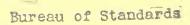


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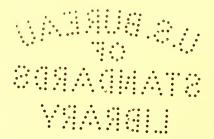
# SAFETY RULES FOR THE INSTALLATION AND MAINTENANCE OF ELECTRICAL SUPPLY AND COMMUNICATION LINES

HANDBOOK OF THE BUREAU OF STANDARDS, No. 10

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## DEPARTMENT OF COMMERCE BUREAU OF STANDARDS George K. Burgess, Director

HANDBOOK SERIES OF THE BUREAU OF STANDARDS, No. 10

# SAFETY RULES FOR THE INSTALLATION AND MAINTENANCE OF ELECTRICAL SUPPLY AND COMMUNICATION LINES

# COMPRISING PART 2 OF THE FOURTH EDITION NATIONAL ELECTRICAL SAFETY CODE

April 15, 1927



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> UNITED STATES GOVERNMENT PRINTING OFFICE WASHINGTON 1927

#### PREFACE

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Previous editions of the National Electrical Safety Code have been published in complete form. There has been some demand, however, for smaller handbooks containing a single part of the code, and in response to this demand a fourth edition is being issued not only as a whole, but also as separate publications dealing with the several subjects covered.

This volume contains part 2 dealing with the construction and maintenance of overhead and underground electrical supply and communication lines.

The present edition of these rules is the result of a revision which has been carried out according to the procedure of the American Engineering Standards Committee. The revised rules have had the approval of a sectional committee organized according to those rules of procedure and containing representatives of the various classes of utilities concerned; representatives of the State utility commissions having jurisdiction; of the electrical workers; of the insurance interests, manufacturers, inspectors, and other classes of persons concerned.

A discussion of these rules will be found in the revised edition of Handbook No. 4. Criticism of the rules and suggestions for their improvement are invited, and in future editions every effort will be made to perfect the rules by modifying any of the requirements which it is found can be improved.

> GEORGE K. BURGESS, Director.

Definiti	ons		
			e, and application of rules
500. 20.			e of rules
			Extent of application
			Not complete specifications
			Conformity with good practice
	201.		ication of the rules and exemptions
		Â.	Intent, modification
			Realization of intent
		C.	Waiver for temporary installations
			Waiver in emergencies
	202.		mum requirements
Sec. 21.	Genera	u requ	irements applying to overhead and under-
	$\mathbf{gr}$	ound	lines
	210.	Desig	gn and construction
			llation and maintenance
			ssibility
	213.		ection and tests of lines and equipment
		А.	When in service
			1. Initial compliance with rules
			2. Inspection
			3. Tests
			4. Record of defects
			5. Remedying defects
		в.	When out of service
			1. Lines infrequently used
			2. Lines temporarily out of service
	014	T	3. Lines permanently abandoned
	214.	Isola	tion and guarding
			Current-carrying parts
	915		Noncurrent-carrying parts
	210.		nding of circuits and equipment
			Methods Parts to be grounded
			Use of ground as part of circuit
		0.	obe of Bround as part of circuit

Sec. 21.	General requirements applying to overhead and under- ground lines—Continued.	Page
	216. Arrangement of switches	17 17
	A. Accessibility	
	B. Indicating open or closed position C. Uniform position	17 17
	SEC. 22-28. RULES FOR OVERHEAD LINES	
Sec. 22.	Relations between various classes of lines	17
	220. Relative levels	17
	A. Standardization of levels	17
	B. Relative levels; supply and communica-	
	tion conductors	18
	1. Preferred levels	18
	2. Minor extensions	18
	3. Special construction for supply cir-	
	cuits, the voltage of which does	
	not exceed 550 volts, and carrying	
	power not in excess of 1,600 watts_	19
	C. Relative levels; supply lines of different	
	voltage classifications	21
	1. At crossings or conflicts	21
	2. On poles used only by supply con-	21
	ductors	21
	221. Avoidance of conflict	22
	222. Joint use of poles by supply and communica-	
	tion circuits	22
	A. Advantages	$\frac{22}{22}$
	B. Cooperative study	$\frac{22}{22}$
	C. Conditions under which joint use is	22
	desirable	22
	223. Separate pole lines	${23}$
Sec. 23.	Clearances	23
	230. General	23
	A. Application	23
	B. Constant-current circuits	$23^{-3}$
	C. Metal-sheathed supply cables	24
	D. Maintenance of clearances	$\frac{-1}{24}$
	231. Horizontal clearances of supporting structures	
	from other objects	<b>24</b>
	A. From fire hydrants	<b>24</b>
	B. From street corners	24

1

2

Sec. 23.	Clearances—Continued	Page
	231. Horizontal clearances of supporting structures	
	from other objects—Continued.	
	C. From curbs	<b>24</b>
	D. From railroad tracks	25
	232. Vertical clearance of wires above ground or	
	rails	25
	A. Basic clearances	25
	B. Increased clearances	28
	1. Spans exceeding 150 feet	28
	(a) General	<b>28</b>
	(b) At railroad crossings	28
	(c) Maximum increase in clear-	
	ance	28
	2. Voltages exceeding 50,000	<b>29</b>
	3. Conductors supported by suspension	
	type insulators at crossings over	
	track rails	29
	4. Methods of avoiding this increase of	
	clearance	29
	C. Supply pole wiring at underground risers_	30
	233. Wire crossing clearances	30
	A. Basic clearances	30
	B. Increased clearances	32
	1. Where the sum of the distances from	
	the nearer supporting structure of	
	each span to the point of intersec-	
	tion exceeds 100 feet	32
	2. Voltages exceeding 50,000	32
	3. Conductors supported by suspension-	
	type insulators at crossings over	
	communication wires	33
	4. Methods of avoiding this increase of	0.0
	clearance	33
	234. Clearances of conductors of one line from other	
	conductors and structures	34
	A. Clearances from conductors of another	9.4
	line	34
	B. Clearances from supporting structures of	34
	another line	04

Sec. 23.	Clearances-Continued.			
	234. Clearances of co	nductors of one line from other		
conductors and structures—Continued.				
	C. Clearances	from buildings	35	
	1. Gener	al	35	
		er space	35	
		supply conductors attached to		
		ldings	35	
		uctors passing by or over		
		ouildings	36	
		Minimum clearances	36	
		Crossing roofs	37	
		Guarding of supply conductors.	37	
		from bridges	38	
	1. Cleara	ances of conductors from		
	brid	lges	38	
	2. Guard	ling trolley contact conductors		
		located under bridges	39	
	<i>(a)</i>	Where guarding is required	39	
	(b)	Nature of guarding	39	
	235. Minimum line-co	onductor clearances and sepa-		
	rations at su	ipports	39	
	A. Separation	between conductors on pole		
	lines		39	
	1. Applie	eation of rule	39	
	(a)	Multi-conductor wires or cables	39	
	<i>(b)</i>	Conductors supported by mes-		
		sengers or span wires	40	
	(c)	Measurement of clearances	40	
	2. Horiz	ontal separations between line		
		conductors	40	
	<i>(a)</i>	Fixed supports	40	
		(1) Minimum horizontal sep-		
		aration between line		
		conductors of the same		
		or different circuits	41	
		(2) Separations according to		
		sags	42	
	<i>(b)</i>	1		
		strained from movement	43	

Sec.

23.	Clearances—Continued.	
	235. Minimum line-conductor clearances and sepa-	
	rations at supports—Continued.	
	A. Separation between conductors on pole	
	lines—Continued.	Page
	3. Clearances in any direction from	
	line conductors to supports, and	
	to vertical or lateral conductors,	
	span or guy wires attached to	
	the same support	44
	(a) Fixed supports	44
	(b) Suspension insulators not re-	
	strained from movement	45
	4. Conductorseparation—vertical racks.	45
	5. Separation between supply lines of	
	different voltage classifications on	
	the same cross arm	46
	B. Separation between conductors attached	
	to buildings	47
	C. Separation between conductors attached	
	to bridges	47
	236. Climbing space	47
	A. Location and dimensions	47
	B. Portions of supporting structures in climbing space	48
	C. Cross arm location relative to climbing	
	space	48
	D. Location of supply apparatus relative to	
	climbing space	48
	E. Climbing space through conductors on	
	cross arms	48
	1. Conductors of same voltage class-	
	ification on same cross arm	48
	2. Conductors of different voltage class-	
	ification on same cross arm	49
	3. Horizontal climbing space dimen-	
	sions	49
	F. Climbing space on buck arm construction.	50
	G. Climbing space for longitudinal runs	50
	1. General	50
	2. Protection of longitudinal runs	51

age
51
52
52
52
<b>5</b> 2
52
<b>5</b> 2
52
53
53
53
54
54
54
54
56
56
56
56
57
57
57
58
58

1

Sec. 23.	Clearances—Continued.	
	238. Vertical separation between line conductors,	
	cables, and equipment located at different	
	levels on the same pole or structure—Con.	Page
	E. Vertical separation between conductors	1 450
	and noncurrent-carrying metal parts	
	of equipment	58
		00
	1. Between supply conductors and	<b>F</b> 0
	communication equipment	58
	2. Between communication conductors	
	and supply equipment	59
	3. Between supply and communica-	
	tion equipment	59
	(a) General	59
	(b) Special separations for span	
	wires or brackets	59
	4. Supply cross-arm braces considered	
	as equipment	60
	F. Vertical separation between communication	
	conductors carried at different levels on	
	railroad crossing poles	60
	239. Clearances of vertical and lateral conductors	
	from other wires and surfaces on the same	
	support	60
	A. Location of vertical or lateral conductors	00
	relative to climbing spaces, working	
	spaces, and pole steps	61
	B. Conductors not in conduit	61
	C. Mechanical protection near ground	61
	<b>D.</b> Requirements for vertical and lateral supply	01
	conductors on supply line poles or	
	within supply space on jointly used	
	poles	62
	1. General clearances	62
	2. Special cases	63
	E. Requirements for vertical and lateral com-	00
	munication conductors on communica-	
	tion line poles or within the communi-	
	cation space on jointly used poles	64
	1. Clearances from wires	64
	2. Clearances from pole and cross arm	09
	surfaces	65
	pulla000	Uu

Sec. 23. Clearances-Continued.

Clearances—Continued.	
239. Clearances of vertical and lateral conductors	
from other wires and surfaces on the same	
support—Continued.	Page
F. Requirements for vertical supply conductors	
passing through communication space	
on jointly used poles	65
1. Metal-sheathed supply cables	65
(a) Extent of covering	65
(b) Nature of covering	66
2. Supply conductors	66
(a) In conduit	66
(b) On pins and insulators	66
3. Supply grounding wires	67

- conductors passing through supply space on jointly used poles\_\_\_\_\_ 67 1. Metal-sheathed communication cables\_ 67 2. Communication conductors 68 3. Communication grounding wires\_\_\_\_\_ 68 4. Separation from through bolts\_\_\_\_\_ 68 Sec. 24. Grades of construction 69 240. General 69 241. Application of grades of construction to different situations 69 A. Supply cables\_\_\_\_\_ 69 1. Specially installed cables\_\_\_\_\_ 69 2. Other cables\_\_\_\_\_ 69 B. Two or more conditions 69 C. Order of grades\_\_\_\_\_ 70D. At crossings 701. Grade of upper line 70 2. Grade of lower line 70 3. Multiple crossings 71
  - (a) Where a line crosess in one span over two other lines..... 71

Sec. 24. Grades of construction—Continued.	
241. Application of grades of construction to differ-	
ent situations—Continued.	
D. At crossings—Continued.	
3. Multiple crossings—Continued.	Page
(b) Where one line crosses over a	
span in another line, which span	
is in turn involved in a second	
crossing	71
(c) Where communication con-	
ductors cross over supply con-	
ductors and railroad tracks in	-
the same span	72
E. Conflicts	73
1. How determined	73
2. Conductor conflict	73
3. Structure conflict	73
242. Grades of construction for conductors	73
A. Status of constant-current circuits	73
B. Status of railway feeders and trolley con-	-
tact conductors	74
C. Status of communication circuits used ex-	
clusively in the operation of supply	-
lines	74
D. Status of fire-alarm conductors	74
243. Grades of supporting structures	76
A. Poles or towers	76
B. Cross arms	77
C. Pins, insulators, and conductor fastenings_	77
Sec. 25. Loading for grades A, B, C, D, and E	78
250. Loading map	78
251. Assumed weather conditions	80
252. Modification of loading	80
253. Conductor loading	80
A. Heavy loading	81
B. Medium loading	81
C. Light loading	81
254. Loads upon line supports	82
A. Assumed vertical loading	82
B. Assumed transverse loading	82
1. Heavy loading	82 83
2. Medium loading	రెచ

Sec. 25. Loading for grades A, B, C, D, as	nd E-Continued.
254. Loads upon line supports-	
B. Assumed transverse	
3. Light loading_	
	conductors8
	8
6. Angles	8
C. Assumed longituding	al loading84
1. Change in grade	e of construction 84
2. Same grade of	construction through-
out	8:
. 3. Jointly used po	oles at crossings over
	communication lines8
4. Dead ends	80
5. Communication	a conductors on un-
guyed suppo	rts at railroad cross-
	80
<b>D.</b> Average span length	
	8
	83
E. Simultaneous applica	
Sec. 26. Strength requirements	
260. Preliminary assumptions_	
261. Grades A, B, and C constr	
A. Poles and towers	
0 0	th of three poles 88
	crete poles 88
**	g structures 89
	se strength 89
	inal strength 89
	a strength 89
	e unit stresses; steel90
	s of steel 91
	rted length of com-
-	n members 91
	r main leg members 92
. ,	al requirement for an-
	wers92
	construction features 92
	e covering or treat-
ment	93

Sec. 26.	. Strength requirements—Continued.	
	261. Grades A, B, and C construction-Continued.	
	A. Poles and towers—Continued.	Page
	4. Wood poles	93
	(a) Transverse strength	93
	(b) Longitudinal strength	93
	(c) Ultimate fiber stress	94
	(d) Treated poles	95
	(1) Preservatives	95
	(2) Full-length treatment	95
	(3) Butt treatment	95
	(e) Allowable fiber stresses	96
	(f) Freedom from defects	97
	(g) Minimum pole sizes	97
	(h) Spliced poles	97
	5. Transverse strength requirements for	
	structures where side guying is re-	
	quired, but can only be installed	
	at a distance	97
	6. Longitudinal-strength requirements	
	for sections of higher grade in lines	
	of a lower grade of construction_	99
	(a) Methods of providing longi-	
	tudinal strength	99
	(b) Flexible supports	100
	7. Strength at angles and dead ends	101
	B. Foundations	101
	1. Use of foundations	101
	(a) Wood and reinforced concrete	•
	poles	101
	(b) Steel poles or towers	101
	2. Strength of foundations	101
	(a) Steel supports	101
	(b) Wood and concrete poles	102
	C. Guys	102
	1. General	102
	2. For lines in exposed locations	103
	3. On steel structures	103
	4. On wood or concrete poles	103
	5. Strength of guys	104

Sec. 26. Strength requirements—Continued.	Page	
261. Grades A, B, and C construction—Continued.		
D. Cross arms	104	
1. Vertical strength	104	
2. Bracing	105	
3. Longitudinal strength	105	
(a) General	105	
(b) At ends of higher-grade con-		
struction in line of lower		
grade	105	
(c) At ends of transversely weak		
sections	106	
(d) Methods of meeting rules 261,		
D, 3, $(b)$ and $(c)$	106	
4. Dimensions of cross arms of selected		
yellow pine or fir	107	
5. Double-cross arms at angles or dead		
ends	107	
6. Location	107	
E. Pins and conductor fastenings	108	
1. Longitudinal strength	108	
(a) General	108	
(b) At ends of higher-grade con-		
struction in line of lower		
grade	108	
(c) At ends of transversely weak		
sections	108	
(d) Methods of meeting rules 261,		
E, 1, $(b)$ and $(c)$	109	
2. Sharp edges on fastenings	109	
3. Height of pin	109	
F. Open supply conductors	110	
1. Material	110	
2. Minimum sizes of supply conductors_	110	
3. Lightning protection wires	112	
4. Sags and tensions	112	
(a) Minimum allowable sag	112	
(b) Two-thousand pound limita-		
tion for conductor tensions_	113	
5. Splices and taps	113	
6. Trolley contact conductors	113	

Sec. 26.	Strength requirements—Continued.
	261. Grades A, B, and C construction—Continued.
	G. Supply cables
	1. Specially installed supply cables
	(a) Messengers
	(b) Grounding of cable sheath and
	messenger
	(c) Cable splices
	(d) Cable insulation
	2. Other supply cables
	(a) Messenger
	(b) Cable
	H. Open communication conductors
	I. Communication cables
	1. Metal-sheathed communication ca-
	bles
	2. Messenger
	J. Paired communication conductors
	1. Paired conductors supported on
	messenger
	(a) Use of messenger
	(b) Sag of messenger
	(c) Size and sag of conductors
	2. Paired conductors not supported on
	messenger
	(a) Above supply lines
	(b) Above trolley contact conduc-
	tors
	K. Short-span crossing construction
	L. Cradles at supply line crossings
	M. Protective covering or treatment for
	metal work
	262. Grades D and E construction
	A. Poles
	1. Strength of unguyed poles
	2. Strength of guyed poles
	3. Strength requirements for poles
	where guying is required but can
	only be installed at a distance
	4. Pole locations at crossings

Sec. 26.	Strength requirements—Continued.	
	262. Grades D and E construction—Continued.	
		Page
		121
	6. Minimum pole size	121
		121
	8. Poles located at crossings over spur	122
	9. Height of poles adjacent to crossing	
	poles	122
		123
		123
•		123
		123
	3. Guys used for transverse strength	124
	4. Guys used for longitudinal strength	124
	(a) Direction of head guys	124
	(b) Size and number of head	
	guys	124
		126
	6. Attachment of guys to poles	126
		126
	D. Cross arms	126
	1. Material	126
		127
	(a) Wood cross arms	127
		127
	3. Double cross arms	127
	E. Brackets and racks	127
	F. Pins	128
		128
	2. Strength	128
		128
		128
	(b) Metal pins	128
		128
	H. Attachment of conductor to insulator	128

# XVI

26.	Strength requirements—Continued.
	262. Grades D and E construction—Continued.
	I. Conductors
	1. Material
	2. Size
	(a) Spans not exceeding 150 feet
	(b) Spans exceeding 150 feet
	3. Paired conductors without mes-
	senger
	(a) Material
	(b) Size
	(c) Limiting span lengths
	4. Sags
	5. Splices and taps
	6. Simultaneous crossing over railroad
	and supply line
	J. Messengers
	1. Minimum size
	(a) Spans not exceeding $150$ feet
	(b) Spans exceeding 150 feet
	2. Sags and tensions
	K. Inspection
	263. Grade N construction
	A. Poles and towers
	B. Guys
	C. Cross-arm strength
	D. Supply-line conductors
	1. Material
	2. Size
	E. Supply services
	1. Material
	2. Size of open-wire services
	(a) Seven hundred and fifty volts
	or less
	(b) Exceeding 750 volts
	3. Sag, open-wire services
	(a) Seven hundred and fifty volts or less
	(b) Exceeding 750 volts

25804°-27-2

Sec.	26. Strength requirements—Continued.	
	263. Grade N construction—Continued.	
	E. Supply services—Continued.	Page
	4. Cabled services	138
	(a) Size	138
	(b) Sag	138
	(c) Insulation	138
	F. Lightning protection wires	138
	G. Trolley contact conductors.	138
	H. Cradles at supply-line crossings	138
	I. Communication conductors	138
Sec.	27. Line insulators	139
	<sup>270.</sup> Application of rule	139
	271. Material and marking	139
	272. Electrical strength of insulators in strain	
	position	139
	273. Ratio of flash over to puncture voltage	139
	274. Test voltages	140
	275. Factory tests	141
	276. Selection of insulators	141
	A. Insulation of constant-current circuits	141
	B. Insulators for nominal line voltages	141
	277. Protection against arcing	142
	278. Compliance with rule 277 at crossings	142
	A. Pin-type insulators	142
	1. Double construction	142
	2. Insulation at crossing supports	143
	B. Suspension insulators	144
	1. Double cross arms	144
	2. Number of insulator strings	144
	(a) Double insulator strings	144
	(b) Single insulator strings	144
	3. Position of insulator strings	145
	4. Insulators in suspended position	145
	(a) Ungrounded crossing supports	145
	(b) Grounded supports at the	
	crossing and elsewhere in	145
	the line	145
	(c) Grounded supports at the	145
	crossing only	$145 \\ 145$
	5. Insulators in strain position 6. Limit for increased number of insu-	140
		146
	lators	140

	CONTENTS	XIX Page
Sec 28	Miscellaneous requirements for overhead lines	146
000. 20.	280. Supporting structures	146
	A. Poles and towers	146
	1. Rubbish	146
	2. Guarding poles	146
	(a) Protection against mechanical	
	injury	146
	(b) Protection against climbing	146
	3. Warning signs	147
	(a) On poles or towers	147
	(b) On bridge fixtures	147
	4. Grounding metal poles	147
	5. Pole steps	147
	(a) Metal steps	147
	(b) Wood blocks	148
	6. Identification of poles	148
	7. Obstructions	148
	B. Cross arms	148
	1. Location	148
	2. Bracing	149
	C. Unusual conductor supports	149
	281. Tree trimming	150
	A. General	150
	B. At wire crossings and railroad crossings	150
	282. Guying	150
	A. Where used	150
	B. Strength	151
	C. Point of attachment	151
	D. Guy fastenings	$\begin{array}{c} 151 \\ 151 \end{array}$
	E. Guy guards F. Insulating guys from metal poles	$151 \\ 152$
	G. Anchor rods	152 152
	H. Grounding	$152 \\ 152$
	283. Guy insulators	$152 \\ 152$
	A. Properties of guy insulators	$152 \\ 152$
	1. Material	$152 \\ 152$
	2. Electrical strength	153
	3.2 Mechanical strength	153
		100

Sec. 28.	Miscellaneous requirements for overhead lines-Con.	
	283. Guy insulators—Continued.	Page
	B. Use of guy insulators	153
	1. One insulator	153
	2. Two insulators	153
	3. Relative location of insulators in	
	guys located one above the other	154
	4. Conditions not requiring guy insula-	
	tors	154
	284. Span-wire insulators	154
	A. Mechanical strength	154
	B. Use of span-wire insulators	154
	285. Conductors	155
	A. Identification	155
	B. Branch connections	155
	1. Accessibility	155
	2. Clearance	155
	286. Equipment on poles	156
	A. Identification	156
	B. Location	156
	C. Guarding	156
	D. Hand clearance	156
	E. Street-lighting equipment	157
	1. Clearance from pole surface	157
	2. Clearance above ground	157
	(a) Over walkways	157
	(b) Over roadways	157
	3. Horizontal clearances	157
	4. Material of suspension	157
	5. Insulators in suspension ropes	158
	6. Arc-lamp disconnectors	158
	287. Protection for exposed communication lines	158
	A. Open wire	158
	B. Metal-sheathed cable	158
	288. Communication circuits used exclusively in the	
	operation of supply lines	159
	A. Choice of method	159
	B. Guarding	159

XX

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Sec.		ous requirements for overhead lines—Con.	
	288. Con	munication circuits used exclusively in the	
		operation of supply lines—Continued.	Pa
	C	. Where ordinary communication line con-	
		struction may be used	15
	D	. Where supply line construction must be	
		used	16
	289. Elec	tric railway construction	16
	А	. Trolley contact conductor supports	16
	В	. High-voltage contact conductors	16
	C	. Third rails	16
	D	Prevention of loss of contact at railroad	
		crossings	16
	E	. Guards under bridges	16
		1. Where guarding is required	16
		2. Nature of guarding	16
Sec.	29. Rules for u	nderground lines	16
	290. Loc:	ation of duct systems and manholes	16
		. General location	16
	В	. Ducts	16
	C	. Manholes	16
		struction of duct systems	16
		. Material, size, and finish of ducts	16
		. Grading of ducts	16
	C	Alignment of ducts	16
		Duct joints	16
		. Protection	16
		1. Settling	16
		2. Damage	16
	F	. Clearances	16
		1. General	16
		2. Railroad tracks	16
	G	. Separation between supply and commun-	
		ication duct systems	16
		1. General	16
		2. Entering manholes	16
	н	. Duct entrances into manholes	16
		1. Clearances	16
		2. Smooth outlet	16
	I.		16
		Duct arrangement for dissipation of heat_	16
	0.	2 and arrangement for dissipation of fical.	10

Sec. 29.	Rules for underground lines—Continued.	Page
	292. Construction of manholes	167
	A. Minimum strength	167
	B. Dimensions	168
	1. Width	168
	2. Working space	168
	C. Drainage	168
	D. Ventilation	168
	E. Manhole openings	168
	F. Manhole covers	169
	G. Supports for cables	169
	293. Manhole location	169
	294. Location of conductors	169
	A. Accessibility	169
	B. Clearance from manhole floor	169
	C. Conductors carrying large currents	169
	D. Separation between conductors	170
	1. Cables of different voltages	170
	2. Cables of different systems	170
	3. Conductors of supply and communi-	
	cation systems	170
	(a) General	170
	(b) In the same manhole	170
	295. Protection of conductors in duct systems and	
	manholes	171
	A. Protection against moisture	171
	B. Protection against arcing	171
	C. Mechanical protection	171
	1. Crossings of supply and communi-	
	cation cables	171
	2. Iron-pipe conduit	172
	296. Guarding of live parts in manholes	172
	A. Conductor joints or terminals	172
	B. Apparatus	172
	1. General	172
	2. Continuity between cable sheath	
	and apparatus cases	172

#### XXII

CON	TENTS
-----	-------

Sec.	29. Rules for underground lines—Continued.
	297. Construction at risers from underground
	A. Separation between risers of communica-
	tion and supply systems
	B. Mechanical protection of conductors
	C. Grounding of riser pipes
	D. Conductor terminal construction
	1. Protection against moisture
	2. Insulation of conductors
	E. Clearance above ground for open supply wiring
	298. Identification of conductors
	299. Identification of apparatus connected in mul- tiple
nn	endixes
	A. Recommended normal sags of copper overhead line
	conductors, with corresponding tensions and stresses
	B. Minimum permissible sags for line conductors of grades
	A, B, and C, and corresponding tensions
	C. Sags for line conductors strung to the 2,000-pound limi-
	tation
	D. Mechanical data for wires and cables
	Copper
	Steel
	Copper-covered steel
	Aluminum
	E. Loads upon conductors and supports
	F. Wood poles
	Moments of resistance of poles
	Depreciation of wood poles
	Allowable number of wires on a given pole with and
	without side guys
	Depth of setting of poles
	<b>G.</b> Definition of American Society for Testing Materials of
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# SAFETY RULES FOR THE INSTALLATION AND MAINTE-NANCE OF ELECTRICAL SUPPLY AND COMMUNICA-TION LINES

# COMPRISING PART 2 OF THE FOURTH EDITION, NATIONAL ELEC-TRICAL SAFETY CODE

### DEFINITIONS

Alive or live means electrically connected to a source of potential difference, or electrically charged so as to have a potential different from that of the earth. The term "live" is sometimes used in place of the term "currentcarrying," where the intent is clear, to avoid repetitions of the longer term.

Automatic means self-acting, operating by its own mechanism when actuated by some impersonal influence—as, for example, a change in current strength. Not manual, without personal intervention. Remote control that requires personal intervention is not automatic, but manual.

Cable vault. See definition of manhole.

Circuit means a conductor or system of conductors through which an electric current is intended to flow.

Circuit-breaker means a device designed to open under abnormal conditions a current-carrying circuit without injury to itself. The term as used in this code applies only to the automatic type designed to trip on a predetermined overload of current.

Climbing space means the vertical space reserved along the side of a pole structure to permit ready access for linemen to equipment and conductors located on the pole structure. Common use means simultaneous use by two or more utilities of the same kind

Communication lines means the conductors and their supporting or containing structures which are located outside of buildings and are used for public or private signal or communication service, and which operate at not exceeding 400 volts to ground or 750 volts between any two points of the circuit, and the transmitted power of which does not exceed 150 watts. When operating at less than 150 volts no limit is placed on the capacity of the system.

Telephone, telegraph, messenger-call, clock, fire, or police alarm and other systems conforming with the above are included.

Lines used for signaling purposes, but not included under the above definition, are considered as supply lines of the same voltage and are to be so run.

Exception is made under certain conditions for communication circuits used in the operation of supply lines. (See rule 288.)

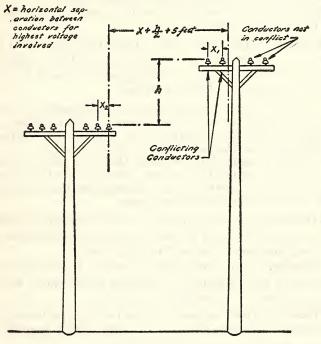
**Conductor** means a metallic conducting material, usually in the form of a wire or cable, suitable for carrying an electric current. Does not include bus bars.

Conductor conflict means that a conductor is so situated with respect to a conductor of another line at a lower level that the horizontal distance between them is less than the sum of the following values:

- (a) Five feet.
- (b) One-half the difference of level between the conductors concerned.
- (c) The value required in Tables 6, 7, or 8 for horizontal separation between conductors on the same support for the highest voltage carried by either conductor concerned.

**Conduit** means (in overhead or interior work) a tube or duct especially constructed for the purpose of inclosing electrical conductors.

Current-carrying part means a part intended to be connected in an electric circuit to a source of voltage. Noncurrent-carrying parts are those not intended to be so connected



Conductor Conflict

Dead means free from any electrical connection to a source of potential difference and from electric charge; not having a potential different from that of the earth. The term is used only with reference to current-carrying parts which are sometimes alive. Disconnector means a switch which is intended to open a circuit only after the load has been thrown off by some other means.

Manual switches designed for opening loaded circuits are usually installed in circuit with disconnectors, to provide a safe means for opening the circuit under load.

**Duct** means (in underground work) a single tubular runway for underground cables.

Electrical supply lines means those conductors and their necessary supporting or containing structures which are located entirely outside of buildings and are used for transmitting a supply of electrical energy.

Does not include open wiring on buildings, in yards or similar locations where spans are less than 20 feet, and all the precautions required for stations or utilization equipment, as the case may be, are observed.

Railway signal lines of more than 400 volts to ground are always supply lines within the meaning of these rules, and of less than 400 volts may be considered as supply lines, if so run and operated throughout.

**Exposed** (applied to circuits or lines) means in such a position that in case of failure of supports or insulation contact with another circuit or line may result.

**Grounded** means connected to earth or to some extended conducting body which serves instead of the earth, whether the connection is intentional or accidental.

Grounded system means a system having a permanent and effective electrical connection to earth. This ground connection may be at one or more points.

"Effective," as herein used, means a connection to earth of sufficiently low resistance and high current-carrying capacity to prevent any current in the grounding wire from causing a harmful voltage to exist between the grounded conductors and neighboring exposed conducting surfaces which are in good contact with the earth, or with neighboring surfaces of the earth itself, under the most severe conditions which are liable to arise in practice.

Permanently grounded means having such an effective connection to the earth (by use of an underground system of metallic pipe mains or other suitable means), as described in the preceding paragraph.

Guarded means covered, shielded, fenced, inclosed, or otherwise protected, by means of suitable covers or casings, barrier rails or screens, mats or platforms, to remove the liability of dangerous contact or approach by persons or objects to a point of danger.

Handhole means an opening in an underground system into which workmen reach, but do not enter.

Inclosed means surrounded by a case which will prevent accidental contact of a person with live parts. A solid inclosure means one which will neither admit accumulations of flyings or dust, nor transmit sparks or flying particles to the accumulations outside.

Insulated means separated from other conducting surfaces by a dielectric substance or air space permanently offering a high resistance to the passage of current and to disruptive discharge through the substance or space.

When any object is said to be insulated, it is understood to be insulated in suitable manner for the conditions to which it is subjected. Otherwise, it is, within the purpose of these rules, uninsulated. Insulating covering of conductors is one means for making the conductors insulated.

Insulating (where applied to the covering of a conductor, or to clothing, guards, rods, and other safety devices) means that a device, when interposed between a person and currentcarrying parts, protects the person making use of it against electric shock from the current-carrying parts with which the device is intended to be used; the opposite of conducting.

Isolated means that an object is not readily accessible to persons unless special means for access are used. Isolation by elevation means elevated sufficiently so that persons may safely walk underneath.

Joint use means simultaneous use by two or more kinds of utilities.

Lateral conductor means, in pole wiring work, a wire or cable extending in a general horizontal direction approximately at right angles to the general direction of the line conductors.

Lateral working space means the space reserved for working between conductor levels outside the climbing space, and to its right and left.

Line conductor means one of the wires or cables carrying electric current, supported by poles, towers, or other structures, but not including vertical or lateral connecting wires.

Manhole (more accurately termed splicing chamber or cable vault) means an opening in an underground system which workmen or others may enter for the purpose of installing cables, transformers, junction boxes, and other devices, and for making connections and tests.

Manual means capable of being operated by personal intervention.

Minor communication lines means communication lines carrying not more than two circuits used mainly for local telephone or telegraph service, or for police or fire-alarm service.

Minor tracks means railway tracks included in the following list:

(a) Spurs less than 2,000 feet long and not exceeding two tracks in the same span.

(b) Branches on which no regular service is maintained or which are not operated during the winter season.

(c) Narrow-gauge tracks or other tracks on which standard rolling stock can not, for physical reasons, be operated.

(d) Tracks used only temporarily for a period not exceeding one year. (e) Tracks not operated as a public utility, such as industrial railways used in logging, mining, etc.

**Open wires** mean overhead wires not in conduits, and consisting of single or paired conductors as opposed to multiple-conductor cables.

Qualified means familiar with the construction and operation of the apparatus and the hazards involved.

**Reconstruction** means replacement of any portion of an existing installation by new equipment or construction. Does not include ordinary maintenance replacements.

Rural districts mean all places not urban, usually in the country, but in some cases within city limits.

Sag.

Apparent sag at any point means the departure of the wire at the particular point in the span from the straight line between the two points of support of the span, at 60° F., with no wind loading.

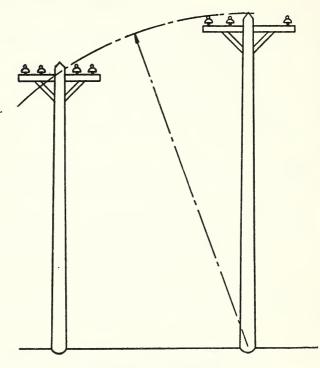
Apparent sag of a span means the maximum departure of the wire in a given span from the straight line between the two points of support of the span, at 60° F., with no wind loading. Where the two supports are at the same level this will be the normal sag.

Normal sag means the difference in elevation between the highest point of support of a span and the lowest point of the conductor in the span (or in the curve of the conductor in the span produced), at 60° F., with no wind loading.

Service means the connecting conductors by which a supply of electrical energy is carried from a supply line to the building or premises served. For overhead circuits, it includes the conductors from the last line pole to the service switch or fuse. The portion of an overhead service between the pole and building is designated as "service drop."

Structure conflict (as applied to a pole line) means that the line is so situated with respect to a second line that the overturning (at the ground line) of the first line will result DEFINITIONS

in contact between its poles or conductors and the conductors of the second line, assuming that no conductors are broken in either line.



Structure Conflict

*Exceptions.*—Lines are not considered as conflicting under the following conditions:

- (1) Where one line crosses another.
- (2) Where two lines are on opposite sides of a highway, street, or alley and are separated by a distance not lei than 60 per cent of the height of the taller pole line an not less than 20 feet.

Substantial means so constructed and arranged as to be of adequate strength and durability for the service to be performed under the prevailing conditions.

Splicing chamber. See definition for manhole.

Switch means a device for opening and closing or for changing the connection of a circuit. In these rules a switch vill always be understood to be manually operated, unless otherwise stated.

Urban districts means thickly settled areas (whether in sities or suburbs) or where congested traffic often occurs. A highway, even though in the country, on which the traffic is often very heavy, is considered as urban.

Utilization equipment means equipment, devices, and connected wiring which utilize electrical energy for mechanical, chemical, heating, lighting, testing, or similar purposes and are not a part of supply equipment, supply lines, or communication lines.

Voltage or volts means the highest effective voltage beween any two conductors of the circuit concerned, except hat in grounded multiwire circuits, not exceeding 750 volts between outer conductors, it means the highest effective roltage between any wire of the circuit and the ground.

In ungrounded circuits not exceeding 750 volts, voltage to ground means the voltage of the circuit.

When one circuit is directly connected to another circuit of higher voltage (as in the case of an autotransformer), both are considered as of the higher voltage, unless the circuit of lower voltage is permanently grounded. Direct connection implies electrical connection as distinguished from connection merely through electromagnetic or electrostatic induction.

Wire gauges.—The American Wire Gauge (A. W. G.), otherwise known as Brown & Sharpe (B. & S.), is the standand gauge for copper, aluminum, and other conductors, excepting steel, for which the Steel Wire Gauge (Stl. W. G.) s used throughout these rules.

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### SEC. 20. SCOPE, NATURE, AND APPLICATION OF RULES

### 200. Scope of Rules.

### A. Extent of Application.

The following rules apply to electrical supply and electrical communication lines in overhead and underground construction whether operated in connection with public utilities, privately or municipally owned, with industrial establishments, or otherwise.

### B. Not Complete Specifications.

These rules are not complete specifications but are intended to embody the requirements which are most important from the standpoint of safety to employees and the public.

### C. Conformity with Good Practice.

Construction should be made according to accepted good practice for the given local conditions in all particulars not specified in the rules.

## 201. Application of the Rules and Exemptions.

### A. Intent, Modification.

The rules shall apply to all installations except as modified or waived by the proper administrative authority. They are intended to be so modified or waived whenever they involve expense not justified by the protection secured or for any other reasons are impracticable; or whenever equivalent or safer construction can be more readily provided in other ways. 201. Application of the Rules and Exemptions-Con.

## B. Realization of Intent.

The intent of the rules will be realized:

- 1. By applying the rules in full to all new installations, reconstructions, and extensions, except where for special reasons any rule is shown to be impracticable or where the advantage of uniformity with existing construction is greater than the advantage of construction in conformity with the rules.
- 2. By placing guards on existing installations or otherwise bringing them into compliance with the rules, except where the expense involved is not justifiable.

Note.—The time allowed for bringing existing installations into compliance with the rules as specified in 2 will be determined by the proper administrative authority.

### C. Waiver for Temporary Installations.

It will sometimes be necessary to modify or waive certain rules in cases of temporary installations or installations which are soon to be discarded or reconstructed.

### D. Waiver in Emergencies.

In case of emergency or pending decision of the administrator, the person responsible for the installation may decide as to modification or waiver of any rule, subject to review by proper authority, but shall first notify all parties directly concerned in advance of construction.

### 202. MINIMUM REQUIREMENTS.

The rules state the minimum requirements for spacings, clearances, and strength of construction. More ample spacings and clearances or greater strength of construction may be provided if other requirements are not neglected in so doing.

Note.—Some of these minimum values are exceeded in much existing construction; service requirements frequently call for stronger supports and higher factors of safety than the minimum requirements of these rules.

### SEC. 21. GENERAL REQUIREMENTS APPLYING TO OVERHEAD AND UNDERGROUND LINES

210. DESIGN AND CONSTRUCTION.

All electrical supply and communication lines and equipment shall be of suitable design and construction for the service and conditions under which they are to be operated.

### 211. INSTALLATION AND MAINTENANCE.

All electrical supply and communication lines and equipment shall be installed and maintained so as to reduce hazards to life as far as practicable.

212. ACCESSIBILITY.

All parts which must be examined or adjusted during operation shall be arranged so as to be readily accessible to authorized persons by the provision of adequate climbing spaces, working spaces, working facilities, and clearances between conductors.

### 213. INSPECTION AND TESTS OF LINES AND EQUIPMENT.

- A. When in Service.
  - 1. INITIAL COMPLIANCE WITH RULES.

Lines and equipment shall comply with these safety rules upon being placed in service.

2. INSPECTION.

Lines and equipment shall be systematically inspected from time to time by the person responsible for the installation.

3. TESTS.

Lines and equipment shall be subjected, when necessary, to tests which will determine their fitness for service.

4. RECORD OF DEFECTS.

Any defects revealed by inspection, if not promptly corrected, shall be recorded.

5. REMEDYING DEFECTS.

Defective lines and equipment shall be put in good order or effectively disconnected.

### B. When Out of Service.

1. LINES INFREQUENTLY USED.

Supply lines and equipment infrequently used shall be inspected to see that they are in safe condition for service.

2. LINES TEMPORARILY OUT OF SERVICE.

Lines temporarily out of service shall be maintained in such condition that a hazard will not be created.

### 213. INSPECTION AND TESTS OF LINES AND EQUIPMENT— Continued.

### B. When Out of Service-Continued.

3. LINES PERMANENTLY ABANDONED.

Lines permanently abandoned shall be removed if they might create a hazard.

Note.—Overhead service drops to consumers are often disconnected without removal when the service is discontinued. This is considered good practice when it is undesirable to remove the service drop entirely.

## 214. ISOLATION AND GUARDING.

### A. Current-carrying Parts.

To promote safety to the general public and to employees not authorized to approach conductors and other current-carrying parts of electrical supply lines, such parts shall be arranged so as to provide adequate clearance from the ground or other space generally accessible, or shall be provided with guards so as to isolate them effectively from accidental contact by such persons.

### B. Noncurrent-carrying Parts.

Ungrounded metal-sheathed service cables, service conduits, metal fixtures, and similar noncurrentcarrying parts, if located in urban districts and where liable to become charged to more than 300 volts to ground, shall be isolated or guarded so as not to be exposed to accidental contact by unauthorized persons.

As an alternative to isolation or guarding, grounding of certain noncurrent-carrying parts is permitted by rule 215, B, and rule 280, A, 4.

### 215. GROUNDING OF CIRCUITS AND EQUIPMENT.

### A. Methods.

The methods to be used for permanent grounding for lightning arresters of supply lines, for circuits, for equipment and for wire raceways are given in section 9. The methods to be used for grounding of lightning arresters of communication lines are specified in rule 393.

### B. Parts to be Grounded.

In urban districts metal conduits, cable sheaths, and frames, cases, and hangers of equipment shall be permanently grounded.

*Exception 1.*—This rule does not apply when such parts are guarded from accidental contact by unauthorized persons.

- Exception 2.—This rule does not apply where such parts are 8 feet or more above the ground.
- Exception 3.—This rule does not apply to metal conduit and cable sheaths inclosing communication conductors, or supply conductors of not more than 300 volts to ground, provided such conduit and sheaths are not exposed to probable contact with circuits of more than 300 volts to ground.
- Recommendation.—It is recommended that supply cables have the sheath bonded to any conduit extending above the ground surface.
- Note.—Metal conduit above ground which contains extensions from metal-sheathed underground cable is considered to be sufficiently grounded by the cable sheath, provided such sheath is in good contact with the earth or is connected to a good ground. (For method of grounding see section 9.)

### C. Use of Ground as Part of Circuit.

In urban districts supply circuits shall not be designed to use the ground normally as the sole conductor for any part of the circuit.

Recommendation.—It is recommended that such use be avoided in rural districts.

### 216. ARRANGEMENT OF SWITCHES.

### A. Accessibility.

All switches shall be readily accessible to authorized persons.

## B. Indicating Open or Closed Position.

All switches shall indicate clearly whether they are open or closed.

### C. Uniform Position.

The handles or control mechanism for all switches throughout any system shall have so far as practicable the same position when open and a uniformly different position when closed, in order to minimize operating errors. Where it is advisable to depart from this practice, the switches should be marked so as to minimize the liability to mistakes in operation.

SEC. 22–28. RULES FOR OVERHEAD LINES

### SEC. 22. RELATIONS BETWEEN VARIOUS CLASSES OF LINES

### 220. Relative Levels.

### A. Standardization of Levels.

The levels at which different classes of conductors are to be located should be standardized where practicable for any given community by agreement of the utilities concerned.

Note.—This practice facilitates the extension of lines and promotes the safety of the public and workers by permitting the relative levels and required clearances to be readily obtained on jointly or commonly used poles as well as at crossings and conflicts.

- 220. RELATIVE LEVELS—Continued.
  - B. Relative Levels—Supply and Communication Conductors.
    - 1. PREFERRED LEVELS.

Where supply and communication conductors cross each other or are in conflict, or are located on the same poles or towers, the supply conductors shall preferably be carried at the higher level.

- *Exception.*—This does not apply to trolley feeders which may be located for convenience approximately at the level of the trolley contact conductor.
- Note.—Supply lines generally use larger conductors than communication lines so there is less liability of contact between the two if the supply conductors are located in the upper position. This relative location also avoids the necessity of workmen on communication conductors passing through supply conductors and working above them, and avoids the necessity of increasing the grade of construction required for communication conductors.
- 2. MINOR EXTENSIONS.

In localities where the practice of placing conductors of communication circuits for public use above supply conductors has been generally established, minor extensions may be made in either system, keeping the conductors in the same relative position. These extensions should not continue beyond a location at which it becomes practicable to change to the arrangement standardized by these rules.

- 220. RELATIVE LEVELS—Continued.
  - B. Relative Levels—Supply and Communication Conductors—Continued.
    - 3. SPECIAL CONSTRUCTION FOR SUPPLY CIRCUITS, THE VOLTAGE OF WHICH DOES NOT EXCEED 550 VOLTS, AND CARRYING POWER NOT IN EXCESS OF 1,600 WATTS.

Where all circuits are owned or operated by one party, or where cooperative consideration determines that the circumstances warrant and the necessary coordinating methods are employed, supply wires carrying a voltage not exceeding 440 volts, where practicable, or in exceptional cases 550 volts between conductors, with transmitted power not in excess of 1,600 watts, when involved in the joint use of poles with communication circuits, may be installed in accordance with Note h (3) of Table 1 in rule 232, A, and Note a of Table 11 in rule 238, A, 1, under the following conditions:

- (a) That such supply circuits are of wire having a good grade of commercial double-braid weatherproof covering not smaller than No. 8
  A. W. G. medium harddrawn copper or its equivalent in strength, and the construction otherwise conforms with the requirements for supply circuits of the same class.
- (b) That the supply circuits be placed on the end and adjacent pins of the bottom cross arm, and that a climbing space of at least 30 inches be maintained up the pole. Special precautions shall be taken to render such circuits conspicuous, such as painting a stripe on the cross arm or using a different form of insulator from the others on the pole line.

220. RELATIVE LEVELS—Continued.

- B. Relative Levels—Supply and Communication Conductors—Continued.
  - (c) That there shall be a vertical clearance of at least 2 feet between the cross arm carrying these supply circuits and the next cross arm above. The other pins on the cross arm carrying the supply circuit may be occupied by communication conductors used in the operation or control of railway or supply apparatus, but not for telegraph or telephone service.
  - (d) That such supply circuits shall be equipped with fuses and arresters installed in the supply end of the circuit. The fuses shall have a capacity not in excess of twice the maximum operating current value of the circuit they protect, but need not be less than 7 amperes. The arresters shall be designed so as to break down at a voltage of approximately twice the voltage between the wires of the circuit. but which need not be less than 500 volts. Where the supply circuits are alternating current, fuses shall be installed in the secondary side of the supply transformer and shall be such as to open the circuit successfully when the voltage is as great as that of the primary voltage of the transformer.

- 220. RELATIVE LEVELS—Continued.
  - C. Relative Levels—Supply Lines of Different Voltage Classifications (as Classified in Table 11).
    - 1. AT CROSSINGS OR CONFLICTS. Where supply conductors of different voltage classifications cross each other or are in conflict, the higher-voltage lines shall preferably be carried at the higher level.
    - 2. ON POLES USED ONLY BY SUPPLY CONDUCTORS.

Where supply conductors of different voltage classifications are on the same poles, relative levels should be as follows:

- (a) Where all circuits are owned by one utility, the conductors of higher voltages should generally be placed above those of lower voltage.
  - Note.—These relative levels will often avoid the necessity of increasing the grade of construction for cross arms, pins, and conductor fastenings of the lower-voltage conductors.
- (b) Where different circuits are owned by separate utilities, the circuits of each utility may be grouped together and one group of circuits may be placed above the other group provided that the circuits in each group are located so that those of higher voltage are at the higher levels and that either of the following conditions is met:
  - A vertical spacing of not less than 4 feet (or 6 feet where required by Table 11, rule 238, A, 1) is maintained between the nearest line conductors of the respective utilities (this space to be identified if necessary as a division space).
  - (2) Conductors of a lower voltage classification are at a higher level than those of a higher classification only where on the opposite side of the pole.

### 221. Avoidance of Conflict.

Two parallel pole lines, either of which carries supply conductors, shall where practicable be so separated from each other that neither conflicts with the other. If this is impracticable, then the conflicting line or lines shall be built of the grade of construction required by section 24 for a conflicting line or the two lines shall be combined in a single pole line.

- 222. JOINT USE OF POLES BY SUPPLY AND COMMUNICATION CIRCUITS.
  - A. Advantages.

Joint use of poles under suitable conditions and with certain types of circuits offers many advantages and promotes safety.

B. Cooperative Study.

Joint use involves contractual relations between utilities, consideration of service requirements, and economies as well as safety. It, therefore, requires cooperative study by the utilities concerned.

## C. Conditions Under Which Joint Use is Desirable.

In the case of local or distribution circuits along the same highway or similar right of way, where, under the provisions of section 24 applying to joint use, grade C construction or less would be required, joint use is generally preferable to separate pole lines (except sometimes in rural districts) unless the number of conductors is very large or the character of the circuits makes joint use undesirable.

Where circuits other than those mentioned above are involved, the choice between joint use of poles and separate pole lines shall be determined through cooperative consideration, by the utilities concerned, of all the factors involved, including the character

- 222. JOINT USE OF POLES BY SUPPLY AND COMMUNICATION CIRCUITS—Continued.
  - C. Conditions Under Which Joint Use is Desirable— Continued.

of circuits, the total number and weight of conductors, tree conditions, number and location of branches and service drops, availability of right of way, etc. Where such joint use is mutually agreed upon, it shall be subject to the appropriate grade of construction as specified in section 24. Where such joint use is not employed, separate lines as specified in rule 223 shall be used.

In any event, joint use is preferable to separate lines where it would be impracticable to avoid an overbuilt conflict with separate lines.

223. SEPARATE POLE LINES.

Where two separate pole lines are to be used, one of which carries supply conductors and the other communication conductors, they shall be separated, if practicable, so that neither conflicts with the other, but if within conflicting distance, they shall be separated as far as practicable.

### SEC. 23. CLEARANCES

230. GENERAL.

### A. Application.

This section covers all clearances involving poles and wires. Clearances of lamps from pole surfaces, from spaces accessible to the general public, and height above ground are covered in rule 286, E.

### B. Constant-Current Circuits.

The clearances for constant-current circuits shall be determined on the basis of their nominal fullload voltage. 230. GENERAL—Continued.

## C. Metal-Sheathed Supply Cables.

As far as clearances are concerned, permanently grounded continuous metal-sheathed supply cables of all voltages are classified the same as open supply wires of 0 to 750 volts.

## D. Maintenance of Clearances.

When initial wire sags have increased, due to permanent elongation of wires or movement of supporting structures, so that the clearances or separations have materially decreased, slack should be taken up.

Note.—As soft copper stretches more than medium or hard, the taking up of slack will be necessary chiefly in lines where soft wire is used.

231. HORIZONTAL CLEARANCES OF SUPPORTING STRUCTURES FROM OTHER OBJECTS.

Poles, towers, and other supporting structures and their guys and braces shall have the following horizontal clearances from other objects. The clearance shall be measured between the nearest parts of the objects concerned.

## A. From Fire Hydrants.

Not less than 3 feet.

Recommendation.—Where conditions permit, a clearance of not less than 4 feet is recommended.

B. From Street Corners.

Where hydrants are located at street corners, poles and towers should not be set so far from the corners as to make necessary the use of flying taps inaccessible from the poles.

C. From Curbs.

Not less than 6 inches measured to the street side of the curb.

231. HORIZONTAL CLEARANCES OF SUPPORTING STRUCTURES FROM OTHER OBJECTS—Continued.

### D. From Railroad Tracks.

Where railroad tracks are paralleled or crossed by overhead lines, the poles shall, if practicable, be located not less than 12 feet from the nearest track rail.

Exception 1.—At sidings a clearance of not less than 7 feet may be allowed, provided sufficient space for a driveway be left where cars are loaded or unloaded.

- *Exception 2.*—Supports for overhead trolley contact conductors may be located as near their own track rail as conditions require. If very close, however, permanent screens on cars will be necessary to protect passengers.
- *Exception 3.*—Where necessary to provide safe operating conditions which require an uninterrupted view of signals, signs, etc., along tracks, the parties concerned shall cooperate in locating poles to provide the necessary clearance where practicable.
- 232. VERTICAL CLEARANCE OF WIRES ABOVE GROUND OR RAILS.

The vertical clearance of all wires above ground in generally accessible places or above rails shall be not less than the following:

A. Basic Clearances.

The clearances in Table 1 apply under the following conditions.

Temperature of 60° F., no wind.

Span lengths 0 to 150 feet.

Voltage 0 to 50,000 volts.

Fixed conductor supports.

For other conditions see rule 232, B.

25804°-27-4

# 232. VERTICAL CLEARANCE OF WIRES ABOVE GROUND OR RAILS—Continued.

A. Basic Clearances-Continued.

### Table 1.—Minimum Vertical Clearance of Wires Above Ground or Rails

[All voltages are between wires unless otherwise stated. Supply wires include trolley feeders]

Nature of ground or rails underneath wires	Guys; messen- gers; communi- cation, span, and lightning protection wires; per- manently grounded continu- ous-metal- sheath cables. All voltages	Open supply line wires, arc wires and service drops			Trolley con- tact conduc- tors and associ- ated span or messenger wires <sup>a</sup>	
		0 to 750 volts	750 to 15, 000 volts	15, 000 to 50, 000 volts	0 to 750 volts to ground	Ex- ceed- ing 750 volts to ground

### WHERE WIRES CROSS OVER

Track rails of railroads handling freight cars on top of which men are permitted •	Feet • 27	Feet • 27	Feet • 28	Feet 30	Feet <sup>d</sup> 22	Feet <sup>d</sup> 22
Track rails of railroads not in- cluded above. •	18	18	20	22	• 18	• 20
Streets, alleys or roads in urban or rural districts	1 18	18	20	22	• 18	• 20
Driveways to residence garages	10	10	20	22	• 18	• 20
Spaces or ways accessible to pe- destrians only	ø 15	Å 15	15	17	* 16	<b>ن</b> 18

### WHERE WIRES RUN ALONG

Streets or alleys in urban dis- tricts	i.k 18	<i>i</i> 18	20	22	• 18	• 20
Roads in rural districts	i.k.1 15	i 15	18	20	• 18	• 20

See footnotes on page 27

### 232. VERTICAL CLEARANCE OF WIRES ABOVE GROUND OR RAILS-Continued.

### A. Basic Clearances—Continued.

#### Footnotes for Table 1

a Where subways, tunnels, or bridges require it, lcss clearances above ground than required by Table 1 may be used locally. The trolley contact conductor should be graded very grad-ually from the regular construction down to the reduced elevation.

b For white crossings over railways handling only cars considerably lower than ordinary freight cars, the clearance may be reduced by an amount equal to the difference in height between the highest car handled and the highest ordinary freight car, but the clearance shall not be reduced below that required for street crossings.

c This clearance may be reduced to 25 feet where paralleled by trolley contact conductor on the same street or highway.

d In communities where 21 feet has been established, this clearance may be continued if carefully maintained. The elevation of the contact conductor should be the same in the crossing and next adjacent spans. (See rule 289 D, 2, for conditions which must be met where uniform height above rail is impracticable.)

*e* In communities where 16 feet has been established for trolley contact conductors 0 to 750 volts or 18 feet for trolley contact conductors exceeding 750 volts, this clearance may be continued if carefully maintained.

f Where a guy crosses a street or alley in urban districts and the section of the guy above the street or alley is effectively insulated against the highest voltage to which it is exposed, up to 7,500 volts, the clearance may be reduced to 16 feet at the side of the traveled way. g This clearance may be reduced as follows: Fect

- (1) For communication conductors of circuits limited to 160 volts to ground and
- carrying not more than 50 watts\_\_\_\_\_
- (2) For conductors of other communication circuits.
   (3) For guys 10 8

h This clearance may be reduced as follows:

- (1) Supply wires (except trolley contact wires) limited to 300 volts to ground\_\_\_\_\_ 12 (2) Supply wires (except trolley contact wires) limited to 150 volts to ground and 10
- (2) Supply writes text to the control of t

ways may be placed at a less height if suitably guarded. *j* Where a pole line along a road is located relative to fences, ditches, embankments, etc., so that the ground under the line will never be traveled except by pedestrians, this clearance may be reduced as follows: Foot

(1)	Communication conductors limited to 160 volts to ground and transmitted	000
	power of 50 watts	8
(2)	Supply conductors	12

k No clearance from ground is required for anchor guys not crossing streets, driveways, roads, or pathways nor for anchor guys provided with traffic guards and paralleling sidewalk curbs.

I This clearance may be reduced to 13 feet for communication conductors where no part of the line overhangs any part of the highway which is ordinarily traveled, and where it is unlikely that loaded vehicles will be crossing under the line into the fields.

- 232. VERTICAL CLEARANCE OF WIRES ABOVE GROUND OR RAILS—Continued.
  - B. Increased Clearances.

Greater clearances than given in Table 1 (rule 232, A) shall be provided under the following conditions. The increases required in 1, 2, and 3 below are cumulative where more than one applies.

- 1. SPANS EXCEEDING 150 FEET.
  - *Exception.*—Trolley contact conductors are exempted from this rule.
  - (a) GENERAL. For spans exceeding 150 feet the clearance shall be increased by 0.1 foot for each 10 feet of the excess over 150 feet. See (c) below.
  - (b) AT RAILROAD CROSSINGS. Where the clearance of conductors is determined by the presence of railroad or railway tracks in the span, the increase in clearance may be determined by the following:

Where the distance from the nearer crossing support to the farthest track rail does not exceed 75 feet, no increase is required.

Where this distance exceeds 75 feet, 0.2 foot for each 10 feet of excess. See (c) below.

(c) MAXIMUM INCREASE IN CLEARANCE. The increase in clearance given by (a) or (b) above need not exceed the limiting values given in the table below provided conductor sags are such that the maximum tension in the conductor does not exceed the specified percentages of its breaking load:

Percentage of breaking load of conductor	Limiting clearance increase in feet for different loading districts				
	Heavy	Medium	Light		
50 60	$2.5 \\ 2.5$	$3.0 \\ 4.0$	4. 0 5. 0		

- 232. VERTICAL CLEARANCE OF WIRES ABOVE GROUND OR RAILS—Continued.
  - B. Increased Clearances—Continued.
    - 2. VOLTAGES EXCEEDING 50,000.

For these voltages the clearances given in Table 1 (rule 232, A) shall be increased at the rate of 0.5 inch for each 1,000 volts of the excess.

- 3. CONDUCTORS SUPPORTED BY SUSPENSION-TYPE INSULATORS AT CROSSINGS OVER TRACK RAILS. The clearance shall be increased by such an amount that the values specified in Table 1 (rule 232, A) will be maintained in case of a broken conductor in either adjoining span, if the conductor is supported as follows:
  - (a) At one support by suspension-type insulators in a suspended position, and at the other support by insulators which are not free to swing (including semistrain-type insulators).
  - (b) At one support by strain insulators and at the other support by semistrain-type insulators.
- 4. METHODS OF AVOIDING THIS INCREASE OF CLEAR-ANCE.

Any of the following construction methods will avoid the necessity for the increase in clearance required by rule 232, B, 3.

- (a) Suspension-type insulators in a suspended position at both supports.
- (b) Semistrain-type insulators at both supports.
- (c) Arrangement of insulators so that they are restrained from displacement toward the crossing.

- 232. VERTICAL CLEARANCE OF WIRES ABOVE GROUND OR RAILS—Continued.
  - C. Supply Pole Wiring at Underground Risers.

Supply wires connecting to underground systems shall not be run open closer to the ground than is indicated by Table 2:

Table 2.—Clearance Above Ground for Open Supply Wiring						
	Voltage					
Location on pole	0 to 750 volts	750 to 15, 000 volts	More than 15,000 volts			
Side of pole adjacent to vehic- ular traffic	Feet 14	Feet 16	Feet 18			
Side of pole not adjacent to vehicular traffic	8	11	13			

## 233. WIRE CROSSING CLEARANCES.

The clearance between any two wires crossing each other and carried on different supports shall be not less than the following:

### A. Basic Clearances.

The clearances given in Table 3 below apply under the following conditions:

Temperature of 60° F., no wind.

Where the sum of the distances from the point of intersection of two crossing wires to the nearer supporting structure of each span does not exceed 100 feet.

Where the upper conductor or wire has fixed supports.

Conductors of lines operating at the voltages indicated at the heads of columns should, in general, be installed above those to the left of the table, where a clearance is given in boldface type.

### 233. WIRE CROSSING CLEARANCES—Continued. A. Basic Clearances—Continued.

### Table 3.-Wire Crossing Clearances

[All voltages are between wires except for trolley contact wires where voltages are to ground]

[The insertion of a given clearance in italics indicates that in general the lines operating at the voltage named above this clearance should not cross over the lines at the voltage to the left of the clearance in italics]

Nature of wires crossed over	Com- muni- cation wires	wires ( volts a ground tinuous sheath cables	supply 0 to 750 nd per- ently ed con- s-metal- supply s of all ages	wires a	Open supply wires and serv- ice drops	
		Line wires	Serv- ice drops	750 to 7,500 volts	7,500 to 50,000 volts	wires a
Communication, including cables and messengers	Feet	Feet ¢4	Feet 2	Feet 4	Feet 6	Feet
Supply cables having permanently grounded continuous metal sheath, all voltages	4	2	2	2	4	2
Open supply wires: 0 to 750 volts 750 to 7,500 volts 7,500 to 50,000 volts	4 4 6	<b>2</b> 2 4	<b>2</b> 4 6	2 2 4	4 4 4	2 4 4
Trolley contact conductors	d 4	d, e 4	d 4	6	6	d 4
Guys, messengers, span wires, lightning-protection wires, serv- ice drops 0 to 750 volts	b 2	2	2	4	4	b 2

<sup>a</sup> Completely insulated sections of guys attached to supporting structures having no conductor of more than 7,500 volts may have less than this clearance from each other.

