.2771 | 1.2826 | 1.19512 | 1. 22488 | 2B | UNC | 1.375-6 |
|  |  |  | 1. 2639 | 1.1913 | 1. 2567 | 1. 2559 | 1. 2210 | 1.37248 | 1.35452 | 1. 34542 | 1. 3758 | 1. 2671 | 1.3485 | 1. 2767 | 1. 2775 | 1.19512 | 1.22488 |  |  |  |
|  |  | 3A | 1. 2667 | 1. 1994 | 1. 2607 | 1. 2607 | 1. 2246 | 1.37500 | 1. 356880 |  | 1. 3750 | 1.2667 | 1. 34467 | 1. 2774 | ${ }_{1}^{1.2745}$ | 1.19500 | 1. 21460 | 3B |  |  |
|  |  |  | 1. 2663 | 1. 1937 | 1. 2611 | 1. 2603 | 1. 2254 | 1.37488 | 1.35692 |  | 1.3758 | 1.2671 | 1.3459 | 1. 2741 | 1.2749 | 1.19512 | 1.21448 |  |  |  |
| 1.375-8 | UN | 2 A | 1. 2916 | 1. 2375 | 1. 2844 | 1. 2844 | 1.2573 | 1.37280 | 1.35780 | 1. 35030 | 1. 3750 | 1. 2938 | 1.3572 | 1. 3031 | 1. 3031 | 1. 24000 | 1. 26500 | 2B |  |  |
|  |  | 3A | 1. 2912 | 1. 2368 1.2397 | 1.2848 | 1.2840 | 1.2580 1.2613 | 1.37268 1.37500 | 1.35792 1.36000 | 1.35042 | 1.3757 | 1. 2942 1.2938 | 1.3565 | 1. 3027 1.3008 | 1.3035 1.3008 | 1. 24012 | 1.26488 |  | UN | 1.375-8 |
|  |  | 3 A | 1. 2934 | 1. 2390 | 1. 2888 | 1.2880 | 1. 2620 | 1.37488 | 1.36012 |  | 1. 3757 | 1. 2942 | 1.3542 | 1. 3004 | 1.3012 | 1. 24012 | 1. 25458 | 3 |  |  |
| 1.375-12 | UNF | 1A | 1.3190 | 1. 2829 | 1. 3096 | 1.3096 | 1. 2916 | 1.37310 | 1.35590 |  | 1. 3750 | 1. 3209 | 1.3693 | 1. 3332 | 1.3332 | 1. 28500 | 1. 30300 | 1B |  |  |
|  |  | 2 A | 1.3187 1.3190 | 1. 2823 | 1.3099 1.3127 | 1.3093 | 1. 2922 1.2947 | 1.37298 1.37310 | 1.35602 |  | 1.3756 | 1.3212 | 1.3687 1.3652 | 1.3329 | 1.3335 | 1.28512 1.28500 | 1.30288 1.30300 | 2B | UNF | 1. 375-12 |
|  |  |  | 1.3187 | 1.2823 | 1.3130 | 1.3124 | 1.2953 | 1.37298 | 1.36182 |  | 1.3756 | 1.3212 | 1. 3646 | 1.3288 | 1.3294 | 1.28512 | 1. 30288 |  |  |  |
|  |  | 3 A | 1. 3209 | 1. 2848 | 1.3162 | 1. 3162 | 1. 2988 | 1.37500 | 1.36360 |  | 1. 3750 | 1.3209 | 1. 3631 | 1. 3270 | 1.3270 | 1. 28500 | 1. 29480 | 3B |  |  |
|  |  |  | 1.3206 | 1.2842 | 1.3165 | 1.3159 | 1. 2988 | 1.37488 | 1.36372 |  | 1. 3756 | 1.3212 | 1.3625 | 1. 3267 | 1. 3273 | 1. 28512 | 1. 29468 |  |  |  |
| 1.375-16 | UN | 2 A | 1. 3329 | 1. 3058 | 1.3278 | 1.3278 | ${ }^{1.3143}$ | 1.37350 | 1.36410 |  | 1.3750 | 1. 3344 | 1. 3681 | 1. 3410 | 1. 3410 | 1.30700 | 1.32100 | 2B |  |  |
|  |  | 3A | 1.3326 1.3344 1. | 1.3052 | 1.3281 | 1.3275 1.3306 | 1.3149 1.3171 1 | 1.37338 1.37500 | 1.36422 1.36560 |  |  | 1.3347 | 1.3675 | 1.34394 | 1.3413 1.3394 | 1.30712 | 1.32088 | 3B | UN | 1.375-16 |
|  |  |  | 1.3341 | 1.3067 | 1.3309 | 1.3303 | 1.3177 | 1.37488 | 1. 36572 |  | 1. 3756 | 1.3347 | 1.3659 | 1.3391 | 1.3397 | 1. 30712 | 1. 31568 |  |  |  |
| 1.375-18 | UNEF | 2 A | 1.3374 | 1.3133 | 1.3325 | 1.3325 | 1. 3205 | 1.37350 | 1. 36480 |  | 1. 3750 | 1. 3389 | 1. 3693 | 1. 3452 | 1. 3452 | 1. 31500 | 1. 32800 | 2B |  |  |
|  |  | 3A | 1.3371 1.3389 | 1.3128 | 1.3328 | 1.3322 | (1.3210 | 1.37338 1.37500 | 1.36692 1.36630 |  | 1.3755 1.3750 | 1.3392 | 1.3688 | 1.3449 1.336 | 1.3455 1.336 1.3 | 1.31512 | 1.32788 | 3B | UNEF | 1. 375-18 |
|  |  | 3 A | 1.3386 | ${ }_{1.3143}$ | 1.3356 | 1.3350 | 1.3238 | 1.37488 | 1.36642 |  | 1.3755 | 1.3392 | 1.3672 | 1. 3433 | 1.3439 | 1. 31512 | 1. 32288 |  |  |  |


| UN | $1.375-20$ |
| :---: | :---: |
| UN | $1.375-28$ |
| UN | $1.4375-6$ |
| UN | $1.4375-8$ |
| UN | $1.4375-12$ |
| UN | $1.4375-16$ |
| UNEF | $1.4375-18$ |
| UN | $1.4375-20$ |
| UN | $1.4375-28$ |
| UNF | $1.500-12$ |
| UNE | $1.500-6$ |
| UN | $1.500-8$ |
|  | $1.500-18$ |
|  |  |




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|  |  |  |  | $\begin{array}{ll} 108 \\ 0 \end{array}$ |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  | $\begin{aligned} & \text { NeNous } \\ & \text { Nomod } \\ & \text {-irinitiri } \end{aligned}$ |  |  |  |  |
|  |  | 웅ㅇㅇ ลํํํํ <br> －iットゥ～ |  |  |  | 皮梁に日 | $\text { son } \infty_{\infty}^{\infty}$ |  | Noses |  |  |  |  |
|  |  | © －iッドーシ | $\begin{aligned} & \text { Hes } \\ & \text { Hon } \\ & \text { ninn } \\ & \text { ninn } \end{aligned}$ |  |  |  |  |  |  |  |  ぞずずず <br>  |  |  |
| ざ ङ゙ | से ल | जै | स ल | से | जू ल゙ | स ¢ | जे ल゙ | से ल゙ | 【 से | ลิ ¢ | य दे | बू ल | से ल |
| ＇${ }_{5}$ | 台 | $\underset{S}{7}$ | $\stackrel{y}{2}$ | $\stackrel{y}{4}$ | $\stackrel{7}{4}$ | $\begin{aligned} & \text { 寽 } \\ & y \\ & \hline \end{aligned}$ | $\stackrel{\square}{\square}$ | 方 | $\begin{aligned} & 0 \\ & Z \\ & S \end{aligned}$ | 号 | $\begin{aligned} & \text { 空 } \\ & \vdots \end{aligned}$ | \％ | $\begin{aligned} & \text { 䛼 } \\ & \frac{2}{2} \end{aligned}$ |
|  | $\begin{aligned} & \infty \\ & \underset{\sim}{1} \\ & \stackrel{0}{6} \\ & - \\ & -1 \end{aligned}$ | $\begin{aligned} & 0 \\ & \stackrel{1}{\circ} \\ & \stackrel{1}{0} \\ & \end{aligned}$ |  |  |  |  | $\begin{aligned} & \stackrel{\rightharpoonup}{1} \\ & \stackrel{1}{0} \\ & \stackrel{1}{2} \\ & \underset{\sim}{7} \end{aligned}$ |  | $$ | $\begin{aligned} & \infty \\ & 0 \\ & 0 \\ & 0 \\ & -1 \end{aligned}$ | $\begin{aligned} & \text { a } \\ & \stackrel{1}{1} \\ & \stackrel{\rightharpoonup}{6} \\ & -i \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \\ & -0 \\ & - \end{aligned}$ | $\begin{aligned} & \infty \\ & \substack{1 \\ \hline \\ \stackrel{0}{2} \\ -\\ \hline \\ \hline} \end{aligned}$ |


| Nominal size and threads p | $\begin{gathered} \text { Series } \\ \text { designa- } \\ \text { tion } \end{gathered}$ | Class | Gages for external threads |  |  |  |  |  |  |  | Gages for internal threads |  |  |  |  |  |  | Class | Seriesdesignation | Nominalsize andthreadsper ine |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | X thread ring gages |  |  |  |  | Z plain ring gages for major diameter |  |  | X thread plug gages |  |  |  |  | Z plain plug gages for minor diameter |  |  |  |  |
|  |  |  | go |  | LO |  |  | GO | NOT GO |  | GO |  | HI |  |  | go | $\begin{gathered} \text { NOT } \\ \text { GO } \end{gathered}$ |  |  |  |
|  |  |  | $\begin{aligned} & \text { Piteh } \\ & \text { diam- } \\ & \text { eter } \end{aligned}$ | $\begin{aligned} & \text { Minor } \\ & \text { diam- } \\ & \text { diam- } \end{aligned}$ | Piteh diameter |  | $\begin{gathered} \text { Minor } \\ \text { diam. } \\ \text { diter } \end{gathered}$ |  | Semi-finished |  | Major eter eter | Piteh eter eter | $\begin{aligned} & \text { Major } \\ & \text { diam- } \\ & \text { eter } \end{aligned}$ | Piteh diameter |  |  |  |  |  |  |
|  |  |  |  |  | Plus anee gage | Minus tolerance |  |  |  |  |  |  |  | Minus ance gage | $\begin{aligned} & \text { Plus } \\ & \text { toler- } \\ & \text { anee } \\ & \text { gage } \end{aligned}$ |  |  |  |  |  |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 |
| 1. $500-20$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | in 1.4661 1.4658 1.4675 1.4672 | in 1.4444 1.449 1.4458 1.4453 1 | in 1.4613 1.4666 1.4639 1.4642 | in 1. 4613 1.4610 11.4639 1.4636 | in 1. 4505 1. 410 1.4531 1.4536 |  |  | in | in 11.5000 1.5005 1.5000 1.5005 | in 1. 4675 1.4678 1.4675 1.4678 | in 1.4954 1.4999 11.4938 1.4933 | in 1. 4377 1. 4734 1. 4721 1.4718 | in 1.4737 1. 4740 1.7721 1. 4724 |  |  | 2 B 3 B | UN | 1. $500-20$ |
| 1. 500-28 | UN | 2 A3 A | 1.4755 | 1.4600 1.4595 1 | 1.4713 <br> 1.4776 | 1.4713 1.4710 1 | 1.4636 | 1. 498870 | 1. 492220 |  | 1. 5000 | 1. 4768 | 1.4978 1.4973 | 1. 4823 1.4820 1 | 1. 4823 | 1. 46100 1.46112 | 1. 47000 1.46988 | 2B | UN | 1. $500-28$ |
|  |  |  | 1.4768 | 1.4613 | 1.4737 | 1.4737 | 1. 46660 | 1. 50000 | 1. 493350 |  | 1. 5000 1.5005 | 1. 4768 1.4771 | 1.4964 1.4959 | 1. 4889 1.4806 | 1. 4889 1.4812 | 1.46100 1.46112 | (1.46760 | 3B |  | 1.5002 |
| 1. $5625-6$ | UN | 2 A3 A | 1. 4518 | 1.3796 | 1. 4436 | 1.4436 | 1. 4075 | 1. 56010 | 1.54190 |  | 1. 5625 | 1. 4542 | 1. 5370 | 1. 4648 | 1. 4648 | 1.38200 | 1. 41300 | 2 B |  |  |
|  |  |  | 1.4513 | 1.3788 1.3820 | 1.4441 | 1.4431 | 1. 4083 | 1.55994 | 1.54206 1.54430 |  | 1.5633 1.5625 | 1. 4547 | 1.5362 1.5344 1 | 1.4643 | 1. 46453 | 1.38216 1.38200 | 1.41284 1.40210 | 3B | UN | 1. $5625-6$ |
|  |  |  | 1.4537 | 1.3812 | 1.4486 | 1.4476 | 1.4128 | 1. 56234 | 1.54446 |  | 1.5633 | 1. 4547 | 1.5336 | 1.4617 | 1. 4627 | 1. 38216 | 1. 40194 |  |  |  |
| 1. $5625-8$ | UN | 3 A | 1. 1.4791 | 1.4250 | 1.4717 | 1. 47717 | 1. 14446 | 1. 56030 | 1. 544330 |  | 1. 5625 | 1. 4813 | 1. 54500 | 1. 4909 | 1. 4999 | 1. 42700 | 1.45200 | 2B |  |  |
|  |  |  | 1. ${ }_{\text {1. } 47813}$ 1. | 1.4243 | 1.4722 | (1.4772 | 1.4453 | 1. 1.560250 | 1.54546 1.54750 |  | 1. 56622 | 1.4818 | 1.5443 1.5426 | 1.4904 | 1. 4914 | 1. 1.42716 | 1.45184 1.44220 1 | 3B | UN | 1. 5625-8 |
|  |  |  | 1. 4808 | 1. 2265 | 1.4763 | 1.4753 | 1. 4494 | 1. 56234 | 1.54766 |  | 1. 5632 | 1.4818 | 1. 5419 | 1.4880 | 1. 4890 | 1. 42716 | 1. 44204 |  |  |  |
| 1. 5625-12 | UN | 2 A | 1. 5066 | 1.4705 | 1. 5007 | 1. 5007 | 1. 4827 | 1. 56070 | 1.51930 |  | 1. 5625 | 1.5084 | 1.5521 | 1. 5160 | 1. 5160 | 1. 47200 | 1. 49000 | 2B |  |  |
|  |  | 3A | 1.5062 | (1.4699 | 1.5011 | 1.5003 1.5040 | 1. 48880 | 1.56054 | 1.54946 1.55110 |  | 1. 1.56325 | 1.5088 | 1.5515 | 1.5156 | 1.5164 1.5141 | 1. 1.472200 | 1. 48984 | 313 | UN | 1.5625-12 |
|  |  |  | 1.5080 | 1.4717 | 1.5044 | 1.5036 | 1. 4866 | 1. 56234 | 1.55126 |  | 1.5631 | 1.5088 | 1.5496 | 1.5137 | 1.5145 | 1.47216 | 1.48214 |  |  |  |
| 1. 5625-16 | UN | 2 A | 1.5203 | 1.4932 1.4926 | 1.5151 1.5155 | 1.5151 | 1. 5016 | 1. 56090 | 1.55150 1.55166 1.515 |  | 1.5625 | 1. 5219 | 1. 5558 | 1.5287 | 1.5287 | 1. 499500 | 1. 50900 | 2B | UN | 1.562-16 |
|  |  | 3A | 1. 5219 | 1.4948 | 1.5180 | 1.5180 | 1.5045 | 1. 56250 | 1.55310 |  | 1.5625 | 1.5219 | 1.5541 | 1.5270 | 1.5270 | 1. 49500 | 1.50330 | 3B | UN | 1. 5625-16 |
|  |  |  | 1.5215 | 1. 4942 | 1.5184 | 1.5176 | 1. 5051 | 1. 56234 | 1.55326 |  | 1. 5631 | 1. 5223 | 1.5535 | 1.5266 | 1.5274 | 1. 49516 | 1. 50314 |  |  |  |
| 1. $5625-18$ | UNEF | 2 A | 1. 5249 | 1. 5008 | 1. 5199 | 1. 5199 | 1. 5079 | 1. 56100 | 1. 55230 |  | 1. 5625 | 1. 5264 | 1.5570 | 1. 5329 | 1. 5329 | 1. 50200 | 1. 51500 | 2B |  |  |
|  |  | 3A | 1. 5264 | 1.5023 | 1.5227 | 1.5227 | 1.5107 | 1. 566250 | 1.55546 |  | 1.5630 | 1. 52688 | 1.5565 1.5553 | 1.5325 | 1.5333 1.5312 | ${ }_{1}^{1.50216}$ | 1.51484 | 3B | UNEF | 1. $5625-18$ |
|  |  |  | 1. 5260 | 1.5018 | 15231 | 1.5223 | 1.5112 | 1.56234 | 1.55396 |  | 1.5630 | 1.5268 | 1. 5548 | 1.5308 | 1.5316 | 1. 50216 | 1.51034 |  |  |  |
| 1. $5625-20$ | UN | 2 A | 1. 5288 | 1. 5069 | 1. 5238 | ${ }_{1}^{1.5238}$ | 1.5130 | 1. 56110 | 1.55300 |  | 1. 5625 | 1. 5300 | 1. 5579 | 1.5362 | 1. 5362 | 1. 50800 | 1. 52000 | 2B |  |  |
|  |  | 3A | 1.52320 | 1.5084 | 1.5264 | ${ }_{1.5264}^{1.5234}$ | ${ }_{1}^{1.5156}$ | 1. 565650 | 1. 55440 | --- | 1.5625 | 1.5304 | 1.5563 | 1.5346 | 1.5336 | ${ }_{1}^{1.508800}$ | ${ }_{1}^{1.51984}$ | 3B | UN | 1. $5625-20$ |
|  |  |  | 1. 5296 | 1.5078 | 1.5268 | 1. 5260 | 1. 5161 | 1. 56:234 | 1. 55456 |  | 1.5630 | 1.5304 | 1.5558 | 1.5342 | 1.5350 | 1. 50816 | 1.51604 |  |  |  |
| 1. $625-6$ | UN | 2 A | 1. 5142 | 1.4420 | 1. 5060 | 1. 5060 | 1. 4699 | 1. 62230 | 1. 60430 |  | 1.6250 | 1. 5167 |  | 1.5274 | 1. 5274 |  |  | 2B |  |  |
|  |  | 3 A | 1.5137 1.5167 | 1.4412 | 1. 5065 1.5105 | 1.5055 | 1. 47774 | 1.62234 | 1.60446 |  | 1.6258 1.6250 | 1.5172 1.5167 | 1. 5988 1.5969 | 1.5269 1.5247 | 1.5279 | 1.44516 | 1.47484 |  | UN | 1. $625-6$ |
|  |  |  | 1.5162 | 1.4437 | 1.5110 | 1.5100 | 1.4752 | 1.62484 | 1.60696 |  | 1.6258 | ${ }_{1.5172}$ | 1.5961 | 1.5242 | 1. 5252 | 1.44516 | 1. 46444 | ${ }^{\text {B }}$ |  |  |
| 1.625-8 | UN | 2 A | 1. 5416 | 1.4875 | 1.5342 | 1. 5342 | 1.5071 | 1. 62280 | 1. 60780 | 1. 60030 | 1. 6250 | 1. 5438 | 1.6076 | 1.5335 | 1. 5535 | 1. 49000 |  | 2B |  |  |
|  |  | 3 A | 1.5411 1.5438 | 1.4868 1.4897 | 1.5347 1.5382 | 1.5337 1.5382 | 1.5078 | 1. 62264 1.62500 | 1.60796 1.61000 | 1. 60046 | 1.6257 1.6250 | 1.5443 1.5438 1.54 | 1.6069 1.6051 1 | 1.5520 1.5510 | 1.5540 | 1.49016 | 1.51484 |  | UN | 1.625-8 |
|  |  |  | 1.5433 | 1.4890 | 1.5387 | 1.5377 | 1.5118 | 1.62484 | 1.61016 |  | 1.6257 | 1.5443 | 1.6044 | 1.5505 | 1.5515 | 1.49016 | ${ }_{1.50454}$ |  |  |  |







| $\underset{\square}{Z}$ | $\begin{aligned} & Z \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { 左 } \\ & \underset{5}{7} \\ & \vdots \end{aligned}$ | Z | $\underset{\Delta}{Z}$ | $\underset{i}{Z}$ | $\begin{aligned} & \text { Z } \\ & \hline \end{aligned}$ | $\underset{\vdots}{Z}$ | $\begin{aligned} & \text { ए } \\ & 1 \\ & 7 \\ & \vdots \\ & b \end{aligned}$ | $\underset{b}{Z}$ | $\square$ <br> $\square$ | 吕 | 号 | 云 | 号 |
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| $\begin{aligned} & \text { N } \\ & 1 \\ & 0 \\ & 0 \\ & -1 \end{aligned}$ | $\begin{aligned} & 9 \\ & 1 \\ & 0 \\ & 0 \\ & \hline \end{aligned}$ | $$ | $\begin{aligned} & \text { y } \\ & 1 \\ & 1 \\ & 0 \\ & 0 \\ & -1 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & 0 \\ & \hline 8 \end{aligned}$ | $\begin{aligned} & \infty \\ & 1 \\ & 10 \\ & \infty \\ & 8 \end{aligned}$ | $$ | $\begin{aligned} & 0 \\ & 1 \\ & 10 \\ & \infty \\ & 0 \end{aligned}$ | $\begin{aligned} & \infty \\ & \frac{1}{2} \\ & \frac{\infty}{8} \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & 8 \\ & 1 \\ & 10 \\ & 10 \\ & 0 \end{aligned}$ | 108 | 1 8 8 $i$ $i$ | $\infty$ $\stackrel{1}{5}$ $\sim$ -1 | $\begin{aligned} & \stackrel{N}{1} \\ & \frac{1}{5} \\ & 1 \\ & \text {-i } \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 1 \\ & 10 \\ & -1 \end{aligned}$ |

Table 6.19. Gages for standard thread series, Unified screw threads-Continued


| $1.9375-6$ |
| :--- |
| $1.9375-8$ |
| $1.9375-12$ |
| $1.9735-16$ |
| $1.9375-20$ |
| $2.000-4.5$ |
| $2.000-6$ |
| $2.000-8$ |
| $2.000-12$ |
| $2.125-16$ |
| $2.125-12$ |
| $2.000-16$ |
| $2.125-6$ |
| $20-8$ |




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|  |  |  |  | Ser |  |  | $\begin{aligned} & 8989 \\ & 0.10 \\ & 0.00 \infty \end{aligned}$ | $\begin{aligned} & 868 \\ & 868 \\ & 6=\frac{1}{6} \% \end{aligned}$ | $\begin{aligned} & \text { B } \\ & \text { MN } \\ & \text { Wh } \\ & \text { Wh } \end{aligned}$ |  |  |  |  |  |
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| Wion $\infty \infty$ |  | $\begin{aligned} & \infty \sim \infty \\ & \mathcal{F}_{\infty}^{\infty} \mathscr{N}_{\infty}^{\infty} \underset{\infty}{\infty} \end{aligned}$ | Wisi fir |  |  | wn in in |  |  |  |  | $\begin{aligned} & \text { NㅜN } \\ & \text { N } \\ & \text { NS } \end{aligned}$ |  |  |  |
| －iriniri | －i－ini－i | －～ini－ | －iーiーi | －i～i～i | ～i～i～i～i～i～i | ～－i $\sim$－i | －riri | －i－－i－i | －－－ | －i～i～iri | sicicis | cicicis | cicicic | Nicicio |
| moisp 애心 M |  |  |  |  |  |  |  |  |  | $6 \text { Co B }$ | $\begin{aligned} & \text { 2NG } \\ & \text { A888 } \end{aligned}$ |  |  | 펑웅웅 |
| －iヵiri | －iーiーi | －i～i～in | －iッiri | － | －iriー～ー | －ュー～ー | － | ～～～～～ | － | －iririri | ciovoici | ciciovi | －${ }^{\text {covici }}$ | vicuci |
|  | $\begin{aligned} & \text { ザ心N } \\ & \text { CNO } \end{aligned}$ |  | BUN: | 태N్N M |  |  | $\begin{aligned} & \text { Nas } \\ & \text { No } \\ & \infty \\ & \infty \\ & \infty \\ & \infty \end{aligned}$ |  |  |  |  |  |  |  |
| ～irini | －i～ini | －iririri | －iriri～i | －i | －iririmiri | －iャiri | －iririri | べーシーシ | ～－でーi | －i－i－i～i | sisisis | sioisis | －${ }^{\text {cosoi }}$ |  |
|  |  | $\begin{aligned} & W_{N}^{\infty} \prod_{\infty}^{\infty} \\ & \infty \\ & \infty \\ & \infty \\ & \infty \end{aligned}$ |  |  | NiNA 15010 |  |  |  | $\theta \sigma \sigma \sigma$ |  |  |  | BERM |  |
| $\begin{aligned} & \text { Non M } \\ & \text { Nos \% } \end{aligned}$ |  ભ |  |  |  | 응ㅇㅇㅇㅇㅇㅇㅇㅇㅇㅇ | $88888$ | $88888$ | $8888$ | $\begin{aligned} & 8.898 \\ & 88888 \\ & \hline 8 \end{aligned}$ |  |  |  |  |  |
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|  |  | $\begin{gathered} \text { 97 } \\ \text { 点 } \end{gathered}$ | $\begin{gathered} 0 \\ 0 \\ 6 \\ 6.6 \end{gathered}$ |  | $\begin{aligned} & \text { m } \\ & \text { ú } \\ & 8 \\ & \text { i } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & 9 \\ & \mathbf{1} \\ & 8 \\ & \text { din } \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{0} \\ & \stackrel{0}{\text { an }} \end{aligned}$ |  |  |  | ＋ | $\begin{gathered} \infty \\ \stackrel{\leftrightarrow}{4} \\ \stackrel{4}{9} \end{gathered}$ |  | －11 |

Table 6.19. Gages for standard thread series, Unified screw threads-Continued


|  |  | $\begin{aligned} & \text { I } \\ & \stackrel{8}{6} \\ & \text { on } \end{aligned}$ | $\begin{aligned} & 0 \\ & \stackrel{0}{0} \\ & \text { in } \\ & \text { in } \end{aligned}$ |  |  | $\begin{gathered} 9 \\ \stackrel{1}{1} \\ \stackrel{y}{6} \\ \text { in } \end{gathered}$ |  |  |  |  | $\begin{aligned} & \stackrel{0}{6} \\ & \text { 总 } \\ & \text { ai } \end{aligned}$ | $\begin{aligned} & \text { \& } \\ & \text { d } \\ & \text { dy } \\ & \text { ain } \end{aligned}$ | $\stackrel{H}{1}$ | ¢ |
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Table 6.19. Gages for standard thread series, Unified screw threads-Continued


| $\begin{aligned} & 0 \\ & \substack{1 \\ \vdots \\ 0 \\ \hline} \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{1}{8} \\ & \stackrel{c}{6} \\ & 0 \end{aligned}$ | $\begin{aligned} & 9 \\ & \frac{1}{6} \\ & 8 \\ & 0 \end{aligned}$ | $\begin{aligned} & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \end{aligned}$ | $\begin{aligned} & \bar{\Psi} \\ & \stackrel{1}{8} \\ & \stackrel{y}{8} \\ & \text { on } \end{aligned}$ |  | $\begin{aligned} & \infty \\ & \stackrel{\infty}{\infty} \\ & \stackrel{y}{*} \end{aligned}$ |  |  | $\begin{aligned} & \text { T } \\ & \stackrel{\rightharpoonup}{9} \\ & c \end{aligned}$ | $\begin{gathered} 0 \\ \stackrel{1}{9} \\ \text { c } \end{gathered}$ | $\begin{aligned} & \infty \\ & \stackrel{\infty}{9} \\ & \text { 菏 } \end{aligned}$ |  | $\begin{gathered} \stackrel{0}{T} \\ \stackrel{\rightharpoonup}{9} \\ \underset{\sim}{c} \end{gathered}$ | ＋ |
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| $\begin{aligned} & 0 \\ & \vdots \\ & 8 \\ & 0 \\ & \dot{\infty} \end{aligned}$ | $\begin{aligned} & \infty \\ & \stackrel{1}{8} \\ & \vdots \\ & \infty \end{aligned}$ | $\begin{aligned} & 9 \\ & \stackrel{y}{1} \\ & \vdots \\ & 0 \\ & 0 \end{aligned}$ | $\begin{array}{r} 0 \\ \stackrel{1}{\mathbf{8}} \\ \stackrel{8}{\infty} \end{array}$ | $\begin{aligned} & \stackrel{\otimes}{1} \\ & \stackrel{1}{6} \\ & \text { on } \end{aligned}$ | $\begin{aligned} & \text { d } \\ & \text { d } \\ & \text { N } \end{aligned}$ | $\begin{gathered} \infty \\ \stackrel{y}{c} \\ \stackrel{y}{4} \\ \infty \end{gathered}$ | $\begin{aligned} & \stackrel{9}{7} \\ & \stackrel{\square}{96} \\ & \end{aligned}$ |  | $\begin{aligned} & \stackrel{\rightharpoonup}{⿳ 亠 口 冋 日 木 ~} \\ & \infty \\ & \infty \end{aligned}$ | $\begin{aligned} & 0 \\ & \stackrel{i}{1} \\ & \dot{\omega} \\ & \infty \end{aligned}$ |  | $\begin{aligned} & \text { I } \\ & \stackrel{7}{7} \\ & \text { 感 } \end{aligned}$ |  | ＋ |

Table 6．19．Gages for standard inread series，Unified screw threads－Continued

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| $\begin{aligned} & \mathscr{D}_{2}^{2} \\ & \underset{0}{0} \end{aligned}$ |  |  |  |  | $\stackrel{\square}{\square}$ | $\cdots$ | ＊＊ | $\stackrel{\sim}{\sim}$ | $\triangle \sim$～ | $\stackrel{\sim}{\sim}$ | $\cdots$ | ผ लै | $\stackrel{\sim}{\sim}$ | 숭 | ¢ लै |
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Table 6．19．Gages for standard thread series，Unified screw threads－Continued

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Table 6.19. Gages for standard thread series, Unified serew threads-Continued


| $\begin{aligned} & \frac{0}{1} \\ & \frac{10}{10} \\ & 10 \\ & 10 \end{aligned}$ | $\begin{aligned} & 1 \\ & 8 \\ & 8 \\ & 10 \\ & 1 \end{aligned}$ | $\begin{gathered} \text { N } \\ \underset{6}{1} \\ 10 \end{gathered}$ | $\frac{0}{8}$ | $\begin{aligned} & 9 \\ & 1 \\ & 10 \\ & 1 \\ & 10 \\ & 10 \end{aligned}$ |  | $\frac{\pi}{15}$ | $\begin{aligned} & \frac{2}{1} \\ & \frac{1}{8} \\ & \text { is } \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{1}{1} \\ & 10 \\ & 10 \end{aligned}$ | $\begin{aligned} & \frac{2}{1} \\ & \frac{10}{10} \\ & \infty \\ & 10 \end{aligned}$ | $\begin{aligned} & 0 \\ & \frac{1}{1} \\ & 15 \\ & 10 \\ & \text { in } \end{aligned}$ | $\begin{aligned} & i \\ & 8 \\ & 8 \\ & 8 \end{aligned}$ | $\begin{aligned} & \frac{1}{1} \\ & \frac{1}{8} \\ & 0 \end{aligned}$ | $\begin{gathered} \frac{\varphi}{1} \\ \stackrel{8}{8} \\ 0 \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Z | $\stackrel{7}{\square}$ | $\underset{Z}{z}$ | $\begin{aligned} & 7 \\ & b \end{aligned}$ | $\stackrel{1}{4}$ | $\stackrel{Z}{2}$ | 営 | $\stackrel{7}{8}$ | $\underset{\Delta}{Z}$ | $\underset{B}{Z}$ | $\stackrel{2}{2}$ | $\begin{aligned} & 2 / 2 \\ & \vdots \end{aligned}$ | 営 | $\stackrel{2}{7}$ |
| 会 | ＊＊＊ | －$\stackrel{\sim}{\sim}$ | $\cdots$ | ベッ | －$\frac{\cdots}{\text { m }}$ | ผै \％ै | 氼 | ก ¢ | ล | ค คึ | 幺 $\stackrel{\text { a }}{\text { c }}$ | ल लิ | ज $\frac{\mathrm{m}}{\text { m }}$ |
|  |  |  |  | 010810 <br> $81-\infty$ 15157 <br>  | 319815 $=1015$ 10 10 1515150 |  |  |  |  |  |  |  |  |
|  |  |  |  | 용용N 15 icx 10 <br>  <br>  | §はㅋN <br> KN <br> 151515 <br>  | －20 817 <br> 8．8\％ <br>  <br>  |  |  | 8193 <br> 1020.5 <br> $1 \infty \times \infty$ <br> $15 \times 15 \times \sim \times \underbrace{\circ}$ |  |  |  |  |
|  |  | － 10 等 $\cdots 20$ <br>  | $\mathfrak{N B}$ $0$ xc เ | 81209 T001515 $x 0^{\circ} \times 0^{\circ} \times 0^{\circ} \times 5^{\circ}$ | $19-12=$ 장웅 <br>  |  | 路领定 RRRP $15 \times 2 \times 2 \times 15$ |  | S29R0 Not $\infty \infty$ <br>  |  |  | 3150 M <br> W10 10 <br> \％$\sigma \%$ <br>  |  |
|  |  |  |  | 为刕に RNME <br>  | 109208 WWふ <br>  |  |  |  | B\％R <br> GRE <br> $\infty \infty \infty$ <br>  |  | N二88 <br> 15 in <br> $\infty \infty \infty$ <br>  |  |  |
|  <br> 为 <br> ッッッm <br> 154 $15 \times 5$ |  |  | F9 N15 <br> 完 <br>  | $\begin{gathered} 8 \\ 3 \\ =0 \\ 0 \end{gathered} \frac{1}{6}$ | $\begin{aligned} & =0 N \\ & =0=0 \\ & =0 \end{aligned}$ |  |  |  |  | とにっ！ O x |  |  | ッにはに Bi $12 \times 15 \times 25^{\circ}$ |
|  |  |  |  | $8: 8.3$ <br> RTRT <br> $15.12 x 20$ <br> $152025 \times 2$ |  <br> $0 \infty 0$ <br> 102000 <br> $15 \times 1 \times 1510$ |  | 12.512 <br> $\overbrace{8}^{8} 88$ <br>  |  |  |  $\infty \times 0$ <br>  | जde8我 <br>  | R19 212 <br> कुण <br> 10． 15150 | あった8 <br> 46 <br> ふめ क क <br> $15 \times 5 \times 50$ |
| 心が心 <br>  |  |  |  | 운용 NQ <br>  |  © 9 O $1512 \times 2 \times 15$ |  |  |  |  |  | $\begin{aligned} & 8.38: 9 \\ & 8.88 \\ & 0.0 \end{aligned}$ | $$ |  |
|  |  | － |  |  | ! |  |  |  |  |  |  |  |  |
|  <br> Wis <br> MN <br>  |  |  |  |  |  | 81084 NA B NNON <br>  |  <br>  ペッペー い゙ い゙さくらい | 810812 $\infty_{0}^{\infty} 98$ ミ゚ッボ <br>  |  |  <br> $\rightarrow 20$ <br> $\infty-\infty$ <br> 15251515 |  | 813812 <br> ${ }_{3}{ }^{1}$ <br> \％ 808 <br> $15 \times 5 \times 505$ | $8198 x$ <br> $\infty 88$ <br> $\bigcirc \%$ \％ <br> $15 \times 50^{\circ} 10^{\circ} 15^{\circ}$ |
| 82810 －N N N MNM N <br>  |  |  |  | 819810 운 N09 <br>  |  |  |  | 012812 <br> － 28 <br> が， <br> ールト <br>  |  |  |  |  |  |
| Mosmen |  |  |  |  | NNN <br> $\hat{H}_{0} 0$ <br>  |  |  |  | ふッに8 ぶすが客 FRRF $155^{\circ} \mathrm{L}$ |  | Nロ～N象家灾 <br>  |  |  |
| 12.8 \％ N ¢ Cm <br>  | O20 29 － ल人 ल <br>  |  |  | $\frac{\pi}{6} \frac{\pi}{2 x}$ <br> 以 <br>  | ® 心क <br>  x | に＝$-\infty$ <br> －No <br> 125154 <br> $x 0^{\circ} \times x^{\circ} \times x^{\circ} \times 5^{\circ}$ |  |  |  | のにお Nise <br>  $2515 \times 15 \times 5$ |  |  |  |
| ＊－ G18 \％ ल⿵人 $10^{\circ} \times 0^{\circ} 150^{\circ}$ | Su 1020 －N NO 썽N यธ |  |  | Q10に～ <br> $=028$ <br> 亿ิ <br>  |  | にな8 <br> TiN10 15 <br>  | $8121=2$ <br>  <br> $150^{\circ} \times 5^{\circ} \times 15^{\circ} \times 15^{\circ}$ |  | $\begin{aligned} & -\frac{10}{\infty} \frac{1}{\infty} \frac{0}{\infty} \\ & 12 x+10 \end{aligned}$ | 3810 NONM <br>  |  |  |  |
|  | ッチッか ผN Nิ <br>  |  |  | Nome <br> 领拥调 <br>  | W20 20 $12 \pm 15$ $1210251 \%$ <br>  |  | $\begin{array}{rl}1 \\ 1000 \\ 0 & 0 \\ 0\end{array}$ <br> 12.5010 <br> 10， <br> 10 上 |  |  |  <br> ${ }^{3} 850.5$ <br>  |  |  | すく8 シ ふึ คึ 凡 $10^{\circ} \times 0^{\circ} 40^{\circ}$ เ |
|  | 풍N |  |  | $\infty$ か8 <br> 象解行 <br>  |  | 为に日 2010 151010 <br>  | © © <br>  |  |  | $120+x$ <br>  <br>  | かに会 <br> ค <br> $\infty \infty \infty$ <br>  | 小的娍 <br> おらずす <br>  | $1087 \infty$ <br> 15.96 <br> $\stackrel{2}{\circ}=\stackrel{\infty}{\circ}$ <br> เร゙ เร่ เร゙ เన் |
| जे | वे | 可 | 会管 | ब ले | ज | जे | से ${ }^{\text {a }}$ | 可 | उ ${ }_{8}$ | जे | 大 | ज ${ }^{3}$ | 令 ${ }^{\text {a }}$ |
| 岩 | \％ | \％ | $\stackrel{4}{4}$ | \％ | S | 年 | 光 | \％ | 2 | V1 | \％ | 5 | 号 |
| $\frac{6}{1}$ | 7 8 10 10 | $N$ <br> $\stackrel{N}{5}$ <br> 10 <br> 1 |  | $\begin{aligned} & 0 \\ & \frac{0}{1} \\ & 2 \\ & 0 \\ & 10 \end{aligned}$ | $$ | $\begin{aligned} & 1 \\ & 18 \\ & 18 \\ & 8 \end{aligned}$ | $\frac{9}{1}$ | $\begin{aligned} & 9 \\ & \frac{1}{6} \\ & 15 \\ & 10 \end{aligned}$ | $\begin{aligned} & \frac{9}{1} \\ & 10 \\ & 10 \\ & 10 \end{aligned}$ | 2 1 10 10 10 | $\begin{aligned} & \Pi \\ & \frac{1}{8} \\ & 0 \end{aligned}$ | $\stackrel{N}{3}$ | $\begin{aligned} & 0 \\ & \frac{1}{8} \\ & 0 \end{aligned}$ |

Table 6.20. Setting plug gages, Unified screw threads

| Nominal size and threads per inclı | Series designation | Class | W truneated setting plugs |  |  |  |  |  |  | 13asie-erest setting plugs |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Plug for GO thread gage a |  |  | Plug for LO thread gage a |  |  |  | Major diameter |  |  |  |
|  |  |  | Major diameter |  | 1'iteh diameter | Majok diameter |  | Pitel diameter |  | Plug for GO thread gage a,b |  | Plug for LO thread gage ${ }^{a, 0}$ |  |
|  |  |  | Truncated | Full |  | $\begin{aligned} & \text { Trun- } \\ & \text { eated } \end{aligned}$ | Full | Plus tolerance gage | Minus tolerance gage | W tolerance | X tolerance | W tolerance | X tolerance |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11A | 1113 | 12A | 1213 |
| . $060-80$ | UNF | 24 3 A | $\begin{aligned} & \text { in } \\ & 0.0561 \\ & .0558 \\ & .0566 \\ & .0563 \end{aligned}$ | $\begin{gathered} i n \\ 0.0595 \\ .0598 \\ .0600 \\ .0603 \end{gathered}$ | $\begin{gathered} i n \\ 0.0514 \\ .0513 \\ .0519 \\ .0518 \end{gathered}$ | $\begin{gathered} i n \\ 0.0550 \\ .0547 \\ .0560 \\ .0557 \end{gathered}$ | $\begin{aligned} & \text { in } \\ & 0.0584 \\ & .0587 \\ & 0594 \\ & .0597 \end{aligned}$ | $\begin{gathered} i n \\ 0.0496 \\ .0497 \\ .0506 \\ .0507 \end{gathered}$ | $\begin{gathered} i n \\ 0.0496 \\ .0495 \\ .0506 \\ .0505 \end{gathered}$ | in 0.0595 .0598 .0600 .0603 | in 0.0595 .0598 .0600 .0603 | in 0.0584 .0587 .0594 .0597 | in <br> 0.0584 <br> . 0587 <br> . 0594 <br> . 0597 |
| . 073-64 | UNC | 2 A 3 A | .0684 .0681 .0690 .0687 | .0724 .0727 .0730 .0733 | .0623 .0622 .0629 .0628 | .0671 .0668 .0682 .0679 | .0717 .0720 .0788 .0731 | .0603 .0604 .0614 .0615 | .0603 .0602 .0614 .0613 | .0724 .0727 .0730 .0733 | .0724 .0728 .0730 .0734 | .0717 .0720 .0728 .0731 | .0717 .0721 .0728 .0732 |
| . $073-72$ | UNF | 2.4 3 A | .0687 .0684 .0693 .0690 | .0724 .0727 .0730 .0733 | .0634 .0633 .0640 .0639 | .0675 .0672 .0686 .0683 | .0715 .0718 .0726 .0729 | .0615 .0616 .0626 .0627 | .0615 .0614 .0626 .0625 | .0724 .0727 .0730 .0733 | .0724 .0727 .0730 .0733 | .0715 .0718 .0726 .0729 | .0715 .0718 .0726 .0729 |
| . 086-56 | UNC | 2 A 3 A | .0810 .0807 .0816 .0813 | .0854 .0857 .0860 .0863 | .0738 .0737 .0744 .0743 | .0794 .0791 .0805 .0802 | .0850 .0853 .0860 .0863 | .0717 .0718 .0728 .0729 | .0717 .0716 .0728 .0727 | .0854 .0857 .0860 .0863 | .0854 .0858 .0860 .0864 | .0850 .0853 .0860 .0863 | .0850 .0854 .0860 .0864 |
| . 086-64 | UNF | 2 A 3.4 | .0814 .0811 .0820 .0817 | .0854 .0857 .0860 .0863 | .0753 .0752 .0759 .0758 | .0801 .0798 .0812 .0809 | .0847 .0850 .0858 .0861 | .0733 .0734 .0744 .0745 | .0733 .0732 .0744 .0743 | .0854 .0857 .0860 .0863 | .0854 .0858 .0860 .0864 | .0847 .0850 .0858 .0861 | .0847 .0851 .0858 .0862 |
| . 099-48 | UNC | 2 A 3 A | .0934 .0931 .0941 .0938 | .0983 .0986 .0990 .0993 | .0848 .0847 .0855 .0854 | .0915 .0912 .0928 .0925 | .0981 .0984 .0990 .0993 | .0825 .0826 .0838 .0839 | .0825 .0824 .0838 .0837 | .0983 .0986 .0990 .0993 | .0983 .0987 .0990 .0994 | .0981 .0984 .0990 .0993 | .0981 .0985 .0990 .0994 |
| .099-56 | UNF | 2 A 3 A | .0939 .0936 .0946 .0943 | .0983 .0986 .0990 .0993 | .0867 .0866 .0874 .0873 | .0922 .0919 .0935 .0932 | .0978 .0981 .0990 .0993 | .0845 .0846 .0858 .0859 | .0845 .0844 .0858 .0857 | .0983 .0986 .0990 .0993 | .0983 .0987 .0990 .0994 | .0978 .0981 .0990 .0993 | .0978 .0982 .0990 .0994 |
| . 112-40 | UNC | 2 A 3 A | .1056 .1053 .1064 .1061 | .1112 .1115 .1120 .1123 | .0950 .0949 .0958 .0957 | .1033 .1030 .1047 .1044 | .1112 .1115 .1120 .1123 | .0925 .0926 .0939 .0940 | .0925 .0924 .0939 .0938 | .1112 .1115 .1120 .1123 | .1112 .1116 .1120 .1124 | .1112 .1115 .1120 .1123 | .1112 .1116 .1120 .1124 |
| . 112-48 | UNF | 2 A 3 A | .1064 .1061 .1071 .1068 | .1113 .1116 .1120 .1123 | .0978 .0977 .0985 .0984 | .1044 .1041 .1057 .1054 | .1110 .1113 .1120 .1123 | .0954 .0955 .0967 .0968 | .0954 .0953 .0967 .0966 | .1113 .1116 .1120 .1123 | .1113 .1117 .1120 .1124 | .1110 .1113 .1120 .1123 | .1110 .1114 .1120 .1124 |
| . 125 -40 | UNC | 2 A 3 A | .1186 .1183 .1194 .1191 | .1242 .1245 .1250 .1253 | .1080 .1079 .1088 .1087 | .1162 .1159 .1177 .1174 | .1242 .1245 .1250 .1253 | .1054 .1055 .1069 .1070 | .1054 .1053 .1069 .1068 | .1242 .1245 .1250 .1253 | .1242 .1246 .1250 .1254 | .1242 .1245 .1250 .1253 | .1242 .1246 .1250 .1254 |
| . 125-44 | UNF | 2 A 3 A | .1191 .1188 .1198 .1195 | .1243 .1246 .1250 .1253 | .1095 .1094 .1102 .1101 | .1168 .1165 .1181 .1178 | .1240 .1243 .1250 .1253 | .1070 .1071 .1083 .1084 | .1070 .1069 .1083 .1082 | .1243 .1246 .1250 .1253 | .1243 .1247 .1250 .1254 | .1240 .1243 .1250 .1253 | .1240 .1244 .1250 .1254 |
| . 138-32 | UNC | 2 A 3 A | .1307 .1304 .1315 .1312 | .1372 .1375 .1380 .1383 | .1169 .1168 .1177 .1176 | .1276 .1273 .1291 .1288 | .1372 .1375 .1380 .1383 | .1141 .1142 .1156 .1157 | .1141 .1140 .1156 .1155 | 1372 .1375 .1380 .1383 | .1372 .1377 .1380 .1385 | .1372 .1375 .1380 .1383 | .1372 .1377 .1380 .1385 |
| . 138-40 | UNF | 24 3 A | .1316 .1313 .1324 .1321 | .1372 .1375 .1380 .1383 | .1210 .1209 .1218 .1217 | 11292 .1289 .1306 .1303 | .1372 .1375 .1380 .1383 | .1184 .1185 .1198 .1199 | .1184 .1183 .1198 .1197 | 1372 .1375 .1380 .1383 | .1372 .1376 .1380 .1384 | .1372 .1375 .1380 .1383 | .1372 .1376 .1380 .1384 |
| . 164-32 | UNC | 2 A 3 A | .1566 .1563 .1575 .1572 | .1631 .1634 .1640 .1643 | .1428 .1427 .1437 .1436 | .1534 .1531 .1550 .1547 | .1631 .1634 .1640 .1643 | .1399 .1400 .1415 .1416 | .1399 .1398 .1415 .1414 | .1631 .1634 .1640 .1643 | .1631 .1636 .1640 .1645 | .1631 .1634 .1640 .1643 | .1631 .1636 .1640 .1645 |
| . 164-36 | UNF | 2 A 3 A | .1572 .1569 .1580 .1577 | .1632 .1635 .1640 .1643 | .1452 .1451 .1460 .1459 | .1544 .1541 .1559 .1556 | .1632 .1635 .1640 .1643 | $\begin{aligned} & .1424 \\ & .1425 \\ & .1439 \\ & .1440 \end{aligned}$ | .1424 .1423 .1439 .1438 | $\begin{aligned} & .1632 \\ & .1635 \\ & .1640 \\ & .1643 \end{aligned}$ | .1632 .1636 .1640 .1644 | .1632 .1635 .1640 .1643 | .1632 .1636 .1640 .1644 |
| . $190-24$ | UNC | 2 A 3 A | .1811 .1806 .1821 .1816 | $\begin{aligned} & .1890 \\ & .1895 \\ & .1900 \\ & .1905 \end{aligned}$ | $\begin{array}{r} .1619 \\ .1618 \\ .1629 \\ .1628 \end{array}$ | $\begin{aligned} & .1766 \\ & .1761 \\ & .1784 \\ & .1779 \end{aligned}$ | $\begin{array}{r} .1890 \\ .1895 \\ .1900 \\ .1905 \end{array}$ | $\begin{aligned} & .1586 \\ & .1587 \\ & .1604 \\ & .1605 \end{aligned}$ | $\begin{aligned} & .1586 \\ & .1585 \\ & .1604 \\ & .1603 \end{aligned}$ | $\begin{array}{r} .1890 \\ .1895 \\ .1900 \\ .1905 \end{array}$ | $\begin{array}{r} .1890 \\ .1895 \\ .1900 \\ .1905 \end{array}$ | .1890 .1895 .1900 .1905 | .1890 .1895 .1900 .1905 |

See footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Class | W truneated setting plugs |  |  |  |  |  |  | Basie-erest setting plugs |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Plug for GO thread gage ${ }^{\text {a }}$ |  |  | Plug for LO thread gage a |  |  |  | Major diameter |  |  |  |
|  |  |  | Major diameter |  | Pitch diameter | Major diameter |  | Piteh diameter |  | Plug for GO thread gage $a, b$ |  | Plug for LO thread gage a.c |  |
|  |  |  | Truneated | Full |  | Truneated | Full | Plus tolerance gage | Minus tolerance gage | W toleranee | X <br> tolerance | W tolerance | X toleranee |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11A | 11 B | 12A | 12B |
| . 190-32 | UNF | 2 A 3 A | in 0.1826 .1823 .1835 .1832 | in 0.1891 .1894 .1900 .1903 | $\begin{gathered} i n \\ 0.1688 \\ .1687 \\ .1697 \\ .1696 \end{gathered}$ | $\begin{aligned} & \text { in } \\ & 0.1793 \\ & .1790 \\ & .1809 \\ & .1806 \end{aligned}$ | in 0.1891 .1894 .1900 .1903 | $\begin{gathered} i n \\ 0.1658 \\ .1659 \\ .1674 \\ .1675 \end{gathered}$ | $\begin{array}{r} i n \\ 0.1658 \\ .1657 \\ .1674 \\ .1673 \end{array}$ | in 0.1891 .1894 .1900 .1903 | $\begin{aligned} & \text { in } \\ & 0.1891 \\ & .1896 \\ & .1990 \\ & .1905 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & 0.1891 \\ & .1894 \\ & .1900 \\ & .1903 \end{aligned}$ | in <br> 0.1891 <br> .1896 <br> $\begin{array}{r}.1900 \\ . \\ \hline\end{array}$ <br> . 1905 |
| . 216 -24 | UNC | 2 A 3 A | .2071 .2066 .2081 .2076 | .2150 .2155 .2160 .2165 | .1879 .1878 .1889 .1888 | .2025 .2020 .2043 .2038 | .2150 .2155 .2160 .2165 | .1845 .1846 .1863 .1864 | .1845 .1844 .1863 .1862 | .2150 .2155 .2160 .2165 | .2150 .2155 .2160 .2165 | .2150 .2155 .2160 .2165 | .2150 .2155 .2160 .2165 |
| . 216 -28 | UNF | 2 A 3 A | .2079 .2074 .2089 .2084 | .2150 .2155 .2160 .2165 | .1918 .1917 .1928 .1927 | .2041 .2036 .2059 .2054 | .2150 .2155 .2160 .2165 | .1886 .1887 .1904 .1905 | .1886 .1885 .1904 .1903 | .2150 .2155 .2160 .2165 | .2150 .2155 .2160 .2165 | .2150 .2155 .2160 .2165 | .2150 .2155 .2160 .2165 |
| . 216-32 | UNEF | 2 A 3 A | .2086 .2083 .2095 .2092 | .2151 .2154 .2160 .2163 | .1948 .1947 .1957 .1956 | .2052 .2049 .2068 .2065 | .2151 .2154 .2160 .2163 | .1917 .1918 .1933 .1934 | .1917 .1916 .1933 .1932 | .2151 .2154 .2160 .2163 | .2151 .2156 .2160 .2165 | .2151 .2154 .2160 .2163 | .2151 .2156 .2160 .2165 |
| . $250-20$ | UNC | 14 2 A 3A | . 2399 .2394 .2399 .2394 .2410 .2405 | .2489 .2494 .2489 .2494 .2500 .2505 | .2164 .2163 .2164 .2163 .2175 .2174 | .2325 .2320 .2344 .2339 .2364 .2359 | .2483 .2488 .2489 .2494 .2500 .2505 | .2108 .2109 .2127 .2128 .2147 .2148 | .2108 .2107 .2127 .2126 .2147 .2146 | .2489 .2494 .2489 .2494 .2500 .2505 | .2489 .2494 .2489 .2494 .2500 .2505 | .2483 .2488 .2489 .2494 .2500 .2505 | .2483 .2488 .2489 .2494 .2500 .2505 |
| . $250-28$ | UNF | 14 24 3 A | .2419 .2414 .2419 .2414 .2429 .2424 | .2490 .2495 .2490 .2495 .2500 .2505 | .2258 .2257 .2258 .2257 .2268 .2267 | .2363 .2358 .2380 .2375 .2398 .2393 | .2476 .2481 .2490 .2495 .2500 .2505 | .2208 .2209 .2225 .2226 .2243 .2244 | .2208 .2207 .2225 .2224 .2243 .2242 | .2490 .2495 .2490 .2495 .2500 .2505 | .2490 .2495 .2490 .2495 .2506 .2595 | .2476 .2481 .2490 .2495 .2500 .2505 | .2476 .2481 .2490 .2495 .2500 .2505 |
| . 250-32 | UNEF | 2A 3 A | .2425 .2422 .2435 .2432 | .2490 .2493 .2500 .2503 | .2287 .2286 .2297 .2296 | .2390 .2387 .2408 .2405 | .2489 .2492 .2500 .2503 | .2255 .2256 .2273 .2274 | .2255 .2254 .2273 .2272 | .2490 .2493 .2500 .2503 | .2420 .2495 .2500 .2505 | .2489 .2492 .2500 .2503 | .2489 .2494 .2500 .2505 |
| . 3125-18 | UNC | 1 A 2 A 3 A | .3016 .3011 .3016 .3011 .3028 .3023 | .3113 .3118 .3113 .3118 .3125 .3130 | .2752 .2751 .2752 .2751 .2764 .2763 | .2932 .2927 .2953 .2948 .2975 .2970 | .3108 .3113 .3113 .3118 .3125 .3130 | .2691 .2692 .2712 .2713 .2734 .2735 | .2691 .2690 .2712 .2711 .2734 .2733 | .3113 .3118 .3113 .3118 .3125 .3130 | .3113 .318 .3113 .3118 .3125 .3130 | .3108 .3113 .3113 .3118 .3125 .3130 | .3108 .3113 .3113 .3118 .3125 .3130 |
| . 3125-20 | UN | 2 A 3 A | .3023 .3018 .3035 .3030 | .3113 .3118 .3125 .3130 | .2788 .2787 .2800 .2799 | .2965 .2960 .2987 .2982 | .3113 .3118 .3125 .3130 | .2748 .2749 .2770 .2771 | .2748 .2747 .2770 .2769 | .3113 .3118 .3125 .3130 | .3113 .3138 .3125 .3130 | .3113 .3118 .3125 .3130 | .3113 .3118 .3125 .3130 |
| . 3125-24 | UNF | 1 A 2A 3A | .3035 .3030 .3035 .3030 .3046 .3041 | .3114 .3119 .3114 .3119 .3125 .3130 | .2843 .2842 .2843 .2842 .2854 .2853 | .2968 .2963 .2986 .2981 .3007 .3002 | .3100 .3105 .3114 .3119 .3125 .3130 | .2788 .2789 .2806 .2807 .2827 .2828 | .2788 .2787 .2806 .2805 .2827 .2826 | .3114 .3119 .3114 .3119 .3125 .3130 | $\begin{array}{r} .3114 \\ .3119 \\ .3114 \\ .3119 \\ .3125 \\ .3130 \end{array}$ | .3100 .3105 .3114 .3119 .3125 .3130 | .3100 .3105 .3114 .3119 .3125 .3130 |
| . 3125-28 | UN | 2 A 3 A | .3044 .3039 .3054 .3049 | .3115 .3120 .3125 .3130 | .2883 .2882 .2893 .2892 | .3004 .2999 .3022 .3017 | $\begin{aligned} & .3115 \\ & .3120 \\ & .3125 \\ & .3130 \end{aligned}$ | $\begin{array}{r} .2849 \\ .2850 \\ .2867 \\ .2868 \end{array}$ | .2849 .2848 .2867 .2866 | .3115 .3120 .3125 .3130 | $\begin{array}{r} .3115 \\ .3120 \\ .3125 \\ .3130 \end{array}$ | .3115 .3120 .3125 .3130 | .3115 .3120 .3125 .3130 |
| . 3125-32 | UNEF | 2 A 3 A | .3050 .3047 .3060 .3057 | .3115 .3118 .3125 .3128 | .2912 .2911 .2922 .2921 | .3015 .3012 .3033 .3030 | .3114 .3117 .3125 .3128 | $\begin{array}{r} .2880 \\ .2881 \\ .2898 \\ .2899 \end{array}$ | $\begin{array}{r} .2880 \\ .2879 \\ .2898 \\ .2897 \end{array}$ | .3115 .3118 .3125 .3128 | $\begin{aligned} & .3115 \\ & .3120 \\ & .3125 \\ & .3130 \end{aligned}$ | $\begin{array}{r} .3114 \\ .3117 \\ .3125 \\ .3128 \end{array}$ | .3114 .3119 .3125 .3130 |
| . 375-16 | UNC | 1 A 2A 3A | .3632 .3626 .3632 .3626 .3645 .3639 | $\begin{array}{r} .3737 \\ .3743 \\ .3737 \\ .3743 \\ .3750 \\ .3756 \end{array}$ | $\begin{array}{r} .3331 \\ .3330 \\ .3331 \\ .3330 \\ .3344 \\ .3343 \end{array}$ | $\begin{aligned} & .3537 \\ & .3531 \\ & .3558 \\ & .3552 \\ & .3582 \\ & .3576 \end{aligned}$ | $\begin{array}{r} .3735 \\ .3741 \\ .3737 \\ .3743 \\ .3750 \\ .3756 \end{array}$ | $\begin{array}{r} .3266 \\ .3327 \\ .3287 \\ .3288 \\ .3311 \\ .3312 \end{array}$ | $\begin{array}{r} .3266 \\ .3265 \\ .3287 \\ .3286 \\ .3311 \\ .3310 \end{array}$ | $\begin{array}{r} .3737 \\ .3743 \\ .3737 \\ .3743 \\ .3759 \\ .3756 \end{array}$ | $\begin{array}{r} .3737 \\ .3774 \\ .3737 \\ .3737 \\ .3743 \\ .3750 \\ .3756 \end{array}$ | $\begin{array}{r} .3735 \\ .3741 \\ .3737 \\ .3743 \\ .3750 \\ .3756 \end{array}$ | .3735 .3741 .3737 .3743 .3750 .3756 |
| . $375-20$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | $\begin{array}{r} .3648 \\ .3643 \\ .3660 \\ .3655 \end{array}$ | $\begin{array}{r} .3738 \\ .3743 \\ .3750 \\ .3755 \end{array}$ | $\begin{array}{r} .3413 \\ .3412 \\ .3425 \\ .3424 \end{array}$ | $\begin{array}{r} .3589 \\ .3584 \\ .3611 \\ .3606 \end{array}$ | $\begin{array}{r} .3738 \\ .3743 \\ .3750 \\ .3755 \end{array}$ | $\begin{array}{r} .3372 \\ .3373 \\ .3394 \\ .3395 \end{array}$ | $\begin{array}{r} .3372 \\ .3371 \\ .3394 \\ .3393 \end{array}$ | $\begin{array}{r} .3738 \\ .3743 \\ .3750 \\ .3755 \end{array}$ | $\begin{array}{r} .373 .3 \\ .3743 \\ .3750 \\ .3755 \end{array}$ | $\begin{aligned} & .3738 \\ & .3743 \\ & .3750 \\ & .3755 \end{aligned}$ | .3738 .3743 .3750 .3755 |

See footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued

| Nominal size and threads per ineh | Series designation | Class | W truneated setting plugs |  |  |  |  |  |  | Basie-erest setting plugs |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Plug for GO thread gage ${ }^{\text {a }}$ |  |  | Plug for LO thread gage ${ }^{\text {a }}$ |  |  |  | Major diameter |  |  |  |
|  |  |  | Major diameter |  | Piteh diameter | Major diameter |  | Piteh diameter |  | Plug for GO thread gage a,b |  | Plug for LO thread gage ${ }^{\text {a,c }}$ |  |
|  |  |  | Truneated | Full |  | Truneated | Full | $\begin{aligned} & \text { Plus } \\ & \text { tolerance } \\ & \text { gage } \end{aligned}$ | Minus toleranee gage | $\begin{gathered} \mathrm{W} \\ \text { toleranee } \end{gathered}$ | $\underset{\text { tolerance }}{\mathrm{X}}$ | $\begin{gathered} \text { W } \\ \text { toleranee } \end{gathered}$ | X tolerance |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 A | 11 B | 12A | 1213 |
| .375-24 | UNF | 14 2 A 3A | in 0.3660 .3655 .3660 .3655 .3671 .3666 | $\begin{gathered} i n \\ 0.3739 \\ .3744 \\ .3739 \\ .3744 \\ .3750 \\ .3755 \end{gathered}$ | $\begin{gathered} i n \\ 0.3468 \\ .3467 \\ .3468 \\ .3467 \\ .3479 \\ .3478 \end{gathered}$ | $i n$ 0.3591 .3586 .3610 .3605 .3630 .3625 | in 0.3724 .3729 .3739 .3744 .3750 .3755 | in 0.3411 .3412 .3430 .3431 .3450 .3451 | $i n$ 0.3411 .3410 .3430 .3429 .3450 .3449 | in 0.3739 .3744 .3739 .374 .3750 .3755 | in 0.3739 .3744 .3739 .3744 .3750 .3755 | in 0.3724 .3729 .3739 .3744 .3750 .3755 | $\begin{aligned} & i n \\ & 0.3724 \\ & .3729 \\ & .3739 \\ & .3744 \\ & .3750 \\ & .3755 \end{aligned}$ |
| . 375-28 | UN | 2 A 3 A | .3668 .3663 .3679 .3674 | $\begin{array}{r} .3739 \\ .3744 \\ .3750 \\ .3755 \end{array}$ | $\begin{aligned} & .3507 \\ & .3506 \\ & .3518 \\ & .3517 \end{aligned}$ | .3626 .3621 .3646 .3641 | .3739 .3744 .3750 .3755 | .3471 .3472 .3491 .3492 | .3471 .3470 .3491 .3490 | .3739 .3744 .3750 .3755 | .3739 .3744 .3750 .3755 | .3739 .3744 .3750 .3755 | .3739 .3744 .3750 .3755 |
| .375-32 | UNEF | 2 A 3 A | .3675 .3672 .3685 .3682 | $\begin{array}{r} .3740 \\ .3743 \\ .3750 \\ .3753 \end{array}$ | .3537 .3536 .3547 .3546 | .3638 .3635 .3657 .3654 | .3737 .3740 .3750 .3753 | .3503 .3504 .3522 .3523 | .3503 .3502 .3522 .3521 | .3740 .3743 .3750 .3753 | .3740 .3745 .3750 .3755 | .3737 .3740 .3750 .3753 | .3737 .3742 .3750 .3755 |
| .4375-14 | UNC | 1 A 2A 3 A | .4246 .4240 .4246 .4240 .4260 .4254 | .4361 .4367 .4361 .4367 .4375 .4381 | .38970 .38955 .38970 .38955 .39110 .39095 | .4135 .4129 .4159 .4153 .4185 .4179 | .4361 .4367 .4361 .4367 .4375 .4381 | .38260 .38275 .38500 .38515 .38760 .38775 | .38260 .38245 .38500 .38485 .38760 .38745 | .4361 .4367 .4361 .4367 .4375 .4381 | .4361 .4367 .4361 .4367 .4375 .4381 | .4361 .4367 .4361 .4367 .4375 .4381 | .4361 .4367 .4361 .4367 .4375 .4381 |
| .4375-16 | UN | 2 A 3 A | .4256 .4250 .4270 .4264 | .4361 .4367 .4375 .4381 | .3955 .3954 .3969 .3968 | .4180 .4174 .4206 .4200 | .4361 .4367 .4375 .4381 | .3909 .3910 .3935 .3936 | .3909 .3908 .3935 .3934 | .4361 .4367 .4375 .4381 | .4361 .4367 .4375 .4381 | .4361 .4367 .4375 .4381 | .4361 .4367 .4375 .4381 |
| . 4375-20 | UNF' | 1 A 2 A 3 A | .4272 .4267 .4272 .4207 .4285 .4280 | $\begin{array}{r}.4362 \\ .4367 \\ .4362 \\ .4367 \\ .4375 \\ .4380 \\ \hline\end{array}$ | .4037 .4036 .4037 .4036 .4050 .4049 | .4191 .4186 .4212 .4207 .4236 .4231 | .4350 .4355 .4362 .4367 .4375 .4380 | .3974 .3975 .3995 .3996 .4019 .4020 | .3974 .3973 .3995 .3994 .4019 .4018 | .4362 .4367 .4362 .4367 .4375 .4380 | .4362 .4367 .4362 .4367 .4375 .4380 | .4350 .4355 .4362 .4367 .4375 .4380 | .4350 .4355 .4362 .4367 .4375 .4380 |
| .4375-28 | UNEF | 24 $3 A$ | .4293 .4288 .4304 .4299 | .4364 .4369 .4375 .4380 | .4132 .4131 .4143 .4142 | .4251 .4246 .4271 .4266 | .4364 .4369 .4375 .4380 | .4096 .4097 .4116 .4117 | .4096 .4095 .4116 .4115 | .4364 .4369 .4375 .4380 | .4364 .4369 .4375 .4380 | .4364 .4369 .4375 .4380 | .4364 .4369 .4375 .4380 |
| .4375-32 | UN | 2 A 3 A | .4300 .4297 .4310 .4307 | .4365 .4368 .4375 .4378 | .4162 .4161 .4172 .4171 | .4263 .4260 .4282 .4279 | .4362 .4365 .4375 .4378 | .4128 .4129 .4147 .4148 | .4128 .4127 .4147 .4146 | .4365 .4368 .4375 .4378 | .4365 .4370 .4375 .4380 | .4362 .4365 .4375 .4378 | .4362 .4367 .4375 .4380 |
| . $500-13$ | UNC | 1 A 2A 3A | .4863 .4857 .4863 .4857 .4878 .4872 | .4985 .4991 .4985 .4991 .5000 .5006 | $\begin{array}{r} .44850 \\ .44835 \\ .44850 \\ .44835 \\ .45000 \\ .44985 \end{array}$ | .4744 .4738 .4768 .4762 .4796 .4790 | .4985 .4991 .4985 .4991 .5000 .5006 | $\begin{aligned} & .44110 \\ & .44125 \\ & .44350 \\ & .44365 \\ & .44630 \\ & .44645 \end{aligned}$ | $\begin{array}{r} .44110 \\ .44095 \\ .44350 \\ .44335 \\ .44630 \\ .44615 \end{array}$ | .4985 .4991 .4985 .4991 .5000 .5006 | .4985 .4991 .4985 .4991 .5000 .5006 | .4985 .4991 .4985 .4991 .5000 .5006 | .4985 .4991 .4985 .4991 .5000 .5006 |
| . $500-16$ | UN | 2 A 3 A | ( 4881 .4875 .4895 .4889 | $\begin{array}{r} .4986 \\ .4992 \\ .5000 \\ .5006 \end{array}$ | $\begin{array}{r} .4580 \\ .4579 \\ .4594 \\ .4593 \end{array}$ | $\begin{aligned} & .4804 \\ & .4798 \\ & .4830 \\ & .4824 \end{aligned}$ | $\begin{array}{r} .4986 \\ .4992 \\ .5000 \\ .5006 \end{array}$ | .4533 .4534 .4559 .4560 | .4533 .4532 .4559 .4558 | .4986 .4992 .5000 .5006 | $\begin{array}{r} .4986 \\ .4992 \\ .5000 \\ .5006 \end{array}$ | .4986 .4992 .5000 .5006 | .4986 .4992 .5000 .5006 |
| . $500-20$ | UNF | 1 A 2A 3A | .4897 .4892 .4897 .4892 .4910 .4905 | .4987 .4992 .4987 .4992 .5000 .5005 | .4662 .4661 .4662 .4661 .4675 .4674 | $\begin{array}{r} .4815 \\ .4810 \\ .4836 \\ .4831 \\ .4860 \\ .4855 \end{array}$ | $\begin{array}{r} .4973 \\ .4978 \\ .4987 \\ .4992 \\ .5000 \\ .5005 \end{array}$ | .4598 .4599 .4619 .4620 .4643 .4644 | $\begin{array}{r} .4598 \\ .4597 \\ .4619 \\ .4618 \\ .4643 \\ .4642 \end{array}$ | .4987 .4992 .4987 .4992 .5000 .5005 | $\begin{array}{r} .4987 \\ .4992 \\ .4987 \\ .4992 \\ .5000 \\ .5005 \end{array}$ | .4973 .4978 .4987 .4992 .5000 .5005 | .4973 .4978 .4987 .4992 .5000 .5005 |
| . $500-28$ | UNEF | 2 A 3 A | .4918 .4913 .4929 .4924 | .4989 .4994 .5000 .5005 | .4757 .4756 .4768 .4767 | $\begin{array}{r} .4875 \\ .4870 \\ .4895 \\ .4890 \end{array}$ | $\begin{array}{r} .4988 \\ .4993 \\ .5000 \\ .5005 \end{array}$ | $\begin{array}{r} .4720 \\ .4721 \\ .4740 \\ .4741 \end{array}$ | $\begin{array}{r} .4720 \\ .4719 \\ .4740 \\ .4739 \end{array}$ | $\begin{array}{r} .4989 \\ .4994 \\ .5000 \\ .5005 \end{array}$ | $\begin{array}{r} .4989 \\ .4994 \\ .5000 \\ .5005 \end{array}$ | $\begin{array}{r} .4988 \\ .4993 \\ .5000 \\ .5005 \end{array}$ | . 4988 <br> . 4993 <br> . 5000 <br> . 5005 |
| . $500-32$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | .4925 .4922 .4935 .4932 | $\begin{array}{r} .4990 \\ .4993 \\ .5000 \\ .5003 \end{array}$ | $\begin{array}{r} .4787 \\ .4786 \\ .4797 \\ .4796 \end{array}$ | $\begin{array}{r} .4887 \\ .4884 \\ .4906 \\ .4903 \end{array}$ | $\begin{array}{r} .4986 \\ .4989 \\ .5000 \\ .5003 \end{array}$ | $\begin{array}{r} .4752 \\ .4753 \\ .4771 \\ .4772 \end{array}$ | $\begin{array}{r} .4752 \\ .4751 \\ .4771 \\ .4770 \end{array}$ | .4990 <br> . 4993 <br> . 5000 <br> . 5003 | $\begin{array}{r} .4990 \\ .4995 \\ .5000 \\ .5005 \end{array}$ | $\begin{array}{r} .4986 \\ .4989 \\ .5000 \\ .5003 \end{array}$ | . 4986 <br> . 4991 <br> . 5000 <br> . 5005 |

See footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued


See footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued


See footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued


Sce footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued


See footnotes at end of table.

Table 6.20. Setting plug gages, Unified serew threads-Continued

| Nominal size and threads per inch | Series designation | Class | W truncated setting plugs |  |  |  |  |  |  | $\frac{\text { Basic-crest setting plugs }}{\text { Major diameter }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Plug for GO thread gage ${ }^{\text {a }}$ |  |  | Plug for LO thread gage ${ }^{3}$ |  |  |  |  |  |
|  |  |  | Major diameter |  | Pitch diameter | Major diameter |  | Pitch diameter |  | Plug for GO thread gage ${ }^{\text {a,b }}$ | Plug for LO thread gage a.c |
|  |  |  | Truncated | Full |  | Truncated | Full | Plus tolerance gage | Minus tolerance gage | W and X tolcrances | W and X tolerances |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 1. 125-16 | UN | 24$3 A$ |  |  |  |  |  | in |  |  | in |
|  |  |  | 1. 1130 | 1.1235 | 1. 0829 | 1. 1050 | 1. 1235 | 1. 0779 | 1. 0779 | 1.1235 | 1. 1235 |
|  |  |  | 1.1124 | 1.1241 1.1250 | 1. 1.08274 | 1.1044 1.1078 | 1.1241 | 1. 0781 1.0807 | 1.0777 | 1.1241 1.1250 | 1. 121241 |
|  |  |  | 1. 1139 | 1. 1256 | 1.0842 | 1. 1072 | 1. 1256 | 1. 0809 | 1. 0805 | 1. 1256 | 1.1256 |
| 1. 125-18 | UNEF | 2A | 1.1139 | 1.1236 | 1.08750 | 1. 1069 | 1. 1236 | 1. 08280 | 1. 08280 | 1.1236 | 1. 1236 |
|  |  | $3 \mathrm{~A}$ | 1. 1134 | 1. 1241 | 1. 08735 | 1. 1064 | 1. 1241 | 1. 08295 | 1. 08265 | 1.1241 | 1.1241 |
|  |  |  | 1.1153 1 | 1.1250 | 1. 088890 | 1. 1094 | 1. 1250 | 1. 08530 | 1. 085330 | 1.1250 | 1.1250 |
| 1. 125-20 | UN | 2A | 1.1146 | 1. 1236 | 1. 09110 | 1. 1083 | 1. 1236 | 1.08660 | 1. 08660 | 1. 1236 | 1.1236 |
|  |  | $3 \mathrm{~A}$ | 1.1141 | 1. 1241 | 1. 09095 | 1.1078 | 1. 1241 | 1. 08675 | 1.08645 | 1. 1241 | 1. 1241 |
|  |  |  | 1.1160 | 1.1250 | 1.09250 | 1. 1108 | 1. 1250 | 1.08910 | 1.08910 | 1. 1250 | 1. 1250 |
|  |  |  | 1.1155 | 1.1255 | 1. 09235 | 1.1103 | 1. 1255 | 1.08925 | 1.08895 | 1. 1255 | 1.1255 |
| 1. 125-28 | UN | 2A | 1. 1167 | 1.1238 | 1. 10060 | 1.1121 | 1. 1234 | 1. 09660 | 1. 09660 | 1. 1238 | 1. 1234 |
|  |  | 3A | 1. 1162 | 1. 1243 | 1. 10045 | 1. 1116 | 1. 1239 | 1.09675 | 1. 09645 | 1. 1243 | 1. 1239 |
|  |  |  | 1.1179 1.1174 | 1.1250 | 1. 10180 | 1.1143 1.1138 | 1. 121250 | 1.09880 1.09895 | 1.09880 1.09865 | 1.1250 1.1255 | 1.1250 1.1255 |
| 1. 1875-8 | UN | 2 A | 1.1683 | 1. 1854 | 1. 1042 | 1.1513 | 1. 1854 | 1. 0972 | 1.0972 | 1. 1854 | 1. 1854 |
|  |  |  | 1. 1676 | 1. 1861 | 1. 1040 | 1. 1506 | 1. 1861 | 1. 0974 | 1. 0970 | 1. 1861 | 1. 1861 |
|  |  | 3A | 1.1704 | 1.1875 | 1. 1063 | 1. 1552 | 1. 1875 | 1. 1011 | 1. 1011 | 1. 1875 | 1. 1875 |
|  |  |  | 1. 1697 | 1. 1882 | 1. 1061 | 1.1545 | 1. 1882 | 1. 1013 | 1. 1009 | 1. 1882 | 1.1882 |
| 1. 1875-12 | UN | 2A | 1. 1729 | 1. 1858 | 1. 1317 | 1. 1620 | 1. 1858 | 1. 1259 | 1. 1259 | 1. 1858 | 1. 1858 |
|  |  |  | 1.1723 | 1. 1864 | 1. 1315 | 1. 1614 | 1. 1864 | 1. 1261 | 1. 1257 | 1. 1864 | 1. 1864 |
|  |  | 3A | 1.1746 | 1. 1875 | 1. 1334 | 1. 1652 | 1. 1875 | 1. 1291 | 1. 1291 | 1. 1875 | 1. 1875 |
|  |  |  | 1.1740 | 1. 1881 | 1. 1332 | 1.1646 | 1. 1881 | 1. 1293 | 1. 1289 | 1. 1881 | 1. 1881 |
| 1. 1875-16 | UN | 2A | 1. 1755 | 1. 1860 | 1. 1454 | 1.1674 | 1. 1860 | 1. 1403 | 1.1403 | 1. 1860 | 1. 1860 |
|  |  |  | 1. 1749 | 1. 1866 | 1. 1452 | 1. 1668 | 1. 1866 | 1. 1405 | 1.1401 | 1. 1866 | 1. 1866 |
|  |  | 3 A | 1. 1770 | 1.1875 | 1. 1469 | 1. 1702 | 1.1875 | 1.1431 | 1.1431 | 1.1875 | 1. 1875 |
|  |  |  | 1. 1764 | 1. 1881 | 1. 1467 | 1.1696 | 1. 1881 | 1. 1433 | 1. 1429 | 1.1881 | 1.1881 |
| 1.1875-18 | UNEF | 2A | 1.1763 | 1. 1860 | 1. 14990 | 1. 1691 | 1. 1860 | 1. 14500 | 1. 14500 | 1.1860 | 1. 1860 |
|  |  |  | 1. 1758 | 1. 1865 | 1. 14975 | 1. 1686 | 1. 1865 | 1. 14515 | 1. 14485 | 1. 1865 | 1. 1865 |
|  |  | 3A | 1.1778 1.1773 | 1.1875 | 1. 15140 1.15125 | 1.1719 1.1714 | 1.1875 1.1880 | 1. 14780 1.14795 | 1.14780 1.14765 | 1.1875 1.1880 | 1. 1875 |
| 1.1875-20 | UN | 2A | 1. 1771 | 1. 1861 | 1. 15360 | 1.1706 | 1. 1861 | 1.14890 | 1. 14890 | 1.1861 | 1. 1861 |
|  |  |  | 1.1766 | 1. 1866 | 1.15345 | 1.1701 | 1. 1866 | 1. 14905 | 1.14875 | 1.1866 | 1. 1866 |
|  |  | 3A | 1.1785 | 1. 1875 | 1. 15500 | 1.1732 | 1. 1875 | 1. 15150 | 1.15150 | 1. 1875 | 1. 1875 |
|  |  |  | 1. 1780 | 1. 1880 | 1. 15485 | 1.1727 | 1. 1880 | 1. 15165 | 1. 15135 | 1. 1880 | 1. 1880 |
| 1.1875-28 | UN | 2A | 1. 1792 | 1. 1863 | 1. 16310 | 1. 1745 | 1. 1858 | 1. 15900 | 1. 15900 | 1.1863 | 1. 1858 |
|  |  |  | 1.1787 | 1. 1868 | 1. 16295 | 1. 1740 | 1. 1863 | 1. 15915 | 1.15885 | 1.1868 | 1. 1863 |
|  |  | 3A | 1. 1804 1.1799 | 1. 1875 1.1880 | 1. 16430 1.16415 | 1. 1767 1.1762 | 1. 1875 | 1. 16120 1. 16135 | 1. 1.16120 1.16105 | 1.1875 1.1880 | 1. 1875 |
| 1. 250-7 | UNC | 1A | 1. 2290 | 1. 2478 | 1. 1550 | 1. 2058 | 1. 2478 | 1. 1439 | 1. 1439 | 1. 2478 | 1.2478 |
|  |  |  | 1. 2283 | 1. 2485 | 1. 1548 | 1. 2051 | 1. 2485 | 1.1441 | 1. 1437 | 1.2485 | 1. 2485 |
|  |  | 2 A | 1. 2290 | 1. 2478 | 1. 1550 | 1. 2095 | 1.2478 | 1.1476 | 1. 1476 | 1. 2478 | 1. 2478 |
|  |  |  | 1. 2283 | 1. 2485 | 1.1548 | 1. 2088 | 1. 2485 | 1. 1478 | 1. 1474 | 1.2485 | 1. 2485 |
|  |  | 3 A | 1. 2312 | 1. 2500 | 1. 1572 | 1. 2136 | 1. 2500 | 1. 1517 | 1.1517 | 1.2500 | 1. 2500 |
|  |  |  | 1. 2305 | 1. 2507 | 1.1570 | 1. 2129 | 1. 2507 | 1. 1519 | 1. 1515 | 1. 2507 | 1. 2507 |
| 1. 250-8 | UN | 2A | 1. 2308 | 1. 2479 | 1. 1667 | 1. 2138 | 1. 2479 | 1. 1597 | 1. 1597 | 1. 2479 | 1. 2479 |
|  |  |  | 1. 2301 | 1. 2486 | 1. 1665 | 1. 2131 | 1. 2486 | 1. 1599 | 1. 1595 | 1. 2486 | 1. 2486 |
|  |  | 3 A | 1. 2329 | 1. 2500 | 1. 1688 | 1. 2176 | 1. 2500 | 1. 1635 | 1. 1635 | 1. 2500 | 1. 25500 |
|  |  |  | 1. 2322 | 1. 2507 | 1. 1686 | 1. 2169 | 1. 2507 | 1. 1637 | 1. 1633 | 1. 2507 | 1.2507 |
| 1. $250-12$ | UNF | 1A | 1. 2353 | 1. 2482 | 1. 1941 | 1. 2210 | 1. 2474 | 1.1849 | 1. 1849 | 1. 2482 | 1. 2474 |
|  |  |  | 1. 2347 | 1. 2488 | 1. 1939 | 1. 2204 | 1. 2480 | 1. 1851 | 1. 1847 | 1. 2488 | 1. 2480 |
|  |  | 2A | 1. 2353 | 1. 2482 | 1. 1941 | 1. 2240 | 1. 2482 | 1. 1879 | 1. 1879 | 1.2482 | 1. 2482 |
|  |  |  | 1.2347 | 1. 2488 | 1.1939 | 1. 2234 | 1. 2488 | 1. 1881 | 1.1877 | 1. 2488 | 1. 2488 |
|  |  | 3A | 1. 2371 | 1. 2500 | 1. 1959 | 1. 2274 | 1. 2500 | 1. 1913 | 1. 1913 | 1. 2500 | 1. 2500 |
|  |  |  | 1. 2365 | 1. 2506 | 1. 1957 | 1. 2268 | 1. 2506 | 1.1915 | 1. 1911 | 1. 2506 | 1. 2506 |
| 1. $250-16$ | UN | 2A | 1. 2380 | 1. 2485 | 1. 2079 | 1. 2299 | 1. 2485 | 1. 2028 | 1. 2028 | 1. 2485 | 1. 2485 |
|  |  |  | 1. 2374 | 1. 2491 | 1. 2077 | 1. 2293 | 1.2491 | 1. 2030 | 1. 2026 | 1. 2491 | 1. 2491 |
|  |  | 3 A | 1. 2395 | 1. 2500 | 1. 2094 | 1. 2327 | 1. 2500 | 1. 2056 | 1. 2056 | 1. 2500 | 1. 2500 |
|  |  |  | 1. 2389 | 1. 2506 | 1. 2092 | 1. 2321 | 1. 2506 | 1. 2058 | 1. 2054 | 1. 2506 | 1.2506 |
| 1. $250-18$ | UNEF | 2 A | 1. 2388 | 1. 2485 | 1. 21240 | 1. 2316 | 1. 2485 | 1. 20750 | 1. 20750 | 1. 2485 | 1. 2485 |
|  |  |  | 1. 2383 | 1. 2490 | 1.21225 | 1. 2311 | 1. 2490 | 1. 20765 | 1. 20735 | 1. 2490 | 1. 2490 |
|  |  | 3A | 1.2403 | 1. 2500 | 1. 21390 | 1. 2344 | 1. 2500 | 1.21030 | 1. 2121030 | 1. 2500 | 1. 2500 1.2505 |
|  |  |  | 1. 2398 | 1. 2505 | 1. 21375 | 1. 2339 | 1. 2505 | 1. 21045 | 1. 21015 | 1. 2505 | 1. 2505 |

See footnotes at end of table.


See footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued

| Nominal size and threads per ineh | Series designation | Class | W truncated setting plugs |  |  |  |  |  |  | $\frac{\text { Basic-erest setting plugs }}{\text { Major diameter }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Plug for GO thread gage a |  |  | Plug for LO thread gage ${ }^{\text {a }}$ |  |  |  |  |  |
|  |  |  | Major diameter |  | Piteh diameter | Major diameter |  | Piteh diameter |  | Plug for GO thread gage ${ }^{\text {a,b }}$ | Plug for LO thread gage ${ }^{a, c}$ |
|  |  |  | Truneated | Full |  | Truneated | Full | Plus toleranee gage | Minus tolerance gage | W and X toleranees | W and X tolerances |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 1.4375-8 | UN | 2A | in in |  | in 1.3541 | in 1.4010 | in 1.4353 | 1.3469 | in | in 1.4353 | ${ }^{\text {in }}$ 1. 4353 |
|  |  |  | 1. 4182 | 1. 4353 |  |  |  |  | 1. 3469 |  |  |
|  |  |  | 1.4175 | 1. 4360 | 1. 3539 | 1. 4003 | 1.4360 | 1. 3471 | 1. 3467 | 1. 4360 | 1. 4360 |
|  |  | 3A | 1. 4204 | 1. 4375 | 1. 3563 | 1. 4050 | 1.4375 | 1. 3509 | 1. 3509 | 1. 4375 | 1. 4375 |
|  |  |  | 1.4197 | 1. 4382 | 1.3561 | 1. 4043 | 1. 4382 | 1. 3511 | 1. 3507 | 1. 4382 | 1. 4382 |
| 1.4375-12 | UN | 24$3 A$ | 1. 4228 | 1.4357 | 1. 3816 | 1. 4118 | 1. 4357 | 1. 3757 | 1. 3757 | 1. 4357 | 1. 4357 |
|  |  |  | 1.4222 | 1. 4363 | 1. 3814 | 1. 4112 | 1. 4363 | 1. 3759 | 1.3755 | 1. 4363 | 1. 4363 |
|  |  |  | 1. 424246 | 1.4375 | 1. 3834 | 1.4151 | 1. 4375 | 1. 3790 | 1. 3790 | 1. 4375 | 1. 4373 |
| 1. 4375-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | 1. 4254 | 1.4359 | 1. 3953 | 1. 4172 | 1. 4359 | 1. 3901 | 1. 3901 | 1. 4359 | 1. 4359 |
|  |  |  | 1. 4248 | 1. 4365 | 1. 3951 | 1. 4166 | 1. 4365 | 1.3903 | 1.3899 | 1. 4365 | 1.4365 |
|  |  |  | 1.4270 | 1.4375 1.4381 | 1. 3969 1.3967 | 1.4201 1.4195 | 1.4375 1.4381 | 1.3930 | 1.3930 1.3928 | 1. 1.4375 1.4381 | 1. 4375 1.4381 |
| 1. 4375-18 | UNEF | 24$3 A$ | 1. 4263 | 1. 4360 | 1. 39990 | 1.4190 | 1. 4360 | 1. 39490 | 1. 39490 | 1. 4360 | 1. 4360 |
|  |  |  | 1. 4258 | 1. 4365 | 1. 39975 | 1.4185 | 1. 4365 | 1. 39505 | 1. 39475 | 1. 4365 | 1. 4365 |
|  |  |  | 1.4278 1.4273 | 1.4375 1.4380 | 1.40140 1.40125 | 1.4218 1.4213 | 1.4375 1.4380 | 1. 39770 1.39785 | 1.39770 1.39755 | 1. 1.4375 | 1.4375 1.4380 |
| 1.4375-20 | UN | 2A | 1. 4271 | 1. 4361 | 1.40360 | 1. 4205 | 1. 4361 | 1. 39880 | 1. 39880 | 1. 4361 | 1.4361 |
|  |  |  | 1. 4266 | 1. 4366 | 1.40345 | 1. 4200 | 1. 4366 | 1.39895 | 1. 39865 | 1. 4366 | 1. 4386 |
|  |  |  | 1.4285 1.4280 | 1. 4375 1.4380 | 1.40500 1.40485 | 1.4231 1.4226 | 1.4375 1.4380 | 1.40140 | 1.40140 1.40125 | 1. 4375 1.4380 | 1.4375 1.4380 |
| 1. 4375-28 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | 1.4291 | 1. 4362 | 1. 41300 | 1. 4243 | 1.4356 | 1. 40880 | 1. 40880 | 1. 4362 | 1.4356 |
|  |  |  | 1. 4286 | 1. 4367 | 1.41285 | 1. 4238 | 1. 4361 | 1. 40895 | 1. 40865 | 1. 4367 | 1. 4361 |
|  |  |  | 1.4304 | 1. 4375 | 1. 41430 | 1. 4267 | 1. 4375 | 1.41120 | 1.41120 | 1.4375 | 1. 4375 |
|  |  |  | 1. 4299 | 1. 4380 | 1. 41415 | 1. 4262 | 1. 4380 | 1. 41135 | 1.41105 | 1. 4380 | 1. 4380 |
| 1. 500-6 | UNC | 1A | 1. 4766 | 1. 4976 | 1.3893 | 1. 4494 | 1. 4976 | 1. 3772 | 1.3772 | 1.4976 | 1. 4976 |
|  |  |  | 1. 14758 | 1. 4984 | 1. 3891 | 1. 4486 | 1. 4984 | 1. 3774 | 1. 3770 | 1. 4984 | 1. 4984 |
|  |  | 2 A | 1.4766 1 | 1. 4976 | 1. 3893 | 1. 4534 | 1. 4976 | 1. 3812 | 1. 3812 | 1. 4976 | 1. 4976 |
|  |  |  | 1.4758 1.4790 | 1. 4984 | 1. 3891 | 1.4526 1.4578 1.4 | 1. 4984 | 1. 3814 | 1. 3810 | 1.4984 1 1.5000 | 1. 4984 |
|  |  | 3A | 1.4790 1.4782 | 1. 5000 1.5008 | 1. 3917 | 1.4578 1.4570 | 1. 5000 1.5008 | 1. 3856 | 1.3856 1.3854 | 1.5000 1.5008 | 1. 5000 |
| 1. $500-8$ | UN | 2 A | 1. 4807 | 1.4978 | 1. 4166 | 1. 4634 | 1.4978 | 1. 4093 | 1. 4093 | 1. 4978 | 1. 4978 |
|  |  |  | 1. 4800 | 1. 4985 | 1. 4164 | 1. 4627 | 1. 4985 | 1. 4095 | 1. 4091 | 1. 4985 | 1. 4985 |
|  |  | 3A | 1.4829 1.4822 | 1. 5000 | 1. 1.4188 | 1.4674 1.4667 | 1. 5000 1.5007 | 1.4133 1.4135 | 1.4133 | 1. 5000 | 1. 5000 |
| 1. $500-12$ | UNF | 1A | 1. 4852 | 1. 4981 | 1. 4440 | 1. 4705 | 1. 4969 | 1. 4344 | 1. 4344 | 1. 4981 | 1. 4969 |
|  |  |  | 1. 4846 | 1. 4987 | 1. 4438 | 1. 4699 | 1. 4975 | 1. 4346 | 1. 4342 | 1.4987 | 1. 4975 |
|  |  | 2 A | 1. 4852 | 1.4981 | 1. 4440 | 1.4737 | 1.4981 | 1. 4376 | 1. 4376 | 1. 4981 | 1. 4981 |
|  |  |  | 1. 4846 | 1. 4987 | 1. 4438 | 1. 4731 | 1. 4987 | 1. 4378 | 1. 4374 | 1. 4987 | 1. 4987 |
|  |  | 3A | 1. 18871 | 1. 5000 | 1. 1.4459 | 1. 4772 1.4766 | 1. 5000 | 1.4411 | 1. 44411 | 1. 1.5000 | 1. 1.50006 |
|  |  |  | 1. 4865 | 1. 5006 | 1. 4457 | 1. 4766 | 1. 5006 | 1. 4413 | 1.4409 | 1.5006 | 1. 5006 |
| 1. $500-16$ | UN | 2 A | 1. 4879 | 1. 4984 | 1. 4578 | 1. 4797 | 1. 4984 | 1. 4526 | 1.4526 | 1. 4984 | 1. 4984 |
|  |  |  | 1. 4873 | 1. 4990 | 1. 4576 | 1. 4791 | 1. 4990 | 1. 4528 | 1. 4524 | 1. 4990 | 1. 4990 |
|  |  | 3 A | 1.4895 | 1. 5000 | 1. 4594 | 1. 4826 1.4820 | 1. 5000 | 1. 1.4555 | 1.4555 | 1. 5000 | 1. 5000 |
| 1. $500-18$ | UNEF | 2 A | 1. 4888 | 1.4985 | 1. 46240 | 1.4815 | 1. 4984 | 1. 45740 | 1.45740 | 1. 4985 | 1. 4985 |
|  |  |  | 1. 4883 | 1. 4990 | 1. 46225 | 1. 4810 | 1. 4990 | 1. 45755 | 1.45725 | 1. 4990 | 1. 4990 |
|  |  | 3 A | 1. 4903 | 1. 5000 | 1. 46390 | 1. 4843 | 1. 5000 | 1. 46020 | 1. 46020 | 1. 5000 | 1. 5000 |
|  |  |  | 1. 4898 | 1. 5005 | 1.46375 | 1. 4838 | 1. 5005 | 1.46035 | 1.46005 | 1. 5005 | 1. 5005 |
| 1. $500-20$ | UN | 2 A | 1. 4896 | 1.4986 | 1. 45610 | 1. 4830 | 1. 4986 | 1. 46130 | 1. 46130 | 1. 4986 | 1. 4986 |
|  |  |  | 1. 4891 | 1. 4991 | 1.46595 | 1. 4825 | 1.4991 | 1. 46145 | 1. 46115 | 1. 4991 | 1. 4991 |
|  |  | 3A | 1. 4910 | 1. 5000 | 1.46750 1.46735 | 1. 48585 | 1. 50000 | 1.46390 1.46405 | 1.46390 1.46375 | 1. 5000 | 1. 5000 1.5005 |
| 1. $500-28$ | UN | 2 A | 1.4916 | 1. 4987 | 1.47550 | 1. 4868 | 1. 4981 | 1. 47130 | 1. 47130 | 1. 4987 | 1. 4981 |
|  |  |  | 1. 4911 | 1. 4992 | 1.47535 | 1.4863 | 1. 4986 | 1. 47.145 | 1. 47115 | 1. 4992 | 1. 4986 |
|  |  | 3A | 1. 4929 | 1. 5000 | 1. 47680 | 1. 4892 | 1. 5000 | 1. 47370 | 1. 47370 | 1. 5000 | 1. 5000 |
|  |  |  | 1. 4924 | 1. 5005 | 1.47665 | 1. 4887 | 1. 5005 | 1. 47385 | 1. 47355 | 1. 5005 | 1. 5005 |
| 1. 5625-6 | UN | 2 A | 1. 5391 | 1. 5601 | 1. 45180 | 1. 5158 | 1. 5601 | 1. 44360 | 1. 44360 | 1. 5601 | 1. 5601 |
|  |  |  | 1. 5383 | 1. 5609 | 1. 45155 | 1. 5150 | 1. 5609 | 1. 44385 | 1. 44335 | 1. 5609 | 1. 5609 |
|  |  | 3 A | 1. 5415 | 1. 5625 | 1. 45420 | 1. 5203 | 1. 5625 | 1. 44810 | 1. 44810 | 1. 5625 | 1. 5625 |
|  |  |  | 1. 5407 | 1. 5633 | 1.45395 | 1. 5195 | 1. 5633 | 1. 44835 | 1. 44785 | 1. 5633 | 1. 5633 |
| 1. 5625-8 | UN | 2A | 1. 5432 | 1. 5603 | 1. 47910 | 1. 5258 | 1. 5603 | 1. 47170 | 1. 47170 | 1. 5603 | 1. 5603 |
|  |  |  | 1. 5425 | 1. 5610 | 1. 47885 | 1. 5251 | 1. 5610 | 1.47195 | 1. 47145 | 1. 5610 | 1. 5610 |
|  |  | 3A | 1. 5454 | 1. 5625 | 1. 48130 | 1. 5299 | 1. 5625 | 1. 47580 | 1. 47580 | 1. 5625 | 1. 5625 |
|  |  |  | 1. 5447 | 1. 5632 | 1. 48105 | 1. 5292 | 1. 5632 | 1. 47605 | 1.47555 | 1. 5632 | 1. 5632 |

See footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued


See footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued

| Nominal size and threads per ineh | Series designation | Class | W truneated setting plugs |  |  |  |  |  |  | $\frac{\text { Basie-erestsettingplugs }}{\text { Major diameter }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Plug for GO thread gage ${ }^{\text {a }}$ |  |  | Plug for Lo thread gage ${ }^{\text {a }}$ |  |  |  |  |  |
|  |  |  | Major diameter |  | Piteh diameter | Major diameter |  | Piteh diameter |  | Plug for QO thread gage ${ }^{a, b}$ | Plug for LO thread gage ${ }^{a, c}$ |
|  |  |  | Truneated | Full |  | Truneated | Full | Plus tolerance gage | Minus tolerance gage | W and X tolerances | W and X toleranees |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 1.750-5 | UNC | 1A | in | in | in | in | $\mathrm{in}_{1.7473}$ |  | in |  | in |
|  |  |  | $1.7234-1.7473$ |  | 1. 61740 | 1. 6906 |  | 1. 60400 | in 1.60400 | 1. 7473 | $\begin{array}{r} 1.7473 \\ \text { 1. } 7481 \end{array}$ |
|  |  |  | 1. 1.7226 | 1.7481 | 1. 61715 | 1. 68981.6951 | 1. 7481 | 1. 604251.60850 | 1.60375 | 1. 7473 |  |
|  |  | 2 A |  | 1. 7473 | 1. 61740 |  | 1. 7473 |  |  |  | $\begin{aligned} & 1.7473 \\ & 1.7481 \end{aligned}$ |
|  |  |  | 1. 7226 | 1.7481 | 1. 61715 | 1. 6943 | 1. 7481 | 1. 60875 | 1. 60825 | 1. 7481 |  |
|  |  | 3A | $\begin{aligned} & 1.7261 \\ & 1.7253 \end{aligned}$ | 1. 7500 <br> 1. 7508 | 1.620101.61985 | 1. 70001.6992 | $\begin{aligned} & 1.7500 \\ & 1.7508 \end{aligned}$ | 1.613401.61365 | $\begin{aligned} & 1.61340 \\ & 1.61315 \end{aligned}$ | $\begin{aligned} & 1.7500 \\ & 1.7508 \end{aligned}$ | 1. 75001. 7508 |
|  |  |  |  |  |  |  |  |  |  |  |  |
| 1. 750-6 | UN | 2 A | 1.7265 <br> 1. 7257 <br> 1. 7290 | $\begin{aligned} & 1.7475 \\ & 1.7483 \\ & 1.7500 \\ & 1.7508 \end{aligned}$ | 1. 63920 | 1. 7031 | 1.7475 | 1.63090 | 1. 63090 <br> 1. 63065 | 1. 7475 | 1.74751.7483 |
|  |  |  |  |  | 1.63895 | 1. 7023 | 1.7483 | 1. 63115 |  |  |  |
|  |  | 3A. |  |  | 1.64170 1.64145 | 1. 7076 <br> 1. 7068 | 1.7500 1.7508 | 1. 1.63565 | 1. 1.63515 | 1. 7508 | 1. 17508 |
| 1.750-8 | UN | 2A | $\begin{aligned} & \text { 1. } 7306 \\ & \text { 1. } 7299 \\ & \text { 1.7329 } \\ & 1.7322 \end{aligned}$ | 1. 7477 | 1. 66650 | 1. 7131 | 1.7477 | 1.65900 | 1.65900 | 1. 7477 | 1. 74771. 7484 |
|  |  |  |  | 1.7484 | 1. 66625 | 1.7124 | 1. 7484 | 1. 65925 | 1. 65875 | 1. 7484 |  |
|  |  | 3A |  | $\begin{aligned} & 1.7500 \\ & 1.7507 \end{aligned}$ | 1. 66880 <br> 1. 66855 | 1.71721.7165 | 1.75001.7507 | 1. 1.66310 | 1. 66310 <br> 1. 66285 | 1. 7500 | 1.7500 |
|  |  |  |  |  |  |  |  |  |  | 1.7507 |  |
| 1. 750-12 | UN | 2A | 1. 7353 <br> 1. 7347 <br> 1. 7371 | 1. 7482 1. 7488 1. 7500 1.750 f |  | $\begin{aligned} & 1.7242 \\ & 1.7236 \\ & 1.7275 \\ & 1.7269 \end{aligned}$ |  | 1. 68810 | 1.68810 | 1. 7482 | $\begin{aligned} & 1.7482 \\ & 1.7488 \\ & 1.7509 \\ & 1.7500 \end{aligned}$ |
|  |  | 3A |  |  |  |  |  | 1. 688835 | 1.68785 1.69140 | 1.7488 <br> 1.7500 |  |
|  |  |  |  |  |  |  |  | 1. 69165 | 1.69115 | 1. 7506 |  |
| 1.750-16 | UN | 2 A3 A | $\begin{aligned} & \text { 1. } 7379 \\ & \text { 1. } 7373 \\ & \text { 1.7395 } \\ & 1.7389 \end{aligned}$ |  |  | 1. 7296 1. 7290 <br> 1. 7325 | 1. 7484 1. 7490 <br> 1. 7500 <br> 1. 7506 | $\begin{aligned} & 1.70250 \\ & 1.70275 \\ & 1.70540 \\ & \text { 1. } 70565 \end{aligned}$ | $\begin{aligned} & 1.70250 \\ & 1.70225 \\ & 1.70540 \\ & 1.70515 \end{aligned}$ | 1. 74841. 74901. 75001. 7506 | 1. 7484 <br> 1. 7490 <br> 1. 7500 <br> 1. 7506 |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |
| 1. $750-20$ | UN | 2A | 1. 73951. 7390 1. 7410 |  | $\begin{aligned} & 1.7160 \\ & 1.7158 \\ & 1.7175 \end{aligned}$ | 1. 7329 <br> 1. 7324 1. 7356 | 1. 7485 <br> 1. 7500 | $\begin{aligned} & 1.7112 \\ & 1.7114 \\ & 1.7139 \end{aligned}$ | 1.71121.71101.7139 | $\begin{aligned} & 1.7485 \\ & 1.7490 \\ & 1.7500 \\ & 1.7505 \end{aligned}$ | 1.74851.74001.75001. 7505 |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 3A |  |  |  |  |  |  |  |  |  |
| 1.8125-6 | UN | 2A | 1. 7890 | 1.8100 | 1.70170 | 1.7655 | $\begin{aligned} & 1.8100 \\ & 1 . \succcurlyeq 108 \end{aligned}$ | 1. 69330 | 1. 69330 | 1.8100 | $\begin{aligned} & 1.8100 \\ & 1.8108 \\ & 1.8125 \\ & 1.8133 \end{aligned}$ |
|  |  |  | 1. 7882 | 1.8108 | 1.70145 | 1. 7647 |  | 1. 69355 | 1. 69305 | 1.8108 |  |
|  |  | 3A | 1. 7915 | 1.8125 | 1.70395 | 1.7693 | 1.8133 | $\begin{aligned} & 1.69790 \\ & 1.69815 \end{aligned}$ | 1. 69765 | $\begin{aligned} & 1.8125 \\ & 1.8133 \end{aligned}$ |  |
| 1.8125-8 | UN | 2A | 1. 7931 | 1.8102 | 1.72900 | 1. 7755 | 1.8102 | 1.72140 | 1. 72140 | 1.8102 | 1.81021.81091.81251.8132 |
|  |  |  | 1. 7924 | 1.8109 | 1.72875 | 1. 7748 | 1.8109 | 1.72165 | 1. 72115 | $\begin{aligned} & 1.8102 \\ & 1.8109 \\ & 1.8125 \end{aligned}$ |  |
|  |  | 3A | 1. 7954 | 1.8125 | 1. 73130 | 1. 7797 | 1. 8125 | 1.72560 | 1. 72560 |  |  |
|  |  |  | 1.7947 | 1.8132 | 1.73105 | 1. 7790 | 1.8132 | 1. 72585 | 1. 72535 | 1.8132 |  |
| 1. 8125-12 | UN | 2 A3 A | 1. 7978 |  |  | $\begin{aligned} & 1.7867 \\ & 1.7861 \\ & 1.7900 \\ & 1.7894 \end{aligned}$ | $\begin{aligned} & 1.8107 \\ & 1.8113 \\ & 1.8125 \\ & 1.8131 \end{aligned}$ | 1. 75060 <br> 1.75085 1.75390 <br> 1. 75415 | $\begin{aligned} & 1.75060 \\ & 1.75035 \\ & 1.75390 \\ & 1.75365 \end{aligned}$ | $\begin{aligned} & 1.8107 \\ & 1.8113 \\ & 1.8125 \\ & 1.8131 \end{aligned}$ | $\begin{aligned} & \text { 1. } 8107 \\ & \text { 1. } 8113 \\ & 1.8125 \\ & 1.8131 \end{aligned}$ |
|  |  |  | 1.7972 |  |  |  |  |  |  |  |  |
|  |  |  | 1.7996 1.7990 |  |  |  |  |  |  |  |  |
| 1. 8125-16 | UN | 2 A | 1. 8004 | 1.8109 | 1. 77030 | 1. 7921 | 1.8109 | 1. 76500 | 1. 76500 | 1.8109 | 1.8109 |
|  |  |  | 1.7998 | 1.8115 | 1. 77005 | 1. 7915 | 1.8115 | 1. 76525 | 1. 76475 | 1. 8115 | 1.8115 |
|  |  | 3A | 1. 1.8020 | 1.8125 1.8131 | 1.77190 1.77165 | 1.7950 1.7944 | 1.8125 1.8131 | 1.76790 1.76815 | 1. 767900 | 1.8125 | 1.8125 1.8131 |
|  |  | 2 A | 1. 8020 | 1. 8110 | 1. 7785 | 1.7954 | 1.8110 | 1. 7737 | 1. 7737 | 1.8110 | 1. 8110 |
| 1. 8125-20 | UN |  | 1.8015 | 1.8115 | 1. 7783 | 1. 7949 | 1.8115 | 1. 7739 | 1. 7735 | 1.8115 | 1.8115 |
|  |  | 3A | 1. 8035 | 1. 8125 | 1. 7800 | 1. 7981 | 1. 8125 | 1.7764 | 1. 7764 | 1.8125 | 1. 8125 |
|  |  |  | 1. 8030 | 1.8130 | 1.7798 | 1.7976 | 1.8130 | 1.7766 | 1. 7762 | 1. 8130 | 1. 8130 |
|  |  | 2 A | 1. 8515 | 1. 8725 | 1. 76420 | 1.8280 | 1.8725 | 1.75580 | 1. 75580 | 1. 8725 | 1. 8725 |
| 1.875-6 | UN |  |  | 1.8733 | 1. 76395 | 1. 8272 | 1. 8733 | 1.75605 | 1. 755555 | 1. 8733 | 1.8733 |
|  |  | 3A | 1. 1.8540 | 1. 1.8750 | 1.76670 1.76645 | 1.8326 1.8318 | 1.8750 1.8758 | 1.76040 1.76065 | 1.76040 1.76015 | 1.8750 1.8758 | 1.8750 1.8758 |
|  |  | 2 A | 1. 8556 | 1. 8727 | 1.79150 | 1.8379 | 1.8727 | 1.78380 | 1.78380 | 1. 8727 | 1.8727 |
| 1. 875-8 | UN | 2 A | 1. 8549 | 1.8734 | 1. 79125 | 1. 8372 | 1.8734 | 1.78405 | 1.78355 | 1. 8734 | 1.8734 |
|  |  | 3A | 1. 8579 | 1.8750 | 1.79380 | 1.8422 | 1.8750 | 1.78810 | 1. 78810 | 1. 8750 | 1.8750 |
|  |  |  | 1. 8572 | 1.8757 | 1. 79355 | 1.8415 | 1.8757 | 1.78835 | 1.78785 | 1.8757 | 1.8757 |
|  |  | 2A | 1. 8603 | 1. 8732 | 1.81910 | 1.8492 | 1. 8732 | 1.81310 | 1. 81310 | 1. 8732 | 1. 8732 |
| 1. 875-12 | UN |  | 1. 8597 | 1.8738 | 1.81885 | 1. 8486 | 1.8738 | 1.81335 | 1.81285 | 1. 8738 | 1.8738 |
|  |  | 3A | 1. 8621 | 1.8750 | 1.82090 | 1. 8525 | 1. 8750 | 1.81640 | 1.81640 | 1.8750 | 1.8750 1.8756 |
|  |  |  | 1. 8615 | 1.8756 | 1.82065 | 1.8519 | 1.8756 | 1.81665 | 1.81615 | 1.8756 | 1.8756 |
|  |  | 2A | 1. 8629 | 1. 8734 | 1.83280 | 1. 8546 | 1. 8734 | 1. 82750 | 1. 82750 | 1. 8734 | 1. 8734 |
| 1. $875-16$ | UN |  | 1. 8623 | 1.8740 | 1.83255 | 1. 8540 | 1.8740 | 1. 82775 | 1.82725 | 1. 8740 | 1. 8740 |
|  |  | 3A | 1. 8645 | 1.8750 | 1.83440 | 1.8575 | 1.8750 | 1.83040 | 1.83040 | 1. 8750 | 1.8750 |
|  |  |  | 1. 8639 | 1.8756 | 1.83415 | 1.8569 | 1.8756 | 1.83065 | 1.83015 | 1.8756 | 1.8756 |
|  |  | 2 A | 1. 8645 | 1. 8735 | 1. 8410 | 1. 8579 | 1.8735 | 1.8362 | 1.8362 | 1. 8735 | 1. 8735 |
| 1. 875-20 | UN |  | 1.8640 | 1.8740 | 1. 8408 | 1.8574 | 1.8740 | 1.8364 | 1.8360 | 1. 8740 | 1.8740 |
|  |  | 3A | 1. 8660 | 1. 8750 | 1. 8425 | 1.8606 | 1.8750 | 1.8389 | 1.8389 | 1.8750 | 1.8750 |
|  |  |  | 1.8655 | 1. 8755 | 1.8423 | 1.8601 | 1.8755 | 1. 8391 | 1.8387 | 1.8755 | 1.8755 |
|  |  | 2A | 1. 9139 | 1. 9349 | 1. 82660 | 1.8903 | 1. 9349 | 1. 81810 | 1. 81810 | 1. 9349 | 1. 9349 |
| 1. 9375-6 | UN |  | 1. 9131 | 1. 9357 | 1.82635 | 1.8895 | 1. 9357 | 1.81835 | 1.81785 | 1. 9357 | 1. 9357 |
|  |  | 3A | 1. 9165 | 1. 9375 | 1.82920 1.82895 | 1.8950 | 1.9375 | 1.82280 1.82305 | 1.82280 1.82255 | 1.9375 1.9383 | 1. 1.93785 |
|  |  |  | 1.9157 | 1. 9383 | 1.82895 | 1.8942 | 1.9383 | 1.82305 | 1.82255 | 1.9383 | 1. 9383 |

See footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Class | W truncated setting plugs |  |  |  |  |  |  | Basic-crest sctting plugs <br> Major diameter |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Plug for GO thread gage * |  |  | Plug for Lo thread gage a |  |  |  |  |  |
|  |  |  | Major diameter |  | Pitch diametcr | Major diameter |  | Pitch diameter |  | Plug for GO thrcad gage ${ }^{\text {a,b }}$ | Plug for LO thread gage ${ }^{\text {a,c }}$ |
|  |  |  | Truncated | Full |  | Truncated | Full | Plus tolerance gage | Minus tolerance gage | $W$ and $X$ tolerances | W and X tolerances |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 1.9375-8 | UN | 2 A | in | in | in | in | in$\text { 1. } 9352$ | in 1.84630 | $\stackrel{i n}{1.84630}^{1.8}$ | in |  |
|  |  |  | 1. 9181 | 1.9352 | 1. 85400 |  |  |  |  | 1. 9352 | 1. 9352 |
|  |  |  | 1. 9174 | 1.9359 | 1.85375 | 1. 8997 | 1.9359 | 1. 84655 | 1.84605 | 1. 9359 | 1. 9359 |
|  |  | 3A | 1.9204 | 1. 9375 | 1. 85630 | 1. 9046 | 1. 9375 | 1.85050 | 1.85050 | 1. 9375 | 1. 9375 |
|  |  |  |  | 1.9382 | 1. 85605 | 1. 9039 | 1. 9382 | 1.85075 | 1.85025 | 1. 9382 | 1. 9382 |
| 1.9375-12 | UN | 2A | 1.92281.92221.9246 | 1.93571.93631.9375 | 1.881601.88135 | 1.91161.91101.9150 | $\begin{aligned} & 1.9357 \\ & 1.9363 \end{aligned}$ | $\begin{aligned} & 1.87550 \\ & 1.87575 \end{aligned}$ | $\begin{aligned} & 1.87550 \\ & 1.87525 \end{aligned}$ | 1.93571.9363 | 1. 9357 |
|  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 3 A |  |  | $\begin{aligned} & 1.88340 \\ & 1.88315 \end{aligned}$ |  | 1.9375 | 1.87890 | 1.87890 | 1. 9375 | 1. 9375 |
|  |  |  | 1.9240 | 1. 9381 |  | $\begin{aligned} & 1.9150 \\ & \text { 1. } 9144 \end{aligned}$ | 1.9381 | 1.87915 | 1. 87865 | 1. 9381 | 1. 9381 |
| 1. 9375-16 | UN | 2 A | 1. 9254 | 1.9359 | 1. 89530 | 1. 9170 | 1.9359 | 1.88990 | 1. 88990 | 1. 9359 | 1. 93359 |
|  |  |  | 1.9248 | 1. 9365 | 1. 89505 | 1. 9164 | 1. 9365 | 1.89015 | 1. 88965 | 1. 9365 |  |
|  |  | 3 A | 1.9270 1.9264 | $\begin{aligned} & \text { 1. } 9375 \\ & 1.9381 \end{aligned}$ | 1.89690 | 1. 1.9200 1.9194 | 1.9375 1.9381 | $\begin{aligned} & 1.89290 \\ & 1.89315 \end{aligned}$ | 1.89290 1.89265 | 1.9375 | $\begin{aligned} & 1.9375 \\ & 1.9381 \end{aligned}$ |
| 1. 9375-20 | UN | 2 A | 1. 9270 | 1. 9360 | 1. 9035 | 1.9203 | 1.9360 | 1.8986 | 1. 8986 | $1.9360 \quad 1.9360$ |  |
|  |  |  | 1. 9265 | 1. 193651.93751. | 1. 9033 | 1.919811.9230 | $\begin{aligned} & 1.9365 \\ & 1.9375 \end{aligned}$ | $\begin{aligned} & 1.8988 \\ & 1.9013 \end{aligned}$ | $\begin{aligned} & 1.8984 \\ & 1.9013 \end{aligned}$ | 1. 9365 | $\begin{aligned} & 1.9365 \\ & 1.9375 \end{aligned}$ |
|  |  | 3 A | 1. 9285 |  | 1. 9050 |  |  |  |  |  |  |
| 2.000-4.5 | UNC | 1A | 1.9713 | 1.9971 | 1.85280 | 1.9347 | 1.9971 | 1.83850 | 1.83850 | 1. 9971 | 1. 9971 |
|  |  |  | 1. 9705 | 1. 9979 | 1.85255 | $\text { 1. } 9395$ | 1.9979 | 1.83875 | 1.838251.84330 | 1.9979 <br> 1.9971 |  |
|  |  | 2 A | 1.9713 | 1. 9971 | 1.85280 |  | 1.9971 | 1.84330 |  |  |  |  |
|  |  |  | 1. 9705 | 1. 9979 | 1. 85255 | 1.9387 | 1. 9979 | 1.84355 1.84860 | 1.84330 1.84305 | $1.9979 \quad 1.9979$ |  |
|  |  | 3A | 1.9742 1.9734 | 2. 0000 2.0008 | 1.85545 | 1.9440 | 2.0008 | 1.84885 | 1. 84835 | 2. 0008 | 2. 2.40000 |
| 2. $000-6$ | UN | 2 A | 1.9764 |  | 1.88910 | 1.9527 | 1. 9974 | 1. 88050 | 1. 88050 | 1.99741 .9974 |  |
|  |  |  | 1.9756 | $\begin{aligned} & 1.9964 \\ & \text { 1. } 9982 \\ & \text { 2. } 0000 \end{aligned}$ | 1.88885 | 1. 9519 | 1. 9982 | 1. 88075 | 1.88025 | 1. 9982 | 1. 9982 |
|  |  | 3A | 1.9790 |  | 1. 89170 | 1. 9575 | 2. 0000 | 1.88530 | 1.88530 | 2. 0000 | 2. 0000 |
|  |  |  | 1. 9782 | 2. 0008 | 1. 89145 | 1. 9567 | 2.0008 | 1.88555 | 1.88505 | 2.0008 | 2. 0008 |
|  |  | 2 A | 1. 9806 | 1. 9977 | 1.91650 | 1.9628 | 1. 9977 | 1. 90870 | 1. 90870 | 1. 9977 | 1. 9977 |
| 2. 000-8 | UN |  | 1. 9799 | 1. 9984 | 1.91625 | 1.9621 | 1. 9984 | 1. 90895 | 1.90845 | 1. 9984 | 1. 9984 |
|  |  | 3A | 1. 9829 | 2. 0000 | 1. 91880 | 1. 9671 | 2. 0000 | 1. 91300 | 1. 91300 | 2. 0000 | 2. 0000 |
|  |  |  | 1.9822 | 2. 0007 | 1.91855 | 1. 9664 | 2.0007 | 1. 91325 | 1. 91275 | 2.0007 | 2. 0007 |
|  |  | 2 A | 1. 9853 | 1. 9982 | 1.94410 | 1.9741 | 1. 9982 | 1.93800 | 1.93800 | 1. 9982 | 1.9982 |
| 2.000-12 | UN |  | 1. 9847 | 1. 9988 | 1. 94385 | 1.9735 | 1. 9988 | 1. 93825 | 1. 93775 | 1. 9988 | 1. 9988 |
|  |  | 3A | 1. 9871 | 2.0000 | 1.94500 | 1. 9775 | 2. 0000 | 1. 94140 | 1.94140 | 2. 0000 | 2. 0000 |
|  |  |  | 1.9865 | 2. 0006 | 1. 94565 | 1.9769 | 2.0006 | 1. 94165 | 1. 94115 | 2.0006 | 2.0006 |
|  |  | 2 A | 1. 9879 | 1. 9984 | 1. 95780 | 1. 9795 | 1. 9984 | 1. 95240 | 1.95240 | 1.9984 | 1. 9984 |
| 2.000-16 | UN |  | 1. 9873 | 1. 9990 | 1. 95755 | 1. 9789 | 1. 9990 | 1. 95265 | 1. 95215 | 1. 9990 | 1. 9990 |
|  |  | 3 A | 1.9895 | 2. 0000 | 1. 95940 | 1. 9825 | 2. 0000 | 1. 95540 | 1.95540 | 2.0000 | 2.0000 |
|  |  |  | 1.9889 | 2.0006 | 1.95915 | 1.9819 | 2.0006 | 1. 95565 | 1. 95515 | 2.0006 | 2.0006 |
|  |  | 2 A | 1. 9895 | 1. 9985 | 1. 9660 | 1.9828 | 1. 9985 | 1. 9611 | 1. 9611 | 1. 9985 | 1.9985 |
| 2.000-20 | UN |  | 1. 9890 | 1. 9990 | 1. 9658 | 1.9823 | 1. 9900 | 1. 9613 | 1. 9609 | 1. 9990 | 1. 9990 |
|  |  | 3A | 1. 9910 | 2. 0000 | 1. 9675 | 1. 9855 | 2.0000 | 1.9638 | 1.9638 | 2. 0000 | 2. 0000 |
|  |  |  | 1.9905 | 2. 0005 | 1. 9673 | 1. 9850 | 2.0005 | 1. 9640 | 1. 9636 | 2. 0005 | 2.0005 |
|  |  | 2 A | 2.1014 | 2. 1224 | 2. 01410 | 2.0776 | 2. 1224 | 2. 00540 | 2.00540 | 2.1224 | 2.1224 |
| 2. 125-6 | UN |  | 2.1006 | 2. 1232 | 2.01385 | 2.0768 | 2. 1232 | 2.00565 | 2.00515 | 2. 1232 | 2. 1232 |
|  |  | 3 A | 2. 1040 | 2. 1250 | 2. 01670 | 2.0824 | 2. 1250 | 2. 01020 | 2.01020 | 2. 1250 | 2. 1250 |
|  |  |  | 2.1032 | 2.1258 | 2.01645 | 2.0816 | 2.1258 | 2. 01045 | 2.00995 | 2.1258 | 2.1258 |
|  |  | 2 A | 2.1055 | 2. 1226 | 2.04140 | 2.0876 | 2. 1226 | 2. 03350 | 2.03350 | 2. 1226 | 2. 1226 |
| 2. 125-8 | UN |  | 2.1048 | 2. 1233 | 2.04115 | 2. 0869 | 2. 1233 | 2.03375 | 2.03325 | 2. 1233 | 2. 1233 |
|  |  | 3 A | 2.1079 2.1072 | 2.1250 | 2. 2.043835 | 2.0920 2.0913 | 2.1250 2.1257 | 2.03790 2.03815 | 2.03790 2.03765 | 2.1250 2.1257 | 2. 1250 2.1257 |
|  |  | 2 A |  | 2.1232 | 2. 06910 | 2.0991 | 2. 1232 | 2.06300 | 2. 06300 | 2. 1232 | 2. 1232 |
| 2. 125-12 | UN |  | 2. 1097 | 2.1238 | 2.06885 | 2.0985 | 2. 1238 | 2.06325 | 2.06275 | 2. 1238 | 2.1238 |
|  |  | 3A | 2.1121 | 2.1250 | 2.07090 | 2.1025 | 2.1250 | 2. 06640 | 2.06640 | 2. 1250 | 2.1250 |
|  |  |  | 2.1115 | 2.1256 | 2.07065 | 2.1019 | 2.1256 | 2. 06665 | 2.06615 | 2. 1256 | 2.1256 |
|  |  | 2A | 2.1129 | 2. 1234 | 2.08280 | 2. 1045 | 2. 1234 | 2. 07740 | 2.07740 | 2. 1234 |  |
| 2. 125-16 | UN |  | 2.1123 | 2. 1240 | 2.08255 | 2. 1039 | 2. 1240 | 2.07765 | 2.07715 | 2. 1240 | 2. 1240 |
|  |  | 3A | 2.1145 | 2. 1250 | 2.08440 | 2. 1075 | 2. 1250 | 2.08040 | 2.08040 | 2. 1250 | 2. 1250 |
|  |  |  | 2.1139 | 2. 1256 | 2.08415 | 2. 1069 | 2.1256 | 2. 08065 | 2.08015 | 2. 1256 | 2.1256 |
|  |  | 2 A | 2.1145 | 2. 1235 | 2.0910 | 2. 1078 | 2. 1235 | 2. 0861 | 2.0861 | 2. 1235 | 2. 1235 |
| 2. 125-20 | UN |  | 2. 1140 | 2. 1240 | 2. 0908 | 2. 1073 | 2. 1240 | 2.0863 | 2. 0859 | 2. 1240 | 2. 1240 |
|  |  | 3 A | 2. 1160 | 2. 1250 | 2. 0925 | 2. 1105 | 2. 1250 | 2. 0888 | 2.0888 | 2. 1250 | 2. 1250 |
|  |  |  | 2.1155 | 2. 1255 | 2.0923 | 2. 1100 | 2. 1255 | 2.0890 | 2. 0886 | 2. 1255 | 2. 1255 |

