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U. S. DEPARTMENT OF COMMERCE HARRY L. HOPKINS, Secretary NATIONAL BUREAU OF STANDARDS LYMAN J. BRIGGS, Director

NATIONAL BUREAU OF STANDARDS HANDBOOK H25

# SCREW-THREAD STANDARDS FOR FEDERAL SERVICES 1939

# (Superseding the Reports of the National Screw Thread Commission)



UNITED STATES GOVERNMENT PRINTING OFFICE WASHINGTON : 1940

#### FOREWORD

The Interdepartmental Screw Thread Committee has been established by the Departments of War, Navy, and Commerce to promote uniformity in screw-thread standards in the Departments concerned.

The Committee is charged: (1) With the development of standards for screw threads; (2) the standardization of gages, dies, and taps; and (3) the standardization of dimensions of nuts, bolt heads, wrenches and other items associated with the manufacture and use of interchangeable threaded parts. Standards developed by the Committee, when approved by the Departments concerned, are to be published together with a joint order making their use mandatory in the Departments of War, Navy, and Commerce, except where a need for deviations therefrom is shown. Standards thus established are subject to such extension and revision as the Committee may find desirable.

To meet the immediate needs of the Federal Services, the Committee has adopted and is republishing the screw-thread standards as established by the National Screw Thread Commission (save for minor corrections and editorial changes). These standards have been approved by the Departments concerned and are now in full force and effect.

Certain additions to and revisions of these standards are now under consideration by the Committee, working in cooperation with a liaison committee of the American Standards Association.

LYMAN J. BRIGGS, Chairman.

II

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#### APPROVAL BY THE SECRETARIES OF WAR, NAVY, AND COMMERCE

The accompanying report on screw-thread standards for Federal services, as approved on November 9, 1939, by the Interdepartmental Screw Thread Committee, is hereby approved, and the use of these standards by the Departments of War, Navy, and Commerce, except where a need for deviation therefrom is shown, is hereby ordered.

> HARRY H. WOODRING, Secretary of War.

> > CHARLES EDISON, Secretary of the Navy.

J. MONROE JOHNSON, Assistant Secretary of Commerce.

VI

# 1939 HANDBOOK OF SCREW THREAD STANDARDS FOR FEDERAL SERVICES

As Approved November 9, 1939

### SECTION I. INTRODUCTION

#### 1. PURPOSE OF FEDERAL STANDARDS FOR THREADED PRODUCTS

The purpose of this handbook is to present complete dimensional data upon which specifications may be based for threaded products for Government requirements. So far as practicable, these data are intended to conform to generally accepted commercial practice, although certain special requirements of the Government necessitate the inclusion of some standards not generally applicable outside the Government services.

One of the present generally recognized standards for threaded product is Report B1.1-1935 of the American Standards Association entitled: "American Standard (National Standard) Screw Threads for Bolts, Nuts, Machine Screws, and Threaded Parts." This ASA report was adopted subsequent to the 1933 report of the National Screw Thread Commission, and differences occur in some details between the standards republished herein and those in ASA B1.1-1935.

For the convenience of the users of the two publications, the principal points of difference are listed below. It should be stated clearly and emphatically, however, that in all important respects the two screw-thread standards are identical.

Coarse-Thread Series.—Maximum minor diameters of nuts for classes 1, 2, and 3, sizes Nos. 1 to 10, inclusive, are smaller than the ASA B1.1–1935 values.

Fine-Thread Series.—The class 1 fit in the fine-thread series has been deleted entirely from ASA B1.1, but is still carried herein. Also maximum minor diameters of nuts for classes 2 and 3, sizes Nos. 0 to 12, are smaller than the ASA B1.1–1935 values.

8-Pitch Thread Series.—With the exception of the 1-in. size, the maximum minor diameters of nuts as given in B1.1-1935 are greater than the values herein.

12-Pitch-Thread Series. B1.1-1935 includes the 2%-, 2%-, 2%-, 2%-, 3%-, 3%-, 3%-, and 3%-in. sizes not given herein. 16-Pitch-Thread Series. With the exception of the %-in. size the

16-Pitch-Thread Series. With the exception of the  $\frac{3}{10}$ -in. size the maximum minor diameters of nuts as given in B1.1-1935 are greater than the values herein. Also the following sizes included in B1.1-1935 are not included herein:  $\frac{13}{16}$ ,  $\frac{15}{16}$ ,  $\frac$ 

#### 2. PERSONNEL OF THE COMMITTEE

The personnel of the Interdepartmental Screw Thread Committee is as follows:

Representing the War Department:

Maj. George C. Kenney, Chief, Production Engineering Section, Matériel Division, Wright Field, Dayton, Ohio.

Capt. Mervin E. Gross, Air Corps, Office of the Chief of Air Corps, Washington, D. C. (succeeding Maj. George C. Kenney, November 15, 1939).

Mr. Harry B. Hambleton, Office of Chief of Ordnance, War Department, Washington, D. C.

Representing the Navy Department:

Comdr. Harry B. Slocum, U. S. Navy, Naval Gun Factory, U. S. Navy Yard, Washington, D. C.

Lt. Comdr. Guy Chadwick, U. S. Navy, Bureau of Engineering, Navy Department, Washington, D. C.

Lt. Comdr. William K. Mendenhall, Jr., U. S. Navy, Naval Gun Factory, Navy Yard, Washington, D. C. (succeding Comdr. Harry B. Slocum, December 4, 1939).

Representing the Department of Commerce:

Dr. Lyman J. Briggs, Chairman, Director, National Bureau of Standards, Washington, D. C.

Mr. Henry W. Bearce, Secretary, Co-Chief, Division of Weights and Measures, National Bureau of Standards, Washington, D. C.

the

ASA

the

Committee B18)

ASME and SAE)

of

Liaison Representatives of the American Standards Association:

Mr. Earle Buckingham, Professor, Massachusetts Insti-(Member of tute of Technology, Cambridge, Mass. ASME and SAE) (Member of

Mr. J. H. Edmonds, General Manager, Lebanon Plant, Bethlehem Steel Co., Lebanon, Pa.

Mr. R. E. Flanders, President, Jones & Lamson Machine (Member Co., Springfield, Vt.

Mr. A. M. Houser, Engineer of Standardization, Crane (Member of the Co., 4100 South Kedzie Avenue, Chicago, Ill. ASME)

#### 3. ARRANGEMENT OF REPORT

There are included in the body of the report specifications for threaded products and gages, embodying sufficient information to permit the writing of definite and complete specifications for the purchase of screw-thread products. In the appendixes there is arranged supplementary information of both a general and a technical nature, including such specifications as are not intended to be mandatory.

The specifications in the report have been arranged, as far as possible, by products. For example, one section deals with threads for bolts and nuts, etc., another with hose-coupling threads, another with pipe threads, etc. As far as practicable, each section is arranged in the following order:

- 1. Form of thread.
- 2. Thread series.
- 3. Classification and tolerances.
- 4. Tables of dimensions.
- 5. Gages.

## SECTION II. TERMINOLOGY

In this report there are utilized, as far as possible, nontechnical words and terms which best convey alike to the producer and user of screw threads the information presented.

#### 1. DEFINITIONS

The following definitions are given of the more important terms used in the report. Definitions of terms which are obviously elementary in character are intentionally omitted.

(a) TERMS RELATING TO SCREW THREADS.—1. Screw thread.—A ridge of uniform section in the form of a helix on the surface of a cylinder or cone.

2. External and internal threads.<sup>2</sup>—An external thread is a thread on the outside of a member. Example: A threaded plug.

An internal thread is a thread on the inside of a member. Example: A threaded hole.

3. Major diameter (formerly known as "outside diameter").—The largest diameter of the thread of the screw or nut. The term "major diameter" replaces the term "outside diameter" as applied to the thread of a screw and also the term "full diameter" as applied to the thread of a nut.

4. Minor diameter (formerly known as "core diameter").—The smallest diameter of the thread of the screw or nut. The term "minor diameter" replaces the term "core diameter" as applied to the thread of a screw and also the term "inside diameter" as applied to the thread of a nut.

5. Pitch diameter.—On a straight screw thread, the diameter of an imaginary cylinder, the surface of which would pass through the threads at such points as to make equal the width of the threads and the width of the spaces cut by the surface of the cylinder. On a taper screw thread, the diameter, at a given distance from a reference plane perpendicular to the axis of an imaginary cone, the surface of which would pass through the threads at such points as to make equal the width of the threads and the width of the spaces cut by the surface of which would pass through the threads at such points as to make equal the width of the threads and the width of the spaces cut by the surface of the cone.

6. *Pitch.*—The distance from a point on a screw thread to a corresponding point on the next thread measured parallel to the axis.

The pitch in inches =  $\frac{1}{\text{Number of threads per inch}}$ 

7. Lead.—The distance a screw thread advances axially in one turn. On a single-thread screw the lead and pitch are identical; on a double-thread screw the lead is twice the pitch; on a triple-thread screw the lead is three times the pitch, etc.

8. Angle of thread.—The angle included between the sides of the thread measured in an axial plane.

9. Helix angle.—The angle made by the helix of the thread at the pitch diameter with a plane perpendicular to the axis.

10. Crest.—The top surface joining the two sides of a thread.

11. Root.—The bottom surface joining the sides of two adjacent threads.

<sup>&</sup>lt;sup>2</sup> These terms are here defined because of possible confusion arising from the fact that an "internal member" has an "external thread," and vice versa. For the sake of brevity an external thread is hereinafter referred to as a "screw," and an internal thread as a "nut."

12. Side.—The surface of the thread which connects the crest with the root.

13. Axis of a screw.-The longitudinal central line through the screw.

14. Base of thread.—The bottom section of the thread; the greatest section between the two adjacent roots.

15. Depth of thread.—The distance between the crest and the base of thread measured normal to the axis.

16. Number of threads.-Number of threads in 1 inch of length.

17. Length of engagement.—The length of contact between two mating parts, measured axially.

18. Depth of engagement.—The depth of thread contact of two mating parts, measured radially.

19. Pitch line.—An element of the imaginary cylinder or cone specified in definition 5.

20. Thickness of thread.—The distance between the adjacent sides of the thread measured along cr parallel to the pitch line.

(b) TERMS RELATING TO CLASSIFICATION AND TOLERANCES.— 1. Allowance.—An intentional difference in the dimensions of mating parts. It is the minimum clearance or the maximum interference which is intended between mating parts. It represents the condition of the tightest permissible fit, or the largest internal member mated with the smallest external member. Examples:

One-half inch, class 1, loose fit, American National coarse thread series:	
Minimum pitch diameter of nut	0.4500
Maximum pitch diameter of screw	. 4478
-	
Allowance (positive)	.0022
One-half inch, class 4, close fit, American National coarse thread series:	
Minimum pitch diameter of nut	. 4500
Maximum pitch diameter of screw	. 4504
-	

2. Tolerance.—The amount of variation permitted in the size of a part. Example:

# One-half-inch screw, class 1, loose fit, American National coarse thread series:

maximum pite	in diameter	'	 	 0.4478
Minimum pite	h diameter		 	 . 4404
1			 	

3. *Basic size.*—The theoretical or nominal standard size from which all variations are made.

4. Crest clearance.—Defined on a screw form as the space between the crest of a thread and the root of its mating thread.

5. *Finish.*—The character of the surface on a screw thread or other product.

6. *Fit.*—The relation between two mating parts with reference to the conditions of assembly; for example: Wrench fit; close fit; medium fit; free fit; loose fit. The quality of fit is dependent upon both the relative size and finish of the mating parts.

7. Neutral zone.—A positive allowance. (See "Allowance".)

8. Limits.—The extreme permissible dimensions of a part. Example:

One-half-inch screw, class 1, loose fit, American National coars	se	thread series:
Maximum pitch diameter	0.	4478\These are
Minimum pitch diameter		4404∫the limits

# 2. ILLUSTRATIONS SHOWING TERMINOLOGY

Figures 1 and 2 illustrate the use of the terms and symbols used in the report as herein defined.



FIGURE 1.—Screw-thread notation:

#### 3. SYMBOLS

For use in formulas for expressing relations of screw threads, and for use on drawings and for similar purposes, the following symbols should be used:

Major diameter	D
Corresponding radius	d
Pitch diameter	E
Corresponding radius	е
Minor diameter	K
Corresponding radius	k
Angle of thread	A
One half angle of thread	a
Number of turns per inch	N
Number of threads per inch	n
· · · ·	- 1
Lead	$L = \overline{N}$





FIGURE 2.—Screw-thread notation.

Additional symbols for American National Pipe Threads are given in section VII.

Symbols are for use on correspondence, drawings, shop and storeroom cards, specifications for parts, taps, dies, gages, etc., and on tools and gages.

The method of designating a screw thread by means of symbols is by the use of the initial letters of the thread series, preceded by the diameter in inches (or the screw number) and number of threads per inch, all in Arabic characters, and followed by the classification of fit in Arabic numerals. If the thread is left hand, the symbol "LH" shall follow the class of fit. No symbol is used to distinguish right-

hand threads. For screw threads of American Na special diameters, pitches, and lengths of engage "NS" is used. Examples:	ational form but of ement, the symbol
American National coarse thread series:	Mark
per inch, class 1 fit	1''8NC1
Threaded part 1 inch diameter, 8 threads per inch,	1''
American National fine thread series:	
Threaded part 1 inch diameter, 14 threads per inch,	1'' 1 / NF /
American National 8-, 12-, or 16-pitch thread series:	1 14111 4
Threaded part 1 inch diameter, 12 threads per inch, class 3 fit	1''-12N-3
Threaded part 1½ inches diameter, 8 threads per inch,	
American National form, special pitch:	1 <sup>7</sup> /2 <sup>7</sup> 8 <i>I</i> V2 <i>L</i> H
Threaded part 1 inch diameter, 18 threads per inch,	111 10 10 0
Threaded part 1¼ inches diameter, 20 threads per	1°18/ND2
inch, class 3 fit, left hand	1¼''—20NS—3LH
American National taper pipe thread. Threaded	
part 1 inch diameter, 11½ threads per inch	$1^{\prime\prime}-11^{\prime}_{2}NPT$
American National fire-hose coupling threads and	1
American National hose-coupling threads:	OU CNU
Threaded part 1 inch diameter 111/2 threads per inch	1''11%NH

The number of threads per inch shall be indicated in all cases, irrespective of whether it is the standard number of threads for that particular size of threaded part, or special.

#### Symbols for Wire Measurements

Measurement over wires	M
Diameter of wire	G
Corresponding radius	g

### SECTION III. SCREW THREADS FOR BOLTS, MACHINE SCREWS, NUTS, TAPPED HOLES, ETC.

#### 1. AMERICAN NATIONAL FORM OF THREAD

The form of thread profile specified herein, known previously as the "United States standard or Sellers' profile", is adopted by the Commission and shall hereafter be known as the "American National form of thread."

The American National form of thread shall be used for all screwthread work except when otherwise specified for special purposes.

#### (a) SPECIFICATIONS

1. ANGLE OF THREAD.—The basic angle of thread (A) between the sides of the thread measured in an axial plane is  $60^{\circ}$ . The line bisecting this  $60^{\circ}$  angle is perpendicular to the axis of the screw thread.

2. FLAT AT CREST AND ROOT.—The flat at the root and crest of the basic thread form is  $\frac{1}{5} \times p$ , or  $0.125 \times p$ .

3. DEPTH OF THREAD.— The depth of the basic thread form is

$$h = 0.649519 \times p$$
, or  $h = \frac{0.649519}{n}$ 

where

p = pitch in inchesn = number of threads per inchh = basic depth of thread

4. CLEARANCE AT MINOR DIAMETER.—A clearance shall be provided at the minor diameter of the nut by removing from the crest of the basic thread form an amount such as to provide a depth of thread not less than 62 to 75 percent (depending on the size), and not more than 83½ percent of the basic thread depth. (See fig. 17, p. 31.)

5. CLEARANCE AT MAJOR DIAMETER.—A clearance shall be provided at the major diameter of the nut by removing from above the basic thread form an amount such that the width of flat shall be less than  $\frac{1}{2} \times p$ , but not less than  $\frac{1}{24} \times p$ .

#### (b) ILLUSTRATION

There are indicated in figure 3 the relations as specified herein for the American National form of thread for the minimum nut and maximum screw, free or medium fits. These relations are further shown in figures 7 and 9.

#### 2. THREAD SERIES

It is the aim of the Commission, in establishing thread systems for general use, to eliminate all unnecessary sizes and, in addition, to utilize as far as possible present predominating sizes. While from certain standpoints it would have been desirable to make simplifications in the thread systems and to establish more thoroughly consistent standards, it is believed that any radical change at the present time would be out of place and interfere with manufacturing conditions, and would involve great economic loss.

The testimony given at the various hearings held by the Commission is very consistent in favoring the maintenance of the present coarsethread and fine-thread series, the coarse-thread series being the "United States standard" threads, supplemented in the sizes below one fourth inch by sizes taken from the standard established by the American Society of Mechanical Engineers (A.S.M.E.). The finethread series is composed of standards that have been found necessary, and consists of sizes taken from the standards of the Society of Automotive Engineers (S.A.E.) and the fine-thread series of the American Society of Mechanical Engineers (A.S.M.E.).



FIGURE 3.—American National form of thread.

Note.—No allowance is shown. This condition exists in class 2, free fit, and class 3, medium fit, where both the minimum nut and the maximum screw are basic.

#### NOTATION

 $\begin{array}{l} n = \text{number of threads per inch} \\ H = 0.866025 \ p \ depth of \ 60^\circ \ sharp \ V \ thread} \\ h = 0.649519 \ p \ depth of \ American \ National \ form \ of \ thread} \\ \frac{56h = 0.541266 \ p \ maximum \ depth \ of \ engagement}{17ish = 0.613435 \ p} \\ F = 0.125000 \ p \ width \ of \ flat \ at \ crest \ and \ root \ of \ American \ National \ form \\ f = 0.108253 \ p) \\ = \frac{156H}{160} \ depth \ of \ truncation \\ = \frac{156H}{160} \ depth \ of \ truncation \\ \end{array}$ 

#### (a) AMERICAN NATIONAL COARSE-THREAD SERIES

In table 1 are specified the nominal sizes and basic dimensions of the "American National coarse-thread series."

The American National coarse-thread series is recommended for general use in engineering work, in machine construction where conditions are favorable to the use of bolts, screws, and other threaded components where quick and easy assembly of the parts is desired, and for all work where conditions do not require the use of fine-pitch threads.

Identif	lication	Ba	sic diame	eters	Thread data						
Sizes	Threads per inch, n	Major diam- eter, D	Pitch diam- eter, E	Minor diam- eter, <i>K</i>	Metric equiva- lent of major diam- eter	Pitch,	Depth of thread, h	Basic width of flat, p/8	Mini- mum width of flat at major diam- eter of nut, p/24	Helix an- gle at basic pitch diameter, g	Basic area of section at root of thread, $\frac{\pi K^3}{4}$
1	2	3	4	5	6	7	8	9	10	11	i2
1 2 3 4 5 6 8 10	64 56 48 40 40 32 32 24 24	Inches 0.073 .086 .099 .112 .125 .138 .164 .190 .216	Inches 0.0629 .0744 .0855 .0958 .1088 .1177 .1437 .1629 .1880	Inches 0. 0527 . 0628 . 0719 . 0795 . 0925 . 0974 . 1234 . 1359 . 1610	mm 1.854 2.184 2.515 2.845 3.175 3.505 4.166 4.826 5.486	Inch 0. 01562 . 01786 . 02083 . 02500 . 02500 . 03125 . 03125 . 03125 . 04167	Inch 0. 01015 . 01160 . 01353 . 01624 . 01624 . 02030 . 02030 . 02706	Inch 0.00195 .00223 .00260 .00312 .00312 .00391 .00391 .00391 .00521	Inch 0.00065 .00074 .00087 .00104 .00104 .00104 .00130 .00130 .00174	$\begin{array}{c} \hline Deg.\ Min. \\ 4 \ 31 \\ 4 \ 22 \\ 4 \ 26 \\ 4 \ 45 \\ 4 \ 11 \\ 4 \ 50 \\ 3 \ 58 \\ 4 \ 39 \\ 4 \ 31 \\ \end{array}$	Square inches 0.0022 .0031 .0041 .0050 .0067 .0120 .0145 .0206
14 5/16 38 7/16	20 18 16 14 13	. 2500 . 3125 . 3750 . 4375 . 5000	. 2175 . 2764 . 3344 . 3911 . 4500	. 1850 . 2403 . 2938 . 3447 . 4001	6. 350 7. 938 9. 525 11. 113 12. 700	.05000 .05556 .06250 .07143 .07692	. 03248 . 03608 . 04059 . 04639 . 04996	. 00625 . 00694 . 00781 . 00893 . 00962	.00208 .00231 .00260 .00298 .00321	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	. 0200 . 0269 . 0454 . 0678 . 0933 . 1257
9/16 58 34 78 1	12 11 10 9 8	. 5625 . 6250 . 7500 . 8750 1. 0000	. 5084 . 5660 . 6850 . 8028 . 9188	. 4542 . 5069 . 6201 . 7307 . 8376	14. 288 15. 875 19. 050 22. 225 25. 400	.08333 .09091 .10000 .11111 .12500	.05413 .05905 .06495 .07217 .08119	.01042 .01136 .01250 .01389 .01562	.00347 .00379 .00417 .00463 .00521	$\begin{array}{cccc} 2 & 59 \\ 2 & 56 \\ 2 & 40 \\ 2 & 31 \\ 2 & 29 \end{array}$	. 1620 . 2018 . 3020 . 4193 . 5510
1 1/8 1 1/4 1 3/8 1 1/2 1 3/4	7 7 6 5	1, 1250 1, 2500 1, 3750 1, 5000 1, 7500	$\begin{array}{c} 1.\ 0322\\ 1.\ 1572\\ 1.\ 2667\\ 1.\ 3917\\ 1.\ 6201 \end{array}$	. 9394 1. 0644 1. 1585 1. 2835 1. 4902	28. 575 31. 750 34. 925 38. 100 44. 450	. 14286 . 14286 . 16667 . 16667 . 20000	.09279 .09279 .10825 .10825 .12990	.01786 .01786 .02083 .02083 .02500	.00595 .00595 .00694 .00694 .00833	$egin{array}{cccc} 2 & 31 \\ 2 & 15 \\ 2 & 24 \\ 2 & 11 \\ 2 & 15 \end{array}$	. 6931 . 8898 1. 0541 1. 2938 1. 7441
2 21/4 21/2 23/4 3	415 415 4 4 4 4	$\begin{array}{c} 2,0000\\ 2,2590\\ 2,5000\\ 2,7500\\ 3,0000 \end{array}$	$\begin{array}{c} 1.8557\\ 2.1057\\ 2.3376\\ 2.5876\\ 2.8376\end{array}$	1.7113 1.9613 2.1752 2.4252 2.6752	50.800 57.150 63.500 69.850 76.200	. 22222 . 22222 . 25000 . 25000 . 25000	. 14434 . 14434 . 16238 . 16238 . 16238 . 16238	$\begin{array}{r} . \ 02778 \\ . \ 02778 \\ . \ 03125 \\ . \ 03125 \\ . \ 03125 \\ . \ 03125 \end{array}$	.00926 .00926 .01042 .01042 .01042	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 2.\ 3001\\ 3.\ 0212\\ 3.\ 7161\\ 4.\ 6194\\ 5.\ 6209 \end{array}$
314 314 314 334 4	4 4 4 4	$\begin{array}{c} 3.\ 2500\\ 3.\ 5000\\ 3.\ 7500\\ 4.\ 0000 \end{array}$	3.0876 3.3376 3.5876 3.8376	2. 9252 3. 1752 3. 4252 3. 6752	82. 550 88. 900 95. 250 101. 600	. 25000 . 25000 . 25000 . 25000 . 25000	. 16238 . 16238 . 16238 . 16238 . 16238	. 03125 . 03125 . 03125 . 03125 . 03125	.01042 .01042 .01042 .01042 .01042	$     \begin{array}{cccc}       1 & 29 \\       1 & 22 \\       1 & 16 \\       1 & 11     \end{array} $	6.7205 7.9183 9.2143 10.6084

#### TABLE 1.—American National coarse-thread series

#### (b) AMERICAN NATIONAL FINE-THREAD SERIES

In table 2 are specified the nominal sizes and basic dimensions of the "American National fine-thread series".

The American National fine-thread series is recommended for general use in automotive and aircraft work, for use where the design requires both strength and reduction in weight, and where special conditions require a fine thread.

Identi	Identification Basic diameters		ters	Thread data							
Sizes	Threads per inch, n	Major diam- eter, D	Pitch diam- eter, E	Minor diam- eter, K	Metric equiv- alent of major diam- eter	Pitch, p	Depth of thread, h	Basic width of flat, p/8	Mini- mum width of flat at major diam- eter of nut, p/24	Helix angle at basic pitch diameter 8	Basic area of section at root of thread, $\frac{\pi K^2}{4}$
1	2	3	4	5	6	7	8	9	10	11	12
0 1 2 3 4 5 6 8 10 12 14	80 72 64 56 48 44 40 36 32 28 28 28 28 24 24 20	Inches 0.060 .073 .099 .112 .125 .138 .164 .190 .216 .2500 .3125 .3750 .4375	Inches 0.0519 .0640 .0759 .0874 .0985 .1102 .1218 .1460 .1697 .1928 .2268 .2854 .2854 .3479 .4050	Inches 0.0438 .0550 .0655 .0758 .0849 .0955 .1279 .1494 .1696 .2036 .2036 .2036 .3209 .3725	$\begin{array}{c} mm \\ 1.524 \\ 1.854 \\ 2.515 \\ 2.845 \\ 3.175 \\ 3.505 \\ 4.166 \\ 4.826 \\ 5.486 \\ 6.350 \\ 7.938 \\ 9.525 \\ 11.113 \\ 1.12$	Inch 0.01250 01389 01562 02083 02273 02500 02778 03125 03571 03571 04167 04167 04167	Inch 0.00812 .00902 .01015 .01160 .01353 .01476 .01624 .01802 .02320 .02320 .02320 .02320 .02320 .02320 .02328 .023248 .02248	Inch 0.00156 .00174 .00195 .00223 .00260 .00284 .00312 .00347 .00391 .00446 .00446 .00521 .00521 .00625	Inch 0. 03052 .00058 .00068 .00074 .00095 .00104 .00130 .00130 .00149 .00174 .00174 .00174	$\begin{array}{c} Deg, Min \\ 4 & 23 \\ 3 & 57 \\ 3 & 45 \\ 3 & 43 \\ 3 & 51 \\ 3 & 44 \\ 3 & 28 \\ 3 & 21 \\ 3 & 22 \\ 2 & 40 \\ 2 & 11 \\ 2 & 15 \\ \end{array}$	Square inches 0.0015 .0024 .0035 .0057 .0057 .0027 .0028 .0175 .0226 .0326 .0326 .0524 .0326
32 916 34 76 1 116	20 18 16 14 14 14 12	. 5000 . 5625 . 6250 . 7500 . 8750 1. 0000 1. 1250	. 4675 . 5264 . 5889 . 7094 . 8286 . 9536 1. 0709	. 4350 . 4903 . 5528 . 6688 . 7822 . 9072 1. 0167	12. 700 14. 288 15. 875 19. 050 22. 225 25. 400 28. 575	. 05000 . 05556 . 05556 . 06250 . 07143 . 07143 . 08333	. 03248 . 03608 . 03608 . 04059 . 04639 . 04639 . 04639	.00625 .00694 .00694 .00781 .00893 .00893 .00893	. 00208 . 00231 . 00231 . 00260 . 00298 . 00298 . 00347	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	. 1486 . 1888 . 2400 . 3513 . 4805 . 6464 . 8118
174 13/8 11/2	12 12 12	1. 3750 1. 5000	1. 3209 1. 4459	1. 2667 1. 3917	34. 925 38. 100	. 08333 . 08333 . 08333	.05413 .05413 .05413	.01042 .01042 .01042	.00347 .00347 .00347	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	1. 0238 1. 2602 1. 5212

TABLE 2.—American National fine-thread series

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### 3. CLASSIFICATION AND TOLERANCES

There are established herein for general use four distinct classes of screw-thread fits as specified in the following brief outline. These four classes of fits, together with the accompanying specifications, are for the purpose of insuring the interchangeable manufacture of screw-thread parts throughout the country.

It is not the intention of the Commission arbitrarily to place a general class or grade of work in a specific class of fit. Each manufacturer and user of screw threads is free to select the class of fit best adapted to his particular needs. The tolerances and dimensions for four classes of fit are given in tables 3 to 14, inclusive, and summarized in tables 15 and 16.

Class 1, loose fit	Includes screw-thread work of rough com- mercial quality, where the threads must assemble readily, and a certain amount
	of shake or play is not objectionable.
	Includes the great bulk of screw-thread
Class 2, free fit	work of ordinary quality, of finished
	and semifinished bolts and nuts, machine
	screws, etc.
Class 3, medium fit	Includes the better grade of interchangeable
	screw-thread work.
	Includes screw-thread work requiring a fine
Class 4, close fit	snug fit, much closer than the medium fit,
	In this class of fit selective assembly of
	parts may be necessary.

An examination of the dimensional specifications for the various classes of fit shows that a screw made to one class of fit may be used with a nut or tapped hole made to some other class of fit. The resulting quality of fit may represent an intermediate class or may approximate one of the classes of fit adopted as standard. The use of different classes of fit on the screw and threaded hole may be justified when equipment available is such that one member can be economically produced to a higher accuracy than the other. For instance, common commercial machine screws are made to class 2, free fit, while machine-screw nuts are commonly supplied in class 1, loose fit; or, ground-thread taps may make it practicable to produce class 3 nuts for use with class 1 or class 2 screws.

#### (a) GENERAL SPECIFICATIONS

The following general specifications apply to all classes of fit specified for the American National coarse-thread series and the American National fine-thread series.

1. UNIFORM MINIMUM NUT.—The pitch diameter of the minimum threaded hole or nut corresponds to the basic size.

2. UNIFORM MINOR DIAMETER OF NUT.—The minor diameter of the threaded hole or nut, of any given size and pitch, is the same for fits of classes 1 to 4, inclusive.

3. LENGTH OF ENGAGEMENT.—A length of engagement equal to the basic major diameter is the basis of the tolerances specified herein for screw-thread products.

4. TOLERANCES.<sup>3</sup>—(a) The tolerances specified represent the extreme variations permitted on the product.

<sup>\*</sup> Recommendations and explanations regarding the application of tolerances are given in appendix 1.

(b) The tolerance on the nut is plus, and is applied from the basic size to above basic size.

(c) The tolerance on the screw is minus, and is applied from the maximum screw size to below the maximum screw size.



FIGURE 4.—Illustration of tolerances, allowance (neutral space), and crest clearances for class 1, loose fit.

(d) The pitch diameter tolerances for a screw and nut of a given class of fit are the same.

(e) Pitch diameter tolerances include lead and angle variations. (See footnote 1, tables 3, 4, 5, and 6.)

(f) The tolerances on the major diameters of class 1, loose fit, or class 2, free fit screws are twice the tolerance values allowed on the

pitch diameters of the same respective classes and pitches with the following exception: On class 2, free fit, American National coarsethread series, externally threaded parts of unfinished, hot-rolled material, the same tolerances on major diameter are applied as on class 1, loose fit screws.

The tolerances on the major diameters of class 3, medium fit, and class 4, close fit screws, American National coarse-thread series, are the same as those on class 2, free fit finished screws of the same thread series; and for the American National fine-thread series are the same as those on class 2, free fit of that series.

(g) The minimum minor diameter of a screw of a given pitch is such as to result in a basic flat  $(\frac{1}{2} \times p)$  at the root when the pitch



FIGURE 5.—Illustration of loosest condition for class 1, loose fit, one-fourth inch, 20 threads.

diameter of the screw is at its minimum value. When the maximum screw is basic, the minimum minor diameter of the screw will be below the basic minor diameter by the amount of the specified pitch diameter tolerance.

(h) The maximum minor diameter of a screw of a given pitch may be such as results from the use of a worn or rounded threading tool, when the pitch diameter is at its maximum value. In no case, however, should the form of a thread, as results from tool wear, be such as to cause the screw to be rejected on the maximum minor diameter by a "go" ring gage, the minor diameter of which is equal to the minimum minor diameter of the nut.

(i) The maximum major diameter of the nut of a given pitch is such as to result in a flat equal to one third of the basic flat  $(\frac{1}{24} \times p)$ 

when the pitch diameter of the nut is at its maximum value. When the minimum nut is basic, its maximum major diameter will be above the basic major diameter by the amount of the specified pitch diameter tolerance plus two ninths of the basic thread depth.

(j) The nominal minimum major diameter of a nut is the basic major diameter. In no case, 'however, should the minimum major diameter of the nut, as results from a worn tap or cutting tool, be such as to cause the nut to be rejected on the minimum major diameter by a "go" plug gage made to the standard form at the crest.



FIGURE 6.—Illustration of tightest condition for class 1, loose fit, one-fourth inch, 20 threads.

NOTATION D=major diameter E=pitch diameter K=minor diameter h=0.0325=basic thread depth

(k) Tolerances are based on the pitch of the thread and a length of engagement equal to the basic major diameter, but may be used for lengths of engagement up to  $1\frac{1}{2}$  diameters. (For longer lengths of engagement see section V, p. 76.)

#### (b) CLASSIFICATION OF FITS

1. CLASS 1, LOOSE FIT.—(a) Definition.—The loose-fit class is intended to cover the manufacture of threaded parts where quick and easy assembly is necessary and a considerable amount of shake or play is not objectionable.

Threads per inch	Allowances	Pitch- diameter tolerances <sup>1</sup>	Lead errors consuming one half of pitch- diameter tolerances <sup>2</sup>	Errors in half-angle consuming one half of pitch- diameter tolerances	
1	2	3	4		
80' 7264 56 48	Inch 0.0007 .0007 .0007 .0008 .0008 .0009	Inch 0.0024 .0025 .0026 .0028 .0031	Inch 0.0007 .0007 .0008 .0008 .0009	Deg. Min 3 40 3 20 3 10 3 0 2 50	
44 40 36 32 28	.0009 .0010 .0011 .0011 .0011 .0012	. 0032 . 0034 . 0036 . 0038 . 0043	.0009 .0010 .0010 .0011 .0012	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	
24 20 18 16	. 0013 . 0015 . 0016 . 0018	. 0046 . 0051 . 0057 . 0063	. 0013 . 0015 . 0016 . 0018	$     \begin{array}{c}       2 & 0 \\       1 & 57 \\       1 & 58 \\       1 & 55     \end{array} $	
14	.0021 .0022 .0024 .0026	.0070 .0074 .0079 .0085	.0020 .0021 .0023 .0025	$     \begin{array}{ccc}       1 & 52 \\       1 & 50 \\       1 & 49 \\       1 & 47 \\     \end{array} $	
109 987	. 0028 . 0031 . 0034 . 0039	. 0092 . 0100 . 0111 . 0124	. 0027 . 0029 . 0032 . 0036	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	
65 54½ 4½4	. 0044 . 0052 . 0057 . 0064	. 0145 . 0169 . 0184 . 0204	. 0042 . 0049 . 0053 . 0059	$     \begin{array}{cccc}       1 & 40 \\       1 & 37 \\       1 & 38 \\       1 & 35     \end{array} $	

TABLE 3.—Class 1, loose fit, allowances and tolerances for screws and nuts

<sup>1</sup> The tolerances specified for pitch diameter include all errors of pitch diameter, lead, and angle. The full tolerance cannot, therefore, be used on pitch diameter unless the lead and angle of the thread are perfect. Col-umns 4 and 5 give, for information, the errors in lead (per length of thread engaged) and in angle, each of which can be compensated for by half the tolerance on the pitch diameter given in column 3. If lead and angle errors both exist to the amount tabulated, the pitch diameter of a bott, for example, must be reduced by the full tolerance or it will end error the loc? or it will not enter the "go" gage. <sup>2</sup> Between any 2 threads not farther apart than the length of engagement.

This class has an allowance on the screw to permit ready assembly even when the threads are slightly bruised or dirty.

(b) Minimum nut basic.-The pitch diameter of the minimum nut of a given diameter and pitch corresponds to the basic pitch diameter, as specified in the tables of thread series given herein, which is computed from the basic major diameter of the thread. The pitch diameter of the minimum nut is the theoretical pitch diameter for that size.

(c) Maximum screw below basic.<sup>4</sup>—The dimensions of the maximum screw of a given pitch and diameter are below the basic dimensions as specified in the tables of thread series given herein, which are computed from the basic major diameter of the threads, by the amount of the allowance given in table 3.

(d) Allowance and tolerance values.—Allowances and tolerances are specified in table 3.

2. CLASS 2, FREE FIT.—(a) Definition.—The free-fit class is intended to apply to interchangeable manufacture where the threaded members

<sup>&</sup>lt;sup>4</sup> The maximum minor diameter of the screw is above the basic minor diameter as shown in fig. 4.

are to assemble nearly or entirely with the fingers, where a moderate amount of shake or play between the assembled threaded members is not objectionable, and where no allowance is required. This class includes the great bulk of fastening screws.



FIGURE 7.—Illustration of tolerances and crest clearances for class 2, free fit:

(b) Minimum nut basic.—The pitch diameter of the minimum nut of a given diameter and pitch corresponds to the basic pitch diameter, as specified in tables of thread series given herein, which is computed from the basic major diameter of the thread.

Threads per inch	Allowances	Pitch- diameter tolerances <sup>1</sup>	Lead errors consuming one half of pitch- diameter tolerances <sup>2</sup>	Errors in half-angle consuming one half of pitch- diameter tolerances 5 Deg. Min. 2 36 2 28 2 19 2 8 8 2 1	
1	2	3	4		
80 72	Inch 0.0000 .0000 .0000 .0000 .0000	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Inch 0.0005 .0005 .0005 .0006 .0006		
44	.0000 .0000 .0000 .0000 .0000 .0000	. 0023 . 0024 . 0025 . 0027 . 0031	.0007 .0007 .0007 .0008 .0009	$     \begin{array}{ccc}       1 & 5 \\       1 & 5 \\       1 & 4 \\       1 & 3 \\       1 & 3 \\       1 & 3   \end{array} $	
24	. 0000 . 0000 . 0000 . 0000	. 0033 . 0036 . 0041 . 0045	.0010 .0010 .0012 .0013	$     \begin{array}{cccc}       1 & 3 \\       1 & 2 \\  $	
14	. 0000 . 0000 . 0000 . 0000	. 0049 . 0052 . 0056 . 0059	,0014 .0015 .0016 .0017	1 1 1 1 1 1 1 1	
10987	. 0000 . 0000 . 0000 . 0000	. 0064 . 0070 . 0076 . 0085	.0018 .0020 .0022 .0025	$egin{array}{ccc} 1 & 1 \\ 1 & 1 \\ 1 & 1 \\ 1 & 1 \end{array}$	
65 5 4½ 4	. 0000 . 0030 . 0000 . 0000	. 0101 . 0116 . 0127 . 0140	. 0029 . 0033 . 0037 . 0040	1 1 1 1	

TABLE 4.—Class 2, free fit, tolerances for screws and nuts (no allowances)

<sup>1</sup> The tolerances specified for pitch diameter include all errors of pitch diameter, lead, and angle. The full tolera ace cannot, therefore, be used on pitch diameter unless the lead and angle of the thread are perfect. Columns 4 and 5 give, for information, the errors in lead (per length of thread engaged) and in angle, each of which can be compensated for by half the tolerance on the pitch diameter given in column 3. If lead and angle errors both exist to the amount tabulated, the pitch diameter of a both, for example, must be reduced by the full tolerance or it will not enter a basic nut or gage. <sup>3</sup> Between any two threads not farther apart than the length of engagement.

(c) Maximum screw basic.<sup>5</sup>-The major diameter and pitch diameter of the maximum screw of a given pitch and diameter correspond to the basic dimensions, as specified in tables of thread series given herein, which are computed from the basic major diameter of the thread.

(d) Allowance and tolerance values.—Allowances and tolerances are specified in table 4.

3. CLASS 3, MEDIUM FIT.—(a) Definition.—The medium-fit class is intended to apply to the manufacture of the higher grade of threaded parts which are to assemble nearly or entirely with the fingers and must have the minimum amount of shake or play between the threaded members. It is the same in every particular as class 2, free fit, except that the tolerances are smaller.

<sup>5</sup> The maximum minor diameter of the screw is above the basic minor diameter, as shown in fig. 7.



FIGURE 8.—Illustration of loosest condition for class 2, free fit, one-fourth inch, 20 threads.



FIGURE 9.—Illustration of tightest condition for class 2, free fit, one-fourth inch, 20 threads.

#### NOTATION

D=major diameter E=pitch diameter K=minor diameter h=0.0325=basic thread depth (b) Minimum nut basic.—The pitch diameter of the minimum nut of a given diameter and pitch corresponds to the basic pitch diameter, as specified in tables of thread series given herein, which is computed from the basic major diameter of the thread.

Threads per inch	Allowances	Pitch- diameter tolerances <sup>1</sup>	Lead errors consuming one half of pitch- diameter tolerances <sup>2</sup>	Errors in half-angle consuming one half of pitch- diameter tolerances	
1	2	3	4	5	
80	Inch 0.0000 .0000 .0000 .0000 .0000	Inch 0.0013 .0013 .0014 .0015 .0016	Inch 0.0004 .0004 .0004 .0004 .0004 .0005	Deg. 1 1 1 1 1 1	Min. 59 47 43 36 28
44	. 0000 . 0000 . 0000 . 0000 . 0000	. 0016 . 0017 . 0018 . 0019 . 0022	. 0005 . 0005 . 0005 . 0005 . 0005 . 0006	1 1 1 1	21 18 14 10 11
24	. 0000 . 0000 . 0000 . 0000	. 0024 . 0026 . 0030 . 0032	. 0007 . 0008 . 0009 . 0009	1 1 1 0	6 0 2 59
14 13	. 0000 . 0000 . 0000 . 0000	. 0036 . 0037 . 0040 . 0042	.0010 .0011 .0012 .0012	0 0 0	58 55 55 53
109 98 87	. 0000 . 0000 . 0000 . 0000	. 0045 . 0049 . 0054 . 0059	. 0013 . 0014 . 0016 . 0017	0 0 0 0	52 51 50 47
6 5	. 0000 . 0000 . 0000 . 0000	. 0071 . 0082 . 0089 . 0097	. 0020 . 0024 . 0026 . 0028	0 0 0	49 47 46 44

TABLE 5.—Class 3, medium fit, tolerances for screws and nuts (no allowances)

<sup>1</sup> The tolerances specified for pitch diameter include all errors of pitch diameter, lead, and angle. The full tolerance cannot, therefore, be used on pitch diameter unless the lead and angle of the thread are perfect. Columns 4 and 5 give, for information, the errors in lead (per length of thread engaged) and in angle, each of which can be compensated for by half the tolerance on the pitch diameter given in column S. If lead and angle errors both exist to the amount tabulated, the pitch diameter of a bolt, for example, must be reduced by the full tolerance or it will not enter a basic nut or gage.

<sup>2</sup> Between any 2 threads not farther apart than the length of engagement.

(c) Maximum screw basic.<sup>6</sup>—The major diameter and pitch diameter of the maximum screw of a given pitch and diameter correspond to the basic dimensions, as specified in tables of thread series given herein, which are computed from the basic major diameter of the thread.

(d) Allowance and tolerance values.—Allowances and tolerances are specified in table 5.

4. CLASS 4, CLOSE FIT.—(a) Definition.—The close-fit class is intended for threaded work of the finest commercial quality where very little shake or play is desirable, and where a screw driver or wrench may be necessary for assembly. In the manufacture of

<sup>3</sup> The maximum minor diameter of the screw is above the basic minor diameter, as shown in fig. 10.

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FIGURE 10.—Illustration of tolerances and crest clearances for class 3, medium fit.



FIGURE 11.—Illustration of loosest condition for class 3, medium fit, one-fourth inch, 20 . hreads.



FIGURE 12.--Illustration of tightest condition for class 3, medium fit, one-fourth inch, 20 threads.

NOTATION D = major diameter E = pitch diameter K = minor diameter h = 0.0325 = basic thread depth


FIGURE 13.—Illustration of tolerances, allowance (interference), and crest clearances for class 4, close fit.

screw-thread products belonging in this class it will be necessary to use precision tools,<sup>7</sup> gages made to special tolerances for this class (see table 21, p. 58), and other refinements. This quality of work should, therefore, be used only in cases where requirements of the mechanism being produced are exacting, or where special conditions require screws having a precision fit. In order to secure the fit desired it may be necessary in some cases to select the parts when the product is being assembled.

(b) Minimum nut basic.—The pitch diameter of the minimum nut of a given diameter and pitch corresponds to the basic pitch diameter, as specified in tables of thread series given herein, which is computed from the basic major diameter of the thread.

(c) Maximum screw above basic.—The pitch diameter of the maximum screw of a given diameter and pitch is above the basic dimensions as specified in tables of thread series given herein, which are computed from the basic major diameter of the thread, by the amount of the allowance (interference) specified in table 6.

(d) Allowance and tolerance values.—Allowances and tolerances are specified in table 6.

Threads per inch	Interfer- ences or negative allowances	Pitch- diameter tolerances <sup>1</sup>	Lead errors consuming one half of pitch- diameter tolerances <sup>1</sup>	Errors in half angle consuming one half of pitch- diameter tolerances
1	2	3	4	5
28	Inch 0.0002 .0003 .0003 .0004 .0004 .0004 .0005 .0006 .0006 .0006 .0006 .0006 .0008 .0009 .0009 .0010 .0011 .0013	Inch           0.0011           .0012           .0013           .0016           .0018           .0019           .0021           .0023           .0024           .0027           .0030           .0023           .0024           .0030	Inch 0.0003 .0004 .0004 .0005 .0005 .0005 .0006 .0006 .0007 .0007 .0007 .0007 .0007 .0009 .0012 .0012 .0014	$\begin{array}{c} Deg.\ Min. \\ 0 & 35 \\ 0 & 33 \\ 0 & 30 \\ 0 & 31 \\ 0 & 29 \\ 0 & 28 \\ 0$

TABLE 6.—Class 4, close fit, allowances and tolerances for screws and nuts

<sup>11</sup> The tolerances specified for pitch diameter include all errors of pitch diameter, lead, and angle. The full tolerance cannot, therefore, be used on pitch diameter unless the lead and angle of the thread are perfect. Columns 4 and 5 give, for information, the errors in lead (per length of thread engaged) and in angle, each of which can be compensated for by half the tolerance on the pitch diameter given in column 3. If lead and angle errors both exist to the amount tabulated, the pitch diameter of a bolt, for example, must be reduced by the full tolerance or it will not enter the "go" gage. <sup>3</sup> Between any 2 threads not farther apart than the length of engagement.

<sup>1</sup> Including positive control of taps and dies by means of a lead screw. See p. 145.



FIGURE 14.—Illustration of loosest condition for class 4, close fit, one-fourth inch, 20 threads.



FIGURE 15.—Illustration of tightest condition for class 4, close fit, one-fourth inch. 20 threads.

NOTATION D = major diameter E = pitch diameter K = minor diameterh = 0.0325 = basic thread depth



FIGURE 16.—Relation of maximum and minimum pitch diameters of classes 1, 2, 3, and 4 fits to basic pitch diameters.



FIGURE 17.—Limits for minor diameter of nut, American National coarse and fine thread series.

Note.--Tap-drill sizes which fall within these limits are readily determined by subtracting the pitch from the basic major diameter. The resulting diameter corresponds to 77 percent of the basic thread depth.

## 4. TABLES OF LIMITING DIMENSIONS

The limiting dimensions of American National coarse and American National fine threads, to be made to the tolerances and allowances determining the various classes of fit, as herein established, are here tabulated.

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	Basic major diamete		13	Inches 0.0730 .0860 .0990 .1120 .1250	. 1380 . 1640 . 1900 . 2160 . 2500	. 3125 . 3750 . 4375 . 5000 . 5625	. 6250 . 7500 . 8750 1. 0000 1. 1250	1. 2500 1. 3750 1. 5000 1. 7500
	Major	diameter, minimum <sup>3</sup>	12	Inches 0.0730 0.0730 0.0860 0.0860 0.0890 0.1120 1120	. 1380 . 1640 . 1900 . 2160	. 3125 . 3750 . 4375 . 5000 . 5625	. 6250 . 7500 . 8750 1. 0000 1. 1250	1. 2500 1. 3760 1. 5000 1. 7500
	ameter	Max.	11	Inches 0.0655 0.0772 0.0886 0.0886 0.0992 0.0992	$\begin{array}{c} 1215\\ 1475\\ 1675\\ 1935\\ 2226\end{array}$	. 2821 . 3407 . 3981 . 4574 . 5163	$\begin{array}{c} . 5745 \\ . 6942 \\ . 8128 \\ . 9299 \\ 1.0446 \end{array}$	1. 1696 1. 2812 1. 4062 1. 6370 1. 6370
Nut sizes	Pitch d	Min.	10	Inches 0.0629 .0744 .0855 .0958 .1088	$\begin{array}{c} 11177\\ .1437\\ .1629\\ .1889\\ .2175\end{array}$	. 2764 . 3344 . 3911 . 4500 . 5084	. 5660 . 6850 . 8028 . 9188 1. 0322	1. 1572 1. 2667 1. 3917 1. 6201 1. 6201
	iameter	Max.	6	Inches 0.0604 .0715 .0820 .0913 .1043	.1118 .1378 .1541 .1801 .2060	. 2630 . 3184 . 3721 . 4290 . 4850	. 5397 . 6553 . 7689 . 8795 . 9858	1. 1108 1. 2126 1. 3376 1. 5551 1. 7835
	Minor d	Min.	80	Inches 0. 0561 . 0667 . 0764 . 0849 . 0979	.1042 .1302 .1449 .1709	. 2524 . 3073 . 3602 . 4167 . 4723	.5266 .6417 .7547 .8647 .9704	1. 0954 1. 1946 1. 3196 1. 5335
	Minor	diameter, maximum <sup>1</sup>	7	Inches 0. 0531 0. 0633 0. 0633 0. 0633 0. 0633 0. 0933	.0986 .1246 .1376 .1636	. 2427 . 2965 . 3478 . 4034 . 4579	.5109 .6245 .7356 .8432 .9458	1. 0708 1. 1661 1. 2911 1. 4994 1. 7217
	ameter	Min.	9	Inches 0.0596 0.0598 0.0508 0.0708 0.0815 0.0815 0.0914	$ \begin{array}{c}     1128\\     1388\\     1570\\     1830\\     2109\\   \end{array} $	. 2691 . 3263 . 3283 . 3404 . 4981	. 5549 . 6730 . 7897 . 9043 1. 0159	1. 1409 1. 2478 1. 3728 1. 5980 1. 5316
Screw sizes	Pitch di	Max.	νq	Inches 0.0622 0.0736 0.0736 0.0846 0.0948 0.0948	. 1166 . 1426 . 1616 . 1876 . 2160	. 2748 . 3326 . 3890 . 4478 . 5060	$ \begin{array}{c}     5634 \\     . 6822 \\     . 7997 \\     . 9154 \\     1.0283 \\   \end{array} $	1. 1533 1. 2623 1. 3873 1. 6149 1. 6149
	ameter	Min.	4	Inches 0.0671 .0796 .0919 .1042 .1172	.1293 .1553 .1795 .2055 .2383	. 2995 . 3606 . 4214 . 4830 . 5443	$\begin{array}{c} . 6054 \\ . 7288 \\ . 8519 \\ . 9744 \\ 1.0963 \end{array}$	1. 2213 1. 3416 1. 4666 1. 7110 1. 7110
	Major d	Max.	e	Inches 0.0723 0.0552 0.0852 0.0981 0.1110 .1110 .1240	. 1369 . 1629 . 1887 . 2147 . 2485	. 3109 . 3732 . 4978 . 4978	. 6224 . 7472 . 8719 . 9966 1. 1211	1. 2461 1. 3706 1. 4956 1. 7448 1. 7448
	Threads per inch		2	\$6 \$8 \$8 \$6 \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	888333	18 17 13 18 18	10 8 8 8 8 8 8 8	60667 818
	Sizes		1		004			×88.~

TABLE 7 .--- Class 1, loose fit, American National coarse-thread series

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2¼ 2½	415	2, 2443	2, 2075	2, 1000	2, 0816	1.9717	2. 9094	2. 0335	2, 1057	2, 1241	2, 2500	2, 2500
2% 3	4 4	2.7436	2, 7028	2,5812	2.5608	2, 4369	2. 4794	2. 5064	2, 5876 2, 5876 2, 8376	2, 8080 2, 8680 2, 8580	2, 7500 3, 0000	2, 7500 3, 0000
3½	44	3. 2436 3. 4936	3. 2028	3.0812 3.3312	3. 0608 3. 3108	2. 9369 3. 1869	2. 9794 3. 2294	3. 0064 3. 2564	3. 0876 3. 3376	3, 1080 3, 3580	3, 2500	3, 2500 3, 5000
4	ৰ ৰ	3. 7436 3. 9936	3. 9528	3. 5812 3. 8312	3. 5608 3. 8108	3. 4369 3. 6869	3. 4794 3. 7294	3. 5064 3. 7564	3. 5876 3. 8376	3. 6080 3. 8580	3, 7500	3.7500
<sup>1</sup> <sup>3</sup> See footnotes on p. 41.			-						-		-	

1 <sup>2</sup> See footnotes on p. 41.

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		Basic major diameter		13	Inches 0.0730 0.0730 0.0860 0.0990 0.1120 0.1250	. 1380 . 1640 . 1900 . 2160 . 2500	. 3125 . 3750 . 4375 . 5000 . 5625	. 6250 . 7500 . 8750 1. 0000 1. 1250
		Major diameter, minimum		12	Inches 0.0730 0.0730 0.0860 0.0860 0.08900 0.1120 0.1120	. 1380 . 1640 . 1900 . 2160	. 3125 . 3760 . 4376 . 6000 . 5626	. 6250 . 7500 . 8760 1. 0000
		lameter	Max.	п,	Inches 0.0648 0.0764 0.0764 0.0764 0.0982 0.0982 0.1112	. 1204 . 1464 . 1662 . 1922 . 2211	. 2805 . 3389 . 3389 . 3360 . 4552 . 5140	. 5719 . 6914 . 8098 . 9264 1. 0407
Nut sizes		Pitch d	Min.	10	Inches 0.0629 .0744 .0855 .0958 .1088	. 1177 . 1437 . 1629 . 1889 . 2175	. 2764 . 3344 . 3911 . 4500 . 5084	. 5660 . 6850 . 8028 . 9188 1. 0322
		iameter	Max.	6	Inches 0.0604 0.0715 0.0820 0.0913 0.0913	. 1118 . 1378 . 1541 . 1541 . 2060	. 2630 . 3184 . 3721 . 4290 . 4850	. 5397 . 6553 . 7689 . 7689 . 8795 . 9858
		Minor d	Min.	80	Inches 0.0561 0.0667 0.0667 0.0649 0.0849 0.0849	. 1042 . 1302 . 1449 . 1709	. 2524 . 3073 . 3073 . 3167 . 4167 . 4723	. 5286 . 6417 . 7547 . 7547 . 8647 . 9704
		Minor diameter, maximum 1		7	Inches 0.0538 0.0538 0.0534 0641 0734 0813 0043	. 0997 . 1257 . 1389 . 1649 . 1887	. 2443 . 2983 . 3499 . 4056	. 5135 . 6273 . 7387 . 7387 . 9497
		ameter	Min.	9	Inches 0.0610 0724 0833 0034 0034	. 1150 . 1410 . 1596 . 1856 . 2139	. 2723 . 3209 . 3862 . 4448 . 5028	. 5601 . 6786 . 7958 . 9112 1. 0237
sizes		Pitch di	Max.	λQ	Inches 0.0629 0.0524 0.0744 0.0855 0.0958 0.0958 0.1088	. 1177 . 1437 . 1629 . 1889 . 2175	. 2764 . 3344 . 3911 . 4500 . 5084	. 5660 . 6850 . 8028 . 9188 1. 0322
Bcrew	Threaded parts of parts of hot-rolled material		Min.	48	Inchee 0.0678 0.0804 0.0928 0.1052 0.1182	. 1304 . 1564 . 1868 . 2398	. 3011 . 3624 . 4235 . 4852 . 5467	. 6080 . 7316 . 8550 . 9778 1. 1002
	ajor diamete	Semifin- ished and finished bolts and screws	Min.	4	Inches 0.0692 0.0820 0.0946 1072 1072	. 1326 . 1586 . 1834 . 2094	. 3043 . 3660 . 4277 . 4896 . 5513	. 6132 . 7372 . 8610 . 9848 1. 1080
	M	Maximum		ę	Inches 0.0730 0.0730 0.0730 0.0360 0.0390 0.1120 0.1120	.1380 .1640 .1640 .2500	. 3125 . 3750 . 4375 . 5000 . 5625	. 5260 . 7500 1. 0000 1. 1250
·		Threads per inch		5	40 40 40 40 40 40 40 40 40 40 40 40 40 4	\$\$\$\$33	12 13 14 16 18	10 8 8 8 8 8
		Bizes		1	64	88 110 112 112	22%00 24%0 2%%0	588 3948 778 11 196

TABLE 8.-Class 2, free fit, American National coarse-thread series

34

1.2500	1.3750	1. 7500	2,0000	2.2500	2.5000	2.7500	3.0000	0 9600	3, 5000	3.7500	4.0000	
1.2500	1.3750	1.7500	2.0000	2, 2500	2, 5000	2.7500	3.0000	9 9800	3, 5000	3.7500	4.0000	
1. 1667	1. 2768	1. 6317	1.8684	2.1184	2.3516	2.6016	2.8516	3 1018	3.3516	3.6016	3.8516	
1. 1572	T. 2007	1.6201	1.8557	2. 1057	2.3376	2. 5876	2.8376	3 0876	3. 3376	3. 5876	3.8376	
1. 1108	1.2120	1.5551	1.7835	2. 0335	2.2564	2.5064	2.7564	3 0084	3.2564	3.5064	3.7564	-
1.0954	1 2106	1. 5335	1.7594	2,0094	2.2294	2.4794	2.7294	2 0704	3. 2294	3.4794	3.7294	-
1.0747	1 2055	1. 5046	1.7274	1.9774	2, 1933	2.4433	2.6933	2 0433	3. 1933	3.4433	3.6933	-
1. 1487	1 2818	1.6085	1.8430	2.0930	2.3230	2.5736	2.8236	3 0736	3. 3236	3. 5736	3.8236	
1. 1572	1.2007	1.6201	1.8557	2.1057	2.3376	2.5876	2.8376	3, 0876	3. 3376	3. 5876	3.8376	-
1. 2252	1 4710	1. 7162	1.9632	2, 2132	2.4592	2.7092	2.9592	3, 2002	3. 4592	3.7092	3.9592	
1.2330	1 4708	1.7268	1.9746	2. 2246	2.4720	2.7220	2.9720	3, 2220	3.4720	3.7220	3.9720	-
1. 2500	1.5000	1.7500	2.0000	2.2500	2.5000	2.7500	3.0000	3 2500	3.5000	3.7500	4.0000	-
<b>1</b> - a	0 4	0.00	41/2	41/2	4	4	4	4	4	4	4	-
114	11%	134	2	214	2}2	234	3	314	31/2	3¾	4	

1 2 See footnotes on p. 41.