<sup>b</sup> The clearance of communication conductors and their guy, span, and messenger wires from each other in locations where no other classes of conductors are involved may be reduced by mutual consent of the parties concerned, subject to the approval of the-regulatory body having jurisdiction, except for fire-alarm wires and wires used in the operation of railroads, or where one set of conductors is for public use and the other used in the operation of supply systems.

• A clearance of 2 feet may be permitted where the supply conductor is above the communication conductor, provided the crossing is not within 6 feet from any pole concerned in the crossing and the voltage to ground does not exceed 300 volts.

<sup>4</sup> Trolley-contact conductors of more than 750 volts should have at least 6 feet clearance. This clearance should also be provided over lower-voltage trolley-contact conductors unless the crossover conductors are beyond reach of a trolley pole leaving the trolley-contact conductor or are suitably protected against damage from trolley poles leaving the trolley-contact conconductor.

• Trolley feeders are exempt from this clearance requirement for trolley-contact conductors if they are of the same nominal voltage and of the same system.

### 233. WIRE CROSSING CLEARANCES—Continued.

### B. Increased Clearances.

Greater clearances than given in Table 3 (rule 233, A) shall be provided under the following conditions. The increases required in 1, 2, and 3 below are cumulative where more than one applies.

1. WHERE THE SUM OF THE DISTANCES FROM THE NEARER SUPPORTING STRUCTURE OF EACH SPAN TO THE POINT OF INTERSECTION EXCEEDS 100 FEET.

Under this condition the clearances given in Table 3 (rule 233, A) shall be increased by 0.1 foot for each 10 feet of the excess over 100 feet. This increase need not exceed the limiting values given below when the sag of the upper conductor is such that the maximum stress in that conductor will not exceed the specified percentage of its ultimate stress.

Percentage of ultimate conductor stress	Maximum increase in feet for different loading territories					
	Heavy	Medium	$\mathbf{Light}$			
50 60	$2.5 \\ 2.5$	3. 0 4. 0	4. 0 5. 0			

### 2. VOLTAGES EXCEEDING 50,000.

For these voltages the clearances given in Table 3 (rule 233, A) shall be increased at the rate of 0.5 inch for each 1,000 volts of the excess.

- 233. WIRE CROSSING CLEARANCES—Continued.
  - B. Increased Clearances—Continued.
    - 3. CONDUCTORS SUPPORTED BY SUSPENSION-TYPE INSULATORS AT CROSSINGS OVER COMMUNICA-TION WIRES.

For such conductors the clearance shall be increased by such an amount that the values specified in Table 3 (rule 233, A) will be maintained in case of a broken conductor in either adjacent span, provided such conductor is supported as follows:

- (a) At one support by suspension-type insulators in a suspended position, and at the other support by insulators not free to swing (including semistrain-type insulators).
- (b) At one support by a strain insulator, and at the other support by a semistrain-type insulator.
- 4. METHODS OF AVOIDING THIS INCREASE OF CLEAR-ANCE.

Any of the following construction methods will avoid the necessity for the increase in clearance required by rule 233, B, 3.

- (a) Suspension-type insulators in a suspended position at both supports.
- (b) Semistrain-type insulators at both supports.
- (c) Arrangement of insulators so that they are restrained from displacement toward the crossing.

- 234. CLEARANCES OF CONDUCTORS OF ONE LINE FROM OTHER CONDUCTORS AND STRUCTURES.
  - A. Clearances from Conductors of Another Line. The clearance in any direction between any conductor of one line and any conductor of a second and conflicting line shall be not less than the largest value required by 1, 2, or 3 below at 60° F. and no wind.
    - 1. Four feet.
    - The values required by rule 235, A, 2, (a) (1) or
       (2) for separation between conductors on the same support.
    - 3. The apparent sag of the conductor having the greater sag, plus 0.2 inch per kilovolt of the highest voltage concerned.
  - B. Clearances from Supporting Structures of Another Line.

Conductors of any line passing near a pole or similar supporting structure of a second line without being attached thereto, shall have clearances from any part of such structure not less than the larger value required by either 1 or 2 below at 60° F. and no wind.

- 1. Three feet if practicable.
- The values required by rule 235, A, 2, (a) (1) and (2) for separation between similar conductors on the same support, increased by 1 inch for each 2 feet of the distance from the supporting structure of the second line to the nearest supporting structure of the first line.

The climbing space on the structure of the second line shall in no case be reduced by a conductor of the first line.

 $\mathbf{34}$ 

### 234. CLEARANCES OF CONDUCTORS OF ONE LINE FROM OTHER CONDUCTORS AND STRUCTURES—Continued.

### C. Clearances from Buildings.

1. GENERAL.

Conductors shall be arranged and maintained so as to hamper and endanger firemen as little as possible in the performance of their duties.

2. LADDER SPACE.

Where buildings exceed three stories (or 50 feet) in height, overhead lines should be arranged where practicable so that a clear space or zone at least 6 feet wide will be left, either adjacent to the building or beginning not over 8 feet from the building, to facilitate the raising of ladders where necessary for fire fighting.

- *Exception.*—This requirement does nor apply where it is the unvarying rule of the local fire departments to exclude the use of ladders in alleys or other restricted places which are generally occupied by supply lines.
- 3. OPEN SUPPLY CONDUCTORS ATTACHED TO BUILD-INGS.

Where the permanent attachment of open supply conductors of any class to buildings is necessary for an entrance, such conductors shall meet the following requirements:

- (a) Conductors of more than 300 volts to ground shall not be carried along or near the surface of the building unless they are guarded or made inaccessible.
- (b) Clearance of wires from building surface shall be not less than those required in Table 9 (rule 235, A, 3, (a)) for clearance of conductors from pole surfaces.

### 234. CLEARANCES OF CONDUCTORS OF ONE LINE FROM OTHER CONDUCTORS AND STRUCTURES—Continued.

- C. Clearances from Buildings—Continued.
  - 4. CONDUCTORS PASSING BY OR OVER BUILDINGS.
    - (a) MINIMUM CLEARANCES. Unguarded or accessible supply conductors carrying voltages in excess of 300 volts shall not come closer to any building or its attachments (balconies, platforms, etc.) than listed below.
      - (1) SPANS 0 TO 150 FEET.

Table 4.—Clearances of Supply Conductors from Buildings						
Voltage of supply con- ductors	Horizontal clearance	Vertical clearance				
300 to 7,500	Feet 3	Feet 8				
7,500 to 15,000	8	8				
15,000 to 50,000	10	10				
Exceeding 50,000	10 plus 0.5 inch per kv. in ex- cess.	10 plus 0.5 inch per kv. in ex- cess.				

- (2) SPANS EXCEEDING 150 FEET. Where span lengths exceed 150 feet, the increased clearances required by rule 232, B, 1 shall be provided.
  - *Exception.*—These increased clearances are not required where the voltage of the supply conductors is from 300 to 7,500 volts.

- 234. CLEARANCES OF CONDUCTORS OF ONE LINE FROM OTHER CONDUCTORS AND STRUCTURES—Continued.
  - C. Clearances from Buildings—Continued.

1.5

- (b) CROSSING ROOFS. Supply conductors exceeding 7,500 volts should not be carried over buildings not concerned in the operation of the utility owning them, if this can be avoided.
- (c) GUARDING OF SUPPLY CONDUCTORS. Supply conductors of 300 volts or more shall be properly guarded by grounded conduit, barriers, or otherwise, under the following conditions:
  - (1) Where the clearances set forth in Table 4 (rule 234, C, 4, (a), (1)) can not be obtained.
  - (2) Where such supply conductors are placed near enough to windows, verandas, fire escapes, or other ordinarily accessible places, to be exposed to contact by persons.
  - Note.—Supply conductors in grounded metal-sheathed cable are considered to be guarded within the meaning of this rule.

# 234. CLEARANCES OF CONDUCTORS OF ONE LINE FROM OTHER CONDUCTORS AND STRUCTURES—Continued.

- D. Clearances from Bridges.
  - 1. CLEARANCES OF CONDUCTORS FROM BRIDGES.

Supply conductors, not installed in grounded conduit or metal-sheath cable, which pass under, over, or near a bridge shall have clearances therefrom not less than given in Table 5.

Table 5.—Clearances from Bridges								
Operating voltages	tions (ot traveled any bridg	essible por- her than ways •) of re, including ls or bridge ents	From ordinarily inac- cessible portions <sup>b</sup> of bridges (other than brick, concrete, or masoury) and from abutments					
	For con- ductors attached to bridge •	For con- ductors not attached to bridge		For con- ductors not attached to bridge <sup>d</sup>				
0 to 2,500	Feet 3.0	<i>Fect</i> 3.0	<i>Feet</i> 0. 5	Feet 3.0				
Over 2,500 to 5,000	3.0	3.0	1.0	3.0				
Over 5,000 to 7,500	3.0	3.0	3.0	3.0				
Over 7,500 to 15,000	5.0	5.0	5.0	5.0				
Over 15,000 to 25,000	7.5	7.5	7.5	7.5				
Over 25,000 to 35,000	7.5	9.0	7.5	9.0				
Over 35,000 to 50,000	7.5	12.0	7.5	12.0				

Where over traveled ways on or near bridges the clearances of rule 232 apply.
 Bridge seats of steel bridges carried on masonry, brick, or concrete abutments which require frequent access for inspection shall be considered as readily accessible portions.

· Conductors should have clearance not less than given in this column, where practicable. <sup>d</sup> Conductors should have the clearances given in this column increased as much as practicable.

- 234. CLEARANCES OF CONDUCTORS OF ONE LINE FROM OTHER CONDUCTORS AND STRUCTURES—Continued.
  - D. Clearances from Bridges—Continued.
    - 2. GUARDING TROLLEY CONTACT CONDUCTORS LO-CAJED UNDER BRIDGES.
      - (a) WHERE GUARDING IS REQUIRED. Guarding is required where the trolley contact conductor is located so that a trolley pole leaving the conductor can make simultaneous contact between it and the bridge structure.
      - (b) NATURE OF GUARDING. Guarding shall consist of a substantial inverted trough of nonconducting material located above the contact conductor, or of other suitable means of preventing contact between the trolley pole and the bridge structure.
- 235. MINIMUM LINE-CONDUCTOR CLEARANCES AND SEPA-RATIONS AT SUPPORTS.

### A. Separation Between Conductors on Pole Lines.

- 1. APPLICATION OF RULE.
  - (a) MULTI-CONDUCTOR WIRES OR CABLES. Cables, and duplex, triple or paired conductors supported on insulators or messengers, whether single or grouped, are for the purposes of this rule considered single conductors even though they may contain individual conductors not of the same phase or polarity.

- 235. MINIMUM LINE-CONDUCTOR CLEARANCES AND SEPA-RATIONS AT SUPPORTS—Continued.
  - A. Separation Between Conductors on Pole Lines— Continued.
    - 1. APPLICATION OF RULE-continued;
      - (b) CONDUCTORS SUPPORTED BY MESSENGERS OR SPAN WIRES. Clearances between individual wires or cables supported by the same messenger, or between any group and its supporting messenger, or between a trolley feeder supply conductor, or communication conductor, and their respective supporting span wires, are not subject to the provisions of this rule.
      - (c) MEASUREMENT OF CLEARANCES. The clearances and separations stated may be measured from the center of the supporting insulator instead of from the conductor itself.
    - 2. HORIZONTAL SEPARATIONS BETWEEN LINE CON-DUCTORS.
      - (a) FIXED SUPPORTS. Line conductors attached to fixed supports shall have horizontal separations from each other not less than the larger value required by either (1) or (2) below for the situation concerned.

*Exception 1.*—The pin spacing at buckarm construction may be reduced as specified in rule 236, F, to provide climbing space.

*Exception 2.*—The pin spacing at bridge fixtures may be reduced as specified in rule 235, C.

Exception 3.—Grades D, E, and N need meet only the requirements of (1) below.

- 235. MINIMUM LINE-CONDUCTOR CLEARANCES AND SEPA-RATIONS AT SUPPORTS-Continued.
  - A. Separation Between Conductors on Pole Lines-Continued.
    - 2. HORIZONTAL SEPARATIONS BETWEEN LINE CON-DUCTORS-continued.
      - (a) FIXED SUPPORTS—Continued.
        - (1) MINIMUM HORIZONTAL SEPARATION BE-TWEEN LINE CONDUCTORS OF THE SAME OR DIFFERENT CIRCUITS. Separations shall be not less than given in Table 6:

		aration at Supports Between or Different Circuits
Class of circuit	Separa- tion	Notes
Communication conductors	Inches 6	Preferable minimum. Does not apply at conductor transposition points.
	3	Permitted where pin spacings less than 6 inches have been in regular use. Does not apply at conductor transposition points.
Railway feeders: 0 to 750 volts, No. 4/0 or larger	6	
0 to 750 volts, smaller than No. 4/0	12	Where 10 to 12 inch separation has
750 volts to 7,500 volts	12	already been established by prac- tice, it may be continued, subject to
Other supply conductors: 0 to 7,500 volts	12	the provisions of rule 235, A, 2, (a), (2), for spans having apparent sags not over 3 feet and for voltages not exceeding 7,500.
For all conductors of more than 7,500 volts add for each 1,000 volts in excess of 7,500 volts	0.4	

25804°-27-5

- 235. MINIMUM LINE-CONDUCTOR CLEARANCES AND SEPA-RATIONS AT SUPPORTS-Continued.
  - A. Separation Between Conductors on Pole Lines-Con.
    - 2. HORIZONTAL SEPARATIONS BETWEEN LINE CON-DUCTORS-continued.
      - (a) FIXED SUPPORTS-Continued.
        - (2) SEPARATIONS ACCORDING TO SAGS. The separation at the supports of conductors of the same or different circuits of grades A, B, or C shall in no case be less than the values given by the following formulas, at 60° F. without wind. The requirements of rule 235, A, 2, (a), (1) apply if they give a greater separation than this rule.

For line conductors smaller than No. 2. A. W. G.:

Separation = 0.3 inch per kilovolt +  $7\sqrt{\frac{S}{3}}$  - 8.

For line conductors of No. 2. A. W. G. or larger:

Separation = 0.3 inch per kilovolt +  $8\sqrt{\frac{S}{12}}$ 

where S is the apparent sag in inches of the conductor having the greater sag, and the separation is in inches.

Table 7.—Separ ductors							)n-
Sag (in inches)							
Voltages	36	48	72	96	120	180	240
750	14.0 14.5	20. 0 20. 5	28. 0 28. 5	34. 5 35. 0	40. 0 40. 5	50. 5 51. 0	59.5 60.0
6,600 13,200	$16.0 \\ 18.0$	22.0 24.0	$30.0 \\ 32.0$	36.5 38.5	41.5 43.5	52. 5 54. 5	$\begin{array}{c} 61.5\\ 63.5 \end{array}$
22,000 33,000 44,000	20.5 24.0 27.0	26.5 29.5 33.0	34.5 38.0 41.0	41.0 44.0 47.5	$\begin{array}{c} 46.\ 0\\ 49.\ 5\\ 53.\ 0\end{array}$	57.0 60.5 63.5	66.0 69.5 72.5
66,000		39. 5	48.0	54.0	59. 5	70.5	79.0

- 235. MINIMUM LINE-CONDUCTOR CLEARANCES AND SEPA-RATIONS AT SUPPORTS—Continued.
  - A. Separation Between Conductors on Pole Lines-Continued.
    - 2. HORIZONTAL SEPARATIONS BETWEEN LINE CON-DUCTORS—continued.

Table 8.—Separation in Inches Required for Line Con- ductors of Size No. 2 A. W. G. or Larger										
Voltages	Sag (in inches)									
	36	48	72	96	120	180	240			
750 2, 200 6, 600 13, 200 22, 000 33, 000 44, 000 66, 000	14.0 14.5 16.0 18.0 20.5 24.0 27.0	16. 0 16. 5 18. 0 20. 0 22. 5 26. 0 29. 0 36. 0	20. 0 20. 5 21. 5 23. 5 26. 0 29. 5 33. 0 39. 5	23. 0 23. 5 24. 5 26. 5 29. 0 32. 5 36. 0 42. 5	25. 5 26. 0 27. 5 29. 5 32. 0 35. 0 38. 5 45. 0	31. 0 31. 5 33. 0 35. 0 37. 5 41. 0 44. 0 51. 0	36. 0 36. 5 38. 0 39. 5 42. 5 45. 5 49. 0 55. 5			

(a) FIXED SUPPORTS—Continued.

(b) SUSPENSION INSULATORS NOT RESTRAINED FROM MOVEMENT. Where suspension insulators are used and are not restrained from movement, the conductor separation shall be increased so that one string of line insulators may swing transversely through an angle of 45° from a vertical position without reducing the values given in (a) above.

- 235. MINIMUM LINE-CONDUCTOR CLEARANCES AND SEPA-RATIONS AT SUPPORTS—Continued.
  - A. Separation Between Conductors on Pole Lines-Continued.
    - 3. CLEARANCES IN ANY DIRECTION FROM LINE CON-DUCTORS TO SUPPORTS, AND TO VERTICAL OR LATERAL CONDUCTORS, SPAN OR GUY WIRES, ATTACHED TO THE SAME SUPPORT.
      - (a) FIXED SUPPORTS. Clearances shall be not less than given in Table 9.

Table 9.—Minimum Clearance in Any Direction from Line Conductors to Supports, and to Vertical or Lateral Conductors, Span or Guy Wire, Attached to the Same Support

	ri		1		
	Communica- tion lines		Supply lines		
Clearance of line conductors from—		On jointly used poles	0 to 7,5 In gen- eral	00 volts On jointly used poles	Exceed- ing 7,500 volts add for each 1,000 volts of excess
Vertical and lateral conductors: Of same circuit Of other circuits	Inches 3 3	Inches 3 3	Inches 3 6	Inches 3 6	Inches 0.25 .4
Span and guy wires attached to same pole: General	( <sup>b</sup> ) <sup>3</sup>	o (j (b)	6 . (b)	(b) <sup>6</sup>	.4 .4
Lightning protection wires parallel to line	(b)	(b)	(b)	(b)	.4
Surfaces of cross arms	• 3	¢ 3	3	3	. 25
Surfaces of poles.	• 3	° 5	3	d 5	. 25

<sup>a</sup> If practicable.

<sup>b</sup> Clearance shall not be less than the separation required by Table 6 or rule 235, A, 2, (a), (2) between two line conductors of the voltage concerned.

<sup>6</sup> Communication conductors may be attached to supports on the sides or bottoms of cross arms or surfaces of poles if at least 40 inches from any supply line of less than 7,500 volts and at least 60 inches from any supply line of more than 7,500 volts carried on the same pole.

<sup>d</sup> This clearance applies only to supply conductors carried on cross arms below communication conductors on joint poles. Where supply conductors are above communication conductors the clearance shall be at least 3 inches.

- 235. MINIMUM LINE-CONDUCTOR CLEARANCES AND SEPA-RATIONS AT SUPPORTS—Continued.
  - A. Separation Between Conductors on Pole Lines— Continued.
    - 3. CLEARANCES IN ANY DIRECTION FROM LINE CON-DUCTORS TO SUPPORTS, AND TO VERTICAL OR LATERAL CONDUCTORS, SPAN OR GUY WIRES, ATTACHED TO THE SAME SUPPORT—continued.
      - (b) SUSPENSION INSULATORS NOT RESTRAINED FROM MOVEMENT. Where suspension insulators are used and are not restrained from movement, the conductor clearances from surfaces of supports, from span or guy wires, or from vertical or lateral conductors shall be such that the values of clearances required by (a) above will be maintained with an insulator swing of 45° from the vertical position.
    - 4. CONDUCTOR SEPARATION—VERTICAL RACKS.

Conductors or cables may be carried on vertical racks at one side of the pole with a vertical separation of at least 4 inches if all the following conditions are met:

- (a) The voltage of conductors shall be not more than 750 volts, except that cables having permanently grounded continuous metal sheath may carry any voltage.
- (b) Conductors shall be of the same material or materials.

(c) Spans shall not average more than 150 feet. (See Table 9, rule 235, A, 3, for necessary clearances from pole surfaces and rule 236, G, 1, for method of providing climbing space.)

- 235. MINIMUM LINE-CONDUCTOR CLEARANCES AND SEPA-RATIONS AT SUPPORTS—Continued.
  - A. Separation Between Conductors on Pole Lines— Continued.
    - 5. SEPARATION BETWEEN SUPPLY LINES OF DIFFER-ENT VOLTAGE CLASSIFICATIONS ON THE SAME CROSS ARM.

Supply lines of any one voltage classification as given in Table 11 (rule 238, A, 1) may be maintained on the same cross arm with supply lines of the next consecutive voltage classification only under the following conditions:

- (a) If they occupy pin positions on opposite sides of the pole.
- (b) If in bridge-arm or side-arm construction they are separated by a distance of not less than the climbing space required for the higher voltage concerned and provided for in rule 236.
- (c) If the higher-voltage conductors occupy the outer pin positions and the lower-voltage conductors the inner pin positions.
- (d) If series lighting or similar circuits, which are ordinarily dead during periods of work on or above the cross arm concerned, occupy the inner pin position and the lower-voltage conductors occupy the outer pin position.
- (e) If the two lines concerned are communication lines used in the operation of supply lines, and supply lines of less than 7,500 volts, and are owned by the same utility, provided they are installed as in (a) or (b) above.

- 235. MINIMUM LINE-CONDUCTOR CLEARANCES AND SEPA-RATIONS AT SUPPORTS—Continued.
  - B. Separation Between Conductors Attached to Buildings.

Separation of wires from each other shall not be less than those required in Table 6 (rule 235, A, 2, (a), (1)) for separation of conductors from each other at supports.

*Exception.*—Conductors on vertical racks meeting the requirements of rule 235, A, 4, may have a separation of 4 inches.

C. Separation Between Conductors Attached to Bridges. Supply conductors attached to bridges and supported at frequent intervals may have less separation at supports than required by rule 235, A, 2, (a), (1), and (2). The separation shall not be less than the clearance between supply conductors and the surfaces of poles or cross arms required by rule 235, A, 3, (a), or less than the following:

Span length:	inches
0 to 20 feet	6
20 to 50 feet	

## 236. CLIMBING SPACE.

# A. Location and Dimensions.

- 1. A climbing space having the horizontal dimensions specified in rule 236, E, shall be provided past any conductors, cross arms, or other parts.
- 2. The climbing space need be provided on one side or corner of the pole only.
- The climbing space shall extend vertically past any conductor or other part between levels above and below the conductor as specified in rule 236, E, F, G, and I, but may otherwise be shifted from any side or corner of the pole to any other side or corner.

- 236. CLIMBING SPACE—Continued.
  - **B.** Portions of Supporting Structures in Climbing Space. Portions of the pole or structure when included in one side or corner of the climbing space at buck or reverse-arm construction are not considered to obstruct the climbing space.
  - C. Cross Arm Location Relative to Climbing Space. Recommendation.—Cross arms should be located on the same side of the pole.

*Exception.*—This recommendation does not apply where double cross arms are used on any pole or where cross arms on any pole are not all parallel.

D. Location of Supply Apparatus Relative to Climbing Space.

Transformers, regulators, lightning arresters, and switches when located below conductors or other attachments shall be mounted outside of the climbing space.

- E. Climbing Space Through Conductors on Cross Arms.
  - 1. CONDUCTORS OF SAME VOLTAGE CLASSIFICATION ON SAME CROSS ARM.

Climbing space between conductors shall be of the horizontal dimensions specified in Table 10 (rule 236, E, 3), and shall be provided both along and across the line, and shall be projected vertically not less than 4 feet above and below the limiting conductors. Where communication conductors are above supply conductors of more than 7,500 volts, the climbing space shall be projected vertically at least 6 feet above the highest supply conductor.

*Exception.*—This rule does not apply if it is the unvarying practice of the employers concerned to prohibit employees from ascending beyond the conductors of the given line, unless the line is killed.

# 236. CLIMBING SPACE—Continued.

- E. Climbing Space Through Conductors on Cross Arms—Continued.
  - 2. CONDUCTORS OF DIFFERENT VOLTAGE CLASSIFICA-TIONS ON THE SAME CROSS ARM.

The climbing space shall be that required by Table 10 (rule 236, E, 3) for the highest voltage of any conductor bounding the climbing space.

3. HORIZONTAL CLIMBING SPACE DIMENSIONS.

Table 10	—Minimu	m Horize	ontal Dim	ensions (	of Climbi	ng S <mark>pace</mark>					
			Horizontal dimensions of climbing space (inches)								
Character of conductors adjacent to climbing space	Voltage of	conductors	On poles u by	used solely	On jointly	y used poles					
	To ground	Between wires	Communi- cation con- ductors	Supply conductor <sub>S</sub>	Supply conductors above com- munication conductors	Communica- tion conduc- tors above supply con- ductors <sup>a</sup>					
Communica- cation con- ductors.	0 to 150		No require- ment.		()	No require- ment.					
ductors.	Exceeding 150.		24 recom- mended.		(b)	24 recom- mended.					
	Less than 300.			24	24	30					
Cupple oon	300 to	7,500		30	30	30					
Supply con- ductors.	{	7,500 to 15,000.		36	36	36					
		Exceeding 15,000.		More than ¢ 36.	More than ¢ 36.	More than ¢ 36.					

• This relation of levels is not, in general, desirable and should be avoided where practicable. • The climbing space shall be the same as required for the supply conductors immediately above.

• Where practicable. Attention is called to the operating requirements of rule 422.

- 236. CLIMBING SPACE—Continued.
  - F. Climbing Space on Buckarm Construction.

The full width of climbing space shall be maintained on buckarm construction and shall extend vertically in the same position at least 4 feet (or 6 feet where required by rule 236, E, 1) above and below any limiting conductor.

Method of Providing Climbing Space on Buckarm Construction.

With circuits of less than 7,500 volts and span lengths not exceeding 150 feet and sags not exceeding 15 inches for wires of No. 2 and larger sizes, or 30 inches for wires smaller than No. 2, a six-pin cross arm having pin spacing of  $14\frac{1}{2}$  inches may be used to provide a 30-inch climbing space on one corner of a junction pole by omitting the pole pins on all arms, and inserting pins midway between the remaining pins so as to give a spacing of  $7\frac{1}{2}$  inches, provided that each conductor on the end of every arm is tied to the same side of its insulator, and that the spacing on the next pole is not less than  $14\frac{1}{2}$ inches.

## G. Climbing Space for Longitudinal Runs.

1. GENERAL.

The full width of climbing space shall be provided past longitudinal runs and shall extend vertically in the same position from 4 feet below the run to a point 4 feet above (or 6 feet where required by rule 236, E, 1). The width of climbing space shall be measured from the longitudinal run concerned. 236. CLIMBING SPACE—Continued.

## G. Climbing Space for Longitudinal Runs-Continued.

- 1. GENERAL—continued.
  - *Exception.*—If a supply longitudinal run is placed on the side or corner of the pole where climbing space is provided, the width of climbing space shall be measured horizontally from the center of the pole to the nearest supply conductors on cross arms, under the following conditions:
    - Where the longitudinal run consists of open supply conductors carrying not more than 750 volts or of permanently grounded continuous metal-sheathed supply cable carrying any voltage, and is supported close to the pole as by brackets, racks, or pins close to the pole, and
    - Where the nearest supply conductors on cross arms are parallel to and on the same side of the pole as the longitudinal run and within 4 feet above or below the run.
- 2. PROTECTION OF LONGITUDINAL RUNS.

If a longitudinal run is located between points 2 feet and 6 feet below supply line conductors carried on cross arms, it shall be protected by a suitable guard arm securely fastened to the pole, or by substantial insulating conduit. Such protection shall extend to the following distances from the pole center:

Longitudinal runs in general	20
Longitudinal runs of grounded metal-sheath cable	
uninsulated from metal supports attached to	
the pole	<b>24</b>

## H. Climbing Space Past Vertical Conductors.

Vertical runs incased in suitable conduit or other protective covering and securely attached to the surface of the pole or structure are not considered to obstruct the climbing space.

# 236. CLIMBING SPACE—Continued.

I. Climbing Space Near Ridge-Pin Conductors.

The climbing space specified in rule 236, E, 3 shall be provided above the top cross arm and past the ridge-pin conductor.

*Exception.*—Where a single cross arm carrying only two conductors is mounted so that the conductors are 2 feet below a single ridge-pin conductor, the climbing space specified in rule 236, E, 3 shall be carried up to the ridge-pin conductor, but need not be carried past it.

237. LATERAL WORKING SPACE.

## A. Location of Working Spaces.

Working spaces shall be provided on the climbing face of the pole at each side of the climbing space.

## B. Dimensions of Working Spaces.

1. ALONG THE CROSS ARM.

The working space shall extend from the climbing space to the outmost pin position on the cross arm.

2. PERPENDICULAR TO THE CROSS ARM.

The working space shall have the same dimension as the climbing space (see rule 236, E). This dimension shall be measured from the face of the cross arm.

**3.** VERTICALLY.

The working space shall have a height not less than that required by rule 238 for the vertical separation of line conductors carried at different levels on the same support.

- 237. LATERAL WORKING SPACE-Continued.
  - C. Location of Vertical and Lateral Conductors Relative to Working Spaces.

The working spaces shall not be obstructed by vertical or lateral conductors. Such conductors shall be located on the opposite side of the pole from the climbing side or on the climbing side of the pole at a distance from the cross arms at least as great as the width of climbing space required for the highest-voltage conductors concerned. Vertical conductors inclosed in suitable conduit may be attached on the climbing side of the pole.

**D.** Location of Buck Arms Relative to Working Spaces. Buck arms may be used under any of the following conditions, provided the climbing space is maintained. Climbing space may be obtained as in rule 236, F.

1. STANDARD HEIGHT OF WORKING SPACE.

Lateral working space of the height required by Table 11 (rule 238, A, 1) may be provided between the buck arms and adjacent line arms to which conductors on the buck arms are not attached.

Method of meeting requirements. This may be accomplished by increasing the spacing between the line cross arm gains.

- 237. LATERAL WORKING SPACE-Continued.
  - D. Location of Buck Arms Relative to Working Spaces-Continued.
    - 2. REDUCED HEIGHT OF WORKING SPACE.

Where no circuits exceeding 7,500 volts between conductors are involved, and the clearances of rules 235, A, 2, (a), (1) and (2) are maintained, buck arms may be placed between line arms having normal spacing, even though such buck arms obstruct the normal working space; provided that a working space of not less than 18 inches in height is maintained either above or below each line arm and each buck arm.

238. VERTICAL SEPARATION BETWEEN LINE CONDUCTORS, CABLES, AND EQUIPMENT LOCATED AT DIFFERENT LEVELS ON THE SAME POLE OR STRUCTURE.

All line conductors, cables, or equipment located at different levels on the same pole or structure shall have the vertical separations set forth below.

A. Vertical Separations Between Horizontal Cross Arms.

Cross arms supporting line conductors shall be spaced in accordance with Table 11.

1. BASIC SEPARATIONS.

The separations given in the following table are for cross arms carrying conductors of 0 to 50,000 volts attached to fixed supports.

Table 11.—Vertical Separation of	f Cross A	Arms C	Carryin	g Cond	luctors							
	Supply conductors; preferably at higher levels											
	0 to 750 volts and perma- nently			15,000 to 50,000 volts								
Conductors usually at lower levels	ground- ed con- tinous metal- sheath cables of all volt- ages	750 to 7,500 volts	7,500 to 15,000 volts	Same utility	Differ- ent utilities							
Communication conductors: General Used in operation of supply lines	a b 4 2	4 د 2	6 4	4	6 6							
Supply conductors: 0 to 750 volts	2	d 2	4	4	6							
750 volts to 7,500 volts		<sup>d</sup> 2	4	4	6							
7,500 volts to 15,000 volts— If worked on alive with long-handled tools, and adjacent circuits are neither killed nor covered with shields or protectors			4	4	6							
If not worked on alive except when adjacent circuits (either above or below) are killed or covered by shields or protectors, or by the use of long-handled tools not requiring linemen to go between live wires.			2	• 4	e 4							
Exceeding 15,000 volts, but not exceed- ing 50,000 volts				• 4	• 4							

<sup>o</sup> Where supply circuits of 550 volts or less, with transmitted power of 1,600 watts or less, are run below communication circuits in accordance with rule 220, B, 3 the clearance may be reduced to 2 feet.

<sup>b</sup> In localities where the practice has been established of placing on jointly used poles, cross arms carrying supply circuits of less than 300 volts to ground and cross arms carrying communication circuits at a vertical separation less than specified in the table, such existing construction may be continued until the said poles are replaced provided that-

The minimum separation between existing cross arms is not less than 2 feet, and that-Extensions to the existing construction shall conform to the clearance requirements specified in Table 11.

When communication conductors are all in cable, a supply cross arm carrying only wires of not more than 309 volts to ground may be placed at not less than 2 feet above the point of attachment of the cable to the pole provided that—

The nearest supply wire on such cross arm shall be at least 30 inches horizontally from the center of the pole, and that— The cable be placed so as not otherwise to obstruct the climbing space.

• This shall be increased to 4 feet when the communication conductors are carried above supply conductors unless the communication-line-conductor size is that required for grade C supply lines. Where conductors are operated by different utilities, a minimum vertical spacing of 4 feet is

recommended.

• These values do not apply to adjacent cross arms carrying phases of the same circuit or circuits.

- 238. VERTICAL SEPARATION BETWEEN LINE CONDUCTORS, CABLES, AND EQUIPMENT LOCATED AT DIFFERENT LEVELS ON THE SAME POLE OR STRUCTURE—Continued.
  - A. Vertical Separations Between Horizontal Cross Arms—Continued.
    - 2. INCREASED SEPARATIONS FOR VOLTAGES EXCEED-ING 50,000.

For voltages greater than 50,000, the clearances of Table 11 shall be increased at the rate of 0.4 inch per 1,000 volts of the excess.

B. Vertical Separation Between Line Conductors on Horizontal Cross Arms.

Where line conductors are supported on horizontal cross arms spaced as required in rule 238, A the vertical separation between such conductors shall be not less than the following:

1. WHERE CONDUCTORS ON THE CROSS ARM ARE OF THE SAME VOLTAGE CLASSIFICATION.

Under these conditions, the vertical separation required by Table 11 may be reduced as follows:

Where cross arm separation required by Table 11 is	Separa conduc reduce	tion between etors may be d to—
2 feet		16 inches.
4 feet		40 inches.
6 feet		60 inches.

2. WHERE CONDUCTORS OF DIFFERENT VOLTAGE CLASSIFICATIONS ARE ON SAME CROSS ARM.

Under these conditions, the vertical separation between conductors on adjacent cross arms shall be that required by Table 11 (rule 233 A, 1) above for the highest voltage classification concerned.

- 238. VERTICAL SEPARATION BETWEEN LINE CONDUCTORS, CABLES, AND EQUIPMENT LOCATED AT DIFFERENT LEVELS ON THE SAME POLE OR STRUCTURE—Continued.
  - B. Vertical Separation Between Line Conductors on Horizontal Cross Arms—Continued.
    - 3. CONDUCTORS OF DIFFERENT SAGS ON SAME SUP-PORT.
      - (a) VARIATION IN CLEARANCE. Line conductors supported at different levels on the same structure and strung to different sags shall have vertical spacings at the supporting structures so adjusted that the minimum spacing at any point in the span, at 60° F. with no wind, shall not be reduced more than 25 per cent from that required at the supports by rules 235, A, 2, (a), (1) and (2) and this rule.
      - (b) READJUSTMENT OF SAGS. Sags should be readjusted when necessary to accomplish the foregoing, but not reduced sufficiently to conflict with the requirements of rule 261, F, 4. In cases where conductors of different sizes are strung to the same sag for the sake of appearance or to maintain unreduced clearance throughout storms, the chosen sag should be such as will keep the smallest conductor involved in compliance with the sag requirements of rule 261, F, 4.

25804°-27-6

- 238. VERTICAL SEPARATION BETWEEN LINE CONDUCTORS, CABLES, AND EQUIPMENT LOCATED AT DIFFERENT LEVELS ON THE SAME POLE OR STRUCTURE—Continued.
  - C. Separation in Any Direction.

The separation in any direction between conductors of the same or different voltage classification when carried on the same structure, but on cross arms which are not horizontal, shall not be less than the values given in Table 11 (rule 238, A, 1 and 2) for vertical separation.

The separation in any direction shall not in any case be less than the horizontal separation specified in rule 235, A, 2, (a), (1) and (2).

D. Vertical Separation for Line Conductors Not Carried on Cross Arms.

The vertical separation between conductors not carried on cross arms shall be the same as required in rule 238, A, 1 and 2 for cross arms.

*Exception.*—Conductors on vertical racks may have a vertical separation of 4 inches under the conditions specified in rule 235, A, 4.

E. Vertical Separation Between Conductors and Noncurrent-Carrying Metal Parts of Equipment.

For the purpose of measuring these separations metal supports for conductors are considered as noncurrent-carrying metal parts of equipment.

1. BETWEEN SUPPLY CONDUCTORS AND COMMUNI-CATION EQUIPMENT.

The vertical separations specified in Table 11 (rule 238, A, 1) as 4 feet, may be reduced to 40 inches where the voltage of the supply conductors does not exceed 750, or where supply conductors of any voltage are in permanently grounded continuous-metal-sheath cable.

- 238. VERTICAL SEPARATION BETWEEN LINE CONDUCTORS, CABLES, AND EQUIPMENT LOCATED AT DIFFERENT LEVELS ON THE SAME POLE OR STRUCTURE—Continued.
  - E. Vertical Separation Between Conductors and Noncurrent-Carrying Metal Parts of Equipment—Continued.
    - 2. BETWEEN COMMUNICATION CONDUCTORS AND SUP-PLY EQUIPMENT.

The vertical separations specified in Table 11 (rule 238, A, 1) as 4 and 6 feet, may be reduced to 40 inches and 60 inches, respectively.

- 3. BETWEEN SUPPLY AND COMMUNICATION EQUIP-MENT.
  - (a) GENERAL. The vertical separation specified in Table 11 (rule 238, A, 1) as 4 and 6 feet, may be reduced to 40 inches and 60 inches, respectively.
  - (b) SPECIAL SEPARATIONS FOR SPAN WIRES OR BRACKETS. Span wires or brackets for lamps or trolley contact conductors shall have at least the vertical separation from communication equipment set forth below.

From cross arms carrying communica-

tion conductors\_\_\_\_\_2 feet From messenger wires carrying commu-

nication cables\_\_\_\_\_\_1 foot From terminal box of communication cables, if practicable\_\_\_\_\_\_1 foot

*Exception.*—Where it is not practicable to obtain a clearance of 1 foot from terminal boxes of communication cables, all metal parts of terminals shall have the greatest practicable separation from fixtures or span wires, including all supporting screws and bolts of both attachments.

- 238. VERTICAL SEPARATION BETWEEN LINE CONDUCTORS, CABLES, AND EQUIPMENT LOCATED AT DIFFERENT LEVELS ON THE SAME POLE OR STRUCTURE—Continued.
  - E. Vertical Separation Between Conductors and Noncurrent-Carrying Metal Parts of Equipment—Con.
    - 4. SUPPLY CROSS-ARM BRACES CONSIDERED AS EQUIPMENT.

Where supply cross-arm braces are less than 1 inch from transformer cases or hangers, the vertical separation from communication equipment shall be measured from the nearest part of this supply equipment, including the cross-arm brace.

F. Vertical Separation Between Communication Conductors Carried at Different Levels on Railroad Crossing Poles.

At crossings of communication lines over railroads, the vertical clearance between conductors supported on the same pole or structure and at different levels shall in no case be less than 12 inches and preferably shall be 24 inches.

Exception.—Transpositions are excepted.

239. CLEARANCES OF VERTICAL AND LATERAL CONDUCTORS FROM OTHER WIRES AND SURFACES ON THE SAME SUPPORT.

Vertical and lateral conductors shall have the clearances and separations required by this rule from other conductors, wires, or surfaces on the same support.

- Exception 1.—This rule does not prohibit the placing of supply circuits of the same or next voltage classification in the same iron pipe, if each circuit or set of wires be inclosed in a metal sheath.
- *Exception 2.*—This rule does not prohibit the placing of paired communication conductors in rings attached directly to the pole or to suspension strand.

- 239. CLEARANCES OF VERTICAL AND LATERAL CONDUCTORS FROM OTHER WIRES AND SURFACES ON THE SAME SUPPORT—Continued.
  - A. Location of Vertical or Lateral Conductors Relative to Climbing Spaces, Working Spaces, and Pole Steps.

Vertical or lateral conductors shall be located so that they do not obstruct climbing spaces, or lateral working spaces between line conductors at different levels or interfere with the safe use of existing pole steps.

*Exception 1.*—This rule does not apply to portions of the pole which workmen do not ascend while the conductors in question are alive.

Exception 2.—This rule does not apply to vertical runs incased in suitable conduit or other protective covering. (See rule 236, H.)

B. Conductors not in Conduit.

Conductors not incased in conduit shall have the same clearances from conduits as from other surfaces of structures.

C. Mechanical Protection near Ground.

Where within 8 feet from the ground, all vertical conductors, cables, and grounding wires shall be protected by a covering which gives suitable mechanical protection. For grounding wires from lightning arresters, the protective covering specified above shall be of wood molding, or other insulating material giving equivalent protection.

- *Exception 1.*—This covering may be omitted for armored cables or cables installed in a grounded metal conduit.
- Exception 2.—This covering may be omitted for lead-sheathed cables in rural districts.
- *Exception 3.*—This covering may be omitted for communication circuits on private fenced rights of way in the case of conductors or cables from underground systems.

- 239. CLEARANCES OF VERTICAL AND LATERAL CONDUCTORS FROM OTHER WIRES AND SURFACES ON THE SAME SUPPORT—Continued.
  - C. Mechanical Protection near Ground-Continued.
    - *Exception 4.*—This covering may be omitted for grounding wires in rural districts having triplebraid weather-proof covering, or where such grounding wire is one of a number of grounding wires used to provide multiple grounds.
  - D. Requirements for Vertical and Lateral Supply Conductors on Supply Line Poles or Within Supply Space on Jointly Used Poles.
    - 1. GENERAL CLEARANCES

In general, clearances shall be not less than the values specified in Table 12.

Table 12							
	Clearances (in inches) for highest voltage concerned in the clearance						
Clearance of vertical and lateral conductors	0 to 7,500 volts	Exceeding 7,500 volts (add the fol- lowing for each 1,000 in excess)					
From surfaces of supports	3	0. 25					
From span, guy or messenger wires	6	. 4					
From line conductors rigidly sup- ported on fixed supports, such con- ductors being of—							
Same circuit	3	. 25					
Different circuits	6	. 4					
From line conductors not rigidly supported on fixed supports	(a)	(a)					

<sup>a</sup> The clearances shall be increased beyond the values given above from line conductors on fixed supports (See rule 235, A, 2, (b), and 3, (b)).

- 239. CLEARANCES OF VERTICAL AND LATERAL CONDUCTORS FROM OTHER WIRES AND SURFACES ON THE SAME SUPPORT—Continued.
  - D. Requirements for Vertical and Lateral Supply Conductors on Supply Line Poles or Within Supply Space on Jointly Used Poles—Continued.
    - 2. SPECIAL CASES.

The following apply only to portions of a pole which workmen ascend while the conductors in question are alive.

- (a) Vertical conductors of not more than 7,500 volts shall clear pole centers by not less than 15 inches for a distance of not less than 4 feet above and below any open supply line conductors which are not of more than 7,500 volts when the latter are carried on or within 4 feet from the pole. If the vertical conductors are of more than 7,500 volts, this clearance shall be at least 20 inches. If the supply conductors are of more than 7,500 volts, the clearance from the pole center shall apply for a distance of not less than 6 feet above and below, except as noted in (b), (c), and (d) below.
- (b) Vertical and lateral supply conductors, including grounding wires which are inclosed in insulated conduit or in metal conduit or cable protected by an insulating covering (or wood molding if wire be used having triple-braid weather-proof covering), whenever within 4 feet of open supply lines of less than 7,500 volts or within 6 feet from open supply lines of more than 7,500 volts may have less than the clearances specified in (a) above, except as provided in (c) and (d) below.

- 239. CLEARANCES OF VERTICAL AND LATERAL CONDUCTORS FROM OTHER WIRES AND SURFACES ON THE SAME SUPPORT—Continued.
  - D. Requirements for Vertical and Lateral Supply Conductors on Supply Line Poles or Within Supply Space on Jointly Used Poles—Continued.
    - 2. SPECIAL CASES—continued.
      - (c) Vertical conductors in metal-sheathed cables and grounding wires may be run without the insulating protection specified in (b) above when installed on poles used only for supply lines and employing side-arm construction, if the line conductors are carried only on the side of the pole opposite to the vertical conductors, and if climbing space is provided on the line conductor side of the pole.
      - (d) Vertical and lateral conductors of less than 7,500 volts when on poles used only for supply lines may be run on the street side of the pole in multiple-conductor cable having suitable substantial insulating covering, if such cable is held taut on standard insulators supported on pins and brackets and is arranged so that the cable shall be held at a distance of approximately 5 inches from the surface of the pole, or from any pole step.
  - E. Requirements for Vertical and Lateral Communication Conductors on Communication Line Poles or Within the Communication Space on Joint Poles.

1. CLEARANCES FROM WIRES.

The clearances and separations of vertical and lateral conductors from other conductors (except those in the same ring run) and from guy, span, or messenger wires shall be 3 inches.

- 239. CLEARANCES OF VERTICAL AND LATERAL CONDUCTORS FROM OTHER WIRES AND SURFACES ON THE SAME SUPPORT—Continued.
  - E. Requirements for Vertical and Lateral Communication Conductors on Communication Line Poles or Within the Communication Space on Joint Poles— Continued.
    - 2. CLEARANCES FROM POLE AND CROSS ARM SURFACES.

Vertical and lateral communication conductors may be attached directly to the pole or cross arm by means of rings, knobs, or brackets provided that they are rubber-insulated paired conductors and that in the case of joint poles, the clearances from open supply lines required by Table 11 (rule 238,  $\Lambda$ , 1) are observed.

F. Requirements for Vertical Supply Conductors Passing Through Communication Space on Jointly Used Poles.

Vertical supply conductors, including grounding wires, which pass through communication line space on joint poles shall be installed as follows:

1. METAL-SHEATHED SUPPLY CABLES.

Metal-sheathed supply cables shall be covered as follows:

(a) EXTENT OF COVERING. Covering shall extend from the lowest points of such cables up to the following distances above the highest communication conductors.

Kind of supply cable	Supply voltage	Distance
Metal-sheathed Permanently grounded continuous-metal- sheathed.	{0 to 7,500 Over 7,500 All voltages	Inches <sup>a</sup> 40 60 40

• This distance may be reduced to 24 inches for supply cables less than 300 volts to ground where a vertical joint-use separation of 2 feet exists or is permissible. (See footnote b to Table 11 for conditions under which this separation is permitted.)

- 239. CLEARANCES OF VERTICAL AND LATERAL CONDUCTORS FROM OTHER WIRES AND SURFACES ON THE SAME SUPPORT—Continued.
  - F. Requirements for Vertical Supply Conductors Passing Through Communication Space on Jointly Used Poles—Continued.
    - 1. METAL-SHEATHED SUPPLY CABLES—continued.
      - (b) NATURE OF COVERING. The covering shall consist of wood molding or other suitable insulating material at points higher than 8 feet above the ground.
        - *Exception 1.*—Iron pipe may be used without insulating covering at points more than 6 feet below the lowest communication wire or railway feeder or attachment.
        - Exception 2.—Iron pipe may be used throughout if covered with wood molding or other suitable insulating covering from a point 6 feet below the lowest communication wire or railway feeder or attachment to a point 40 inches or 60 inches above the highest communication wire, depending on the supply voltage.
    - 2. SUPPLY CONDUCTORS.

Supply conductors shall be installed in one of the following ways.

- (a) IN CONDUIT. Conductors of all voltages may be inclosed in the same way and to the same extent as required in 1 above for metalsheathed cables.
- (b) ON PINS AND INSULATORS. Vertical and lateral conductors of street-lighting circuits and service leads of less than 750 volts may be run on the street side of the pole in multiple-conductor cable having suitable substantial insulating covering if such cable is held taut on standard insulators supported

- 239. CLEARANCES OF VERTICAL AND LATERAL CONDUCTORS FROM OTHER WIRES AND SURFACES ON THE SAME SUPPORT—Continued.
  - F. Requirements for Vertical Supply Conductors Passing Through Communication Space on Jointly Used Poles—Continued.
    - 2. SUPPLY CONDUCTORS—continued.

on pins or brackets and arranged so that the cable shall be held at a distance of approximately 5 inches away from the surface of the pole or from any pole steps.

3. SUPPLY GROUNDING WIRES.

Supply grounding wires shall be covered with wood molding or other suitable insulating covering to the extent required for metal-sheathed cables in 1 above, the "voltage" of the grounding wire being taken as the voltage of the supply circuit with which it is associated.

4. SEPARATION FROM THROUGH BOLTS.

Vertical runs of supply conductors shall be separated from the ends of through bolts associated with communication line equipment by oneeighth of the circumference of the pole where practicable, but in no case less than 2 inches.

G. Requirements for Vertical Communication Conductors Passing Through Supply Space on Jointly Used Poles.

All vertical runs of communication conductors passing through supply space shall be installed as follows:

1. METAL-SHEATHED COMMUNICATION CABLES.

Metal-sheathed communication cables shall be covered with wood molding or other suitable insulating covering from a point not more than 8 feet above the ground to the following points above the highest supply conductor.

- 239. CLEARANCES OF VERTICAL AND LATERAL CONDUCTORS FROM OTHER WIRES AND SURFACES ON THE SAME SUPPORT—Continued.
  - G. Requirements for Vertical Communication Conductors Passing Through Supply Space on Jointly Used Poles—Continued.
    - 1. METAL-SHEATHED COMMUNICATION CABLES—continued.

Nature of supply circuit	Voltage of supply cir- cuit	Distance
Permanently grounded continuous-metal-	All voltages	Inches 40
sheathed cable. Open wire and other cable_ Open wire and other cable_		<sup>a</sup> 40 60

 $\bullet$  This distance may be reduced to 24 inches for supply voltages less than 300 volts to ground where a vertical joint-use separation of 2 feet exists or is permissible. (See footnote  $\flat$  to Table 11 for conditions under which this separation is permitted.)

#### 2. COMMUNICATION CONDUCTORS.

Vertical and lateral runs of rubber-insulated paired conductors shall be covered with wood molding or other suitable insulating covering when within 48 or 72 inches from supply conductors of 7,500 volts or less, or more than 7,500 volts, respectively.

3. COMMUNICATION GROUNDING WIRES.

Grounding wires of communication lines shall be covered with wood molding or other suitable insulating covering to the extent required for metal-sheathed cables in 1 above.

4. SEPARATION FROM THROUGH BOLTS.

Vertical runs of communication conductors shall be separated from the ends of through bolts associated with supply-line equipment by oneeighth of the circumference of the pole where practicable, but in no case less than 2 inches.

#### SEC. 24. GRADES OF CONSTRUCTION

## 240. GENERAL.

For the purposes of section 26, "Strength requirements," and section 27, "Line insulators," conductors and their supporting structures are classified under the grades specified in this section on the basis of the relative hazard existing.

241. Application of Grades of Construction to Different Situations.

## A. Supply Cables.

For the purposes of these rules supply cables are divided into two classes as follows:

#### 1. SPECIALLY INSTALLED CABLES.

In this class are included metal-sheathed supply cables installed in accordance with rule 261, G, 1. *Note.*—Such cables are sometimes permitted to have a lower grade of construction than openwire supply conductors of the same voltage.

#### 2. OTHER CABLES.

In this class are included all other supply cables.

Note.—Such cables are required to have the same grade of construction as open-wire supply conductors of the same voltage.

# B. Two or More Conditions.

In any case where two or more conditions affecting the grade of construction exist, the grade of construction used shall be the highest one required by any of the conditions.

- 241. APPLICATION OF GRADES OF CONSTRUCTION TO DIF-FERENT SITUATIONS—Continued.
  - C. Order of, Grades.

For supply and communication conductors and supporting structures, the relative order of grades is A, B, C, and N, grade A being the highest. Where grades D, E, and N are specified for communication lines, grade D is the highest.

- Note.—Grades D and E can not be directly compared with the series A, B, and C, but rule 241, D, 3, (c) provides for cases where these two conditions are present.
- D. At Crossings.
  - 1. GRADE OF UPPER LINE.

Conductors and supporting structures of a line crossing over another line shall have the grade of construction specified in rules 241, D, 3; 242, and 243.

2. GRADE OF LOWER LINE.

Conductors and supporting structures of a line crossing under another line need only have the grades of construction which would be required if the line at the higher level were not there.

- 241. Application of Grades of Construction to Dif-FERENT SITUATIONS—Continued.
  - **D.** At Crossings—Continued.
    - 3. MULTIPLE CROSSINGS.
      - (a) WHERE A LINE CROSSES IN ONE SPAN OVER Two OTHER LINES. The grade of construction of the uppermost line shall be not less than the highest grade which would be required of either one of the lower lines if it crossed the other lower line.
        - *Example.*—If a 2,300-volt line crosses in the same span over a communication line and a direct-current trolley contact conductor of more than 750 volts, the 2,300-volt line is required to comply with grade A construction at the crossing.

This is a double crossing and introduces a greater hazard than where the upper supply line crosses the communication line only.

- (b) WHERE ONE LINE CROSSES OVER A SPAN IN ANOTHER LINE, WHICH SPAN IS IN TURN INVOLVED IN A SECOND CROSSING. The grade of construction for the highest line shall be not less than that required for the next lower line.
  - *Exception.*—This requirement does not apply when the two upper lines are of such a nature and have such circuit protection that the danger of causing a break in the lower of these two lines by mechanical or electrical contact is eliminated.

- 241. Application of Grades of Construction to Dif-FERENT SITUATIONS—Continued.
  - D. At Crossings—Continued.
    - 3. MULTIPLE CROSSINGS—continued.
      - (c) WHERE COMMUNICATION CONDUCTORS CROSS OVER SUPPLY CONDUCTORS AND RAILROAD TRACKS IN THE SAME SPAN. The grades of construction shall be in accordance with Table 13.

Table 13								
	Communication con ductor grades							
When crossing over—	Major lines	Minor lines						
Main tracks and supply line of 0 to 750 volts	D	D						
Main tracks and supply line exceeding 750 volts	A	А						
Minor tracks and supply line of 0 to 750 volts	Е	Е						
Minor tracks and supply line of 750 to 7, 500 volts	в	в						
Minor tracks and supply line exceeding 7, 500 volts	A	в						

Recommendation.—It is recommended that the placing of communication conductors above supply conductors at crossings, conflicts, or on jointly used poles be avoided unless the supply conductors ar trolley contact conductors and their asso ciated feeders.

241. Application of Grades of Construction to Dif-FERENT SITUATIONS—Continued.

- E. Conflicts.
  - 1. HOW DETERMINED.

Where two lines are adjacent (except at crossing spans) the distance between them and the relative heights above ground of poles and of conductors on each line determine whether conflict exists, and, if so, whether the conflict is a structure conflict (see Definition) or a conductor conflict (see Definition), or both.

2. CONDUCTOR CONFLICT.

At conductor conflicts the grade of construction of the conflicting conductor shall be as required by rules 241, D, 3, and 242.

3. STRUCTURE CONFLICT.

At structure conflicts, the grade of construction of the conflicting structure shall be as required by rule 243.

242. GRADES OF CONSTRUCTION FOR CONDUCTORS.

The grades of construction required for conductors of all classes in different situations are given in Tables 14 and 15. For the purpose of these tables certain classes of circuits are treated as follows:

A. Status of Constant-Current Circuits.

In determining grades of construction where constant-current circuits are involved with communication circuits and are not in specially installed cable, the constant-current circuits shall be considered on the basis of their current rating. In all other cases constant-current circuits shall be considered on the basis of their nominal full-load voltage.

25804°-27-7

- 242. GRADES OF CONSTRUCTION FOR CONDUCTORS-Contd.
  - B. Status of Railway Feeders and Trolley Contact Conductors.

In determining grades of construction where railway feeders and trolley contact conductors are involved they shall be considered as other supply conductors of the same voltage.

*Exception.*—Direct-current trolley circuits exceeding 750 volts to ground shall have grade A construction where crossing over, conflicting with, or on joint poles with and above major communication circuits, and grade B where similarly situated with respect to minor communication circuits.

C. Status of Communication Circuits Used Exclusively in the Operation of Supply Lines.

In determining grades of construction where communication circuits used exclusively in the operation of supply lines are concerned, they shall be considered as ordinary communication circuits when run as such (see rule 288, C) and as supply circuits when run as such. (See rule 288, D.)

*Exception.*—Communication circuits located below supply circuits with which they are used shall not require such supply circuits to meet any rules for grade of construction other than that the sizes of such supply conductors shall not be less than required for grade C (see rule 261, F, 2).

## D. Status of Fire-Alarm Conductors.

In determining grades of construction where firealarm conductors are concerned, they shall be considered as other communication circuits.

*Exception.*—Fire-alarm conductors shall always meet grade D where the span length is from 0 to 150 feet, and grade C where the span length exceeds 150 feet.

Table 14Grades of Construction for Supply	Conductors alone, at Crossings, at Confl	icts, or on Same Poles with other Conductors
---	--	--

K	Supply conductors Constant-potential supply conductors other than 0.C. railway feeders Constant-current supply conductors conductors																		Communi	ontine ]																																								
	at hig lev	yela vela		0 tç	750 ts b		to 5 olts		5000 to 7500 Exceeding voltsd 7500 voltse							Constant-current supply conductors						ply	Di ra	rect- ilway	curr fee	ent ders	conduct used ex	ors clu-																																
	Con- ductors,				r i				0 40 7 5 7 5 40 10						0 to 7.5 7.5 to 10 Exceed-					Exceed- ing 10 amperes volts volts					sively in the operation of, and run as,																																			
ta	racks. nd rights	5		_	Rural	Urb	an 	Rural	-	ban		aral		ban v	Rur	81 	ampe	ereš a	amp	eres	ing ampe	10 108	vol	ts		750	supply	lines																																
l	f way at ower leve	els	$\searrow$	Open or Cable	Open Cable	Open	Cable	Open or Cable	Open	Cable	Open	Cable	Open	Cable	Cp∉n	Cable	Open	Cable	Open	Cabl	Open	Cable	Open	Cable	Open	Cable	Open	Cable																																
	ines on f Ights of		ed	N	N	ſŊ	N	N	f <sub>N</sub>	N	H	N	ſN	f <sub>N</sub>	ท	N	B.C.	or N.	See	mili	e 242		B C	: or		0.0	CorN	500																																
L r	ines not ights of	on i way	isnced	N	N	с	н	N	с	N	N	R	В	с	N	N	-,0,	01 11			~ _4-	.,	้ำบไ	, or e 24	2, 8		C or N rule (	242,C																																
Ra	ilroad		Main	A	A	A	A	Λ	A	A	A	٨		4	A	4	A	A	A	4	A	Å	A	A	٨	A	Å	A																																
	traoks	Ì	Minor	В	В	В	в	В	В	В	В	в	В	В	В	В	В	В	В	В	В	В	В	В	В	В	В	В																																
St	reet-rai	lway over	/ tracks rhead ctor	N	N	N	u	N	ษ	N	พ	N	N	N	N	Ŋ	N	N	N	N	N	N	พ	N	N	N	N	N																																
15	0 to J volts	50	Open	N	N	C	H	Ы	С	N	Ы	N	В	C	gC	Ħ	1				-																																							
1	NOI LS-		Cable	N	N	C	N	N	C	N	N	N	B	C	gC	H																																												
Constant-potential	750 to 5000 v		Open	hC	N	C	С	N	С	С	N	N	В	С	N	N						B, C, or N B, C, or N																																						
pot	5000 4		Cable	N	N	C	N	n	С	N	พ	N	B	С	N	N		C, c		2 1						B, C, or N																																		
ant-	5000 t 7500 volts	0	Open	hC	N	C	С	N	С	С	N	N	B	C	N	N	30	See rule 242, A See rule 242, B				4,0	See rule 242,C																																					
nst	volts	d	Cable	N	N	C	N	N	С	N	N	N	B	C	N	N																																												
ő	Exceed ing 75 volts	ōo	Open	hB	b <sub>C</sub>	B	B	N	B	В	31	N	₿	С	N	N																																												
_	volts	e	Cable	Ъс	N	С	N	N	C	N	N	N	₿	С	N	N																																												
รบ	nstant-c pply con en, or c	duct	tors		В, С	), or	N .	See n	ule 2	42,A							B, C	, or 1 24	2, A S	iee m	le		B, C rul	es 2	N. 9 42, A.	Bee B	B,C,or rules 2	N. See 42,≜,C																																
Ta.	rect-cur y feeder ble	rent s op	rail- en or		B, C, or N See r					42,B							B, C,	or N. 42, A	Seand	e rui B	les		9,0 IU	le 2	N. 9 42, B	Sea	B,C,or 1 rules 2	N. See 42, B, C																																
Ĩr du	Trolley contact con- ductors A.C. or D.C. B, C, or N. See rule 242,B											в.с <sub>2</sub>	or 1 42, A	and	ee ru B.	lles		B,C ru	ile 2	N. 42,В	See	B.C. or rules 20	N. See 42, B, C																																					
Communication con- ductors,open or ca- ble,bacd exclusively in the operation of supply lines										A, B, C, or N. See rules A, B, C, or N. See 242A and C rules 242, B, C.				B.C. or rule 20	N. See 12,C																																													
Co	municat nductors	ion	Majori	N	N	с	с	с	В	с	В	с	A	с	A	С	C	C or N See	В	C or N See	A	C or N See	N	N	A	С	B,C, or See rul	N.																																
ur	ban or r 1 open o ble	11- I	Minor <sup>i</sup>	N	N	С	С	С	С	С	С	С	В	с	В	С		rule 242A	С	rule 2424	В	rule 242A	N	N	B	с	242.C																																	

The words "open" and "cable" appearing in the column headings have the following mennings as applied to supply conductors: "Cable" means the specially installed cables described in rule 241, A, 1. "Open" means open wire and also supply cables not "specially installed."
 Voltages to neutral or ground of 0 to 440 yolts.

Voltages to neutral or ground of 440 to 2,900 volts.

d Voltages to neutral or ground of 2,900 to 4,400 volts.