Sce footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued

| Nominal size and threads per ineh | Series designation | Class | W truncated setting plugs |  |  |  |  |  |  | Basie-erest setting pligs <br> Major diameter |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Plug for GO thread gage a |  |  | Plug for Lo thread gage ${ }^{\text {a }}$ |  |  |  |  |  |
|  |  |  | Major diameter |  | Piteh diameter | Major diameter |  | Piteh diameter |  | Plug for GO thread gage a,b | Plug for LO thread gage ${ }^{\text {a }, ~}$ |
|  |  |  | Truncated | Full |  | Truncated | Full | Plus tolerance gage | Minus tolerance gage | W and X toleranees | W and X toleranees |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 2. 250-4. 5 | UNC | 1A | in ${ }^{\text {an }}$ |  | in 2.10280 | ${ }_{\text {in }}{ }_{2} 1844$ | 2. 2471 | ${ }^{\text {in }} \mathbf{2 . 0 8 8 2 0}$ | 2.08820 | in 2471 | in |
|  |  |  | 2. 2213 | 2. 2471 |  |  |  |  |  |  | 2. 2471 |
|  |  |  | 2. 2205 | 2. 2479 | 2. 10255 | 2.1836 | 2. 2479 | 2.08845 | 2.08795 | 2. 2479 | 2. 2479 |
|  |  | 2A | 2. 22213 | 2. 2471 | 2. 10280 | 2.1893 | 2. 2471 | 2.09310 | 2. 09310 | 2. 2471 | 2. 2471 |
|  |  | 3A | 2. 2242 | 2. 2500 | 2. 10570 | 2.1946 | 2. 2500 | 2.09840 | 2.09840 | 2. 2500 | 2. 2500 |
|  |  |  | 2. 2234 | 2.2508 | 2. 10545 | 2.1938 | 2. 2508 | 2.09865 | 2.09815 | 2. 2508 | 2. 2508 |
| 2. 250-6 | UN | 2A | 2. 2264 | 2.2474 | 2. 13910 | 2. 2025 | 2. 2474 | 2. 13030 | 2. 13030 | 2. 2474 | 2. 2474 |
|  |  |  | 2. 2256 | 2. 2482 | 2. 13885 | 2. 2017 | 2. 2482 | 2. 13055 | 2. 13005 | 2. 2482 | 2. 2482 |
|  |  |  | 2. 2290 | 2. 2500 | 2. 14170 | 2. 2073 | 2. 2500 | 2. 13510 | 2. 13510 | 2. 2500 | 2. 2500 |
|  |  |  | 2. 2282 | 2. 2508 | 2. 14145 | 2. 2065 | 2. 2508 | 2. 13535 | 2. 13485 | 2. 2508 | 2. 2508 |
| 2. 250-8 | UN | 2 A3 A | 2. 2305 | 2.2476 | 2. 16640 | 2.2125 | 2. 2476 | 2. 15840 | 2. 15840 | 2. 2476 | 2. 2476 |
|  |  |  | 2. 2298 | 2. 2483 | 2. 16615 | 2. 2118 | 2. 2483 | 2. 15865 | 2. 15815 | 2. 2483 | 2. 2483 |
|  |  |  | 2. 2329 | 2. 252500 | ${ }_{2}^{2.16880}$ | 2. 2169 2.2162 | 2. 25000 | 2. 16280 | 2. 16280 | 2. 2500 | 2. 2500 |
| 2. 250-12 | UN | 2 A3 A | 2. 2353 | 2. 2482 | 2. 19410 | 2. 2241 | 2.2482 | 2. 18800 | 2. 18800 | 2.2482 | 2. 2482 |
|  |  |  | 2. 2347 | 2.2488 | 2. 19385 | 2.2235 | 2. 2488 | 2. 18825 | 2. 18775 | 2.2488 | 2. 2488 |
|  |  |  | 2. 2371 | 2. 2500 | 2. 19590 | 2. 2275 | 2. 2500 | 2. 19140 | 2.19140 | 2. 2500 | 2. 2500 |
|  |  |  | 2. 2365 | 2.2506 | 2.19565 | 2. 2269 | 2. 2506 | 2. 19165 | 2. 19115 | 2. 2506 | 2. 2506 |
| 2. 250-16 | UN | 2 A | 2. 2379 | 2. 2484 | 2. 20780 | 2. 2295 | 2. 2484 | 2. 20240 | 2. 20240 | 2. 2484 | 2. 2484 |
|  |  | 3 A | 2. 2373 | 2. 2490 | 2. 20755 | 2. 2289 | 2. 2490 | 2. 20265 | 2. 20215 | 2. 2490 | 2. 2490 |
|  |  |  | 2. 2395 | 2. 2500 | 2. 20940 | 2. 2325 | 2. 2500 | 2. 20540 | 2. 20540 | 2. 2.2500 | 2. 2500 2. 2506 |
|  |  |  | 2. 2389 | 2. 2506 | 2. 20915 | 2. 2319 | 2. 2506 | 2. 20565 | 2. 20515 | 2. 2506 | 2. 2506 |
| 2. 250-20 | UN | 2 A3 A | 2. 2395 | 2. 2485 | 2. 2160 | 2. 2328 | 2. 2485 | 2. 2111 | 2. 2111 | 2.2485 | 2. 2485 |
|  |  |  | 2. 2390 | 2. 2490 | 2. 2158 | 2. 2323 | 2. 2490 | 2. 2113 | 2. 2109 | 2. 2490 | 2. 2490 |
|  |  |  | 2. 2410 | 2.2500 | 2. 2175 | 2.2355 | 2. 2500 | 2. 2138 | 2. 2138 | 2. 2500 | 2. 2500 |
|  |  |  | 2. 2405 | 2. 2505 | 2. 2173 | 2.2350 | 2. 2505 | 2. 2140 | 2. 2136 | 2. 2505 | 2. 2505 |
| 2. 375-6 | UN | 2 A | 2. 3513 | 2. 3723 | 2. 26400 | 2.3273 | 2.3723 | 2. 25510 | 2. 25510 | 2.3723 | 2. 3723 |
|  |  |  | 2. 3505 | 2.3731 | 2. 26375 | 2.3265 | 2. 3731 | 2. 25535 | 2. 25485 | 2. 3731 | 2.3731 |
|  |  | 3A | 2. 3540 | 2.3750 | 2. 26670 | 2.3323 | 2. 3750 | 2. 26010 | 2. 26010 | 2. 3750 | 2. 3750 |
|  |  |  | 2. 3532 | 2.3758 | 2. 26645 | 2.3315 | 2.3758 | 2. 26035 | 2. 25985 | 2. 3758 | 2. 3758 |
| 2. 375-8 | UN | 2 A | 2. 3555 | 2.3726 | 2. 29140 | 2. 3374 | 2.3726 | 2. 28330 | 2. 28330 | 2. 3726 | 2.3726 |
|  |  |  | 2.3548 | 2. 3733 | 2. 29115 | 2. 3367 | 2. 3733 | 2. 28355 | 2. 28305 | 2.3733 | 2. 3733 |
|  |  | 3 A | 2. 3579 | 2.3750 | 2. 29380 | 2. 3419 | 2. 3750 | 2. 28780 | 2. 28780 | 2.3750 | 2. 3750 |
|  |  |  | 2. 3572 | 2.3757 | 2. 29355 | 2.3412 | 2.3757 | 2. 28805 | 2. 28755 | 2. 3757 | 2. 3757 |
| 2.375-12 | UN | 2A | 2.3602 | 2. 3731 | 2. 31900 | 2. 3489 | 2. 3731 | 2. 31280 | 2. 31280 | 2.3731 | 2. 3731 |
|  |  |  | 2. 3596 | 2.3737 | 2. 31875 | 2. 3483 | 2. 3737 | 2. 31305 | 2. 31255 | 2. 3737 | 2. 3737 |
|  |  | 3A | 2. 3621 2.3615 | 2. 3750 2.3756 | 2. 32090 | 2. 3524 2. 3518 | 2.3750 2.3756 | 2.31630 | 2. 3131630 | 2.3750 2.3756 | 2. 3750 2. 3756 |
|  |  |  | 2. 3615 | 2. 3756 | 2. 32065 | 2. 3518 | 2. 3756 | 2. 31655 | 2. 31605 | 2. 3756 | 2. 3756 |
| 2. 375-16 | UN | 2A | 2. 3628 | 2. 3733 | 2. 33270 | 2. 3543 | 2.3733 | 2. 32720 | 2. 32720 | 2.3733 | 2. 3733 |
|  |  |  | 2. 3622 | 2. 3739 | 2. 33245 | 2. 3537 | 2. 3739 | 2. 32745 | 2. 32695 | 2. 3739 | 2. 3739 |
|  |  | 3A | 2. 3645 2. 3639 | 2. 3750 2. 3756 | 2. 334440 | 2. 3574 2.3568 | 2.3750 2.3756 | 2. 33030 2.33055 | 2. 33030 2. 33005 | 2.3750 2.3756 | 2. 3750 2.3756 |
| 2. 375-20 | UN | 2A | 2. 3645 | 2. 3735 | 2. 3410 | 2. 3576 | 2.3734 | 2. 3359 | 2. 3359 | 2. 3735 | 2. 3734 |
|  |  |  | 2. 3640 | 2.3740 | 2. 3408 | 2. 3571 | 2.3739 | 2.3361 | 2.3357 | 2. 3740 | 2. 3739 |
|  |  | 3A | 2. 3660 | 2.3750 | 2. 3425 | 2. 3604 | 2. 3750 | 2.3387 | 2. 3387 | 2. 3750 | 2. 3750 |
|  |  |  | 2. 3655 | 2.3755 | 2.3423 | 2. 3599 | 2. 3755 | 2.3389 | 2. 3385 | 2. 3755 | 2. 3755 |
| 2. 500-4 | UNC | 1A | 2. 4688 | 2.4969 | 2. 33450 | 2. 4273 | 2. 4969 | 2. 31900 | 2. 31900 | 2. 4969 | 2. 4969 |
|  |  |  | 2. 4679 | 2. 4978 | 2. 33425 | 2. 4264 | 2. 4978 | 2. 31925 | 2.31875 | 2. 4978 | 2. 4978 |
|  |  | 2A | 2. 4688 | 2. 4969 | 2.33450 | 2.4324 | 2. 4969 | 2. 32410 | 2. 32410 | 2.4969 | 2. 4969 |
|  |  | 2 A | 2. 4679 | 2. 4978 | 2.33425 | 2.4315 | 2. 4978 | 2.32435 | 2. 32385 | 2. 4978 | 2. 4978 |
|  |  | 3A | 2. 4719 | 2. 5000 | 2. 33760 | 2. 4381 | 2. 5000 | 2. 32980 | 2. 32980 | 2. 5000 | 2. 5000 |
|  |  |  | 2.4710 | 2. 5009 | 2. 33735 | 2.4372 | 2. 5009 | 2. 33005 | 2. 32955 | 2. 5009 | 2. 5009 |
| 2. 500-6 | UN | 2A | 2. 4763 | 2. 4973 | 2. 38900 | 2. 4522 | 2. 4973 | 2. 38000 | 2. 38000 | 2. 4973 | 2.4973 |
|  |  |  | 2. 4755 | 2. 4981 | 2. 38875 | 2. 4514 | 2. 4981 | 2. 38025 | 2. 37975 | 2. 4981 | 2. 4981 |
|  |  | 3A | 2. 4790 | 2. 5000 | 2. 39170 | 2. 4572 | 2. 5000 | 2. 38500 | 2. 38500 | 2. 5000 | 2. 5000 |
|  |  |  | 2. 4782 | 2. 5008 | 2. 39145 | 2. 4564 | 2. 5008 | 2.38525 | 2. 38475 | 2. 5008 | 2. 5008 |
| 2. $500-8$ | UN | 2 A | 2. 4805 | 2. 4976 | 2.41640 | 2. 4623 | 2. 4976 | 2. 40820 | 2. 40820 | 2. 4976 | 2. 4976 |
|  |  |  | 2. 4798 | 2.4983 | 2. 41615 | 2. 4616 | 2. 4983 | 2. 40845 | 2. 40795 | 2. 4983 | 2. 4983 |
|  |  | 3A | 2.4829 | 2. 5000 | 2.41880 | 2. 4668 | 2. 5000 | 2.41270 | 2. 41270 | 2. 5000 | 2. 5000 |
|  |  |  | 2. 4822 | 2. 5007 | 2.41855 | 2. 4661 | 2. 5007 | 2. 41295 | 2. 41245 | 2. 5007 | 2. 5007 |
| 2. 500-12 | UN | 2A | 2.4852 | 2.4981 | 2. 44400 | 2. 4739 | 2. 4981 | 2. 43780 | 2. 43780 | 2. 4981 | 2. 4981 |
|  |  |  | 2.4846 | 2.4987 | 2. 44375 | 2. 4733 | 2. 4987 | 2. 43805 | 2. 43755 | 2. 4987 | 2. 4987 |
|  |  | 3A | 2. 4871 | 2.5000 | 2. 44590 | 2. 4774 | 2. 5000 | 2. 44130 | 2. 44130 | 2. 5000 | 2. 5000 |
|  |  |  | 2. 4865 | 2. 5006 | 2. 44565 | 2. 4768 | 2. 5006 | 2. 44155 | 2.44105 | 2. 5006 | 2. 5006 |

See footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Class | W truncated setting plugs |  |  |  |  |  |  | Basie-erest setting plugs <br> Major diameter |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Plug for GO thread gage ${ }^{\text {a }}$ |  |  | Plug for LO thread gage ${ }^{\text {a }}$ |  |  |  |  |  |
|  |  |  | Major diameter |  | Pitch diameter | Major diameter |  | Piteh diameter |  | Plug for GO thread gage ${ }^{\text {a,b }}$ | Plug for LO thread gage a, |
|  |  |  | Truncated | Full |  | Truncated | Full | Plus tolerance gage | Minus tolerance gage | W and X toleranees | W and X tolerances |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 2. $500-16$ | UN | 2A | in | in | in | in | in | in | in | in | in |
|  |  |  | 2.4878 | 2. 4983 | 2. 45770 | 2.4793 | 2. 4983 | 2. 45220 | 2.45220 | 2. 4983 | 2. 4983 |
|  |  |  | 2. 4872 | 2.4989 | 2. 45745 | 2. 4787 | 2. 4989 | 2. 45245 | 2. 45195 | 2. 4989 | 2. 4989 |
|  |  | 3A | 2.4895 | 2. 5000 | 2.45940 | 2. 4824 | 2. 5000 | 2. 45530 | 2. 45530 | 2. 5000 | 2. 5000 |
|  |  |  | 2.4889 | 2. 5006 | 2. 45915 | 2. 4818 | 2. 5006 | 2. 45555 | 2. 45505 | 2. 5006 | 2. 5006 |
| 2. $500-20$ | UN | 2A | 2.4895 | 2. 4985 | 2. 4660 | 2. 4826 | 2. 4984 | 2. 4609 | 2. 4609 | 2. 4985 | 2. 4984 |
|  |  | 3A | 2. 4890 | 2. 4990 | 2. 4658 | 2. 4821 | 2. 4989 | 2. 4611 | 2. 4607 | 2. 4990 | 2. 4989 |
|  |  |  | 2. 4910 | 2. 5000 | 2. 4675 | 2. 4854 | 2. 5000 | 2. 4637 | 2. 4637 | 2. 5000 | 2. 5000 |
|  |  |  | 2.4905 | 2. 5005 | 2. 4673 | 2. 4849 | 2. 5005 | 2. 4639 | 2. 4635 | 2.5005 | 2. 5005 |
| 2. 625-6 | UN | 2 A | 2.6013 | 2.6223 | 2. 51400 | 2. 5772 | 2. 6223 | 2. 50500 | 2. 50500 | 2.6223 | 2. 6223 |
|  |  | 3A | 2. 6005 | 2. 6231 | 2. 51375 | 2. 5764 | 2. 6231 | 2. 50525 | 2. 50475 | 2.6231 | 2. 6231 |
|  |  |  | 2. 6040 | 2.6250 | 2. 51670 | 2. 5881 | 2.6250 | 2. 50990 | 2. 50990 | 2.6250 | 2. 6250 |
|  |  |  | 2. 6032 | 2. 6258 | 2. 51645 | 2.5813 | 2. 6258 | 2. 51015 | 2. 50965 | 2.6258 | 2.6258 |
| 2. 625-8 | UN | 2 A | 2. 6054 | 2. 6225 | 2. 54130 | 2. 5872 | 2. 6225 | 2.53310 | 2. 53310 | 2.6225 | 2.6225 |
|  |  |  | 2. 6047 | 2. 6232 | 2. 54105 | 2. 5865 | 2. 6232 | 2. 53335 | 2. 53285 | 2. 6232 | 2. 6232 |
|  |  | 3A | 2. 6079 | 2. 6250 | 2. 54380 | 2.5917 | 2. 6250 | 2. 53760 | 2. 53760 | 2.6250 | 2. 6250 |
|  |  |  | 2. 6072 | 2. 6257 | 2. 54355 | 2.5910 | 2. 6257 | 2.53785 | 2. 53735 | 2.6257 | 2. 6257 |
| 2. 625-12 | UN | 2 A | 2. 6102 | 2. 6231 | 2. 56900 | 2. 5989 | 2. 6231 | 2. 56280 | 2. 56280 | 2. 6231 | 2. 6231 |
|  |  |  | 2. 6096 | 2. 6237 | 2. 56875 | 2. 5983 | 2.6237 | 2.56305 | 2. 56255 | 2.6237 | 2.6237 |
|  |  | 3A | 2. 6121 | 2.6250 | 2. 57090 | 2.6024 | 2. 6250 | 2. 56630 | 2. 56630 | 2.6250 | 2.6250 |
|  |  |  | 2.6115 | 2.6256 | 2. 57065 | 2. 6018 | 2. 6256 | 2. 56655 | 2. 56605 | 2.6256 | 2. 6256 |
| 2. 625-16 | UN | 2 A | 2.6128 | 2.6233 | 2. 58270 | 2.6043 | 2.6233 | 2. 57720 | 2. 57720 | 2.6233 | 2. 6233 |
|  |  |  | 2. 6122 | 2. 6239 | 2. 58245 | 2. 6037 | 2. 6239 | 2. 57745 | 2. 57695 | 2. 6239 | 2. 6239 |
|  |  | 3A | 2.6145 | 2. 6250 | 2. 58440 | 2. 6074 | 2. 6250 | 2.58030 | 2.58030 | 2. 6250 | 2. 6250 |
|  |  |  | 2. 6139 | 2.6256 | 2. 58415 | 2. 6068 | 2.6256 | 2. 58055 | 2. 58005 | 2.6256 | 2. 6256 |
| 2. 625-20 | UN | 2 A | 2. 6145 | 2.6235 | 2.5910 | 2.6076 | 2. 6234 | 2. 5859 | 2. 5859 | 2.6235 | 2. 6234 |
|  |  |  | 2. 6140 | 2. 6240 | 2. 5008 | 2. 6071 | 2. 6239 | 2. 5861 | 2. 5857 | 2.6240 | 2. 6239 |
|  |  | 3 A | 2.6160 | 2. 6250 | 2. 5925 | 2. 6104 | 2. 6250 | 2. 5887 | 2. 5887 | 2.6250 | 2.6250 |
|  |  |  | 2.6155 | 2. 6255 | 2.5923 | 2.6099 | 2. 6255 | 2.5889 | 2.5885 | 2.6255 | 2.6255 |
| 2. 750-4 | UNC | 1 A | 2. 7187 | 2. 7468 | 2. 58440 | 2. 6769 | 2. 7468 | 2. 56860 | 2. 56860 | 2. 7468 | 2. 7468 |
|  |  |  | 2. 7178 | 2. 7477 | 2. 58415 | 2.6760 | 2. 7477 | 2. 56885 | 2. 56835 | 2. 7477 | 2. 7477 |
|  |  | 2 A | 2. 7187 | 2. 7468 | 2. 58440 | 2.6822 | 2. 7468 | 2. 57390 | 2. 57390 | 2.7468 | 2. 7468 |
|  |  |  | 2. 7178 | 2. 7477 | 2. 58415 | 2.6813 | 2. 7477 | 2. 57415 | 2. 57365 | 2.7477 | 2. 4777 |
|  |  | 3A | 2. 7219 2. 7210 | 2. 7500 2. 7509 | 2. 58760 2.58735 | 2.6880 2.6871 | 2. 7500 2. 7509 | 2. 57970 2.57995 | 2. 57970 2. 57945 | 2. 7500 2. 7509 | 2. 7500 2. 7509 |
| 2. 750-6 | UN | 2 A |  |  | 2.63900 | 2. 7021 |  | 2.62990 | 2. 62990 | 2. 7473 |  |
|  |  |  | 2. 7255 | 2. 7481 | 2.63875 | 2. 7013 | 2. 7481 | 2. 63015 | 2. 62965 | 2. 7481 | 2. 7481 |
|  |  | 3 A | 2. 7290 | 2. 7500 | 2. 64170 | 2. 7071 | 2. 7500 | 2. 63490 | 2. 63490 | 2. 7500 | 2. 7500 |
|  |  |  | 2. 7282 | 2. 7508 | 2. 64145 | 2. 7063 | 2. 7508 | 2.63515 | 2. 63465 | 2. 7508 | 2. 7508 |
| 2. 750-8 | UN | 2 A |  |  | 2.66630 | 2.7121 |  | 2. 65800 | 2.65800 | 2. 7475 | 2. 7475 |
|  |  |  | 2. 7297 | 2. 7482 | 2. 66605 | 2.7114 | 2. 7482 | 2. 65825 | 2. 65775 | 2. 7482 | 2. 7482 |
|  |  | 3 A | 2. 7329 | 2. 7500 | 2. 66880 | 2. 7167 | 2. 7500 | 2. 66250 | 2.66250 | 2. 7500 | 2. 7500 |
|  |  |  | 2. 7322 | 2. 7507 | 2. 66855 | 2.7160 | 2. 7507 | 2. 66275 | 2. 66225 | 2. 7507 | 2. 7507 |
| 2. 750-12 | UN | 2 A |  |  | 2. 69400 | 2. 7239 | 2. 7481 | 2. 68780 | 2. 68780 | 2. 7481 | 2. 7481 |
|  |  |  | 2. 7346 | 2. 7487 | 2.69375 | 2.7233 | 2.7487 | 2. 68805 | 2.68755 | 2.7487 | 2. 7487 |
|  |  | 3 A | 2. 7371 | 2. 7500 | 2. 69590 | 2.7274 | 2. 7500 | 2. 69130 | 2.69130 | 2.7500 | 2. 7500 |
|  |  |  | 2.7365 | 2.7506 | 2. 69565 | 2.7268 | 2.7506 | 2. 69155 | 2.69105 | 2.7506 | 2. 7506 |
| 2. 750-16 | UN | 2 A | 2. 7378 | 2. 7483 | 2. 70770 | 2.7293 | 2.7483 | 2. 70220 | 2. 70220 | 2. 7483 | 2. 7483 |
|  |  |  | 2.7372 | 2. 7489 | 2. 70745 | 2. 7287 | 2. 7489 | 2. 70245 | 2. 70195 | 2.7489 | 2. 7489 |
|  |  | 3 A | 2.7395 | 2. 7500 | 2. 70940 | 2. 7324 | 2. 7500 | 2. 70530 | 2. 70530 | 2.7500 | 2. 7500 |
|  |  |  | 2. 7389 | 2. 7506 | 2. 70915 | 2. 7318 | 2. 7506 | 2. 70555 | 2. 70505 | 2.7506 | 2. 7506 |
| 2. $750-20$ | UN | 2 A | 2. 7395 | 2. 7485 | 2. 7160 | 2. 7326 | 2. 7484 | 2. 7109 | 2. 7109 | 2. 7485 | 2. 7484 |
|  |  |  | 2.7390 | 2. 7490 | 2.7158 | 2.7321 | 2. 7489 | 2.7111 | 2.7107 | 2. 7490 | 2. 7489 |
|  |  | 3A | 2. 7410 | 2. 7500 | 2. 7175 | 2. 7354 | 2. 7500 | 2.7137 | 2.7137 | 2. 7500 | 2. 7500 |
|  |  |  | 2. 7405 | 2.7505 | 2.7173 | 2. 7349 | 2. 7505 | 2.7139 | 2.7135 | 2. 7505 | 2. 7505 |
| 2. 875-6 | UN | 2 A | 2. 8512 | 2. 8722 | 2. 76390 | 2.8269 | 2.8722 | 2. 75470 | 2. 75470 | 2.8722 | 2.8722 |
|  |  |  | 2.8504 | 2.8730 | 2.76365 | 2.8261 | 2. 8730 | 2. 75495 | 2.75445 | 2.8730 | 2.8730 |
|  |  | 3 A | 2. 8540 | 2.8750 | 2.76670 | 2.8320 | 2.8750 | 2.75980 | 2.75980 | 2.8750 | 2.8750 |
|  |  |  | 2.8532 | 2.8758 | 2.76645 | 2.8312 | 2.8758 | 2. 76005 | 2. 75955 | 2.8758 | 2. 8758 |
| 2. 875-8 | UN | 2 A | 2. 8554 | 2.8725 | 2. 79130 | 2.8370 | 2.8725 | 2. 78290 | 2. 78290 | 2.8725 | 2.8725 |
|  |  |  | 2.8547 | 2.8732 | 2. 79105 | 2.8363 | 2.8732 | 2. 78315 | 2. 78265 | 2.8732 | 2.8732 |
|  |  | 3 A | 2.8579 | 2.8750 | 2.79380 | 2.8416 | 2.8750 | 2.78750 | 2. 78750 | 2.8750 | 2. 8750 |
|  |  |  | 2.8572 | 2.8757 | 2.79355 | 2.8409 | 2. 8757 | 2. 78775 | 2. 78725 | 2.8757 | 2.8757 |
| 2.875-12 | UN | 2 A | 2.8602 | 2.8731 | 2. 81900 | 2.8488 | 2. 8731 | 2. 81270 | 2.81270 | 2.8731 | 2. 8731 |
|  |  |  | 2.8596 | 2.8737 | 2.81875 | 2.8482 | 2.8737 | 2. 81295 | 2.81245 | 2.8737 | 2. 8737 |
|  |  | 3 A | 2.8621 | 2.8750 | 2. 82090 | 2.8523 | 2. 8750 | 2. 81620 | 2.81620 | 2. 8750 | 2. 8750 |
|  |  |  | 2.8615 | 2. 8756 | 2.82065 | 2.8517 | 2.8756 | 2.81645 | 2.81595 | 2.8756 | 2.8756 |

See footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Class | W truncated setting plugs |  |  |  |  |  |  | $\frac{\text { Basie-erest setting plugs }}{\text { Major diameter }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Plug for GO thread gage ${ }^{\text {a }}$ |  |  | Plug for Lo thread gage a |  |  |  |  |  |
|  |  |  | Major diameter |  | Pitch diameter | Major diameter |  | Piteh diameter |  | Plug for GO thread gage a.b | Plug for LO thread gage $\mathrm{a}, \mathrm{o}$ |
|  |  |  | Truncated | Full |  | Truncated | Full | Plus tolerance gage | Minus tolerance gage | W and X tolerances | $W$ and $X$ tolerances |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 2. 875-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | in | in | in | in | in | in | in | in | in |
|  |  |  | 2.8628 | 2.8733 | 2. 83270 | 2.8542 | 2.8733 | 2.82710 | 2. 82710 | 2.8733 | 2.8733 |
|  |  |  | 2.8622 | 2.8739 | 2.83245 | 2.8536 | 2.8739 | 2.82735 | 2.82685 | 2.8739 | 2. 8739 |
|  |  |  | 2. 8645 | 2.8750 | 2. 83440 | 2. 8573 | 2.8750 | 2. 83020 | 2. 83020 | 2.8750 | 2.8750 |
|  |  |  | 2. 8639 | 2.8756 | 2. 83415 | 2.8567 | 2. 8756 | 2.83045 | 2.82995 | 2.8756 | 2.8756 |
| 2. 875-20 | UN | 2A | 2. 8644 | 2. 8734 | 2. 8409 | 2. 8574 | 2.8732 | 2. 8357 | 2. 8357 | 2. 8734 | 2. 8732 |
|  |  | 3A | 2.8639 | 2.8739 | 2.8407 | 2.8569 | 2.8737 | 2.8359 | 2.8355 | 2.8739 | 2. 8737 |
|  |  |  | 2.8660 | 2.8750 | 2.8425 | 2.8603 | 2.8750 | 2.8386 | 2.8386 | 2.8750 | 2.8750 |
|  |  |  | 2.8655 | 2.8755 | 2. 8423 | 2.8598 | 2.8755 | 2. 8388 | 2. 8384 | 2. 8755 | 2.8755 |
| 3. 000-4 | UNC | $\begin{aligned} & 1 \mathrm{~A} \\ & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | 2. 9687 | 2.9968 | 2. 83440 | 2.9266 | 2.9968 | 2.81830 | 2.81830 | 2.9968 | 2.9968 |
|  |  |  | 2. 9678 | 2. 9977 | 2. 83415 | 2. 9257 | 2. 9977 | 2.81855 | 2. 81805 | 2. 9977 | 2. 9977 |
|  |  |  | 2. 9687 | 2. 9998 | 2. 834440 | 2. 9320 | 2.9968 | 2. 823370 | 2. 82370 | 2. 9968 | 2.9968 |
|  |  |  | 2.9719 2.9719 | 3. 0000 | 2.83415 2.83760 | 2.9379 | 2.9977 3.0000 | 2.82960 | 2. 282960 | 2. 39000 | 2.9977 3.0000 |
|  |  |  | 2.9710 | 3. 0009 | 2.83735 | 2.9370 | 3. 0009 | 2.82985 | 2. 82935 | 3. 0009 | 3. 0009 |
| 3. 000-6 | UN | 2A | 2. 9762 | 2. 9972 | 2. 88890 | 2.9518 | 2.9972 | 2.87960 | 2. 87960 | 2. 9972 | 2.9972 |
|  |  | 3 A | 2.9754 | 2. 9980 | 2. 88865 | 2.9510 | 2.9980 | 2.87985 | 2.87935 | 2. 9980 | 2. 9980 |
|  |  |  | 2.9790 2.9782 | 3. 0000 3.0008 | 2.89170 2.89145 | 2. 9569 2.9561 | 3.0000 3.0008 | 2.88470 2.88495 | 2. 88470 2. 88445 | 3.0000 3.0008 | 3.0000 3.0008 |
| 3. $000-8$ | UN | 2A | 2.9803 | 2. 9974 | 2. 91620 | 2.9618 | 2.9974 | 2. 90770 | 2.90770 | 2.9974 | 2.9974 |
|  |  |  | 2.9796 | 2. 9981 | 2. 91595 | 2. 9611 | 2. 9981 | 2.90795 | 2. 90745 | 2.9981 | 2. 9981 |
|  |  | 3A | 2. 9829 | 3. 0000 | 2. 91880 | 2. 9665 | 3.0000 | 2.91240 | 2. 91240 | 3.0000 | 3. 0000 |
|  |  |  | 2. 9822 | 3. 0007 | 2. 91855 | 2. 9658 | 3.0007 | 2.91265 | 2.91215 | 3.0007 | 3.0007 |
| 3. $000-12$ | UN | 2A | 2. 9852 | 2. 9981 | 2. 94400 | 2.9738 | 2.9981 | 2.93770 | 2.93770 | 2.9981 | 2.9981 |
|  |  |  | 2. 9846 | 2. 9987 | 2. 94375 | 2. 9732 | 2. 9987 | 2.93795 | 2.93745 | 2.9987 | 2.9987 |
|  |  | 3A | 2.9871 | 3. 0000 | 2. 94590 | 2. 9773 | 3.0000 | 2. 94120 | 2. 94120 | 3.0000 | 3.0000 |
|  |  |  | 2.9865 | 3.0006 | 2. 94565 | 2.9767 | 3. 0006 | 2.94145 | 2.94095 | 3.0006 | 3.0006 |
| 3. $000-16$ | UN | 2A | 2.9878 | 2. 9983 | 2. 95770 | 2.9792 | 2. 9983 | 2. 95210 | 2.95210 | 2. 9983 | 2.9983 |
|  |  |  | 2. 9887 | 2. 9989 | 2. 95745 | 2. 9788 | 2. 9989 | 2. 95235 | 2.95185 | 2. 9989 | 2. 9989 |
|  |  | 3A | 2.9895 2.9889 | 3. 0000 3.0006 | 2. 95940 2.95915 | 2.9823 2.9817 | 3.0000 3.0006 | 2. 2.95520 | 2. 9.955490 | 3.0000 3.0006 | 3.0000 3.0006 |
| 3. 000-20 | UN | 2A | 2. 9894 | 2. 9984 | 2. 9659 | 2. 9824 | 2. 9982 | 2. 9607 | 2. 9607 | 2. 9984 | 2. 9982 |
|  |  |  | 2. 9889 | 2.9989 | 2. 9657 | 2. 9819 | 2. 9987 | 2. 9609 | 2. 9605 | 2. 9989 | 2.9987 |
|  |  | 3A | 2. 9910 | 3. 0000 | 2. 9675 | 2.9853 | 3. 0000 | 2. 9636 | 2. 9636 | 3.0000 | 3. 0000 |
|  |  |  | 2. 9905 | 3. 0005 | 2. 9673 | 2. 9848 | 3. 0005 | 2.9638 | 2. 9634 | 3. 0005 | 3. 0005 |
| 3. 125-6 | UN | 2 A | 3. 1012 | 3. 1222 | 3. 01390 | 3.0767 | 3. 1222 | 3.00450 | 3. 00450 | 3. 1222 | 3. 1222 |
|  |  |  | 3. 1004 | 3. 1230 | 3. 01365 | 3.0759 | 3. 1230 | 3.00475 | 3. 00425 | 3. 1230 | 3. 1230 |
|  |  | 3A | 3. 1040 3. 1032 | 3.1250 3.1258 | 3. 01670 3. 01645 | 3.0819 3.0811 | 3. 1250 3.1258 | 3.00970 | 3. 00970 3. 00945 | 3. 3.1250 | 3. 1250 |
| 3. 125-8 | UN | 2A | 3.1053 | 3. 1224 | 3. 04120 | 3.0867 | 3. 1224 | 3.03260 | 3.03260 | 3. 1224 | 3. 1224 |
|  |  |  | 3. 1046 | 3. 1231 | 3.04095 | 3. 0860 | 3. 1231 | 3. 03285 | 3. 03235 | 3. 1231 | 3. 1231 |
|  |  | 3A | 3. 1079 | 3. 1250 | 3.04380 | 3.0915 | 3. 1250 | 3.03740 | 3. 03740 | 3. 1250 | 3. 1250 |
|  |  |  | 3. 1072 | 3. 1257 | 3. 04355 | 3. 0908 | 3. 1257 | 3. 03765 | 3. 03715 | 3. 1257 | 3. 1257 |
| 3. 125-12 | UN | 2A | 3.1102 | 3. 1231 | 3. 06900 | 3. 0988 | 3.1231 | 3. 06270 | 3. 06270 | 3. 1231 | 3. 1231 |
|  |  |  | 3.1096 | 3. 1237 | 3. 06875 | 3.0982 | 3. 1237 | 3. 06295 | 3. 06245 | 3. 1237 | 3. 1237 |
|  |  | 3A | 3.1121 | 3. 1250 | 3.07090 | 3. 1023 | 3. 1250 | 3. 06620 | 3. 06620 | 3. 1250 | 3. 1250 |
|  |  |  | 3.1115 | 3. 1256 | 3. 07065 | 3. 1017 | 3. 1256 | 3. 06645 | 3. 06595 | 3. 1256 | 3. 1256 |
| 3. 125-16 | UN | 2A | 3. 1128 | 3. 1233 | 3. 08270 | 3. 1042 | 3.1233 | 3. 07710 | 3. 07710 | 3. 1233 | 3. 1233 |
|  |  |  | 3.1122 | 3. 1239 | 3.08245 | 3. 1036 | 3. 1239 | 3. 07735 | 3. 07685 | 3. 1239 | 3. 1239 |
|  |  | 3A | 3. 1145 3.1139 | 3. 1250 3.1256 | 3.08440 3.08415 | 3. 1073 3. 1067 | 3. 3. 1250 | 3.08020 3.08045 | 3.08020 3.07995 | 3.1250 3.1256 | 3. 1250 |
| 3. 250-4 | UNC | 1 A | 3. 2186 | 3.2467 | 3. 08340 | 3.1763 | 3. 2467 | 3. 06800 | 3. 06800 | 3.2467 | 3. 2467 |
|  |  |  | 3. 2177 | 3. 2476 | 3. 08405 | 3. 1754 | 3. 2476 | 3. 06825 | 3. 06775 | 3.2476 | 3. 2476 |
|  |  | 2 A | 3. 2186 | 3. 2467 | 3.08430 | 3.1817 | 3. 2467 | 3. 07340 | 3. 07340 | 3. 2467 | 3. 2467 |
|  |  |  | 3. 2177 | 3. 2476 | 3.08405 | 3. 1808 | 3. 2476 | 3. 07365 | 3. 07315 | 3. 2476 | 3. 2476 |
|  |  | 3A | 3. 2219 | 3. 2500 | 3.08760 | 3. 1877 | 3. 2500 | 3. 07940 | 3. 07940 | 3. 2500 | 3. 2500 |
|  |  |  | 3. 2210 | 3. 2509 | 3. 08735 | 3. 1868 | 3. 2509 | 3. 07965 | 3. 07915 | 3. 2509 | 3. 2509 |
| 3. 250-6 | UN | 2 A | 3. 2262 | 3. 2472 | 3.13890 | 3. 2016 | 3. 2472 | 3. 12940 | 3. 12940 | 3.2472 | 3. 2472 |
|  |  |  | 3. 2254 | 3. 2480 | 3. 13865 | 3. 2008 | 3. 2480 | 3. 12965 | 3. 12915 | 3. 2480 | 3. 2480 |
|  |  | 3A | 3. 2290 | 3. 2500 | 3. 14170 | 3. 2068 | 3.2500 | 3. 13460 | 3. 13460 | 3. 2500 | 3. 2500 |
|  |  |  | 3. 2282 | 3. 2508 | 3. 14145 | 3. 2060 | 3. 2508 | 3. 13485 | 3. 13435 | 3. 2508 | 3. 2508 |
| 3. 250-8 | UN | 2 A | 3. 2303 | 3. 2474 | 3. 16620 | 3. 2116 | 3.2474 | 3. 15750 | 3. 15750 | 3. 2474 | 3. 2474 |
|  |  |  | 3. 2296 | 3. 2481 | 3. 16595 | 3. 2109 | 3.2481 | 3. 15775 | 3. 15725 | 3. 2481 | 3. 2481 |
|  |  | 3A | 3. 2329 | 3. 2500 | 3. 16880 | 3. 2164 | 3. 2500 | 3. 16230 | 3. 16230 | 3. 2500 | 3. 2500 |
|  |  |  | 3.2322 | 3. 2507 | 3. 16855 | 3. 2157 | 3. 2507 | 3. 16255 | 3. 16205 | 3. 2507 | 3. 2507 |
| 3. 250-12 | UN | 2A | 3. 2352 | 3. 2481 | 3. 19400 | 3.2238 | 3. 2481 | 3. 18770 | 3.18770 | 3.2481 | 3. 2481 |
|  |  |  | 3. 2346 | 3. 2487 | 3. 19375 | 3. 2232 | 3.2487 | 3. 18795 | 3. 18745 | 3.2487 | 3. 2487 |
|  |  | 3A | 3. 2371 | 3. 2500 | 3. 19590 | 3. 2273 | 3. 2500 | 3. 19120 | 3.19120 | 3. 2500 | 3. 2500 |
|  |  |  | 3. 2365 | 3.2506 | 3. 19565 | 3. 2267 | 3.2506 | 3. 19145 | 3. 19095 | 3. 2506 | 3. 2506 |

See footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Class | W truncated setting plugs |  |  |  |  |  |  | $\frac{\text { Basie-erest setting plugs }}{\text { Major diameter }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Plug for GO thread gage a |  |  | Plug for LO thread gage ${ }^{\text {a }}$ |  |  |  |  |  |
|  |  |  | Major diameter |  | Pitch diameter | Major diameter |  | Pitch diameter |  | Plug for GO thread gage a,b | $\begin{aligned} & \text { Plug for LO } \\ & \text { thread } \\ & \text { gage a,c } \end{aligned}$ |
|  |  |  | Truncated | Full |  | Truncated | Full | Plus tolerance gage | Minus toleranec gage | $W$ and $X$ tolerances | W and X tolerances |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 3. 250-16 | UN | 2 A | in | in | in | ${ }^{\text {in }}$ | in ${ }^{\text {3. } 2483}$ | $\begin{aligned} & \text { in } \\ & 3.20210 \end{aligned}$ | in3.20210 | in | in |
|  |  |  | 3.2378 | 3.2483 | 3. 20770 |  |  |  |  | 3.2483 | 3. 2483 |
|  |  |  | 3. 2372 | 3.2489 | 3. 20745 | 3. 2286 | 3.2489 | 3. 20235 | 3. 20185 | 3.2489 | 3. 2489 |
|  |  | 3 A | 3. 2395 | 3. 2500 | 3. 20940 | 3. 2323 | 3. 2506 | 3. 20520 | 3. 20495 | 3. 2500 | 3. 2506 |
|  |  |  | 3. 2389 | 3. 2506 | 3. 20915 | 3. 2317 |  | 3. 20545 |  | 3. 2506 |  |
| 3.375-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | 3. 3511 | 3.3721 | 3. 26380 | 3.3265 | 3. 3721 | 3.25430 | 3.25430 | 3.3721 | 3.3721 |
|  |  |  | 3. 3503 | 3. 37729 | 3. 263355 | 3. 3235 | 3. 37729 | 3. 25455 | 3. 25405 | 3. 3729 | 3. 3729 |
|  |  |  | 3. 3540 | 3.3750 3.3758 | 3. 266670 | 3. 3317 3.3309 | 3.3750 3.3758 | 3.25950 3.25975 | 3. 25950 | 3.3750 3.3758 | 3.3750 3.3758 |
|  |  |  | 3. 3532 | 3.3758 | 3. 26645 | 3.3309 | 3. 3758 | 3. 25975 | 3. 25925 | 3.3758 | 3. 3758 |
| 3. 375-8 | UN | 2 A | 3. 3553 | 3.3724 | 3. 29120 | 3. 3365 | 3. 3724 | 3. 28240 | 3. 28240 | 3. 3724 | 3. 3724 |
|  |  | $3 \mathrm{~A}$ | 3. 3546 | 3.3731 | 3. 29095 | 3. 3358 | 3. 3731 | 3. 28265 | 3. 28215 | 3. 3731 | 3. 3731 |
|  |  |  | 3. 3579 | 3. 3750 | 3. 29380 | 3. 3413 | 3. 3750 | 3. 28720 | 3. 28720 | 3.3750 | 3. 3750 |
|  |  |  | 3. 3572 | 3.3757 | 3. 29355 | 3.3406 | 3. 3757 | 3. 28745 | 3. 28695 | 3.3757 | 3. 3757 |
| 3. 375-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | 3. 3602 | 3.3731 | 3. 31900 | 3. 3487 | 3. 3731 | 3. 31260 | 3. 31260 | 3.3731 | 3.3731 |
|  |  |  | 3. 3596 | 3. 3737 | 3. 31875 | 3. 3481 | 3. 3737 | 3. 31285 | 3. 31235 | 3. 3737 | 3. 3737 |
|  |  |  | 3.3621 | 3. 3750 | 3. 32090 | 3. 3522 | 3. 3750 | 3. 31610 | 3. 31610 | 3. 3750 | 3. 3750 |
|  |  |  | 3.3615 | 3.3756 | 3.32065 | 3.3516 | 3. 3756 | 3.31635 | 3. 31585 | 3.3756 | 3. 3756 |
| 3. 375-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | 3.3628 | 3.3733 | 3. 33270 | 3. 3540 | 3. 3733 | 3. 32690 | 3. 32690 | 3. 3733 | 3. 3733 |
|  |  |  | 3. 3622 | 3. 3739 | 3. 33245 | 3. 3534 | 3. 3739 | 3. 32715 | 3. 32665 | 3. 3739 | 3. 3739 |
|  |  |  | 3. 3645 | 3.3750 | 3. 33440 | 3.3572 | 3. 3750 | 3. 33010 | 3. 33010 | 3. 3750 | 3. 3750 |
|  |  |  | 3. 3639 | 3. 3756 | 3. 33415 | 3. 3566 | 3. 3756 | 3.33035 | 3. 32985 | 3.3756 | 3. 3756 |
| 3. 500-4 | UNC | 1A | 3.4686 | 3.4967 | 3.33430 | 3.4260 | 3.4967 | 3. 31770 | 3.31770 | 3.4967 | 3.4967 |
|  |  |  | 3. 4677 | 3. 4976 | 3. 33405 | 3.4251 | 3.4976 | 3.31795 | 3.31745 | 3. 4976 | 3.4976 |
|  |  | 2 A | 3. 4686 | 3. 4967 | 3. 33430 | 3.4316 | 3.4967 | 3. 32330 | 3. 32330 | 3. 4967 | 3. 4967 |
|  |  |  | 3. 4677 | 3. 4976 | 3. 33405 | 3.4307 | 3.4976 | 3. 32355 | 3. 32305 | 3. 4976 | 3. 4976 |
|  |  | 3 A | 3. 4719 | 3. 5000 | 3. 33760 | 3.4376 | 3. 5000 | 3. 32930 | 3. 32930 | 3. 5000 | 3. 5000 |
|  |  |  | 3. 4710 | 3. 5009 | 3. 33735 | 3.4367 | 3.5009 | 3. 32955 | 3. 32905 | 3. 5009 | 3. 5009 |
| 3. 500-6 | UN | 24$3 A$ | 3. 4761 | 3.4971 | 3. 38880 | 3. 4514 | 3. 4971 | 3. 37920 | 3. 37920 | 3. 4971 | 3. 4971 |
|  |  |  | 3. 4753 | 3. 4979 | 3. 38855 | 3. 4506 | 3.4979 | 3. 37945 | 3. 37895 | 3. 4979 | 3. 4979 |
|  |  |  | 3. 4790 | 3. 5000 | 3. 39170 | 3. 4567 | 3. 5000 | 3. 38450 | 3. 38450 | 3. 5000 | 3. 5000 |
|  |  |  | 3. 4782 | 3. 5008 | 3. 39145 | 3. 4559 | 3. 5008 | 3. 38475 | 3. 38425 | 3. 5008 | 3. 5008 |
| 3. $500-8$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | 3. 4803 | 3.4974 | 3. 41620 | 3. 4615 | 3. 4974 | 3. 40740 | 3. 40740 | 3.4974 |  |
|  |  |  | 3. 4796 | 3. 4981 | 3. 41595 | 3. 4608 | 3. 4981 | 3. 40765 | 3. 40715 | 3. 4981 | 3. 4981 |
|  |  |  | 3.4829 | 3. 5400 | 3. 41880 | 3. 4663 | 3. 5000 | 3. 41220 | 3.41220 | 3. 5000 | 3. 5000 |
|  |  |  | 3. 4822 | 3.5007 | 3. 41855 | 3.4656 | 3. 5007 | 3. 41245 | 3. 41195 | 3. 5007 | 3. 5007 |
| 3. 500-12 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ |  |  | 3. 44400 | 3. 4737 |  | 3. 43760 | 3.43760 | 3. 4981 | 3. 4981 |
|  |  |  | 3. 4846 | 3. 4987 | 3. 44375 | 3. 4731 | 3. 4987 | 3. 43785 | 3.43735 | 3. 4987 | 3. 4987 |
|  |  |  | 3. 4871 | 3. 5000 | 3. 44590 | 3.4772 | 3. 5000 | 3.44110 | 3.44110 | 3. 5000 | 3. 5000 |
|  |  |  | 3. 4865 | 3. 5006 | 3. 44565 | 3.4766 | 3. 5006 | 3. 44135 | 3.44085 | 3.5006 | 3. 5006 |
| 3. $500-16$ | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ |  |  |  | 3. 4790 | 3. 4983 | 3.45190 | 3. 45190 | 3. 4983 | 3. 4983 |
|  |  |  | 3. 4872 | 3. 4989 | 3. 45745 | 3. 4784 | 3. 4989 | 3. 45215 | 3.45165 | 3. 4989 | 3. 4989 |
|  |  |  | 3. 4895 | 3. 5000 | 3. 45940 | 3.4822 | 3. 5000 | 3. 45510 | 3.45510 | 3. 5000 | 3. 5000 |
|  |  |  | 3. 4889 | 3. 5006 | 3. 45915 | 3.4816 | 3.5006 | 3. 45535 | 3. 45485 | 3. 5006 | 3. 5006 |
| 3. 625-6 | UN | 2 A | 3. 6011 | 3. 6221 | 3. 51380 | 3. 5763 | 3.6221 | 3. 50410 | 3. 50410 | 3. 6221 | 3. 6221 |
|  |  |  | 3. 6003 | 3. 6229 | 3.51355 | 3.5755 | 3.6229 | 3. 50435 | 3. 50385 | 3. 6229 | 3. 6229 |
|  |  | 3 A | 3. 6040 | 3.6250 | 3. 51670 | 3.5816 | 3. 6250 | 3. 50940 | 3. 50940 | 3. 6250 | 3. 6250 |
|  |  |  | 3. 6032 | 3. 6258 | 3. 51645 | 3. 5808 | 3.6258 | 3. 50965 | 3. 50915 | 3. 6258 | 3. 6258 |
| 3. $625-8$ | UN | 2 A | 3. 6052 | 3.6223 | 3.54110 | 3. 5863 | 3. 6223 | 3. 53220 | 3.53220 | 3. 6223 | 3. 6223 |
|  |  |  | 3. 6045 | 3. 6230 | 3. 54085 | 3. 5856 | 3.6230 | 3. 53245 | 3. 53195 | 3. 6230 | 3. 6230 |
|  |  | 3A | 3. 6079 | 3. 6250 | 3. 54380 | 3. 5912 | 3. 6250 | 3. 53710 | 3. 53710 | 3. 6250 | 3. 6250 |
|  |  |  | 3. 6072 | 3.6257 | 3. 54355 | 3. 5905 | 3.6257 | 3. 53735 | 3. 53685 | 3. 6257 | 3. 6257 |
| 3. 625-12 | UN | 2 A | 3.6102 | 3.6231 | 3. 56900 | 3. 5987 | 3.6231 | 3. 56260 | 3. 56260 | 3. 6231 | 3. 6231 |
|  |  |  | 3. 6096 | 3. 6237 | 3. 56875 | 3.5981 | 3. 6237 | 3. 56285 | 3. 56235 | 3. 6237 | 3. 6237 |
|  |  | 3 A | 3.6121 | 3. 6250 | 3. 57090 | 3. 6022 | 3. 6250 | 3. 56610 | 3. 56610 | 3. 6250 | 3. 6250 |
|  |  |  | 3. 6115 | 3. 6256 | 3. 57065 | 3.6016 | 3.6256 | 3. 56635 | 3. 56585 | 3. 6256 | 3. 6256 |
| 3. 625-16 | UN | 2 A3 A | 3.6128 | 3.6233 | 3. 58270 | 3.6040 | 3. 6233 | 3.57690 | 3. 57690 | 3. 6233 | 3.6233 |
|  |  |  | 3. 6122 | 3. 6239 | 3. 58245 | 3. 6034 | 3.6239 | 3. 57715 | 3. 57665 | 3. 6239 | 3. 6239 |
|  |  |  | 3.6145 | 3. 6250 | 3. 58440 | 3. 6072 | 3. 6250 | 3. 58010 | 3. 58010 | 3. 6250 | 3. 6250 |
|  |  |  | 3. 6139 | 3. 6256 | 3. 58415 | 3. 6066 | 3.6256 | 3. 58035 | 3. 57985 | 3.6256 | 3.6256 |
| 3. 750-4 | UNC | 14 | 3. 7185 | 3. 7466 | 3. 58420 | 3. 6757 | 3. 7466 | 3.56740 | 3. 56740 | 3. 7466 | 3.7466 |
|  |  |  | 3.7176 | 3. 7475 | 3.58395 | 3. 6748 | 3. 7475 | 3. 56765 | 3. 56715 | 3. 7475 | 3. 7475 |
|  |  | 2 A | 3. 7185 | 3. 7466 | 3. 58420 | 3. 6813 | 3.7466 | 3. 57300 | 3. 57300 | 3. 7466 | 3. 7466 |
|  |  |  | 3. 7176 | 3. 7475 | 3. 58395 | 3. 6804 | 3.7475 | 3. 57325 | 3. 57275 | 3.7475 | 3. 7475 |
|  |  | 3A | 3. 7219 | 3. 7500 | 3. 58760 | 3.6875 | 3.7500 | 3. 57920 | 3. 57920 | 3. 7500 | 3. 7500 |
|  |  |  | 3. 7210 | 3. 7509 | 3.58735 | 3.6866 | 3.7509 | 3. 57945 | 3. 57895 | 3. 7509 | 3. 7509 |

See footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued


See footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Class | W truncated setting plugs |  |  |  |  |  |  | $\frac{\text { Basie-crest setting plugs }}{\text { Major diameter }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Plug for GO thread gage * |  |  | Plug for LO thread gage ${ }^{\text {a }}$ |  |  |  |  |  |
|  |  |  | Major diameter |  | Pitch diameter | Major diameter |  | Pitch diameter |  | Plug for GO thread gage $\mathrm{a}, \mathrm{b}$ | Plug for LO thread gage a, |
|  |  |  | Truncated | Full |  | 'runcated | Full | Plus tolerance gage | Minus tolerance gage | W and $X$ tolerances | W and X tolerances |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 4. 250-4 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | in | in | in | in | in | in | in |  | in |
|  |  |  | 4. 2185 | 4. 2466 | 4. 0842 | 4. 1810 | 4. 2466 | 4. 0727 | 4.0727 | 4. 2466 | 4. 2466 |
|  |  |  | 4. 2170 | 4. 2481 | 4.0839 | 4.1795 | 4. 2481 | 4.0730 | 4.0724 | 4. 2481 | 4. 2481 |
|  |  |  | 4. 22219 | 4. 2500 4.2515 | 4.0876 4.0873 | 4.1873 4.1858 | 4. 2500 4.2515 | 4.0790 4.0793 | 4.0790 4.0787 | 4. 2500 4.2515 | 4. 2500 |
| 4. 250-6 | UN | 2 A | 4. 2260 | 4. 2470 | 4. 1387 | 4. 2008 | 4.2470 | 4. 1286 | 4. 1286 | 4. 2470 | 4. 2470 |
|  |  |  | 4. 2247 | 4. 2483 | 4. 1384 | 4. 1995 | 4. 2483 | 4. 1289 | 4. 1283 | 4.2483 | 4. 2483 |
|  |  | 3A | 4. 2290 | 4. 2500 | 4. 1417 | 4. 2064 | 4. 2500 | 4. 1342 | 4. 1342 | 4. 2500 | 4. 2500 |
|  |  |  | 4. 2277 | 4.2513 | 4. 1414 | 4. 2051 | 4. 2513 | 4. 1345 | 4. 1339 | 4. 2513 | 4.2513 |
| 4. 250-12 | UN | 2 A | 4. 2351 | 4. 2480 | 4. 1939 | 4. 2235 | 4. 2480 | 4. 1874 | 4. 1874 | 4. 2480 | 4. 2480 |
|  |  |  | 4. 2342 | 4. 2489 | 4. 1936 | 4. 2226 | 4. 2489 | 4. 1877 | 4.1871 | 4. 2489 | 4. 2489 |
|  |  | 3A | 4. 2371 | 4. 2500 | 4. 1959 | 4. 2271 | 4. 2500 | 4. 1910 | 4. 1910 | 4. 2500 | 4. 2500 |
|  |  |  | 4. 2362 | 4. 2509 | 4. 1956 | 4. 2262 | 4.2509 | 4. 1913 | 4. 1907 | 4. 2509 | 4. 2509 |
| 4. $250-16$ | UN | 2 A | 4. 2377 | 4. 2482 | 4. 2076 | 4. 2288 | 4. 2482 | 4. 2017 | 4. 2017 | 4. 2482 | 4. 2482 |
|  |  |  | 4. 2368 | 4.2491 | 4. 2073 | 3. 2279 | 4. 2491 | 4. 2020 | 4. 2014 | 4. 2491 | 4. 2491 |
|  |  | 3 A | 4. 2395 | 4. 2500 | 4. 2094 | 4. 2321 | 4. 2500 | 4. 2050 | 4. 2050 4.2047 | 4.2500 4.2509 | 4. 2500 |
| 4.375-6 | UN | 2A | 4.3510 | 4. 3720 | 4. 2637 | 4.3258 | 4.3720 | 4. 2536 | 4. 2536 | 4.3720 | 4.3720 |
|  |  |  | 4.3497 | 4. 3733 | 4.2634 | 4. 3245 | 4. 3733 | 4.2539 | 4. 2533 | 4.3733 | 4.3733 |
|  |  | 3A | 4. 3540 | 4. 3750 | 4. 2667 | 4.3313 | 4. 3750 | 4. 2591 | 4.2591 | 4. 3750 | 4.3750 |
|  |  |  | 4.3527 | 4.3763 | 4. 2664 | 4.3300 | 4.3763 | 4. 2594 | 4. 2588 | 4.3763 | 4. 3763 |
| 4.375-12 | UN | 2 A | 4. 3601 | 4. 3730 | 4.3189 | 4.3485 | 4. 3730 | 4. 3124 | 4. 3124 | 4. 3730 | 4. 3730 |
|  |  |  | 4.3592 | 4. 3739 | 4.3186 | 4.3476 | 4. 3739 | 4. 3127 | 4.3121 | 4. 3739 | 4. 3739 |
|  |  | 3A | 4. 3621 4.3612 | 4.3750 4.3759 | 4.3209 4.3206 | 4.3521 4.3512 | 4. 3750 4.3759 | 4. 3160 4.3163 | 4.3160 4.3157 | 4. 3750 4.3759 | 4. 3750 4.3759 |
| 4. 375-16 | UN | 2 A | 4.3627 | 4.3732 | 4.3326 | 4.3538 | 4.3732 | 4. 3267 | 4.3267 | 4.3732 | 4. 3732 |
|  |  |  | 4.3618 | 4. 3741 | 4.3323 | 4. 3529 | 4. 3741 | 4. 3270 | 4. 3264 | 4. 3741 | 4. 3741 |
|  |  | 3 A | 4. 3645 | 4. 3750 | 4. 3344 | 4. 3571 | 4. 3750 | 4. 3300 | 4. 3300 | 4. 3750 | 4. 3750 |
|  |  |  | 4.3636 | 4.3759 | 4. 3341 | 4.3562 | 4. 3759 | 4. 3303 | 4.3297 | 4. 3759 | 4. 3759 |
| 4. $500-4$ | UN | 2 A | 4. 4684 | 4.4965 | 4. 3341 | 4.4308 | 4. 4965 | 4. 3225 | 4. 3225 | 4. 4965 | 4. 4965 |
|  |  |  | 4. 4669 | 4. 4980 | 4. 3338 | 4.4293 | 4. 4980 | 4. 3228 | 4. 3222 | 4. 4980 | 4. 4980 |
|  |  | 3A | 4. 4719 4.4704 | 4.5000 4.5015 | 4. 3376 4.3373 | 4. 4372 4.4357 | 4. 5000 | 4. 3289 4.3292 | 4. 3289 4.3286 | 4. 5000 4.5015 | 4. 5000 |
| 4. $500-6$ | UN | 2 A | 4. 4759 |  | 4. 3886 |  |  |  | 4. 3784 | 4.4969 | 4. 4969 |
|  |  |  | 4. 4746 | 4.4982 | 4. 3883 | 4. 4493 | 4. 4982 | 4. 3787 | 4. 3781 | 4. 4982 | 4. 4982 |
|  |  | 3A | 4. 4790 | 4. 5000 | 4. 3917 | 4. 4562 | 4. 5000 | 4. 3840 | 4. 3840 | 4. 5000 | 4. 5000 |
|  |  |  | 4.4777 | 4.5013 | 4.3914 | 4. 4549 | 4. 5013 | 4. 3843 | 4.3837 | 4.5013 | 4.5013 |
| 4. $500-12$ | UN | 2 A | 4. 4851 | 4. 4980 | 4.4439 | 4. 4735 | 4. 4980 | 4. 4374 | 4. 4374 | 4. 4980 | 4. 4980 |
|  |  |  | 4. 4842 | 4. 4989 | 4. 4436 | 4. 4726 | 4. 4989 | 4. 4377 | 4. 4371 | 4. 4989 | 4. 4989 |
|  |  | 3A | 4. 4871 | 4. 5000 | 4. 4459 | 4. 4771 | 4. 5000 | 4. 4410 | 4. 4410 | 4. 5000 | 4. 5000 |
|  |  |  | 4. 4862 | 4.5009 | 4. 4456 | 4. 4762 | 4. 5009 | 4.4413 | 4. 4407 | 4.5009 | 4. 5009 |
| 4. 500-16 | UN | 2 A | 4. 4877 | 4. 4982 | 4. 4576 | 4. 4788 | 4. 4982 | 4. 4517 | 4. 4517 | 4.4982 | 4. 4982 |
|  |  |  | 4. 4868 | 4. 4991 | 4.4573 | 4.4779 | 4. 4991 | 4.4520 | 4. 4514 | 4.4991 | 4. 4991 |
|  |  | 3 A | 4. 4895 | 4. 5000 | 4. 4594 | 4.4821 | 4. 5000 | 4.4550 | 4. 4550 | 4.5000 | 4. 5000 |
|  |  |  | 4.4886 | 4. 5009 | 4.4591 | 4. 4812 | 4. 5009 | 4.4553 | 4. 4547 | 4.5009 | 4. 5009 |
| 4. 625-6 | UN | 2 A | 4. 6009 | 4.6219 | 4. 5136 | 4. 5755 | 4.6219 | 4. 5033 | 4. 5033 | 4. 6219 | 4. 6219 |
|  |  |  | 4. 5996 | 4. 6232 | 4. 5133 | 4. 5742 | 4. 6232 | 4. 5036 | 4. 5030 | 4.6232 | 4. 6232 |
|  |  | 3 A | 4. 6040 | 4. 6250 | 4. 5167 | 4. 5812 | 4. 6250 | 4. 5090 | 4. 5090 | 4.6250 4.6263 | 4. 6250 |
|  |  |  | 4. 6027 | 4.6263 | 4.5164 | 4. 5799 | 4.6263 | 4.5093 | 4.5087 | 4.6263 | 4.6263 |
| 4. 625-12 | UN | 2 A | 4.6101 | 4. 6230 | 4. 5689 | 4. 5983 | 4. 6230 | 4. 5622 | 4. 5622 | 4.6230 | 4. 6230 |
|  |  |  | 4. 6092 | 4. 6239 | 4. 5686 | 4. 5974 | 4. 6239 | 4. 5625 | 4. 5619 | 4.6239 | 4. 6239 |
|  |  | 3 A | 4. 6121 | 4. 6250 | 4. 5709 | 4. 6020 | 4.6250 | 4.5659 | 4. 5659 | 4.6250 | 4. 6250 |
|  |  |  | 4.6112 | 4.6259 | 4.5706 | 4.6011 | 4. 6259 | 4.5662 | 4.5656 | 4.6259 | 4. 6259 |
| 4. 625-16 | UN | 2 A | 4. 6127 | 4. 6232 | 4. 5826 | 4. 6036 | 4. 6232 | 4.5765 | 4. 5765 | 4.6232 | 4. 6232 |
|  |  |  | 4. 6118 | 4. 6241 | 4. 5823 | 4. 6027 | 4. 6241 | 4. 5768 | 4. 5762 | 4. 6241 | 4. 6241 |
|  |  | 3A | 4. 6145 | 4. 6250 | 4. 5844 | 4. 6070 | 4. 6250 | 4. 5799 | 4. 5799 | 4. 6250 | 4. 6250 |
|  |  |  | 4. 6136 | 4. 6259 | 4. 5841 | 4. 6061 | 4. 6259 | 4.5802 | 4.5796 | 4.6259 | 4.6259 |
| 4. 750-4 | UN | 2 A | 4. 7184 | 4. 7465 | 4. 5841 | 4. 6807 | 4. 7465 | 4. 5724 | 4. 5724 | 4. 7465 | 4. 7465 |
|  |  |  | 4. 7169 | 4. 7480 | 4. 5838 | 4. 6792 | 4. 7480 | 4. 5727 | 4. 5721 | 4. 7480 | 4. 7480 |
|  |  | 3A | 4. 7219 | 4. 7500 | 4. 5876 | 4. 6871 | 4. 7500 | 4. 5788 | 4. 5788 | 4. 7500 | 4. 7500 |
|  |  |  | 4. 7204 | 4.7515 | 4. 5873 | 4.6856 | 4.7515 | 4.5791 | 4. 5785 | 4.7515 | 4.7515 |

See footnotes at end of table.

Table 6.20. Setting plug gages, Unified screw threads-Continued

| Nominal size and threads per inch | Series designation | Class | W truncated setting plugs |  |  |  |  |  |  | $\frac{\text { Basic-crest setting plugs }}{\text { Major diameter }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Plug for GO thread gage a |  |  | Plug for LO thread gage ${ }^{\text {a }}$ |  |  |  |  |  |
|  |  |  | Major diameter |  | Pitch diameter | Major diameter |  | Piteh diameter |  | Plug for GO thread gage ${ }^{\text {a,b }}$ | Plug for LO thread gage ${ }^{a}$, |
|  |  |  | Truncated | Full |  | Truncated | Full | Plus tolerance gage | Minus toleranee gage | $W$ and X tolerances | $W$ and X tolerances |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 4. 750-6 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | in | in | in | in | in. | in | in | in | in |
|  |  |  | 4. 7259 | 4. 7469 | 4. 6386 | 4. 7005 | 4. 7469 | 4. 6283 | 4. 6283 | 4. 7469 | 4. 7469 |
|  |  |  | 4. 7246 | 4.7482 | 4.6383 | 4. 6992 | 4. 7482 | 4.6286 | 4.6280 | 4.7482 | 4.7482 |
|  |  |  | 4. 7290 | 4. 7500 | 4. 6417 | 4. 7062 | 4. 7500 | 4.6340 | 4. 6340 | 4.7500 | 4.7500 |
|  |  |  | 4. 7277 | 4.7513 | 4.6414 | 4. 7049 | 4. 7513 | 4.6343 | 4. 6337 | 4.7513 | 4. 7513 |
| 4. 750-12 | UN | 2 A | 4. 7351 | 4. 7480 | 4. 6939 | 4. 7233 | 4. 7480 | 4. 6872 | 4. 6872 | 4. 7480 | 4. 7180 |
|  |  |  | 4. 7342 4. 7371 | 4. 7489 | 4. 69336 | 4. 7224 | 4. 7489 | 4. 6875 | 4. 6869 | 4. 7489 | 4.7489 |
|  |  | 3A | 4. <br> 4. 7371 | 4. 7500 4.7509 | 4. 6959 4.6956 | 4. 7270 4.7261 | 4. 7500 4.7509 | 4. 6909 4.6912 | 4. 6909 4.6906 | 4.7500 4.7509 | 4. 7500 4.7509 |
| 4. 750-16 | UN | 2 A | 4. 7377 | 4. 7482 | 4. 7076 | 4. 7286 | 4. 7482 | 4. 7015 | 4. 7015 | 4.7482 | 4. 7482 |
|  |  |  | 4. 7368 | 4. 7491 | 4. 7073 | 4. 7277 | 4. 7491 | 4. 7018 | 4. 7012 | 4.7491 | 4. 7491 |
|  |  | 3 A | 4. 7395 | 4. 7500 | 4. 7094 | 4. 7320 | 4. 7500 | 4. 7049 | 4. 7049 | 4. 7500 | 4. 7500 |
|  |  |  | 4. 7386 | 4. 7509 | 4.7091 | 4. 7311 | 4. 7509 | 4. 7052 | 4.7046 | 4. 7509 | 4. 7509 |
| 4. 875-6 | UN | 2 A | 4. 8509 | 4. 8719 | 4. 7636 | 4.8254 | 4.8719 | 4. 7532 | 4.7532 | 4. 8719 | 4. 8719 |
|  |  |  | 4. 8496 4.8540 | 4.8732 4.8750 | 4. 7633 4.7667 | 4.8241 4.8311 | 4. 8732 4.8750 | 4. 7535 4.7589 | 4. 7529 4.7589 | 4.8732 4.8750 | 4. 8732 4.8750 |
|  |  | 3 A | 4.8840 4.8527 | 4.8763 | 4. 7664 | 4.8811 4.8298 | 4.8763 | 4.75892 | 4. 7586 | 4.8763 | 4.8780 4.8763 |
| 4. 875-12 | UN | 2 A | 4.8601 | 4. 8730 | 4. 8189 | 4.8483 | 4. 8730 | 4. 8122 | 4.8122 | 4.8730 | 4. 8730 |
|  |  | 3A | 4.8592 4.8621 | 4.8739 4.8750 | 4.8186 4.8209 | 4.8474 4.8520 | 4.8739 4.8750 | 4. 8125 4.8159 | 4.8119 4.8159 | 4. 8739 4.8750 | 4.8739 4.8750 |
|  |  |  | 4.8612 | 4.8759 | 4. 8206 | 4.8511 | 4.8759 | 4.8162 | 4.8156 | 4.8759 | 4.8759 |
| 4. $875-16$ | UN | 2 A | 4. 8627 | 4.8732 | 4. 8326 | 4. 8536 | 4. 8732 | 4. 8265 | 4. 8265 | 4.8732 | 4.8732 |
|  |  |  | 4.8618 | 4.8741 | 4. 8323 | 4.8527 | 4.8741 | 4. 8268 | 4. 8262 | 4. 8741 | 4. 8741 |
|  |  | 3 A | 4.8645 4.8636 | 4.8750 4.8759 | 4.8344 4.8341 | 4.8570 4.8561 | 4. 8750 4.8759 | 4.8299 4.8302 | 4.8299 4.8296 | 4. 8750 | 4.8750 4.8759 |
| 5. 000-4 | UN | 2 A | 4.9683 | 4. 9964 | 4.8340 | 4. 9304 | 4. 9964 | 4.8221 | 4.8221 | 4. 9964 | 4. 9964 |
|  |  |  | 4. 9668 | 4. 9979 | 4. 8337 | 4.9289 | 4. 9979 | 4.8224 | 4.8218 | 4. 9979 | 4. 9979 |
|  |  | 3 A | 4.9719 4.9704 | 5.0000 | 4.8376 | 4.9370 | 5. 0000 | 4. 8287 | 4. 8287 | 5. 50000 | 5. 0000 |
|  |  |  | 4. 9704 | 5.0015 | 4.8373 | 4.9355 | 5. 0015 | 4.8290 | 4. 8284 | 5. 0015 | 5. 0015 |
| 5. $0000-6$ | UN | 2 A | 4.9759 | 4. 9969 | 4.8886 | 4.9503 | 4.9969 | 4.8781 | 4. 8781 | 4. 9969 | 4. 9969 |
|  |  |  | 4.9746 | 4. 9982 | 4.8883 | 4. 9490 | 4. 9988 | 4.8784 | 4.8778 | 4. 9982 | 4. 9982 |
|  |  | 3A | 4. 9790 | 5. 0000 | 4.8917 | 4. 9561 | 5. 0000 | 4.8839 | 4.8839 4.8836 | 5. 0000 | 5. 0000 |
|  |  |  | 4.9777 | 5. 0013 | 4.8914 | 4. 9548 | 5.0013 | 4.8812 | 4.8836 | 5. 0013 | 5. 0013 |
| 5. $000-12$ | UN | 2 A | 4. 9851 | 4. 9980 | 4.9439 | 4. 9733 | 4. 9980 | 4.9372 | 4.9372 | 4. 9980 | 4. 9980 |
|  |  |  | 4.9842 | 4. 9989 | 4. 94346 | 4.9724 4 4 | 4. 9989 | 4. 9375 | 4. 9369 4 4.9409 | 4. 9989 | 4. 9989 |
|  |  | 3A | 4. 9871 4.9862 | 5. 0000 5.0009 | 4. 9459 4.9456 | 4. 9770 4. 9761 | 5. 0000 | 4. 9409 4.9412 | 4. 9409 4.9406 | 5. 0000 5. 0009 | 5. 0000 |
| 5. $000-16$ | UN | 2 A | 4.9877 | 4. 9982 | 4. 9576 | 4. 9786 | 4. 9982 | 4.9515 | 4. 9515 | 4.9982 | 4. 9982 |
|  |  |  | 4. 9868 | 4. 9991 | 4. 9573 | 4. 9777 | 4.9991 | 4.9518 | 4. 9512 | 4. 9991 | 4. 9991 |
|  |  | 3 A | 4. 9895 4.9886 | 5. 0000 | 4. 9594 | 4. 9820 | 5. 0000 5. 0009 | 4. 9549 | 4.9549 4.9546 | 5.0000 5.0009 | 5. 50000 |
| 5. 125-12 | UN | 2 A |  |  | 5. 0689 | 5. 0983 | 5. 1230 | 5. 0622 | 5. 0622 | 5. 1230 | 5. 1230 |
|  |  |  | 5. 1092 | 5. 1239 | 5.0686 | 5.0974 | 5. 1239 | 5. 0625 | 5.0619 | 5. 1239 | 5. 1239 |
|  |  | 3 A | 5. 1121 | 5. 1250 | 5. 0709 | 5. 1020 | 5. 1250 | 5. 0659 | 5. 0659 | 5. 1250 | 5. 1250 |
|  |  |  | 5. 1112 | 5. 1259 | 5. 0706 | 5. 1011 | 5. 1259 | 5. 0662 | 5.0656 | 5. 1259 | 5. 1259 |
| 5. 125-16 | UN | 2 A | 5.1127 | 5. 1232 | 5. 0826 | 5. 1036 | 5. 1232 | 5.0765 | 5.0765 | 5. 1232 | 5. 1232 |
|  |  |  | 5. 1118 | 5. 1241 | 5. 0823 | 5. 1027 | 5. 1241 | 5.0768 | 5. 0762 | 5. 1241 | 5. 1241 |
|  |  | 3 A | 5.1145 5.1136 | 5. 1250 5. 1259 | 5.0844 5.0841 | 5. 1070 5. 1061 | 5.1250 5.1259 | 5.0799 5.0802 | 5. 0799 5.0796 | 5. 12250 5.1259 | 5. 1250 5. 1259 |
| 5. 250-4 | UN | 2 A | 5. 2183 | 5. 2464 | 5. 0840 | 5. 1803 | 5. 2464 | 5. 0720 | 5.0720 | 5. 2464 | 5. 2464 |
|  |  |  | 5. 2168 | 5. 2479 | 5. 0837 | 5. 1788 | 5. 2479 | 5. 0723 | 5. 0717 | 5. 2479 | 5. 2479 |
|  |  | 3 A | 5. 2219 | 5. 2500 | 5.0876 | 5. 1869 | 5. 2500 | 5.0786 | 5. 0786 | 5. 2500 | 5. 2500 |
|  |  |  | 5. 2204 | 5. 2515 | 5. 0873 | 5. 1854 | 5.2515 | 5. 0789 | 5.0783 | 5. 2515 | 5.2515 |
| 5. 250-12 | UN | 2 A | 5. 2351 | 5. 2480 | 5. 1939 | 5. 2233 | 5. 2480 | 5. 1872 | 5. 1872 | 5. 2480 | 5. 2480 |
|  |  |  | 5. 2342 | 5. 2489 | 5. 1936 | 5. 2224 | 5. 2489 | 5.1875 | 5. 1869 | 5. 2489 | 5. 2489 |
|  |  | 3A | 5. 2371 | 5. 2500 | 5. 1959 | 5. 2270 | 5. 2500 | 5. 1909 | 5. 1909 | 5. 2500 | 5. 2500 |
|  |  |  | 5. 2362 | 5. 2509 | 5. 1956 | 5. 2261 | 5. 2509 | 5. 1912 | 5.1906 | 5. 2509 | 5. 2509 |
| 5. 250-16 | UN | 2 A | 5. 2377 | 5. 2482 | 5. 2076 | 5. 2286 | 5. 2482 | 5. 2015 | 5. 2015 | 5. 2482 | 5. 2482 |
|  |  |  | 5. 2368 | 5. 2491 | 5. 2073 | 5. 2277 | 5. 2491 | 5. 2018 | 5. 2012 | 5. 2491 | 5. 2491 |
|  |  | 3 A | 5. 2395 | 5. 2500 | 5. 2094 | 5. 2320 | 5.2500 | 5. 2049 | 5. 2049 | 5. 2500 | 5. 2500 |
|  |  |  | 5.2386 | 5.2509 | 5. 2091 | 5. 2311 | 5. 2509 | 5. 2052 | 5. 2046 | 5. 2509 | 5. 2509 |
| 5. $375-12$ | UN | 2A | 5. 3601 | 5. 3730 | 5. 3189 | 5. 3483 | 5. 3730 | 5. 3122 | 5. 3122 | 5. 3730 | 5. 3730 |
|  |  |  | 5. 3592 | 5. 3739 | 5. 3186 | 5. 3474 | 5. 3739 | 5. 3125 | 5. 3119 | 5. 3739 | 5. 3739 |
|  |  | 3A | 5. 3621 | 5. 3750 | 5. 3209 | 5. 3520 | 5. 3750 | 5.3159 | 5. 3159 | 5. 3750 | 5. 3750 |
|  |  |  | 5.3612 | 5. 3759 | 5. 3206 | 5.3511 | 5. 3759 | 5. 3162 | 5.3156 | 5. 3759 | 5. 3759 |

See footnotes at end of table.

Table 6.20. Setting plug gages, Unified serew threads-Continued

| Nominal size and threads per ineh | Series designation | Class | W truncated setting plugs |  |  |  |  |  |  | $\frac{\text { Basie-erest setting plugs }}{\text { Major diameter }}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Plug for GO thread gage a |  |  | Plug for Lo thread gage ${ }^{\text {a }}$ |  |  |  |  |  |
|  |  |  | Major diameter |  | Piteh diameter | Major diameter |  | Pitch diameter |  | Plug for GO thread gage ${ }^{\text {a,b }}$ | Plug for LO thread gage $\mathbf{a}^{\text {, }}$ |
|  |  |  | Truneated | Full |  | Truncated | Full | Plus toleranee gage | Minus toleranee gage | W and X tolerances | W and X toleranees |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| 5. 375-16 | UN | $\begin{aligned} & 2 \mathrm{~A} \\ & 3 \mathrm{~A} \end{aligned}$ | in 5. 3627 5. 3618 5. 3645 5. 3636 | in 5.3732 5.3741 5.3750 5.3759 | in 5. 3326 5.3323 5.3344 5.3341 | in 5. 5.336 5. 5.327 5. 55601 | in 5. 5732 5.341 5.3750 5.3759 | in 5.3265 5.3268 5.3299 5.3302 | in 5. 3265 5. 3262 5.3299 5.3296 | in 5.3732 5.3741 5.3750 5.3759 | in 5. 5. 5.332 5. 3741 5.3750 5.379 |
| 5. 500-4 | UN | 2 A | 5. 4683 | 5. 4964 | 5. 3340 | 5. 4302 | 5. 4964 | 5. 3219 | 5. 3219 | 5. 4964 | 5. 4964 |
|  |  | 3A | 5.4668 5.4719 | 5.4979 5.5000 | 5. 3337 5. 3376 | 5. 4287 5. 4368 | 5. 4979 5. 5000 | 5. 3222 5.3285 | 5.3216 5.3285 | 5. 4979 5. 5000 | 5. 4979 5. 5000 |
|  |  |  | 5.4704 | 5. 5015 | 5. 3373 | 5. 4353 | 5. 5015 | 5.3288 | 5. 3282 | 5. 5015 | 5. 5009 |
| 5. 500-12 | UN | 2 A | 5. 4851 5. 4842 | 5. 4980 | 5. 4439 5. 4436 | 5. 4733 5.4724 | 5. 4980 | 5. 4372 5. 4375 | 5. 4372 5. 4369 | 5. 4980 5.4989 | 5. 4980 5. 4989 |
|  |  | 3A | 5. 4871 | 5. 5000 | 5. 4459 | 5. 4770 | 5. 5000 | 5. 4409 | 5.4409 | 5. 5000 | 5.5000 |
|  |  |  | 5. 4862 | 5.5009 | 5. 4456 | 5. 4761 | 5. 5009 | 5. 4412 | 5. 4406 | 5. 5009 | 5. 5009 |
| 5. 500-16 | UN | 2 A | 5. 4877 5. 4868 | 5. 4982 5.4991 | 5. 4576 | 5. 4786 5. 4777 | 5. 4982 5. 4991 | 5. 4515 5. 4518 | 5.4515 5.4512 | 5. 4982 5. 4991 | 5. 4982 |
|  |  | $3 \mathrm{~A}$ | 5. 4895 | 5. 5000 | 5. 4594 | 5. 4820 | 5. 5000 | 5. 4549 | 5. 4549 | 5. 5000 | 5. 5000 |
|  |  |  | 5. 4886 | 5. 5009 | 5. 4591 | 5. 4811 | 5. 5009 | 5. 4552 | 5. 4546 | 5. 5009 | 5. 5009 |
| 5. 625-12 | UN | 2A | 5. 6100 5. 6091 | 5. 6229 5. 6238 | 5. 5688 5. 5685 | 5. 5980 5. 5971 | 5. 6229 5. 6238 | 5. 5619 5. 5622 | 5. 5619 | 5. 6229 5.6238 | 5. 6229 5. 6238 |
|  |  | 3A | 5. 6121 | 5. 6250 | 5. 5709 | 5. 6018 | 5. 6250 | 5. 5657 | 5. 5657 | 5. 6250 | 5. 6250 |
|  |  |  | 5. 6112 | 5. 6259 | 5. 5706 | 5. 6009 | 5.6259 | 5. 5660 | 5.5654 | 5. 6259 | 5. 6259 |
| 5.625-16 | UN | 2A | 5.6126 | 5.6231 | 5. 5825 | 5.6034 | 5. 6231 | 5. 5763 | 5. 5763 | 5.6231 | 5. 6231 |
|  |  |  | 5. 6117 | 5. 6240 | 5. 5822 | 5. 6025 | 5. 6240 | 5. 5766 | 5. 5760 | 5. 6240 | 5. 6240 |
|  |  | 3A | 5. 6145 | 5. 6250 | 5. 5844 | 5. 6068 | 5. 6250 | 5. 5797 | 5. 5797 | 5.6250 | 5.6250 |
|  |  |  | 5.6136 | 5. 6259 | 5.5841 | 5. 6059 | 5. 6259 | 5. 5800 | 5. 5794 | 5.6259 | 5. 6259 |
| 5. 750-4 | UN | 2A | 5. 7182 | 5. 7463 | 5. 5839 | 5. 6800 | 5. 7463 | 5. 5717 | 5. 5717 | 5. 7463 | 5. 7463 |
|  |  |  | 5.7167 | 5.7478 | 5. 5836 | 5. 6785 5.6867 | 5. 7478 | 5.5720 | 5. 5714 | 5. 7478 | 5. 7478 |
|  |  | 3 A | 5. 7219 5. 7204 | 5. 7500 5. 7515 | 5. 5876 5.5873 | 5.6867 5.6852 | 5. 7500 5. 7515 | 5. 5784 5.5787 | 5.5784 5.5781 | 5. 7500 5.7515 | 5. 7500 5.7515 |
| 5. 750-12 | UN | 2 A | 5. 7350 | 5. 7479 | 5. 6938 | 5. 7230 | 5. 7479 | 5. 6869 | 5. 6869 | 5. 7479 | 5. 7479 |
|  |  |  | 5. 7341 | 5. 7488 | 5. 6935 | 5. 7221 | 5. 7488 | 5. 6872 | 5. 6866 | 5. 7488 | 5. 7488 |
|  |  | 3A | 5. 7371 | 5. 7500 | 5. 6959 | 5. 7268 | 5. 7500 | 5. 6907 | 5. 6907 | 5. 7500 | 5. 7500 |
|  |  |  | 5. 7362 | 5. 7509 | 5. 6956 | 5. 7259 | 5. 7509 | 5. 6910 | 5.6904 | 5. 7509 | 5. 7509 |
| 5. $750-16$ | UN | 2A | 5. 7376 | 5. 7481 | 5. 7075 | 5. 7284 | 5. 7481 | 5. 7013 | 5. 7013 | 5. 7481 | 5. 7481 |
|  |  |  | 5. 7367 | 5. 7490 | 5. 7072 | 5. 7275 | 5.7490 | 5. 7016 | 5. 7010 | 5. 7490 | 5. 7490 |
|  |  | 3A | 5. 7395 | 5. 7500 | 5. 7094 5.7091 | 5. 7318 5. 7309 | 5. 7500 5. 7509 | 5. 7047 | 5. 7047 | 5. 7500 5. 7509 | 5. 7500 5. 7509 |
| 5. 875-12 | UN | 2A | 5. 8600 | 5.8729 | 5.8188 | 5.8480 | 5. 8729 | 5.8119 | 5.8119 | 5. 8729 | 5. 8729 |
|  |  |  | 4. 8591 | 5. 8738 | 5.8185 | 5. 8471 | 5. 8738 | 5. 8122 | 5. 8116 | 5. 8738 | 5. 8738 |
|  |  | 3A | 5. 8621 5. 8612 | 5. 8750 5.8759 | 5. 8209 5. 8206 | 5. 8518 5.8509 | 5.8750 5.8759 | 5.8157 5.8160 | 5.8157 5.8154 | 5.8750 5.8759 | 5. 8750 5. 8759 |
| 5. 875-16 | UN | 2A | 5. 8626 | 5.8731 | 5.8325 | 5. 8534 | 5.8731 | 5. 8263 | 5. 8263 | 5. 8731 | 5. 8731 |
|  |  |  | 5. 8617 | 5. 8740 | 5. 8322 | 5.8525 | 5. 8740 | 5. 8266 | 5. 8260 | 5. 8740 | 5. 8740 |
|  |  | 3A | 5. 8645 | 5. 8750 | 5. 8344 | 5. 8568 | 5. 8750 | 5. 8297 | 5. 8297 | 5.8750 | 5. 8750 |
|  |  |  | 5. 8636 | 5.8759 | 5.8341 | 5. 8559 | 5.8759 | 5.8300 | 5. 8294 | 5. 8759 | 5.8759 |
| 6.000-4 | UN | 2 A | 5. 9682 | 5. 9963 | 5. 8339 | 5. 9298 | 5. 9963 | 5. 8215 | 5. 8215 | 5. 9963 | 5. 9963 |
|  |  |  | 5. 9667 | 5. 9978 | 5. 83336 | 5. 9283 | 5. 9978 | 5. 8218 | 5. 8212 | 5. 9978 | 5. 9978 |
|  |  | 3A | 5. 9719 5. 9704 | 6.0000 6.0015 | 5.8376 5.8373 | 5. 9366 5. 9351 | 6.0000 6.0015 | 5.8283 5.8286 | 5. 8283 5.8280 | 6.0000 6.0015 | 6.0000 6.0015 |
| 6. 000-12 | UN | 2 A | 5. 9850 | 5. 9979 | 5. 9438 | 5. 9730 | 5. 9979 | 5.9369 | 5.9369 | 5.9979 | 5. 9979 |
|  |  |  | 5. 9841 | 5.9988 | 5. 9435 | 5. 9721 | 5.9988 | 5. 9372 | 5. 9366 | 5. 9988 | 5. 9988 |
|  |  | 3A | 5. 9871 | 6. 0000 | 5. 9459 | 5. 9768 | 6. 0000 | 5. 9407 | 5. 9407 | 6. 0000 | 6. 0000 |
|  |  |  | 5. 9862 | 6.0009 | 5. 9456 | 5. 9759 | 6.0009 | 5. 9410 | 5. 9404 | 6. 0009 | 6. 0009 |
| 6. 000-16 | UN | 2 A | 5.9876 | 5.9981 | 5. 9575 | 5.9784 | 5.9981 | 5. 9513 | 5. 9513 | 5. 9981 | 5. 9981 |
|  |  |  | 5.9867 | 5. 9990 | 5. 9572 | 5. 9775 | 5. 9990 | 5. 9516 | 5. 9510 | 5. 9990 | 5. 9990 |
|  |  | 3A | 5. 9895 | 6. 0000 | 5. 9594 | 5. 9818 | 6. 0000 | 5. 9547 | 5. 9547 | 6. 0000 | 6. 0000 |
|  |  |  | 5. 9886 | 6.0009 | 5. 9591 | 5. 9809 | 6. 0009 | 5. 9550 | 5.9544 | 6. 0009 | 6. 0009 |

${ }^{\text {a }}$ These setting plugs are applieable to thread snap and indieating gages as well as to thread ring gages.
b Piteh diameter limits of $W$ basic-erest setting plug gages are given in eolumn 6 of this table. Pitel diameter limits of X basie-erest setting plug gages are given in eolumn 4 of table 6.19.
c Piteh diameter limits of $W$ basie-erest setting plug gages are given in columns 9 and 10 of this table. Piteh diameter limits of X basie-erest setting plug gages are given in eolumns 6 and 7 of table 6.19.

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# UNITED STATES DEPARTMENT OF COMMERCE NATIONAL BUREAU OF STANDARDS 

## HANDBOOK H28

SCREW-THREAD STANDARDS

FOR FEDERAL SERVICES

## APPENDIX A1

1969
AMERICAN NATIONAL FORM OF THREAD AND THREAD SERIES FOR BOLTS, MACHINE SCREWS, NUTS, TAPPED HOLES, AND GENERAL APPLICATIONS

Since the American National threads have been superseded by the Unified threads, most of appendix 1, as shown in the previous (1957) issue of Part I, has been deleted. Shown herein is data on the class 3 internal threads in the Coarse Thread Series in
nominal sizes from 0.25 to one inch as there is still a need for this information. Data shown is from tables 1.2, 1.8, 1.16, and 1.17 of the 1957 issue. (Appendix number and table numbers now preceded by an A.)

Table A1.2. American National coarse-thread series, NC


Table A1.8. Limits of size and tolerances, classes 1, 2, 3, and 4, American National coarse-thread series, NC

| Limits of size and tolerances | Nominal size |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1/4 | 516 | $3 / 8$ | 7/16 | 1/2 | 916 | 5/8 | $3 / 4$ | 7/8 | 1 |
|  | Threads per inch |  |  |  |  |  |  |  |  |  |
|  | 20 | 18 | 16 | 14 | 13 | 12 | 11 | 10 | 9 | 8 |
| External Threaos | in | in | in | in | in | in | in | in | in | in |
| Class 1, major diameter. | $\begin{array}{r} .2383 \\ .0102 \\ \hline \end{array}$ | 0.3109 .2995 | 0.3732 .3606 .0126 | 0.4354 .4214 .0140 | 0.4978 .4830 | 0.5601 .5443 | 0.6224 .6054 | 0.7472 .7288 | 0.8719 .8519 .0200 | $\begin{array}{r} 0.9966 \\ .9744 \\ .0222 \end{array}$ |
|  | $\begin{aligned} & .2500 \\ & .2428 \\ & .0072 \end{aligned}$ | .3125.3043.0082 | $\begin{aligned} & .3750 \\ & .3660 \end{aligned}$ | .4375 .4277 | .5000 .4896 | . 5625 | .6250 .6132 | . 7300 | .8750 | 1.0000 .9848 |
|  |  |  | . 0090 | . 0098 | . 0104 | . 0112 | . 0118 | . 0128 | . 0140 | . 0152 |
| Class 2, major diameter (threaded parts of un- Max finished, hot-rolled material) | .2500.2398.0102 | $\begin{aligned} & .3125 \\ & .3011 \\ & .0114 \end{aligned}$ | $\begin{aligned} & .3750 \\ & .3624 \\ & .0126 \end{aligned}$ | .4375.4235 | $\begin{aligned} & .5000 \\ & .4852 \\ & .0148 \end{aligned}$ | $\begin{aligned} & .5625 \\ & .5467 \\ & .0158 \end{aligned}$ | $\begin{array}{r} .6250 \\ .6080 \\ .0170 \end{array}$ | $\begin{aligned} & .7500 \\ & .7316 \\ & .0184 \end{aligned}$ | $\begin{array}{r}.8750 \\ .8550 \\ \hline\end{array}$ | $\begin{array}{r} 1.0000 \\ .9778 \\ .0222 \end{array}$ |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | . 0140 |  |  |  |  | . 0200 |  |
| Class 1, minor diameter--------------------- Max ${ }^{\text {- }}$---- | . 1872 | . 2427 | . 2965 | . 3478 | . 4034 | . 4579 | . 5109 | . 6245 | . 7356 | . 8432 |
| Classes 2, 3, and 4, minor diameter---------- Max ${ }^{\text {l }}$--- | . 1887 | . 2443 | . 2983 | . 3499 | . 4056 | . 4603 | . 5135 | . 6273 | . 7387 | . 8466 |
| Class 1, pitch diameter----------------- $\mathrm{Max}^{3}$ | $\begin{aligned} & .2109 \\ & .0051 \end{aligned}$ | . 2691 | . 3263 | . 3820 | .4404 | . 4981 | . 5549 | .6730 | .7897 | $\begin{aligned} & .9154 \\ & .9043 \\ & .0111 \end{aligned}$ |
|  |  | . 0057 | . 0063 | . 0070 | . 0074 | . 0079 | . 0085 | . 0092 | . 0100 |  |
|  | $\begin{array}{r} .2175 \\ .2139 \\ .0036 \end{array}$ | $\begin{array}{r} .2764 \\ .2723 \\ .0041 \end{array}$ | $\begin{aligned} & .3344 \\ & .3299 \\ & .0045 \end{aligned}$ | .3911.3862.0049 | $\begin{array}{r} .4500 \\ .4448 \\ .0052 \end{array}$ | $\begin{array}{r} .5084 \\ .5028 \\ .0056 \end{array}$ | $\begin{aligned} & .5660 \\ & .5601 \\ & .0059 \end{aligned}$ | $\begin{aligned} & .6850 \\ & .6786 \\ & .0064 \end{aligned}$ | .8028.7958.0070 | .9188.9112.0076 |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| Class 3, pitch diameter | $\begin{aligned} & .2175 \\ & .2149 \\ & .0026 \end{aligned}$ | $\begin{aligned} & .2764 \\ & .2734 \\ & .0030 \end{aligned}$ | $\begin{aligned} & .3344 \\ & .3312 \\ & .0032 \end{aligned}$ | .3911.3875.0036 | $\begin{array}{r} .4500 \\ .4463 \\ .0037 \end{array}$ | $\begin{aligned} & .5084 \\ & .5044 \\ & .0040 \end{aligned}$ | .5660.5618.0042 | $\begin{array}{r} .6850 \\ .6805 \\ .0045 \end{array}$ | $\begin{aligned} & .8028 \\ & .7979 \\ & .0049 \end{aligned}$ | .9188.9134.0054 |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
|  | $\begin{aligned} & .2178 \\ & .2165 \\ & .0013 \end{aligned}$ | $\begin{array}{r} .2767 \\ .2752 \\ .0015 \end{array}$ | $\begin{aligned} & .3348 \\ & .3332 \\ & .0016 \end{aligned}$ | $\begin{aligned} & .3915 \\ & .3897 \\ & .0018 \end{aligned}$ | $\begin{array}{r} .4504 \\ .4485 \\ .0019 \end{array}$ | $\begin{aligned} & .5089 \\ & .5069 \\ & .0020 \end{aligned}$ | $\begin{aligned} & .5665 \\ & .5644 \\ & .0021 \end{aligned}$ | $\begin{aligned} & .6856 \\ & .6833 \\ & .0023 \end{aligned}$ | $\begin{aligned} & .8034 \\ & .8010 \\ & .0024 \end{aligned}$ | $\begin{array}{r} .9195 \\ .9168 \\ .0027 \end{array}$ |
|  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |
| Classes 1, 2, 3, and 4, major diameter...-...-- Min ${ }^{2}$ | . 2500 | . 3125 | . 3750 | . 4375 | . 5000 | . 5625 | . 6250 | . 7500 | . 8750 | 1.0000 |
| Min | $\begin{aligned} & .1959 \\ & .2060 \end{aligned}$ | $\begin{aligned} & .2524 \\ & .2630 \end{aligned}$ | $\begin{aligned} & .3073 \\ & .3184 \\ & .0111 \end{aligned}$ | $\begin{array}{r} .3602 \\ .3721 \\ .0119 \end{array}$ | .4167.4290.0123 | .4723.4850.0127 | . 5266 | $\begin{aligned} & .6417 \\ & .6553 \\ & .0136 \end{aligned}$ | $\begin{aligned} & .7547 \\ & .7689 \\ & .0142 \end{aligned}$ | . 8647 |
|  |  |  |  |  |  |  |  |  |  | .8795 .0148 |
| Classes 1, 2, 3, and t, pitch diameter-.-.----- Min ${ }^{\text {3 }}$ | . 2175 | . 2764 | . 3344 | . 3911 | .4500 | . 5084 | . 5660 | . 6860 | . 8028 | . 9188 |
|  | $\begin{aligned} & .2226 \\ & .0051 \end{aligned}$ | $.2821$ | $\begin{aligned} & .3407 \\ & .0063 \end{aligned}$ | . 3981 | $\begin{array}{r} .4574 \\ .0074 \end{array}$ | . 5163 | . 5745 | . 6942 | . 8128 | . 9299 |
|  |  |  |  |  |  |  |  |  |  |  |
|  | $\begin{array}{r} .2211 \\ .0036 \end{array}$ | $\begin{aligned} & .2805 \\ & .0041 \end{aligned}$ | $\begin{aligned} & .3389 \\ & .0045 \end{aligned}$ | $\begin{array}{r} .3960 \\ .0049 \end{array}$ | $\begin{aligned} & .4552 \\ & .0052 \end{aligned}$ | $\begin{aligned} & .5140 \\ & .0056 \end{aligned}$ | . 5719 | . 6914 | . 8098 |  |
| Class 2, pitch diameter.--------------------- Tol-------- |  |  |  |  |  |  | . 0059 | . 0064 | . 0070 | . 0076 |
| Class 3, pitch diameter ${ }^{\text {a }}$ Max | $\begin{aligned} & .2201 \\ & .0026 \end{aligned}$ | $\begin{array}{r} .2794 \\ .0030 \end{array}$ | $\begin{aligned} & .3376 \\ & .0032 \end{aligned}$ | $\begin{array}{r} .3947 \\ .0036 \end{array}$ | $\begin{aligned} & .4537 \\ & .0037 \end{aligned}$ | $\begin{aligned} & .5124 \\ & .0040 \end{aligned}$ | . 5702 | . 6895 | . 8077 | . 9242 |
| Class 3, pitch diameter-------------------- Tol |  |  |  |  |  |  | . 0042 | . 0045 | . 0049 | . 0054 |
| Class 4, pitch diameter (Max | $\begin{aligned} & .2188 \\ & .0013 \end{aligned}$ | $\begin{aligned} & .2779 \\ & .0015 \end{aligned}$ | $\begin{aligned} & .3360 \\ & .0016 \end{aligned}$ | $\begin{aligned} & .3929 \\ & .0018 \end{aligned}$ | $\begin{aligned} & .4519 \\ & .0019 \end{aligned}$ | $\begin{aligned} & .5104 \\ & .0020 \end{aligned}$ | $\begin{aligned} & .5681 \\ & .0021 \end{aligned}$ | $\begin{aligned} & .6873 \\ & .0023 \end{aligned}$ | $\begin{aligned} & .8052 \\ & .0024 \end{aligned}$ | $\begin{aligned} & .9215 \\ & .0027 \end{aligned}$ |
| Class 4, pitch diameter--------------------- Tol $^{-}$ |  |  |  |  |  |  |  |  |  |  |

[^21]Table A1.16. Gages for standard thread series, American National screw threads

Table A1．16．Gages for standard thread series，American National screw threads－Continued

|  |  | $\begin{aligned} & \text { 台名 } \\ & \text { So } \\ & \text { So } \end{aligned}$ | 品 | $\stackrel{\infty}{\sim}$ |  | －以 <br>  |  M M M M M M | $\rho^{\infty} \rho^{\infty} \rho^{\infty}$ 808 にNTNNRNR | $\circ^{\infty} 0^{\infty} 0^{\infty} 0^{\infty}$ な్వ $\infty \infty$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 8 | $\cong$ |  |  MMNMN NN <br>  |  | 옹ㅇNㅇN <br>  <br>  | 옹ㅇㅇㅇN 운운운 <br>  $\infty \infty \infty \infty \infty \infty \infty \infty$ |
|  |  | $\begin{aligned} & \circ \\ & \stackrel{0}{6} \\ & \stackrel{0}{4} \end{aligned}$ |  | $\stackrel{\square}{\sim}$ |  | 눙ㅇN웡ㅇㅇㅇ <br>  |  옹ㅇㅇㅇㅇㅇㅇ |  | 内N MNNNMN <br>  |
|  |  |  |  | 9 |  <br>  |  1515 2520 |  Tis |  |  <br>  ©0，0．0．0．0： |
|  |  |  |  | $\pm$ |  |  <br>  |  |  O |  かめ ๑ロ：．．． |
|  |  | 8 |  | $\because$ |  |  <br>  |  Co 0 |  | $\infty \times \infty \times \infty$ ふঅఠふふふふふ |
|  |  |  |  | $\stackrel{ }{\sim}$ | 玉 | 웅우웅 M్ర | 웅ㅇㅇㅇㅇㅇ응 <br>  |  <br>  $\infty \infty \infty \infty \infty \infty \infty$ |  |
|  |  | $\begin{aligned} & 8 \\ & 80 \\ & 0 \\ & 8 \end{aligned}$ |  | $=$ |  |  |  |  |  |
|  |  |  |  | 9 |  |  ¢8．0．6060 | －NNN゚NN゚ NかNNNMNH | 옹ํ옹N ペッコーシ゚に $15 \times 8.080$ $\infty \infty \infty \infty \infty \infty \infty$ |  |
|  |  | 8 |  | $\bigcirc$ |  |  NNMANMNNT |  | $\circ^{\infty} 0^{\infty} 0^{\infty} 0^{\infty}$ $\sigma_{1}=\mathrm{O}_{4}^{\infty} \mathrm{O}_{1}^{\infty} \mathrm{O}_{1}^{\infty}$ <br>  |  |
|  |  |  |  | $\infty$ |  |  | TOPMR15 <br>  |  | NRFが $\operatorname{Lin}_{\infty}^{\infty} \infty_{\infty}^{\infty} \infty_{\infty}^{\infty} \infty_{\infty}^{\infty}$ |
|  |  | $\begin{aligned} & 8 \\ & \text { 相 } \\ & \text { 8 } \end{aligned}$ |  | － |  |  $\therefore 1060$ सम | ㅇN N M N N N0 0 N080 |  D8 <br>  |  |
|  |  |  |  | $\bigcirc$ |  |  12 <br>  | － たi | $\because F \sqrt{-\infty}$ |  |
|  |  | $8$ |  | 40 |  |  <br>  <br>  |  |  |  |
|  |  |  |  | T |  |  <br>  | NGNㅜㄴNN 080000000 |  $\underset{\sim}{\infty} \varnothing \infty \varnothing \infty$ |  |
| \％ |  |  |  | $\infty$ | $\Rightarrow \text { or m }+$ | $\rightarrow$ ล ๑ サ | $-\infty \quad \infty \quad+$ | $\rightarrow \infty \quad \infty \quad \rightarrow$ | $\rightarrow \text { a m } \dagger$ |
|  |  |  |  | N | 0 | 8 | 0 | 8 | \％ |
|  |  |  |  | － | $\begin{aligned} & \stackrel{y}{1} \\ & \vdots \\ & \infty \end{aligned}$ | $\cdots$ | － | $\cdots$ | $\stackrel{\infty}{1}$ |

Table A1.17. Setting plug gages, American National screw threads

| Nominal size and threads per inch | Series designation | Class | W truncated setting plugs |  |  |  |  |  |  | Basic-crest setting plugs |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Plug for "Go" |  |  | Plug for "Not go" |  |  |  | Major diameter |  |  |  |
|  |  |  | Major diameter |  | Pitch diameter | Major diameter |  | Pitch diameter |  | Gol |  | Not go ${ }^{2}$ |  |
|  |  |  | Truncated | Full |  | Truncated | Full | Plus tol. gage | $\begin{aligned} & \text { Minus } \\ & \text { tol. gage } \end{aligned}$ | $\begin{gathered} W \\ \text { tolerance } \end{gathered}$ | $\underset{\text { tolerance }}{X}$ | tolerance | $\underset{\text { tolerance }}{\text { a }}$ |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11A | 11B | 12A | 12B |
| 1/4-20 | NC |  | in | in | in | in | in | in | in | in | in | in | in |
|  |  |  | 0.2395 | 0.2485 | 0.2160 | 0.2326 | 0.2484 | 0.2109 | 0.2109 | 0.2485 | 0.2485 | 0.2484 | 0.2484 |
|  |  |  | . 2390 | . 2490 | . 2159 | . 2321 | . 2489 | . 2110 | . 2108 | . 2490 | . 2490 | . 2489 | . 2489 |
|  |  |  | . 2410 | . 2500 | . 2175 | . 2356 | . 2500 | . 2139 | . 2139 | . 2500 | . 2500 | . 2500 | . 2500 |
|  |  |  | . 2405 | . 2505 | . 2174 | . 2351 | . 2505 | . 2140 | . 2138 | . 2505 | . 2505 | . 2505 | . 2505 |
|  |  |  | . 2410 | . 2500 | . 2175 | . 2366 | . 2500 | . 2149 | . 2149 | . 2500 | . 2500 | . 2500 | . 2500 |
|  |  |  | . 2405 | . 2505 | . 2174 | . 2361 | . 2505 | . 2150 | . 2148 | . 2505 | . 2505 | . 2505 | . 2505 |
|  |  |  | . 2413 | . 2503 | . 2178 | . 2382 | . 2503 | . 2165 | . 2165 | . 2500 | . 2500 | . 2500 | . 2500 |
|  |  |  | . 2408 | . 2508 | . 2177 | . 2377 | . 2508 | . 2166 | . 2164 | . 2505 | . 2505 | . 2505 | . 2505 |
| 5/16-18 | NC | 1 | . 3012 | . 3109 | . 2748 | . 2932 | . 3108 | . 2691 | . 2691 | . 3109 | . 3109 | . 3108 | . 3108 |
|  |  |  | . 3007 | . 3114 | . 2747 | . 2927 | . 3113 | . 2692 | . 2690 | . 3114 | . 3114 | . 3113 | . 3113 |
|  |  |  | . 3028 | . 3125 | . 2764 | . 2964 | . 3125 | . 2723 | . 2723 | . 3125 | . 3125 | . 3125 | . 3125 |
|  |  | 3 | . 3023 | . 3130 | . 2763 | . 2959 | . 3130 | . 2724 | . 2722 | . 3130 | . 3130 | . 3130 | . 3130 |
|  |  |  | . 3028 | . 3125 | . 2764 | . 2975 | . 3125 | . 2734 | . 2734 | . 3125 | . 3125 | . 3125 | . 3125 |
|  |  | 4 | . 3023 | . 3130 | . 2763 | . 2970 | . 3130 | . 2735 | . 2733 | . 3130 | . 3130 | . 3130 | . 3130 |
|  |  |  | . 3026 | . 3128 | . 27676 | . 29988 | . 3128 | . 2752 | . 2752 | .3125 .3130 | .3125 .3130 | . 3135 | . 31320 |
| 3-8-16 | NC | 1 | . 3627 | . 3732 | . 3326 | . 3534 | . 3732 | . 3263 | . 3263 | . 3732 | . 3732 | . 3732 | . 3732 |
|  |  |  | . 3621 | . 3738 | . 3325 | . 3528 | . 3738 | . 3264 | . 3262 | . 3738 | . 3738 | . 3738 | . 3738 |
|  |  | 2 | . 3645 | . 3750 | . 3344 | . 3570 | . 3750 | . 3299 | . 3299 | . 3750 | . 3750 | . 3750 | . 3750 |
|  |  | 3 | . 3639 | . 3756 | . 3343 | . 3564 | . 3756 | . 3300 | . 3298 | . 3756 | . 3756 | . 3756 | . 3756 |
|  |  |  | . 3645 | . 3750 | . 3344 | . 3583 | . 3750 | . 3312 | . 3312 | . 3750 | . 3750 | . 3750 | . 3750 |
|  |  |  | . 3639 | . 3756 | . 3343 | . 3577 | . 3756 | . 3313 | . 3311 | . 3756 | . 3756 | .3756 | . 3756 |
|  |  | 4 | . 3649 | . 3754 | . 3348 | . 3603 | . 3754 | . 3332 | . 3332 | . 3750 | . 3750 | . 3750 | . 3750 |
|  |  |  | . 3643 | . 3760 | . 3347 | . 3597 | . 3760 | . 3333 | . 3331 | . 3756 | . 3756 | . 3756 | . 3756 |

See footnotes at end of table.

Table A1.17. Setting plug gages, American National screw threads-Continued

${ }^{1}$ Pitch diameter limits of W basic-crest setting plug gages are given in column 6 of this table. Pitch diameter limits of X basic-crest setting plug gages are given in column 4 of table A1.16.
${ }^{2}$ Pitch diameter limits of $W$ basic-crest setting plug gages are givell in columns 9 and 10 of this table. Pitch diameter limits of X basic-crest setting plug gages are given in columns 6 and 7 of table A1.16.

# UNITED STATES DEPARTMENT OF COMMERCE NATIONAL BUREAU OF STANDARDS 

## HANDBOOK H28

## SCREW-THREAD STANDARDS

FOR FEDERAL SERVICES

APPENDIX 2
1957
AMERICAN NATIONAL SCREW
THREADS OF SPECIAL DIAMETERS, PITCHES, AND LENGTHS OF ENGAGEMENT
appendix 2 is being deleted from the 1969 ISSUE of HANDBOOK H28

# UNITED STATES DEPARTMENT OF COMMERCE 

 NATIONAL BUREAU OF STANDARDS
## HANDBOOK H28

SCREW-THREAD STANDARDS FOR FEDERAL SERVICES

## APPENDIX A3

1969
TAP DRILL SIZES FOR UNIFIED SCREW THREADS AND
RECOMMENDED HOLE SIZE LIMITS BEFORE THREADING

## 1. TAP DRILL SIZES FOR UNIFIED SCREW THREADS

When it is important that the minor diameter of an internal thread conform to specified limits it may be necessary to use a reamer to finish the hole. However, a drill often can be made to cut with a sufficient accuracy for this requirement. A variety of factors enter into the production of a clean, round, straight hole of the correct diameter. For a discussion of these and other data on drilling and tapping, reference should be made to "Drilled Holes for Tapping," published by the Drill and Reamer Division and the Tap and Dic Division of the Metal Cutting Tool Institute, 405 Lexington Avenue, New York, N.Y. 10017.

Table A3.1. gives minor diameter limits and corresponding percentages of basic thread height, 0.75 H , for all standard series threads up to and including 3.75 inch diameter for classes 1 B and 2 B . Table A3.2 is a similar table for class 3B. These tables also list sizes of drills that may be expected to drill holes within or near the specified minor diametcr limits. The diameter of the drill, the probable hole size, and the corresponding percentages of basic thread height are tabulated.

As a drill may normally be expected to cut oversize, probable hole sizes are tabulated that are derived from probable mean oversizes, also tabulated. The following is quoted from the above-mentioned report: "These oversizes were determined from a series of tests conducted by a number of drill manufacturers. Using six sizes of dills ranging from $1 / 16$ to 1 in . a total of 2,808 holes were drilled in cast iron and steel. Commercial high speed drills were used and the drilling equipment was of the same type and condition that is normally encountered in metal working shops. The average depth of hole drilled was equal to 1.5 times the drill diameter and the measurement of the hole was made at the midpoint of the depth drilled. . . . . With good drilling practices and with reasonable care in the resharpening of drills the average user may expect to drill oversize in the same manner."

## 2. RECOMMENDED HOLE SIZE LIMITS BEFORE THREADING

Recommended hole size limits before threading and the corresponding tolerances are derived from the minimum and maximum minor diameters of the internal thread to provide for optimum strength of fastenings and tapping conditions. The following rules as illustrated in figure A3.3 are used.

For the range to and including 0.33 D , the minimum hole size is equal to the minimum minor diameter of the internal thread and the maximum hole size is larger by half the minor diameter tolerance.

For the range from $0.33 D$ to 0.67 D , the minimum and maximum hole sizes are each one quarter of the minor diameter tolerance larger than the corresponding limits for the length of engagement to and including 0.33 D .

For the range from $0.67 D$ to $1.5 D$, the minimum hole size is larger than the minimum minor diameter of the internal thread by half the minor diameter tolerance and the maximum hole size is equal to the maximum minor diancter.

For the range from $1.5 D$ to $3 D$, the minimum and maximum hole sizes are cach one quarter of the minor diameter tolerance of the internal thread larger than the corresponding limits for the $0.67 D$ to $1.5 D$ length of engagement.