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Inches 0.0730 0.0860 0.0860 0.0990 11120 1120  $\begin{array}{c} 1.\ 2500\\ 1.\ 3750\\ 1.\ 5000\\ 1.\ 7500\\ 2.\ 0000 \end{array}$ 3, 2500 3, 5000 3, 7500 4, 0000  $1640 \\ 1900 \\ 2160 \\ 2500$ 1.00001.12502, 2500 2, 5000 3, 0000 1380 3125 5000 5625 6250 7500 8750 4371 Basic major diameter 13 Inches 0.0730 0.0730 0.0900 11120 .1120 Major diameter, minimum<sup>2</sup>  $\begin{array}{c} . 1380 \\ . 1640 \\ . 1900 \\ . 2160 \\ . 2500 \end{array}$ . 3125 3750 . 4375 . 5000 . 5625  $\begin{array}{c}
 8250 \\
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 1.1250 \\$  $\begin{array}{c} 1.\ 2500\\ 1.\ 3750\\ 1.\ 5000\\ 2.\ 0000\\ 2.\ 25000\\ 2.\ 7500\\ 3.\ 0000\\ 3.\ 0000\\ 3.\ 0000\\ \end{array}$  $\begin{array}{c} 3.\ 2500\\ 3.\ 5000\\ 3.\ 7500\\ 4.\ 0000\end{array}$ 12 Inches 0.0643 .0759 .0871 .0975 . 5702 . 6895 . 8077 . 9242 1. 0381 119614561653191322012794 3376 3947 4537 6124  $\begin{array}{c} 1. & 1631 \\ 1. & 2738 \\ 1. & 3988 \\ 1. & 3988 \\ 1. & 6283 \\ 1. & 8646 \end{array}$ 2. 1146 2. 3473 2. 5973 2. 8473 2. 8473 0973 3473 5973 8473 Max. **Pitch diameter** 11 ന്ന്ന് Inches 0.0629 .0744 .0855 .0958 .1088 . 5660 . 6850 . 8028 . 9188 1. 0322 1437 1629 1889 2175 3344 4500  $\begin{array}{c} 1.\ 1572\\ 1.\ 2667\\ 1.\ 3917\\ 1.\ 6201\\ 1.\ 8557\end{array}$ 2. 1057 2. 3376 2. 5876 2. 5876 2. 8376 0876 3376 5876 8376 2764 Nut sizes Min. 2 က်က်က် Inches 0.0604 .0715 .0820 .0913 .1043 1118  $\begin{array}{c} 2.\ 0335\\ 2.\ 2564\\ 2.\ 5064\\ 2.\ 7564\end{array}$ . 1378 1541 . 1801 . 2060 2630 3184 3721 4200 4850 5397 6553 7689 8795 9858 1. 1108 1. 2126 1. 3376 1. 5551 1. 7835 0064 5064 7564 Max. Minor diameter 6 ന്ന്ന് Inches 0.0561 0.0667 0764 0799 0979  $\begin{array}{c} 1.\ 0954\\ 1.\ 1946\\ 1.\ 3196\\ 1.\ 5335\\ 1.\ 7594\end{array}$ 13021449170919591042 .4723 2. 0094 2. 2294 2. 4794 2. 7294 2.9794 3.2294 3.4794 3.7294 2524 3073 3002 4167 5266 6417 7547 8647 9704 Min. 00 Minor diameter, maximum<sup>1</sup>  $\begin{array}{c} 1.\ 1705\\ 1.\ 2955\\ 1.\ 5046\\ 1.\ 7274 \end{array}$  $\begin{array}{c} . 0997 \\ . 1257 \\ . 1389 \\ . 1649 \\ . 1887 \end{array}$  $\begin{array}{c} 2443\\ 2983\\ 3499\\ 4056\\ 4603\\ \end{array}$ 5135 6273 6273 7387 8466 9497 1.0747  $\begin{array}{c} 2. \ 9433\\ 3. \ 1933\\ 3. \ 4433\\ 3. \ 6933\\ 3. \ 6933 \end{array}$ Inches 0. 0538 . 0641 0734 0813 0943  $\begin{array}{c} 1.\ 9774\\ 2.\ 1933\\ 2.\ 4433\\ 2.\ 6933\\ \end{array}$ Inches 0.0615 .0729 .0839 .0941 .1071 . 1158 .1418.1605.1865 $\begin{array}{r}
 5618 \\
 .6805 \\
 .7979 \\
 .9134 \\
 1.0263 \\
 \end{array}$  $\begin{array}{c} 1.\ 1513\\ 1.\ 2596\\ 1.\ 3846\\ 1.\ 6119\\ 1.\ 8468\\ 1.\ 8468 \end{array}$ 21493312 3875 4463 5044  $\begin{array}{c} 2.\ 0968\\ 2.\ 3279\\ 2.\ 5779\\ 2.\ 8279\end{array}$ 3.0779 3.3279 3.5779 3.8279 2734 Min. Pitch diameter 9 Inches 0. 0629 . 0744 . 0855 . 5660 . 6850 . 8028 . 9188 1. 0322 Screw sizes .0958.2175 0876 3376 5876 8376 . 1437 . 1629 . 1889  $\begin{array}{c} 1.\ 1572\\ 1.\ 2667\\ 1.\ 3917\\ 1.\ 6201\\ 1.\ 8557\\ \end{array}$ 2. 1057 2. 3376 2. 5876 2. 5876 2. 8376 2764 3344 4500 5084 Max. 10 00000  $Inches \\ 0.0692 \\ 0.0820 \\ 0.0946 \\ 0.1072 \\ 0.1072 \\ 0.1202 \\ 0.1202 \\ 0.020 \\ 0.00$  $\begin{array}{c}
 & 6132 \\
 & 7372 \\
 & 8610 \\
 & 9848 \\
 & 9848 \\
 \end{array}$ 1.1080  $\begin{array}{c} 1.\ 2330\\ 1.\ 3548\\ 1.\ 4798\\ 1.\ 7268\\ 1.\ 9746 \end{array}$  $\begin{array}{c} 2.\ 2246\\ 2.\ 4720\\ 2.\ 7220\\ 2.\ 9720\\ \end{array}$  $\begin{array}{c}
1326\\
1586\\
1834\\
2094\\
2428\\
\end{array}$  $\begin{array}{c} 3043 \\ 3660 \\ 4277 \\ 4896 \\ 5513 \end{array}$ 2220 4720 9720 Min. Major diameter 4 ന്ന്ന് Inches 0. 0730 . 0860 1380 1640 1900 2160 2500  $\begin{array}{c} 3125\\ 3750\\ 4375\\ 5626\end{array}$  $\begin{array}{c} 1.\ 2500\\ 1.\ 3750\\ 1.\ 5000\\ 1.\ 7500\\ 2.\ 0000 \end{array}$ 6250  $\begin{array}{c}
 7500 \\
 8750 \\
 1.0000 \\
 1.1250 \\
 \end{array}$  $\begin{array}{c} 2.\ 2500\\ 2.\ 5000\\ 3.\ 0000\\ 3.\ 0000 \end{array}$  $1120 \\ 1250$ 2500 5000 0000 0660 Max. ŝ ന്ന്ന് Threads per inch 12 12 101 08 2 ~ 8 8 9 ~ S------S  $1\hat{3}\hat{4}$ ......................... -------Sizes -136. 782 372 2228 334 æ 00 X X \*\* ci ~ 10  $\alpha$ 

1 2 See footnotes on p. 41.

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	Basic major diameter		13	Inches 0. 2500 3125 . 3750 . 4375	. 5000 . 5625 . 6250 . 7500	. 8750 1. 0000 1. 1250 1. 2500	1.3750 1.5000 1.7500 2.0000	2. 2500 2. 5000 3. 0000	3. 2500 3. 7500 4. 0000
	Major	minimum <sup>2</sup>	12	Inches 0. 2500 . 3125 . 3750 . 4375	. 5000 . 5625 . 6250 . 7500	.8750 1.0000 1.1250 1.2500	1. 3750 1. 5000 1. 7500 2. 0000	2.2500 2.5000 3.0000	3. 2500 3. 5000 3. 7500 4. 0000
	ameter	Max.	11	Inches 0. 2188 . 2779 . 3360 . 3929	. 4519 . 5104 . 5681 . 6873	. 8052 . 9215 1. 0352 1. 1602	1: 2703 1. 3953 1. 6242 1. 8601	2. 1101 2. 3424 2. 5924 2. 8424	3. 0924 3. 3424 3. 5924 3. 8424 3. 8424
Nut sizes	Pitch di	Min.	10	Inches 0. 2175 . 2764 . 3344 . 3344	. 4500 . 5084 . 5660 . 6860	. 8028 . 9188 1. 0322 1. 1572	1.2667 1.3917 1.6201 1.8557	2. 1057 2. 3376 2. 5876 2. 8376 2. 8376	3. 0876 3. 3376 3. 5876 3. 8376 3. 8376
	ameter	Max.	6	Inches 0. 2060 . 2630 . 3184 . 3721	. 4290 . 4850 . 5397 . 6553	. 7689 . 8795 . 9858 1. 1108	1. 2126 1. 3376 1. 5551 1. 7835	2. 0335 2. 2564 2. 5064 2. 7564	3. 0064 3. 2564 3. 5664 3. 7564
	Minor di	Min.	80	Inches 0. 1959 . 2524 . 3073 . 3002	. 4167 . 4723 . 5266 . 6417	. 7547 . 8647 . 9704 1. 0954	1. 1946 1. 3196 1. 5335 1. 7594	2. 0094 2. 2294 2. 7294 2. 7294	2. 9794 3. 2294 3. 4794 8. 7294
	Minor	maximum <sup>1</sup>	7	Inches 0. 1887 2443 . 2983 . 3499	. 4056 . 4603 . 5135 . 6273	. 7387 . 8466 . 9497 1. 0747	1. 1705 1. 2955 1. 5046 1. 7274	1. 9774 2. 1933 2. 4433 2. 6933	2. 9433 3. 1933 3. 4433 3. 6933
	ameter	Min.	9	Inches 0. 2165 . 2752 . 3332 . 3897	. 4485 . 5069 . 5044 . 6833	. 8010 . 9168 1. 0300 1. 1550	1. 2640 1. 3890 1. 6170 1. 8524	2, 1024 2, 3341 2, 5841 2, 5841 2, 8341	3. 0841 3. 3341 3. 5841 3. 8341
Screw sizes	Pitch di	Max.	ъ	Inches 0. 2178 . 2767 . 3348 . 3345	. 4504 . 5089 . 5665 . 6866	. 8034 . 9195 1. 0330 1. 1580	1. 2676 1. 3926 1. 8568 1. 8568	2, 1068 2, 3389 2, 5889 2, 8389 2, 8389	3. 0889 3. 3389 3. 5889 3. 8389
	ameter	Min.	4	Inches 0. 2428 3043 3660 . 4277	. 4896 . 5513 . 6132 . 7372	. 8610 . 9848 1. 1080 1. 2330	1. 3648 1. 4708 1. 7268 1. 9746	2. 2246 2. 4720 2. 9720 2. 9720	3. 2220 3. 4720 3. 7220 3. 9720
	Major d	Max.	ຕ	Inches 0. 2500 . 3126 . 3750 . 4375	. 5000 . 5825 . 6250 . 7500	. 8750 1. 0000 1. 1250 1. 2500	1. 3750 1. 5000 1. 7500 2. 0000	2, 2500 2, 5000 3, 7500 3, 0000	3. 2500 3. 5000 3. 7500 4. 0000
	Threads per inch		2	20 16 14	11123	0.00	6 5 4 <u>1/</u> 2	4444 2 2 2	<del>र</del> ी से से से
	Sizes		1	240 260	2000 2000 2000 2000 2000 2000	88 194 194	38 141 18	244	222 222 222

1 2 See footnotes on p. 41.

TABLE 10.—Class 4, close fit, American National coarse-thread series

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TABLE

	Basic major diameter		13	Inches 0.060C 0.0860 0.0860 0.0990	. 1250 . 1380 . 1640 . 1900 . 2160	. 2500 . 3125 . 3756 . 4375	. 5625 . 6250 . 7500 . 8750 1. 0000	1. 1250 1. 2500 1. 3750 1. 5000
	Major	minimuna"	12	Inches 0.0600 0.0730 0.0730 0.0730 0.0860 0.0990 0.0990	. 1250 . 1380 . 1640 . 1900 . 2160	. 2500 . 3126 . 3750 . 4375 . 5000	. 5625 . 5250 . 7500 1. 0000	1. 1250 1. 2500 1. 3760 1. 5000
	lameter	Mar.	11	Inches 0.0543 0.0543 0.0865 0785 0785 0785	. 1134 . 1262 . 1496 . 1736	. 2311 . 2900 . 3525 . 4101 . 4726	. 5321 . 5946 . 7157 . 8356 . 9606	1. 0788 1. 2038 1. 3288 1. 4538
Nut sizes	Pitch d	Mir.	10	Inches 0.0519 0640 0759 0874 0885	. 1102 . 1218 . 1460 . 1928	. 227:3 . 2854 . 8479 . 4675	. 5264 . 5889 . 7094 . 8286 . 9536	1. 0709 1. 1959 1. 3209 1. 4459
	lameter	Max.	6	Inches 0.0492 0.0492 0610 0724 0834	. 1049 . 1158 . 1391 . 1318 . 1833	. 2173 . 2739 . 3364 . 3306	. 5100 . 5725 . 6923 . 6923 . 6923 . 9312	1. 0438 1. 1688 1. 2938 1. 4188
	Minor d	Min.	æ	Inches 0.0465 0.0465 0580 0.0580 0.0581 0.0581 0.0591	. 1004 . 1109 . 1339 . 1562 . 1773	. 2113 . 2674 . 3299 . 3834	. 5024 . 5649 . 6823 . 7977 . 9227	1. 0348 1. 1598 1. 2848 1. 4098
	Minor	maximum 1	7	Inches 6. 0440 . 0553 . 0563 . 0763 . 0763	. 0962 . 1063 . 1288 . 1288 . 1710	. 2060 . 2601 . 3228 . 3747 . 4372	. 4927 . 5552 . 6715 . 7853 . 9103	1. 0204 1. 1464 1. 2704 1. 3964
	ameter	Min.	9	Inches 0.0488 0.0488 0.0488 0.0488 0.0488 0.04838 0.0838 0.0838	. 1061 . 1174 . 1413 . 1648 . 1873	. 2213 . 2795 . 3984 . 3600	. 5191 . 5816 . 7013 . 8195 . 9445	1. 0606 1. 1856 1. 3106 1. 4356
Screw sizes	Pitch di	Max.	145)	Inches 0.0512 0.0533 0.0533 0.0586 0.0586 0.0866 0.0866	. 1093 . 1208 . 1440 . 1686 . 1916	. 2256 . 2841 . 3466 . 4660	. 5248 . 5873 . 7076 . 8265 . 9515	1. 0685 1. 1935 1. 2185 1. 4435
	iameter	Min.	4	Inches 0.0545 0.0545 0.0873 0801 0801 0826	. 1177 . 1302 . 1367 . 1813 . 2062	. 2402 . 3020 . 4258 . 4258	$ \begin{array}{c} 5495\\ 6120\\ 7356\\ 8689\\ 8889\\ 9839 \end{array} $	1. 1068 1. 2318 1. 3565 1. 4818
	Major d	Max.	<b>6</b> 5	Inches 0.0693 0.0583 0.0853 0.0853 0.0882 0.0882	. 1241 . 1370 . 1629 . 1859 . 2148	. 2488 . 3112 . 3737 . 4360 . 4985	. 6009 . 6234 . 7482 . 8729 . 9979	1. 1226 1. 2476 1. 3728 1. 4976
	Threads per inch		61	85223	49888	***	18 18 14	121212
	Sizes	1	-			100	8	

<sup>1 2</sup> See footnotes on p. 41.

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	Basic major diameter		13	Inches 0.0600 0.0860 0.0860 0.0990 0.0990 0.1120	. 1250 . 1380 . 1640 . 1900 . 2160	. 2500 . 3125 . 3750 . 4375 . 5000	. 5625 . 6250 . 7500 . 8750 1. 0000	1. 1250 1. 2500 1. 3750 1. 5000
	Major	minimum'	12	Inches 0.0600 0.0500 0.0730 0.0860 0.0990 0.0990	. 1250 . 1380 . 1640 . 1900 . 2160	. 2500 . 3125 . 3750 . 4375 . 4375	. 5625 . 5625 . 7500 . 7500 1. 0000	1. 1250 1. 2500 1. 3750 1. 5000
	ameter	Max.	11	Inches 0.0556 0.0558 0.0658 0.0778 0.0778 0.0778 0.0894	. 1125 . 1242 . 1485 . 1724 . 1959	. 2299 . 2887 . 3512 . 4086	. 5305 . 5305 . 7139 . 7139 . 8335 . 9585	1. 0765 1. 2015 1. 3265 1. 4515
Nut sizes	Pitch di	Min.	10	Inches 0.0519 0.0540 0.0540 0.0540 0.0759 0.0759 0.0874	. 1102 . 1218 . 1460 . 1697 . 1928	. 2268 . 2854 . 3879 . 4050	. 5264 . 5889 . 7094 . 8286 . 9536	1. 0709 1. 1959 1. 3209 1. 4459
	lameter	Max.	6	Inches 0.0492 0.0492 0.0510 0724 0.0334 0.0334	. 1049 . 1158 . 1391 . 1618 . 1833	. 2173 . 2739 . 3364 . 3906 . 4531	. 5100 . 5725 . 6923 . 8062 . 9312	1. 0438 1. 1688 1. 2938 1. 4128
	Minor d	Min.	80	Inches 0.0465 0.0580 0.0580 0.0591 0.0797 0.0797	. 1004 . 1109 . 1339 . 1562 . 1773	. 2113 . 2674 . 3299 . 3834 . 4459	. 5024 . 5649 . 6823 . 7977 . 9227	$\begin{array}{c} 1.\ 0348\\ 1.\ 1598\\ 1.\ 2348\\ 1.\ 2948\\ 1.\ 4098 \end{array}$
	Minor	maximum 1	7	Inches 0.0447 0.0580 0.0580 0.0580 0.0580 0.0771	. 0971 . 1073 . 1299 . 1517 . 1722	. 2062 . 2614 . 3239 . 3762 . 4387	. 4943 . 5568 . 6733 . 7874 . 9124	1. 0228 1. 1478 1. 2728 1. 3978
	lameter	Min.	9	Inches 0.0602 0622 0654 0864 0864	. 1079 . 1194 . 1435 . 1670 . 1897	. 2237 . 2821 . 3446 . 4014 . 4639	. 5223 . 5848 . 7049 . 8237 . 9487	1.0653 1.1903 1.3153 1.4403
Screw sizes	Pitch d	Max.	٤Q	Inches 0.0519 0.0640 0.0580 0.0759 0.0875	.1102 .1218 .1460 .1697	2268 2854 3479 4050	5284 5889 7094 8286	1. 0709 1. 1959 1. 3209 1. 4459
	iameter	Min.	4	Inches 0.0586 0.0586 0.0584 0.0844 0.0822 0.0950 0.0950	.1204 .1332 .1530 .1590 .1846	. 2438 . 3059 . 3694 . 4303 . 4928	$     \begin{array}{c}       5543 \\       6168 \\       7410 \\       8652 \\       9902 \\       902     \end{array} $	1. 1138 1. 2388 1. 3638 1. 4888
	Major d	Max.	es	Inches 0.0600 0.0730 0.0860 0.0860 0.0990 0.0990	. 1250 . 1380 . 1640 . 1900	. 2500 . 3125 . 3750 . 4375 . 5000	. 5625 . 6250 . 7500 . 8750 1. 0000	1. 1250 1. 2500 1. 3750 1. 6000
	Threads per inch		63	\$28 \$738 \$8	<b>\$</b> \$888	****	18 16 14 14	2222
	Sizes		1	013.84	5. 8.8 10. 12.	2440 2450 2410 2410	96.6 565 248 1	116 114 118

TABLE 12.-Class 2, free fit, American National fine-thread series

1 3 See footnotes on p. 41.

ser
fine-thread
National
American
fit,
medium
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13Class
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Inches 0.0600 0.0730 0.0860 0.0990 0.1120 .1250.1380.1640.1900.2160.5625.6250.7500.8750.87501.0000 $\begin{array}{c} 1.\ 1250\\ 1.\ 2500\\ 1.\ 3750\\ 1.\ 5000\\ 1.\ 5000 \end{array}$ 250031253750375037503750Basic major diameter 13 Inches 0.0600 0.0860 0.0860 0.0990 0.1120 Major diameter, minimum<sup>3</sup> .5625.6250.7500.8750.87501250. 1250. 1380. 1640. 1900. 2160. 2160. 250031253750375037503750 $\begin{array}{c} 1.\ 1250\\ 1.\ 2500\\ 1.\ 3750\\ 1.\ 5000\\ \end{array}$ 12 Inches 0. 0532 0. 0653 0. 0653 0773 0773 0773 0773 0773 0773 . 1118 . 1235 . 1478 . 1716 . 1950 22902878350340764701.5294.5919.7126.8322.9572 $\begin{array}{c} 1.\ 0749\\ 1.\ 1999\\ 1.\ 3249\\ 1.\ 4499\\ 1.\ 4499 \end{array}$ Max. **Pitch diameter** Π Inches 0.0519 0.0540 0.0759 0.0759 0.0874  $\begin{array}{c}
 1102 \\
 1218 \\
 11460 \\
 1697 \\
 1928 \\
 \end{array}$ 1. 0709 1. 1959 1. 3209 1. 4459  $\begin{array}{c} 2268\\ 2854\\ 3479\\ 4050\\ 4675\end{array}$ 526452645889709482869536Nut sizes Min. 9 Inches 0.0492 0.0610 .0724 .0834 .0834 .0837 .1049.1158.1391.1618.1833217327393364336439064531 $\begin{array}{c} 1.\ 0438\\ 1.\ 1688\\ 1.\ 2938\\ 1.\ 2938\\ 1.\ 4188 \end{array}$ .5100.5725.6903.8062.9312Max. Minor diameter ຸ Inches 0.0465 0.0580 0691 0797 .0797 .1004.1109.1339.1562.177321132674329938344459 $\begin{array}{c} 1.\ 0348\\ 1.\ 1598\\ 1.\ 2848\\ 1.\ 2848\\ 1.\ 4098\end{array}$ 5024 5649 6823 6823 9227 Mip. 00 Inches 0.0447 0.0560 0.0668 0.0668 0.0771 0.0771 Minor diameter, maximum<sup>1</sup> . 0971 . 1073 . 1299 . 1517 . 1722 20622614323937624387 $\begin{array}{c} 1.\ 0228\\ 1.\ 1478\\ 1.\ 2728\\ 1.\ 3978\\ 1.\ 3978 \end{array}$ 4943 5568 6733 6733 9124 Ŀ-Inches 0.0506 0.0527 0.0527 0.045 0.0859 0.0869  $\begin{array}{c} 1.\ 0669\\ 1.\ 1919\\ 1.\ 3169\\ 1.\ 4419\\ \end{array}$  $\begin{array}{c} . \ 1086 \\ . \ 1201 \\ . \ 1442 \\ . \ 1678 \\ . \ 1906 \end{array}$  $\begin{array}{c} 2246\\ 2830\\ 3455\\ 4024\\ 4649\\ 4649\end{array}$ 5234 5859 5859 7062 8250 9500 Min. 9 **Pitch diameter** Inches 0.0519 0.0540 0.0559 0.0759 0.0759 0.0374 Screw sizes .1102.1218.1460.1697.1928 $\begin{array}{c} 1.\ 0709\\ 1.\ 1959\\ 1.\ 3209\\ 1.\ 4459\\ 1.\ 4459 \end{array}$ 22682854347940504675 $\begin{array}{c} 5264 \\ 5889 \\ 7094 \\ 8286 \\ 9536 \end{array}$ Max. 10 Inches 0.0566 0.0566 0.0822 0.0950 0.0950 1204133215901846209824383059368443034928 $\begin{array}{c} 1.\ 1138\\ 1.\ 2388\\ 1.\ 3638\\ 1.\ 4888\\ 1.\ 4888\end{array}$ .5543.6168.7410.8652.9902Min. Major diameter -Inches 0.0600 0.0860 0.0860 0.0990 0.0120 . 5625 . 6250 . 7500 . 8750 1. 0000 25003125375043755000.1250.1380.1640.1900.2160 $\begin{array}{c} 1.\ 1250\\ 1.\ 2500\\ 1.\ 3750\\ 1.\ 5000\\ 1.\ 5000 \end{array}$ Max. 3 Threads per inch 8118 1212 82388 498888 822288 2 Sizes 5%.--16-2%22 \* 3 8%7% 121 10 6

12 See footnotes on p. 41.

NATIONAL SCREW THREAD COMMISSION

series
fine-thread
National.
American
fit,
close
4,
4Class
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TABLE

				Screw sizes					Nut sizes			
Sizes	Threads per inch	Major d	iameter	Pitch di	ameter	Minor	Minor d	iameter	Pitch di	ameter	Major	Basic major diameter
		Max.	Min.	Max.	Min.	maximum 1	Min.	Max.	Min.	Max.	minimum <sup>3</sup>	
1	8	3	4	ũ	9	1	œ	6	10	n	12	13
	****	Inches 0. 2500 . 3125 . 3750 . 4375	Inches 0. 2438 3659 3684 3684 3684	Inches 0. 2270 . 2857 . 3482 . 4053	Inches 0. 2259 . 2845 . 3470 . 4040	Inches 0.2062 .2014 .3239 .3762	Inches 0. 2113 0. 2113 . 3299 . 3329	Inches 0. 2173 . 2739 . 3364 . 3906	Inches 0. 2268 . 2854 . 3279 . 4050	Inches 0.2279 0.2279 .3491 .4063	Inches 0.2500 .3125 .3750 .4375	Inches 0. 2500 . 3125 . 3750 . 4375
	20 81 81 81 81 81 81 81 81 81 81 81 81 81	. 5000 . 5625 . 6250 . 7500 . 7500	. 4928 . 5543 . 6168 . 7410 . 8652	. 4678 . 5267 . 5892 . 7098 . 8290	$\begin{array}{c} 4665\\ 5252\\ 5877\\ 7082\\ 8272\\ 8272\\ \end{array}$	. 4387 . 4943 . 5568 . 6733 . 7874	$ \begin{array}{c} 4459\\ .5024\\ .5649\\ .6823\\ .7977\\ \end{array} $	. 4531 . 5100 . 5725 . 6903 . 8062	. 4675 . 5264 . 5889 . 7094 . 8286	. 4688 . 5279 . 5904 . 7110 . 8304	. 5000 . 5625 . 6250 . 7500 . 7500	. 5000 . 5625 . 6250 . 7500 . 7500
	12222	1.0000 1.1250 1.2500 1.3750 1.5000	. 9902 1. 1138 1. 2388 1. 3638 1. 4888	. 9540 1. 0714 1. 1964 1. 3214 1. 4464	. 9522 1. 0694 1. 1944 1. 3194 1. 4444	.9124 1.0228 1.1478 1.2728 1.3978	. 9227 1. 0348 1. 1598 1. 2848 1. 2848 1. 4098	. 9312 1. 0438 1. 1688 1. 2938 1. 4188	. 9536 1. 0709 1. 1959 1. 3209 1. 4459	.9554 1.0729 1.1979 1.3229 1.4479	1. 0000 1. 1250 1. 2500 1. 3750 1. 5000	1. 0000 1. 1250 1. 2500 1. 3750 1. 5000
Dimensions given for the n diameter of the screw shall b (or 0 40650) from the m	be that co	minor diamet rresponding t	er of the scre to a flat at the	e minor diam	d to the inte neter of the m	rrsection of th	te worn tool aw equal to }	arc with a ce \$Xp, and me	arter line thr ay be determ	ough crest a ined by sub	nd root. Th tracting the	le minimum basic thread

deput, n or to easy, from the minimum pitter of takened of the sciew. <sup>1</sup> Intensions for the minimum major diameter of the nut correspond to the basic flat ( $\beta \times p$ ), and the profile at the major diameter produced by a worn tool must not fall below <sup>1</sup> Intensions for the minimum major diameter of the nut corresponding to a flat at the major diameter of the maximum nut equal to  $\beta_4 \times p$ , and may be determined by adding 196×K (or 0.7939p) to the maximum pitch diameter of the nut.

TABLE 15.-Limiting dimensions and telerances, classes 1, 2, 3, and 4 fits, American National coarse-thread series

						Mac	shine scr	9w numk	er or noi	minal siz	D					
	-	2	en	4	2	9	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	10	12	74	\$16	3%	7/10	*	9/16	58
					-			Threads ]	per inch	•			-		-	
	64	56	48	40	40	32	32	24	24	30	18	16	14	13	12	11
BOLTS AND SCREWS Mar. Jass 1, major diameter	Inch 0.0723 .0671 .0052	Inch 0.0852 .0796 .0056	Inch 0.0981 .0019 .0062	$\begin{array}{c}Inch\\0.1110\\.1042\\.0068\end{array}$	Inch 0.1240 .1172 .0068	Inch 0. 1369 . 1293 . 0076	Inch 0. 1629 . 1553 . 0076	Inch 0. 1887 . 1795 . 0092	Inch 0. 2147 . 2055 . 0092	Inch 0. 2485 . 2383 . 0102	Inch 0.3109 .2995 .0114	Inch 0.3732 .3606 .0126	Inch 0. 4354 . 4214 . 0140	Inch 0.4978 .4830 .0148	Inch 0.5601 .5443 .0158	Inch 0. 6224 . 6054 . 0170
lasses 2, 3, and 4, major diameter{Mar_ Tol	.0730 .0692 .0038	.0860 .0820 .0040	. 0990 . 0946 . 0044	. 1120 . 1072 . 0048	.1250 .1202 .0048	. 1380 . 1326 . 0054	. 1640 . 1586 . 0054	. 1900 . 1834 . 0066	. 2160 . 2094 . 0066	. 2500 2428 .0072	. 3125 . 3043 . 0082	. 3750 . 3660 . 0090	.4375 .4277 .0098	. 5000 . 4896 . 0104	. 5625 . 5513 . 0112	.6250 .6132 .0118
Mass 2, major diameter (threaded [Max. parts of unfinished, hot-rolled Min. material)		.0860 .0804 .0056	. 0990 . 0928 . 0062	.1120 .1052 .0068	.1250 .1182 .0068	. 1380 . 1304 . 0076	. 1640 . 1564 . 0076	. 1900 . 1808 . 0092	. 2160 . 2068 . 0092	2500 2398 0102	. 3125 . 3011 . 0114	. 3750 . 3624 . 0126	.4375 .4235 .0140	. 5000 . 4852 . 0148	. 5625 . 5467 . 0158	. 6250 . 6080 . 0170
lass 1, minor diameterMax. <sup>1</sup> .	. 0531	. 0633	.0725	. 0803	. 0933	.0986	.1246	. 1376	.1636	. 1872	. 2427	. 2965	.3478	.4034	.4579	.5109
lasses 2, 3, and 4, minor diameter.Max. <sup>1</sup> .	. 0538	.0641	.0734	.0813	. 0943	.0907	.1257	.1389	. 1649	. 1887	. 2443	. 2983	. 3499	. 4058	.4603	.5135
) lass 1, loose fit, pitch diameter $\left\{ \begin{matrix} Max.\\ Min.\\ Tol \end{matrix} \right.$	.0622	.0736 .0708 .0028	.0846 .0815 .0031	. 0948 . 0914 . 0034	.1078 .1044 .0034	.1166 .1128 .0058	. 1426 . 1388 . 0038	.1616	.1876 .1830 .0046	. 2160 . 2109 . 0051	. 2748 . 2691 . 0067	. 3326 . 3263 . 0063	. 3890 . 3820 . 0070	. 4478 . 4404 . 0074	. 5060 . 4981 . 0079	. 5634 . 5549 . 0085
)lass 2, free fit, pitch diameter $Max$ . Tol	.0629	.0744 .0724 .0020	.0855 .0833 .0022	. 0958 . 0934 . 0024	.1083	.1177	. 1437 . 1410 . 0027	.1629 .1596 .0033	.1889 .1856	. 2175 . 2139 . 0036	. 2764 . 2723 . 0041	. 3344 . 3299 . 0045	. 3911 . 3862 . 0049	. 4500 . 4448 . 0052	. 5084 . 5028 . 0056	. 5660 . 5601 . 0059
)lass 3, medium fit, pitch diameter-{Max. Min. Tol		.0744 .0729 .0015	.0855 .0839 .0016	. 0958 . 0941 . 0017	.1088	. 1177	. 1437 . 1418 . 0019	.1629 .1605 .0024	.1889 .1865 .0024	. 2175 . 2149 . 0026	. 2764 . 2734 . 0030	. 3344 . 3312 . 0032	. 3911 . 3875 . 0036	. 4500 . 4463 . 0037	. 5084 . 5044 . 0040	. 5660 . 5618 . 0042
)lass 4, close fit, pitch diameter {Max. Min. Tol										. 2178 . 2165 . 0013	. 2767 . 2752 . 0015	. 3348 . 3332 . 0016	. 3915 . 3897 . 0018	.4504 .4485 .0019	5089 5069 0020	. 5665 . 5644 . 0021

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# DIMENSIONAL LIMITS OF FASTENING-SCREW THREADS 43

250	397 266 131	660	745 085	719 059	702 042	681 021	
	66.6	. 51	50	200	100	0.0	
. 5625	.4850	. 5084	. 5163	. 5140	.5124	. 0020	
. 5000	.4290 .4167 .0123	.4500	. 4574	. 4552	.4537	.4519	
. 4375	.3721 .3602 .0119	. 3911	.3981	. 3960	. 3947	. 3929	p. 49.
.3750	.3184 .3073 .0111	. 3344	. 3407	. 3389	. 3376	. 3360	ote 3 on
.3125	. 2630 . 2524 . 0106	. 2764	. 2821	.2805	2794	. 2779	See footn
. 2500	. 2060 . 1959 . 0101	.2175	. 2226	. 2211	. 2201	.2188	
.2160	.1801 .1709 .0092	. 1880	. 1935	. 1922	. 1913		
. 1900	.1541 .1449 .0092	.1629	. 1675	. 1662	.1653		
.1640	. 1378 . 1302 . 0076	. 1437	. 1475	.1464	. 1456		p. 49.
.1380	.1118 .1042 .0076	.1177	1215	.1204	. 1196		tote 2 on
.1250	. 1043 .0979 .0064	.1088	. 1122	. 1112	. 1105		See footr
.1120	.0913 0849 .0064	. 0958	.0992	.0982	.0975		-
. 0990	.0820 .0764 .0056	. 0855	.0886	.0877	.0016		
. 0880	0715 0667 0048	.0744	.0772	.0020	.0759		
. 0730	.0604 .0561	. 0629	.0655	.0648	.0643		i p. 49.
lasses 1, 2, 3, and 4, major diameter_Min. <sup>3</sup>	lasses 1, 2, 3, and 4, minor diameter. [Max [Tol	lasses 1, 2, 3, and 4, pitch diameter_Min	tass 1, loose fit, pitch diameter{ <sup>Max,3</sup> Tol	lass 2, free fit, pitch diameter{ <sup>Max.3</sup> - Tol	lass 3, medium fit, pitch diameter_{Tol	ass 4, close fit, pitch diameter $\dots \{T_{0}\}$	<sup>1</sup> See footnote 1 or

									Sizes								
	34	3/8	1	11/8	11/4	13/8	$1^{1/2}_{1/2}$	134	2	2}4	21⁄2	23/4	3	3}4	3½2	334	4
								Thre	ads per i	nch	-				-	-	
	10	6	90	2	7	8	9	5	41/2	41/2	4	4	4	4	4	4	4
BOLTS AND SCREWS	4	1	1			-											
Class 1, major diameter{Min Tol	. 7288 . 7288 . 0184	лиси 0. 8719 . 8519 . 0200	итси 0. 9966 . 9744 . 0222	1. 1211 1. 1211 1. 0963 . 0248	1. 2461 1. 2461 1. 2213 . 0248	171Che8 1.3706 1.3416 .0290	<i>Inches</i> 1. 4956 1. 4666 . 0290	Inches 1. 7448 1. 7110 . 0338	Inches 1. 9943 1. 9575 . 0368	Inches 2. 2443 2. 2075 . 0368	Inches 2. 4936 2. 4528 . 0408	Inches 2. 7436 2. 7028 . 0408	Inches 2. 9936 2. 9528 . 0408	Inches 3. 2436 3. 2028 . 0408	Inches 3. 4936 3. 4528 . 0408	Inches 3. 7436 3. 7028 . 0408	Inches 3. 9936 3. 9528 . 0408
Classes 2, 3, and 4, major Min- diameter Tol	. 7500	. 8750 . 8610 . 0140	1.0000 .9848 .0152	1. 1250 1. 1080 . 0170	$\begin{array}{c} 1.\ 2500\\ 1.\ 2330\\ .\ 0170\end{array}$	$1.3750 \\ 1.3548 \\ .0202$	$\begin{array}{c} 1.5000\\ 1.4798\\ .0202\end{array}$	$\begin{array}{c} 1.7500 \\ 1.7268 \\ 1.0232 \end{array}$	$\begin{array}{c} 2.\ 0000\\ 1.\ 9746\\ .\ 0254 \end{array}$	2. 2500 2. 2246 . 0254	2.5000 2.4720 .0280	2. 7500 2. 7220 . 0280	3.0000- 2.9720 .0280	3. 2500 3. 2220 . 0280	3.5000 3.4720 .0280	3. 7500 3. 7220 . 0280	4.0000 3.9720 .0280
Class 2, major diameter [Max (threaded parts of unfin-]Min ished, hot-rolled material) [Tol	. 7316	. 8750 . 8550 . 0200	1.0000 .9778 .0222	1. 2500 1. 1002 . 0248	$\begin{array}{c} 1.\ 2500\\ 1.\ 2252\\ .\ 0248 \end{array}$	$1.3750 \\ 1.3460 \\ .0290$	$\begin{array}{c} 1.5000\\ 1.4710\\ .0290\end{array}$	1. 7500 1. 7162 1. 0338	2.0000 1.9632 .0368	2. 2500 2. 2132 . 0368	2.5000 2.4592 .0408	2.7500 2.7092 .0408	3. 0000 2. 9592 . 0408	3.2500 3.2002 .0408	3. 5000 3. 4592 . 0408	3. 7500 3. 7092 . 0408	4.0000 3.9592 .0408
Class 1, minor diameterMax.1.	. 6245	. 7356	. 8432	. 9458	1.0708	1, 1661	1. 2911	1. 4994	1.7217	1. 9717	2. 1869	2.4369	2.6869	2. 9369	3.1869	3. 4369	3.6869
eterMaxin T, muur utam-	. 6273	. 7387	. 8466	. 9497	1.0747	1.1705	1. 2955	1.5046	1.7274	1.9774	2. 1933	2.4433	2.6933	2.9433	3. 1933	3.4433	3. 6933
Class 1, loose fit, pitch di- Max- ameter	. 6822 . 6730 . 0092	7997 . 7897 . 00100	. 9154 . 9043 . 0111	1.0283 1.0159 .0124	1. 1533 1. 1409 . 0124	$1.2623 \\ 1.2478 \\ .0145$	1. 3873 1. 3728 . 0145	1. 6149 1. 5980 . 0169	1.8500 1.8316 .0184	2.1000 2.0816 .0184	2.3312 2.3108 .0204	2.5812 2.5608 .0204	2.8312 2.8108 .0204	3. 0812 3. 0608 . 0204	3.3312 3.3108 .0204	3.5812 3.5608 .0204	3.8312 3.8108 .0204
Class 2, free fit, pitch diam-{Max eter	. 6850 . 6786 . 0064	. 8028 . 7958 . 0070	.9188 .9112 .0076	$   \frac{1.0322}{1.0237} $	$\begin{array}{c} 1.\ 1572\\ 1.\ 1487\\ .\ 0085\end{array}$	$1.2667\\1.2566\\.0101$	1. 3917 1. 3816 . 0101	1. 6201 1. 6085 1. 6085 . 0116	$\begin{array}{c} 1.8557\\ 1.8430\\ .0127\end{array}$	2. 1057 2. 0930 . 0127	2.3376 2.3236 .0140	2.5876 2.5736 .0140	2.8376 2.8236 .0140	3.0876 3.0736 .0140	3.3376 3.3236 3.3236 .0140	3.5876 3.5736 .0140	3.8376 3.8236 3.0140
Class 3, medium fit, pitch Max diameter	6850 . 6805 . 0045	. 8028 . 7979 . 0049	.9188 .9134 .0054	$   \begin{array}{c}     1.0322 \\     1.0263 \\     .0059   \end{array} $	$   \begin{array}{c}     1.1572 \\     1.1513 \\     1.0059   \end{array} $	1.2667 1.2596 .0071	$\begin{array}{c} 1.\ 3917\\ 1.\ 3846\\ .\ 0071 \end{array}$	1.6201 1.6119 .0082	$\begin{array}{c} 1.8557\\ 1.8468\\ 1.8468\\ .0089\end{array}$	2. 1057 2. 0968 . 0089	2. 3376 2. 3279 . 0097	2.5876 2.5779 .0097	2. 8376 2. 8279 . 0097	3. 0876 3. 0779 . 0097	3.3376 3.3279 .0097	3.5876 3.5779 .0097	3.8376 3.8279 .0097
Class 4, close fit, pitch di-Max ameter	. 6856 . 6833 . 0023	. 8034 . 8010 . 0024	.9195 .9168 .0027	1. 0330 1. 0300 . 0030	$\begin{array}{c} 1.1580\\ 1.1550\\ .0030\end{array}$	$\begin{array}{c} 1.\ 2676\\ 1.\ 2640\\ .\ 0036\end{array}$	1. 3926 1. 3890 . 0036	1. 6211 1. 6170 . 0041	1.8568 1.8524 .0044	2. 1068 2. 1024 . 0044	2.3389 2.3341 .0048	2.5889 2.5841 .0048	2.8389 2.8341 .0048	3.0889 3.0841 3.0048	3.3389 3.3341 .0048	3.5889 3.5841 .0048	3.8389 3.8341 .0048

# DIMENSIONAL LIMITS OF FASTENING-SCREW THREADS 45

			n p. 49.	note 3 oi	See foot				1 p. 49.	note 2 or	<sup>2</sup> See foot				a p. 49.	note 1 oi	1 See foot
3.8424	3.5924 .0048	3.3424	3.0924	2.8424	2.5924 .0048	2. 3424 . 0048	2.1101	1.8601	1.6242	1.3953	1.2703.0036	1.1602 .0030	1.0352.0030	.9215 .0027	. 8052	. 6873	lose fit, pitch di-{Max. <sup>3</sup> Tol
3.8473 .0097	3.5973	3.3473	3. 0973	2.8473	2.5973	2. 3473 . 0097	2.1146	1.8646.0089	1.6283	1. 3988	1.2738.0071	1.1631	1.0381	. 9242	. 8077	. 6895	nedium fit, pitch [Max. <sup>3</sup> br
3.8516 .0140	3.6016	3.3516	3.1016	2.8516	2.6016	2.3516	2.1184	1.8684	1.6317	1.4018	1.2768	1.1657. $0085$	1.0407	. 9264	. 8098	. 6914	ee fit, pitch diam-{Max. <sup>3</sup> Tol
3.8580 .0204	3.6080 .0204	3.3580 .0204	3. 1080 . 0204	2.8580 0.0204	2.6080	2.3580 .0204	2.1241	1.8741	1.6370	1.4062. $0145$	1.2812	1.1696	1.0446	.9299	.8128	. 6942 . (692	oose fit, pitch di-[Max. <sup>3</sup>
3. 8376	3.5876	<b>3.</b> 3376	3. 0876	2. 8376	2.5876	2. 3376	2.1057	1.8557	1.6201	1. 3917	1. 2667	1. 1572	1. 0322	.9188	. 8028	. 6850	2, 3, and 4, pitch diam-
3.7564 3.7294 .0270	3.5064 3.4794 .0270	3. 2564 3. 2294 . 0270	3.0064 2.9794 .0270	2.7564 2.7294 .0270	2.5064 2.4794 .0270	2.2564 2.2294 .0270	$\begin{array}{c} 2.0335\\ 2.0004\\ .0241\end{array}$	$1.7835 \\1.7594 \\1.0241$	$1.5551 \\ 1.5335 \\ 1.5335 \\ .0216$	1.3376 1.3196 .0180	$1.2126 \\ 1.1946 \\ .0180$	1. 1108 1. 0954 . 0154	. 9858 . 9704 . 0154	. 8795 . 8647 . 0148	. 7689 . 7547 . 0142	. 6553 . 6417 . 0136	, 2, 3, and 4, minor [Max er[Tol
4.0000	3.7500	3.5000	3. 2500	3.0000	2.7500	2.5000	2. 2500	2. 0000	1.7500	1.5000	1.3750	1. 2500	1. 1250	1.0000	. 8750	.7500	, 2, 3, and 4, major diam- Min. <sup>3</sup>
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	<u> </u>	0		3	33	4	2	8	8	10	12	74	§16	3/6	7/6	
	I							Threads	per inci							- 17
		08	72	64	58	48	44	40	36	32	78	88	24	24	30	
BOLTS AND SCREWS Class 1, major diameter	Min	Inch 0.0593 .0545 .0048	Inch 0. 0723 . 0050	Inch 0. 0853 0. 0801 0. 0052	Inch 0.0982 .0926 .0056	Inch 0.1111 0.1111 .1049 .0062	$ \begin{array}{c} Inch \\ 0. \ 1241 \\ . \ 1177 \\ . \ 0064 \end{array} $	${}^{Inch}_{0.\ 1370}_{.\ 1302}_{.\ 0068}$	${}^{Inch}_{0.\ 1629}_{.\ 1557}_{.\ 0072}$	${}^{Inch}_{0.1839}$ ${}^{.1813}_{0.076}$	Inch 0.2148 .2062 .0086	Inch 0. 2488 . 2402 . 0086	$I_{nch}^{Inch} \\ 0.3112 \\ .3020 \\ .0092 \\ .0092 \\ .$	Inch 0.3737 .3645 .0092	Inch 0.4360 .4258 .0102	-11111 - 00
Classes 2, 3, and 4, major diameter	Min	.0600 .0566 .0034	0730 0694 0036	.0860 .0822 .0038	. 0990 . 0950 . 0040	. 1120 . 1076 . 0044	. 1250 . 1204 . 0046	. 1380 . 1332 . 0048	.1640 .1590 .0050	.1900 .1846 .0054	. 2160 . 2098 . 0062	. 2500 . 2438 . 0062	. 3125 . 3059 . 0066	. 3750 . 3684 . 0066	. 4375 . 4303 . 0072	1013 11
Ulass 1, mirtor diameter	Max.1 Max.1	.0440	. 0553	.0561	. 0763	. 0864	. 0962	.1063	.1288	. 1506	.1710	2050	. 2601	.3226	.3747	
Class 1, pitch diameter	Min	. 0512 . 0458 . 0024	.0633 .0608 .0025	. 0752 . 0726 . 0026	. 0866 . 0838 . 0028	. 0976 . 0945 . 0031	. 1093 . 1061 . 0032	.1208 .1174 .0034	. 1440 . 1413 . 0036	.1686 .1648 .0038	. 1916 . 1873 . 0043	. 2256 . 2213 . 0043	. 2841 . 2795 . 0046	. 3466 . 3420 . 0046	.4035 .3984 .0051	
Olass 2, pitch diameter	Min	. 0519 . 0502 . 0017	.0640 .0622 .0018	. 0759 . 0740 . 0019	. 0874 . 0854 . 0020	.0085 .0963 .0022	. 1102 . 1079 . 0023	. 1218 . 1194 . 0024	. 1460 . 1435 . 0025	.1697	.1928 .1897 .0031	. 2268 . 2237 . 0031	. 2854 . 2821 . 0033	3479 3446 0033	.4050 .4014 .0036	001111
Class 3, pitch diameter	Min	. 0519 . 0506 . 0013	.0840 .0627 .0013	. 0759 . 0745 . 0014	.0874 .0859 .0015	. 0985 . 0969 . 0016	. 1102 . 1086 . 0016	. 1218	. 1460 . 1442 . 0018	. 1697 . 1678 . 0019	.1928 .1906	. 2268 . 2246 . 0022	. 2854 . 2830 . 0024	. 3479 . 3455 . 0024	. 4050 . 4024 . 0026	TIODI
Class 4, pitch diameter	[Min											. 2270 . 2259 . 0011	. 2857 . 2845 . 0012	.3482 .3470 .0012	. 4053 . 4040 . 0013	014

# DIMENSIONAL LIMITS OF FASTENING-SCREW THREADS 47

NUTS AND TAPPED HOLES												_	_	
Classes 1, 2, 3, and 4, major diameterMin. <sup>2</sup> .	. 0600	. 0730	. 0860	. 0990	.1120	.1250	.1380	.1640	.1900	.2160	. 2500	.3125	. 3750	. 4375
Classes 1, 2, 3, and 4, minor diameter	- 0492 . 0465 . 0027	.0610 .0580 .0030	.0724 .0691 .0033	.0834 .0797 .0037	. 0937 . 0894 . 0043	.1049 .1004	. 1158 . 1109 . 0049	.1391	. 1618 . 1562 . 0056	. 1833 . 1773 . 0060	. 2173 . 2113 . 0060	. 2739 . 2674 . 0065	. 3364 . 3299 . 0065	. 3906 . 3834 . 0072
Classes 1, 2, 3, and 4, pitch diameterMin	. 0519	.0640	.0759	. 0874	. 0985	.1102	. 1218	.1460	. 1697	.1928	. 2268	. 2854	.3479	.4050
Class 1, pitch diameter $\{Max^3, T^0\}$	. 0543	. 0665	.0785	.0902	.1016	.1134	.1252	.1498	. 1735	. 1971	.2311	. 2900	.3525	.4101
Class 2, pitch diameter{Tol	. 0536	. 0658	. 0778	.0894 .0020	. 1007	.1125	.1242	.1485	.1724 .0027	.1959	. 2299	. 2887	.3512	. 4086 . 0036
Class 3, pitch diameter	.0532	.0653	,0773	.0889	.1001	. 1118	.1235	.1478	. 1716	. 1950	. 2290	. 2878	.3503	. 4076
Class 4, pitch diameter $T_{01-}$											. 2279	. 2566	.3491	.4063
<sup>1</sup> See footnote 1 on D. 49.	-	3	See foot:	note 2 on	n. 49.				See foot	note 3 or	n n. 49.	-		

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					Siz	Ses					
	54	9/6	86	34	82	1	146	114	13,6	1}2	
				-	Threads	per inch					TAT
	20	18	18	16	14	14	12	12	12	12	
BOLTS AND SCREWS lass 1, major diameter	Max Min Vin Vin 0.4985 102	$\begin{array}{c} Inch \\ 0.5609 \\ .5495 \\ .0114 \end{array}$	$Inch \\ 0.6234 \\ .6120 \\ .0114$	${Inch} \\ 0.7482 \\ .7356 \\ .0126$	$\begin{array}{c} Inch \\ 0.8729 \\ .8589 \\ .0140 \end{array}$	$\begin{array}{c} Inch \\ 0.9979 \\ .9839 \\ .0140 \end{array}$	Inches 1, 1226 1, 1068 . 0158	Inches 1. 2476 1. 2318 . 0158	Inches 1.3726 1.3568 .0158	<i>Inches</i> 1.4976 1.4818 .0158	AL SU
lasses 2, 3, and 4, major diameter	Max 5000 Min 4928 Fol 0072	. 5625 . 5543 . 0082	.6250 .6168 .0082	.7500 .7410 .0090	.8750 .8652 .0098	1.0000 .9902.	$1.1250 \\ 1.1138 \\ .0112$	$   \begin{array}{c}     1.2500 \\     1.2388 \\     0.0112   \end{array} $	$1.3750 \\ 1.3638 \\ .0112$	$1.5000 \\ 1.4888 \\ 0.0112 \\ 0.0112$	LT ET AA
llass 1, minor diameter	8x. <sup>1</sup> 4372	. 4927	. 5552	. 6715	. 7853	.9103 .9124	1.0204 1.0228	1. 1454 1. 1478	$1.2704 \\ 1.2728$	1,3954 1,3978	1111
lass 1, pitch diameter	Max 4660 Min 4609 Pol 0051	. 5248 . 5191 . 0057	. 5873 . 5816 . 0057	. 7076	.8265 .8195 .0070	.9515 .9445 .0070	1.0685 1.0606 .0079	1.1935 1.1856 .0079	$   \begin{array}{c}     1.3185 \\     1.3106 \\     .0079   \end{array} $	$1.4435 \\ 1.4356 \\ 0.079$	EAD
llass 2, pitch diameter	Max 4675 Min 4639 Vol 0036	. 5264 . 5223 . 0041	.5889 .5848 .0041	. 7094 . 7049 . 0045	. 8286 . 8237 . 0049	.9536 .9487 .0049	$1.0709 \\ 1.0653 \\ .0056$	$1.1959 \\1.1903 \\.0056$	$   \frac{1.3209}{1.3153} $	1.4459 1.4403 .0056	COM
llass 3, pitch diameter	Max 4675 Min 4649 Fol 0026	. 5264 . 5234 . 0030	. 5889 . 5859 . 0030	. 7094 . 7062 . 0032	. 8286 . 8250 . 0036	. 9536 . 9500 . 0036	$   \frac{1.0709}{1.0669} $	$   \frac{1.1959}{1.1919} $	1.3209     1.3169     .0040	$1. \frac{4459}{1419}$ $1. \frac{4419}{0040}$	11991
lass 4, pitch diameter	Max 4678 Min 4665 Fol 4665	. 5267 . 5252 . 0015	. 5892 . 5877 . 0015	.7098 .7082 .0016	. 8290 . 8272 . 0018	.9540 .9522 .0018	$1.0714 \\ 1.0694 \\ .0020$	1.1964 1.1944 .0020	1.3214 1.3194 .0020	1.4464 1.4444 .0020	

NOTS AND LAFFED HOLES										
Jasses 1, 2, 3, and 4, major diameterMin. <sup>2</sup> .	. 5000	. 5625	. 6250	.7500	.8750	1.0000	1.1250	1.2500	1.3750	1, 500
Slasses 1, 2, 3, and 4, minor diameter	. 4531 . 4459 . 0072	. 5100 . 5024 . 0076	. 5725 . 5649 . 0076	. 6903 . 6823 . 0080	. 8062 . 7977 . 0085	. 9312 . 9227 . 0085	1.0438 1.0348 .0090	1. 1688 1. 1598 . 0090	1. 2938 1. 2848 . 0090	1.418 1.409
Jasses 1, 2, 3, and 4, pitch diameterMin	. 4675	. 5264	. 5889	.7094	.8256	. 9536	1. 0709	1. 1959	1.3209	1.445
lass 1, pitch diameter{Tol}	.4726	. 5321	. 5946	. 7157	. 8356	. 0070	1. 0788	1.2038	1.3288	1.453
lass 2, pitch diameter{Tol} [Max <sup>3</sup>	. 4711	. 5305	. 5930	.7139	.8335	. 9585	1.0765	1.2015	1. 3265 . 0056	1.451
lass 3, pitch diameter{Tol}	.4701	. 5294	. 5919	. 7126	. 8322	. 9572	1.0749	1.1999	1.3249	1.449
Max. <sup>3</sup> {Tol{Tol	.4688	. 5279	. 5904	. 7110	.8304	.9554	1.0729 0020	1.1979. $0020$	1.3229	1.447.002
									-	

mm 00 G mm 10 m •• 00 <sup>1</sup> Dimensions given for the maximum minor diameter of the screw are figured to the intersection of the worn tool arc with a center line through crest and root. The minimum minor diameter of the minimum screw equal to  $\frac{1}{2}$ X,p, and may be determined by subtracting the basic thread dopth, discrew shall be that corresponding to a flat at the minor diameter of the minimum screw equal to  $\frac{1}{2}$ X,p, and may be determined by subtracting the basic thread dopth, discrem for the minimum pitch diameter of the screw. <sup>2</sup> Dimensions for the minimum major diameter of the nut correspond to the basic flat ( $\frac{1}{2}$ X,p) and the profile at the major diameter produced by a worn tool must not fall below the basic screet. <sup>3</sup> Dimensions for the minimum major diameter of the nut corresponding to a flat at the major diameter of the maximum may diameter of the unt of a data at the major diameter of the maximum may diameter of the unt. <sup>3</sup> Dimensions  $\frac{1}{2}$ M,  $\frac{1}{2}$ M

#### 5. GAGES

The art of measuring screw threads has developed very rapidly during the past two decades. This development still continues, so that it would be inadvisable to attempt to specify any definite method as standard for this purpose. The objects are to establish the fundamentals of this subject, and to point out practices now successfully used.

## (a) FUNDAMENTALS

1. OBJECT OF GAGING.—The final results sought by gaging are to secure interchangeability, that is, the assembly of mating parts without selection or fitting of one part to another, and to insure that the product conforms to the specified dimensions within the limits of variation establishing the closest and loosest conditions of fit permissible in any given case, as provided for in the foregoing specifications. This requires the use of gages representing the limit of maximum metal, known as "go" gages, which control the minimum looseness or maximum tightness in the fit of mating parts, and which accordingly control interchangeability; and the use of gages representing the limit of minimum metal, known as "not go" gages, which limit the amount of looseness between mating parts, and thus control in large measure the proper functioning of the parts.

Gaging should be as much employed to prevent unsatisfactory parts from being produced as to sort out the correct from the incorrect parts.

2. PURPOSE OF "GO" AND "NOT GO" GAGES.—The "go" gages control the extent of the tolerance in the direction of the limit of maximum metal, and represent the maximum limit of the internal member and the minimum limit of the external member. To pass inspection, parts must be acceptable to proper "go" gages, and such mating parts will always assemble. Successful interchangeable manufacturing has been carried on for many years with the use of "go" gages only.

"Not go" gages control the extent of the tolerance in the direction of the limit of minimum metal, and represent the minimum limit of the internal member and the maximum limit of the external member. To be acceptable, parts must not enter or be entered by proper "not go" gages. It is general practice to permit "not go" thread gages to enter or be entered by the product not more than 1½ turns.

There is a broad, general principle in regard to limit gages which should be kept in mind; a "go" gage should check simultaneously as many elements as possible, a "not go" gage, to be effective, can check but one element. By effective inspection is meant assurance that specified requirements in regard to size are not exceeded. A "not go" thread gage made to check only the pitch diameter is usually sufficient for practical purposes. In order that the "not go" gage may check pitch diameter only, it is necessary that the crest of the thread be removed so that the major diameter of the plug gage shall never be greater than that specified for the "go" plug gage and the minor diameter of the ring gage shall never be less than that specified for the "go" ring gage. A correspondingly greater relief should be provided at the root of the thread of the "not go" gage than of the "go" gage. (See "thread form of thread plug and ring gages", p. 53.) 3. GAGE CLASSIFICATION.—The limiting dimensions of the threaded parts to be produced should be represented in: (a) Gages used in checking the product as it is machined, known as "working gages"; (b) gages for use in the acceptance of the product, known as "inspection gages"; and (c) gages used to determine the accuracy of the two preceding classes of gages, known as "master gages".

4. GAGES USED TO MEASURE THE PRODUCT.—The gages used to check the product may be divided into two general types: "Mechanical" and "optical". Both types, however, are controlled by the master gages. Most of the product accepted by one type of gaging with a correct gage will be accepted by the other. It should be pointed out, however, that those parts which are near either rejection point may be accepted by one system and rejected by the other.

(a) Mechanical gages.—Mechanical gages ordinarily comprise the inspection and working gages as above defined, and these two classes are generally of the same design. The dimensions of inspection gages are such that they represent very nearly the extreme limits of the part. It is recommended that, when successive inspections are required, the working gages, either by design or selection, be of such dimensions that they are inside the limits of the gages used in succeeding inspections.

Standard designs for certain types of mechanical gages are available in the report of the American Gage Design Committee, U.S. Department of Commerce Commercial Standard No. CS8-33, "Gage Blanks."<sup>2</sup>

(b) Optical gages.—When gages of the optical type are employed, the elements of wear and "feel" are not involved, hence no difference in size between inspection and working gages is necessary, but is desirable.

5. GAGES FOR REFERENCE.—(a) Master gage.—The master gage is a thread-plug gage which represents the physical dimensions of the nominal or basic size of the part. It clearly establishes the minimum size of the threaded hole and the maximum size of the screw at the point at which interference between mating parts begins. A master gage shall be accompanied by a record of its measurement. In case of question, the deviations of this gage from the basic size shall be ascertained by the Bureau of Standards at Washington, D.C.

(b) Setting gage (check gage).—A setting gage is a thread-plug gage to which adjustable thread-ring gages, thread-snap gages, and other thread comparators are adjusted for size. In adjusting thread-ring gages to size, the setting plug gage should control the pitch diameter, and it will do so if proper clearance is provided at the major diameter of the ring gage, and if the minor diameter is within the specified limits. The ring gage should be given further inspection as to these points. The minor diameter may be inspected by means of "go" and "not go" plain plug gages, and the major diameter by optical examination of a sulphur-graphite, plaster-of-paris, or other suitable cast of the thread.

6. DIRECTION OF TOLERANCES ON GAGES.—The sizes for limit gages shall never be outside of the limits specified for the product. All variations in the gages, whatever their cause or purpose, shall bring these gages within these extreme limits. Thus, a gage which represents a minimum limit may be larger, but never smaller, than the minimum

<sup>&</sup>lt;sup>8</sup> For sale by the Superintendent of Documents, Government Printing Office, Washington, D.C.

size specified for the part, while the gage which represents a maximum limit may be smaller, but never larger, than the maximum size specified for the part.