Voltages to neutral or ground exceeding 4,400 volts.

f Where lines are located so that they can fall outside the fenced right of way into urban districts the construction shall comply with the grades specified for lines not on fenced rights of way for corresponding voltage. • Grade N if crossing over or conflicting with supply services. • If the wires are service drops, they may have grade N sizes and sags as set forth in Tables 32 and 33 (rule 263, E). • Where the communication conductors consist of individual paired conductors only, supply conductors in the upper position need only be grade N due to this condition.

grade N due to this condition.

25804°-27, (Face p. 74)



# 242. GRADES OF CONSTRUCTION FOR CONDUCTORS-Contd.

Table 15.—Grades of Construction for Communication Conductors Alone, or in Upper Position at Crossings, at Conflicts, or on Joint Poles

Conduc- tors, tracks and rights of way at lower	Communication of at hi	Communication conductors, rural or urban, open of cable, including communication conductors run as such, but used erclusively in the operation of supply lines				
			Major	Minor		
Lines on fend	ced rights of way		N	N		
Lines not on	fenced rights of	way	N	N		
Railroad trad	aka	Main	D	D		
hailiteau tiau	640	Minor	E	E		
Street-railwa no overhead o	ay tracks having contact wire		N	N		
ial	0 to 750 volts <sup>c</sup>	Open or cable	N	N .		
ent sb	750 to 5000 v.d	Open or cable	C	C		
tor	5000 to 7500 m B	Open	В	gc		
Constant-potential supply conductorsb	5000 to 7500 v. <sup>e</sup>	Cable	C	C		
su con	Exceeding 7500 voltsf	Open	A	В		
Cor	7500 volts <sup>I</sup>	Cable	С	С		
the last	0 to 7.5 amp.	Op <b>en<sup>i</sup></b>	С	C		
con- stant current supply conduc- tors.b	7.5 to 10 amp.	Open <sup>i</sup>	В	gC		
Cor sta	Exceeding 10 amp.	Cpen <sup>i</sup>	A	. B		
Direct-cur-	0 to 750 volts	Open or cable	N	N		
rent railway feeders <sup>b</sup>	Exceeding 750 v.	Open or cable	A	В		
Trolley contact	0 to 750 volts	A.C. or D.C.	hD	hp		
conductorsb	Exceeding 750 volts	A.C. D.C:	A.B. or C	See rule 242.B		
Communication used exclusiv Supply lines	n conductors, open vely in the opera	B, C, or N See rule 242,C				
Communication urban or rura	n conductors, open al, major or mino:	N	N			

<sup>a</sup> It is recommended that the placing of communication conductors above supply con-

It is recommended that the placing of communication conductors above supply conductors at crossings, conflicts, or jointly used poles be avoided, unless the supply conductors are trolley contact conductors and their associated feeders.
The words "open" and "cable" appearing in the headings have the following meaning is applied to supply conductors: "Cable" means the specially installed cables described in ule 241, A, 1. "Open" means open wire and also supply cables not specially installed.
Voltages to neutral or ground of 2400 volts.
Voltages to neutral or ground of 2,900 to 4,400 volts.
Voltages to neutral or ground at creding 4,400 volts.

1 Voltages to neutral or ground exceeding 4,400 volts.

• For spans 150 feet or less in length, grade C supply-conductor sizes and sags shall apply nstead of grade D as permitted by rule 261, H.
• Applies only to line-conductor sizes and sags in spans 0 to 150 feet long with following exceptions: Copper or steel, spans 0-100 feet, use No. 12 wire; steel, spans 125 to 150 feet, use No. 9 wire. For spans exceeding 150 feet, grade C supply-conductor sizes and sags shall be met. For paired conductors grade C paired-conductor requirements shall be met.
• Where constant-current circuits are in specially installed cable, they are considered on the basis of the normal full head weltare.

the basis of the nominal full-load voltage.

#### 243. Grades of Supporting Structures.

#### A. Poles or Towers.

The grade of construction shall be that required for the highest grade of conductors supported.

- Exception 1.—The grade of construction of joint poles, or poles used only by communication lines, need not be increased merely because of the fact that communication wires carried on such poles cross over trolley contact conductors of 0 to 750 volts.
- *Exception 2.*—Poles carrying grade C or D fire-alarm conductors, where alone, or where concerned only with other communication conductors, need meet only the requirements of grade N.
- *Exception 3.*—Poles carrying supply service loops of 0 to 750 volts shall have at least the grade of construction required for supply line conductors of the same voltage.
- Exception 4.—Where communication lines cross over supply conductors and a railroad in the same span and grade A or B is required by rule 241, D, 3, (c) for the communication conductors, due to the presence of railroad tracks, the grade of the poles or towers shall be D or E.
- *Exception 5.*—At structure conflicts even though no conductor conflict exists, the grade of construction which would be required by rule 242, if the conductors were in conflict, shall be applied to the pole or tower.
  - Note.—This requirement may result in a higher grade of construction for the pole or tower than for the conductors carried thereon.
- *Exception 6.*—In the case where a structure conflict does not exist, but any conductor is in conductor conflict, the grade of constructure of the pole or tower is not required to meet the conductor grade due to the conductor conflict.

243. GRADES OF SUPPORTING STRUCTURES—Continued.

B. Cross Arms.

The grade of construction shall be that required for the highest grade of conductors carried by the cross arm concerned.

- *Exception 1.*—The grade of construction of cross arms carrying only communication conductors need not be increased merely because of the fact that such conductors cross over trolley contact conductors of 0 to 750 volts.
- *Exception 2.*—Cross arms carrying grade C or D fire-alarm conductors, where alone or where concerned with other communication conductors need meet only the requirements for grade N.
- *Exception* 3.—Cross arms carrying supply service loops of 0 to 750 volts shall have at least the grade of construction required for supply line conductors of the same voltage.
- *Exception* 4.—Where communication lines cross over supply conductors and a railroad in the same span and grades A or B is required by rule 241, D, 3, (c) for the communication conductors due to the presence of railroad tracks, the grade of the cross arm shall be D or E.

#### C. Pins, Insulators, and Conductor Fastenings.

The grade of construction shall be that required for the conductor concerned.

- Exception 1.—The grade of construction of pins, insulators, and conductor fastenings carrying only communication conductors need not be increased merely because of the fact that such conductors cross over trolley contact conductors of 0 to 750 volts.
- *Exception 2.*—In case of grade C or D fire-alarm conductors where alone or where concerned only with other communication conductors, pins, insulators, and conductor fastenings need meet only the requirements for grade N.

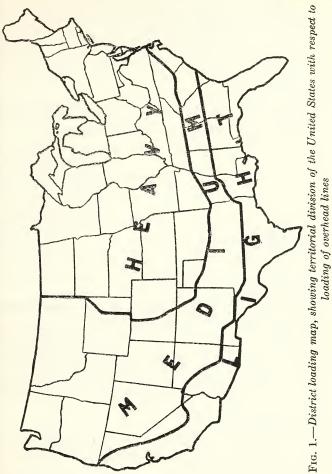
- 243. GRADES OF SUPPORTING STRUCTURES—Continued.
  - C. Pins, Insulators, and Conductor Fastenings-Con.
    - Exception 3.—In the case of supply service loops of 0 to 750 volts, pins, insulators, and conductor fastenings shall have at least the same grade of construction as required for supply line conductors of the same voltage.
    - Exception 4.—Where communication lines cross over supply conductors and a railroad in the same span, and grade A or B is required by rule 241, D, 3, (c) for the communication conductors due to the presence of railroad tracks, the grade of pins, insulators, and conductor fastenings shall be D or E.
    - *Exception 5.*—In case communication conductors are required to meet grade A, B, or C, the insulators need meet only the requirements for mechanical strength for these grades.

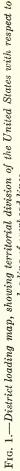
#### SEC. 25. LOADING FOR GRADES A, B, C, D, AND E

#### 250. LOADING MAP.

Three degrees of severity are recognized for the loading, due to weather conditions, and are designated, respectively, as heavy, medium, and light loading. The districts in which these loadings apply are determined by weather reports as to wind and ice and by local experience of utilities using overhead lines. It is expected that detailed districting will be carried out by State authorities, but a general districting for the entire United States is given in the map (fig. 1).

Note.—The localities in the different groups are classed according to the relative prevalence of high wind velocity and thickness of ice which accumulates on wires, light loading being, in general, for places where little, if any, ice ever accumulates on wires.





250. LOADING MAP-Continued.

Where high wind velocities are frequent in a given place the loading for that place may be classed as heavy even though ice does not accumulate to any greater extent than at some other place having less severe winds which has been classed as a medium loading district.

# 251. Assumed Weather Conditions.

The following weather conditions are assumed to act simultaneously in different loading districts:

	Thickness of ice	Horizontal wind pressure on pro- jected area of cylindrical sur- face	Tempera- ture
Heavy loading districts (H) Medium loading districts (M)_ Light loading districts (L)	Inches # 0.50 .25 None.	Lbs. per sq. ft. 8 8 12	$^{\circ F.}_{\begin{array}{c}0\\+15\\+30\end{array}}$

### 252. Modification of Loading.

In the absence of any action by the administrative authority fixing the loadings for any given territory, the classification of loadings shown on the map (fig. 1), shall apply unless the party or parties responsible for the line concerned secure approval from the administrative authority for modification, based upon local experience, or weather records, or both.

253. Conductor Loading.

The loading on conductors shall be assumed as in A, B, or C below, according to the climatic conditions of the locality concerned.

Where cables are concerned, the specified loadings shall be applied to both cable and messenger.

80 -

# 253. CONDUCTOR LOADING—Continued.

In applying loadings to bare stranded conductors, the coating of ice shall be considered as a hollow cylinder touching the outer strands.

Ice is assumed to weigh 57 pounds per cubic foot.

# A. Heavy Loading (H).

The resultant loading, due to the weight of the conductor plus the added weight of a layer of ice 0.5 inch in radial thickness, combined with a transverse horizontal wind pressure of 8 pounds per square foot on the projected area of the ice-covered conductor, shall be called heavy loading. The minimum temperature shall be assumed as 0°F.

# B. Medium Loading (M).

The resultant loading due to the weight of the conductor plus the added weight of a layer of ice 0.25 inch in radial thickness, combined with a transverse horizontal wind pressure of 8 pounds per square foot on the projected area of the ice-covered conductor, shall be called medium loading. The minimum temperature shall be assumed as  $+15^{\circ}$  F.

C. Light Loading (L).

The resultant loading due to the weight of the conductor without ice combined with a transverse horizontal wind load of 12 pounds per square foot on the projected area of the conductor, shall be called light loading. The minimum temperature shall be assumed as  $+30^{\circ}$ F.

## 254. LOADS UPON LINE SUPPORTS.

# A. Assumed Vertical Loading.

The vertical loads upon poles, towers, foundations, cross arms, pins, insulators, and conductor fastenings shall be their own weight plus the superimposed weight which they support, including all wires and cables, ice-coated in heavy and medium loading districts, together with the effect of any difference in elevation of supports. The radial thickness of ice shall be computed only upon wires, cables, and messengers, and shall be taken as the following:

Heavy loading districts (H), 0.50 inch of ice. Medium loading districts (M), 0.25 inch of ice. Light loading districts (L), no ice.

Ice is assumed to weigh 57 pounds per cubic foot. Note.—The weight of ice upon supports is ignored for the sake of simplicity. (See Appendix E, Table 81, for vertical loads of conductors.)

# B. Assumed Transverse Loading.

In computing the stresses in poles, towers, and side guys the loading shall be taken as one of the following according to climatic conditions of the locality concerned.

#### 1. HEAVY LOADING (H).

A horizontal wind pressure, at right angles to the direction of the line, of 8 pounds per square foot upon the projected area of cylindrical surfaces of all supported conductors and messengers, when covered with a layer of ice 0.5 inch in radial thickness and on surfaces of the poles and towers without ice covering, shall be called heavy loading. (See 4 and 5 following.)

## 254. LOADS UPON LINE SUPPORTS—Continued.

- B. Assumed Transverse Loading—Continued.
  - 1. HEAVY LOADING (H)-continued.

For supporting structures carrying more than 10 wires, not including cables supported by messengers, where the pin spacing does not exceed 15 inches, the transverse load shall be calculated on two-thirds of the total number of such wires with a minimum of 10 wires.

2. MEDIUM LOADING (M).

A horizontal wind pressure at right angles to the direction of the line, of 8 pounds per square foot upon the projected area of cylindrical surfaces of all supported conductors and messengers when covered with a layer of ice 0.25 inch in radial thickness and on the surfaces of the poles and towers without ice covering, shall be called medium loading. (See 4 and 5 following.)

For supporting structures carrying more than 10 wires not including cables supported by messengers, where the pin spacing does not exceed 15 inches, the transverse load shall be calculated on two-thirds of the total number of such wires with a minimum of 10 wires.

3. LIGHT LOADING (L).

A horizontal wind pressure at right angles to the direction of the line of 12 pounds per square foot upon the projected area of cylindrical surfaces of all supported conductors and messengers, poles and towers without ice covering, shall be called light loading. (See 4 and 5 following.)

- 254. LOADS UPON LINE SUPPORTS-Continued.
  - B. Assumed Transverse Loading-Continued.
    - 4. TROLLEY CONTACT CONDUCTORS.

When a trolley contact conductor is supported on a commonly used pole it shall be included in the computation of the transverse load on the structure.

5. FLAT SURFACES.

For flat surfaces the assumed unit wind pressure shall be increased by 60 per cent. Where latticed structures are concerned the actual exposed area of one lateral face shall be increased by 50 per cent to allow for the pressure on the opposite face; this total, however, need not exceed the pressure which would occur on a solid structure of the same outside dimensions. The results obtained by more exact calculations may be substituted for the values obtained by this simple rule.

6. ANGLES.

In cases where, due to change in direction of conductors, an unbalanced side pull is imposed on the supporting structure, a transverse load shall be assumed equal to the resultant of all conductor and messenger tensions, as determined by the loadings of rule 253.

- C. Assumed Longitudinal Loading.
  - 1. CHANGE IN GRADE OF CONSTRUCTION.

The longitudinal loading upon supporting structures, including poles, towers, cross arms, pins, and conductor fastenings, at ends of sections required to be of grade A or B construction when

# 254. LOADS UPON LINE SUPPORTS-Continued.

- C. Assumed Longitudinal Loading—Continued.
  - 1. CHANGE IN GRADE OF CONSTRUCTION—continued. located in lines of a lower grade of construction, shall be taken as an unbalanced pull in the direction of the higher-grade section equal to the total pull in one direction of all conductors and cables supported thereon, the conductor loading to be that given in rule 253.
    - *Exception.*—For such higher-grade sections having no span exceeding 500 feet in length where the total pull in the direction of the highergrade section exceeds 30,000 pounds, the assumed loading is modified to 30,000 pounds, plus one-fourth the excess above 30,000 pounds, with a maximum of 50,000 pounds.
  - 2. SAME GRADE OF CONSTRUCTION THROUGHOUT.

Where lines are built throughout their length, or between dead-ended points, of grade A or B construction, respectively, although not so required, the longitudinal loading upon supporting structures (including poles, towers, cross arms, pins, and conductor fastenings) at crossings, at ends of sections of joint use, and at ends of conflicts required to be of grade A or B construction, respectively, shall be taken as an unbalanced pull in the direction of the crossing, conflict, or joint-use section equal to the pull of one-third of the total number of conductors carried (not including overhead ground wires), such one-third of the conductors being selected so as to produce the maximum stress in the supports. If the application of the above results in a fractional part of a conductor, the nearest whole number shall be used

- 254. LOADS UPON LINE SUPPORTS-Continued.
  - C. Assumed Longitudinal Loading-Continued.
    - 3. JOINTLY USED POLES AT CROSSINGS OVER RAIL-ROADS OR COMMUNICATION LINES.

Where a joint line crosses over a railroad or a communication line and grade A or B is required for the crossing span, the tension in the communication conductors of the joint line may be considered as limited to one-half their breaking strength, provided they are smaller than No. 8 Stl. W. G., if of steel, or No. 6 A. W. G., if of copper, regardless of how small the initial sags of the communication conductors at 60° F.

4. DEAD ENDS.

The longitudinal loading upon supporting structures shall be taken as an unbalanced pull equal to the tensions of all conductors and messengers under the conditions of loading specified in rule 253.

5. COMMUNICATION CONDUCTORS ON UNGUYED SUP-PORTS AT RAILROAD CROSSINGS.

The longitudinal load shall be assumed equal to an unbalanced pull in the direction of the crossing, of all conductors supported, the pull of each conductor being taken as one-half its ultimate strength. 254. LOADS UPON LINE SUPPORTS—Continued.

D. Average Span Lengths.

1. GENERAL.

The calculated transverse loads, upon poles, towers, and cross arms, except as provided in 2 below, shall be based upon the average span length of a section of line that is reasonably uniform as to height, number of wires, grade, and span length. In no case shall the average value taken be less than 75 per cent or more than 125 per cent of the actual average of the two spans adjacent to the structure concerned.

2. CROSSINGS.

In the case of crossings over railroads or communication lines (other than minor communication lines) the actual lengths of the two spans adjacent to the two structures concerned shall be used.

#### E. Simultaneous Application of Loads.

- 1. When calculating transverse strength, the assumed transverse and vertical loads shall be taken as acting simultaneously.
- 2. In calculating longitudinal strength, the assumed longitudinal loads shall be taken without consideration of the vertical or transverse loads.

## SEC. 26. STRENGTH REQUIREMENTS

#### 260. PRELIMINARY ASSUMPTIONS.

In calculation of stresses no allowance shall be made for deformaton, deflection, or displacement of any part of the supporting structure, including suspension insulators.

# 261. GRADES A, B, AND C CONSTRUCTION.

# A. Poles and Towers.

The strength requirements for poles and towers may be met by the structures alone or with the aid of guys or braces.

1. AVERAGE STRENGTH OF THREE POLES.

A pole (single-base structure) not individually meeting the transverse strength requirements will be permitted when reinforced by a stronger pole on each side, if the average strength of the three poles meets the transverse strength requirements, and the weak pole has not less than 75 per cent of the required strength.

An extra pole inserted in a normal span for the purpose of supporting a service loop may be ignored, if desired, in the calculation of the strength of the line.

Exception for crossing poles.—In the case of crossings over railroads or communication lines (other than minor communication lines), the actual strengths of the crossing poles shall be used.

#### 2. REINFORCED-CONCRETE POLES.

Reinforced-concrete poles shall be of such material and dimensions as to withstand for transverse strength the loads assumed in rules 254, A and B and for longitudinal strength the loads in rule 254, C without exceeding the following percentages of their ultimate strength. (Where guys are used, see rule 261, C.)

261.	GRADES A, B, AND C CONSTRUCTION—Continued.
	A. Poles and Towers-Continued.

	Percentage of ultimate strength for different grades		
-	Grade A	Grade B	Grade C
For transverse strength (when installed) For longitudinal strength	331/3	50	75
(at all times) in general At dead-ends	$100 \\ 33\frac{1}{3}$	$\begin{array}{c} 100 \\ 50 \end{array}$	75

- 3. STEEL SUPPORTING STRUCTURES. Steel supports, steel towers, and metal poles shall be designed and constructed so as to meet the following requirements:
  - (a) TRANSVERSE STRENGTH.—Under the transverse and vertical loads assumed in rule 254, A and B the calculated stresses in steel members shall not exceed the allowable stresses for transverse strength given in (d) below.
  - (b) LONGITUDINAL STRENGTH.
     Grades A and B. Under the longitudinal loads assumed in rule 254, C the calculated steel members shall not exceed the allowable stresses for longitudinal strength given in (d) below.

Grade C. No longitudinal-strength requirements except at dead-ends.

(c) MINIMUM STRENGTH. Steel towers shall have strength sufficient to withstand a transverse load on the towers without conductors due to three times the specified transverse wind pressure, without exceeding the allowable stresses for longitudinal strength in Table 16.

25804°-27----8

- 261. GRADES A, B, AND C CONSTRUCTION-Continued.
  - A. Poles and Towers-Continued.
    - 3. STEEL SUPPORTING STRUCTURES—continued.
      - (d) ALLOWABLE UNIT STRESSES; STEEL. The values in Table 16 for structural steel are for material having an ultimate tensile stress between 55,000 and 65,000 pounds per square inch and yield point not less than 50 per cent of the ultimate stress.

In the case of special steels having higher yield points, purchased under rigid specification and inspection conditions, an allowance above the tabular stresses in proportion to the respective yield points will be permitted.

As the unit stresses in Table 16 are the maximum allowable, sufficient allowance should be made in the design to insure that in the completed structure the specified unit stresses will not be exceeded.

	Allowable	e stresses for strength		e stresses for nal strength	
	Grade A	Grade B	Grade C	Grades A and B crossings	Grades A and B excep at crossings
Structural steel: Tension Compression	$ \begin{array}{c c}     Lbs. per \\     sq. in. \\     20,000 \\     \begin{cases}     20,000 \\     -80 L/R   \end{array} $	Lbs. per sq. in. 26,000 26,000 -90 L/R	Lbs. per sq. in. 30,000 30,000 -100L/R	Lbs. per sq. in. 30,000 30,000 - 100 L/R	Lbs. per sq. in. 33,000 33,000 -100L/R
Bolts: Shear Bearing	20, 000 40, 000	24, 000 48, 000	35, 000 70, 000	35, 000 70, 000	40, 000 80, 000
Rivets: Shear Bearing	18,000 36,000	22, 000 44, 000	30, 000 60, 000	30, 000 60, 000	33, 000 66, 000

 Fable 16.—Allowable Unit Stresses in Steel for Transverse an

# A. Poles and Towers—Continued.

3. STEEL SUPPORTING STRUCTURES—continued.

(e) THICKNESS OF STEEL. Steel poles or towers shall have no less thickness of metal in members than the following:

Table 17.—Thickness of Steel		
Kind of member	Thickness of main members of cross arms and legs	Thickness of other members
Galvanized: For localities where experience has shown deterioration of gal- vanized material is rapid	Inches 1/4	Inches
For other localities	10	1/8
Painted	1/4	° 1/4

• Painted bracing members having L/R not exceeding 125 may be  $\frac{1}{16}$  inch in thickness.

(f) UNSUPPORTED LENGTH OF COMPRESSION MEMBERS. The ratio of L, the unsupported length of a compression member, to R, the least radius of gyration of the member, shall not exceed the following: (These figures do not apply to the complete structure.)

Table 18.—L/R for Compression Members				
Kind of compression member	L/R			
Leg members	150			
Other members having figured stresses	200			
Secondary members without figured stresses	250			

- 261. GRADES A, B, AND C CONSTRUCTION—Continued. A. Poles and Towers—Continued.
  - 3. STEEL SUPPORTING STRUCTURES—continued.
    - (g) Splices for MAIN LEG MEMBERS. In splices for main leg members where under the application of the values in Table 16, rule 261,  $\Lambda$ , 3, (d) four or more bolts or rivets are called for, the number of bolts or rivets shall be increased by 10 per cent with a minimum of one additional bolt or rivet.
    - (h) ADDITIONAL REQUIREMENT FOR ANCHOR TOWERS. When steel supports or towers are used which are not capable of withstanding approximately as great a force longitudinally as transversely, anchor towers shall be placed at intervals not greater than 10 spans. These anchor towers shall be able to withstand the combined longitudinal tension of all conductors under the loads specified in rule 253 up to 10,000 pounds plus one-half the excess above 10,000 pounds, without exceeding their ultimate strength.
    - (i) GENERAL CONSTRUCTION FEATURES. Steel poles or towers, including parts of footings above ground, shall be constructed so that all parts are accessible for inspection, cleaning, and painting, and so that pockets are not formed in which water can collect.
      - Recommendation.—Unless sample structures, or similar ones, have been tested to assure the compliance of structures in any line with these requirements, it is recommended that structures be designed to have a computed strength at least 10 per cent greater than that required by these rules.

- A. Poles and Towers-Continued.
  - 3. STEEL SUPPORTING STRUCTURES—continued.
    - (j) PROTECTIVE COVERING OR TREATMENT. All iron or steel poles, towers, or supporting structures shall be protected by galvanizing, painting, or other treatment which will effectively retard corrosion.
  - 4. WOOD POLES.

Wood poles shall be of such material and dimensions as to meet the following requirements. Where guys are used, see rule 261, C.

- (a) TRANSVERSE STRENGTH. Wood poles shall withstand the transverse and vertical loads assumed in rule 254, A and B without exceeding at the ground line for unguyed poles, or at the point of guy attachment for guyed poles, the appropriate allowable fiber stresses given in Table 20.
- (b) LONGITUDINAL STRENGTH.

Grades A and B. The longitudinal strength of wood poles shall be maintained at all times so that they will withstand the longitudinal loading specified in rule 254, C without exceeding at the ground line for unguyed poles, or at the point of guy attachment for guyed poles, the appropriate ultimate fiber stress given in Table 19.

Grade C. No longitudinal-strength requirements except at dead-ends.

- A. Poles and Towers—Continued.
  - 4. WOOD POLES—continued.
    - (c) ULTIMATE FIBER STRESS. Different kinds of wood poles are considered as having the ultimate fiber stresses given in Table 19. These ultimate fiber stresses are given so as to identify different kinds of pole timbers with the ultimate fiber stress appearing at the heads of the columns in Table 20.

Table 19.—Ultimate Fiber Stresses of Wood Poles					
Kind of wood	Ultimate fiber stress				
Dense yellow pine (meeting standard of A.S.T. M., see Appendix G)	Lbs. per sq. in. 6, 500				
Other yellow pine Chestnut Western cedar (western red cedar) Cypress	5, 000				
Eastern cedar (northern white cedar) Redwood	} 3,600				

Tests are under way to determine ultimate stresses of woods and when values for ultimate stresses have been adopted as standard by the American Engineering Standards Committee, the values thus determined shall be applied under this code and the values in Table 20 adjusted proportionately.

- 261. GRADES A, B, AND C CONSTRUCTION—Continued.
  - A. Poles and Towers—Continued.
    - 4. WOOD POLES-continued. .
      - (d) TREATED POLES. The use of treated poles is not required. However, under certain circumstances Table 20 permits higher allowable stresses for treated poles than for untreated poles. Treated poles are poles meeting the following requirements:
        - (1) PRESERVATIVES. The preservative used shall be coal-tar creosote or other preservative equally satisfactory with regard to electrical resistance, retention of the preservative within the timber, and efficiency as a preservative. In the case of poles which are butt-treated only, the electrical resistance of the preservative may be disregarded.
        - (2) FULL-LENGTH TREATMENT. Pine and other timber subject to rapid decay above ground shall be treated full length by a pressure process or some other equally effective method.
        - (3) BUTT TREATMENT. Cedar, chestnut, and other timber not subject to rapid decay above ground shall be treated by any process which will produce impregnation of most of the sapwood from at least 2 feet below the ground line to at least 1 foot above the ground line. In the case of treatments which require perforation, no method shall be used which results in perforation to the cross section required at replacement.

- A. Poles and Towers-Continued.
  - 4. WOOD POLES—continued.
    - (e) ALLOWABLE FIBER STRESSES. The allowable fiber stresses to be used in computing the strength of treated and untreated poles to withstand vertical and transverse loads are given in Table 20.

		Wh	en insta	alled		At replacement		
	Treated poles			Untreated poles		Treated or untreated poles		
	For ultimate fiber stress of—			fiber	timate stress		ultimat stress of	
	6, 500	5, 000	3, 600	5,000	3, 600	6, 500	5,000	3, 600
At crossings: Poles in lines of one grade of construction throughout- Grade A	2, 170	1,670	1, 200	1,670	1, 200	3, 250	2, 500	1, 800
Grade B	3,250	2, 500	1,800	2, 500	1,800	4,870	3, 750	2, 700
Grade C	4,870	3, 750	2,700	3,750	2, 700	9,750	7, 500	5, 400
Poles in isolated sections of higher grade of con- struction in lines of a lower grade of con- struction— Grade A	2, 170	1, 670	1, 200	1, 250	900	3, 250	2, 500	1, 800
Grade B	3, 250	2, 500	1,800	1,670	1, 200	4,870	3, 750	2, 700
Grade C	4, 870	3, 750	2, 700	3,000	2, 160	9, 750	7, 500	5, 400
Elsewhere than at crossings: Grade A	2, 600	2, 000	1, 440	1,670	1, 200	3, 900	3, 000	2, 160
Grade B	3, 900	3,000	2, 160	2, 500	1,800	6, 500	5,000	3, 600
Grade C	6, 500	5,000	3, 600	3, 750	2,700	9,750	7, 500	5, 400

261. GRADES A, B, AND C CONSTRUCTION—Continued. A. Poles and Towers—Continued.

- 4. WOOD POLES—continued.
  - (f) FREEDOM FROM DEFECTS. Wood poles shall be selected timber free from observable defects that would decrease their strength and durability.
  - (g) MINIMUM POLE SIZES. Wood poles shall have nominal top diameters not less than the following:

Table 21Minimum Top Diameters for Wood Poles					
Grade of construction	Minimum top diameters for different loading districts				
	Heavy	Medium	Light		
A	Inches 7	Inches 7	Inches 6		
B	6	6	6		
C	6	6	6		

(h) Spliced Poles. Spliced poles shall not be used at crossings, conflicts, or joint-use sections requiring grade A, B, or C construction.

5. TRANSVERSE STRENGTH REQUIREMENTS FOR STRUCTURES WHERE SIDE GUYING IS REQUIRED, BUT CAN ONLY BE INSTALLED AT A DISTANCE. Grades A and B. In the case of structures where, because of very heavy or numerous conductors or relatively long spans, the transverse-strength requirements of this section can not be met ex-

- 261. GRADES A, B, AND C CONSTRUCTION-Continued.
  - A. Poles and Towers-Continued.
    - 5. TRANSVERSE STRENGTH REQUIREMENTS FOR STRUCTURES WHERE SIDE GUYING IS REQUIRED, BUT CAN ONLY BE INSTALLED AT A DISTANCE continued.

cept by the use of side guys or special structures, and it is physically impracticable to employ side guys, the transverse-strength requirements may be met by side-guying the line at each side of, and as near as practicable to, the crossing or other transversely weak structure, and with a distance between such side-guyed structures of not over 800 feet, provided that:

- (a) The side-guyed structures for each such section of 800 feet or less shall be constructed to withstand the calculated transverse load due to wind on the supports and ice-covered conductors, on the entire section between the side-guyed structures.
- (b) The line between such side-guyed structures shall be substantially in a straight line and the average length of span between the sideguyed structures shall not be in excess of 150 feet.
- (c) The entire section between the transversely strong structures shall comply with the highest grade of construction concerned in the given section, except as to the transverse strength of the intermediate poles or towers. *Grade C.* The above provision is not applicable to grade C.

- A. Poles and Towers-Continued.
  - 6. LONGITUDINAL-STRENGTH REQUIREMENTS FOR SECTIONS OF HIGHER GRADE IN LINES OF A LOWER GRADE OF CONSTRUCTION.
    - (a) METHODS OF PROVIDING LONGITUDINAL STRENGTH.

Grades A and B. The longitudinal-strength requirements for sections of line of higher grade in lines of a lower grade (see for assumed longitudinal loading rule 254, C, 1) are usually met by placing supporting structures of the required longitudinal strength at either end of the higher-grade section of the line.

Where this is impracticable, the supporting structures of the required longitudinal strength may be located one or more span lengths away from the section of higher grade, within 500 feet on either side and with not more than 800 feet between the longitudinally strong structures, provided such structures and the line between them meet the requirements, as to transverse strength and stringing of conductors, of the highest grade occurring in the section, and provided that the line between the longitudinally strong structures is approximately straight or suitably guyed.

The requirements may also be met by distributing the head guys over two or more structures on either side of the crossing, such structures and the line between them complying with the requirements for the crossing 261. GRADES A, B, AND C CONSTRUCTION—Continued. A. Poles and Towers—Continued.

> as to transverse strength and as to conductors and their fastenings.

> Where it is impracticable to provide the longitudinal strength, the longitudinal loads shall be reduced by increasing the conductor sags. This may require greater conductor separations. (See rule 235,  $\Lambda$ , 2, (a).)

Grade C. The above provision is not applicable to grade C.

(b) FLEXIBLE SUPPORTS.

Grades A and B. When supports of the section of higher grade are capable of considerable deflection in the direction of the line, as with wood or concrete poles, or some types of metal poles and towers, it may be necessary to increase the normal clearances specified in section 23, or to provide head guys or special reinforcement to prevent such deflection.

So-called flexible steel towers or frames, if used at such locations, shall be adequately reinforced to meet the requirements of rule 261, A, 3 (b).

When the situation is one involving an isolated crossing of higher grade in a line of lower-grade construction, then the structure shall, when practicable, be head-guyed or otherwise reinforced to prevent reduction in the clearances required in section 23.

Grade C. The above provision is not applicable to grade C.

- A. Poles and Towers—Continued.
  - 7. STRENGTH AT ANGLES AND DEAD-ENDS.

In cases where, due to change of direction of the line or because of dead ends, the longitudinal tensions in the conductors are not normally balanced, the construction shall be such as to withstand the total combined load without exceeding the working stresses for transverse strength.

Where the section of higher grade is not in line with the line beyond this section, suitable guys shall be placed to withstand the resulting transverse forces.

# B. Foundations.

- 1. USE OF FOUNDATIONS.
  - (a) WOOD AND REINFORCED-CONCRETE POLES. No special foundation construction is generally required.
  - (b) STEEL POLES OR TOWERS. Steel poles or towers should preferably be placed on concrete or other suitable foundations extending above the ground line. If, however, the steel is set in earth, it shall be suitably protected against injurious corrosion at and below the ground line.
- 2. STRENGTH OF FOUNDATIONS.
  - (a) STEEL SUPPORTS. The foundations shall be so designed and constructed as to withstand the stresses due to the loads assumed in rule 254. The calculated stresses in any steel parts shall not exceed the stresses specified in rule 261, A, 3, (d).

- 261. GRADES A, B, AND C CONSTRUCTION—Continued.
  - B. Foundations—Continued.
    - 2. STRENGTH OF FOUNDATIONS—continued.

Since in many localities the soil and climatic conditions are such as to alter the strength of foundations considerably from time to time, there should usually be provided a considerable margin of strength in foundations above that which (by calculation) will just withstand the loads under the assumption of average conditions of climate and soil.

(b) WOOD AND CONCRETE POLES. Foundations for poles shall be of such material and dimensions as to withstand the loads assumed in rule 254, A, B, and C without exceeding the following percentages of their ultimate strength.

	Percentag for	es of ultimat different gra	e strength des
	Grade A	Grade B	Grade C
For transverse loads (when stalled) For longitudinal loads (at all	50	50	75
times) in general At dead ends	$\begin{array}{c} 100 \\ 50 \end{array}$	$\begin{array}{c} 100 \\ 50 \end{array}$	75

## C. Guys.

1. GENERAL.

The general requirements for guys are covered under "Miscellaneous requirements for overhead construction" (sec. 28).

C. Guys—Continued.

2. FOR LINES IN EXPOSED LOCATIONS.

Grades A and B. In exposed situations, such as open country in rural districts, the transverse strength of wood or reinforced-concrete crossing poles in sections of higher grade in lines of a lower grade of construction shall, where practicable, be obtained by the use of side guys in the following situations:

Where more than ten wires are carried, for all span lengths.

Where more than six wires are carried if the span length exceeds 150 feet.

Grade C. The above provisions do not apply to grade C.

3. ON STEEL STRUCTURES.

The use of guys to obtain compliance with these requirements is regarded as generally undesirable. When guys are necessarily used, the steel supports or towers, unless capable of considerable deflection, shall be regarded as taking all of the load up to their allowable working load, and the guys shall have sufficient strength to take the remainder of the assumed maximum load. (See rule 261, A, 6, (b) for flexible supports.)

4. ON WOOD OR CONCRETE POLES.

When guys are used to meet the strength requirements for wood or concrete poles, they shall be considered as taking the entire load in the direction in which they act, the poles acting as struts only.

- C. Guys-Continued.
  - 5. STRENGTH OF GUYS.

Guys, when used, shall be of such material and dimensions as will withstand the transverse load assumed in rule 254, B and the longitudinal load assumed in rule 254, C without exceeding the following percentages of their ultimate strength:

	Percentages of ultimate strength for different grades		
	Grade A	Grade B	Grade C
For transverse strength (when installed) For longitudinal strength (at	50	50	75
all times) in general At dead-ends	$\begin{array}{c} 100\\ 50 \end{array}$	$\begin{array}{c} 100 \\ 50 \end{array}$	75

## D. Cross Arms.

#### 1. VERTICAL STRENGTH.

Cross arms shall, when installed, withstand the vertical loads specified in rule 254, A without the stress under these loads exceeding 50 per cent of the assumed ultimate stress of the material.

*Exception.*—For built-up steel cross arms on steel structures, see rule 261, A, 3, (d) for allowable working stresses in steel.

D. Cross Arms-Continued.

2. BRACING.

Cross arms shall be securely supported by bracing, if necessary, so as to support safely all other loads to which they may be subjected in use, including linemen working on them. Any cross arm or buck arm except the top one shall be capable of supporting a vertical load of 225 pounds at either extremity in addition to the weight of the conductors.

### 3. LONGITUDINAL STRENGTH.

- (a) GENERAL. Cross arms shall withstand any unbalanced longitudinal loads to which they are exposed, with a limit of unbalanced tension where conductor pulls are normally balanced, of 700 pounds at the outer pin.
- (b) AT ENDS OF HIGHER-GRADE CONSTRUCTION IN LINE OF LOWER GRADE. Grades A and B. Wood cross arms shall be of sufficient strength to withstand at all times, without exceeding their ultimate strengths, an unbalanced pull in the direction of the higher-grade section equal to the tension in all supported conductors under assumed maximum loading as given in rule 254, C, 1. Steel arms shall withstand this load without exceeding the working stresses for longitudinal loads given in rule 261, A, 3, (d).

*Grade C.* The above provisions do not apply to Grade C.

25804°-27~-9

- 261. GRADES A, B, AND C CONSTRUCTION-Continued. D. Cross Arms-Continued.
  - - 3. LONGITUDINAL STRENGTH—continued.
      - (c) AT ENDS OF TRANSVERSELY WEAK SECTIONS. Grades A and B. The cross arms connected to the structure at each end of the transversely weak section, such as described in rule 261, A, 5, shall be such as to withstand at all times without exceeding their ultimate strengths, under the conditions of loading prescribed in rule 254, C, 1, an unbalanced load equivalent to the combined pull in the direction of the transversely weak section of all the conductors supported.

Grade C. The above provision does not apply to grade C.

(d) METHODS OF MEETING RULES 261, D, 3, (b) AND (c).

Grades A and B. Where conductor tensions are limited to a maximum of 2,000 pounds. per conductor, double wood cross arms fitted with spacing bolts equipped with spacing. nuts and washers, pipe spacers, or similar construction, or with spacing blocks or plates, will be considered as meeting the strength requirements in (b) and (c) preceding.

Grade C. The above provisions do not apply. to grade C.

- **D.** Cross Arms—Continued.
  - 4. DIMENSIONS OF CROSS ARMS OF SELECTED YELLOW PINE OR FIR.

The cross-sectional dimensions of selected yellow pine or fir cross arms shall be not less than the values of Table 22.

Table 22.—Cross-arm Cross Sections						
Number of pins	Grades A and B	Grade C				
Number of pins	Grades A and B	Supply	Communication			
2 or 4	Inches 3 by 4	Inches 2 <sup>3</sup> ⁄4 by 3 <sup>3</sup> ⁄4	Inches			
6 or 8	$3\frac{1}{4}$ by $4\frac{1}{4}$	3 by 4				
6			$2\frac{3}{4}$ by $3\frac{3}{4}$			
10			3 by 4			

5. DOUBLE CROSS ARMS AT ANGLES OR DEAD ENDS. Grades A and B. Where conductors are supported on pin insulators, double cross arms shall be used at unbalanced corners and dead ends in order to permit conductor fastenings at two insulators and so prevent slipping.

*Grade C.* The above provision does not apply to grade C.

6. LOCATION.

In general, cross arms should be maintained at right angles to the axis of the pole and to the direction of the attached conductors. At crossings, cross arms should be attached to that face of the structure away from the crossing, unless special bracing or double cross arms are used.

- 261. GRADES A, B, AND C CONSTRUCTION-Continued.
  - E. Pins and Conductor Fastenings.
    - 1. LONGITUDINAL STRENGTH.
      - (a) GENERAL. Pins and ties or other conductor fastenings shall have sufficient strentgh to withstand an unbalanced tension in the conductor, up to a limit of 700 pounds per pin or fastening.
      - (b) AT ENDS OF HIGHER-GRADE CONSTRUCTION IN LINE OF LOWER GRADE.

Grades A and B. Pins and ties or other conductor fastenings connected to the structure at each end of the higher-grade section shall be of sufficient strength to withstand at all times without exceeding their ultimate strength, an unbalanced pull in the direction of the higher-grade section due to the loading specified in rule 254, C, 1.

*Grade C.* The above provisions do not apply to grade C.

(c) AT ENDS OF TRANSVERSELY WEAK SECTIONS. Grades A and B. Pins and ties or other conductor fastenings connected to the structure at each end of the transversely weak section as 'described in rule 261, A, 5 shall be such as to withstand at all times without exceeding their ultimate strength under conditions of loading prescribed in rule 254, C, 1 the unbalanced pull in the direction of the transversely weak section of the conductor supported.

Grade C. The above provisions do not apply to grade C.

- E. Pins and Conductor Fastenings—Continued.
  - 1. LONGITUDINAL STRENGTH—continued.
    - (d) Method of Meeting Rules 261, E, 1, (b), and (c).

Grades A and B. Where conductor tensions are limited to 2,000 pounds and such conductors are supported on pin insulators, double pins, and ties or equivalent fastenings will be considered to meet the requirements (b) and (c) preceding.

Grade C. The above provision does not apply to grade C.

2. SHARP EDGES ON FASTENINGS.

Tie wires or fastenings shall have no sharp edges or burrs at contacts with the conductors.

3. HEIGHT OF PIN.

The height of the pin and the conductor fastenings and the material and cross section of the pin should be chosen so as to afford the required strength.

Note.—The method of attaching conductors by suitable ties to single pin-type insulators mounted on 1½ by 9 inch wood pins of locust or equivalent wood will usually provide strength up to 1,000 pounds conductor tension with the conductor 3.5 inches above the cross arm. Steel pins may afford greater strength both for the pins and for the cross arms.

- 261. GRADES A, B, AND C CONSTRUCTION-Continued.
  - F. Open Supply Conductors.
    - 1. MATERIAL.

Conductors shall be of copper, aluminum (with or without steel reinforcement), copper-covered steel, or other material which will not corrode excessively under the prevailing conditions.

Recommendation.—It is recommended that medium-hard-drawn copper wire (conforming to the specifications of the American Society for Testing Materials) be used instead of soft in new construction, especially for sizes smaller than No. 2.

Note.—Soft copper wire has a yield point less than one-half that of medium-drawn copper, and hence stretches permanently with a correspondingly lighter loading of ice and wind.

Copper wire does not have so sharply defined a yield point as steel, but for practical purposes, the yield point may be considered as that point beyond which the wire is permanently elongated and the sag permanently increased.

If the wire when first strung is pulled to a tension approximately equal to half its breaking strength and then released and tied, its yield point is thereby raised and it will be less likely to stretch and its sag to increase materially under moderate loading of ice and wind.

2. MINIMUM SIZES OF SUPPLY CONDUCTORS.

Supply conductors shall be not smaller than indicated in Table 23.

Exception 1.—Longer spans than specified in the table may be used with any listed conductor size if the separations and clearances of section 23 and the sags of Appendix B are correspondingly increased.

F. Open Supply Conductors-Continued.

Exception 2.—Supply service leads of 0 to 750 volts may have the sizes set forth in rule 263, E.
Exception 3.—Where the short-span method of construction is employed in accordance with rule 261, K, the conductor sizes and sags herein specified are not required.

Table 23.—Minimum Allowable Conductor Sizes [Sizes are A. W. G. for copper, copper-covered steel, and aluminum; Stl. W. G. for steel]												
Kind of wire	Loading district	Grade of construction	Wire sizes for span lengths up to and including the following limits (in feet)									
			150	175	200	250	300	40 <b>0</b>	500	700	1,000	
Covered wires: Copper, medium or hard-drawn. Copper-covered steel.	Heavy Medium Light	{A and B C A B C A B C C	6 8 6 8 6 8 8 8		$     \begin{array}{c}       4 \\       4 \\       4 \\       4 \\       4 \\       4 \\       4 \\       6 \\       6 \\       6     \end{array} $		$\begin{array}{c}2\\2\\2\\2\\2\\2\\2\\2\\2\\2\\2\\2\end{array}$					
Bare wires: Copper, medium or hard-drawn. Copper-covered steel.	Heavy Medium Light	{A and B C B C A A B B C	6 8 6 8 6 8 6 8 8 8		$     \begin{array}{c}       4 \\       4 \\       4 \\       4 \\       6 \\       6 \\       6 \\       6     \end{array} $		4 4 4 4 4 4 4 4	$     \begin{array}{c}       2 \\       2 \\       4 \\       4 \\       4 \\       4 \\       4 \\       4 \\       4 \\       4   \end{array} $	$     \begin{array}{c}       2 \\       2 \\       2 \\       2 \\       4 \\       4 \\       4    \end{array} $	$\begin{array}{c} 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\\ 2\end{array}$	00 00 00 1 1 1 1	
Covered or bare wires: Copper, soft- drawn.	Heavy Medium Light	{A B C A and B C A, B, and C.		2 $2$ $2$ $4$ $4$ $4$	$\begin{array}{c}1\\2\\2\\2\\2\\4\end{array}$	$\begin{array}{c} & & \\$						
				Exceeding 150								
Steel wire	All	{A and B C	6 9		4 6							
Stranded alumi- num wire: Without steel reinforcement. With steel rein- forcement.	A11	A, B, and C. A, B, and C.	1 6	0 4								

- 261. GRADES A, B, AND C CONSTRUCTION--Continued.
  - F. Open Supply Conductors—Continued.
    - 3. LIGHTNING PROTECTION WIRES.

Lightning protection wires paralleling the line conductors shall be regarded in respect to size, material, separation, and stringing requirements as supply conductors with which they are associated.

- 4. SAGS AND TENSIONS.
  - (a) MINIMUM ALLOWABLE SAG. Conductor sags shall be such that, under the assumed loading of rule 253 for the district concerned, the tension in the conductor shall not be more than 50 per cent of its breaking strength for grades A and B, nor more than 60 per cent for grade C.
    - Note.—The sag tables of Appendix B are based upon a stringing temperature of 30, 60, or 90° F. to comply with these requirements.
    - Recommendation.—It is recommended that conductors of hard, medium, and softdrawn copper have normal sags, at 60° F. and no wind, as near as practicable to those given in the tables of Appendix A.

Note.—The sags given for copper in the tables are based upon experience and are designed to give the best results from the standpoint of safety and continuity of service.

In order to minimize the danger from wires swinging together and to permit the moderate pin spacings and cross-arm spacings sanctioned by modern good practice in overhead line construction, it is necessary to assign a limit to the sag, and hence to the recommended length of span of the smaller sized wires, as indicated by the blank spaces in the tables.

- F. Open Supply Conductors—Continued.
  - 4. SAGS AND TENSIONS—continued.
    - (b) Two-THOUSAND-POUND LIMITATION FOR CON-DUCTOR TENSIONS. In order to apply the methods given in rule 261, D, 3, (d) and rule 261, E, 1, (d) it is necessary that conductor tensions be limited to 2,000 pounds. The curves given in Appendix C show sags based on these limitations for conductors having an ultimate strength of 4,000 pounds or more.
  - 5. SPLICES AND TAPS.

Grades A and B. Splices shall not be made in the crossing span and preferably not in the adjacent spans, which are depended upon for withstanding the longitudinal tension of the crossing conductors. Taps shall not be made in the crossing span. If a splice or tap is made in any conductor in the span next to the crossover span, it shall, where practicable, be placed at a point nearer to the crossover support than is the nearest conductor crossed over.

*Exception.*—In the case of large-gauge conductors where the application of this rule would work a hardship and where proper methods are available for making high-strength splices, such splices may be used in the crossing span provided they are of a type which has been shown by tests and experience to be at least as strong as the conductor.

Grade C. The above does not apply to grade C.6. TROLLEY CONTACT CONDUCTORS.

In order to provide for wear, no trolley contact conductor shall be installed of less size than No. 0, if of copper, or No. 4, if of silicon bronze. 114 SEC. 26—STRENGTH REQUIREMENTS

8

- 261. GRADES A, B, AND C CONSTRUCTION—Continued.G. Supply Cables.
  - 1. SPECIALLY INSTALLED SUPPLY CABLES.

Cables having permanently grounded continuous metal sheath or armor, where located on joint poles, or where located on other poles and having a grade of construction less than that required for open wire supply lines of the same voltage, shall meet the requirements of (a), (b), (c), and (d) below.

- (a) MESSENGERS. Messengers shall be stranded and of galvanized or copper-covered steel with strengths and sags as specified in rule 262, J for grade D, or if of other sizes shall not be stressed beyond half their ultimate strength under the loadings specified in rule 253.
- (b) GROUNDING OF CABLE SHEATH AND MESSEN-GER. Each section of cable between splices shall be suitably and permanently bonded to the messenger wire at not less than two places. The messenger wire shall be grounded at the ends of the line and at intermediate points not exceeding 800 feet apart. (See section 9 for method.)
- (c) CABLE SPLICES. Splices in the cable shall be made so that their insulation is not materially weaker than the remainder of the cable. The sheath or armor at the splice shall be made electrically continuous.

261. GRADES A, B, AND C CONSTRUCTION—Continued.

G. Supply Cables—Continued.

- 1. SPECIALLY INSTALLED SUPPLY CABLES—continued.
  - (d) CABLE INSULATION. The conductors of the cable shall be insulated so as to withstand a factory potential test of at least twice the operating voltage at operating frequency applied continuously for five minutes between conductors and between any conductor and the sheath or armor.
- 2. OTHER SUPPLY CABLES.

The following requirements apply to all supply cables not included in 1 above.

(a) MESSENGER. The messenger shall have such strength and sag that it will not be stressed
 beyond the following percentages of its ultimate strength under the loadings specified in rule 253:

Grade of construction:	of ulti	mate
A and B		50
C		60

(b) CABLE. There are no strength requirements for cables supported by messengers.

# H. Open Communication Conductors.

Open-wire communication conductors in grade A, B, or C construction shall have the sizes and sags given in rule 261, F, 2 and 4 for supply conductors of the same grade.

*Exception.*—Where the span length is 150 feet or less, conductors may have grade D sizes and sags instead of grade C sizes and sags except as provided in Note <sup>g</sup> to Table 15, rule 242.

# 116 SEC. 26—STRENGTH REQUIREMENTS

261. GRADES A, B, AND C CONSTRUCTION-Continued.

- I. Communication Cables.
  - 1. METAL-SHEATHED COMMUNICATION CABLES.

There are no strength requirements for such cables supported by messengers.

2. MESSENGER.

The messenger shall have such strength and sag that it will not be stressed beyond the following percentages of its ultimate strength under the loading specified in rule 253:

Grade of construction:	of ultin stren	mate
A and B		50
C		60

- J. Paired Communication Conductors.
  - 1. PAIRED CONDUCTORS SUPPORTED ON MESSENGER.
    - (a) USE OF MESSENGER. A messenger may be used for supporting paired conductors in any location, but is only required for paired conductors crossing over trolley contact conductors of more than 7,500 volts.
    - (b) SAG OF MESSENGER. Messenger used for supporting paired conductors required to meet grade A or B construction because of crossing over trolley contact conductors shall meet the sag requirements for grade D messengers.
    - (c) SIZE AND SAG OF CONDUCTORS. There are no requirements for paired conductors when supported on messenger.

261. GRADES A, B, AND C CONSTRUCTION—Continued.

- J. Paired Communication Conductors—Continued.
  - 2. PAIRED CONDUCTORS NOT SUPPORTED ON MES-SENGER.
    - (a) Above Supply Lines.

Grades A and B. Sizes and sags shall not be less than those required by rule 261, F, 2 and 4 for supply conductors of similar grade. Grade C.

Spans 0 to 100 feet. No sag requirements. Sizes shall be not less than the following:

		0
Hard-drawn copper	No.	14 AWG.
Bronze	No.	17 AWG.
Copper-covered steel	No.	17 AWG.

- Spans 100 to 150 feet. Sizes and sags shall be not less than required for grade D communication conductors.
- Spans exceeding 150 feet. Sizes and sags shall be not less than required for Grade C supply conductors.
- (b) Above Trolley Contact Conductors.

*Grades A and B.* Sizes and sags shall not be less than the following:

- Spans 0 to 100 feet. No size requirements. Sags shall be not less than for No. 8 A. W. G. hard-drawn copper as given in Appendix B.
- Spans exceeding 100 feet. Sizes shall be not less than the following:

Hard-drawn copper	No. 14 AWG.
Bronze	No. 17 AWG.
Copper-covered steel	No. 17 AWG.

# 261. GRADES A, B, AND C CONSTRUCTION--Continued.

J. Paired Communication Conductors—Continued.

Sags shall be not less than for No. 8 A. W. G.

hard-drawn copper as given in Appendix B. Grade C. Sizes and sags shall be as follows: Spans 0 to 100 feet. No requirements.

Spans exceeding 100 feet. No sag requirements. Size shall be not less than the following:

Hard-drawn copper	No. 14 AWG.
Bronze	No. 17 AWG.
Copper-covered steel	No. 17 AWG.

### K. Short-Span Crossing Construction.

Where supply lines cross over railways or communication lines by the short-span method, the requirements for grade A, B, or C conductor sags and sizes are waived, in so far as such grades are required by the crossing, provided that a permanently grounded guard arm is installed at each crossover support in such a manner as to prevent conductors which break in either adjoining span from swinging back into the conductors crossed over, or in the case of a railroad crossing into the space between the crossing supports.

*Explanation.*—The short-span method of crossing requires the crossover span to be of such a height that a conductor breaking in that span can not come within 15 feet of the ground or rails at a railroad crossing or make contact with any wires crossed over at a wire crossing.

This character of construction is facilitated where the crossover supports can be placed quite near together and in the case of wire crossings where the span crossed over is at a minimum elevation above ground.

261. GRADES A, B, AND C CONSTRUCTION—Continued.

L. Cradles at Supply-Line Crossings.

Cradles should not be used.

Note.—It is less expensive and better to build the supply line strong enough to withstand extreme conditions than to build a cradle of sufficient strength to catch and hold the supply line if it falls.

M. Protective Covering or Treatment for Metal Work.

All hardware, including bolts, washers, guys, anchor rods, and similar parts of material subject to injurious corrosion under the prevailing conditions, shall be protected by galvanizing, painting, or other treatment which will effectively retard corrosion.

262. GRADES D AND E CONSTRUCTION.

A. Poles.

1. STRENGTH OF UNGUYED POLES.

Unguyed poles, at the time of installation, shall withstand the vertical and transverse loads specified in rule 254, A and B and the longitudinal loads specified in rule 254, C without exceeding the following percentages of their ultimate strength.

a	Percentages of ultimate strength for different grades		
	Grade D Grade H		
For transverse strength For longitudinal strength (for poles carrying not more than two wires)	25 50	37. 5 75	

# 120 SEC. 26—STRENGTH REQUIREMENTS

- 262. GRADES D AND E CONSTRUCTION—Continued.
  - A. Poles-Continued.
    - 2. STRENGTH OF GUYED POLES.

Where poles are guyed, the poles shall be considered as acting as struts, resisting the vertical component of the tension in the guy calculated as in rule 262, C combined with the vertical load.

3. STRENGTH REQUIREMENTS FOR POLES WHERE GUYING IS REQUIRED, BUT CAN ONLY BE IN-STALLED AT A DISTANCE.

Where on account of physical conditions it is impracticable to guy or brace the crossing poles as specified in rule 262, C the requirements there given may be met by head-guying and sideguying the line as near as practicable to the crossing, but at a distance not exceeding 500 feet from the nearest crossing pole, provided that the line is approximately straight and that a stranded steel wire of strength equivalent to that of the head guy is run between the two guyed poles, being attached to the guyed poles at the point at which the head guys are attached, this wire being securely attached to every pole between the guyed poles.

4. POLE LOCATIONS AT CROSSINGS.

Where communication lines cross over railroads, the poles shall be located as follows:

(a) The poles supporting the crossing span and the adjacent spans should be located in a straight line, if practicable. Where the poles supporting the crossing span and the adjacent spans are not in line, additional guying shall be placed to take care of the unbalanced load. 262. GRADES D AND E CONSTRUCTION—Continued.

- A. Poles—Continued.
  - 4. POLE LOCATIONS AT CROSSINGS-continued.
    - (b) The crossing span shall be as short as practicable, and, in general, shall not be longer than the normal span of the line. No crossing span shall exceed 125 feet in length if this can be avoided.
  - 5. FREEDOM FROM DEFECTS.

Wood poles supporting the crossing span shall be selected timber, sound and reasonably straight.

6. MINIMUM POLE SIZES.

Poles shall have top diameters not smaller than the values given in Table 24 below.

Table 24.—Minimum pole sizes for grades D and E				
Diameter of				
Number of wires carried by pole	Grade D	Grade E		
1 to 20 21 to 40 More than 40	Inches 6 7 8	Inches 6 6 7		

#### 7. SPLICED POLES.

Spliced poles shall not be used at grade D or E crossings or conflicts.

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- 262. GRADES D AND E CONSTRUCTION-Continued.
  - A. Poles—Continued.
    - 8. POLES LOCATED AT CROSSINGS OVER SPUR TRACKS. Where a communication line paralleling a railroad track on the right of way of the railroad crosses a spur or stub track without any change in the general direction of line, the transverse strength requirements for grade E construction may be met without the use of side guys, providing the pole is not stressed beyond one-half its ultimate strength. No requirements for longitudinal strength are made if the conductor tensions are balanced. Where conductor tensions are not balanced, due to a small angle in the line at one or both poles, or to dead-ending any of the wires, either guys or braces shall be installed capable of withstanding such unbalanced tensions.

#### 9. HEIGHT OF POLES ADJACENT TO CROSSING POLES.

The height of poles adjacent to crossing poles shall be such that the vertical distance from the top cross arm of the crossing pole to a straight line connecting the top cross arms of the next adjacent poles on either side of this crossing pole shall not exceed the values given below:

	vertice	
	distanc	e
Average Length of Span:	F	'eet
Less than 100 feet		4
100 to 130 feet		5
Exceeding 130 feet		6

Allowable

# 262. GRADES D AND E CONSTRUCTION—Continued.

B. Pole Settings.

Poles shall be set to such a depth and in such a manner and back filling shall be so thoroughly tamped that the applied load will break the pole before the butt is pulled loose from its setting.

Recommendation.—A table of recommended depths of setting is given in Appendix F.

C. Guys.

1. GENERAL.

The general requirements for guys are covered under "Miscellaneous requirements for overhead construction" (sec. 28).

2. WHERE USED.

Side guys or braces shall be used on poles supporting the crossing span to withstand the loads put upon them in accordance with the conditions specified in rule 254, B.

Head guys shall be installed in accordance with Table 25.

- Exception 1.—Side guys are not required where the crossing poles have the transverse strength specified in rule 262 A, 1. Head guys are not required where the crossing poles carry not more than two wires and have the strength specified in rule 262 A, 1.
- *Exception 2.*—This rule does not apply to crossing poles under the special conditions set forth in rule 262 A, 3, above.
- *Exception 3.*—Where an overhead crossing which makes an angle with the tracks of less than 45° involves at either crossing pole an angle in the pole line, the side guy within the angle may be omitted.
- *Exception* 4.—Guying may be omitted where communication lines cross over spur or stub tracks as provided in rule 262 A, 8.

# 262. GRADES D AND E CONSTRUCTION-Continued.

- C. Guys—Continued.
  - 3. GUYS USED FOR TRANSVERSE STRENGTH.

Guys shall be considered as taking the entire load in the direction in which they act, without exceeding the following percentages of the ultimate strength of the material.

- 4. GUYS USED FOR LONGITUDINAL STRENGTH.
  - (a) DIRECTION OF HEAD GUYS. Poles supporting the crossing span shall be head-guyed away from the crossing.
  - (b) SIZE AND NUMBER OF HEAD GUYS. Guys for various wire loads shall be supplied as per Table 25.