From the foregoing it will be seen that the difference between limits in each range is the same and equal to half of the minor diameter tolerance. This is a general rule. However, the minimum differences for sizes below 0.25 in are equal to the minor diameter tolerances given in tables 3.9 and 3.10 for lengths of engagement to and including $0.33 D$. For lengths of engagement greater than 0.33 D for sizes 0.25 in and larger, the values are adjusted so that the difference bet ween limits is ne ver less than 0.0040 in .
2.1. Recommended Hole Size Limits for Standard Unified Threads and Some UNS Threads are Given in Tables A3.5 and A3.6.-For diam-eter-pitch combinations other than those given in these tables, the tolerances given in table 2.21 or the tolerance derived from the formula, should be similarly applied to determine the hole size limits.

Internal threads requiring modified minor diameters for lengths of engagement less than 0.67 D to develop the optimum strength of the fastening, or longer than 1.5 D to reduce tapping difficulties, should be designated as specified in section 2. (See under "Designating threads having modified crests" in that section.)
2.2. For Unified Miniature threads, the distribution of hole size limits differs from the above, to accord with conditions peculiar to miniature threads and is shown in figure A3.4. The maximum limits are based on providing a functionally adequate fastening for the most common applications, where the material of the externally threaded member is of a strength essentially equal to or greater than that of its mating part. In applications where, because of considerations other than the fastening, the screw is made of an appreciably weaker material, the use of smaller hole sizes is usually necessary to extend thread engagement to a greater depth on the external thread. However, hole sizes down to the minimum limit of the minor diameters must be avoided to allow for the spin-up developed as the result of the negative rake with which these small taps are ground.

Recommended hole size limits for these threads are tabulated in table A3.7.

Table A3.1. Tap drill sizes, Unified screw threads, classes $1 B$ and 2B


See footnotes at end of table.

Table A3.1. Tap drill sizes, Unified screw threads, classes $1 B$ and 2B-Continued

| Thread size | Threads per inch | Designation | Classes 1B and 2B minor diameter, internal threads |  |  |  | Tap drills and percent basic thread height |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimum | Percent ${ }^{3}$ basic thread height | Maximum | Percent a basic thread height | Drill size |  | Percent of thread | Probable oversize, mean | Probable hole size | Percent of thread |
| in |  |  | in |  | in |  | in | in |  | in | in |  |
|  |  |  |  |  |  |  | \# $\begin{aligned} & \text { \# } \\ & \# \\ & \text { 8 }\end{aligned}$ | .1960 .1990 | 83 79 | .0038 <br> .0038 | .1998 <br> .2028 | 77 73 |
| . 250 | 20 | UNC | . 196 | 83.1 | . 207 | 66.2 | \# $\begin{array}{r}\text { \# } \\ \# \\ \text { \% }\end{array}$ | . 2010 | 79 75 | .0038 | . 2028 | 73 70 |
|  |  |  | . 196 | 83.1 | . 207 | 66.2 | 13/64 | . 2031 | 72 | . 0038 | . 2069 | 66 |
|  |  |  |  |  |  |  | \# 6 | . 2040 | 71 | . 0038 | . 2078 | 65 |
|  |  |  |  |  |  |  | \#5 | . 2055 | 69 | . 0038 | . 2093 | 63 |
| . 250 | 28 | UNF | . 211 | 84.1 | . 220 | 64.7 | \#3 | . 213180 | 80 67 | .0038 .0038 | . 2168 | 72 59 |
| . 250 | 32 | UNEF | . 216 | 83.8 | . 224 | 64.0 | 7 7 52 | . 2188 | 77 | . 0038 | . 2226 | 67 |
| . 250 | 36 | UNS | . 220 | 83.1 | . 226 | 66.5 | \# $\#$ $\# 2$ | . 22210 | 71 80 | . 00038 | . 22248 | 62 70 |
| . 3125 | 18 | UNC | . 252 | 83.8 | . 265 | 65.8 | F | . 2570 | 77 | . 0038 | . 2608 | 72 |
|  |  |  |  |  |  |  | G | . 2610 | 71 | . 0041 | . 2651 | 66 |
| . 3125 | 20 | UN | . 258 | 83.9 | . 270 | 65.4 | $\left\{\begin{array}{l}\text { F } \\ \text { G }\end{array}\right.$ | . 2570 | 85 | .0038 .0041 | . 26081 | 80 73 |
|  |  |  |  |  |  |  | H | . 2660 | 72 | . 0041 | .2701 | 65 |
| 3125 | 24 |  |  |  |  |  | ( $\mathrm{H}^{\text {H }}$ | . 2660 | 86 | . 0041 | . 2701 | 78 |
| . 3125 | 24 | UNF | . 267 | 84.1 | . 277 | 65.6 | \{ | . 2720 | 75 | . 0041 | . 2761 | 67 58 |
|  |  |  |  |  |  |  | J | . 2770 | 66 77 | . 0041 | . 2811 | 68 |
| .3125 | 28 | UN | . 274 | 83.0 | . 282 | 65.7 | \{K | . 2810 | 68 | . 0042 | . 2852 | 59 |
|  |  |  |  |  |  |  | 9 9/32 | . 2812 | 67 | . 0042 | . 2854 | 58 |
| . 3125 | 32 | UNEF | . 279 | 82.5 | . 286 | 65.3 | $(\mathrm{K}$ | . 2810 | 78 | . 0042 | . 2852 | 67 |
| . 3125 | 36 | UNS | . 282 | 84.5 | . 289 | 65.1 | ${ }^{9 / 32} 7.25 \mathrm{~mm}$ | . 28854 | 77 75 | .0042 | . 28894 | 67 63 |
| . 375 | 16 | UNC | . 307 | 83.8 | . 321 | 66.5 |  | . 3125 | 77 | . 0044 | . 3169 | 72 |
|  | 16 | UNO | . 307 | 83.8 | . 321 | 66.5 | O | . 3160 | 73 | . 0044 | . 3204 | 67 |
| . 375 | 20 | UN | . 321 | 83.1 | . 332 | 66.2 | P ${ }_{\mathrm{Q}}^{\mathrm{P}}$ | . 32320 | 80 66 | . 00044 | . 3274 | 73 59 |
| . 375 | 24 | UNF | . 330 | 83.1 | . 340 | 64.7 | Q | . 3320 | 79 | . 0044 | . 3364 | 71 |
| . 375 | 2 | UNF | . 330 | 83.1 | . 840 | 64.7 | R | . 3390 | 67 | . 0044 | . 3434 | 58 |
| . 375 | 28 | UN | . 336 | 84.1 | . 345 | 64.7 | $\left\{\begin{array}{l}\text { R } \\ 11 / 2\end{array}\right.$ | .3390 .3438 | 78 67 | . 00044 | .3434 .3483 . | 68 58 |
| . 375 | 32 | UNEF | . 341 | 83.8 | . 349 | 64.0 | ${ }^{11 / 32}$ | . 3438 | 77 | . 0045 | . 3483 | 66 |
| . 375 | 36 | UNS | . 345 | 83.1 | . 352 | 63.7 | (S | . 34480 | 67 75 | . 00045 | . 3525 | 55 62 |
| . 4375 |  | UNC | 360 | 83.5 |  | 66.3 | T | . 3580 | 86 | . 0046 | . 3626 | 81 |
| . 4375 | 14 | UNC | . 360 | 83.5 | . 376 | 66.3 | $\{2364$ | . 3594 | 84 | . 0046 | . 3640 | 79 |
| . 4375 | 16 | UN | . 370 | 83.1 | . 384 | 65.9 | \{3/8 | $\begin{array}{r}.3750 \\ .3770 \\ \hline\end{array}$ | 77 75 | . 00046 | .3796 .3816 | 71 69 |
| . 4375 | 20 | UNF | . 383 | 83.9 | . 395 | 65.4 | W | . 3860 | 79 | . 0046 | . 3906 | 72 |
|  |  |  | . 399 | 83.0 | . 407 | 65.7 | ${ }^{25}$ | . 3906 | 72 | . 0046 | . 3952 | 65 |
| . 4375 | 28 | UNEF | . 399 | 83.0 | . 407 | 65.7 | Y | . 4040 | 72 | . 0046 | . 4086 | 62 |
| . 4375 | 32 | UN | . 404 | 82.5 | . 411 | 65.3 | $\{13$ /32 | . 404062 | 83 77 | .0046 | . 4086 | 71 66 |
| . 500 | 12 | UNS | . 410 | 83.1 | . 428 | 66.5 | $\left\{\begin{array}{l}1 \\ 27\end{array}\right.$ | .4130 | 80 | . 0047 | .4177 | 76 |
|  |  |  |  |  | . 434 | 66.0 | 2764 | . 4219 | 72 | . 0047 | . 4266 | 68 |
| . 500 | 16 | UN | . 4317 | 83.1 83.8 | . 4446 | 66.0 66.5 | ${ }^{27} 64$ | .4219 | 78 | . 0047 | .4266 | 73 |
| . 500 | 20 | UNF | . 446 | 83.1 | . 457 | 66.2 | ${ }^{29} 5$ | ${ }^{.4351}$ | 72 | . 00047 | . 4422 | 71 |
| . 500 | 28 | UNEF | . 461 | 84.1 | . 470 | 64.7 | 15/32 | . 4688 | 67 | . 0048 | . 4736 | 57 |
| . 500 | 32 | UN | . 466 | 83.8 | . 474 | 64.0 | 15\% 62 | . 4688 | 77 | . 0048 | .4736 | 65 |
| . 5625 | 12 | UNC | . 472 | 83.6 | . 490 | 67.0 | $\left\{\begin{array}{l}15 \\ 3\end{array}\right.$ | . 4688 | 87 | . 0048 | . 4736 | 82 |
|  |  |  |  |  |  |  | 31/64 | . 4844 | 72 | . 0048 | . 4892 | 68 |
| . 5625 | 16 | UN | . 495 | 83.1 | . 509 | 65.9 | $\left\{\begin{array}{l}1 / 2 \\ 0\end{array}\right.$ | . 5000 | 77 | . 00048 | . 50418 | 71 |
|  |  |  |  |  |  |  | $1 / 2$ | . 5000 | 87 | . 0048 | . 5048 | 80 |
| . 5625 | 18 | UNF | . 502 | 83.8 | . 515 | 65.8 | 0.5062 | . 5062 | 78 | . 0048 | . 5110 | 71 |
| . 5625 | 20 | UN | . 508 | 83.9 | . 520 | 65.4 | 3364 | . 5156 | 72 | . 0048 | . 5204 | 65 |
| . 5625 | 24 | UNEF | . 517 | 84.1 | . 527 | 65.6 | $\left\{\begin{array}{l}33 / 4.4 \\ 0.5203\end{array}\right.$ | . 5156 | 87 78 | . 00048 | . 5204 | 78 |
|  |  |  |  |  |  |  | 17/22 | . 5312 | 67 | . 0049 | . 5361 | 57 |
| . 0625 | 28 | UN | . 524 | 83.0 | . 532 | 65.7 | 0.5263 | . 5263 | 78 | . 0049 | . 5312 | 67 |
| . 5625 | 32 | UN | . 529 | 82.5 | . 536 | 65.3 | 17/32 | . 5312 | 77 | . 0049 | . 5361 | 65 |
| . 625 | 11 | UNC | . 527 | 83.0 | . 546 | 66.9 | 17,62 | . 5312 | 79 | . 0049 | . 5361 | 75 |
| . 625 | 12 | UN | . 535 | 83.1 | . 553 | 66.5 | 35\% 6 | . 5469 | 72 | . 0049 | . 5518 | 68 |
| . 625 | 16 | UN | . 557 | 83.8 | . 571 | 66.5 | $\left\{\begin{array}{l}9,16 \\ 0.5687\end{array}\right.$ | . 5625 | 77 69 | . 00049 | . 5674 | 71 |
|  |  |  |  |  |  |  | 9.16 | . 5625 | 87 | . 00049 | . 5674 | 80 |
| . 625 | 18 | UNF | . 565 | 83.1 | . 578 | 65.1 | \{0.5687 | . 5687 | 78 | . 0049 | . 5736 | 71 |
| . 625 | 20 | UN | . 571 | 83.1 | . 582 | 66.2 | ${ }^{37} 66_{4}$ | . 5781 | 72 | . 0049 | . 5830 | 65 |
| . 625 | 24 | UNEF | . 580 | 83.1 | . 590 | 64.7 | $\left\{\begin{array}{l}37 / 64 \\ 588\end{array}\right.$ | . 57828 | 87 | . 00049 | . 5838 | 78 |
|  |  |  |  |  |  |  | 0.5828 | . 58828 | 78 67 | . 00049 | . 58877 | 69 |
| . 625 | 32 | UN | . 591 | 83.8 | . 599 | 64.0 | $19 \%$ | . 5938 | 77 | . 0049 | . 5987 | 65 |

See footnotes at end of table.

Table A3.1. Tap drill sizes, Unified screw threads, classes $1 B$ and $2 B$-Continued

| Thread size | Threads per inch | Designation | Classes 1 B and 2B minor dianeter, internal threads |  |  |  | Tap drills and percent basic thread height |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimum | $\left\lvert\, \begin{gathered} \text { Percent a } \\ \text { basic thread } \\ \text { height } \end{gathered}\right.$ | Maximum | Percent a basic thread height | Drill size |  | Percent of thread | Probable oversize, mean | Probable hole size | Percent of thread |
| in |  |  | in |  | in |  | in |  |  |  |  |  |
| . 6875 | 12 | UN | . 597 | 83.6 | . 615 | 67.0 | $\left\{\begin{array}{l}19 / 32 \\ 39\end{array}\right.$ | . 5938 | 87 | . 0049 | . 5987 | 82 |
| . 6875 | 16 | UN | . 620 | 83.1 | . 634 | 65.9 | (139/64 | . 6094 | 72 77 | .0049 .0050 | .6143 .6300 | 71 |
| .6875 | 20 | UN | . 633 | 83.9 | . 645 | 65.4 | 41164 | . 62406 | 77 | . 00050 | . 63456 | 65 |
| . 6875 | 24 | UNEF | . 642 | 84.1 | . 652 | 65.6 | 4164 | . 6406 | 87 | . 00050 | . 6456 | 65 77 |
| . 68875 | 28 | UN | . 649 | 83.0 82.5 | . 657 | 65.7 65.3 | $21 / 38$ | . 6562 | 67 | . 0050 | . 6612 | 57 |
| . 6875 | 32 | UN | . 654 | 82.5 | . 661 | 65.3 | 21/32 | . 6562 | 77 | . 0050 | . 6612 | 65 |
| . 750 | 10 | UNC | . 642 | 83.1 | . 663 | 67.0 | $\left\{\begin{array}{l}11 / 64 \\ 216\end{array}\right.$ | . 6406 | 84 | . 0050 | . 6456 | 80 |
| . 750 | 12 | UN | . 660 | 83.1 | . 678 | 66.5 |  | . 65562 | 72 | .0050 .0050 | . 66612 | 68 82 |
| .750 | 12 | UN | . 660 | 83.1 | . 678 | 66.5 | \{43, ${ }_{6}$ | . 6719 | 72 | . 0050 | . 6769 | 88 |
| .750 .750 | 16 20 | UNF | . 682 | 83.8 | .696 .707 | 66.5 | ${ }^{1116}$ | . 6875 | 77 | . 0050 | . 6925 | 71 |
| .750 .750 | 28 | UNEF | .696 .711 | 83.1 84.1 | . 720 | 66.2 | 45/64 | . 7031 | 72 67 | . 00051 | .7082 .7239 | 64 |
| . 750 | 32 | UN | . 716 | 83.8 | . 724 | 64.0 | 23/32 | . 7188 | 77 | . 0051 | .7239 .7239 | 56 64 |
| . 8125 | 12 | UN | . 722 | 83.6 | . 740 | 67.0 | 4764 | . 7344 | 72 |  |  |  |
| . 8125 | 16 20 | UN | . 745 | 83.1 | . 759 | 65.9 | $3 / 4$ | . 7500 | 77 | . 00052 | . 7395 | 67 71 |
| . 8125 | 20 | UNEF | . 758 | 83.9 | . 770 | 65.4 | 4964 | . 7656 | 72 | . 0052 | . 7708 | 64 |
| .8125 .8125 | 28 | UN | .774 .779 | 83.0 | .782 .786 | 65.7 65.3 | 25.32 | . 7812 | 67 | . 0052 | . 7864 | 56 |
| . 8125 | 32 | UN | . 779 | 82.5 | . 786 | 65.3 | 25/32 | . 7812 | 77 | . 0052 | . 7864 | 64 |
| . 875 | 9 | UNC | . 755 | 83.1 | . 778 | 67.2 | ${ }^{49} 64$ | . 7656 | 76 | . 0052 | . 7708 | 2 |
| . 875 | 12 | UN | . 785 | 83.1 | . 803 | 66.5 | $\left\{\begin{array}{l}25 / 32 \\ 51 / 4\end{array}\right.$ | . 7812 | 87 | . 0052 | . 7864 | 82 |
|  |  |  |  |  |  |  | ${ }^{51 / 64}$ | .7969 .7969 | 72 84 78 | . 00052 | . 8021 | 67 79 |
| . 875 | 14 | UNF | . 798 | 83.0 | . 814 | 65.7 | $\{0.8024$ | . 8024 | 78 | . 0052 | . 8076 | 73 |
| . 875 | 16 | UN | . 807 | 83.8 | . 821 | 66.5 | $13 / 16$ $13 / 16$ | . 8125 | 67 77 | . 00052 | . 8177 | 62 70 |
| . 875 | 20 | UNEF | . 821 | 83.1 | . 832 | 66.2 | 33,64 | . 81281 | 77 72 | . 00053 | .8178 | 70 |
| . 875 | 28 | UN | . 836 | 84.1 | . 845 | 64.7 | 27/32 | . 8438 | 67 | . 0055 | .8393 | 64 |
| . 875 | 32 | UN | . 841 | 83.8 | . 849 | 64.0 | 27/32 | . 8438 | 77 | . 0055 | . 849493 | ${ }_{63}$ |
| . 9375 | 12 | UN | . 847 | 83.6 | . 865 | 67.0 | $\left\{\begin{array}{l}27 / 32 \\ 51\end{array}\right.$ | . 8438 | 87 | . 0055 | . 8493 | 81 |
| . 9375 | 16 | UN | . 870 | 83.1 | . 884 | 65.9 | [5964 | . 85750 | 72 77 | . 0056 | . 8680 | ${ }^{67}$ |
| . 9375 | 20 | UNEF | . 883 | 83.9 | . 895 | 65.4 | ${ }^{57} 864$ | . 87800 | 77 | . 0057 | .8807 | 70 63 |
| .9375 .9375 | 28 | UN | . 899 | 83.0 | . 907 | 65.7 | 29/32 | . 9062 | 67 | . 0060 | . 9122 | 53 |
| . 9375 | 32 | UN | . 904 | 82.5 | . 911 | 65.3 | $29 / 32$ | . 9062 | 77 | . 0060 | . 9122 | 62 |
| 1.000 | 8 | UNC | . 865 | 83.1 | . 890 | 67.7 | $\left\{\begin{array}{l}55 \\ 764\end{array}\right.$ | . 8594 | 87 | . 0059 | . 8653 | 83 |
|  | 12 |  |  |  |  |  | 3/8/8 | . 8750 | 77 87 | .0059 .0060 | .8809 .9122 | 73 |
| 1.000 | 12 | UNF | . 910 | 83.1 | . 928 | 66.5 |  | . 9219 | 72 | . 0060 | . 91.9279 | 87 |
| 1.000 | 14 | UNS | . 923 | 83.0 | . 938 | 66.8 | 59964 | . 9219 | 84 | . 0060 | . 9279 | 78 |
| 1.000 | 16 | UN | . 932 | 83.8 | . 946 | 66.5 | ${ }_{15}^{15} 10274$ | . 9274 | 78 | . 00061 | . 93335 | 72 69 |
| 1.000 | 20 | UNEF | . 946 | 83.1 | . 957 | 66.2 | ${ }_{61} 164$ | . 93751 | 77 | . 0062 | . 94378 | 69 63 |
| 1.000 | 28 | UN | . 966 | 84.1 | . 970 | 64.7 | ${ }^{31} 164$ | . 9688 | 67 | . 0065 | . 9753 | 53 |
| 1.000 | 32 | UN | . 966 | 83.8 | . 974 | 64.0 | $31 / 32$ | . 9688 | 77 | . 0065 | . 9753 | 61 |
| 1.0625 | 8 | UN |  |  |  |  | $\left\{\begin{array}{l}5964 \\ 0.6274\end{array}\right.$ | . 9219 | 87 | . 0060 | . 9279 | 83 |
| 1.0625 | 8 | UN | . 927 | 83.4 | . 952 | 68.0 | $\left\{\begin{array}{l}0.9274 \\ 15 / 16\end{array}\right.$ | . 9274 | 83 77 | . 00061 | . 93335 | 79 |
| 1.0625 | 12 | UN | . 972 | 83.6 | . 990 | 67.0 | ${ }^{31 / 52}$ | . 9688 | 87 | . 0065 | . 9753 | 81 |
| 1.0625 | 16 | UN | . 995 | 83.1 | 1.009 | 65.9 | ${ }^{63} 164$ | . 9844 | 72 | . 0067 | . 9911 | 66 |
| 1.0625 | 18 | UNEF | 1.002 | 83.8 | 1.015 | 65.8 | 1 | 1.0000 | 87 | . 00669 | 1.0069 | 68 |
| 1.0625 | 20 | UN | 1.008 | 83.9 | 1.020 | 65.4 | $1_{1 / 64}$ | 1.0156 | 72 | . 00070 | 1.0226 | 61 |
| 1.0625 | 28 | UN | 1.024 | 83.0 | 1.032 | 65.7 | 11/32 | 1.0312 | 67 | . 0071 | 1.0383 | 52 |
| 1.125 | 7 | UNC | . 970 | 83.5 | . 998 | 68.4 | \{1/32 | . 9688 | 84 | . 0062 | . 9750 | 81 |
| 1.125 | 8 | UN | . 990 | 83.1 | 1.015 | 67.7 | ${ }_{1}^{16364}$ | .9844 1.0000 | 76 77 | . 00067 | .9911 1.0069 | 72 |
| 1.125 | 12 | UNF | 1.035 | 83.1 | 1.053 | 66.5 | [11/32 | 1.0312 | 87 | . 0071 | 1.0383 | 80 |
| 1.125 | 16 | UN | 1.057 | 83.8 | 1.071 | 66.5 | ${ }_{(11264}^{16}$ | 1.0469 1.0625 | 72 | . 0072 | 1.0541 1.0699 | 65 68 |
| 1.125 | 18 | UNEF | 1.065 | 83.1 | 1.078 | 65.1 | $\left\{1^{116}\right.$ | 1.0625 | 87 |  |  |  |
| 1.125 | 20 | UN | 1.071 | 83.1 | 1.082 | 66.2 | $1_{156}^{156}$ | 1.0781 | 65 | ----- |  |  |
| 1.125 | 28 | UN | 1.086 | 84.1 | 1.095 | 64.7 | $13 / 32$ | 1.0781 1.0938 | 67 |  |  |  |
| 1.1875 | 8 | UN | 1.052 | 83.4 | 1.077 | 68.0 | 11/16 | 1.0625 | 77 |  |  |  |
| 1.1875 | 12 | UN | 1.097 | 83.6 | 1.115 | 67.0 | 13/52 | 1.0938 | 87 |  |  |  |
| 1.1875 | 16 | UN | 1.120 | 83.1 | 1.134 | 65.9 | $11 / 8$ | 1.1250 | 77 |  |  |  |
| 1.1875 | 18 | UNEF | 1.127 | 83.8 | 1.140 | 65.8 | [11/8 | 1.1250 | 87 |  |  |  |
| 1.1875 | 20 | UN | 1.133 | 83.9 | 1.145 | 65.4 | ${ }_{1}^{19} 19.64$ | 1.1406 1.1406 | 65 72 |  |  |  |
| 1.1875 | 28 | UN | 1.149 | 83.0 | 1.157 | 65.7 | 15/32 | 1.1562 | 67 |  |  |  |
| 1.250 | 7 | UNC | 1.095 | 83.5 | 1.123 | 68.4 | 13/32 | 1.0938 | 84 |  |  |  |
| 1.250 | 8 | UN | 1.115 | 83.1 | 1.140 | 67.7 | $11 / 8$ | 1.1250 | 77 |  |  |  |
| 1.250 | 12 | UNE | 1.160 | 83.1 | 1.178 | 66.5 | $\left\{\begin{array}{l}15 / 32 \\ 11^{1 / 64}\end{array}\right.$ | 1.1562 1.1719 | 87 | ----- |  |  |
| 1.250 | 16 | UN | 1.182 | 83.8 | 1.196 | 66.5 | $1{ }^{3} 16$ | 1.1875 | 77 |  |  |  |
| 1.250 | 18 | UNEF | 1.190 | 83.1 | 1.203 | 65.1 | $\left\{1^{3,16}\right.$ | 1.1875 | 87 | - |  |  |
| 1.250 | 20 | UN | 1.196 | 83.1 | 1.207 | 66.2 |  | 1.2031 1.2031 | 65 72 |  |  |  |
| 1.250 | 28 | UN | 1.211 | 84.1 | 1.220 | 64.7 | 17/38 | 1.2188 | 67 |  |  |  |

See footnotes at end of table.

Table A3.1. Tap drill sizes, Unified screw threads, classes $1 B$ and $2 B$-Continued

| Thread size | Threads per inch | Designation | Classes 1 B and 2B minor diameter, internal threads |  |  |  | Tap drills and percent basic thread height |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimum | Percent ${ }^{\text {a }}$ basic thread height. | Maximum | Percent a basic thread height | Drill size |  | Percent of thread | Probable oversize, mean | Probable hole size | Percent of thread |
| in |  |  | in |  | in |  | in | in |  | in | in |  |
| 1.3125 | 8 | UN | 1.177 | 83.4 | 1.202 | 68.0 | $\left\{\begin{array}{l}111 / 6 \\ 1^{13 / 4}\end{array}\right.$ | 1.1719 | 87 |  |  |  |
| 1.3125 | 12 | UN | 1.222 | 83.6 | 1.240 | 67.0 | 17 1/32 | 1.2188 | 87 |  |  |  |
|  |  |  |  |  | 1.240 | . 0 | $11^{15}$ 的 | 1.2344 | 72 |  |  |  |
| 1.3125 | 16 | UN | 1.245 | 83.1 | 1.259 | 65.9 | $11 / 4$ | 1.2500 | 77 |  |  |  |
| 1.3125 | 18 | UNEF | 1.252 | 83.8 | 1.265 | 65.8 | $\left\{\begin{array}{l}11,4 \\ 117\end{array}\right.$ | 1.2500 1.26 .56 | 87 |  |  |  |
| 1.3125 | 20 | UN | 1.258 | 83.9 | 1.270 | 65.4 | ${ }_{1}^{117} 6.64$ | 1.2606 1.2656 | 65 |  |  |  |
| 1.3125 | 28 | UN | 1.274 | 83.0 | 1.282 | 65.7 | 19/32 | 1.2812 | 67 |  |  |  |
| 1.375 | 6 | UNC | 1.195 | 83.1 | 1.225 | 69.3 | $\left\{\begin{array}{l}1^{3 / 6 / 6} \\ 1^{336 / 4}\end{array}\right.$ | 1.1875 1.2031 | 87 79 |  |  |  |
| 1.375 | 6 | UNC | 1.195 | 83.1 | 1.225 | 69.3 | $\left\{\begin{array}{l}1.864 \\ 11564\end{array}\right.$ | 1.2081 | 79 |  |  |  |
| 1.375 | 8 | UN | 1.240 | 83.1 | 1.265 | 67.7 | $1_{11}^{15} 6$ | 1.2344 | 87 |  |  | - |
| 1.375 | 12 | UNF | 1.285 | 83.1 | 1.303 | 66.5 | 19/32 | 1.2812 | 87 | --- |  |  |
| 1.375 | 16 | UN | 1.307 | 83.8 | 1.321 | 66.5 |  | 1.2969 1.3125 | 72 | -- |  |  |
| 1.375 | 18 | UNEF | 1.315 | 83.1 | 1.328 | 65.1 | $\left\{\begin{array}{l}15 \\ 1 / 26\end{array}\right.$ | 1.3125 | 87 |  |  |  |
| 1.375 | 20 | UN | 1.321 | 83.1 | 1.332 | 66.2 | ${ }_{1}^{12164}$ | 1.3281 1.3281 | 65 |  |  |  |
| 1.375 | 28 | UN | 1.336 | 84.1 | 1.345 | 64.7 | $111 / 38$ | 1.3438 | 67 |  |  |  |
| 1.4375 | 6 | UN | 1.257 | 83.4 | 1.288 | 69.1 | $\left\{\begin{array}{l}117 / 64 \\ 19\end{array}\right.$ | 1.2656 1.2812 | 79 |  |  |  |
| 1.4375 | 8 | UN | 1.302 | 83.4 | 1.327 | 68.0 | $\left\{\begin{array}{l}11964 \\ 15\end{array}\right.$ | 1.2969 | 87 |  |  |  |
|  |  |  |  |  |  |  | ${ }^{1111_{32}}$ | 1.3438 | 87 |  |  |  |
| 1.4375 | 12 | UN | 1.347 | 83.6 | 1.365 | 67.0 | $1^{23,364}$ | 1.3594 | 72 |  |  |  |
| 1.4375 | 16 | UN | 1.370 | 83.1 | 1.384 | 65.9 | 13/8 | 1.3750 | 77 |  |  |  |
| 1.4375 | 18 | UNEF | 1.377 | 83.8 | 1.390 | 65.8 | $13 / 8$ | 1.3750 | 87 |  |  |  |
| 1.4375 | 20 | UN | 1.383 | 83.9 | 1.395 | 65.4 | $1{ }^{125} 6$ | 1.3906 | 72 |  |  |  |
| 1.4375 | 28 | UN | 1.399 | 83.0 | 1.407 | 65.7 | $1^{13 / 32}$ | 1.4062 | 67 |  |  |  |
| 1.500 | 6 | UNC | 1.320 | 83.1 | 1.350 | 69.3 |  | 1.3125 1.3281 | 87 |  |  |  |
|  |  |  |  |  |  |  | 123.64 | 1.3594 | 87 |  |  |  |
| 1.500 | 8 | UN | 1.365 | 83.1 | 1.390 | 67.7 | $13 / 8$ | 1.3750 | 77 |  |  |  |
| 1.500 | 12 | UNF | 1.410 | 83.1 | 1.428 | 66.5 | $\left\{\begin{array}{l}113 / 22 \\ 12764\end{array}\right.$ | 1.4062 1.4219 | 87 72 | - |  |  |
| 1.500 | 16 | UN | 1.432 | 83.8 | 1.446 | 66.5 | 1716 | 1.4375 | 77 |  |  |  |
| 1.500 | 18 | UNEF | 1.440 | 83.1 | 1.452 | 66.5 | $17 / 16$ | 1.4375 | 87 |  |  |  |
| 1.500 | 20 | UN | 1.446 | 83.1 | 1.457 | 66.2 | 1296 | 1.4531 | 72 |  |  |  |
| 1.500 | 28 | UN | 1.461 | 84.1 | 1.470 | 64.7 | $1^{15 / 32}$ | 1.4688 | 67 |  |  |  |
| 1.5625 | 6 | UN | 1.382 | 83.4 | 1.413 | 69.1 | $\left\{\begin{array}{l}125 / 64 \\ 1{ }^{13,383}\end{array}\right.$ | 1.3906 1.4062 | 79 |  |  |  |
|  |  |  |  |  |  |  | $1^{27}{ }^{38} 4$ | 1.4219 | 87 |  |  |  |
| 1.5625 | 8 | UN | 1.427 | 83.4 | 1.452 | 68.0 | $1^{17} 16$ | 1.4375 | 77 |  |  |  |
| 1.5625 | 12 | UN | 1.472 | 83.6 | 1.490 | 67.0 | $\left\{\begin{array}{l}1{ }^{15} \text { /32 } \\ 13164\end{array}\right.$ | 1.4688 1.4844 | 87 |  |  |  |
| 1.5625 | 16 | UN | 1.495 | 83.1 | 1.509 | 65.9 | $11 / 2$ | 1.5000 | 77 | - |  |  |
| 1.5625 | 18 | UNEF | 1.502 | 83.8 | 1.515 | $\bigcirc 5.8$ | $\left\{\begin{array}{l}11 / 2 \\ 1^{33} 64\end{array}\right.$ | 1.5000 1.5156 | 87 |  |  |  |
| 1.5625 | 20 | UN | 1.508 | 83.9 | 1.520 | 65.4 | $13{ }^{3364}$ | 1.5156 | 72 |  |  |  |
| 1.625 | 6 | UN | 1.445 | 83.1 | 1.475 | 69.3 | $\left\{\begin{array}{l}129 \\ 1254\end{array}\right.$ | 1.4531 | 79 | -- |  |  |
| 1.625 | 8 | UN | 1.490 | 83.1 | 1.515 | 67.7 | $1{ }^{31} 164$ | 1.4844 | 87 |  |  |  |
|  | 8 | U |  | 83.1 | 1.515 | 67.7 | $11 / 2$ | 1.5000 | 77 | - |  |  |
| 1.625 | 12 | UN | 1.535 | 83.1 | 1.553 | 66.5 | $\left\{\begin{array}{l}117 / 32 \\ 1^{35,64}\end{array}\right.$ | 1.5312 1.5469 | 87 |  |  |  |
| 1.625 | 16 | UN | 1.557 | 83.8 | 1.571 | 66.5 | 19,16 | 1.5625 | 77 |  |  |  |
| 1.625 | 18 | UNET | 1.565 | 83.1 | 1.578 | 65.1 | $\left\{\begin{array}{l}19,16 \\ 137 / 4\end{array}\right.$ | 1.5625 1.5781 1.581 | 87 |  |  |  |
| 1.625 | 20 | UN | 1.571 | 83.1 | 1.582 | 66.2 | $1{ }^{37} 64$ | 1.5781 | 72 | ----- | ----- |  |
|  |  |  |  |  |  |  |  | 1.5000 | 87 |  |  |  |
| 1.6875 | 6 | UN | 1.507 | 83.4 | 1.538 | 69.1 | $\left\{\begin{array}{l}133 / 84 \\ 117 / 3\end{array}\right.$ | 1.5156 1.5312 | 79 | - | -- |  |
| 1.6875 | 8 | UN | 1.552 | 83.4 | 1.577 | 68.0 | $1^{9} / 16$ | 1.5625 | 77 |  |  |  |
| 1.6875 | 12 | UN | 1.597 | 83.6 | 1.615 | 67.0 | $\left\{\begin{array}{l}119 / 52 \\ 139\end{array}\right.$ | 1.5938 | 87 | ------ |  |  |
| 1.6875 | 16 | UN | 1.620 | 83.1 | 1.634 | 65.9 | 15/84 | 1.6094 | 77 |  |  |  |
| 1.6875 | 18 | UNEF | 1.627 | 83.8 | 1.640 | 65.8 | $\left\{\begin{array}{l}15 / 8 \\ 1{ }^{11} \text {, }\end{array}\right.$ | 1.6250 1.6406 | 87 | ----- |  |  |
| 1.6875 | 20 | UN | 1.633 | 83.9 | 1.645 | 65.4 | 14164 | 1.6406 | 72 |  |  |  |
| 1.750 | 5 | UNC | 1.534 | 83.1 | 1.568 | 70.1 | $\left\{\begin{array}{l}177 / 32 \\ 1356 \\ 15\end{array}\right.$ | 1.5312 | 84 |  |  |  |
| 1.750 | 5 | UNC | 1.534 | 83.1 | 1.868 | 70.1 | $\left\{\begin{array}{l}135 \\ 19 \\ 1964\end{array}\right.$ | 1.5469 1.5625 | 78 |  |  |  |
| 1.750 | 6 | UN | 1.570 | 83.1 | 1.600 | 69.3 | $\left\{1^{37} 6.6\right.$ | 1.5781 | 79 | - | - |  |
|  |  |  |  |  |  |  | $1^{19} 38$. | 1.5938 | 72 |  |  |  |
|  |  |  |  |  |  |  | 13964 | 1.6094 | 87 |  |  |  |
| 1.750 | 8 | UN | 1.615 | 83.1 | 1.640 | 67.7 | $\left\{\begin{array}{l}15 / 8 \\ 1 / 1\end{array}\right.$ | 1.6250 | 77 | ------- | ------ |  |
|  |  |  |  |  |  |  | $1_{121}^{1 / 4}$ | 1.6406 1.6562 | 67 87 | --------- |  |  |
| 1.750 | 12 | UN | 1.660 | 83.1 | 1.678 | 66.5 | $\left\{\begin{array}{l}121 / 32 \\ 14364\end{array}\right.$ | 1.6562 1.6719 | 87 |  |  |  |
| 1.750 | 16 |  |  | 83.8 |  |  | $11_{16}^{\text {6/ }}$ | 1.6875 | 77 |  |  |  |
| 1.750 | 20 | UN | $1.696$ | 83.1 | 1.707 | 66.2 | 14564 | 1.7031 | 72 | ------- |  | -------- |

[^22]Table A3.1. Tap drill sizes, Unified screw threads, classes 1B and 2B-Continued

| Thread size | Threads per inch | Designation | Classes 1B and 2B minor diameter, internal threads |  |  |  | Tap drills and percent basic thread height |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimum | Percent a basic thread height | Maximum | Percent a basic thread height | Drill size |  | Percent of thread | Probable oversize, mean | Probable hole size | Percent of thread |
| in |  |  | in |  | in |  | $\left(15 /{ }^{\text {in }}\right.$ | $\begin{aligned} & i n \\ & 1.6250 \end{aligned}$ | 87 |  |  |  |
| 1.8125 | 6 | UN | 1.632 | 83.4 | 1.663 | 69.1 |  | 1.6406 | 79 |  |  |  |
|  |  |  |  |  |  |  | $1^{21 / 32}$ | 1.6562 | 72 |  |  |  |
| 1.8125 | 8 | UN | 1.677 | 83.4 | 1.702 | 68.0 | $\left\{\begin{array}{l}1{ }^{13 / 364} \\ 1^{11 / 16}\end{array}\right.$ | 1.6719 1.6875 | 87 |  |  |  |
| 1.8125 | 12 | UN | 1.722 | 83.6 | 1.740 | 67.0 | $1{ }^{23}$ \% 31 | 1.7188 | 87 |  |  |  |
| 1.8125 | 16 | UN | 1.745 | 83.1 | 1.759 | 65.9 |  | 1.7344 1.7500 | 72 |  |  |  |
| 1.8125 | 20 | UN | 1.758 | 83.9 | 1.770 | 65.4 | 1496 | 1.7656 | 72 | - |  |  |
| 1.875 | 6 | UN | 1.695 | 83.1 | 1.725 | 69.3 | $\left\{\begin{array}{l}145 / 64 \\ 123\end{array}\right.$ | 1.7031 1.7188 | 79 |  |  |  |
| 1.875 | 8 | UN | 1.740 | 83.1 | 1.765 | 67.7 | $13 / 4$ | 1.7500 | 77 |  |  |  |
| 1.875 | 12 | UN | 1.785 | 83.1 | 1.803 | 66.5 | $\left\{\begin{array}{l}125 / 32 \\ 1^{51} \text { /4,4 }\end{array}\right.$ | 1.7812 1.7969 | 87 |  |  |  |
| 1.875 | 16 | UN | 1.807 | 83.8 | 1.821 | 66.5 | ${ }^{1} 13$ 13/16 | 1.8125 | 77 |  |  |  |
| 1.875 | 20 | UN | 1.821 | 83.1 | 1.832 | 66.2 | $1{ }^{53} 64$ | 1.8281 | 72 |  |  |  |
| 1.9375 | 6 | UN | 1.757 | 83.4 | 1.788 | 69.1 | $\left\{\begin{array}{l}1+964 \\ 1256\end{array}\right.$ | 1.7656 | 79 |  |  |  |
|  |  |  |  |  |  |  | ${ }^{151 / 64}$ | 1.7812 1.7969 | 72 |  |  |  |
| 1.9375 | 8 | UN | 1.802 | 83.4 | 1.827 | 68.0 | $\left\{\begin{array}{l}1{ }^{13 / 64} \\ 13^{16}\end{array}\right.$ | 1.7965 | 77 |  |  |  |
| 1.9375 | 12 | UN | 1.847 | 83.6 | 1.865 | 67.0 | $\left\{\begin{array}{l}127 / 32 \\ 155 / 64\end{array}\right.$ | 1.8438 1.8594 | 87 72 |  |  |  |
| 1.9375 | 16 | UN | 1.870 | 83.1 | 1.884 | 65.9 | $17 / 8$ | 1.8750 | 77 |  |  |  |
| 1.9375 | 20 | UN | 1.883 | 83.9 | 1.895 | 65.4 | 1576 | 1.8906 | 72 |  |  |  |
| 2.000 | 4.5 | UNC | 1.759 | 83.5 | 1.795 | 71.0 | $1^{25 / 52}$ | 1.7812 | 76 |  |  |  |
| 2.000 | 6 | UN | 1.820 | 83.1 | 1.850 | 69.3 | $\left\{\begin{array}{l}153 \\ 127 / 82\end{array}\right.$ | 1.8281 1.8438 | 79 72 72 |  |  |  |
| 2.000 | 8 | UN | 1.865 | 83.1 | 1.890 | 67.7 | $17 / 8$ | 1.8750 | 77 |  |  |  |
| 2.000 | 12 | UN | 1.910 | 83.1 | 1.928 | 66.5 | $\left\{\begin{array}{l}129 / 22 \\ 159\end{array}\right.$ | 1.9062 1.9219 | 87 |  |  |  |
| 2.000 | 16 | UN | 1.932 | 83.8 | 1.946 | 66.5 | $1^{15,16}$ | 1.9375 | 77 |  |  |  |
| 2.000 | 20 | UN | 1.946 | 83.1 | 1.957 | 66.2 | $1^{61} 16$ | 1.9531 | 72 |  |  |  |
| 2.0625 | 16 | UNS | 1.995 | 83.1 | 2.009 | 65.9 | 2 | 2.0000 | 77 |  |  |  |
| 2.125 | 6 | UN | 1.945 | 83.1 | 1.975 | 69.3 | $\left\{\begin{array}{l}161 / 64 \\ 131 / 32\end{array}\right.$ | 1.9531 1.9688 | 79 72 |  |  |  |
| 2.125 | 8 | UN | 1.990 | 83.1 | 2.015 | 67.7 | 2 | 2.0000 | 77 |  |  |  |
| 2.125 | 12 | UN | 2.035 | 83.1 | 2.053 | 66.5 | ${ }^{21} 13$ | 2.0312 | 87 |  |  |  |
| 2.125 | 16 | UN | 2.057 | 83.8 | 2.071 | 66.5 | ${ }_{2}^{116}$ | 2.0625 | 77 |  |  |  |
| 2.125 | 20 | UN | 2.071 | 83.1 | 2.082 | 66.2 | 21/16 | 2.0625 | 96 | - |  |  |
| 2.1875 | 16 | UNS | 2.120 | 83.1 | 2.134 | 65.9 | 21/8 | 2.1250 | 77 |  |  |  |
| 2.250 | 4.5 | UNC | 2.090 | 83.5 | 2.045 | 71.0 | $\left\{\begin{array}{l}21 / 32\end{array}\right.$ | 2.0000 2.0312 | 87 |  |  |  |
| 2.250 | 6 | UN | 2.070 | 83.1 | 2.100 | 69.3 | 21.16 | 2.0625 | 87 |  |  |  |
| 2.250 | 8 | UN | 2.115 | 83.1 | 2.140 | 67.7 | $21 / 8$ | 2.1250 | 77 |  |  |  |
| 2.250 | 12 | UN | 2.160 | 83.1 | 2.178 | 66.5 | $2^{5 / 32}$ | 2.1562 | 87 |  |  |  |
| 2.250 | 16 | UN | 2.182 | 83.8 | 2.196 | 66.5 | $2^{3}$ /16 | 2.1875 | 77 |  |  |  |
| 2.250 | 20 | UN | 2.196 | 83.1 | 2.207 | 66.2 | $2^{3}$ /16 | 2.1875 | 96 | - |  |  |
| 2.3125 | 16 | UNS | 2.245 | 83.1 | 2.259 | 65.9 | $21 / 4$ | 2.2500 | 77 | -- |  |  |
| 2.375 | 6 | UN | 2.195 | 83.1 | 2.226 | 68.8 | $2^{3}$, 16 | 2.1875 | 87 |  |  |  |
| 2.375 2.375 | 8 | UN | 2.240 | 83.1 | 2.265 | 67.7 | $21 / 4$ | 2.2500 | 77 |  |  |  |
| 2.375 2.375 | 12 | UN | 2.285 | 83.1 | 2.303 | 66.5 | ${ }_{2}^{58} \mathrm{~mm}$ | 2.2835 2.3125 | 85 |  |  |  |
| 2.375 2.375 | 16 20 | UN | 2.307 2.321 | 83.8 83.1 | 2.321 2.332 | 66.5 66.2 | $2^{5} / 66$ $2^{5} / 16$ | 2.3125 2.3125 | 77 |  |  |  |
| 2.4375 | 16 | UNS | 2.370 | 83.1 | 2.384 | 65.9 | $23 / 8$ | 2.3750 | 77 |  |  |  |
| 2.500 | 4 | UNC | 2.229 | 83.4 | 2.267 | 71.7 | $\left\{\begin{array}{l}27 / 32 \\ 18\end{array}\right.$ | ${ }_{2}^{2.2188}$ | 87 |  |  |  |
| 2.500 | 6 | UN | 2.320 | 83.1 | 2.350 | 69.3 | ${ }_{2}{ }^{5} 16$ | 2.3125 | 87 |  |  |  |
| 2.500 | 8 | UN | 2.365 | 83.1 | 2.390 | 67.7 | $23 / 8$ | 2.3750 | 77 |  |  |  |
| 2.500 | 12 | UN | 2.410 | 83.1 | 2.428 | 66.5 | $2^{13} 3{ }^{1}$ | 2.4062 | 87 | ----- |  |  |
| 2.500 | 16 | UN | 2.432 | 83.8 | 2.446 | 66.5 | $2^{7} 16$ | 2.4375 | 77 |  |  |  |
| 2.500 | 20 | UN | 2.446 | 83.1 | 2.457 | 66.2 | $2^{7}$ \%6 | 2.4375 | 96 | -------- | ------ | --------- |
| 2.625 | 4 | UN | 2.354 | 83.4 | 2.392 | 71.7 | $\left\{{ }_{2}^{211 / 32}\right.$ | ${ }_{2}^{2.3438}$ | 87 | -- |  |  |
| 2.625 | 6 | UN | 2.445 | 83.1 | 2.475 | 69.3 | ${ }^{27} 16$ | 2.4375 | 87 |  |  |  |
| 2.625 | 8 | UN | 2.490 | 83.1 | 2.515 | 67.7 | $21 / 2$ | 2.5000 | 77 |  |  |  |
| 2.625 | 12 | UN | 2.535 | 83.1 | 2.553 | 66.5 | $2^{17} / 38$ | 2.5312 | 87 |  |  |  |
| 2.625 | 16 | UN | 2.557 | 83.8 | 2.571 | 66.5 | 29 /6 | 2.5625 | 77 |  |  |  |
| 2.625 | 20 | UN | 2.571 | 83.1 | 2.582 | 66.2 | $2^{9}$ /6 | 2.5625 | 96 |  |  |  |
| 2.750 | 4 | UNC | 2.479 | 83.4 | 2.517 | 71.7 | 21/2 | 2.5000 | 77 |  |  |  |
| 2.750 | 6 | UN | 2.570 | 83.1 | 2.600 | 69.3 | $2^{9}$ 16 | 2.5625 | 87 |  |  |  |
| ${ }_{2}^{2.750}$ | 8 | UN | 2.615 | 83.1 | 2.640 | 67.7 | $25 / 8$ | ${ }_{2}^{2.6250}$ | 77 |  |  |  |
| 2.750 | 12 | UN | 2.660 | 83.1 | 2.678 | 66.5 | $2^{21 / 32}$ | 2.6562 | 87 |  |  |  |
| 2.750 2.750 | 16 | UN | 2.682 | 83.8 | 2.696 | 66.5 | $2^{111} 16$ | 2.6875 | 77 |  |  |  |
| 2.750 | 20 | UN | 2.696 | 83.1 | 2.707 | 66.2 | $2^{11 / 16}$ | 2.6875 | 96 | ------- | ------- | -------- |

[^23]Table A3.1. Tap drill sizes, Unified screw threads, classes 1B and 2B—Continued

| Thread size | Threads per inch | Designation | Classes 1B and 2B minor diameter, internal threads |  |  |  | Tap drills and percent basic thread height |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimuin | Percent a basic thread height | Maximum | Percent ${ }^{\text {a }}$ basic thread height | Drill size |  | Percent of thread | Probable oversize, mean | Probable hole size | Percent of thread |
| $\stackrel{\text { in }}{2}$ |  |  | $\begin{gathered} i n \\ 2.604 \end{gathered}$ |  | ${ }_{2}^{\text {in }} 642$ |  | 25. in | in |  |  |  |  |
| 2.875 2.875 | 4 | UN | $\begin{aligned} & 2.604 \\ & 2.695 \end{aligned}$ | 83.4 83.1 | 2.642 2.725 | 71.7 69 | ${ }_{2}^{25 / 8}$ | 2.6250 | 77 |  |  |  |
| 2.875 | 8 | UN | 2.740 | 83.1 | 2.765 | 67.7 | $23 / 4$ | 2.6875 2.7500 | 87 |  |  |  |
| 2.875 | 12 | UN | 2.785 | 83.1 | 2.803 | 66.5 | $2{ }^{25 / 3}$ | 2.7812 | 87 |  |  |  |
| 2.875 | 16 | UN | 2.807 | 83.8 | 2.821 | 66.5 | $2{ }^{13} 116$ | 2.8125 | 77 |  |  |  |
| 2.875 | 20 | UN | 2.821 | 83.1 | 2.832 | 66.2 | $2^{13 / 16}$ | 2.8125 | 96 |  |  |  |
| 3.000 | 4 | UNC | 2.729 | 83.4 | 2.767 | 71.7 | 23/4 | 2.7500 | 77 |  |  |  |
| 3.000 | ${ }_{8}$ | UN | 2.820 | 83.1 | 2.850 | 69.3 | $2^{13, / 46}$ | 2.8125 | 87 |  |  |  |
| 3.000 | 8 | UN | 2.865 2.910 | 83.1 | 2.890 2 | 67.7 | $27 / 8$ | 2.8750 | 77 |  |  |  |
| 3.000 | 12 | UN | 2.910 | 83.1 | 2.928 | 66.5 | 74 mm | 2.9134 | 80 |  |  |  |
| 3.000 | 16 | UN | 2.932 | 83.8 | 2.946 | 66.5 | ${ }^{215} / 16$ | 2.9375 | 77 |  |  |  |
| 3.000 | 20 | UN | 2.946 | 83.1 | 2.957 | 66.2 | 215/16 | 2.9375 | 96 |  |  |  |
| 3.250 | 4 | UNC | 2.979 | 83.4 | 3.017 | 71.7 | 3 | 3.0000 | 77 |  |  |  |
| 3.500 | 4 | UNC | 3.229 | 83.4 | 3.267 | 71.7 | $31 / 4$ | 3.2500 | 77 |  |  |  |
| 3.750 | 4 | UNC | 3.479 | 83.4 | 3.517 | 71.7 | $31 / 2$ | 3.5000 | 77 |  |  |  |

${ }^{\text {a }} 100 \%$ basic thread height $=0.75 H$ (values of 0.75 H are shown in col. 14 , table 2.1 ).

Table A3.2. Tap drill sizes, Unified screw threads, class $3 B$


See footnotes at end of table.