7. TEMPERATURE AT WHICH GAGES SHALL BE STANDARD.—The nominal dimensions of gages and product shall be correct at a temperature of  $68^{\circ}$  F. ( $20^{\circ}$  C.).—As gages and products are ordinarily checked at room temperature, whatever it may happen to be, it is desirable that the thermal coefficient of expansion of gages be the same as that of the product on which they are used. Inasmuch as the majority of threaded products consist of iron and steel, and as screw-thread gages are ordinarily made of hardened steel, because of its high wearresisting qualities, this condition is ordinarily fulfilled without giving it special attention.

8. MEASURING PRESSURE FOR THREE-WIRE MEASUREMENTS.<sup>9</sup>—In measuring the pitch diameter of hardened screw-thread gages by means of wires, and in measuring the wires themselves, the same contact pressure should be used. A contact pressure of 14 to 16 ounces is recommended for pitches finer than 20 threads per inch and of 2½ to 2½ pounds for 20 threads per inch and coarser. It is also recommended as standard practice that wires be measured between a flat contact and a cylindrical contact 0.750 inch in diameter.

### (b) SPECIFICATIONS FOR GAGES

The following specifications are for the purpose of establishing definite limits for thread gages rather than for the purpose of specifying the gages required for the various inspection operations:

1. CLASSIFICATION OF GAGES, AND GAGE TOLERANCES.—Screwthread gages for classes 1, 2, and 3 are classified according to accuracy into classes X, Y, and Z, the class X being the most accurate. Gages for class 4, close-fit product, are made to smaller tolerances and are designated as class W. The tolerance limits on classes Y and Z "go" gages are placed inside of the extreme product limits to provide allowance for wear of the gages. The tolerances on all "not go" gages, however, are applied from the extreme product limit as the starting point, as no allowance for wear is necessary. The selection of gages from among these classes for use in the inspection of threaded product depends entirely upon the specifications for the product. For example, in the production of parts to class 3, medium fit specifications, class X gages may be required for all purposes. On the other hand, for parts made to class 1, loose-fit specifications, class Z gages may be sufficiently accurate for all purposes.

(a) Master gages.—No fixed tolerances are specified for master gages. These should be made to the basic size as accurately as possible and be within the tolerances specified for class X gages. The variations from basic size shall be plus. Each master gage shall be marked with an identification number or symbol, and be accompanied by a record of its measurement on major diameter, pitch diameter, lead, and angle. In case of question, the deviations of such gages from the exact standard shall be ascertained by the Bureau of Standards at Washington, D.C.

(b) Class X gages.—Class X gages should be suitable for inspection and setting gages for classes 1, 2, and 3. The tolerances on these

<sup>&</sup>lt;sup>9</sup> Methods of measuring pitch diameter of screw-thread gages are described in appendix 2, p. 129.

gages are given in table 18. In all cases the tolerances s all be such that the gage does not fall outside of the component toler nces. For example, if a thread-plug gage is used as the "go" gage i ir checking a tapped hole, it can be larger, but not smaller than the minimum size specified. On the other hand, if a thread-plug gage is used as the "go" setting plug for thread-ring gages or for optical or other comparators, it can be smaller, but never larger than the maximum size of the screw.

Class X tolerances, as given in table 18, are specified for all "not

go" gages for classes 1, 2, and 3. (c) Class Y gages.—Class Y gages should be suitable for inspection gages for classes 1, 2, and 3 fits. They may also be desired as working gages for classes 2 and 3 fits. The tolerances on these gages are given in table 19.

(d) Class Z gages.—Class Z gages should be suitable for working gages for class 1, loose fit. The tolerances on these gages are given in table 20.

(e) Class W gages.—For the inspection of class 4, close-fit product, gages made within especially close limits are necessary. The tolerances for such gages, designated as class W, are given in table 21. (f) Wear on gages.—"Go" gages may be permitted to wear to the

extreme product limits. It is desirable, however, that working and inspection gages be so selected that the dimensions of the working gages are inside of the limiting dimensions represented by the inspection gages, in order that all parts passed by the working gage will be accepted by the inspection gage.

As to wear on "not go" gages, it is purely a question of economy as to when the "not go" gage should be discarded. Continued use reduces the available working tolerance on the product, and the resulting loss must be balanced against the cost of a new gage.

(g) Tolerances on lead.—The tolerances on lead given in tables 18 to 21, inclusive, are specified as an allowable variation between any two threads not farther apart than the length of engagement of the assembled threaded product. When this length of engagement is equal to the diameter, the permissible progressive lead errors per inch may be determined by dividing these lead tolerances by the corresponding diameters.

(h) Tolerances on angle of thread.—The tolerances on angle of thread, as specified in tables 18 to 21, inclusive, for the various pitches, are tolerances on one half of the included angle. This insures that the bisector of the included angle will be perpendicular to the axis of the thread within proper limits. The equivalent deviation from the true thread form caused by such irregularities as convex or concave sides of thread, rounded crests, or slight projections on the thread form, should not exceed the tolerances permitted on angle of thread.

2. THREAD FORM OF THREAD PLUG AND RING GAGES.—The major diameter of the "go" thread plug gage is the same as the basic major diameter, with a plus gage tolerance. The minor diameter of the "go" thread ring gage is the same as the minimum minor diameter of the nut or tapped hole with a minus gage tolerance.

The crest of the thread of the "not go" plug gage is truncated below the basic major diameter an amount equal to one sixth of the basic thread depth with a plus gage tolerance. On a basic thread

form the corresponding width of flat would be one fourth of the pitch. On a "not go" plug gage the flat is wider than one fourth of the pitch by an amount depending upon the product pitch diameter tolerance.

The crest of the thread of the "not go" ring gage is truncated above the basic minor diameter an amount equal to one third of the basic thread depth with a minus gage tolerance. On a basic thread form the corresponding width of flat would be three eighths of the pitch. On a "not go" ring gage the flat is wider than three eighths of the pitch by an amount depending upon the product pitch diameter tolerance. However, adjustable gages, such as thread snap gages,



FIGURE 18.—Thread form of "go" and "not go" thread plug and ring gages.

which may be set to the "not go" limit of any class of fit should have a width of flat equal to three eighths of the pitch. A relief is provided at the root of the "go" thread plug or ring

A relief is provided at the root of the "go" thread plug or ring gage, the width of which is not greater than one eighth of the pitch. Also a relief is provided at the root of the "not go" thread plug or ring gage, the width of which is approximately one fourth of the pitch.

Thus contact of the "not go" thread gage on the sides of the threads, rather than at the corners of the crest and root, is assured. Also the effect of angle error on the fit of the "not go" gage with the product is minimized.

The above requirements are illustrated in figure 18.

3. TOLERANCES FOR PLAIN GAGES.—For plain plug gages, plain ring gages, and plain snap gages required for measuring diameters of screw-thread work, the gage tolerances specified in table 18 should be used. Attention is directed to the fact that the tolerances on thread diameters vary in accordance with the number of threads per inch. In manufacturing a plain plug, ring, or snap gage, in the absence of information as to the number of threads per inch of the screw to be made, or for gage dimensions other than thread diameters, the tolerances for plain gages given in table 22 may be used. This table contains recommended tolerances for plain gages, designated as classes X, Y, and Z, which have been tentatively adopted by the Sectional Committee on the Standardization of Plain Limit Gages for General Engineering Work. These tolerances are applicable to all classes of product.

4. RECOMMENDED GAGE PRACTICE.—There are given in table 17 the recommended uses for the foregoing classes of gages. Tables 23, 24, 25, and 26 give limiting dimensions of gages of the several classifications for the American National coarse and American National fine thread series.

TABLE 17.-Recommended uses for classes W, X, Y, and Z "go" thread gages

Class of fit	Setting gage	Inspection gage	Working gage
1	2	3	4
Class 1, loose fit Class 2, free fit Class 3, medium fit Class 4, close fit	Class X, table 18 dodo Class W, table 21	Class Y, table 19 class X, table 18 Class W, table 21	Class Z, table 20. Class Y, table 19. Do. Class W, table 21.

NOTE .- "Not go" thread gages for classes 1, 2, and 3 are class X, and for class 4 are class W.

### NOTE

The rule for direction of gage tolerances given in footnote 1 of tables 18, 19, 20, and 21 is not applicable to the crests of truncated "not go" thread plug and thread ring gages. This exception is covered by statements at the bottom of page 53 and top of page 54, as well as by the limiting dimensions for major diameter of "not go" plug gages and minor diameter of "not go" ring gages given in tables 23, 24, 25, and 26. The explanation for this is that the truncation itself conforms to the principle stated at the bottom of page 50, and is in effect an application of the rule, since the truncation includes the zone of the gage tolerance of a full-form gage. The direction of the gage tolerances, as actually applied herein to crests of truncated "not go" thread gages, serves to limit the truncation to a maximum of %h, as shown in figure 18. If this maximum were exceeded by reversing direction of gage tolerances, several sizes of class 1 "not go" thread ring gages would be truncated beyond the pitch line.

Threads per inch	Tolerance diam	e on pitch eter <sup>1</sup>	Tolerance	Tolerance on half	Tolerance of minor dis	on major or ameters <sup>1</sup>
-	From-	То—	in lead *	thread	From—	То—
1	2	3	4	5	6	7
	Inch	Inch	Inch	Deg. Min.	Inch	Inch
80	0.0000	0.0002	<u> </u>	0 30	0.0000	0.000
72	0000	0002	0.0002	0 30	0000	0003
RA	0000	0002	.0002	0 30	. 0000	0004
58	0000	0002	. 0002	0 30	0000	0004
48	. 0000	.0002	.0002	0 30	. 0000	. 0004
44	. 0000	.0002	. 0002	0 20	. 0000	. 0004
40	. 0000	. 0002	. 0002	0 20	. 0000	. 0004
36	. 0000	. 0002	. 0002	0 20	. 0000	. 0004
32	. 0000	. 0003	. 0003	0 15	. 0000	. 0004
28	. 0000	. 0003	, 0003	0 15	. 0000	. 0008
24	. 0000	. 0003	. 0003	0 15	. 0000	. 000
20	. 0000	. 0003	. 0003	0 15	.0000	.000
18	. 0000	. 0003	. 0003	0 10	.0000	. 000
16	. 0000	. 0003	. 0003	0 10	.0000	. 000
14	. 0000	. 0003	. 0003	0 10	.0000	. 000
13	. 0000	. 0003	. 0003	0 10	.0000	. 000
12	. 0000	. 0003	. 0003	0 10	. 0000	. 000
11	, 0000	. 0003	. 0003	0 10	. 0000	. 000
10	.0000	. 0003	. 0003	0 10	. 0000	. 000
9	. 0000	. 0003	. 0003	0 10	.0000	. 000
8	. 0000	.0004	.0004	0 5	.0000	. 000
7	. 0000	. 0004	. 0004	0 5	. 0000	. 000
6	. 0000	. 0004	. 0004	0 5	. 0000	. 000
5	. 0000	.0004	. 0004	0 5	. 0000	.000
41/2	. 0000	. 0004	. 0004	0 5	.0000	.000
4	. 0000	. 0004	. 0004	0 5	. 0000	. 000
			1	1	1	1

TABLE 18.—Tolerances for class X "go" thread gages, and "not go" thread gages for classes 1, 2, and 3, and all plain gages

<sup>1</sup> On "go" plugs the tolerance is plus, and on "go" rings the tolerance is minus. On "not go" plugs the tolerance is minus, and on "not go" rings the tolerance is plus. <sup>3</sup> Allowable variation in lead between any two threads not farther apart than the standard length of engagement, which is equal to the basic major diameter.

It is suggested that, in case of question between the manufacturer and purchaser of threaded products in regard to their size, if the manufacturer produces limit gages which do not measure outside of the specified limits for the threaded components and which pass the parts in question, they be accepted as meeting the specifications for size. In case the dimensions of the gages are questioned, their sizes shall be determined by a disinterested third party, preferably the Bureau of Standards at Washington, D.C., which maintains a department for this service.

4. MARKING OF GAGES.—Each gage shall be plainly and permanently marked, for identification, with the diameter, pitch, thread series, and class of fit. See section II, division 3, "Symbols."

For example: A 1-inch, 8-pitch gage of the American National coarse-thread series, class 2, free fit, shall be marked 1"-8NC-2.

A 1-inch, 14-pitch gage of the American National fine-thread series, class 3, medium fit, shall be marked 1"-14NF-3.

LUDDE 10					Jagoo	
Threads per inch	Tolerance diam	e on pitch eter <sup>1</sup>	Tolerance	Tolerance on half	Tolerance o minor di	on major or ameters <sup>1</sup>
	From-	То	III Ieau -	thread	From-	То—
1	2	3	4	5	6	7
	Inch	Inch	Inch	Deg. Min.	Inch	Inch
80	0.0001	0.0003	0.0002	$0^{\pm}$ 45 0 45	0,0000	0.0003
8484	.0001	.0004	.0002	0 45	.0000	.0004
48	.0001	.0004	.0002	0 45	. 0000	.0004
44	.0001	.0004	.0002	0 30 0 30	.0000	.0004
36 32	.0001	.0004	.0002	0 30 0 20	.0000	.0004
28	.0002	.0005	. 0003	0 20	.0000	. 0005
20	.0002	.0005	. 0003	0 20	.0000	. 0005
l6	.0002	.0005	. 0003	0 15	.0000	.0005
4	.0002	.0006	.0003	$ \begin{array}{ccc} 0 & 15 \\ 0 & 15 \end{array} $	.0000	.0006
2	.0002	.0006	. 0003	$\begin{array}{ccc} 0 & 10 \\ 0 & 10 \end{array}$	.0000	.0006
0	.0002	.0006	. 0003	0 10	. 0000	.0006
3	.0002	.0007	.0003	0 5	.0000	.0007
3	.0002	.0007	.0004	0 5	.0000	.0007
5 146	.0003	. 0008	.0004	0 5	.0000	.0008
	. 0003	. 0009	. 0004	0 5	. 0000	. 0009

## TABLE 19 - Tolerances for class Y "ao" thread gages

<sup>1</sup> On "go" plugs the tolerance is plus and on "go" rings the tolerance is minus. <sup>a</sup> Allowable variation in lead between any two threads not farther apart than the standard length of engagement, which is equal to the basic major diameter.

TABLE 20.—Tolerances	for	class	Ζ	"go'	'threa	d gage	28
----------------------	-----	-------	---	------	--------	--------	----

Threads per inch	Tolerance diam	e on pitch eter <sup>1</sup>	Tolerance	Tolerance on half	Tolerance of minor dia	on major or ameters <sup>1</sup>
r moads por mon	From-	То—	in lead <sup>2</sup>	angle of thread	From—	То—
1	2	3	4	5	6	7
	Inch	Inch	Inch	Deg. Min.	Inch	Inch
80 72	0.0002 .0002 .0002 .0002 .0002 .0002	0.0006 .0006 .0006 .0007 .0007	0.0002 .0002 .0002 .0002 .0002 .0002	$\begin{array}{cccc} & & & & \\ 0 & & 45 \\ 0 & & 45 \\ 0 & & 45 \\ 0 & & 45 \\ 0 & & 45 \end{array}$	0.0000 .0000 .0000 .0000 .0000	0.0003 .0003 .0004 .0004 .0004
44 40 38 32 28	. 0002 . 0002 . 0003 . 0003 . 0003	.0007 .0007 .0008 .0008 .0008	.0002 .0002 .0002 .0003 .0003	0 30 0 30 0 30 0 20 0 20	. 0000 . 0000 . 0000 . 0000 . 0000	.0004 .0004 .0004 .0004 .0005
24 20 18 16	. 0003 . 0003 . 0004 . 0004	.0009 .0009 .0010 .0010	. 0003 . 0003 . 0004 . 0004	$\begin{array}{ccc} 0 & 20 \\ 0 & 20 \\ 0 & 15 \\ 0 & 15 \end{array}$	.0000 .0000 .0000 .0000	. 0005 . 0005 . 0005 . 0006
14 13 12 11	. 0004 . 0004 . 0004 . 0004	.0010 .0011 .0011 .0011	. 0004 . 0004 . 0004 . 0004	$\begin{array}{ccc} 0 & 15 \\ 0 & 15 \\ 0 & 10 \\ 0 & 10 \end{array}$	. 0000 . 0000 . 0000 . 0000	. 0096 . 0006 . 0006 . 0006
109	. 0005 . 0005 . 0006 . 0006	. 0012 . 0012 . 0013 . 0013	.0004 .0004 .0005 .0005	$\begin{array}{ccc} 0 & 10 \\ 0 & 10 \\ 0 & 5 \\ 0 & 5 \end{array}$	.0000 .0000 .0000 .0000	. 0006 . 0007 . 0007 . 0007
65 5 4½ 4	. 0006 . 0007 . 0007 . 0007	.0014 .0015 .0015 .0016	. 0005 . 0005 . 0005 . 0005	0 5 0 5 0 5 0 5	. 0000 . 0000 . 0000 . 0000	. 0008 . 0008 . 0008 . 0009

<sup>1</sup> On "go" plugs the tolerance is plus, and on "go" rings the tolerance is minus. <sup>3</sup> Allowable variation in lead between any two threads not farther apart than the standard length of engagement, which is equal to the basic major diameter.

TABLE 21.—Tolerances for class	W	"go" close	and fit	"not	go"	thread	gages	for	class	4,
--------------------------------	---	---------------	------------	------	-----	--------	-------	-----	-------	----

			1 1 1				
Threads per inch	Tolerance dian	on pitch leter <sup>1</sup>	Tolerance	Tolerance on half	Total cu- mulative	Tolerance o minor di	n major or ameters
	From	То—	ш нево -	thread	tolerance 8	From	То—
1	2	3	4	5	6	7	8
	Inch	Inch	Inch	Deg. Min.	Inch	Inch	Inch
28	0.0000	0.0001	0.00015	0 8	0.00048	0.0000	0.0005
24	.0000	.0001	.00015	0 8	. 00051	. 0000	. 0005
20	.0000	.0001	.00015	0 8	. 00053	.0000	. 0005
18	.0000	.0001	.00015	0 8	. 00055	.0000	. 0005
16	.0000	. 0001	. 00015	0 8	. 00058	.0000	. 0006
14	. 0000	.00015	. 0002	0 6	. 00068	. 0000	. 0006
13	. 0000	. 00015	. 0002	0 6	. 00070	. 0000	. 0006
12	.0000	. 00015	. 0002	0 6	. 00071	. 0000	. 0006
11	.0000	.00015	. 0002	0 6	. 00073	. 0000	. 0006
10	0000	0002	00025	0 5	00085	0000	0006
9	. 0000	.0002	00025	0 Š	. 00088	.0000	0007
8	. 0000	. 0002	.00025	l õ š	. 00091	. 0000	.0007
7	· .0000	. 00025	. 0003	0 4	.00102	. 0000	. 0007
ß	0000	00025	0003	0 4	00106	0000	0008
5	. 0000	00025	0003		00112	. 0000	. 0008
416	0000	00020	0003		0012	. 0000	. 0000
1/2	.0000	0003	0003		00126	0000	. 0000
7	.0000	. 0005	.0005	1 1	.00120	.0000	. 0003

<sup>1</sup> On "go" plugs the tolerance is plus, and on "go" rings the tolerance is minus. On "not go" plugs the tolerance is minus, and on "not go" rings the tolerance is plus. <sup>4</sup> Allowable variation in lead between any two threads not farther apart than the standard length of engagement, which is equal to the basic major diameter. <sup>8</sup> The tolerance for one element, namely pitch diameter, lead, or angle, as given above, may be exceeded provided that the errors in the other 2 elements are sufficiently small so that the total cumulative tolerance shown in column 6 is not exceeded.

	Clas	s X 2	Clas	58 Y	Cla	ss Z
Size of gage in inches	From-	То—	From—	To	From—	То—
1	2	3	4	5	6	7
0 to 1, inclusive 1 to 3, inclusive	<i>Inch</i> 0.0000 .0000	<i>Inch</i> 0. 0001 . 0002	Inch 0.0001 .0001	Inch 0.0002 .0003	<i>Inch</i> 0. 0002 . 0003	Inch 0.0003 .0005

## TABLE 22.— Tolerances for plain gages 1

<sup>1</sup> On "go" plugs the tolerance is plus, and on "go" rings the tolerance is minus. On "not go" plugs the tolerance is minus, and on "not go" rings the tolerance is plus. <sup>3</sup> All "not go" gages are made to class X tolerances.

							series													
								-	Machi	ne scre	ana w	ther or	nomin	al size						
			1	2	3	4	5	9	8	10	12	14	16	1 8/2	16	34	9/6	5%	34	%
										E.	hreads	per in	ų							
			64	56	48	40	40	32	32	24	24	20	18	16 1	4	13	12	Ξ	9	6
"Go" ( Major diameter of set- ting plug.	AGES FOR SCREW Class 1 Classes 2, 3, and 4.	vs (Max (Min I Max	Inch 0.0723( 0.0723( 0730 0730	Inch 0.08520 0.0848 0.0860 0.0860	Inch 0.0981 0977 0990	<i>Inch</i> 11100. 1120 1120	[nch ] I 1240 0. 1236 1250 1250	nch I 1369 0. 1365 . 1380 . 1380 . 1376 .	$\begin{array}{c c} nch & l \\ 1629 & 0. \\ 1625 & 1640 \\ 1640 & 1636 \\ \end{array}$	nch $11887 0. 11882 0. 11900 11895 .$	nch   21470. 2142 2150	nch 1 2485 0. 2480 . 2500 . 2495 .	nch I 31090. 3125 3125	nch In 3732 0. 4: 3726 . 4: 3750 . 4: 3744 . 4:	1 1 1 254 0.4 2354 0.4 2348 0.4 2355 0.4 2355 0.4 2355 0.4 24 255 0.5 255 0.5 0.5 255 0.5 255 0.5 255 0.5 255	nch 4978 0. 5000 . 1994 .	Inch 5601 0 5595 5619 5619	Inch 6224 6218 6218 6218 6244	Inch I 74720 7466 7500 7500	nch . 8719 . 8712 . 8750 . 8743
	Class 1, loose fit.	Max., class X Min., class X Max., class Y Min., class Y	.0622 .0620 .0621 .0618	0736 0734 0735 0735 0732	.0846 .0845 .0845 .0845 .0842	0948 0946 0947 0944 0946	1078 1076 1077 1074 1076	1166 . 1163 . 1163 . 1162 .	1426 . 1423 . 1423 . 1423 .	1616 1613 1613 1614 1611	1876 1873 1873 1871 1871	2160 2157 2158 2158 2155	2748 2745 2746 2743 2744	3326 3328 3328 3328 3322 3322 3322 3322	890 887 888 888 888 888 886	4478	5060 5057 5058 5058 5056	5634 5631 5632 5632 5628 5630	.6822 .6819 .6820 .6820 .6816	. 7997 . 7994 . 7995 . 7990 . 7992
Pitch diameter of set- ting plug or ring gage.	Class, 2, free fit, and class 3, medium fit.	Min., class Z Max., class Z Min., class X Min., class Y Min., class Y	0616 0629 0627 0627 0628 0628	0729 0744 0742 0743 0743	0839 0855 0853 0854 0851 0851	0941 0958 0956 0957 0957	1071 1088 1086 1086 1087	1158 1177 1177 1176	1418 . 1437 . 1434 . 1436 .	1607 1629 1626 1627 1624	1867 1889 1886 1887 1884	2151 . 2175 . 2172 . 2173 . 2173 .	2738 . 2764 . 2761 . 2762 . 2759 .	3316 3344 3341 3342 3342 3338 3342 3338 3338 3338 3338	905 908 908 908	4467 4500 4497 4498	5049 5084 5081 5081 5078	5623 5660 5657 5658 5658 5654	6810 6850 6847 6848 6848	. 7985 . 8028 . 8025 . 8026 . 8026
	Class 4, close fit.	[Max., class W [Min., class W										2178 .	2767 .	3348 . 3 3347 . 3	915 .	4504 45025	50875	. 56635	. 6854	. 8032
Minor diameter of ring, gage.	Classes 1, 2, 3 and 4.	,{Max. <sup>1</sup>	.0561	. 0667	. 0764	0849	. 0079	1042 . 1038 .	1302 .	1449 . 1444 .	1709	1959	2524 . 2519 .	3073 .3	602 596	4167 . 4161 .	4723	. 5266	.6417	. 7547 . 7540
Major diameter of set- ting plug.	Class 1 CAGES FOR SC Class 1 Classes 2, 3, and 4.	REWS [Min [Min [Min Max	. 0671 . 0675 . 0692 . 0696	. 0796 . 0800 . 0820 . 0824	0919 0923 0946 0950	1042 1046 1072	1172 1176 1202	1293 . 1297 . 1326 .	1553 . 1557 . 1586 .	1795 . 1800 . 1834 .	2055 2094 2099	2433 . 2428 . 2433 .	2995 3043 3048	3606 . 4 3612 . 4 3660 . 4 3666 . 4	214 220 283 283	4830 4825 4896 4902	5443 5449 5519 5519	.6054 .6060 .6132 .6138	. 7288 . 7294 . 7372 . 7378	.8519 .8526 .8610 .8617
Pitch diamater of set- ting plug or ring gage.	Class 1, loosa fit. Class 2, free fit Class 3, medium fit.	Min. Max. Min. Min. Max. Max.	.0596 .0598 .0598 .0610 .0612 .0615	0708 0710 0724 0726 0729 0731	0815 0817 0833 0835 0835 0835 0841 0841	0914 0916 0934 0936 0941 0943	1044 1046 1066 1066 1071 1073	1128 1131 1150 1153 1153 1158	1388 1391 1410 1413 1413 1421	1570 1573 1596 1599 1605 1605	1830 1833 1833 1856 1859 1865	2109 . 2112 . 2139 . 2142 . 2142 . 2152 . 2155 .	2691 - 2691 - 2694 - 2723 - 2726 - 2734 - 2737 - 2737 - 2737 - 2752 - 2752 - 2752 - 2752 - 2752 - 2752 - 2752 - 2752 - 2752 - 2752 - 2752 - 2752 - 2752 - 2752 - 2752 - 2752 - 27555 - 27555 - 27555 - 27555 - 27555 - 27555 - 27555 - 27555 - 27555 -	3263 .3 3266 .3 3266 .3 3299 .3 3315 .3 3312 .3 33312 .3 33312 .3 33312 .3 33312 .3 33312 .3 33312 .3 33312 .3 3332 .3	820 862 875 875 875 875 875	4404 44407 44487 44451 44463 4466 4485	4981 5028 5031 5047 5069 5047	5549 5552 5601 5604 5618 5621 5621	. 6730 . 6733 . 6733 . 6733 . 6739 . 6739 . 6789 . 6789 . 6789 . 6789 . 6789 . 6789 . 6789 . 6789 . 6789 . 6788	7897 7900 7958 7961 7979 8010
Minor diametor of ring, gage.	(Classes 1, 2, 3, (Classes 1, 2, 3, and 4.	(Min. <sup>3</sup> Min. <sup>3</sup>	.0591	1020	0806	0899	1029	1105	1365	1534 .	1794	2166 2062 2067	2753 . 2639 . 2644 .	3333 . 2 3203 . 3 3209 . 3	8985 . 756 .	44800 4328 4334	4897 4903	. 5457 . 5463	. 0000 . 6628 . 6634	. 7781

1 2 See footnotes on p. 63.

DIMENSIONAL LIMITS OF GAGES

l coarse-thread
Nationa
American
and 4 fits,
<i>2</i> , 3,
classes 1,
s of
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									Size	s						
			1	11%	11/4	138	1½	134	2	214 2	12 23	3	334	335	334	4
								E	breads I	er inch						
			∞	7	2	9	9	5	4 1/2	172	4	4	4	4	4	4
$M_{ajor}$ diameter of setting plug $\begin{cases} C \\ C \\ C \end{bmatrix}$	ars FOR SCREWS Jlass 1		$ \begin{array}{c c} Inch \\ 9966 \\ 9959 \\ 0000 \\ 9993 \\ 1 \end{array} \\ \end{array} $	nches 1211 1204 1264 1243 1243	<i>nches</i> 2461 1 2454 1 2454 1 24593 1 2493 1	Inches 3706 3750 3750 3750 3742	Inches . 4956 . 4948 . 5000 . 4992	Inches 1. 7448 1. 7440 1. 7492 1. 7492	<i>Inches Inches Inches 1</i> , 9943 2. 00000 2. 00000 2. 00000 2. 00000 2. 00000 2. 000000 2. 0000 2.	2443 2. 2435 2. 2435 2. 2500 2. 2492 2.	ches Inc 9362.7 9272.7 9912.7 9912.7	$\begin{array}{c}hes\\hes\\1362.96\\5003.06\\4272.96\\12.96\\12.96\end{array}$	ies Inch 363 24 273. 24 000 3. 25 091 3. 24	es Inch 363.49 273.49 003.500 313.49	28 Inche 28 Inche 28 743 742 03.749 03.749 13.749	8 <i>Inches</i> 53.9936 73.9927 73.9927 13.9991
5	Mi Mi Mi Mi Mi	n., class X n., class X x., class Y n., class Y x., class Z	. 91541 . 91501. . 91521. . 91471. . 91481.	0283 1 0279 1 0281 1 0281 1 0276 1 0277 1	1533 1 1529 1 1529 1 1531 1 1526 1 1526 1 1527 1	2623 1 2619 1 2619 1 2615 1 2617 1	. 3873 . 3869 . 3865 . 3865 . 3865	L. 6149 L. 6145 L. 6145 L. 6146 L. 6141 L. 6141	L 85002. L 84962. L 84922. L 84922.	10002. 09962. 09972. 09932.	312255 309255 3032255 3032255	800 10 10 10 10 10 10 10 10 10	05 05 03 03 03 03 05 05 05 05 05 05 05 05 05 05 05 05 05	233 233 233 233 233 233 233 233 233 233	23.581 83.580 83.580 83.580 83.580 83.580 83.580	23. 8312 83. 8308 93. 8309 93. 8309 83. 8309 83. 8309
Pitch diameter of setting plug or C	[Mi Mi Dlass 2, free fit, and Mi class 3, medium fit. Mi	n., class Z ix., class Z n., class X ix., class Y	9141 1. 9188 1. 9188 1. 9184 1. 9186 1.	0270 10322 11 0322 11 0322 11 0322 11 0320 11 0320 11 0320 11 0320 11 0320 11 0315 11 0	. 1520 1 . 1572 1 . 1568 1 . 1568 1 . 1570 1	2609 2667 2663 2664 2664			1.84852. 1.85572. 1.85532. 1.85542. 85423	09852 10572 10532 10542	2962.5 33762.5 337322.5 337322.5	79612 87612 87222 87322 87322 9873 9873 9873 9873 9873 9873 9873 9873	9663.077 7763.08 7733.08 7733.08	763.33 763.33 733.33	63.587 63.587 23.587 33.587 33.587	33.8296 33.8376 33.8372 33.8372 33.8373 33.8373
(c	Class 4, close fit{ $M_{\rm M}^{\rm c}$	ux., class W	91951	0330 1 03275 1	15775	2676	3926	6211	L 8568 2.	1068 2.	389 2. 5	889 2.2.2	8893.08 863.08	800 80 80 80 80 80 80 80 80 80 80 80 80	03.588 63.588	93.8389 33.8386
Minor diameter of ring gage	. Classes 1, 2, 3, and 4 ${I \choose N}$	dax. 1	. 8640	9704 1	. 0954 1 . 0947 1	. 1946 1	. 3196	L. 5335	l. 7594 2. l. 7586 2.	0094 2.5	234 2.4	794 2. 75 785 2. 75	94 2.97	94 3. 220 35 3. 220	43.479	13.7294 53.7285
D "NOT GO" G	AGES FOR SCREWS															
Major diameter of setting plug	Class 1{ [] Classes 2, 3, and 4{]	Ain Aax Ain Aax	. 9744 1. 9751 1. 9848 1. 9855 1.	0963 1 0970 1 1080 1 1087 1	2213 1 2220 1 2330 1 2337 1	. 3416 . 3424 . 3548 . 3556	. 4666 . 4674 . 4798 . 4806	L. 7110 L. 7118 L. 7268 L. 7276	L. 9575 2. L. 9583 2. L. 9754 2. L. 9754 2.	2075 2. 2083 2. 2246 2. 2254 2.	528 2. 7 537 2. 7 720 2. 7 729 2. 7	028 2.90 037 2.90 220 2.97 229 2.97	28 37 37 20 3.22 20 3.22 20 3.22 20 3.22 20 3.22 20 3.22	28 3. 45 37 3. 45 20 3. 47 29 3. 47	83.702 773.703 03.722 93.722	83.9528 73.9537 03.9720 3.9729
Fitch diameter of setting plug or, ring gage.	Class 1, loose fit	din dax din din din din	90431 90471 91121 91121 91161 91341 91381 91381	0159 1 0163 1 0237 1 0241 1 0267 1 0267 1 0300 1 030251	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2478 1 2482 1 2566 1 2570 1 2596 1 2596 1 2690 1 2690 1 2642 1 2642 1 2642 1	3728 3732 3816 3820 3846 3850 3850 3890	L 5980 1 L 5984 1 L 6085 1 L 6085 1 L 6089 1 L 6119 1 L 6112 1 L 6112 1 L 6170 1 L 6170 1	L 83162. L 83202. L 84302. L 84342. L 84342. L 84722. L 85242. L 85242.	08162. 08202. 09302. 09342. 09722. 10242. 102722.	11082.5 1122.5 2362.5 22402.5 3412.5 3412.5 3412.5 3412.5	808 2 81 736 2 81 736 2 81 779 2 85 841 2 85 841 2 85 842 85	08 3.06 33.06 35 3.07 35 3.07 279 3.07 279 3.07 279 3.07 279 3.07 279 3.07 279 3.07 279 3.07 279 3.07 283 3.07 279 3.07 283 3.07 20 20 20 20 20 20 20 20 20 20 20 20 20	200 200 200 200 200 200 200 200	83. 560 23. 560 63. 573 03. 574 93. 577 13. 584 13. 584 13. 584	833.8108 23.8112 23.8112 33.8236 03.8240 03.8240 03.8240 13.8341 13.8341 13.8341
Minor diameter of ring gage	. Classes 1, 2, 3, and 4 $\{ I \}$	4in. 2	. 8910 1.	0006 1 0013 1	. 1256 1	2209 1	3549	. 5760	L. 8068 2. L. 8076 2.	0568 2.	8262.5 8352.5	326 2. 78 335 2. 78	36 3. 03 35 3. 03	263.28	63. 532	33. 7826 53. 7835

1 <sup>2</sup> See footnotes on p. 63.

				M	achine sc	rew nun	nber or n	ominal s	size			
	0	1	2	e	4	2	9	80	10	12	14	§1.e
						Threads	per inch					
	80	72	64	56	48	44	40	36	32	28	82	24
"Go" GAGES FOR SCREWS Major diameter of setting plugClass 1RMin Classes 2, 3, and 4. [Min	$\begin{bmatrix} Inch \\ 0.0593 \\ 0.0590 \\ 0.0590 \\ 0.0600 \\ 0.0597 \end{bmatrix}$	$Inch \\ 0.0723 \\ .0720 \\ .0730 \\ .0727 \\ .072$	$\begin{array}{c c} Inch \\ Inch \\ 0.0853 \\ 0.0849 \\ 0.0860 \\ 0.0856 \end{array}$	Inch 0.0982 .0978 .0990 .0986	Inch 0.1111 1107 11107 11120	Inch 0.1241 .1237 .1250 .1250	Inch 0.1370 .1366 .1380 .1380	Inch 0.1629 .1625 .1640 .1636	Inch 0. 1889 1885 1900 1896	Inch 0. 2148 . 2143 . 2160 . 2155	Inch 0. 2488 2483 2483 2483 2483	Inch 0.3112 .3107 .3125 .3125
Max, class X Max, class X Max, class Y Class 1, loose fitMin, class Y	- 0512 - 0510 - 0509	. 0631 . 0631 . 0632 . 0630	. 0752 . 0750 . 0751	. 0866 . 0865 . 0865 . 0862	. 0976 . 0974 . 0975 . 0972	.1093 .1091 .1092 .1089	.1208 .1206 .1207	. 1449 . 1447 . 1448 . 1448	.1686 .1683 .1683 .1685	. 1916 . 1913 . 1914 . 1914	2256 2253 2254 2254	. 2841 . 2838 . 2839 . 2839
Pitch diameter of setting plug or ring Class 2, free fit, Max., class Z gage. Max., class Z gage. Max., class X dium fit. Max., class Y	. 0516 . 0519 . 0517 . 0517 . 0517 . 0518	. 0631 . 0640 . 0640 . 0638 . 0639 . 0637	.0750 .0746 .0759 .0757 .0758	0864 0859 0874 0874 0872 0872 0872 0872 0870	.0974 .0969 .0985 .0983 .0984	.1091 .1086 .1102 .1102 .1101	. 1201 . 1201 . 1218 . 1216 . 1217	1446 1441 1460 1458 1458 1456	.1683 .1678 .1678 .1697 .1694 .1696 .1693	. 1913 . 1908 . 1928 . 1925 . 1926 . 1933	. 2253 2248 . 2248 . 2268 . 2266 . 2266	2838 2832 2854 2851 2851 2852 2849
(Class 4, close fit{ Min., class W { Min., class W											. 2269	.2857
Minor diameter of ring gage	0465	. 0580	.0687	. 0797	.0894	. 1004	. 1109	.1339	.1562 .1558	.1773 .1768	. 2113	. 2674
Major diameter of setting plug{Min	- 0545 - 0548 - 0566 - 0569	.0673 .0676 .0694 .0697	. 0801 . 0805 . 0822 . 0826	. 0926 . 0930 . 0950 . 0954	.1049 .1053 .1076 .1080	. 1177 . 1181 . 1204 . 1208	.1302 .1306 .1332 .1333	.1557 .1561 .1590 .1594	. 1813 . 1817 . 1846 . 1850	. 2062 . 2067 . 2098 . 2103	2402 2407 2438 2438	.3020 .3025 .3059 .3064
Pitch diameter of setting plug or ring Class 2, free fit{Max	. 0188 . 0490 . 0502 . 0504 . 0506 . 0506	.0608 .0610 .0622 .0624 .0624 .0629	.0726 .0728 .0740 .0745 .0745 .0747	$\begin{array}{c} 0838\\ 0840\\ 0854\\ 0856\\ 0856\\ 0859\\ 0861\\ 0861 \end{array}$	$\begin{array}{c} .0945\\ .0947\\ .0963\\ .0965\\ .0965\\ .0969\\ .0971\\ .0971\end{array}$	. 1061 . 1063 . 1079 . 1081 . 1086	.1174 .1176 .1194 .1194 .1201 .1203	.1413 .1415 .1435 .1437 .1437 .1442 .1444	.1648 .1651 .1670 .1670 .1673 .1673 .1673 .1678	$ \begin{array}{c}     .1873 \\     .1876 \\     .1897 \\     .1900 \\     .1906 \\     .1909 \\     .1909 \\   \end{array} $	2213 2216 2237 2240 2240 2249 2259	2795 2798 2821 2824 2830 2833 2838 2838 2846 2846
Minor diameter of ring gage{and 4, 1, 2, 3, {Min, <sup>2</sup> }}	- 0489	. 0607	. 0721	. 0831 . 0835	. 0936	.1049	. 1159	.1395	.1625 .1629	.1846	.2186	.2769

1 2 See footnotes, p. 63.

DIMENSIONAL LIMITS OF GAGES

TABLE 24.—Limiting dimensions of setting plug and thread ring gages for screws of classes 1, 2, 3, and 4 fits, American National fine-thread series—Continued

						Siz	Se						
	3%	7/16	375	9/6	58	34	%	1	1}6	114	13%	1}5	
		-		-		<b>Fhreads</b>	per inch						14111
	24	30	30	18	18	16	14	14	12	12	12	12	
"Go" GAGES FOR SCREWS	•			1	T	Total	1	Tack	Trates	Tucker	Tuchan	Tuches	
Major diameter of setting plug	Inch 0.3737 .3732 .3750 .3745	1 mcn 0. 4360 . 4355 . 4375 . 4375 . 4370	1ncn 0.4985 .4980 .5000 .4995	1 nch 0.5609 .5604 .5625 .5620	1 mcn 0. 6234 . 6229 . 6250 . 6245	1ncn 0.7482 .7476 .7500 .7494	1 nch 0.8729 .3723 .8750 .8750	1 ncn 0. 9979 . 9973 1. 0000 . 9994	1. 1226 1. 1226 1. 1220 1. 1250 1. 1244	1.2476 1.2476 1.2470 1.2500 1.2594	1.3726 1.3726 1.3720 1.3750 1.3744	1. 4976 1. 4970 1. 5000 1. 4994	SOILD W
Max, class X Min, class X	. 3466 . 3463 . 3464	. 4035 . 4032 . 4033	. 4660 . 4657 . 4658	. 5248 . 5245 . 5246	. 5873 . 5870 . 5871	. 7076	.8265 .8262 .8263	.9515 .9512 .9513	$\begin{array}{c} 1.\ 0685\\ 1.\ 0682\\ 1.\ 0683\\ 1.\ 0683\\ \end{array}$	$\begin{array}{c} 1.\ 1935\\ 1.\ 1932\\ 1.\ 1933\\ 1.\ 1933\\ 1.\ 1933\\ 1.\ 1933\\ 1.\ 1000\ 1.\ 1000\\ 1.\ 1000\$	$\begin{array}{c} 1.3185\\ 1.3182\\ 1.3182\\ 1.3183\\ 1.3182\\$	$1.4435 \\ 1.4432 \\ 1.4433 \\ 1.4433 \\ 1.4433 \\ 1.4430 \\ 1.4430 \\ 1.4400 \\ 1$	1 1110
Mary class Y	.3461	. 4032	. 4657	. 5243 . 5244 5238	. 5869	. 7072	.8261 .8261	. 9511	1. 06/9 1. 0681 1. 0674	1. 1924 1. 1931	1.3181	1.4431 1.4431 1.4424	
Pitch diameter of setting plug or ring Class 2. free fit. Max. class Z.	.3479	. 4050	. 4675	. 5264	. 5889	. 7094	.8286	.9536	1. 0709	1. 1959	1.3209	1.4459	D
gago. and class 3, me <sup>-</sup> Max, class Y dium fb. Max, class Y Min, class Y	. 3470 . 3477 . 3474 . 3489	. 4048 . 4048 . 4045 4053	. 4673 . 4673 . 4670	. 5262 . 5262 . 5259	.5887 .5884 .5884	.7092	. 8284 . 8284 . 8280	. 9534 . 9534 . 9530	1. 0707 1. 0707 1. 0703 1. 0714	1. 1957 1. 1957 1. 1953 1. 1953	1.3207 1.3207 1.3203 1.3214	1.4457 1.4453 1.4464	00111.
Class 4, close fif{Min., class W	.3481	.4052	.4677	. 5266	. 5891	. 7097	. 82885	.95385	1.07125	1. 19625	1. 32125	1.44625	LAT T 1
Minor diameter of ring gage{Classes 1, 2, 3, {Max <sup>1</sup> } and 4. [Min	. 3299	.3834	. 4459	.5024	.5649 .5644	. 6823	11267.	.9227	1.0348 1.0342	1. 1598 1. 1592	1.2848 1.2842	1.4098 1.4092	0010

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<sup>1</sup> The maximum minor diameter of the "go" thread ring gage is the same as the minimum minor diameter of the tapped hole. <sup>2</sup> In order that the "not go" gage may check pitch diameter only, it is necessary that the minor diameter of the "not go" ring gage shall never be less than that specified for the "go". Furthermore, it is desirable that the created a considerable amount, as shown in fig. 18, in order to minimize the effect of angle eror on the fact of the "not go" ring gage with the product. A truncation from the basic dimension corresponding to a width of the "not go" ring momentation of the "not go" gage with the product. A truncation from the basic dimension corresponding to a width of the "not go" gage with the product. The turo the safe represent these conditions.

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								A	Iachin	e screv	⊿um	Der or I	omina	l size						1
			1	5	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	4	2		8	0	2 1	14	9	3 7/16		9/6	- 12 - 12 - 12	34	\$2	- 20
		1								Τĥ	reads p	er inch								1
			64	56	48	40	40 3	32 3	2	4	2 2	0 15	3 16	14	13	12	=	10	6	
"Go" Major diameter of plug 3, and 4.	GAGES FOR NUT gage, classes 1, 2,	rs {Min0	Inch 0.0730 0.0734	<i>Inch</i> 0860 0. 0864	nch 1 09900. 0994	$\begin{bmatrix} nch & I \\ 1120 & 0. \\ 1124 & . \end{bmatrix}$	nch $In$ $In$ $1250$ $0.1$ $1254$ $.1$	vch In 380 0.1 384	2ch In 640 0.1 644 .1	cch I7. 900 0.2 905 .2	2ch In 160 0.2 165 .2	ch $In500 0.31505 .31$	ch Inc 25 0. 37 30 . 37	2h Inc. 50 0.437 56 .438	h Inc 5 0.500 1.500	h Inc 0 0.562 06 .563	h Inc 55 0.621 11 .621	h Inc 10 0.75 16 .75	h Inc 00 0.871 06 .871	ch 750
Pitch diameter Cla. of plug gage. Cla: Cla:	ss 4	(Min., class W Max., class W Min., class X Max., class X Min., class Y Max., class Y Max., class Z	0629 0631 0631 0633 0633 0635	0746 0746 0746 0746 0746 0751	0857 0857 0857 0859 0857 0857 0857	0959 0960 0965 0965 0965	1090 1092 1096 1092	1177 1177 1180 1181 185 185	[437]           [437]           [440]           [441]           [441]           [445]	629 631 631 632 11 633 11 632 11 632 11	8992 22 8922 22 8924 22 8928 2	175 1778 1778 180 180 1778 180 1778 1778 17	764	444 .391 445 .391 447 .391 446 .391 446 .391 550 .391 550 .391 551 .392	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	00000000000000000000000000000000000000	260 260 260 260 260 260 260 260 260 260	00100 0000 0000 0000 0000 0000 0000 00	00000000000000000000000000000000000000	403350128028 333520128028
"Nor G Major diameter of plug 3, and 4	o" GAGES FOR N gage, classes 1, 2,	JUTS [Max. <sup>1</sup>	0020	0825	0949 0945	1070	1200 .1	316 .1	576 .1	815 . 2 810 . 2	075 .2	397 .30 392 .30	05 . 36	21 . 422 15 . 422	6 . 483	. 545 . 545 . 544	11 1000 1000 1000		88 - 85 . 85	216
Pitch diameter Cla. of plug gage. Cla.	ss 1, loose fit ss 2, free fit ss 3, medium fit ss 4, close fit	Min Min Miax Miax Miax Min Min Min	0655 0653 0653 0648 0648 0648 0641	0772 0770 0764 0762 0759	0886 0877 0877 0877 0871 0871	0992 0982 0982 0975 0975	1122 11120 1110 1110 11103 11103 1103	215 .1 204 .1 201 .1 196 .1 193 .1	475 .1 475 .1 464 .1 464 .1 464 .1 461 .1 455 .1 455 .1 .1 .1 455 .1 .1 .1 .1 .1 .1 .1 .1 .1 .1 .1 .1 .1	675 672 .1 662 .1 653 .1 653 .1	91935 .2 919 .2 919 .2 919 .2 919 .2 919 .2	2228 2211 2211 2223 2228 2228 2228 2228	221 321 3318 334 302 333 302 333 794 333 799 335 799 3	007 395 004 395 889 395 886 395 886 395 886 395 860 392 773 394 773 394 800 392 599 392	1 457 8 457 1 457 1 457 1 457 1 453 1	71 510 11 510 11 510 11 510 12 512 12 512	251 257 257 257 257 257 257 257 257 257 257	91 9 7 9 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	71 800 71 800 71 800 71 800 71 800 71 800 71 800 71 800 71 800	000225880000000000000000000000000000000

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		1}8	114	13%	1½	134	63	214	21/2	34	3	¥ 3	72 3	34	4
						£	hreads	per inc	q						
	80	7	7	8	9	2	4 }2	41/2	4	4	4	4	4	4	4
" Go" GAGES FOR NUTS Major diameter of plug gage, classes 1, 2, 3, and 4{Máx	Inches 1 1. 0000 1 1. 0007 1	nches 1250 1257	Inches 2500 1	Inches . 3750	Inches 1.5000 1.5008	Inches 1. 7500* 1. 7508	Inches I 2.00002 2.00082	nches In 25002. 25082.	17 2009 2. 5009 2.	ches Inc 75003.0 75093.0	Ches In 00003.5	<i>ches In</i> 25003. 25093.	5000 3. 5000 3.	ches In 7500 4. 7509 4.	tches 0000
Pitch diameter of plug gage{Min., class W	91921 91921 91921 91921 91921 91951 91941	$\begin{array}{c} 0322\\ 03245\\ 03245\\ 0328\\ 032$	1572 1574 1574 1574 1576 1576 1579 1579 1579 1579 1579	2667 26695 2667 2671 2671 2673 2673 2673 2673 2673 2673 2673	L 3917 L 39195 L 39195 L 3917 L 3921 L 3921 L 3923 L 3931	1. 6201 1. 62035 1. 62035 1. 6204 1. 6204 1. 6209 1. 6209 1. 6208	1. 8557 2 1. 8557 2 1. 8560 2 1. 8560 2 1. 8560 2 1. 8566 2 1. 8566 2 1. 8572 2 1. 8572 2 1. 8572 2	$\begin{array}{c} 10572.\\ 10602.\\ 10612.\\ 10662.\\ 10662.\\ 10662.\\ 10662.\\ 10722.\\ \end{array}$	33762. 33792. 33792. 33802. 33852. 33852. 338352. 338352. 33822.2	58762.8 58762.8 58762.8 58792.8 588792.8 58852.8 58852.8 58922.8	33763. 33763. 33763. 33793. 33853. 33853. 33853.	08763. 08763. 08793. 08853. 088233.	33763. 33763. 33793. 33793. 33853. 33853. 338233.	5876 3. 5876 3. 5879 3. 5879 3. 5885 3. 5883 3. 5884 3	8376 8379 8379 8379 8380 8379 8385 8385 8385 8385 8385 8385 8385
"NOT GO" GAGES FOR NUTS															
Major diameter of plug gage, classes 1, 2, 3, and 4{Max. <sup>1</sup>	. 97361.	0948 1000000000000000000000000000000000000	2198 1	. 3397	. 4647	1. 7075	1.9527 $2.9519$ $2$	2027 2. 2019 2.	4468 2. 4459 2.	6968 2.9 6959 2.9	9468 3. 9459 3.	1968 3. 1959 3.	1468 3. 1459 3.	5968 3. 3959 3.	9468 9459
Pitch diameter of plug gage	92991 92691 92691 92691 92691 9281 92381 92381	$\begin{array}{c} 0446 \\ 0442 \\ 0407 \\ 0403 \\ 0381 \\ 0377 \\ 0357 \\ 0352 \\ 03495 \\ 1 \\ 03495 \\ 1 \\ 03495 \\ 1 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0$	$\begin{array}{c} 1696 \\ 1692 \\ 1692 \\ 1657 \\ 1653 \\ 1631 \\ 1631 \\ 1602 \\ 1002 \\ 10$	2812 2808 2808 2768 2768 2768 2738 2705 2705	$\begin{array}{c} 1.4062\\ 1.4058\\ 1.4018\\ 1.4018\\ 1.3988\\ 1.3988\\ 1.3953\\ 1.39505\\ 1.3$	L. 6370 1. 6366 1. 6317 1. 6313 1. 6313 1. 6233 1. 6233 1. 62395 1. 62395	1. 87412 1. 87372 1. 86842 1. 86842 1. 86842 1. 86462 1. 86422 1. 86422 1. 86422 1. 86422 1. 86982 1. 869852 1. 869852 1. 869852 1. 869852 1. 869852 1. 869852 1. 869	$\begin{array}{c} 1241 \\ 1237 \\ 1184 \\ 1180 \\ 1180 \\ 1142 \\ 1101 \\ 2. \\ 1101 \\ 2. \\ 1008 $	3580 2. 3576 2. 3516 2. 3516 2. 3473 2. 3424 2. 3424 2.	60802.8 60762.8 60162.8 60122.8 59732.8 592692.8 59242.8	85803. 85163. 85163. 85123. 84733. 84733. 84243. 84213.	10803. 10763. 10163. 09733. 092444.	35803. 35763. 35163. 35123. 34733. 34243. 34243.	30803. 50763. 50163. 59733. 59243. 59213.	8580 8576 8576 8516 8512 8473 8473 8473 8424 8424 8424



				W	achine so	rew nun	ther or n	ominal s	ize			
	0	1	63	en	4	2	9	90	10	12	14	<u> </u>
						Threads	per inch					
	80	72	64	56	48	44	40	36	32	58	*	24
"Go" GAGES FOR NUTS Major diameter, classes 1, 2, 3, and 4	Inch 0.0600 .0603	Inch 0. 0730 . 0733	Inch 0. 0860 . 0864	Inch 0. 0990 . 0994	Inch 0. 1120 . 1124	Inch 0. 1250 . 1254	Inch 0. 1380 . 1384	<i>Inch</i> 0. 1640 . 1644	Inch 0. 1900 . 1904	<i>Inch</i> 0. 2160 . 2165	Inch 0. 2500 . 2505	Inch 0.3125 .3130
Pitch diameter of plug gage	.0521 .0521 .0520 .0520 .0521 .0522	. 0640 . 0640 . 0641 . 0643 . 0643 . 0643	. 0769 . 0769 . 0761 . 0760 . 0760 . 0761	.0874 .0876 .0876 .0875 .0875 .0878	0985 0985 0986 0989 0989 0987 0987		. 1218 . 1220 . 1220 . 1222 . 1222	. 1460 . 1460 . 1461 . 1461 . 1464 . 1464 . 1468		. 1928 . 1931 . 1930 . 1933 . 1933	2268 2268 2271 2271 2271 2271 2271 2271	$\begin{array}{c} 2854\\ 2855\\ 2855\\ 2856\\ 2856\\ 2856\\ 2856\\ 2856\\ 2855\\$
". Nor Go" GAGES FOR NUTS Major diameter of plug gage, classes 1, 2, 3, and 4	.0576	0020	. 0830	. 0955	.1079	.1205	.1330	.1584	.1836	. 2088	. 2428 . 2423	. 3040 . 3035
Pitch diameter of plug gage Class 2, free fit{Max Min Class 3, medium fit. [Min	.0530 .0534 .0534 .0534 .0532 .0530	. 0665 . 0663 . 0658 . 0658 . 0656 . 0653 . 0651	. 0785 . 0778 . 0778 . 0778 . 0778 . 0777 . 0777 . 0777	. 0902 . 0900 . 0894 . 0892 . 0889 . 0889	. 1016 . 1014 . 1007 . 1005 . 1001 . 0999	. 1134 . 1132 . 1125 . 1123 . 1118 . 1116	.1252 .1250 .1242 .1242 .1235	. 1496 . 1494 . 1485 . 1483 . 1478 . 1476	. 1735 . 1732 . 1724 . 1724 . 1716 . 1713	. 1971 . 1968 . 1959 . 1956 . 1950 . 1947	2311 2308 2296 2296 2296 2296 2287 2287 2279	. 2900 . 2897 . 2887 . 2884 . 2884 . 2875 . 2865 . 2865

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						Siz	So					
	3%	7/16	34	9/6	86	34	8%	1	11%	1}4	13%	1}2
					T	ireads pe	r inch					
	24	20	20	18	18	16	14	14	12	12	12	12
"Go" GAGES FOR NUTS Major diameter, classes 1, 2, 3, and 4	Inch 0. 3750 . 3755	Inch 0. 4375 . 4380	Inch 0. 5000 . 5005	Inch 0. 5625 . 5630	Inch 0. 6250 . 6255	Inch 0. 7500 . 7506	Inch . 8750 . 8756	<i>Inches</i> 1. 0000 1. 0006	Inches 1. 1250 1. 1256	<i>Inches</i> 1. 2500 1. 2506	Inches 1. 3750 1. 3756	<i>Inches</i> 1. 5006 1. 5006
Pitch diameter of plug gage	$\begin{array}{c} 3479\\ 3479\\ 3479\\ 3480\\ 3482\\ 3482\\ 3481\\ 3482\\$	$\begin{array}{r} 4050\\ 4051\\ 4051\\ 4050\\ 4053\\ 4053\\ 4053\\ 4053\\ 4053\\ 4059\end{array}$	4675 4675 4675 4675 4678 4677 4678 4678	. 5264 . 5264 . 5264 . 5267 . 5266 . 5269 . 5269	$ \begin{array}{c} 5889\\ 5890\\ 5892\\ 5892\\ 5892\\ 5893$	7094 7095 7094 7097 7097 7096 7100	.8286 .8286 .8286 .8289 .8289 .8289 .8292 .8292 .8290 .8290	9536 95375 9536 9539 9539 9542 9542 9540	1.0709 1.07105 1.07105 1.0712 1.0712 1.0713 1.0713 1.0720	1. 1959 1. 1959 1. 1959 1. 1962 1. 1962 1. 1965 1. 1963 1. 1963	L 3209 L 3209 L 32105 L 3212 L 3212 L 3215 L 3213 L 3213 L 3213 L 3220	$\begin{array}{c} 1.\ 4459\\ 1.\ 44605\\ 1.\ 4460\\ 1.\ 4461\\ 1.\ 4461\\ 1.\ 4465\\ 1.\ 4465\\ 1.\ 4465\\ 1.\ 4463\\ 1.\ 4470\end{array}$
"Nor Go" GAGES FOR NUTS Maior diamatar of ning gaga classes 1 2 3 and 4	. 3665	. 4272	. 4897	. 5510	. 6135	. 7371	. 8601	.9851	1. 1076	1. 2326	1. 3576	1.4826
Pitch diameter of plug gage	$ \begin{array}{c} 3525\\ 3522\\ 3522\\ 3503\\ 3503\\ 3503\\ 3503\\ 3491\\ 3490\\ \end{array} $	$\begin{array}{c} 4267\\ 4101\\ 4098\\ 4098\\ 4086\\ 4083\\ 4076\\ 4073\\ 4073\\ 4063\\ 4063\\ 4063\\ 4063\\ 4063\\ 4062\\$	$\begin{array}{c} 4892 \\ 4726 \\ 4771 \\ 4711 \\ 4701 \\ 4701 \\ 4698 \\ 4688 \\ 4688 \\ 4688 \end{array}$	.5505 .5321 .5318 .5305 .5305 .5305 .5305 .5302 .5294 .5294 .5278	. 6130 5946 5943 5930 5927 5919 5919 5904 5904	. 7365 . 7157 . 7154 . 7154 . 7139 . 7136 . 7126 . 7126 . 7123 . 7120 . 7110	. 8595 . 8356 . 83355 . 83355 . 83355 . 83355 . 83355 . 83325 . 8304 . 8304 . 83025	$\begin{array}{c} .9845\\ .9606\\ .9603\\ .9585\\ .9585\\ .9582\\ .9569\\ .9569\\ .9554\\ .95525\end{array}$	1. 1070 1. 0788 1. 0785 1. 0765 1. 0765 1. 0762 1. 0749 1. 0729 1. 07275	1, 2320 1, 2038 1, 2015 1, 2015 1, 2015 1, 1999 1, 1996 1, 1979 1, 19775	L. 3570 L. 3288 L. 3286 L. 3286 L. 3286 L. 3286 L. 3286 L. 3229 L. 3229 L. 3229	$\begin{array}{c} 1.4820\\ 1.4538\\ 1.4535\\ 1.4515\\ 1.4515\\ 1.4499\\ 1.4479\\ 1.4479\\ 1.44775\\ 1.44775\end{array}$
<sup>1</sup> In order that the "not go" gage may check pitch diameter only, it is nee shall never be greater than that specified for the "go" plug gage. Furthermor	e, it is de	at the c	rest of tl	he thread	he rem	oved so t go" gage	hat the j	najor di cated a c	ameter o	f the "no	ot go" pli int, as sh	ug gage 10wn in

fig. 18, in order to minimize the effect of angle error on the fit of the "not go" gage with the product. A truncation from basic dimensions corresponding to a width of flat equal to KXp is recommended. The limiting dimensions given in this table for the major diameter of the "not go" plug gage represent these conditions.

## SECTION IV.—UNIFORM PITCH SCREW-THREAD SERIES FOR HIGH-PRESSURE FASTENINGS, RAILROAD APPLI-CATIONS, MACHINERY COMPONENTS, ETC.

#### 1. FORM OF THREAD

The American National form of thread profile as specified in section III shall be used.