*Exception.*—This rule does not prevent the omission of head guys where the crossing poles have the strength specified in rule 262, A, 1 above and carry not more than two wires.

	bading Di	istricts In		-	ed for
Ratio of guy lead to height not less than—				-	
Number of wires	11/4	1	3⁄4	2⁄3	1⁄2
G	RADE D,	HEAVY LO	DADING		
2 6 10 20 30 40 50 60 70 80	$\begin{array}{c} 4,000\\ 4,000\\ 6,000\\ 10,000\\ 16,000\\ 20,000\\ 20,000\\ 26,000\\ 30,000\\ 36,000\\ 36,000\\ \end{array}$	$\begin{array}{c} 4,000\\ 4,000\\ 6,000\\ 10,000\\ 16,000\\ 20,000\\ 20,000\\ 30,000\\ 30,000\\ 40,000\\ \end{array}$	$\begin{array}{c} 4,000\\ 4,000\\ 6,000\\ 12,000\\ 20,000\\ 26,000\\ 30,000\\ 36,000\\ 40,000\\ 48,000\\ \end{array}$	$\begin{array}{c} 4,000\\ 4,000\\ 10,000\\ 10,000\\ 20,000\\ 26,000\\ 32,000\\ 32,000\\ 36,000\\ 48,000\\ 60,000\\ \end{array}$	$\begin{array}{c} 4,000\\ 6,000\\ 10,000\\ 16,000\\ 26,000\\ 32,000\\ 42,000\\ 48,000\\ 60,000\\ 70,000\\ \end{array}$

Table 25.—Strength Loading			Iead Guy I—Contin		ed for
[Combinat	ions of stand	lard-size gu	ys may be us	ed]	
Number of mine	Rac	lio of guy lea	d to height	not less than	
Number of wires	11/4	1	3⁄4	2⁄3	1⁄2
GRADE D, MEDIUM	LOADING	, AND GR	ADE E, H	EAVY LOA	DING
2 6 0 0 0	4,000 4,000 4,000 6,000	4,000 4,000 4,000 10,000	$\begin{array}{c} 4,000\\ 4,000\\ 6,000\\ 10,000\end{array}$	4,000 4,000 6,000 10,000	4,000 4,000 6,000 12,000
30 40 50 50 70 80	10,000 12,000 16,000 20,000 20,000 26,000	10,000 16,000 16,000 20,000 20,000 26,000	12,000 16,000 20,000 26,000 26,000 30,000	16,000 16,000 20,000 26,000 30,000 32,000	16,000 20,000 26,000 30,000 36,000 40,000
GRADE D, LIGHT LO	ADING, A	ND GRAI	DE E, MED	IUM LOA	DING
26 6 10 20 30	4,000 4,000 4,000 4,000 6,000	4,000 4,000 4,000 6,000 10,000	4,000 4,000 4,000 6,000 10,000	4,000 4,000 4,000 6,000 10,000	4,000 4,000 4,000 10,000 12,000
40 50 10 70 80	$\begin{array}{c} 10,000\\ 10,000\\ 12,000\\ 16,000\\ 16,000\\ 16,000 \end{array}$	$\begin{array}{c} 10,000\\ 10,000\\ 16,000\\ 16,000\\ 20,000 \end{array}$	$\begin{array}{c} 10,000\\ 16,000\\ 16,000\\ 20,000\\ 20,000\\ 20,000 \end{array}$	$\begin{array}{c} 12,000\\ 16,000\\ 16,000\\ 20,000\\ 26,000 \end{array}$	$\begin{array}{c} 16,000\\ 20,000\\ 20,000\\ 26,000\\ 30,000 \end{array}$
G.	RADE E, 1	LIGHT LO.	ADING		
2 6 	4,000 4,000 4,000 4,000 4,000 6,000	$\begin{array}{c} 4,000\\ 4,000\\ 4,000\\ 4,000\\ 6,000 \end{array}$	$\begin{array}{c} 4,000\\ 4,000\\ 4,000\\ 4,000\\ 4,000\\ 6,000 \end{array}$	4,000 4,000 4,000 4,000 6,000	4,000 4,000 4,000 6,000 10,000
40 50 80 70 80	6,000 6,000 10,000 10,000 10,000	6,000 6,000 10,000 10,000 12,000	10, 000 10, 000 10, 000 12, 000 16, 000	10, 000 10, 000 12, 000 16, 000 16, 000	10, 000 12, 000 16, 000 16, 000 20, 000

See note on page 126.

### 262. GRADES D AND E CONSTRUCTION—Continued.

- C. Guys-Continued.
  - 4. GUYS USED FOR LONGITUDINAL STRENGTH continued.

Note to Table 25.—This table is based on ultimate or breaking strength of guys equal to seven-sixths of the nominal strengths shown in the table and a wire load of 50 per cent No. 8 B. W. G. iron and 50 per cent No. 9 A. W. G. copper with an average pull of 408.75 pounds per wire.

No guy will be required for cable, since the suspension strand serves as a head guy.

5. LOCATION OF GUY ANCHORS.

Guy anchors shall, where possible, be located so that the horizontal distance from the ground line of the pole to the guy or guy rod will be not less than the height above ground of the attachment of the guy to the poles for head guys, and not less than one-third that height for side guys.

6. ATTACHMENT OF GUYS TO POLES.

The guys shall be attached as near to the center of the load as practicable.

7. MAINTENANCE.

The guys and anchors shall be maintained so that the guys are kept taut.

### D. Cross Arms.

1. MATERIAL.

Wood cross arms supporting the crossing span shall be of yellow pine, fir, or other suitable timber

262. GRADES D AND E CONSTRUCTION—Continued.

- **D.** Cross Arms—Continued.
  - 2. MINIMUM SIZE.
    - (a) WOOD CROSS ARMS. Wood cross arms shall have a cross section not less than the following:

Length of arm:	Cross section (inches)
6 feet or less	$2\frac{3}{4}$ by $3\frac{3}{4}$
More than 6 feet	3 by 4

- *Exception.*—In rural districts in arid regions where the practice has been established of using  $2\frac{3}{4}$  by  $3\frac{3}{4}$  inch arms in 8 and 10 pin lengths, this practice may be continued where conductors are not larger than No. 10.
- (b) STEEL OR IRON CROSS ARMS. Galvanized or painted iron or steel cross arms of strength equal to wood cross arms may be used.
- 3. DOUBLE CROSS ARMS.

Cross arms and insulators shall be double on the crossing poles. The cross arms shall be held together with properly fitted spacing blocks or bolts placed immediately adjoining the outside pins. Double cross arms shall not support more than 10 conductors.

E. Brackets and Racks.

Brackets or racks may be used only if used in duplicate or otherwise designed so as to afford two points of support for each conductor.

*Exception.*—For supporting paired conductors, a single metal bracket, designed to safely withstand the full dead-end pull of the wires, may be used.

# 262. GRADES D AND E CONSTRUCTION-Continued.

F. Pins.

1. MATERIAL.

Insulator pins shall be of steel, wrought iron, malleable cast iron, or locust or equivalent wood.

2. STRENGTH.

Insulator pins shall have sufficient strength to withstand the loads to which they may be subjected.

- 3. SIZE.
  - (a) WOOD PINS. Wood pins shall be sound and straight-grained with a diameter of shank not less than  $1\frac{1}{4}$  inches.
  - (b) METAL PINS. Steel or iron pins shall have diameter of shank not less than one-half inch.

# G. Insulators.

Each insulator shall be of such pattern, design, and material that when mounted it will withstand without injury and without being pulled off the pin, the ultimate strength of the conductor attached to the insulator.

H. Attachment of Conductor to Insulator.

The conductors shall be securely tied to each supporting insulator.

- I. Conductors.
  - 1. MATERIAL.

Conductors shall be of hard-drawn copper, coppercovered steel, galvanized steel, or other hard-drawn corrosion-resisting metal, provided, however, that galvanized steel shall not be used in localities where excessive corrosion would result.

262. GRADES D AND E CONSTRUCTION—Continued.

- I. Conductors—Continued.
  - 2. SIZE.

Conductors of the crossing span, if of hard-drawn copper or galvanized steel, shall have sizes not less than specified in (a) and (b) below. Conductors of material other than the above shall be of such size and so erected as to have a mechanical strength not less than that of the sizes of copper conductors given in (a) and (b) below.

(a) SPANS NOT EXCEEDING 150 FEET. The sizes in Table 26 apply.

Table 26.—Grades D an [A. W. G. for copper				Sizes	
Conductor	Loading	Spans feet o	of 125 r less	Spans to 150	125 feet ) feet
Conductor	district	Grade D	Grade E	Grade D	Grade E
Copper, hard-drawn	{Heavy Medium Light	10 10 10	$10 \\ 12 \\ 12 \\ 12$	9 9 9	10 10 10
In general	All	10	12	8	10
In rural districts of arid regions	All	12	12	10	10

(b) SPANS EXCEEDING 150 FEET. If spans in excess of 150 feet are necessary, the size of conductors specified above or the sags of the conductors shall be correspondingly increased. SEC. 26-STRENGTH REQUIREMENTS

- 262. GRADES D AND E CONSTRUCTION-Continued.
  - I. Conductors—Continued.
    - 3. PAIRED CONDUCTORS WITHOUT MESSENGERS. Paired wires without a supporting messenger shall be eliminated as far as practicable and where used shall meet the following requirements:
      - (a) MATERIAL. Each conductor shall be made of bronze, hard-drawn copper, or coppercovered steel, and shall be tinned.
      - (b) SIZE. Each wire shall be not smaller than the following:

Hard-drawn copper	No.	<b>14</b>	А.	<b>W</b> .	G.
Bronze	No.	17	A.	W.	G.
Copper-covered steel	No.	17	А.	W.	G.

(c) LIMITING SPAN LENGTHS. Paired wires shall in no case be used without a supporting messenger in longer spans than the following:

	reet
For grade D construction	100
For grade E construction	125

4. SAGS.

Conductors of the crossing span shall be strung with sags not less than shown in Table 27.

Table 27.—Minimu Wire or Steel	m Strin Wire f	ging Sag for Load	s of Ban ling Dis	e Hard- tricts In	Drawn dicated	Copper
	HEA	VY LOA	DING			
Sag (in inches)						
Liength of Span (in feet)	100° F.	80° F.	60° F.	40° F.	20° F.	0° F.
75 80 90 100 110	$51/2 \\ 61/2 \\ 8 \\ 10 \\ 12$	5 5½ 7 8½ 10	4 41/2 51/2 7 81/2	$3^{1}_{4}$ $3^{1}_{2}$ $4^{1}_{2}$ $5^{1}_{2}$ $6^{1}_{2}$	$2^{3}_{4}_{3}_{3^{1}_{2}_{4^{1}_{2}_{5^{1}_{2}_{5^{1}_{2}}}}}$	$2\frac{1}{4}$ $2\frac{1}{2}$ 3 4 5
120 130 140 150	14 17 20 23	$12 \\ 14 \\ 17 \\ 20$	10 12 14 16		$     \begin{array}{c}       6^{1} / 2 \\       8 \\       9^{1} / 2 \\       11     \end{array} $	6 7 8 9
	MEI	DIUM LO	ADING			
	100° F.	80° F.	60° F.	40° F.	20° F.	0° F.
75 80 90 100 110	4 5 6 7 <sup>1</sup> ⁄2 9	$3\frac{1}{2}$ $4$ $5$ $6$ $7\frac{1}{2}$	31/2 4 5 6	21/2 3 31/2 41/2 51/2	$214 \\ 21/2 \\ 3 \\ 31/2 \\ 41/2 \\ 41/2 \\ \end{array}$	$134 \\ 2 \\ 21/2 \\ 3 \\ 334$
120 130 140 150	11 13 15 17	$9\\10\frac{1}{2}\\12\\14$	$7\\81/2\\10\\12$	$6\frac{1}{2}$ $7\frac{1}{2}$ $8\frac{1}{2}$ 10	$5\frac{1}{2}$ $6\frac{1}{2}$ $7\frac{1}{2}$ $8\frac{1}{2}$	$\begin{array}{c} 4^{1} \\ 5^{1} \\ 6^{1} \\ 7^{1} \\ 7^{1} \\ 2 \end{array}$
LIGHT LOADING						
	120° F.	100° F.	80° F.	60° F.	40° F.	20° F.
75 80 90 100 110	$4 \\ 5 \\ 6 \\ 7 \\ 8^{1/2}$	31/2 4 5 6 7	31/2 4 5 6	21/2 3 31/2 4 5	$2 \\ 2^{1}/2 \\ 3 \\ 3^{1}/2 \\ 4$	$1^{3}_{2}^{4}$ $2^{1}_{2}^{2}$ 3 $3^{1}_{2}^{1}$
120 130 140 150	$10 \\ 12 \\ 14 \\ 16$	$     \begin{array}{r}             81/2 \\             10 \\             12 \\             14 \\             14         \end{array}     $	$7\\8^{1}/2\\10\\12$	$678^{1/2}$	5 6 7 8	4 5 6 7

- 262. GRADES D AND E CONSTRUCTION-Continued.
  - I. Conductors—Continued.
    - 5. SPLICES AND TAPS.

Splices and taps shall not be made in the crossing span and preferably not in the adjacent spans.

6. SIMULTANEOUS CROSSING OVER RAILROAD AND SUPPLY LINE.

Where conductors cross in the same span over a railroad track and a supply line carrying from 750 volts alternating current (440 volts to neutral or ground) to 5,000 volts alternating current (2,900 volts to neutral or ground) the minimum allowable conductor sizes shall be the same as required by rule 261, F, 2 for grades A and B construction when crossing main and minor tracks, respectively.

- J. Messengers.
  - 1. MINIMUM SIZE.
    - (a) SPANS NOT EXCEEDING 150 FEET. Table 28 gives the minimum sizes of galvanized steelstrand messenger to be used for supporting different sizes of cables:

Table 28.—Minimum Sizes of Messenger			
Size of cable in weight per foot	Messenger (nominal break- ing load)		
Less than 2.25 pounds	Pounds 6, 000		
2.25 to 5 pounds	10, 000		
Exceeding 5 and less than 8 pounds	16, 000		

62. GRADES D AND E CONSTRUCTION—Continued.

- J. Messengers—Continued.
  - 1. MINIMUM SIZE—continued.
    - (b) SPANS EXCEEDING 150 FEET. For spans exceeding 150 feet or for heavier cables a proportionately larger messenger or other proportionately stronger means of support shall be used.
  - 2. SAGS AND TENSIONS.

Multiple-wire cables and their messengers shall be suspended with a normal sag at 60°F., so that when they are subjected to the loading prescribed in rule 253 the tension in the messenger will not exceed the following values of safe working tension:

Table 29.—Safe Working Tension in Messengers			
Nominal breaking load of messenger (in pounds)	Safe working tension of mes- senger		
6,000	Pounds 3, 500		
10,000	5, 900		
16,000	9, 500		

### K. Inspection.

All parts of the supporting structures of the crossing span shall be examined annually by the owner and all defective parts shall be promptly restored to a safe condition.

### 134 SEC. 26—STRENGTH REQUIREMENTS

# 263. GRADE N CONSTRUCTION.

### A. Poles and Towers.

Poles used for lines for which neither grade A, B, C, D, or E is required shall be of such initial size and so guyed or braced, where necessary, as to withstand safely the loads to which they may be subjected, including linemen working on them.

B. Guys.

The general requirements for guys are covered under "Miscellaneous requirements for overhead construction" (sec. 28).

### C. Cross-Arm Strength.

Cross arms shall be securely supported, by bracing if necessary, so as to support safely loads to which they may be subjected in use, including linemen working on them. Any cross arm, or buck arm, except the top one, shall be capable of supporting a vertical load of 225 pounds at either extremity in addition to the weight of the conductors.

Note.—Double cross arms are generally used at crossings, unbalanced corners, and dead-ends in order to permit conductor fastenings at two insulators, and so prevent slipping, although single cross arms might provide sufficient strength. To secure extra strength, double cross arms are frequently used, and cross-arm guys are sometimes used.

### D. Supply-line Conductors.

1. MATERIAL.

All supply conductors shall be of copper, aluminum (with or without steel reinforcement), copper-covered steel, or other material which will not corrode excessively under the prevailing conditions. 263. GRADE N CONSTRUCTION-Continued.

D. Supply-line Conductors-Continued.

2. SIZE.

Supply-line conductors shall be not smaller than the following:

Table 30.—Grade N Minimu Supply-Line Con		Sizes for	
[A. W. G. for copper and aluminum	; Stl. W. G. for	steel]	
	Urban	Rural	
Soft copper	6	8	
Medium or hard-drawn cop- per	8	8	
Steel	9	9	
	Urban and rural		
Stranded aluminum	Spans 150 feet or less	Spans exceed- ing 150 feet	
Not reinforced	1	0	
Steel-reinforced	6	4	

Recommendation.—It is recommended that except as modified in Table 23, rule 261, F, 2, these minimum sizes for copper and steel be not used in spans longer than 150 feet for heavy-loading districts, and 175 feet for medium and light loading districts.

### 263. GRADE N CONSTRUCTION—Continued.

- E. Supply Services.
  - 1. MATERIAL.

All supply-service conductors shall be of copper, aluminum (with or without steel reinforcement), copper-covered steel, or other material which will not corrode excessively under the prevailing conditions.

- 2. SIZE OF OPEN-WIRE SERVICES.
  - (a) SEVEN HUNDRED AND FIFTY VOLTS OR LESS.
     Supply-service leads of 750 volts or less shall be not smaller than required by (1) or (2) below.
    - (1) SPANS NOT EXCEEDING 150 FEET-

Table 31.—Minimum Sizes of Service Leads Carrying 750 Volts or Less				
[A. W. G. for copper; Stl. W.	G. for steel]			
dj	Copp			
Situation	Soft-drawn	Medium or hard-drawn	Steel wire	
Alone	10	12	12	
Concerned with communication con- ductors	10	12	12	
Over supply conductors of— 0 to 750 volts 750 to 7,500 volts a Exceeding 7,500 volts a	10 8 6	$\begin{array}{c} 12\\10\\8\end{array}$	$\begin{array}{c} 12\\ 12\\ 9\end{array}$	
Over trolley contact conductors— 0 to 750 volts a. c. or d. c Exceeding 750 volts d. c	8 6	10 8	$\begin{array}{c} 12\\9\end{array}$	

<sup>a</sup> Installation of service leads of not more than 750 volts over supply lines of more than 750 volts should be avoided where practicable.

- 263. GRADE N CONSTRUCTION—Continued.
  - E. Supply Services-Continued.
    - 2. SIZE OF OPEN-WIRE-SERVICES-continued.
      - (a) Open-wire services of 750 volts or less—Con.
        (2) SPANS EXCEEDING 150 FEET. Sizes shall not be smaller than required for Grade C. (Rule 261, F, 2.)
      - (b) EXCEEDING 750 VOLTS. Sizes of supply-service leads of more than 750 volts shall be not less than required for supply-line conductors of the same voltage.
    - 3. SAG, OPEN-WIRE SERVICES.
      - (a) SEVEN HUNDRED AND FIFTY VOLTS OR LESS. Supply service leads of 750 volts or less shall have sags not less than the following:

Table 32.—Sags for Open-Wire Services				
Span lengths (in feet)	· Sag			
100 or less	Inches 12.			
100 to 125	18.			
125 to 150	27.			
Exceeding 150	Grade C sags. (See tables of Appendix B.)			

(b) EXCEEDING 750 VOLTS. Supply service leads of more than 750 volts shall comply as to sags with the requirements for supply line conductors of the same voltage.

25804°-27-11

- 263. GRADE N CONSTRUCTION—Continued.
  - E. Supply Services—Continued.
    - 4. CABLED SERVICES.
      - Supply service leads may be grouped together in a cable, provided the following requirements are met.
      - (a) SIZE. The size of each conductor shall be not less than required for leads of separate conductors (rule 263, E, 2).
      - (b) SAG. The sag of the cable should be not less than required for leads of separate conductors (rule 263, E, 3).
      - (c) INSULATION. The insulation should be sufficient to withstand twice the normal operating voltage.

# F. Lightning Protection Wires.

Lightning protection wires paralleling the line conductors shall be regarded, in respect to size and material requirements, as supply conductors.

G. Trolley Contact Conductors.

In order to provide for wear, no trolley contact conductors shall be installed of less size than No. 0, if of copper, or No. 4, if of silicon bronze.

# H. Cradles at Supply-Line Crossings.

Cradles should not be used.

Note.—It is less expensive and better to build the supply line strong enough to withstand extreme conditions than to build a cradle of sufficient strength to catch and hold the supply line if it falls.

## I. Communication Conductors.

There are no specific requirements for grade N communication line conductors or service drops.

#### SEC. 27. LINE INSULATORS

### 270. Application of Rule.

These requirements apply only to situations where grade A or B construction is required. They do not apply to line insulators in grades C, D, E, or N construction.

### 271. MATERIAL AND MARKING.

Insulators for operation on supply lines at voltages of 2,300 and above shall be of porcelain, made by the wet process or one equally suitable as regards electrical and mechanical properties, or other material which will give equally good results in respect to mechanical and electrical performance and durability. These insulators should be marked by the maker with a classification number and maker's name or trademark, the marks being applied so as not to reduce the electrical or mechanical strength of the insulator.

# 272. Electrical Strength of Insulators in Strain Position.

Where insulators are used in strain position they shall have not less electrical strength than the insulators generally used on the line when under the normal mechanical stresses imposed by the loadings specified in section 25.

# 273. RATIO OF FLASH OVER TO PUNCTURE VOLTAGE.

Insulators shall be designed so that their dry flashover voltage is not more than 75 per cent of their puncture voltage at a frequency of 60 cycles per second. 274. Test Voltages.

Insulators when tested under American Institute of Electrical Engineers' specifications shall flash over at values not less than given in Table 33.

#### Table 33.-Test Voltage Requirements

[Based on Line Conditions of Rule 276, B, 1]

Nominal line voltage	Minimum test dry flash-over voltage of insulators
750	_ 5, 000
2,300	_ 20, 000
4,000	_ 30, 000
6,600	_ 40, 000
11,000	_ 50, 000
22,000	_ 75, 000
33,000	_ 100, 000
44,000	125, 000
55,000	_ 150, 000
66,000	_ 175, 000
88,000	_ 220, 000
110,000	315, 000
132,000	
150,000	420, 000
200,000	_ 560, 000
(Interpolate for intermediate value	s)

275. FACTORY TESTS.

Each insulator or part thereof for use on lines operating at voltages in excess of 15,000 volts shall be subjected to a routine flash-over dry test at the factory for a period of three minutes at a frequency of 60 cycles per second or to any other test sanctioned by good modern practice, such as high-frequency tests.

- 276. Selection of Insulators.
  - A. Insulation of Constant-Current Circuits.

The insulation for constant-current circuits shall be determined on the basis of their nominal full-load voltage.

B. Insulators for Nominal Line Voltages.

In selecting insulators of the test voltage to be used for any nominal line voltage, consideration shall be given to the conditions under which the line will operate and to the presence of crossings as follows:

- 1. Where the system is of moderate extent with grounded neutral in open country subject to intermittent rains and moderate lightning and uses wood poles with suspension or pin-type insulators, insulators of the flash-over voltage required in Table 33 for the contemplated line voltage shall be used.
- 2. Where operating conditions are more severe than set forth in 1 above, due to steel construction, extent of system, use of ungrounded neutral, prevalence of exceptionally severe lightning, bad atmosphere due to chemical fumes, smoke, cement, dust, salt fog, or other foreign matter, or to a long dry season with heavy dust accumulation followed by moisture, larger insulators than the minimum specified in Table 33 should be used. The amount of increase is to be determined by local experience.

### 276. Selection of Insulators-Continued.

### B. Insulators for Nominal Line Voltages-Continued.

3. At crossings over steam railroads or over communication lines other than minor communication lines where grounded construction or ungrounded metallic pin or cross-arm construction is used, but where the line elsewhere is of woodpin construction the insulator shall have a dry flash-over test voltage of not less than 25 per cent greater than given in Table 33.

*Exception.*—The 25 per cent increase does not apply if all the insulators in the line are of the suspension type or if construction in accordance with rule 278 below is employed.

277. PROTECTION AGAINST ARCING.

In installing the insulators and conductors, such precautions as are sanctioned by good modern practice shall be taken to prevent, as far as possible, any are from forming or to prevent any arc which might be formed from injuring or burning any parts of the supporting structures, insulators or conductors which might render the conductors liable to fall.

278. Compliance with Rule 277 at Crossings.

At crossings, construction in accordance with the following methods will be considered as a means of meeting the requirements of rule 277 above.

A. Pin-Type Insulators.

1. DOUBLE CONSTRUCTION.

Double cross arms, pins, insulators, and conductor fastenings on the crossing supports.

?78. COMPLIANCE WITH RULE 277 AT CROSSINGS—Continued.

- A. Pin-Type Insulators-Continued.
  - 2. INSULATION AT CROSSING SUPPORTS.
    - (a) Insulators which meet the minimum values as given in Table 33 and have a rating not less than those in the remainder of the line, under the following conditions:
      - (1) Wood pins, ungrounded at the crossing supports, with wood or metal pins grounded or ungrounded throughout the line.
    - (b) Insulators which have a rating of 25 per cent greater than the requirements of Table 33, but not less than the insulators in the remainder of the line, under the following conditions:
      - (1) Wood pins, grounded at the crossing supports and throughout the line.
      - (2) Metal pins, grounded or ungrounded at crossing supports and throughout the line.
    - (c) Insulators at the crossing support which have a rating 50 per cent greater than those in the rest of the line, but not less than 25 per cent greater than required by Table 33 under the following conditions:
      - (1) Wood pins, grounded at crossing support and pins ungrounded throughout the remainder of the line.
      - (2) Metal pins, grounded at the crossing support and pins ungrounded throughout the remainder of the line.
      - (3) Metal pins, ungrounded at the crossing support with wood pins ungrounded throughout the remainder of the line.

- 278. COMPLIANCE WITH RULE 277 AT CROSSINGS-Continued.
  - B. Suspension Insulators.
    - 1. DOUBLE CROSS ARMS.

Double cross arms on crossing supports.

- Exception.—This does not apply to latticed or trussed steel cross arms nor to steel cross arms used with a single string of insulators as per 2 (b) following.
- 2. NUMBER OF INSULATOR STRINGS.
  - (a) DOUBLE INSULATOR STRINGS. Double strings of the insulators used on the crossing supports except under the special conditions covered in (b) following.
  - (b) SINGLE INSULATOR STRINGS. Where preferred single strings of insulators may be used if all the following conditions obtain.
    - (1) Steel cross arms on steel poles or structures.
    - (2) Hardware throughout providing a factor of safety of not less than 2 against the assumed maximum tension in the conductor in one direction.
    - (3) A high-strength clamp which will prevent the conductor under assumed maximum loading conditions from slipping into the crossing span.
    - (4) An extra unit where strings of 5 or less are used elsewhere in the line and 2 extra units where strings of 6 or more are normally used, these extra units to be provided in addition to those in 4 below.

278. COMPLIANCE WITH RULE 277 AT CROSSINGS—Continued. B. Suspension Insulators—Continued.

- 3. POSITION OF INSULATOR STRINGS. Insulators of the suspension type on crossing supports preferably should be used in the suspension or semistrain position except where conditions are such as to require the insulators to be used in the full-strain position.
- 4. INSULATORS IN SUSPENDED POSITION.
  - (a) UNGROUNDED CROSSING SUPPORTS. Insulators which meet the requirements of Table 33. In all cases the insulation at the crossing to be at least equal to that elsewhere in the line.
  - (b) GROUNDED SUPPORTS AT THE CROSSING AND ELSEWHERE IN THE LINE. Where supports throughout the line are grounded, insulators which meet the requirements of Table 33 with one extra unit in each string normally requiring 5 or less and 2 extra units in each string normally requiring 6 or more; in all cases, the insulation at the crossing to be at least equal to that elsewhere in the line.
  - (c) GROUNDED SUPPORTS AT CROSSING ONLY. Insulator strings which have one extra unit where the strings in other portions of the line normally have 5 or less and 2 extra units where the strings elsewhere in the line have 6 or more units; in all cases the insulators to meet (b) above.
- 5. INSULATORS IN STRAIN POSITION.

Where insulators are used in the strain position, one more unit than in 4 above to be used in each string.

- 278. Compliance with Rule 277 at Crossings—Continued.
  - B. Suspension Insulators-Continued.
    - 6. LIMIT FOR INCREASED NUMBER OF INSULATORS. In no case is the application of the above paragraphs to result in the addition of more than 2 disks to strings normally requiring 5 or less, nor more than 3 disks to strings normally requiring 6 or more.

### SEC. 28. MISCELLANEOUS REQUIREMENTS FOR OVERHEAD LINES

### 280. Supporting Structures.

# A. Poles and Towers.

1. RUBBISH.

Poles and towers shall be placed, guarded, and maintained so as to be exposed as little as practicable to brush, grass, rubbish, or building fires.

- 2. GUARDING POLES.
  - (a) PROTECTION AGAINST MECHANICAL INJURY. Where poles and towers are exposed to abrasion by traffic or to other damage which would materially affect their strength, they shall be protected by guards.
  - (b) PROTECTION AGAINST CLIMBING. On closely latticed poles or towers carrying supply conductors exceeding 300 volts to ground, either guards or warning signs shall be used except as follows:

Exception 1.—Where the right of way is completely fenced.

Exception 2.—Where the right of way is not completely fenced, provided the poles or towers are not adjacent to roads, regularly traveled thoroughfares, or places where people frequently gather, such as schools or public playgrounds.

280. SUPPORTING STRUCTURES—Continued.

A. Poles and Towers-Continued.

- 3. WARNING SIGNS.
  - (a) ON POLES OR TOWERS. For warning signs on poles or towers, see rule 280, A, 2, (b).
  - (b) ON BRIDGE FIXTURES. Structures attached to bridges for the purpose of supporting conductors shall be plainly marked with the name, initials, or trade-mark of the utility responsible for the attachment and, in addition, where the voltage exceeds 750 volts, by the following sign or its equivalent.

te." "Danger-Do Not Touch."

### 4. GROUNDING METAL POLES.

Metal poles not guarded or isolated shall always be specially grounded where in contact with metal-sheathed cable or the metal cases of equipment operating at voltages exceeding 750 volts.

Metal poles not guarded, isolated, or specially grounded should always be considered as imperfectly grounded and the insulators supporting line conductors as well as the strain insulators in attached span wires should, therefore, have a suitable margin of safety and be maintained with special care to prevent leakage to the pole as far as practicable.

### 5. POLE STEPS.

(a) METAL STEPS. Steps closer than  $6\frac{1}{2}$  feet from the ground or other readily accessible place shall not be placed on poles.

- 280. Supporting Structures—Continued.
  - A. Poles and Towers-Continued.
    - 5. POLE STEPS—continued.
      - (b) WOOD BLOCKS. One wood block (or on private right of way more than one) may be placed on poles carrying communication cables or paired conductors below supply conductors; but the lowest block is not to be less than 3½ feet from the ground or other readily accessible place. On poles carrying only communication conductors, additional wood blocks may be used.
    - 6. IDENTIFICATION OF POLES.

Poles, towers and other supporting structures on which are maintained electrical conductors shall be so constructed, located, marked, or numbered as to facilitate identification by employees authorized to work thereon. Date of installation of such structures shall be recorded where practicable by the owner.

7. OBSTRUCTIONS.

All poles should be kept free from posters, bills, tacks, nails, and other unnecessary obstructions, such as through bolts not properly trimmed.

- B. Cross Arms.
  - 1. LOCATION.

In general, cross arms should be maintained at right angles to the axis of the pole and to the direction of the attached conductors, and at crossings should be attached to that face of the structure away from the crossing, unless special bracing or double cross arms are used.

### 280. SUPPORTING STRUCTURES—Continued.

- B. Cross Arms—Continued.
  - 1. LOCATION—continued.

Note.—Double cross arms are generally used at crossings, unbalanced corners, and dead ends in order to permit conductor fastenings at two insulators and so prevent slipping, although single cross arms might provide sufficient strength. To secure extra strength, double cross arms are frequently used and cross arm guys are sometimes used.

2. BRACING.

Cross arms shall be securely supported, by bracing if necessary, so as to support safely loads to which they may be subjected, including linemen working on them. Any cross arm or buck arm, except the top one, shall be capable of supporting a vertical load of 225 pounds at either extremity in addition to the weight of the conductors.

C. Unusual Conductor Supports.

Where conductors are attached to structures other than those used solely or principally for supporting the lines, all rules shall be complied with as far as they apply and such additional precautions as may be deemed necessary by the administrative authority shall be taken to avoid injury to such structures or to the person using them. The supporting of conductors on trees and roofs should be avoided where practicable.

# 281. TREE TRIMMING.

# A. General.

Where trees exist near supply-line conductors, they shall be trimmed, if practicable, so that neither the movement of the trees nor the swinging or increased sagging of conductors in wind or ice storms or at high temperatures will bring about contact between the conductors and the trees.

*Exception.*—For the lower-voltage conductors, where trimming is difficult, the conductor may be protected against abrasion and against grounding through the tree by interposing between it and the tree a sufficiently nonabsorptive and substantial insulating material or device.

# B. At Wire Crossings and Railroad Crossings.

The crossing span and the next adjoining spans shall be kept free, as far as practicable, from overhanging or decayed trees which might fall into the line.

#### 282. GUYING.

#### A. Where Used.<sup>\*</sup>

When the loads to be imposed on poles, towers, or other supporting structures are greater than can be safely supported by the poles or towers alone, additional strength shall be provided by the use of guys, braces or other suitable construction.

Guys shall be used also, where necessary, whereever conductor tensions are not balanced, as at corners, angles, dead ends, and changes of grade of construction.

Note.—This is to prevent undue increase of sags in adjacent spans as well as to provide sufficient strength for those supports on which the loads are considerably unbalanced.

### 282. GUYING—Continued.

### B. Strength.

The strength of the guy shall meet the requirements of section 26 for the grade of construction that applies.

When guys are used with wood or other poles or towers capable of considerable deflection before failure, the guys shall be able to support the entire load in the direction in which they act, the pole acting simply as a strut.

C. Point of Attachment.

The guy should be attached to the structure as near as practicable to the center of the conductor load to be sustained.

D. Guy Fastenings.

Guys should be standard and where attached to anchor rods should be protected by suitable guy thimbles or their equivalent. Cedar and other soft wood poles to which any guy having a strength of 10,000 pounds or more is attached should be protected by the use of suitable guy shims and, where there is a tendency for the guy to slip off the shim, guy hooks or other suitable means of preventing this action should be used. Shims are not necessary in the case of supplementary guys, such as storm guys.

### E. Guy Guards.

The ground end of all guys attached to ground anchors exposed to traffic shall be provided with a substantial and conspicuous wood or metal guard not less than 8 feet long.

*Recommendation.*—It is recommended that in exposed or poorly lighted locations such guards be painted white or some other conspicuous color.

282. GUYING-Continued.

### F. Insulating Guys from Metal Poles.

Where anchors would otherwise be subject to electrolysis, guys attached to metal poles or structures and not containing guy insulators should be insulated from the metal pole or structure by suitable blocking.

G. Anchor Rods.

Anchor rods shall be installed so as to be in line with the pull of the attached guy when under load, except in rock or concrete. The anchor rod shall have an ultimate strength in the eye and shank equal to that required of the guy.

H. Grounding.

The anchored end of guys attached to wood poles carrying circuits of more than 15,000 volts shall be permanently grounded (see section 9 for method) wherever this part of the guy has a clearance of less than 8 feet to ground.

Exception 1.—This does not apply to guys in rural districts.

- Exception 2.—This does not apply if the guy contains an insulator which will meet the requirements of rule 283, A, 2 for the highest voltage liable to be impressed on it.
- 283. GUY INSULATORS.

¢.

### A. Properties of Guy Insulators.

- 1. MATERIAL.
  - (a) GRADES A AND B. Guy insulators shall be made by the wet-porcelain process or a process equally suitable as regards electrical and mechanical properties.
  - (b) GRADES C, D, E, AND N. No requirements are made for material.

- 283. GUY INSULATORS-Continued.
  - A. Properties of Guy Insulators-Continued.
    - 2. ELECTRICAL STRENGTH.

Guy insulators shall have a dry flash-over voltage at least double the normal line voltage and a wet flash-over voltage at least as high as the normal line voltage between conductors.

3. MECHANICAL STRENGTH.

Guy insulators shall have a mechanical strength at least equal to that required of the guys in which they are installed.

## B. Use of Guy Insulators.

1. ONE INSULATOR.

An insulator shall be located in each guy which is attached to a pole or structure carrying any supply conductors of more than 300 volts to ground and not more than 15,000 volts between conductors, or in any guy which is exposed to such voltages. This guy insulator shall be located from 8 to 10 feet above the ground.

*Exception*.—A guy insulator is not required where the guy is grounded under the conditions set forth in 4 following.

2. TWO INSULATORS.

Where a guy attached to any pole carrying communication or supply conductors or both, is carried over or under overhead supply conductors of more than 300 volts to ground and where hazard would otherwise exist, two or more guy insulators shall be placed so as to include the exposed section of the guy between them as far as possible. Neither insulator shall be within 8 feet of the ground.

*Exception.*—These insulators are not required where the guy is grounded under the conditions set forth in 4 following.

25804°-27-12

- 283. GUY INSULATORS-Continued.
  - B. Use of Guy Insulators-Continued.
    - 3. RELATIVE LOCATION OF INSULATORS IN GUYS LOCATED ONE ABOVE THE OTHER.

Where guys in which it is necessary to install insulators are so arranged that one crosses or is above another, insulators shall be so placed that in case any guy sags down upon another the insulators will not become ineffective.

- 4. CONDITIONS NOT REQUIRING GUY INSULATORS. Insulators are not required in guys under the following conditions:
  - (a) Where the guy is electrically connected to grounded steel structures or to a ground connection on wood poles.
  - (b) Where the guys are uniformly permanently grounded throughout any system of overhead lines.

### 284. Span-Wire Insulators.

### A. Mechanical Strength.

Span-wire insulators shall have a mechanical strength at least equal to that required of the span wire in which they are installed.

B. Use of Span-Wire Insulators.

All span wires, including bracket span wires, shall have a suitable strain insulator (in addition to an insulated hanger if used) inserted between each point of support of the span wire and the lamp or trolley contact conductor supported, except that single insulation, as provided by an insulated hanger, may be permitted when the span wire or bracket is supported on wooden poles supporting

### 284. SPAN-WIRE INSULATORS-Continued.

### B. Use of Span-Wire Insulators—Continued.

only trolley, railway feeder, or communication conductors used in the operation of the railway concerned. In case insulated hangers are not used, the strain insulator shall be located so that in the event of a broken span wire the energized part of the span wire can not be reached from the ground. *Exception.*—This rule does not apply to insulated feeder taps used as span wires.

### 285. Conductors.

### A. Identification.

All conductors of electrical supply and communication lines should be arranged to occupy definite positions throughout, as far as practicable, or shall be so constructed, located, marked, or numbered as to facilitate identification by employees authorized to work thereon. This does not prohibit systematic transposition of conductors.

### B. Branch Connections.

1. ACCESSIBILITY.

Connections of branches to supply circuits, service loops, and equipment in overhead construction shall be readily accessible to authorized employees. When possible, connections shall be made at poles or other structures.

2. CLEARANCE.

Branch connections shall be supported and placed so that swinging or sagging can not bring them in contact with other conductors, or interfere with the safe use of pole steps, or reduce the climbing or lateral working space.

### 286. Equipment on Poles.

### A. Identification.

All equipment of electrical supply and communication lines should be arranged to occupy definite positions throughout, as far as practicable, or shall be constructed, located, marked, or numbered so as to facilitate identification by employees authorized to work thereon.

### B. Location.

Transformers, regulators, lightning arresters, and switches when located below conductors or other attachments shall be mounted outside of the climbing space.

# C. Guarding.

Current-carrying parts of switches, automatic circuit-breakers, and lightning arresters shall be suitably inclosed or guarded if all the following conditions apply.

- 1. If of more than 300 volts to ground, and,
- 2. If located on the climbing side of the pole less than 20 inches from the pole center, and,
- 3. If located below the top cross arm.

### D. Hand Clearance.

All current-carrying parts of switches, fuses, lightning arresters, also transformer connections and other connections which may require operation or adjustment while alive and are exposed at such times, shall be arranged so that in their adjustment while alive the hand need not be brought nearer to any other current-carrying part at a different voltage than the clearances from pole surfaces required in Table 9, rule 235, A, 3, (*a*), for conductors of corresponding voltages. (See also rules 422 A, B, and C, pt. 4, NES Code, for Clearances from Live Parts.)

286.	<ul> <li>EQUIPMENT ON POLES—Continued.</li> <li>E. Street-Lighting Equipment.</li> <li>1. CLEARANCE FROM POLE SURFACE.</li> <li>All exposed metal parts of lamps and their supports (unless effectively insulated from the current-carrying parts) shall be maintained at the following distances from the surface of wood poles: Inches</li> </ul>
	(a) In general 20
	<ul> <li>(b) If located on the side of the pole opposite the designated climbing side_ 5</li> <li>Exception.—This does not apply where lamps are located at pole tops.</li> </ul>
	2. CLEARANCE ABOVE GROUND.
	Street lamps shall be mounted at not less than the following heights above ground.
	(a) Over Walkways 10
	(b) OVER ROADWAYS-
	Connected to circuits of 150 volts or less14
	Connected to circuits of more than 150 volts
	3. HORIZONTAL CLEARANCES.
	Arc and incandescent lamps in series circuits should have at least 3 feet horizontal clearance from windows, porches, and other spaces acces-
	sible to the general public.

4. MATERIAL OF SUSPENSION.

The lowering rope or chain for lighting units arranged to be lowered for examination or maintenance shall be of a material and strength designed to withstand climatic conditions and to sustain the lighting unit safely. The lowering rope or chain, its supports, and fastenings shall be examined periodically.

- 286. Equipment on Poles-Continued.
  - E. Street-Lighting Equipment-Continued.
    - 5. INSULATORS IN SUSPENSION ROPES. Effective insulators as specified in rule 283, A, should be inserted at least 8 feet from the ground in metallic suspension ropes or chains supporting lighting units of series circuits.
    - 6. ARC-LAMP DISCONNECTORS.

A suitable device shall be provided by which each arc lighting unit on series circuits of more than 300 volts to ground may be safely and entirely disconnected from the circuit before the lamp is handled unless the lamps are always worked on from suitable insulating stools, platforms, or tower wagons, or handled with suitable insulating tools, and treated as under full voltage of the circuit concerned.

- 287. PROTECTION FOR EXPOSED COMMUNICATION LINES.
  - A. Open Wire.

Communication lines for public use and fire-alarm lines shall be treated as follows if at any point they are exposed to supply (including trolley) lines of more than 400 volts to ground.

- 1. At stations for public use they shall be protected by one of the methods specified in part 3, section 39.
- 2. Elsewhere they shall be isolated by elevation or otherwise guarded so as to be inaccessible to the public.

### B. Metal-Sheathed Cable.

Metal-sheathed cables and messengers shall be isolated or grounded in conformity with the general requirements of section 21.

- 288. Communication Circuits Used Exclusively in the Operation of Supply Lines.
  - A. Choice of Method.

Communication circuits used exclusively in the operation of supply lines may be run either as ordinary communication circuits or as supply circuits under the conditions specified in rule 288, C and D, respectively. After selection of the type of communication-circuit construction and protection for any section which is isolated, or is separated by transformers, such construction and protection shall be consistently adhered to throughout the extent of such isolated section of the communication system.

B. Guarding.

Communication circuits used in the operation of supply lines shall be isolated by elevation or otherwise guarded at all points so as to be inaccessible to the public.

C. Where Ordinary Communication Line Construction May Be Used.

Communication circuits used in the operation of supply lines may be run as ordinary communication conductors under the following conditions:

- 1. Where such circuits are below supply conductors in the operation of which they are used (including high voltage trolley feeders) at crossings, conflicts, or on commonly used poles, provided:
  - (a) Such communication circuits occupy a position below all other conductors or equipment at crossings, conflicts or on commonly used poles.
  - (b) Such communication circuits and their connected equipment are adequately guarded and are accessible only to authorized persons.
  - (c) The precautions of section 39, part 3, and section 44, part 4, have been taken.

- 288. COMMUNICATION CIRCUITS USED EXCLUSIVELY IN THE OPERATION OF SUPPLY LINES—Continued.
  - C. Where Ordinary Communication Line Construction May Be Used—Continued.
    - 2. Where such circuits are below supply conductors in the operation of which they are used and are above other supply or communication conductors at wire crossings, conflicts, or on the same poles, provided the communication circuits are protected by fuseless lightning arresters, drainage coils, or other suitable devices to prevent the communication circuit voltage from normally exceeding 400 volts to ground.

Note.—The grades of construction for cominunication conductors with inverted levels apply.

### D. Where Supply Line Construction Must Be Used.

Communication circuits used in the operation of supply lines shall comply with all requirements for the supply lines with which they are used, where they do not comply with the provisos of C, 1 above or the proviso of C, 2 above.

- Exception 1.—Where the voltage of the supply conductors concerned exceeds 7,500, the communication conductors need only meet the requirements for a 7,500-volt supply circuit.
- Exception 2.—Where the supply conductors are required to meet grade C, the size of the communication conductors may be the same as for grade D (see rule 262, I, 2) for spans up to 150 feet.

289. ELECTRIC RAILWAY CONSTRUCTION.

A. Trolley Contact Conductor Supports.

All overhead trolley contact conductors shall be supported and arranged so that the breaking of a single contact conductor fastening will not allow the trolley conductor, live span wire, or current-carrying connection to come within 10 feet (measured vertically) from the ground, or from any platform accessible to the general public.

Span-wire insulation for trolley contact conductors shall comply with rule 284.

### B. High-Voltage Contact Conductors.

Every trolley contact conductor of more than 750 volts in urban districts where not on fenced right of way shall be suspended so as to minimize the liability of a break and, as far as practicable, so that if broken at a single point, it can not fall within 12 feet (measured vertically) from the ground or any platform accessible to the general public.

### C. Third Rails.

Third rails shall be protected where not on fenced rights of way by adequate guards composed of wood or other suitable material.

# **D.** Prevention of Loss of Contact at Railroad Crossings. Trolley contact conductors shall be arranged as set forth in either 1 or 2 following, at grade crossings with interurban or other heavy-duty or high-speed railroad systems.

1. The trolley contact conductor shall be provided with live trolley guards of suitable construction, or,

- 289. ELECTRIC RAILWAY CONSTRUCTION—Continued.
  - D. Prevention of Loss of Contact at Railroad Crossings-Continued.
    - 2. The trolley contact conductor shall be as far as practicable at the same height above its own track throughout the crossing span and the next adjoining spans. Where a uniform height above rail is not adhered to, the change shall be made in a very gradual manner. Where the crossing span exceeds 100 feet, catenary construction shall be used.
    - Exception.—This rule does not apply where the system is protected by interlocking derails or by gates.

### E. Guards Under Bridges.

1. WHERE GUARDING IS REQUIRED.

Guarding is required where the trolley contact conductor is so located that a trolley pole leaving the conductor can make simultaneous contact between it and the bridge structure.

2. NATURE OF GUARDING.

Guarding shall consist of a substantial inverted trough of nonconducting material located above the contact conductor, or other suitable means of preventing contact between the trolley pole and the bridge structure.

# SEC. 29. RULES FOR UNDERGROUND LINES

### 290. LOCATION OF DUCT SYSTEMS AND MANHOLES.

### A. General Location.

Underground systems of electrical conductors should be located so as to be subject to the least practicable disturbance. All railway tracks and all underground structures, including catch basins, gas pipes, etc., should be avoided where practicable. Conductors and cables carried underground under railways shall be placed in suitable ducts.

### B. Ducts.

The ducts between adjacent manholes or other outlets should be installed in straight lines. If curves are necessary, they should be of the longest practicable radius, and the spacing between adjacent manholes should be reduced proportionately.

# C. Manholes.

Manholes shall, where practicable, be located so as to provide convenient access and so that the least horizontal distance from any track rail to the nearest edge of the manhole opening will be not less than 3 feet. At crossings under railroads, manholes, pull boxes, and terminals shall be located away from the roadbed (preferably outside the fenced right of way).

### 291. Construction of Duct Systems.

### A. Material, Size, and Finish of Ducts.

Ducts shall be of such material, size, mechanical strength, and finish as to facilitate the installation and maintenance of conductors or cables. Ducts shall be freed from burrs before laying and shall have clear bores.

- 291. CONSTRUCTION OF DUCT SYSTEMS-Continued.
  - B. Grading of Ducts.

Grade of, ducts shall be such as to drain toward manholes or handholes. A grade of not less than 3 inches in 100 feet of length shall be provided where practicable.

C. Alignment of Ducts.

Ducts shall be laid so as to prevent inside shoulders at joints.

D. Duct Joints.

Joints in duct runs shall be made mechanically secure to maintain individual ducts in alignment.

- E. Protection.
  - 1. SETTLING.

Ducts should be suitably reinforced or be laid on suitable foundations of sufficient mechanical strength where necessary to protect them from settling.

2. DAMAGE.

Ducts should be protected by concrete or other covering where necessary to prevent being damaged by workmen when digging, or by other causes.

- F. Clearances.
  - 1. GENERAL.

The clearances between duct systems and other underground structures, particularly gas lines paralleling them, shall be as great as practicable. The distance between the top covering of the duct system and the pavement surface, or other surface under which the duct system is constructed, shall be sufficient to protect the duct system from injury.

291. CONSTRUCTION OF DUCT SYSTEMS-Continued.

F. Clearances-Continued.

2. RAILROAD TRACKS.

The distance between the top of the duct system structure and the base of the rail shall be not less than 30 inches in the case of street railways and not less than 42 inches in the case of steam and electric railroads.

Exception 1.—Where the ballast section subject to working and cleaning is less than 42 inches, the clearance may be reduced for street railways to not less than 18 inches; and for steam and electric railroads to not less than 30 inches; but in no case to less than the depth of ballast section plus 6 inches. In lieu of the additional depth of 6 inches, a 1½-inch creosoted plank, or 3 inches of concrete, or iron pipe may be provided.

Note.—The above clearances are based on a duct system, the width of which is not more than 3 creosoted wood ducts, 4 vitrified clay ducts, 4 impregnated fiber ducts or 4 iron or mild steel pipes. These clearances do not apply to bridge-type structures designed to sustain the weight of the roadbed and the operating load.

When a wider duct system is contemplated, additional strength of construction and protection should be provided, or the duct system should be placed at a greater depth.

Where unusually hard digging, as in rock, or when obstructions are encountered, a conduit run may be spread to a width of six ducts, so as to maintain the required clearance beneath the base of the rail.

Exception 2.—Where physical and chemical conditions will permit, a duct system consisting of not more than two iron pipes, not exceeding 3 inches in diameter, or two creosoted wood

- 291. CONSTRUCTION OF DUCT SYSTEMS-Continued.
  - F. Clearances—Continued.
    - 2. RAILROAD TRACKS—continued.

ducts, not exceeding  $4\frac{1}{2}$  inches square, used for communication lines or for service supply lines not exceeding 750 volts, may be laid in the ground beneath the tracks without any other form of protection at a depth not less than 18 inches below the base of the rail unless the worked ballast section of the roadbed exceeds 18 inches, in which case the duct system shall be laid below the ballast section.

# G. Separation Between Supply and Communication Duct Systems.

1. GENERAL.

Duct systems, including laterals, to be occupied by communication conductors for public use should be separated, where practicable, from duct systems, including laterals, for supply conductors by not less than 3 inches of concrete, 4 inches of brick masonry, or 12 inches of welltamped earth.

*Exception.*—Extensions may, however, be made to existing interconnected or jointly owned and jointly occupied duct systems used in common by municipalities, communication companies, or power companies with less effective separations than above specified.

. 91

2. ENTERING MANHOLES.

Where communication conductors and supply conductors occupy ducts terminating in the same manhole, the two classes of ducts should be separated as widely as practicable and where practicable should enter the manhole at opposite sides. *Explanation.*—This requirement is made so that cables can be racked along side walls with a minimum of crosses between the two classes of conductors.

291. CONSTRUCTION OF DUCT SYSTEMS-Continued.

H. Duct Entrances into Manholes.

1. CLEARANCES.

Duct entrances into manholes should, where practicable, have a clearance above the floor or below the roof line of not less than 6 inches, and from either side wall of at least 4 inches.

2. SMOOTH OUTLET.

Iron pipe conduit terminating in manholes, handholes, or other permanent openings of underground systems, shall be provided with an effective shield, bushing or other smooth outlet.

I. Sealing Laterals.

Lateral ducts for service connections to buildings, through which gas or water may enter buildings or other duct systems should be effectively plugged or cemented by the use of asphaltum, pitch, or other suitable means.

J. Duct Arrangement for Dissipation of Heat.

Duct systems intended to carry supply cables of large current capacity should be arranged where practicable, so that ducts carrying such cables, will not dissipate their heat solely through other ducts.

292. Construction of Manholes.

### A. Minimum Strength.

The design and construction of manholes and handholes shall provide sufficient strength to sustain, with a suitable margin of safety, the loads which may reasonably be imposed on them.

# 292. CONSTRUCTION OF MANHOLES-Continued.

### B. Dimensions.

Manholes should meet the following requirements where practicable:

1. WIDTH.

The least horizontal inside dimension should be not less than 3 feet 6 inches.

2. WORKING SPACE.

A clear working space should be provided. The horizontal dimension should be not less than 3 feet. The vertical dimension should be not less than 6 feet except in manholes where the opening is within 1 foot on each side of the full size of the manhole.

- *Exception.*—The dimensions specified in 1 and 2 above are not necessary in service boxes, handholes, or in manholes serving a small number of ducts, or in manholes used exclusively for communication system equipment and cables.
- C. Drainage.

Where drainage is into sewers, suitable traps shall be provided to prevent entrance of sewer gas into manholes.

D. Ventilation.

Adequate ventilation to open air shall be provided for manholes from which any openings exist into subways entered by the public.

Exception.—Subways under water or in other locations where it is impracticable to comply.

### E. Manhole Openings.

The opening to any manhole should be not less than 24 inches minimum dimension.

Recommendation. — Round openings are recommended.

292. CONSTRUCTION OF MANHOLES—Continued.

F. Manhole Covers.

Manholes and handholes, while not being worked in, shall be securely closed by covers of sufficient strength to sustain such loads as reasonably may be imposed upon them.

G. Supports for Cables.

Supports shall be provided, where necessary, for all cables at each manhole, handhole, or other permanent opening.

Note.—In handholes which reach the top line of ducts only, or in small manholes, the duct line itself may serve as sufficient support for the cables.

293. MANHOLE LOCATION.

Manhole openings, shall where practicable, be located so that barriers or other suitable guards can be placed to protect the opening effectively when uncovered.

- 294. LOCATION OF CONDUCTORS.
  - A. Accessibility.

Cables in manholes shall be reasonably accessible from the clear working space at all times. When cables pass by or cross over other cables, sufficient clearance shall be provided between them to prevent abrasion and to permit reasonable access to any cable for inspection or repair.

- B. Clearance from Manhole Floor. Each cable shall be maintained at a vertical clearance above the manhole floor of at least 6 inches, where practicable.
- C. Conductors Carrying Large Currents.

Conductors intended to carry large currents should be located, where practicable, in outside ducts so that they will not necessarily dissipate heat solely through adjacent ducts.

25804°-27-13

# 294. LOCATION OF CONDUCTORS—Continued.

# D. Separation Between Conductors.

1. CABLES OF DIFFERENT VOLTAGES.

Cables shall be arranged and supported in ducts and manholes so that those operating at higher voltages will be separated as far as practicable from those operating at lower voltages.

2. CABLES OF DIFFERENT SYSTEMS.

Cables belonging to different systems, particularly supply distribution and communication systems, shall not be installed in the same duct.

- 3. CONDUCTORS OF SUPPLY AND COMMUNICATION SYSTEMS.
  - (a) GENERAL. Supply conductors and communication conductors for public use should, in general, be maintained in separate duct systems, and particularly in separate manholes.
    - Exception.—Cable extensions may be made to existing interconnected or jointly owned and jointly occupied duct systems used in common by municipalities, communication companies or power companies.
  - (b) IN THE SAME MANHOLE. Supply conductors and communication conductors for public use occupying the same manhole should be maintained at opposite sides of the manhole.

Where supply and communication cables must cross, a separation of at least 1 foot shall be maintained.

295. PROTECTION OF CONDUCTORS IN DUCT SYSTEMS AND MANHOLES.

# A. Protection Against Moisture.

Cables shall be provided with a water-tight metal sheath or other waterproof covering over their insulating coverings.

*Exception.*—This requirement does not apply to rubber-insulated cables nor to cables used as ground connections or neutrals.

# B. Protection Against Arcing.

A suitable fire-resisting covering should be placed on the following cables to prevent injury from arcing:

- 1. Closely grouped lead-sheathed supply cables of more than 7,500 volts, or of large-current capacity operating at more than 750 volts a. c. or 300 volts d. c.
- 2. Communication cables and supply cables of large current capacity if they are within the the same manhole and within arcing distance of each other.
- 3. Communication cables and supply cables which cross each other in the same manhole. In this case the protective covering above specified is mandatory.

# C. Mechanical Protection.

1. CROSSINGS OF SUPPLY AND COMMUNICATION CABLES.

Special mechanical protection shall be provided against abrasion where supply and communication conductors must cross in the same manhole.

# 295. PROTECTION OF CONDUCTORS IN DUCT SYSTEMS AND MANHOLES—Continued.

### C. Mechanical Protection—Continued.

2. IRON PIPE CONDUIT.

Iron pipe conduit, terminating in manholes, handholes, or other permanent openings of underground systems, shall be provided with an effective shield, bushing, or other smooth outlet.

## 296. GUARDING OF LIVE PARTS IN MANHOLES.

### A. Conductor Joints or Terminals.

Joints or terminals of conductors or cables of supply

systems shall be arranged so that there are no bare ungrounded current-carrying metal parts exposed to accidental contact within manholes or handholes.

### B. Apparatus.

1. GENERAL.

Live parts of protective, control, or other apparatus of supply lines installed and maintained in manholes or handholes shall be inclosed in suitable grounded cases.

2. CONTINUITY BETWEEN CABLE SHEATH AND APPA-RATUS CASES.

The metal sheathing of all conductors or cables shall be made mechanically and electrically continuous with the metal cases of protective, control, or other apparatus.

# 297. CONSTRUCTION AT RISERS FROM UNDERGROUND.

A. Separation Between Risers of Communication and Supply Systems.

The placing of risers for communication systems and risers for supply systems on the same pole should be avoided where practicable. If it is necessary to use the same pole for the risers of both systems, they shall be placed on opposite semicircumferences of the pole where practicable.

### B. Mechanical Protection of Conductors.

All conductors or cables from underground systems which connect to overhead systems shall be protected by a covering which gives suitable mechanical protection up to a point 8 feet above the ground.

*Exception 1.*—Armored cables or cables installed in a grounded metal conduit.

Exception 2.—Communication circuits on private fenced rights of way.

### C. Grounding of Riser Pipes.

Exposed metal riser pipes containing supply conductors shall be grounded unless such conductors are covered with a grounded metal sheath or are themselves grounded.

# D. Conductor Terminal Construction.

The terminals of underground cables operating at more than 750 volts to ground and connecting to overhead open-wire systems shall meet the following requirements:

### 1. PROTECTION AGAINST MOISTURE.

Protection shall be provided so that moisture will not enter the cable.

### 297. CONSTRUCTION AT RISERS FROM UNDERGROUND-Con.

- D. Conductor Terminal Construction-Continued.
  - 2. INSULATION OF CONDUCTORS.

Conductors shall be properly insulated from the grounded metal sheath. In addition, the conductors of multiple conductor cable shall be properly separated and insulated from each other.

Note.—These requirements may be fulfilled by the use of potheads or other equivalent devices, such as oil switches, if incidentally they accomplish the same purpose.

**E.** Clearance Above Ground for Open Supply Wiring. Supply wires connecting to underground systems shall not be run open closer to the ground than is indicated by the following table:

	Voltage						
Location on pole	0 to 750 volts	750 to 15,000 volts	Exceeding 15,000 volts				
Side of pole adjacent to vehic- ular traffic	Feet 14	Feet 16	Feet 18				
Side of pole not adjacent to vehicular traffic	8	11	13				

Table 34.-Clearance Above Ground for Open Supply Wiring

### 298. Identification of Conductors.

Cables shall be permanently identified by tags or otherwise at each manhole, handhole, or other permanent opening of the underground system.

*Exception.*—This requirement does not apply where the position of a cable, in conjunction with diagrams supplied to workmen, gives sufficient identification, or where the manhole is occupied solely by the communication cables of one utility.

299. IDENTIFICATION OF APPARATUS CONNECTED IN MUL-TIPLE.

Where transformers, regulators, or other similar apparatus not located in the same manhole operate in multiple, special tags, diagrams, or other suitable means shall be used to indicate that fact.

*Exception.*—This requirement does not apply where disconnecting devices are provided to permit cutting such equipment completely off the system.

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# APPENDIXES TO PART 2 NATIONAL ELECTRICAL SAFETY CODE

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### Appendix A.—RECOMMENDED NORMAL SAGS OF COPPER OVERHEAD LINE CONDUCTORS, WITH CORRESPONDING TENSIONS AND STRESSES

While the following sags are those generally recommended, circumstances will sometimes call for modifications. For instance, where many large conductors are carried by a pole line, greater sags than those listed for the large conductors will sometimes be advisable, to reduce the loads on poles at turns and dead ends, and to permit smaller longitudinal guys where such guying is called for by the rules. (See rule 254 C.)

The figures given for the sags and tensions have been rounded off to the nearest value which can be readily measured by methods and instruments in practical use for this purpose. Simple and fairly accurate methods for measuring sags will be given in a future supplementary volume.

The sags are intended to apply to both solid and stranded conductors. The corresponding tensions and stresses, however, have been computed only for solid conductors.