Table A3.2. Tap drill sizes, Unified screw threads, class 3B-Continued

| Thread size | Threads per inch | Designation | Class 3B minor diameter, internal threads |  |  |  | Tap drills and percent basic thread height |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimum | Percent a basic thread height | Maximum | Percent a basic thread height | Drill size |  | Percent of thread | Probable oversize, mean | Probable hole size | Percent of thread |
| $\begin{aligned} & i n \\ & .164 \end{aligned}$ | 32 | UNC | $\begin{aligned} & \text { in } \\ & .1300 \end{aligned}$ | 83.8 | $\begin{aligned} & \text { in } \\ & .1389 \end{aligned}$ | 61.8 | \# $29{ }^{\text {in }}$ | in 1360 | 69 | in | in .1389 |  |
|  |  |  |  |  |  |  | \#29 | . 1360 | 78 | . 0029 | . 1389 | 62 70 |
| . 164 | 36 | UNF | . 1340 | 83.1 | . 1416 | 62.1 | \#28 | . 1405 | 65 | . 0029 | . 1434 | 57 |
|  |  |  |  |  |  |  |  | . 1406 | 65 | . 0029 | . 1435 | 57 |
|  |  |  |  |  |  |  | ( +27 | . 1440 | 85 | . 0032 | . 1472 | 79 |
| . 190 | 24 | U NC | . 1450 | 83.1 | . 1555 | 63.7 | $\left\{\begin{array}{l}\text { \#26 } \\ \# 25\end{array}\right.$ | .1470 .1495 | 79 75 | .0032 .0032 | .1502 .1527 | 74 69 |
| . 190 | 24 | UNC | . 1450 | 83.1 | . 1505 | 63.7 | $\left\{\begin{array}{l}\text { \#25 } \\ \# 24\end{array}\right.$ | . 1520 | 70 | .0032 | . 1552 | 69 64 |
|  |  |  |  |  |  |  | \#23 | . 1540 | 66 | . 0032 | . 1572 | 61 |
|  |  |  |  |  |  |  | $\int_{\text {¢ }}^{5} \mathrm{~s} 22$ | .1562 .1570 | 83 81 81 | . 00032 | .1594 .1602 | 75 73 |
| . 190 | 32 | UNF | . 1560 | 83.8 | . 1641 | 63.8 | $\left\{\begin{array}{l}\text { \#22 } \\ \# 21\end{array}\right.$ | . 1590 | 81 76 | .0032 | . 1602 | 73 68 |
|  |  |  |  |  |  |  | \# 20 | . 1610 | 71 | . 0032 | . 1642 | 64 |
|  |  |  |  |  |  |  |  | . 1719 | 82 | . 0035 | . 1754 | 75 |
| . 216 | 24 | UNC | .1710 | 83.1 | .1807 | 65.2 | \#17 $\# 16$ | .1730 .1770 | 79 72 | . 00035 | .1765 .1805 | 73 66 |
|  |  |  |  |  |  |  | \#15 | . 1800 | 67 | .0035 | . 1835 | 66 60 |
|  |  |  |  |  |  |  | \#16 | . 1770 | 84 | . 00035 | .1805 | 77 |
| . 216 | 28 | UNF | . 1770 | 84.1 | . 1857 | 65.3 | \#15 | .1800 .1820 | 78 | . 00035 | . 1835 | 70 66 |
|  |  |  |  |  |  |  | \#14 | . 1820 | 73 67 | . 00035 | . 1855 | 66 59 |
|  |  |  |  |  |  |  | \#14 | . 1820 | 84 | . 0035 | . 1855 | 75 |
| . 216 | 32 | UNEF | . 1820 | 83.8 | .1895 | 65.3 | \# 13 | . 1850 | 76 70 | .0035 | .1885 .1910 | 68 68 |
|  |  |  |  |  |  |  | \# 12 | . 1890 | 67 | . 0035 | . 1925 | 58 |
|  |  |  |  |  |  |  | \# 9 | . 1960 | 83 | . 0038 | . 1998 | 77 |
|  |  |  |  |  |  |  | \#8 | . 1990 | 79 | . 0038 | . 2028 | 73 |
| . 250 | 20 | UNC | . 1960 | 83.1 | . 2067 | 66.7 | $\underset{13}{\# 7}$ | . 2010 | 75 | . 0038 | . 2048 | 70 |
|  |  |  |  |  |  |  | \% 64 $\# 6$ | . 20310 | 71 | . 0038 | . 2069 | 66 65 |
|  |  |  |  |  |  |  | \#5 | . 2055 | 69 | . 0038 | . 2093 | 63 |
| . 250 | 28 | UNE | . 2110 | 84.1 | . 2190 | 66.8 | \#3 | . 213188 | 80 | . 00038 | . 2168 | 72 59 |
| . 250 | 32 | UNEF | . 2160 | 83.8 | . 2229 | 66.8 | 7/32 | . 2188 | 77 | . 0038 | . 2226 | 67 |
| . | 32 | UNET |  | 83.8 | .222 | 66.8 | \#2 | . 2210 | 71 | . 0038 | . 2248 | 62 |
| . 3125 | 18 | UNC | . 2520 | 83.8 | . 2630 | 68.6 | S F | . 2570 | 77 | . 0038 | . 2608 | 72 |
|  |  |  |  |  | . |  | G | . 2610 | 71 85 | . 00041 | . 2651 | 66 80 |
| . 3125 | 20 | UN | . 2580 | 83.9 | . 2680 | 68.5 | G ${ }_{\text {G }}$ | . 2610 | 89 | . 00038 | . 26651 | 80 73 |
|  |  |  |  |  |  |  | H | . 2660 | 72 | . 00041 | . 2701 | 65 |
| . 3125 | 24 | U NF | . 2670 | 84.1 | . 2754 | 68.5 | [ 1 | . 2660 | 86 | . 0041 | . 2701 | 78 |
| . 3125 | 28 | UN | . 2740 | 83.0 | . 2807 | 68.5 | J | . 2770 | 77 | . 0041 | . 2811 | 68 |
| . 3125 | 32 | UNEF | . 2790 | 82.5 | . 2847 | 68.5 | $\left\{\begin{array}{l}\text { K }\end{array}\right.$ | . 2810 | 78 78 | .0042 .0042 | . 2852 | 67 67 |
|  |  |  |  |  |  |  | 29/32 | . 2812 | 77 | . 0042 | . 2854 | 67 |
| . 375 | 16 | UNC | . 3070 | 83.8 | . 3182 | 70.0 | $\left\{\begin{array}{l}5,16 \\ 0\end{array}\right.$ | . 3125 | 77 | . 0044 | . 3169 | 72 |
| . 375 | 20 | UN | . 3210 | 83.1 | . 3297 | 69.7 | P | . 3230 | 80 | . 0044 | . 3274 | 73 |
| . 375 | 24 | UNF | . 3300 | 83.1 | . 3372 | 69.8 | Q | . 3320 | 79 | . 0044 | . 3364 | 71 |
| . 375 | 28 | UN | . 3360 | 84.1 | . 3426 | 69.8 | R | . 3390 | 78 | . 0044 | . 3434 | 68 |
| . 375 | 32 | UNEF | .3410 | 83.8 | . 3469 | 69.2 | 11/32 | . 3438 | 77 | . 0045 | . 3483 | 66 |
| . 4375 | 14 | UNC | . 3600 | 83.5 | .3717 | 70.9 | T | . 3580 | 86 | . 0046 | . 3626 | 81 |
|  |  |  |  |  |  |  | ${ }^{23 / 64}$ | . 3594 | 84 | . 0046 | . 3640 | 79 |
| . 4375 | 16 | UN | . 3700 | 83.1 | . 3800 | 70.8 | $\left\{\begin{array}{l}3 / 8 \\ V\end{array}\right.$ | .3750 .3770 | 77 | . 00046 | . 3796 | 71 69 |
| . 4375 | 20 | UNF | . 3830 | 83.9 | . 3916 | 70.7 | W | . 3860 | 79 | . 00046 | . 3906 | 72 65 |
|  |  |  |  |  |  |  | [25 64 | . 3906 | 72 | . 0046 | . 3952 | 65 |
| . 4375 | 28 | UNEF | . 3990 | 83.0 | . 4051 | 69.8 | Y | . 4040 | 72 | . 0046 | . 4086 | 62 |
| . 4375 | 32 | UN | . 4040 | 82.5 | . 4094 | 69.2 | $\left\{\begin{array}{l}\mathrm{Y} \\ 13 / 3\end{array}\right.$ | .4040 .4062 | 83 77 | . 00046 | .4086 .4108 | 71 66 |
|  |  |  |  |  |  |  |  | . 4130 | 80 | . 0047 | . 4177 | 76 |
| . 500 | 12 | UNS | .4100 | 83.1 | . 4223 | 71.8 | $\{2764$ | . 4219 | 72 | . 0047 | . 4266 | 68 |
| . 500 | 13 | UNC | . 4170 |  | .4284 |  | ${ }^{27 \% 64}$ | .4219 | 78 | . 00047 | . 4266 | 73 |
| . 500 | 16 20 | UNF | .4320 .4460 | 83.8 83.1 | .4419 .4537 | 71.6 | 7/16, | . 4375 | 77 | . 00047 | . 4422 | 71 |
| . 500 | 28 | UNEF | . 4610 | 84.1 | . 4676 | 69.8 | 11.811111 | . 4646 | 76 | . 0047 | . 4693 | 66 |
| . 500 | 32 | UN | . 4660 | 83.8 | . 4719 | 69.2 | 15/32 | . 4688 | 77 | . 0048 | . 4736 | 65 |
| . 5625 | 12 | UNC | . 4720 | 83.6 | . 4843 | 72.2 | $\left\{\begin{array}{l}15 / 3 \\ 31 / 2\end{array}\right.$ | .4688 .4844 | 87 72 | .0048 .0048 | .4736 .4892 | 82 |
| . 5625 | 16 | UN | . 4950 | 83.1 | . 5040 | 72.1 | $1 / 24$ | . 5000 | 77 | . 0048 | . 5048 | 71 |
| . 5625 | 18 | UNF | . 5020 | 83.8 | . 5106 | 71.9 | $\left\{\begin{array}{l}1 / 2 \\ 0.5069\end{array}\right.$ | . 50000 | 87 78 | . 00048 | . 5048 | 80 71 |
| . 5625 | 20 | UN | . 5080 | 83.9 | . 5162 | 71.3 | 3364 | . 5156 | 72 | . 0048 | . 5204 | 65 |
| . 5625 | 24 | UNEF | . 5170 | 84.1 | . 5244 | 70.4 | $\left\{{ }^{33,64}\right.$ | . 5156 | 87 | . 0048 | . 5204 | 78 |
| . 5625 | 28 | UN | . 5240 | 83.0 | . 5301 | 69.8 | 0.5203 0.5263 | . 52263 | 78 78 | . 0048 | . 52312 | 69 67 |
| . 5625 | 32 | UN | . 5290 | 82.5 | . 5344 | 69.2 | $17 / 32$ | . 5312 | 77 | . 0049 | . 5361 | 65 |

[^24]Table A3.2. Tap drill sizes, Unified screw threads, class $3 B$-Continued

| Thread size | Threads per inch | Designation | Class 3B minor diameter, internal threads |  |  |  | Tap drills and percent basic thread height |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimum | Percent a basic thread height | Maximum | Percent a basic thread height | Drill size |  | Percent of thread | Probable oversize, mean | Probable hole size | Percent of thread |
| in |  |  | in |  | in |  | 17 in |  |  |  |  |  |
| $.625$ | 11 | UNC | $.5270$ | 83.0 | . 5391 | 72.7 | 17/32 | . 5312 | 79 | . 0049 | . 5361 | 75 |
| . 625 | 12 | UN | . 5350 | 83.1 | . 5463 | 72.7 | ${ }^{39} 64$ | . 5469 | 72 | . 0049 | . 5518 | 68 |
| . 625 | 16 | UN | . 5570 | 83.8 | . 5662 | 72.4 | 9,16 | . 5625 | 87 | . 0049 | . 5674 | 71 |
| . 625 | 18 | UNF | . 5650 | 83.1 | . 5730 | 72.1 | $\left\{\begin{array}{l}\text { 26 } \\ 0.5687\end{array}\right.$ | . 56258 | 87 78 | . 00049 | . 5674 | 80 |
| . 625 | - 20 | UN | . 5710 | 83.1 | . 5787 | 71.3 | $37 / 64$ | . .5781 | 78 | . 0049 | . 58380 | 61 |
| . 625 | 24 | UNEF | . 5800 | 83.1 | . 5869 | 70.4 | $\left\{\begin{array}{l}37 / 48 \\ 0.5828\end{array}\right.$ | .5781 .5828 .5828 | 87 78 | . 0049 | . 58380 | 78 |
| . 625 | 28 | UN | . 5860 | 84.1 | . 5926 | 69.8 | 0.5828 | . 58828 | 78 91 | . 0049 | . 58877 | 69 80 |
| . 625 | 32 | UN | . 5910 | 83.8 | . 5969 | 69.2 | 19 万2 | . 5938 | 77 | . 0049 | . .5987 | 65 |
| . 6875 | 12 | UN | . 5970 | 83.6 | . 6085 | 73.0 | 19/32 | . 5938 | 87 | . 0049 | . 5987 | 82 |
| . 6875 | 16 | UN | . 6200 | 83.1 | . 6284 | 72.8 | $5 / 8$ | . 6250 | 77 | . 0050 | . 6300 | 71 |
| . 68875 | 20 | UN | . 6330 | 83.9 | . 6412 | 71.3 | 4164 | . 6406 | 72 | . 0050 | . 6456 | 65 |
| . 68875 | 24 28 | UNEF | .6420 .6490 | 84.1 83.0 | . 6494 | 70.4 | ${ }^{416.6}$ | .6406 | 87 | . 0050 | .6456 | 77 |
| . 6875 | 32 | UN | . 6549 | 83.0 82.5 | . 65594 | 69.8 69.2 | ${ }_{21}^{16.5} 5$ | . 6496 | 82 77 | .0050 .0050 | . 6546 | 71 65 |
| . 750 | 10 | UNC | . 6420 | 83.1 | . 6545 | 73.5 | $41 / 64$ | . 6406 | 84 | . 0050 | . 6456 | 80 |
| . 750 | 12 | UN | . 6600 | 83.1 | . 6707 | 73.3 | ${ }^{21 / 32}$ | . 6562 | 87 | . 0050 | . 6612 | 82 |
| .750 .750 | 16 | UNF | . 6820 | 83.8 | . 6908 | 72.9 | 11.16 | . 6875 | 77 | . 0050 | . 6925 | 71 |
| . 750 | 28 | UN | . 69110 | 84.1 | . 70376 | 69.8 | 18 mm | .7031 .7087 | 72 89 | . 00051 | . 71382 | 64 78 |
| . 750 | 32 | UN | . 7160 | 83.8 | . 7219 | 69.2 | ${ }^{23} / 32$ | . 7188 | 77 | . 0051 | . 7239 | 64 |
| . 8125 | 12 | UN | . 7220 | 83.6 | . 7329 | 73.5 | 18.5 mm | . 7283 | 78 | . 0051 | . 7334 | 73 |
| . 8125 | 16 | UN | . 7450 | 83.1 | . 7533 | 72.9 | $3 / 4$ | . 7500 | 77 | . 0052 | . 7552 | 71 |
| . 8125 | 20 | UNEF | . 7580 | 83.9 | . 7662 | 71.3 | 9964 | . 7656 | 72 | . 0052 | . 7708 | 64 |
| . 8125 | 28 | UN | . 7740 | 83.0 | . 7801 | 69.8 | 19.75 mm | . 7776 | 75 | . 0052 | . 7828 | 64 |
| . 8125 | 32 | UN | . 7790 | 82.5 | . 7844 | 69.2 | ${ }^{25} / 32$ | . 7812 | 77 | . 0052 | .7864 | 64 |
| . 875 | 9 | UNC | . 7550 | 83.1 | . 7681 | 74.1 | ${ }^{49} 6.6$ | . 7656 | 76 | . 0052 | . 7708 | 72 |
| . 875 | 12 | UN | . 7850 | 83.1 | . 7952 | 73.7 | 25/32 | . 7812 | 87 | . 0052 | . 7864 | 82 |
| . 875 | 14 | UNF | . 7980 | 83.0 | . 8068 | 73.5 | $\left\{\begin{array}{l}51 / 64 \\ 0.8024\end{array}\right.$ | . 7969 | 84 | . 00052 | .8021 .8076 | 79 73 |
| . 875 | 16 | UN | . 8070 | 83.8 | . 8158 | 72.9 | 13/66 | . 8125 | 77 | . 0053 | . 8076 | 73 70 |
| . 875 | 20 | UNEF | . 8210 | 83.1 | . 8287 | 71.3 | ${ }^{53} 6$. | . 8281 | 72 | . 0054 | . 8335 | 64 |
| . 875 | 28 | UN | . 8360 | 84.1 | . 8426 | 69.8 | 21.25 mm | . 8366 | 83 | . 0054 | . 8420 | 71 |
| . 875 | 32 | UN | . 8410 | 83.8 | . 8469 | 69.2 | 27/32 | . 8438 | 77 | . 0055 | . 8493 | 63 |
| . 9375 | 12 | UN | . 8470 | 83.6 | . 8575 | 73.9 | 27/32 | . 8438 | 87 | . 0055 | . 8493 | 81 |
| . 9375 | 16 | UN | . 8700 | 83.1 | . 8783 | 72.9 | 7/8 | . 8750 | 77 | . 0057 | . 8807 | 70 |
| . 9375 | 20 | UNEF | . 8830 | 83.9 | . 8912 | 71.3 |  | . 8906 | 72 | . 0059 | . 8965 | 63 |
| . 9375 | 28 | UN | . 8990 | 83.0 | . 9051 | 69.8 | 22.75 mm | . 8957 | 90 | . 0060 | . 9017 | 77 |
| . 9375 | 32 | UN | . 9040 | 82.5 | . 9094 | 69.2 | 29/32 | . 9062 | 77 | . 0060 | . 9122 | 62 |
| 1.000 | 8 | UNC | . 8650 | 83.1 | . 8797 | 74.1 | $\left\{\begin{array}{l}55 \\ 7 / 84\end{array}\right.$ | .8594 8750 | 87 | . 0059 | . 86533 | 83 |
| 1.000 | 12 | UNF | . 9100 | 83.1 | . 9198 | 74.1 | ${ }_{29} 8$ /38 | . 9062 | 87 | . 0060 | . 9122 | 81 |
| 1.000 | 14 | UNS | . 9230 | 83.0 | . 9315 | 73.8 | $\left\{\begin{array}{l}59 \\ 0.64 \\ 0.9274\end{array}\right.$ | . 9219 | 84 78 | . 00660 | . 92735 | 78 |
| 1.000 | 16 | UN | . 9320 | 83.8 | . 9408 | 72.9 | ${ }_{15,16}^{0.9274}$ | . 92375 | 78 | . 00661 | . 93335 | 72 69 |
| 1.000 | 20 | UNEF | . 9460 | 83.1 | . 9537 | 71.3 | ${ }^{61 / 64}$ | . 9531 | 72 | . 0063 | . 9594 | 63 |
| 1.000 | 28 | UN | . 9610 | 84.1 | . 9676 | 69.8 | 24.5 mm | . 9645 | 77 | . 0064 | . 9709 | 63 |
| 1.000 | 32 | UN | . 9660 | 83.8 | . 9719 | 69.2 | ${ }^{31 / 38}$ | . 9688 | 77 | . 0065 | . 9753 | 61 |
|  |  |  |  |  |  |  | 59\%6 | . 9219 | 87 | . 0060 | . 9279 | 83 |
| 1.0625 | 8 | UN | . 9270 | 83.4 | . 9422 | 74.1 | $\{0.9274$ | . 9274 | 83 | . 0061 | . 9335 | 79 |
|  |  |  |  |  |  |  | ${ }^{15} / 16$ | . 9375 | 77 | . 0062 | . 9437 | 73 |
| 1.0625 | 12 | UN | . 9720 | 83.6 | . 9823 | 74.1 | 31/32 | . 9688 | 87 | . 0065 | . 9753 | 81 |
| 1.0625 1.0625 | 16 | UN | . 9950 | 83.1 | 1.0033 | 72.9 | 1 | 1.0000 | 77 | . 0069 | 1.0069 | 68 |
| 1.0625 1.0625 | 18 | UNEF | 1.0020 | 83.8 | 1.0105 | 72.1 | 1 | 1.0000 | 87 | . 0069 | 1.0069 | 77 |
| 1.0625 | $\stackrel{20}{28}$ | UN | 1.0080 1.0240 | 83.9 83.0 | 1.0162 1.0301 | 71.3 69.8 | ${ }^{11 / 64}$ | 1.0156 | 72 67 | . 00070 | 1.0226 | 61 |
| 1.0625 |  | UN | 1.0240 | 83.0 | 1.0301 | 69.8 | 1/32 | 1.0312 | 67 | . 0071 | 1.0383 | 52 |
| 1.125 | 7 | UNC | . 9700 | 83.5 | . 9875 | 74.1 | $\left\{\begin{array}{l}31 / 32 \\ 63\end{array}\right.$ | . 9688 | 84 | . 0062 | .9750 | 81 |
| 1.125 | 8 | UN | . 9900 | 83.1 | 1.0047 | 74.1 | $1{ }^{64}$ | 1.9000 | 77 | . 0069 | 1.9911 | 72 |
| 1.125 | 12 | UNF | 1.0350 | 83.1 | 1.0448 | 74.1 | 11/32 | 1.0312 | 87 | . 0071 | 1.0383 | 80 |
| 1.125 | 16 | UN | 1.0570 | 83.8 | 1.0658 | 72.9 | $11 / 16$ | 1.0625 | 77 | . 0074 | 1.0699 | 68 |
| 1.125 | 18 | UNEF | 1.0650 | 83.1 | 1.0730 | 72.1 | 11/16 | 1.0625 | 87 |  |  |  |
| 1.125 | 20 | UN | 1.0710 | 83.1 | 1.0787 | 71.3 | 15/64 | 1.0781 | 72 |  |  |  |
| 1.125 | 28 | UN | 1.0860 | 84.1 | 1.0926 | 69.8 | 13/32 | 1.0938 | 67 |  |  |  |
| 1.1875 | 8 | UN | 1.0520 | 83.4 | 1.0672 | 74.1 | 11 价 | 1.0625 | 77 |  |  |  |
| 1.1875 | 12 | UN | 1.0970 | 83.6 | 1.1073 | 74.1 | $13 / 32$ | 1.0938 | 87 |  |  |  |
| 1.1875 | 16 | UN | 1.1200 | 83.1 | 1.1283 | 72.9 | 11/8 | 1.1250 | 77 |  |  |  |
| 1.1875 | 18 | UNEF | 1.1270 | 83.8 | 1.1355 | 72.1 | 11/8 | 1.1250 | 87 |  |  |  |
| 1.1875 | 20 | UN | 1.1330 | 83.9 | 1.1412 | 71.3 | 19.64 | 1.1406 | 72 | - |  |  |
| 1.1875 | 28 | UN | 1.1490 | 83.0 | 1.1551 | 69.8 | 29.25 mm | 1.1516 | 77 | ------ | ---- | -------- |
| 1.250 | 7 | UNC | 1.0950 | 83.5 | 1.1125 | 74.1 | $13 / 32$ | 1.0938 | 84 |  |  |  |
| 1.250 | 8 | UN | 1.1150 | 83.1 | 1.1297 | 74.1 | 11/8 | 1.1250 | 77 |  |  |  |
| 1.250 | 12 | UNF | 1.1600 | 83.1 | 1.1698 | 74.1 | 15/32 | 1.1562 | 87 | ------ |  |  |
| 1.250 | 16 | UN | 1.1820 | 83.8 | 1.1908 | 72.9 | 13,16 | 1.1875 | 77 |  |  |  |
| 1.250 | 18 | UNEF | 1.1900 | 83.1 | 1.1980 | 72.1 | 13,16 | 1.1875 | 87 |  |  |  |
| 1.250 | 20 | UN | 1.1960 | 83.1 | 1.2037 | 71.3 | $1{ }^{13} / 4$ | 1.2031 | 72 |  |  |  |
| 1.250 | 28 | UN | 1.2110 | 84.1 | 1.2176 | 69.8 | 30.75 mm | 1.2106 | 85 | ---- | ---- |  |

See footnotes at end of table.

Table A3.2. Tap drill sizes, Unified screw threads, class 3B-Continued

| Thread size | Threads per inch | Designation | Class 3B minor diameter, internal threads |  |  |  | Tap drills and percent basic thread height |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimum | Percent ${ }^{\text {a }}$ basic thread height | Maximum | Percent a basic thread height | Drill size |  | Percent of thread | Probable oversize, mean | Probable hole size | Percent of thread |
| in |  |  | in |  | in |  | (111/4 ${ }^{\text {in }}$ | $\stackrel{i n}{1.1719}$ |  | in | in |  |
| $1.3125$ | 8 | UN | $1.1770$ | 83.4 | $1.1922$ | 74.1 | $\left\{\begin{array}{l}11 / 64 \\ 1^{3 / 16}\end{array}\right.$ | 1.1719 1.1875 | 87 |  |  |  |
| 1.3125 | 12 | UN | 1.2220 | 83.6 | 1.2323 | 74.1 | 1732 | 1.2188 | 87 |  |  |  |
| 1.3125 | 16 | UN | 1.2450 | 83.1 | 1.2533 | 72.9 | $11 / 4$ | 1.2500 1.2500 | 77 |  |  |  |
| 1.3125 1.3125 | 18 | UNEF | 1.2520 | 83.8 83.9 | 1.2605 1.2662 | 72.1 71.3 | $1{ }^{11 / 4}$ | 1.2500 1.2656 | 87 |  |  |  |
| 1.3125 1.3125 | 20 28 | UN | 1.2580 | 83.9 83.0 | 1.2662 1.2801 | 71.3 69.8 | 32.5 mm | 1.2656 1.2795 | 71 |  |  |  |
| 1.375 | 6 | UNC | 1.1950 | 83.1 | 1.2146 | 74.1 | $\left\{\begin{array}{l}13 / 16 \\ 113 / 4\end{array}\right.$ | 1.1875 1.2031 | 87 |  |  |  |
| 1.375 |  | UN | 1.2400 | 83.1 | 1.2547 | 74.1 | 11564 | 1.2344 | 87 |  |  |  |
| 1.375 | 8 | UN | 1.2400 | 83.1 | 1.2547 | 74.1 | $11 / 4$ | 1.2500 | 77 |  |  |  |
| 1.375 | 12 | UNF | 1.2850 1.3070 | 83.1 | 1.2948 | 74.1 | 19/32 | 1.2812 | 87 |  |  |  |
| 1.375 | 16 | UNEF | 1.3070 1.3150 | 83.8 83.1 | 1.3158 1.3230 | 72.9 | ${ }^{15 / 16}$ | 1.3125 1.3125 | 77 87 |  |  |  |
| 1.375 1.375 | 18 20 | UNEF | 1.3150 1.3210 | 83.1 83.1 | 1.3230 1.3287 | 72.1 71.3 | $15 / 16$ $1^{21 / 64}$ | 1.3125 1.3281 | 87 |  |  |  |
| 1.375 | 28 | UN | 1.3360 | 84.1 | 1.3426 | 69.8 | 34 mm | 1.3386 | 78 |  |  |  |
| 1.4375 | 6 | UN | 1.2570 | 83.4 | 1.2771 | 74.1 | 11764 | 1.2656 | 79 |  |  |  |
| 1.4375 | 8 | UN | 1.3020 | 83.4 | 1.3172 | 74.1 | $\left\{\begin{array}{l}119 / 4 \\ 1^{5} / 16\end{array}\right.$ | 1.2969 1.3125 | 87 | ------ |  |  |
| 1.4375 | 12 | UN | 1.3470 | 83.6 | 1.3573 | 74.1 | $111 / 82$ | 1.3438 | 87 |  |  |  |
| 1.4375 | 16 | UN | 1.3700 | 83.1 | 1.3783 | 72.9 | $13 / 8$ | 1.3750 | 77 |  |  |  |
| 1.4375 | 18 | UNEF | 1.3770 | 83.8 | 1.3855 | 72.1 | $13 / 8$ | 1.3750 | 87 |  |  |  |
| 1.4375 | 20 | UN | 1.3830 | 83.9 | 1.3912 | 71.3 | $1{ }^{125} 64$ | 1.3906 | 72 |  |  |  |
| 1.4375 | 28 | UN | 1.3990 | 83.0 | 1.4051 | 69.8 | 35.5 mm | 1.3976 | 86 | ------ |  |  |
| 1.500 | 6 | UNC | 1.3200 | 83.1 | 1.3396 | 74.1 | $\left\{\begin{array}{l}15 / 16 \\ 1{ }^{21 / 64} \\ 123\end{array}\right.$ | 1.3125 1.3281 | 87 79 89 |  |  |  |
| 1.500 | 8 | UN | 1.3650 | 83.1 | 1.3797 | 74.1 | $\left\{\begin{array}{l}123 / 44 \\ 13 / 8\end{array}\right.$ | 1.3594 1.3750 | 87 | -- |  |  |
| 1.500 | 12 | UNF | 1.4100 | 83.1 | 1.4198 | 74.1 | $1^{13} 18$ | 1.4062 | 87 |  |  |  |
| 1.500 | 16 | UN | 1.4320 | 83.8 | 1.4408 | 72.9 | 17/6 | 1.4375 | 77 |  |  |  |
| 1.500 | 18 | UNEF | 1.4400 | 83.1 | 1.4480 | 72.1 | 17 \% 16 | 1.4375 | 87 | ------- |  |  |
| 1.500 | 20 | UN | 1.4460 | 83.1 | 1.4537 | 71.3 | $1{ }^{29} 96$ | 1.4531 | 72 |  |  |  |
| 1.500 | 28 | UN | 1.4610 | 84.1 | 1.4676 | 69.8 | 37 mm | 1.4567 | 93 |  |  |  |
| 1.5625 | 6 | UN | 1.3820 | 83.4 | 1.4021 | 74.1 | 12564 | 1.3906 | 79 |  |  |  |
| 1.5625 | 8 | UN | 1.4270 | 83.4 | 1.4422 | 74.1 | $\left\{\begin{array}{l}12764 \\ 176\end{array}\right.$ | 1.4219 1.4375 | 87 |  |  |  |
| 1.5625 | 12 | UN | 1.4720 | 83.6 | 1.4823 | 74.1 | $1{ }^{15 / 82}$ | 1.4688 | 87 | -------- |  |  |
| 1.5625 | 16 | UN | 1.4950 | 83.1 | 1.5033 | 72.9 | $11 / 2$ | 1.5000 | 77 |  |  |  |
| 1.5625 | 18 | UNEF | 1.5020 | 83.8 | 1.5105 | 72.1 | $11 / 2$ | 1.5000 | 87 |  |  |  |
| 1.5625 | 20 | UN | 1.5080 | 83.9 | 1.5162 | 71.3 | 133 64 | 1.5156 | 72 | -------- |  |  |
| 1.625 | 6 | UN | 1.4450 | 83.1 | 1.4646 | 74.1 | 12964 | 1.4531 | 79 |  |  |  |
| 1.625 | 8 | UN | 1.4900 | 83.1 | 1.5047 | 74.1 | $\left\{\begin{array}{l}131 / 4 \\ 11 / 2\end{array}\right.$ | 1.4844 | 87 |  |  |  |
| 1.625 | 12 | UN | 1.5350 | 83.1 | 1.5448 | 74.1 | 117/32 | 1.5312 | 87 |  |  |  |
| 1.625 | 16 | UN | 1.5570 | 83.8 | 1.5658 | 72.9 | 1916 | 1.5625 | 77 | ------ |  |  |
| 1.625 | 18 | UNEF | 1.5650 | 83.1 | 1.5730 | 72.1 | 19.16 | 1.5625 | 87 | ------- |  |  |
| 1.625 | 20 | UN | 1.5710 | 83.1 | 1.5787 | 71.3 | $1{ }^{37} / 64$ | 1.5781 | 72 | ---- |  |  |
| 1.6875 | 6 | UN | 1.5070 | 83.4 | 1.5271 | 74.1 | $\left\{\begin{array}{l}11 / 2 \\ 133 / 64\end{array}\right.$ | 1.5000 1.5156 | 87 |  |  |  |
| 1.6875 | 8 | UN | 1.5520 | 83.4 | 1.5672 | 74.1 | $19 / 16$ | 1.5625 | 77 | ------- |  |  |
| 1.6875 | 12 | UN | 1.5970 | 83.6 | 1.6073 | 74.1 | 19962 | 1.5938 | 87 | ------- |  |  |
| 1.6875 | 16 | UN | 1.6200 | 83.1 | 1.6283 | 72.9 | 15/8 | 1.6250 | 77 | -------- |  |  |
| 1.6875 | 18 | UNEF | 1.6270 | 83.8 | 1.6355 | 72.1 | 15/8 | 1.6250 | 87 | ------ |  |  |
| 1.6875 | 20 | UN | 1.6330 | 83.9 | 1.6412 | 71.3 | $1{ }^{11 / 64}$ | 1.6406 | 72 | -------- |  |  |
| 1.750 | 5 | UNC | 1.5340 | 83.1 | 1.5575 | 74.1 | $\left\{\begin{array}{l}137 / 8.8 \\ 135 / 64\end{array}\right.$ | 1.5312 | 84 | ------ |  |  |
| 1.750 | 6 | UN |  | 83.1 | 1.5896 |  | $19 / 16$ | 1.5625 | 87 |  |  |  |
| 1.750 | 6 | UN | 1.5700 | 83.1 | 1.5896 | 74.1 | $137 / 64$ | 1.5781 | 79 | - |  |  |
| 1.750 | 8 | UN | 1.6150 | 83.1 | 1.6297 | 74.1 | $\left\{\begin{array}{l}13964 \\ 158\end{array}\right.$ | 1.6094 1.6250 | 87 |  |  |  |
| 1.750 | 12 | UN | 1.6600 | 83.1 | 1.6698 | 74.1 | $121 / 32$ | 1.6562 | 87 |  |  |  |
| 1.750 | 16 | UN | 1.6820 | 83.8 | 1.6908 | 72.9 | $1{ }^{111}$ /66 | 1.6875 | 77 | ------- |  |  |
| 1.750 | 20 | UN | 1.6960 | 83.1 | 1.7037 | 71.3 | $1{ }^{45} / 64$ | 1.7031 | 72 | -------- |  |  |
| 1.8125 | 6 | UN | 1.6320 | 83.4 | 1.6521 | 74.1 | $\left\{\begin{array}{l}15 / 8 \\ 1{ }^{\text {4/3/4 }}\end{array}\right.$ | 1.6250 1.6406 | 87 | ------ |  |  |
| 1.8125 | 8 | UN | 1.6770 | 83.4 | 1.6922 | 74.1 | $\left\{\begin{array}{l}1.13 / 64 \\ 1113_{4} 4\end{array}\right.$ | 1.6406 1.6719 | 79 87 |  |  |  |
| 1.8125 | 12 | UN | 1.7220 | 83.6 | 1.7323 | 74.1 | ${ }^{1} 111 / 16$ | 1.6875 1.7188 | 87 |  |  |  |
| 1.8125 | 16 | UN | 1.7450 | 83.1 | 1.7533 | 72.9 | $13 / 4$ | 1.7500 | 77 |  |  |  |
| 1.8125 | 20 | UN | 1.7580 | 83.9 | 1.7662 | 71.3 | $1{ }^{19} 6.6$ | 1.7656 | 72 | -------- |  |  |
| 1.875 | 6 | UN | 1.6950 | 83.1 | 1.7146 | 74.1 | 15564 | 1.7031 | 79 |  |  |  |
| 1.875 | 8 | UN | 1.7400 | 83.1 | 1.7547 | 74.1 | $13 / 4$ | 1.7500 | 77 | -------- |  |  |
| 1.875 | 12 | UN | 1.7850 | 83.1 | 1.7948 | 74.1 | 125/32 | 1.7812 | 87 | ------- |  |  |
| 1.875 | 16 | UN | 1.8070 | 83.8 | 1.8158 | 72.9 | $1{ }^{13} 16$ | 1.8125 | 77 |  |  |  |
| 1.875 | 20 | UN | 1.8210 | 83.1 | 1.8287 | 71.3 | 15364 | 1.8281 | 72 |  |  |  |
| 1.9375 | 6 | UN | 1.7570 | 83.4 | 1.7771 | 74.1 | $1^{19} 64$ | 1.7656 | 79 |  |  |  |
| 1.9375 | 8 | UN | 1.8020 | 83.4 | 1.8172 | 74.1 |  | 1.7969 1.8125 | 87 77 |  |  |  |
| 1.9375 | 12 | UN | 1.8470 | 83.6 | 1.8573 | 74.1 | $127 \% 3$ | 1.8438 | 87 |  |  |  |
| 1.9375 | 16 | UN | 1.8700 | 83.1 | 1.8783 | 72.9 | $17 / 8$ | 1.8750 | 77 |  |  |  |
| 1.9375 | 20 | UN | 1.8830 | 83.9 | 1.8912 | 71.3 | $1{ }^{57} 64$ | 1.8906 | 72 |  | ----- |  |

See footnotes at end of table.

Table A3.2. Tap drill sizes, Unified screw threads, class 3B-Continued

| Thread size | Threads per inch | Designation | Class 3B minor diameter, internal threads |  |  |  | Tap drills and percent basic thread height |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Minimum | Percent a basic thread height | Maximum | Percent a basic thread height | Drill size |  | Percent of thread | Probable oversize, mean | Probable hole size | Percent of thread |
| in |  |  | in ${ }^{\text {n }}$ |  | ${ }^{\text {in }}$ |  | 125. in | ${ }_{\text {in }}^{\text {in }}$ |  | in | in |  |
| 2.000 | 4.5 | UNC | 1.7590 | 83.5 | 1.7861 | 74.1 | $1{ }^{25} 53 / 3$ | 1.7812 | 76 |  |  |  |
| 2.000 | 6 | UN | 1.8200 | 83.1 | 1.8396 | 74.1 | $153 / 4$ | 1.8281 | 79 |  |  |  |
| 2.000 | 8 | UN | 1.8650 | 83.1 | 1.8797 | 74.1 | $17 / 8$ | 1.8750 | 77 |  |  |  |
| 2.000 | 12 | UN | 1.9100 | 83.1 | 1.9198 | 74.1 | $1^{129} / 5$ | 1.9062 | 87 |  |  |  |
| 2.000 | 16 20 | UN | 1.9320 1.9460 | 83.8 | 1.9408 | 72.9 | ${ }^{15156}$ | 1.9375 | 77 |  |  |  |
| 2.000 2.0625 | 20 16 | UNS | 1.9460 1.9950 | 83.1 | 1.9537 2.0033 | 71.3 | $2^{161 / 64}$ | 1.9531 2.0000 | 72 |  |  |  |
| 2.125 | 6 | UN | 1.9450 | 83.1 | 1.9646 | 74.1 | $161 / 64$ | 1.9531 | 79 |  |  |  |
| 2.125 | 8 | UN | 1.9900 | 83.1 | 2.0047 | 74.1 | 2 | 2.0000 | 77 |  |  |  |
| 2.125 | 12 | UN | 2.0350 | 83.1 | 2.0448 | 74.1 | $2^{1 / 32}$ | 2.0312 | 87 |  |  |  |
| ${ }_{2}^{2.125}$ | 16 20 | UN | 2.0570 2.0710 | 83.8 83.1 | 2.0658 2.0787 | 72.9 71.3 | 21 | 2.0625 2.0625 | 77 96 |  |  |  |
| 2.125 | 20 | UN | 2.0710 | 83.1 | 2.0787 |  |  |  | 96 |  |  |  |
| 2.1875 | 16 | UNS | 2.1200 | 83.1 | 2.1283 | 72.9 | 21/8 | 2.1250 | 77 |  |  |  |
| 2.250 | 4.5 | UNC | 2.0090 | 83.5 | 2.0361 | 74.1 | $\left\{\begin{array}{l}2 \\ 2^{1} \times 2\end{array}\right.$ | 2.0000 2.0312 | 87 |  |  |  |
| 2.250 | 6 | UN | 2.0700 | 83.1 | 2.0896 | 74.1 | ${ }_{2}{ }^{1 / 16}$ | 2.0625 | 87 |  |  |  |
| 2.250 | 8 | UN | 2.1150 | 83.1 | 2.1297 | 74.1 | $21 / 8$ | 2.1250 | 77 |  |  |  |
| 2.250 | 12 | UN | 2.1600 | 83.1 | 2.1698 | 74.1 | 25/32 | 2.1562 | 87 |  |  |  |
| 2.250 | 16 | UN | 2.1820 | 83.8 | 2.1908 | 72.9 | 23 /6 | 2.1875 | 77 |  |  |  |
| 2.250 | 20 | UN | 2.1960 | 83.1 | 2.2037 | 71.3 | 23/16 | 2.1875 | 96 |  |  |  |
| 2.3125 | 16 | UNS | 2.2450 | 83.1 | 2.2533 | 72.9 | 21/4 | 2.2500 | 77 |  |  |  |
| 2.375 | 8 | UN | 2.1950 | 83.1 | 2.2146 | 74.1 | $2^{3}$, 16 | 2.1875 | 87 |  |  |  |
| 2.375 2.375 | 8 12 | UN | 2.2400 | 83.1 | 2.2547 2.2948 | 74.1 | 21/4 | 2.2500 | 77 |  |  |  |
| 2.375 2.375 | 12 | UN | 2.2850 2.3070 | 83.1 83.8 | 2.2948 2.3158 | 74.1 | ${ }_{25}^{58 / 16}$ | 2.2835 2.3125 | 85 |  |  |  |
| 2.375 | 20 | UN | 2.3210 | 83.1 | 2.3287 | 71.3 | $2^{5 / 16}$ | 2.3125 | 96 |  |  |  |
| 2.4375 | 16 | UNS | 2.3700 | 83.1 | 2.3783 | 72.9 | 23/8 | 2.3750 | 77 |  |  |  |
| 2.500 | 4 | UNC | 2.2290 | 83.4 | 2.2594 | 74.1 | $\left\{\begin{array}{l}2^{7} / 8 \\ 21 / 2\end{array}\right.$ | 2.2188 2.2500 | 87 |  |  |  |
| 2.500 | 6 | UN | 2.3200 | 83.1 | 2.3396 | 74.1 | $2{ }^{5} 16$ | 2.3125 | 87 |  |  |  |
| 2.500 | 8 | UN | 2.3650 | 83.1 | 2.3797 | 74.1 | 23/8 | 2.3750 | 77 |  |  |  |
| 2.500 | 12 | UN | 2.4100 | 83.1 | 2.4198 | 74.1 | $2{ }^{13} / 38$ | 2.4062 | 87 |  |  |  |
| 2.500 | 16 | UN | 2.4320 | 83.8 | 2.4408 | 72.9 | $2^{7} 16$ | 2.4375 | 77 |  |  |  |
| 2.500 | 20 | UN | 2.4460 | 83.1 | 2.4537 | 71.3 | 27/16 | 2.4375 | 96 | --------- |  |  |
| 2.625 | 4 | UN | 2.3540 | 83.4 | 2.3844 | 74.1 | $\left\{\begin{array}{l}211 / 32 \\ 23 / 8\end{array}\right.$ | 2.3438 2.3750 | 87 | -- |  |  |
| 2.625 | 6 | UN | 2.4450 | 83.1 | 2.4646 | 74.1 | 27 | 2.4375 | 87 |  |  |  |
| 2.625 | 8 | UN | 2.4900 | 83.1 | 2.5047 | 74.1 | $21 / 2$ | 2.5000 | 77 |  |  |  |
| 2.625 | 12 | UN | 2.5350 | 83.1 | 2.5448 | 74.1 | $2^{17 / 52}$ | 2.5312 | 87 |  |  |  |
| 2.625 | 16 | UN | 2.5570 | 83.8 | 2.5658 | 72.9 | 29 961 | 2.5625 | 77 |  |  |  |
| 2.625 | 20 | UN | 2.5710 | 83.1 | 2.5787 | 71.3 | 23,16 | 2.5625 | 96 | ----- |  |  |
| 2.750 | 4 | UNC | 2.4790 | 83.4 | 2.5094 | 74.1 | 21/2 | 2.5000 | 77 |  |  |  |
| 2.750 | 6 | UN | 2.5700 | 83.1 | 2.5896 | 74.1 | 29 16 | 2.5625 | 87 |  |  |  |
| 2.750 | 8 | UN | 2.6150 | 83.1 | 2.6297 | 74.1 | $25 / 8$ | 2.6250 | 77 |  |  |  |
| 2.750 | 12 | UN | 2.6600 | 83.1 | 2.6698 | 74.1 | $2^{21 / 32}$ | 2.6562 | 87 |  |  |  |
| 2.750 | 16 | UN | 2.6820 | 83.8 | 2.6908 | 72.9 | $211 / 16$ $211 / 6$ | 2.6875 | 77 |  |  |  |
| 2.750 | 20 | UN | 2.6960 | 83.1 | 2.7037 | 71.3 | 211/16 | 2.6875 | 96 |  |  |  |
| 2.875 2.875 | 4 6 |  | 2.6040 2.6950 | 83.4 | 2.6344 |  |  | 2.6250 2.6875 | 77 87 |  |  |  |
| 2.875 2.875 | 6 | UN | 2.6950 2.7400 | 83.1 83.1 | 2.7146 2.7547 | 74.1 74.1 | $23 / 4$ | 2.6875 2.7500 | 87 |  |  |  |
| 2.875 | 12 | UN | 2.7850 | 83.1 | 2.7948 | 74.1 | $2{ }^{25} / 32$ | 2.7812 | 87 |  |  |  |
| 2.875 | 16 | UN | 2.8070 | 83.8 | 2.8158 | 72.9 | 213,16 | 2.8125 | 77 |  |  |  |
| 2.875 | 20 | UN | 2.8210 | 83.1 | 2.8287 | 71.3 | $2{ }^{13} / 16$ | 2.8125 | 96 |  |  |  |
| 3.000 | 4 | UNC | 2.7290 | 83.4 | 2.7594 | 74.1 | $23 / 4$ | 2.7500 | 77 |  |  |  |
| 3.000 | 6 | UN | 2.8200 | 83.1 | 2.8396 | 74.1 | $2{ }^{13} / 16$ | 2.8125 | 87 |  |  |  |
| 3.000 | 8 | UN | 2.8650 | 83.1 | 2.8797 | 74.1 | $27 / 8$ | 2.8750 | 77 |  |  |  |
| 3.000 | 12 | UN | 2.9100 | 83.1 | 2.9198 | 74.1 | 74 mm | 2.9134 | 80 |  |  |  |
| 3.000 3.000 | 16 20 | UN | 2.9320 2.9460 | 83.8 83.1 | 2.9408 2.9537 | 72.9 71.3 | $215 / 16$ $2{ }^{15 / 16}$ | 2.9375 2.9375 | 77 96 |  |  |  |
| 3.000 | 20 | UN | 2.9460 | 83.1 | 2.9537 | 71.3 | 2.16 | 2.9375 | 96 |  |  |  |
| 3.250 | 4 | UNC | 2.9790 | 83.4 | 3.0094 | 74.1 | 3 | 3.0000 | 77 |  |  |  |
| 3.500 | 4 | UNC | 3.2290 | 83.4 | 3.2594 | 74.1 | $31 / 4$ | 3.2500 | 77 |  |  |  |
| 3.750 | 4 | UNC | 3.4790 | 83.4 | 3.5094 | 74.1 | $31 / 2$ | 3.5000 | 77 |  |  |  |

${ }^{\text {a }} 100 \%$ basic thread height $=0.75 \mathrm{H}$ (values of 0.75 H are shown in col. 14 , table 2.1).



Figure A3.4. Distribution of hole size limits before tapping, Unified Miniature threads.

Figure A3.3. Distribution of hole size limits before tapping, Unified threads.
Table A3.5. Recommended hole size limits before threading for different lengths of engagement, standard Unified and some UNS threads,

| Nominal size in inches and threads per inch | $\begin{gathered} \text { Series } \\ \text { designation } \end{gathered}$ | Minor diameter of internal threads |  |  |  | Recommended hole size limits for different lengths of engagement |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min | Percent basic thread | Max ${ }^{\text {c }}$ | $\begin{aligned} & \text { Percent } \\ & \text { basic } \\ & \text { thread } \\ & \text { height b } \end{aligned}$ | To and including 0.33D |  | Above 0.33D thru 0.67 D |  | Above 0.67 D thru 1.5D |  | Above 1.5D thru 3D |  |
|  |  |  |  |  |  | Min | Max | Min | Max | Mın | Max | Min | Max |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 |
| .060-80 or No. 0-80 | UNF | $\begin{aligned} & \text { in } \\ & 0.0465 \end{aligned}$ | 83.1 | $\begin{aligned} & \text { in } \\ & 0.0514 \end{aligned}$ | 53.0 | $i_{0.0465}^{i n}$ | $\begin{aligned} & i n \\ & 0.0500 \end{aligned}$ | $\begin{aligned} & i n \\ & 0.0479 \end{aligned}$ | $\begin{aligned} & i n \\ & 0.0514 \end{aligned}$ | $\begin{aligned} & { }_{0.0479}^{i n} \\ & 0.0 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & 0.0514 \end{aligned}$ | ${ }_{\text {in }}^{\text {in }}$ | ${ }_{0}^{\text {in }} 0.0514$ |
| $\begin{aligned} & .073-54 \text { or No. 1:64 } \\ & .073-72 \text { or No. } 1-72 \end{aligned}$ | UNC | $\begin{aligned} & .0561 \\ & .0580 \end{aligned}$ | $\begin{aligned} & 83.3 \\ & 83.1 \end{aligned}$ | $\begin{aligned} & .0623 \\ & .0635 \end{aligned}$ | $\begin{aligned} & 52.7 \\ & 52.7 \end{aligned}$ | $\begin{array}{r} .0561 \\ .0580 \end{array}$ | $\begin{aligned} & .0599 \\ & .0613 \end{aligned}$ | $\begin{aligned} & .0580 \\ & .0596 \end{aligned}$ | $\begin{aligned} & .0618 \\ & .0629 \end{aligned}$ | $\begin{aligned} & .0585 \\ & .0602 \end{aligned}$ | $\begin{aligned} & .0623 \\ & .0635 \end{aligned}$ | $\begin{aligned} & .0585 \\ & .0602 \end{aligned}$ | $\begin{aligned} & .0623 \\ & .0635 \end{aligned}$ |
| .086-56 or No. 2-56 .086-64 or No. 2-64 | UNF | $\begin{aligned} & .0667 \\ & .0691 \end{aligned}$ | $\begin{aligned} & 83.2 \\ & 83.3 \end{aligned}$ | $\begin{aligned} & .0737 \\ & .0753 \end{aligned}$ | $\begin{aligned} & 53.0 \\ & 52.7 \end{aligned}$ | $\begin{aligned} & .0667 \\ & .0691 \end{aligned}$ | $\begin{aligned} & .0705 \\ & .0724 \end{aligned}$ | . 06786 | $\begin{aligned} & .0724 \\ & .0740 \end{aligned}$ | .0699 | . 07375 | . 06799 | . 0737 |
| $\begin{aligned} & .099-48 \text { or No. 3-48 } \\ & .099-56 \text { or No. 3-56 } \end{aligned}$ | $\begin{aligned} & \text { UNC } \\ & \text { UNF } \end{aligned}$ | $\begin{aligned} & .0764 \\ & .0797 \end{aligned}$ | $\begin{aligned} & 83.5 \\ & 83.2 \end{aligned}$ | $\begin{aligned} & .0845 \\ & .0865 \end{aligned}$ | $\begin{aligned} & 53.6 \\ & 53.9 \end{aligned}$ | . 07679 | $\begin{aligned} & .0804 \\ & .0831 \end{aligned}$ | .0785 | $\begin{aligned} & .0825 \\ & .0848 \end{aligned}$ | . 08805 | .0845 .0865 | . 080638 | . 08846 |
| $\begin{aligned} & .112-40 \text { or No. } 4-40 \\ & .112-48 \text { or No. 4-48 } \end{aligned}$ | UNC | $\begin{aligned} & .0849 \\ & .0894 \end{aligned}$ | 883.4 | $\begin{aligned} & .0939 \\ & .0968 \end{aligned}$ | $\begin{aligned} & 55.7 \\ & 56.2 \end{aligned}$ | . 0849 | $\begin{aligned} & .0894 \\ & .0931 \end{aligned}$ | . 08712 | $\begin{gathered} .0916 \\ .0949 \end{gathered}$ | . 08934 | $\begin{aligned} & .0939 \\ & .0968 \end{aligned}$ | .0902 .0939 | . 09977 |
| $\begin{aligned} & .125-40 \text { or No. } 5-40 \\ & .125-44 \text { or No. } 5-44 \end{aligned}$ | UNC | .0979 .1004 | $\begin{aligned} & 83.4 \\ & 83.3 \end{aligned}$ | .1062 .1079 | 57.9 57.9 | .0979 .1004 | $\begin{aligned} & .1020 \\ & .1041 \end{aligned}$ | . 10000 | . 1041 | . 1021 | .1062 .1079 | .1036 .1057 | . 107097 |
| $\begin{array}{r} .138-32 \text { or No. 6-32 } \\ .138-40 \text { or No. 6-40 } \end{array}$ | $\begin{aligned} & \text { UNC } \\ & \text { UNF } \end{aligned}$ | $\begin{aligned} & 104 \\ & .111 \end{aligned}$ | $\begin{aligned} & 83.8 \\ & 83.1 \end{aligned}$ | $\begin{array}{r} .114 \\ .119 \end{array}$ | 59.1 58.5 | . 1111 | $\begin{aligned} & .109 \\ & .115 \end{aligned}$ | . 1113 | . 1112 | . 109 | . 1114 | . 1111 | . 1121 |
| $\begin{aligned} & .164-32 \text { or No. 8-32 } \\ & .164-36 \text { or No. } 8-36 \end{aligned}$ | UNC | . 134 | 83.8 83.1 | . 139 | 61.6 61.0 | . 130 | . 138 | . 132 | .137 .140 | . 138 | . 139 | . 1370 | . 1441 |
| $\begin{aligned} & .190-24 \text { or No. 10-24 } \\ & .190-32 \text { or No. } 10-32 \end{aligned}$ | UNC | . 145 | 83.1 83.8 | . 156 | 62.8 64.0 | .145 | .150 .160 | . 1478 | . 153 | .150 .160 | .156 .164 | . 153 | . 158 |
| $\begin{aligned} & .216-24 \text { or No. } 12-24 \\ & .216-28 \text { or No. } 12-28 \\ & .216-32 \text { or No. } 12-32 \end{aligned}$ | UNC UNF UNEF | .171 .177 .182 | 83.1 84.1 83.8 | .181 .186 .190 | 64.7 64.7 64.0 | .171 .177 .182 | .176 .182 .186 | .173 .179 .184 | .178 .184 .188 | .176 .181 .186 | .181 .186 .190 | .178 .183 .188 | .183 .188 .192 |
| $\begin{aligned} & .250-20 \text { or } 1 / 4-20 \\ & .250-28 \text { or } 1 / 4-28 \\ & .250-32 \text { or } 1 / 4-32 \\ & .250-36 \text { or } 1 / 4-36 \end{aligned}$ | UNC UNF UNEF UNS | .196 .211 .216 .220 | 83.1 84.1 83.8 83.1 8.1 | .207 .220 .224 .226 | 66.2 64.7 64.0 66.5 | .196 .211 .216 .220 | .202 .216 .220 .223 | .199 .213 .218 .221 | .204 .218 .222 .225 | .202 .216 .220 .222 | .207 .200 .224 .226 | .204 .218 .221 .224 | .210 .222 .225 .228 |
| 3125-18 or 5/16-18 <br> 3125-20 or 5/16-20 <br> .3125-24 or 5/16-24 <br> $.3125-28$ or $5 / 16-28$ <br> . $3125-36$ or $5 / 16-36$ | UNC 20UN UNF 28UN UNEF UNS | .252 .258 .267 .274 .279 .282 | 83.8 83.9 84.1 83.0 82.5 84.5 | .265 .270 .278 .282 .286 .889 | 65.8 65.4 65.4 65.6 65.7 6.5 .3 65.1 | .252 .258 .267 .274 .279 .282 | .259 .264 .2672 .288 .288 .286 | .256 .261 .260 .276 .280 .883 | .262 .267 .265 .280 .284 .287 | .259 .264 .267 .278 .882 .885 | .265 .270 .277 .282 .286 .889 | .262 .267 .275 .280 .284 .887 | .268 .273 .280 .284 .288 .291 |
| $\begin{aligned} & .375-16 \text { or } 3 / 8-16 \\ & .375-20 \text { or } 3 / 8-20 \\ & .375-24 \text { or } 3 / 8-24 \\ & .375-28 \text { or } 3 / 8-28 \\ & .375-32 \text { or } 3 / 8-32 \\ & .375-36 \text { or } 3 / 8-36 \end{aligned}$ | UNC 20UN UNF 2NUN UNEF UNS | .307 .321 .330 .336 .341 .345 | 83.8 83.1 83.1 84.1 83.8 83.1 8.1 | .321 .332 .340 .345 .349 .352 | 66.5 66.2 64.7 64.7 64.0 63.7 | .307 .321 .330 .366 .341 .345 | .314 .327 .335 .340 .345 .448 | .311 .324 .332 .338 .343 .446 | .318 .330 .337 .333 .347 .350 | .314 .327 .335 .300 .345 .348 | .321 .332 .340 .345 .349 .352 | .318 .330 .337 .334 .346 .349 | .325 .335 .342 .347 .350 .353 |
| 4375-14 or 7/16-14 <br> .4375-16 or 7/16-16 <br> $.4375-20$ or $7 / 16-20$ <br> $.4375-28$ or $7 / 16-28$ $.4375-32$ or $7 / 16-32$ $\cdot 43 / 0-52 \text { or } / / 10-32$ | UNC 16 UN UNF UNEF 32UN | .360 .370 .383 .399 .404 | 83.5 83.1 83.9 83.0 82.5 | .376 .384 .395 .407 .411 | 66.3 65.9 65.9 65.4 65.7 65.3 | .360 .370 .383 .399 .404 | .368 .377 .389 .483 .407 | .364 .373 .386 .481 .405 | .372 .380 .392 .405 .409 | .368 .377 .389 .403 .407 | .376 .384 .395 .407 .411 | .372 .380 .392 .405 .409 | .380 .387 .398 .409 .413 |
| $\begin{array}{r} .500-12 \text { or } 1 / 2-12 \\ .500-13 \text { or } 1 / 2 / 13 \\ .500-16 \text { or } 1 / 2-16 \\ .500-20 \text { or } 1 / 2-20 \\ .500-28 \text { or } 1 / 2-28 \\ .500-32 \text { or } 1 / 2-32 \end{array}$ | UNS UNC UNN UNF UNEF 32UN | .410 .417 .432 .466 .461 .466 | 83.1 <br> 83.1 <br> 83.1 <br> 83.8 <br> 83.1 <br> 84.1 <br> 83.8 | .428 .434 .446 .457 .470 .474 | $\begin{aligned} & 66.5 \\ & 66.0 \\ & 66.5 \\ & 66.2 \\ & 64.7 \\ & 64.0 \\ & \hline \end{aligned}$ | .410 .417 .432 .466 .466 .466 | $\begin{array}{r} .419 \\ .425 \\ .439 \\ .462 \\ .466 \\ \hline \end{array}$ | $\begin{aligned} & .414 \\ & .421 \\ & .436 \\ & .449 \\ & .463 \\ & .468 \\ & \hline \end{aligned}$ | $\begin{array}{r} .423 \\ .430 \\ .443 \\ .454 \\ .468 \\ .472 \end{array}$ | $\begin{aligned} & .419 \\ & .425 \\ & .439 \\ & .452 \\ & .466 \\ & .470 \end{aligned}$ | $\begin{aligned} & .428 \\ & .434 \\ & .456 \\ & .470 \\ & .474 \\ & .474 \end{aligned}$ | .423 .430 .438 .454 .468 .471 | .432 .438 .450 .460 .472 .475 |


| Nominal size in inches and threads per inch | Series designation | Minor diameter of internal threads |  |  |  | Recommended hole size limits for different lengths of engagement |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min | Percent basic thread height ${ }^{b}$ | Max ${ }^{\text {c }}$ | Percent basic thread height b | To and including 0.33 D |  | Above 0.33 D thru 0.67 D |  | Above 0.67 D thru 1.5 D |  | Above 1.5D thru 3 D |  |
|  |  |  |  |  |  | Min | Max | Min | Max | Min | Max | Min | Max |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 |
|  |  | in |  | in |  | in | in | in | ${ }^{\text {in }}$ | in ${ }^{\text {a }}$ | in $^{490}$ | in | in 495 |
| . $5625-12$ or $9 / 16-12$ | UNC | .472 .495 | 83.6 | . 490 | 67.0 65.9 | .472 .495 | . 481 | .477 .498 | . 486 | . 4802 | .490 .509 | .486 .505 | .495 .512 |
| . $5625-16$ or $9 / 16-16$ | UNF | .495 .502 | 83.1 83.8 | . 509 | 65.9 65.8 | . 495 | . 509 | . 598 | . 512 | . 509 | . 515 | . 512 | . 518 |
| . $5625-20$ or $9 / 16-20$ | 20UN | . 508 | 83.9 | . 520 | 65.4 | . 508 | . 514 | . 511 | . 517 | . 514 | . 520 | . 517 | . 523 |
| . $5625-24$ or 9/16-24 | UNEF | . 517 | 84.1 | . 527 | 65.6 | . 517 | . 522 | . 520 | . 525 | . 522 | . 527 | . 525 | . 530 |
| . $5625-28$ or 9/16-28 | 28 UN | . 524 | 83.0 | . 532 | 65.7 | . 524 | . 528 | . 526 | . 5330 | . 532 | . 5332 | . 5330 | . 5334 |
| . $5625-32$ or 9/16-32 | 32 UN | . 529 | 82.5 | . 536 | 65.3 | . 529 | . 532 | . 530 | . 534 | . 532 | . 536 | . 534 | . 538 |
| . $625-11$ or 5/8-11 | UNC | . 527 | 83.0 | . 546 | 66.9 | . 527 | . 536 | . 532 | . 541 | . 536 | . 546 | . 541 | . 551 |
| .625-12 or 5/8-12 | 12UN | . 535 | 83.1 | . 553 | 66.5 | . 535 | . 544 | . 539 | . 548 | . 544 | . 573 | . 548 | . 557 |
| . $625-16$ or 5/8-16 | 16UN | . 557 | 83.8 | . 571 | 66.5 | . 557 | . 564 | . 561 | . 568 | . 564 | . 571 | . 568 | . 575 |
| .625-18 or 5/8-18 | UNF | . 565 | 83.1 | . 578 | 65.1 | . 571 | . 571 | . 568 | .574 .580 | . 571 | . 578 | . 5880 | . 5885 |
| .625-20 or 5/8-20 | UNEN | . 571 | 833.1 | .582 .590 | 66.2 64.7 | . 571 | . 585 | . 582 | . 587 | . 585 | . 590 | . 587 | . 592 |
| . $625-28$ or 5/8-28 | 28 UN | . 586 | 84.1 | . 595 | 64.7 | . 586 | . 590 | . 588 | . 593 | . 590 | . 595 | . 593 | . 597 |
| .625-32 or 5/8-32 | 32 UN | . 591 | 83.8 | . 599 | 64.0 | . 591 | . 595 | . 593 | . 597 | . 595 | . 599 | . 596 | . 600 |
| .6875-12 or 11/16-12 | 12UN | . 597 | 83.6 | . 615 | 67.0 | . 597 | . 606 | . 602 | . 611 | . 606 | . 615 | . 611 | . 620 |
| . $6875-16$ or $11 / 16-16$ | 16 UN | . 620 | 83.1 | . 634 | 65.9 | . 620 | . 627 | . 623 | . 630 | . 627 | . 634 | . 633 | . 637 |
| . $6875-18$ or $11 / 16-18$ | UNS | . 637 | 83.8 83.9 | . 6445 | 65.8 65.4 | . 627 | .634 .639 | .630 .636 | .637 .642 | . 634 | . 640 | . 6372 | . 643 |
| . $6875-24$ or 11/16-24 | UNEF | . 642 | 84.1 | . 652 | 65.6 | . 642 | . 647 | . 645 | . 650 | . 647 | . 652 | . 650 | . 654 |
| . $6875-28$ or 11/16-28 | 28 UN | . 649 | 83.0 | . 657 | 65.7 | . 649 | . 653 | . 651 | . 655 | . 653 | . 657 | . 655 | . 659 |
| .6875-32 or 11/16-32 | 32 UN | . 654 | 82.5 | . 661 | 65.3 | . 654 | . 657 | . 655 | . 659 | . 657 | . 661 | . 659 | . 663 |
| . $750-10$ or $3 / 4-10$ | UNC | . 642 | 83.1 | . 663 | 67.0 | . 642 | . 652 | . 647 | . 658 | . 652 | . 663 | . 657 | . 668 |
| . $750-12$ or $3 / 4-12$ | 12UN | . 660 | 83.1 | . 678 | 66.5 | . 660 | . 669 | . 664 | . 673 | . 669 | . 678 | . 673 | . 682 |
| . $750-16$ or $3 / 4-16$ | UNF | . 682 | 83.8 | . 696 | 66.5 | . 682 | . 689 | . 686 | . 693 | . 689 | . 696 | . 693 | . 700 |
| . $750-18$ or 3/4-18 | UNS | . 690 | 83.1 | . 703 | 65.1 | . 690 | . 696 | . 693 | . 699 | . 696 | . 703 | . 699 | . 706 |
| . $750-20$ or 3/4-20 | UNEF | . 696 | 83.1 | . 707 | 66.2 | . 696 | . 702 | . 699 | . 704 | . 7102 | . 727 | . 718 | . 710 |
| . $750-28$ or $3 / 4-28$ | 28UN | . 7116 | 84.1 83.8 | . 720 | 64.7 64.0 | . 7116 | .716 .720 | . 713 | . 722 | .716 .720 | . 724 | . 721 | .725 |
| .8125-12 or 13/16-12 | 12UN | . 722 | 83.6 | . 740 | 67.0 | . 722 | . 731 | . 727 | . 736 | . 731 | . 740 | . 736 | . 745 |
| .8125-16 or 13/16-16 | 16UN | . 745 | 83.1 | . 759 | 65.9 | . 745 | . 752 | . 748 | . 755 | . 752 | . 795 | . 755 | . 762 |
| . $8125-18$ or $13 / 16-18$ | UNS | . 752 | 83.8 | . 765 | 65.8 | . 752 | . 759 | . 756 | . 762 | . 759 | . 765 | . 762 | . 768 |
| . 8125-20 or 13/16-20 | UNEF | . 758 | 83.9 | . 770 | 65.4 | . 758 | . 764 | . 761 | . 767 | . 764 | . 770 | . 767 | . 773 |
| .8125-28 or 13/16-28 | 28 UN | . 774 | 83.0 | . 782 | 65.7 | . 774 | . 778 | . 776 | . 780 | . 778 | . 782 | . 780 | . 784 |
| .8125-32 or 13/16-32 | 32UN | . 779 | 82.5 | . 786 | 65.3 | . 779 | . 782 | . 780 | . 784 | . 782 | . 786 | . 784 | . 788 |
| .875-9 or 7/8-9 | UNC | . 755 | 83.1 | . 778 | 67.2 | . 755 | . 766 | . 760 | . 772 | . 766 | . 778 | . 772 | . 783 |
| . $875-12$ or 7/8-12 | 12UN | . 785 | 83.1 | . 803 | 66.5 | . 785 | . 794 | . 789 | . 798 | . 794 | . 803 | . 798 | . 818 |
| . 875-14 or 7/8-14 | UNF | . 798 | 83.0 | . 814 | 65.7 | . 798 | . 806 | . 802 | . 810 | . 806 | . 814 | . 810 | . 818 |
| . 875-16 or 7/8-16 | 16 UN | . 807 | 83.8 | . 821 | 66.5 | . 807 | . 814 | . 811 | . 818 | . 814 | . 821 | . 818 | . 825 |
| . $8755-18$ or 7/8-18 | UNS | . 815 | 83.1 | . 8282 | 65.1 66.2 | . 815 | . 827 | . 8184 | . 8324 | . 827 | . 832 | . 830 | . 835 |
| . $875-28$ or 7/8-28 | 28UN | . 836 | 84.1 | . 845 | 64.7 | . 836 | . 840 | . 838 | . 843 | . 840 | . 845 | . 843 | . 847 |
| .875-32 or 7/8-32 | 32UN | . 841 | 83.8 | . 849 | 64.0 | . 811 | . 845 | . 843 | . 847 | . 845 | . 849 | . 846 | . 850 |
| .9375-12 or $15 / 16-12$ | 12 UN | . 877 | 83.6 | . 868 | 67.0 | .847 .870 | . 8786 |  |  |  |  |  |  |
| . $9375-16$ or $15 / 16-16$ | UNEF | . 8780 | 83.1 83.9 | .884 .895 | 65.9 65.4 | . 870 | . 877 | . 8738 | . 889 | . 8789 | . 8895 | . 889 | . 888 |
| . $9375-28$ or 15/16-28 | 28 UN | . 899 | 83.0 | . 907 | 65.7 | . 899 | . 903 | . 901 | . 905 | . 903 | . 907 | . 905 | . 909 |
| .9375-32 or 15/16-32 | 32UN | . 904 | 82.5 | . 911 | 65.3 | . 904 | . 907 | . 905 | . 909 | . 907 | . 911 | . 909 | . 913 |