# 2. THREAD SERIES

Where special threads are required, it is sometimes essential to select a certain pitch as standard for a range of sizes. Also, in general practice, where the pitch of a special thread is optional, the uniform use of a selected pitch is advantageous. For such applications 8, 12, and 16 threads per inch are widely used.

#### (a) AMERICAN NATIONAL 8-PITCH THREAD SERIES

In table 27 are specified the nominal sizes and basic dimensions of the "American National 8-pitch thread series."

Bolts for high-pressure pipe flanges, cylinder-head studs, and similar fastenings against pressure require that an initial tension be set up in the fastening, by elastic deformation of the fastening and the components held together, such that the joint will not open up when the steam or other pressure is applied. To secure a proper initial tension it is not practicable that the pitch should increase with the diameter of the thread, as the torque required to assemble the fastening would be excessive. Accordingly, for such purposes the 8-pitch thread has come into general use.

## (b) AMERICAN NATIONAL 12-PITCH THREAD SERIES

The nominal sizes and basic dimensions of the "American National 12-pitch thread series" are specified in table 28.

Sizes of 12-pitch threads from one-half inch to and including one and three-fourths inches are used in **boiler** practice, which require that worn stud holes be retapped with a tap of the next larger size, the increment being one-sixteenth inch throughout most of the range. Die-head chasers for sizes up to 3 inches are stocked by manufacturers.<sup>10</sup>

The 12-pitch threads are also widely used in machine construction, as for thin nuts on shafts and sleeves. From the standpoints of good design and simplification of practice, it is desirable to maintain shoulder diameters to one-eighth-inch steps. The 12 pitch is the coarsest in general use, which will permit a threaded collar which screws onto a threaded shoulder to slip over a shaft, the difference in diameter between shoulder and shaft being one-eighth inch.

#### (c) AMERICAN NATIONAL 16-PITCH THREAD SERIES

The nominal sizes and basic dimensions of the American National 16-pitch thread series are specified in table 29.

The 16-pitch series is a uniform pitch series for such applications as require a relatively fine thread. It is intended primarily for use on threaded adjusting collars and bearing retaining nuts.

<sup>&</sup>lt;sup>10</sup> See U.S. Department of Commerce Simplified Practice Recommendation R51-29, Die Head Chasers.

#### 3. CLASSIFICATION, TOLERANCES, AND LIMITING DIMENSIONS

The general specifications and classification of fits given in section V, herein, are applicable to the American National 8-pitch, 12-pitch, and 16-pitch thread series. The dimensions and tolerances for two classes of fit derived from tables 35 and 60 are given in tables 30, 31, and 32.

Identificatio	'n	В	asic diamete	rs		Thread data	
Sizes	Threads per inch	Major diameter, D	Pitch diameter, E	Minor diameter, K	Metric equivalent of major diameter	Helix angle at basic pitch diameter, s	Basic area of section at root of thread, $\frac{\pi K^2}{4}$
1	2	3	4	5	6	7	8
1 1 134 134 134 134 134 134 134 13	88888 88888 88888 88888 88888 88888 8888	Inches 1. 0000 1. 1250 1. 2500 1. 3750 1. 5000 1. 6250 1. 7500 2. 1250 2. 2500 2. 25000 2. 25000 2. 7500 3. 0000 3. 25000 3. 5000 3. 5000 4. 2500 4. 2500 4. 2500 4. 5000 4. 5000 5. 0000 5. 00000 5. 00000 5. 00000 5. 00000 5. 000000 5. 00000000 5. 000000000000000000000000000000000000	Inches 0.9188 1.0438 1.1688 1.2938 1.4188 1.5438 1.6688 1.7938 2.0438 2.1688 2.1688 2.1688 3.1688 3.1688 3.4188 3.6688 3.9188 4.1688	Inches 0.8376 9626 1.0876 1.2126 1.3376 1.4626 1.5876 1.5876 1.9626 2.0876 2.0876 2.5876 2.5876 3.3376 3.3376 3.5876 3.5876 4.0876 4.3376 4.5876 4.5876 4.5876 4.5876 4.5876 4.5876 4.5876 4.5876 4.5876 4.5876 4.5876 4.5876 4.5876 4.5876 5.5876	$\begin{array}{c} mm \\ 25, 400 \\ 28, 575 \\ 31, 750 \\ 34, 925 \\ 38, 100 \\ 41, 275 \\ 44, 450 \\ 47, 625 \\ 50, 800 \\ 53, 975 \\ 57, 150 \\ 63, 500 \\ 69, 850 \\ 76, 200 \\ 82, 550 \\ 88, 900 \\ 95, 250 \\ 101, 600 \\ 107, 950 \\ 114, 300 \\ 127, 000 \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Square inches 0.5510 1.1548 1.4052 2.3036 2.6521 3.0252 3.4228 4.2917 5.2588 6.3240 7.4874 8.7490 10.1088 11.5667 13.1228 14.7771
514 514 514 514 514 514	8 8 8	5. 2500 5. 5000 5. 7500	5. 1688 5. 4188 5. 6688	5. 0876 5. 3376 5. 5876	133. 350 139. 700 146. 050	0 28 0 26 0 25 0 24	20. 3290 22. 3760 24. 5211
6	8	6. 0000	5. 9188	5. 8376	152. 400	0 23	26.7645

TABLE 27.—American National 8-pitch thread series

<sup>1</sup> Standard size of the American National coarse-thread series.

NOTE.—Pitch, p=0.12500 inch; depth of thread, h=0.08119 inch; basic width of flat, p/8=0.01562 inch; minimum width of flat at major diameter of nut, p/24=0.00521 inch.

TABLE 28.—American	n National	12-pitch	thread	series
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Identificatio	n	в	asic diamete	rs		Thread day	ta
Sizes	Threads per inch	Major diameter, D	Pitch diameter, E	Minor diameter, <i>K</i>	Metric equivalent of major diameter	Helix angle at basic pitch diameter, 8	Basic area of section at root of thread $\frac{\pi K^2}{4}$
1	2	3	4	5	6	7	8
14 9/8 1 58 11/0 94	12 12 12 12 12 12	Inches 0.5000 .5625 .6250 .6875 .7500	<i>Inches</i> 0. 4459 . 5084 . 5709 . 6334 . 6959	Inches 0.3917 .4542 .5167 .5792 .6417	<i>mm</i> 12.700 14.288 15.875 17.463 19.050	Deg. Min. 3 24 2 59 2 40 2 24 2 11	Square inches 0.1205 .1620 .2097 .2635 .3234
13/18 76 15/16 1 1	12 12 12 12 12 12	.8125 .8750 .9375 1.0000 1.0625	. 7584 . 8209 . 8834 . 9459 1. 0084	.7042 .7667 .8292 .8917 .9542	20. 638 22. 225 23. 813 25. 400 26. 988	$\begin{array}{cccc} 2 & 0 \\ 1 & 51 \\ 1 & 43 \\ 1 & 36 \\ 1 & 30 \end{array}$	. 3895 . 4617 . 5400 . 6245 . 7151
1162 1346 142 1546 1546 1546 1362	12 12 12 12 12 12	1. 1250 1. 1875 1. 2500 1. 3125 1. 3750	1.0709 1.1334 1.1959 1.2584 1.3209	$\begin{array}{c} 1.\ 0167\\ 1.\ 0792\\ 1.\ 1417\\ 1.\ 2042\\ 1.\ 2667\end{array}$	28. 575 30. 163 31. 750 33. 338 34. 925	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	. 8118 . 9147 1. 0237 1. 1389 1. 2602
17/6 1½2 15/8 13/4 17/6	12 12 12 12 12 12	$\begin{array}{c} 1.\ 4375\\ 1.\ 5000\\ 1.\ 6250\\ 1.\ 7500\\ 1.\ 8750 \end{array}$	1, 3834 1, 4459 1, 5709 1, 6959 1, 8209	1. 3292 1. 3917 1. 5167 1. 6417 1. 7667	$\begin{array}{r} 36.513\\ 38.100\\ 41.275\\ 44.450\\ 47.625\end{array}$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1. 3876 1. 5212 1. 8067 2. 1168 2. 4514
2 2¼ 2½ 2¾ 3	12 12 12 12 12 12	2.0000 2.2500 2.5000 2.7500 3.0000	1. 9459 2. 1959 2. 4459 2. 6959 2. 9459	1. 8917 2. 1417 2. 3917 2. 6417 2. 8917	50, 800 57, 150 63, 500 69, 850 76, 200	$\begin{array}{c ccc} 0 & 47 \\ 0 & 42 \\ 0 & 37 \\ 0 & 34 \\ 0 & 31 \end{array}$	2, 8100 3, 6028 4, 4927 5, 4810 6, 5674
314 31 <u>4</u> 33 <u>4</u> 4	12 12 12 12	$\begin{array}{c} 3.2500 \\ 3.5000 \\ 3.7500 \\ 4.0000 \end{array}$	3. 1959 3. 4459 3. 6959 3. 9459	3. 1417 3. 3917 3. 6417 3. 8917	82. 550 88. 900 95. 250 101. 600	0 29 0 26 0 25 0 23	7.7521 9.0349 10.4159 11.8951
41/4 41/2 43/4 5	12 12 12 12 12	$\begin{array}{c} 4.\ 2500\\ 4.\ 5000\\ 4.\ 7500\\ 5.\ 0000\end{array}$	$\begin{array}{r} 4.1959 \\ 4.4459 \\ 4.6959 \\ 4.9459 \end{array}$	4. 1417 4. 3917 4. 6417 4. 8917	107. 950 114. 300 120. 650 127. 000	$\begin{array}{c ccc} 0 & 22 \\ 0 & 21 \\ 0 & 19 \\ 0 & 18 \end{array}$	13. 4725 15. 1480 16. 9217 18. 7936
5¼ 5½ 5¾ 6	12 12 12 12 12	5. 2500 5. 5000 5. 7500 6. 0000	5. 1959 5. 4459 5. 6959 5. 9459	5. 1417 5. 3917 5. 6417 5. 8917	133. 350 139. 700 146. 050 152. 400	0 18 0 17 0 16 0 15	20. 7630 22. 8319 24. 9983 27. 2628

<sup>1</sup> Standard size of the American National coarse-thread series. <sup>3</sup> Standard size of the American National fine-thread series.

Note.—Pitch, p=0.08333 inch; depth of thread, h=0.05413 inch; basic width of flat, p/8=0.01042 inch; minimum width of flat at major diameter of nut, p/24=0.00347 inch.

## UNIFORM PITCH THREAD SERIES

Identificatio	n	В	asic diamete	rs		Thread data	
Sizes	Threads per inch	Major diameter, D	Pitch diameter, E	Minor diameter, K	Metric equivalent of major diameter	Helix angle at basic pitch diameter, g	Basic area of section at root of thread, $\frac{\pi K^2}{4}$
1	2	3	4	5	6	7	8
3/4 1           7/8           1           1/4	16 16 16 16 16 16 16 16 16	Inches 0.7500 .8750 1.0000 1.1250 1.2500 1.3750 1.5000 1.6250 1.7500 1.8750	Inches 0.7094 .8344 .9592 1.0844 1.2094 1.3344 1.4594 1.5844 1.7094 1.8344	Inches 0. 6688 . 7938 1. 0438 1. 1688 1. 2938 1. 4188 1. 5438 1. 6688 1. 7938	mm 19.050 22.225 25.400 28.575 31.750 34.925 38.100 41.275 44.450 47.625	Deg. Min. 1 36 1 22 1 11 1 3 0 57 0 51 0 47 0 43 0 40 0 37	Square inches 0,3513 . 4949 . 6630 . 8557 1. 0729 1. 3147 1. 5810 1. 8719 2. 1873 2. 5272
2 2 <sup>1</sup> /8 2 <sup>1</sup> /8 2 <sup>1</sup> /4 2 <sup>1</sup> /2 2 <sup>3</sup> /4	16 16 16 16 16	2.0000 2.1250 2.2500 2.5000 2.7500	1.9594 2.0844 2.2094 2.4594 2.7094	1.9188 2.0438 2.1688 2.4188 2.6688	<b>50.</b> 800 53. 975 57. 150 63. 500 69. 850	0 35 0 33 0 31 0 28 0 25	2. 8917 3. 2807 3. 6943 4. 5950 5. 5940
3 3¼ 3¼ 3¼ 4	16 16 16 16 16	$\begin{array}{c} 3.\ 0000\\ 3.\ 2500\\ 3.\ 5000\\ 3.\ 7500\\ 4.\ 0000 \end{array}$	2. 9594 3. 2094 3. 4594 3. 7094 3. 9594	2.9188 3.1688 3.4188 3.6688 3.9188	76. 200 82. 550 88. 900 95. 250 101. 600	0 23 0 21 0 20 0 18 0 17	6. 6911 7. 8864 9. 1799 10. 5715 12. 0614

#### TABLE 29.—American National 16-pitch thread series

<sup>1</sup> Standard size of the American National fine-thread series.

NOTE.—Pitch, p=0.06250 inch; depth of thread, h=0.04059 inch; basic width of flat, p/8=0.00781 inch; minimum width of flat at major diameter of nut, p/24=0.00260 inch.

TABLE	30.— <i>Limiting</i>	dimensions	and	tolerances	, classes	2	and	3	fits,	American
		National	! 8-pi	itch thread	series					

				Si	ze (inch	es)			
Dimensions and tolerances i	1 2	11%	11/4	13%	11/2	15⁄8	13⁄4	17⁄8	2
BOLTS AND SCREWS	Inch	Inches	Inches	Inches	Inches	Inches	Inches	Inches	Inches
Classes 2 and 3, major diame- terTol	1.0000 .9848 .0152	1. 1250 1. 1098 . 0152	$1.2500 \\ 1.2348 \\ .0152$	1.3750 1.3598 .0152	1.5000 1.4848 .0152	1.6250 1.6098 .0152	1.7500 1.7348 .0152	1.8750 1.8598 .0152	2.0000 1.9848 .0152
Classes 2 and 3, minor diame- terMax. <sup>3</sup>	.8466	.9716	1.0966	<b>1. 22</b> 16	1.3466	1.4716	1.5966	1.7216	1.8466
Class 2, pitch diameter (for Max general use)	.9188 .9112 .0076	1.0438 1.0359 .0079	1.1688 1.1605 .0083	1. 2938 1. 2852 . 0086	1.4188 1.4098 .0090	1.5438 1.5345 .0093	1.6688 1.6591 .0097	1.7938 1.7838 .0100	1.9188 1.9084 .0104
Class 3, pitch diameter {Min Tol	.9188 .9134 .0054	1.0438 1.0383 .0055	1.1688 1.1630 .0058	1.2938 1.2877 .0061	1.4188 1.4125 .0063	1. 5438 1. 5373 . 0065	$1.6688 \\ 1.6620 \\ .0068$	1.7938 1.7868 .0070	1.9188 1.9115 .0073
NUTS AND TAPPED HOLES									
Classes 2 and 3, major diame- terMin.4	1.0000	1.1250	1. 2500	1.3750	1. 5000	1.6250	1.7500	1.8750	2.0000
Classes 2 and 3, minor diame-{Min ter{Min	.8647 .8795 .0148	.9897 1.0032 .0135	${}^{1.\ 1147}_{1.\ 1282}_{.\ 0135}$	1.2397 1.2532 .0135	$1.3647 \\ 1.3782 \\ .0135$	${}^{1.\ 4897}_{1.\ 5032}_{.\ 0135}$	$1.6147 \\ 1.6282 \\ .0135$	1.7397 1.7532 .0135	1.8647 1.8782 .0135
Classes 2 and 3, pitch diame- terMin	. 9188	1.0438	1.1688	1. 2938	1. 4188	1.5438	1.6688	1. 7938	1.9188
Class 2, pitch diameter (for [Max. <sup>4</sup> general use)	. 9264 . 0076	$1.0517 \\ .0079$	$1.1771 \\ .0083$	$1.3024 \\ .0086$	1.4278 .0090	1.5531 .0093	1.6785 .0097	1.8038 .0100	1.9292 .0104
Class 3, pitch diameter {Max. <sup>5</sup> Tol	. 9242 . 0054	1.0493 .0055	$1.1746 \\ .0058$	1. 2999 . 0061	$1.4251 \\ .0063$	1.5503 .0065	1.6756 .0068	1.8008 .0070	1.9261 .0073

Footnotes at end of table.

				Siz	e (inch	es)			
Dimensions and tolerances <sup>1</sup>	21/8	2¼	21/2	2¾	3	334	332	3¾	4
BOLTS AND SCREWS	Inches								
Classes 2 and 3, major diame- ter	2. 1250 2. 1098 . 0152	2. 2500 2. 2348 . 0152	2. 5000 2. 4848 . 0152	2. 7500 2. 7348 . 0152	3. 0000 2. 9848 . 0152	3. 2500 3. 2348 . 0152	3. 5000 3. 4848 . 0152	3. 7500 3. 7348 . 0152	4. 0000 3. 9848 . 0152
Classes 2 and 3, minor diame- terMax. <sup>3</sup>	1.9716	2.0966	2.3466	2. 5966	2.8466	3.0966	3. 3466	3. 5966	3.8466
Class 2, pitch diameter (for Max general use)	2. 0438 2. 0331 . 0107	2. 1688 2. 1578 . 0110	2. 4188 2. 4071 . 0117	2.6688 2.6564 .0124	2.9188 2.9058 .0130	3. 1688 3. 1556 . 0132	3. 4188 3. 4055 . 0133	3. 6688 3. 6554 . 0134	3.9188 3.9053 .0135
Class 3, pitch diameter	2.0438 2.0363 .0075	2. 1688 2. 1611 . 0077	2. 4188 2. 4106 . 0082	2. 6688 2. 6601 . 0087	2.9188 2.9096 .0092	3. 1688 3. 1595 . 0093	3. 4188 3. 4095 . 0093	3. 6688 3. 6594 . 0094	3.9188 3.9093 .0095
NUTS AND TAPPED HOLES									
Classes 2 and 3, major diame- terMin.4	2.1250	2. 2500	2. 5000	2.7500	3.0000	3. 2500	3. 5000	3.7500	4.0000
Classes 2 and 3, minor diame-{Min terTol	1.9897 2.0032 .0135	2. 1147 2. 1282 . 0135	2.3647 2.3782 .0135	2. 6147 2. 6282 . 0135	2.8647 2.8782 .0135	3. 1147 3. 1282 . 0135	3.3647 3.3782 .0135	3.6147 3.6282 .0135	3.8647 3.8782 .0135
Classes 2 and 3, pitch diame- terMin	2.0438	2. 1688	2. 4188	2.6688	2.9188	3. 1688	3. 4188	3.6688	3.9188
Class 2, pitch diameter (for{Max. <sup>5</sup> general use)Tol	2.0545 .0107	2.1798 .0110	2.4305 .0117	2.6812 .0124	2.9318 .0130	3.1820 .0132	3. 4321 . 0133	3.6822 .0134	3.9323 .0135
Class 3, pitch diameter {Max. <sup>5</sup> Tol	2.0513 .0075	2. 1765 . 0077	2. 4270 . 0082	2. 6775 . 0087	2.9280 .0092	3. 1781 . 0093	3. 4281 . 0093	3.6782 .0094	3.9283 .0095
					Size (i	nches)			
Dimensions and tolerances		4¼	41/2	43⁄4	5	51⁄4	51/2	53/4	6
BOITS AND SOPEWS		Inches							

TABLE	30Limiting	dimensions	and to	olerances,	classes	2	and	3	fits,	American
	Ň	ational 8-pit	ch three	ad series-	-Contir	nue	ed		• •	

				Size (i	nches)			
Dimensions and tolerances	41⁄4	41/2	43/4	5	51⁄4	51/2	53/4	6
BOLTS AND SCREWS	Inches	Inches						
Classes 2 and 3, major diameter Min Tol	4. 2348 4. 2348 . 0152	4. 5000 4. 4848 . 0152	4.7348 .0152	4. 9848 . 0152	5. 2348 5. 0152	5. 4848 . 0152	5.7348 .0152	5. 9848 . 0152
Classes 2 and 3, minor diameter Max. <sup>3</sup> .	4.0966	4. 3466	4. 5966	4. 8466	5. 0966	5. 3466	5. 5966	5.8466
Class 2, pitch diameter (for general use)	4. 1688 4. 1551 . 0137	4. 4188 4. 4050 . 0138	4. 6688 4. 6549 . 0139	4.9188 4.9048 .0140	5. 1688 5. 1547 . 0141	5. 4188 5. 4046 . 0142	5.6688 5.6545 .0143	5.9188 5.9044 .0144
Class 3, pitch diameter $\begin{cases} Max_{-} \\ Min_{-} \\ Tol_{-} \end{cases}$	4. 1688 4. 1592 . 0096	4. 4188 4. 4091 . 0097	4.6688 4.6590 .0098	4. 9188 4. 9089 . 0099	5. 1688 5. 1589 . 0099	5. 4188 5. 4088 . 0100	5.6688 5.6587 .0101	5.9188 5.9086 .0102
NUTS AND TAPPED HOLES								
Classes 2 and 3, major diameter Min.4.	4. 2500	4. 5000	4. 7500	5.0000	5.2500	5. 5000	5.7500	6.0000
Classes 2 and 3, minor diameter	4. 1147 4. 1282 . 0135	4. 3647 4. 3782 . 0135	4. 6147 4. 6282 . 0135	4.8647 4.8782 .0135	5. 1147 5. 1282 . 0135	5. 3647 5. 3782 . 0135	5. 6147 5. 6282 . 0135	5.8647 5.8782 .0135
Classes 2 and 3, pitch diameter Min	4. 1688	4. 4188	4. 6688	4.9188	5. 1688	5. 4188	5. 6688	5. 9188
Class 2, pitch diameter (for general {Max. <sup>5</sup> _ use){Tol	4. 1825 . 0137	4. 4326 . 0138	4. 6827 . 0139	4. 9328 . 0140	5. 1829 . 0141	5. 4330 . 0142	5. 6831 . 0143	5.9332 .0144
Class 3, pitch diameter $\{ \begin{array}{c} Max, b \\ Tol \\ - \end{array} \}$	4. 1784 . 0096	4. 4285 . 0097	4.6786 .0098	4. 9287 . 0099	5. 1787 . 0099	5. 4288 . 0100	5. 6789 . 0101	5.9290 .0102

<sup>1</sup> Pitch diameter tolerances include errors of lead and angle. The class 2 tolerances are based on the formulas in table 60 and a length of engagement equal to the basic major diameter for sizes from 1½ to 3 inches, inclusive, and a length of engagement equal to the basic major diameter for sizes from 1½ to 3 inches, inclusive, and a length of engagement of 3 inches for sizes over the 3-inch. The class 3 tolerances are 70 percent of the class 2 tolerances. The 1-inch size being in the American National coarse-thread series, the tolerances for this size correspond to that series.

the tolerances for this size correspond to that series. <sup>3</sup> Standard size screw and nut of the American National coarse-thread series. <sup>3</sup> Dimensions given for the maximum minor diameter of the screw are figured to the intersection of the worn tool arc with a center line through crest and root. The minimum minor diameter of the screw shall be that corresponding to a flat at the minor diameter of the minimum screw equal to  $\frac{1}{2} \times p$ , and may be determined by subtracting 0.0812 inch from the minimum pitch diameter of the screw. <sup>4</sup> Dimensions for the minimum major diameter of the nut correspond to the basic flat ( $\frac{1}{2} \times p$ ), and the profile at the major diameter produced by a worn tool must not fall below the basic outline. The maxi-mum major diameter of the nut shall be that corresponding to a flat at the major diameter of the maximum nut equal to  $\frac{1}{12} \times \frac{1}{12} + \frac$ 

nut equal to  $\frac{1}{24} \times p$ , and may be determined by adding 0.0992 inch to the maximum pitch diameter of

<sup>b</sup> These dimensions are the minimum metal or "not go" size. The "go" or basic size is the one that should be placed on the component drawing with the tolerance.

					Size (i	nches)				
Dimensions and tolerances 1	1/2	%16 <sup>2</sup>	5⁄8	11/16	3⁄4	13/16	7/8	15/16	1	11/16
BOLTS AND SCREWS	Inch	Inch	Inch	Inch	Inch	Inch	Inch	Inch	Inch	Inches
Classes 2 and 3, major diameter . Min Tol	. 4888 . 0112	. 5513 . 0112	. 6138 . 0112	. 6763	.7388 .0112	. 8013 . 0112	. 8638 . 0112	. 9263 . 0112	. 9888 . 0112	1. 0625 1. 0513 . 0112
Classes 2 and 3, minor diameter. Max. 4	. 3978	. 4603	. 5228	. 5853	. 6478	.7103	. 7728	. 8353	. 8978	. 9603
Class 2, pitch diameter (for gen- eral use)	. 4459 . 4403 . 0056	. 5084 . 5028 . 0056	. 5709 . 5653 . 0056	.6334 .6278 .0056	. 6959 . 6903 . 0056	.7584 .7528 .0056	.8209 .8153 .0056	.8834 .8778 .0056	.9459 .9403 .0056	1.0084 1.0028 .0056
Class 3, pitch diametor	.4459 .4419 .0040	. 5084 . 5044 . 0040	. 5709 . 5669 . 0040	. 6334 . 6294 . 0040	. 6959 . 6919 . 0040	.7584 .7544 .0040	.8209 .8169 .0040	. 8834 . 8794 . 0040	.9459 .9419 .0040	1.0084 1.0044 .0040
NUTS AND TAPPED HOLES										
Classes 2 and 3, major diameter. Min. 3.	. 5000	. 5625	. 6250	. 6875	. 7500	.8125	. 8750	.9375	1. 0000	1.0625
Classes 2 and 3, minor diameter. $\begin{cases} Min\\Max\\Tol\end{cases}$	. 4098 . 4225 . 0127	. 4723 . 4850 . 0127	. 5348 . 5438 . 0090	. 5973 . 6063 . 0090	. 6598 . 6688 . 0090	.7223 .7313 .0090	. 7848 . 7938 . 0090	. 8473 . 8563 . 0090	. 9098 . 9188 . 0090	.9723 .9813 .0090
Classes 2 and 3, pitch diameter Min	. 4459	. 5084	. 5709	. 6334	. 6959	.7584	. 8209	. 8834	. 9459	1.0084
Class 2, pitch diameter	. 4515 . 0056	. 5140 . 0056	. 5765 . 0056	. 6390 . 0056	. 7015 . 0056	. 7640 . 0056	. 8265 . 0056	.8890 .0056	. 9515 . 0056	1.0140 .0056
Class 3, pitch diameter	. 4499 . 0040	. 5124 . 0040	. 5749 . 0040	. 6374 . 0040	. 6999 . 0040	. 7624 . 0040	. 8249 . 0040	.8874 .0040	. 9499 . 0040	1,0124 .0040

TABLE	31.—Limiting	dimensions	and	tolerances,	classes	2	and	3	fits,	American
		National	12-1	pitch thread	series					

	Size (inches)										
Dimensions and tolerances <sup>1</sup>	11/8 3	13/16	11/4 3	15/16	13% 3	17/16	11/2 3	15%	1¾		
BOLTS AND SCREWS	Inches	Inches	Inches	Inches	Inches	Inches	Inches	Inches	Inches		
Classes 2 and 3, major diame- ter	1. 1250 1. 1138 . 0112	1.1875 1.1763 .0112	1.2500 1.2388 .0112	1.3125 1.3013 .0112	1.3750 1.3638 .0112	1. 4375 1. 4263 . 0112	1.5000 1.4888 .0112	1.6250 1.6138 .0112	1.7500 1.7388 .0112		
Classes 2 and 3, minor diame- ter Max. 4	1.0228	1.0853	1. 1478	1.2103	1. 2728	1.3353	1. 3978	1. 5228	1.6478		
Class 2, pitch diameter (for Max- general use)	1.0709 1.0653 .0056	1. 1334 1. 1278 . 0056	1. 1959 1. 1903 . 0056	1. 2584 1. 2528 . 0056	1.3209 1.3153 .0056	1. 3834 1. 3778 . 0056	1.4459 1.4403 .0056	1.5709 1.5645 .0064	1.6959 1.6894 .0065		
Class 3, pitch diameter {Min Tol	1.0709 1.0669 .0040	1. 1334 1. 1294 . 0040	1. 1959 1. 1919 . 0040	1.2584 1.2544 .0040	1.3209 1.3169 .0040	$\begin{array}{c} 1.3834 \\ 1.3794 \\ .0040 \end{array}$	1.4459 1.4419 .0040	1.5709 1.5664 .0045	1.6959 1.6913 .0046		
NUTS AND TAPPED HOLES											
Classes 2 and 3, major diame- ter Min. 4.	1.1250	1. 1875	1, 2500	1. 3125	1. 3750	1. 4375	1. 5000	1. 6250	1.7500		
Classes 2 and 3, minor diame-{Min ter	1.0348 1.0438 .0090	1.0973 1.1063 .0090	1.1598 1.1688 .0090	1. 2223 1. 2313 . 0090	1.2848 1.2938 .0090	1.3473 1.3563 .0090	1.4098 1.4188 .0090	1.5348 1.5438 .0090	1.6598 1.6688 .0090		
Classes 2 and 3, pitch diame- ter Min	1.0709	1. 1334	1, 1959	1, 2584	1. 3209	1.3834	1. 4459	1. 5709	1.6959		
Class 2, pitch diameter (for [Max. <sup>6</sup> ] general use)	1.0765 .0056	1.1390 .0056	1.2015 .0056	1.2640 .0056	1.3265 .0056	1.3890 .0056	1.4515 .0056	1.5773 .0064	1.7024 .0065		
Class 3, pitch diameter {Max. <sup>6</sup> - Tol	1.0749 .0040	1.1374	1.1999 .0040	1.2624 .0040	1.3249 .0040	1.3874 .0040	1.4499 .0040	1.5754 .0045	1.7005 .0046		

Footnotes at end of table.

Dimensions and tolerances 1	Size (inches)								
Dimensions and tolerances *	17⁄8	2	21/4	23⁄2	23⁄4	3	31/4	31/2	334
BOLTS AND SCREWS	In.	In.	In.	In.	In.	In.	In.	In.	In.
Classes 2 and 3, major diameter	1.8638	1.9888	2. 2300 2. 2388 . 0112	2. 3000	2.7388	2.9888	3. 2388	3. 4888 . 0112	3. 7388 . 0112
Classes 2 and 3, minor diameter Max.4	1. 7728	1. 8978	2.1478	2.3978	2. 6478	2.8978	3. 1478	3. 3978	3. 6478
Class 2, pitch diameter (for general use) Max. J. Min Tol	1.8209 1.8143 .0066	1.9459 1.9392 .0067	2. 1959 2. 1890 . 0069	2. 4459 2. 4388 . 0071	2. 6959 2. 6887 . 0072	2.9459 2.9385 .0074	3. 1959 3. 1884 . 0075	3. 4459 3. 4383 . 0076	3. 6959 3. 6881 . 0078
Class 3, pitch diameter{Min Tol	1.8209 1.8163 .0046	1.9459 1.9412 .0047	2. 1959 2. 1911 . 0048	2. 4459 2. 4410 . 0049	2, 6959 2, 6909 , 0050	2.9459 2.9408 .0051	3. 1959 3. 1907 . 0052	3. 4459 3. 4406 . 0053	3. 6959 3. 6905 . 0054
NUTS AND TAPPED HOLES									
Classes 2 and 3, major diameterMin. <sup>5</sup>	1. 8750	2.0000	2. 2500	2.5000	2.7500	3. 0000	3. 2500	3. 5000	3.7500
Classes 2 and 3, minor diameter	1. 7848 1. 7938 . 0090	1.9098 1.9188 .0090	2. 1598 2. 1688 . 0090	2. 4098 2. 4188 . 0090	2. 6598 2. 6688 . 0090	2.9098 2.9188 .0090	3. 1598 3. 1688 . 0090	3. 4098 3. 4188 . 0090	3. 6598 3. 6688 . 0090
Classes 2 and 3, pitch diameterMin	1. 8209	1.9459	2. 1959	2. 4459	2. 6959	2.9459	3. 1959	3. 4459	3. 6959
Class 2, pitch diameter (for general use) ${Max.^6_{-Tol_{}}}$	1.8275	1.9526 .0067	2. 2028	2.4530 .0071	2.7031	2.9533 .0074	3. 2034 . 0075	3. 4535 . 0076	3.7037 .0078
Class 3, pitch diameter	1, 8255	1.9506 .0047	2. 2007 . 0048	2. 4508 . 0049	2.7009	2. 9510 . 0051	3. 2011 . 0052	3. 4512 . 0053	3.7013 .0054

#### TABLE 31.-Limiting dimensions and tolerances, classes 2 and 3 fits, American National 12-pitch thread series-Continued

Dimensions and tolerances <sup>1</sup>	Size								
Dimensions and tolerances 4	4	41⁄4	41/2	43⁄4	5	534	51/2	53⁄4	6
Bolts and Screws	In. 4.0000	In. 4.2500	In. 4. 5000	In. 4.7500	In. 5.0000	In. 5. 2500	In. 5. 5000	In. 5.7500	In. 6.0000
Classes 2 and 3, major diameter	3.9888 .0112	4. 2388 . 0112	4.4888	4.7388 .0112	4.9888 .0112	5. 2388 . 0112	5. 4888 . 0112	5.7388 .0112	5.9888 .0112
Classes 2 and 3, minor diameterMax.4	3. 8978	4. 1478	4. 3978	4. 6478	4.8978	5. 1478	5. 3978	5. 6478	5. 897 <b>8</b>
Class 2, pitch diameter (for general use)	3.9459 3.9380 .0079	4. 1959 4. 1879 . 0080	4. 4459 4. 4378 . 0081	4. 6959 4. 6876 . 0083	4. 9459 4. 9375 . 0084	5. 1959 5. 1874 . 0085	5. 4459 5. 4373 . 0086	5.6959 5.6872 .0087	5. 9459 5. 9371 . 0086
Class 3, pitch diameter	3.9459 3.9404 .0055	4. 1959 4. 1903 . 0056	4. 4459 4. 4402 . 0057	4. 6959 4. 6901 . 0058	4.9459 4.9400 .0059	5. 1959 5. 1900 . 0059	5. 4459 5. 4399 . 0060	5. 6959 5. 6898 . 0061	5.9459 5.9397 .0062
NUTS AND TAPPED HOLES									
Classes 2 and 3, major diameterMin. <sup>s</sup>	4.0000	4. 2500	4. 5000	4.7500	5.0000	5. 2500	5. 5000	5.7500	6.0000
Classes 2 and 3, minor diameter	3.9098 3.9188 .0090	4. 1598 4. 1688 . 0090	4. 4098 4. 4188 . 0090	4. 6598 4. 6688 . 0090	4. 9098 4. 9188 . 0090	5. 1598 5. 1688 . 0090	5. 4098 5. 4188 . 0090	5.6598 5.6688 .0090	5. 9098 5. 9188 . 0090
Classes 2 and 3, pitch diameterMin	3. 9459	4. 1959	4. 4459	4. 6959	4. 9459	5. 1959	5. 4459	5. 6959	5.9459
Class 2, pitch diameter (for general use) ${Max.6 - Tol_{Tol_{Tol_{Tol_{Tol_{Tol_{Tol_{Tol_{$	3.9538 .0079	4. 2039 . 0080	4. 4540 . 0081	4.7042 .0083	4.9543 .0084	5. 2044 . 0085	5. 4545	5.7046 .0087	5.9547 .0088
Class 3, pitch diameter	3.9514 .0055	4. 2015	4. 4516 . 0057	4.7017	4.9518 .0059	5. 2018 . 0059	5. 4519 . 0060	5.7020 .0061	5.9521 .0062

<sup>1</sup> Pitch diameter tolerances include errors of lead and angle. The class 2 tolerances for sizes above 1½ <sup>1</sup> From Grandeer Contrainces include errors of read and angle. I he class 2 contrainces for Sizes above 1/2 inches are based on the formulas in table 60 and a length of engagement of 6 threads or 1/2 inches 3 tolerances are 70 percent of the class 2 tolerances. For lengths of engagement of 1 inch, 0.0010 inch may be added to these tolerances. As certain sizes up to 1/2 inches are included in the American National coarse or fine thread series.
<sup>3</sup> Standard size screw and nut of the American National fine thread series.
<sup>3</sup> Standard size screw and nut of the American National fine thread series.

<sup>4</sup> Dimensions given for the maximum minor diameter of the screw are figured to the intersection of the worn tool arc with a center line through crest and root. The minimum minor diameter of the screw shall be that corresponding to a flat at the minor diameter of the minimum screw equal to  $\frac{1}{2}$ , and may be determined by subtracting 0.0541 inch from the minimum pitch diameter of the screw.

<sup>6</sup> Dimensions for the minimum major diameter of the nut correspond to the basic flat,  $(\frac{1}{2}\times p)$ , and the profile at the major diameter produced by a worn tool must not fall below the basic outline. The maximum major diameter of the nut shall be that corresponding to a flat at the major diameter of the maximum nut equal to  $\frac{1}{24} \times p$ , and may be determined by adding 0.0662 inch to the maximum pitch diameter of the nut.

<sup>6</sup> These dimensions are the minimum metal or "not go" size. The "go" or basic size is the one that should be placed on the component drawing with the tolerance.

					Size (i	nches)				
Dimensions and tolerances <sup>1</sup>	3/4 2	7/8	1	13%	11/4	13%	13/2	15%	13⁄4	17/8
Bolts AND SCREWS Major diameter	In. 0. 7500 . 7410 . 0090	In. 0. 8750 . 8660 . 0090	In. 1.0000 .9910 .0090	Ins. 1. 1250 1. 1160 . 0090	Ins. 1. 2500 1. 2410 . 0090	Ins. 1. 3750 1. 3660 . 0090	Ins. 1. 5000 1. 4910 . 0090	Ins. 1.6250 1.6160 .0090	Ins. 1.7500 1.7410 .0090	Ins. 1.8750 1.8660 .0090
Minor diameterMax.3	. 6733	. 7983	. 9233	1. 0483	1. 1733	1. 2983	1. 4233	1. 5483	1. 6733	1. 7983
Pitch diameter	.7094 .7062 .0032	.8344 .8308 .0036	. 9594 . 9557 . 0037	${\begin{array}{c} 1.\ 0844\\ 1.\ 0806\\ .\ 0038 \end{array}}$	1. 2094 1. 2056 . 0038	$1.3344 \\ 1.3305 \\ .0039$	${}^{1.\ 4594}_{1.\ 4554}_{.\ 0040}$	${}^{1.\ 5844}_{1.\ 5803}_{.\ 0041}$	1.7094 1.7053 .0041	1.834 1.830 .0042
NUTS AND TAPPED HOLES										
Major diameterMin.4	. 7500	. 8750	1.0000	1.1250	1. 2500	1. 3750	1. 5000	1.6250	1.7500	1.8750
Minor diameter	. 6823 . 6903 . 0080	.8073 .8141 .0068	. 9323 . 9391 . 0068	1.0573 1.0641 .0068	1. 1823 1. 1891 . 0068	$\begin{array}{c} 1.\ 3073\ 1.\ 3141\ .\ 0068 \end{array}$	$\begin{array}{c} 1.\ 4323\\ 1.\ 4391\\ .\ 0068 \end{array}$	$1.5573 \\ 1.5641 \\ .0068$	1.6823 1.6891 .0068	1, 8073 1, 8141 , 0068
Pitch diameter{Max Tol	.7094 .7126 .0032	.8344 .8380 .0036	. 9594 . 9631 . 0037	${}^{1.\ 0844}_{1.\ 0882}_{.\ 0038}$	${\begin{array}{c} 1.\ 2094\\ 1.\ 2132\\ .\ 0038 \end{array}}$	${}^{1.\ 3344}_{1.\ 3383}_{.\ 0039}$	${}^{1.\ 4594}_{1.\ 4634}_{.\ 0040}$	${\begin{array}{c} 1.5844\\ 1.5885\\ .0041 \end{array}}$	1. 7094 1. 7135 . 0041	1.8344 1.8386 .0042

#### TABLE 32.—Limiting dimensions and tolerances, class 3 fit, American National 16-pitch thread series

					Size (i	inches)				
Dimensions and tolerances <sup>1</sup>	2	21⁄8	21/4	23⁄2	2¾	3	31/4	31/2	33/4	4
BOLTS AND SCREWS	Inches	Inches	Inches	Inches						
Major diameter	2.0000 1.9910 .0090	2.1250 2.1160 .0090	2. 2500 2. 2410 . 0090	2.5000 2.4910 .0090	2.7500 2.7410 .0090	3.0000 2.9910 .0090	$\begin{array}{c} 3.\ 2500\\ 3.\ 2410\\ .\ 0090 \end{array}$	3. 5000 3. 4910 . 0090	3.7500 3.7410 .0090	4.0000 3.9910 .0090
Minor diameterMax. <sup>3</sup>	1. 9233	2. 0483	2. 1733	2. 4233	2. 6733	2, 9233	3. 1733	3. 4233	3. 6733	3. 9233
Pitch diameter	1. 9594 1. 9551 . 0043	2.0844 2.0801 .0043	2. 2094 2. 2050 . 0044	2. 4594 2. 4549 . 0045	2. 7094 2. 7048 . 0046	2.9594 2.9547 .0047	3. 2094 3. 2046 . 0048	$3.4594 \\ 3.4545 \\ .0049$	3. 7094 3. 7044 . 0050	3.9594 3.9543 .0051
NUTS AND TAPPED HOLES										
Major diameterMin.4	2.0000	2. 1250	2. 2500	2. 5000	2.7500	3. 0000	3. 2500	3. 5000	3.7500	4.0000
Minor diameter	1. 9323 1. 9391 . 0068	2. 0573 2. 0641 . 0068	2. 1823 2. 1891 . 0068	2. 4323 2. 4391 . 0068	2, 6823 2, 6891 , 0068	2, 9323 2, 9391 , 0068	3. 1823 3. 1891 . 0068	3. 4323 3. 4391 . 0068	3. 6823 3. 6891 . 0068	3. 9323 3. 9391 . 0068
Pitch diameter	1.9594 1.9637 .0043	2. 0844 2. 0887 . 0043	2. 2094 2. 2138 . 0044	2. 4594 2. 4639 . 0045	2. 7094 2. 7140 . 0046	2.9594 2.9641 .0047	3.2094 3.2142 .0048	3. 4594 3. 4643 . 0049	3. 7094 3. 7144 . 0050	3.9594 3.9545 .0051

<sup>1</sup> Pitch diameter tolerances include errors of lead and angle, and are 70 percent of the tolerances for class 2 based on the formulas in table 60 and a length of engagement of 6 threads or  $\frac{3}{2}$  inch. The  $\frac{3}{4}$ -inch size being in the American National fine-thread series, the tolerance for this size corresponds to that series. <sup>2</sup> Standard size screw and nut of the American National fine-thread series. <sup>3</sup> Dimensions given for the maximum minor diameter of the screw are figured to the intersection of the worn-tool are with a center line through crest and root. The minimum minor diameter of the screw equal to  $\frac{1}{2}\times p$ , and may be determined by subtracting 0.0406 inch from the minimum pitch diameter of the basic flat ( $\frac{1}{2}\times p$ ) and the profile at the major diameter of the nut correspond to the basic flat ( $\frac{1}{2}\times p$ ) and the profile at the major diameter of the at at the maximum major diameter of the basic outline. The maximum major diameter of the basic outline. The maximum major diameter of the nut shall be that correspond to the basic flat ( $\frac{1}{2}\times p$ ) and the profile at the major diameter of the nut shall be that correspond to the basic flat ( $\frac{1}{2}\times p$ ) and the profile at the major diameter of the maximum major diameter of the maximum major diameter of the nut shall be that corresponding to a flat at the major diameter of the maximum mator diameter of the maximum maximum maximum major diameter of the maximum ma

#### 4. GAGES

The specifications for gages given in section III are applicable to the American National 8-, 12-, and 16-pitch thread series. Toler-ances on diameter, lead, and angle for classes W, X, Y, and Z gages, as specified in section III, are given in table 33.

Each gage shall be marked for identification, with the diameter, pitch, and class of fit as specified in section II, division 3, "Symbols."

TABLE 33.-Tolerances for thread gages, American National 8-, 12-, and 16-pitch thread series

Class of gage	Tolerance diam	e on pitch eter <sup>1</sup>	Tolerance	Tolerance on half	Tolerance on major or minor diameters <sup>1</sup>			
	From	То—	on lead 3	angle of thread	From—	То—		
Class W Class X and "not go" Class Y Class Z	Inch 0.0000 .0000 .0002 .0006	Inch 0.0002 .0004 .0007 .0013	Inch 0.00025 .0004 .0004 .0005	Deg. Min. 0 5 0 5 0 5 0 5 0 5	<i>Inch</i> 0.0000 .0000 .0000 .0000 .0000	Inch 0.0007 .0007 .0007		
		12-PITC	н					
Class W Class X and "not go" Class Y Class Z	0.0000 .0000 .0002 .0004	0.00015 .0003 .0006 .0011	0. 0002 . 0003 . 0003 . 0004	0 6 0 10 0 10 0 10 0 10	0.0000 .0000 .0000 .0000	0.0006 .0006 .0006 .0006		
		16-PITC	ΈE					
Class W Class X and "not go" Class Y	0.0000 .0000 .0002	0.0001 .0003 .0006	0.00015 .0003 .0003	0 8 0 10 0 15	0.0000 .0000 .0000	0.0006 .0006 .0006		

#### 8-PITCH

<sup>1</sup> On "go" plugs the tolerance is plus, and on "go" rings the tolerance is minus. On "not go" plugs the tolerance is minus, and on "not go" rings the tolerance is plus. <sup>2</sup> Allowable variation in lead between any 2 threads not farther apart than the standard length of engage-

. 0010

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.0006

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ment

## SECTION V. SCREW THREADS OF SPECIAL DIAMETERS. PITCHES, AND LENGTHS OF ENGAGEMENT

The tolerances specified in section III of this report apply in general to bolts, nuts, and tapped holes of standard pitches and diameters. They are based on the pitch of the thread and a length of engagement equal to the basic major diameter, but are used for lengths of engagement up to  $1\frac{1}{2}$  diameters.

In addition to the foregoing threaded components, there are large quantities of threaded parts produced, such as hub and radiator caps in the automotive industry, threaded collars on machine tools, etc., where the diameters are larger, the pitches finer, and the lengths of engagement shorter than for bolt and nut practice. The following specifications have been adopted for such threaded parts, and the tolerances are based on the diameter, pitch, and length of engagement of the components.

### 1. FORM OF THREAD

The American National form of thread profile as specified in section III shall be used.

#### 2. THREAD SERIES

In section IV there are given the limiting dimensions for an 8-pitch, a 12-pitch, and a 16-pitch thread series. The use of these series,

Class Z

wherever possible, is recommended for all applications requiring other than American National coarse or fine threads. Whenever sizes and pitches in the American National coarse or

Whenever sizes and pitches in the American National coarse or fine, or the 8-, 12-, or 16-pitch thread series are not suitable, it is recommended that one of the following pitches be selected: 4, 6, 8, 10, 12, 14, 16, 18, 20, 24, 28, 32, 36, 40, 48, 56, 64 threads per inch. Basic thread data for these pitches are given in table 34.

## 3. CLASSIFICATION AND TOLERANCES

There are established herein for general use four classes of screwthread fits, which are named and numbered to correspond to the regular classification of fits given in section III. These four classes, together with the accompanying specifications, are intended to insure a uniform practice for screw threads not included in the American National coarse or fine thread series, nor in the 8-, 12-, or 16-pitch thread series.

Threads per inch, n	Pitch, <b>p</b>	Depth of thread, h	Basic width of flat, p/8	Minimum width of flat at major diameter of nut, p/24
1	2	3	4	5
64	Inch 0.01562	Inch 0.01015	Inch 0.00195	Inch 0.00065
56	.01786	. 01160	. 00223	. 00074
48	. 02083	. 01353	. 00260	. 00087
40	. 02500	. 01624	. 00312	. 00104
36	. 02778	.01804	. 00347	.00116
20	02125	02030	00201	00120
2	03571	02320	00446	00130
20 9A	04167	02706	00521	00174
20	05000	03248	00625	00208
	. 00000	.00210	.00040	. 00200
18	. 05556	. 03608	. 00694	. 00231
16	. 06250	. 04059	. 00781	. 00260
14	. 07143	. 04639	. 00893	. 00298
12	08333	05413	01042	00347
	.00000		. 01012	. 00011
10	. 10000	. 06495	. 01250	. 00417
8	. 12500	. 08119	. 01562	. 00521
6	16667	10825	02083	. 00694
4	25000	16238	03125	01042
	. 20000	. 10200	. 00120	.01012

TABLE 34.—Thread data for recommended pitches for special threads

It is not the intention of the Commission arbitrarily to place a general class or grade of work in a specific class of fit. Each manufacturer and user of screw threads is free to select the class of fit best adapted to his particular needs.

#### (a) GENERAL SPECIFICATIONS

The following general specifications apply to all classes of fit specified for screw threads of special diameters, pitches, and lengths of engagement.

1. UNIFORM MINIMUM NUT.—The pitch diameter of the minimum threaded hole or nut corresponds to the basic size.<sup>11</sup>

<sup>&</sup>lt;sup>11</sup> Special cases will arise, however, when a class 1 thread is required on finished drawn tubing with thin walls, and in such cases the allowance should be made on the nut.

2. TOLERANCES.<sup>12</sup>—(a) The tolerances specified represent the extreme variations allowed on the product.

(b) The tolerance on the nut is plus, and is applied from the basic size to above basic size.

(c) The tolerance on the screw is minus, and is applied from the maximum screw size to below the maximum screw size.

(d) The pitch diameter tolerances for a screw and nut of a given class of fit are the same.

(e) Pitch diameter tolerances include all errors of pitch diameter, lead, and angle. The full tolerance cannot, therefore, be used on pitch diameter unless the lead and angle of the thread are perfect.

(f) The pitch diameter tolerances are obtained by adding three values, or increments; one dependent upon the basic major diameter, another upon the length of engagement, and the third upon the pitch of the thread. These increments are based on formulas given in appendix 1. However, where tolerance values so obtained exceed those given in section III for corresponding pitches of the American National coarse or fine thread series, and for any diameters equal to or less than these standard sizes and lengths of engagement equal to or less than one diameter, the tolerances given in section III are used. (See rules for using tolerance tables on p. 81.)

(g) The tolerances on the major diameters of the screws and minor diameters of the nuts are based on the pitch of the thread, as these control the depth of engagement; they are, therefore, based on the pitch alone.

(h) The minimum minor diameter of a screw of a given pitch is such as to result in a basic flat  $(\frac{1}{2} \times p)$  at the root when the pitch diameter of the screw is at its minimum value. When the maximum screw is basic, the minimum minor diameter of the screw will be below the basic minor diameter by the amount of the specified pitch diameter tolerance.

(i) The maximum minor diameter of a screw of a given pitch may be such as results from the use of a worn or rounded threading tool, when the pitch diameter is at its maximum value. In no case, however, should the form of the screw, as results from tool wear, be such as to cause the screw to be rejected on the maximum minor diameter by a "go" ring gage, the minor diameter of which is equal to the minimum minor diameter of the nut.

(j) The maximum major diameter of the nut of a given pitch is such as to result in a flat equal to one third of the basic flat  $(\frac{1}{24} \times p)$ when the pitch diameter of the nut is at its maximum value. When the minimum nut is basic, its maximum major diameter will be above the basic major diameter by the amount of the specified pitch diameter tolerance plus two ninths of the basic thread depth.

(k) The nominal minimum major diameter of a nut is the basic major diameter. In no case, however, should the minimum major diameter of the nut, as results from a worn tap or cutting tool, be such as to cause the nut to be rejected on the minimum major diameter by a "go" plug gage made to the standard form at the crest.

<sup>&</sup>lt;sup>1:</sup> Recommendations and explanations regarding the application of tolerances are given in appendix 1, p. 127.

(1) The tolerance on minor diameter of a nut of a given pitch is one sixth of the basic thread depth regardless of the class of fit.<sup>13</sup>

#### (b) CLASSIFICATION OF FITS

1. CLASS 1, LOOSE FIT.-This class is intended to cover the manufacture of threaded parts where quick and easy assembly is necessary and a considerable amount of shake or play is not objectionable.

This class is made with an allowance on the screw, so as to permit ready assembly, even when the threads are slightly bruised or dirty, in conformity with the practice in section III.<sup>14</sup>

Tables 35 and 36 give the limiting dimensions and tolerances for major, pitch, and minor diameters of threads of special diameters. pitches, and lengths of engagement.

2. CLASS 2, FREE FIT.—This class is intended to cover the manufacture of threaded parts which are to assemble nearly or entirely with the fingers, and where a slight amount of shake or play between the assembled threaded members is not objectionable. It is the same in every particular as class 1 except that it has no allowance and the tolerances are smaller.

Tables 35 and 37 give the limiting dimensions and tolerances for major, pitch, and minor diameters of threads of special diameters, pitches, and lengths of engagement.

3. CLASS 3, MEDIUM FIT.-This class is intended to cover the manufacture of the higher grade of threaded parts which are to assemble nearly or entirely with the fingers, and must have the minimum amount of shake or play between the threaded members. It is the same as class 2 in every particular except that the tolerances are smaller.

Tables 35 and 38 give the limiting dimensions and tolerances for major, pitch, and minor diameters of threads of special diameters, pitches, and lengths of engagement.

4. CLASS 4, CLOSE FIT.—This class is intended to cover the manufacture of threaded parts of the finest commercial quality, where very little shake or play is desirable, and where a screw driver or wrench may be necessary for assembly.

In the manufacture of screw-thread products belonging to this class it may be necessary to use precision tools, gages made to special tolerances for this class (see table 21, p. 58), and other refinements. This quality of work should, therefore, be used only in cases where requirements of the mechanism being produced are exacting. In order to secure the fit desired, it may be necessary in some cases to select the parts when the product is being assembled.

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<sup>&</sup>lt;sup>13</sup> Special threads having a length of engagement considerably less than one diameter will not develop the full strength of the screw. The minimum minor diameter of the nut of the American National form of thread is such as to provide a minimum clearance on diameter at the minor diameter equal to two ninths of the basic thread depth. If this clearance is reduced by providing a greater percentage of thread depth in the nut, the strength of such a fastening is increased. In such cases when the screw is subject to considerable tension, it is permissible to make the minor diameter of the nut less than the minimum specified in order to give the necessary depth of engagement. On the other hand, when the length of engagement is exceptionally long the minor diameter of the nut may be greater than the maximum specified without impairing the strength of the fastening. <sup>14</sup> See footnote 11, p. 77.

The maximum pitch diameters of the screws are slightly larger than the minimum pitch diameters of the nuts determined from table 35.

Tables 35 and 39 give the limiting dimensions and tolerances for major, pitch, and minor diameters, of threads of special diameters, pitches, and lengths of engagement.

## 4. TABLES OF DIMENSIONS

In order to simplify the specification of dimensions of special fastening screw threads, tables 35, 36, 37, 38, and 39 are arranged herein, and are intended to cover all practical combinations of diameter, pitch, length cf engagement, and class of fit. The use of these tables instead of the application of formulas to determine limiting dimensions of a special thread facilitates placing dimensions on drawings. Also, in cases of special threads of the same diameter, pitch, and class of fit, but slightly different lengths of engagement, the threads may be gaged by a single set of gages, as identical pitch diameter tolerances will be applied.

(a) ARRANGEMENT OF TABLES.—The arrangement of dimensions and tolerances given in these tables has the following features:

All thread dimensions of threads of special diameters, pitches, and lengths of engagement, except pitch diameter tolerances, are derived from table 35.

Pitch diameter tolerances are taken from tables 36, 37, 38, or 39, depending upon the class of fit required. These pitch diameter tolerances were obtained by adding increments 15 corresponding to the major diameters at the top, the threads per inch at the side of the table, and mean lengths of engagement of  $\frac{1}{4}$ , 1, and  $\frac{2}{4}$  inches for pitches from 64 to 12 threads per inch, inclusive, and 1/2, 2, and 41/2 inches for pitches from 10 to 4 threads per inch, inclusive. Thus, the increments of the pitch diameter tolerances based on length of engagement and on diameter vary by definite steps instead of continuously. However, in order that the tolerances given in these tables might be wholly consistent with those given in section III, certain values as listed are greater or less than those yielded by the above method. This modification was made by inserting in the tables, in the positions corresponding to standard sizes, pitches, and lengths of engagement of the American National coarse-and finethread series, the pitch diameter tolerances listed in section III. Then, wherever necessary, all values above and to the left of these inserted values were reduced so that none of them should exceed these standard values, and those below and to the right were increased so that none should be less than the standard values. This has the important advantage that in a series of sizes, frequently occurring in practice, consisting partly of standard sizes and partly of special sizes, there will be no undue irregularity in the progression of the pitch diameter tolerance, with consequent difficulties in securing gages, etc.

<sup>&</sup>lt;sup>15</sup> The formulas for determining such increments are listed on p. 128.

The maximum pitch diameter tolerances listed are equal to the tolerances on the major diameter of the screws of the same pitch, as given in table 35.

(b) RULES FOR USE OF TABLES.—For consistent application of these pitch diameter tolerance tables to all cases, adherence to the following rules relative to the use of the tables is necessary:

1. Tolerances on pitch diameter corresponding to major diameters between those for which values are given in the tables shall be those of the next larger diameter.

2. Tolerances on pitch diameter for pitches between those for which values are given in the tables shall be those of the next coarser pitch, except that for screws having 80, 72, 44, 13, 11, 9, 7, 5, or  $4\frac{1}{2}$  threads per inch, lengths of engagement of one and one half diameters or less, and diameters less than the standard diameters for the respective pitches as given in section III, the tolerances given in section III shall be used.

3. Tolerances on pitch diameter for pitches coarser than 4 threads per inch shall be the same as those for 4 threads per inch.

4. Tolerances on pitch diameter when the length of engagement is exactly  $\frac{1}{2}$ , or  $\frac{1}{2}$ , inches for 12 threads per inch and finer, or 1, or 3, inches for pitches coarser than 12 threads per inch, shall correspond to the interval of which these are the upper limits.

5. Tolerances on pitch diameter for lengths of engagement greater than those for which values are given shall be the maximum values listed for the pitch concerned.

(c) EXAMPLES.—The following examples illustrate the use of these tables:

*Example:* 3¼-inch, 16-thread, class 1, with allowance on screw, one-half inch length of engagement:

#### From table 36:

	Pitch diameter tolerance	= = 0.0095
Also	from table 35, for the screw:	
	Maximum major diameter $= 3.2$	2500 - 0.0018 = 3.2482
	Minimum major diameter $= 3.2$	24820126 = 3.2356
	Maximum minor diameter $=3.2$	25000785 = 3.1715
	Maximum pitch diameter $=3.2$	25000424 = 3.2076
	Minimum pitch diameter $=3.2$	20760095 = 3.1981
And	for the nut:	
	Minimum major diameter	= 3. 2500
	Minimum minor diameter $=3.2$	25000677 = 3.1823
	Maximum minor diameter $= 3$ .	1823 + .0068 = 3.1891
	Minimum pitch diameter $=3.2$	25000406 = 3.2094
	Maximum pitch diameter $=3$ .	2094 + .0095 = 3.2189

*Example*: 3-inch, 24-thread, class 2, free fit, five-eighths inch length of engagement:

From table 37:

Pitch diameter tolerance.....=0. 0066

In this instance the pitch diameter tolerance is printed in italics. In accordance with the footnote under table 35 it is desirable to avoid the use of tolerances set in italics as the combination of class of fit, length of engagement, pitch, and diameter is disproportionate. If it is decided to use a closer fit, class 3-medium fit or class 4-close fit may be chosen. Assuming the choice of class 3-medium fit, the following dimensions are obtained:

From table 38:
Pitch diameter tolerance $= 0.0065$
From table 35 for the screw:
Maximum major diameter $= 3.0000$
Minimum major diameter $= 3.0000 - 0.0066 = 2.9934$
Maximum minor diameter $= 3.00000511 = 2.9489$
Maximum pitch diameter $=3.00000271 = 2.9729$
Minimum pitch diameter $=2.97290065 = 2.9664$
And for the nut:
Minimum major diameter $= 3.0000$
Minimum minor diameter $=3.00000451=2.9549$
Maximum minor diameter $= 2.9549 + .0045 = 2.9594$
Minimum pitch diameter $=3.00000271=2.9729$
Maximum pitch diameter $=2.9729 + .0065 = 2.9794$
* · · ·

If, instead, it is decided to reduce the length of engagement to one-half inch, the following dimensions are obtained:

#### 5. GAGES

The classification of gages and gage tolerances, as well as the thread form of plug and ring thread gages presented in section III, division 5, "Gages" apply also to gages for special threads. In ordering gages for a special thread, the length of engagement of the component thread (as distinct from the length of the gage), and the diameter, pitch, and class of fit, should be stated.