### APPENDIX A

### Table 35.—Sags for Hard and Medium-Drawn Bare Copper Wire for Different Span Lengths

[At 30, 60, and 90° F.—wires without load]

Size	Grade of	Temper-		Sags for span length of—										
A. W. G. No.	construction	ature	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.	250 ft.	300 ft.	400 ft.	500 ft			
8	C	° F. 30 60 90	$In. \\ 8 \\ 12 \\ 16$	$In. \\ 11 \\ 18 \\ 22$	$In. \\ 22 \\ 27 \\ 32 \\ 32 \\ \end{bmatrix}$	In.	In.	In.	In.	In.	In.			
6	A	20 60 90	$     \begin{array}{c}       8 \\       12 \\       16     \end{array}   $	11 18 22	22 27 32									
6	В	30 60 90	$     \begin{array}{c}       6 \\       10 \\       14     \end{array}   $	10. 5 15 19. 5	16 22 27									
6	с	30 60 90	$     \begin{array}{c}       6 \\       10 \\       14     \end{array}   $	10. 5 15 19. 5	16 22 27	28 33 39								
4	All	30 60 90		10. 5 15 19. 5	$     \begin{array}{c}       16 \\       21 \\       26.5     \end{array} $	$22 \\ 28 \\ 34$	$32 \\ 38 \\ 45$	64 71 77	109 115 120					
2	All	30 60 90	$     \begin{array}{c}       6 \\       10 \\       14     \end{array}   $	10. 5 15 19. 5	13 18 23. 5	16 21 28	18.5 24 31	$35 \\ 44 \\ 51$	59 68 75	129 137 144	218 220 234			
1	All	30 60 90	6 10 14	$10.5 \\ 15 \\ 19.5$	13 18 23. 5	$     \begin{array}{c}       16 \\       21 \\       28     \end{array} $	$18.5 \\ 24 \\ 31$	$32 \\ 40 \\ 47$	51 59 67	113 120 130	19 20 21			
0	All	30 60 90	6 10 14	10. 5 15 19. 5	$13 \\ 18 \\ 23.5$	16 21 28	18.5 24 31	$31 \\ 38 \\ 46$	45 55 63	$100 \\ 110 \\ 120$	170 180 190			
00	All	30 60 90	6 10 14	10. 5 15 19. 5	13 18 23. 5	16 21 28	18.5 24 31	29 36 44	42 50 58	92 102 111	15 168 179			
0000	All	30 60 90	6 10 14	10.5 15 19.5	13 18 23. 5	16 21 28	$     \begin{array}{r}       18.5 \\       24 \\       31     \end{array} $	$26 \\ 32 \\ 40$	$34 \\ 42 \\ 50$	73 84 94	118 132 142			

#### HEAVY LOADING DISTRICTS

# Table 35.—Sags for Hard and Medium-Drawn Bare Copper Wire for Different Span Lengths—Continued

Size	Grade	Tem-				Sags	for sp	an leng	gth of—				
A.W.G. No.	of con- struc- tion	pera- ture	100 feet	125 feet	150 feet	175 feet	200 feet	250 feet	300 feet	400 feet	500 feet	700 feet	1,000 feet
8	c	° F 30 60 90	$In. \\ 5.5 \\ 8 \\ 12$	In. 8.5 12 17	$In. \\ 13 \\ 18 \\ 23. 5$	In.	In.	In.	In.	In.	In.	In.	In.
6	All	30 60 90	$5.5 \\ 8 \\ 12$	8.5 12 17	$13 \\ 18 \\ 23.5$	$18.5 \\ 24 \\ 30$							
4	All	30 60 90	5.5 $8$ $12$	$8.5 \\ 12 \\ 17 $	$13 \\ 18 \\ 23.5$	$18.5 \\ 24 \\ 30$	25 32 39	$35 \\ 42 \\ 50$	61 69 77	$134 \\ 141 \\ 149$			
2	All	30 60 90	5.5 $8$ $12$	$8.5 \\ 12 \\ 17 \\ 17$	$13 \\ 18 \\ 23.5$	16. 5 22 28	20 26 33	29 36 44	$41 \\ 50 \\ 58$	78 88 100	139 150 161	313 324 334	
1	All	30 60 90	5.5 $8$ $12$	$8.5 \\ 12 \\ 17 \\ 17$	$13 \\ 18 \\ 23.5$	$15.5 \\ 21 \\ 28$	$18.5 \\ 24 \\ 31$	24.5 31 39	$\begin{array}{c} 32\\ 40\\ 48 \end{array}$	$     \begin{array}{c}       62 \\       72 \\       83     \end{array}   $	$111 \\ 124 \\ 135$	275 286 298	
0	All	30 60 90	5.5 $8$ $12$	$8.5 \\ 12 \\ 17 \\ 17$	$^{13}_{18}_{23.5}$	15.5 20.5 27.5	18 23 29. 5	23. 5- 29 36	$29 \\ 37 \\ 44$	$54 \\ 64 \\ 74$	$95 \\ 108 \\ 120$	218 239 253	
00	A11	30 60 90	5.5 $8$ $12$	$8.5 \\ 12 \\ 17 \\ 17$	$13 \\ 18 \\ 23.5$	$15 \\ 20 \\ 26$	17 22 28	21. 27 34	$27 \\ 33 \\ 41$	$47 \\ 55 \\ 65$	80 92 104	177 192 208	396 415 429
0000	A11	30 60 90	$5.5 \\ 8 \\ 12$		$13 \\ 18 \\ 23.5$	$14.5 \\ 19 \\ 25$	16 21 27	19 24 30	23 27 33	41 48 57	66 76 88	140 154 171	304 323 340

#### MEDIUM LOADING DISTRICTS

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#### APPENDIX A

### Table 35.—Sags for Hard and Medium-Drawn Bare Copper Wire for Different Span Lengths—Continued

Size	Grade of con-				Sags	fo <b>r</b> spa	an leng	gth of	-				
A.W. G. No.	of con- struc- tion	struc-	100 feet	' 125 feet	150 feet	175 feet	200 feet	250 feet	300 feet	400 feet	500 feet	700 feet	1,000 feet
8	c	°F 30 60 90	In. 4.5 6 9	In. 6.5 9 13	In. 9.5 13 18	In. 15 20 26	In.	In.	In.	In.	In.	In.	In.
6	All	30 60 90	4.5 6 9	6.5 9 13	9.5 13 18	13. 5 18 24	18.5 24 30						
4	. <sup>All</sup>	30 60 90	4.5 6 9	6.5 9 13	9.5 13 18	$13.5 \\ 18 \\ 24$	17 22 28	20 25 32	32 40 48	69 80 90	$126 \\ 137 \\ 148$		
2	All	30 60 90	4, 5 6 9	6.5 9 13	9.5 13 18	$13.5 \\ 18 \\ 24$	14 18 23. 5	16.5 20 25	24.5 30 37	50 59 69	86 98 110	193 208 222	
1	A11	30 60 90	4, 5 6 9	6.5 9 13	9.5 13 18	$13.5 \\ 18 \\ 24 \\ 24$	14 18 23. 5	$16.5 \\ 20 \\ 25$	23 28 34	44 52 61	74 85 96	163 178 193	362 380 396
0	All	30 60 90	4.5 6 9	6.5 9 13	9.5 13 18	$13.5 \\ 18 \\ 24 \\ 24$	14 18 23. 5	16. 5 20 25	23 27 33	41 49 58	68 79 89	146 159 175	316 335 353
00	All	30 60 90	4.5 6 9	6.5 9 13	9.5 13 18	$13.5 \\ 18 \\ 24$	14 18 23. 5	$16.5 \\ 20 \\ 25$	22 26 32	39 46 54	62 72 83	125 140 154	276 290 309
0000	All	30 60 90	4.5 6 9	6.5 9 13	9.5 13 18	13.5 18 24	14 18 23. 5	16. 5 20 25	20 24 29	37 43 51	57 66 76	$113 \\ 126 \\ 141$	$225 \\ 246 \\ 264$

#### LIGHT LOADING DISTRICTS

### Table 36.—Sags for Hard and Medium-Drawn Covered Copper Wire for Different Span Lengths

[At 30, 60, and 90° F.-wires without load]

HEAVY LOADING DISTRICTS

Size	Grade of construc-	Tem-	Sags for span length of-									
A. W. G. No.	tion	per- ature	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.	250 ft.	300 ft.			
8	с	° <i>F</i> . 30 60 90	In. 15 18 21, 5	In. 23 27 31	In. 36 40 44	In.	In.	In.	In.			
6	A	30 60 90	15 18 21, 5	23 27 31	36 40 45							
6	В	30 60 90	11 15 18	$17.5 \\ 22 \\ 26 \\ 26 \\$	27 33 38				 			
6	C	30 60 90	8.5 12 15.5	$14 \\ 18 \\ 22.5$	22 27 32	31 36 40						
4	All	30 60 90	8.5 12 17	$14 \\ 18 \\ 22.5$	21.5 27 32	31 36 41	43 48 54					
2	All	30 60 90	8.5 12 17	$14 \\ 18 \\ 22.5$	21. 5 27 32	23.5 30 35	$30 \\ 36 \\ 42$	53 60 67	89 96 103			
1	All	30 60 90	8.5 12 15.5	$13.5 \\ 18 \\ 22.5$	$21 \\ 26 \\ 31$	23 29 34	27 33 39	44 52 59	72 80 87			
0	All	30 60 90	8.5 12 15.5	$13.5 \\ 18 \\ 22.5$	20.5 26 31	22.5 28 34	26 32 38	42 49 56	66 72 82			
00	All	30 60 90	8.5 12 16	$13.5 \\ 18 \\ 22.5$	20 25 30	22.5 28 34	25 31 38	38 46 53	57 66 73			
0000	A11	30 60 90	8.5 12 16	$13.5 \\ 18 \\ 22.5$	18.5 24 29	21 27 33	24.5 30 36	$31 \\ 38 \\ 46$	43 50 59			

### APPENDIX A

### Table 36.—Sags for Hard and Medium-Drawn Covered Copper Wire for Different Span Lengths—Continued

Size	Grade of construc-	Tem-										
A. W. G. No.	tion	per- ature	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.	250 ft.	300 ft.			
8	C	° <i>F</i> . 30 60 90	$In. \\ 11.5 \\ 15 \\ 18.5$	$In. \\ 18 \\ 22 \\ 26 $	In. 29 33 37	In.	In.	In.	In,			
6	A	30 60 90	$     11.5 \\     15 \\     18.5     $	$     \begin{array}{c}       18 \\       22 \\       26     \end{array} $	28 33 37							
6	В	30 60 90	$8.5 \\ 12 \\ 15.5$	$     \begin{array}{c}       14 \\       18 \\       22     \end{array} $	22 27 32	$31 \\ 36 \\ 41$						
6	C	30 60 90	$7.5 \\ 10 \\ 13.5$	11     15     19     1	$17.5 \\ 22 \\ 27 \\ 27$	25 30 36						
4	All	30 60 90	7 10 13, 5	$11.5 \\ 15 \\ 19.5$	$17.5 \\ 22 \\ 27 \\ 27$	$24 \\ 30 \\ 36$	$33 \\ 39 \\ 45$					
2	All	30 60 90	$     \begin{array}{c}       7 \\       10 \\       13.5     \end{array}   $	$11.5 \\ 15 \\ 19.5$	17.5 22 27	$22.5 \\ 27 \\ 34$	26 32 38	43 50 57	68 76 83			
1	All	30 60 90	7 10 14	$11 \\ 15 \\ 19.5$	17 22 27	$19.5 \\ 25 \\ 30$	23. 5 29 35	33 39 46	52 60 68			
0	All	30 60 90	$\begin{array}{c} 7\\10\\14\end{array}$	$11 \\ 15 \\ 19.5$	$17.5 \\ 22 \\ 27 \\ 27$	$19.5 \\ 24 \\ 31$	21. 5 27 33	$30 \\ 36 \\ 43$	40 54 62			
00	A11	30 60 90	7 10 14	$11 \\ 15 \\ 19.5$	$     \begin{array}{c}       17 \\       22 \\       27     \end{array} $	$19 \\ 24 \\ 30$	$21 \\ 26 \\ 32$	$\begin{array}{c} 27\\33\\40\end{array}$	40 48 56			
0000	All	30 60 90	$7 \\ 10 \\ 13.5$	$11 \\ 15 \\ 19.5$	$17 \\ 22 \\ 27 \\ 27$	18 23 29	$     \begin{array}{c}       19 \\       24 \\       30     \end{array} $	$23.5 \\ 29 \\ 35$	33 40 47			

#### MEDIUM LOADING DISTRICTS

### Table 36.—Sags for Hard and Medium-Drawn Covered Copper Wire for Different Span Lengths—Continued

LIGHT	LOADING	DISTRICTS
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Size	Grade of construc-	Tem-	Sags for span length of—									
A. W. G. No.	tion	per- ature	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.	250 ft.	300 ft.			
8	с	° F. 30 60 90	$In. \\ 8.5 \\ 12 \\ 15.5$	In. 14 18 22. 5	In. 22.5 27 32	$In. \\ 31 \\ 36 \\ 41$	In.	In.	In.			
6	A	30 60 90	$8.5 \\ 12 \\ 15.5$	$14 \\ 18 \\ 22.5$	22 27 32	$31 \\ 36 \\ 41$						
6	В	30 60 90	7 10 13	$11.5 \\ 15 \\ 19.5$	$17.5 \\ 22 \\ 27 \\ 27$	25 30 36	32 38 44					
6	C	30 60 90	6 8 11	9 12 16	14 18 22, 5	19.5 24 29	26 32 38					
4	All	30 60 90	6.5 $8$ 11.5	9 12 16	$14 \\ 18 \\ 22$	19 24 30	26 32 38					
2	All	30 60 90	6.5 $8$ 11.5	9 12 16	14 18 22	$17.5 \\ 22 \\ 27 \\ 27$	$21 \\ 26 \\ 32$	$28 \\ 34 \\ 41$	45 52 60			
1	All	30 60 90	5.5 $8$ $11.5$	9 12 16	$13.5 \\ 18 \\ 23$	$16.5 \\ 21 \\ 26$	19 24 30	26 31 38	38 45 53			
0	All	30 60 90	5.5 8 11.5	9 12 16.5	14 18 23	$16.5 \\ 21 \\ 27$	18 23 28	24.5 30 36	34 41 47			
00	All	30 60 90	5.5 8 11.5	9 12 16	13.5 18 23	$16 \\ 20 \\ 25$	$17.5 \\ 22 \\ 28 \\ 28 \\ 317 \\ 328 \\ 317 \\ 328 \\ 317 \\ $	23 28 35	31 37 45			
0000	All	30 60 90	5.5 8 11	$8.5 \\ 12 \\ 16 \\ 16 \\ 16 \\ 10 \\ 10 \\ 10 \\ 10 \\ 10$	$13.5 \\ 18 \\ 23$	$16 \\ 19 \\ 24.5$	$16.5 \\ 21 \\ 26$	20. 5 25 31	27 32 39			

25804°-27-14

#### APPENDIX A

### Table 37.—Sags for Soft-Drawn Covered Copper Wires for Different Span Lengths

[At 30, 60, and 90° F.—wires without load]

Size		Tem-		Sags for	span ler	igth of—	
A. W. G. No.	Grade of construction	pera- ture	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.
6	0	° <i>F</i> 30 60 90	In. 18 21 24	In. 28 32 36	In. 44 48 51	In.	In.
4	A	30 60 90	17.5 21 24	28 32 35	45 48 51		
4	B and C	30 60 90	14.5 18 21.5	23 27 31	36 40 44		
2	A	30 60 90	14.5 18 21.5	23 27 31	36 40 44	49 54 58	
2	B and C	30 60 90	11 15 18. 5	$17.5 \\ 22 \\ 26 \\ 26 \\ 17.5 \\$	28 33 38	40 45 50	55 60 64
1	Α	30 60 90	$10.5 \\ 15 \\ 18.5$	$17.5 \\ 22 \\ 26$	28 33 37	40 45 50	55 60 65
1	B and C	30 60 90	$8.5 \\ 12 \\ 15.5$	$13.5 \\ 18 \\ 22.5$	$21.5 \\ 27 \\ 32$	31 37 42	43 48 53
0	All	30 60 90	$     \begin{array}{r}       8.5 \\       12 \\       15.5 \\     \end{array} $	$13.5 \\ 18 \\ 22.5$	20.5 26 31	29 35 39	39 45 51
00	All	30 60 90	$8.5 \\ 12 \\ 15.5$	$     \begin{array}{r}       13.5 \\       18 \\       22.5     \end{array} $	20 25 30	28 33 38	36 42 48
0000	All	30 60 90	8.5 12 16	13.5 18 22.5	18.5 24 29	24.5 30 36	30 36 42

#### HEAVY LOADING DISTRICTS

# Table 37.—Sags for Soft-Drawn Covered Copper Wires for Different Span Lengths—Continued

Size		Tem-		Sag	s for spa	n length	of—	
A. W. G. No.	Grade of construction	pera- ture	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.	250 ft.
6	с	° <i>F</i> . 30 60 90	In. 14.5 18 21	In. 22 27 31	In. 36 40 44	In.	In.	In.
4	All	30 60 90	11 15 18, 5	$18 \\ 22 \\ 26 \\ 26 \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 \\ 18 \\ 1$	28 33 37	44 48 53		,
2	All	30 60 90	8.5 12 15.5	13.5 18 22	22, 5 27 32	31 36 41	43 48 53	
1	All	30 60 90	8.5 12 15.5	$13.5 \\ 18 \\ 22.5$	20 25 30	28 33 38	36 42 48	53 60 67
0	A]].	30 60 90	8.5 12 15.5	13.5 18 22.5	19 24 29	25 31 37	33 39 45	47 54 61
00	All	30 60 90	8.5 12 15.5	13.5 18 22.5	19 24 29	24.5 30 36	30 36 42	41 48 55
0000	A11	30 60 90		$13.5 \\ 18 \\ 22.5$	18, 5 24 29	24.5 30 36	30 36 42	41 48 55

#### MEDIUM LOADING DISTRICTS

#### APPENDIX A

# Table 37.—Sags for Soft-Drawn Covered Copper Wires for Different Span Lengths—Continued

Size		Tem-		Sag	s for span	n length	of—	
A. W.G. No.	Grade of construction	pera- ture	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.	250 ft.
6	A	° <i>F</i> . 30 60 90	In.     14     18     21.5	In. 23 27 31	$In. \\ 36 \\ 40 \\ 44$	In.	In.	In.
6	B and C	30 60 90	$11 \\ 15 \\ 18.5$	$17.5 \\ 22 \\ 26$	29 33 37			
4	All	30 60 90	$8.5 \\ 12 \\ 15.5 $	$13.5 \\ 18 \\ 22.5$	20 25 30	26 32 37	$\begin{array}{c} 36\\42\\47\end{array}$	
2	All	30 60 90	7 10 13. 5	$^{11}_{15}_{19.5}$	$16 \\ 21 \\ 26$	22 27 33	$30 \\ 36 \\ 42$	41 48 55
1	All	30 60 90	7 10 14	$^{11}_{15}_{19.5}$	$15 \\ 20 \\ 25$	$19.5 \\ 25 \\ 31$	24 30 36	$35 \\ 42 \\ 49$
0	All	30 60 90	7 10 14	$11 \\ 15 \\ 19.5$	$15.5 \\ 20 \\ 25$	$20 \\ 25 \\ 31$	$24.5 \\ 30 \\ 36$	$35 \\ 42 \\ 49$
00	All	30 60 90	7 10 14	11 15 19, 5	$15 \\ 20 \\ 25$	$19.5 \\ 25 \\ 31$	$24 \\ 30 \\ 36$	$35 \\ 42 \\ 49$
0000	All	30 60 90	7 10 14	$10.5 \\ 15 \\ 19.5$	$15.5 \\ 20 \\ 25$	$19.5 \\ 25 \\ 31$	$24 \\ 30 \\ 36$	$35 \\ 42 \\ 49$

#### LIGHT LOADING DISTRICTS

HEAVY LOADING DISTRICTS

-											
Size A W G	Grade of con-	Conditions of load and			T	Tensions for span length of-	or span ]	length of	.ł.		
	struction	temperature	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.	250 ft.	300 ft.	400 ft.	500 ft.
		° F. 30 no load 60 no load 90 no load 0 loaded	Lbs. 94 63 47 442	Lbs. 92 53 53 503	Lbs. 76 54 520	Lbs.	Lbs.	Lbs.	Lbs.	Lbs.	Lbs.
A		30 no load 60 no load 90 no load 0 loaded	150 99 74 570	145 105 85 630	120 99 86 670						
		30 no load 60 no load 90 no load 0 loaded	120 120 84 590	180 125 95 650	165 120 710						
о. С		30 no load 60 no load 90 no load 0 loaded	120 120 84 590	180 125 95 650	165 120 710	$125 \\ 110 \\ 96 \\ 740$					
AII.		30 no load 60 no load 90 no load 0 loaded	290 190 135 740	280 150 840	270 200 160 900	260 210 175 960	$^{240}_{170}$	$185 \\ 170 \\ 155 \\ 1,000 $	160 150 145 990		
ПА		30 no load 60 no load 90 no load 0 loaded	460 300 210 1,000	$^{450}_{240}$	$ \begin{array}{c} 510 \\ 380 \\ 290 \\ 1, 250 \\ \end{array} $	590 440 340 1, 350	$650 \\ 500 \\ 400 \\ 1, 450$	540 430 370 1, 550	470 400 370 1, 550	380 350 340 1, 600	350 340 330 1,600

# TENSIONS FOR HARD COPPER

189

Lengths	
Span	
pper Wire for Different Span Le	ed Sags of Table 35-Continued
Coppe	gs of T
Table 38,Tensions in Hard and Medium-Drawn Bare C	Corresponding to the Recommended Sags

HEAVY LOADING DISTRICTS-Continued

Size	Grade of con-	Conditions of load and			Te	nsions fo	Tensions for span length of-	ength of	1		
A. W. G. No.		temperature	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.	250 ft.	300 ft.	400 ft.	500 ft.
	All	◦ F. 30 no load 60 no load 90 no load 0 loaded	Lbs. 580 380 1, 200	Lbs. 520 400 300 1, 250	${ Lbs. \\ 650 \\ 650 \\ 470 \\ 370 \\ 1, 450 \\ \end{array} }$	Lbs. 740 550 430 1,600	Lbs. 820 630 500 1,700	Lbs. 730 600 1,800	Lbs. 670 580 1,900	Lbs. 540 510 1,900	Lbs. 490 470 1,900
00	All-	39 no load 60 no load 90 no load 0 loaded	$ \begin{array}{c} 730 \\ 480 \\ 340 \\ 1,400 \end{array} $	$^{720}_{500}$ $^{380}_{1,500}$	820 600 1, 650	930 700 540 1, 850	1,050 800 630 2,000	970 790 660 2, 150	950 790 690 2, 200	760 710 650 2, 300	$^{710}_{670}$
00	All	30 no load 60 no load 90 no load 0 loaded	920 600 1, 700	910 630 480 1,750	$1,050\\750\\580\\1,950$	$\begin{smallmatrix} 1, 150 \\ 880 \\ 680 \\ 2, 150 \end{smallmatrix}$	$^{1,300}_{1,000}$ $^{2,350}_{2,350}$	$1,300 \\ 1,050 \\ 850 \\ 2,550 \\ 1,050 $	$1,300 \\ 1,100 \\ 930 \\ 2,900$	$\substack{1,050\\950\\880\\2,650}$	960 910 850 <b>2,</b> 650
0000	All.	30 no load 60 no load 90 no load 0 loadd	$\begin{smallmatrix} 1,450\\960\\680\\2,500\end{smallmatrix}$	$1,450 \\ 1,000 \\ 770 \\ 2,500$	$\begin{smallmatrix} 1, 650 \\ 1, 200 \\ 2, 800 \\ 2, 800 \\ \end{smallmatrix}$	1,850 1,400 3,100	2,050 1,600 3,350 3,350	2,300 1,850 3,750 3,750	2, 500 2, 050 4, 100	$\begin{matrix} 2,100\\ 1,850\\ 1,650\\ 4,000 \end{matrix}$	2,000 1,850 1,700 4,150

190

# APPENDIX A

	1,000ft.	Lbs.						$1,550 \\ 1,450 \\ 1,400 \\ 2,850 \\$
	700 ft.	Lbs.			$^{480}_{460}$ $^{450}_{1,350}$	680 650 620 1,600	$1,050 \\ 980 \\ 930 \\ 2,100$	$^{1,650}_{1,550}$
	500 ft.	Lbs.			540 500 470 1,350	850 770 1,700	1,250 1,100 2,100	1,850 1,650 1,450 2,850
	400 ft.	Lbs.		230 220 810 810	620 550 460 1, 350	980 850 740 1, 700	1,400 1,200 2,200 2,200	$\begin{array}{c} 2,050\\ 1,750\\ 1,500\\ 2,850 \end{array}$
Tensions for span length of-	300 ft.	Lbs.		220 220 220 220 220	$650 \\ 540 \\ 470 \\ 1, 250 \\ 1$	1,050 850 700 1,650	$^{1,450}_{1,200}$ $^{980}_{2,050}$	$\begin{array}{c} 2,000\\ 1,650\\ 2,650\\ 2,650\end{array}$
or span l	250 ft.	Lbs.		340 280 820	650 520 430 1, 150	950 760 610 1, 500	$1,300 \\ 1,050 \\ 830 \\ 1,850$	$1,750\\1,400\\1,150\\2,350$
ensions f	200 ft.	Lbs.		300 240 720	600 460 370 1,050	840 630 490 1, 300	${}^{1,050}_{830} \\ {}^{830}_{650} \\ {}^{1,550}_{1,550}$	$1,400 \\ 1,100 \\ 850 \\ 1,950$
Т	175 ft.	Lbs.	200 150 125 540	320 240 690	550 290 970	740 550 420 1, 150	940 710 540 1,450	1, 250 920 1, 750
	150 ft.		2002 1120 2002 2002 2002	320 240 185 660	510 380 900	650 470 370 1,050	$^{820}_{600}$ $^{470}_{470}$ 1, 250	$1,050 \\ 590 \\ 1,500 $
	125 ft.	Lbs. 140 97 71	360 220 1155 110 470	360 250 630	570 390 860	710     490     360     1,050	$^{900}_{620}$	$1, 150 \\ 780 \\ 570 \\ 1, 500 \\ .$
	100 ft.	Lbs. 140 94 63	330 150 130 430	360 240 160 580	570 380 830 830	$^{720}_{480}$ $^{480}_{320}$ $^{320}_{1,000}$	$^{910}_{600}$ $^{400}_{1, 200}$	$^{1,150}_{760}$ $^{510}_{1,450}$
Conditions of	perature	◦ F. 30 no load 60 no load 90 no load	15 loaded 30 no load 60 no load 90 no load 15 loaded	30 no load 60 no load 90 no load 15 loaded	30 no load 60 no load 90 no load 15 loaded	30 no load 60 no load 90 no load 15 loaded	30 no load 60 no load 90 no load 15 loaded	30 no load 60 no load 90 no load 15 loaded -
Grade of	tion	G	All	All	All	All	All	АЛ
Size	No.	œ	60	4	2	1	00	00

MEDIUM LOADING DISTRICTS

IDISTRICTS

191

Table 38.—Tensions in Hard and Medium-Drawn Bare Copper Wire for Different Span Lengths         Corresponding to the Recommended Sags of Table 35—Continued         MEDIUM LOADING DISTRICTS—Continued	Tensions for span length of	5 ft. 150 ft. 175 ft. 200 ft. 250 ft. 300 ft. 400 ft. 500 ft. 700 ft 1,000 ft.	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	LIGHT LOADING DISTRICTS	180         175         150           130         130         115           91         94         90           220         230         230	290         280         270         260           110         210         200         200           145         150         160           340         350         350	460         450         430         450         590         520         440         380           330         330         320         340         470         330         340         470         500	
m-Drawn Bare commended Sa JADING DISTRI	Ter	150 ft.	Lbs. 1, 650 1, 200 2, 250 2, 250	T LOADING DI	175 130 94 230	280 210 340	450 330 240 510	710 680 520 510 380 300
rd and Mediu ling to the Re- MEDIUM L		100 ft. 125 ft.	Lbs.         Lbs.           1, 800         1, 800           1, 200         1, 250           2, 250         2, 300	LIGH		280 290 290 210 210 210 210 210 210 210 210 210 21	490 500 500 500 500 500 500 500 500 500 5	710 730 510 520 330 370
nsions in Ha Correspond		- load and tem-	° F. 30 no load 60 no load 90 no load 15 loaded		30 no load 60 no load 90 no load 30 loaded	30 no load 60 no load 90 no load 30 load	30 no load 60 no load 90 no load 30 loaded	
ie 38.—Te	ze Grade of	W. G. construc- No. tion	0000 All	-	00	6 All	All	All

192

# APPENDIX A

## TENSIONS FOR HARD COPPER

1,050 1,000 970 1,450	$1,500 \\ 1,450 \\ 1,350 \\ 2,050 \\ 2,050 \\ 2,050 \\ 2,050 \\ 3,05$	2,200 2,100 1,950 2,750	$\begin{array}{c} 4,\ 250\\ 3,\ 900\\ 4,\ 750\end{array}$	
1, 150 1, 050 1, 500	$1,600\\1,450\\1,350\\2,000$	2,350 2,100 2,700 2,700	$\begin{array}{c} 4, 150\\ 3, 700\\ 3, 350\\ 4, 550\end{array}$	0.00
$1,300\\1,100\\980\\1,550$	$^{1,750}_{1,500}$	2,400 2,100 2,650	$\begin{array}{c} 4,\ 200\\ 3,\ 600\\ 4,\ 400\end{array}$	0.00
$1,400\\1,150\\990\\1,550$	$\substack{1,\ 800\\1,\ 550\\1,\ 300\\2,\ 050\end{array}$	2,450 2,100 1,800 2,650	$\begin{array}{c} 4,\ 200\\ 3,\ 550\\ 4,\ 400\end{array}$	
$1, \frac{450}{1}, 200$ 1, 200 1, 550	$^{1,\ 900}_{1,\ 600}$	$\begin{array}{c} 2,500\\ 2,100\\ 1,700\\ 2,600\end{array}$	$\begin{array}{c} 4, \ 300 \\ 3, \ 600 \\ 2, \ 950 \\ 4, \ 300 \end{array}$	
$1, 450 \\ 1, 200 \\ 940 \\ 1, 500$	1,800 1,500 1,200 1,900	2,300 1,900 2,350 2,350	$\begin{array}{c} 3,650\\ 3,000\\ 2,400\\ 3,700\end{array}$	_
$1,100\\840\\650\\1,200$	$1,400 \\ 1,050 \\ 820 \\ 1,450$	$1,750 \\ 1,350 \\ 1,050 \\ 1,80$	$\begin{array}{c} 2,750\\ 2,100\\ 1,650\\ 2,900 \end{array}$	
860 640 940	$1,100 \\ 810 \\ 620 \\ 1,200$	$1,350 \\ 1,050 \\ 780 \\ 1,450$	$\begin{array}{c} 2,150\\ 1,650\\ 1,250\\ 2,250 \end{array}$	
890 650 980 980	$1,150\\830\\600\\1,200$	$1, 400 \\ 1, 050 \\ 760 \\ 1, 500 \\$	$\substack{2, 250\\1, 650\\2, 350\\2, 350\end{array}$	
920 660 970	$1,150 \\ 830 \\ 580 \\ 1,200 \\ 1,200 \\$	$1, 450 \\ 1, 050 \\ 730 \\ 1, 500 \\ 1, 500 \\ 1$	$\begin{matrix} 2, 350 \\ 1, 650 \\ 1, 150 \\ 2, 350 \end{matrix}$	
900 640 940	$1,150\\800\\520\\1,200$	$1, 450 \\ 1, 000 \\ 660 \\ 1, 500$	$\begin{array}{c} 2,\ 200\\ 1,\ 600\\ 2,\ 300\\ 2,\ 300 \end{array}$	
<b>30</b> no load <b>60</b> no load <b>90</b> no load	30 no load 60 no load 90 no load	30 no load 60 no load 90 no load 30 loaded	30 no load 60 no load 90 no load 30 loaded	
All	All	All	All	
11	0	00	0000	

## APPENDIX A

## Table 39.—Tensions in Hard and Medium-Drawn Covered Copper Wire for Different Span Lengths Corresponding to the Recommended Sags of Table 36

Size	Grade of	Conditions of		Te	nsions f	or span	length	of—	
A. W. G. No.	construc- tion	load and tem- perature	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.	250 ft.	300 ft.
		° <i>F</i> .	Lbs.	Lbs.	Lbs.	Lbs.	Lbs.	Lbs.	Lbs.
8	C	30 no load	77	77	72				
		60 no load	62	65	63				
		90 no load 0 loaded	54 470	58 520	59 560				
6	A	30 no load 60 no load	115	115	105				
		90 no load	94 81	98 87	95 87				
		0 loaded	580	640	670				
6	В	30 no load	155	155	135				
0	D	60 no load	110	$155 \\ 120$	135				
		90 no load	94	105	105				
		0 loaded	600	680	720				
6	С	30 no load	195	190	170	165	1.15		
0		60 no load	140	145	140	145			
		90 no load	108	120	120	130			
		0 loaded	640	710	760	820			
4	All	30 no load	270	280	260	240	230		
		60 no load	210	210	210	210	210		
		90 no load	155	170	175	185	185		
		0 loaded	820	900	950	1,000	1,050		
2	All	30 no load	430	440	410	500	530	460	400
		60 no load	330	340	330	400	430	410	370
		90 no load	250	270	280	340	380	370	320
		0 loaded	1, 100	1, 150	1, 200	1, 350	1, 500	1, 550	1, 500
1	All	30 no load	560	540	510	630	710	660	590
		60 no load	400	410	410	500	570	570	540
		90 no load 0 loaded	310 1, 200	330 1, 300	350 1,350	430 1,550	490	510 1,700	490 1,850
							·	, i	
0	All	30 no load	710	690	670	820	930	910	870
		60 no load	510	530	530	660	750	780 680	770 680
		90 no load	390 1,450	430 1,550	450	550 1,850	630 2,000	2,050	2,200
				l '				( ·	
00	All	30 no load	890	860	840	1,000	1,200	1,200	1,200
		60 no load 90 no load	630 480	650 520	680 570	830 680	970 810	1,000	1,050 910
		0 loaded	1,700	1,800	1,850	2,100	2,350	2,500	2,600
0000	A11	30 no load	1,350	1,350	1,400	1,650	1,850	2,250	2, 450
0000	A	60 no load	960	1,000	1,100	1,300	1,550	1,900	2, 050
		90 no load	730	810	920	1,100	1,300	1,600	1,750
		0 loaded	2,450	2, 500	2,650	3,000	3, 300	3,850	4, 200

#### HEAVY LOADING DISTRICTS

# Table 39.—Tensions in Hard and Medium-Drawn Covered Copper Wire for Different Span Lengths Corresponding to the Recommended Sags of Table 36—Continued

Size	Grade of	Conditions of		Te	nsions f	or span	length	of—	
A. W. G. No.	construc- tion	load and tem- perature	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.	250 ft.	300 ft.
		° <i>F</i> .	Lbs.	Lbs.	Lbs.	Lbs.	Lbs.	Lbs.	Lbs.
8	C	30 no load	98 75	98 80	89 76				
		90 no load	61	68	69				
		15 loaded	330	400	390				
6	A	30 no load	150	150	135				
		60 no load	115	120	115				
		90 no load	93	100	105				
		15 loaded	420	460	480				
6	В	30 no load	195	190	170	170			
		60 no load	140	145	140	145			
		90 no load 15 loaded	110 450	120 490	120 520	130 550			
		10 10/10/10/10/10	100			000			
6	C	30 no load	230	230	220	210			
		60 no load 90 no load	$170 \\ 125$	175 140	170 140	175 150			
		15 loaded	480	530	560	590			
4	All	30 no load	350 250	340	320 250	290 250	300		
		60 no load 90 no load	180	200	230	250	250 220		
		15 loaded	620	680	710	750	780		
2	All	30 no load	560	540	510	530	600	560	520
		60 no load	390	410	400	440	490	490	470
		90 no load	290	320	330	360	410	430	430
		15 loaded	870	930	950	1,050	1,150	1,200	1, 200
1	All	30 no load	670	670	620	750	820	900	830
		60 no load	470	490	490	580	660	760	710
		90 no load 15 loaded	350 1,000	390 1,100	390 1,100	480	540 1,350	640 1,550	630
		10 10aueu	1,000	1,100	1,100	1, 200	1,000	1,000	1,550
0	All	30 no load	870	850	790	950	1,100	1,250	1,200
		60 no load 90 no load	610 440	630 490	620 510	710 610	900 730	1,050	1,000
		15 loaded	1,250	1,300	1,300	1,500	1,700	880 1,950	890 1,950
00		00 1 1							
00	All	30 no load 60 no load	$1,050 \\ 750$	1,050 780	990 770	1,200 960	1,450	1,750	1,650
		90 no load	550	610	630	780	950	1,400 1,200	1,400 1,200
		15 loaded	1,500	1,550	1,500	1,750	2,000	2,350	2,400
0000	All	30 no load	1,700	1,650	1,500	1,950	2,400	3,050	3,100
0000		60 no load	1,150	1, 200	1,200	1, 550	1,900	2,450	2,600
		90 no load	840	920	970	1,250	1,550	2,100	2,200
		15 loaded	2,200	2,250	2, 150	2,600	3, 150	3, 750	3, 950

#### MEDIUM LOADING DISTRICTS

# APPENDIX A

# Table 39.—Tensions in Hard and Medium-Drawn Covered Copper Wire for Different Span Lengths Corresponding to the Recommended Sags of Table 36—Continued

Size	Grade of	Conditions of		$\mathbf{T}e$	nsions f	or span	length	of—	
A. W. G. No.	construc- tion	load and tem- perature	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.	250 ft.	300 ft.
8	с	°F. 30 no load	Lbs. 130	Lbs. 125	Lbs. 115	Lbs. 115	Lbs.	Lbs.	Lbs.
		60 no load 90 no load 30 loaded	94 73 220	97 79 240	94 79 260	96 84 270			
6	A	30 no load 60 no load 90 no load 30 loaded	$195 \\ 140 \\ 110 \\ 310$	$     \begin{array}{r}       190 \\       150 \\       120 \\       330     \end{array} $	$170 \\ 140 \\ 120 \\ 340$	$170 \\ 145 \\ 130 \\ 360$			
6	В	30 no load 60 no load 90 no load 30 loaded	$250 \\ 170 \\ 130 \\ 340$	$230 \\ 175 \\ 140 \\ 360$	$220 \\ 175 \\ 140 \\ 380$	$210 \\ 170 \\ 145 \\ 400$	$200 \\ 180 \\ 155 \\ 420$		
6	C	30 no load 60 no load 90 no load 30 loaded	290 210 155 380	$     \begin{array}{r}       290 \\       220 \\       165 \\       410     \end{array} $	$270 \\ 210 \\ 170 \\ 420$	$270 \\ 220 \\ 180 \\ 440$	$260 \\ 210 \\ 180 \\ 450$		
4	All	30 no load 60 no load 90 no load 30 loaded	$430 \\ 310 \\ 220 \\ 530$	$     \begin{array}{r}       430 \\       320 \\       240 \\       560     \end{array} $	390 310 230 570	$390 \\ 310 \\ 250 \\ 600$	$380 \\ 310 \\ 260 \\ 620$		
2	All	30 no load 60 no load 90 no load 30 loaded	690 490 340 770	680 510 380 810	$630 \\ 490 \\ 360 \\ 810$	690 540 430 900	740 600 490 970	870 720 600 1, 150	790 670 590 1, 100
1	All	30 no load 60 no load 90 no load 30 loaded	840 600 410 920	840 620 460 960	790 600 470 940	890 700 560 1, 050	1,000 790 640 1,200	1, 150 960 790 1, 400	1, 100 950 810 1, 400
0	All	30 no load 60 no load 90 no load 30 loaded	$1,050\760\540\1,150$	$1,050 \\790 \\590 \\1,200$	990 750 590 1, 150	1, 100 890 700 1, 300	${ \begin{smallmatrix} 1,\ 350\\ 1,\ 050\\ 850\\ 1,\ 550 \end{smallmatrix} }$	$1,550 \\ 1,250 \\ 1,050 \\ 1,750$	1, 600 1, 350 1, 150 1, 850
00	All	30 no load 60 no load 90 no load 30 loaded	${ \begin{smallmatrix} 1,\ 350\\ 950\\ 660\\ 1,\ 300 \end{smallmatrix} }$	$1,350 \\990 \\730 \\1,450$	$1,250 \\ 940 \\ 740 \\ 1,400$	$1,450 \\ 1,150 \\ 900 \\ 1,650$	1,700 1,350 1,100 1,900	2,050 1,650 1,350 2,250	2, 150 1, 800 1, 550 2, 400
0000	A11	30 no load 60 no load 90 no load 30 loaded		2, 100 1, 500 1, 100 2, 200	1,900 1,450 1,150 2,050	2, 400 1, 850 1, 450 2, 500	2,750 2,200 1,750 2,900	3, 500 2, 850 2, 350 3, 700	3, 850 3, 200 2, 700 4, 050

#### LIGHT LOADING DISTRICTS

# Table 40.—Tensions in Soft-Drawn Covered Copper Wire for Different Span Lengths Corresponding to the Recommended Sags of Table 37

HEAVY LOADING DISTRICTS

Size	Grade of	Conditions of load and	Т	'ensions f	for span	length of	·
A. W. G. No.	construction	temperature	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.
6	C	°F. 30 no load 60 no load 90 no load 0 loaded	<i>Lbs.</i> 97 82 71 540	<i>Lbs.</i> 94 85 76 590	Lbs. 87 80 75 610	Lbs.	Lbs.
4	A	30 no load 60 no load 90 no load 0 loaded	140 120 105 670	140 120 115 710	$125 \\ 115 \\ 110 \\ 720$		
	B and C	30 no load 60 no load 90 no load 0 loaded	$175 \\ 140 \\ 115 \\ 720$	$165 \\ 145 \\ 130 \\ 770$	$155 \\ 140 \\ 130 \\ 800$		
	A	30 no load 60 no load 90 no load 0 loaded	280 220 185 900	270 230 200 970	250 220 200 970	240 225 210 1,050	
	B and C	30 no load 60 no load 90 no load 0 loaded	350 260 210 980	350 280 240 1,050	310 270 240 1, 100	300 270 240 1, 100	290 260 24( 1, 150
	A	30 no load 60 no load 90 no load 0 loaded	430 320 260 1, 100	430 340 290 1, 200	380 330 290 1,200	370 330 300 1, 250	350 320 300 1, 250
	B and C	30 no load 60 no load 90 no load 0 loaded	$560 \\ 390 \\ 310 \\ 1, 250$	540 410 330 1, 300	490 400 340 1, 350	470 400 350 1, 400	$450 \\ 400 \\ 360 \\ 1,450$
	All	30 no load 60 no load 90 no load 0 loaded	$710 \\ 510 \\ 460 \\ 1,450$	690 530 430 1, 550	$670 \\ 530 \\ 450 \\ 1,600$	630 530 480 1,600	$630 \\ 540 \\ 480 \\ 1,700 $
0	All	30 no load 60 no load 90 no load 0 loaded	890 630 490 1,700	860 650 520 1, 800	850 680 570 1,850	840 700 600 1, 900	840 720 640 2,000
000	All	30 no load	1,3509607302,400	$1,350 \\ 1,000 \\ 810 \\ 2,500$	$1,400 \\ 1,100 \\ 900 \\ 2,600$	1,450 1,200 1,000 2,750	1,550 1,300 1,100 3,000

## APPENDIX A

# Table 40.—Tensions in Soft-Drawn Covered Copper Wire for Different Span Lengths Corresponding to the Recommended Sags of Table 37—Continued

Size	Grade of	Conditions of load		Tensi	ons for s	pan leng	th of—	
A. W. G. No.	construc- tion	and temperature	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.	250 ft.
6	с	° F. 30 no load 60 no load	Lbs. 120 95	Lbs. 120 99	Lbs. 105 96	Lbs.	Lbs.	Lbs.
		90 no load 15 loaded	80 390	88 420	88 440			
4	All	30 no load 60 no load 90 no load 15 loaded	$220 \\ 165 \\ 135 \\ 530$	$220 \\ 175 \\ 145 \\ 580$	195 170 150 590	$170 \\ 160 \\ 145 \\ 580$		
2	All	30 no load 60 no load 90 no load 15 loaded	450 330 250 800	450 340 280 850	390 330 280 860	390 330 290 900	370 330 300 880	
1	All	30 no load 60 no load 90 no load 15 loaded	560 400 310 920	540 410 330 970	540 430 360 1,050	530 440 380 1, 050	530 450 400 1, 100	560 500 450 1, 200
0	All	30 no load 60 no load 90 no load 15 loaded	710 510 390 1, 100	690 530 430 1, 150	720 560 470 1, 250	730 600 510 1, 300	740 620 540 1, 350	810 700 630 1, 500
00	All	30 no load 60 no load 90 no load 15 loaded	890 630 480 1, 300	860 650 520 1, 350	900 700 590 1, 400	950 770 650 1, 500	1,000 840 720 1,650	1, 150 980 860 1, 850
0000	A]1	30 no load 60 no load 90 no load 15 loaded	1, 350 960 730 1, 900	1, 350 1, 000 810 1, 900	$1,400 \\ 1,100 \\ 900 \\ 2,000$	1,450 1,200 1,000 2,100	1,550 1,300 1,100 2,150	$1,750 \\ 1,500 \\ 1,300 \\ 2,450$

#### MEDIUM LOADING DISTRICTS

# Table 40.—Tension in Soft-Drawn Covered Copper Wire for Different Span Lengths Corresponding to the Recommended Sags of Table 37.—Continued

Size	Grade of	Conditions of load		Tensio	ons for sp	oan lengt	h of—	
A. W. G. No.	construc- tion	and temperature	100 ft.	125 <b>f</b> t.	150 ft.	175 ft.	200 ft.	250 ft.
6	A	° F. 30 no load 60 no load 90 no load 30 loaded	Lbs. 120 95 80 250	Lbs. 115 99 88 260	$Lbs. \\ 105 \\ 97 \\ 89 \\ 270$	Lbs.	Lbs.	Lbs.
6	B and C.	30 no load 60 no load 90 no load 30 loaded	150 115 92 280	150 120 105 300	$135 \\ 115 \\ 105 \\ 300$			
4	All	30 no load 60 no load 90 no load 30 loaded	290 210 155 430	280 220 175 450	280 220 185 470	280 230 210 510	280 230 210 520	
2	All	30 no load 60 no load 90 no load 30 loaded	560 390 290 680	550 410 320 710	540 410 340 740	550 440 370 770	520 440 700 780	600 510 440 900
1	All	30 no load 60 no load 90 no load 30 loaded	690 480 350 790	680 490 390 830	700 530 430 890	740 580 480 950	790 630 730 1,050	850 710 610 1, 150
0	All	30 no load 60 no load 90 no load 30 loaded	860 600 440 980	850 630 490 1,000	890 690 550 1, 100	940 750 610 1, 150	990 810 670 1, 250	1, 100 910 780 1, 350
00	All	30 no load 60 no load 90 no load 30 loaded	$1,100\760\550\1,150$	1,050 780 610 1,200	1, 100 840 680 1, 300	1, 150 920 760 1, 350	$1,250 \\ 1,000 \\ 840 \\ 1,450$	$1,350 \\ 1,100 \\ 960 \\ 1,600$
0000	All	30 no load 60 no load 90 no load 30 loaded	1, 700 1, 150 840 1, 750	1, 650 1, 200 930 1, 800	1, 700 1, 300 870 1, 900	1, 800 1, 400 1, 150 2, 000	1, 900 1, 550 1, 250 2, 150	2,050 1,700 1,450 2,350

#### LIGHT LOADING DISTRICTS

HEAVY LOADING DISTRICTS	Ŭ	ustruction temperature 100 ft. 125 ft. 150 ft. 175 ft. 200 ft. 250 ft. 300 ft. 400 ft. 500 ft. 700 ft. 1,000 ft.	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$
			30 nc 60 nc 90 nc 0 loa	20 nc 60 nc 90 nc 0 loar	30 nc 60 nc 90 nc 0 loav	30 nc 60 nc 90 no 0 loav	30 nc 60 nc 90 nc 0 loav	30 nc 60 nc 90 nc 0 loav
		00	G		B	G		
	Size	A. W. G. No.	8	6.	9		4	2

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 Table 41.—Stresses in Hard and Medium-Drawn Bare Copper Wire for Different Span Lengths

 Corresponding to the Recommended Sags of Table 35

# APPENDIX A

$\begin{array}{c} 7,500\\ 7,150\\ 6,850\\ 29,000\end{array}$	$\begin{array}{c} 8,550\\ 8,050\\ 7,600\\ 27,000\end{array}$	$egin{array}{c} 9, 250 \\ 8, 650 \\ 8, 100 \\ 25, 400 \end{array}$	$\begin{array}{c} 12,150\\ 11,000\\ 10,150\\ 24,850\end{array}$	
$\begin{array}{c} 8,250\\7,750\\7,300\\28,900\end{array}$	$\begin{array}{c} 9,200\\ 8,500\\ 7,800\\ 27,500\end{array}$	$egin{array}{c} 10,100\ 9,100\ 8,400\ 25,400 \end{array}$	$12, 550\\11, 050\\9, 850\\24, 000$	
$\begin{array}{c} 10,250\\ 8,850\\ 7,850\\ 28,700\\ 28,700 \end{array}$	${ \begin{array}{c} 11,400\\ 9,500\\ 8,250\\ 26,800 \end{array} }$	${ \begin{array}{c} 12,500\\ 10,400\\ 8,950\\ 27,600 \end{array} }$	$\begin{array}{c} 15,100\\ 12,350\\ 10,350\\ 24,600\end{array}$	
$\begin{array}{c} 11,150\\ 9,100\\ 7,600\\ 27,500\end{array}$	$\begin{array}{c} 11,700\\ 9,500\\ 7,900\\ 26,000\end{array}$	${ \begin{array}{c} 12,400\\ 10,000\\ 8,150\\ 24,200\end{array}}$	$\begin{array}{c} 13,850\\ 11,250\\ 9,050\\ 22,700 \end{array}$	CTS
$12,400 \\ 9,600 \\ 7,600 \\ 26,000$	$\begin{array}{c} 12,400\\ 9,600\\ 7,600\\ 24,150\end{array}$	$^{12,\ 400}_{9,\ 600}_{7,\ 600}_{22,\ 500}$	$^{12,400}_{9,600}$	DISTRI
$\begin{array}{c} 11,200\\ 8,400\\ 6,450\\ 24,000\end{array}$	$\substack{11,\ 200\\ 8,\ 400\\ 6,\ 450\\ 22,\ 200\\ 22,\ 200\\ \end{array}$	$^{11,\ 200}_{8,\ 450}_{6,\ 450}_{20,\ 800}$	${ \begin{array}{c} 11,200\\ 8,400\\ 6,450\\ 18,600 \end{array} }$	MEDIUM LOADING DISTRI
$     \begin{array}{c}       9,850 \\       7,200 \\       5,600 \\       21,700     \end{array} $	$\substack{9,850\\5,600}\\20,200$	$\begin{array}{c} 9,850\\ 7,200\\ 5,600\\ 18,800\end{array}$	$\begin{array}{c} 9,850\ 7,200\ 5,600\ 16,900 \end{array}$	M LOA
$\begin{smallmatrix} 8,700\\6,000\\4,650\\19,250\end{smallmatrix}$	$\begin{array}{c} 8,700\\ 6,000\\ 4,650\\ 18,200\end{array}$	$\begin{array}{c} 8,700\\ 6,000\\ 4,650\\ 16,800\end{array}$	$\begin{array}{c} 8,700\\ 6,000\\ 4,650\\ 15,100\end{array}$	MEDIU
$\begin{smallmatrix} 8,800\\ 5,800\\ 4,100\\ 18,200\end{smallmatrix}$	$     \begin{array}{c}       8,800 \\       5,800 \\       4,100 \\       17,100     \end{array} $	$\begin{array}{c} 8,800\\ 5,800\\ 4,100\\ 16,100\end{array}$	$\begin{array}{c} 8,800\\ 5,800\\ 4,100\\ 15,000\end{array}$	-
30 no load 60 no load 90 no load 0 loaded	30 no load 60 no load 90 no load 0 loaded	30 no load 60 no load 90 no load	30 no load 60 no load 90 no load 0 loaded	
All	All	All	All	
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		6, 950 6, 600 6, 250 24, 700	11,900         10,400         9,190           10,500         9,650         8,800           8,900         9,000         8,600           25,000         25,750         25,500
		$ \begin{array}{c c} 10,450 \\ 8,600 \\ 7,250 \\ 7,250 \\ 25,000 \\ 25,000 \end{array} , 8,650 \\ 6,850 \\ 25,050 \\ 25,050 \end{array} $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
	0000	$egin{array}{c} 9, 250 \ 7, 250 \ 6, 050 \ 22, 050 \ \end{array}$	$ \begin{array}{c} 11,450\\ 8,900\\ 7,000\\ 20,200 \end{array} $
9, 850 7, 200 5, 650 30, 200	$ \begin{array}{c cccc} 9,850 \\ 7,200 \\ 7,200 \\ 5,650 \\ 6,000 \\ 24,400 \\ 26,000 \end{array} $	$ \begin{array}{c c} 9,850 \\ 7,200 \\ 5,650 \\ 5,650 \\ 20,150 \\ 21,300 \end{array} , \begin{array}{c} 9,600 \\ 7,400 \\ 6,000 \\ 21,300 \end{array} $	$ \begin{array}{c c} 9,850\\7,200\\5,650\\17,150\\18,600\\18,600\\18,600 \end{array} $
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c cccc} 900 & 10,850 \\ 250 & 7,500 \\ 900 & 5,450 \\ 800 & 19,300 \end{array}$	
10, 7, 25,	10, 20,	17,47	load 10,900 load 4,900 load 15,800
30 no load. 60 no load. 90 no load. 15 loaded.	30 no load. 60 no load. 90 no load. 15 loaded	30 no load 60 no load 90 no load 15 loaded	30 no load. 60 no load. 90 no load. 15 loaded
C	All 30 no lo 60 no lo 90 no lo 15 loadd	All 30 no lo 60 no lo 90 no lo 15 load	All 30 no 60 no 90 no 15 loa

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MEDIUM LOADING DISTRICTS-Continued

Size		Conditions of				SO	Stresses for span length of	or span le	ength of-				
A. W. G. No.	construc- tion	load and temperature	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.	250 ft.	300 ft.	400 ft.	500 ft.	700 ft.	1,000 ft.
	All	°F. 30 no load 60 no load 99 no load	$\begin{array}{c c} Lbs./in.^2 \\ 10,900 \\ 7,250 \\ 4,900 \\ 15,050 \end{array}$	$\begin{array}{c} Lbs./in.^{2}\\ 10,850\\ 7,500\\ 5,450\\ 15,900\\ 15,900 \end{array}$	$\begin{array}{c} Lbs./in.^{2}\\ 9,850\\ 7,200\\ 5,650\\ 16,200\end{array}$	$\begin{array}{c} Lbs, in.^2\\ 11, 250\\ 8, 350\\ 6, 450\\ 17, 900 \end{array}$	$\begin{array}{c} Lbs./in.^2\\ 12,700\\ 9,600\\ 7,500\\ 19,500\end{array}$	$Lbs, in.^2$ 14, 500 11, 550 9, 350 22, 700	$Lbs_{s}/in.^{2}$ 15,900 12,900 10,700 24,900	$\begin{array}{c} Lbs./in.^{2}\\ 14,950\\ 12,850\\ 11,200\\ 26,250\end{array}$	$\begin{array}{c} Lbs./in.^{2}\\ 12.950\\ 111,700\\ 10,700\\ 25,800 \end{array}$	$\begin{array}{c} Lbs./in.^2\\ 10,300\\ 9,850\\ 9,500\\ 24,750\end{array}$	Lbs./in. <sup>3</sup>
00	All	30 no load 60 no load 90 no load	$10,900 \\ 7,250 \\ 4,900 \\ 14,600 \\ 14,600 \\ 14,600 \\ 10,00 \\ $	10,850 7,500 5,450 15,250	$   \begin{array}{c}     9,850 \\     7,200 \\     5,650 \\     15,300 \\   \end{array} $	11,350 8,600 6,500 17,200	$12,900 \\ 10,000 \\ 7,850 \\ 18,900$	$\begin{array}{c} 15,550\\ 12,400\\ 10,000\\ 22,050 \end{array}$	$17,600\\14,200\\11,800\\24,650$	$\begin{array}{c} 17,150\\ 14,500\\ 12,500\\ 26,350\end{array}$	$\begin{array}{c} 15,250\\ 13,300\\ 12,000\\ 25,600 \end{array}$	$\begin{array}{c} 12,550\\ 11,800\\ 111,150\\ 25,300 \end{array}$	
00	All	30 no load 60 no load 90 no load	$\begin{array}{c} 10,900\\ 7,250\\ 4,900\\ 14,100\end{array}$	$10,850 \\ 7,500 \\ 5,450 \\ 14,600 \\ 14,600 \\ 12,10 \\ 10,10 \\ 1$	$   \begin{array}{c}     9,850 \\     7,200 \\     5,650 \\     14,600 \\   \end{array} $	$11,750\\8,800\\6,900\\16,550$	$13,550 \\ 10,450 \\ 8,150 \\ 18,750 \\ 18$	$\begin{array}{c} 16,  900 \\ 13,  300 \\ 10,  800 \\ 22,  400 \end{array}$	$19,200 \\ 15,650 \\ 12,750 \\ 25,250$	$\begin{array}{c} 19,750\\ 16,750\\ 14,300\\ 27,300 \end{array}$	$17,850 \\ 15,700 \\ 13,900 \\ 27,250 \\ 2$	$\substack{16,000\\14,800\\13,850\\27,300\end{array}$	$\begin{array}{c} 14,750\\ 14,100\\ 13,650\\ 27,400 \end{array}$
0000	All.	30 no load 60 no load 90 no load 15 loaded	$\begin{array}{c} \mathbf{10,\ 900} \\ \mathbf{7,\ 250} \\ \mathbf{4,\ 900} \\ \mathbf{13,\ 550} \\ \mathbf{13,\ 550} \end{array}$	$10,850 \\ 7,500 \\ 5,450 \\ 14,000 \\ 14,000 \\ 10,$	$\begin{array}{c} 9,850\\ 7,200\\ 5,650\\ 13,500\end{array}$	$12,250 \\ 9,250 \\ 7,150 \\ 16,300 \\ 16,300 \\ 10,$	${ \begin{array}{c} 14,300\\ 10,950\\ 8,500\\ 18,000 \end{array} }$	$\begin{array}{c} 18,850\\ 15,000\\ 12,000\\ 22,850 \end{array}$	$\begin{array}{c} 22,800\\ 19,150\\ 15,650\\ 27,150\end{array}$	$\begin{array}{c} 22,750\\ 19,200\\ 16,200\\ 28,000 \end{array}$	$\begin{array}{c} 21,850\\ 18,900\\ 16,400\\ 28,200\end{array}$	$\begin{array}{c} 20,250\\ 18,300\\ 16,650\\ 28,200 \end{array}$	$\begin{array}{c} 19,050\\ 18,000\\ 17,050\\ 28,450\\ \end{array}$

202

# APPENDIX A

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				$\begin{array}{c} 16,000\\ 15,250\\ 14,700\\ 22,500\end{array}$	$\begin{array}{c} 18,300\\ 17,250\\ 16,500\\ 24,850 \end{array}$	20, 900 19, 900 18, 700 26, 250	25,600 23,500 21,850 28,550
			$14,650 \\ 13,650 \\ 12,700 \\ 21,100 \\$	${}^{17,800}_{15,800}\\{}^{14,700}_{22,800}$	$\begin{array}{c} 19,4 \\ 17,750 \\ 16,150 \\ 24,000 \end{array}$	$\begin{array}{c} 22,500\\ 20,200\\ 18,300\\ 26,000\end{array}$	$\begin{array}{c} 25,000\\ 22,400\\ 20,000\\ 27,300\end{array}$
		${}^{11, 500}_{9, 750}_{9, 750}_{18, 700}$	$16,700 \\ 14,750 \\ 13,100 \\ 21,900$	$\begin{array}{c} 19,500\\ 16,950\\ 14,900\\ 23,400 \end{array}$	$\begin{array}{c} 21,150\\ 18,250\\ 16,050\\ 24,300\end{array}$	$\begin{array}{c} 23,100\\ 19,900\\ 17,350\\ 25,450\end{array}$	$\begin{array}{c} 25,250\\ 21,700\\ 18,850\\ 26,500\end{array}$
		$\substack{13,400\\11,550\\10,300\\19,400\end{array}$	$\begin{array}{c} 18,400\\ 15,650\\ 13,450\\ 22,400 \end{array}$	$\begin{array}{c} 21,000\\ 17,650\\ 15,050\\ 23,950\end{array}$	$21,850\\18,900\\15,900\\24,600$	$\begin{array}{c} 23,700\\ 20,050\\ 17,000\\ 25,250\end{array}$	$\begin{array}{c} 25,150\\ 21,400\\ 18,150\\ 26,350\end{array}$
		15,850 12,950 10,700 20,250	$\begin{array}{c} 21,100\\ 17,250\\ 14,000\\ 23,500 \end{array}$	$\begin{array}{c} 22,350\\18,500\\15,000\\23,850\end{array}$	$\begin{array}{c} 22,800\\ 19,150\\ 15,650\\ 24,500 \end{array}$	$\begin{array}{c} 23,850\\ 20,000\\ 16,350\\ 25,000\end{array}$	$\begin{array}{c} 25,700\\ 21,550\\ 17,850\\ 25,800\end{array}$
		${}^{18,000}_{11,400}_{111,400}_{21,200}$	$\begin{array}{c} 21,900\\ 18,000\\ 14,300\\ 23,450\end{array}$	$\begin{array}{c} 21,900\\ 18,000\\ 14,300\\ 23,200\end{array}$	$\begin{array}{c} 21,900\\ 18,000\\ 14,300\\ 22,900 \end{array}$	$\begin{array}{c} 21,900\\ 18,000\\ 14,300\\ 22,700\end{array}$	$\begin{array}{c} 21,900\\ 18,000\\ 14,300\\ 22,400\end{array}$
	$^{12,450}_{9,600}$ $^{7,600}_{17,000}$	$^{13,600}_{\begin{array}{c}10,500\\8,200\\16,500\end{array}}$	$16,600 \\ 12,750 \\ 9,850 \\ 18,050$	${}^{16,600}_{12,750}_{9,850}_{18,000}$	${}^{16,600}_{\begin{array}{c} 12,750\\ 9,850\\ 17,650\end{array}}$	${ 16,600 \atop { 0,000  0,000 \atop { 0,$	${ \begin{smallmatrix} 16,  600 \\ 12,  750 \\ 9,  850 \\ 17,  150 \\ \end{split} }$
$11,750 \\ 8,800 \\ 6,900 \\ 17,250$	$13,000 \\ 9,800 \\ 7,450 \\ 16,750$	$^{13,000}_{9,800}$	$13,000 \\ 9,800 \\ 7,450 \\ 14,700 \\ 14,700 \\ 12,700 \\ 12,700 \\ 13,700 \\ 13,700 \\ 14,$	$13,000 \\ 9,800 \\ 7,450 \\ 14,350 \\ 14,350 \\ 14,350 \\ 12,350 \\ 14,$	$13,000 \\ 9,800 \\ 7,450 \\ 14,350$	$13,000\\9,800\\7,450\\14,100$	$13,000 \\ 9,800 \\ 7,450 \\ 13,700$
$13,550\\9,950\\7,250\\17,950$	$^{13, 550}_{9, 950}$	$^{13,550}_{9,950}$	$^{13, 550}_{9, 950}$	$\begin{array}{c} 13,550\\ 9,950\\ 7,250\\ 14,900\end{array}$	$13,550\\9,950\\7,250\\14,550$	$13,550 \\ 9,950 \\ 7,250 \\ 14,400 \\ 14,400 \\ 12,20 \\ 14,400 \\ 14,1$	$\begin{array}{c} 13,550\\ 9,950\\ 7,250\\ 14,100\end{array}$
${}^{14,000}_{10,000}_{7,000}_{17,150}$	14,000 10,000 7,000 16,350	$14,000 \\ 10,000 \\ 7,000 \\ 15,350$	$^{14,000}_{10,000}$	14,000 10,000 7,000 14,800	14,000 10,000 7,000 14,650	${}^{14,000}_{7,000}$	14,000 10,000 7,000 14,300
$\substack{13,700\\9,700\\6,300\\16,200\end{array}$	$ \begin{array}{c} 13,700\\ 9,700\\ 6,300\\ 15,250\end{array} $	$13,700 \\ 9,700 \\ 6,300 \\ 15,000 \\ 15,000 \\ 15,000 \\ 12,$	$^{13,700}_{9,700}_{6,300}$	$\begin{array}{c} 13,700\\ 9,700\\ 6,300\\ 14,400\end{array}$	$\substack{13,700\\9,700\\6,300\\14,200}$	$13,700 \\ 9,700 \\ 6,300 \\ 14,200$	$13, 700\\9, 700\\6, 300\\14, 000$
30 no load 60 no load 90 no load 30 loaded	30 no load 60 no load 90 no load 30 loaded	30 no load 60 no load 90 no load 30 loaded	30 no load 60 no load 90 no load	30 no load 60 no load 90 no load 30 loaded	30 no load 60 no load 90 no load 30 loaded	30 no load 60 no load 90 no load 30 loaded	30 no load 60 no load 90 no load 30 loaded
C	All	All	<u>All</u>	All	All	All.	All.
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STRESSES FOR HARD COPPER