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|  | $\infty$ NWM NO <br> 125102510210 <br> ת9988898 | $\cdots \infty$ No <br>  <br> NんNWNW <br>  | $\infty \stackrel{\sim}{1}-\infty 0_{0}^{\infty}$ <br> $\cdots 1151$ <br> $-\infty-\infty$ <br> $\infty \rightarrow \infty$ |  |  |  202012.2101010 にたににNに <br>  | $\omega_{1} \sim_{1}^{\infty} 0_{0}^{\infty}$ 1015151115 －ハーNーN <br>  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

Table A3.5. Recommended hole size limits before threading for different lengths of engagement, standard Unified and some UNS threads,

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \multirow[t]{3}{*}{Nominal size in inches and threads per inch} \& \multirow[t]{3}{*}{\[
\begin{array}{|c||}
\text { Series } \\
\text { designation }
\end{array}
\]} \& \multicolumn{4}{|l|}{Minor diameter of internal threads} \& \multicolumn{8}{|l|}{Recommended hole size limits for different lengths of engagement} \\
\hline \& \& \multirow[t]{2}{*}{Min} \& \multirow[t]{2}{*}{Percent
basic
thread
height 5} \& \multirow[t]{2}{*}{Max \({ }^{\text {c }}\)} \& \multirow[t]{2}{*}{Percent
basic thread height} \& \multicolumn{2}{|l|}{To and including 0.33D} \& \multicolumn{2}{|l|}{Above 0.33D thru 0.67D} \& \multicolumn{2}{|l|}{Above 0.67D thru 1.5D} \& \multicolumn{2}{|l|}{Above 1.5D thru 3D} \\
\hline \& \& \& \& \& \& Min \& Max \& Min \& Max \& Min \& Max \& Min \& Max \\
\hline 1 \& 2 \& 3 \& 4 \& 5 \& 6 \& 7 \& 8 \& 9 \& 10 \& 11 \& 12 \& 13 \& 14 \\
\hline  \&  \& \begin{tabular}{l} 
in \\
1.445 \\
1.490 \\
1.595 \\
1.557 \\
1.567 \\
1.571 \\
\hline 1.57 \\
\hline 1.07
\end{tabular} \& 83.1
83.1
83.1
83.1
83.8
83.1
83.1 \& in
1.475
1.515
11551
11571
1.578
1.582 \& \[
\begin{gathered}
69.3 \\
67.7 \\
66.7 \\
66.5 \\
65.5 \\
66.2
\end{gathered}
\] \& in
1.445
1.450
1.535
1.557
11.565
1.571 \& in
1.460
1.450
1.544
1.564
1.561
1.571
1.577 \& in
1.452
1.496
1.539
1.561
1.568
1.574

1.574 \& | in |
| :--- |
| 1.468 |
| 1.468 |
| 1.508 |
| 1.548 |
| 1.568 |
| 1.574 |
| 1.580 | \& in

11.460
1.502
1.5024
1.564
1.561
1.577
1.57 \& in
1.475
1.575
1.553
1.553
1.571
1.588
1.582 \& in
1.468
1.568
1.5088
1.5488
1.568
1.580
1.580 \& in
i.
1.483
1.521
1.557
1.575
1.581
1.585 <br>
\hline $1.6875-6$
$1.685-8$
$1.685-12$
$1.6857-16$
1.685718
$1.6875-20$ \& 6UN
8UN
110 N
1UN
UNEF
20UN \& 1.507
1.552
1.597
1.620
1.627
1.633
1.633 \& 83.4
83.4
83.6
83.6
83.1
83.8
83.9 \& 1.538
1.577
1.615
1.634
1.640
1.645

1.645 \& \begin{tabular}{l}
69.1 <br>
69.1 <br>
68.1 <br>
67.0 <br>
65.9 <br>
65.8 <br>
65.4 <br>
\hline 8.4

 \& 

1.507 <br>
11.552 <br>
11.597 <br>
11.620 <br>
1.627 <br>
1.633 <br>
\hline
\end{tabular} \& 1.522

1.565
1.666
1.667
1.634
1.639
1.639 \& 1.515
1.558
11.602
11.623
1.630
1.636 \& 1.530
1.571
1.671
1.630
1.630
1.642
1.642 \& 1.522
1.565
11.606
11.627
1.634

1.639 \& | 1.538 |
| :--- |
| 1.577 |
| 11.675 |
| 11.634 |
| 1.640 |
| 1.645 |
| 1.8 | \& 1.530

1.571
1.671
1.630
1.637
1.642
1.64
1.6 \& 1.545
1.583
1.620
1.637
1.643
1.648
1.648 <br>
\hline $1.750-5$
$1.750-6$
$1.750-8$
$1.750-12$
1.75016
$1.750-20$ \& UNC
6UN
8UN
12 UN
16 UW

20 UN \& | 1.533 |
| :--- |
| 1.570 |
| 1.665 |
| 1.660 |
| 1.682 |
| 1.696 | \& 83.1

83.1
83.1
83.1
83.1
83.8
83.1 \& 1.568
1.660
1.600
1.670
1.698
1.707
1.707 \& 70.1
60.3
69.7
67.7
66.5
66.5
66.2 \& 1.534
1.570
1.675
1.660
1.682
1.696
1.69 \& 1.550
1.585
1.667
1.669
1.669
1.702
1.702 \& 1.542
1.577
1.621
11.664
1.686
1.699

1.69 \& | 1.559 |
| :--- |
| 1.593 |
| 1.693 |
| 1.663 |
| 1.693 |
| 1.693 |
| 1.704 | \& 1.550

1.58 .5
1.627
1.669
1.689
1.702
1.702 \& 1.568
1.600
1.640
1.678
1.696
1.707

1.7 \& | 1.559 |
| :--- |
| 1.592 |
| 1.633 |
| 1.673 |
| 1.693 |
| 1.704 |
| 1.74 |
| 1.64 | \& 1.576

1.608
1.646
1.682
1.780
1.710 <br>

\hline  \&  \& | 1.632 |
| :--- |
| 1.677 |
| 1.722 |
| 1.745 |
| 1.758 |
|  | \& 83.4

83.4
83.6
83.6
83.1
83.9 \& 1.663
1.702
1.740
1.759
1.770 \& 69.1
68.1
67.0
67.9
65.9
65.4 \& 1.632
1.677
1.672
1.725
1.758
1.758 \& 1.647
1.690
1.751
1.752
1.764
1.764 \& 1.640
1.684
1.627
1.748
1.761 \& 1.655
1.696
1.676
1.755
1.767
1.767 \& 1.647
1.690
1.631
1.752
1.764
1.764 \& 1.663
1.702
1.740
1.759
1.770 \& 1.655
1.696
1.736
1.755
1.767
1.767 \& 1.670
1.708
1.745
1.762
1.773 <br>
\hline $1.875-6$
$1.875-8$
$1.875-12$
$1.875-16$
$1.875-20$ \& 6UN
8 UN
120 N
16 N
20UN \& 1.695
1.740
1.785
1.887
1.821

1.8 \& 83.1
83.1
83.1
83.8
83.8
83.1 \& 1.725
1.765
1.803
1.821
1.832

1.82 \& 69.3
67.7
66.7
66.5
66.5
66.2 \& 1.695
1.740
1.785
1.887
1.821
1.82 \& 1.710
1.752
1.784
1.884
1.827

188 \& 1.702
1.746
1.789
1.811
1.824
1.824 \& 1.718
1.758
1.798
1.788
1.830
1.880 \& 1.710
1.752
1.794
1.814
1.814
1.827 \& 1.725
1.765
1.803
1.821
1.832

1.8 \& 1.718
1.758
1.798
1.888
1.830
1.83
1.8 \& 1.733
1.771
1.807
1.825
1.835
1.85 <br>
\hline $1.9375-6$
$11.935-8$
$1.935-12$
$1.935-16$
$1.9375-20$ \& 6UN
8UN
12UN
16 UNW
20UN \& 1.757
1.802
1.887
1.870
1.883

1.88 \& 83.4
83.4
83.4
83.6
83.1
83.9 \& 1.788
1.887
1.865
1.884
1.889
1.895 \& 69.1
68.1
67.0
65.9
65.9

65.4 \& | 1.757 |
| :--- |
| 1.802 |
| 1.847 |
| 1.870 |
| 1.883 |
| 1.88 | \& 1.772

1.85
1.856
1.857
1.887
1.889 \& 1.765
1.808
1.852
1.853
1.886

1.88 \& 1.780
1.81
1.81
1.81
1.880
1.892 \& 1.772
1.815
1.856
1.877
1.889
1.88 \& 1.788
1.887
1.865
1.884
1.895

1.885 \& 1.780
1.821
1.861
1.880
1.892
1.802 \& 1.795
1.833
1.870
1.887
1.898 <br>

\hline  \& $$
\begin{aligned}
& \text { UNC } \\
& \text { 6UN } \\
& \text { 8UN } \\
& 126 \mathrm{NN} \\
& 16 \mathrm{NN}
\end{aligned}
$$ \& 1.759

1.820
1.865
1.970
1.932
1.936
1.946 \& 83.5
83.1
83.1
83.1
83.8
83.8 \& 1.795
1.850
1.890
1.928
1.926

1.957 \& $$
\begin{aligned}
& { }^{79.0} 1.0 \\
& 67.7 \\
& 66.75 \\
& 66.5 \\
& 66.5 \\
& 66.2
\end{aligned}
$$ \& 1.759

1.820
1.865
1.961
1.932

1.936 \& $$
\begin{aligned}
& 1.787 \\
& 1.875 \\
& 1.877 \\
& 1.979 \\
& 1.939 \\
& 1.952
\end{aligned}
$$ \& 1.768

1.827
1.871
1.974
1.936

1.949 \& $$
\begin{aligned}
& 1.786 \\
& 1.883 \\
& 1.884 \\
& 1.823 \\
& 1.943 \\
& 1.993 \\
& 1.954
\end{aligned}
$$ \& 1.777

1.835
1.877
1.979
1.939
1.952 \& 1.795
1.850
1.890
1.928
1.946
1.957 \& 1.786
1.842
1.883
1.923
1.923
1.943
1.954 \& $1.80 \pm$
1.858
1.896
1.932
1.950
1.960 <br>
\hline
\end{tabular}

| 2.0625-16 | UNS | 1.995 | 83.1 | 2.009 | 65.9 | 1.995 | 2.002 | 1.998 | 2.005 | 2.002 | 2.009 | 2.005 | 2.012 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2.125-6 | 6UN | 1.945 | 83.1 | 1.975 | 69.3 | 1.945 | 1.960 | 1.952 | 1.968 | 1.960 | ${ }^{1.975}$ | 1.968 2.008 | ${ }_{2}^{1.983}$ |
| $2.125-8$ | 8UN | 1.990 | 83.1 | ${ }_{2}^{2.015}$ | 67.7 | ${ }^{1.990}$ | ${ }_{2}^{2.002}$ | ${ }_{2}^{1.996}$ | ${ }_{2}^{2.008}$ | ${ }_{2}^{2.002}$ | ${ }_{2}^{2.015}$ | 2.008 2.048 | ${ }_{2}^{2.057}$ |
| ${ }_{2}^{2.125-12}$ | 12 UN | ${ }_{2}^{2.035}$ | 83.1 83.8 | ${ }_{2}^{2.053}$ | 66.5 66.5 | 2.035 2.057 | 2.064 | ${ }_{2}^{2.061}$ | ${ }_{2}^{2.068}$ | ${ }_{2} .064$ | ${ }_{2} .071$ | ${ }_{2}^{2} .068$ | ${ }_{2}^{2.075}$ |
| ${ }_{2}^{2.125-20}$ | 20 UN | ${ }_{2} .071$ | 83.1 | 2.082 | 66.2 | 2.071 | 2.077 | 2.074 | 2.080 | 2.077 | 2.082 | 2.080 | 2.085 |
| 2.1875-16 | UNS | 2.120 | 83.1 | 2.134 | 65.9 | 2.120 | 2.127 | 2.123 | 2.130 | 2.127 | 2.134 | 2.130 | 2.137 |
| 2.250-4.5 | UNC | 2.009 | 83.5 | ${ }_{2}^{2.045}$ | 71.0 | $\stackrel{2}{2.009}$ | ${ }_{2}^{2.027}$ | ${ }_{2}^{2.018}$ | 2.036 2.093 | ${ }_{2}^{2.027}$ | 2.045 2.100 | 2.036 2.092 | 2.051 2.108 |
| ${ }_{2} .250-6$ | 6 UN | 2.070 | 83.1 | 2.100 | 69.3 | 2.070 | 2.085 |  |  |  |  |  |  |
| 2.500-4 | UNC | 2.229 | 83.4 | 2.267 | 71.7 | 2.229 | 2.248 | 2.239 | 2.258 | 2.248 | ${ }^{2} .267$ | ${ }_{2}^{2.258}$ | ${ }_{2}^{2.276}$ |
| $2.750-4$ | UNC | 2.479 | 83.4 | 2.517 | 71.7 | 2.479 | 2.498 | ${ }_{2}^{2} .489$ | ${ }_{2}^{2.508}$ | ${ }_{2}^{2} .748$ | ${ }_{2}^{2.517}$ | ${ }_{2}^{2.08}$ | ${ }_{2}^{2.776}$ |
| $3.000-4$ | UNC | 2.729 | 83.4 | ${ }_{2}^{2.767}$ | 71.7 | $\stackrel{2}{2.729}$ | 2.748 $\stackrel{2}{2998}$ | 2.739 2.989 | 2.758 3.008 | - 2.998 | + ${ }_{3}^{2.767}$ | ${ }_{3}$ | 2.776 3.026 |
| $3.250-4$ | UNC | 2.979 | 83.4 | 3.017 | 71.7 | 2.979 |  | 2.989 |  |  |  |  |  |
| ${ }^{a}$ The differences between limits are equal to the minor diameter tolerances given in table 3.9 for lengths of engagement to and including $0.33 D$. However, the minimum greater than 0.33 D in sizes 0.25 in . and larger are adjusted so that the difference between limits is never less than 0.0040 in . For diameter-pitch combinations other than those given in table 3.9 should be similarly applied to determine hole size limits. |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| (1) with the same pitch and(2) with a diameter that is less by an integral amount than the diameter of the diameter-pitch combination for which hole size values are desired. (NOTE: Values in the |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 0.25 in . cannot be used for this purpose.) <br> EXAMPLE: To obtain the values for the $4.000-8 \mathrm{UN}-1 \mathrm{~B}$ or -2 B thread, add 2.000 to values for the $2.000-8 \mathrm{UN}$ thread shown in the table. These values would then becal |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Table A3.6. Recommended hole size limits before threading for different lengths of

| Nominal size in inches and threads per inch | Seriesdesignation | Minor diameter of internal threads |  |  |  | Recommended hole size limits for different lengths of engagement |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Min | Percent basic thread height | Max ${ }^{\text {c }}$ | Percent basic height height | To and including 0.33D |  | Above 0.33D thru 0.67D |  | Above 0.67D thru 1.5D |  | Above 1.5D thru $3 D$ |  |
|  |  |  |  |  |  | Min | Max | Min | Max | Min | Max | Min | Max |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 |
| .060-80 or No. 0-80 | UNF | $\begin{aligned} & \text { in } \\ & 0.0465 \end{aligned}$ | 83.1 | $\begin{aligned} & i n \\ & 0.0514 \end{aligned}$ | 53.0 | $i n$ 0.0465 | ${ }^{\text {in }}$ | in 0.0479 | ${ }_{0}^{\text {in }}$ | $\begin{aligned} & i n \\ & 0.0479 \end{aligned}$ | $\begin{aligned} & i n \\ & 0.0514 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & 0.0479 \end{aligned}$ | $\begin{aligned} & \text { in } \\ & 0.0514 \end{aligned}$ |
| $\begin{aligned} & .073-64 \text { or No. } 1-64 \\ & .073-72 \text { or No. 1-72 } \end{aligned}$ | $\begin{aligned} & \text { UNC } \\ & \text { UNF } \end{aligned}$ | $\begin{aligned} & .0561 \\ & .0580 \end{aligned}$ | 83.3 83.1 | $\begin{aligned} & .0623 \\ & .0635 \end{aligned}$ | $\begin{aligned} & 52.7 \\ & 52.7 \end{aligned}$ | $\begin{aligned} & .0561 \\ & .0580 \end{aligned}$ | . 05699 | $\begin{aligned} & .0580 \\ & .0596 \end{aligned}$ | $\begin{array}{r} .0618 \\ .0629 \end{array}$ | $\begin{aligned} & .0585 \\ & .0602 \end{aligned}$ | $\begin{array}{r} .0623 \\ .0635 \end{array}$ | $\begin{gathered} .0585 \\ .0602 \end{gathered}$ | $\begin{array}{r} .0623 \\ .0635 \end{array}$ |
| $.086-56 \text { or No. } 2-56$ <br> .086-64 or No. 2-64 | $\begin{aligned} & \text { UNC } \\ & \text { UNF } \end{aligned}$ | . 06697 | 83.2 83.3 | . 07375 | $\begin{aligned} & 53.0 \\ & 52.7 \end{aligned}$ | . 06697 | .0705 | . 06786 | .0724 | $\begin{aligned} & .0699 \\ & .0720 \end{aligned}$ | $\begin{array}{r} .0737 \\ .0753 \end{array}$ | $\begin{aligned} & .0699 \\ & .0720 \end{aligned}$ | . 07375 |
| $\begin{aligned} & .099-48 \text { or No. 3-488 } \\ & .099-56 \text { or No. 3-56 } \end{aligned}$ | $\begin{aligned} & \text { UNC } \\ & \text { UNF } \end{aligned}$ | ..0764 | 83.5 83.2 | . 08865 | $\begin{aligned} & 53.6 \\ & 53.9 \end{aligned}$ | .0764 .0797 | $.0804$ | $\begin{aligned} & .0785 \\ & .0814 \end{aligned}$ | $\begin{aligned} & .0825 \\ & .0848 \end{aligned}$ | $\begin{aligned} & .0805 \\ & .0831 \end{aligned}$ | $\begin{aligned} & .0845 \\ & .0865 \end{aligned}$ | $\begin{aligned} & .0806 \\ & .0833 \end{aligned}$ | $.0846$ |
| $\begin{aligned} & .112-40 \text { or No. } 4-40 \\ & .112-48 \text { or No. 4-48 } \end{aligned}$ | $\begin{aligned} & \text { UNC } \\ & \text { UNF } \end{aligned}$ | $\begin{aligned} & .0849 \\ & .0894 \end{aligned}$ | 83.4 | . 09968 | 55.7 56.2 | . 0849 | .0894 | .0871 | . 09949 | .0894 .0931 | . 09368 | . 09092 | . 09977 |
| $\begin{aligned} & .125-40 \text { or No. } 5-40 \\ & .125-44 \text { or No. } 5-44 \end{aligned}$ | $\begin{aligned} & \text { UNC } \\ & \text { UNF } \end{aligned}$ | .0979 .1004 | 83.4 83.3 | . 1062 | 57.9 57.9 | .0979 .1004 | . 1020 | .1000 .1023 | . 1041 | . 1021 | . 10679 | . 1036 | . 1077 |
| .138-32 or No. 6-32 <br> .138-40 or No. 6-40 | UNC | .1040 .1110 | 83.8 83.1 | .1140 .1186 | 59.1 | .1040 .1110 | . 11448 | . 1066 | .1115 .1167 | .1091 .1147 | .1140 .1186 | .1115 .1166 | . 11264 |
| .164-32 or No. 8-32 <br> .164-36 or No. 8-36 | $\begin{aligned} & \text { UNC } \\ & \text { UNF } \end{aligned}$ | .1300 .1340 | 83.8 83.1 | .1389 .1416 | 61.8 62.1 | .1300 .1340 | .1345 <br> .1377 | . 1324 | .1367 .1397 | . 1346 | .1389 .1416 | . 13397 | . 14435 |
| $\begin{aligned} & .190-24 \text { or No. 10-24 } \\ & .190-32 \text { or No. } 10-32 \end{aligned}$ | $\begin{aligned} & \text { UNC } \\ & \text { UNF } \end{aligned}$ | .1450 .1560 | 83.1 83.8 | . 15541 | 63.7 63.8 | .1450 .1560 | . 1502 | . 1475 | . 11621 | .1502 .1602 | . 1555 | . 1528 | . 11581 |
| $\begin{aligned} & .216-24 \text { or No. } 12-24 \\ & .216-28 \text { or No. 12-28 } \\ & .216-32 \text { or No. } 12-32 \end{aligned}$ | UNC | .1710 .1770 .1820 | 83.1 84.1 84.1 83.8 | .1807 .1857 .1895 | 65.2 65.3 65.3 | .1710 .1770 .1820 | .1758 .1855 .1858 | .1733 .1794 .1841 .1986 | .1782 .1836 .1877 | .1758 .1815 .1859 | .1807 .1857 .1895 | .1782 .1836 .1877 | .1831 .1878 .1913 |
| $.250-20$ $.250-28$ $.250-32$ $.250-36$ | UNC UNF UNEF UNS | .1960 .2110 .2160 .2200 | 83.1 84.1 83.8 83.1 | .2067 .2190 .2229 .2258 | 66.7 66.8 66.8 67.1 | .1960 .2110 .2160 .2200 | .2013 .2152 .2196 .2229 | .1986 .2131 .2172 .2203 | .2040 .2171 .2212 .2243 | .2013 .2150 .2189 .2218 | .2067 .2190 .2229 .2258 | .2040 .2169 .2206 .2233 | .2094 .2209 .2246 .2273 |
| $.3125-18$ $.3125-20$ $.3125-24$ $.3125-28$ $.3125-32$ $.3125-36$ | UNC 20UN UNF $28 U N$ UNEF UNS | .2520 .2580 .2670 .2740 .2790 .2820 | 83.8 83.9 84.1 83.0 82.0 84.5 84.5 | .2630 .2680 .2754 .2807 .2847 .2877 | 68.6 68.5 68.5 68.5 68.5 68.5 68.7 | .2520 .2580 .2670 .2740 .2790 .2820 | .2577 .2632 .2714 .2772 .2817 .2850 | .2551 <br> .2608 <br> .2694 <br> .2749 <br> .2792 <br> .2823 | .2604 .2656 .2734 .2789 .2832 .2863 | .2577 .2632 .2714 .2767 .2807 .2837 | .2630 .2680 .2754 .2807 .2847 .2877 | .2604 .2656 .2734 .2784 .2822 .2850 | .2657 .2704 .2774 .2824 .2862 .2890 |
| $.375-16$ $.75-20$ $.375-24$ $.35-28$ $.35-32$ $.375-36$ | UNC 20UN UNF 28UN UNEF UNS | .3070 .3210 .3300 .3360 .3410 .3450 | 83.8 83.1 83.1 84.1 83.1 83.8 83.1 | .3182 .3297 .3372 .3426 .3469 .3501 | 70.0 69.7 69.8 69.8 69.8 69.0 | .3070 .3210 .3300 .3360 .3410 .3450 | .3127 .3253 .3336 .3395 .3441 .3475 | .3101 .3231 .3314 .3370 .3415 .3450 | .3155 .3275 .3354 .3410 .3455 .3490 | .3128 .3253 .3332 .3386 .3429 .3461 | .3182 .3297 .3372 .3426 .3469 .3501 | .3155 .3275 .3351 .3402 .3444 .3474 | .3209 .3319 .3391 .3442 .3484 .3514 |
| $.4375-14$ $.4375-16$ $.4375-20$ $.4375-28$ $.435-32$ | UNC 16UN UNF UNEF 32UN | .3600 .3700 .3830 .3990 .4040 | 83.5 83.5 83.1 83.9 83.0 82.5 | .3717 .3800 .3916 .4051 .4094 | 70.9 70.8 70.7 69.8 69.2 | .3600 .3700 .3830 .3990 .4040 | .3660 .3749 .3875 .4020 .4066 | .3630 .3723 .3855 .3995 .4040 | .3688 .3774 .3896 .4035 .4080 | .3659 .3749 .3875 .4011 .4054 | .3717 .3800 .3916 .4051 .4094 | .3688 .3774 .3896 .4027 .4069 | .3746 .3825 .3937 .4067 .4109 |











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|  | $\text { Above } 1.5 D \text { thru } 3 D$ | $\begin{gathered} \text { 侖 } \\ \hline \end{gathered}$ | $\pm$ |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\underset{B}{E}$ | 9 |  |  |  |  | ューーシーシーシ |  |  |  |
|  | $\begin{aligned} & \text { B } \\ & = \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 4 \end{aligned}$ | $\stackrel{\text { ※゙̈ }}{\underset{\sim}{7}}$ | ヘ |  |  58ㅎ․ㅇ․ <br> oーシーシームー～ |  |  | ann Med Nis NWN <br> －inninia |  |  |  |
|  |  | E | こ |  |  |  |  | Tis80 No 0 ఝ엉 －MNaNM <br>  |  |  －O이Nが <br>  |  |
|  | 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 <br> 0 | $\stackrel{\text { 㙳 }}{2}$ | 9 |  |  |  ササ゚ <br>  がーロー～ |  －ज10 0 O－ シュ゙ゥーシームーシ |  |  |  |  |
| $\begin{aligned} & \text { o } \\ & \text { g } \\ & \text { ت } \\ & \text { ت } \\ & ~ \end{aligned}$ |  | 号 | $\bigcirc$ |  |  |  |  |  がNぱN ュースームー～ |  |  |  |
| $\begin{gathered} \text { Ü } \\ \text { 世4 } \end{gathered}$ |  | $\stackrel{\text { x }}{\underset{y}{\mathrm{E}}}$ | $\infty$ |  |  |  |  |  |  |  |  |
|  |  | $\underset{A}{E}$ | r |  |  | 9R8웅 ○SNan －$-\mathrm{C}=\mathrm{H}$ |  | ㅇNNㅇNㅇN NはNNは |  | 영ㅇㅇㅇㅇ NTににか。 <br>  |  |
| Minor diameter of internal threads |  |  | $\bigcirc$ |  |  |  |  |  |  |  |  |
|  |  |  | 25 |  |  |  |  |  |  Nล $\qquad$ |  |  |
|  |  |  | ＋ | ＋0に一毋0． <br>  | $\dot{\infty} \tilde{\infty}_{\infty}^{\infty} \tilde{\infty}_{\infty}^{\infty} \infty_{\infty}$ | $+0-\infty 00$ <br>  | $\mathfrak{\infty} \infty$ | Nonco |  |  |  |
|  | $\underset{y}{E}$ |  | $\infty$ |  | $\begin{aligned} & 8888808 \\ & \text { 心. } 08080 \\ & 0 \end{aligned}$ | $\begin{aligned} & \text { Nogsog } \\ & \text { iso } \\ & 0=1 \end{aligned}$ | 9888889 <br> ○このが心 <br> ームームールー | 웅NㅇN <br> NNHNNO <br> ューシーシュース | 98989요 $\rightarrow \pi \infty-$－ T•Nmmon ーールームーム | coogerg <br>  <br>  <br>  |  |
|  |  |  | ar |  |  |  |  |  |  |  |  |
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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 8． 9009 10 H0 10 － 2 ？ | जलை NOONMO | 13980 $120 \times 1006$ $\therefore 106001$ |  | $\begin{aligned} & 9999 \\ & 8109.9 \\ & -1.0 \infty \end{aligned}$ |  |  | $\underset{8}{7}$ | $\begin{aligned} & \text { Bondo } \\ & \text { oryos } \end{aligned}$ | $$ | $\begin{aligned} & \text { HO } \\ & \text { No } \\ & \hline 0 \end{aligned}$ | $\begin{aligned} & 9090 \\ & 208: 28 \\ & \text { Nis } \end{aligned}$ |


|  |  | NNNMNN NOSOMザ | $100^{-\infty} 0^{\infty} \mathrm{O}$ To 12120001 | －NM～N NWNM $001-1$ |  |  |  | $\stackrel{\infty}{\circ}$ |  | $\begin{aligned} & \infty \\ & \sim \\ & \sim \\ & \sim \end{aligned}$ | $\begin{aligned} & -1.6 \\ & \text { ल్ర } \end{aligned}$ |  |
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| －1ヵ－1～－ |  |  |  |  |  |  | ーームームの | N | －NNMN | $\cdots$ | N® | N＊N\％ |



|  |  |  | $\begin{aligned} & 200610 N \\ & 7000000 \\ & 100001 \end{aligned}$ |  | $\begin{aligned} & 6891 \\ & 8.980 \\ & \qquad 1000 \end{aligned}$ |  |  | $\stackrel{\text { N }}{8} \underset{8}{8}$ |  | $\begin{aligned} & \text { O } \\ & \text { © } \\ & \underset{\sim}{1} \end{aligned}$ | $\begin{aligned} & 40 \\ & 80 \\ & 80 \\ & 00 \\ & \text { No } \end{aligned}$ | $\begin{aligned} & 9009 \\ & 12.108 \\ & \text { NWN } \\ & \text { NaNm } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |




| 000090 NNNLNO <br>  <br>  | ㅇㅇㅇㅇ <br>  H H 10252210 ーーローーロ | 909000 जNGCNM 15120000 ールールーコ | 999808 Mr－ $0 \times 0$ 1500000. ールールール |  |  |  | 88989 12 N 0 Nㅓ トのかった。 ーームームーム | $\begin{aligned} & 8 \\ & \stackrel{8}{0} \\ & \stackrel{8}{8} \\ & - \end{aligned}$ |  | $\begin{aligned} & 8 \\ & \underset{\sim}{\mathbf{N}} \\ & \stackrel{y}{c} \end{aligned}$ | $\begin{aligned} & 88 \\ & 88 \\ & 80 \\ & \text { No } \end{aligned}$ | 998 Nに NT NサいO Nलिब |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
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| サザNN゙ | －＋icio |  |  |  | ＋サयल゙ | ＋サ＋ベ－ | サササみパ | N | सせせN－ | N | － | ぜざい |
| 1－1－T－T5 | Mtrotic |  |  | いただった | －1－NT | N－TN0 | －1－10 | N | －NTMN | $\cdots$ | －1． | 1－「ご， |





[^25]Table A3.7. Recommended hole size limits before threading for different lengths of engagement, Unified National Miniature, UNM, thread series

| Thread designation |  |  | Minor diameter of internal threads |  |  |  | Recommended hole size limits for different lengths of engagement a |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Preferred | Secondary |  | Min | Percent basic thread height | Max | Percent basic thread height | To and including 0.67D |  | Above 0.67 D to 1.5 D |  | Above $1.5 D$ to $3 D$ |  |
|  |  |  |  |  |  |  | Min | Max | Min | Max | Min | Max |
|  |  | Pitch |  |  |  |  | mm | mm | mm | mm | mm | mm |
| .30UNM |  | ${ }_{0} 0.080$ | ${ }_{0}{ }^{\text {m }}$ | 100 | 0.260 | 51.9 | 0.232 | 0.246 | 0.241 | 0.260 | 0.251 | 0.269 |
| .30UNM | .35UNM | . 090 | . 264 | 100 | . 305 | 52.3 | . 274 | . 290 | . 2824 | .305 .348 | . 295 | ${ }^{.} 315$ |
| .40UNM | .45UNM | .100 .100 | .304 .354 | 100 100 | .348 .398 | 54.2 54.2 | .315 .365 | . 332 | . 326 | .348 .398 | .337 .387 | .359 .409 |
| . 50 UNM |  | . 125 | . 380 | 100 | . 432 | 56.7 | . 393 | . 412 | . 406 | . 432 | . 419 | . 445 |
|  | .55UNM | . 125 | .430 .456 | 100 100 | . 482 | 56.7 58.3 | . 4731 | . 462 | . 456 | . 482 | . 469 | . 495 |
| .60UNM | .70UNM | . 175 | .456 .532 | 100 100 | . 600 | 59.5 | . 549 | . 574 | . 566 | . 600 | . 583 | . 617 |
| .80UNM |  | . 200 | . 608 | 100 | . 684 | 60.4 | . 627 | . 656 | . 646 | . 684 | . 665 | . 703 |
| .80UNM | .90UNM | . 225 | . 684 | 100 | . 768 | 61.1 | . 705 | . 736 | . 726 | . 768 | . 747 | . 789 |
| 1.00UNM | 1.10UNM | . 250 | .760 .860 | 100 100 | . 8552 | 61.7 61.7 | .783 .883 | . 81818 | .806 .906 | . 8552 | .829 .929 | .875 .975 |
| 1.20UNM |  | . 250 | . 960 | 100 | 1.052 | 61.7 | . 983 | 1.018 | 1.006 | 1.052 | 1.029 | 1.075 |
|  | 1.40UNM | . 300 | 1.112 | 100 | 1.220 | 62.5 | 1.139 | 1.180 | ) 1.166 | 1.220 | 1.193 | 1.247 |
|  |  | Thds per inch |  |  |  |  | in |  | in | in |  | in |
| .30UNM |  | ${ }^{\text {anch }} 318$ | 0.0088 | 100 | 0.0102 | 51.9 | 0.0092 | 0.0097 | 0.0095 | 0.0102 | 0.0098 | 0.0106 |
| .30UNM | .35UNM | 282 | . 0104 | 100 | . 0120 | 52.3 | . 0108 | . 0114 | . 0112 | . 0120 | . 0116 | . 0124 |
| .40UNM | .45UNM | 254 254 | .0120 .0139 | 100 100 | . 0137 | 54.2 54.2 | .0124 .0143 | . 0131 | .0128 .0148 | . 0137 | . 0133 | . 0141 |
| .50UNM |  | 203 | . 0150 | 100 | . 0170 | 56.7 | . 0155 | . 0162 | . 0160 | . 0170 | . 0165 | . 0175 |
| . | .55UNM | 203 | . 0169 | 100 | . 0190 | 56.7 | . 0174 | . 0182 | . 0179 | . 0190 | . 0185 | . 0195 |
| .60UNM |  | 169 | . 0180 | 100 | . 0203 | 58.3 | . 0186 | . 0194 | . 0192 | . 0203 | . 0197 | . 0209 |
|  | .70UNM | 145 | . 0209 | 100 | . 0236 | 59.5 | . 0216 | . 0226 | . 0223 | . 0236 | . 0229 | . 0243 |
| .80UNM |  | 127 | . 0239 | 100 | . 0269 | 60.4 | . 0247 | . 0258 | . 0254 | . 0269 | . 0261 | . 0277 |
|  | .90UNM | 113 | . 0269 | 100 | . 0302 | 61.1 | . 0277 | . 02921 | . 02885 | . 0302 | .0294 | . 0310 |
| 1.00UNM | 1.10UNM | 102 | . 02399 | 100 | . 0335 | 61.7 61.7 | . 0308 | . 0321 | . 0357 | . 0375 | . 0366 | . 0384 |
| 1.20UNM |  | 102 | . 0378 | 100 | . 0414 | 61.7 | . 0387 | . 0400 | . 0396 | . 0414 | . 0405 | . 0423 |
|  | .1.40UNM | 85 | . 0438 | 100 | . 0480 | 62.5 | . 0448 | . 0464 | . 0459 | . 0480 | . 0470 | . 0490 |



# UNITED STATES DEPARTMENT OF COMMERCE National bureau of standards 

## HANDBOOK H28

SCREW-THREAD STANDARDS

FOR FEDERAL SERVICES

## APPENDIX A4 <br> 1969

METHODS OF WIRE MEASUREMENT OF PITCH DIAMETER OF $60^{\circ}$ THREADS

On a straight thread, the pitch diameter is the diameter of the cylinder whose surface passes through the thread profiles at such points as to make the widths of thread groove and thread ridge equal.

On a taper thread, the pitch diameter at a given position on the thread axis is the diameter of the pitch cone at that position.

The degree of accuracy to which the pitch diameter can be measured will depend on the accuracy of lead, helix, and form of thread. As thread plug gages and thread setting plug gages have highly accurate threads, their pitch diameters may be measured to a correspondingly high degree of accuracy by applying the methods described in this appendix. In turn, the virtual diameters (or effective sizes) of thread ring, most snap, and most indicating gages may be determined by fitting or comparison with such setting plug gages. Those snap and indicating gages which utilize elements with curved contacts have a pitch (simple effective) diameter determined by comparison to the applicable settingplug gages.

As most threads of mechanical fasteners and components are made to a lesser degree of accuracy than gage threads, their pitch diameters are not susceptible to accurate determination by direct measuring methods. Therefore, it is not recommended that such threads be measured by the use of wires. On such threads, the pitch diameter is to be regarded as the pitch cylinder or cone which would bound, on the maximum-material side, the approximately cylindrical or conical surface which would pass through the thread profiles at all points such that the widths of the thread and groove are equal. Accordingly, the conformity of such threads with specified pitch diameter limits is determined by gaging means and methods specified in section 6 .

The accurate measurement of pitch diameter of a thread, which may be perfect as to form and lead, presents certain difficulties which result in some uncertainty as to its true value. The adoption of a standard uniform practice in making such measurements is, therefore, desirable in order to reduce such uncertainty of measurement to a minimum. The so-called "three-wire method" of measuring pitch diameter of straight thread plug gages, as outlined herein, has been found to be the most generally satisfactory method when properly carried out, and is recommended for universal use in the direct measurement of thread plug and thread setting plug gages. (See fig. A4.1.)

## 1. SIZE OF WIRES

In the three-wire method of measuring pitch diameter, small hardened steel cylinders or wires of


Figure A4.1. Three-wire method of measuring pitch diameter of straight thread pluggages.
correct size are placed in the thread groove, two on one side of the screw and one on the opposite side, as shown in figure A4.1. The contact face of the comparator, measuring machine, or micrometer anvil or spindle over the two wires must be sufficiently large in diameter to touch both wires; that is, the diameter must be greater than the pitch of the thread. It is best to select wires of such size that they touch the flanks of the thread at the midslope since the measurement of pitch diameter is least affected by any deviation in thread angle that may be present when such size is used. The size of wire that touches exactly at the midslope of a perfect thread of a given pitch is termed the "best-size" wire for that pitch. Any size, however, may be used that will permit the wires to rest on the flanks of the thread and also project above the crest of the thread.

The depth at which a wire of given diameter will rest in a thread groove depends primarily on the pitch and included angle of the thread and, secondarily, on the angle made by the helix at the point of contact of the wire and the thread, with a plane perpendicular to the axis of the screw. Inasmuch as variation in the lead angle has a very small effect in determining the diameter of the wire that touches at the midslope of the thread, and as it is desirable to use one size of wire to measure all
threads of a given pitch and included angle, the best-size wire is taken as that size which will touch at the midslope of a groove cut around a cylinder perpendicular to the axis of the cylinder, and of the same angle and depth as the thread of the given pitch. This is equivalent to a thrcad of zero lead angle. The size of wire touching at the midslope, or "best-size" wire, is given by the formula:

$$
W=\frac{p}{2} \sec \alpha
$$

in which

$$
\begin{aligned}
W & =\text { diameter of wire } \\
p & =\text { pitch } \\
\alpha & =\text { half included angle of thread. }
\end{aligned}
$$

This formula reduces to-
$W=0.57735 p$, for $60^{\circ}$ threads.
Table A4.2. Wire sizes and constants for all USA
Standard 60' threads (Unified, hose-coupling, and pipe)

| Threads per inch, $n$ | Pitch.$p=\frac{1}{n}$ | $\begin{aligned} & \frac{\text { Pitch }}{2} \\ & \frac{p}{2}=\frac{1}{2 n} \end{aligned}$ | Depth of V thread, $\frac{\cot 30^{\circ}}{2 \pi}$ | Wire sizes ${ }^{\text {a }}$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $\begin{aligned} & \text { Best, } \\ & 0.577350 p \end{aligned}$ | $\begin{aligned} & \text { Maximum, } \\ & 1.010363 p \end{aligned}$ | $\begin{aligned} & \text { Minimum, } \\ & 0.505182 p \end{aligned}$ |
| 1 | 2 | 3 | 4 | 5 | 6 | 7 |
|  | in | in | in | $2 n$ | in | in |
| 80 | 0.012500 | 0.00625 | 0.010825 | 0.00722 | 0.01263 | 0.00631 |
| 72 | . 013889 | . 00694 | . 012028 | . 00802 | . 01403 | . 00702 |
| 64 | . 015625 | . 00781 | . 013532 | . 00902 | . 01579 | . 00789 |
| 56 | . 017857 | . 00893 | . 015465 | . 01031 | . 01804 | . 00902 |
| 50 | . 020000 | . 01000 | . 017321 | . 01155 | . 02021 | . 01010 |
| 48 | . 020833 | . 01042 | . 018042 | . 01203 | . 02105 | . 01052 |
| 44 | . 022727 | . 01136 | . 019682 | . 01312 | . 02296 | . 01148 |
| 40 | . 025000 | . 01250 | . 021651 | . 01443 | . 02526 | . 01263 |
| 36 | . 027778 | . 01389 | . 024056 | . 01604 | . 02807 | . 01403 |
| 32 | . 031250 | . 01562 | . 027063 | . 01804 | . 03157 | . 01579 |
| 30 | . 033333 | . 01667 | . 028868 | . 01925 | . 03368 | . 01684 |
| 28 | . 035714 | . 01786 | . 030929 | . 02062 | . 03608 | . 01804 |
| 27 | . 037037 | . 01852 | . 032075 | . 02138 | . 03742 | . 01871 |
| 26 | . 038462 | . 01923 | . 033309 | . 02221 | . 03886 | . 01943 |
| 24 | . 041667 | . 02083 | . 036084 | . 02406 | . 04210 | . 02105 |
| 22 | . 045445 | . 02273 | . 039365 | . 02624 | . 04592 | . 02296 |
| 20 | . 050000 | . 02500 | . 043301 | . 02887 | . 05052 | . 02526 |
| 18 | . 055556 | . 02778 | . 048113 | . 03208 | . 05613 | . 02807 |
| 16 | . 062500 | . 03125 | . 054127 | . 03608 | . 06315 | . 03157 |
| 14 | . 071429 | . 03571 | . 061859 | . 04124 | . 07217 | . 03608 |
| 13 | . 076923 | . 03846 | . 066617 | . 04441 | . 07772 | . 03886 |
| 12 | . 083333 | . 04167 | . 072169 | . 04811 | . 08420 | . 04210 |
| 11.5 | . 086957 | . 04348 | . 075307 | . 05020 | . 08786 | . 04393 |
| 11 | . 090909 | . 04545 | . 078730 | . 05249 | . 09185 | . 04593 |
| 10 | . 100000 | . 05000 | . 086603 | .05774 | . 10104 | . 05052 |
| 9 | . 111111 | . 05556 | . 096225 | . 06415 | . 11226 | . 05613 |
| 8 | . 125000 | . 06250 | . 108253 | . 07217 | . 12630 | . 06315 |
| 7.5 | . 133333 | . 06667 | . 115470 | . 07698 | . 13472 | . 06736 |
| 7 | . 142857 | . 07143 | . 123718 | . 08248 | . 14434 | . 07217 |
| 6 | . 166667 | . 08333 | . 144338 | . 09623 | . 16839 | . 08420 |
| 5.5 | . 181818 | . 09091 | . 157459 | . 10497 | . 18370 | . 09185 |
| 5 | . 200000 | . 10000 | . 173205 | . 11547 | . 20207 | . 10104 |
| 4.5 | . 222222 | . 11111 | . 192450 | . 12830 | . 22453 | . 11226 |
| 4 | . 250000 | . 12500 | . 216506 | . 14434 | . 25259 | . 12630 |

[^26]It is frequently desirable, as, for example, when a best-size wire is not available, to measure pitch diameter by means of wires of other than the best size. The minimum size that may be used is limited to that permitting the wire to project above the crest of the thread, and the maximum to that permitting the wire to rest on the flanks of the thread just below the crest, and not ride on the crest of the thread. The diameters of the best size, maximum, and minimum wires for all USA Standard $60^{\circ}$ threads are given in tables A4.2 and A4.3.

When using wires of other than the best-size, precautions must be observed in the calculation of pitch diameter. Actual measured values for halfangles and the angle between the axis of the wire and a plane perpendicular to the axis of the thread must be used for the calculation of pitch diameter when using wires other than best-size. The uncertainties of the values used and the differcnt wire contact conditions will increase the uncertainty of the pitch diameter measurement.

## 2. METHODS OF MEASURING AND USING WIRES

The computed value for the pitch diametcr of a screw thread gage obtained from readings over wires will depend upon the accuracy of the measuring instrument used, the contact force, and the value of the diameter of the wires uscd in the computations. In order to measure the pitch diameter of a $60^{\circ}$ screw-thread gage to an accuracy within 0.0001 in by means of wires, it is necessary to know the wire diameters to within 0.00002 in . Accordingly, it is neccssary to use a measuring instrument that reads accurately to 0.00001 in .

Variations in diameter around the wire should be determined by rotating the wire between a flat measuring contact and an anvil having the form of a $60^{\circ} \mathrm{V}$-groove. Variations in diameter along the wire should be determined by measuring between a flat contact and a cylindrical anvil.

A wire presses on the flanks of a $60^{\circ}$ thread with the force that is applied to the wire by the measuring instrument. Inasmuch as the wire and thread deform at the contact areas, it is desirable to determine the size of the wire under conditions which will compensate for this deformation. It is rccommended for standard practice that diametcrs of wires be measured between a flat contact and a hardened and accurately ground and lapped steel cylinder having a diameter of 0.125 in . for wires used on threads having more than 40 up to and including 80 tpi and 0.750 in . for wires used on threads having 40 and fewer tpi with the force used in measuring the pitch diameter of the gage. The plane of the

Table A4.3. Relation of best wire diameters to pitches for all L'SA Standard $60^{\circ}$ threads (Unified, hose-coupling, and pipe) ${ }^{\text {a }}$

${ }^{a}$ The crosses $(X)$ indicate those wire diameters which can be used for each pitch. An encircled cross ( $\otimes$ ) indicates the "best wire" diameter for that tpi which heads the column.
flat contact should be parallel to the contact element of the cylinder within 0.000005 in .

To avoid a permanent deformation of the material of the wires or gages, it is necessary to limit the contact force and, for consistent results, a uniform practice as to contact force in making wire measurements of hardened screw threads gages is necessary. The practice recommended is to use the following forces:

| Threads per inch | Measuring force ( $\pm 10 \%$ ) |
| :---: | :---: |
| 20 or less | 2.5 pounds |
| Above 20 thru 40 | 1 pound |
| Above 40 thru 80 | 8 ounces |
| Above 80 thru 140 | 4 ounces |
| Above 140 | 2 ounces |

The use of other contact forces will cause a difference in the reading over the wires and to completely compensate for such errors is impractical.

The practice of using holding means, such as rubber bands, which has a tendency to prevent the wires from adjusting themselves to the proper position in the thread grooves, will result in false measurements. In some cases it has also been the practice to support the gage being measured on two
wires, which are in turn supported on a horizontal surface, and measuring from this surface to the top of a wire placed over and between the other wires. If the gage is of large diameter, its weight causes an increase in the elastic deformation at the contact points and an inaccurate reading is obtained. Tests on a 1-12 UNF setting plug gage showed a 0.00001 in . error when measured in this manner. This practice should therefore be avoided for gages of such size and larger. Wires from different sets of the same nominal diameter should not be mixed unless calibrated because thread wires in different sets may not have the same diameter. (See par. 3.2.)

In order to minimize the deviation of the measured pitch diameter from the true pitch diameter (neglecting the effect of lead angle) and reduce the chance of permanently deforming the gages and wires, this revision contains a change in the recommended measuring practice for threads and wires for threads having more than 40 up to and including S0 tpi. The new recommended practice reduces the force for measuring gages and wires from one to 0.5 lb and the size of the cylinder over which the wires are measured from 0.750 to 0.125 in . As a result of this change, the measured pitch diameters of threads in this range will be approximately 0.00005 in. larger than they were under the previous recommended practice.

The measured value will be much closer to the truc pitch diameter, however. Plug gages manu-
factured prior to this revision and within tolerance when measured under the previous recommended practice but not within tolerance when measured under the new recommended practice should be considered as within tolerance for a transition period. With the new rccommended practice, it can be shown that for all sizes of threads up to 1.500 in . in the fine thread scries (UNF) and all sizes up to 2.000 in. in the coarse thread series (UNC), the measurcd pitch diameter will not differ from the true pitch diameter (neglecting the effect of lead angle) in excess of 0.000035 in. Slightly larger discrepancies in the 2 to 4 in .size range are rclatively unimportant because
these sizes have larger tolerances. The measured diameter of the thread wires for threads having more than 40 up to and including 80 tpi under the new recommended practice differ by less than two microinches from the measurcd diameter under the previous recommended practice. Therefore, neither wire diameters nor corrections for computing pitch diameter need be changed.
Measurcments of a thread plug gage madc in accordance with these instructions, with wires that conform to the following specifications, should be accurate to within 0.0001 in.

## 3. STANDARD SPECIFICATION FOR WIRES AND STANDARD PRACTICE IN MEASUREMENT OF WIRES

The following specifications represent present practice relative to thread measuring wires:
3.1. Composition.-The wires shall be accurately finished, hardened steel cylinders of the maximum possible hardness without being brittle. The hardness shall not be less than that corresponding to a Knoop indentation number of 630 . A wire of this hardness can be cut with a file only with difficulty. The surface shall not be rougher than the equivalent of one having a surface roughness rating of 2 microinches arithmetical average.
3.2. Diameter of Wires.-One set of wires shall consist of three wires that shall have the same diameter within 0.00001 in., and this common diameter shall be within 0.00002 in of that corresponding to the best size for the tpi for which the wire is to be uscd. Wires shall be measured between a flat contact and a hardened and accurately finished cylinder having a surface roughness rating not in excess of 2 microinches arithmetical average. The measuring forces and cylinder diameters shall be as follows:

| 'Threads per inch | Measuring force ( $\pm 10 \%$ ) | Cylinder diameter |
| :---: | :---: | :---: |
| 20 or less | 2.5 pounds | 0.750 inch |
| Above 20 thru 40 | 1 pound | 0.750 inch |
| Above 40 thru 80 | 8 ounces | 0.125 inch |
| Above 80 thru 140 | 4 ounces | 0.050 inch |
| Above 140 | 2 ounces | 0.020 inch |

Using these conditions, the uncertainties of the wire diamcter measurement duc to other metrological considerations should be limited and not exceed 0.000010 in.

An acceptable technique for the measurement of the diameter of each set of thread mcasuring wires is to compare them to a reference master wire with a suitable comparison measuring instrument having any anvil shape or measuring force consistent with good metrological practice. The diameter of each refercnce master wire, however, must be calibrated by the specified technique with an uncertainty not in excess of 0.00000 j in.

Wircs which are to be used where the contact of the wire is a line contact, such as in gear wires, should not be used for measuring thread gages. The recommended practice for measuring such wires is between flat parallel contacts with a one pound force.
3.3. Variations in Diameter.-Variations in diameter along a wire (taper) over the 1 in. interval at the center of its length shall not exceed 0.000010 in as determined by measuring between a flat contact and a cylindrical contact. Variations from true cylindrical contour of a wire (out-of-roundness or noncircular cross section) over its 1 in. central interval shall not exceed 0.000010 in as determined by measuring between a flat measuring contact and a well finished $60^{\circ} \vee$-groove.

Tests for compliance of thread measuring wires with the above specifications are made by the National Bureau of Standards for a stated fee.

## 4. GENERAL FORMULA FOR MEASUREMENT OF PITCH DIAMETER

The general formula for determining the pitch diameter of any thread whose flanks are symmetrical with respect to a line drawn through the vertex and perpendicular to the axis of the thread, in which the slight effect of lead angle is taken into account, is
$E=M_{w}+\frac{\cot \alpha}{2 n}-w\left[1+\left(\operatorname{cosec}^{2} \alpha+\cot ^{2} \alpha \tan ^{2} \lambda^{\prime}\right)^{1 / 2}\right]$,
in which

$$
\begin{aligned}
E & =\text { pitch diameter } \\
M_{w} & =\text { measurement over wires } \\
\alpha & =\text { half angle of thread } \\
n & =\text { number of threads per inch }=1 / p \\
w & =\text { mean diameter of wires } \\
\lambda^{\prime} & =\text { angle between axis of wire and plane perpen- } \\
& \text { dicular to axis of thread. }
\end{aligned}
$$

This formula is a very close approximation, being based on certain assumptions regarding the positions of the points of contact between the wire and the thread.

Formula (1) can be converted to the following simplified form, which is particularly uscful when measuring threads of large lead angle:

$$
\begin{equation*}
E=M_{w}+\frac{\cot \alpha}{2 n}-w\left(1+\operatorname{cosec} \alpha^{\prime}\right), \tag{2}
\end{equation*}
$$

in which $\alpha^{\prime}=$ the angle whose tangent $=\tan \alpha \cos \lambda^{\prime}$.
When formula (1) is used, the usual practice is to expand the square root tcrm as a series, retaining only the first and second terms, which gives the following:
$E=M_{w}+\frac{\cot \alpha}{2 n}-w\left(1+\operatorname{cosec} \alpha+\frac{\tan ^{2} \lambda^{\prime} \cos \alpha \cot \alpha}{2}\right)$.

For large lead angles it is necessary to measure the wire angle, $\lambda^{\prime}$, but for lead angles of $5^{\circ}$ or less, if the "best-size" wire is uscd, this angle may be assumed to be equal to the lcad angle of the thread at the pitch linc, $\lambda$. The value of $\tan \lambda$, the tangent of the lead angle, is given by the formula

$$
\tan \lambda=\frac{L}{3.1416 E}=\frac{1}{3.1416 N E}
$$

in which
$L=$ lead
$N=$ number of turns per inch
$E=$ nominal pitch diametcr, or an approximation of the measured pitch diameter.

## 5. MEASUREMENT OF PITCH DIAMETER OF ALL USA STANDARD $60^{\circ}$ STRAIGHT THREADS (UNIFIED, HOSE-COUPLING, AND PIPE)

For threads of the Unified standard series, the term

$$
\frac{w \tan ^{2} \lambda^{\prime} \cos \alpha \cot \alpha}{\mathscr{n}}
$$

is neglected, as its value is small, being in all cases less than 0.00015 in for standard fastening screws when the best-size wire is used, and the above formula (3) takes the simplified form

$$
\begin{equation*}
E=M_{w}+\frac{\cot \alpha}{2 n}-w(1+\operatorname{cosec} \alpha) \tag{4}
\end{equation*}
$$

This practicc is permissible provided that it is uniformly followed, and in order to maintain uniformity of practice, and thus avoid confusion, the National Burcau of Standards uses formula (4) for such threads. The Bureau also uses formula (4) for special $60^{\circ}$ threads, cxcept when the value of the term

$$
\frac{w \tan ^{2} \lambda^{\prime} \cos \alpha \cot \alpha}{2}
$$

excecds 0.00015 in ., as in the case of multiple threads, or other threads having exceptionally large lead angles. For $60^{\circ}$ threads this term excceds 0.00015 when $N E \sqrt{n}$ is less than 17.1.

For a $60^{\circ}$ thread of correct angle and thread form formula (4) simplifies to

$$
\begin{equation*}
E=M_{w w}+\frac{0.86603}{n}-3 w . \tag{5}
\end{equation*}
$$

For a giveu sct of best-size wires

$$
E=M_{w}-C
$$

when

$$
C=w(1+\operatorname{cosec} \alpha)-\frac{\cot \alpha}{2 n}
$$

The quantity $C$ is a constant for a given thread angle, and, when the wircs are used for measuring threads of the pitch and angle for which they are the best size, the pitch diameter is obtained by the simple operation of subtracting this constant from the measurement taken over the wires. In fact, when best-size wircs are used, this constant is changed very littlc by a moderate deviation in the angle of the thread. Conscquently, the constants for the various sets of wires in use may be tabulated, thus saving a considcrable amount of time in the inspection of gages. However, when wires of other than the best size are used, this constant changes apprcciably with a deviation in the angle of the thread.

It has becn shown that, with the exception of coarse pitch screws, variation in angle from the basic size causes no appreciable change in the quantity $C$ for the best-size wires. On the other hand, when a wire near the maximum or minimum allowable size is used, a considerable change occurs, and the valucs of the cotangent and cosecant of the actual measured half angle are to be used. It is apparent, therefore, that there is a great advantage in using wires very closcly approximating the best size. For convenience in carrying out computations,
the values of $\cot \alpha / 2 n$ for standard pitches are given in table A4.2.

When the value of the term

$$
\left(\frac{w \tan ^{2} \lambda^{\prime} \cos \alpha \cot \alpha}{2}\right)
$$

exceeds 0.00015 in., the following pitch diameter formula should be used:

$$
E=M_{w}-(C+c)
$$

Tabular values for $(C+c)_{1}$ for a 1 -in axial pitch screw for $60^{\circ}$ threads are given in table A4.4 which values should be divided by the threads per inch for a given case. (See appendix in Part III, titled "Three-wire method of measurement of pitch diameter of $29^{\circ}$ Acme, $29^{\circ}$ Stub Acme, and Buttress threads," for further details.)