With regard to the marking of gages, each gage shall be plainly marked, for identification, with the diameter, pitch, thread series that is, "NS" to indicate a special thread of American National form—and class of fit. See section II, division 3, "Symbols." For example, a 1-inch, 16-pitch gage of American National form of thread, class 3, medium fit, shall be marked: 1"—18NS—3.

for minor, t the values t the basic the basic	Major	diameter,* minimum		$Inch \\ 0.0000 \\ 0.0$	000000	00000	0000
uzzs dimensions ers, subtract olumas fron nd 39 for pit	Pitch	diameter, minimum	, 3, and 4	Inch 0.0101 0.0116 0.0135 0135 0135 0162	0203 0232 0232 0271 0325	.0361 .0406 .0464 .0541	. 0650 . 0812 . 1083 . 1624
NUT S n minimum najor diamen inimum '' ce teter. eter. s6, 37, 38, al	iameter	Tolerance	Classes 1, 2	Inch 0.0017 0.0019 0.0023 0.0023	.0034 .0039 .0045 .0054	. 0060 . 0068 . 0077 . 0090	. 0109 . 0135 . 0180 . 0270
To obtair pitch, and i in the "m major diam Apply tol See tables tolerances.	Minor d	Minimum		Inch 0.0169 0.0193 0.0226 0.0271 0.0271	.0338 .0387 .0451 .0541	. 0601 . 0677 . 0773 . 0902	. 1083 . 1353 . 1804 . 2706
.he "maxi-	ameter.1	uma	Classes 2, 3, 4	Inch 0.0192 0.0219 0.0256 0.0256 0.0307	. 0383 . 0438 . 0511 . 0613	. 0682 . 0767 . 0876 . 1022	. 1227 . 1534 . 2045 . 3067
e values in t	Minor dis	maxin	Class 1	$Inch \\ 0.0199 \\ 0.0227 \\ 0.0265 \\ 0.0265 \\ 0.0317 \\ 0.0352 \\ 0.0$	. 0394 . 0450 . 0524 . 0628	. 0698 . 0785 . 0897 . 1046	. 1255 . 1568 . 2089 . 3131
, subtract th			Class 4	$Inch \\ 0.0100 \\ 0.0114 \\ 0.0133 \\ 0.0133 \\ 0.0160 \\ 0.0178 \\ 0.0018 \\ 0.0$	.0201 .0230 .0268 .0322	. 0358 . 0402 . 0536	. 0644 . 0805 . 1074 . 1611
or diameters.		ашеюг, шах	Classes 2, 3	$Inch \\ 0.0101 \\ 0.0116 \\ 0.0135 \\ 0.0135 \\ 0.0162 \\ 0.0180 \\ 0.000 \\ 0.0$	. 0203 . 0232 . 0271 . 0325	.0361 .0406 .0464	. 0650 . 0812 . 1083 . 1624
CREW SIZES ch, and min olerances.	1.1.1 D:1.1	FIGH O	Class 1	$Inch \\ 0.0108 \\ 0.0124 \\ 0.0124 \\ 0.0124 \\ 0.0172 \\ 0.0172 \\ 0.0191 \\ 0.0$	.0214 .0244 .0284 .0340	. 0377 . 0424 . 0485 . 0565	. 0678 . 0846 . 1127 . 1688
s or major, pitt r diameter. h diameter to		апсе	Classes 2, 3, 4	Inch 0.0038 0.0040 0044 0044 0048	. 0054 . 0062 . 0066 . 0072	.0082 .0090 .0098 .0112	. 0128 . 0152 . 0202 . 0280
dimensions f e basic major 18. ad 39 for pitc	iameter	Toler	Class 1	Inch 0.0052 0.0056 0.0058 0.0068 0.0068	.0076 .0086 .0092 .0102	.0114 .0126 .0140 .0158	. 0184 . 0222 . 0290 . 0408
t maximum mus from th erances min 36, 37, 38, at	Major d	mum	Classes 2, 3, 4	$Inch \\ 0.0000 \\ 0.0$	00000	000000	000000
To obtain mum" colu: Apply tol See tables		Maxiı	Class 1	$Inch \\ 0.0007 \\ 0.0008 \\ 0.0009 \\ 0.0010 \\ 0.0011 \\ 0.0$	.0011 .0012 .0013 .0015	. 0016 . 0018 . 0021 . 0024	. 0028 . 0034 . 0044 . 0064
Threads per inch				64 56 48 40 36	32 28 24 20	18- 16- 14- 12-	88 6- 4

<sup>1</sup> Dimensions given for the maximum minor diameter of the screw are figured to the intersection of the worn tool arc with a center line through crest and root. The minimum minor diameter of the screw shall be that corresponding to a flat at the minor diameter of the minimum screw equal to  $\frac{1}{5}$ , and may be determined by subtracting the basic thread

depth, h (or 0.6495p) from the minimum pitch diameter of the screw. <sup>1</sup> Dimensions for the minimum major diameter of the nut correspond to the basic flat ( $\frac{1}{8} \times p$ ), and the profile at the major diameter produced by a worn tool must not fall below to basic outline. The maximum major diameter of the nut screespond to the basic flat at the major diameter of the maximum nut equal to  $\frac{1}{24} \times x$ , and may be determined by adding  $\frac{1}{2} \times x$  (or 0.7389p) to the maximum pitch diameter of the nut.

TABLE 35.-Values for obtaining thread dimensions of special screw threads, classes 1, 2, 3, and 4 fits

TABLE 36.-Pitch diameter tolerances for special screw threads, class 1, loose fit

24 inches ---------------In.20 inches -----In.18 inches i In.14 16 inches inches In.In. 12 inches In.inches 10 In.Pitch diameter tolerances for diameters up to and including-8 inches In.6 inches 0.0099 In.2 3 4 inches inches ---------.0090 0.0083 .0086 In..0075 . 0077 .0080 .0084 .0099 .0072 In. .0062 .0067 .0069 .0078 .0065 0074 .0071 In.1½ inches 0058. 0062 .0061 0063. 0072 . 0065 . 0070 .0074 .0102 In. 0052.0067 0056 o' .0054 .0058 0700 0700 In. 00500052 . 0057 .0060 .0063 .0066 1 inch  $\frac{In}{0.0047}$ .0054 .0056 .0057 . 0057 .0057 .0049 .0051 .0057 34 inch In. 0044 .0048.0057.0051 .0051\*.0051 .0057 .0102 .0046 .0051 .0051 .0051 1/2 inch .0046.00570046 <sup>2</sup>. 0046 . 0057 In. 0042.0046 .0046 0046 .0051 .0057 .0102 0044 0056 3/8 Inch .0046 1. 0051 . 0057 . 0100  $\frac{In}{0.0038}$ .0038 .0038 .0038 .0038 .0038 .0043  $\frac{1}{10}$ .0043 .0046 . 0051 . 0057 . 0098 .0034 .0034 .0036 .0038 In. 00340034 316 inch -----1. 0034 . 0057 . 0036 . 0038 1n. 0.0026 0028 .0031 ys nch In. In.  $y_2 | 0.0026$ .0028 .0031 .0034 i ¥,6 Inch 32.22 22 22 72 To and in-clud-ing-72 72 12/2 122 Lengths of engagement 12 12 12 12 12 12 12 122 From-In.Threads per inch 64-----56\_\_\_\_ 36\_\_ -0<del>1</del> 32-24.--28-20--**8** 

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### NATIONAL SCREW THREAD COMMISSION

			.0171 .0184 .0184	. 0179 . 0209 . 0222	$0190 \\ 0220 \\ 0270 \\ 0270$	.0208	
		0.0152 .0168 .0168	.0163 .0184 .0184	.0170 .0200 .0222	.0181 .0211 .0261	.0199 .0229 .0279	
		0.0148 0168 0168	.0158 .0184 .0184	. 0166 . 0196 . 0222	. 0176 . 0206 . 0256	.0195 .0225 .0275	
	0140	.0143 .0158	.0158 .0183 .0184	.0161 .0191 .0222	0172 0202 0252	.0190 .0220 .0270	.8
	0.0133	.0138 .0153 .0168	.0153 .0178 .0184	.0156 .0186 .0222	.0166 .0196 .0246	.0185 .0215 .0265	ad serie
	0.0124 0126 0126 0128 0128 0140	.0132 .0147 .0168	.0147 .0172 .0184	. 0150 . 0180 . 0222	.0161 .0191 .0241	. 0179 . 0209 . 0259	fine-thre
0.0114 0114 0114	0118 0126 0126 0126 0122 0137	.0126 .0141 .0168	.0141 .0166 .0184	.0144 .0174 .0222	.0155 .0185 .0235	.0173 .0204 .0253	ational
0.0109	$0112 \\ 0126 \\ 0126 \\ 0115 \\ 0115 \\ 0130 \\ 0140 $	.0119 .0134 .0158	.0134 .0160 .0184	.0137 .0167 .0217	.0148 .0178 .0228	.0167 .0204 .0247	rican N
.0101 .0114 .0114	0104 0126 0126 0128 0123 0140	.0112 .0127 .0152	0127 0152 0184	.0130 .0160 .0210	.0141 .0171 .0221	. 0159 . 0204 . 0239	he Ame
.0092 .0107 .6114	0095 0110 0126 0126 0099 0139	.0103 .0118 .0143	.0118 .0143 .0184	.0121 .0151 .0201	.0132 .0162 .0212	.0150 .0204 .0230	sizeoft
.0087 .0102 .0114	0090 0105 0126 0128 0108 0133	.0097 .0112 .0137	.0112 .0138 .0138	.0115 .0145 .0195	.0126 .0156 .0206	. 0145 1. 0204 . 0225	andard
.0080 .0095 .0114	0083 0098 0123 0087 0087 0102	.0091 .0106 .0131	.0106 .0132 .0181	.0111 .0139 .0189	.0120 .0150 .0200	.0138 .0168 .0168	3 St
. 0077 . 0079 . 0114	0079 0079 0120 0079 0079 0079	2.0079 2.0079 2.0127	.0102 .0128 .0178	.0111 .0135 .0135	.0116 1.0145 .0196	.0134 .0164 .0215	
.0070 .0070 .0112	0200 0700 0700 0700 0700 0700 0700 0700	.0079 .0079 .0123	. 0098 . 0123 . 0173	1,0111 .0131 .0181	.0112 .0142 .0192	.0130 .0160 .0210	
. 0057 . 0057 . 0109	<sup>1</sup> ,0063 0112 0112 0070 0070	.0079 .0079 .0120	1.0092 .0120 .0171	.0098 .0128 .0178	.0109 .0139 .0189		ad serie
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18	16	12	10				

Norz.-It is preferable to avoid the use of tolerances set in italics by choosing a closer flt, shorter length of engagement, coarser pitch, or smaller diameter.

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fit
free
62
class
threads,
screw
special
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tolerances
diameter
37Pitch
LABLE .

	24 inches	In.											
	20 inches	In.											
	18 inches	In.											
	16 inches	In.											
	14 inches	In.											
	12 inches	In.											0.0098 0098 0098
6	10 inches	In.										0600.0000.0000	.0095 .0098 .0098
includir	8 inches	In.									0.0082 .0082 .0082	0600 · 0600 ·	.0088 8600. 8600.
to and	6 inches	In.								0.0072	.0078 .0082 .0082	0600 . 0600 .	.0081 .0096 .0098
ters up	4 inches	In.						0.0062	.0065	.0067	.0069 .0082 .0082	.0090 .0085	.0072 .0087 .0098
r diame	3 inches	In.					0.0054	.0058	.0060	.0062	.0063 .0082 .0082	.0065 .0080 .0090	.0066 0081 0098
Inces for	2 inches	In.			0.0048	.0050	.0051	.0052	.0054	.0056	.0057 .0072 .0082	. 0058 . 0090	.0060 .0075 .0098
er tolers	11/2 inches	In.	0.0040	.0044	.0045	.0046	.0047	.0048	. 0050	.0052	.0053 .0056 .0082	.0054 	. 0056 . 0056 . 0096
diamet	1 inch	$_{0.0038}^{In.}$	.0038	.0039	.0041	.0042	.0043	.0044	.0045	.0047	.0049 .0049 .0082	.0049 .0049 .0090	.0049 .0049 .0092
Pitch	34 inch	$_{0.\ 0035}^{In.}$	.0036	.0037	.0038	.0039	.0040	.0041	.0041	.0041	$0041 \\ 0041 \\ 0082$	.0045 .0045 .0087	.0049 .0049 .0089
	34 inch	$_{0.0032}^{In.}$	.0033	.0034	.0035	.0036	.0036	.0036	.0036	<sup>2</sup> .0036 .0041	.0041 .0041 .0082	.0045 .0045 .0084	.0048 .0049 .0086
	3% inch	$_{0.\ 0030}^{In.}$	.0031	.0032	.0033	.0033	.0033	.0033	<sup>2</sup> .0033	.0036	.0041 .0041	1.0045 .0045 .0082	.0045 .0049 .0084
	M inch	$_{0.0027}^{In.}$	.0027	.0027	.0027	.0027	.0027	<sup>2</sup> .0031 .0041	.0033	1.0036 .0041	. 0039 . 0041 . 0079	.0040 .0045 .0080	
	316 inch	$_{0.\ 0024}^{In.}$	.0024	.0024 .0041	.0024	.0025	.0027.0041	.0031	.0033	.0036			
	ys inch	${}^{In.}_{0.\ 0019}$	.0020	.0022	1.0024 .0041	.0025	.0027.0041						
	M6 inch	$_{0.\ 0019}^{In}$	.0020	.0022	.0024								
hs of ment	To and in- clud- ing-	In. 15	112	1122	112	112	112	727	122	22	322	3122	A A M
Lengt engage	From-	In.	{}	{}	} %	}	}	}	}	}			
	Threads per inch	64	26	48	40	36	32	28	24	20	18	16	14

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## SPECIAL THREAD DIMENSIONS AND TOLERANCES

		0.0143 .0152 .0152	.0149 .0179 .0202	.0158 .0188 .0238	
	0.0128 .0128 .0128	0135 0152 0152	.0140 .0170 .0202	.0149 .0179 .0229	
	0.0126 .0128 .0128	.0130 .0152 .0152	. 0136 . 0166 . <i>0202</i>	0145 0175 0225	
0112	.0122 .0128 .0128	.0125 .0152 .0152	.0131 .0161	0140. 0170	series.
0109 0112 0112	.0116 .0128	0120 0150 0152	0126 0156 0202	. 0135 . 0165 . 0215	thread
.0103 .0112 .0112	.0112 .0128 .0128	.0115 .0145	.0120 .0150 .0200	0129 0159 0209	nal fine-
.0097 .0112 .0112	.0112 .0128 .0128	$0112 \\ 0139 \\ 0152 $	0114 0144 0194	. 0123 . 0153 . 0203	n Natio
.0090	.0105 .0128 .0128	0105 0132 0152	.0107 .0137 .0137	.0117 .0147 .0197	merical
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.0074 .0089 .0112	.0089 .0112 .0128	.0089 .0115 .0152	.0091 .0121 .0171	.0100 .0140 .0180	rd size (
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2.0056 .0056 .0098	.0073 .0098 .0128	.0150 .0150	.0075 .0101	.0084 .0114 .0164	
.0054 .0056 .0094	.0069 .0094 .0128	<sup>1</sup> .0076 .0095 .0145	.0101 .0101	.0080 .0110 .0160	ies.
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<u> </u>					
12	10		6	4	

NOTE.-It is preferable to avoid the use of tolerances set in italics by choosing a closer fit, shorter length of engagement, coarser pitch, or smaller diameter.

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TABLE 38.—Pitch diameter tolerances for special screw threads, class 3, medium fit

	24 inches	In.										
	20 inches	In.										
	18 inches	In.										
	16 inches	In.										
	14 inches	In.										
	12 inches	In.										0.0087 .0090 .0090
181	10 inches	In.									0.0080 .0082 .0082	.0000 .0090
includi	8 inches	In.								0.0072 .0072 .0072	.0073 .0082 .0082	.0074 .0089 .0090
to and	6 inches	In.						0.0062	.0064	.0065 .0072 .0072	.0066 .0081 .0082	.0066 .0081 .0090
ters up	4 inches	In.				0.0050	.0054	.0054	.0055	.0056 .0071 .0072	.0057 .0072 .0082	.0058 .0073 .0090
r diame	3 inches	In.		0.0044	.0048	.0048	.0048	.0049	.0050	.0051 .0066 .0072	.0051 .0066	.0052 .0067 .0090
ances fo	2 inches	<i>In.</i> 0.0038 . <i>0038</i>	.0040	.0041	.0041	.0042	.0042	.0043	.0044	.0045 .0060 . <i>0072</i>	.0045 .0060 .0082	.0046 .0061 .0084
er toler	1½ inches	${}^{In.}_{0.0036}$	.0036	.0037	.0037	.0038	.0038	.0039	.0040	.0040 .0040 .0071	.0040 .0040 .0071	.0040 .0040 .0071
diamet	1 inch	${}^{In.}_{0.0031}$	.0032	.0032	.0033	.0033	.0034	.0034	.0035	.0036 .0036 .0071	. 0036 . 0036 . 0071	.0036 .0036 .0071
Pitch	34 inch	$\tilde{i}n.$ 0.0028 .0030	.0029	.0029	.0030	. 0030	.0030	.0030	.0030	.0030 .0030 .0071	.0030 .0030 .0071	. 0032 2. 0032 . 0071
	yź inch	${}^{In}_{.\ 0025}$	.0026	.0026	.0026	.0026	.0026	.0026	.0026	<sup>2</sup> .0026 .0030 .0070	.0030 .0030 .0071	. 0032 . 0032 . 0071
	34 inch	${}^{In.}_{0.0023}$	.0024	. 0024	.0024	. 0224	.0024	.0024	<sup>2</sup> .0024 .0030	. 0026 . 0030 . 0068	. 0030 . 0030 . 0069	$^{1}_{-0032}$
	₩ inch	${}^{In.}_{0.0019}$	.0019	.0019	.0019	.0019	.0019	<sup>2</sup> .0022 .0030	.0024	1.0026 .0030 .0066	.0027 .0030 .0067	.0028 .0032 .0068
	346 inch	${In.\atop 0.\ 0017} 0.\ 0030$	.0030	.0017	.0030	.0018	. 0019	.0022	.0024	. 0025 . 0030 . 0065		
	ys inch	${}^{In.}_{0.0014}$	. 0015	.0016	1. 0017 . 0030	.0018	.0019					
	yí inch	${In. \atop 0.0014} 0.0014$	. 0015	.0016	.0017							
ths of sment	To and in- clud- ing—	In. 112 112	1/2	1/22	172	11/2	1722	122	1/2	3722	3112	3112
Lengt	From	$\left\{ \begin{array}{c} In. \\ \hline y_2 \end{array} \right\}$	ží}	ží}	×}	×}	×	}	}			
	Threads per inch	64	565	48	40	36	32	28	24	20	18	16

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#### NATIONAL SCREW THREAD COMMISSION

		0.0124 .0128 .0128	. 0126 . 0152 . 0152	0128.0158.0202	0133 0163 0163 0213	
	0.0109 .0112 .0112	.0115 .0128 .0128	.0117 .0147 .0162	.0120	.0124 .0154 .0204	
	0.0104	.0112 .0128 .0128	.0113 .0143 .0162	.0115 .0145 .0195	. 0120 . 0150 . 0200	
.0098	.0112	.0112 .0128 .0128	.0112 .0138 .0162	.0112 .0140 .0190	.0115 .0145 .0195	d soutos
.0093 0098	.0094 .0109 .0112	.0109 .0128 .0128	.0109 .0132 .0152	.0109 .0135 .0135	.0110 .0140 .0190	- three
.0088 8600 8600	.0089 .0104 .0112	.0104 .0125 .0128	.0104 .0127 .0152	.0104 .0130 .0130	0104	I anoi
.0082 .0097 .0098	.0083 .0098 .0112	.0098 .0119 .0128	.0098 .0121 .0162	.0098 .0124 .0174	.0098 .0128 .0178	Can Nat
. 0075 . 0090 . 0098	.0076 .0091	.0091 .0112 .0128	.0091 .0114 .01 <i>52</i>	.0001 .0117 .0167	.0092 .0122 .0172	Ameri
.0067 .0082 .0098	.0068 .0083	.0083 .0108 .0128	.0083 .0108	.0083 .0109 .0159	.0084 .0114 .0164	the of the
.0058 .0073 .0098	.0059 .0074 .0099	.0074 .0099 .0128	.0074 .0099 .0148	.0074 .0100 .0150	. 0075 . 0105 . 0155	dard siz
.0053 .0068 .0092	.0054 .0069 .0092	.0069 .0092 .0128	.0069 .0092 .0142	.0069 .0095 .0145	. 0070 1. 0097 . 0150	<sup>3</sup> Stan
.0047 .0062 .0084	.0048 .0063 .0084	.0063 .0084 .0128	. 0063 . 0086 . 0136	. 0063 . 0139 . 0139	.0063 .0093 .0143	
.0040 .0040 .0071	.0040 1.0040 .0071	.0059 .0071 .0128	.0059 .0071 .0132	. 0059 1. 0071 . 0135	. 0059 . 0089 . 0139	
.0036 1.0036 .0071	.0040 .0040 .0071	.0054 .0071 .0126	1, 0054 .0071 .0128	.0054 .0071 .0130	. 0055 . 0085 . 0135	eries.
.0036 .0036 .0071	.0040 .0040 .0071	$^{1.0045}_{.0071}$	.0045 .0071 .0125	.0048 .0071 .0122		hread s
.0036 .0036 .0071	.0036 .0040 .0071	.0040 .0071 .0120	.0042 .0071 .0128			coarse-f
.0032 .0036 .0071	.0032 .0040 .0071					ational
						rican N
						he Ame
						size of t
						andard
3112	352	991	931	- 69 -	- e o	1 Sti
132	11/2	3	3	3	31	
14	12	10		9	4	

HUR-UNFBAG Series. Nore.-It is preferable to avoid the use of tolerances set in italics by choosing a closer fit, shorter length of engagement, coarser pitch, or smaller diameter. 89

	Lengths gagem	of en-					Pit	ch dian	neter to	lerance	s for dia	meters	up to aı	nd inclu	iding					
Threads per inch	From-1	To and nelud- ing-	$\mathcal{M}$ inch	38 inch	12 Juch inch	34 inch	1 inch	1½ nches i	2 inches i	3 inches	4 inches	6 inches	8 inches i	10 nches	12 nches	14 nches	16 nches	18 inches	20 Inches	24 inches
28. 29. 16. 16. 12. 12. 10. 10. 10. 10. 13. 4.	Image: state	and the set of a set of a	0,0011,0012,0012,0012,0012,0012,0012,00	0.0012 0.0012 0.0013 0.0013 0.0014 0.0015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0015 0.0016 0.0016 0.0016 0.0016 0.0016 0.0016 0.0015 0.0000000000	Tar.         Tar.         Tar.           0         0013         0         0013         0           0         0015         0013         0	Tar.         Tar.         Tar.           0.0015         0.0015         0.0015           0.0015         0.0015         0.0015           0.0015         0.0015         0.0015           0.0015         0.0015         0.0015           0.0015         0.0015         0.0015           0.0015         0.0015         0.0015           0.0015         0.0016         0.0016           0.0016         0.0016         0.0023           0.0023         0.0023         0.0023           0.0023         0.0023         0.0023           0.0023         0.0023         0.0023           0.0023         0.0023         0.0023           0.0023         0.0023         0.0023           0.0023         0.0023         0.0023           0.0023         0.0023         0.0023           0.0023         0.0023         0.0023           0.0023         0.0023         0.0023           0.0023         0.0023         0.0023	Tar.         Tar.           0.0018         0017         0017           0.0018         0018         0018           0.0018         0018         0018           0.0018         0018         0018           0.0018         0018         0018           0.0018         0018         0018           0.0018         0018         0018           0.0027         0028         0018           0.0027         00203         0022           0.0036         0022         0023           0.0037         0023         0023           0.0037         0023         0023           0.0036         0023         0023           0.0037         0023         0023           0.0036         0023         0023           0.0037         0023         0023           0.0036         0023         0033           0.0037         0036         0036           0.0038         0036         0036	J.         0.019           J.         0.019           0.0020         0.0020           0.0020         0.0020           0.0020         0.0020           0.0020         0.0020           0.0020         0.0020           0.0020         0.0020           0.0020         0.0020           0.0020         0.0020           0.0020         0.0020           0.0020         0.0020           0.0020         0.0020           0.0020         0.0020           0.0020         0.0020           0.0020         0.0020           0.0020         0.0020           0.0020         0.0020           0.0021         0.0020           0.0021         0.0020           0.0021         0.0020           0.0021         0.0020           0.0021         0.0020           0.0021         0.0020           0.0021         0.0020           0.0021         0.0020           0.0021         0.0020           0.0021         0.0020	$\begin{array}{c} J_{1} J_{1}$	Tr.           0.0025           0.0025           0.0035           0.0035           0.0035           0.0035           0.0035           0.0035           0.0035           0.0035           0.0035           0.0035           0.0035           0.0035           0.0036           0.0036           0.0036           0.0036           0.0036           0.0036           0.0036           0.0036           0.0036           0.0036           0.0037           0.0036           0.0036           0.0037           0.0036           0.0036           0.0037           0.0036           0.0037           0.0036           0.0037           0.0037           0.0038           0.0034           0.0034           0.0034           0.0035           0.0036           0.0037           0.0038           0.0038           0.0037           0.003	Image: 1000000000000000000000000000000000000	0.0039 0.0032 0052 0052 0052 0041 0041 0043 0043 0043 0043 0043 0042 0042 0042	$\begin{array}{c} J_{1} J_{1}$	Image: Non-state         Image: Non-state<	$\begin{array}{c} P_{11}P_{11}P_{12$	Image: Non-state         Image: Non-state           0.045         0045           0.045         0045           0.045         0045           0.045         0045           0.045         0045           0.045         0055           0.054         0055           0.055         0056           0.055         0056           0.055         0057           0.055         0065           0.055         0057           0.055         0057           0.055         0057           0.057         0057           0.057         0057           0.057         0057           0.057         0057           0.055         0057           0.055         0057           0.055         0057           0.055         0057           0.055         0055           0.055         0055           0.055         0055           0.055         0055           0.055         0075	In.         0.0055           0.0055         00655           0.0055         00656           0.0056         00656           0.0056         00656           0.0056         00656           0.0056         00656           0.0056         00056           0.0057         00056           0.0057         00057           0.0057         00057           0.0057         00057           0.0057         00057           0.0057         00057           0.0057         00057           0.0057         00057           0.0057         00057           0.0057         00057           0.0057         00057           0.0057         00057           0.0057         00057           0.0057         00057           0.0057         00057           0.0057         00057           0.0057         00057           0.0057         00057	In.         0.0057           0.0057         00567           0.0057         00567           0.0057         00567           0.0057         00567           0.0057         00567           0.0057         00567           0.0057         00057           0.0057         00058           0.0057         00058           0.0057         00058           0.0057         00059           0.0057         00059           0.0057         00059           0.0057         00059           0.0057         00059           0.0056         00059           0.0057         00059           0.0056         00059           0.0056         00059           0.0056         00059           0.0056         00059           0.0056         00059           0.0056         00059           0.0056         00059           0.0056         00058           0.0056         00058	$\begin{array}{c} I_{77}\\ I_{77}\\$	In.           0.0055           0.0657           0.079           0.079           0.079           0.079           0.079           0.079           0.079           0.079           0.079           0.079           0.079           0.079           0.079           0.079           0.079

<sup>2</sup> Standard size of the American National coarse-thread serics.

Nors.-It is preferable to avoid the use of tolerances set in italics by choosing a shorter length of engagement, coarser pitch, or smaller diameter.

<sup>1</sup> Standard size of the American National fine-thread series.

TABLE 39.—Pitch diameter tolerances for special screw threads, class 4, close fit

# SECTION VI. AMERICAN NATIONAL HOSE-COUPLING AND FIRE-HOSE COUPLING THREADS

Several years ago specifications for American National standard fire-hose coupling threads were approved by the National Board of Fire Underwriters, National Fire Protection Association, American Society of Mechanical Engineers, American Society of Municipal Improvements, New England Water Works Association, American Water Works Association, the Bureau of Standards, and other interested organizations. These specifications were published in 1911 as the Specifications of the National Board of Fire Underwriters, recommended by the National Fire Protection Association and approved by the various other organizations. They were also published in 1914 as Circular No. 50 of the Bureau of Standards. This circular was revised and republished in 1917.

When the National Screw Thread Commission took up its work on the standardization of screw threads, the specifications for fire-hose coupling threads above referred to were accepted as the basis of its work on fire-hose coupling threads. It was found, however, that the specifications as originally drawn were inadequate in that they specified nominal dimensions only, with no maximum and minimum limits. The limiting dimensions herein specified have met with general approval, including adoption as "American" standards by the American Standards Association. State-wide adoption of the American National fire-hose coupling threads is completed or under effective headway in 36 States, and their use has been made compulsory by State legislative acts in California, Massachusetts, Oregon, and Texas.

With regard to the American National hose-coupling threads, the purpose of this specification is to provide a standard which will be recognized and adopted at once by a majority of manufacturers and consumers and toward which the minority may be brought, thus eliminating many threads now in use and the confusion and misunderstandings that now prevail.

As in other lines of work, current practice in use and manufacture must be recognized as well as the specific advantages of certain thread proportions for specific uses. This prevents the adoption of a single specification for each one of the nominal sizes.

These standards apply to the threaded parts of hose couplings, valves, nozzles, and all other fittings used in direct connection with hose intended for fire protection or for domestic, industrial, and general service in nominal sizes of  $\frac{1}{2}$ ,  $\frac{5}{2}$ ,  $\frac{3}{4}$ , 1, 1 $\frac{1}{4}$ , 1 $\frac{1}{2}$ , and 2 inches.

In ordering threading tools <sup>16</sup> for producing American National hosecoupling and fire-hose coupling threads, it should be pointed out that new taps should be near the maximum permissible size of the coupling, and new dies near the minimum permissible size of the nipple, in order that reasonable wear may be provided. As the threading tools wear by use, the couplings will become smaller and the nipples larger

<sup>&</sup>lt;sup>19</sup> In the interest of the universal adoption of the American National fire-hose threads throughout the United States, attention is directed to the fact that sets of tools for rethreading existing hydrants and hose couplings are commercially available. Such sets comprise roughing and finishing taps, roughing and finishing ing dies, expanders for expanding undersize externally threaded fittings preparatory to rethreading, gages, and various accessories. The tools are applicable where existing threaded fittings do not differ so widely from the American National standards as to leave insufficient stock for the new thread. By the use of such tools a considerable number of municipalities have at small expense converted their existing equipment, and thus availed themselves of the important advantages which standardization affords.

until the limiting dimensions are reached. These must not be exceeded. When the product reaches, or comes dangerously close to the limiting size, the threading tools should be readjusted or replaced.

## 1. FORM OF THREAD

1. ANGLE OF THREAD.—The basic angle of thread (A) between the sides of the thread measured in an axial plane is 60°. The line bisecting this 60° angle is perpendicular to the axis of the screw thread. 2. FLAT AT CREST AND ROOT.—The flat at the root and crest of

the basic thread form is  $\frac{1}{8} \times p$ , or  $0.125 \times p$ .

3. DEPTH OF THREAD.—The depth of the basic thread form is

$$h = 0.649519 \times p$$
, or  $h = \frac{0.649519}{n}$ 

where

connections.

11/2-----

p = pitch in inchesn = number of threads per inch h = basic depth of thread

#### 2. THREAD SERIES

(a) AMERICAN NATIONAL HOSE-COUPLING THREADS.—There are specified in table 40 a thread series and basic dimensions for hosecoupling threads which apply to the threaded parts of hose couplings, valves, nozzles, and all other fittings used in direct connection with hose intended for fire protection or for domestic, industrial, and general service in nominal sizes of 1/2, 5/8, 3/4, 1, 11/4, 11/2, and 2 inches.

TABLE 40.—American National hose-coupling threads

BASIC MINIMUM COUPLING DIMENSIONS

Nominal size of hose (in inches)	Service	Num- ber of threads per inch	Pitch	Depth of thread	Major diam- eter	Pitch diam- eter	Minor diam- eter	Al- low- ance
1	` 2	3	4	5	6	7	8	9
1/2, 5/6, 3/4 3/4, 1 1/2 3/4 3/4 1 1./4 1./2 2	Garden hose Chemical engine and booster hose Fire-protection hose Steam, air, water, and all other hose connections.	$ \begin{cases} 11\frac{1}{2}\\ 8\\ 9\\ 14\\ 14\\ 11\frac{1}{2}\\ 11\frac{1}{2}\\ 11\frac{1}{2}\\ 11\frac{1}{2}\\ 11\frac{1}{2} \end{cases} $	Inch 0. 08696 . 12500 . 11111 . 07143 . 07143 . 08696 . 08696 . 08696 . 08696	Inch 0. 05648 . 08119 . 07217 . 04639 . 04639 . 05648 . 05648 . 05648 . 05648	Inches 1.0725 1.3870 2.0020 .8323 1.0428 1.3051 1.6499 1.8888 2.3628	Inches 1. 0160 1. 3058 1. 9298 . 7859 . 9964 1. 2486 1. 5934 1. 8323 2. 3063	Inches 0. 9595 1. 2246 1. 8577 . 7395 9500 1. 1921 1. 5369 1. 7758 2. 2498	Inch
	BASIC MAXIMUM N	IPPLE	DIME	NSION	IS			
1/2, 5/8, 3/4 3/4, 1 1/2 1/2 3/4	Garden hose Chemical-engine and booster hose Fire-protection hose	111/2 8 9 14 14 14	0.08696 .12500 .11111 .07143 .07143	0.05648 .08119 .07217 .04639 .04639	1.0625 1.3750 1.9900 .8248 1.0353 1.2051	1.0060 1.2938 1.9178 .7784 .9889	0.9495 1.2126 1.8457 .7320 .9425	0.0100 .0120 .0120 .0075 .0075

111/2

.08696 . 08696

. 08696

.05648 1.6399 1.5834 1.5269

1.8223

2. 2963

.05648 1.8788 .05648 2.3528

.0100

.0100

1.7658 2.2398



FIGURE 19.—American National hose-coupling and American National fire-hose coupling threads.

See tables 42, 43, 44, and 45 for dimensions and tolerances.

(b) AMERICAN NATIONAL FIRE-HOSE COUPLING THREADS.—There are specified in table 41 a thread series and basic dimensions for firehose couplings from 2½ to 4½ inches in diameter which will be known as the "American National fire-hose threads." These basic sizes and dimensions correspond in all details to those recommended by the National Fire Protection Association and by the Bureau of Standards.

The American National fire-hose coupling thread is recommended for use on all couplings and hydrant connections for fire-protection systems, and for all other purposes where hose couplings and connections are required in sizes between  $2\frac{1}{2}$  and  $4\frac{1}{2}$  inches in diameter.

#### TABLE 41.—American National fire-hose coupling threads

Nominal size of hose (in inches)	Number of threads per inch	Pitch	Depth of thread	Major diame- ter	Pitch diame- ter	Minor diame- ter	Allow- ance
1	2	3	4	5	6	7	8
2½	$7\frac{1}{2}$ 6 6 4	Inch 0. 13333 . 16667 . 16667 . 25000	Inch 0.08660 .10825 .10825 .16238	<i>Inches</i> 3. 0836 3. 6389 4. 2639 5. 7859	Inches 2, 9970 3, 5306 4, 1556 5, 6235	Inches 2. 9104 3. 4223 4. 0473 5. 4611	Inch

#### BASIC MINIMUM COUPLING DIMENSIONS

BASIC MAXIMUM NIPPLE DIMENSIONS

## 3. ALLOWANCES AND TOLERANCES

(a) Specified allowances and tolerances, given in table 42, apply to-American National hose coupling and American National fire-hose coupling threads. The tolerances represent extreme variations permitted on the product. There are shown, in figure 20, the relations between nipple and coupling dimensions and thread form as specified herein.

(b) The tolerance on the coupling is plus, and is applied from the minimum coupling dimension to above the minimum coupling dimension.

(c) The tolerance on the nipple is minus, and is applied from the maximum nipple dimension to below the maximum nipple dimension.

(d) The pitch diameter tolerances provided for a mating nipple and coupling are the same.

(e) Pitch diameter tolerances include lead and angle variations. (See footnote 1, table 42.)

(f) The tolerance on the major diameter is twice the tolerance on the pitch diameter.

(g) The tolerance on the minor diameter of the nipple is equal to the tolerance on pitch diameter plus two ninths of the basic thread depth. The minimum minor diameter of a nipple is such as to result in a flat equal to one third of the basic flat  $(\frac{1}{24} \times p)$  at the root when the pitch diameter of the nipple is at its minimum value. The maxi-

mum minor diameter is basic, but may be such as results from the use of a worn or rounded threading tool.

(h) The tolerance on major diameter of the coupling is equal to the tolerance on pitch diameter plus two ninths of the basic thread depth. The minimum major diameter of the coupling is such as to result in a basic flat  $(\frac{1}{2} \times p)$  when the pitch diameter of the coupling



FIGURE 20.—American National hose-coupling and American National fire-hose coupling threads.

is at its minimum value. The maximum major diameter of the coupling is that corresponding to a flat equal to one third the basic flat  $(\frac{1}{24} \times p)$ .

(i) The tolerance on the minor diameter of the coupling is twice the tolerance on pitch diameter of the coupling. The minimum minor diameter of a coupling is such as to result in a basic flat  $(\frac{1}{2} \times p)$ at the crest when the pitch diameter of the coupling is at its minimum value.

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Nominal size of hose (in inches) Service		Threads per inch	Allow- ances	Toler- ances on pitch di- ameter <sup>1</sup>	Lead errors consum- ing one half of pitch-di- ameter toler- ances <sup>2</sup>	Errors in half angl consum- ing one half of pitch-di- ameter- toler- ances	
1	2	3	4	5	6	7	
14, 56, 34 34, 1 11/2	Garden hose Chemical engine and booster hose Fire protection hose	11½ 8 9	Inch 0.0100 .0120 .0120	Inch 0.0085 .0111 .0111	Inch 0.0025 .0032 .0032	Deq. M 1 1	in. 52 42 54
142	Steam, air, water, and all other hose connections.	$\left\{\begin{array}{c} 14\\ 14\\ 11\frac{1}{2}\\ 11\frac{1}{2}\\ 11\frac{1}{2}\\ 11\frac{1}{2}\\ 11\frac{1}{2}\\ 11\frac{1}{2}\end{array}\right.$	.0075 .0075 .0100 .0100 .0100 .0100	.0070 .0070 .0085 .0085 .0085 .0085 .0085	. 0020 . 0020 . 0025 . 0025 . 0025 . 0025 . 0025	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	52 52 52 52 52 52 52
2½ 3 3½ 4½	Fire hose		. 0150 . 0150 . 0200 . 0250	. 0160 . 0180 . 0180 . 0250	. 0046 . 0052 . 0052 . 0072	2 2 2 1	17 4 4 55

TABLE 42.-Tolerances and allowances for American National hose coupling and American National fire-hose coupling threads

<sup>1</sup> The tolerances specified for pitch diameter include all errors of pitch diameter, lead, and angle. The full tolerance cannot, therefore, be used on pitch diameter unless the lead and angle of the thread are perfect. Columns 6 and 7 give, for information, the errors in lead (per length of thread engaged) and in angle, each of which can be compensated for by half the tolerance on the pitch diameter given in column 5. If lead and angle errors both exist to the amount tabulated, the pitch diameter of a nipple, for example, must be reduced by the full tolerance or it will not enter the "go" gage. <sup>3</sup> Between any two threads not farther apart than the length of engagement.

#### 4. TABLES OF LIMITING DIMENSIONS

TABLE 43.—Limiting dimensions and tolerances, American National hose coupling threads

Nomi		inch		read	Major diameter			Pite	h dian	neter	Minor diameter		
nal size of hose (in inches)	Service	Threads per	Pitch	Depth of th	Maximum	Tolerance	Minimum	Maximum	Tolerance	Minimum	Maximum	Tolerance	Minimum
1	2	3	4	5	6	7	8	9	10	11	12	13	- 14
12, 58, 34 84, 1	Garden hose Chemical en- gine and booster hose.	1111/2 8	Inch 0. 08696 . 12500	Inch 0. 05648 . 08119	In.	In.	In. <sup>1</sup> 1.0725 <sup>1</sup> 1.3870	In. 1. 0245 1. 3169	In. 0. 0085 . 0111	In. 1.0160 1.3058	In. 0. 9765 1. 2468	In. 0. 0170 . 0222	In. 0. 9595 1. 2246
172 1/2 3/4 1/4 1/4 1/2 2	Steam, air, wa- ter and all other hose connections.	$\begin{cases} 14 \\ 14 \\ 11\frac{12}{11} \\ 11\frac{12}{11} \\ 11\frac{12}{11} \\ 11\frac{12}{11} \\ 11\frac{12}{12} \end{cases}$	.07143 .07143 .08696 .08696 .08696 .08696 .08696	. 04639 . 04639 . 05648 . 05648 . 05648 . 05648			1, 8323 1, 8323 1, 0428 1, 3051 1, 6499 1, 8888 1, 2, 3628	1. 9409 . 7929 1. 0034 1. 2571 1. 6019 1. 8408 2. 3148	. 0070 . 0070 . 0085 . 0085 . 0085 . 0085	. 7859 . 9964 1. 2486 1. 5934 1. 8323 2. 3063	. 7535 . 9640 1. 2091 1. 5539 1. 7928 2. 2668	.0140 .0140 .0170 .0170 .0170 .0170	. 7395 . 9500 1. 1921 1. 5369 1. 7758 2. 2498

COUPLING THREAD

<sup>1</sup> Dimensions for the minimum major diameter of the coupling correspond to the basic flat  $(\frac{1}{6} \times p)$ , and the profile at the major diameter produced by a worn tool must not fall below the basic outline. The maximum major diameter of the coupling shall be that corresponding to a flat at the major diameter of the maximum coupling equal to  $\frac{1}{2}4 \times p$ , and may be determined by adding  $\frac{1}{2}4 \times h$  (or 0.7939p) to the maxi-mum pitch diameter of the coupling.

# threads-Continued

Nomia		inch		read	Major diameter			Pitch diameter			Minor diameter		
nal size of hose (in inches)	Service	Threads per	Pitch	Depth of th	Maximum	Talerance	Minimum	Maximum	Tolerance	Minimum	Maximum	Tolerance	Minimum
1	2	3	4	5	6	7	6	9	10	11	12	13	14
12, 58, 34 14, 1	Garden hose Chemical en- gine and booster hose	11½ 8	Inch 0. 08696 . 12500	Inch 0. 05648 . 08119	In. 1.0625 1.3750	In. 0. 0170 . 0222	In. 1.0455 1.3528	In. 1.0060 1.2938	In. 0. 0085 . 0111	In. 0. 9975 1. 2827	In. 30.9495 31.2126	In.	In.
1/2	Fire protection hose.	9	. 11111	. 07217	1.9900	. 0222	1.9878	1. 9178	. 0111	1.9067	<b>*</b> 1. 8457		
4 4 1/4 1/4	Steam, air, wa- ter and all other hose connections.	$\begin{bmatrix} 14 \\ 14 \\ 111\frac{1}{2} \\ 111\frac{1}{2} \\ 111\frac{1}{2} \\ 111\frac{1}{2} \\ 11\frac{1}{2} \end{bmatrix}$	.07143 .07143 .08696 .08696 .08696 .08696	. 04639 . 04639 . 05648 . 05648 . 05648 . 05648	. 8248 1. 0353 1. 2951 1. 6399 1. 8788 2. 3528	.0140 .0140 .0170 .0170 .0170 .0170	. 8108 1. 0213 1. 2781 1. 6229 1. 8618 2. 3358	. 7784 . 9889 1. 2386 1. 5834 1. 8223 2. 2963	.0070 .0070 .0085 .0085 .0085 .0085	.7714 .9819 1.2301 1.5749 1.8138 2.2878	<sup>3</sup> .7320 <sup>3</sup> .9425 <sup>3</sup> 1.1821 <sup>3</sup> 1.5269 <sup>3</sup> 1.7658 <sup>3</sup> 2.2398		

TABLE 43.-Limiting dimensions and tolerances, American National hose coupling

<sup>3</sup> Dimensions given for the maximum minor diameter of the nipple are figured to the intersection of the worn tool are with a center line through crest and root. The minimum minor diameter of the nipple shall be that corresponding to a flat at the minor diameter of the minimum nipple equal to  $\frac{1}{16} \times p$ , and may be determined by subtracting  $\frac{1}{16} \times k$  (or 0.7939p) from the minimum pitch diameter of the nipple.

 TABLE 44.—Lengths of threads for American National hose-coupling threads

 and
 American National fire-hose coupling threads





Nominal size of hose (in inches)	Service	Threads per inch, n	Length of nip- ple, L	Depth of cou- pling, H	Thread length for cou- pling, T	Length of pilot, J	Inside diame- ter of nipple, C Maxi- mum	Approx- imate number of threads in length T
12, 58, 34_ 34, 1 12, 34_ 1 1, 11,4 11,4 2,	Garden hose Chemical engine and boost- er hose. Fire protection hose Steam, air, water, and all other hose connections.	$\begin{cases} 111/2 \\ 8 \\ 9 \\ 14 \\ 113/2 \\ 111/2 \\ 111/2 \\ 111/2 \\ 111/2 \\ 111/2 \end{cases}$	Inch 9/16 5/8 9/16 9/16 9/16 9/16 5/8 5/6 3/4	Inck 1732 1932 1932 1532 1732 1732 1932 1932 2332	Inch 38 1532 1542 916 36 36 1542 1542 1942	Inch 1/8 5/52 1/8 1/8 1/8 5/52 5/52 5/52 5/52 3/16	Inches 2532 1/32 1752 1752 2552 1/32 152 152 1752 2532 152 1532 1	414 334 414 414 514 514 514 634
2½ 3 3½ 4½	Fire hose	$ \left\{\begin{array}{c} 7{6}\\ 6\\ 4\\ 4 \end{array}\right. $	1 1½8 1½8 1¼4	15/16 13/16 13/16 13/16	1 1/16 1 3/16 1 3/16 1 5/16	34 5/16 5/16 7/16	21732 3132 31732 41732	514 5 5 334

#### NIPPLE THREAD

 TABLE 45.—Limiting dimensions and tolerances, American National fire-hose coupling threads

Nominal	Threads		Depth	Major diameter			Pitch diameter			Minor diameter		
size of hose (in inches)	per inch	Pitch	of thread	Maxi- mum	Toler- ance	Mini- mum	Maxi- mum	Tole <b>r</b> - ance	Mini- mum	Maxi- mum	Toler- ance	Mini- mum
1	2	3	4	5	6	7	8	9	10	11	12	13
2½ 3 3½ 4½	7½ 6 6 4	Inch 0. 13333 . 16667 . 16667 . 25000	Inch 0. 08660 . 10825+ . 10825+ . 16238	Inches	Inch	Inches <sup>1</sup> 3.0836 <sup>1</sup> 3.6389 <sup>1</sup> 4.2639 <sup>1</sup> 5.7859	Inches 3. 0130 3. 5486 4. 1736 5. 6485	Inch 0. 0160 . 0180 . 0180 . 0250	Inches 2. 9970 3. 5306 4. 1556 5. 6235	Inches 2. 9424 3. 4583 4. 0833 5. 5111	Inch 0. 0320 . 0360 . 0360 . 0500	Inches 2. 9104 3. 4223 4. 0473 5. 4611

COUPLING THREAD

#### NIPPLE THREAD

$2\frac{1}{2}$	$\begin{array}{c} 7\frac{1}{2}\\ 6\\ 6\\ 6\\ 4\\ 25000 \end{array} 0.1333; \\ .1666; \\ .1666; \\ .25000 \end{array}$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	686 239 439 609 .0360 .0360 .0500	3. 0366 3. 5879 4. 2079 5. 7109	2. 9820 3. 5156 4. 1356 5. 5985	0.0160 .0180 .0180 .0250	2.9660 3.4976 4.1176 5.5735	<sup>2</sup> 2. 8954 <sup>2</sup> 3. 4073 <sup>2</sup> 4. 0273 <sup>2</sup> 5. 4361		
----------------	---	--	---	--	--	-----------------------------------	--------------------------------------	--	--	--

<sup>1</sup> Dimensions for the minimum major diameter of the coupling correspond to the basic flat  $(\frac{1}{2} \times p)$ , and the profile at the major diameter produced by a worn tool must not fall below the basic outline. The maximum major diameter of the coupling shall be that corresponding to a flat at the major diameter of the maximum coupling equal to  $\frac{1}{2}(\frac{1}{2} \times p)$ , and may be determined by adding  $\frac{1}{2} + \frac{1}{2} \times \frac{1}{2}$  (or 0.7939) to the maximum pitch diameter of the coupling.

<sup>a</sup> Dimensions given for the maximum minor diameter of the nipple are figured to the intersection of the worn tool arc with a center line through crest and root. The minimum minor diameter of the nippl shall be that corresponding to a flat at the minor diameter of the minimum nipple equal to  $\frac{1}{24} \times p$ , and may be determined by subtracting  $1\frac{2}{5} \times h$  (or 0.7939p) from the minimum pitch diameter of the nipple.

#### 5. GAGES

(a) GAGES FOR AMERICAN NATIONAL FIRE-HOSE COUPLING THREADS.—It is recommended that American National fire-hose coupling threads be inspected in the field by means of gages made within the tolerances given in table 46. Limiting dimensions for these gages are given in tables 47 and 48.

It is further recommended that American National fire-hose coupling threads be given final inspection by the manufacturer by means of gages made within the limiting dimensions given in tables 47 and 48, by whatever amount may be desired, in order to avoid, as far as possible, disagreements which might otherwise arise as the result of slight differences in the sizes of gages.

TABLE 46.—Tolerances on gages for American National fire-hose coupling threads

Allowable variation in lead between any two threads not farther apart than length of engagement	Allowable variation in one half angle of thread	Tolerance on diam- eter of minimum thread gage	Tolerance on diam- eter of maximum thread gage						
1	2	3	4						
Inch ±0.0005	Deg. Min. ±0 10	$ \{ \begin{array}{c} Inch \\ -0.000 \\ +.001 \end{array} \}$	Inch +0.000 001						
		"	Go'' or mi	nimum gag	(e	"N	ot go" or n	naximum g	age
----------------------------------	---------------------	---	--	--	---	--	--	--	--
Nominal size of	Threads per inch	Major d	liameter	Pitch d	iameter	Major d	liameter	Pitch d	iameter
1036		Maxi- mum	Mini- mum	Maxi- mum	Mini- mum	Maxi- mum	Mini- mum	Maxi- mum	Mini- mum
1	2	3	4	5	6	7	8	9	10
2.500 3.000 3.500 4.500	7½ 6 6 4	<i>Inches</i> 3. 0846 3. 6399 4. 2649 5. 7869	Inches 3. 0836 3. 6389 4. 2639 5. 7859	Inches 2. 9980 3. 5316 4. 1566 5. 6245	<i>Inches</i> 2. 9970 3. 5306 4. 1556 5. 6235	Inches 3. 0836 3. 6389 4. 2639 5. 7859	Inches 3. 0826 3. 6379 4. 2629 5. 7849	Inches 3. 0130 3. 5486 4. 1736 5. 6485	Inches 3. 0120 3. 5476 4. 1726 5. 6475

TABLE 47.—Limiting dimensions of field inspection thread plug gages for couplings (internal threads)<sup>1</sup>

<sup>1</sup> The minor diameters of plug gages and the major diameters of ring gages are undercut beyond the nominal diameters to give a clearance for grinding or lapping. The allowable variation in lead between any two threads not farther apart than the length of engagement is  $\pm 0.0005$  inch. The allowable variation in one half angle of thread is  $\pm 10$  minutes.

TABLE 48.—Limiting dimensions of field inspection thread ring gages for coupling nipples (external threads)<sup>1</sup>

		"	Go" or ma	ximum gag	( <del>0</del>	"N	ot go" or n	ninimum g	age
Nominal size of hose	Threads per inch	Pitch d	iameter	Minor d	iameter	Pitch d	iameter	Minor d	liameter
2000		Maxi- mum	Mini- mum	Maxi- mum	Mini- mum	Maxi- mum	Mini- mum	Maxi- mura	Mini- mum
1	2	3	4	5	6	7	8	9	10
2.500 3.000 3.500 4.500	7½ 6 6 4	Inches 2. 9820 3. 5156 4. 1356 5. 5985	Inches 2.9810 3.5146 4.1346 5.5975	Inches 2. 9104 3. 4223 4. 0473 5. 4611	Inches 2. 9094 3. 4213 4. 0463 5. 4601	Inches 2. 9670 3. 4986 4. 1186 5. 5745	Inches 2. 9660 3. 4976 4. 1176 5. 5735	Inches 2. 9114 3. 4233 4. 0483 5. 4621	Inches 2.9104 3.4223 4.0473 5.4611

<sup>1</sup> The minor diameters of plug gages and the major diameters of ring gages are undercut beyond the nominal diameters to give clearance for grinding or lapping. The allowable variation in lead between any two threads not farther apart than the length of engagement is  $\pm 0.0005$  inch. The allowable variation in one half angle of thread is  $\pm 10$  minutes.

# SECTION VII. AMERICAN NATIONAL PIPE THREADS

The material on the subject of pipe threads presented herewith is essentially the same as that in the report prepared by a special committee of the Committee of Manufacturers on Standardization of Fittings and Valves, acting in cooperation with pipe and gage manufacturers and the A.S.M.E. Committee on International Standards for Pipe Threads. It was published in October 1919, under the title "Manual on American Standard Pipe Threads." It has been endorsed by the American Society of Mechanical Engineers and the American Gas Association, and is adopted by the commission with only such changes as are necessary to bring it into conformity with the remainder of the report. The material on gages for pipe threads has, however, been extensively revised.

The American National pipe-thread standard for taper threaded pipe joints was formulated prior to the year 1882 by Robert Briggs, of Philadelphia, Pa. This standard, with certain modifications and additions, is now in general use throughout the United States and Canada.

## 1. FORM OF THREAD

(a) Specifications.-1. Angle of thread.-The angle between the sides of the thread is 60° when measured in an axial plane, and the line bisecting this angle is perpendicular to the axis of the pipe for either taper or straight threads.

2. Depth of thread.<sup>17</sup>—The crest and root of the thread form are truncated an amount equal to 0.0330p; the depth of thread is, therefore, equal to 0.8p.



FIGURE 21.—American National taper pipe thread form and notation.

#### NOTATION

 $A = 60^{\circ}$  angle of thread

 $\begin{array}{l} A = 50^{\circ} \text{ angle of thread} \\ a = 30^{\circ} \text{ one half angle of thread} \\ y = 1^{\circ} 47^{\circ} \text{ approx. taper angle=one sixteenth inch per inch on diameter} \\ I = 0.866025p \text{ depth of } 60^{\circ} \text{ sharp V thread} \\ k = 0.80000p \\ = 0.923761H1 \\ \text{depth of thread on work} \end{array}$ 

- =0.033012p= 0.038120H depth of truncation
- = 0.041266h
- p=1/n pitch (measured parallel to axis) n = number of threads per inch

3. Taper of thread.—The taper of the thread is 1 in 16, or three fourths inch per foot, measured on the diameter.

(b) ILLUSTRATION.—There are shown in figure 21 the relations as specified herein for form of thread, and general notation. Special notation is given in figures 22, 23, and 25.

<sup>&</sup>lt;sup>17</sup> While Mr. Briggs originally advocated a slightly rounded crest and root, cutting tools are actually slightly flattened at the crest and root.

<sup>&</sup>lt;sup>18</sup> For a symmetrical straight screw thread,  $H=\frac{p}{2}$  cot a. For a symmetrical taper screw thread  $H=\frac{p}{2}$ (cot  $a-\tan^2 y$  tan a), so that the exact value for an American National taper pipe thread is H=0.8657339as against H=0.866025p, the value given above. For an 8-pitch thread, which is the coarsest standard taper pipe thread pitch, the corresponding values of H are 0.108218 inch and 0.108253 inch, respectively, the differ-ence being 0.000035 inch. This difference being too small to be significant, the value of H=0.866025p con-tinues in use for threads of three fourths inch, or less, taper per foot.

## 2. SYMBOLS

The list of symbols given in section II, 3, together with additional symbols given below, should be used in formulas for expressing relations of pipe threads, on drawings, etc.

Pitch diameter of thread at end of pipe	$E_0$
Pitch diameter of thread at gaging notch	$E_1$
Pitch diameter of thread at $L_2$ from end of pipe	$E_2$
Maximum pitch diameter, external locknut thread	$E_{e}$
Minimum pitch diameter, internal locknut thread	$E_1$
Distance from gaging notch to end of pipe=normal engagement by hand	$L_1$
Length of effective thread	$L_2$
Outside diameter of pipe=major diameter of pipe thread at $L_2$ from end of	
pipe	D
Internal diameter of nine	d



FIGURE 22.--American National taper pipe thread notation.

NOTATION  $E_0 = D - (0.05D + 1.1)p$   $E_1 = E_0 + 0.0625L_1$   $L_2 = p (0.8D + 6.8)$ h = 0.8p

### 3. THREAD SERIES

(a) AMERICAN NATIONAL TAPER PIPE THREADS.—Taper external and internal pipe threads are recommended for threaded pipe joints and pipe fittings for any service. The sizes and basic dimensions of the "American National taper pipe threads" are specified in table 49.