203

#### APPENDIX A

#### Table 42.—Stresses in Hard and Medium-Drawn Covered Copper Wire for Different Span Lengths Corresponding to Recommended Sags of Table 36

Size	Grade of con-	Conditions		S	tresses f	or span l	ength of-	-	
A. W. G. No.	struc- tion	of load and temperature	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.	250 ft.	300 ft.
8	C	°F. 30 no load 60 no load 90 no load 0 loaded	5,900 4,800 4,150	Lbs./in. <sup>2</sup> 5, 900 5, 050 4, 500 40, 000	$\begin{array}{c} Lbs./in.^2\\ 5,550\\ 4,900\\ 4,550\\ 42,800\end{array}$			Lbs./in.2	
6	A	30 no load 60 no load 90 no load 0 loaded	4, 550 3, 900	5,600 4,750 4,200 30,800	5,150 4,600 4,250 32,500				
6	В	30 no load 60 no load 90 no load 0 loaded	4, 550	$\begin{array}{c} 7,400\\ 5,950\\ 5,000\\ 33,100 \end{array}$	$\begin{array}{c} 6,500\ 5,600\ 5,000\ 34,800 \end{array}$				
6	C	30 no load 60 no load 90 no load 0 loaded	6,800	9,150 7,100 5,750 34,600		8, 050 6, 950 6, 250 39, 800			
4	All	30 no load 60 no load 90 no load 0 loaded	$\begin{array}{c} 8,300 \\ 6,250 \\ 4,800 \\ 24,900 \end{array}$	$\begin{array}{c} 8,500 \\ 6,550 \\ 5,250 \\ 27,400 \end{array}$	7, 800 6, 250 5, 400 28, 900	$\begin{array}{c} 7,450\\ 6,400\\ 5,700\\ 30,700\end{array}$	7,000 6,250 5,650 31,700		
2	All	30 no load 60 no load 90 no load 0 loaded	4,800	8, 500 6, 550 5, 250 22, 300	7,800 6,250 5,400 23,000	9, 550 7, 650 6, 500 26, 250	10, 200 8, 350 7, 200 28, 300	$\begin{array}{r} 8,750 \\ 7,800 \\ 7,150 \\ 29,300 \end{array}$	7,650 7,050 6,150 29.000
1	All	30 no load 60 no load 90 no load 0 loaded	6,050 4,650	8,200 6,300 5,000 20,000	7, 700 6, 250 5, 250 20, 800	9, 650 7, 650 6, 500 23, 700	$\begin{array}{c} 10 & 800 \\ 8, 700 \\ 7, 400 \\ 26, 050 \end{array}$	10, 050 8, 700 7, 700 26, 000	9,000 8,150 7,500 28,000
0	All	30 no load 60 no load 90 no load 0 loaded			$\begin{array}{c} 8,050\ 6,450\ 5,400\ 19,000 \end{array}$	9, 950 8, 000 6, 600 22, 100	$\begin{array}{c} 11,200\\ 9,100\\ 7,650\\ 24,300 \end{array}$	$\begin{array}{c} 11,000\\ 9,400\\ 8,200\\ 24,500\end{array}$	10, 350 9, 250 8, 200 26, 500
60	All	30 no load 60 no load 90 no load 0 loaded	6, 000 4, 550	$\begin{array}{c} 8,200 \\ 6,250 \\ 5,000 \\ 17,100 \end{array}$	$\begin{array}{c} 8,000\\ 6,450\\ 5,450\\ 17,700 \end{array}$	9, 800 7, 900 6, 500 20, 250	$\begin{array}{c} 11,300\\ 9,250\\ 7,700\\ 22,550 \end{array}$	$11,550 \\ 9,750 \\ 8,500 \\ 24,200$	11, 150 9, 850 8, 750 25, 100
0000	All	30 no load 60 no load 90 no load 0 loaded	5, 800 4, 400	8,000 6,050 4,850 15,000	8, 500 6, 600 5, 500 15, 800	9, 850 7, 900 6, 500 17, 900	11, 200 9, 250 7, 700 19, 950	$\begin{array}{c} 13,650\\ 11,350\\ 9,550\\ 23,200 \end{array}$	14,600 12,450 10,550 25,250

#### HEAVY LOADING DISTRICTS

# Table 42.—Stresses in Hard and Medium-Drawn Covered Copper Wire for Different Span Lengths Corresponding to Recommended Sags of Table 36—Continued

A. W. G. No.	Grade of con-	Conditions		S	tresses f	or span l	ength of-	-	
	struc- tion	of load and temperature	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.	250 ft.	300 ft.
8	с	°F. 30 no load 60 no load 90 no load 15 loaded	7,600 5,800 4,700	Lbs./in. <sup>2</sup> 7,600 6,200 5,250 31,000	$\begin{array}{c} Lbs./in.^2\\ 6,850\\ 5,900\\ 5,300\\ 30,050\end{array}$			Lbs./in.2	
6	A	30 no load 60 no load 90 no load 15 loaded	7, 200 5, 500 4, 500 20, 400	7,200 5,850 4,950 22,400	$\begin{array}{c} 6,500\ 5,600\ 5,000\ 23,200 \end{array}$				
6	В	30 no load 60 no load 90 no load 15 loaded	9, 500 6, 850 5, 250 21, 850	9,200 7,150 5,850 24,000	8, 300 6, 850 5, 800 25, 350	8, 250 6, 950 6, 200 26, 800			
6	с	30 no load 60 no load 90 no load 15 loaded	11, 350 8, 250 6, 050 23, 200	$11,350 \\ 8,500 \\ 6,650 \\ 25,500$	10, 500 8, 300 6, 900 27, 250	10, 150 8, 400 7, 150 28, 800			
4	All	30 no load 60 no load 90 no load 15 loaded	10, 700 7, 500 5, 500 19, 000	10, 400 7, 800 6, 150 20, 900	*9,700 7,700 6,350 21,900	8,800 7,600 6,500 22,850	$9,150 \\7,700 \\6,750 \\24,050$		
2	All	30 no load 60 no load 90 no load 15 loaded	$10,700 \\7,500 \\5,500 \\16,700$	10, 400 7, 800 6, 150 17, 750	9,700 7,650 6,350 18,200	10, 100 8, 500 6, 800 19, 750	$11,500 \\ 9,400 \\ 7,900 \\ 21,650$	10, 750 9, 350 8, 250 22, 800	9, 900 8, 950 8, 200 22, 750
1	All	30 no load 60 no load 90 no load 15 loaded	$10, 150 \\7, 200 \\5, 250 \\15, 500$	$10,250 \\ 7,500 \\ 5,900 \\ 16,500$	9,400 7,400 6,000 16,700	$11,350 \\ 8,850 \\ 7,300 \\ 18,800$	12,400 9,950 8,200 20,800	$13,650 \\ 11,500 \\ 9,750 \\ 23,600$	$12,600 \\ 10,850 \\ 9,600 \\ 23,600$
0	All	30 no load 60 no load 90 no load 15 loaded	7,300 5,300	$10,250 \\ 7,600 \\ 5,850 \\ 15,600$	9, 500 7, 500 6, 100 15, 600	11, 400 8, 500 7, 300 18, 300	13,400 10,800 8,850 20,200	15, 250 12, 700 10, 600 23, 250	14, 300 12, 250 10, 750 23, 300
00	A11	30 no load 60 no load 90 no load 15 loaded	5, 250	$10,250 \\ 7,500 \\ 5,900 \\ 14,750$	9,400 7,400 6,000 14,500	11,550 9,150 7,500 16,900	13,800 11,050 9,100 19,350	$16,500 \\ 13,500 \\ 11,300 \\ 22,750$	$15,900 \\ 13,450 \\ 11,650 \\ 23,200$
0000	A11	30 no load 60 no load 90 no load 15 loaded	6,950 5,050	9,900 7,150 5,550 13,450	9,150 7,150 5,800 13,100	$11,700 \\ 9,250 \\ 7,450 \\ 15,800$	$14,550 \\ 11,450 \\ 9,250 \\ 18,900$	18,300 14,850 12,100 22,700	18,800 15,500 13,250 23,900

#### MEDIUM LOADING DISTRICTS

# APPENDIX A

#### Table 42.—Stresses in Hard and Medium-Drawn Covered Copper Wire for Different Span Lengths Corresponding to Recommended Sags of Table 36—Continued

Size	Grade of con-	Conditions		S	tresses fo	or span le	ength of-	-	
A. W. G. No.	struc- tion	of load and temperature	100 ft.	125 ft.	150 ft.	175 ft.	200 ft.	250 ft.	300 ft.
8	C	°F 30 no load 60 no load 90 no load 30 loaded	Lbs./in. <sup>2</sup> 9,950 7,200 5,650 17,400	Lbs./in. <sup>2</sup> 9, 500 7, 500 6, 150 19, 000	Lbs./in. <sup>2</sup> 8,750 7,200 6,150 19,750	Lbs./in. <sup>2</sup> 8,750 7,400 6,500 20,750		Lbs./in. <sup>2</sup>	
6	A	30 no load 60 no load 90 no load 30 loaded	9, 500 6, 800 5, 250 15, 100	9, 200 7, 200 5, 800 16, 150	8, 300 6, 850 5, 800 16, 350	8, 250 7, 000 6, 200 17, 450			
6	В	30 no load 60 no load 90 no load 30 loaded	$11,950 \\ 8,200 \\ 6,350 \\ 16,450$	$11,250 \\ 8,500 \\ 6,700 \\ 17,600$	$10,550 \\ 8,400 \\ 6,900 \\ 18,650$	10, 200 8, 350 7, 100 19, 350	10, 150 8, 600 7, 500 20, 300		
6	C	30 no load 60 no load 90 no load 30 loaded	14, 200 10, 300 7, 450 18, 350	$\begin{array}{c} 14,200\\ 10,650\\ 8,100\\ 19,950 \end{array}$	$13,200\\10,200\\8,200\\20,500$	$13,050 \\ 10,450 \\ 8,650 \\ 21,500$	12, 450 10, 250 8, 700 22, 050		
4	A11	30 no load 60 no load 90 no load 30 loaded	$\begin{array}{c} 13,200\\9,400\\6,600\\16,300\end{array}$	13, 050 9, 750 7, 300 17, 250	12, 000 9, 350 6, 850 17, 500	11, 850 9, 500 7, 750 18, 450	11, 500 9, 450 8, 000 18, 900		
2	All	30 no load 60 no load 90 no load 30 loaded		13, 050 9, 750 7, 300 15, 600	$12,000 \\ 9,350 \\ 6,850 \\ 15,500$	13, 200 10, 300 8, 300 17, 150	$14,250\\11,450\\9,350\\18,500$	$16,700 \\13,800 \\11,550 \\21,700$	$15,100 \\ 12,950 \\ 11,250 \\ 21,200$
1	All	30 no load 60 no load 90 no load 30 loaded	$12,800 \\ 9,100 \\ 6,300 \\ 14,000$	$12,800 \\ 9,450 \\ 7,000 \\ 14,600$	$12,000 \\ 9,050 \\ 7,150 \\ 14,400$	$\begin{array}{c} 13,600\\ 10,600\\ 8,500\\ 16,400 \end{array}$	15, 300 12, 000 9, 750 18, 000	17, 550 14, 550 12, 100 21, 300	$17,100 \\ 14,450 \\ 12,250 \\ 21,650$
0	All	30 no load 60 no load 90 no load 30 loaded	$12,950 \\ 9,200 \\ 6,450 \\ 14,050$	$12,800 \\ 9,500 \\ 7,100 \\ 14,400$	$\begin{array}{c} 11,900\\ 9,050\\ 7,150\\ 14,100 \end{array}$	$13,550 \\10,700 \\8,500 \\16,000$	16,000 12,750 10,300 18,450	$18,750 \\ 15,250 \\ 12,700 \\ 21,250$	$19,550 \\ 16,400 \\ 14,000 \\ 22,600$
00	All	30 no load 60 no load 90 no load 30 loaded	12, 800 9, 100 6, 300 13, 350	$12,800 \\ 9,450 \\ 7,000 \\ 13,850$	11, 750 9, 000 7, 050 13, 350	13, 900 10, 950 8, 650 15, 650	16, 350 13, 000 10, 400 18, 050	19, 500 15, 900 12, 950 21, 550	20,700 17,300 14,750 22,900
0000	A11	30 no load 60 no load 90 no load 30 loaded	8,650 6,250	12, 500 9, 050 6, 700 13, 350	11, 550 8, 700 6, 850 12, 350	14, 500 11, 100 8, 700 15, 150	16, 650 13, 000 10, 400 17, 600	21, 050 17, 250 14, 100 22, 250	23,000 19,300 16,150 24,300

#### LIGHT LOADING DISTRICTS

# Table 43.—Stresses in Soft-Drawn Covered Copper Wire for Different Span Lengths Corresponding to the Recommended Sags of Table 37

A. W. G.	Grade of	Conditions of load and tem-		Stresses	for span lei	ngth of—	
No.	construc- tion	perature	100 feet.	125 feet.	150 feet.	175 feet.	200 feet.
	G	° F.	Lbs./in.2	Lbs./in.2	Lbs./in.2	Lbs./in.2	
6	C	30 no load	4,700 3,950	4,550 4,100	4,250 3,900		
		60 no load 90 no load	3, 950	4,100	3,650		
		0 loaded	26, 250	28,550	29, 500		
4	Α	30 no load	4,350	4,250	3,850		
		60 no load	3,600	3,750	3,550		
		90 no load	3,150	3,450	3,300		
-		0 loaded	20, 400	21,600	22,000		
4	B and C	30 no load	5,300	5,100	4,750		
		60 no load	4,200	4,400	4,300		
		90 no load	3,550	3,900	3,900		
		0 loaded	21,850	23, 500	24,300		
2	A	30 no load	5,300	5,100	4,750	4,700	
		60 no load	4,200	4,400	4,300	4,300	
		90 no load	3,550	3,850	3,900	4,000	
		0 loaded	17, 300	18,500	18,650	19,800	
2	B and C	30 no load	6,650	6,700	6,000	5,700	5,500
		60 no load	5,050	5,350	5,150	5,150	5,000
		90 no load	4,050	4,500	4,550	4,700	4,700
		0 loaded	18,750	20,300	20, 800	21,500	21,750
1	A	30 no load	6,500	6,500	5,800	5,550	5,300
		60 no load	4,800	5,150	4, 950	4,950	4,850
		90 no load	3,900	4,400	4,400	4,500	4,500
		0 loaded	17,050	18,400	18,550	18,850	18,950
1	B and C	30 no load	8, 550	8,200	7,500	7,050	6,850
		60 no load	6,000	6,250	6,050	6,000	6,000
		90 no load	4,650	5,000	5,200 20,500	5,300	5,500 21,800
		o loaded	18,800	20,100	20,000	21,300	21,800
0	All	30 no load	8,600	8,350	8,050	7,650	7,500
		60 no load	6,150	6,350	6,450	6,400	6,500
		90 no load	4,700	5,150	5,400	5,750	5,800
		0 loaded	17,650	18, 500	19,000	19,600	20, 250
00	All	30 no load	8, 500	8,200	8,100	8,000	8,000
		60 no load	6,000	6,250	6,500	6,650	6,850
		90 no load	4,650	5,000	5,450	5,750	6,100
		0 loaded	16,400	17,000	17,750	18,300	19,000
0000	All	30 no load	8,150	8,100	8,350	8,700	9,250
		60 no load	5,750	6,100	6, 550	7,150	7,650
		90 no load	4,400	4,850	5,450	6,000	6, 550
		0 loaded	14, 450	15,000	15,700	16,600	18,000

#### HEAVY LOADING DISTRICTS

#### APPENDIX A

# Table 43.—Stresses in Soft-Drawn Covered Copper Wire for Different Span Lengths Corresponding to the Recommended Sags of Table 37—Continued

Size	Grade of	Conditions of		Stre	sses for sp	an length	of—	
A. W. G. No.	construc- tion	load and temperature	100 feet	125 feet	150 feet	175 feet	200 feet	250 feet
6	c	°F 30 no load 60 no load 90 no load 15 loaded	3,900	$\begin{array}{c} Lbs./in.^2\\ 5,850\\ 4,800\\ 4,250\\ 20,400\end{array}$	$\begin{array}{c} Lbs./in.^2\\ 5,150\\ 4,650\\ 4,250\\ 21,200\end{array}$		Lbs./in. <sup>2</sup>	
4	All	30 no load 60 no load 90 no load 15 loaded	$\begin{array}{c} 6,650\ 5,050\ 4,100\ 16,300 \end{array}$	$\begin{array}{c} 6,700\ 5,350\ 4,550\ 17,850 \end{array}$	$\begin{array}{c} 6,000\\ 5,150\\ 4,600\\ 18,000 \end{array}$	5,250 4,800 4,350 17,800		
2	All	30 no load 60 no load 90 no load 15 loaded		$\begin{array}{c} 8,550 \\ 6,500 \\ 5,300 \\ 16,300 \end{array}$	7,500 6,250 5,300 16,550	7,500 6,400 5,650 17,150	$\begin{array}{c} 7,000\\ 6,250\\ 5,700\\ 16,900 \end{array}$	
1	A11	30 no load 60 no load 90 no load 15 loaded	6,000 4,650	$\begin{array}{c} 8,200 \\ 6,250 \\ 5,000 \\ 14,800 \end{array}$	8,200 6,600 5,550 16,200	$8,000 \\ 6,750 \\ 5,750 \\ 16,200$	$\begin{array}{c} 8,000\\ 6,850\\ 6,100\\ 16,750 \end{array}$	$8,500 \\ 7,550 \\ 6,850 \\ 18,250$
0	All	30 no load 60 no load 90 no load 15 loaded	6,150	$egin{array}{c} 8,350 \ 6,350 \ 5,150 \ 13,800 \end{array}$	$8,650 \\ 6,800 \\ 5,700 \\ 14,850$		$8,900 \\ 7,500 \\ 6,500 \\ 16,000$	9,750 8,500 7,550 17,800
©0	All	30 no load 60 no load 90 no load 15 loaded	4,600	$8,200 \\ 6,250 \\ 5,000 \\ 13,000$	$8,550 \\ 6,750 \\ 5,650 \\ 13,600$	9,050 7,350 6,250 14,450	9,750 8,000 6,850 15,700	$10,900 \\ 9,400 \\ 8,200 \\ 17,800$
<b>9</b> 000	All	30 no load 60 no load 90 no load 15 loaded	5,800 4,400	8,1006,1004,85011,550	8, 300 6, 550 5, 450 12, 150	8,700 7,100 6,000 12,700	9, 300 7, 700 6, 550 13, 000	$10,550 \\ 9,050 \\ 7,900 \\ 14,900$

#### MEDIUM LOADING DISTRICTS

# Table 43.--Stresses in Soft-Drawn Covered Copper Wire for Different Span Lengths Corresponding to the Recommended Sags of Table 37--Continued

#### LIGHT LOADING DISTRICTS

Size	Grade of	Conditions of		Stre	sses for sp	an length	of—	
A.W.G. No.	construc- tion	load and tem- perature	100 fe <b>et</b>	125 feet	150 feet	175 feet	200 feet	250 feet
6	A	°F. 30 no load 60 no load 90 no load 30 loaded	3,850		$\begin{array}{c} Lbs./in.^2\\ 5,150\\ 4,700\\ 4,300\\ 13,000\end{array}$		Lbs./in. <sup>2</sup>	·
6	B and C.	30 no load 60 no load 90 no load 30 loaded	7,250 5,500 4,450 13,600	7,300 5,900 5,000 14,600	6,450 5,650 5,000 14,600			
4	All	30 no load 60 no load 90 no load 30 loaded	$\begin{array}{r} 8,750\\ 6,250\\ 4,700\\ 13,100\end{array}$	8, 500 6, 600 5, 300 13, 700	8, 400 6, 800 5, 700 14, 400	8, 650 7, 150 6, 250 15, 500	8, 400 7, 150 6, 350 15, 800	
2	All	30 no load 60 no load 90 no load 30 loaded	$10,700 \\ 7,500 \\ 5,500 \\ 12,950$	$\begin{array}{c} 10,500\\ 7,800\\ 6,050\\ 13,500 \end{array}$	10, 350 7, 950 6, 500 14, 150	10, 500 8, 500 7, 000 14, 750	9, 950 8, 350 7, 150 15, 000	11,4009,7508,50017,200
1	All	30 no load 60 no load 90 no load 30 loaded	$10, 450 \\ 7, 250 \\ 5, 250 \\ 12, 050$	$10,300 \\ 7,500 \\ 5,900 \\ 12,600$	$10,700 \\ 8,100 \\ 6,500 \\ 13,600$	11, 300 8, 850 7, 300 14, 450	$\begin{array}{c} 12,000\\ 9,600\\ 8,000\\ 15,700\end{array}$	$12,900 \\10,750 \\9,250 \\17,400$
0	All	30 ne load 60 no load 90 no load 30 loaded	5, 250	$10,250 \\ 7,600 \\ 5,900 \\ 12,200$	$10,700 \\ 8,300 \\ 6,600 \\ 13,000$	11, 350 9, 000 7, 350 13, 850	$\begin{array}{c} 12,000\\ 9,750\\ 8,100\\ 15,000 \end{array}$	$13,100 \\ 10,900 \\ 9,400 \\ 16,490$
00	All	30 no load 60 no load 90 no load 30 loaded	7,250	10,200 7,500 5,850 11,500	$10,650 \\ 8,050 \\ 6,500 \\ 12,300$	$11,200 \\ 8,800 \\ 7,250 \\ 13,000$	$11,900 \\ 9,600 \\ 8,000 \\ 14,000$	$\begin{array}{c} 12,750\\ 10,650\\ 9,200\\ 15,450\end{array}$
0000	All	30 no load 60 no load 90 no load 30 loaded	6, 950	9, 850 7, 200 5, 600 10, 900	10, 150 7, 800 6, 250 11, 350	10, 750 8, 450 6, 950 12, 100	$11,450 \\ 9,200 \\ 5,650 \\ 13,000$	$\begin{array}{c} 12,350 \\ 10,250 \\ 8,850 \\ 14,150 \end{array}$

# Appendix B.—MINIMUM PERMISSIBLE SAGS FOR LINE CONDUCTORS OF GRADES A, B, AND C, AND CORRESPONDING TENSIONS

Sags of line conductors of different materials at 30, 60, and 90° F. have been computed, such that when loaded according to the loading specification for the district, the resulting tension in the conductor will equal 50 per cent of its ultimate strength for grades A and B, and 60 per cent for grade C (see rule 261, F, 4).

Tables 44 to 46 present values of the sag in the conductor for various spans for hard-drawn and medium copper; Table 47 (pp. 220 to 222) for soft copper; Tables 48 to 53 (pp. 223 to 235) for three grades of steel; Tables 54 and 55 (pp. 236 to 238) for copper-covered steel designated as standard grade; Table 56 (pp. 239 to 241) for aluminum; and Table 57 (pp. 242 to 244) for aluminum cable with steel core. Tables 58 to 71 (pp. 245 to 278) give the corresponding stringing tensions in the various conductors.

The properties of the various conductors involved in the computation of sags and tensions are given in Appendix D. These sags and tensions are not applicable to conductor materials having properties which differ considerably from the values on which the tables are based. When such materials are used, the sags and tensions should be based upon the actual properties of the material concerned.

## Table 44.--Sags for Medium and Hard-Drawn Bare Solid Copper Wire

HEAVY LOADING DISTRICT

[The sags being such that when loaded at 0° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B, and 60 per cent for grade C]

Size	Grade of	Tem-		Sa	gs (inc	hes) fo	r span	length	s (feet)	of	
A. W. G. No.	construction	per- ature	100	125	150	175	200	250	300	400	500
8	с	$egin{array}{c} {}^{\circ}F. \\ {30} \\ {60} \\ {90} \end{array}$	4.4 6.5 9.7	$15.6 \\ 20.4 \\ 24.6$	36. 5 40. 7 44. 5						
6	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{r} 4.4 \\ 6.5 \\ 9.7 \\ 2.6 \\ 3.1 \\ 4.1 \end{array}$	$12.3 \\ 16.9 \\ 21.6 \\ 5.1 \\ 6.8 \\ 9.4$	$\begin{array}{c} 27.\ 7\\ 32.\ 8\\ 37.\ 1\\ 10.\ 6\\ 14.\ 8\\ 19.\ 8\end{array}$						
4	{A and B C	$     \begin{cases}             30 \\             60 \\             90 \\             30 \\             60 \\             90             90          $	$\begin{array}{c} 3.\ 0\\ 3.\ 8\\ 5.\ 3\\ 2.\ 2\\ 2.\ 6\\ 3.\ 1\end{array}$	5.5 7.7 10.8 3.6 4.5 5.7	$10.6 \\ 14.6 \\ 19.6 \\ 6.1 \\ 7.2 \\ 9.5$	$19.3 \\ 25.2 \\ 31.5 \\ 9.4 \\ 11.9 \\ 16.2$	$\begin{array}{c} 33.\ 1\\ 39.\ 1\\ 45.\ 1\\ 15.\ 1\\ 19.\ 4\\ 25.\ 2\end{array}$	$\begin{array}{c} 66.\ 6\\ 72.\ 3\\ 78.\ 4\\ 37.\ 2\\ 44.\ 7\\ 52.\ 2\end{array}$	109 115 121 71. 0 79. 0 86. 0		
2	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$2.9 \\ 3.5 \\ 4.8 \\ 2.1 \\ 2.6 \\ 3.1$	$\begin{array}{c} 4.8 \\ 6.2 \\ 8.3 \\ 3.4 \\ 4.2 \\ 5.3 \end{array}$	7.6 9.7 13.3 5.4 6.5 7.9	$11.8 \\ 15.5 \\ 20.6 \\ 7.6 \\ 9.5 \\ 11.8$	$\begin{array}{c} 17.8\\ 23.0\\ 29.5\\ 11.0\\ 13.4\\ 17.3 \end{array}$	$\begin{array}{c} 38.4 \\ 45.6 \\ 53.1 \\ 21.0 \\ 26.4 \\ 33.3 \end{array}$	$\begin{array}{c} 67.\ 0\\ 74.\ 5\\ 82.\ 4\\ 38.\ 9\\ 46.\ 8\\ 55.\ 4\end{array}$	$142 \\ 150 \\ 158 \\ 97 \\ 106 \\ 117$	$238 \\ 252 \\ 260 \\ 172 \\ 191 \\ 202$
1	{A and B C	$\begin{cases} 30\\ 60\\ 90\\ 30\\ 60\\ 90 \end{cases}$	$\begin{array}{c} 2.9\\ 3.5\\ 4.8\\ 2.2\\ 2.6\\ 3.2 \end{array}$	4.6 6.0 7.9 3.3 3.9 5.2	$7.0 \\ 9.0 \\ 12.4 \\ 5.0 \\ 6.5 \\ 7.9$	$10.5 \\ 13.6 \\ 18.1 \\ 7.6 \\ 9.0 \\ 11.3$	$\begin{array}{c} 15.\ 4\\ 20.\ 1\\ 25.\ 4\\ 10.\ 1\\ 12.\ 5\\ 15.\ 8\end{array}$	$\begin{array}{c} 30.\ 6\\ 37.\ 8\\ 45.\ 6\\ 18.\ 3\\ 22.\ 8\\ 28.\ 8\end{array}$	$53. \ 6 \\ 62. \ 6 \\ 70. \ 6 \\ 31. \ 7 \\ 38. \ 9 \\ 46. \ 8$	$118 \\ 127 \\ 135 \\ 77.8 \\ 88.4 \\ 98.4$	$203 \\ 212 \\ 220 \\ 148 \\ 157 \\ 168$
0	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 2.8\\ 3.5\\ 4.8\\ 2.2\\ 2.6\\ 3.4 \end{array}$	4.5 6.0 7.9 3.3 4.2 5.3	$\begin{array}{c} 6.8\\ 9.0\\ 12.2\\ 5.2\\ 6.5\\ 7.9 \end{array}$	$\begin{array}{c} 10.\ 1\\ 13.\ 0\\ 17.\ 2\\ 7.\ 6\\ 8.\ 8\\ 11.\ 6\end{array}$	$\begin{array}{c} 14.\ 1\\ 18.\ 2\\ 23.\ 7\\ 10.\ 1\\ 12.\ 5\\ 15.\ 6\end{array}$	$\begin{array}{c} 26.\ 4\\ 33.\ 6\\ 40.\ 2\\ 17.\ 4\\ 21.\ 6\\ 26.\ 7\end{array}$	$\begin{array}{r} 45.\ 3\\ 53.\ 2\\ 61.\ 9\\ 28.\ 4\\ 34.\ 9\\ 42.\ 5\end{array}$	$99.8 \\109 \\119 \\65.8 \\75.8 \\86.4$	$173 \\ 184 \\ 193 \\ 122 \\ 135 \\ 146$
	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	2.9 3.7 5.0 2.3 2.8 3.4	4.8 6.0 8.1 3.6 4.3 5.4	$\begin{array}{c} 6.8\\ 9.0\\ 11.9\\ 5.2\\ 6.3\\ 8.1 \end{array}$	9.6 12.6 16.8 7.6 9.0 11.3	$\begin{array}{c} 13.\ 7\\ 17.\ 7\\ 23.\ 0\\ 10.\ 1\\ 12.\ 2\\ 15.\ 1\end{array}$	$\begin{array}{c} 24.\ 6\\ 30.\ 6\\ 37.\ 5\\ 16.\ 8\\ 21.\ 0\\ 26.\ 1\end{array}$	40. 0 47. 9 56. 5 26. 6 32. 4 39. 6	86. 9 97. 0 107 58. 1 68. 2 77. 8	152 163 171 106 117 129
0000	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3.1 4.1 5.5 2.5 3.0 3.8	5.0 6.5 8.7 3.9 4.8 6.2	$7.2 \\ 9.4 \\ 12.8 \\ 5.6 \\ 6.8 \\ 8.6$	10. 1 13. 0 17. 0 7. 8 9. 5 11. 8	13. 2 17. 3 22. 3 10. 1 12. 7 15. 9	22. 8 28. 8 35. 7 16. 8 20. 4 26. 1	$\begin{array}{c} 35.\ 7\\ 43.\ 2\\ 51.\ 8\\ 25.\ 2\\ 30.\ 6\\ 37.\ 8\end{array}$	$\begin{array}{c} 71.\ 1\\ 81.\ 6\\ 91.\ 2\\ 50.\ 9\\ 60.\ 0\\ 69.\ 2 \end{array}$	121 133 144 88.8 101 112

#### APPENDIX B

#### Table 44.—Sags for Medium and Hard-Drawn Bare Solid Copper Wire—Continued

#### MEDIUM LOADING DISTRICT

[The sags being such that when loaded at 15° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B and 60 per cent for grade C]

Size	Grade of	Tem-	•		Sags	(inch	es) fo	r spar	ı leng	ths (fo	eet) of-	-	
A.W.G. No.	construction	pera- ture	100	125	150	175	200	250	300	400	500	700	1,000
8	{B C	$ \begin{array}{c} \circ F. \\ 30 \\ 69 \\ 90 \\ 30 \\ 60 \\ 90 \end{array} $	$2.8 \\ 3.4 \\ 4.4 \\ 2.0 \\ 2.3 \\ 2.8$	5.3 6.9 9.4 3.3 3.9 4.9	13.7 18.7 5.6								
6	A and B		2.4 2.9 3.7	$3.9 \\ 5.1 \\ 6.6$	6.5 8.1 10.8	10.1 13.0 17.2							
	lc	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	1.9 2.2 2.6	3.1 3.4 4.3	4.7 5.4 6.5	6.7 8.0 9.7							
4	∫A and B	6 90	2.3 2.8 3.4	$3.3 \\ 4.3 \\ 5.5 \\ 3.5 \\ 3.5 \\ 5.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 3.5 \\ 5.5 \\ 3.5 \\ 5.5 $	$5.4 \\ 6.7 \\ 8.6$	8.0 9.6 12.4	11. 0 13. 9 17. 8	25.8 32.1	43.9 52.2	96.5 106.0			
1	lc	$     \begin{cases}             30 \\             60 \\             90             90          $	1.9 2.2 2.6	3.0 3.3 3.9	4.5 5.0 5.9	$6.1 \\ 6.9 \\ 8.2$	8.2 9.4 11.3	16.2		63.4			
2	A and B	1 90	$2.3 \\ 2.9 \\ 3.4$	3.6 4.2 5.5 3.0	5.4 6.7 8.3	7.6 9.2 11.8	$10.1 \\ 12.5$	$\begin{array}{c c} 17.1 \\ 21.6 \\ 26.7 \end{array}$	27.7 33.8 42.1	61.0 71.0 81.6	$112.0\\125.0\\136.0$	273 284	
	lc	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	1.9 2.2 2.6	3.0 3.5 4.0	4.5 5.0 5.9	6.1 6.9 8.4	9.1	15.3	23.0		86.4	204	
	A and B	90	2.4 2.9 3.6	$3.6 \\ 4.5 \\ 5.7 \\ 1$	5.4 6.7 8.5		12.5 15.9	26.1	38.9		111.0 122.0	242 255	
1	lc	$     \begin{cases}             30 \\             60 \\             90             90          $	2.0 2.3 2.8	3.1 3.4 4.2	4.3 5.0 6.3	5.7 7.1 8.4	8.2 9.1 11.3	15.0	19.4 23.0 27.3	45.1	78.6	181	
0	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \end{cases}$	2.5 3.0 3.8 2.0	3.7 4.6 6.0 3.1	5.6 6.8 8.8 4.5	7.6 9.4 12.0 6.3	12.7	21.0 26.1	25.2 31.0 37.8 19.4	61. 4 71. 0	103.0 114.0	220 233	
	lc	$\begin{cases} 50 \\ 60 \\ 90 \end{cases}$	2.0 2.4 2.9	3. 6 4. 5	5.2	7.3	9.6 11.5	15.6	23.0	44.2	74.4	165	
00	A and B	90	2.6 3.1 4.1	3.9 4.9 6.3	5.8 6.8 9.0	7.8 9.7 12.2	$13.0 \\ 16.3$	20.7 26.4	25.2 31.0 37.8	50.4 59.5 69.1	97. 2 109. 0	204 218	$     439 \\     455 $
	lc	$\begin{cases} 30 \\ 60 \\ 90 \end{cases}$	2.2 2.5 3.0	3.3 3.7 4.6	4.7 5.4 6.7	6.3 7.6 9.0		15.9	19.8 23.4 28.1		72.0	154	329 346 366
0000	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \end{cases}$	2.6 3.2 4.4 2.2	4.2 5.4 6.9 3.4	$\begin{array}{c} 6.1 \\ 7.6 \\ 10.1 \\ 4.9 \end{array}$	8.2 10.5 13.4 6.9		27.0	25.9 31.7 38.9 20.5		93.0	171 185 201 132	410
	lo	{ 60 90	2.8 3.2	4. 0 5. 3	5.8	8.0	10.8		24.1	44.6	70.8	146	317

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#### MINIMUM SAGS FOR HARD COPPER

#### Table 44.—Sags for Medium and Hard-Drawn Bare Solid Copper Wire—Continued

#### LIGHT LOADING DISTRICT

[The sags being such that when loaded at 30° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B, and 60 per cent for grade C]

Size A. W. G.	Grade of	Tem-			Sags	(inch	es) fo	r spai	ı leng	ths (f	eet) of		
No.	construction	pera- ture	100	125	150	175	200	250	300	400	500	700	1,000
8	{B {C	$ \begin{smallmatrix} \circ & F. \\ & 30 \\ & 60 \\ & 90 \\ & 30 \\ & 60 \\ & 90 \end{smallmatrix} $	$     \begin{array}{r}       1.9\\       2.3\\       2.6\\       1.6\\       1.9\\       2.2     \end{array} $	3.0 3.6 4.2 2.5 2.8 3.3	$\begin{array}{c} 4.5\\ 5.0\\ 6.1\\ 3.6\\ 4.3\\ 4.8\end{array}$								
6	$ \begin{cases} A \text{ and } B_{\dots} \\ C_{\dots} \end{cases} $	$     \begin{cases}             30 \\             60 \\             90 \\             30 \\             60 \\             90             90         $	$2.0 \\ 2.3 \\ 2.8 \\ 1.7 \\ 2.0 \\ 2.2$	3.1 3.4 4.3 2.7 3.0 3.4	4.7 5.2 6.3 4.0 4.5 4.9	$\begin{array}{c} 6.1 \\ 7.1 \\ 8.4 \\ 5.0 \\ 5.9 \\ 6.7 \end{array}$	9.4 11.5						
4	{A and B C	f 30	2.0 2.4 2.9 1.7 1.9	3.1 3.6 4.3 2.8 3.0	4.7 5.2 6.5 3.8 4.5	6.3 7.1 8.8 5.0 6.1	8.2 9.4 11.5 6.7 7.9	$12.9 \\ 15.0 \\ 18.0 \\ 10.8 \\ 12.0$	18.722.026.615.117.3	35.5 41.3 49.0 27.8 31.7	67.2 78.0 45.0		
2	{A and B C	{ 90 ( 30	2.3 2.2 2.5 3.0 1.7 2.0	3.4 3.3 3.6 4.6 2.7 3.3	5.0 4.9 5.4 6.5 4.3 4.7	6.7 6.3 7.6 9.0 5.5 6.1	8.9 8.4 10.1 12.0 7.0 8.2		20.2 19.4 22.3 27.0	36. 5 35. 5 41. 3 49. 5 28. 8 33. 1	58.8 58.2 67.2	124.0 138.0 153.0 97.4	
1	A and B	1 90 f 30	2.4 2.2 2.6 3.1 1.8 2.2	3.4 3.3 3.9 4.8 2.7 3.3	5.2 4.9 5.8 6.8 4.1 4.7	7.1 6.5 7.6 9.5 5.5 6.3	9.1 8.6 10.1 12.5 7.2 8.2	15.3 13.5 16.2 19.5 11.1 12.9	20.9 19.8 23.0	37.9 36.5 42.2 49.9	60.0 58.2 67.2 78.0 46.2	122.0 124.0 139.0	276 294
0	$\begin{cases} A and B_{\dots} \\ C_{\dots} \end{cases}$	[ 90 [ 30	2.5 2.2 2.6 3.2 1.9 2.2	3.8 3.3 4.0 5.1 3.0 3.3	5.4 5.0 5.9 7.2 4.3 4.9	7.4 6.7 8.0 9.9 5.7 6.5	9.6 8.6 10.6		22.0 20.2 23.7 28.8	39.4 36.9 43.2 50.9 29.7 34.5	61.2 60.0 69.0	122.0 124.0 138.0 154.0 97.5	252 274 293
00	A and B	{ 90 { 30 { 60	2.5 2.3 2.8 3.4 1.9 2.2	3.9 3.4 4.4 5.4 3.2 3.4	5.8 5.0 6.3 7.7 4.5 5.0	7.8 6.9 8.4 10.3 5.9 6.7	9.1 11.0 13.4 7.7 8.9	15.6 14.4 16.8 21.0 12.0 13.8	22.3 20.9 24.5 30.2 17.3 19.4	$\begin{array}{r} 44.2 \\ 51.8 \\ 30.7 \\ 36.0 \end{array}$		124.0 139.0 153.0 99.2 112.0	273 291 312 216 234
0000	{A and B C	$   \begin{cases}     90 \\     60 \\     90 \\     30 \\     60 \\     90 \\     90   \end{cases} $	2.6 2.5 3.0 3.8 2.1 2.5 2.9	4.1 3.8 4.6 5.9 3.3 3.6 4.5	5.9 5.4 6.5 8.5 4.7 5.4 6.5	7.4 8.8	8.2 9.4	$12.6 \\ 15.3$	20.9	39.8 46.1 55.7 32.6 37.4	$\begin{array}{r} 63. \ 6\\ 73. \ 2\\ 84. \ 0\\ 51. \ 6\\ 59. \ 4\end{array}$	129.0144.0158.0104.0116.0	274 293 312 222 241

#### APPENDIX B

#### Table 45.—Sags for Medium and Hard-Drawn Bare Stranded Copper Wire

#### HEAVY LOADING DISTRICT

[The sags being such that when loaded at 0° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B, and 60 per cent for grade C]

Size	Grade of	Tem.		Sa	gs (inc	ehes) fo	or span	lengths	(feet) o	of—	
A.W.G. No.	construction	pera- ture	100	125	150	200	250	350	500	700	1,000
4	{A and B C	$ \begin{cases} {}^{\circ}F. \\ 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases} $	2.9 3.6 5.0 2.2 2.6 3.1	5.47.210.23.64.25.4	10. 4 14. 4 19. 4 5. 7 7. 2 9. 4	32. 6 39. 4 45. 1 14. 9 19. 2 25. 0	$\begin{array}{c} 67.\ 2\\72.\ 6\\79.\ 2\\36.\ 0\\43.\ 8\\51.\ 6\end{array}$				
2	A and B	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array} \right.$	2.6 3.4 4.3 2.2 2.4 2.9	$\begin{array}{r} 4.5 \\ 5.7 \\ 7.8 \\ 3.3 \\ 3.9 \\ 4.8 \end{array}$	$7.2 \\ 9.4 \\ 13.0 \\ 5.0 \\ 5.7 \\ 7.5$	$\begin{array}{c} 16.8\\ 22.1\\ 28.3\\ 10.1\\ 12.5\\ 15.8 \end{array}$	$\begin{array}{c} 36.0\\ 43.8\\ 51.6\\ 19.8\\ 25.2\\ 31.2 \end{array}$	$\begin{array}{r} 99.\ 1\\ 107.\ 0\\ 115.\ 0\\ 62.\ 2\\ 72.\ 2\\ 81.\ 5\end{array}$	$240 \\ 248 \\ 256 \\ 176 \\ 186 \\ 196$		
1	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 2.\ 6\\ 3.\ 4\\ 4.\ 6\\ 2.\ 2\\ 2.\ 6\\ 3.\ 1\end{array}$	4.5 5.7 7.5 3.3 3.9 5.1	$\begin{array}{c} 6.8\\ 9.0\\ 11.9\\ 5.0\\ 6.1\\ 7.9\end{array}$	$14.9 \\19.7 \\25.0 \\10.1 \\12.0 \\15.4$	$\begin{array}{c} 31.\ 2\\ 36.\ 6\\ 44.\ 4\\ 17.\ 4\\ 23.\ 4\\ 27.\ 6\end{array}$	$\begin{array}{r} 82.\ 3\\ 90.\ 7\\ 100.\ 0\\ 51.\ 2\\ 59.\ 6\\ 69.\ 7\end{array}$	$203 \\ 212 \\ 221 \\ 146 \\ 157 \\ 167$	438 447 454 338 348 358	761 770 780
0	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 2.\ 6\\ 3.\ 1\\ 4.\ 3\\ 2.\ 2\\ 2.\ 4\\ 2.\ 9\end{array}$	$\begin{array}{r} 4.2\\ 5.4\\ 6.9\\ 3.3\\ 3.9\\ 4.8 \end{array}$	$\begin{array}{c} 6.5 \\ 7.9 \\ 10.8 \\ 5.0 \\ 5.8 \\ 6.8 \end{array}$	$12.5 \\ 15.8 \\ 21.1 \\ 9.1 \\ 11.0 \\ 13.4$	$\begin{array}{c} 23.\ 4\\ 29.\ 4\\ 37.\ 2\\ 15.\ 6\\ 19.\ 8\\ 23.\ 4\end{array}$	$\begin{array}{c} 63.\ 0\\ 72.\ 2\\ 82.\ 3\\ 38.\ 6\\ 47.\ 0\\ 50.\ 4\end{array}$	161 172 181 113 119 137	349 368 378 270 282 296	787 797 806 624 634 648
00	A and B	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$2.6 \\ 3.4 \\ 4.3 \\ 2.2 \\ 2.6 \\ 3.1$	$ \begin{array}{c} 4.2\\ 5.4\\ 7.2\\ 3.3\\ 3.9\\ 4.8 \end{array} $	$\begin{array}{c} 6.5\\ 7.9\\ 10.4\\ 4.7\\ 5.8\\ 7.2 \end{array}$	12.515.420.29.110.613.0	$\begin{array}{c} 21.\ 6\\ 27.\ 0\\ 33.\ 6\\ 15.\ 0\\ 18.\ 0\\ 22.\ 2\end{array}$	$54. \ 6 \\ 63. \ 8 \\ 73. \ 1 \\ 36. \ 1 \\ 42. \ 8 \\ 51. \ 2$	$140 \\ 144 \\ 149 \\ 96 \\ 107 \\ 120$	$307 \\ 319 \\ 331 \\ 232 \\ 245 \\ 259$	$\begin{array}{r} 682 \\ 691 \\ 698 \\ 535 \\ 547 \\ 562 \end{array}$
0000	A and B	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right. $	2.63.14.32.22.63.1	4. 2 5. 1 6. 9 3. 3 3. 9 4. 8	$\begin{array}{c} 6.1 \\ 7.6 \\ 9.7 \\ 4.7 \\ 5.7 \\ 6.8 \end{array}$	$11.5 \\ 13.9 \\ 18.2 \\ 8.6 \\ 10.0 \\ 12.5$	18. 622. 828. 813. 816. 821. 0	$\begin{array}{c} 42.\ 0\\ 50.\ 4\\ 58.\ 8\\ 30.\ 2\\ 36.\ 1\\ 43.\ 7\end{array}$	$102 \\ 114 \\ 126 \\ 73 \\ 84 \\ 96$	$\begin{array}{c} 222\\ 244\\ 257\\ 160\\ 176\\ 188 \end{array}$	$506 \\ 523 \\ 535 \\ 396 \\ 413 \\ 432$

# Table 45.—Sags for Medium and Hard-Drawn Bare Stranded Copper Wire—Continued.

#### MEDIUM LOADING DISTRICT

[The sags being such that when loaded at 15° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B, and 60 per cent for grade C]

Size	Grade of	Tem-		Sa	gs (inc	hes) fo	r span	length	s (feet)	of—	
A. W. G. No. 1	construction	pera- ture	100	125	150	200	250	350	500	700	1,000
4	{A and B C	$\circ_{F.}$ $\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	2. 2 2. 6 3. 1 1. 9 2. 2 2. 4	3. 6 4. 2 5. 4 3. 0 3. 3 3. 9	5.4 6.5 8.3 4.3 5.0 5.7	11. 0 13. 4 16. 8 8. 2 9. 1 11. 0	19. 8 25. 8 29. 4 13. 2 15. 6 19. 8	60. 5 69. 7 79. 8 36. 1 42. 8 49. 6			
2	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	2.4 2.6 3.4 1.9 2.2 2.6	3.6 4.2 5.4 3.0 3.3 3.9	5.0 6.1 7.9 4.3 5.0 5.7	10. 1 12. 0 15. 4 7. 7 9. 1 11. 0	$16.8 \\ 20.4 \\ 25.2 \\ 12.6 \\ 14.4 \\ 17.4$	41. 2 49. 6 58. 8 27. 7 33. 6 39. 5	$112 \\ 124 \\ 133 \\ 74.4 \\ 85.2 \\ 97.2$	260 274 286 188 203 217	590 602 614 458 473 487
1	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	2.42.93.41.92.22.6	3.64.55.73.0 $3.34.2$	$5.4 \\ 6.5 \\ 7.9 \\ 4.3 \\ 5.0 \\ 6.1$	$10.1 \\ 12.0 \\ 14.9 \\ 7.7 \\ 9.1 \\ 11.0$	$16.8 \\19.8 \\25.2 \\12.6 \\15.0 \\17.4$	$\begin{array}{r} 37.8 \\ 45.4 \\ 53.8 \\ 27.7 \\ 31.9 \\ 38.6 \end{array}$	99.6 112 124 68.4 79.2 90.0	230 244 257 166 183 197	521 538 550 403 420 437
0	{A and B C	$\begin{cases} 30\\ 60\\ 90\\ 30\\ 60\\ 90\\ 90 \end{cases}$	2.4 2.9 3.4 1.9 2.2 2.6	3.6 4.2 5.4 3.0 3.3 3.9	5.0 6.5 7.9 4.3 5.0 5.8	$9.6 \\ 11.5 \\ 14.4 \\ 7.7 \\ 8.6 \\ 10.6$	$15. \ 6 \\ 18. \ 6 \\ 23. \ 4 \\ 12. \ 0 \\ 14. \ 4 \\ 16. \ 8 $	$\begin{array}{r} 34.\ 4\\ 41.\ 2\\ 49.\ 6\\ 25.\ 2\\ 30.\ 2\\ 35.\ 3\end{array}$	85. 2 96. 0 109 60. 0 69. 6 79. 2	$191 \\ 210 \\ 225 \\ 141 \\ 156 \\ 171$	446 461 475 343 360 379
00	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 2.4 \\ 2.9 \\ 3.6 \\ 1.9 \\ 2.4 \\ 2.9 \end{array}$	3.6 4.5 5.7 3.0 3.3 4.2	5.4 6.5 7.9 4.3 5.0 6.1	9.611.514.97.79.111.0	$15.6 \\ 18.6 \\ 22.8 \\ 12.6 \\ 14.4 \\ 16.8$	33. 6 40. 3 47. 0 26. 0 30. 2 39. 5	$\begin{array}{r} 79.\ 2\\ 91.\ 2\\ 102\\ 58.\ 8\\ 67.\ 2\\ 76.\ 8\end{array}$	$176 \\ 191 \\ 207 \\ 133 \\ 146 \\ 161$	396 415 430 305 324 343
9000	{A and B C	$\left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right.$	2.4 2.9 3.6 1.9 2.4 2.6	3.6 4.5 5.7 3.0 3.6 4.2	5.4 6.5 8.3 4.3 5.0 6.1	9.6 11.5 14.4 7.7 9.1 10.6	15.0 18.0 22.2 12.0 14.4 16.8	$\begin{array}{c} 31.\ 1\\ 37.\ 8\\ 43.\ 7\\ 25.\ 2\\ 28.\ 6\\ 34.\ 4\end{array}$	69. 6 80. 4 91. 2 52. 8 62. 4 72. 0	$149 \\ 173 \\ 180 \\ 114 \\ 128 \\ 143$	331 350 367 259 276 298

#### APPENDIX B

#### Table 45.—Sags for Medium and Hard-Drawn Bare Stranded Copper Wire—Continued.

#### LIGHT LOADING DISTRICT

[The sags being such that when loaded at 30° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B, and 60 per cent for grade C]

Size	Grade of	Tem!		Sa	gs (inc	hes) fo	r span	lengths	(feet)	of	
A. W. G. No.	construction	pera- ture	100	125	150	200	250	350	500	700	1,000
4	{A and B {C	$ \begin{array}{c} ^{\circ}F. \\ 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array} $	1.9 2.4 2.9 1.7 1.9 2.2	$3.0 \\ 3.6 \\ 4.2 \\ 2.4 \\ 3.0 \\ 3.3$	$\begin{array}{c} 4.3 \\ 5.0 \\ 6.1 \\ 3.6 \\ 4.3 \\ 4.7 \end{array}$	7.79.111.0 $6.77.28.6$	$12.0 \\ 14.4 \\ 17.4 \\ 10.2 \\ 11.4 \\ 13.8$	$\begin{array}{c} 25.\ 2\\ 30.\ 2\\ 37.\ 0\\ 21.\ 0\\ 23.\ 5\\ 27.\ 7\end{array}$	$\begin{array}{c} 61.\ 2\\ 70.\ 8\\ 81.\ 6\\ 45.\ 6\\ 52.\ 8\\ 60.\ 0\end{array}$		
2	{A and B {C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 2.2 \\ 2.4 \\ 2.9 \\ 1.7 \\ 1.9 \\ 2.4 \end{array}$	3.33.64.52.43.03.6	$\begin{array}{r} 4.7\\ 5.4\\ 6.5\\ 4.0\\ 4.3\\ 5.0 \end{array}$	$\begin{array}{r} 8.2\\ 9.6\\ 11.5\\ 6.7\\ 7.7\\ 9.1 \end{array}$	$\begin{array}{c} 12.\ 6\\ 15.\ 0\\ 18.\ 0\\ 10.\ 2\\ 12.\ 0\\ 13.\ 8\end{array}$	$\begin{array}{c} 26.9\\ 30.2\\ 37.0\\ 21.0\\ 24.4\\ 27.7 \end{array}$	58.8 67.2 78.0 45.6 51.6 60.0	$129 \\ 143 \\ 153 \\ 99.1 \\ 111 \\ 124$	
1	$\begin{cases} A and B \\ C \end{bmatrix}$	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	2.22.42.91.92.22.4	3.3 3.6 4.8 2.7 3.0 3.6	$\begin{array}{r} 4.7\\ 5.4\\ 6.8\\ 4.0\\ 4.3\\ 5.0 \end{array}$	$\begin{array}{r} 8.2\\ 9.6\\ 12.0\\ 7.2\\ 8.2\\ 9.6\end{array}$	$\begin{array}{c} 13.\ 2\\ 15.\ 6\\ 19.\ 2\\ 10.\ 8\\ 12.\ 6\\ 14.\ 4 \end{array}$	$\begin{array}{c} 26.\ 9\\ 31.\ 1\\ 38.\ 6\\ 21.\ 8\\ 25.\ 2\\ 29.\ 4 \end{array}$	$\begin{array}{r} 46.8\\ 68.4\\ 78.0\\ 46.8\\ 54.0\\ 61.2 \end{array}$	$128 \\ 141 \\ 156 \\ 99.1 \\ 111 \\ 124$	290 207 326 223 242 262
0	{A and B C	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array} \right.$	$2.2 \\ 2.4 \\ 2.9 \\ 1.7 \\ 1.9 \\ 2.4$	3.3 3.6 4.5 2.7 3.3 3.6	$\begin{array}{r} 4.\ 7\\ 5.\ 4\\ 6.\ 5\\ 4.\ 0\\ 4.\ 7\\ 5.\ 4\end{array}$	$\begin{array}{r} 8.2\\ 9.6\\ 12.0\\ 6.7\\ 7.7\\ 9.1 \end{array}$	$\begin{array}{c} 12.\ 6\\ 15.\ 0\\ 18.\ 0\\ 10.\ 8\\ 12.\ 6\\ 14.\ 4 \end{array}$	$\begin{array}{c} 26.\ 7\\ 30.\ 2\\ 37.\ 0\\ 21.\ 8\\ 24.\ 4\\ 28.\ 6\end{array}$	$57. \ 6 \\ 66. \ 0 \\ 75. \ 6 \\ 45. \ 6 \\ 52. \ 8 \\ 60. \ 0$	$121 \\ 134 \\ 149 \\ 95.8 \\ 106 \\ 119$	$271 \\ 290 \\ 310 \\ 211 \\ 228 \\ 247$
00	$\begin{cases} A \text{ and } B \\ C \\ \end{cases}$	$ \left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90 \end{array}\right\} $	$\begin{array}{c} 2.2 \\ 2.4 \\ 3.1 \\ 1.9 \\ 2.2 \\ 2.4 \end{array}$	3.3 3.6 4.8 3.0 3.3 3.6	$\begin{array}{r} 4.7\\ 5.8\\ 6.8\\ 4.3\\ 4.7\\ 5.4\end{array}$	$\begin{array}{c} 8.2\\ 10.1\\ 12.0\\ 7.2\\ 8.2\\ 9.6\end{array}$	13. 215. 619. 210. 812. 615. 0	$\begin{array}{c} 26.9\\ 31.1\\ 37.8\\ 21.8\\ 25.2\\ 29.4 \end{array}$	$57. \ 6 \\ 66. \ 0 \\ 76. \ 8 \\ 46. \ 8 \\ 52. \ 8 \\ 60. \ 0 \\$	$\begin{smallmatrix} 102 \\ 133 \\ 148 \\ 94.1 \\ 106 \\ 119 \end{smallmatrix}$	$264 \\ 281 \\ 302 \\ 209 \\ 226 \\ 242$
0600	{A and B C	$ \left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90 \end{array}\right\} $	$\begin{array}{c} 2.2 \\ 2.6 \\ 3.1 \\ 1.9 \\ 2.2 \\ 2.4 \end{array}$	3.3 3.9 4.8 3.0 3.3 3.6	$\begin{array}{c} 4.7\\ 5.8\\ 6.8\\ 4.3\\ 4.7\\ 5.4 \end{array}$	$\begin{array}{c c} 8.6\\ 10.1\\ 12.5\\ 7.2\\ 8.2\\ 9.6\end{array}$	$\begin{array}{c} 13.\ 2\\ 15.\ 6\\ 19.\ 2\\ 10.\ 8\\ 12.\ 6\\ 15.\ 0\end{array}$	$\begin{array}{c} 26.\ 9\\ 31.\ 1\\ 37.\ 0\\ 22.\ 7\\ 25.\ 2\\ 29.\ 4 \end{array}$	56.4 64.8 74.4 46.8 52.8 61.2	$116 \\ 129 \\ 143 \\ 92.4 \\ 104 \\ 116$	247 266 286 199 216 235

## Table 46.—Sags for Medium and Hard-Drawn T. B. W. P. Solid Copper Wire

#### HEAVY LOADING DISTRICT

[The sags being such that when loaded at 0° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B, and 60 per cent for grade C]

Size	Grade of	Tem-		Sags (in	ches) for	span le	ngths (fe	et) oí—	
A. W. G. No.	construction	pera- ture	100	125	150	175	200	250	300
8	с	$ \begin{cases} {}^{\circ}F_{*} \\ 30 \\ 60 \\ 90 \end{cases} $	$10.2 \\ 13.3 \\ 17.2$	29.7 31.5 35.1	50.4 53.6 56.6				
6	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	8.712.215.64.15.47.2	$\begin{array}{c} 23.\ 1\\ 26.\ 6\\ 30.\ 6\\ 9.\ 7\\ 12.\ 7\\ 16.\ 9\end{array}$	$\begin{array}{c} 37.1 \\ 44.7 \\ 48.1 \\ 22.5 \\ 27.7 \\ 32.0 \end{array}$	38.9 44.1 48.5			
4	{A and B C	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \end{array}\right\} $	4, 4 6, 1 8, 2 2, 9 3, 7	9.6 12.4 16.6 5.3 6.6	18.423.028.19.211.5	32.8 38.0 42.9 16.2 20.2	$\begin{array}{r} 48.7\\54.2\\58.8\\26.4\\32.6\\32.6\end{array}$		
2	$ \begin{cases} A and B \\ C \end{bmatrix} $	$ \left\{\begin{array}{c} 90\\ 30\\ 90\\ 30\\ 60\\ 60 \end{array}\right\} $	$\begin{array}{c} 4.6\\ 3.8\\ 5.0\\ 6.5\\ 3.0\\ 3.5\\ \end{array}$	8.46.68.711.54.85.7	$15.1 \\ 11.2 \\ 14.8 \\ 18.9 \\ 7.4 \\ 9.0 \\ 10$	$25. 4 \\ 18. 7 \\ 23. 1 \\ 28. 6 \\ 11. 3 \\ 14. 3 \\ 14. 3 \\ $	38. 9 28. 3 34. 1 40. 1 16. 3 20. 1	55.5 62.4 68.4 33.3 39.6	$90. 0 \\ 97. 2 \\ 104 \\ 60. 2 \\ 67. 4$
1	{A and B C	$   \begin{cases}     90 \\     60 \\     90 \\     30 \\     60 \\     90 \\     90   \end{cases} $	$\begin{array}{c} 4.3\\ 3.6\\ 4.6\\ 6.2\\ 2.8\\ 3.2\\ 4.2 \end{array}$	$\begin{array}{c} 7.1 \\ 6.1 \\ 7.8 \\ 10.8 \\ 4.6 \\ 5.5 \\ 6.9 \end{array}$	$11.5 \\ 9.7 \\ 12.6 \\ 16.7 \\ 6.8 \\ 8.5 \\ 10.6$	17. 2 $15. 5$ $19. 7$ $24. 6$ $10. 1$ $12. 2$ $15. 7$	25. 0 22. 6 38. 1 34. 1 13. 9 17. 7 21. 8	46. 2 44. 4 52. 2 58. 2 27. 3 33. 6 40. 2	75. 673. 481. 888. 246. 1 $55. 162. 3$
0	{A and B C	$ \begin{cases}     30 \\     60 \\     90 \\     30 \\     60 \\     90 \end{cases} $	$ \begin{array}{c} 3.7 \\ 4.8 \\ 6.4 \\ 2.8 \\ 3.5 \\ 4.4 \end{array} $	$\begin{array}{c} 6.0\\ 7.8\\ 10.6\\ 4.6\\ 5.5\\ 6.7\end{array}$	$9.4 \\ 12.1 \\ 15.6 \\ 6.8 \\ 8.1 \\ 10.1$	$ \begin{array}{c} 13.1 \\ 14.1 \\ 17.8 \\ 22.9 \\ 9.9 \\ 12.2 \\ 14.9 \end{array} $	21.8 $20.6$ $25.4$ $31.2$ $13.7$ $16.8$ $20.9$	38. 4 45. 0 52. 8 24. 6 30. 3 35. 7	$\begin{array}{c} 62.6\\ 70.6\\ 78.2\\ 41.0\\ 48.6\\ 55.8\end{array}$
00	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3.6 4.6 6.1 2.6 3.2 4.2	$\begin{array}{c} 6.0\\ 7.8\\ 10.5\\ 4.6\\ 5.5\\ 6.9 \end{array}$	$9.0 \\ 11.5 \\ 15.1 \\ 7.0 \\ 8.3 \\ 10.4$	13.216.821.49.711.814.5	18.523.028.513.216.120.1	$\begin{array}{c} 33.\ 6\\ 39.\ 9\\ 46.\ 8\\ 22.\ 8\\ 27.\ 6\\ 33.\ 6\end{array}$	$54.0 \\ 61.9 \\ 70.9 \\ 36.0 \\ 43.6 \\ 50.8$
0000	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 3.7\\ 4.8\\ 6.6\\ 2.9\\ 3.6\\ 4.6\end{array}$	$\begin{array}{c} 6.0\\ 7.8\\ 10.5\\ 4.6\\ 5.7\\ 7.4 \end{array}$	$9.0 \\ 11.5 \\ 15.1 \\ 6.8 \\ 8.5 \\ 10.4$	$12. \ 6 \\ 16. \ 2 \\ 20. \ 4 \\ 9. \ 7 \\ 11. \ 8 \\ 14. \ 5 \\$	$   \begin{array}{r}     17.5 \\     21.1 \\     27.1 \\     12.7 \\     15.6 \\     19.7 \\   \end{array} $	28.834.842.020.425.530.9	$\begin{array}{c} 45.0\\ 53.3\\ 61.2\\ 32.4\\ 38.9\\ 45.7\end{array}$