Table A4.4. Best wire diameters and constants for large lead angles, 1 -in axial pitch $60^{\circ}$ threads

| $\begin{gathered} \text { Lead } \\ \text { angle, } \lambda \end{gathered}$ | 1-start threads |  | 2-start threads |  | Lead angle, $\lambda$ | 2-start threads |  | 3 -start threads |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $w_{1}$ | $(C+c)_{1}$ | $w_{1}$ | $(C+c)_{1}$ |  | $w_{1}$ | $(C+c)_{1}$ | $w_{1}$ | $(C+c)_{1}$ |
| 1 | 2 | 3 | 4 | 5 | 1 | 4 | 5 | 6 | 7 |
| deg | in | in | in | in | deg | in |  |  | in |
| 5.0 | 0.57493 | 0.86181 | 0.57477 | 0.86145 | 10.0 | 0.56767 | 0.84918 | 0.56728 | 0.84830 |
| 5.1 | . 57483 | . 86165 | . 57467 | . 86127 | 10.1 | . 56749 | . 84887 | . 56709 | . 84797 |
| 5.2 | . 57474 | . 86149 | . 57456 | . 86109 | 10.2 | . 56730 | . 84856 | . 56689 | . 84763 |
| 5.3 | . 57465 | . 86133 | . 57446 | .86091 | 10.3 | . 56711 | . 81884 | . 56669 | . 84729 |
| 5.4 | . 57456 | . 86117 | . 57435 | . 86072 | 10.4 | . 56693 | . 84793 | . 56649 | . 84695 |
| 5.5 | . 57446 | . 86100 | . 57425 | . 86053 | 10.5 | . 56674 | . 84761 | . 56629 | . 84660 |
| 5.6 | . 57436 | . 86083 | . 57114 | . 86034 | 10.6 | . 56656 | . 84729 | . 56609 | . 84625 |
| 5.7 | . 57426 | . 86066 | . 57103 | . 86015 | 10.7 | . 56637 | . 84697 | . 56589 | . 84589 |
| 5.8 | . 57416 | . 86049 | . 57392 | .85995 | 10.8 | . 56617 | . 84664 | . 56568 | . 84553 |
| 5.9 | . 57406 | . 86032 | . 57381 | . 85976 | 10.9 | . 56598 | . 84631 | . 56547 | . 84517 |
| 6.0 | . 57395 | . 86014 | . 57369 | . 85956 | 11.0 | . 56578 | . 84598 | . 56526 | . 84481 |
| 6.1 | . 57385 | .85996 | . 57358 | . 85936 | 11.1 | . 56558 | . 84564 | . 56506 | . 84445 |
| 6.2 | . 57374 | . 85978 | . 57346 | . 85915 | 11.2 | . 56538 | . 84530 | . 56485 | . 84409 |
| 6.3 | . 57363 | . 85960 | . 57333 | .85893 | 11.3 | . 56518 | . 84497 | . 56463 | . 84372 |
| 6.4 | . 57352 | . 85942 | . 57320 | . 85871 | 11.4 | . 56498 | . 84463 | . 56441 | . 84335 |
| 6.5 | . 57341 | . 85923 | . 57308 | . 85850 | 11.5 | . 56478 | . 84429 | . 56420 | . 84298 |
| 6.6 | . 57330 | . 85904 | . 57295 | . 85828 | 11.6 | . 56457 | . 81394 | . 56398 | . 84260 |
| 6.7 | . 57318 | . 85885 | . 57282 | . 85805 | 11.7 | . 56437 | . 84360 | . 56375 | . 84221 |
| 6.8 | . 57307 | . 85866 | . 57269 | . 85782 | 11.8 | . 56416 | . 81325 | . 56353 | . 84183 |
| 6.9 | . 57295 | . 85847 | . 57256 | . 85760 | 11.9 | . 56396 | . 81290 | . 56331 | . 84145 |
| 7.0 | . 57284 | . 85828 | . 57242 | . 85737 | 12.0 | . 56375 | . 84255 | . 56308 | . 84106 |
| 7.1 | . 57272 | . 85808 | . 57228 | . 85713 | 12.1 | . 56353 | . 81219 | . 56285 | . 84067 |
| 7.2 | . 57260 | . 85788 | . 57215 | . 85689 | 12.2 | . 56332 | . 84183 | . 56263 | . 84028 |
| 7.3 | . 57248 | . 85768 | . 57201 | . 85664 | 12.3 | . 56311 | . 81117 | . 56240 | .83989 .83949 |
| 7.4 | . 57236 | . 85747 | . 57187 | . 85640 | 12.4 | . 56289 | . 8.4111 | . 56217 | . 83949 |
| 7.5 | . 57223 | . 85727 | . 57173 | . 85616 | 12.5 | . 56267 | . 84075 | . 56193 | . 83908 |
| 7.6 | . 57211 | . 85706 | . 57159 | . 85591 | 12.6 | . 56245 | . 81038 | . 56170 | . 83868 |
| 7.7 | . 57198 | . 85685 | . 57144 | . 85566 | 12.7 | . 56223 | . 84001 | . 56147 | . 83828 |
| 7.8 | . 57185 | . 85664 | . 57129 | . 85540 | 12.8 | . 56201 | . 83964 | . 56123 | . 83787 |
| 7.9 | . 57171 | . 85642 | . 57114 | . 85515 | 12.9 | . 56179 | . 83927 | . 56099 | . 83746 |
| 8.0 | . 57158 | . 85620 | . 57100 | . 85490 | 13.0 | . 56157 | . 83890 | . 56075 | . 83705 |
| 8.1 | . 5714 | . 85598 | . 57085 | . 85464 | 13.1 | . 56135 | . 83853 | . 56051 | . 83664 |
| 8.2 | . 57131 | . 85576 | . 57070 | . 85438 | 13.2 | . 56113 | . 83815 | . 56027 | . 83622 |
| 8.3 | . 57117 | . 85554 | . 57054 | . 85411 | 13.3 | . 56090 | . 83777 | . 56002 | . 83579 |
| 8.4 | . 57104 | . 85533 | . 57038 | . 85383 | 13.4 | . 56067 | . 83739 | . 55977 | . 83537 |
| 8.5 | . 57090 | . 85511 | . 57022 | . 85356 | 13.5 | . 56044 | . 83701 | . 55952 | . 83495 |
| 8.6 | . 57076 | . 85489 | . 57007 | . 85329 | 13.6 | . 56021 | . 83662 | . 55927 | . 83452 |
| 8.7 | . 57063 | . 85466 | . 56991 | . 85301 | 13.7 | . 55997 | . 83623 | . 55902 | . 83409 |
| 8.8 | . 57049 | . 8544 | . 56974 | . 855273 | 13.8 | . 55974 | . 83584 | . 555877 |  |
| 8.9 | . 57035 | . 85421 | . 56958 | . 85245 | 13.9 | . 55950 | . 83545 | . 55852 | . 83323 |
| 9.0 | . 57021 | . 85398 | . 56941 | . 85217 | 14.0 | . 55926 | . 83506 | . 55827 | . 83280 |
| 9.1 | . 57007 | . 85375 | . 56924 | . 85188 | 14.1 | .55903 | . 83467 | . 55802 | . 83237 |
| 9.2 | . 56993 | . 85352 | . 56907 | . 85159 | 14.2 | . 558880 | . 83428 | . 55776 | . 83193 |
| 9.3 | . 56978 | . 85329 | . 56890 | . 85130 | 14.3 | . 55856 | . 83388 | . 55750 | . 83149 |
| 9.4 | . 56964 | . 85305 | . 56873 | . 85100 | 14.4 | . 55831 | . 83347 | . 55724 | . 83105 |
| 9.5 | . 56949 | . 85282 | . 56856 | . 85070 | 14.5 | . 55807 | . 83307 | . 55698 | . 83060 |
| 9.6 | . 56935 | . 85258 | . 56838 | . 85040 | 14.6 | . 55782 | . 83266 | . 55671 | . 83014 |
| 9.7 | . 56920 | . 85235 | . 56820 | . 85010 | 14.7 | . 55757 | . 83225 | . 55645 | . 82969 |
| 9.8 | . 56905 | . 85211 | . 56803 | . 84980 | 14.8 | . 55733 | . 83185 | . 55618 | . 82923 |
| 9.9 | . 56890 | . 85187 | . 56785 | .84949 | 14.9 | . 55709 | . 83145 | . 55590 | . 82877 |
| 10.0 | . 56875 | . 85163 | . 56767 | . 84918 | 15.0 | . 55684 | . 83104 | . 55563 | . 82831 |

Table A4.4. Best wire diameters and constants for large lead angles, 1 -in axial pitch $60^{\circ}$ threads-Continued

| Lead angle, $\lambda$ | 3 -start threads |  | 4-start threads |  | Lead angle, $\lambda$ | 3-start threads |  | 4-start threads |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $w_{1}$ | $(C+c)_{1}$ | $w_{1}$ | $(C+c)_{1}$ |  | $w_{1}$ | $(C+c)_{1}$ | $w_{1}$ | $(C+c)_{1}$ |
| 1 | 6 | 7 | 8 | 9 | 1 | 6 | 7 | 8 | 9 |
| deg | in | in 0305 | in | in | deg |  |  |  |  |
| 13.0 | . 56075 | . 83705 | . 56033 | . 83609 | 18.0 | . 54682 | . 81344 | . 54579 | . 81109 |
| 13.1 | . 56051 | . 83664 | . 56008 | 83566 | 18.1 | . 54651 | . 81291 | . 54546 | . 81053 |
| 13.2 | . 56027 | . 83622 | . 55982 | . 83522 | 18.2 | . 54619 | . 81238 | . 54513 | . 80997 |
| 13.3 | . 56002 | . 835379 | . 559556 | . 83477 | 18.3 | . 54588 | . 81185 | . 54480 | . 80940 |
| 13.4 | . 55977 | . 83537 | . 55931 | . 83433 | 18.4 | . 54556 | . 81132 | . 54447 | . 80883 |
| 13.5 | . 55952 | . 83495 | . 55905 | . 83388 | 18.5 | . 54524 | . 81078 | . 54414 | . 80826 |
| 13.6 | . 55927 | . 83452 | . 55879 | . 83342 | 18.6 | . 54492 | . 81024 | . 54380 | . 80768 |
| 13.7 | . 55902 | . 83409 | . 55853 | . 83297 | 18.7 | . 54459 | . 80970 | . 54345 | . 80710 |
| 13.8 13.9 | . 555877 | .83366 .83323 | .55827 .55800 | .83252 .83207 | 18.8 18.9 | .54427 .54394 | .80916 .80861 | $\xrightarrow{.54311}$ | .80652 .80594 |
| 13.9 | . 5582 | . 83323 | . 55800 | . 83207 | 18.9 | . 54394 | . 80861 | . 54277 | . 80594 |
| 14.0 | . 55827 | . 83280 | . 55774 | . 83161 | 19.0 | . 54361 | . 80805 | . 54242 | . 80535 |
| 14.1 | . 55802 | . 83237 | . 555747 | . 83115 | 19.1 | . 54328 | . 80749 | . 54208 | . 80477 |
| 14.2 | . 55776 | . 83193 | . 55720 | . 83068 | 19.2 | . 51295 | . 80694 | . 54173 | . 80418 |
| 14.3 | . 55750 | . 83149 | . 55693 | . 83022 | 19.3 | . 54261 | . 80638 | . 54138 | . 80358 |
| 14.4 | . 55724 | . 83105 | . 55666 | . 82975 | 19.4 | . 54227 | . 80582 | . 54103 | . 80298 |
| 14.5 | . 55698 | . 83060 | . 55639 | . 82928 | 19.5 | . 54193 | . 80526 | . 54067 | . 80238 |
| 14.6 | . 55671 | . 83014 | . 55611 | . 82880 | 19.6 | . 54160 | . 80470 | . 54032 | . 80178 |
| 14.7 | . 55645 | . 82969 | . 55583 | . 82831 | 19.7 | . 54126 | . 80414 | . 53997 | . 80118 |
| 14.8 | . 55618 | . 82923 | . 55555 | . 82783 | 19.8 | . 54092 | . 80358 | . 53961 | . 80057 |
| 14.9 | . 55590 | . 82877 | . 55527 | . 82735 | 19.9 | . 54058 | . 80301 | . 53925 | . 79997 |
| 15.0 | . 55563 | . 82831 | . 55499 | . 82687 | 20.0 | . 54025 | . 80245 | . 53889 |  |
| 15.1 | . 55536 | . 82784 | . 55471 | . 82638 | 20.1 |  |  | . 53852 | . 79874 |
| 15.2 | . 55509 | . 82737 | . 55442 | . 82589 | 20.2 |  |  | . 53816 | . 79812 |
| 15.3 | . 55481 | . 82690 | . 55414 | . 82540 | 20.3 |  |  | . 53779 | . 79750 |
| 15.4 | . 55453 | . 82643 | . 55385 | . 82490 | 20.4 |  |  | . 53743 | . 79689 |
| 15.5 | . 55425 | . 82596 | . 55356 | . 82440 | 20.5 |  |  | . 53706 | . 79627 |
| 15.6 | . 55397 | . 82549 | . 55327 | . 82390 | 20.6 | - |  | . 53669 | . 79564 |
| 15.7 | . 55369 | . 82501 | . 55297 | . 82339 | 20.7 | ---- |  | . 53632 | . 79502 |
|  | . 55340 | . 82453 | . 55268 | . 82289 | 20.8 |  |  | . 53595 | . 79440 |
| 15.9 | . 55312 | . 82405 | . 55239 | . 82238 | 20.9 |  |  | . 53558 | . 79377 |
| 16.0 | . 55283 | . 82356 | . 55209 | . 82187 | 21.0 |  |  | . 53521 | 79314 |
| 16.1 | . 55254 | . 82307 | . 55179 | . 82135 | 21.1 | ------- | ------- | . 53484 | . 79251 |
| 16.2 | . 55225 | . 82258 | . 55148 | . 82083 | 21.2 |  |  | . 53446 | . 79187 |
| 16.3 | . 55196 | . 82209 | . 55117 | . 82031 | 21.3 |  |  | . 53408 | . 79123 |
| 16.4 | . 55167 | . 82160 | . 55087 | . 81979 | 21.4 | ---- |  | . 53370 | . 79059 |
| 16.5 | . 55138 | . 82110 | . 55057 | . 81926 | 21.5 |  |  | . 53332 | . 78994 |
| 16.6 | . 55109 | . 82061 | . 55026 | . 81873 | 21.6 |  |  | . 53294 | . 78930 |
| 16.7 | . 55079 | . 82011 | . 54995 | . 81821 | 21.7 |  |  | . 53255 | . 78865 |
| 16.8 | . 55050 | . 81962 | . 54964 | . 81768 | 21.8 |  |  | . 53217 | . 78801 |
| 16.9 | . 55020 | . 81912 | . 54933 | . 81715 | 21.9 | ----- | --- | . 53178 | . 78736 |
| 17.0 | . 54990 | . 81862 | . 54902 | . 81661 | 22.0 |  |  | . 53139 | . 78670 |
| 17.1 | . 54960 | . 81811 | . 54870 | . 81607 | 22.1 |  |  | . 53100 | . 78604 |
| 17.2 | . 54929 | . 81759 | . 54839 | . 81552 | 22.2 | - |  | . 53061 | . 78539 |
| 17.3 | . 54898 | . 81707 | . 54807 | . 814147 | 22.3 |  |  | . 53022 | .78473 .78406 |
| 17.4 | . 54867 | . 81655 | . 54774 | . 81442 | 22.4 |  |  | . 52983 | . 78406 |
| 17.5 | . 54837 | . 81604 | . 54742 | . 81387 | 22.5 |  |  | . 52943 | . 78339 |
| 17.6 | . 54806 | . 81552 | . 51710 | . 81333 | 22.6 |  |  | . 52903 | . 78272 |
| 17.7 | . 54775 | . 81500 | . 54677 | . 81277 | 22.7 |  |  | . 52863 | . 78205 |
| 17.8 | . 54744 | . 81448 | . 54645 | . 81222 | 22.8 |  |  | . 52823 | . 78138 |
| 17.9 | . 54713 | . 81396 | . 54612 | . 81166 | 22.9 |  |  | . 52783 | . 78071 |
| 18.0 | . 54682 | . 81344 | . 54579 | . 81109 | 23.0 | ----- | - | . 52743 | . 78004 |

Note.-This table courtesy of the Van Keuren Co.


Pigure A4.5. Measurement of pitch diameter of taper threal gages by the 2-wire method.

## 6. MEASUREMENT OF PITCH DIAMETER OF USA STANDARD TAPER THREADS

The pitch diameter of a taper thread plug gage is measured in much the same manner as that of a straight thread gage, except that a definite position at which the measurement is to be made must be located. A point at a known distance, $L$, from the reference end of the gage is located by means of a combination of precision gage blocks and the cone point furnished as an accessory with these blocks, as shown in the inset in figure A4.5. The gage is set vertically on a surface plate, the cone point is placed with its axis horizontal at the desired height, and the plug is turned until the point fits accurately into the thread. The position of this point is marked carefully with a pencil or a bit of prussian blue.
6.1. Two-Wire Method.-Assuming that the measurement is to be made with a horizontal comparator, the gage is set in the comparator with its axis vertical, that is, the line of measurement and the thread axis are perpendicular to each other. The measurement is made with two wires, as shown in figure A4.5, one of which is placed in the thread to make contact at the same axial section of the thread as was touched by the cone point. This wire is designated the fixed wire. The second wire is placed in the thread groove, on the opposite side of
the gage, which is next above the fixed wire, and the measurement over the wires is made. The second wire is then placed in the thread groove next below the fixed wire, and a second measurement is made. The average of these two measurements is $M_{w}$, the measurement over the wires at the position of the fixed wire.

The general formula for a taper thread, corresponding to formula (3) is

$$
\begin{align*}
E=M_{w}+ & \frac{\cot \alpha-\tan ^{2} \beta \tan \alpha}{2 n} \\
& -w\left(1+\operatorname{cosec} \alpha+\frac{\tan ^{2} \lambda^{\prime} \cos \alpha \cot \alpha}{2}\right) \tag{6}
\end{align*}
$$

in which

$$
\begin{aligned}
E & =\text { pitch diameter } \\
M_{w} & =\text { measurement over wires } \\
\beta & =\text { half angle of taper of thread } \\
n & =\text { number of threads per inch }=1 / p \\
\alpha & =\text { half angle of thread } \\
w & =\text { mean diameter of wires } \\
\lambda^{\prime} & =\text { wire angle. }
\end{aligned}
$$

The term

$$
\frac{\cot \alpha-\tan ^{2} \beta \tan \alpha}{2 n}
$$

is the exact value of the depth of the fundamental triangle of a taper thread, which is less than that of the same-pitch thread cut on a cylinder. For steeptapered thread gages, having an included taper larger than $0.75 \mathrm{in} / \mathrm{ft}$ this more accurate term should be applied. For such a thread, which has a small lead angle, formula (6) takes the form

$$
\begin{equation*}
E=M_{w}+\frac{\cot \alpha-\tan ^{2} \beta \tan \alpha}{2 n}-w(1+\operatorname{cosec} \alpha) \tag{7}
\end{equation*}
$$

Otherwise, as for USA Standard taper pipe threads having an included taper of $0.75 \mathrm{in} / \mathrm{ft}$, the simplified formula (5)

$$
E=M_{w}+\frac{0.86603}{n}-3 w
$$

for $60^{\circ}$ threads may be used. This simplified formula gives a value of $E$ that is 0.00005 in larger than
that given by the above general formula (6) for the 2.5-8 USA Standard taper pipe thread, the worst case in this thread series.

The pitch diameter at any other point along the thread, as at the gaging notch, is obtained by multiplying the distance parallel to the axis of the thread, between this point and the point at which the measurement was taken, by the taper per inch, then adding the product to or subtracting it from the measured pitch diameter according to the direction in which the second point is located with respect to the first.
6.2. Three-Wire Method.-Depending on the measuring facilities available or other circumstances, it is sometimes more convenient to use three wires. In such cases measurement is made in the usual manner, but care must be taken that the measuring contacts touch all three wires, as the line of measurement is not perpendicular to the axis of the screw when there is proper contact. (See fig. A4.6.)

On account of this inclination, the measured distance between the axes of the wires must be multiplied by the secant of the half angle of the taper of


Figure A4.6. Measurement of pitch diameter of taper thread gages by the 3-wire method.
the thread. The formula for the pitch diameter of any taper thread plug gage, the threads of which are symmetrical with respect to a line perpendicular to the axis, then has the form corresponding to formula (4) :

$$
\begin{equation*}
E=\left(M_{w}-w\right) \sec \beta+\frac{\cot \alpha}{2 n}-w \operatorname{cosec} \alpha \tag{S}
\end{equation*}
$$

in which $\beta=$ half-angle of taper of thread. Thus the pitch diameter of a USA Standard pipe-thread gage having correct angle ( $60^{\circ}$ ) and taper ( $0.75 \mathrm{in} / \mathrm{ft}$ ) is then given by the formula

$$
\begin{equation*}
E=1.00049\left(M_{w}-w\right)+0.86603 p-2 w \tag{9}
\end{equation*}
$$

An adaption of the three-wire method is frequently used to reduce the time required when the pitch diameter of a number of gages of the same size is to be measured. Only light gages, up to about 1 in nominal size, can be measured accurately by this method. The gage is supported on two wires placed several threads apart, which are in turn supported on a taper thread testing fixture. The third wire is placed in the threads at the top of the gage and measurement is made from the top of this wrie to the bottom of the fixture with a vertical comparator having a flat anvil, using a gage block combination as the standard. The fixture consists of a block, the upper surface of which is at an angle to the base plane equal to the nominal angle of taper of the thread, $2 \beta$. Thus the element of the cone at the top of the thread gage is made parallel to the base of the mstrument. The direction of measurement is not perpendicular to the axis of the gage but at an angle, $\beta$, from perpendicularity. A stop is provided at the thick end of the block with respect to which the gage is positioned on the fixture. As the plane of the end of the gage may not be perpendicular to the axis, a roil approximately equal to the diameter of the gage should be inserted between the stop and the gage to assure contact at the axis of the gage. For a given fixture and roll, a constant is computed which, when subtracted from the measured distance from the top of the upper wire to the base plane, gives $M$ corresponding to the pitch diameter, $E_{0}$, at the small end of the gage. $E_{0}$ is then determined by applying formula ( 8 ) or (9).
6.3. Four-Wire Method.-A four-wire method of measurement that yields measurements of the pitch diameter, $E_{0}$, at the small end of the gage, and the half-angle of taper, $\beta$, is also sometimes used. This method is illustrated in figure A4.7 and requires four thread wires of equal diameter, a pair of gage


Figure A4.7. Measurement of pitch diameter of taper thread gages by the 4-wire method.
blocks of equal thickness, and two pairs of rolls of different diameters, the rolls of each pair being equal in diameter. Two measurements, $M_{1}$ and $M_{2}$, are made over the rolls and formulas are applied as follows:

$$
\begin{gather*}
\cot \frac{90-\beta}{2}=\frac{M_{2}-M_{1}+d_{1}-d_{2}}{d_{2}-d_{1}}  \tag{10}\\
M_{v v}=M_{2}-d_{2}\left(1+\cot \frac{90^{\circ}-\beta}{2}\right)-2 g \sec \beta \tag{11}
\end{gather*}
$$

in which

$$
\begin{aligned}
M_{2} & =\text { measurement over larger rolls } \\
M_{1} & =\text { measurement over smaller rolls } \\
d_{2} & =\text { diameter of larger rolls } \\
d_{1} & =\text { diameter of smaller rolls } \\
\beta & =\text { actual half-angle of taper of thread } \\
g & =\text { thickness of each gage block. }
\end{aligned}
$$

To determine $E_{0}$, the pitch diameter at the small end of the gage, $M_{y}$, as determined from formula (11), is substituted in formula (6) or (7).

The errors of measurement by this method may be slightly but not significantly larger than by the other methods described, on account of elastic deformations of the rolls and gage blocks under the measuring force, and differing conditions of loading of the thread wires.

## 7. MEASUREMENT OF PITCH DIAMETER OF THREAD RING GAGES

The application of direct methods of measurement to determine the pitch diameter of thread ring gages presents serious difficulties, particularly in securing proper contact load when a high degree of precision is required. The usual practice is to fit the ring gage to a threaded setting plug. When the thread ring
gage is of correct lead, angle, and thread form, within close limits, this method is satisfactory and represents standard practice in the United States. It is the only method available for small sizes of threads. For the larger sizes, various more or less satisfactory methods have been devised, but none of these have found wide application.

UNITED STATES DEPARTMENT OF COMMERCE NATIONAL BUREAU OF STANDARDS

## HANDBOOK H28

SCREW-THREAD STANDARDS
FOR FEDERAL SERVICES
APPENDIX A5
1969
DESIGN OF SPECIAL THREADS

## 1. GENERAL

In general, any given problem in thread design may be suseeptible to several more or less satisfaetory solutions based on the prelimiuary selection of eertain elements of the design and the proper adjustment of the other elements. In other words, thread design is to a large extent empirical and is partially based on previous experience with similar designs and the judgment of the designer. Accordingly, it is not practieable to present a definite system of approaeh to the design of a threaded assembly but merely to present a diseussion of various design factors.

The interrelation of length of engagement, minimum major diameter of the external thread, maximum minor diameter of the internal thread, and the strength of the assembled thread needs to be understood and carefully eonsidered in order to produce the optimum design of a special thread. It is not economical to use either a length of thread engagement which is longer than required or shorter than that which will develop the full strength of the externally threaded member. Other faetors, such as eontrol of tap breakage, proper seating of a threaded part on a shoulder, the prevention of eross threading, eonditions of loading when the assembled parts are not eoneentric, and possible eollapse of a hollow externally threaded member, require eareful analysis and adjustment of the design with respeet to seleetion of the diameter-pitch combination, the class of thread, length of engagement, and major and minor diameter toleranees.

In redesigning threads from American National to Unified standards, it should be remembered that exact correspondenee between the old and new elass numbers does not exist. For most, but not all,
diameter-pitel eombinations, the combined toleranees and allowanees of the Unified elasses are somewhat larger than American National elasses of eorresponding number. Recommended proeedure is to eonvert the thread to the eorresponding elass of Unified thread, compare the new major, piteh, and minor diameter toleranees with the old toleranees, and then give careful eonsideration to the desirability of the new limits of size.

Taking, for example, the conversion of a class 1 thread to elasses 1A and 1B: Under ordinary eonditions where the thread is being used only as a simple fastener and the length of engagement is normal, sueh substitution may be made. If, for any reason, the previously speeified toleranees may not be exeeeded, it may be necessary to specify elass 2 A or 2 B or both. Also, if the thread must carry a high axial stress or if concentricity of the two mating parts is a faetor, the conversion should be from elass 1 to elasses 2 A and 2 B .

A elose fitting thread assembly under some eonditions may fail, whereas the cause of failure may be eliminated by providing a looser fit. A eap serew that seats only on one side of the bearing surface under the head may break off when the serew is tightened. When a screw has a large bearing surfaee under the head or when the head must be square with a projeeting pin, suffieient piteh diameter clearanee must be provided to allow for any out-ofsquareness of the screw axis with the bearing surface under the head. Thus, as large a piteh diameter tolerance as possible, together with providing proper toleranees on squareness of face with the thread axis where seating is required, may avoid the neeessity for speeifying a heat treated bolt.

## 2. ECCENTRICITY OF ASSEMBLY AND CROSS THREADING

In assembly and use, the combined tolerances and allowanees on both mating parts should not allow threads to disengage on one side when assembly is eecentric. The axis of the internal thread can be displaeed radially from eoineidence with the axis of the external thread by an amount equal to the sum of the piteh diameter toleranees and the allowanee. This radial displaeement may be suffieient so that the flank eontact is entirely on one side and on the opposite side the crest of the external thread will be in line with the erest of the internal thread with the following results when the serew is constrained in such a position in a tapped hole: (1) There will be danger of erossing the threads in starting, and (2) the serew may pull out of the hole when tension is exerted in this constrained position. The minimum amount of overlap is arbitrary and eontroversial, but the following general rule can be used in lieu of more specific data:

As the first step to assure the minimum safe overlap on both sides when the assembly is concentric, the differenee between the minimum major diameter of the external thread and the maximum minor diameter of the internal thread should not be less than twice the addendum of the external thread $(0.75 \mathrm{H}$, table 2.1). Otherwise stated, the sum of the major-diameter tolerance and allowance, if any, of the external thread and the minor-diameter toleranee of the internal thread should not be greater than $4 / 3$ the addendum of the external thread, $0.5 H$, table 2.1. This provides for a minimum of 50 pereent thread engagement. As the seeond step, to assure the minimum safe overlap on one side when the assembly is eeeentrie, the difference between the maximum piteh diameter of the internal thread and the minimum piteh diameter of the external thread should not be greater than twice the addendum of
the external thread $(0.75 \mathrm{H}$, table 2.1). Otherwise stated, the sum of the pitch-diameter tolerances of both threads and the allowance, if any, should not be greater than twice the addendum of the external thread, $(0.75 H$, table 2.1). This provides for an eccentric assembly condition equal to the addendum of external thread $(0.375 \mathrm{H}$, table 2.1) and zero minimum overlap on one side. If the results from the limits of size selected violate the above rules, the tolerances should be reduced by using a closer class of tolerance, assuming tolerances consistent
with manufacturing possibility, or a coarser pitch should be used to increase the amount of overlap. The major-diameter tolerance of the external thread or minor-diameter tolerance of the internal thread should not be less than the pitch-diameter tolerance of the respective thread to maintain thread form.

It should be noted that, if the tolerance on the minor diameter of the internal thread must necessarily be large, the major diameter of the external thread must be held close to the maximum major diameter and vice versa.

## 3. STRENGTH FACTORS

Critical Areas---The critical areas of mating threads, as related to the tensile strength of the thread assembly, are: The effective cross-sectional area, or stress area, of the external thread, (2) the shear area of the external thread that depends principally on the minor diameter of the tapped hole, and (3) the shear area of the internal thread that depends principally on the major diameter of the external thread. The formulas for tensile stress area and thread shear area are shown below. These areas are indicated in figure A5.1.

Tensile Stress Area.--The tensile stress area is the assumed area of an external threaded part that is used for the purpose of computing the tensile strength.

Direct Tensile Stress.--When parts are subjected only to a direct tensile stress the assumed area
applicable to steel parts up to 180,000 psi used in calculating the ultimate strength is computed from the following formula:

$$
A_{s}=3.1416\left(\frac{E}{2}-\frac{3 H}{16}\right)^{2}
$$

or

$$
A_{s}=0.7854(D-0.9743 / n)^{2}
$$

where
$E=$ basic pitch diameter
$D=$ basic major diameter
$n=$ threads per inch
For $3 H / 16$, see table 2.1. Tabulated stress areas are listed in tables 2.8 through 2.18.


Figure Ais.1. Critical sections in a thread assembly.
See table A5.2 for formulas corresponding to item numbers.

Table A5.2. Data for determining strength factors in special thread design

| $D=$ basic major diameter. <br> $D_{s}=$ major diameter of external thread. <br> $K_{n}=$ minor diameter of internal thread. <br> $T_{K n}=$ tolerance on minor diameter of internal thread. <br> $T_{E s}=$ tolerance on pitch diameter of external thread. |  |  |  |  |  | NOTATION |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | $G=$ allowance on all diameters of external thread. <br> $L_{e}=$ length of thread engagement. |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  | $A_{s}=$ stress area of external thread. |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  | $S_{s}=$ area in shear on external thread in line with $K_{n}$. $S_{n}=$ area in shear in internal thread in line with $D n$. |  |  |  |  |  |  |  |  |  |
| CONSTANTS |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $C_{1}=\frac{3}{4} \pi=2.356$ | Threads per inch, $n$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  | 40 | 36 | 32 | 28 | 27 | 24 | 20 | 18 | 16 | 14 | 12 | 10 | 8 | 6 | 4 |
| $C_{2}=\frac{5}{8} \frac{\cot 30^{\circ}}{n}=\frac{1.08253}{n}=\ldots$ | 0.0271 | 0.0301 | 0.0338 | 0.0387 | 0.0401 | 0.0451 | 0.0541 | 0.0601 | 0.0677 | 0.0773 | 0.0902 | 0.1083 | 0.1353 | 0.1804 | 0.02706 |
| $C_{3}=\frac{9}{16} \frac{\cot 30^{\circ}}{n}=\frac{0.974279}{n}=-$ | . 0244 | . 0271 | . 0304 | . 0348 | . 0361 | . 0406 | . 0487 | . 0541 | . 0609 | . 0696 | . 0812 | . 0974 | . 1218 | . 1624 | . 2436 |
| $C_{4}=n \tan 30^{\circ}=0.57735 n=\ldots$ | 23.09 | 20.78 | 18.48 | 16.17 | 15.59 | 13.86 | 11.55 | 10.39 | 9.328 | 8.083 | 6.928 | 5.774 | 4.619 | 3.464 | 2.309 |
| $C_{5}=\pi n \tan 30^{\circ}=1.8138 n \ldots$ | 72.55 | 65.30 | 58.04 | 50.79 | 48.97 | 43.53 | 36.25 | 32.65 | 29.02 | 25.39 | 21.76 | 18.14 | 14.51 | 10.88 | 7.255 |

FORMULAS
1tem

1. $K_{n} \min =D-C_{2}$.
2. Max area in shear of external thread per inch $=S_{y}$ max per inch $=C_{1} K_{n}$ min.
3. Min length of thread engagement, $L_{e} \min =\frac{L_{e}}{D} \times D_{\mathrm{s}} \max$, with $\frac{L_{e}}{D}$ taken from graph, figure A5.3.
4. Area in shear of external thread in length $L_{\varepsilon} \min =S_{s} \max$ per inch $\times L_{\varepsilon} \min (=$ item $2 \times$ item 3 ).
5. Max stress area of external thread $=A_{s} \max =\frac{S_{s} \max \text { per inch } \times L_{c} \min }{2}\left(=\frac{1}{2}\right.$ item 4) $=\frac{C_{1} K_{n} \min \times \frac{L_{c}}{D} \times D_{s} \max }{2}$.
maximum material external thread, $K_{n}$ maximum
6. $K_{n} \max =K_{n} \min +T_{K n}$.
7. Min area in shear of external thread per inch $=S_{s} \min$ per inch $=K_{n} \max \left(C_{1}-C_{5} T_{K n}\right)$.
8. $L_{e}$ required to develop full strength of external thread for $T_{K n}$ selected $=\frac{2 A_{s} \max }{S_{s} \min \text { per inch }}=\left(\frac{2 \times \text { item } 5}{\text { item } 7}\right)$ or $=\left(\frac{\text { item } 4}{\text { item } 7}\right)$.
minimum material for both external and internal threads
9. Min stress area of external thread $=A_{s} \min =0.785 t\left[D-C_{3}-\left(T_{E s}+G\right)\right]^{2}$.
10. Min area in shear of external thread in length $L_{e}=S_{s} \min =K_{n} \max \left[C_{1}-C_{5}\left(T_{K n}+T_{E_{s}}+G\right)\right] L_{e}$ or $=\pi K_{n} \max \left[0.75-C_{4}\left(T_{K n}+T_{E_{s}}+G\right)\right] L_{s}$
11. Min area in shear of internal thread in length $L_{e}=S_{n} \min =\pi D_{s} \min \left[0.875-C_{s}\left(T_{D s}+T_{E_{n}}+G\right)\right] L_{e}$.

$$
\text { Minimem tapped hole, } D_{S} \text { Minimum, when tapped material is weaker than screw material }
$$

12. $R_{1}=\frac{\text { area in shear of screw in length } L_{e}}{\text { area in shear of tapped hole in length } L_{e}}=\left(\frac{\text { item } 4}{\text { item } 11}\right)=\frac{0.75 K_{n} \min }{D_{s} \min \left[0.875-C_{4}\left(T_{D s}+T_{E n}+G\right)\right]}$
13. $R_{2}=\frac{\text { ultimate tensile strength of tapped material }}{\text { ultimate tensile strength of screw material }}$.
14. If $R_{2}<R_{1}$, then $L_{e}$ required $=L_{e}$ for $T_{K n}$ selected $\times \frac{R_{1}}{R_{2}}=\left(\frac{\text { item } 8 \times \text { item } 12}{\text { item } 13}\right)$.

Combined Tensile Stress.-When parts are subject to a direct tensile stress plus a torsional stress due to tightening the nut or bolt head, it is necessary to consider the combined shear and tensile stresses when calculating the strength of the externally threaded part. It is recommended that the combined stresses be computed on the basis of the section at the minimum minor diameter of the external thread. The direct tensile stress is given by the formulas:

$$
\begin{aligned}
& S_{t}=F / A \\
& A_{r}=0.7854\left[\left(K_{s} \min \right)^{2}-d^{2}\right]
\end{aligned}
$$

where
$A_{r}=$ area in sq in at the minimum minor diameter. $F=$ axial load on externally threaded parts in lb.
The direct torsional stress is given by the formulas:

$$
\begin{aligned}
& S_{s}=T_{1} / Z_{p} \\
& Z_{p}=0.1963 \frac{\left[\left(K_{s} \min \right)^{4}-d^{4}\right]}{K_{s} \min }
\end{aligned}
$$

where
$T_{1}=$ wrench torque transmitted through the threaded section, approximately equal to half of the total wrench torque in lb-in.
$Z_{p}=$ polar section modulus in in ${ }^{3}$
$K_{s} \min =$ minimum minor diameter of external thread in in.
$d=$ inside diameter of externally threaded part in in; if part is solid, $d=$ zero.
The combined shear stress in psi is given by the formula:

$$
S_{s}^{\prime}=\sqrt{\left(\frac{S_{t}}{2}\right)^{2}+\left(S_{s}\right)^{2}}
$$

The combined tensile stress in psi is given by the formula:

$$
S_{t}^{\prime}=S_{s}{ }^{\prime}+S_{t} / 2
$$

Having once determined the combined stresses due to a given set of conditions for wrench torque and
coefficient of friction, other combined stresses will be directly proportional to the wrench torque.

Thread Shear Area.-The diameter corresponding to the effective thread shear area will vary with the relative unit tensile strengths of the materials of the internal and external threads. When the external and internal threads are manufactured from materials of equal unit tensile strength, failure will usually take place simultaneously in both threads at or near a diameter equal to the basic pitch diameter. The shear area ( $A S$ ) for external and internal threads made of such materials can be computed from the following formula:

$$
A S=3.1416 E \frac{L_{e}}{2}
$$

where
$E=$ basic pitch diameter
$L_{e}=$ length of engagement at basic pitch diameter.
When the unit tensile strength of the external thread material greatly exceeds that of the internal thread material, as in the case of a threaded hole in a cast aluminum block mated with a 100,000 psi ultimate strength material bolt, the shear area of the internal thread ( $A S_{n}$ ) can be computed from the following formulas:
(1) For simplified calculations that will provide shear areas within about 5 percent of those given by the precise formula shown below, the shear area of the internal thread may be computed as follows:

$$
A S_{n}=3.1416 E \frac{3 L_{e}}{4}
$$

where $L_{e}=$ length of engagement at the basic pitch diameter.
(2) The precise equation for shear area of the internal thread at a diameter equal to the minimum major diameter of the external thread is as follows:
$A S_{n}$

$$
=3.1416 n L_{e} D_{s} \min \left[\frac{1}{2 n}+0.57735\left(D_{s} \min -E_{n} \max \right)\right]
$$

where

$$
\begin{aligned}
n & =\text { number of threads per inch } \\
D_{s} \min & =\underset{\text { thinimum }}{\text { minead }} \text { major diameter of external } \\
E_{n} \max & =\underset{\text { thread }}{\text { maximum }} \text { pitch diameter of internal }
\end{aligned}
$$

$L_{\epsilon}=$ length of engagement at minimum major diameter of external thread. (Use $L_{e}$ at basic pitch diameter for simplicity; this is conservative.)

When the unit tensile strength of the internal thread material greatly exceeds that of the external thread material, the shear area of the external thread $\left(A S_{s}\right)$ can be computed from the following formulas:
(1) For simplified calculations for diameters 0.250
in and larger, that will provide shear areas within about 5 percent of those given by the precise formula shown below, the shear area of the external thread may be computed as follows:

$$
A S_{s}=3.1416 E \frac{5 L_{e}}{5}
$$

where $L_{e}=$ length of engagement at the basic pitch diameter.
(2) The precise equation for shear area of the external thread at a diameter equal to the maximum minor diameter of the internal thread is as follows:
$A S_{s}$
$=3.1416 n L_{e} K_{n} \max \left[\frac{1}{2 n}+0.57735\left(E_{s} \min -K_{n} \max \right)\right]$
where
$K_{n} \max =$ maximum minor diameter of internal thread.
$E_{s} \min =$ minimum pitch diameter of external thread.

If failure of a thread assembly should occur it is desirable that the external thread (screw) will break rather than that either the external or internal thread will strip. In other words, the length of thread engagement shall be sufficient to develop the full strength of the screw. Thus, the length of internal thread and the dimensions of this thread, particularly its minor diameter, should be such that, taking into account a possible difference in strength of material of the internal and external threads, the threaded portion of the external thread will break before either the external or internal threads strip.

Length of Thread Engagement-The length of engagement of a threaded unit that will develop maximum strength of an assembly threaded with external and internal threads manufactured from materials of near or equal unit tensile strength may be computed from the following formula, which incorporates the factor "half"' relation of unit shearing strength to unit tensile strength:

$$
L_{e}=4 A_{s} / 3.1416 E
$$

where

$$
A_{s}=3.1416\left(\frac{E}{2}-\frac{3 H}{16}\right)^{2}
$$

When the unit tensile strength of the external thread materially exceeds that of the internal thread, the required length of engagement to develop maximum strength may be computed from the following formula, which is also based on the shear area being twice the tensile stress area:


Likewise, when the unit tensile strength of the internal thread materially exeeeds that of the external thread, the following formula should be used:

$$
L_{e}=\frac{2 A_{s}}{3.1416 n K_{n} \max \left[\frac{1}{2 n}+0.57735\left(E_{s} \min -K_{n} \max \right)\right]}
$$

The faetor 2 used in the numerator of this formula means that it is assumed that the area in shear must be twiee the tensile stress area to develop the full strength of the serew. This assumption is based on experiments made by the National Bureau of Standards in 1929, in whieh it was found that for hot-rolled and eold-rolled steel, and brass serews and nuts, this faetor varied from 1.7 to 2.0 . Taking the faetor as 2 provides in general a small faetor of safety against stripping of the threads.

To facilitate the applieation of this formula various notations, constants, and formulas applieable to the determination of the relation of eritieal areas to thread dimensions are given in table A5.2 and are diseussed below.
(a) Length of engagement determined by shear area of external thread.-Formula S, table A5.2, gives the length of engagement required to develop the full strength of the serew when the strength of the material in which the hole is tapped is the same as, or slightly less than, the strength of the material of the serew. The value of $L_{e}$ thus obtained is suffieient for a permanently-fastened connection. If, however, the serew is an adjusting or lead serew, or if the eonneetion will be frequently unserewed, $L_{e}$ should be inereased to allow for the expeeted wear on the flanks of the threads during the useful life of the components.

For tapped holes in sheet metal, the maximum size of the serew to be speeified should be such that the thiekness of sheet equals the $L_{e}$ required to develop full strength. In order to use the largest possible serew, it is neeessary that the tolerance, $T_{K n}$, on the minor diameter of the hole should be the practieal minimum. If it should prove to be impraetieable to reduce the minor diameter tolerance to such a value, it may be neeessary to deerease the minimum minor diameter of the internal thread and to inerease the minor diameter tolerance by the same amount. If this is done, the maximum minor diameter of the serew must be redueed by the same amount to prevent interferenee, and the minor diameter of the "go" thread ring gage must likewise be deereased, as this is the only eontrol of the minor diameter of the serew. In all sueh eases, where dimensions are altered from those ealeulated aeeording to the standard, the threads should be designated as speeified in seetion?. (See under "Designating threads having modified erests" in that seetion.)
(b) Length of engagement determined by shear area of internal thread.-The ratio of the area in shear in the serew and the area in shear in the tapped hole is given by formula 12, table A5.2. This ratio, $R_{1}$, will usually be less than 1 and the strength of the material of the tapped hole ean be less than the strength of the material of the serew by this ratio with no indieated inerease in $L_{e}$ by formula S. If, however, the ratio

$$
R_{2}=\frac{\text { ultimate tensile strength of tapped material }}{\text { ultimate tensile strength of serew material }}
$$

is less than $R_{1}$, then $L_{e}$ should be multiplied by $R_{1} / R_{2}$ to provide sufficient length of thread to prevent stripping of the threads in the tapped hole.

For retaining eollars on shafts where the expeeted axial foree resisted by the eollar is appreeiably less than the tensile foree that the shaft itself is eapable of resisting, $L_{e}$ need only be long enough to withstand the expeeted axial foree on the collar. If $F_{c}$ is the axial foree to be earried by the collar and uts is the tensile strength of the material of the shaft in pounds per square ineh, then the length of thread engagement required on the shaft is equal to $2 F_{c} /$ (uts $\times S_{s} \mathrm{~min}$ ), where $S_{s}$ min is given by formula 7 , when the strength of material of the eollar is the same or slightly less than the strength of material of the shaft. Ratios $R_{1}$ and $R_{2}$ should be eomputed as previously explained to determine whether or not a greater length is required to prevent stripping of the threads in the eollar.
(c) Hollow externally threaded parts.-For serews with through axial holes, the length of engagement required is of eourse less than if the serew is solid. For this eondition, formula : beeomes

$$
L_{c} \max =\frac{2\left(A_{s} \max -A_{n} \max \right)}{S_{s} \text { min per ineh }}
$$

where $A_{n}$ is the eross-sectional area of the hole.
However, as the wall thiekness of either or both the internal and external members beeomes thin, the tendeney of the external member to enlarge and the internal member to neek down in the thread means that an $L_{e}$ greater than given by the above formula must be used, also that the toleranees on minor diameter of the internal thread and major diameter of the external thread, $T_{K n}$ and $T_{D s}$, must be small to obtain the maximum praetieable depth of thread engagement. For eomponents having threads on thin-wall tubing, tests under aetual working eonditions should be made to determine proper seleetion of wall thicknesses, length of engagement, and piteh of thread.

## 4. THREAD PROPORTIONS IN RELATION TO TAPPING

In the production of threads it is considered impractical to tap a thread unless its diameter is greater than six times the basic thread height; therefore, when the ratio of $D$ to $H$ is less than 4.5 , the use of a larger diameter, a finer pitch of thread, or both, should be considered.

The size of $K_{n}$ is a factor in controlling tap
breakage. Tap breakage is infrequent if the diameter of the tap is over 0.5 in or if the length of thread to be tapped is less than $0.5 D$. For sizes less than 0.5 in and length of thread over $0.5 D$, tap breakage can be minimized by use of a large $K_{n}$, that is $T_{K n}$ maximum. However, this means that $L_{e}$ may have to be increased to develop the full strength of the screw.

## 5. EXAMPLES OF THREAD DESIGN

The design of special threads for particular purposes is illustrated by the following examples:

Example: A gun barrel is subjected to an internal explosive pressure that produces a tensile stress in the threaded end. The length of engagement of the threads should be sufficient to produce a minimum area in shear on the threads of the screw in line with the minor diameter of the tapped hole threads equal to twice the maximum stress area of the threaded portion of the barrel.

Assume that the thread on the barrel is $1.500-$ SUN-2A and the minimum internal diameter of the barrel at the threaded end is 0.792 in .

In table 2.21 will be found the following maximum dimensions of the external thread:

$$
\begin{aligned}
& D_{s} \max =1.497 \mathrm{Sin} \\
& E_{s} \max =1.4166 \mathrm{in} \\
& K_{s} \max =1.3444 \mathrm{in} .
\end{aligned}
$$

From table 2.21, $K_{n} \min =1.365 \mathrm{in}$. If we select the tolerance for minor diameter of hole $T_{K n}=0.0250$ in, $K_{n}$ max will equal $1.365+0.025=1.390$, which will permit the use of a 1.375 in tap drill.

The minimum area in shear per inch can be computed, using formula 7, table A5.2:

$$
\begin{aligned}
S_{s} \min & =K_{n} \max \left(C_{1}-C_{5} T_{K n}\right) \\
& =1.390(2.356-14.51 \times 0.025) \\
& =2.7706 \mathrm{in}^{2}
\end{aligned}
$$

The maximum stress area of the external thread, if solid, using formula 5 , table A5.2, is

$$
\begin{aligned}
A_{s} \max = & 0.5\left(C_{1} K_{n} \min \times \frac{L_{e}}{D} \times D_{s} \max \right) \\
& \frac{L_{e}}{D} \text { from chart, fig. A } 5.3=0.6185 \\
= & 0.5(2.356 \times 1.365 \times 0.6185 \times 1.4978) \\
= & 1.4896
\end{aligned}
$$

Area of minimum center hole

$$
=(\pi / 4) \times 0.792^{2}=0.4926
$$

Max stress area of external threaded member

$$
1.4896-0.4926=0.9970
$$

Length of thread engagement required

$$
\begin{aligned}
=L_{e} & =\frac{2 \times \max A_{s}}{S_{s} \min } \\
& =\frac{2 \times 0.997}{2.7706} \\
& =0.7197 \mathrm{in} .
\end{aligned}
$$

If a length of engagement of 0.72 in cannot be obtained, the tolerance on minor diameter, $T_{K n}$, of the internal thread should be reduced. If a space for a longer length of engagement is available, $T_{K n}$ can be increased.

Example: The dimension is required of the largest steel cap screw that can be used to hold a bracket on a cast iron body. The tensile strength of the steel is $60,000 \mathrm{psi}$, the tensile strength of the cast iron $20,000 \mathrm{psi}$, and the thickness of the cast iron is such that the length of thread engagement cannot exceed 1.750 in . The screws on the top side of the bracket will be in tension. From the ratio of the tensile strengths of the two materials, $R_{2}=$ $20,000 / 60,000=0.333$, it is evident that the length of the tapped hole thread must be considerably longer than the length of thread engagement required to develop the full strength of the screw. $R_{1}$ will be of the order of 0.85 and the length of thread in the tapped hole will be approximately $R_{1} / R_{2}=0.85 / 0.333=2.55$ times as long as the length required to develop the full strength of the screw. $L_{e}$ required to develop the full strength of the screw must be of the order of $1.750 / 2.55=0.686 \mathrm{in}$.

Inasmuch as the hole is tapped in cast iron, a relatively coarse thread would be required, that is UNC or coarser. For such threads $L_{e} / D$, as shown on the chart, figure A5.3, varies between 0.57 and 0.61. Taking $L_{e} / D=0.59$, the approximate diameter required is $0.686 / 0.59=1.163$. Try $D=11 / 16=1.0625$ in. The selected pitch could be either 10 or 8 threads per inch with 8 threads per inch preferred. For a bracket screw, class 2 A would be the preferred class.


Thus, the screw is $1.0625-8 \mathrm{UN}-2 \mathrm{~A}$ and the hole $1.0625-$ SUN-2B.

Next, read the dimensions of the screw and hole from table 2.21 to determine whether or not the above selection is correct.
\ax major diameter of screw, $D_{s} \max =1.0605$
Xin major diameter of screw, $D_{s} \mathrm{~min}=1.0455$
Nin minor diameter of tapped hole, $K_{n} \mathrm{~min}=0.927$
The number of $1.0625-8$ screws required will depend on the torque that may develop on the bracket that will produce tension in the screws. It should be possible to tighten these screws to the yield strength of the steel without stripping the cast iron threads.

The complete table of dimensions of the tapped hole and screw is (From table 2.21)

Internal thread, 1.0625-SUN-2B
ITin major diameter $=1.0625$
Min pitch diameter $=0.9813$
Max pitch diameter $=0.9902$
Min minor diameter $=0.927$
Max minor diameter $=0.952$

External thread, 1.0625-8UN-2A
Max major diameter $=1.0605$
Min major diameter $=1.0455$
Max pitch diameter $=0.9793$
Min pitch diameter $=0.9725$
Max minor diameter $=0.9071$
$L_{e} / D$ from chart, figure A5.3 $=0.5990$
$L_{e} \min =L_{e} / D \times D_{s} \max =0.5990 \times 1.0605=0.6352$
$T_{E_{n}}($ table 2.21 $)=0.0089$
$R_{1}$, table A5.2, formula 12

$$
\begin{aligned}
& =\frac{0.75 K_{n} \min }{D_{s} \min \left[0.575-C_{4}\left(T_{E_{n}}+T_{D_{s}}+G\right)\right]} \\
& =\frac{0.75 \times 0.927}{1.0455[0.575-4.619(0.0089+0.0150+0.0020)]} \\
& =0.8803
\end{aligned}
$$

$L_{e}$ required in hole

$$
=L_{e} \min \times \frac{R_{1}}{R_{2}}=0.6352 \times 0.8803 / 0.3333=1.6777 \mathrm{in},
$$

which is less than the $L_{e}$ ( 1.750 in .) permitted.

# UNITED STATES DEPARTMENT OF COMMERCE NATIONAL BUREAU OF STANDARDS <br> HANDBOOK H28 <br> SCREW-THREAD STANDARDS <br> FOR FEDERAL SERVICES 

## APPENDIX 6 1957 <br> REFERENCES

appendix 6 IS being deleted from the 1969 Issue of handbook h2


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[^0]:    ; Headquarters and Laboratories at Gaithersburg, Maryland, unless otherwise noted; mailing address Washington, D.C. 20234.
    ${ }^{2}$ Located at Boulder. Colorado 80302.
    ${ }^{3}$ Located at 5285 Port Royal Road, Springfield, Virginia 22151.

[^1]:    NOTE: Threads produced employing a cam actuated single tool process (frequently referred to as the Cridan process) or by a process employing similar type equipment, may have fully formed roots which run out on a vanish cone which is formed by the tool withdrawal pattern.

[^2]:    NOTE: When the crest of a thread is truncated beyond the pitch line, the pitch diameter, pitch cylinder, or pitch cone would be based on a theoretical extension of the thread flanks.

[^3]:    Note: Also called the Virtual Diameter, Effective Size, or Virtual Effective Diameter.

[^4]:    ${ }^{\text {a }}$ This series superseded by UN series.

[^5]:    ${ }^{\text {a }}$ For sizes larger than 1.5 inch, use the 12 -thread series. See tabie 2.14
    ${ }^{6}$ Desiga form. See fig. 2.3.
    ${ }^{0}$ See formula under definition of tensile stress area in appendix A5.

[^6]:    ${ }^{\text {a }}$ These are standard sizes of the UNC series.
    ${ }^{\mathrm{b}}$ Design form. See fig. 2.3.
    ${ }^{\text {e }}$ See formula under definition of tensile stress area in appendix A5.

[^7]:    ${ }^{\text {a }}$ These are standard sizes of the UNC or UNF Series.
    ${ }^{b}$ Design form. See fig. 2.3.
    c See formula under definition of tensile stress area in appendix A5.

[^8]:    ${ }^{\text {a }}$ These are standard sizes of the UNC. UNF, or UNEF series.
    b Design form. See fig. 2.3.

    - See formula under definition of tensile stress area in appendix A5.

[^9]:    ${ }^{1}$ The maximum allowance at the maximum material condition of six times the minimum coating thickness is derived by dividing the deposit on the flank of the thread by the sine of the 30 degree half angle and multiplying the result by two for the diameter equivalent, then adding 50 percent for the plater's tolerance. The minimum allowance at the minimum material condition of four times the minimum coating thickness ance at the mimimum material condition of four times the mimimum coating thickness is two-thirds the maximum allowance, inasmuch as the thekness of coating will bring
    the limits of size within standard limits with the additional allowance for the plater's the limits of size within standard limits with the additional allowance for the plater tolerance omitted.

[^10]:    ${ }^{2}$ Threads accepted to class $2 A$ limits before coating are accepted after coating by basic size thread gages. The allowance given in the dimensional tables for class 2 A threads is sufficient to allow for a limited amount of coating as described in par. 9 . Coated threads, p. 2.22 , but if a greater coating thickness is required, it will be necessary to calculate the before coating limits in accordance with that paragraph.

[^11]:    See footnotes at end of table.

[^12]:    ${ }^{\text {a }}$ Regarding combinations of thread classes, see under Thread classes in section 2.
    b For class 2 A threads having an additive finish the maximum is increased to the basic size. See under Classes 2A and 2B threads, and Coated threads in section 2 .

    - See figures 2.3,2.4, and 2.5.
    ${ }^{\mathrm{d}}$ The $1.000-14$ size was formerly NF. The tolerances and allowances for this size are based on one diameter length of engagement.

[^13]:    ${ }^{\text {a }}$ Tolerances for lengths of engagement in terms of pitch should be selected from equivalent lengths of engagement in terms of diameter ranges.

[^14]:    a Tolerances for lengths of engagement in terms of pitch should be selected from equivalent lengths of engagement in terms of diameter ranges.
    b If the minor-diameter tolerance as selected from the table is less than pitch-diameter tolerance, use the latter. See Design of Special Threads in appendix A5.

    - For 0.151 in diam sizes and smaller, tolerance values for all three classes are the same. For these smaller sizes, tolerance values are given in table 3.9.

[^15]:    See previous page for footnotes.

[^16]:    1"HI" and "LO" gages were previously shown in 1128 as "Not go" gages.

[^17]:    *NOTE: It has been customary in the past to specify tolerances on lead as plus or minus ( $\pm$ ) values. Under the requirement established above, the width of the tolerance zone is the nominal tolerance value specified regardless of sign. In view of the preceding, the tolerance symbols, plus or minus, $( \pm)$, should be omitted in referencing lead tolerances. The omission of the plus and minus does not change the total tolerance.

[^18]:    ${ }^{\text {a }}$ Allowable variation in lead between any 2 threads not farther apart than the length of the standard gage, shown in CS8 or B47.1.
    It has been customary in the past to specify tolerances on lead as plus or minus ( $\pm$ ) values. Under the requirement established above, the width of the toleranee zone is the nominal tolerance valuc spccified regardless of sign. In view of the preeeding, the tolerance symbols, plus or minus ( $\pm$ ), should be ramoved in refercncing lead toleranees. The omission of the plus and minus does not change the total tolerance.
    ${ }^{\text {b }}$ A bove 12 inehes the tolerance is dircctly proportional to the toleranec in column 12, in the ratio of the diameter to 12 inches.

[^19]:    ${ }^{2}$ External and internal threads larger than 6 in nominal diameter present additional problems for technical and economical reasons. It is recommended that acceptance of these be alternatively based on measurement of the thread elements. A clear understanding of requirements and method of gaging should be reached between supplier and consumer.

[^20]:    ${ }^{3}$ The values obtained by the use of gaging elements shown above (Types d, $f, g$, and i) may be used to determine deviations from the size of respective setting plugs and may, through calculation, yield pitch diameter of the product threads.
    " "Cone" signifies a single contact design which engages the product thread groove and complete reference must also state profile of contact. "Vee" signifies a double contact design which engages the product thread ridge and complete reference must also state profile of contact.

[^21]:    ${ }_{2}^{1}$ Dimensions given for the maximum minor diameter of the external thread are figured to the intersection of the worn tool arc with a center line through crest and root. The minimum minor diameter of the external thread shall be that corresponding to a flat at the minor diameter of the minimum external thread equal to $1 / 8 \times p$, and may be determined by subtracting the basic thread depth, $h$ (or $0.6495 p$ ), from the minimum pitch diameter of the external thread.
    2 Dimensions for the minimum major diameter of the internal thread correspond to the basic flat ( $1 / 8 \times p$ ) and the profile at the major diameter produced by a worn tool must not fall below the basic outline. The maximum major diameter of the internal thread shall be that corresponding to a flat at the major diameter of the maximum internal thread equal to $1 / 24 \times p$, and may be determined by adding $11 h / 9$ (or $0.7939 p$ ) to the maximum pitch diameter of the internal thread.
    ${ }^{3}$ These dimensions are the maximum material or "go" size and are those which should be placed on the component drawing with the tolerances.

[^22]:    See footnotes at end of table.

[^23]:    See footnotes at end of table.

[^24]:    See footnotes at end of table

[^25]:    
    
    
    
     ${ }^{\circ}$ Based on a length of engagement equal to the nominal diameter．

[^26]:    ${ }^{\text {a }}$ These wire sizes are based on zero lead angle. Also maximum and minimum sizes are based on a width of flat at the crest equal to $0.125 p$. The width of flat of USA Standard pipe thread gages is slightly less than this, so that the minimum size listed is slightly too small for such gages. In any case the use of wires of either extreme size is to be avoided.