1. Outside diameter of *pipe*.—The outside diameters of pipe are given in column 5 of table 49.

2. Diameters of taper threads.—The pitch diameters of the taper threads are determined by formulas based on the outside diameter

oe threads
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of Ame
49Dimensions
TABLE

[For notation, see fig. 22]

	Basic minor diameter at small end of pipe, $^1$		13	Inches 0.33388 .43294 .56757 .70129 .91054	1. 14407 1. 48757 1. 72652 2. 19946 2. 61953	<ol> <li>24063</li> <li>73750</li> <li>73750</li> <li>23438</li> <li>4, 73125</li> <li>5, 29073</li> </ol>	6. 34609 7. 33984 8. 33359 9. 32734 10. 44531
	r at end of	Minimum	12	Inches 0.37129 .48468 .62181 .77173 .98217	$\begin{array}{c} 1.\ 23048\\ 1.\ 57523\\ 1.\ 81418\\ 2.\ 28812\\ 2.\ 75044 \end{array}$	3. 37678 3. 87709 4. 37541 4. 87422 5. 43757	6, 49425 7, 49062 8, 48831 9, 48625 10, 60022
ters	$L_1$ on pipe, of coupling, $B_1 = E_0 + \frac{L_1}{16}$	Basic	11 .	Inches 0.37476 .48989 .62701 .77843 .98887	1. 23863 1. 58338 1. 82234 2. 29627 2. 76216	<ol> <li>3.38850</li> <li>3.8881</li> <li>3.8881</li> <li>4.38712</li> <li>4.88504</li> <li>5.44929</li> </ol>	6, 50597 7, 50234 8, 50003 9, 49797 10, 62094
Pitch diame	At length .	Maximum	10	Inches 0.37823 .49510 .63222 .78513 .78513	$\begin{array}{c} 1. \ 24678 \\ 1. \ 59153 \\ 1. \ 83049 \\ 2. \ 30442 \\ 2. \ 77388 \end{array}$	3. 40022 3. 90053 4. 39884 4. 89766 5. 46101	6. 51769 7. 51406 8. 51175 9. 50969 10. 63266
	At end of pipe, or at length $L_1$ from end of coupling, $E_0 = D - \frac{0.05D+1.1}{n}$	Basic	6	Inches 0.36351 0.47739 0.61201 0.61201 0.96768	1. 21363 1. 55713 1. 79609 2. 26902 2. 71953	3. 34062 3. 83750 4. 33438 4. 83125 5. 39073	6. 44609 7. 43984 8. 43359 9. 42734 10. 54531
	Increase in diameter per thread, $\frac{0.0625}{n}$		~~~		.00543 .00543 .00543 .00543 .00543	.00781 18700 18700 18700 18700 .0781	.00781 18700 18700 18700 .00781
	Length of effec- tive thread, $L_3$		7	Inches 0. 26385 . 40178 . 40778 . 53371 . 54571	. 68278 . 70678 . 72348 . 756652 1. 13750	$\begin{array}{c} 1.\ 20000\\ 1.\ 25000\\ 1.\ 36000\\ 1.\ 36000\\ 1.\ 40630\end{array}$	1. 61250 1. 61250 1. 71250 1. 81250 1. 92500
	Length of normal engage- ment by hand, $L_1$		9	Inches 0. 180 2200 320 339	. 400 . 420 . 436 . 682	. 766 . 821 . 844 . 875 . 937	. 958 1. 000 1. 063 1. 130 1. 210
	Outside diameter of pipe, D		2	Inches 0.405 .540 .675 .840 1.050	1. 315 1. 660 1. 900 2. 875 2. 875	3, 500 5, 600 5, 500 5,	6. 625 7. 625 8. 625 9. 625 9. 625
	Depth of thread, h		4	Imch 0. 02963 0. 04444 0. 04444 0. 05714	. 06957 . 06957 . 06957 . 06957 . 06957 . 10000	10000 10000 10000	. 10000 10000 10000 10000
	Pitch,		e	Inch 0. 03704 0. 05556 0. 05556 0. 05556 0. 07143 0. 07143	08696 08696 08696 08696 08696	12500 12500 12500 12500 12500	.12500 .12500 .12500 .12500
	Number of threads per inch,		67	27 188 144 144	8 8 8 8	00 00 00 00 00	00 00 00 00 00
	Nominal size of pipe in inches		1	222222	1 1 )% 2 )% 2 )%	3 33 4 5 4 5 4 1 5	22 22 00

NATIONAL SCREW THREAD COMMISSION

11	80	0.12500	0.10000	11.750	1.285	2. 02500	0.00781	11.53906	11.63109 1	11.61938	11.60766	11 43006
12	80	.12500	.10000	12.750	1.360	2.12500	. 00781	12.53281	12.62953	12.61781	12.60609	12.43281
14 O.D.	90	. 12500	.10000	14.000	1.562	2.25000	. 00781	13.77500	13.88434	13.87262	13.86091	13 67500
15 O.D.	00	.12500	. 10000	15.000	1.687	2.35000	. 00781	14.76875	14.88591	14.87419	14.86247	14.66875
16 0.D	80	.12500	.10000	16.000	1.812	2.45000	. 00781	15.76250	15.88747	15.87575	15.86403	15.66250
	¢	COACT.	0000	0000 11		000	1010					
	00	. 12500	00001	10,000	1. 900	2. 55000	.00781	16. 75625	16.88672	16.87500	16.86328	16.65625
18 U.U.	20	. 12500	. 10000	18.000	2.000	2.65000	. 00781	17.75000	17.88672	17.87500	17.86328	17.65000
20.0.0	00	.12500	.10000	20.000	2.125	2.85000	. 00781	19.73750	19.88203	19.87031	19.85859	19.63750
22 0.D	8	.12500	.10000	22.000	2.250	3. 05000	. 00781	21.72500	21.87734	21.86562	21.85391	21.62500
24 0.D	00	.12500	. 10000	24.000	2.375	3. 25000	. 00781	23.71250	23.87266	23 86094	23 84022	23 61250
										-		00=TO 00=
26 O.D	00	.12500	.10000	26,000	2.500	3.45000	. 00781	25. 70000	25.86797	25 85625	25 84453	95 60000
28 O. D.	00	.12500	. 10000	28,000	2.625	3.65000	. 00781	27.68750	27, 86328	27, 85156	27 83084	27 58750
30 O. D	00	.12500	. 10000	30,000	2.750	3.85000	00781	29, 675:00	29.85859	29.84688	29,83516	29 57500
											04000	
<sup>1</sup> Given as information for use in sel	ecting te	p drills.				-	-					

of pipe and the pitch of thread. These are as follows <sup>19</sup> (see Symbols above):

 $E_0 = D - (0.05D + 1.1)p$ 

 $E_1 = E_0 + 0.0625L_1$ 

3. Length of thread.-The length of the taper external thread is determined by a formula based on the outside diameter of pipe and the pitch of the thread. This is as follows <sup>19</sup> (see Symbols above):

$$L_2 = (0.8D + 6.8)p$$

4. Length of engagement.—The normal length of engagement be-tween taper external and internal threads, when screwed together by hand, is shown in column 6 of table 49. This length is controlled by means of gages.

5. Tolerances.—The tolerance on diameter is the equivalent of the variation in diameter due to taper over one and one half turns either way from the basic dimensions.<sup>20</sup>

(b) AMERICAN NATIONAL STRAIGHT PIPE THREADS.—The speci-fied sizes and basic dimensions on the "American National straight pipe threads" are given in table 50.

1. Diameters of straight threads.—The basic pitch diameter of the straight thread is equal to the diameter at the gaging notch of American National taper pipe thread, and is determined by the following formula based on the outside diameter of pipe and the pitch of thread (see Symbols above):

$$E_1 = D - (0.05D + 1.1)p + 0.0625L_1$$

2. Tolerances .- The tolerance on pitch diameter of a straight pipe thread is the equivalent of the variation in diameter over one and one half turns either way from the gaging notch of the American National taper pipe thread.<sup>21</sup> (See columns 4 and 6 of table 50.)

 <sup>&</sup>lt;sup>19</sup> These formulas are not expressed in the same terms as the formulas originally established by Mr. Briggs, because they are used to determine directly the pitch diameter and the length of effective thread, which includes two threads slightly imperfect at the crest; whereas the Briggs formulas determined the major diameter and the length of perfect thread, the two threads imperfect on the crest not being included in the formula. However, both forms give identical results.
 <sup>20</sup> See figs. 29 and 30.
 <sup>21</sup> The coupling thread may be gaged with a taper threaded plug gage. On account of the gage tolerance of one half turn on working taper pipe thread gages, the working tolerance is equivalent to one turn either way from the gaging note. In gaging, care must be taken to gage at the first thread scratch and not at the end of the coupling when the thread is chamfered.

3. Application to internal threads.—Straight threaded internal wrought iron or wrought steel couplings of the weight known as "standard" may be used with taper threaded pipe for ordinary



FIGURE 23.—American National straight pipe thread notation (internal).

Norz.—This thread is gaged with the taper threaded plug gage and should gage flush at the bottom of the chamfer (first thread scratch) with the gaging notch, allowing a maximum variation of one and one-half turns plus or minus from the notch.

pressures, as they are sufficiently ductile to adjust themselves to the taper external thread when properly screwed together.

For high pressures, only taper external and internal threads should be used.

4. Application to external threads.—Straight external threads are recognized only for special applications, such as long screws and tank nipples.

 TABLE 50.—Dimensions of American National straight pipe threads (for couplings)

 [For notation see fig. 23]

Nominal sizes (in inches)	Threads	Major diameter 1	Pit	ch diameter	, <i>E</i> 1	Minor diameter 1
	per men	basic	Maximum	Basic	Minimum	Basic
1	2	3	4	5	6	7
¥6	27 18 18	Inches 0. 40439 . 53433 . 67145	Inches 0. 37823 . 49510 . 63222	Inches 0. 37476 . 48989 . 62701	Inches 0. 37129 . 48468 . 62181	Inches 0. 34513 . 44544 . 58257
72	14 111/2 111/2 111/2	1. 04600 1. 30819 1. 65294 1. 89190	. 99556 1. 24678 1. 59153 1. 83049	.98887 1.23863 1.58338 1.82234	.98217 1.23048 1.57523 1.81418	. 93172 1. 16907 1. 51382 1. 75277
2 2 3 3 3 3 4 2 3 4	11142 8 8 8	2. 36583 2. 86216 2. 48850 3. 98881	2. 30442 2. 77388 3. 40022 3. 90053	2. 29627 2. 76216 3. 38850 3. 88881	2. 28812 2. 75044 3. 37678 3. 87709	2. 22671 2. 66216 3. 28850 3. 78881
4 4 <u>1/2</u> 5 6	8 8 8 8	4. 48713 4. 98594 5. 54929 6. 60597	4: 39884 4. 89766 5. 46101 6. 51769	4. 38712 4. 88594 5. 44929 6. 50597	4. 37541 4. 87422 5. 43757 6. 49425	4. 28713 4. 78594 5. 34929 6. 40597

<sup>1</sup> The American National pipe thread form is maintained; therefore, the major and minor diameters vary with the pitch diameter and are determined by the threading tools.

5. Application to long screw joints.—Long screw joints are used to a limited extent. This joint is not considered satisfactory when subjected to high temperature or pressure. In this application the coupling has a straight thread and must make a joint with an American National taper pipe thread. (See fig. 23.) It is necessary that the coupling be screwed on the straight external thread for the full length of the coupling and then back until it engages the taper external thread. The straight thread on the pipe enters the coupling freely



FIGURE 24.—Illustration of "long screw" joint between straight threaded coupling and taper threaded pipe.

by hand, the joint being made by a packing material between the locknut and the coupling. (See fig. 24.) On account of the long engagement of thread, imperfections in

On account of the long engagement of thread, imperfections in pitch affect the fit when the coupling is screwed on the pipe its full length. Refinements of manufacture and gaging to insure a properly interchangeable product are more costly than the commercial



FIGURE 25.—American National locknut thread notation.

NOTATION

 $E_1$  = pitch diameter at gaging notch of American National taper plug gage  $E_0 = E_1 + (4p \times 0.0625)$   $E_1 = E_1 + (5p \times 0.0625)$ 

NOTE.-See table 51 for relation to taper pipe thread.

use warrants; therefore, the use of this type of joint is not recommended. For this reason, specifications for tolerances and gaging are not included herein.

(c) AMERICAN NATIONAL LOCKNUT THREADS.—Occasional requirements make it advisable to have a straight thread of the largest diameter it is possible to cut on a pipe. This practice has been standardized and is known as "maximum external and minimum internal locknut threads." For dimensions, see table 51. The "tank nipple" shown in figure 26 is an example of this thread. In this application an American National standard taper pipe thread is cut on the end of the pipe after having first cut the "external locknut thread."



FIGURE 26.—Illustration of "tank nipple" thread.

TABLE 51.—Dimensions of American National locknut threads

Nominal sizes (in inches)	Threads per inch	E. (maxi- mum) <sup>1</sup>	Ei (mini- mum) 1	Depth of thread
1	2	3	4	5
½           ¼           ¾           ¾           ¾           ¾           ¾           ¾           ¾           ¾           ¾           ¾           ¾           ¾           ¾           1           1½           1½           2           2¼	$27 \\ 18 \\ 18 \\ 14 \\ 114 \\ 1114 \\ 1114 \\ 1114 \\ 1114 \\ 1114 \\ 1114 \\ 8 \\ 8$	Inches 0. 38402 50378 64090 79629 1. 00672 1. 26037 1. 60512 1. 84408 2. 31801 2. 79341	Inches 0. 38633 .50725 .64427 .80075 1.01119 1.26580 1.61055 1.84951 2.32345 2.80122	Inch 0. 02963 . 04444 . 04444 . 05714 . 05714 . 06957 . 06957 . 06957 . 06957 . 06957 . 06957
3 3½ 4 4½	8 8 8 8	3. 41975 3. 92006 4. 41838 4. 91719	3. 42756 3. 92787 4. 42619 4. 92500	. 10000 . 10000 . 10000 . 10000
56 67 78	8 8 8 8	5. 48054 6. 53722 7. 53359 8. 53128	5. 48836 6. 54503 7. 54141 8. 53909	. 10000 . 10000 . 10000 . 10000
9 10 11 12	8 8 8	9. 52922 10. 65219 11. 65063 12. 64906	9. 53703 10. 66000 11. 65844 12. 65688	. 10000 . 10000 . 10000 . 10000

[For notation, see fig. 25]

<sup>1</sup> A tolerance equivalent to one and one half turns of the American National taper pipe thread is recommended, the tolerance being minus on  $E_{\bullet}$  and plus on  $E_{i}$ .

## 4. TABLES OF PIPE DIMENSIONS

Tables 52, 53, 54, and 55, which follow, are not a part of the thread standard, but are reprinted as part of the Manual on American Standard Pipe Threads.

				Transve	rse areas	Length of pipe	Nominal weight
Nominal sizes (in inches)	Inside diameter	Outside diameter	Nominal thickness	Internal	Metal	square foot of external surface	per foot threaded and coupled
1	2	3	4	5	6	7	8
96	Inches 0. 269 . 364 . 493 . 622 . 824	Inches 0.405 .540 .675 .840 1.050	Inch 0.068 .088 .091 .109 .113	Square inches 0.057 .104 .191 .304 .533	Square inches 0.072 .125 .167 .250 .333	Feet 9. 431 7. 073 5. 658 4. 547 3. 637	Pounds 0. 245 . 425 . 568 . 852 1. 134
1 1¼ 1½	1.049 1.380 1.610 2.067 2.469	1.315 1.660 1.900 2.375 2.875	. 133 . 140 . 145 . 154 . 203	. 864 1. 495 2. 036 3. 355 4. 788	. 494 . 669 . 799 1. 075 1. 704	2. 904 2. 301 2. 010 1. 608 1. 328	1. 684 2. 281 2. 731 3. 678 5. 819
3 3 <sup>1</sup> / <sub>2</sub> 4 4 <sup>1</sup> / <sub>2</sub> 1 5	3.068 3.548 4.026 4.506 5.047	3. 500 4. 000 4. 500 5. 000 5. 563	. 216 . 226 . 237 . 247 . 258	7. 393 9. 886 12. 730 15. 947 20. 006	2, 228 2, 680 3, 174 3, 688 4, 300	1.091 .954 .848 .763 .686	7. 616 9. 202 10. 889 12. 642 14. 810
6 7 1 8 1 8 9	6. 065 7. 023 8. 071 7. 981 8. 941	6. 625 7. 625 8. 625 8. 625 9. 625	. 280 . 301 . 277 . 322 . 342	28. 891 38. 738 51. 161 50. 027 62. 786	5. 581 6. 926 7. 265 8. 399 9. 974	. 576 . 500 . 442 . 442 . 396	19. 185 23. 769 25. 000 28. 809 34. 188
10 1 10 1 10 11 1 12 1 12 2	10. 192 10. 136 10. 020 11. 000 12. 090 12. 000	$\begin{array}{c} 10.\ 750\\ 10.\ 750\\ 10.\ 750\\ 11.\ 750\\ 12.\ 750\\ 12.\ 750\\ 12.\ 750\end{array}$	. 279 . 307 . 365 . 375 . 330 . 375	81. 585 80. 691 78. 855 95. 033 114. 800 113. 097	9. 178 10. 072 11. 908 13. 401 12. 876 14. 579	. 355 . 355 . 355 . 325 . 299 . 299	32. 000 35. 000 41. 132 46. 247 45. 000 50. 706

## TABLE 52.—Dimensions of standard wrought pipe

<sup>1</sup> Not included in simplified list of sizes as given in Department of Commerce Simplified Practice Recommendation R57-32.

TABLE 53.—Dimensions of extra strong wrought pipe

				Transve	rse areas	Length of pipe	Nominal
Nominal sizes (in inches)	Inside diameter	Outside diameter	Nominal thickness	Internal	Metal	square foot of external surface	per foot, plain ends
1	2	3	4	5	6	7	8
16 14 76 15 74	Inches 0. 215 . 302 . 423 . 546 . 742	Inches 0.405 .540 .675 .840 1.050	<i>Inch</i> 0.095 .119 .126 .147 .154	Square inches 0.036 .072 .141 .234 .433	Square inches 0.093 .157 .217 .320 .433	Feet 9. 431 7. 073 5. 658 4. 547 3. 637	Pounds 0.314 .535 .738 1.087 1.473
1 1}4 1}4 1}2 2 2}2	. 957 1. 278 1. 500 1. 939 2. 323	1. 315 1. 660 1. 900 2. 375 2. 875	. 179 . 191 . 200 . 218 . 276	. 719 1. 283 1. 767 2. 953 4. 238	. 639 . 881 1. 068 1. 477 2. 254	2.904 2.301 2.010 1.608 1.328	2. 171 2. 996 3. 631 5. 022 7. 661
33 <u>}<u>4</u> 4 4<u>}<u>4</u><u>3</u><u>4</u></u></u>	2. 900 3. 364 3. 826 4. 290	3. 500 4. 000 4. 500 5. 000	. 300 . 318 . 337 . 355	6. 605 8. 888 11. 497 14. 455	3. 016 3. 678 4. 407 5. 180	1.091 .954 .848 .763	10. 252 12. 505 14. 983 17. 611
56 7 7 18	4. 813 5. 761 6. 625 7. 625	5. 563 6. 625 7. 625 8. 625	. 375 . 432 . 500 . 500	$\begin{array}{c} 18.\ 194\\ 26.\ 067\\ 34.\ 472\\ 45.\ 663\end{array}$	$\begin{array}{c} 6.\ 112 \\ 8.\ 405 \\ 11.\ 192 \\ 12.\ 763 \end{array}$	. 686 . 576 . 500 . 442	20, 787 28, 573 38, 048 43, 388
9 1 10 11 1 12	8.625 9.750 10.750 11.750	9.625 10.750 11.750 12.750	. 500 . 500 . 500 . 500	58. 426 74. 662 90. 763 108. 434	14. 334 16. 101 17. 671 19. 242	. 396 . 355 . 325 . 299	48. 728 54. 735 60. 075 65. 415

<sup>1</sup> Not included in simplified list of sizes as given in Department of Commerce Simplified Practice Recommendation R57-32.

				Transve	rse areas	Length of pipe	Nominal
Nominal sizes (in inches)	Inside diameter	Outside diameter	Nominal thickness	Internal	Metal	per square foot of external surface	weight per foot, plain ends
1	2	3	4	5	6	7	8
<u>5</u> 4 14 14	Inches 0. 252 . 434 . 599 . 896 1. 100	Inches 0.840 1.050 1.315 1.660 1.900	Inch 0. 294 . 308 . 358 . 382 . 400	Square inches 0,050 .148 .282 .630 .950	Square inches 0.504 .718 1.076 1.534 1.885	Feet 4. 547 3. 637 2. 904 2. 301 2. 010	Pounds 1.714 2.440 3.659 5.214 6.408
¥4	1.503 1.771 2.300 2.728 3.152	2. 375 2. 875 3. 500 4. 000 4. 500	. 436 . 552 . 600 . 636 . 674	1.774 2.464 4.155 5.845 7.803	2. 656 4. 028 5. 466 6. 721 8. 101	1.608 1.328 1.091 .954 .848	9, 029 13, 695 18, 583 22, 850 27, 541
1 <u>4</u> 1	3. 580 4. 063 4. 897 5. 875 6. 875	5.000 5.563 6.625 7.625 8.625	.710 .750 .864 .875 .875	10. 066 12. 966 18. 835 27. 109 37. 122	9. 569 11. 340 15. 637 18. 555 21. 304	. 763 . 686 . 576 . 500 . 442	32, 530 38, 552 53, 160 63, 079 72, 424

13111 22334 45678

#### TABLE 54.—Dimensions of double extra strong wrought pipe

<sup>1</sup> Not included in simplified list of sizes as given in Department of Commerce Simplified Practice Recommendation R57-32.

TABLE 55.—Diameters of large O.D. pipe

Naminal sizes (in	Out-				Insi	ide diam	eter			
inches)	diam- eter	14 inch thick	⁵⁄ís inch thick	⅔ inch thick	%s inch thick	½ inch thick	%s inch thick	5% inch thick	34 inch thick	1 inch thick
1	2	3	4	5	6	7	8	9	10	11
14 15 16 17 18	Inches 14 15 16 17 18	Inches 13½ 14½ 15½ 16½ 17½	Inches 133% 143% 153% 163% 163%	Inches 13¼ 14¼ 15¼ 15¼ 16¼ 17¼	Inches 13½ 14½ 15½ 16½ 17½	Inches 13 14 15 16 17	Inches 127/6 137/6 147/8 157/8 167/8	Inches 1234 1334 1434 1534 1634	Inch es 12½ 13½ 14½ 15½ 16½	Inches 12 13 14 15 16
20222426283030303030	20 22 24 26 28 30		1938 2138 	19¼ 21¼ 23¼ 25¼	19% 21% 23% 25% 25% 27% 29%	19 21 23 25 27 29	187⁄8 207⁄8 227⁄8 247⁄8 277⁄8 287⁄8	1834 2034 2234 2434 2634 2834	1834 2034 2234 2434 2634 2834	18

#### 5. GAGES

#### (a) FUNDAMENTALS

The same fundamentals apply as those outlined in section III covering gages for fastening screws, with the single exception that, with taper threaded gages, separate "go" and "not go" gages are not necessary.

## (b) SPECIFICATIONS FOR GAGES

The following specifications are for the purpose of establishing definite limits for thread gages rather than for the purpose of specifying the design of gages required for the various inspection operations.

Basic dimensions of taper pipe thread gages are given in table 57

All such gages should be made to the basic dimensions within the tolerances for each element given in table 56 and footnotes thereto. It is possible for taper thread plug and ring gages, which come within the tolerances specified for each element, to vary from being flush with each other at the gaging end, or at the gaging notch, when screwed together tightly by hand. The maximum variation which might occur and be permissible, expressed in terms of longitudinal distance or stand-off, is given in column 9 of table 56.

In order properly to maintain interchangeability of pipe threads, gages should consist of "master," "checking," "inspection," and "working" gages.

1. CLASSIFICATION OF GAGES—(a) Master gage.—The master gage is a taper threaded plug gage. (See fig. 27.) It is the gage to which all other gages are ultimately referred, either by transfer of measure-



FIGURE 27.—Master gage or check gage for checking inspection gages.

ments or direct comparison by engagement. It is intended primarily for the use of gage and thread tool manufacturers. It should be made to the basic size as accurately as possible and be within the tolerances given in table 56.

Each master gage shall be marked with an identification number or symbol, and be accompanied by a report showing the error on each of the elements of thread and a statement of the accumulative error derived from the errors in the various elements. In case of question, the deviations of this gage from the basic size shall be ascertained by the Bureau of Standards at Washington, D.C. (b) Checking plug gage.—The checking plug gage is similar in all

(b) Checking plug gage.—The checking plug gage is similar in all respects to the master gage, and is used to inspect inspection and working taper threaded ring gages.

(c) Inspection gages.—Inspection gages consist of one taper threaded plug gage and one taper threaded ring gage.

Inspection gages are for the use of the purchaser of pipe thread products. When used, the extreme tolerances on the work should be applied. This tolerance is one and one-half turns either way from the gaging notch in the case of internal threads inspected with the inspection plug gage, and when inspecting external threads the tolerance is one and one-half turns either way from the small end of the inspection ring. Inspection gages should be checked frequently and in use their errors should be taken into account.

(d) Working gages.—The working gages consist of one taper threaded plug and one taper threaded ring gage. These gages are similar in all respects to the inspection plug and ring gages. The working gages are used by the manufacturer to inspect his product. In using the working gages, the tolerance to be applied is one turn either way from the gaging notch in the case of internal threads inspected with the plug gage, and in the case of external threads the tolerance is one turn either way from the small end of the working ring gage.

2. THREAD FORM OF TAPER PIPE THREAD PLUG AND RING GAGES.—The roots of the threads of all taper pipe thread gages are



FIGURE 28.—Inspection or working gages for checking product.

cut to sharp V or may be undercut to facilitate making the thread. The crests are truncated an amount equal to 0.1p, but otherwise the gages are made to the dimensions given in table 49.<sup>22</sup>

## (c) GAGING PRACTICES

A common practice in the gaging of taper pipe threads is illustrated in figures 27, 28, 29, and 30. However, other practices, some of which may be equally satisfactory, are widely used.

The basic gaging length is equal to the dimension  $L_1$ . In figures 27 and 28 this dimension is shown as the thickness of the ring gage, and as the distance from the small end to the gaging notch of the plug gage.

1. GAGING INTERNAL THREADS.—The inspection and working plug gages, figure 29, should screw tight by hand into the fitting or coupling until the notch is flush with the face. When the thread is chamfered, the notch should be flush with the bottom of the chamfer, (first thread scratch). The fitting or coupling is within the working or net tolerance if the working gage notch is within one turn of the

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<sup>&</sup>lt;sup>22</sup> The object of truncating the crests on gages (truncation 0.1*p*) is to insure that, when gaging commercial threads cut with a slightly dull tool, the gage bears on the sides of the thread instead of on the roots.

coupling or fitting face when screwed in tight by hand. In the same way the coupling or fitting is within the inspection or extreme tolerance if the inspection gage notch is within one and one-half turns of the coupling or fitting face when screwed on tight by hand.



INTERNAL THREAD INTERNAL THREAD INTERNAL THREAD BASIC SIZE MAXIMUM SIZE MINIMUM SIZE

FIGURE 29.—Gaging of internal American National taper pipe threads.

This method of gaging is used either for taper internal threads or for straight internally threaded couplings which screw together with taper external threads.

2. GAGING TAPER EXTERNAL THREADS.—The ring gage, figure 30, should screw tight by hand on the pipe or external thread until the



FIGURE 30.—Gaging of external American National taper pipe threads.

small end of the gage is flush with the end of the thread. The pipe or external thread is within the working or net tolerance if the working ring gage screws on until the end of pipe or external thread is within one turn of the small end of the gage. The pipe or external thread is within the inspection or extreme tolerance if the inspection ring screws on until the end of pipe is within one and one-half turns of the small end of the gage.

#### GAGES FOR PIPE THREADS

#### **TABLE 56.**—Tolerances for American National taper pipe thread plug and ring gages

Nominal sizes (in inches)	Number of threads per inch	Toler- ance on pitch diam- eter 12 (includ- ing taper)	Toler- ance on lead <sup>3</sup>	Toler- ance on half angle of thread	Toler- ance on major diameter of plug gage	Toler- ance on minor diameter of ring gage	Maxi- mum longitu- dinal variation from basic for plug or ring gage	Maxi- mum stand-off between plug and ring gages at gaging end when screwed together tightly by hand
1	2	3	4	5	6	7	8	9
1/4           1/4	$\begin{array}{c} 27\\ 18\\ 18\\ 14\\ 14\\ 11\frac{12}{11\frac{12}{2}}\\ 11\frac{12}{2}\\ 11\frac{12}{2}\\ 8\\ 8\\ 8\end{array}$	Inch 0.0002 .0003 .0003 .0003 .0003 .0003 .0003 .0003 .0003 .0004	Inch ± 0,0002 .0002 .0002 .0002 .0002 .0003 .0003 .0003 .0003 .0003 .0004	$\begin{array}{c} Deg. \ Min. \\ \pm \\ 0 \\ 10 \\ 0 \\ 10 \\ 0 \\ 8 \\ 0 \\ 8 \\ 0 \\ 8 \\ 0 \\ 8 \\ 0 \\ 8 \\ 0 \\ 8 \\ 0 \\ 8 \\ 0 \\ 5 \\ 0 \\ 5 \\ 0 \\ 5 \\ \end{array}$	Inch + 0.0005 .0005 .0010 .0010 .0010 .0010 .0010 .0010 .0010 .0015	Inch 	Inch 0.0115 .0144 .0144 .0146 .0146 .0181 .0181 .0181 .0181 .0181 .0219 .0219	Inch 0.0230 .0288 .0292 .0292 .0362 .0362 .0362 .0362 .0362 .0362 .0362 .0438
1½ 1¼	8 8 8 8	.0004 .0004 .0004 .0004	. 0004 . 0004 . 0004 . 0004	0 5 0 5 0 5 0 5	.0015 .0015 .0015 .0015	. 0015 . 0015 . 0015 . 0015	.0219 .0219 .0219 .0219 .0219	. 0438 . 0438 . 0438 . 0438
0 2 4 O.D	8 8 8 8 8	. 0004 . 0005 . 0005 . 0005 . 0006	. 0004 . 0005 . 0005 . 0005 . 0006	0 5 0 5 0 5 0 5 0 5 0 5	. 0015 . 0020 . 0020 . 0020 . 0025	. 0015 . 0020 . 0020 . 0020 . 0025	. 0219 . 0264 . 0264 . 0264 . 0264 . 0307	. 0438 . 0528 . 0528 . 0528 . 0528 . 0614
6 0.D. 8 0.D. 20 0.D. 4 0.D.	8 8 8 8	. 0006 . 0006 . 0006 . 0006	.0006 .0006 .0006 .0006	0 5 0 5 0 5 0 5 0 5	. 0025 . 0025 . 0025 . 0025 . 0025	. 0025 . 0025 . 0025 . 0025 . 0025	. 0307 . 0307 . 0307 . 0307 . 0307	.0614 .0614 .0614 .0614

<sup>1</sup> The taper of the pitch diameter cone shall be such that the pitch diameter will be within the tolerance given at all points. For example, if the gage is to maximum size at the small end, the taper shall not be greater than 0.750 inch taper per foot. If a gage is to minimum size at the small end, the taper shall not be less than 0.750 inch taper per foot. <sup>3</sup> Pitch diameter tolerance is to be applied plus on plug gages (other than checking plug gages); minus on shacking study gages.

checking plug gages and ring gages. <sup>3</sup> Allowable variation in lead between any 2 threads.

Note.—The tolerance for the height from the gaging end to notch of all piug gages shall be plus 0.000 inch, minus 0.001 inch for sizes ½ inch to 2 inches, inclusive, and plus 0.000 inch, minus 0.002 inch for sizes 2½ to 24 inches, inclusive. The tolerance for the over-all thread length of plug gages shall be plus ½2 inch, minus 0.000 inch for sizes ½ inch to 2 inches, inclusive, and plus ½5 inch, minus 0.000 inch for sizes 2½ to 24 inches, inclusive. The thickness of the ring gage shall be held within a tolerance of plus 0.001 inch, minus 0.000 inch for sizes ½ inch to 2 inches, inclusive, and plus 0.002 inch, minus 0.000 inch for sizes 2½ to 24 inches, inclusive

	-	Thick- ness of full ring, $L_2$	15	Inches 0. 26385 . 40178 . 53371 . 54571	. 68278 . 70678 . 72348 . 75652 1. 13750	$\begin{array}{c} 1.\ 20000\\ 1.\ 25000\\ 1.\ 35000\\ 1.\ 35000\\ 1.\ 40630 \end{array}$	1. 51250 1. 61250 1. 71250 1. 71250 1. 92500	2, 02500 2, 12500 2, 25000 2, 35000 2, 45000
	Ē	Thick- ness of thin ring, $L_1$	14	Inches 0.180 200 .200 .320 .339	.400 .420 .436 .682	. 766 . 821 . 844 . 875 . 937	. 958 1. 000 1. 163 1. 130 1. 210	1. 285 1. 360 1. 562 1. 687 1. 812
ireads	Increase in	diameter per thread, $\frac{0.0625}{n}$	13	Inch 0.00231 00347 00347 00347 003446 00446	. 00543 . 00543 . 00543 . 00543 . 00543		.00781 .00781 .00781 .00781 .00781 .00781	18200 18700 18700 18700
er pipe tl	ing gages <sup>1</sup>	At large end, full ring, $E_2$ - 0.666025 n	12	Inches 0.35533 46550 .46550 .60050 .74421 .95421	$\begin{array}{c} 1. \ 19839\\ 1. \ 54339\\ 1. \ 78339\\ 2. \ 25839\\ 2. \ 70737\\ \end{array}$	3. 33237 3. 83237 4. 33237 4. 83237 5. 39537	6. 45737 7. 45737 8. 45737 9. 45737 9. 45737 10. 58237	11. 58237 12. 58237 13. 83237 14. 83237 14. 83237 15. 83237
onal tape	meters of r	At gaging notch, $E_{1-}$ 0.666025 $\pi$	11	Inches 0.35009 .45289 .59001 .73086 .94129	$\begin{array}{c} 1.\ 18072\\ 1.\ 52547\\ 1.\ 52547\\ 1.\ 76442\\ 2.\ 23836\\ 2.\ 67890 \end{array}$	3. 30525 3. 80556 4. 30387 4. 80268 5. 36604	6. 42272 7. 41909 8. 41678 9. 41472 10. 53768	$\begin{array}{c} 11.53612\\ 12.53456\\ 13.78937\\ 14.79093\\ 15.79250\\ \end{array}$
an Natie	Minor dia	At small end, $E_0$ 0.666025 n	10	Inches 0.33884 .44039 .57501 .71086 .92011	$\begin{array}{c} 1.15571\\ 1.49921\\ 1.73817\\ 2.21111\\ 2.63628 \end{array}$	3. 25737 3. 75425 4. 25112 4. 74800 5. 30748	6. 36284 7. 35659 8. 35034 9. 34409 10. 46206	$\begin{array}{c} 11. 45581\\ 12. 44956\\ 13. 69175\\ 14. 68550\\ 14. 68550\\ 15. 67925\end{array}$
Americ	olug and	At large end, full ring, $E_2$	5	Inches 0.38000 50250 .50250 .79179 1.00179	$\begin{array}{c} 1.\ 25630\\ 1.\ 60130\\ 1.\ 84130\\ 2.\ 31630\\ 2.\ 79062 \end{array}$	3. 41562 3. 91562 4. 41562 4. 91562 5. 47862	$\begin{array}{c} 6.54062\\ 7.54062\\ 8.54062\\ 9.54062\\ 9.54062\\ 10.66562\end{array}$	$\begin{array}{c} 11. \ 66562 \\ 12. \ 66562 \\ 13. \ 91562 \\ 14. \ 91562 \\ 15. \ 91562 \end{array}$
gages for	meters of 1 ring gages	At gaging notch, <i>E</i> <sub>1</sub>	œ	Inches 0.37476 0.37476 .48989 .62701 .77843 .98887	$\begin{array}{c} 1.\ 23863\\ 1.\ 58338\\ 1.\ 58338\\ 1.\ 82234\\ 2.\ 29627\\ 2.\ 76216 \end{array}$	3. 38850 3. 88881 4. 38712 4. 88594 5. 44929	$\begin{array}{c} 6.50597\\ 7.50234\\ 8.50003\\ 9.49797\\ 10.62094\end{array}$	$\begin{array}{c} 11.\ 61938\\ 12.\ 61781\\ 13.\ 87262\\ 14.\ 87419\\ 15.\ 87575\end{array}$
nd ring	Pitch dia	At small end, $E_0$	7	Inches 0.36351 .47739 .61201 .75843 .96768	$\begin{array}{c} 1.\ 21363\\ 1.\ 55713\\ 1.\ 79609\\ 2.\ 26902\\ 2.\ 71953\\ \end{array}$	3. 34062 3. 83750 4. 33438 4. 83125 5. 39073	$\begin{array}{c} 6.\ 44609\\ 7.\ 43984\\ 8.\ 43359\\ 9.\ 42734\\ 10.\ 54531\end{array}$	$\begin{array}{c} 11.53906\\ 12.53281\\ 13.77500\\ 14.76875\\ 15.76250\end{array}$
d plug a	ug gages 1	At large end, full ring, $E_2+$ 0.666025 n	9	Inches 0.40467 0.40467 0.53950 .53950 .83936 1.04936	$\begin{array}{c} 1. & 31422 \\ 1. & 65922 \\ 1. & 89922 \\ 2. & 37422 \\ 2. & 87388 \end{array}$	$\begin{array}{c} \textbf{3. } \textbf{49888} \\ \textbf{3. } \textbf{49888} \\ \textbf{4. } \textbf{49888} \\ \textbf{4. } \textbf{49888} \\ \textbf{5. } \textbf{56188} \\ \textbf{5. } \textbf{56188} \end{array}$	$\begin{array}{c} 6.\ 62388\\ 7.\ 62388\\ 8.\ 62388\\ 9.\ 62388\\ 9.\ 62388\\ 10.\ 74888\end{array}$	$\begin{array}{c} 11. \ 74888 \\ 12. \ 74888 \\ 12. \ 74888 \\ 13. \ 99888 \\ 14. \ 99888 \\ 15. \ 99888 \\ 15. \ 99888 \\ 15. \ 99888 \\ 15. \ 99888 \\ 16. \ 99888 \\ 16. \ 99888 \\ 16. \ 99888 \\ 16. \ 99888 \\ 16. \ 99888 \\ 16. \ 99888 \\ 10. \ 99888 \\ 10. \ 99888 \\ 10. \ 99888 \\ 10. \ 99888 \\ 10. \ 99888 \\ 10. \ 99888 \\ 10. \ 99888 \\ 10. \ 99888 \\ 10. \ 99888 \\ 10. \ 908888 \\ 10. \ 908888 \\ 10. \ 908888 \\ 10. \ 90888 \\ 10. \ $
threader	At gag.	At gag- ing notch, $E_1 +$ 0.666025 n	20	$\begin{array}{c} Inches\\ 0.39943\\ 0.39943\\ .52689\\ .66402\\ .82600\\ 1.03644\end{array}$	$\begin{array}{c} 1.\ 29655\\ 1.\ 64130\\ 1.\ 88025\\ 2.\ 35419\\ 2.\ 84541 \end{array}$	$\begin{array}{c} 3.\ 47175\\ 3.\ 97207\\ 4.\ 47038\\ 4.\ 96919\\ 5.\ 53255\end{array}$	$\begin{array}{c} 6. \ 58922 \\ 7. \ 58560 \\ 8. \ 58328 \\ 9. \ 58122 \\ 10. \ 70419 \end{array}$	$\begin{array}{c} 11.\ 70263\\ 12.\ 70107\\ 13.\ 95588\\ 14.\ 95744\\ 14.\ 95744\\ 15.\ 95900 \end{array}$
nsions of	Major diar	At small end, $E_0+$ 0.666025 n	4	$\begin{array}{c} Inches\\ 0.38818\\ 0.38818\\ 0.38818\\ 0.51439\\ 0.64902\\ 0.64902\\ 0.64902\\ 1.01525\end{array}$	$\begin{array}{c} 1.\ 27155\\ 1.\ 61505\\ 1.\ 85400\\ 2.\ 32694\\ 2.\ 80278 \end{array}$	$\begin{array}{c} 3.\ 42388\\ 3.\ 92075\\ 4.\ 41763\\ 4.\ 91450\\ 5.\ 47398\end{array}$	$\begin{array}{c} 6.52935\\ 7.52310\\ 8.51685\\ 9.51060\\ 9.51060\\ 10.62857\end{array}$	$\begin{array}{c} 11.\ 62232\\ 12.\ 61607\\ 13.\ 85825\\ 14.\ 85200\\ 15.\ 84575\\ 15.\ 84575\\ \end{array}$
ric dimer		Pitch, <i>p</i>	50	$ \begin{array}{c} Inch \\ 0.\ 03704 \\ 0.\ 05556 \\ 0.\ 05556 \\ 0.\ 05556 \\ 0.\ 07143 \end{array} . \\ 0.\ 77143 \end{array} $	. 08696 . 08696 . 08696 . 08696 . 08696 . 12500	.12500 .12500 .12500 .12500 .12500	12500 12500 12500 12500 12500	.12500 .12500 .12500 .12500
57.—Ba		Number of threads per inch, n	67	27 188 144 148	111 11 11 12 12 12 12 12 12 12 12 12 12	ao ao oo oo oo	00 00 00 00 00	ac ac ac ac ac
TABLE		Nominal size of pipe (in inches)	I		26 26	54. 54.	0	2 4 0.D 5 0.D

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1 These dimensions are based on a crest truncation of 0.1p for pipe thread gages, which insures bearing of the gage on the sides of the thread, when cut with a slightly dull tool, instead of at the roots of the thread.

# SECTION VIII. AMERICAN NATIONAL SCREW, BOLT, AND NUT PROPORTIONS 23

A project to which the Commission gave early attention was the standardization of bolt and nut proportions. A subcommittee of the Commission and subcommittee no. 2 of the Sectional Committee on the Standardization of Bolt, Nut, and Rivet Proportions organized under the procedure of the American Standards Association, worked in close cooperation in developing standards for wrench-head bolts and nuts which are referred to below.

The Commission endorses the standards for proportions of the following threaded products as listed in the references below:

Bolt heads:	Reference
Heavy	_ 2
Regular	_ 1.2
Cap screw heads, hexagon	_ 2
Cap screws, slotted head	3.4
Carriage bolts:	, -
Countersunk	_ 5
Fin-neck	5
Ribbed	5
Square-neck	1.5
Castellated nuts	1.2
Heavy nuts	2
Jam nuts	1.2
Jam nuts. heavy	2
Light nuts	1.2
Regular nuts	1.2
Machine bolts	1
Machine bolts, button-head	1.5
Machine screws, slotted-head	3.4
Machine screw nuts	2
Plow bolts	8
Set screws	2.3
Step bolts	5
Stove bolts	3
Stove bolt nuts	2
Tap rivets	1
Track bolts	7
Track bolt nuts	7
Wood screws	4.6

- Federal Specification for Bolts, Nuts, Studs, and Tap Rivets (and material for same), No. FF-B-571a, January 9, 1934. Sold by the Superintendent of Documents, Washington, D. C. Price, 5 cents.
   American Standard Wrench-head Bolts and Nuts and Wrench Openings. Report No. B18.2-1933, issued and sold by the American Standards Asso-ciation, 29 West Thirty-ninth Street, New York, N. Y. Price, 50 cents.
   Federal Specifications for Screws, Machine, Cap, and Set; and Bolts, Stove, No. FF-S-91, April 22, 1933. Sold by the Superintendent of Documents, Washington, D. C. Price, 5 cents.
   American Standard Slotted Head Proportions—Machine Screws, Cap Screws, and Wood Screws. Report No. B18c-1930. issued and sold by the American
- and Wood Screws. Report No. B18c-1930, issued and sold by the American Standards Association, 29 West Thirty-ninth Street, New York, N. Y. Price, 45 cents.
- 5. American Standard Round Unslotted Head Bolts-Carriage, Step, and Machine Bolts. Report No. B18e-1928, issued and sold by the American Standards Association, 29 West Thirty-ninth Street, New York N. Y. Price, 40 cents.
- 6. Federal Specifications for Screws, Wood, No. FF-S-111, April 28, 1931. Sold by the Superintendent of Documents, Washington, D. C. Price, 5 cents.

<sup>23</sup> See also appendix 5, p. 161.

- 7. American standard track bolts and nuts. Report No. B18d-1930, issued and
- merican standard track boils and huls. Report No. 138d-1930, Issued and sold by the American Standards Association, 29 West Thirty-ninth Street, New York, N.Y. Priče, 40 cents. low Bolts. United States Department of Commerce Simplified Practice Recommendation R23, February 19, 1924. Issued by the Bureau of Standards and sold by the Superintendent of Documents, Washington, D.C. Price, 5 cents. Also published as Report No. B18f-1928, American Stand-ard for Plow Bolts. Issued and sold by the American Standards Association, 00 Word Thirty eight Street Num York, NY Price 25 cents 8. Plow Bolts. 29 West Thirty-ninth Street, New York, N.Y. Price, 35 cents.

# SECTION IX. MISCELLANEOUS SPECIAL THREADS

# Section IX A. Screw Threads for Oil-Well Drilling Equipment

The Commission, through its subcommittee on oil-well casing threads and the staff of the Bureau of Standards, has at various times extended assistance to the American Petroleum Institute in those parts of its program of standardization of oil-field equipment which deal with specifications for screw threads and methods of gaging screw threads.

The first problem in this field brought to the attention of the Commission was the great need for standardization of oil-well casing threads. Definite work toward such standardization was initiated by the Mid-Continent Oil and Gas Association in 1921, but this was complicated by a proposal to simplify casing sizes and weights, and provide new standard sizes of nesting casing required for the deeper well drilling which is now necessary. Certain manufacturers had also endeavored to come to an agreement on thread standards. Through the cooperative efforts of the American Petroleum Institute, the Standardization Committee of the Mid-Continent Oil and Gas Association, and the Commission, certain agreements as to diameters, pitches, and tapers were effected. The complete standard for casing threads, together with standards for drill pipe and tubing, are now published as A.P.I. Standard No. 5-A, "Pipe Specifications", issued by the division of standardization, American Petroleum Institute, 1508 Kirby Building, Dallas, Tex.

The Commission endorses the screw thread and screw-thread gage specifications included in the following American Petroleum Institute standards:

No. 3. A.P.I. dimensional standards for cable drilling tools.

No. 5-A. A.P.I. pipe specifications. No. 5-L. A.P.I. line pipe specifications. No. 7-B. A.P.I. specifications for rotary drilling taper joints.

No. 11-A. A.P.I. specifications for oil-well pumps (barrels, plungers, valves, etc.). No. 11-B. A.P.I. sucker rod specifications.

## Section IX B. American National Standard Hose Connections for Welding and Cutting Torches

The specifications given herein, covering hose connections for welding and cutting torches, were approved and adopted by the Commission June 28, 1926. These specifications were formulated and adopted in 1925, in essentially the same form, by the International Acetylene Association and the Gas Products Association, and have been adopted by various manufacturers.

Dimensions essential to the interchangeability of parts have been standardized. Other dimensions and details of design are optional, so that manufacturers may use their own judgment and follow their usual practice as much as possible. Two sizes of connections are specified, as illustrated in figures 31 and 32.

## 1. STANDARD DIMENSIONS

1. Screw threads corresponding to the American National finethread series, and class 3, medium fit, are specified in figures 31 and 32, for which dimensions are given in table 13. Right-hand threads are specified for oxygen and left-hand threads for fuel gas.

2. Angle and outside diameter of internal seat.

3. Radius and distance of radius center of external seat from shank shoulder.

4. Diameter of shank shoulder.

5. Diamter of hole in nut.

6. Small and large diameters of shank.

7. Diameter of hole through shank.

## 2. OPTIONAL FEATURES

1. MATERIAL.—Strength equal to or greater than that of freeturning high brass.

2. Diameter of hole through nipple.

3. Form of end of shank, except seating section as covered in  $C_{i}$ figures 31 and 32.

4. Length of shank.

5. Type and number of serrations on shank.

6. A second shoulder equal to the large diameter of the largest shank to extend through the hole in the nut for appearance, to be used or omitted for smaller diameter shanks.

7. Length and location of hexagon section on nut.

## 3. GAGES

Dimensions and designs of gages for maintaining the hose connection standards for welding and cutting torches are recommended as follows:

Note.-In connection with screw-thread gages see also section III, division 5. Gage no.

1. "Go" and "not go" gage for depth of threaded recess and shank bore:

A size hose connection, as shown in figure 33.

B size hose connection, as shown in figure 38.
2. "Go" adjustable thread-ring gage for right-hand nipple thread: A size, <sup>3</sup>/<sub>2</sub>-24NF-3: Minor diameter, maximum, 0.3299; minimum, 0.3294 inch.

Pitch diameter, maximum, 0.3477; minimum, 0.3474 inch. B size, %16-18NF-3:

Minor diameter, maximum, 0.5024; minimum, 0.5019 inch.

Pitch diameter, maximum, 0.5262; minimum, 0.5259 inch. 3. "Go" adjustable thread-ring gage for left-hand nipple thread:

A size, <sup>%</sup>-24NF-3LH:

Minor diameter, maximum, 0.3299; minimum, 0.3294 inch. Pitch diameter, maximum, 0.3477; minimum, 0.3474 inch. B size, %16-18NF-3LH:

Minor diameter, maximum, 0.5024; minimum, 0.5019 inch. Pitch diameter, maximum 0.5262; minimum, 0.5259 inch.

4. "Not go" adjustable thread-ring gage for right-hand nipple thread: A size, <sup>3</sup>/<sub>8</sub>-24NF-3:

Minor diameter, maximum, 0.3304; minimum, 0.3299 inch. Pitch diameter, maximum, 0.3458; minimum, 0.3455 inch. B size, %16-18NF-3:

Minor diameter, maximum, 0.5029; minimum, 0.5024 inch. Pitch diameter, maximum, 0.5237; minimum, 0.5234 inch.



FIGURE 31.—"A" size of standard hose connections for welding and cutting torches.



FIGURE 32.—"B" size of standard hose connections for welding and cutting torches.



FIGURE 33.—"Go" and "not go" gage for depth of threaded recess, and shank bore, A size.



FIGURE 34.—Taper gage for nipple seat, A size.



FIGURE 35.—"Go" ring gage for diameter of shank shoulder and concentricity of servated portion, A size.



FIGURE 36.-Master template for nose of shank, A size.



FIGURE 37.—Template gage for nose of shank, A size.



FIGURE 38.—"Go" and "not go" gage for depth of threaded recess, and shank bore, B size.

Gage no. 5. "Not go" adjustable thread-ring gage for left-hand nipple thread-A size, 3/8-24NF-3LH: Minor diameter, maximum, 0.3304; minimum, 0.3299 inch. Pitch diameter, maximum, 0.3458; minimum, 0.3299 lifeh. B size, %s-18NF-3LH: Minor diameter, maximum, 0.5029; minimum, 0.5024 inch. Pitch diameter, maximum, 0.5237; minimum, 0.5234 inch. 6. "Go" and "not go" double-end threaded setting-plug gage for nos. 2 and 4: A size, %-24NF-3: "Go" end: Major diameter, maximum, 0.3750; minimum, 0.3740 inch. Pitch diameter, maximum, 0.3477; minimum, 0.3474 inch. "Not go" end: Major diameter, maximum, 0.3689; minimum, 0.3684 inch. Pitch diameter, maximum, 0.3458; minimum, 0.3455 inch. B size, %16-18NF-3: "Go" end: Major diameter, maximum, 0.5625; minimum, 0.5620 inch. Pitch diameter, maximum, 0.5262; minimum, 0.5259 inch. "Not go" end: Major diameter, maximum, 0.5548; minimum, 0.5543 inch. Pitch diameter, maximum, 0.5237; minimum, 0.5234 inch. 7. "Go" and "not go" double-end threaded setting-plug gage for nos. 3 and 5: A size, 3%-24NF-3LH: "Go" end: Major diameter, maximum, 0.3750; minimum, 0.3745 inch. Pitch diameter, maximum, 0.3477; minimum, 0.3474 inch. "Not go" end: Major diameter, maximum, 0.3689; minimum, 0.3684 inch. Pitch diameter, maximum, 0.3458; minimum, 0.3455 inch. B size, %16-18NF-3LH: "Go" end: Major diameter, maximum, 0.5625; minimum, 0.5620 inch. Pitch diameter, maximum, 0.5262; minimum, 0.5259 inch. "Not go" end: Major diameter, maximum, 0.5548; minimum, 0.5543 inch. Pitch diameter, maximum, 0.5237; minimum, 0.5234 inch. 8. "Go" and "not go" double-end thread plug gage for right-hand nut thread: A size, %-24NF-3: "Go" end: Major diameter, maximum, 0.3755; minimum, 0.3750 inch. Pitch diameter, maximum, 0.3484; minimum, 0.3481 inch. Gaging notch, 0.125 inch from back. "Not go" end: Major diameter, maximum, 0.3665; minimum, 0.3660 inch. Pitch diameter, maximum, 0.3503; minimum, 0.3500 inch. B size, %16-18NF-3: "Go" end: Major diameter, maximum, 0.5630; minimum, 0.5625 inch. Pitch diameter, maximum, 0.5269; minimum, 0.5266 inch. Gaging notch, 0.125 inch from back. "Not go" end: Major diameter, maximum, 0.5510; minimum, 0.5505 inch. Pitch diameter, maximum, 0.5294; minimum, 0.5291 inch. 9. "Go" and "not go" double-end thread plug gage for left-hand nut thread: A size, 3%-24NF-3LH: "Go" end: Major diameter, maximum, 0.3755; minimum, 0.3750 inch. Pitch diameter, maximum, 0.3784; minimum, 0.3481 inch. Gaging notch, 0.125 inch from back. "Not go" end: Major diameter, maximum, 0.3665; minimum, 0.3660 inch. Pitch diameter, maximum, 0.3503; minimum, 0.3500 inch.



FIGURE 39.—Taper gage for nipple seat, B size.



FIGURE 40.—"Go" ring gage for diameter of shank shoulder and concentricity of servated portion, B size.



FIGURE 41.-Master template for nose of shank, B size.



FIGURE 42.—Template gage for nose of shank, B size.

Gage no.

9. "Go" and "not go" double-end thread plug gage for left-hand nut thread-Continued. B size, %16-18NF-3LH: "Go" end: Major diameter, maximum, 0.5630; minimum, 0.5625 inch. Pitch diameter, maximum, 0.5269; minimum, 0.5266 inch. Gaging notch, 0.125 inch from back. "Not go" end: Major diameter, maximum, 0.5510; minimum, 0.5505 inch. Pitch diameter, maximum, 0.5294; minimum, 0.5291 inch. 10. Taper gage for nipple seat: A size, as shown in figure 34. B size, as shown in figure 39. 11. "Go" ring gage for diameter of shank shoulder and concentricity of serrated portion: A size, as shown in figure 35. B size, as shown in figure 40. 12. "Not go" snap gage for shank shoulder diameter: A size, maximum, 0.3241; minimum, 0.3240 inch.
B size, maximum, 0.4961; minimum, 0.4960 inch.
13. "Go" and "not go" snap gage for diameter of ¾-inch shank: B size: "Go" end, maximum, 0.4298; minimum, 0.4297 inch. 0.4251; minimum, 0.4250 in "Not go" end, maximum, 0.4251; minimum, 0.4250 inch. 14. "Go" and "not go" snap gage for diameter of 5/16-inch shank: B size: "Go" end, maximum, 0.3748; minimum, 0.3747 inch. "Not go" end, maximum, 0.3701; minimum, 0.3700 inch. 15. "Go" and "not go" snap gage for diameter of ¼-inch shank: B size: "Go" end, maximum, 0.3118; minimum, 0.3117 inch. "Not go" end, maximum, 0.3071; minimum, 0.3070 inch. 16. "Go" and "not go" snap gage for diameter of 3/16-inch shank: A size: "Go" end, maximum, 0.2478; minimum, 0.2477 inch. "Not go" end, maximum, 0.2431; minimum, 0.2430 inch. B size: "Go" end, maximum, 0.2498; minimum, 0.2497 inch. "Not go" end, maximum, 0.2451; minimum, 0.2450 inch. 17. "Go" and "not go" snap gage for diameter of <sup>1</sup>/<sub>8</sub>-inch shank: A and B sizes: "Go" end, maximum, 0.1868; minimum, 0.1867 inch. "Not go" end, maximum, 0.1821; minimum, 0.1820 inch. 18. Master template for nose of shank: A size, as shown in figure 36. B size, as shown in figure 41. 19. Template gage for nose of shank: A size, as shown in figure 37. B size, as shown in figure 42. Section IX C. American National Rolled Threads for Screw Shells of Electric Sockets and Lamp Bases

The specifications given herein for American National rolled threads for screw shells of electric sockets and lamp bases, with the exception of the recently adopted intermediate size, were published in Bulletin No. 1474 of the American Society of Mechanical Engineers entitled "Rolled Threads for Screw Shells of Electric Sockets and Lamp Bases", which was a report of the A.S.M.E. Committee on Standardization of Special Threads for Fixtures and Fittings.

## 1. FORM OF THREAD

The thread form is composed of two circular segments tangent to each other and of equal radii, as shown in figure 43.

# 2. THREAD SERIES

The sizes for which standard dimensions and tolerances have been adopted are designated as follows: "Miniature, candelabra, intermediate, medium, and mogul".

The threads per inch, radii of thread form, and diameter limits for these sizes of lamp base screw shells, which are used on lamp bases, fuse plugs, attachment plugs, and similar devices, are given in table 58.



FIGURE 43.—Illustration of allowance and tolerances, American National rolled threads for screw shells of electric sockets and lamp bases.

The corresponding dimensions and limits for socket screw shells, which are used in electric sockets, receptacles, and similar devices, are given in table 59.

	Threads per inch	Pitch	Depth of thread	Radius	Major diameter		Minor diameter	
Size					Maxi- mum	Mini- mum	Maxi- mum	Mini- mum
1	2	3	4	5	6	7	8	9
Miniature Candelabra Intermediate Medium Mogul	14 10 9 7 4	Inch 0.07143 .10000 .11111 .14286 .25000	Inch 0. 020 . 025 . 027 . 033 . 050	Inch 0. 0210 . 0312 . 0353 . 0470 . 0906	Inches 0.375 .465 .651 1.037 1.555	Inches 0.370 .460 .645 1.031 1.545	Inches 0.335 .415 .597 .971 1.455	Inches 0. 330 . 410 . 591 . 965 1. 445

TABLE 59.—American National rolled threads for socket screw shells

	Threads per inch	Pitch	Depth of thread	Radius	Major diameter		Minor diameter	
Size					Maxi- mum	Mini- mum	Maxi- mum	Mini• mum
1	2	3	4	5	6	7	8	9
Miniature Candelabra Intermediate Medium Mogul	14 10 9 7 4	Inch 0.07143 .10000 .11111 .14286 .25000	Inch 0.020 .025 .027 .033 .050	Inch 0.0210 .0312 .0353 .0470 .0006	Inches 0.3835 .476 .664 1.053 1.577	Inches 0. 3775 . 470 . 657 1. 045 1. 565	Inches 0.3435 .426 .610 .987 1.477	Inches 0. 3375 . 420 . 603 . 979 1. 465

## 3. GAGES

Gages are necessary to control dimensions in manufacture and to insure interchangeability and proper assembly. (a) GAGING OF LAMP BASE SCREW SHELLS—(1) Working gages.—

(a) GAGING OF LAMP BASE SCREW SHELLS—(1) Working gages.— For each size of lamp base screw shell there should be provided for control in manufacture, a "go" and a "not go" threaded ring gages to govern the minor diameter and thread form, and "go" and "not go" plain ring gages to govern major diameter.

(2) Inspection gages.—For purposes of inspection in the final acceptance of the product, a "go" threaded ring gage governing minor diameter and thread form, and a "not go" plain ring gage governing major diameter are sufficient.

(b) GAGING OF SOCKET SCREW SHELLS—(1) Working gages.—For each size of socket screw shell there should be provided, for control in manufacture, a "go" and a "not go" thread plug gages to govern the major diameter and thread form, and "go" and "not go" plain plug gages to govern minor diameter.

(2) Inspection gages.—For the final acceptance of the product, a "go" threaded plug gage governing the major diameter and thread form, and a "not go" plain plug governing minor diameter are sufficient.

(c) TOLERANCES ON GAGES.—Manufacturing tolerances on inspection or working gages should not exceed 10 percent of the tolerance on the product, and should be applied in such direction that the limiting dimensions of the screw shells which they are intended to gage are never exceeded.

Radii at the crest of the thread on gages should not exceed values given in column 5, tables 58 and 59, and should not be more than 10 percent less than these radii; also, radii at the root of the thread on gages should not be less than the values given in column 5 nor more than 10 percent greater. . .

# APPENDIX 1. DERIVATION OF TOLERANCES

#### 1. PITCH DIAMETER TOLERANCES

(a) TOLERANCES FOR FASTENING SCREWS.—The tolerances for fastening screws specified in section III were arrived at by combining two factors, known as the net pitch diameter tolerance and the gage tolerance. The theoretical net tolerances for all screws and nuts of a given class of fit bear a definite mathematical relationship to each other, and it was intended that these should in no way be reduced by permissible manufacturing tolerances for master gages; that is, gages within class X tolerances. Consequently the net tolerances were increased by the equivalent diametrical space required to provide for the class X tolerances. Concequently the new force of the class X tolerances on diameter, lead, and angle, to produce the extreme tolerances specified for the product. In practice, the actual net tolerances will depend upon the method of gaging and upon the accuracy of the gages used. 1. Basis of net tolerances.—The net pitch diameter tolerances for the various

classes of fit are based on the following series for a pitch of  $\frac{1}{20}$  inch:

	Inch
Class 1, loose fit	0.0045
Class 2, free fit	. 0030
Class 3, medium fit	. 0020
Class 4, close fit	. 0010

Pitch diameter tolerances for pitches finer than  $\frac{1}{20}$  inch are to each other and to the tolerance for  $\frac{1}{20}$  inch as the 0.6th power of their respective pitches. Pitch diameter tolerances for pitches coarser than  $\frac{1}{20}$  inch are to each other and to the tolerance for  $\frac{1}{20}$  inch as the 0.9th power of their respective pitches.

The exponent 0.6 was chosen for pitches finer than 1/20 inch because the result-

ing tolerances, except in two instances, do not vary more than 0.0001 inch from the pitch diameter tolerances specified in the A.S.M.E. Machine Screw Standard.

2. Gage tolerance.—The gage tolerance to be added to the net tolerance to obtain the extreme tolerance, which determines the absolute limits within which all variations of the work must be kept, is determined as follows: Add together the following:

Pitch diameter tolerance of "go" gage. Diametrical equivalent of lead tolerance of "go" gage. Diametrical equivalent of angle tolerance of "go" gage. Pitch diameter tolerance of "not go" gage.

Then subtract the following from the above sum:

One half diametrical equivalent of lead tolerance of "not go" gage.