25804°-27-16

#### APPENDIX B

# Table 46.—Sags for Medium and Hard-Drawn T. B. W. P. Solid Copper Wire—Continued

#### MEDIUM LOADING DISTRICT

[The sags being such that when loaded at  $15^{\circ}$  F, the wires will be stressed to 50 per cent of their ultimate strength for grades A and B, and 60 per cent for grade C]

Size A. W. G. No.	Grade of construction	Tem-	Sags (inches) for span lengths (feet) of-							
		pera- ture	100	125	150	175	200	250	300	
8	{B C	$ \begin{cases} {}^{\circ}F. \\ {}^{60} \\ {}^{90} \\ {}^{30} \\ {}^{60} \\ {}^{90} \end{cases} $	4.8 6.2 8.6 3.2 3.7 4.6	11. 2 14. 7 18. 4 6. 0 7. 4 9. 3	23. 2 27. 3 32. 1 10. 8 13. 7 17. 3					
6	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3.6 4.4 5.8 2.8 3.1 3.6	6.6 8.3 10.8 4.6 5.4 6.6	11.514.819.17.28.610.6	$19.7 \\ 24.4 \\ 29.6 \\ 11.1 \\ 13.6 \\ 16.8$				
4	{A and B C	$ \begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \\ 90 \end{cases} $	$\begin{array}{c} 3.0\\ 3.7\\ 4.7\\ 2.5\\ 2.9\\ 3.4 \end{array}$	5.1 6.1 7.8 4.0 4.5 5.4	7.99.712.6 $5.86.8$	10. 8 11. 8 14. 9 18. 9 8. 6 10. 1 12. 2	$17. \ 3 \\ 21. \ 6 \\ 26. \ 6 \\ 11. \ 5 \\ 13. \ 7 \\ 16. \ 8$			
2	{A and B C	$ \begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \\ 90 \end{cases} $	$\begin{array}{c} 3. \ 4 \\ 3. \ 0 \\ 3. \ 7 \\ 4. \ 7 \\ 2. \ 5 \\ 2. \ 9 \\ 3. \ 5 \end{array}$	$\begin{array}{c} 5.4\\ 4.8\\ 6.0\\ 7.6\\ 4.0\\ 4.5\\ 5.4\end{array}$	$8.1 \\ 7.2 \\ 8.1 \\ 11.2 \\ 5.8 \\ 6.7 \\ 8.1$	12. 2 10. 7 13. 0 16. 4 8. 0 9. 2 11. 3	16. 8 14. 4 18. 0 22. 1 10. 8 12. 7 15. 4	25.8 31.2 37.5 18.6 21.0 25.5	41. 8 49. 7 56. 9 28. 8 33. 8 40. 3	
1	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \\ 90 \\ 90 \end{cases}$	$\begin{array}{c} 2.9\\ 3.6\\ 4.6\\ 2.5\\ 2.8\\ 3.4 \end{array}$	$\begin{array}{c} 4.8 \\ 5.8 \\ 7.5 \\ 4.0 \\ 4.5 \\ 5.4 \end{array}$	7.2 8.6 11.0 5.8 6.7 7.9	10. 1 12. 2 15. 1 7. 8 9. 2 10. 9	$   \begin{array}{r}     13.7 \\     16.8 \\     20.9 \\     10.3 \\     12.2 \\     14.9   \end{array} $	23.428.534.517.419.824.3	36. 7 43. 9 50. 8 26. 6 31. 0 36. 7	
0	{A and B C	<pre>     30     60     90     30     60     90 </pre>	$\begin{array}{c} 3.1\\ 3.8\\ 4.9\\ 2.6\\ 3.0\\ 3.7 \end{array}$	4.9 6.0 7.8 4.2 4.8 5.7	$7.2 \\ 8.8 \\ 11.2 \\ 5.8 \\ 6.8 \\ 8.1$	10. 1 12. 2 15. 5 8. 0 9. 2 11. 3	13. 716. 820. 910. 812. 715. 1	23. 4 28. 2 34. 2 17. 4 20. 4 24. 6	34. 5 40. 7 49. 0 25. 2 29. 5 35. 3	
00	A and B	$\begin{cases} & 30 \\ & 60 \\ & 90 \\ & 30 \\ & 60 \\ & 90 \end{cases}$	$\begin{array}{c} 3.2 \\ 4.0 \\ 5.0 \\ 2.5 \\ 2.9 \\ 3.6 \end{array}$	$5.1 \\ 6.0 \\ 7.9 \\ 4.1 \\ 4.8 \\ 5.7$	7.29.011.5 $5.86.88.3$	10. 1 12. 6 15. 9 8. 2 9. 7 10. 8	13. 416. 620. 610. 612. 515. 4	22, 2 26, 7 32, 7 17, 1 20, 1 24, 3	34. 2 40. 3 47. 2 25. 9 30. 2 35. 6	
0000	A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 3.1\\ 4.1\\ 5.4\\ 2.6\\ 3.1\\ 3.9\end{array}$	$5.1 \\ 6.5 \\ 8.4 \\ 4.2 \\ 5.0 \\ 6.2$	7.6 9.4 12.1 6.1 7.2 9.0	10. 5 12. 6 16. 4 8. 4 10. 1 12. 2	13. 716. 821. 110. 812. 715. 8	$\begin{array}{c} 21.\ 6\\ 26.\ 4\\ 32.\ 4\\ 16.\ 8\\ 20.\ 4\\ 24.\ 6\end{array}$	32.8 39.2 45.7 25.9 30.2 36.0	

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218

# Table 46.—Sags for Medium and Hard-Drawn T. B. W. P. Solid Copper Wire—Continued

#### LIGHT LOADING DISTRICT

[The sags being such that when loaded at  $30^\circ$  F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B and 60 per cent for grade C]

Size	Grade of	Tem- pera- ture	Sags (inches) for span lengths (feet) of-							
A. W. G. No.	construction		100	125	150	175	200	250	300	
8	{ <sup>B</sup>	$ \begin{cases} {}^{\circ}F. \\ {}^{60}\\ {}^{90}\\ {}^{30}\\ {}^{60}\\ {}^{60} \end{cases} $	3.1 3.6 4.4 2.4 2.9	5.1 6.0 7.5 3.9 4.6	7.79.411.2 $5.96.7$	8. 2 9. 2				
	(A and B	$ \begin{cases} 90 \\ 30 \\ 60 \end{cases} $	2. 8 3. 2 2. 8 3. 0	5.3 4.6 5.4	7.7 6.8 8.1	11.3 9.7 11.6	13. 2 15. 8			
6	{c	$\begin{cases} 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3.8 2.4 2.8 3.0	6.5 3.8 4.3 4.9	9.9 5.6 6.5 7.4	14.1 7.6 8.8 10.5	$19.2 \\ 10.1 \\ 11.5 \\ 13.7$			
4	A and B	1 90	2.8 3.1 3.7	4.2 4.8 5.9	6.3 7.0 8.6	$8.6 \\ 10.1 \\ 12.2$	11. 8 13. 7 16. 6			
1	lc	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	2.4 2.6 2.9	3.6 3.9 4.5	5.0 5.8 6.5	7.1 8.0 9.0	9.1 10.3 12.5			
2	A and B	<pre>     30     60     90     30 </pre>	2.8 3.2 4.1 2.4	4.3 5.1 6.2 3.6	$\begin{array}{c} 6.1 \\ 7.2 \\ 8.6 \\ 5.0 \end{array}$	$     \begin{array}{r}       8.4 \\       10.1 \\       12.2 \\       7.1     \end{array} $	$     11.8 \\     13.4 \\     16.8 \\     9.6   $	$ \begin{array}{c} 18.3 \\ 21.9 \\ 25.8 \\ 15.0 \end{array} $	27.3 32.0 37.8 21.6	
	lc	60 90	2.6 2.9	4.2 4.8	5.8 6.8	8.0 9.7	$10.6 \\ 12.5$	16. 8 19. 8	24. 5 28. 8	
1	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \end{cases}$	2.6 2.9 4.0 2.3	4.2 4.9 6.2 3.8	$\begin{array}{c} 6.1 \\ 7.2 \\ 8.6 \\ 5.0 \end{array}$	$     \begin{array}{r}       8.4 \\       10.1 \\       12.2 \\       7.1     \end{array} $	$     \begin{array}{r}       11.3 \\       13.2 \\       16.3 \\       9.1     \end{array} $	17.4 21.0 25.5 14.4	$\begin{array}{c} 26.\ 6\\ 31.\ 3\\ 36.\ 7\\ 20.\ 9\end{array}$	
	lc	{ 60 { 90	2. 6 2. 6 3. 0	4.0 4.8	5.8 6.8	7.8 9.2	10.6 12.5	16.8 19.2	20. 9 24. 5 28. 4	
0	A and B	$   \begin{cases}     30 \\     60 \\     90 \\     20   \end{cases} $	2.8 3.4 4.2	4.5 5.3 6.6	6.3 7.6 9.4	9.0 10.7 12.8	11.5 13.9 16.8	$   \begin{array}{r}     18.0 \\     21.6 \\     26.4 \\   \end{array} $	27.3 32.0 37.4	
	lc	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	2.4 2.8 3.1	$3.8 \\ 4.3 \\ 5.1$	$5.2 \\ 6.1 \\ 7.2$	7.1 8.4 10.1	9,6 11,0 13,0	$15.0 \\ 17.1 \\ 20.1$	22. 0 25. 2 29. 1	
00	A and B	$   \begin{cases}     30 \\     60 \\     90 \\     20   \end{cases} $	2.8 3.5 4.3	4.5 5.4 6.6	6.5 7.9 9.7	8.8 10.1 12.8	11.5 13.4 16.6	18.3 21.6 26.7	27.0 31.3 37.4	
	lc	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	2.4 2.6 3.2	5.9 4.2 5.1	5.4 6.5 7.4	7.1 8.2 10.1	9.6 11.0 13.2	15.0 17.1 20.4	21. 6 25. 2 29. 5	
0000	A and B	90	2.9 3.5 4.6	4.5 5.4 7.2	6.7 7.9 9.9	8.8 10.9 13.6	$11.5 \\ 14.4 \\ 17.7$	18.6 22.2 27.0	27.3 32.4 38.6	
	lc	$\left\{\begin{array}{c} 30\\60\\90\end{array}\right.$	2.6 2.8 3.5	3.9 4.5 5.4	5.6 6.5 7.9	7.6 9.0 10.5	9.6 11.3 13.4	15.3 17.4 21.0	22.7 26.3 31.0	

#### APPENDIX B

# Table 47 .--- Sags for T. B. W. P. Solid Soft Copper Wire

HEAVY LOADING DISTRICT

[The sags being such that when loaded at 0° F, the wires will be stressed to 50 per cent of their ultimate strength for grades A and B and 60 per cent for grade C]

Size A. W. G.	Grade of construction	Tem- pera- ture	Sags (inches) for span lengths (feet) of-						
No.			100	125	150	175	200	250	
6	C	$\left\{ \begin{array}{c} {}^{\circ}F.\\ {}^{30}\\ {}^{60}\\ {}^{90} \end{array} \right.$	$29.1 \\ 31.4 \\ 33.6$	50. 2 52. 8 55. 2	76. 9 78. 9 81. 0				
4	∫A and B C	$     \begin{cases}             30 \\             60 \\             90 \\             30             \end{bmatrix}     $	$22.8 \\ 25.8 \\ 28.4 \\ 14.5$	$39.3 \\ 42.5 \\ 45.3 \\ 28.3$	$\begin{array}{c} 60.1 \\ 62.8 \\ 65.5 \\ 45.5 \end{array}$				
	(C	$ \begin{cases} 60 \\ 90 \end{cases} $	$     \begin{array}{r}       18.1 \\       21.6     \end{array} $	$32.0 \\ 35.0$	48.9     50.4				
2	{A and B C	$ \left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90 \end{array}\right\} $	12.416.119.77.210.114.0	$\begin{array}{c} 22.9\\ 27.3\\ 30.9\\ 14.2\\ 18.6\\ 23.1 \end{array}$	37.1 41.2 45.0 25.1 30.2 34.7	53.4 58.0 61.4 38.7 43.9 48.3	72.876.380.655.059.363.8		
1	{A and B C	$ \left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\\ 90 \end{array}\right. $	$9.6 \\ 12.6 \\ 17.0 \\ 6.0 \\ 8.0 \\ 11.7$	$17.9 \\ 22.5 \\ 26.2 \\ 10.9 \\ 14.7 \\ 19.2$	$28.8 \\ 33.6 \\ 37.8 \\ 18.4 \\ 23.8 \\ 28.4$	$\begin{array}{r} 43.3\\ 47.9\\ 52.3\\ 29.8\\ 34.9\\ 40.3 \end{array}$	$58.1 \\ 63.6 \\ 68.4 \\ 42.2 \\ 48.0 \\ 53.6$		
0	{A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$7.8 \\ 11.3 \\ 15.0 \\ 5.4 \\ 7.4 \\ 10.6$	$14.4 \\ 18.9 \\ 23.1 \\ 9.4 \\ 12.9 \\ 16.8$	$23. \ 6 \\ 28. \ 3 \\ 33. \ 1 \\ 15. \ 5 \\ 20. \ 2 \\ 25. \ 0$	$\begin{array}{c} 35.3 \\ 40.5 \\ 45.0 \\ 23.9 \\ 29.4 \\ 34.4 \end{array}$	$\begin{array}{r} 48.2 \\ 53.3 \\ 57.2 \\ 34.6 \\ 40.1 \\ 45.8 \end{array}$		
00	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 6.8\\ 9.6\\ 13.6\\ 4.8\\ 6.6\\ 9.5 \end{array}$	$12.0 \\ 16.2 \\ 20.5 \\ 8.3 \\ 11.2 \\ 15.3$	19. 124. 328. 813. 017. 522. 0	28.834.039.519.324.430.3	$\begin{array}{r} 39.8 \\ 45.6 \\ 51.4 \\ 27.6 \\ 33.3 \\ 40.1 \end{array}$		
0000	{A and B C	$     \begin{cases}             30 \\             60 \\             90 \\             30 \\             60 \\             90             90          $	5.8 8.2 11.3 4.4 5.9 8.5	$9.6 \\ 13.3 \\ 17.4 \\ 7.2 \\ 9.7 \\ 13.3$	$14.8 \\ 19.3 \\ 24.5 \\ 10.8 \\ 14.2 \\ 18.5$	21. 426. 732. 815. 520. 025. 2	$28.8 \\ 35.3 \\ 40.8 \\ 20.6 \\ 26.4 \\ 32.2$		

# Table 47.-Sags for T. B. W. P. Solid Soft Copper Wire-Continued

MEDIUM LOADING DISTRICTS

[The sags being such that when loaded at  $15^{\circ}$  F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B, and 60 per cent for grade C]

A. W. G. No.	Grade of construction	Tem- pera- ture	Sags (inches) for span lengths (feet) of-						
			100	125	150	175	200	250	
6	c	${ { 8 \\ { 60 \\ { 60 \\ { 90 } } } } } $	8.8 12.2 15.8	19. 7 23. 8 27. 7	33.838.242.1				
4	{A and B C	$     \begin{cases}             30 \\             60 \\             90 \\             30 \\             60             \end{bmatrix}     $	$\begin{array}{r} 8.3 \\ 11.9 \\ 15.5 \\ 5.5 \\ 7.6 \end{array}$	$ \begin{array}{r} 16.8\\ 21.0\\ 25.5\\ 10.0\\ 13.8 \end{array} $	28. 332. 637. 118. 022. 5	$\begin{array}{r} 42.2 \\ 47.1 \\ 51.0 \\ 28.4 \\ 34.1 \end{array}$			
		( 90 ( 30	10.6 6.0	18.0 10.5	27.9 16.9	38.7 26.9	37.2		
2	{A and B C	$ \begin{cases}     60 \\     90 \\     30 \\     60 \\     90 \end{cases} $	$ \begin{array}{r} 8.3\\ 11.7\\ 4.4\\ 6.0\\ 8.0 \end{array} $	$ \begin{array}{r} 10.0\\ 14.1\\ 18.4\\ 7.5\\ 10.0\\ 13.5 \end{array} $	$\begin{array}{c} 21.8\\ 26.8\\ 11.5\\ 15.3\\ 19.6 \end{array}$	$\begin{array}{c} 20.0\\ 31.7\\ 37.6\\ 17.6\\ 22.7\\ 27.7\end{array}$	$\begin{array}{c} 43.2 \\ 48.7 \\ 25.9 \\ 31.2 \\ 37.4 \end{array}$		
1	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	5.5 7.4 10.7 4.1 5.5 7.4	$9.3 \\ 12.7 \\ 16.8 \\ 6.9 \\ 8.9 \\ 11.8$	14. 418. 724. 110. 413. 317. 8	$\begin{array}{c} 21.8\\ 27.1\\ 33.2\\ 14.7\\ 19.1\\ 23.9 \end{array}$	$\begin{array}{c} 31.\ 2\\ 36.\ 7\\ 43.\ 0\\ 21.\ 6\\ 26.\ 8\\ 32.\ 6\end{array}$	53. 460. 666. 9 $38. 445. 052. 2$	
0	A and B	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right. $	$5.3 \\ 7.3 \\ 10.1 \\ 4.1 \\ 5.4 \\ 7.4$	$\begin{array}{c} 8.9\\ 11.7\\ 16.1\\ 6.6\\ 8.7\\ 11.7\end{array}$	$\begin{array}{c} 13.\ 3\\ 18.\ 0\\ 22.\ 5\\ 10.\ 1\\ 13.\ 0\\ 16.\ 9\end{array}$	$19. \ 3 \\ 23. \ 9 \\ 30. \ 0 \\ 14. \ 3 \\ 18. \ 3 \\ 23. \ 1$	$\begin{array}{c} 26.\ 6\\ 32.\ 4\\ 38.\ 6\\ 19.\ 7\\ 24.\ 5\\ 30.\ 3\end{array}$	$\begin{array}{c} 47.\ 4\\ 53.\ 7\\ 61.\ 0\\ 34.\ 2\\ 40.\ 5\\ 47.\ 7\end{array}$	
00	A and B	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right. $	$\begin{array}{c} 4.9\\ 6.7\\ 9.6\\ 3.8\\ 4.9\\ 6.8 \end{array}$	$\begin{array}{c} 8.1\\ 10.9\\ 14.7\\ 6.5\\ 8.3\\ 11.1 \end{array}$	12. 216. 020. 99. 412. 115. 8	17. 222. 027. 312. 816. 420. 8	$23.5 \\ 28.8 \\ 35.8 \\ 17.7 \\ 22.3 \\ 28.1$	$\begin{array}{c} 39.\ 6\\ 47.\ 4\\ 54.\ 0\\ 29.\ 7\\ 35.\ 4\\ 42.\ 6\end{array}$	
0000	A and B	$     \begin{cases}             30 \\             60 \\             90 \\             30 \\             60             \end{bmatrix}     $	$\begin{array}{c} 4.6 \\ 6.2 \\ 9.0 \\ 3.7 \\ 4.8 \end{array}$	7.410.013.6 $5.97.5$	$10.8 \\ 14.4 \\ 18.9 \\ 8.6 \\ 11.2$	15.3 19.3 25.0 12.2 15.1	$20.3 \\ 25.7 \\ 31.7 \\ 15.6 \\ 19.9$	33. 3 39. 9 47. 4 25. 8 31. 5	
		1 90	6.7	10.3	14.6	19.1	24.8	38.1	

#### APPENDIX B

# Table 47.-Sags for T. B. W. P. Solid Soft Copper Wire-Continued

LIGHT LOADING DISTRICT

[The sags being such that when loaded at 30° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B, and 60 per cent for grade C]

A. W. G. No.	Grade of construction	Tem- pera- ture	Sags (inches) for span lengths (feet) of-						
			100	125	150	175	200	250	
6	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 6.1 \\ 8.4 \\ 11.5 \\ 5.0 \\ 6.6 \\ 8.8 \end{array}$	11. 214. 818. 97. 810. 113. 3	$18.7 \\ 23.4 \\ 28.3 \\ 12.2 \\ 15.8 \\ 18.9$				
4	{A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	4, 8 6, 5 9, 1 4, 0 4, 9 6, 6	$\begin{array}{r} 8.4 \\ 11.1 \\ 14.7 \\ 6.2 \\ 7.9 \\ 10.5 \end{array}$	$12.8 \\ 16.6 \\ 21.2 \\ 9.4 \\ 11.9 \\ 15.5 \\$	19.724.129.813.817.622.0	28. 334. 140. 319. 223. 929. 7		
2	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{r} 4.\ 7\\ 6.\ 0\\ 8.\ 4\\ 3.\ 7\\ 4.\ 6\\ 6.\ 2\end{array}$	7.5 9.6 12.9 5.7 7.4 9.6	$10.8 \\ 14.2 \\ 18.4 \\ 8.5 \\ 10.4 \\ 13.7$	15.920.024.811.814.718.9	$\begin{array}{c} 22.1 \\ 26.8 \\ 32.6 \\ 16.6 \\ 20.3 \\ 25.0 \end{array}$	37. 2 43. 8 51. 0 27. 6 33. 3 39. 3	
1	{A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	4.3 5.6 7.8 3.4 4.3 5.9	$\begin{array}{c} 6.9\\ 9.1\\ 12.3\\ 5.5\\ 6.9\\ 9.1 \end{array}$	$10.3 \\ 13.0 \\ 17.3 \\ 7.9 \\ 10.1 \\ 13.1$	13. 8 18. 5 23. 1 11. 1 13. 8 17. 6	19. 2 23. 9 29. 7 15. 1 18. 2 23. 4	33. 0 39. 3 47. 1 25. 2 30. 3 36. 6	
0	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	4. 2 5. 8 7. 8 3. 7 4. 4 6. 0	6.8 8.9 12.0 5.5 7.1 9.1	$10.\ 1\\12.\ 8\\17.\ 1\\7.\ 9\\10.\ 1\\13.\ 0$	14. 3 17. 4 22. 3 11. 1 13. 6 17. 4	18.723.729.114.918.523.0	31.837.243.524.330.036.0	
00	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	4.1 5.3 7.6 3.2 4.2 5.6	$\begin{array}{c} 6.3\\ 8.7\\ 11.7\\ 5.4\\ 6.6\\ 8.9 \end{array}$	9.7 12.2 16.0 7.9 9.7 12.6	$13.0 \\ 16.4 \\ 21.4 \\ 10.9 \\ 13.4 \\ 17.0$	17.521.827.614.417.521.8	29. 4 34. 8 42. 0 22. 8 27. 6 33. 9	
0000	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3.8 5.2 7.2 3.1 4.1 5.5	6.0 8.1 10.8 5.1 6.3 8.4	9.0 11.7 15.5 7.7 9.4 12.1	12. 415. 520. 210. 312. 616. 2	$16. \ 3 \\ 20. \ 6 \\ 25. \ 9 \\ 13. \ 7 \\ 16. \ 8 \\ 20. \ 9 \\$	25. 8 31. 8 38. 4 21. 0 25. 8 31. 5	

222

#### MINIMUM SAGS FOR STEEL

### Table 48.—Sags for Ordinary Grade Steel Wire

#### HEAVY LOADING DISTRICT

[At 30, 60, and 90° F. without load, the sags being such that when loaded at 0° F. the wire will be stressed to 50 per cent of ultimate strength for grades A and B and to 60 per cent for grade C]

Steel	Grade of con-	Tem-		Sags (in inches) for span lengths (in feet) of										
wire gage No.	struction	pera- ture	100	125	150	175	. 200	250	300	400	500			
8	C {A and B C	$ \begin{array}{c} \circ F. \\ 30 \\ 60 \\ 90 \\ \\ 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array} $	4.1 6.2 11.1 4.7 7.4 11.0 2.5 3.6 5.3	12.5 16.5 20.0 12.0 16.0 20.0 5.4 7.7 11.2	26. 0 30. 0 33. 5 24. 5 28. 5 32. 0 11. 2 15. 5 20. 5	22. 0 27. 0 31. 5	35. 0 40. 5 45. 0	65. 0 70. 0 75. 0	104 109 113	213 216 220	341 344 348			
4	{A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 3.1\\ 4.7\\ 7.4\\ 2.2\\ 2.8\\ 4.0 \end{array}$	6.6 9.8 14.0 3.7 5.1 7.2	$13.0 \\ 17.5 \\ 22.0 \\ 6.3 \\ 9.2 \\ 12.5$	$\begin{array}{c} 22.\ 0\\ 27.\ 5\\ 32.\ 5\\ 11.\ 1\\ 15.\ 5\\ 20.\ 5\end{array}$	34. 5 40. 0 44. 0 18. 0 24. 0 29. 5	$\begin{array}{c} 64.\ 0\\ 69.\ 0\\ 73.\ 0\\ 41.\ 0\\ 47.\ 5\\ 53.\ 0\end{array}$	99 104 108 71 77 82	189 193 197 147 152 158	309 314 318 245 250 256			

#### MEDIUM LOADING DISTRICT

[At 30, 60, and  $90^{\circ}$  F. without load, the sags being such that when loaded at  $15^{\circ}$  F. the wire will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

8	C	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	1.9 2.4 3.1	3.1 4.1 5.5	5. 2 6. 8 9. 7						
6	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	2.22.94.31.72.02.6	3.9 5.3 7.5 2.7 3.5 4.5	$\begin{array}{r} 6.3\\ 8.6\\ 12.0\\ 4.3\\ 5.4\\ 7.2 \end{array}$	6.3 8.2 11.1	9.4 12.0 16.0	$     18.5 \\     23.5 \\     30.5     $	34. 5 42. 0 49. 5	85 93 101	161 169 177
4	{A and B	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	2.0 2.6 3.8 1.7 2.0 2.5	3.4 4.5 6.3 2.7 3.3 4.2	5.47.09.94.04.96.3	$7.8 \\ 10.7 \\ 14.5 \\ 5.7 \\ 6.9 \\ 9.2$	11. 315. 020. 07. 79. 612. 5	$\begin{array}{c} 22.\ 0\\ 28.\ 0\\ 34.\ 5\\ 14.\ 0\\ 17.\ 5\\ 23.\ 0 \end{array}$	$\begin{array}{c} 38.5\\ 46.0\\ 53.0\\ 23.5\\ 29.0\\ 36.0 \end{array}$	88 96 104 58 67 76	$150 \\ 158 \\ 166 \\ 107 \\ 117 \\ 127$

# Table 48 .--- Sags for Ordinary Grade Steel Wire--Continued

LIGHT LOADING DISTRICT

[At 30, 60, and 90° F. without load, the sags being such that when loaded at 30° F. the wire will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C.]

Steel	Grade of con-	Tem-												
wire gage No.	struction	pera- ture-	100	125	150	175	200	250	300	400	500			
8	с	${\circ \ F.} \\ {30 \\ 60 \\ 90}$	$1.4 \\ 1.7 \\ 2.2$	2.2 2.8 3.3	3.2 4.0 4.9									
6	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1.8 \\ 2.3 \\ 2.8 \\ 1.4 \\ 1.7 \\ 2.2$	$2.7 \\ 3.5 \\ 4.4 \\ 2.2 \\ 2.7 \\ 3.3 $	$\begin{array}{c} 3.9\\ 5.0\\ 6.3\\ 3.2\\ 4.0\\ 4.7\end{array}$	4.6 5.5 6.5	5.8 7.2 8.9	$     \begin{array}{c}             9.6 \\             11.7 \\             14.0         \end{array}     $	14.5 17 21	27.5 32.0 39.0	48 55 64			
4	A and B	$\left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right.$	$1.7 \\ 2.2 \\ 2.8 \\ 1.4 \\ 1.7 \\ 2.1$	$2.7 \\ 3.5 \\ 4.5 \\ 2.3 \\ 2.7 \\ 3.3 $	$\begin{array}{c} 4.0\\ 4.9\\ 6.3\\ 3.3\\ 4.0\\ 4.7 \end{array}$	5.5 6.7 8.8 4.6 5.5 6.5	$7.2 \\ 9.1 \\ 11.5 \\ 6.0 \\ 7.2 \\ 8.6$	$11.7 \\ 14.5 \\ 18.5 \\ 9.3 \\ 11.4 \\ 14.0$	17.521.526.513.51720	$\begin{array}{c} 33.\ 5\\ 40.\ 5\\ 48.\ 0\\ 26.\ 0\\ 30.\ 5\\ 37.\ 0\end{array}$	$54 \\ 67 \\ 77 \\ 43 \\ 50 \\ 59$			

#### Table 49 .- Sags for Siemens-Martin Steel Wire

HEAVY LOADING DISTRICT

[At 30, 60, and 90° F, without load, the sags being such that when loaded at 0° F, the wire will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

Steel wire	Grade of con-	Tem-												
gage No.	struction	pera- ature	200	250	300	400	500	600	700	1,000				
6	с	$ \begin{array}{c} \circ \ F. \\ \{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right. $	$13.5 \\ 18.5 \\ 23.5$	35.5 42.5 48.5	67. 0 73. 0 79. 0	147 152 158	$251 \\ 256 \\ 261$	379 384 389	528 533 538					
4	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$15.0 \\ 20.5 \\ 26.0 \\ 8.2 \\ 10.6 \\ 14.0$	$\begin{array}{r} 37.\ 0\\ 43.\ 5\\ 50.\ 0\\ 17.\ 5\\ 22.\ 5\\ 29.\ 0\end{array}$	$\begin{array}{c} 65.\ 0\\ 72.\ 0\\ 78.\ 0\\ 36.\ 0\\ 43.\ 0\\ 51.\ 0\end{array}$	$136 \\ 143 \\ 148 \\ 94 \\ 102 \\ 110$	$231 \\ 237 \\ 242 \\ 172 \\ 179 \\ 188$	$357 \\ 362 \\ 367 \\ 268 \\ 276 \\ 282$	487 492 382 388 395	815 822 830				

## Table 49.-Sags for Siemens-Martin Steel Wire-Continued

#### MEDIUM LOADING DISTRICT

[At 30, 60, and 90° F. without load, the sags being such that when loaded at 15° F. the wire will be stressed to 50 per cent of ultimate strength for grades A and B and to 60 per cent for grade C]

Steel	Grade of con-	Tem- pera-	Sags (in inches) for span lengths (in feet) of-											
gage No.	struction	âture	200	250	300	400	500	600	700	1,000				
6	с	$ \begin{array}{c} \circ F, \\ 30 \\ 60 \\ 90 \end{array} $	5.5 7.0 8.7	$10.5 \\ 12.5 \\ 16.0$	17.5 21.5 27.0	$\begin{array}{c} 48\\54\\63\end{array}$	100 109 119	161 171 181	$242 \\ 251 \\ 262$	559 564 578				
4	{A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$7.2 \\ 9.1 \\ 11.5 \\ 5.3 \\ 6.3 \\ 7.7$	$12.5 \\ 16.0 \\ 20.0 \\ 9.0 \\ 11.1 \\ 13.0 $	$\begin{array}{c} 21.\ 0\\ 26.\ 5\\ 33.\ 0\\ 14.\ 0\\ 17.\ 0\\ 20.\ 0 \end{array}$	$52 \\ 60 \\ 70 \\ 31 \\ 37 \\ 45$	$98\\109\\118\\61\\71\\82$	$162 \\ 171 \\ 182 \\ 109 \\ 120 \\ 131$	235 246 255 168 182 193	$534 \\ 545 \\ 555 \\ 408 \\ 420 \\ 432$				

#### LIGHT LOADING DISTRICT

[At 30, 60, and 90° F. without load, the sags being such that when loaded at 30° F. the wire will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

6	σ	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	$4.8 \\ 5.3 \\ 6.2$	$7.5 \\ 8.4 \\ 10.2$	$10.8 \\ 12.5 \\ 15.0$	20.0 23.0 27.0	$33.0 \\ 38.0 \\ 44.0$	50 58 66	73 83 94	$178 \\ 196 \\ 212$
4	{A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	5.5 6.7 8.2 4.8 5.3 6.2	$\begin{array}{r} 8.7 \\ 10.8 \\ 13.0 \\ 7.2 \\ 8.4 \\ 9.9 \end{array}$	$\begin{array}{c} 13.\ 0\\ 15.\ 5\\ 18.\ 5\\ 10.\ 4\\ 12.\ 0\\ 14.\ 5\end{array}$	$\begin{array}{c} 24.5\\ 29.0\\ 34.5\\ 18.5\\ 22.0\\ 26.0 \end{array}$	$\begin{array}{r} 40.\ 0\\ 47.\ 5\\ 55.\ 0\\ 32.\ 0\\ 36.\ 5\\ 42.\ 0\end{array}$		$90 \\ 103 \\ 116 \\ 69 \\ 77 \\ 86$	$212 \\ 229 \\ 245 \\ 158 \\ 174 \\ 192$

## Table 50 .- Sags for High-Tension Steel Wire

#### HEAVY LOADING DISTRICT

[At 30, 60, and 90° F. without load, the sags being such that when loaded at 0° F. the wire will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

Steel wire	Grade of con-	Tem-	Sags (in inches) for span lengths (in feet) of-										
gage No.	struction	pera- ture	200	250	300	400	500	600	700	1,000			
6	c	$ \begin{cases} {}^{\circ} F. \\ {}^{30} \\ {}^{60} \\ {}^{90} \end{cases} $	3.6 4.0 4.3	6.0 6.8 7.5	9.7 11.2 12.5	25. 0 30. 0 34. 5	66. 0 75. 0 87. 0	$130 \\ 143 \\ 154$	218 231 244	595 602 610			
4	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{r} 4.1\\ 4.7\\ 5.3\\ 3.4\\ 3.7\\ 4.1 \end{array}$	7.28.29.3 $5.25.86.4$	11.5 13.5 16.0 7.9 8.8 <b>9.7</b>	$\begin{array}{c} 29.5 \\ 34.5 \\ 42.0 \\ 16.5 \\ 19.0 \\ 21.5 \end{array}$	71. 082. 092. 034. 039. 545. 5	$135 \\ 147 \\ 159 \\ 68 \\ 79 \\ 89$	$215 \\ 225 \\ 237 \\ 126 \\ 140 \\ 154$	537 547 556 394 405 419			

#### MEDIUM LOADING DISTRICT

[At 30, 60, and 90° F. without load, the sags being such that when loaded at  $15^{\circ}$  F. the wire will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

6	C	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	3.1 3.4 3.7	4.6 5.2 5.8	6.8 7.5 8.3	12.5 14.0 16.0	23.0 25.0 27.5	36. 0 41. 0 47. 0	60 67 77	$202 \\ 216 \\ 234$
4	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3.8 4.2 4.6 3.1 3.3 3.6	5.7 6.4 7.2 4.8 5.2 5.7	$\begin{array}{r} 8.3\\ 9.4\\ 10.5\\ 6.8\\ 7.5\\ 8.3 \end{array}$	$15.5 \\ 18.0 \\ 20.5 \\ 12.0 \\ 13.0 \\ 14.5$	$\begin{array}{c} 27.\ 5\\ 32.\ 0\\ 36.\ 0\\ 20.\ 0\\ 21.\ 5\\ 24.\ 0\end{array}$	$\begin{array}{c} 45.\ 5\\ 52.\ 0\\ 59.\ 0\\ 31.\ 0\\ 33.\ 0\\ 37.\ 5\end{array}$	$71\\82\\92\\46\\51\\57$	$216 \\ 233 \\ 248 \\ 132 \\ 146 \\ 162$

#### LIGHT LOADING DISTRICT

[At 30, 60, and 90° F, without load, the sags being such that when loaded at 30° F, the wire will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

6	C	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	2.9 3.3 3.6	4.5 4.9 5.3	6.5 6.8 7.5	11. 1 12. 0 13. 0	18.0 19.0 20.5	26. 0 27. 5 29. 5	35.5 38.5 42.0	75 81 90
4	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3.6 3.9 4.3 2.9 3.1 3.4	5.76.16.64.24.85.4	$7.9 \\ 8.6 \\ 9.4 \\ 6.1 \\ 6.8 \\ 7.6 $	$13.5 \\ 14.5 \\ 16.0 \\ 10.6 \\ 11.8 \\ 13.0$	$\begin{array}{c} 20.5 \\ 22.5 \\ 24.5 \\ 17.0 \\ 18.5 \\ 20.5 \end{array}$	29.5 33.0 37.5 25.0 27.5 30.5	$\begin{array}{c} 41.\ 5\\ 46.\ 0\\ 52.\ 0\\ 34.\ 5\\ 38.\ 0\\ 41.\ 0\end{array}$	$95 \\ 104 \\ 114 \\ 74 \\ 80 \\ 86$

### MINIMUM SAGS FOR STEEL

## Table 51.—Sags for Ordinary Grade Steel Cable

## HEAVY LOADING DISTRICT

[At 30, 60, and 90° F. without load, the sags being such that when loaded at 0° F. the cable will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

Cable diam-	Grade of con-	Tem-		Sags	(in inc	hes) fo	r span	length	s (in fee	et) of—	
eter (inches)	struction	pera- ture	100	125	150	175	200	250	300	400	500
¼	{A and B C		3.8 5.4 7.8 2.3 2.0 3.8	8.9 12.5 16.0 4.5 5.9 7.8	19.0 23.0 27.0 8.5 11.4 15.0	32. 5 36. 5 40. 5 16. 0 20. 5 25. 0	48. 0 52. 0 56. 0 28. 0 33. 0 38. 0	86. 0 90. 0 93. 0 58. 0 63. 0 68. 0	131 135 138 97. 0 102 106	250 254 257 195 200 205	406 409 413 323 328 332
5 16	{A and B {C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	2.6 3.6 4.7 1.9 2.3 2.9	4.8 6.3 8.4 3.3 4.1 5.2	$7.9 \\10.8 \\14.0 \\5.2 \\6.3 \\8.1$	13.0 17.0 21.0 7.8 9.9 12.5	$\begin{array}{c} 20.\ 5\\ 25.\ 5\\ 31.\ 0\\ 11.\ 5\\ 14.\ 5\\ 18.\ 0 \end{array}$	$\begin{array}{r} 43.\ 0\\ 48.\ 5\\ 54.\ 0\\ 24.\ 0\\ 29.\ 0\\ 35.\ 0\end{array}$	$\begin{array}{c} 72.\ 0\\ 78.\ 0\\ 83.\ 0\\ 44.\ 0\\ 51.\ 0\\ 58.\ 0\end{array}$	$147 \\ 151 \\ 157 \\ 105 \\ 112 \\ 118$	$241 \\ 247 \\ 252 \\ 185 \\ 191 \\ 199$
3/8	{ <sup>A</sup> and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	2.4 3.1 4.3 1.9 2.3 2.8	4.2 5.4 7.0 3.1 3.7 4.6	$\begin{array}{c} 6.7\\ 8.6\\ 11.2\\ 4.7\\ 5.6\\ 7.0 \end{array}$	10. 1 13. 0 16. 5 6. 7 8. 2 10. 3	$14.5 \\18.5 \\23.0 \\9.6 \\11.8 \\14.5$	$\begin{array}{c} 29.\ 0\\ 35.\ 0\\ 40.\ 5\\ 17.\ 5\\ 21.\ 5\\ 26.\ 5\end{array}$	$\begin{array}{r} 49.5\\ 56.0\\ 63.0\\ 30.0\\ 36.0\\ 42.0 \end{array}$	107 114 121 73. 0 81. 0 89. 0	183 190 197 134 142 151
7 16	{A and B {C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	2.3 2.9 3.8 1.9 2.2 2.6	3.9 5.0 6.3 3.0 3.5 4.4	5.8 7.4 9.7 4.3 5.2 6.5	8.4 10.7 13.5 6.3 7.4 9.0	11.514.518.58.610.112.0	$\begin{array}{c} 21.\ 0\\ 25.\ 5\\ 31.\ 0\\ 14.\ 5\\ 17.\ 0\\ 21.\ 0 \end{array}$	34. 0 40. 5 47. 5 22. 5 27. 0 32. 5	$\begin{array}{c} 75.\ 0\\ 83.\ 0\\ 91.\ 0\\ 50.\ 0\\ 57.\ 0\\ 66.\ 0\end{array}$	$131 \\ 139 \\ 148 \\ 92 \\ 102 \\ 112$
<sup>1</sup> ⁄2	{A and B {C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	2.3 2.9 3.8 1.9 2.2 2.5	3.7 4.8 6.1 3.0 3.5 4.2	5.6 7.0 9.2 4.3 5.2 6.3	8.0 10.1 13.0 6.1 7.1 8.8	11. 0 13. 5 17. 5 8. 2 9. 8 12. 0	19.023.528.513.516.019.5	$\begin{array}{c} 30.\ 0\\ 36.\ 5\\ 43.\ 0\\ 21.\ 0\\ 25.\ 0\\ 30.\ 0 \end{array}$	66. 0 74. 0 83. 0 44. 0 51. 0 59. 0	$116 \\ 125 \\ 135 \\ 80 \\ 91 \\ 100$
9 16	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	2.3 2.8 3.7 1.9 2.2 2.6	3.6 4.7 6.0 3.0 3.5 4.2	5.4 6.7 8.6 4.3 5.0 6.1	7.6 9.5 12.0 5.9 6.9 8.4	10.3 12.5 16.0 7.7 9.4 11.0	$\begin{array}{c} 17.\ 0\\ 21.\ 0\\ 26.\ 0\\ 12.\ 5\\ 15.\ 0\\ 18.\ 5\end{array}$	$\begin{array}{c} 26.\ 5\\ 31.\ 5\\ 37.\ 5\\ 19.\ 5\\ 23.\ 0\\ 27.\ 5\end{array}$	54.062.070.038.544.551.0	$94 \\ 104 \\ 113 \\ 66 \\ 75 \\ 85$
5/8	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\\ 90\end{array}\right.$	2.2 2.8 3.7 1.9 2.2 2.5	3.6 4.5 5.8 3.0 3.4 4.2	5.46.58.64.34.96.1	$7.69.311.85.96.7\cdot 8.4$	$10.1 \\ 12.0 \\ 15.5 \\ 7.7 \\ 9.1 \\ 11.0$	$\begin{array}{c} 16.\ 0\\ 20.\ 0\\ 24.\ 5\\ 12.\ 5\\ 14.\ 5\\ 17.\ 5\end{array}$	$\begin{array}{c} 25.\ 0\\ 29.\ 5\\ 35.\ 5\\ 18.\ 5\\ 22.\ 0\\ 26.\ 0 \end{array}$	$\begin{array}{r} 49.\ 0\\ 57.\ 0\\ 65.\ 0\\ 35.\ 5\\ 41.\ 5\\ 48.\ 0\end{array}$	85 94 103 61 69 78

# Table 51.-Sags for Ordinary Grade Steel Cable-Continued

#### MEDIUM LOADING DISTRICT

[At 30, 60, and  $90^{\circ}$  F. without load, the sags being such that when loaded at  $15^{\circ}$  F. the cable will be stressed to 50 per cent of ultimate strength for grades A and B and to 60 per cent for grade C]

Cable diam-	Grade of con-	Tem-		Sags	(in inc	hes) fo	r span	length	s (in fee	et) of—	
eter (inches)	struction	pera- ture	100	125	. 150	175	200	250	300	400	500
14	{A and B {C	$ \begin{cases} {}^{\circ}F. \\ {}^{\circ}60 \\ {}^{90} \\ {}^{30} \\ {}^{60} \\ {}^{90} \end{cases} $	$2.3 \\ 2.9 \\ 3.8 \\ 1.9 \\ 2.2 \\ 2.5 $	3.9 5.1 6.4 3.0 3.5 4.4	$\begin{array}{c} 6.1 \\ 7.9 \\ 10.4 \\ 4.5 \\ 5.4 \\ 6.5 \end{array}$	9.9 13.0 16.0 6.5 8.0 9.9	14.518.523.59.411.014.0	$\begin{array}{c} 39.5\\ 36.0\\ 42.5\\ 17.5\\ 21.5\\ 26.5 \end{array}$	55. 0 62. 0 68. 0 31. 5 37. 5 44. 5	117. 0 124. 0 130. 0 81. 0 88. 0 97. 0	201. 0 208. 0 214. 0 151. 0 160. 0 167. 0
, 16	{A and B {C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$\begin{array}{c} 2.\ 2\\ 2.\ 6\\ 3.\ 2\\ 1.\ 9\\ 2.\ 0\\ 2.\ 3 \end{array}$	$\begin{array}{c} 3.5 \\ 4.2 \\ 5.4 \\ 2.8 \\ 3.3 \\ 3.9 \end{array}$	$5.2 \\ 6.5 \\ 8.1 \\ 4.1 \\ 4.5 \\ 5.8$	$7.6 \\ 9.2 \\ 11.6 \\ 5.7 \\ 6.7 \\ 8.0$	10.3 12.5 16.0 7.7 9.1 10.8	18.522.527.513.015.518.5	$\begin{array}{c} 29.5 \\ 35.5 \\ 41.5 \\ 20.0 \\ 24.0 \\ 28.5 \end{array}$	$\begin{array}{c} 66.\ 0\\ 75.\ 0\\ 83.\ 0\\ 43.\ 5\\ 51.\ 0\\ 58.\ 0\end{array}$	120.0 130.0 138.0 82.0 91.0 101.0
3⁄s	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 2.0\\ 2.5\\ 3.2\\ 1.8\\ 2.0\\ 2.3 \end{array}$	$\begin{array}{c} \textbf{3.3} \\ \textbf{4.2} \\ \textbf{5.3} \\ \textbf{2.8} \\ \textbf{3.2} \\ \textbf{3.6} \end{array}$	$\begin{array}{r} 4.9\\ 6.1\\ 7.7\\ 4.1\\ 4.7\\ 5.6 \end{array}$	$\begin{array}{c} 6.9\\ 8.6\\ 10.9\\ 5.7\\ 6.5\\ 7.6\end{array}$	$9.3 \\ 11.5 \\ 14.0 \\ 7.4 \\ 8.6 \\ 10.3$	$15.5 \\ 19.0 \\ 24.0 \\ 12.0 \\ 14.0 \\ 16.5$	$\begin{array}{c} 25.\ 0\\ 30.\ 0\\ 35.\ 5\\ 18.\ 0\\ 21.\ 5\\ 25.\ 0\end{array}$	52.060.068.036.542.049.0	$\begin{array}{c} 94.\ 0\\ 103.\ 0\\ 113.\ 0\\ 65.\ 0\\ 73.\ 0\\ 83.\ 0\end{array}$
75	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 2.\ 0\\ 2.\ 5\\ 3.\ 2\\ 1.\ 8\\ 2.\ 0\\ 2.\ 3 \end{array}$	$\begin{array}{c} 3.\ 3\\ 4.\ 0\\ 5.\ 1\\ 2.\ 8\\ 3.\ 2\\ 3.\ 8\end{array}$	$\begin{array}{r} 4.7 \\ 5.8 \\ 7.4 \\ 4.0 \\ 4.5 \\ 5.4 \end{array}$	$\begin{array}{c} 6.7\\ 8.2\\ 10.3\\ 5.5\\ 6.3\\ 7.6 \end{array}$	$\begin{array}{r} 8.9 \\ 10.8 \\ 13.5 \\ 7.2 \\ 8.4 \\ 9.8 \end{array}$	14.517.521.511.413.015.5	$\begin{array}{c} 22 & 0 \\ 26 & 5 \\ 31 & 5 \\ 16 & 5 \\ 20 & 0 \\ 23 & 0 \end{array}$	$\begin{array}{r} 43.\ 0\\ 50.\ 0\\ 57.\ 0\\ 31.\ 5\\ 37.\ 5\\ 43.\ 0\end{array}$	74. 0 84. 0 93. 0 55. 0 62. 0 70. 0
1⁄2	{A and B {C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\\ 90\end{array}\right.$	$\begin{array}{c} 2.0\\ 2.5\\ 3.2\\ 1.8\\ 2.0\\ 2.3 \end{array}$	$\begin{array}{c} 3.\ 3\\ 4.\ 1\\ 5.\ 1\\ 2.\ 7\\ 3.\ 1\\ 3.\ 7\end{array}$	$\begin{array}{r} 4.9 \\ 5.8 \\ 7.4 \\ 4.0 \\ 4.5 \\ 5.4 \end{array}$	$\begin{array}{c} 6.7\\ 8.0\\ 10.1\\ 5.4\\ 6.3\\ 7.3 \end{array}$	$\begin{array}{c} 8.9\\ 10.6\\ 13.0\\ 7.2\\ 8.4\\ 9.8 \end{array}$	14. 0 17. 0 21. 0 11. 4 13. 0 15. 5	$\begin{array}{c} 21.\ 5\\ 25.\ 5\\ 30.\ 0\\ 16.\ 5\\ 19.\ 0\\ 22.\ 5\end{array}$	$\begin{array}{c} 41.\ 0\\ 47.\ 5\\ 55.\ 0\\ 31.\ 0\\ 36.\ 0\\ 42.\ 0\end{array}$	69.0 79.0 88.0 52.0 59.0 67.0
9	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 2.\ 0\\ 2.\ 4\\ 3.\ 1\\ 1.\ 8\\ 2.\ 0\\ 2.\ 3\end{array}$	3.3 3.9 4.9 2.7 3.0 3.6	$\begin{array}{r} 4.7\\ 5.8\\ 7.2\\ 4.0\\ 4.5\\ 5.4\end{array}$	6.5 8.0 9.9 5.5 6.3 7.3	$\begin{array}{r} 8.6 \\ 10.6 \\ 12.5 \\ 7.2 \\ 8.2 \\ 9.6 \end{array}$	14. 0 16. 0 20. 0 11. 1 12. 5 15. 0	$\begin{array}{c} 20.\ 5\\ 24.\ 0\\ 29.\ 0\\ 16.\ 0\\ 18.\ 5\\ 22.\ 0 \end{array}$	$\begin{array}{c} 39.\ 0\\ 44.\ 5\\ 52.\ 0\\ 30.\ 0\\ 34.\ 0\\ 40.\ 5\end{array}$	$\begin{array}{c} 63.\ 0\\ 71.\ 0\\ 81.\ 0\\ 48.\ 5\\ 55.\ 0\\ 62.\ 0\end{array}$
5⁄8	A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 2.0\\ 2.4\\ 3.1\\ 1.8\\ 2.0\\ 2.3 \end{array}$	$\begin{array}{c} 3.3\\ 3.9\\ 5.1\\ 2.7\\ 3.2\\ 3.8 \end{array}$	4.7 5.6 7.2 4.0 4.5 5.4	$\begin{array}{c} 6.5 \\ 7.8 \\ 9.7 \\ 5.4 \\ 6.1 \\ 7.4 \end{array}$	8.6 10.3 12.5 7.0 7.9 9.6	$\begin{array}{c} 13.\ 5\\ 16.\ 0\\ 19.\ 5\\ 10.\ 8\\ 12.\ 5\\ 14.\ 5\end{array}$	$\begin{array}{c} 20.\ 0\\ 23.\ 5\\ 28.\ 0\\ 16.\ 0\\ 18.\ 5\\ 21.\ 5\end{array}$	$\begin{array}{c} 37.\ 0\\ 42.\ 5\\ 50.\ 0\\ 29.\ 0\\ 33.\ 0\\ 39.\ 0 \end{array}$	$\begin{array}{c} 60.\ 0\\ 69.\ 0\\ 78.\ 0\\ 47.\ 5\\ 54.\ 0\\ 61.\ 0\end{array}$

# Table 51.-Sags for Ordinary Grade Steel Cable-Continued

### LIGHT LOADING DISTRICT

[At 30, 60, and 90° F, without load, the sags being such that when loaded at 30° F, the cable will be stressed to 50 per cent of ultimate strength for grades A and B and to 60 per cent for grade C]

Cable diam-	Grade of con-	Tem-		Sags (	in incł	nes) for	r span	length	s (in fea	et) of	
eter (inches)	struction	pera- ature	100	125	150	175	200	250	300	400	500
¥	A and B	$ \begin{cases} {}^{\circ}F. \\ {}^{30} \\ {}^{60} \\ {}^{90} \\ {}^{30} \\ {}^{60} \\ {}^{90} \end{cases} $	1.92.32.81.81.92.0	3.0 3.6 4.6 2.7 3.0 3.3	$\begin{array}{c} 4.5\\ 5.4\\ 6.5\\ 3.8\\ 4.5\\ 5.0 \end{array}$	$\begin{array}{c} 6.3 \\ 7.6 \\ 9.0 \\ 5.2 \\ 6.1 \\ 6.9 \end{array}$	$\begin{array}{c} 8.5\\ 10.2\\ 12.0\\ 6.7\\ 7.9\\ 9.4 \end{array}$	$14.0 \\ 16.5 \\ 19.5 \\ 10.8 \\ 12.5 \\ 14.5$	21. 025. 029. 516. 018. 521. 5	$\begin{array}{c} 41.\ 5\\ 48.\ 5\\ 56.\ 0\\ 31.\ 7\\ 36.\ 0\\ 41.\ 7\end{array}$	74. 0 84. 0 94. 0 54. 0 61. 0 70. 0
16	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$1.9 \\ 2.2 \\ 2.6 \\ 1.7 \\ 1.8 \\ 2.0$	3.0 3.6 4.3 2.7 3.0 3.3	$\begin{array}{c} 4.5\\ 5.4\\ 6.5\\ 3.8\\ 4.3\\ 4.9 \end{array}$	$\begin{array}{c} 6.1 \\ 7.3 \\ 8.8 \\ 5.0 \\ 5.9 \\ 6.7 \end{array}$	$\begin{array}{r} 8.1\\ 9.6\\ 11.3\\ 6.7\\ 7.7\\ 8.9 \end{array}$	$12.5 \\ 15.0 \\ 18.5 \\ 10.2 \\ 12.0 \\ 14.0$	18.522.526.515.017.520.0	$\begin{array}{c} 36.\ 0\\ 42.\ 0\\ 48.\ 5\\ 28.\ 5\\ 32.\ 0\\ 37.\ 0 \end{array}$	$\begin{array}{c} 60.\ 0\\ 68.\ 0\\ 77.\ 0\\ 47.\ 0\\ 53.\ 0\\ 60.\ 0\end{array}$
3⁄8	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 1.9\\ 2.3\\ 2.8\\ 1.7\\ 1.9\\ 2.2 \end{array}$	$\begin{array}{c} 3.\ 0\\ 3.\ 6\\ 4.\ 3\\ 2.\ 7\\ 3.\ 0\\ 3.\ 4 \end{array}$	$\begin{array}{r} 4.3\\ 5.2\\ 6.3\\ 3.8\\ 4.3\\ 4.9 \end{array}$	5.9 7.1 8.6 5.0 5.7 6.7	$7.9 \\ 9.4 \\ 11.3 \\ 6.6 \\ 7.4 \\ 8.6$	$12.5 \\ 15.0 \\ 17.5 \\ 10.5 \\ 11.7 \\ 13.5$	$\begin{array}{c} 18.5\\ 22.0\\ 26.0\\ 15.0\\ 17.5\\ 20.0 \end{array}$	$\begin{array}{c} 34.5 \\ 40.5 \\ 46.5 \\ 27.5 \\ 31.0 \\ 36.0 \end{array}$	57. 0 65. 0 73. 0 45. 0 51. 0 58. 0
7. 16	{A and B C	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array} \right.$	$\begin{array}{c} 1.9\\ 2.2\\ 2.6\\ 1.7\\ 1.9\\ 2.2 \end{array}$	3.0 3.5 4.3 2.7 3.0 3.3	$\begin{array}{c} 4.\ 3\\ 5.\ 0\\ 6.\ 2\\ 3.\ 8\\ 4.\ 3\\ 4.\ 9\end{array}$	5.9 7.1 8.6 5.0 5.7 6.7	$7.7 \\ 9.4 \\ 11.3 \\ 6.5 \\ 7.4 \\ 8.7$	$12.5 \\ 14.5 \\ 17.5 \\ 10.2 \\ 11.4 \\ 13.5$	$\begin{array}{c} 18.\ 0\\ 21.\ 0\\ 25.\ 0\\ 15.\ 0\\ 16.\ 5\\ 19.\ 5\end{array}$	$\begin{array}{c} 33.\ 0\\ 38.\ 5\\ 44.\ 5\\ 27.\ 0\\ 30.\ 0\\ 34.\ 5\end{array}$	53.0 61.0 68.0 43.0 48.5 55.0
1⁄2	{A and B C	$\left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \\ 90 \end{array}\right.$	$ \begin{array}{c} 1.8\\ 2.2\\ 2.6\\ 1.8\\ 1.9\\ 2.0 \end{array} $	3.0 3.6 4.3 2.7 3.0 3.3	$\begin{array}{c} 4.\ 3\\ 5.\ 2\\ 6.\ 1\\ 3.\ 8\\ 4.\ 3\\ 4.\ 9\end{array}$	$5.9 \\ 7.1 \\ 8.6 \\ 5.0 \\ 5.7 \\ 6.7$	7.79.111.0 $6.57.48.9$	$\begin{array}{c} 12.5\\ 14.5\\ 17.0\\ 10.2\\ 11.7\\ 13.5 \end{array}$	$\begin{array}{c} 18.0\\ 21.0\\ 25.0\\ 15.0\\ 16.5\\ 19.5 \end{array}$	$\begin{array}{c} 32.5\\ 38.5\\ 44.0\\ 27.0\\ 30.0\\ 34.5 \end{array}$	53.0 60.0 68.0 42.5 48.0 55.0
9 16	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1.9 2.2 2.6 1.8 1.9 2.0	$\begin{array}{c} 3.\ 0\\ 3.\ 5\\ 4.\ 4\\ 2.\ 7\\ 3.\ 0\\ 3.\ 3\end{array}$	$\begin{array}{r} 4.\ 3\\ 5.\ 0\\ 6.\ 1\\ 3.\ 8\\ 4.\ 2\\ 4.\ 8\end{array}$	5.96.98.4 $5.05.76.5$	7.79.111.0 $6.57.58.6$	$\begin{array}{c} 12.0\\ 14.0\\ 17.0\\ 10.2\\ 11.4\\ 13.0 \end{array}$	17.521.024.515.016.519.0	$\begin{array}{c} 31.\ 5\\ 37.\ 5\\ 43.\ 0\\ 26.\ 0\\ 30.\ 0\\ 34.\ 0\end{array}$	52.0 58.0 66.0 42.0 47.0 53.0
<sup>5</sup> ⁄8	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 1.9\\ 2.2\\ 2.6\\ 1.7\\ 1.9\\ 2.2 \end{array}$	3.0 3.5 4.2 2.7 3.0 3.5	$\begin{array}{c} 4.\ 3\\ 5.\ 0\\ 6.\ 2\\ 3.\ 8\\ 4.\ 3\\ 4.\ 9\end{array}$	5.9 6.9 8.4 5.0 5.7 6.5	7.79.011.0 $6.57.48.4$	$\begin{array}{c} 12.0\\ 14.0\\ 17.0\\ 10.2\\ 11.4\\ 13.0 \end{array}$	$\begin{array}{c} 17.\ 5\\ 20.\ 5\\ 24.\ 5\\ 15.\ 0\\ 16.\ 5\\ 19.\ 5\end{array}$	$\begin{array}{c} 31.\ 5\\ 37.\ 0\\ 43.\ 0\\ 26.\ 0\\ 30.\ 0\\ 33.\ 5\end{array}$	50.0 58.0 65.0 41.5 47.0 53.0

# Table 52 .--- Sags for Siemens-Martin Steel Cable

#### HEAVY LOADING DISTRICT

[At 30, 60, and 90° F. without load, the sags being such that when loaded at 0° F. the cable will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

Cable diam-	Grade of con-	, Tem-	Sags (in inches) for span lengths (in feet) of-								
eter (inches)	struction	pera- ture	200	250	300	400	500	600	700	1,000	
	{A and <b>B</b> {C	l 90	10. 3 12. 5 16. 0 7. 0 8. 2 9. 6	20. 5 25. 0 31. 0 12. 5 15. 5 18. 5	39. 5 46. 0 53. 0 22. 0 26. 0 31. 5	96. 0 103. 0 110. 0 57. 0 66. 0 74. 0	166. 0 176. 0 188. 0 119. 0 127. 0 137. 0	270 280 287 197 205 213	381 389 396 289 297 306	792 799 806 664 672 680	
* 3⁄8	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	8.9 10.6 12.5 6.5 7.5 8.6	$15.5 \\ 19.0 \\ 23.5 \\ 10.8 \\ 12.5 \\ 14.5 \\ 14.5 \\ 14.5 \\ 15.5 \\ 14.5 \\ 15.5 \\ 14.5 \\ 14.5 \\ 10.5 \\ $	$\begin{array}{c} 26.5\\ 32.0\\ 38.0\\ 17.5\\ 20.0\\ 24.0 \end{array}$	64. 0 72. 0 80. 0 39. 5 45. 5 52. 0	$123.\ 0\\131.\ 0\\140.\ 0\\77.\ 0\\87.\ 0\\96.\ 0$	198     208     216     137     144     155	288 295 302 208 218 229	640 649 657 499 509 520	
<del>7</del> 16	A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$7.9 \\ 9.4 \\ 11.3 \\ 6.0 \\ 6.9 \\ 7.9$	13. 0 15. 5 19. 0 9. 9 11. 4 13. 0	$\begin{array}{c} 21.\ 0\\ 24.\ 5\\ 29.\ 5\\ 15.\ 0\\ 17.\ 5\\ 20.\ 0 \end{array}$	45. 0 51. 0 59. 0 30. 0 35. 0 40. 5	84. 0 93. 0 103. 0 55. 0 63. 0 71. 0	140 150 159 93 104 115	$203 \\ 214 \\ 224 \\ 144 \\ 154 \\ 167$	479 487 496 358 370 383	
1⁄2	A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	7.4 9.1 11.0 6.2 7.0 7.9	$12.5 \\ 15.5 \\ 18.0 \\ 9.9 \\ 11.3 \\ 12.5$	20. 0 23. 5 27. 5 15. 0 17. 0 19. 0	$\begin{array}{r} 41.\ 0\\ 47.\ 0\\ 55.\ 0\\ 29.\ 0\\ 33.\ 0\\ 37.\ 5\end{array}$	73. 0 83. 0 92. 0 50. 0 57. 0 65. 0	$121 \\ 131 \\ 142 \\ 82 \\ 92 \\ 102$	179 190 201 123 136 148	414 426 438 312 326 340	
9 16	A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	7.4 9.0 10.6 6.0 6.8 7.7	12. 0 14. 0 17. 0 9. 5 10. 9 12. 5	18. 0 21. 0 25. 0 14. 0 16. 0 18. 0	35. 0 41. 0 47. 5 25. 5 30. 0 34. 0	61. 0 69. 0 79. 0 44. 0 51. 0 57. 0	98 109 119 69 78 87	145 158 170 103 113 125	337 350 364 253 269 285	
5⁄8	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	7.2 8.7 10.3 5.8 6.6 7.4	11. 8 14. 0 16. 0 9. 4 10. 8 12. 0	17.520.524.013.515.517.5	$\begin{array}{r} 33.5\\ 39.5\\ 45.0\\ 25.5\\ 29.0\\ 32.5\end{array}$	57. 064. 073. 042. 047. 553. 0	88 98 109 64 71 81	$130 \\ 140 \\ 153 \\ 93 \\ 104 \\ 115$	301 315 330 227 241 260	