Diametrical equivalent of angle tolerance of "not go" gage.

(b) TOLERANCES FOR SCREW THREADS OF SPECIAL DIAMETERS, PITCHES, AND LENGTHS OF ENGAGEMENT.—As stated in section V, the pitch diameter tolerances for special sizes of threads of American National form as given in tables 36, 37, 38, and 39 were obtained by adding three values, or increments, one dependent upon the basic major diameter, another upon the length of en-gagement, and the third upon the pitch, except that pitch diameter tolerances listed in section III were inserted in the tables in the positions correspond-ing to standard sizes, pitches, and lengths of engagement of the American National coarse and fine thread series, and values above and to the left of these inserted values were reduced where necessary so that none should account the section that the section the section the section the tables in the postion of the American National coarse and fine thread series, and values above and to the left of these inserted values were reduced where necessary so that none should exceed these standard values. Likewise values below and to the right of these inserted values were increased where necessary so that none should be less than these standard values. The formulas from which the increments are derived are given in table 60.

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Class of fit	Diameter increment	Length of engagement increment	Pitch in- crement
1	2	3	4
Class 1, loose fit Class 2, free fit Class 3, medium fit Class 4, close fit	$\begin{array}{c} 0.\ 002\sqrt{D}\\ .\ 002\sqrt{D}\\ .\ 002\sqrt{D}\\ .\ 001\sqrt{D}\end{array}$	0.002Q .002Q .002Q .001Q	$\begin{array}{c} 0.\ 020 \ \sqrt{p} \\ .\ 010 \ \sqrt{p} \\ .\ 005 \ \sqrt{p} \\ .\ 0025 \ \sqrt{p} \end{array}$

#### TABLE 60.—Schedule of tolerance increments for special threads

#### 2. RELATION OF LEAD AND ANGLE ERRORS TO PITCH DIAMETER TOLERANCES

It has been stated in various sections of the report that the tolerances specified for pitch diameter include all errors of pitch diameter, lead, and angle. Also, there were tabulated the errors in lead and angle, each of which could be compensated for by one half of the specified pitch diameter tolerances. These equivalents were derived from definite mathematical relations, which are given below. A rigorous mathematical analysis upon which these formulas are based is presented in appendix 3 of Letter Circular No. 23, issued by the Bureau of Standards.

(a) DIAMETER EQUIVALENT OF LEAD ERROR.—The formula expressing the relation between lead error between any two threads within the length of engagement and its diameter equivalent is as follows:

$$E' = (\pm p') \cot a$$

in which

E' = pitch diameter increment due to lead error

p' =the maximum lead error between any two of the threads engaged

a =half angle of thread

The quantity E' is always added to the measured pitch diameter in the case of an external thread, and it is always subtracted in the case of an internal thread, regardless of the sign introduced by the lead error p'.

For threads of American National form, the above formula reduces to—

$$E' = 1.7321 p'$$

(b) DIAMETER EQUIVALENT OF ANGLE ERROR.—The general formula express-ing the relation between error in the half angle of thread and its diameter equiva-lent—that is, the amount of the pitch diameter tolerance absorbed by such an error-is:

$$\cot a' = \frac{h}{E'' \sin a \cos a} \pm \cot a$$

in which

E'' =pitch diameter increment due to error in half angle

h = basic thread depth

a = basic half angle of thread

a' = error in half angle of thread

In solving for E'' the average value of a' for the two sides of the thread, regardless of their signs, should be taken. The sign of  $\cot a$  is plus when the half angle of the thread d' for the two sides d' for the two sides of the thread d' for the two sides of thread is less than basic, and minus when the half angle is greater than basic. By omitting  $\pm \cot a$  from the formula an approximate mean value for a' or E'' is obtained which differs very little from either extreme value. The Commission has, therefore, adopted for general use the formula:

$$\cot a' = \frac{h}{E'' \sin a \cos a}$$

 $\cot a' = \frac{3p}{2E''}$  $E'' = 1.5 \ p \ \tan a'$ 

or

For the form of thread recommended for pipe-thread gages the formula becomes-

$$\cot a' = \frac{1.53812p}{E''}$$
$$E'' = \frac{1.53812}{n} \tan a'$$

or

## APPENDIX 2. WIRE METHODS OF MEASUREMENT OF PITCH DIAMETER

Throughout this report emphasis has been placed on pitch diameter tolerances and limits, as upon these the fit of a screw thread largely depends. The maintenance of these tolerances and limits requires the use of limit thread gages, and these, in turn, depend upon the absolute values or measurements of master gages. The measurement of pitch diameter presents certain difficulties which may result in an uncertainty as to its true value. The adoption of a uniform practice in making such measurement is, therefore, desirable. The so-called "three-wire method" of measuring pitch diameter, as here outlined, has been found to be the most accurate and satisfactory when properly carried out, and is recommended for universal use in the direct measurement of thread-plug gages.

#### 1. SIZE OF WIRES

In the three-wire method of measuring pitch diameter small hardened steel cylinders or wires of correct size are placed in the thread groove, two on one side of the screw and one on the opposite side, as shown in figure 44. The contact face of the micrometer anvil or spindle over the two wires must be sufficiently large in diameter to touch both wires; that is, it must be greater than the pitch of the thread. It is best to select wires of such a size that they touch the sides of the thread at the mid slope, for the reason that the measurement of pitch diameter is least affected by any error in thread angle which may be present when such size is used. The size of wire which touches exactly at the mid slope of a perfect thread of a given pitch is termed the "best-size" wire for that pitch. Any size, however, may be used which will permit the wires to rest on the sides of the thread and also project above the top of the thread. The depth at which a wire of given diameter will rest in a thread groove de-

The depth at which a wire of given diameter will rest in a thread groove depends primarily on the pitch and included angle of the thread; and secondarily, on the angle made by the helix, at the point of contact of the wire and the thread, with a plane perpendicular to the axis of the screw. Inasmuch as variation in the helix angle has a very small effect in determining the diameter of the wire which touches at the mid slope of the thread, and as it is desirable to use one size of wire to measure all threads of a given pitch and included angle, the best size wire is taken as that size which will touch at the mid slope of a groove cut around a cylinder perpendicular to the axis of the cylinder, and of the same angle and depth as the thread of the given pitch. This is equivalent to a thread of zero helix angle. The size of wire touching at the mid slope, or "best-size" wire, is given by the formula:

$$G = \frac{p}{2} \sec a$$

in which

G = diameter of wire p = pitch $a = \frac{1}{2}$  included angle of thread

This formula reduces to-

#### $G=0.57735 \times p$ , for 60° threads

It is frequently desirable, as, for example, when a best-size wire is not available, to measure pitch diameter by means of wires of other than the best size. The minimum size which may be used is limited to that permitting the wire to project above the crest of the thread, and the maximum to that permitting the wire to rest on the sides of the thread just below the crest, and not ride on the creast of the thread. The diameters of the best size, maximum, and minimum wires for American National coarse, fine, hose-coupling, and pipe threads are given in tables 61 and 62.

#### 2. SPECIFICATION FOR WIRES

A suitable specification for wires is as follows:

1. The wires should be cylinders of steel with working surfaces glass hard and accurately finished.

2. The working surface should be about 1 inch in length, and the wire may have a suitable handle which is provided at one end with an eye or other suitable



FIGURE 44.—Three-wire method of measuring pitch diameter of thread plug gages.

means of suspension. One side of the handle, which should be flattened, should be marked with the pitch for which the wire is the best size, and with the diameter of the working part of the wire as determined by measurements under standard conditions as specified below.

3. A suitable container should be provided for each set of wires, and if wires are furnished without handles, the pitch for which the wires are the best size and the diameter of the working part of the wires as determined by measurements under standard conditions as specified below, should be marked on the container.

4. The wire should be round within 0.00002 inch and should be straight to 0.00002 inch over the half-inch interval at the center of its length.

5. One set of wires should consist of three wires which should have the same diameter within 0.00003 inch, and this common diameter should be within 0.0001 inch of that corresponding to the best size for the pitch for which the wire is to be used.

#### 3. METHODS OF MEASURING AND USING WIRES

In order to measure the pitch diameter of a screw-thread gage to an accuracy of 0.0001 inch by means of wires, it is necessary to know the wire diameters to 0.00002 inch. The micrometer to be used for measuring wires should be one which is graduated to ten-thousandths of an inch and upon which hundredthousandths of an inch can be estimated. Such micrometers are available in various forms of precision bench micrometers, and measuring machines. Care should be taken to make sure that the measuring faces of the micrometer are flat and parallel to within 0.00002 inch. The taper of wires can best be determined by measuring between a flat micrometer contact and a cylindrical anvil. Any pits or worn spots on the wires can be detected with the same arrangement. Variations in roundness and straightness are usually determined by rotating the wire between flat contacts one fourth inch in diameter. However, one form of variation in roundness can only be detected by rotating the wire in a V groove against a flat micrometer contact. The V groove may be the thread space in a hardened and well-finished thread plug gage.

The contact pressure used in making measurements is also an important factor, since the wires, when in use, rest on the sides of the thread, and a given pressure exerted on the top of the thread has a magnified effect in distorting the wire and causing the measurement of the pitch diameter to be slightly less than it should be. In making measurements over the wires inserted in the thread groove, it has been common shop practice to hold the wires down into the thread by means of elastic bands. This has a tendency to prevent the wires from adjusting themselves to the proper position in the thread grooves; thus a false measurement is obtained. In some cases it has also been the practice to support the screw being measuring from this surface to the top of a wire placed in a thread over the gage. If the screw is of large diameter, its weight causes a distortion of the wires and an inaccurate reading is obtained. For these reasons these practices should be avoided and subsidiary apparatus for supporting the wires and micrometer should be used.

For consistent results a standard practice as to contact pressure in making wire measurements of hardened screw thread gages is necessary. The computed value for the pitch diameter of a screw thread gage obtained from readings over wires will depend upon the accuracy of the measuring instrument used, the contact pressure, and the value of the diameter of the wires used in the computations. The use of different contact pressures will cause a difference in the readings over the wires, and such errors can only be compensated by the use of a value for the diameter of the wires depending on the contact pressure used. The effect of variation in contact pressure in measuring threads of fine pitches is indicated by the difference in readings obtained with 2 and 5 pounds pressure on a 24-pitch thread plug gage. The reading over the wires with 5 pounds pressure was 0.00013 inch less than with 2 pounds pressure. A wire presses on the sides of a 60° thread with the pressure that is applied to the wire by the measuring instrument. This fact would indicate that the diameter of the wire should be determined by readings made on the wire over

A wire presses on the sides of a  $60^{\circ}$  thread with the pressure that is applied to the wire by the measuring instrument. This fact would indicate that the diameter of the wire should be determined by readings made on the wire over a hardened and lapped cylinder having a radius equal to the radius of curvature of the helical surface of the thread at the point of contact, using the pressure to be used in determining the pitch diameter of the gage. However, it is not practical to employ such a variety of cylinders as would be required, and it is recommended for standard practice that wires be measured between a flat contact and a 0.750-inch hardened and accurately ground and lapped steel cylinder with the pressure used in measuring the pitch diameter of the gage. Furthermore, to avoid a permanent deformation of the material of the wires and gages it is necessary to limit the contact pressure. For pitches finer than 20 threads per inch a pressure of 14 to 16 ounces is recommended. For pitches of 20 threads per inch and coarser a pressure of  $2\frac{1}{4}$  to  $2\frac{1}{2}$  pounds is recommended.

Measurements of a thread plug gage made in accordance with these instructions, with wires which conform to the above specifications, should be accurate to 0.0001 inch. If the diameters of the wires are known only to an accuracy of 0.0001 inch, an accuracy better than 0.0003 inch in the measurement of pitch diameter cannot be expected.

#### 4. MEASUREMENT OF PITCH DIAMETER OF AMERICAN NATIONAL STRAIGHT THREADS

The general formula for determining the pitch diameter of any thread whose sides are symmetrical with respect to a line drawn through the vertex and perpendicular to the axis of the thread, in which the very slight effect of helix angle is not taken into account, is:<sup>1</sup>

$$E = M + \frac{\cot a}{2n} - G \ (1 + \operatorname{cosec} a)$$

in which

E = pitch diameter M = measurement over wires a = one half included angle of thread

n = number of threads per inch

G = diameter of wires

This formula differs from those formerly given in engineering handbooks in that the latter, as generally given, yield a result which should check with the major diameter of the screw measured, while the pitch diameter itself is not mentioned. For a 60° thread of correct angle and thread form this formula simplifies to—

$$E = M + \frac{0.86603}{n} - 3G$$

For a given set of best-size wires

$$E = M - X$$

when

$$X = G (1 + \operatorname{cosec} a) - \frac{\cot a}{2n}$$

The quantity X is a constant for a given thread angle, and, when the wires are used for measuring threads of the pitch and angle for which they are the best size, the pitch diameter is obtained by the simple operation of subtracting this constant or factor from the measurement taken over the wires. In fact, when best-size wires are used, this factor is changed very little by a moderate variation or error in the angle of the thread. Consequently, the factors for the various sets of wires in use may be tabulated, thus saving a considerable amount of time in the inspection of gages. However, when wires of other than the best size are used, this factor changes quite appreciably with a variation in the angle of the thread.

It has been shown that, with the exception of coarse pitch screws, variation in angle from the basic value causes no appreciable change in the quantity X for the best-size wires. On the other hand, when a wire near the maximum or minimum allowable size is used, a considerable change occurs, and the values of the cotangent and cosecant of the actual measured half angle are to be used. It is apparent, therefore, that there is a great advantage in using wires very closely approximating the best size. For convenience in carrying out computations, the values of cot a

 $\frac{\cot a}{2n}$  for standard pitches are given in table 61.

<sup>1</sup> The general formula, in which the helix angle is taken into account, is:

$$E = M + \frac{\cot a}{2n} - G(1 + \csc a + \frac{S^2}{2} \cos a \cot a)$$

in which S=tangent of the helix angle.

The value of S, the tangent of the helix angle, is given by the formula

 $S = \frac{L}{3.1416E} = \frac{1}{3.1416 NE}$ 

in which

L = leadN = number of turns per inch

E=nominal pitch diameter

In commercial practice the term  $\left(\frac{G S^2}{2} \cos a \cot a\right)$  is neglected, as its value is small, being in all cases less than 0.00015 inch for standard factoring straws when the best size wire is used and the above formula takes

than 0.00015 inch for standard fastening screws when the best-size wire is used, and the above formula takes the simplified form given above. The practice is permissible provided that it is uniformly followed, and in order to maintain uniformity of practice, and thus avoid confusion, the Bureau of Standards uses the latter  $\langle G S^2 \rangle$ 

formula except when the value of the term  $\left(\frac{G S^2}{2} \cos a \cot a\right)$  exceeds 0.00015 inch, as in the case of Acme

and multiple threads, or other threads having exceptionally large helix angles. For 60° threads this corresponds to NE  $\sqrt{n=17.1}$ .

#### 5. MEASUREMENT OF PITCH DIAMETER OF AMERICAN NATIONAL TAPER THREADS

The pitch diameter of a taper thread plug gage is measured in much the same manner as that of a straight thread gage, except that a definite position at which the measurement is to be made must be located. A point at a known distance L from the end of the gage is located by means of a combination of precision gage blocks and the cone point furnished as an accessory with these blocks, as



FIGURE 45.—Measurement of pitch diameter of taper thread gages by the 3-wire method.

shown in figure 45 at A. The gage is set vertically on a surface plate, the cone point is placed with its axis horizontal at the desired height, and the plug is turned until the point fits accurately into the thread. The position of this point is marked by placing a bit of prussian blue or wax immediately above it. Measurement is made over the wires in the usual manner, but care must be taken that the contact surfaces of the micrometer make contact with all three wires, since the micrometer is not perpendicular to the axis of the screw when there is proper contact. (See fig. 45.) On account of this inclination, the measurement over the wires must be multiplied by the secant of the half angle of the taper of the thread. The formula for the pitch diameter of any taper thread plug gage, the



FIGURE 46.—Measurement of pitch diameter of taper thread gages by the 2-wire method.
threads of which are symmetrical with respect to a line perpendicular to the axis, then has the form:<sup>3</sup>

$$E = M \sec y + \frac{\cot a}{2n} - G \ (1 + \operatorname{cosec} a)$$

in which

E = pitch diameter M = measurement over wires y = half angle of taper of thread n = number of threads per inch = 1/p a = half angle of threadG = diameter of wires

Thus the nitch diameter of an American Na

Thus the pitch diameter of an American National standard pipe-thread gage having correct angle ( $60^{\circ}$ ) and taper ( $\frac{3}{4}$  inch per foot) is then given by the formula:

#### E=1.00049 M+0.86603 p-3G

The pitch diameter at any other point along the thread, as at the gaging notch, is obtained by multiplying the distance parallel to the axis of the thread, between this point and the point at which the measurement was taken, by the taper per inch, then adding the product to or subtracting it from the measured pitch diameter according to the direction in which the second point is located with respect to the first.

In recent years measuring machines have replaced micrometer calipers generally for the measurement of taper thread plug gages, and the following method, illustrated in figure 46, is applied: This method has a theoretical advantage over the first method in that it is independent of the taper of the thread, and, therefore, requires less computation; or if the taper is not measured, but assumed to be correct, it is more accurate. The axis of the gage and the line of measurement are constrained perpendicular to each other. This is easily done on a measuring machine if the gage is supported on centers mounted on a slide whose ways are perpendicular to the line of measurement. If a micrometer caliper is used, its spindle is constrained perpendicular to the axis of the screw. One method is to place the gage on a surface plate with its axis vertical, and support the micrometer in a horizontal position with its anvil and spindle resting on two equal combinations of gage blocks as shown in figure 46 at A. A single wire is inserted in the thread at the point located as in the previous method, and one other wire is placed in the upper thread on the opposite side. A measurement is taken over the two wires; the second wire is then moved to the thread immediately below and a second reading is taken. The mean of these two readings is substituted in any of the above formulas in the place of M sec y, or 1.00049 M.

#### 6. MEASUREMENT OF PITCH DIAMETER OF THREAD RING GAGES

The application of direct methods of measurement to determine the pitch diameter of thread ring gages presents serious difficulties, particularly in securing proper contact pressure when a high degree of precision is required. The usual practice is to fit the ring gage to a master setting plug. When the thread ring gage is of correct lead, angle, and thread form, within close limits, this method is quite satisfactory and represents standard American practice. It is the only method available for small sizes of threads. For the larger sizes, various more or less satisfactory methods have been devised, but none of these have found wide application.

<sup>2</sup> See footnotes 18 and 1, pp. 100, 132. In the above formula for the value of *E*, the term  $\frac{\cot a}{2n}$  is an approxi-

mation for the value of H. The exact value of H is used when the value of the term  $\frac{\tan^2 y \tan a}{2n}$  exceeds

0.00004 inch, which ordinarily occurs only on special taper threads of coarse pitch or steep taper. Also the multiplication of the measurement over the wires by the secant of the half angle of the taper of the thread is not an exact correction for the inclination of the measurement. The complete formula is—

$$\mathbf{E} = (M-G) \sec y + \frac{\cot a - \tan^2 y \tan a}{2n} - \mathbf{G} \ (\operatorname{cosec} a + \frac{S^2}{2} \ \cos a \ \cot a)$$

This formula gives a value of E which is 0.000081 inch smaller than that given by the simplified formula for the  $2\frac{1}{2}$ -inch-8 American National taper pipe thread, the worst case in this thread series.

#### NATIONAL SCREW THREAD COMMISSION

	the second s					
	Wire sizes 1		Threads	Pitch	$\frac{\text{Pitch}}{2}$	Depth of V thread
Best 0.577350p	Maximum 1.010363p	Minimum 0.505182p	n	$p = \frac{1}{n}$	$\frac{p}{2} = \frac{1}{2n}$	$\frac{\cot 30^{\circ}}{2n}$
1	2	3,	4	5	6	7
Inch 0.00722 .00802 .00902 .01031 .01203	Inch 0. 01263 . 01403 . 01579 . 01804 . 02105	Inch 0.00631 .00702 .00789 .00902 .01052	80 72 64 56 48	Inch 0.01250 .01389 .01562 .01786 .02083	Inch 0. 00625 . 00694 . 00781 . 00893 . 01042	0. 01083 . 01203 . 01353 . 01546 . 01804
.01312	. 02296	. 01148	44	. 02273	.01136	. 01968
.01443	. 02526	. 01263	40	. 02500	.01250	. 02165
.01604	. 02807	. 01403	36	. 02778	.01389	. 02406
.01804	. 03157	. 01579	32	. 03125	.01562	. 02706
.02062	. 03608	. 01804	28	. 03571	.01786	. 03093
. 02138	. 03742	. 01871	27	. 03704	. 01852	. 03208
. 02406	. 04210	. 02105	24	. 04167	. 02083	. 03608
. 02887	. 05052	. 02526	20	. 05000	. 02500	. 04330
. 03208	. 05613	. 02807	18	. 05556	. 02778	. 04811
. 03608	. 06315	. 03157	16	. 06250	. 03125	. 05413
.04124	. 07217	. 03608	14	. 07143	. 03571	.06186
.04441	. 07772	. 03886	13	. 07692	. 03846	.06662
.04811	. 08420	. 04210	12	. 08333	. 04167	.07217
.05020	. 08786	. 04393	11½	. 08696	. 04348	.07531
.05249	. 09185	. 04593	11	. 09091	. 04545	.07873
.05773	. 10104	. 05052	10	. 10000	. 05000	.08660
.06415	. 11226	. 05613	9	. 11111	. 05556	.09623
.07217	. 12630	. 06315	8	. 12500	. 06250	.10825
.07698	. 13472	. 06736	7½	. 13333	. 06667	.11547
.08248	. 14434	. 07217	7	. 14286	. 07143	.12372
. 09623	. 16839	. 08420	6	. 16667	. 08333	.14434
. 11547	. 20207	. 10104	5	. 20000	. 10000	.17321
. 12830	. 22453	. 11226	4½	. 22222	. 11111	.19245
. 14434	. 25259	. 12630	4	. 25000	. 12500	.21651

TABLE 61.—Wire sizes and c	constants, America	n National coarse,	fine, hose-coupling,
	and pipe threa	ds	

<sup>1</sup> These wire sizes are based on zero helix angle. Also maximum and minimum sizes are based on a width of flat at the crest equal to  $\frac{1}{8} \times p$ . The width of flat of American National pipe thread gages is slightly less than this, so that the minimum size listed is slightly too small for such gages. In any lease the use of wires of either extreme size is to be avoided.

TABLE 62.—Relation of best wire diameters and pitches 1—wires for American National coarse, fine, hose-coupling, and pipe threads

7         6         5         4142           1         1         1         1         1           1         1         1         1         1           1         1         1         1         1           1         1         1         1         1           1         1         1         1         1           1         1         1         1         1           1         1         1         1         1           1         1         1         1         1           1         1         1         1         1           1         1         1         1         1           1         1         1         1         1           1         1         1         1         1           1         1         1         1         1           1         1         1         1         1           1         1         1         1         1           1         1         1         1         1           1         1         1         1         1	×⊗×       ⊗××       ⊗××       ×⊗×       ×⊗×       ×⊗×       ×⊗×       ×⊗×       ×⊗×       ×⊗×       ×⊗×       ×⊗×       ×⊗×       ×⊗×       ×⊗×       ×⊗×
	Image: Second state         Image: Second state
9	Image: Second
	×8     ×××       ×8×     ×××       ×8×     ×××       ×8×     ×××       ×8××     ×××
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2 X 8×××× × I I I I I I I I I I I I I I I I	
5 X0XX XX	
8 9 9 7 7 7 9 9 9 9 9 9 9 9 9 9 9 9 9 9	
est wire sizes (in 10022 10002	72113 77213 17698 18248 18248 1847 14131 1417 1700 14131 1700 1700 1700 1700 1700 1700 1700 1

ses (X) indicate those wire diameters which can be used for each pitch. An encircled cross (3) indicates the "best wire" diameter for that pitch which heads the column.

#### WIRE METHODS OF MEASUREMENT

#### 7. WIRE METHODS OF MEASUREMENT OF THREAD THICKNESS OF ACME THREADED PLUG GAGES

For threads having a thread angle less than 45° the quality of fit can be more accurately controlled by checking the element of thread thickness, in relation to the basic major diameter (that is, the thread thickness at the nominal pitch diameter), than by checking pitch diameter. For this purpose the 3-wire method may be applied in the same manner as for measuring pitch diameter, but the method of computation is slightly different. On account of the small thread angle, the cotangent of which is large, it is always necessary to take the helix angle into account in measuring thread thickness by the 3-wire method. The general formula to be applied in determining thread thickness is as follows:

$$t = p - \tan a \left[ D - 2B - M + G(1 + \operatorname{cosec} a + \frac{S^2}{2} \cos a \cot a) \right]$$

in which

D =basic major diameter of screw M =measurement over wires G = diameter of wiresa =half angle of thread S =tangent of helix angle at pitch line p = pitchB = depth at which thread thickness is measuredt =thread thickness at depth B

On Acme screw threads

$$B = p/4$$

and the thread angle being 29°, the above formula reduces to-

 $t = 1.12931p + 0.25862(M - D) - G(1.29152 + 0.48407S^2)$ 

The same formula applies to taps for Acme threads, although the major diameter

is larger than basic, since the formula is based on the basic major diameter. The diameters of the best size, maximum, and minimum wires for standard pitches of Acme threads are listed in table 63. Also, for convenience in carrying out computations, the values of 1.12931p and of  $1.29152+0.48407S^2$  for various diameters and pitches of single, double, triple, and quadruple threads are given in tables 64, 65, 66, and 67.

TABLE 63.—Wire sizes and constants, American National Acme threads  $(29^{\circ})$ 

	Pitch		Wire sizes	1
Threads per inch	$p = \frac{1}{n}$	Best 0.516450p	Maximum, 0.650013p	Minimum, 0.487263p
1	2	3	4	5
1 1 1 1 2 2 2 2 2 3 	Inch 1.00000 .75000 .66667 .50000 .40000 .33333 .25000 .20000 .16667	Inch 0.51645 .38734 .34430 .25822 .20658 .17215 .12911 .10329 .08608	<i>Inch</i> 0. 65001 . 48751 . 4334 . 32501 . 26001 . 21667 . 16250 . 13000 . 10834	Inch 0.48726 .36545 .32484 .24363 .19491 .16242 .12182 .09745 .08121
8 10 12 14 16	. 12500 . 10000 . 08333 . 07143 . 06250	. 06456 . 05164 . 04304 . 03689 . 03228	. 08125 . 06500 . 05417 . 04643 . 04063	. 06091 . 04873 . 04061 . 03480 . 03045

<sup>1</sup> Based on zero helix angle.

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					Thre	ads per	inch, n	=1/p				
~	12	10	8	6	5	4	3	21⁄2	2	11/2	113	1
Basic major diameter (inches)						1.12	931 <i>p</i>					
(inches)	0. 09411	0. 11293	0. 14116	0. 18822	0.22586	0. 28233	0. 37644	0.45172	0.56465	0. 75287	0.84698	1. 12931
					1.5	291518+	0.484074	S2				
1/					1						1	
5/16												
3/8	1. 29458	1 20479										
/18	314	394	1.29552									
9/ 4	277	339	458									
5/8	252	300	394									
11/16	233	272	348	1 90459								
13/16	209	236	288	408								
7/8	201	224	268	369	1. 29478							
15/16	194	214	252	339	432							
1	189	206	239	314 277	394	1. 29458						
11/4	175	186	206	252	300	394						
13%	171	180	196	233	272	348						
11/2	168	175	189 183	220	252	314	1. 29458					
13/4	163	169	179	201	224	268	369	1. 29478				
17⁄8	162	167	175	194	214	252	339	431				
2	161	165	172	189	206	239	314	394				
21/8	150	163	168	184	200	228	294	364	1. 29458			
238	158	161	166	178	190	212	264	318	423			
2½	157	160	165	175	186	206	252	300	394			
25/8	157	159	163	173	183	201	242	285	369			
27/8	156	158	161	169	177	190	235	261	330			
3	156	157	161	168	175	189	220	252	314	1. 29458		
35/8	155	107	100	107	173	180	214	244	300	431		
3%	155	157	159	165	172	183	209 205	236	288	408		
31/2	155	156	158	163	169	179	201	224	268	369	1. 29434	
3%	154	156 155	158	163 162	168	177	197	219	259	353	413	
37.6	154	155	157	161	166	174	191	210	245	326	377	
4	154	155	157	161	165	172	189	206	239	314	362	
41/8	154	155	156	160	164	171	187	203	233	303	348	
43/8	154	155	150	159	163	169	184	197	228	294	324	
432	154	154	156	159	162	168	181	194	220	277	314	1. 29458
458	153	154	155	158	161	167	179	192	216	270	305	440
4%4476	153	154	155 155	158	161	166	178	190	212 209	264	296	423
5	153	154	155	157	160	165	175	186	206	252	281	394
534	153	154	155	157	159	163	173	183	201	242	268	369
534	153	153	154	156	159	162	171	180	196	233	257	348
6	153	153	154	156	157	161	168	175	189	220	239	314
6¼	153	153	154	155	157	160	167	173	186	214	232	300
61/2	153	153	154	155	157	159	165	172	183	209	225	288
0%4	153	153	154	155	156	159	164	169	181	205	220	268
7¼	152	153	153	154	156	158	163	168	177	197	210	259
7 /2	152	153	153	154	155	157	162	167	175	194	206	252
8	152	153	153	154	155	157	161	166	174	191	203	245
8¼	152	153	153	154	155	156	160	164	171	187	199	233
81/2	152	152	153	154	155	156	160	163	170	184	194	228
074	152	152	153	154	154	156	159	163	169	183	191	224
91/4	152	152	153	154	154	156	159	162	168	181	189	220
912	152	152	153	153	154	155	158	161	166	178	185	212
9%	152 1, 29152	1. 29152	153 1.29153	153	154 1 29154	155 1.29155	158 1.29157	160 1 29160	1 29165	1 29175	183	209
					-1 =0101						-1 20102	

# TABLE 64.—Values of 1.12931p and 1.29152+0.48407S<sup>2</sup> for various diameters and pitches, Acme threads SINGLE THREADS

### TABLE 65.—Values of 1.12931p and 1.29152+0.48407S<sup>2</sup> for various diameters and pitches, Acme threads

DOUBLE THREADS

					Thre	ads per	inch, n	=1/p				
	12	10	8	6	5	4	3	21⁄2	2	1½	11/3	1
Basic major diameter						1.12	931 <b>p</b>					
(inches)	0. 09411	0.11293	0.14116	0. 18822	0. 22586	0. 28233	0.37644	0.45172	0. 56465	0. 75287	0. 84698	1. 12931
					1.5	291518+	0.484074	.S²				
1/	1 39901	1 34056	1 37871									
74 5/16	1.31009 1.30378	1. 31999	1. 34056	1 35559								
78	1. 30021	1.30458 1.30121	1.31332 1.30753	1. 33496	1.36041 1.34056	1 37871						
9/16	654	1. 29899	1. 30378	1. 31525	1. 32820	1. 35558						
58 11/16	552 478	745 635	1.30121 1.29937	1.31009 1.30645	1.31999 1.31425	1.34056 1.33027	1. 37188					
<sup>34</sup> <sup>13</sup> / <sub>16</sub>	423 \$81	552 489	800 697	1.30378 1.30177	1.31009 1.30698	1.32291 1.31746	1.35558 1.34378	1.37519				
78	348 322	440 401	616 552	1.30021 1.29899	$1.30458 \\ 1.30271$	$1.31332 \\ 1.31009$	$1.33496 \\ 1.32820$	$1.36041 \\ 1.34923$				
1	300 268	369 322	501 423	800 654	1.30121 1.29899	1.30753 1.30378	1.32291 1.31525	$1.34056 \\ 1.32820$	1.37871 1.35558			
114	245	288	369	552	745	1.30121	1. 31009	1.31999	1.34056	1.07100		
198	228	204 245 221	330 300	478	552	1. 29937	1. 30045	1. 31425	1. 33027	1. 37188	1. 37871	
198	198	231 220 211	259	348	489	616	1. 30021	1.30098 1.30458 1.20271	1.31740 1.31332 1.21000	1. 34378	1. 34989	
2	192	203	245	322	369	501	1. 29899	1. 30271	1. 30753	1. 32291	1. 33331	1. 3787 1
21/8 21/4	183 180	197 192	224 216	283 268	343 322	458 423	720 654	1. 29999 899	$1.30547 \\ 1.30378$	$1.31868 \\ 1.31525$	1.32755 1.32291	1.36581 1.35558
238 216	177 174	188 184	209 203	$256 \\ 245$	303 288	394 369	599 552	815 745	$1.30238 \\ 1.30121$	1.31244 1.31009	1.31911 1.31596	1.34732
258	172	181 179	198 194	236 228	275 264	348 330	513 478	686 635	1.30021 1.29937	1.30812 1.30645	1.31332 1.31108	1.33496
278	169 167	176	191 187	222 216	254 245	314 300	449	590 552	864 800	1.30502	1.30917 1.30753	1. 32630
318	166	173	184	211	238	288	401	519	745	1. 30271	1. 30611	1. 31999
3¼ 3¾	$165 \\ 164$	171 170	182 180	206 202	231 225	277 268	381 364	489 463	697 654	1.30177 1.30094	1.30487 1.30378	1.31746 1.31525
3½ 358	163	168	178	198 195	220	259	348	440	582	1. 30021	1. 30282	1. 31332
394	162	165	174	192	211 207	245	322	401 384	525	899	1. 30121	1. 31009
4	160 160	164     164	172 170	187 185	203 200	234 228	300 291	369 356	501 478	800 758	1. 29992 937	1.30753
414	159 159	163 162	169 168	183 181	197 195	224 220	283 275	343 332	458 440	720 686	887 842	1. 30547 1. 30458
412	159	162	167	180	192	216	268	322	423	654	800	1. 30378
<b>4</b> 34 474	158	161	166	170	188	209	256	303	394	599	728	1. 30238
± /8 5	157	160	164	174	184	203	245	288	369	552	668	1. 30121
5}4 5}2	157 156	159 158	163     162	172 170	181 179	198 194	236 228	275 264	348 330	513 478	616 572	$\begin{array}{c} 1.\ 30021\\ 1.\ 29937 \end{array}$
5¾ 6	156 156	158 157	$161 \\ 160$	169 167	176 174	191	222	254 245	314 300	449	534	864
614	155 155	157 157	160 159	166 165	173	184	211 206	238	288	401	472	697
6¾7	155 155	156 156	159 158	164 163	170 168	180 178	202 198	225 220	268 259	364 348	423 403	654 616
714	154 154	156 155	158 157	162 162	167 166	176 174	195 192	215 211	252 245	334 322	385 369	582 552
7¾	154	155	157	161	165	173	190	207	239	310	355	525
ð 81⁄4 91/	154	155	156	160	104 164 162	172	187	203	234 228 224	291 282	330	478
834	154	155	156	159	163	169	185	197	224	283	309	440
9 9¼	153 153	154 154	156 155	159 158	162 161	167 167	180 178	192 190	216 212	268 261	300 292	423 408
9 <u>1</u> 6 9 <u>3</u> 4	153 153	154 154	155 155	158 158	161 160	166 165	177	188 186	209 206	256 250	284 277	394
10	1. 29153	1. 29154	1. 29155	1. 29157	1.29160	1. 29164	1. 29174	1. 29184	1.29203	1. 29245	1. 29271	1. 29369

#### WIRE METHODS OF MEASUREMENT

### TABLE 66.—Values of 1.12931p and 1.29152+0.48407S<sup>2</sup> for various diameters and pitches, Acme threads

TRIPLE THREADS

					Thre	ads per	inch, n	=1/p				
	12	10	8	6	5	4	3	21/2	2	11/2	11/3	1
diameter						1.12	931 <i>p</i>					
(110100)	0. 09411	0. 11293	0. 14116	0. 18822	0.22586	0. 28233	0.37644	0. 45172	0. 56465	0. 75287	0.84698	1. 12931
					1.2	291518+	0.484074	1.52				
14	1.36215	1. 40187	1. 48771									
5/16	1. 33331	1.35558	1.40187									
3/8 7/1 c	1.31911 1.31108	1.33331	1.36215 1.34057	1.43565 1.38927	1 44653							
/16 1⁄2	1. 30611	1. 31332	1. 32755	1.36215	1. 40187	1. 48771						
9/16	1.30282	1.30832	1. 31911	1.34492	1.37406	1. 43566						
5⁄8	1. 30053	1.30487	1.31332	1.33331	1.35558	1.40187	1 47000					
3/	1. 29887 763	1.30238	1.30918 1.30611	1.32511 1.31911	1.34267 1.33331	1.37871 1.36215	1. 47233					
13/16	668	1. 29911	1. 30378	1.31458	1.32630	1.34989	1. 40911	1.47978				
7/8	593	800	1. 30197	1.31108	1.32092	1. 34057	1. 38927	1.44653				
15/16	534	712	1.30053 1.20027	1.30832	1.31669	1.33331 1 22755	1.37406 1.26215	1.42137	1 49771			
148	400	534	1. 29937 763	1. 30282	1. 30832	1. 31911	1. 34492	1. 37406	1. 43566			
1¼	362	458	641	1. 30053	1.30487	1.31332	1.33331	1.35558	1.40187			
13%	324	403	552	1. 29887	1.30238	1.30918	1.32511	1.34267	1.37871	1.47233		
11/2	296 274	362	486 434	763	1.30053 1.29911	1.30611 1.30378	1.31911 1.31458	1.33331 1.32630	1.36215 1.34989	1,43565 1 40911	1,48771	
134	257	305	394	593	800	1. 30197	1. 31108	1.32092	1. 34057	1. 38927	1. 42285	
178	243	284	362	534	712	1.30053	1.30832	1.31669	1.33331	1.37406	1. 40188	
2	232	268	336	486	641 592	1. 29937	1.30611	1.31332	1.32755	1. 36215	1.38555	1. 48771
21/4	215	243	296	413	534	763	1. 30282	1. 30832	1. 31911	1. 34492	1. 36214	1. 43566
238	208	233	281	385	493	697	1.30158	1. 30645	1.31596	1. 33858	1.35359	1.41708
2/2	203	225	208	302	408	041	1. 30053	1. 30487	1. 31334	1. 33331	1. 34050	1.40187
2% 23/4	198	218	207	342	429	552	1. 29903 887	1. 30355	1. 31108	1. 32887	1. 34050	1. 38927
27/8	190	207	239	309	381	517	820	1.30139	1.30753	1.32189	1.33125	1.36977
3 316	187	203 199	232 225	296 284	362 345	486 458	763	1,30053 1,29977	1.30611 1 30487	1.31911 1.31669	1.32755 1.32435	1.36215 1.35558
314	182	105	220	274	330	434	668	911	1 30378	1 31458	1 32156	1 34080
33/8	179	192	215	265	316	413	628	852	1. 30282	1. 31272	1. 31911	1. 34493
31/2	177	189	210	257	305	394	593	800	1.30197	1.31108	1.31694	1. 34056
3%	170	180	200	250	294 284	362	534	712	1. 30121	1.30962 1.30832	1. 31302	1. 33672
378	173	182	199	237	276	348	508	675	1. 29992	1. 30716	1.31179	1.33027
4	171	180	196	232	268	336	486	641	937	1.30611	1.31041	1.32755
4/8 414	170	178	194	227	261 254	324	465	610 582	887	1.30516 1.30431	1.30917	1.32511 1.32901
43/8	168	175	189	218	248	305	429	557	800	1. 30353	1. 30704	1. 32091
4½	167	174	187	215	243	296	413	534	763	1. 30282	1.30611	1.31911
45/8	166	173	185	211	238	288	399	513	738	1.30217	1.30526	1. 31746
47/8	165	171	182	208	233	274	373	455	668	1. 30103	1. 30378	1. 31395
5	164	170	180	203	225	268	362	458	641	1.30053	1. 30313	1. 31332
51/4	163	168	177	198	218	257	342	429	593	1. 29963	1.30197	1.31108
534	162	167	175	194	212 207	247	324	403	552	887	1.30097	1.30918
6	160	164	171	187	203	232	296	362	486	763	1. 29937	1.30611
61/4	160	163	170	184	199	225	284	345	458	712	871	1.30487
6½ 634	159	162 162	168 167	182	195 102	220	274	330	434	668	814	1.30378
7	158	161	166	177	189	210	257	305	394	593	717	1. 30197
714	158	160	165	176	186	206	250	294	377	562	677	1.30121
73/	157	150	169	179	104	100	410 007	204	940	500	600	1. 20003
8	157	159	163	173	182	199	232	268	348	486	579	937
81/4	156	158	162	170	178	194	227	261	324	465	552	887
834	156 156	158	162	169	177	191	222 218	254	314 305	446	528 506	842
9	156	157	160	167	174	187	215	243	296	413	486	763
914	155	157	160	166	173	185	211	238	288	399	467	728
91/2	155	157	160 159	166	172	183	208	233	281 274	385	450	697
10	1. 29155	1. 29156	1. 29159	1. 29164	1. 29170	1. 29180	1. 29202	1. 29225	1. 29268	1. 29362	1. 29420	1. 29641
			1									1

## TABLE 67.—Values of 1.12931p and 1.29152+0.48407S<sup>2</sup> for various diameters and pilches, Acme threads

QUADRUPLE THREADS

	1				Thre	ads per	inch, n	=1/p				
	12	10	8	6	5	4	3	21⁄2	2	11/2	133	1
Basic major diameter						1.12	931 <i>p</i>					·
(inches)	0. 09411	0. 11293	0.14116	0. 18822	0. 22586	0. 28233	0. 37644	0.45172	0. 56465	0. 75287	0.84698	1. 12931
		1	,		1.5	291518+	0.484074	S2	1	·	!	
14	1 41705	48771	1 64030		1							
5/16	1. 36582	1.40540	1. 48771	1 54776								
7°	1. 32630	1. 34378	1. 37871	1. 46530	1. 56710	1 64020						
916	1, 31161	1. 32139	1. 34056	1. 38646	1. 43827	1. 54776						
5%8	1.30753	1. 31525	1, 33027 1, 32291	1.36581 1.35124	1.40540 1.38246	1.48771 1.44653	1. 61295					
<sup>3</sup> ⁄ <sub>4</sub> <sup>13</sup> ⁄ <sub>16</sub>	1. 30238	1.30753	1.31746 1.31332	1.34056 1.33252	1.36581 1.35335	1.41708 1.39529	1.54777 1.50057	1.62621				
76	1. 29937	1. 30305	1.31009	1. 32630	1. 34378	1.37871	1. 46531	1.56710 1.52237				
1	745	1. 30021	1. 30547	1. 31746	1. 33027	1. 35558	1. 41708	1. 48771	1.64030			
11/4	525	697	1. 30238	1. 31161	1. 31525	1. 34050	1. 36581	1. 40540	1. 48771			
13%	458 408	599 525	1. 29864 745	1.30458 1.30238	1.31083 1.30753	1.32291 1.31746	1.35124 1.34056	1.38246 1.36581	1. 44653 1. 41708	1. 61295 1. 54776	1. 64030	
156 134	369	468	654 582	1.30069 1.29937	1.30502 1.30305	1.31332 1.31009	1.33252 1.32630	1.35335 1.34378	1.39529 1.37871	1.50056 1.46530	1.57403 1.52499	
2	314	387	525	831	1.30148	1.30753	1.32140	1.33627	1.36581	1. 43827	1,48771	1 64030
21/8	277	334	440	675	1. 29917	1. 30378	1. 31425	1. 32540	1. 34732	1. 40017	1. 43566	1. 58870
23/8	252	297	381	567	758	1. 30121	1.30940 1.30753	1. 31806	1. 33496	1. 37519	1. 40187	1. 51473
25%	233	270	339	489	644	1. 29937	1. 30595	1. 31287	1. 32630	1. 35793	1. 37871	1. 46530
234 27/8	226 220	259 250	322 307	458 431	599 559	864 800	1.30458 1.30341	1.31083 1.30907	1.32291 1.31999	1.35124 1.34551	1.36977 1.36215	1.44653 1.43064
3	214 209	242 235	294 283	408 387	525 495	745 697	1.30238 1.30148	1.30753 1.30619	$1.31746 \\ 1.31525$	1.34056 1.33627	1.35558 1.34989	1. 41708 1. 40540
31/4	205	228	272	369	468	654	1.30069 1.20099	1.30502 1.30397	1.31332	1.33252	1.34493 1.34056	1.39529 1.38647
31/2	197	218	256	339	423	582 552	937 881	1.30305 1.30222	1.31009 1.30874	1. 32630	1. 33672	1.37871 1.37188
334	191	209	242	314	387	525	831	1. 30148	1.30753	1. 32139	1. 33027	1.36581
4	189	205 202	236 231	303 294	372 358	501 478	786 745	1.30081 1.30021	1.30645 1.30547	1.31932 1.31746	1.32755 1.32511	1.36041 1.35558
4/8	184	199 196	226 222	285 277	346	458 440	708 675	1. 29967 917	1.30458 1.30378	$1.31578 \\ 1.31426$	1.32291 1.32091	1.35124 1.34732
4%	181	194	218	270 264	324	423	644 616	872	1. 30305	1. 31287	1.31911	1. 34377
45% 434	178	189	211 208	257	305 297	394 381	591 567	793 758	1.30177 1.30121	1.31045	1.31595 1.31458	1.33764 1.33495
47/8	175	186 184	205 202	247 242	289 283	369 358	545 525	726 697	1.30069 1.30021	1.30843 1.30753	1.31331 1.31215	1.33251 1.33027
514	172	181	197	233	270	339	489	644	1. 29937	1. 30595	1. 31009	1. 32630
534	169	178	193	226	259	322	408	599	804	1.30458 1.30340	1.30832 1.30680	1. 32291
6 <sup>1</sup> /4	166	174	187	214 209	242 235	294 283	408	525 495	697	1.30238 1.30148	1.30547 1.30431	1.31740 1.31525
6½ 6¾	165 164	171 169	181 179	205 201	228 223	272 263	369 353	468 444	654 616	1.30069 1.29999	1.30329 1.30238	$1.31332 \\ 1.31161$
7734	163 162	168 167	177 175	197 194	218 213	256 248	339 326	423 404	582 552	937 881	1.30157 1.30086	$1.31009 \\ 1.30874$
7½	162	166	174	191	209	242	314	387	525	831	1. 30021	1.30753
8 814	160	164	173	189	205	230	294	358	478	745	911	1. 30547
8½ 8¾	159	163	169	184	199	220	200	334 204	408	675	803	1. 30378
9	159	162	168	181	194	218	270	324 314	423	616	745	1. 30305
9¼ 9½	158 158	161 161	166 166	178 176	189 187	211 208	257 252	305 297	394 381	591 567	712 682	1.30177 1.30121
934 10	158 1. 29157	160 1.29160	165 1. 29164	$175 \\ 1.29174$	$186 \\ 1.29184$	205 1. 29202	$247 \\ 1.29242$	289 1. 29283	369 1. 29358	545 1. 29525	654 1. 29629	$\begin{array}{c} 1,30069\\ 1,30021 \end{array}$
					1				1			

#### APPENDIX 3. CONTROL OF ACCURACY OF THREAD ELE-MENTS IN THE PRODUCTION OF THREADED PRODUCT

#### 1. INTRODUCTION

In order to maintain the dimensions of threaded product within the limiting sizes specified, it is essential that the tools used and the processes applied be suitable for the particular requirements. An analysis of the various factors controlling the accuracy of the individual thread elements is here presented. In this analysis, the fundamental factors controlling the accuracy of the elements of a screw thread are stated, and are followed by a brief discussion of the relationship of these factors to each of the prevailing commercial methods of producing screw threads. It is recognized, however, that certain varying factors are involved, such as lubrication, method of holding the work or tool, sharpness of cutting edges, etc., so that it is not always possible to predetermine the exact sizes of the tools required to accomplish the desired results.

Screw threads are usually produced either by cutting or rolling. Five general methods of cutting, two of rolling, and two of finishing screw threads are in common use.

Screws or external threads are commonly produced by lathe tools, solid or adjustable dies, adjustable or opening die heads with removable chasers, thread milling cutters, threading hobs, and roller dies.

Of these, the dies, die-head chasers, and hobs are all multiple toothed, cutting in several thread spaces simultaneously, and finishing the operation at one pass. Lathe tools are ordinarily single-pointed and operate in a single thread, which is finished by repeated passes; but multiple-pointed chasers for use as lathe tools are sometimes made.

All rolled threads and many cut threads are produced with dies, chasers, or hobs made with master tools, such as hobs, taps, or milling cutters. These master tools are frequently made with forming cutters or other tools, but the primary tool is always made with a single-point tool. Angle and pitch errors tend to accumulate in a series of master tools and must be carefully considered in the design and use of this single-point tool.

Internal threads or tapped holes are commonly produced by means of taps and sometimes by lathe tools. Much progress has been made in the standardization of the dimensions and tolerances for cut and ground thread taps.<sup>3</sup>

#### 2. FUNDAMENTAL FACTORS

The accuracy of the individual elements of a thread is controlled mainly as follows:

Angle by the angle between, and contour of the cutting edges of the tool used for cutting, or of the sides of the grooves of the die used for rolling.

Lead by the rate of the longitudinal motion of the tool with respect to the rate of revolution of the part to be threaded. Major diameter of external thread by the outside diameter of the stock, or by

the forming tool.

Minor diameter of internal thread by the diameter of the hole in the work before threading. In the case of a drilled hole, this depends on the diameter and accuracy of grinding of the tap drill used.

Pitch diameter by the radial setting of the forming surface of the tool.

Thread form by the form and position of the tool, and the conditions under which it is used.

(a) CONTROL OF TOOTH OUTLINES.—Inspection of the angle and profile of the thread-forming tool is essential to control the accuracy of the thread produced. All threading tools, whether for use in a lathe, die head, thread miller, or roller, and whether single or multiple pointed, must produce the proper tooth profile on an axial section of the work. The final test of accuracy in any threading tool is its ability to produce a thread of the proper axial section as defined in the body of this report.

Most cutting tools for standard threads have their cutting edges in the axial plane of the work, so that the shape of those edges tends to reproduce itself on the screw thread. In forming and inspecting the cutting edges of these tools, their forms may be directly compared with standard outlines. This can be done by means of accurately formed templets, carefully applied under the microscope. A more satisfactory and practical way is to draw the desired outline on a chart

\* See Report No. B5e-1930, "Taps: Cut and Ground Threads" of the American Standards Association.

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to a magnification of 50 or 150 times, and then project on this chart the image of the cutting tool under inspection magnified to the corresponding degree. By this means the tool shape may be quickly compared with the standard shape to a degree of accuracy much greater than that required for commercial work. Care must be taken to use a lens system free from distortion. Optical projection machines and comparators are available for this work in commercial designs. (See "Thread comparators." p. 151.)

In table 68 are given useful data for drawing the charts for any standard pitch.

 TABLE 68.—Dimensions for determining shape of cutter, chaser, hob, or tap teeth

 American National coarse, fine, and hose coupling threads

Threads per inch, n	Pitch,	<u>}</u> ∕2×p	3⁄8×p	½4×p	Depth of thread, h	½×h	}⁄3×h	R=%×h	<del>}</del> 6×h	⅓18×h	One half pitch diam- eter toler- ance for class 2 fit, $\frac{1}{2} \times T$	$h+\frac{1}{2} \times T$
1	2	3	4	5	6	7	8	9	10	11	12	13
30 72 64 56 48	Inch 0.01250 .01389 .01562 .01786 .02083	Inch 0.00625 .00694 .00781 .00893 .01042	Inch 0. 00156 . 00174 . 00195 . 00223 . 00260	Inch 0.00052 .00058 .00065 .00074 .00087	Inch 0.00812 .00902 .01015 .01160 .01353	Inch 0.00406 .00451 .00507 .00580 .00677	Inch 0.00271 .00301 .00338 .00387 .00451	Inch 0.00180 .00200 .00226 .00258 .00301	Inch 0. 00135 . 00150 . 00169 . 00193 . 00226	Inch 0. 00045 . 00050 . 00056 . 00064 . 00075	Inch 0. 00085 . 00090 . 00095 . 00100 . 00110	Inch 0.00897 .00992 .01110 .01260 .01463
44 40 36 32 28	.02273 .02500 .02778 .03125 .03571	.01136 .01250 .01389 .01562 .01786	. 00284 . 00312 . 00347 . 00391 . 00446	. 00095 . 00104 . 00116 . 00130 . 00149	. 01476 . 01624 . 01804 . 02030 . 02320	.00738 .00812 .00902 .01015 .01160	. 00492 . 00541 . 00601 . 00677 . 00773	.00328 .00361 .00401 .00451 .00515	. 00246 . 00271 . 00301 . 00338 . 00387	.00082 .00090 .00100 .00113 .00129	.00115 .00120 .00125 .00135 .00155	. 01591 . 01744 . 01929 . 02165 . 02475
24 20 18 16 14	.04167 .05000 .05556 .06250 .07143	. 02083 . 02500 . 02778 . 03125 . 03571	. 00521 . 00625 . 00694 . 00781 . 00893	. 00174 . 00208 . 00231 . 00260 . 00298	.02706 .03248 .03608 .04059 .04639	. 01353 . 01624 . 01804 . 02030 . 02320	.00902 .01083 .01203 .01353 .01546	.00601 .00722 .00802 .00902 .01031	. 00451 . 00541 . 00601 . 00677 . 00773	. 00150 . 00180 . 00200 . 00226 . 00258	$\begin{array}{r} .\ 00165\\ .\ 00180\\ .\ 00205\\ .\ 00225\\ .\ 00245\end{array}$	.02871 .03428 .03813 .04284 .04884
13 12 $11\frac{1}{2}$ 11 10	. 07692 . 08333 . 08696 . 09091 . 10000	.03846 .04167 .04348 .04545 .05000	.00962 .01042 .01087 .01136 .01250	$\begin{array}{r} .\ 00321\\ .\ 00347\\ .\ 00362\\ .\ 00379\\ .\ 00417\end{array}$	.04996 .05413 .05648 .05905 .06495	$\begin{array}{r} . \ 02498 \\ . \ 02706 \\ . \ 02824 \\ . \ 02952 \\ . \ 03248 \end{array}$	$\begin{array}{r} .\ 01665\\ .\ 01804\\ .\ 01883\\ .\ 01968\\ .\ 02165\end{array}$	.01110 .01203 .01255 .01312 .01443	.00833 .00902 .00941 .00984 .01083	. 00278 . 00301 . 00314 . 00328 . 00361	.00260 .00280 1.00425 .00295 .00329	05256 05693 06073 06200 06815
9 8 7 <sup>1</sup> /2 7 6	111111 12500 13333 14286 16667	. 05556 . 06250 . 06667 . 07143 . 08333	.01389 .01562 .01667 .01786 .02083	.00463 .00521 .00556 .00595 .00694	.07217 .08119 .08660 .09279 .10825	.03608 .04059 .04330 .04639 .05413	.02406 .02706 .02887 .03093 .03608	.01604 .01804 .01925 .02062 .02406	.01203 .01353 .01443 .01546 .01804	. 00401 . 00451 . 00481 . 00515 . 00601	.00350 .00380 1.00800 .00425 .00505	.07567 .08499 .09460 .09704 .11330
5 4½ 4	. 20000 . 22222 . 25000	. 10000 . 11111 . 12500	. 02500 . 02778 . 03125	.00833 .00926 .01042	. 12990 . 14434 . 16238	.06495 .07217 .08119	.04330 .04811 .05413	. 02887 . 03208 . 03608	.02165 .02406 .02706	. 00722 . 00802 . 00902	. 00580 . 00635 . 00700	. 13570 . 15069 . 16938

<sup>1</sup> Based on hose-coupling thread tolerances.

(b) CONTROL OF LEAD ERRORS.—The sources of lead errors require special consideration and for this purpose the methods of producing screw threads may be considered under two headings, namely, those in which relative longitudinal motion of the tool and product is controlled by means of a lead screw and those in which the tool is self-leading.

(1) Tool controlled by lead screw.—In cutting a thread on a lathe or other machine embodying a lead screw, using a single point cutting tool or single milling cutter, progressive lead errors are caused by (1) a progressive lead error in the lead screw; (2) lack of parallelism of the motion of the cutting tool, the axis of the lead screw, and the axis of the part to be threaded; and (3) incorrect ratio of the rate of revolution of the spindle to that of the lead screw, due to an incorrect or approximate combination of gears.

Local lead errors are caused by (1) local lead errors in the lead screw; (2) lost motion in the action of the lead screw or connecting mechanism; (3) varying frictional resistance in the mechanism; (4) when a live center is used, irregular play of its spindle in the bearings; and (5) variations in the amount of metal removed by the cutting tool.

Periodic lead errors are caused by (1) periodic lead errors in the lead screw; (2) eccentricity of motion of the lead screw; (3) thrust bearings of spindle or lead screw running out of true; (4) variations in the spacing of gear teeth, or eccentric gears or mountings; (5) when a live center is used, eccentricity of motion of its spindle; and (6) periodic variations in the amount of metal removed, due to lack of uniformity of the material in diameter, straightness, or physical properties.

When a multiple-toothed threading tool is controlled by a lead screw, variations from correct spacing of the teeth of the tool are superimposed on the lead errors resulting from any of the above causes in that portion of the thread not passed over by every tooth of the tool. In the portion of the thread completely passed over by the tool, the effect of the difference in lead between the tool and lead screw is to produce a thin thread.

The simplest method of inspecting a machine tool to determine whether it will cut a screw thread within satisfactory limits is to cut carefully a sample screw on the machine and measure the lead errors of the screw. The obvious remedy for errors from such sources is the careful inspection of the various elements of the machine, and correction of the errors thus located, either by improving the design or by carefully refinishing or remaking the parts to a greater degree of accuracy.

(2) Self-leading threading tool.—When a thread is cut by means of a tap or die, which, as ordinarily used, are self-leading and not controlled by a lead screw, lead errors may occur as the result of (1) incorrect lead of the tap or die; (2) too much or too little relief at the throat of the die or on the chamfer at the end of the tap; (3) the setting of an adjustable die or tap chaser to cut a thread considerably larger or smaller than that for which the tool was intended—that is, to cut a helix angle considerably different from the helix angle of the chaser; (4) excessive resistance to longitudinal motion; (5) improper alinement of the axis of the tap or die with that of the work, etc.; and (6) excessive angle relief. The control of accuracy of the lead of the tap or of the chasers in the die is the

The control of accuracy of the lead of the tap or of the chasers in the die is the most difficult of these sources of error, and indeed presents serious difficulties. There is, first, the difficulty of cutting a tap or chaser which is free from lead errors resulting from any of the causes outlined above; and second, the distortion which the steel composing the tap or die undergoes in hardening.

When especially accurate work is required, as in producing threaded product to class 4, close-fit specifications, it is very desirable, and sometimes necessary, that the feed of the tap or die be controlled by means of a lead screw.

In the inspection of such thread-forming tools practically the same means and methods can be applied as in the measurement of screw-thread gages. For checking the lead, indicating gages or some of the usual lead-measuring devices for screw-thread gages may be used. To measure the lead of a die chaser, the chaser must be held in a fixture in such a position that the direction of measurement corresponds to the direction of longitudinal motion of the chaser threads when cutting a thread.

#### 3. CUTTING OF SCREW THREADS

(a) SINGLE-POINT TOOL.—A screw thread may be produced by traversing a single-point threading tool—shaped to correspond to the shape of the thread space in an axial plane, and so placed as to cut an angle, equal to the angle of the top surface of the tool, in correct relation to the axis of the thread—along the revolving part to be threaded at such a rate as to produce a thread of the desired lead. This is the common method of cutting screws in an engine lathe, a lead screw driven by gearing being the usual means for imparting to the tool the longitudinal motion at the desired rate. This method is used commercially only when special conditions make it necessary, as when the thread to be cut is not standard, or when it is not practicable to apply other methods.

Various forms of single-point cutting tools for cutting threads of American National form are illustrated in figure 47 at A, B, C, and D. The circular tool shown at C has the advantage that it can be reground indefinitely without destroying its correct form. The diagram at D shows the method for calculating the angle X of the cutting tool, having a clearance angle V, in a plane perpendicular to the edge MN; and the formula for determining the clearance angle V, of a tool for cutting a thread of helix angle s, is also given. Such tools usually consist of hardened tool steel, ground to the correct form after hardening; special alloys such as "stellite" are also used for this purpose.

(b) THREAD CHASER.—A screw thread may be produced by successively traversing a multiple-point thread tool, known as a chaser, along the part to be threaded, each tooth following in the thread in the same manner as a single-point thread tool. Two forms of chasers are shown in figure 47 at E and F, the one at F being especially suitable for cutting fine threads. Chasers are well adapted to roughing out threads, as they cut rapidly, and may be used for finishing threads accurately if the teeth are ground after hardening.

(c) TAP OR DIE.—A screw thread may be produced by using a tap for internal threads or a die for external threads. These tools occur in considerable variety in their commercial forms, but consist essentially of a number of multiple-point cutters or chazers, usually four, 'arranged circumferentially. They may be either solid or adjustable, and collapsible or self-opening, respectively, for withdrawing quickly from the work after threading. By their use a thread is generally finished by one passage of the tool, although a second or finishing cut is some-



FIGURE 47.—Single point and multiple point thread cutting tools.

times made to secure greater accuracy. Dies 'are applied, in general, to threading screws, bolts, and studs; and taps to nuts or other internal threads within the usual range of sizes. They are also applied to the threading of pipe and pipe fittings. The rapidity with which threading operations may be performed by the use of taps and dies, within the limits of accuracy suitable for a large percentage of commercial work, makes them most efficient and widely used threading tools. It is only in cutting large sizes or coarse pitches, or where a high degree of accuracy is desired, that their use may be less economical than other means of cutting threads.

Aside from lead errors, which have been previously considered, the accuracy of the thread produced depends on the form of the cutting teeth, character of the cutting edges, clearance or relief for cutting edges, construction of the tool, and the conditions under which it is used.

(d) MILLING CUTTER.—A screw thread may be produced by feeding in to the depth of the thread and then traversing a rapidly revolving single milling cutter

<sup>&</sup>lt;sup>4</sup> Simplified lists of sizes and varieties, for threads of American National form, of die-head chasers for self-opening and adjustable die heads, as adopted at general conferences of representative manufacturers, distributors, and users, are promulgated in United States Department of Commerce Simplified Practice Recommendation R51-29.

along the slower revolving part to be threaded at such a rate as to produce a thread of the desired lead; the profile of the cutting edges of the cutter conforming approximately to the shape of the thread groove in an axial plane, and the axis of the cutter being set at an angle to the axis of the thread, in a plane parallel to the axis of the thread, equal to the mean helix angle of the thread cut. The single-cutter method of thread milling is especially applicable to the cutting of large threads of coarse pitch, multiple threads, and the heavier classes of work. When the amount of metal to be removed is large, as compared with the size of the screw, this method is especially suitable because the torsional strain is much smaller than that produced by a die, and consequently the accuracy of the screw produced is greater.5

(e) THREADING HOB.—A screw thread may be produced by feeding in to the depth of the thread, and then traversing a rapidly revolving multiple milling cutter or thread hob, somewhat longer than the length of the thread to be cutwhich consists of annular rows of teeth, whose centers lie in planes perpendicular to the axis of the cutter (in effect a series of single cutters formed into one solid piece), and the axis of which is parallel to the axis of the thread—along the slowly revolving part to be threaded slightly more than either one or two complete revolutions of the work, at a rate per revolution of the work equal to the pitch The multiple-cutter method of thread milling is used largely for of the thread. cutting comparatively short threads, usually of fine or medium pitches, when smoothness or a considerable degree of accuracy is desired, or when the thread

must maintain a fixed relation with a point or surface on the work. The error introduced in the form of thread produced by cutter teeth having the same form as that of the intended form of thread, as the result of the axes of cutter and thread being parallel, is usually not serious except when the helix angle is large.<sup>6</sup>

#### 4. ROLLING OF SCREW THREADS

The second general process for forming screw threads—namely, that of rolling is a cold-forging process. It may be defined as an impression or displacement method whereby the threads are formed by means of a die or roll having threads or ridges, which are forced into the material to be threaded, and, by displacing it, produce a thread of the required form and pitch. In this process no material is removed, but the metal is displaced from the thread space and forced up on each side above the original surface of the piece to be threaded. Thus, the major diameter of a V-shaped 60° thread so produced is found in practice to be greater than the original diameter of the blank by an amount varying from 65 percent of the single depth of thread for small screws to 85 percent for large screws. An approximate formula, based on geometrical considerations only, for the diameter of a blank to be threaded to American National form is as follows:

$$D_1 = \sqrt{D^2 - 1.3Dp + 0.63p^2}$$

in which

 $D_1 = \text{diameter of blank}$ D = major.diameter of threadp = pitch of thread

In case the thread required must be accurate within close limits, the exact value of  $D_1$  necessary in any given case must be determined experimentally, as its value is affected by the physical properties of the material.<sup>7</sup>

The thread-rolling process is the most rapid and economical method of forming screw threads in quantity production, when the part to be threaded is of such form as to permit its use. It is used only for external threads and is not regarded as being feasible for internal threads, since the area of contact of the roll in an internal thread is relatively much larger than on an external thread, and in order to displace the metal a very heavy pressure is required. It is difficult to support

 <sup>&</sup>lt;sup>3</sup> For refinements in connection with the determination of the profile of cutting edge of a thread milling cutter, see The Milling of Screw Threads and Other Problems in the Theory of Screw Threads, by H. H. Jeffcott. Proceedings of the Institution of Mechanical Engineers, 1922-1, pp. 515-528, and discussion pp. 529-562; or Engineering (London), vol. 113, Apr. 7, 1922, pp. 441-442, and discussion pp. 112-414.
 <sup>6</sup> For formulas which may be applied in such cases to determine and plot the exact contour of the cutting edges to produce, as nearly as possible, the thread form required, see Side-Cutting of Thread Milling Hobs, by Earle Buckingham. Transactions of the American Society of Mechanical Engineers, vol. 42, 1920, pp. 569-593; also the reference cited in footnote 5, for thread milling cutter profile.
 <sup>7</sup> This formula is derived in Size of Stock for Bolts Having Rolled Threads, by F. Webster. American Machinist, vol. 30, Oct. 31, 1907, p. 630.

the work with the necessary rigidity to withstand the heavy pressure, and to provide a bearing for the roll which will withstand the stress.

Screw threads may be rolled by either of two methods, as follows:

(a) THREADING ROLL.—By forcing a cylindrical disk or roll, having a threaded periphery and being free to rotate on the pin or bolt on which it is mounted, against the piece to be threaded while the latter is revolving. The cylindrical roll is used when the work is in an automatic screw machine or turret lathe, and it is impossible to cut the thread required by means of a thread-cutting die, or when an additional operation would be necessary before cutting the thread. The thread on the roll corresponds in pitch, and approximately in form, to the thread to be rolled. The roll may be presented to the work in either a tangential direction as shown at A, figure 48, or radially as shown at B; a satisfactory thread is formed in either case.

(b) THREAD-ROLLING DIES.—By rolling the blank between dies, which may be either flat or cylindrical in form, when performed by machines designed exclusively for this work. When flat dies are used, as shown in figure 48 at C, one die, M, remains stationary and the other die, N, which is parallel or nearly parallel to M, has a reciprocating movement. The faces of the dies have parallel milled or planed grooves of approximately the same form as that of the required thread



FIGURE 48.—Methods of rolling screw threads.

which are set at an angle to the line of motion of the blank equal to the helix angle of the thread to be produced. The angles of the grooves and ridges in a plane perpendicular to the direction of the grooves are given by the formula—

Tan 
$$a_1 = \tan a \cos s$$

in which

 $a_1$ =half angle of ridge of die a =half angle of thread to be rolled s =helix angle of thread

The spacing of the ridges is determined by the formula-

 $p_1 = p \cos s$ 

in which

 $p_1$ =spacing of ridges of die p=pitch of thread to be rolled s=helix angle of thread

The blank is inserted at one end of the stationary die, and rolls between the die faces until it is ejected at the other, the thread being formed in one passage of the blank. When cylindrical dies are used, one of the dies, which is a complete cylinder, revolves continuously in one direction and the other is a stationary cylindrical segment. This method is used extensively for threading almost all forms of small and medium sizes of screws and bolts, when required in sufficiently large quantities to warrant the use of a thread-rolling machine.<sup>8</sup>

#### 5. FINISHING OF SCREW THREADS

On account of the difficulty of producing an accurately finished thread by means of a cutting tool, in ordinary gage-making practice the thread is ground, lapped, or ground and lapped, in order to finish all elements of the thread to correct dimensions. The process of grinding is applied to hardened screws only, and is intended to correct any errors present as the result of distortion in the hardening process, as well as those resulting from the cutting operation. Lapping is usually applied to hardened screw threads, and may be either substituted for grinding, or performed after grinding to remove the marks left by the grinding wheel and to



FIGURE 49.—Thread form of laps for lapping screw threads.

produce a smooth and highly finished surface. These processes are used largely in the production of screw-thread gages.

(a) GRINDING.—The grinding of a thread is similar to the process of milling a thread by the single-cutter method. The profile of the periphery of the grinding wheel is "dressed" by means of a diamond to conform to the shape of the thread groove in an axial plane, with the axis of the wheel set at an angle to the axis of the thread, in a plane parallel to the axis of the thread, equal to the helix angle. In order to produce a thread having straight sides and correct angle, the periphery of the wheel should be dressed to the required angle after the wheel has been set to the helix angle, in the plane containing the axis of the thread and the center of the wheel. The same considerations as to the exact profile of the periphery of the grinding wheel, to produce a thread of exactly correct form, apply as for the tooth profile of a single milling cutter set at the helix angle of the thread. The principal differences between the thread milling and grinding processes are that a large diameter of grinding wheel is desirable, and several light

<sup>&</sup>lt;sup>8</sup> The principles involved in determining the spacing and angle of ridges of flat dies, and position of the dies, are considered in Principles of Thread Rolling and the Setting of Dies, by J. F. Springer, American Machinist, vol. 33, Apr. 21, 1910, pp. 739-741.

cuts are taken, whereas, a small diameter of milling cutter is desirable and a single cut is taken.

(b) LAPPING.—The lapping of a screw thread may be defined as a process of abrasion by successively traversing the thread, as it revolves, with a so-called lap, which consists of an engaging screw thread of softer material, usually fine-grained cast iron, brass, or cold-rolled steel, in which very fine abrasive material is embedded in the thread surface. For removing considerable material, the laps are charged with coarser abrasive, and for imparting fine finish, a finer abrasive; in either case the abrasive used is very fine, and the lap is thoroughly lubricated. A number of laps may be necessary to finish either an internal or external thread to the required form and dimensions, as illustrated in figure 49.

#### 6. GAGING PRACTICES AND TYPES OF GAGES

The production of accurate parts is primarily a matter of constant vigilance and of training of workmen. The smaller the tolerances which are to be maintained, the more complete the inspection or gaging system must be. In order to secure satisfactory results, the manufacturing tools provided must be sufficiently accurate, and the manufacturing methods must be sufficiently reliable, to produce the required results. After tools and methods of proved reliability are provided, it is necessary to watch the wear on the tools or changes in their set-up to insure that the required conditions are maintained. This is accomplished by periodical tests of the tools, by periodical gaging of the product, and sometimes by both.

The most difficult element of a screw thread to gage is the lead. Lead-testing devices for checking tools and gages are available, but, in general, their operation is too slow for use as production inspection equipment. In addition, the lead is the most important element of a screw thread as regards the nature of the contact between the surfaces of the mating parts. Furthermore, the result of an error in lead is almost double that of an equal error in diameter as regards interchangeability. For exacting threaded work, if the method of inspection of the product does not effectively detect lead errors, the tools used must be carefully inspected for lead. In order to reduce the possibilities of disagreement to a minimum, the manufacturer should strive to produce parts well within the specified limits rather than close to the limiting sizes.

(a) THREAD MICROMETERS.—Thread micrometers are sometimes used to measure the pitch diameter of taps and screws. Thread micrometers should be calibrated periodically against a master gage, to avoid errors due to wear on the anvils of the instrument. As thread micrometers give no indication of lead and angle errors, the results of tests made with thread micrometers alone cannot be taken as conclusive, and a "go" gage should always be used as a supplementary test. Thread micrometers are very effective means of checking against the change in set-up due to wear on tools, etc.

(b) THREAD SNAP GAGES.—Thread snap gages are generally adjustable and have contact points consisting of cone-pointed anvils, wedge-shaped prisms with rounded edges, serrated or grooved plates, or grooved or threaded cylinders adjustably mounted and suitably spaced in a U-shaped frame. These gages are used to some extent in gaging external threads and have the advantages that work may be inspected with great rapidity by the single motion of passing it between the anvils of the gage and given a visual examination for clearance as well as a tactile inspection. The positions of the anvils are set to a setting gage, and the anvils are then clamped in position and sealed. Thread snap gages are to be preferred as "not go" gages.

The cone-pointed snap gage usually has a single point on each side of the frame, and is an effective "not go" gage. It does not, however, fully meet the requirements for a "go" gage, as it does not check the lead, and, therefore, must be supplemented with some type of indicating gage to check the lead when used for checking pitch diameter, angle, and thread form. Also, as it checks only a single diameter at a time, the "go" snap gage must be tried at a series of points to determine whether the maximum diameter of an external thread is within the tolerance. When provided with three contact points, two on one side spaced an integral number of threads apart and one on the other, such a gage checks the lead for progressive, but not always for local or periodic lead errors, and, thus, it more nearly fulfills the requirements for a "go" thread gage. This type or other types of short engagement are suitable for product of classes 4 and 5, provided that an independent inspection of the lead is made. Thread snap gages having multiple toothed contact points, that is, toothed blades, serrated or grooved plates, or grooved or threaded cylinders, are made in a variety of forms, either as separate or combined "go" and "not go" gages. The fit of a screw in such a gage is affected by variations in pitch diameter, lead, and angle of the screw, and the gage accordingly may be used as a "go" gage for the less accurate classes of work, such as classes 1 and 2, and, if well designed and accurately made, also for classes 3, 4, and 5.

(c) THREAD RING GAGES.—Thread ring gages are extensively used to inspect the threads on screws. These are usually adjustable to suitable setting gages. When the product is to be within specified limits, "go" and "not go" gages are required. The use of such gages gives some information as to lead and angle errors as well as pitch diameter errors.

(d) THREAD COMPARATORS.—A development in the art of measuring threaded parts is the optical thread comparator, which embodies the principle of gaging in an optical projection system. In addition to giving a rapid indication of whether the elements of the screw thread lie within the limiting dimensions specified, such instruments furnish more detailed information as to the errors in screw threads than is usually obtained by means of mechanical gages, particularly as to irregularities in thread form, lead, and diameter. These instruments can be adapted to measure taps and other threading tools.

The available forms of projection comparators differ somewhat in design and principle, but each consists primarily of a source of parallel light, such as an electric arc or concentrated filament lamp with condensing lens system, a projection lens system, a screen upon which the magnified shadow image of the work is projected, and a device for holding the work in position in front of the projection lenses. The screen consists of a tolerance chart on which two outlines of the correct thread form at the magnification used are spaced one above the other a distance equal to the tolerance multiplied by the magnification. The chart and gage holder are adjusted to position by projecting the shadow image and certain lines of the chart into coincidence, after which the system may be used as a gaging device.

The above types of optical thread comparators are applicable to external threads. Two types of optical thread comparators for internal threads have been developed by the Bureau of Standards, one knownas an "optical coincidence thread gage", and the other as a "stereoscopic thread gage."<sup>9</sup>

(e) INDICATING GAGES.—An indicating thread gage has movable contact points, which are set to a setting gage, and is intended to give an exact indication of the variations of the dimensions of a screw thread within the specified limits, rather than to show merely that the thread is within, or outside of, the specified limits, as is the case with limit gages. In such gages the movable contact points actuate a multiplying lever system, or other means for magnifying their motion, and the amount of the motion is registered on a graduated dial or scale. Indicating gages are made according to a variety of designs, some to indicate progressive lead error only, some to indicate pitch diameter only, some to indicate both separately but on the same gage, others to indicate the major and minor diameters as well, and still others to indicate the apparent size. They have been applied almost exclusively to external threads. Those which indicate the apparent size may be considered as most nearly fulfilling the requirements of a gaging system. However, those indicating lead errors are very useful in controlling lead errors in threading tools and screw-thread products. Also certain types can be used to indicate the variation in roundness on pitch or major diameters.

(f) THREAD PLUG GAGES.—At the present time the most practical means of gaging threaded holes or nuts is by the use of thread plug gages. When the product is to be within specified limits, "go" and "not go" gages are required. The use of such gages gives some information as to lead and angle errors as well as pitch diameter errors. A correct "go" plug gage will reject any parts which fall below the minimum dimensions specified.

One practice of inspecting tapped holes is first to inspect the tap, and then to test the tapped holes periodically with "go" and "not go" gages. The tap can be watched for wear by testing the tapped holes with a "go" thread gage. One widely used practice consists of using a "go" thread plug gage, and a "not go" plain plug gage for the minor diameter.

One practice of inspecting taps is to measure the several elements, such as pitch dia meter, angle, and lead. Another practice consists of tapping a hole with

<sup>&</sup>lt;sup>9</sup> Described in B.S. Jour. Research, vol. 6, pp. 229-237, February 1931.

each tap before it is issued from the tool crib and testing these tapped holes with "go" and "not go" thread plug gages.

Sometimes the tap is tested after it is returned to the tool crib. If it is correct, it is replaced in its proper compartment. If it has worn below the limits, it is discarded and work produced by it is checked and corrected when necessary.

(g) PLAIN GAGES.—"Go" and "not go" plain cylindrical plug gages are used for inspecting the minor diameter of the tapped hole. Plain ring or snap gages are used for inspecting the major diameter of the screw. When used, it is recommended that the "go" inspection gage be a ring gage and the "not go" inspection gage be a snap gage. The working gages may be combined as a "go" and "not go" snap gage. ' (h) GEAR-TOOTH CALIFER FOR THREAD THICKNESS.—A device which is par-

(h) GEAR-TOOTH CALIPER FOR THREAD THICKNESS.—A device which is particularly useful in the measurement of thread thickness of Acme screw threads, or of tools for producing them, is the gear-tooth caliper. With this device the depth at which the measurement is made is controlled by means of a scale and vernier or a micrometer and the thickness is determined by means of another.

(i) TESTING OF GACES.—Gages should be tested periodically for wear and to insure that the gages are properly distributed. When successive inspections in the same plant are involved, it is good practice to inspect all gages of the same nominal size against each other periodically, and to distribute these gages so that the earlier inspections are made with those which are the greatest amount inside of the component limits, while the later inspections are made with those gages closest in size to the component limits.

The original testing of a thread gage should include measurements of diameters, lead, and angle. If these elements test satisfactorily, the later inspection need be only measurements of pitch diameter.<sup>10</sup>

#### APPENDIX 4. CLASS 5, WRENCH FIT FOR THREADED STUDS (TENTATIVE SPECIFICATIONS)

The tentative specifications embodied herein for class 5, wrench fit for threaded studs, are based partly upon experimental data obtained in an investigation conducted by the Bureau of Standards and partly upon data obtained from manufacturers relative to existing practice. The specifications are complete only for studs set in hard materials (cast iron, steel, bronze, etc.), and are not complete for studs set in aluminum for which larger interference of metal is permissible. They are presented for the information of those who may have use for them but are in no way mandatory.

#### 1. FORM OF THREAD

The American National form of thread profile, as specified in section III, shall be used. The thread form of the tapped hole is modified, however, by truncating the crest of the thread a greater amount than that specified for threads of strictly American National form. This truncation is such that the minimum depth of thread engagement is one half of the basic thread depth. The maximum depth of engagement is governed by the tolerances specified for the major diameter of the stud and the minor diameter of the tapped hole.

#### 2. THREAD SERIES

The range of sizes from  $\frac{1}{2}$  inches, inclusive, of the American National coarse-thread series and the American National fine-thread series of sizes and pitches as given in section III, are recommended for general use for class 5, wrench fit for threaded studs.

#### 3. CLASSIFICATION AND TOLERANCES

The accompanying specifications are intended for use in the production and assembly of threaded studs and tapped holes on an interchangeable basis.

#### (a) GENERAL SPECIFICATIONS

The following general specifications apply for all materials to class 5, wrench fit for threaded studs, American National coarse-thread series and American National fine-thread series.

<sup>&</sup>lt;sup>10</sup> Methods of measuring pitch diameter of screw-thread gages are described in appendix 2, p. 129.

1. DEFINITION .- The wrench fit class is intended to cover the manufacture of threaded studs and holes which are to be assembled permanently by the application of power.

2. MINIMUM TAPPED HOLE.—The pitch diameter of the minimum threaded hole corresponds to the basic size, the tolerances being applied above the basic size.

3. MAXIMUM AND MINIMUM STUD ABOVE BASIC.—The pitch diameter of both the maximum and minimum studs of a given size and pitch are above the basic dimensions, which are computed from the basic major diameter of the thread. The maximum major diameter of the stud is basic. 4. LENGTH OF ENGAGEMENT.—A length of engagement equal to one and one

half times the basic major diameter for studs set in hard materials, and two times the basic major diameter for studs set in soft materials, is the basis of the toler-ances and allowances specified herein. The length of engagement of two diameters is especially desirable for studs set in soft materials when subject to alternating stresses or to vibration.

5. MINIMUM INTERFERENCES.—The minimum interferences specified are such that a wrench-tight fit will result in all cases. If the thread surfaces are smooth and thread form is maintained, these interferences will permit disassembly and reassembly of the same stud and hole as many as four times and still produce a satisfactory wrench-tight fit.

6. MAXIMUM INTERFERENCES.—The maximum interferences specified are such that all conditions necessary for a good wrench fit are fulfilled. If threads are well lubricated with a suitable lute no galling or seizing of the threads will result. Also, mild-steel studs, even of the smaller sizes, will not break if the rate of assembly is not excessive.

When a mixture of white lead and oil is used as a lute it is important that it be of a thick fluid consistency in order to prevent galling or seizing, particularly when fine threads in hard materials are concerned, and that it be applied liberally. If a lute consisting of 40 percent zinc dust, which has passed through a 200-mesh sieve, and 60 percent petrolatum is used, the tendency for the threads to gall or seize with maximum interference is materially reduced. 7. TOLERANCES.—(a) The tolerances specified represent the extreme variations

permitted on the product.

(b) The tolerance on the tapped hole is plus, and is applied from the basic size to above basic size.

(c) The tolerance on the screw is minus, and is applied from the maximum

screw size to below the maximum screw size. (d) The pitch diameter tolerances for the tapped hole are the same as for the class 4, close-fit nut, except on the ¼-inch size, as noted in table 69. These tolerances necessitate the use of ground-thread taps.

(e) The pitch diameter tolerances for the stud are as given in tables 69 and 70. They are the maximum variations permissible for each individual size of stud, as determined by the maximum and minimum interferences.

(f) Pitch diameter tolerances include angle variations but do not include lead variations.

(g) The tolerances on the major diameters of class 5, wrench-fit studes are the same as for class 2, free-fit finished screws.

(h) The minimum minor diameter of a stud of a given pitch is such as to result in a basic flat  $(\frac{1}{8} \times p)$  at the root. It is equal to the measured pitch diameter of the stud minus the basic thread depth.

(i) The maximum minor diameter of a screw of a given pitch may be such as results from the use of a worn or rounded threading tool, when the pitch diameter is at its maximum value. In no case, however, should the form of the thread, as results from tool wear, be such as to cause the screw to be rejected on the maximum minor diameter by a "go" ring gage, the minor diameter of which is equal to the minimum minor diameter of the class 2 nut.

(j) The maximum major diameter of the tapped hole of a given pitch is such as to result in a flat equal to one third of the basic flat  $(\frac{1}{24} \times p)$ . When the minimum hole is basic, its maximum major diameter will be above the basic major diameter by the amount of the specified pitch diameter tolerance plus two ninths of the basic thread depth.

(k) The minimum major diameter of a tapped hole is the basic major diameter. In no case, however, should the minimum major diameter of the hole, as results from a worn tap or cutting tool, be such as to cause it to be rejected on the mini-mum major diameter by a "go" plug gage made to the standard form at the crest. (l) The tolerance on the minor diameter of a tapped hole of a given pitch is one sixth of the basic thread depth.

8. ILLUSTRATION.—The relations of the maximum and minimum major, pitch, and minor diameters of stud and tapped hole specified herein are shown in figures 50, 51, and 52.

#### (b) CLASSIFICATION

1. ALLOWANCE AND TOLERANCE VALUES.—Allowances and tolerances are specified in tables 69 and 70, inclusive, for coarse-threaded and fine-threaded



FIGURE 50.—Illustration of tolerances, allowance, and crest clearances for class 5, wrench fit for threaded studs.

studs set in hard materials—namely, cast iron, steel, and bronze. These are based upon data obtained in an experimental investigation and fulfill the conditions outlined in the above specifications.

#### 4. TABLES OF DIMENSIONS

Tables 71 and 72 give recommended thread dimensions of studs and tapped holes which meet the above specifications for coarse-threaded and fine-threaded studs set in hard materials. Also the limiting values of the torques at full engagement (lever-arm times force) which may be expected in the assembly of studs and tapped holes made to these dimensions are given.



FIGURE 51.—Illustration of loosest condition for class 5, wrench fit for threaded studs, one-half inch, 13 threads, set in hard materials.

#### NOTATION

- $\begin{array}{l} D = \text{major diameter.} \\ E = \text{pitch diameter.} \\ K = \text{minor diameter.} \\ h = 0.0500 = \text{basic thread depth.} \end{array}$

,



FIGURE 52.—Illustration of tightest condition for class 5, wrench fit for threaded studs, one-half inch, 13 threads, set in hard materials.

NOTATION

 $\begin{array}{l} D = \text{major diameter,} \\ E = \text{pitch diameter,} \\ K = \text{minor diameter,} \\ h = 0.0500 = \text{basic thread depth.} \end{array}$ 

 
 TABLE 69.—Class 5, wrench fit for threaded studs, allowances and tolerances for studs and tapped holes, coarse threaded studs in hard materials

Sizes	Threads per inch	Interfer pitch di	ence on iameter	Pitch d tolera	iameter nces <sup>1</sup>	Erro c c ha an	orsin onsu alf of neter	half ming pitc toler	angle 3 one h di- ances
		Mini- mum	Maxi- mum	Stud	Tapped hole <sup>2</sup>	St	ud	Tap	ped le
1	2	3	4	5	6		7	8	3
¼ 5/ 6 3& 7/ 6 5/	20 18 16 14 13	Inch 0.0003 .0005 .0005 .0006 .0007	Inch 0.0018 .0040 .0045 .0050 .0055	Inch 0.0007 .0020 .0024 .0026 .0029	Inch 0.0008 .0015 .0016 .0018 .0019	Deg. 0 0 0 0 0	$Min. \\ 16 \\ 41 \\ 44 \\ 42 \\ 44 \\ 44 \\ 44 \\ 44 \\ 44$	Deg. 0 0 0 0 0	$Min. \\ 25 \\ 31 \\ 29 \\ 29 \\ 28 \\ 28$
916 56 34	12 11 10 9	.0008 .0008 .0009 .0010	.0060 .0060 .0065 .0065	.0032 .0031 .0033 .0031	. 0020 . 0021 . 0023 . 0024	0 0 0 0	44 39 38 32	0 0 0 0	28 26 26 25
1 146 144 134 134	8 7 6 6	.0011 .0011 .0012 .0012 .0013	.0065 .0065 .0065 .0065 .0065 .0070	.0027 .0024 .0023 .0017 .0021	.0027 .0030 .0030 .0036 .0036	0 0 0 0	25 19 18 12 14	0 0 0 0	25 24 24 25 25

<sup>1</sup> Inasmuch as a moderate difference in lead between stud and tapped hole (about 0.005 inch per inch) has been shown to improve the quality of a stud fit having minimum pitch diameter interference, no lead tolerance is specified. Therefore, the tolerances specified for pitch diameter include all errors of pitch diameter and angle but not of lead. (See "5. Gages and gaging" herein.) Excessive lead errors, however, should be avoided, as they increase the tendency of the stud to loosen when subjected to load. Columns 7 and 8 give, for information, the errors in angle which can be compensated for by half the tolerances on pitch diameter given in columns 5 and 6.

<sup>4</sup> The tolerances on the tapped hole given in column 6 are the same as those specified for class 4, close-fit screws and nuts, with the exception of the ¼-inch size.

 

 TABLE 70.—Class 5, wrench fit for threaded studs, allowances and tolerances for studs and tapped holes, fine-threaded studs in hard materials

Sizes	Threads per inch	Interfer pitch d	ence on iameter	Pitch d tolera	iameter Inces 1	Erre co ha an	ors in onsul alf of meter	half a n i n g pitcl tolera	angle cone di- ances
		Mini- mum	Maxi- mum	Stud	Tapped hole <sup>2</sup>	St	ud	Tap ho	ped le
1	2	3	4	5	6		7	8	;
у Я а Ха	28 24 24 20 20	Inch 0.0005 .0005 .0006 .0006 .0007	Inch 0.0034 .0037 .0044 .0044 .0050	Inch 0.0018 .0020 .0026 .0025 .0030	Inch 0.0011 .0012 .0012 .0013 .0013	Deg. 0 1 0 1	Min. 58 55 11 57 9	Deg. 0 0 0 0 0	Min. 35 33 33 30 30
916 96 94 76	18 18 16 14	. 0007 . 0008 . 0008 . 0008	.0050 .0055 .0059 .0061	. 0028 . 0032 . 0035 . 0035	.0015 .0015 .0016 .0018	0 1 1 0	$58 \\ 6 \\ 4 \\ 56$	0 0 0 0	31 31 29 29
1	14 12 12 12 12 12	.0009 .0009 .0011 .0011 .0012	.0069 .0067 .0060 .0055 .0050	.0042 .0038 .0029 .0024 .0018	.0018 .0020 .0020 .0020 .0020	1 0 0 0	$7 \\ 52 \\ 40 \\ 33 \\ 25$	0 0 0 0	29 28 28 28 28

<sup>1</sup>Inasmuch as a moderate difference in lead between stud and tapped hole (about 0.005 inch per inch) has been shown to imploye the quality of a stud fit having minimum pitch diameter interference, no lead tolerance is specified. Therefore, the tolerances specified for pitch diameter and angle but not of lead. (See "5. Gages and gaging" herein.) Excessive lead errors, however, should be avoided, as they increase the tendency of the stud to loosen when subjected to load. Columns 7 and 8 give, for information, the errors in angle which can be compensated for by half the tolerances on pitch diameter in columns 5 and 6.

pitch diameter given in columns 5 and 6. <sup>2</sup> The tolerances on the tapped hole given in column 6 are the same as those specified for class 4, close-fit screws and nuts.

				Stud sizes				Tar	ped-hole s	izes		1		A norosin	oto towarro
Sizes	Threads per inch	Major d	liameter	Pitch di	iameter	Minor diameter	Minor d	iameter	Pitch d	iameter	Major diameter	Recomme drill	nded tap size	at full er of $1\frac{1}{2}D$	igagement unique
		Maxi- mum	Mini- mum	Mari- mum	Mini- mum	Maxi- mum 1	Mini- mum	Maxi- mum	Mini- mum	Maxi- mum	Mini- mum <sup>1</sup>	Nominal size	Diam- eter	Maxi- mum	Mini- mum
1	~	e.	4	ъ	9	2	œ	5	10	11	12	13	14	15	16
	20 18 14 13	Inches 0. 2500 . 3125 . 3750 . 4375 . 5000	Inches 0. 2428 . 3043 . 3660 . 4277 . 4277 . 4896	Inches 0. 2163 . 2804 . 3389 . 3389 . 3961	Inches 0. 2186 . 2784 . 3365 . 3935 . 4526	Inches 0. 1904 2483 . 2483 . 3028 . 3549 . 4111	Inches 0.2049 .2622 .3186 .3736 .4313	Inches 0.2103 .2682 .3254 .3313 .4396	Inches 0.2175 .2764 .3344 .3344 .3911 .4500	Inches 0. 2183 . 2779 . 3579 . 3529 . 4519	Inches 0.2500 0.3125 .3750 .4375 .5000	No.4 日 日 万16	Inches 0.2090 2660 .3230 .3770 .4375	Inlbs. 105 265 420 610 850	Inlbs. 355 1200 1200 1800 2655
	9 11 10 10 10	. 5625 . 6250 . 7500 . 8750	. 5513 . 6132 . 7372 . 8610	5144 5720 6915 8093	. 5112 . 5689 . 6882 . 8062	. 4663 . 5195 . 6333 . 7452	. 4882 . 5444 . 6614 . 7768	. 4972 . 5542 . 6722 . 7888	. 5084 . 5660 . 6850 . 8028	. 5104 . 5681 . 6873 . 8052	. 5625 . 6250 . 7500 . 8750	12.5 mm 3564 4364 2552	.4921 .5460 .6719 .7812	$1, 170 \\ 1, 450 \\ 2, 300 \\ 3, 200 \\ 3, 200 \\ 1, 170 \\ 1, 100 \\ 1, 100 \\ 1, 100 \\ 1, 100 \\ 1, 100 \\ 1, 100 \\ 1, 100 \\ 1, 100 \\ 1, 100 \\ 1, 100 \\ 1, 100 \\ 1$	$ \begin{array}{c} 360\\ 450\\ 730\\ 1,080 \end{array} $
	000110	$\begin{array}{c} 1.\ 0000\\ 1.\ 1250\\ 1.\ 2500\\ 1.\ 3750\\ 1.\ 5000 \end{array}$	. 9848 1. 1080 1. 2330 1. 3548 1. 4798	. 9253 1. 0387 1. 1637 1. 2732 1. 3987	.9226 1.0363 1.1614 1.2715 1.2966	.8531 .9562 1.0812 1.1770 1.3025	. 8901 . 9998 1. 1248 1. 2286 1. 3536	. 9036 1. 0152 1. 1402 1. 2466 1. 3716	.9188 1.0322 1.1572 1.2667 1.3917	. 9215 1. 0352 1. 1602 1. 2703 1. 3953	1, 0000 1, 1250 1, 2500 1, 3750 1, 5000	5764 1 1564 1564 12564	. 8906 1. 0000 1. 1250 1. 3594 1. 3594	4, 250 5, 300 6, 950 8, 150 10, 400	1,500 1,875 2,535 2,970 3,900

 $h_{v}$  (or 0.04890) from the minimum major drameter of the tapped hole correspond to the basic flat ( $34\times p_{v}$ ), and the profile at the major drameter produced by a worn tool must not <sup>1</sup> Dimensions for the minimum major drameter of the tapped hole correspond to the basic flat ( $34\times p_{v}$ ), and the profile at the major drameter produced by a worn tool must not fall below the basic outline. The maximum major drameter of the tapped hole corresponding to a flat at the major drameter of the tapped hole equal to  $34\times p_{v}$ , and may be determined by adding  $19\times A$  (or 0.7393) to the maximum pitch drameter of the bandet of the band. <sup>3</sup> Selective assembly in the case of the 34-inch size may be required on account of the small tolerances necessary on pitch drameter. To avoid breaking a mild steal stud, the maximum interference on pitch drameter of 0.0018 inch must not be exceeded.

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#### NATIONAL SCREW THREAD COMMISSION

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Approximate torque at full engagemen of 135D		Mini- mum	16	<i>Inlb</i> . 4 2 2 2 2 8 8 8 8 8 8 8 8 8 3 3 3 3 3 3 3
		Maxi- mum	15	<i>InLbs.</i> 140 140 140 540 540 810 1, 040 1, 430 3, 070 3, 070 5, 980 6, 980 6, 980 10, 070 10, 070
Recommended tap <sup>A</sup>		Diam- eter	14	<i>Inches</i> 0.2188 0.2188 3370 4576 .4576 .51156 .5156 .51156
		Nominal size	13	732 J R R 364 35,64 13/6 13/6
	Major diameter	Mini- mum <sup>3</sup>	12	Inches 0.2500 0.2500 1.3750 1.3750 0.5000 0.5500 0.5500 0.8750 0.8750 1.25000 1.25000 1.25000 1.25000 1.25000 1.25000000000000000000000000000000000000
izes	ameter	Maxi- mum	11	Inches 0.2279 0.2279 0.2279 3396 3406 4063 .4063 .5279 .55229 .5229 .5
Tapped-hole si	Pitch di	Mini- mum	10	Inches 0. 2268 3254 3254 3475 4075 4075 55294 55294 55294 55294 55294 55294 55294 55294 55295 119599 119599 119599 119599 119599 119509 119509 119509 119509 119509 1195000 1195000 1195000 1195000 1195000 1195000 1195000 1195000 1195000 1195000 11950000 1195000 1195000 1195000 11950000000000
	Minor diameter	Maxi- mum	6	Inches 0. 2206 3413 3978 4603 4603 4603 5807 5807 5807 5807 5804 8188 8188 8188 8188 1. 0597 1. 0597 1. 1847 1. 1847 1. 1847 1. 4347
		Mini- mum	80	Inches 0. 2167 0. 2167 3368 3368 4549 4549 65347 55247 55247 55247 55247 55247 56336 56336 56336 1110 5607 111757 111757 112507 110507 110000000000
	Minor diameter	Maxi- mum 1	7	Inches 0. 2096 0. 2096 1. 22650 1. 22650 1. 4436 1. 4436 1. 6792 1. 0295 1. 1538 1. 1538 1. 4028 1. 4028 1. 4028
	Pitch diametor	Mini- mum	9	Inches 0. 2284 0. 2284 1. 33497 1. 33497 1. 4069 1. 4069 1. 65286 1. 65286 1. 6718 1. 6758 1. 9563 1. 1990 1. 3240 1. 4491
Stud sizes		Maxi- mum	5	Inches 0. 2302 0. 2302 3523 4034 4725 5314 55314 55314 55314 55314 55314 55314 15325 100776 11. 2019 1. 2019 1
	iameter	Mini- mum	4	Inches 0. 2438 3659 3659 4928 4928 6543 6168 8652 8652 1. 2388 1. 2488 1. 24888 1. 2488 1. 24888 1. 2488 1. 24888 1. 248888 1. 248888 1. 248888 1. 248888 1. 248888 1. 248888 1. 248888 1. 248888 1. 2488888 1.
	Major d	Maxi- mum	3	Inches 0. 2500 3750 . 3375 . 5000 . 5000 . 7500 . 77500 . 8750 . 8750 . 1. 1250 1. 1250 1. 2500 1. 2500 1. 2500 1. 2500
Threads per inch		5	55555 T 22588 8857 78588	
	Sizes		-	28281 www.g. 5900

#### WRENCH FIT FOR THREADED STUDS

330 460 945 945

 $\begin{array}{c}
410\\
750\\
530\\
215\\
215
\end{array}$ 

bs. 45 70 125 170 260

1

<sup>1</sup> Dimensions given for the maximum minor diameter of the screw are figured to the intersection of the worn tool are with a center line through crest and root. The minimum minor diameter of the screw shall be that corresponding to a flat at the minor diameter of the screw equal to  $\frac{1}{2}$   $\frac$ 

#### 5. GAGES AND GAGING

The fundamentals of this subject, as it relates to screw threads, are laid down in section III. The relatively close limits on pitch diameter specified for class 5, wrench fit for threaded studs, necessitate careful and accurate gaging of both the stud and tapped hole, particularly since the actual measurements obtained depend somewhat upon the methods of gaging used.

both the stud and tapped hole, particularly since the actual measurements obtained depend somewhat upon the methods of gaging used. Considering first the case of minimum interference: The minimum stud and maximum hole are selected by means of "not go" gages. With the usual or recommended forms of "not go" gages, the presence of lead errors does not affect the gaging. It has been shown by the experimental data obtained that this is a desirable condition, as the presence of a slight difference in lead between stud and hole is an advantage, especially with minimum pitch diameter interference. It is important, however, as with the other classes of fit, that the "not go" gage should check the pitch diameter only, for upon this the minimum tightness of a stud fit depends, assuming that the correct thread form and smoothness of thread surface are maintained. In the case of maximum interference the maximum stud and minimum hole

In the case of maximum interference the maximum stud and minimum hole are selected by means of "go" gages, and these may or may not be the usual types of threaded plugs and rings. Plug and ring gages control pitch diameter, lead, thread angle, maximum minor diameter of stud, and minimum major diameter of hole. The minimum minor diameter of the hole being considerably above basic, it is not controlled by the "go" threaded plug gage, and as it has been shown that a certain minimum clearance at minor diameter must be maintained, it is very important that the hole should be gaged further by means of a "go" plain plug gage. Gaging the tapped hole by means of a "not go" plain plug gage is also desirable, but not strictly necessary.

Gaging of the major diameter of the stud thread is not essential; this element may be controlled by the size of stock. Some means of controlling the minimum minor diameter of the stud is, however, very desirable, particularly on studs of the smaller sizes, because the shearing strength of the stud depends upon this element. For this purpose the projection comparator is very useful, but inspection of the cutting tool to assure a width of flat at the root of the thread not less than  $\frac{1}{4} \times p$  is sufficient.

The use of thread micrometers or "go" thread snap gages of short engagement for checking the pitch diameter of the stud is good practice provided that the thread form is ascertained by optical inspection. Gaging for lead errors is not essential provided that the lead of the threading tools is maintained within the usual limits of good commercial practice.

If the tap (ground thread tap) is a close fit in the hole after tapping—that is, if the tap cannot be screwed easily (without the use of a wrench) through the hole after tapping—it may be assumed that the pitch diameter of the hole is very nearly the same as that of the tap.

#### APPENDIX 5. COMMON PRACTICE AS TO THREAD SERIES AND CLASS OF FIT FOR SCREWS, BOLTS, AND NUTS

The usual commercial practice as to application of thread series and class of fit to screws, bolts, and nuts is indicated in table 73.

TABLE 73.—Common practice as to thread series and class of fit for screws, bolts, and nuts

Product	Thread series	Class of fit
1	2	3
Rough machine bolts Semifinished machine bolts: General applications Automotive vehicles Finished machine bolts: General applications Automotive vehicles	Coarsedo Fine Coarse Fine	Class 1, loose fit. Class 2, free fit. Class 3, medium fit. Do. Do.
Aircraft	Coarse or fine	Do. Class 2, free fit. Class 1, loose fit. Class 2, free fit. Do. Class 1, loose fit.
Carriage bolts Step bolts Button-head machine bolts Set screws Threaded studs: Nut end Stud end Tap rivets	do do {do {Fine Coarse or fine Coarse do	Class 2, free fit. Do. Do. Class 3, medium fit. Class 2, free fit. Class 3, medium fit. Class 5, wrench fit. Class 2, free fit. Class 3, medium fit.

#### APPENDIX 6. AMERICAN NATIONAL ACME SCREW THREADS (TENTATIVE SPECIFICATIONS)

#### 1. GENERAL AND HISTORICAL

When formulated, prior to 1895, Acme screw threads were intended to replace square threads and a variety of threads of other forms used chiefly for the purpose of producing traversing motions on machines, tools, etc. Acme screw threads are now extensively used for a variety of purposes. For ordinary use, where lateral looseness is not objectionable, clearances between the screw and nut are provided at the major and minor diameters and on the sides of the thread. These allow free movement of the screw in the nut without appreciable longitudinal looseness or end play. This quality of fit is provided for herein.

#### 2. TERMINOLOGY

The terms and symbols relating to screw threads, which are used herein and not otherwise defined, are defined in section II.

#### 3. AMERICAN NATIONAL ACME FORM OF THREAD

#### (a) SPECIFICATIONS

1. ANGLE OF THREAD.—The angle between the sides of the thread measured in an axial plane shall be 29°. The line bisecting this 29° angle shall be perpendicular to the axis of the screw thread. 2. DEPTH OF THREAD.—The basic depth of the thread shall be equal to one

half of the pitch.

3. THICKNESS OF THREAD.-The basic thickness of the thread at a diameter smaller by one half the pitch than the basic major diameter shall be equal to one half of the pitch.<sup>11</sup>

<sup>&</sup>lt;sup>11</sup> The diameter at which the thickness of thread is measured corresponds to the basic pitch diameter of 60° screw threads used for bolts, nuts, etc. On threads whose included angle is equal to 45° or more, the thickness of the thread is controlled and measured by the pitch diameter. On threads whose included angle is less than 45°, the thickness of the thread should be controlled directly. See p. 138.

4. CLEARANCE AT MINOR DIAMETER.—A clearance shall be provided at the minor diameter by making the minor diameter of the screw 0.020 inch smaller than basic for 10 or less threads per inch and 0.010 inch smaller than basic for more than 10 threads per inch.

5. CLEARANCE AT MAJOR DIAMETER.—A clearance shall be provided at the major diameter by making the major diameter of the nut or threaded hole 0.020 inch larger than basic for 10 or less threads per inch, and 0.010 inch larger than basic for more than 10 threads per inch.

6. FILLETS AT MINOR DIAMETER.—Fillets at the juncture of sides and root of the thread of the screw will develop on account of the rounding of the corners of the threading tool and the side cutting action of milling cutters when these threads are milled. It will be necessary, therefore, on tapped holes for all classes of fits, to provide a fillet or bevel at the minor diameter of the tap to remove the corner of the crest of the thread of the tapped hole. This fillet, or bevel, should be at least 0.010 inch for pitches of 3 threads per inch and finer, and at least 0.020 inch for pitches coarser than 3 threads per inch.

#### (b) ILLUSTRATION

The basic form of this thread is shown in figure 53.





NOTATION

 $\begin{array}{l} A=29^{\circ}\ 00'\\ a=14'\ 30'\\ p=pitch\\ n=number\ of\ threads\ per\ inch\\ N=number\ of\ turns\ per\ inch\\ h=0.5p,\ basic\ depth\ of\ thread\\ f=thickness\ of\ thread\\ f=0.37068p=basic\ width\ of\ flat \end{array}$ 

#### 4. THREAD SERIES

For general purposes there has been selected a series of diameters and pitches of Acme threads, listed in table 74, which are designated as standard. When it is not feasible to use one of these sizes, it is recommended that, as far as practicable, some one of the pitches shown in table 75 be used; also, that the diameter be within the range specified for each pitch. If a greater lead is required on a given diameter than that corresponding to the recommended maximum pitch, it is advisable to use a multiple thread of finer pitch rather than a single thread of coarser pitch.

											_
Identifi	ication	Basic diameters			Thread data						
Sizes	Threads per inch	Major diam- eter, D	Pitch diam- eter, E	Minor diam- eter, K	Pitch, p	Thread thickness at pitch line	Basic depth of thread, h=0.5 p	Depth of thread with clearance	Basic width of flat, F= 0.37069 $p$	Eeli angl at ba pitc diame \$	x sic h ter,
1	2	3	4	5	6	7	8	9	10	11	
34       \$10       \$4       \$6       \$6       \$6       \$76       \$10       \$6       \$10       \$12       \$134       \$134       \$134       \$2       \$2       \$2       \$2       \$2       \$2       \$2       \$2       \$2       \$2       \$2       \$2       \$2       \$2       \$2       \$2	$ \begin{array}{c} 16\\ 12\\ 12\\ 10\\ 8\\ 8\\ 5\\ 5\\ 5\\ 4\\ 4\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\$	Inches 0. 2500 .3125 .3750 .4375 .5000 .6250 .7500 .8750 1.0000 1.1250 1.2500 1.3750 1.5000 1.5000 1.5000 2.6000 2.5000 3.0000 4.0000 5.0000	Inches 0. 2187 . 2768 . 3333 . 3958 . 4500 . 5625 . 6875 . 8125 . 9000 1. 0250 1. 2750 1. 3750 1. 6250 1. 8750 2. 2500 2. 7500 2. 7500	Inches 0. 1875 . 2411 . 2816 . 3541 . 4000 . 5000 . 6250 . 7500 . 8000 . 9250 1. 0500 1. 17500 1. 2500 1. 25000 2. 5000 2. 5000 3. 5000	Inch 0. 66250 .07143 .08333 .08333 .10000 .12500 .12500 .20000 .20000 .20000 .20000 .20000 .25000 .25000 .50000 .50000 .50000	Inch 0.03125 .03571 .04167 .04167 .05000 .06250 .06250 .06250 .0000 .10000 .10000 .10000 .10000 .12500 .12500 .25000 .25000	Inch 0.03125 .03671 .04167 .0400 .06250 .06250 .06250 .06250 .06250 .06250 .06250 .06250 .06250 .10000 .10000 .10000 .10000 .12500 .12500 .25000 .25000 .25000	Inch 0.03625 .04071 .04667 .04667 .06000 .07250 .07250 .07250 .11000 .11000 .11000 .11000 .13500 .13500 .26000 .26000	Inch 0.0232 .0265 .0309 .0309 .0371 .0463 .0464 .0741 .0927 .1853 .1853 .1853	Deg. N. 5 4 4 3 4 4 3 2 4 3 2 2 4 3 2 2 4 3 2 2 4 3 2 2 1	$\begin{array}{c} \hline fin. \\ 12 \\ 422 \\ 330 \\ 500 \\ 3 \\ 199 \\ 488 \\ 3 \\ 333 \\ 100 \\ 522 \\ 199 \\ 488 \\ 266 \\ 3 \\ 199 \\ 266 \\ 55 \\ \end{array}$

TABLE 74.—American National Acme general purpose thread series

TABLE 75.—Recommended pitches, corresponding range of major diameters, and basic thread data, American National Acme threads

Number of threads per inch, $n$	Recommen major di	ded range of ameters <sup>1</sup>	Pitch, p	Basic depth of thread,	Basic width of flat,	
	Least	Greatest		<i>n</i> =0.5 <i>p</i>	F=0.37008p	
1	2	3	4	5	6	
1 1 1 1 2 2 2 2 2 2 3 	<i>Inches</i> 4, 5000 3, 5000 3, 0000 2, 2500 1, 7500 1, 5000 1, 1250	<i>Inches</i> 13, 5000 10, 5000 9, 0000 6, 7500 5, 2500 4, 5000 3, 3750	Inch 1.00000 .75000 .66667 .50000 .40000 .33333 .25000	Inch 0.5000 .3750 .3333 .2500 .2000 .1667 .1250	Inch 0.3707 .2780 .2471 .1853 .1483 .1236 .0927	
5 6	. 8750 . 7500 . 5625	2. 6250 2. 2500 1. 6875	. 20000 . 16667 . 12500	.1000 .0833 .0625	. 0741 . 0618 . 0463	
10	. 4375     . 3750     . 3125     . 2500	$1.3125 \\ 1.1250 \\ .9375 \\ .7500$	. 10000 . 08333 . 07143 . 06250	. 0500 . 0417 . 0357 . 0312	. 0371 . 0309 . 0265 . 0232	

<sup>1</sup> These recommended least diameters correspond to a maximum helix angle (at the minor diameter) of approximately 5°. The recommended greatest diameters are 3 times the least.

#### 5. CLASSIFICATION AND TOLERANCES

There is established herein for general use a single class of fit of American National Acme screw threads.

#### (a) GENERAL SPECIFICATIONS

The following general specifications apply to all standard Acme screw threads: 1. BASIC DIAMETERS.—The maximum major and pitch diameters of the screw, and the minimum minor diameter of the nut are basic. 2. TOLERANCES.—(a) The tolerances specified represent the extreme varia-

tions allowed on the product.

(b) The tolerances on diameters of the nuts or threaded holes are plus, and are applied from the minimum nut sizes to above the minimum nut sizes.

(c) The tolerances on diameters of the screws are minus, and are applied from the maximum screw sizes to below the maximum screw sizes.

(d) The tolerances on the thicknesses of threads are minus, and are applied from the maximum thread thickness to below the maximum thread thickness.

(e) The thread thickness tolerances for a screw and nut of the same diameter and pitch are equal.

The thread thickness tolerances include lead and angle errors.

(f) The thread thickness tolerances include lead and angle errors. (g) The tolerances on the major diameters of the screws and minor diameters of the nuts are based upon the pitch of the thread. (h) The minimum major diameter of the nut is at least 0.020 inch larger than

the basic major diameter.



FIGURE 54.-Illustration of allowances, tolerances, and crest clearances, Acme threads.

#### NOTATION

p = pitch.h = basic thread depth.Heavy line shows basic size.

(i) The maximum major diameter of the nut of a given pitch is such as to result in a flat equal to 0.3707p - 0.0052 inch when the pitch diameter of the nut is at its maximum value.

(j) The maximum minor diameter of a screw of a given pitch is such as to result in a flat at the root equal to 0.3707p - 0.0052 inch when the pitch diameter of the screw is at its maximum value.12

#### (b) LIMITING DIMENSIONS AND TOLERANCES

Limiting dimensions for standard Acme threads are given in table 76. The application of these limits is illustrated in figures 54, 55, and 56.

<sup>&</sup>lt;sup>13</sup> When the width of flat of the cutting tool is at this maximum value the entire thread thickness or pitch diameter tolerance cannot be used without falling below the minimum limit on minor diameter of the screw.



FIGURE 55.—Illustration of loosest condition for 1½-inch 4 Acme threads.



FIGURE 56.—Illustration of tightest condition for 1½-inch 4 Acme threads.

Nut sizes	rance valent m · diameter, fress mum eads		4 15	$ \begin{array}{c c} ch & Inches \\ \hline 0.002 & 0.2600 \\ 0.002 & 0.3225 \\ 0.003 & 3825 \\ 0.003 & 4475 \\ 0.003 & 5200 \\ \end{array} $	.004 .6450 .004 .7700 .004 .8950 .005 1.1450	.006 1.2700 .006 1.3950 .007 1.5200 .007 1.7700 .008 2.0200	. 011 2. 5200 . 011 3. 0200 . 011 4. 0200 . 011 5. 0200	
	meter Toler	Maxi- mum thre	13 1	Inches In 0.2347 0.2328 .2928 .3573 .4198 .4740	. 5945 . 7195 . 8445 . 9400 1. 0650	1. 1980 1. 3230 1. 4310 1. 6810 1. 9390	2. 3380 2. 8380 4. 8380 4. 8380	
	Pitch dis	Mini- mum	12	Inches 0. 2267 . 2848 . 3453 . 3453 . 4078 . 4620	. 5785 . 7035 . 8285 . 9200 1. 0450	1. 1740 1. 2990 1. 4030 1. 6530 1. 9070	2. 2940 2. 7940 3. 7940 4. 7940	
	ameter	liameter	Maxi- mum	11	Inches 0.1906 .2447 .2858 .3583 .3583	. 5063 . 6313 . 7563 . 8100 . 9350	1. 0600 1. 1850 1. 2625 1. 5125 1. 7625	2. 0200 3. 5200 4. 5200
	Minor d	Mini- mum (basic)	10	Inches 0. 1875 2411 2411 2816 . 3541 . 4000	. 5000 . 6250 . 7500 . 8000 . 9250	1. 0500 1. 1750 1. 2500 1. 5000 1. 7500	2. 5000 4. 5000 4. 5000	
		Minor diameter	Mini- mum	6	Inches 0. 1744 2275 2674 3399 . 3399 . 3750	. 4737 . 5987 . 7237 . 7700 . 8950	1. 0200 1. 1450 1. 2175 1. 4675 1. 7175	1. 9600 2. 4600 3. 4600 4. 4600
			Maxi- mum	ø	Inches 0.1775 0.1775 .2311 .2311 .2311 .3341 .3341 .3800	. 4800 . 6050 . 7300 . 7800 . 9050	1. 0300 1. 1550 1. 2300 1. 4800 1. 7300	1. 9800 3. 4800 4. 4800
	S	Tolerance equivalent on thickness of threads		7	Inch 0.002 0.003 0.003 0.003 0.003			10. 110. 110.
	Screw size	iameter	Mini- mum	9	<i>Inches</i> 0. 2107 2688 . 2688 . 3213 . 3328 . 3338 . 4380	. 5465 . 6715 . 7965 . 8800 1. 0050	1. 1260 1. 2510 1. 3470 1. 5980 1. 8430	2, 2060 3, 7060 4, 7060
		Pitch d	Maxi- mum (basic)	26	Inches 0. 2187 0. 2768 . 3333 . 3958 . 3958 . 4500	. 5625 . 6875 . 8125 . 9000 1. 0250	1. 1500 1. 2750 1. 3750 1. 3750 1. 6250 1. 8750	2. 2500 2. 7500 3. 7500 4. 7500
		liameter	Mini- mum	4	Inches 0. 2469 . 3089 . 3708 . 4333 . 4950	. 6187 . 7437 . 8687 . 9900 1. 1150	1. 2400 1. 3650 1. 4875 1. 7375 1. 9875	2. 4800 3. 9800 4. 9800
		Major 6	Maxi- mum (basic)	e	Inches 0. 2500 . 3125 . 3750 . 4375 . 5000	. 6250 . 7500 . 8750 1. 0000 1. 1250	$\begin{array}{c} 1.\ 2500\\ 1.\ 3750\\ 1.\ 5000\\ 1.\ 7500\\ 2.\ 0000 \end{array}$	2. 5000 3. 0000 5. 0000
		Threads	inch	63	10212	00 00 00 00 00 00 00	r0 r0 4 4 4	0000
		Sizes		I		68 68 168	2% 2%	

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TABLE 76.—American National Acme general purpose thread series, limiting dimensions and tolerances

### NATIONAL SCREW THREAD COMMISSION

#### 6. GAGES

The inspection of threaded product by means of gages and measuring tools is necessary to maintain the product within the limits specified and to prevent the use of threading tools after they have worn beyond proper limits. With the application of suitable methods of gaging and with reasonably good workmanship, uniform and known thread sizes will result.

#### (a) FUNDAMENTALS

Both "go" and "not go" gages, representing the extreme product limits, are necessary for the proper inspection of American National Acme screw threads. This and other fundamentals of the subject of gaging screw threads, which are stated for fastening screws in division 5 of section III, are also applicable to Acme threads.

#### (b) GAGE TOLERANCES

Table 77 is given herein for the purpose of establishing definite limits for gages used in the inspection of Acme threads, rather than for the purpose of specifying the gages required for the various inspection operations. The dimensions of gages should be in accordance with the principles (a) that the "go" gage should check simultaneously as many elements as possible and a "not go" gage can effectively check but one element; and (b), that permissible variations in the gages be within the extreme product limits. 1. TOLERANCES ON LEAD.—The tolerances on lead given in table 77 are specified

I. TOLERANCES ON LEAD.—The tolerances on lead given in table 77 are specified as an allowable variation between any two threads not farther apart than 12 inches.

2. TOLERANCES ON ANGLE OF THREAD.—The tolerances on angle of thread, as specified in table 77 for the various pitches, are tolerances on one half of the included angle. This insures that the bisector of the included angle will be perpendicular to the axis of the thread within proper limits. The equivalent deviation from the true thread form caused by such irregularities as convex or concave sides of thread, or slight projections on the thread form, should not exceed the tolerances permitted on angle of thread. 3. FILLETS AT MINOR DIAMETER.—"Go" threaded plug gages for nuts have

3. FILLETS AT MINOR DIAMETER.—"Go" threaded plug gages for nuts have fillets at the minor diameter, the radii of which are not less than 0.010 inch for pitches of three threads per inch and finer, and not less than 0.020 inch for pitches coarser than three threads per inch.

Threads per inch	Tolerance on thread thickness at basic pitch line		Tolerance in lead	Tolerand on half angle of	e Toleranc diar	e on major neter	Tolerance on minor diameter		
	From—	То—	То-		From-	T0	From—	То—	
1	2	3	4	5	6	7	8	9	
1	In h 0.0000 0000 0000 0000 0000 0000 0000	Inch 0.0008 .0007 .0006 .0005 .0005 .0004 .0003 .0003 .0003 .0002 .0002 .0002 .0002	$\begin{array}{c} Inch \\ \pm \\ 0.0005 \\ .0005 \\ .0005 \\ .0005 \\ .0005 \\ .0005 \\ .0005 \\ .0005 \\ .0005 \\ .0005 \\ .0005 \\ .0005 \\ .0005 \\ .0005 \\ .0005 \end{array}$	Deg. Mix 0 0 0 0 0 0 0 0 0 0 0 0 0	$\begin{array}{c} 1. \\ Inch \\ 6 \\ 0.0000 \\ 6 \\ 0000 \\ 6 \\ 0000 \\ 6 \\ 0000 \\ 6 \\ 0000 \\ 6 \\ 0000 \\ 6 \\ 0000 \\ 6 \\ 0000 \\ 6 \\ 0000 \\ 0 \\ $	Inch 0.0010 .0010 .0010 .0010 .0010 .0010 .0010 .0008 .0008 .0008 .0004 .0004 .0004	Inch 0.0000 00000 0000 0000 0000 0000 0000 0000 0000 0000 0000 000	Inch 0.0010 .0010 .0010 .0010 .0010 .0010 .0010 .0010 .0010 .0005 .0006 .0005 .0004 .0005	

TABLE	77.—Tolerances	for	"go"	and "not go	o'' thread	gages,	American	National
		-	-	Acme thread	ds			



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