# Table 52.-Sags for Siemens-Martin Steel Cable-Continued

#### MEDIUM LOADING DISTRICT

[At 30, 60, and  $90^{\circ}$  F. without load, the sags being such that when loaded at  $15^{\circ}$  F. the cable will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

Cable diam-	Grade of con-	Tem-	Sags (in inches) for span lengths (in feet) of—									
eter (inches)	struction	per- ature	200	250	300	400	500	600	700	1, 000		
<u>*</u>	{A and B C	$ \begin{cases} {}^{\circ}F. \\ {}^{60} \\ {}^{90} \\ {}^{30} \\ {}^{60} \\ {}^{90} \end{cases} $	7.2 8.6 10.1 5.8 6.6 7.4	12. 0 14. 5 17. 0 9. 4 10. 7 12. 0	18.522.025.513.516.018.0	$\begin{array}{c} 40.\ 0\\ 46.\ 0\\ 53.\ 0\\ 27.\ 5\\ 31.\ 5\\ 35.\ 5\end{array}$	75. 0 85. 0 94. 0 49. 0 55. 0 63. 0	124 134 145 81 91 101	186 197 208 128 139 150	$442 \\ 453 \\ 465 \\ 331 \\ 344 \\ 358$		
<sup>3</sup> /8	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	7.28.49.6 $5.86.57.2$	$11.\ 4\\13.\ 0\\15.\ 5\\9.\ 3\\10.\ 5\\11.\ 7$	17.520.024.013.515.517.5	$\begin{array}{c} 33.5\\ 40.5\\ 47.5\\ 25.0\\ 29.0\\ 32.5\end{array}$	$\begin{array}{c} 60.\ 0\\ 69.\ 0\\ 78.\ 0\\ 42.\ 5\\ 48.\ 5\\ 54.\ 0\end{array}$	99 109 120 67 76 85	$144 \\ 157 \\ 171 \\ 102 \\ 113 \\ 124$	$348 \\ 361 \\ 378 \\ 256 \\ 272 \\ 287$		
<del>18</del>	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 6.7 \\ 8.0 \\ 9.4 \\ 5.8 \\ 6.5 \\ 7.2 \end{array}$	$10.8 \\ 13.0 \\ 15.0 \\ 9.0 \\ 10.0 \\ 11.1$	$16.0 \\ 18.5 \\ 21.5 \\ 12.5 \\ 14.5 \\ 16.0$	$\begin{array}{c} 30.\ 0\\ 35.\ 0\\ 40.\ 0\\ 24.\ 0\\ 27.\ 0\\ 30.\ 0 \end{array}$	$51.0 \\ 57.0 \\ 65.0 \\ 38.5 \\ 44.0 \\ 49.5$	79 88 98 58 65 73	$114 \\ 127 \\ 137 \\ 85 \\ 93 \\ 103$	$273 \\ 287 \\ 301 \\ 203 \\ 216 \\ 232$		
<u>1⁄2</u>	{ <sup>A</sup> and B C	$\begin{cases} 30\\ 60\\ 90\\ 30\\ 60\\ 90 \end{cases}$	$7.0 \\ 8.2 \\ 9.4 \\ 5.7 \\ 6.4 \\ 7.2$	$10.8 \\ 12.5 \\ 14.5 \\ 8.7 \\ 9.9 \\ 11.1$	16. 0 18. 5 21. 0 12. 5 14. 0 16. 0	$\begin{array}{c} 29.5\\ 34.0\\ 39.0\\ 23.5\\ 26.5\\ 29.5 \end{array}$	$\begin{array}{r} 48.0\\ 55.0\\ 63.0\\ 37.0\\ 42.0\\ 47.5 \end{array}$	$73 \\ 84 \\ 93 \\ 56 \\ 62 \\ 69$	$104 \\ 117 \\ 129 \\ 81 \\ 88 \\ 98$	$251 \\ 268 \\ 282 \\ 188 \\ 202 \\ 219$		
9 16	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 6.7 \\ 7.9 \\ 9.1 \\ 5.5 \\ 6.3 \\ 7.2 \end{array}$	$10.5 \\ 12.5 \\ 14.0 \\ 8.7 \\ 9.9 \\ 11.0$	$15.5 \\ 17.5 \\ 20.5 \\ 12.5 \\ 14.0 \\ 16.0$	$\begin{array}{c} 28.0\\ 32.5\\ 37.5\\ 23.0\\ 26.0\\ 29.0 \end{array}$	$\begin{array}{r} 46.\ 0\\ 53.\ 0\\ 59.\ 0\\ 36.\ 5\\ 41.\ 0\\ 45.\ 5\end{array}$		$98 \\ 108 \\ 119 \\ 76 \\ 83 \\ 93$	$221 \\ 236 \\ 251 \\ 164 \\ 181 \\ 194$		
5%	A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\\ 90\\ \end{array}\right.$	6.7 7.9 9.1 5.5 6.2 7.0	10. 5 12. 0 14. 0 8. 7 9. 7 10. 8	$15.0 \\ 17.5 \\ 20.0 \\ 12.5 \\ 14.0 \\ 16.0$	$\begin{array}{c} 28.\ 0\\ 32.\ 0\\ 36.\ 5\\ 22.\ 5\\ 25.\ 5\\ 28.\ 5\end{array}$	$\begin{array}{r} 45.\ 0\\ 51.\ 0\\ 58.\ 0\\ 36.\ 0\\ 40.\ 5\\ 45.\ 0\end{array}$	66 75 84 53 58 65	93 104 114 73 80 89	$210 \\ 222 \\ 240 \\ 162 \\ 175 \\ 189$		

# Table 52 .- Sags for Siemens-Martin Steel Cable-Continued

#### LIGHT LOADING DISTRICT

[At 30, 60, and 90° F. without load, the sags being such that when loaded at 30° F. the cable will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

Cable diam-	Grade of con-	Ťem-	S	ags (in	inches)	for spar	n length	ıs (in fe	et) of—	
eter (inches)	struction	pera- ture	200	250	300	400	500	600	700	1,000
5 16	{A and B C	$ \begin{tabular}{c} \bullet & F. \\ & 30 \\ & 60 \\ & 90 \\ & 30 \\ & 60 \\ & 90 \end{tabular} \end{tabular} \end{tabular} \end{tabular} \end{tabular} \end{tabular} \end{tabular}$	$\begin{array}{c} 6.5\\ 7.4\\ 8.4\\ 5.3\\ 6.0\\ 6.7 \end{array}$	$10.2 \\ 11.7 \\ 13.0 \\ 8.1 \\ 9.3 \\ 10.5$	$15.0 \\ 17.0 \\ 19.0 \\ 11.9 \\ 13.5 \\ 15.0$	26.530.535.021.524.027.0	$\begin{array}{r} 44.\ 0\\ 50.\ 0\\ 56.\ 0\\ 35.\ 0\\ 39.\ 0\\ 43.\ 0\end{array}$	$\begin{array}{c} 66.\ 0\\ 74.\ 0\\ 83.\ 0\\ 51.\ 0\\ 57.\ 0\\ 63.\ 0\end{array}$	94 104 115 73 81 88	221 235 250 165 179 194
³⁄8	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 6.2 \\ 7.2 \\ 8.2 \\ 5.3 \\ 6.0 \\ 6.7 \end{array}$	$\begin{array}{c} 9.9\\ 11.4\\ 130\\ 8.6\\ 9.6\\ 10.6\end{array}$	$14.5 \\ 16.5 \\ 19.0 \\ 12.0 \\ 13.5 \\ 15.0$	$\begin{array}{c} 26.\ 0\\ 29.\ 5\\ 33.\ 5\\ 21.\ 5\\ 24.\ 0\\ 26.\ 5\end{array}$	$\begin{array}{c} 43.\ 0\\ 49.\ 0\\ 55.\ 0\\ 35.\ 0\\ 39.\ 0\\ 43.\ 0\end{array}$	$\begin{array}{c} 63.\ 0\\ 72.\ 0\\ 81.\ 0\\ 50.\ 0\\ 57.\ 0\\ 63.\ 0\end{array}$	$90\\100\\110\\71\\78\\86$	$203 \\ 218 \\ 234 \\ 156 \\ 170 \\ 184$
<del>.</del>	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 6.2\\ 7.2\\ 8.2\\ 5.3\\ 6.0\\ 6.7 \end{array}$	$9.6 \\ 11.1 \\ 12.5 \\ 8.5 \\ 9.6 \\ 10.7$	$14.5 \\ 16.5 \\ 18.5 \\ 11.9 \\ 13.5 \\ 15.0 \\$	$\begin{array}{c} 25.\ 5\\ 29.\ 5\\ 53.\ 5\\ 20.\ 5\\ 23.\ 0\\ 26.\ 0 \end{array}$	$\begin{array}{r} 41.\ 0\\ 46.\ 5\\ 52.\ 0\\ 33.\ 5\\ 37.\ 5\\ 41.\ 5\end{array}$	$\begin{array}{c} 60.\ 0\\ 67.\ 0\\ 75.\ 0\\ 48.\ 0\\ 54.\ 0\\ 59.\ 0\end{array}$	$84 \\ 93 \\ 102 \\ 67 \\ 74 \\ 82$	$182 \\ 198 \\ 212 \\ 145 \\ 157 \\ 170 \\ 170 \\ 180 \\ 190 \\ 100 $
½	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 6.2 \\ 7.2 \\ 8.2 \\ 5.3 \\ 5.9 \\ 6.5 \end{array}$	$9.7 \\ 11.1 \\ 12.5 \\ 8.4 \\ 9.5 \\ 10.2$	$\begin{array}{c} 14.0\\ 16.5\\ 18.5\\ 11.9\\ 13.5\\ 15.0 \end{array}$	$\begin{array}{c} 25.\ 5\\ 29.\ 5\\ 33.\ 5\\ 20.\ 5\\ 23.\ 0\\ 26.\ 0\end{array}$	$\begin{array}{c} 41.\ 0\\ 46.\ 5\\ 52.\ 0\\ 33.\ 5\\ 37.\ 0\\ 41.\ 0\end{array}$	$\begin{array}{c} 60.\ 0\\ 67.\ 0\\ 75.\ 0\\ 48.\ 0\\ 54.\ 0\\ 59.\ 0\end{array}$	$\begin{array}{r} 83\\91\\102\\67\\74\\81\end{array}$	180     194     210     144     156     169     169
9 16	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 6.\ 2 \\ 7.\ 2 \\ 8.\ 3 \\ 5.\ 3 \\ 6.\ 0 \\ 6.\ 7 \end{array}$	$9.9 \\11.3 \\12.5 \\8.1 \\9.3 \\10.5$	$\begin{array}{c} 14.\ 0\\ 16.\ 0\\ 18.\ 0\\ 11.\ 5\\ 13.\ 5\\ 14.\ 5\end{array}$	$\begin{array}{c} 25.\ 0\\ 28.\ 5\\ 32.\ 0\\ 20.\ 0\\ 23.\ 0\\ 26.\ 0\end{array}$	$\begin{array}{r} 40.\ 0\\ 45.\ 5\\ 50.\ 0\\ 33.\ 0\\ 36.\ 5\\ 40.\ 0\end{array}$	$59.\ 0\\66.\ 0\\73.\ 0\\47.\ 5\\53.\ 0\\58.\ 0$	81 90 99 66 73 80	$168 \\ 184 \\ 201 \\ 138 \\ 150 \\ 163$
5⁄8	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 6.2 \\ 7.2 \\ 8.2 \\ 5.3 \\ 5.9 \\ 6.5 \end{array}$	9.911.212.58.19.110.2	$14.0 \\ 16.0 \\ 18.0 \\ 11.5 \\ 13.0 \\ 14.5$	$\begin{array}{c} 25.\ 0\\ 28.\ 5\\ 32.\ 5\\ 20.\ 5\\ 23.\ 0\\ 26.\ 0\end{array}$	$\begin{array}{c} 39.\ 5\\ 45.\ 0\\ 50.\ 0\\ 32.\ 5\\ 36.\ 5\\ 40.\ 0\end{array}$	58. 0 65. 0 72. 0 47. 0 53. 0 58. 0	80 87 98 65 72 79	$169 \\ 181 \\ 198 \\ 134 \\ 147 \\ 160$

#### MINIMUM SAGS FOR STEEL

# Table 53.---Sags for High-Tension Steel Cable

#### HEAVY LOADING DISTRICT

[At 30, 60, and 90° F. without load, the sags being such that when loaded at 0° F. the cable will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

Cable . diam- Grade of con-	Tem-	Sags (in inches) for span lengths (in feet) of-									
eter (inches)	pera- ture,	200	250	300	400	500	600	700	1,000		
A and B C	$\left\{\begin{array}{c} \circ F. \\ 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right.$	$\begin{array}{r} 4.3 \\ 4.8 \\ 5.3 \\ 3.1 \\ 3.4 \\ 3.8 \end{array}$	6.9 7.6 8.4 4.8 5.4 6.0	10. 4 11. 7 13. 0 7. 2 7. 9 8. 6	22. 0 24. 0 27. 0 15. 0 16. 5 17. 5	$\begin{array}{r} 43.\ 0\\ 47.\ 5\\ 54.\ 0\\ 26.\ 5\\ 30.\ 0\\ 33.\ 5\end{array}$	78.088.097.045.550.056.0	134 147 159 74. 0 82. 0 90. 0	391 405 418 252 270 284		
3/8{A and B C	$ \begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array} $	$\begin{array}{c} 4.1 \\ 4.5 \\ 5.0 \\ 3.1 \\ 3.4 \\ 3.8 \end{array}$	$\begin{array}{c} 6.3\\ 7.2\\ 8.1\\ 5.4\\ 5.7\\ 6.3 \end{array}$	9.4 10.8 12.0 7.6 8.3 8.9	$19.0 \\ 21.0 \\ 24.0 \\ 14.5 \\ 15.5 \\ 16.5$	$\begin{array}{c} 33.5\\ 37.0\\ 42.0\\ 23.5\\ 25.0\\ 28.0 \end{array}$	$56.0 \\ 62.0 \\ 69.0 \\ 37.0 \\ 40.5 \\ 44.5$	89.0 99.0 110.0 57.0 63.0 70.0	$\begin{array}{c} 271 \\ 286 \\ 301 \\ 162 \\ 171 \\ 180 \end{array}$		
A and B	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right. $	$\begin{array}{c} 4.0\\ 4.4\\ 4.8\\ 3.1\\ 3.3\\ 3.6\end{array}$	6.3 7.0 7.8 4.8 5.2 5.7	$9.0 \\ 10.2 \\ 11.4 \\ 7.0 \\ 7.5 \\ 8.3$	$17.5 \\ 19.5 \\ 21.5 \\ 13.5 \\ 14.5 \\ 15.5 \\ $	$\begin{array}{c} 29.0\\ 32.5\\ 35.5\\ 22.0\\ 23.5\\ 26.0 \end{array}$	$\begin{array}{r} 44.\ 5\\ 49.\ 5\\ 55.\ 0\\ 33.\ 5\\ 36.\ 0\\ 38.\ 0\end{array}$	$\begin{array}{c} 67.\ 0\\ 74.\ 0\\ 81.\ 0\\ 48.\ 0\\ 51.\ 0\\ 55.\ 0\end{array}$	181 196 211 118 127 137		
3/2{A and B C	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right. $	3.8 4.3 4.8 3.1 3.4 3.6	5.7 6.6 7.5 5.0 5.4 5.7	$\begin{array}{r} 8.3\\ 9.7\\ 11.2\\ 7.2\\ 7.6\\ 8.2 \end{array}$	$16.5 \\ 18.0 \\ 20.0 \\ 13.5 \\ 14.5 \\ 15.5$	$\begin{array}{c} 27.5\\ 30.5\\ 33.5\\ 21.5\\ 23.0\\ 24.0 \end{array}$	$\begin{array}{r} 42.5\\ 47.5\\ 53.0\\ 32.5\\ 34.5\\ 36.5\end{array}$	62. 0 69. 0 76. 0 45. 5 49. 0 52. 0	160 173 187 109 118 126		
Å and B	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right. $	3.8 4.3 4.8 3.1 3.4 3.6	5.76.67.54.95.45.7	8.3 9.4 10.8 7.2 7.7 8.3	15.518.020.013.514.515.5	$\begin{array}{c} 26.5\\ 29.5\\ 32.5\\ 21.0\\ 22.0\\ 24.0 \end{array}$	39.5 44.0 48.0 31.0 33.0 36.0	57. 0 62. 0 69. 0 44. 0 46. 0 50. 0	134 146 158 97 106 113		
% {A and B C	$ \begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array} $	3.84.34.83.13.43.6	5.8 6.6 7.5 4.9 5.4 5.8	8.3 9.4 10.4 7.2 7.9 8.6	15.517.519.513.014.015.0	$\begin{array}{c} 25.0\\ 28.0\\ 31.0\\ 21.0\\ 22.5\\ 24.0 \end{array}$	$\begin{array}{c} 37.5 \\ 42.0 \\ 46.0 \\ 30.5 \\ 33.0 \\ 35.0 \end{array}$	$54.0 \\ 60.0 \\ 66.0 \\ 43.0 \\ 45.5 \\ 48.0$	$124 \\ 134 \\ 146 \\ 90 \\ 96 \\ 106$		

25804°-27-17

# Table 53 .- Sags for High-Tension Steel Cable-Continued

#### MEDIUM LOADING DISTRICT

 $[\rm At 30, 60, and 90^\circ\,F.$  without load, the sags being such that when loaded at 15° F. the cable will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

Cable diam-	Grade of con-	Tem-	Sags (in inches) for span lengths (in feet) of-									
eter (inches)	struction	pera- ture	200	250	300	400	500	600	700	1,000		
5 16	{A and B C	$\left\{\begin{array}{c}{}^{\circ}F,\\ 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	3.8 4.2 4.6 3.1 3.3 3.6	5.76.36.94.85.15.7	8.4 9.4 10.4 6.8 7.5 8.3	15.5 17.5 19.5 13.0 14.0 15.0	27.530.033.021.022.524.0	41. 0 45. 5 50. 0 31. 0 33. 0 35. 5	61. 0 68. 0 75. 0 45. 0 48. 0 50. 0	$166 \\ 180 \\ 194 \\ 108 \\ 117 \\ 126$		
3⁄8	{A and B {C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3.8 4.2 4.6 2.9 3.1 3.4	6. 0 6. 4 6. 9 5. 0 5. 4 5. 8	$\begin{array}{r} 8.6\\ 9.3\\ 10.1\\ 7.2\\ 7.7\\ 8.4 \end{array}$	15.5 17.0 18.5 13.0 14.0 15.0	$\begin{array}{c} 25.\ 0\\ 28.\ 0\\ 31.\ 0\\ 20.\ 5\\ 22.\ 0\\ 23.\ 5\end{array}$	$\begin{array}{c} 37.5 \\ 41.5 \\ 46.0 \\ 29.5 \\ 32.5 \\ 34.5 \end{array}$	54. 060. 066. 043. 045. 548. 0	132 144 156 101 109 118		
<del>γ</del> 16	{A and B {C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3.8 4.2 4.6 3.1 3.4 3.6	6. 0 6. 4 7. 0 5. 0 5. 4 5. 7	8.6 9.3 10.1 7.2 7.6 8.0	$15.5 \\ 16.5 \\ 18.0 \\ 12.5 \\ 13.5 \\ 14.5$	$\begin{array}{c} 24.\ 0\\ 26.\ 5\\ 29.\ 5\\ 20.\ 0\\ 21.\ 5\\ 23.\ 0 \end{array}$	$\begin{array}{c} 36.\ 0\\ 39.\ 5\\ 43.\ 0\\ 29.\ 5\\ 32.\ 0\\ 34.\ 0 \end{array}$	49. 5 55. 0 61. 0 40. 5 43. 0 46. 0	$     \begin{array}{r}       118 \\       127 \\       136 \\       88 \\       94 \\       101     \end{array} $		
1⁄2	{A and B {C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3.8 4.1 4.3 3.1 3.4 3.6	5.7 6.3 6.9 4.8 5.4 5.7	8.2 9.0 10.1 6.8 7.6 8.3	$15.5 \\ 17.0 \\ 18.0 \\ 12.5 \\ 13.5 \\ 14.5$	$\begin{array}{c} 24.\ 0\\ 26.\ 5\\ 29.\ 0\\ 20.\ 0\\ 21.\ 0\\ 22.\ 0\end{array}$	35.5 39.0 42.5 29.0 31.0 33.0	49. 0 54. 0 60. 0 39. 5 43. 0 46. 0	112 120 128 87 93 100		
ie	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3.6 4.1 4.6 2.9 3.1 3.4	5.7 6.3 7.0 4.8 5.1 5.4	8.3 9.0 10.1 6.8 7.6 8.3	$15.5 \\ 16.5 \\ 18.0 \\ 12.5 \\ 13.5 \\ 14.5$	$\begin{array}{c} \textbf{24.0}\\ \textbf{26.0}\\ \textbf{29.0}\\ \textbf{19.5}\\ \textbf{21.0}\\ \textbf{23.0} \end{array}$	35. 5 37. 5 41. 0 29. 0 31. 0 33. 0	48. 5 52. 0 57. 0 39. 5 42. 0 44. 5	$     \begin{array}{r}       106 \\       114 \\       123 \\       84 \\       89 \\       95     \end{array} $		
5⁄8	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30_{-}\\ 60\\ 90\end{array}\right.$	3.6 4.1 4.6 2.9 3.1 3.4	5.9 6.3 7.1 5.0 5.3 5.6	8.3 9.0 9.7 7.2 7.6 7.9	$\begin{array}{c} 15.\ 0\\ 16.\ 0\\ 18.\ 0\\ 12.\ 5\\ 13.\ 5\\ 14.\ 5\end{array}$	$\begin{array}{c} 23.5\\ 26.0\\ 29.0\\ 20.0\\ 21.0\\ 23.0 \end{array}$	34. 5 37. 5 41. 0 29. 0 31. 0 33. 0	48. 0 52. 0 57. 0 40. 5 43. 0 45. 5	103 112 120 83 88 93		

#### MINIMUM SAGS FOR STEEL

# Table 53.—Sags for High-Tension Steel Cable—Continued

#### LIGHT LOADING DISTRICT

[At 30, 60, and 90° F, without load, the sags being such that when loaded at 30° F. the cable will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

Cable diam-	Grade of con-	Tem-		Sags (	in inche	es) for s	pan len	gths (in	feet) of	í—
eter (inches)	struction	pera- ture	200	250	300	400	500	600	700	1,000
5 16	{A and B C	$ \begin{cases} {}^{\circ}F. \\ {}^{60} \\ {}^{90} \\ {}^{30} \\ {}^{60} \\ {}^{90} \\ {}^{90} \end{cases} $	3.6 3.9 4.3 2.9 3.1 3.4	5.7 6.0 6.6 4.5 4.8 5.4	8.0 8.7 9.4 6.5 7.0 7.6	$14.5 \\ 15.5 \\ 17.0 \\ 12.5 \\ 13.0 \\ 14.0$	$23.0 \\ 25.0 \\ 27.0 \\ 20.0 \\ 21.0 \\ 22.0$	34. 0 36. 5 40. 5 28. 0 30. 0 31. 5	$\begin{array}{c} 47.\ 0\\ 51.\ 0\\ 55.\ 0\\ 38.\ 5\\ 41.\ 5\\ 44.\ 5\end{array}$	$     \begin{array}{r}       104 \\       112 \\       120 \\       82 \\       87 \\       92     \end{array} $
∛≋	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3.6 3.9 4.3 2.9 3.1 3.4	$5.6 \\ 6.0 \\ 6.6 \\ 4.5 \\ 4.8 \\ 5.2$	7.9 8.4 9.0 6.5 7.2 7.9	$14.5 \\ 16.0 \\ 17.0 \\ 12.0 \\ 13.0 \\ 14.0$	$\begin{array}{c} 23.5\\ 25.0\\ 27.0\\ 19.0\\ 20.5\\ 22.0 \end{array}$	34.0 36.5 39.0 27.5 29.5 31.5	$\begin{array}{c} 46.0\\ 50.0\\ 54.0\\ 38.5\\ 41.5\\ 44.5 \end{array}$	$100 \\ 107 \\ 115 \\ 81 \\ 85 \\ 90$
7 16	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3.4 3.9 4.3 3.0 3.2 3.4	5.7 6.0 6.3 4.5 4.9 5.4	8.3 8.7 9.0 6.5 7.2 7.9	$14.5 \\ 15.5 \\ 16.5 \\ 12.0 \\ 13.0 \\ 14.0$	$\begin{array}{c} 23.0\\ 24.5\\ 26.5\\ 19.0\\ 20.5\\ 21.5 \end{array}$	$\begin{array}{c} 33.\ 0\\ 35.\ 5\\ 38.\ 0\\ 27.\ 5\\ 29.\ 0\\ 31.\ 0 \end{array}$	$\begin{array}{r} 46.\ 0\\ 49.\ 0\\ 52.\ 0\\ 38.\ 5\\ 40.\ 5\\ 43.\ 0\end{array}$	$96 \\ 104 \\ 112 \\ 78 \\ 83 \\ 89$
<sup>1</sup> ⁄2	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \\ 90 \end{cases}$	3.4 3.8 4.3 2.9 3.1 3.4	$5.4 \\ 6.0 \\ 6.6 \\ 4.8 \\ 5.1 \\ 5.5$	$7.9 \\ 8.6 \\ 9.4 \\ 6.8 \\ 7.6 \\ 8.3$	$\begin{array}{c} 14.5\\ 15.5\\ 16.5\\ 12.0\\ 13.0\\ 14.0 \end{array}$	$\begin{array}{c} 23.0\\ 24.5\\ 26.5\\ 18.5\\ 20.5\\ 22.0 \end{array}$	34.0 35.5 38.0 27.5 29.5 31.5	$\begin{array}{r} 45.5 \\ 48.5 \\ 52.0 \\ 38.0 \\ 40.5 \\ 43.0 \end{array}$	96 104 113 78 83 88
9 16	{A and B {C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3.64.04.32.93.13.4	5.7 6.2 6.6 4.6 4.9 5.4	8.3 9.0 9.4 6.7 7.2 7.7	$14.5 \\ 15.5 \\ 16.5 \\ 12.0 \\ 13.0 \\ 14.0$	$\begin{array}{c} 23.0\\ 24.5\\ 26.5\\ 18.5\\ 20.0\\ 21.0 \end{array}$	33.0 35.5 37.5 27.5 29.0 31.0	$\begin{array}{r} 45.5\\ 48.0\\ 51.0\\ 38.0\\ 40.5\\ 43.0 \end{array}$	$95 \\ 103 \\ 110 \\ 77 \\ 83 \\ 88$
5⁄8	{A and B C	$\begin{cases} 30\\60\\90\\30\\60\\90 \end{cases}$	3.4 3.8 4.3 2.9 3.1 3.4	5.5 6.0 6.7 4.5 5.0 5.4	$8.1 \\ 8.5 \\ 9.0 \\ 6.5 \\ 7.2 \\ 7.9$	$14.5 \\ 15.5 \\ 16.5 \\ 12.0 \\ 13.0 \\ 14.0$	$\begin{array}{c} 23.\ 0\\ 24.\ 0\\ 25.\ 0\\ 19.\ 0\\ 20.\ 5\\ 21.\ 5\end{array}$	$\begin{array}{c} 33.\ 0\\ 35.\ 5\\ 37.\ 5\\ 27.\ 5\\ 29.\ 0\\ 31.\ 0\end{array}$	44.5 48.0 51.0 37.0 39.5 43.0	94 102 110 77 82 88

# Table 54.—Sags for Bare Copper-Covered Steel Wire (Ordinary Grade)

#### HEAVY LOADING DISTRICT

[The sags being such that when loaded at 0° F. the wires will be stressed to 50 per cent of their ultimate strength]

Size	Orada of	Tem-		Sags (in inches) for span lengths (in feet) of-										
A. W. G. No.	Grade of construction	pera* ture	100	125	150	175	200	<b>2</b> 50	300	400	500			
6	A and B	F. 30 60 90	1.7 2.0 2.3	3.2 3.8 4.9	5.9 7.2 9.4	10.9 13.7 17.3								
4	do	30 60 90	$1.7 \\ 1.9 \\ 2.3$	$2.9 \\ 3.4 \\ 4.0$	4.6 5.4 6.6	7.0 8.6 10.8	10. 8 13. 7 17. 4	27.4 34.6 39.6	$57.4 \\ 64.2 \\ 70.7$					

#### MEDIUM LOADING DISTRICT

[The sags being such that when loaded at 15° F. the wires will be stressed to 50 per cent of their ultimate strength]

8 B	30 60 90	$1.4 \\ 1.5 \\ 1.7$	$2.3 \\ 2.6 \\ 2.9$	$3.6 \\ 4.1 \\ 4.7$						
6 A and B	30 60 90	$1.4 \\ 1.5 \\ 1.6$	2.2 2.5 2.8	$3.3 \\ 3.7 \\ 4.3$	4.8 5.4 6.3					
4do	30 60 90	$1.4 \\ 1.6 \\ 1.9$	2.3 2.6 3.0	$3.4 \\ 3.8 \\ 4.4$	4.7 5.4 6.3	6.4 7.3 8.4	$10.9 \\ 13.0 \\ 14.8$	$17.6 \\ 20.5 \\ 24.2$	$\begin{array}{c} 41.7 \\ 48.7 \\ 56.5 \end{array}$	

#### LIGHT LOADING DISTRICT

[The sags being such that when loaded at  $30^\circ$  F. the wires will be stressed to 50 per cent of their ultimate strength]

8 B	30 60 90	1. 2 1. 3 1. 4	2.6 2.9 3.3	 	 		
6 A and B	30 60 90	1. 2 1. 4 1. 5	$2.8 \\ 3.1 \\ 3.5$	 5.0 5.5 6.2	 		
4do	30 60 90	$\begin{array}{c} 1.3\\ 1.5\\ 1.7\\ \end{array}$	3.0 3.3 3.8	 5.4 6.0 6.8	 $12.\ 2\\13.\ 5\\15.\ 7$	$\begin{array}{c} 22.\ 7\\ 25.\ 5\\ 28.\ 8\end{array}$	37.0 41.4 46.7

# Table 55 .- Sags for Bare Copper-Covered Steel Cable

#### HEAVY LOADING DISTRICT

[The sags being such that when loaded at 0° F. the cable will be stressed to 50 per cent of its ultimate strength]

Diam- eter	Grade of construc-	Tem-	Sags (in inches) for span lengths (in feet) of-										
(inch)	tion	pera- ture	200	250	300	400	500	600	800	1,000			
5 16	A and B	° <i>F</i> . 30 60 90	5.6 6.2 7.0	9.3 10.4 11.9	15.0 17.1 19.7	$34.6 \\ 39.9 \\ 45.6$	73. 8 83. 4 93. 4						
3/8	do	30 60 90	5.6 6.1 6.9	9.1 10.1 11.4	$13.7 \\ 15.2 \\ 17.3$	$\begin{array}{c} 27.\ 4\\ 30.\ 6\\ 34.\ 8\end{array}$	49. 9 56. 2 63. 5	85.6 95.2 106.0	$202 \\ 215 \\ 228$				
<del>1</del> 6	do	30 60 90	$5.7 \\ 6.4 \\ 7.2$	9.2 10.2 11.5	$13.8 \\ 15.3 \\ 17.2$	26. 6 29. 8 33. 6	46. 8 52. 3 58. 8	77. 0 85. 6 95. 0	$172 \\ 186 \\ 200$	$316 \\ 331 \\ 345$			
1⁄2	do	30 60 90	5.7 6.2 7.0	9.1 10.0 11.1	$13.4 \\ 14.8 \\ 16.5$	$25.2 \\ 28.0 \\ 31.2$	$\begin{array}{r} 42.\ 7\\ 47.\ 3\\ 52.\ 8\end{array}$	$\begin{array}{r} 67.\ 0\\74.\ 2\\82.\ 2\end{array}$	$146 \\ 157 \\ 171$	265 280 295			
9 16	do	30 60 90	5.8 6.4 7.1	9.1 10.1 11.2	$13.4 \\ 14.8 \\ 16.5$	25. 1 27. 5 31. 1	41.3 45.5 50.4	63. 7 69. 8 77. 0	$131 \\ 142 \\ 154$	234 248 262			

# Table 55.—Sags for Bare Copper-Covered Steel Cable—Continued MEDIUM LOADING DISTRICT

[The sags being such that when loaded at 15° F. the cable will be stressed to 50 per cent of its ultimate strength]

Diam-		Tem- pera-						
eter (inch)	Grade of construction	ture	100	250	400	600	800	1,000
<u>5</u> 16	A and B	° <i>F</i> . 30 60 90	$1.2 \\ 1.3 \\ 1.4$	7.7 8.5 9.5	21, 5 23, 9 26, 7	58.1 64.7 72.2		
<sup>3</sup> /8	do	30 60 90	$1.2 \\ 1.4 \\ 1.5$	8.0 8.8 9.8	$21.5 \\ 23.6 \\ 26.4$	$54.0 \\ 59.5 \\ 66.4$	$110.0 \\ 119.0 \\ 130.0$	
<u>7</u> 16	do	30 60 90	$1.3 \\ 1.4 \\ 1.6$	$8.3 \\ 9.1 \\ 10.1$	$22.0 \\ 24.2 \\ 26.7$	$53.4 \\ 58.6 \\ 64.7$	$104.\ 0\\114.\ 0\\124.\ 0$	$178 \\ 194 \\ 208$
1⁄2	do	30 60 90	$1.3 \\ 1.4 \\ 1.6$	$8.3 \\ 9.1 \\ 10.1$	$21.9 \\ 24.0 \\ 26.5$	$\begin{array}{c} 52.1 \\ 56.9 \\ 62.8 \end{array}$	99.5 108.0 117.0	168 180 193
9 16	do	30 60 90 .	$1.3 \\ 1.5 \\ 1.6$	8.5 9.3 10.3	$22. \ 3 \\ 24. \ 4 \\ 26. \ 8$	$52.5 \\ 57.1 \\ 62.4$	98.5 106.0 115.0	163 175 188

#### LIGHT LOADING DISTRICT

[The sags being such that when loaded at 30° F. the cable will be stressed to 50 per cent of its ultimate strength]

5 A and B	30 60 90	$1.1 \\ 1.2 \\ 1.4$	7.0 7.8 8.6	$18.5 \\ 20.2 \\ 22.6$	$\begin{array}{c} 43.2 \\ 47.2 \\ 51.8 \end{array}$	81.5 88.8 97.1	
3⁄8do	30 60 90	$1.2 \\ 1.3 \\ 1.4$	7.5 8.2 9.1	$19.\ 3\\21.\ 2\\23.\ 3$	$\begin{array}{c} 44.\ 5\\ 49.\ 0\\ 53.\ 5\end{array}$	82.5 89.5 98.5	$134 \\ 144 \\ 156$
7 <u>16</u> do	30 60 90	$1.3 \\ 1.4 \\ 1.5$	7.8 8.5 9.4	$\begin{array}{c} 20.\ 2\\ 22.\ 0\\ 24.\ 2\end{array}$	$\begin{array}{c} 46.3\\ 50.4\\ 55.2 \end{array}$	84.7 91.8 98.6	137 147 159
½do	30 60 90	$1.3 \\ 1.4 \\ 1.5$	7.9 8.6 9.4	$20.4 \\ 22.2 \\ 24.3$	$\begin{array}{c} 46.\ 6\\ 50.\ 6\\ 55.\ 1\end{array}$	84. 8 91. 6 99. 1	$     \begin{array}{r}       136 \\       146 \\       157     \end{array} $
9 16do	30 60 90	$1.3 \\ 1.4 \\ 1.5$	8, 1 8, 8 9, 7	$21.6 \\ 22.7 \\ 24.9$	$47.8 \\ 51.8 \\ 56.3$	$\begin{array}{c} 86.7\\93.4\\101.0\end{array}$	137 148 159

# Table 56 .- Sags for Bare Stranded Aluminum

#### HEAVY LOADING DISTRICT

[Sags being such that when loaded at 0° F. the conductor will be stressed to 50 per cent of its ultimate strength for grades A and B and 60 per cent for grade C]

Size	Grade of	Tem-		Sags	(in inc	hes) fo	r span	lengths	(in feet	) of—	
A. W. G. No.	construction	pera- ture	100	125	150	200	250	300	400	500	600
1	{A and B {C	$\begin{cases} {}^{\circ}F. \\ {}^{60}\\ {}^{90}\\ {}^{30}\\ {}^{60}\\ {}^{90} \end{cases}$	$12.5 \\ 18.2 \\ 23.0 \\ 4.3 \\ 9.4 \\ 16.1$	24. 630. 335. 112. 320. 126. 4	$\begin{array}{r} 42.1\\ 47.2\\ 51.8\\ 26.6\\ 33.5\\ 39.6 \end{array}$						
0	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 7.4\\ 13.0\\ 19.7\\ 2.9\\ 6.2\\ 12.7\end{array}$	$\begin{array}{c} 16.\ 2\\ 24.\ 6\\ 30.\ 0\\ 7.\ 2\\ 14.\ 1\\ 21.\ 6\end{array}$	$\begin{array}{c} 31.\ 0\\ 37.\ 1\\ 44.\ 6\\ 15.\ 5\\ 25.\ 2\\ 32.\ 4\end{array}$	$\begin{array}{c} 63.\ 4\\ 69.\ 6\\ 75.\ 4\\ 45.\ 1\\ 53.\ 3\\ 60.\ 0\end{array}$	$109. 0 \\115. 0 \\120. 0 \\81. 0 \\88. 8 \\95. 4$	$\begin{array}{c} 170.\ 0\\ 177.\ 0\\ 182.\ 0\\ 127.\ 0\\ 133.\ 0\\ 140.\ 0 \end{array}$	$294 \\ 304 \\ 310 \\ 239 \\ 246 \\ 251$		
00	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	5.010.816.82.65.010.8	$10.8 \\ 18.6 \\ 25.2 \\ 5.1 \\ 9.9 \\ 17.4$	$\begin{array}{c} 22.\ 0\\ 29.\ 5\\ 36.\ 0\\ 9.\ 7\\ 18.\ 0\\ 26.\ 3\end{array}$	$\begin{array}{r} 49.\ 4\\ 56.\ 6\\ 63.\ 4\\ 29.\ 7\\ 39.\ 4\\ 48.\ 0\end{array}$	$\begin{array}{c} 85.2\\ 91.2\\ 97.2\\ 60.6\\ 70.2\\ 78.0 \end{array}$	$\begin{array}{c} 127.\ 0\\ 133.\ 0\\ 140.\ 0\\ 96.\ 5\\ 106.\ 0\\ 114.\ 0 \end{array}$	$241 \\ 247 \\ 254 \\ 189 \\ 198 \\ 207$		462 472 479
000	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3.87.714.62.23.88.4	7.514.721.94.27.515.0	$ \begin{array}{c} 14. \\ 23. \\ 31. \\ 6. \\ 13. \\ 21. \\ \end{array} $	$\begin{array}{r} 37.\ 4\\ 46.\ 5\\ 54.\ 2\\ 20.\ 6\\ 31.\ 2\\ 41.\ 3\end{array}$	$\begin{array}{c} 73.\ 2\\ 75.\ 6\\ 84.\ 0\\ 45.\ 0\\ 56.\ 4\\ 65.\ 4\end{array}$	$\begin{array}{c} 102.\ 0\\ 111.\ 0\\ 119.\ 0\\ 74.\ 2\\ 92.\ 2\\ 95.\ 0 \end{array}$	$     \begin{array}{r}       197 \\       205 \\       213 \\       151 \\       161 \\       172     \end{array} $		469 478 487 376 387 396
0000	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	3.1 6.5 13.2 2.2 3.6 7.9	$\begin{array}{c} 6.0\\ 12.0\\ 19.5\\ 3.6\\ 6.3\\ 12.0 \end{array}$	10. 4 19. 1 27. 0 6. 1 10. 4 19. 1	29.3 39.4 48.0 14.9 24.9 35.0	53. 462. 474. 431. 843. 855. 2	83. 5 92. 9 102. 0 57. 6 70. 5 81. 4	165 175 183 125 137 148		$395 \\ 403 \\ 413 \\ 312 \\ 324 \\ 335$

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# Table 56.—Sags for Bare Stranded Aluminum—Continued

#### MEDIUM LOADING DISTRICT

[Sags being such that when loaded at 15° F. the conductor will be stressed to 50 per cent of its ultimate strength for grades A and B, and 60 per cent for grade C]

Size	Grade of	Tem-		Sags	(in incl	hes) fo	r span	lengths	(in feet	) of—	
A. W. G. No.	construction	pera- ture	100	125	150	200	250	300	400	500	600
1	{A and B C	$ \begin{cases} {}^{\circ}F. \\ {}^{30} \\ {}^{60} \\ {}^{90} \\ {}^{30} \\ {}^{60} \\ {}^{90} \end{cases} $	$2.6 \\ 5.3 \\ 11.3 \\ 1.7 \\ 2.9 \\ 6.0$	5.4 10.5 18.6 3.3 5.4 11.1	10. 4 18. 7 27. 4 5. 4 9. 4 17. 3						
0	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$\begin{array}{c} 2.4 \\ 4.3 \\ 9.6 \\ 1.9 \\ 2.6 \\ 5.0 \end{array}$	4.5 8.1 15.6 3.0 4.5 8.7	7.514.023.04.77.614.0	$\begin{array}{c} 22.\ 6\\ 33.\ 1\\ 42.\ 7\\ 11.\ 0\\ 18.\ 7\\ 29.\ 3\end{array}$	$\begin{array}{r} 46.8\\ 57.6\\ 66.6\\ 24.6\\ 42.6\\ 49.2 \end{array}$	$\begin{array}{c} 76.\ 3\\ 90.\ 7\\ 96.\ 5\\ 47.\ 5\\ 61.\ 2\\ 73.\ 4 \end{array}$	$156 \\ 165 \\ 176 \\ 113 \\ 122 \\ 138$	$257 \\ 265 \\ 275 \\ 196 \\ 208 \\ 220$	380 392 400 297 310 321
00	{A and B C	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array} \right.$	2.23.88.41.42.44.6	$\begin{array}{r} 3.9 \\ 6.9 \\ 13.5 \\ 2.7 \\ 4.2 \\ 7.5 \end{array}$	$\begin{array}{c} 6.\ 1 \\ 11.\ 2 \\ 19.\ 8 \\ 4.\ 0 \\ 6.\ 5 \\ 11.\ 9 \end{array}$	16. 325. 936. 59. 113. 923. 5	$\begin{array}{r} 33.\ 0\\ 46.\ 2\\ 56.\ 4\\ 18.\ 0\\ 28.\ 2\\ 40.\ 8\end{array}$	59. 071. 382. 833. 148. 2 $61. 2$	$122 \\ 134 \\ 146 \\ 84.5 \\ 99.8 \\ 114$	$210 \\ 222 \\ 233 \\ 155 \\ 170 \\ 185$	314 325 337 243 259 272
000	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 2.\ 2\\ 3.\ 6\\ 7.\ 9\\ 1.\ 7\\ 2.\ 6\\ 4.\ 6\end{array}$	3.6 6.3 12.3 2.7 3.9 7.2	$5.8 \\ 9.7 \\ 18.0 \\ 4.3 \\ 6.5 \\ 10.8$	13.021.132.28.212.921.6	25. 8 37. 2 49. 8 15. 0 22. 8 34. 8	46. 8 60. 5 72. 7 25. 9 38. 9 52. 6	99.8 113 127 65.3 82.6 97.9	$173 \\ 187 \\ 199 \\ 124 \\ 140 \\ 156$	263 276 288 199 214 232
0000	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	2.2 3.4 7.2 1.4 2.4 4.3	$\begin{array}{c} 3.6 \\ 6.0 \\ 11.4 \\ 2.7 \\ 3.9 \\ 6.9 \end{array}$	5. 4 9. 0 16. 2 4. 3 5. 8 10. 4	11.519.229.87.211.519.2	20. 4 31. 8 44. 4 13. 8 20. 4 31. 8	$\begin{array}{c} 38.\ 2\\ 51.\ 8\\ 64.\ 1\\ 22.\ 3\\ 33.\ 1\\ 46.\ 8\end{array}$	80. 6 96. 0 110 50. 9 67. 2 84. 5	142 158 173 101 119 137	$217 \\ 233 \\ 248 \\ 160 \\ 178 \\ 199$

# Table 56.—Sags for Bare Stranded Aluminum—Continued

#### LIGHT LOADING DISTRICT

[Sags being such that when loaded at 30° F. the conductor will be stressed to 50 per cent of its ultimate strength for grades A and B, and 60 per cent for grade C]

Size	Grade of	Tem-		Sags (	in incl	nes) for	span	lengths	(in feet	) of —	
A. W. G. No.	construction	pera- ture	100	125	150	200	250	300	400	500	600
1	{A and B C	$\left\{\begin{array}{c} {}^\circ F.\\ {}^{30}\\ {}^{60}\\ {}^{90}\\ {}^{30}\\ {}^{60}\\ {}^{90}\end{array}\right.$	1.7 2.6 5.0 1.4 1.9 3.1	2.7 4.5 8.1 2.4 3.0 5.1	4.3 6.8 12.6 3.6 4.7 7.6						
0	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1.9 2.9 4.8 1.7 1.9 2.9	2.7 4.2 7.8 2.4 3.3 4.8	4.0 6.5 11.9 3.2 5.0 7.9	$\begin{array}{r} 8.2 \\ 13.0 \\ 21.1 \\ 6.2 \\ 9.1 \\ 14.4 \end{array}$	15. 622. 236. 011. 415. 623. 4	$\begin{array}{c} 27.\ 4\\ 38.\ 9\\ 52.\ 6\\ 17.\ 3\\ 24.\ 5\\ 36.\ 7\end{array}$	65. 3 82. 6 97. 0 40. 3 55. 7 72. 0	120 138 161 81.6 101 120	$193 \\ 210 \\ 226 \\ 141 \\ 161 \\ 180$
00	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1.7 2.6 4.8 1.4 1.9 3.1	$2.7 \\ 4.2 \\ 7.5 \\ 2.1 \\ 3.0 \\ 4.8 $	$\begin{array}{r} 4.0\\ 6.5\\ 11.2\\ 3.2\\ 4.7\\ 7.2 \end{array}$	$\begin{array}{r} 8.2 \\ 12.5 \\ 20.2 \\ 6.2 \\ 8.6 \\ 13.9 \end{array}$	$13.8 \\ 21.0 \\ 32.4 \\ 10.8 \\ 14.4 \\ 22.2$	23. 8 35. 3 49. 0 16. 6 23. 0 33. 8	55.7 72.0 89.3 35.5 49.0 65.3	${ \begin{smallmatrix} 103 \\ 122 \\ 139 \\ 67.2 \\ 88.8 \\ 108 \end{smallmatrix} }$	$166 \\ 184 \\ 203 \\ 115 \\ 138 \\ 158 $
000	A and B C	{ 30 60 90 30 60 90	$1.7 \\ 2.6 \\ 4.8 \\ 1.4 \\ 1.9 \\ 3.1$	$2.7 \\ 3.9 \\ 7.2 \\ 2.4 \\ 3.0 \\ 4.8 $	$\begin{array}{r} 4.3 \\ 6.1 \\ 10.8 \\ 3.2 \\ 4.3 \\ 7.2 \end{array}$	$7.7 \\ 11.0 \\ 19.7 \\ 6.2 \\ 8.2 \\ 13.0$	$\begin{array}{c} 12.\ 6\\ 19.\ 8\\ 30.\ 6\\ 9.\ 6\\ 13.\ 8\\ 21.\ 0\end{array}$	$\begin{array}{c} 21.\ 6\\ 31.\ 0\\ 44.\ 6\\ 15.\ 1\\ 20.\ 9\\ 31.\ 0\end{array}$	46. 1 62. 4 79. 7 30. 7 43. 2 58. 6	91.2 109 127 58.8 78.0 97.2	$ \begin{array}{c c} 144 \\ 164 \\ 186 \\ 97 \\ 119 \\ 143 \\ \end{array} $
0000	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1.4 2.4 4.6 1.2 1.9 2.9	2.7 3.9 7.2 2.1 3.0 4.8	4.0 6.1 10.4 3.2 4.3 6.8	7.2 11.0 18.2 6.2 7.7 12.5	12.0 18.6 28.8 9.6 13.2 20.4	$20.2 \\ 28.8 \\ 41.8 \\ 15.1 \\ 20.9 \\ 30.2$	42. 2 58. 6 74. 9 29. 8 40. 3 54. 7	79. 2 98. 4 118 54. 0 69. 6 88. 8	128 150 168 89 109 132

# Table 57.--Sags for Bare Stranded Aluminum, Steel-Reinforced

HEAVY LOADING DISTRICT

[Sags being such that when loaded at 0° F. the cable will be stressed to 50 per cent of its ultimate strength for grades A and B, and 60 per cent for grade C]

Size	Grade of	Tem-		lags in (	(inches)	for spa	n lengtl	hs (in fe	eet) of—	
A. W. G. No.	construction	pera- ture	100	150	200	300	400	500	700	1,000
4	{A and B C	$ \begin{array}{c} ^{\circ}F. \\ 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array} $	3.0 5.6 10.7 1.6 2.2 3.5	$24.\ 0\\30.\ 6\\36.\ 0\\7.\ 6\\12.\ 8\\20.\ 0$	$\begin{array}{c} 61.\ 2\\ 66.\ 4\\ 71.\ 2\\ 35.\ 6\\ 43.\ 3\\ 50.\ 0 \end{array}$	164. 0 169. 0 173. 0 123. 0 129. 0 135. 0	$312 \\ 316 \\ 321 \\ 244 \\ 250 \\ 255$	$511 \\ 515 \\ 520 \\ 405 \\ 410 \\ 415$		
2	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1.9 \\ 2.7 \\ 4.7 \\ 1.3 \\ 1.7 \\ 2.3$	$\begin{array}{c} 6.9\\ 11.4\\ 18.4\\ 3.7\\ 5.1\\ 7.6 \end{array}$	$\begin{array}{c} 25.\ 4\\ 34.\ 0\\ 41.\ 8\\ 9.\ 7\\ 14.\ 6\\ 22.\ 4\end{array}$	$95. \ 3 \\ 103. \ 0 \\ 110. \ 0 \\ 58. \ 9 \\ 69. \ 3 \\ 78. \ 7$	$192 \\199 \\206 \\141 \\150 \\158$	$319 \\ 325 \\ 332 \\ 245 \\ 254 \\ 262$	555 562 570	
1	A and B C	{	$1.8 \\ 2.5 \\ 3.9 \\ 1.3 \\ 1.6 \\ 2.2$	5.3 8.0 13.5 3.3 4.4 6.3	$\begin{array}{c} 15.\ 2\\ 23.\ 2\\ 32.\ 0\\ 7.\ 4\\ 10.\ 4\\ 15.\ 6\end{array}$	70. 7 79. 6 88. 1 36. 5 48. 0 59. 2	$151 \\ 159 \\ 168 \\ 103 \\ 114 \\ 125$	$\begin{array}{c} 255 \\ 263 \\ 271 \\ 190 \\ 201 \\ 211 \end{array}$	$540 \\ 548 \\ 556 \\ 424 \\ 434 \\ 443$	$1, 193 \\ 1, 200 \\ 1, 207 \\ 944 \\ 953 \\ 962$
0	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1.62.23.51.21.52.1	$\begin{array}{r} 4.5\\ 6.4\\ 10.4\\ 3.1\\ 4.0\\ 5.5 \end{array}$	$10.5 \\ 16.0 \\ 24.2 \\ 6.3 \\ 8.3 \\ 12.1$	48. 6 59. 8 70. 0 23. 0 32. 1 43. 4	115 126 136 70. 8 84. 5 97. 3	$\begin{array}{c} 202 \\ 212 \\ 221 \\ 143 \\ 156 \\ 168 \end{array}$	435 444 454 336 348 360	954 963 972 757 768 779
00	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1.62.03.21.31.52.0	4.0 5.4 8.6 2.9 3.6 5.0	$\begin{array}{r} 8.4\\ 12.4\\ 18.9\\ 5.6\\ 7.3\\ 10.1 \end{array}$	$\begin{array}{r} 32.\ 7\\ 44.\ 0\\ 55.\ 5\\ 17.\ 0\\ 23.\ 2\\ 32.\ 4\end{array}$	85.5 98.2 110 47.0 60.6 74.7	$157 \\ 169 \\ 181 \\ 103 \\ 118 \\ 133$	350 362 373 262 277 291	772 783 794 607 620 634
000	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1.3 \\ 1.8 \\ 3.0 \\ 1.2 \\ 1.4 \\ 2.0$	$\begin{array}{c} 3.9\\ 5.3\\ 8.0\\ 2.6\\ 3.5\\ 4.7 \end{array}$	$7.7 \\ 10.3 \\ 15.9 \\ 5.3 \\ 6.6 \\ 9.2$	$\begin{array}{r} 24.1\\ 33.8\\ 45.2\\ 14.4\\ 18.9\\ 26.5 \end{array}$	$\begin{array}{c} 63.\ 2\\ 77.\ 3\\ 90.\ 5\\ 34.\ 6\\ 45.\ 7\\ 59.\ 2\end{array}$	$122 \\ 137 \\ 150 \\ 74.4 \\ 90.7 \\ 107$	$284 \\ 298 \\ 311 \\ 206 \\ 223 \\ 240$	$\begin{array}{c} 636\\ 649\\ 662\\ 496\\ 512\\ 528\end{array}$
0000	{A and B C	{ 30 60 90 30 60 90	$1.5 \\ 2.0 \\ 2.8 \\ 1.2 \\ 1.5 \\ 1.9$	$\begin{array}{c} 3.7 \\ 4.6 \\ 7.0 \\ 2.7 \\ 3.5 \\ 4.5 \end{array}$	$\begin{array}{c} 6.\ 6\\ 9.\ 2\\ 14.\ 1\\ 5.\ 1\\ 6.\ 4\\ 8.\ 6\end{array}$	19. 427. 137. 613. 016. 722. 6	$\begin{array}{r} 47.\ 0\\ 60.\ 0\\ 74.\ 9\\ 27.\ 8\\ 36.\ 1\\ 47.\ 8\end{array}$	93 109 125 55.1 69.8 85.9	230 245 260 157 177 196	524 539 554 399 418 437

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# Table 57.—Sags for Bare Stranded Aluminum, Steel-Reinforced— Continued

#### MEDIUM LOADING DISTRICT

[Sags being such that when loaded at 15° F. the cable will be stressed to 50 per cent of the ultimate strength for grades A and B, and 60 per cent for grade C]

Size	Grade of	Tem-	s	ags (in	inches)	for spa	n lengtl	ıs (in fe	et) of—	
A. W. G. No.	construction	pera- ture	100	150	200	300	400	500	700	1,000
4	{A and B C	$\begin{cases} {}^{\circ}F.\\ {}^{60}\\ {}^{90}\\ {}^{30}\\ {}^{60}\\ {}^{90} \end{cases}$	1.52.02.91.11.41.8	4.3 6.1 9.9 2.9 3.7 5.0	$11.5 \\ 17.8 \\ 26.5 \\ 6.3 \\ 8.3 \\ 12.1$	$\begin{array}{c} 62.2 \\ 72.3 \\ 81.4 \\ 28.9 \\ 39.7 \\ 51.3 \end{array}$	$142 \\ 151 \\ 159 \\ 92.8 \\ 105 \\ 116$	$250 \\ 252 \\ 261 \\ 179 \\ 190 \\ 200$		
2	{A and B C	$\begin{cases} 30\\60\\90\\30\\60\\90 \end{cases}$	$1.3 \\ 1.6 \\ 2.2 \\ 1.1 \\ 1.3 \\ 1.7$	3.44.56.62.63.24.2	7.19.714.65.0 $6.28.3$	$\begin{array}{c} 26.1\\ 36.4\\ 48.0\\ 14.5\\ 19.0\\ 26.3 \end{array}$	75. 288. 610138. 750. 965. 0	$145 \\ 158 \\ 170 \\ 90 \\ 106 \\ 122$		
1	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1.4 \\ 1.7 \\ 2.5 \\ 1.1 \\ 1.3 \\ 1.7$	$\begin{array}{c} 3.3 \\ 4.3 \\ 6.1 \\ 2.6 \\ 3.1 \\ 4.0 \end{array}$	$\begin{array}{c} 6.4\\ 8.6\\ 12.6\\ 4.8\\ 6.0\\ 7.7 \end{array}$	$\begin{array}{c} 20.1\\ 27.8\\ 38.4\\ 12.7\\ 16.3\\ 21.9 \end{array}$	$54.1 \\68.2 \\82.0 \\29.5 \\38.5 \\50.7$	$111 \\ 126 \\ 140 \\ 63.9 \\ 79.6 \\ 96.1$	270 285 298 190 209 226	616 629 642 475 492 509
0	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$1.4 \\ 1.7 \\ 2.4 \\ 1.0 \\ 1.3 \\ 1.7$	3.24.25.82.53.03.9	$6.0 \\ 7.9 \\ 11.3 \\ 4.6 \\ 5.7 \\ 7.3$	$\begin{array}{c} 16.\ 6\\ 22.\ 7\\ 31.\ 7\\ 11.\ 7\\ 14.\ 5\\ 19.\ 2 \end{array}$	$\begin{array}{c} 40.2\\ 52.7\\ 66.8\\ 24.4\\ 31.3\\ 41.2 \end{array}$	$\begin{array}{r} 83.2\\99.6\\115\\48.0\\61.0\\76.5\end{array}$	216 232 248 144 163 182	505 522 537 382 402 421
00	{A and B c	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1.3 \\ 1.7 \\ 2.3 \\ 1.0 \\ 1.3 \\ 1.7$	$3.1 \\ 4.0 \\ 5.5 \\ 2.4 \\ 3.0 \\ 3.8 $	5.7 7.5 10.4 4.4. 5.5 7.0	$14.8 \\ 19.7 \\ 27.3 \\ 10.9 \\ 13.5 \\ 17.5$	$\begin{array}{c} 32.5 \\ 42.8 \\ 55.8 \\ 21.7 \\ 27.2 \\ 35.4 \end{array}$	$\begin{array}{c} 63.8 \\ 79.6 \\ 96.1 \\ 39.6 \\ 49.9 \\ 63.3 \end{array}$	$171 \\ 190 \\ 208 \\ 110 \\ 131 \\ 151$	416 435 453 305 329 351
000	{ <sup>A</sup> and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$1.3 \\ 1.7 \\ 2.3 \\ 1.0 \\ 1.3 \\ 1.7$	3.0 3.9 5.4 2.5 3.0 4.0	5.6 7.1 10.0 4.4 5.3 6.9	$13.9 \\ 18.0 \\ 24.8 \\ 10.5 \\ 12.9 \\ 16.6$	28.437.048.820.225.032.2	52.3 66.7 82.7 35.0 43.7 55.4	$138 \\ 159 \\ 178 \\ 89 \\ 108 \\ 128$	346 368 388 248 273 298
0000	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$     \begin{array}{r}       1.3 \\       1.6 \\       2.3 \\       1.0 \\       1.3 \\       1.6 \\       \end{array} $	3.03.85.22.42.93.7	5.4 6.9 9.6 4.3 5.3 6.8	$13.0 \\ 16.9 \\ 23.0 \\ 10.2 \\ 12.5 \\ 15.9 \\$	$\begin{array}{c} 25.8\\ 33.2\\ 43.8\\ 19.2\\ 23.5\\ 30.0 \end{array}$	45. 5 57. 8 72. 8 32. 3 39. 7 50. 0	$114 \\ 134 \\ 155 \\ 71.8 \\ 86.8 \\ 105$	289 313 336 203 229 255

# Table 57.—Sags for Bare Stranded Aluminum, Steel-Reinforced— Continued

### LIGHT LOADING DISTRICT

[Sags being such that when loaded to 30° F. the cable will be stressed to 50 per cent of the ultimate strength for grades A and B, and 60 per cent for grade C]

Size	Grade of	Tem-	s	lags (in	inches)	for spa	n length	ns (in fe	et) of—	
A.W.G. No.	construction	pera- ture	100	150	200	300	400	500	700	1,000
4	{A and B C		1.2 1.5 2.0 1.0 1.2 1.5	2.8 3.5 4.7 2.3 2.7 3.4	5.2 6.7 9.0 4.1 5.0 6.2	13. 8 18. 0 25. 2 10. 1 12. 4 16. 0	$\begin{array}{c} 31.\ 5\\ 41.\ 5\\ 54.\ 3\\ 20.\ 6\\ 25.\ 8\\ 33.\ 3\end{array}$	65. 6 81. 7 98. 0 38. 9 48. 9 62. 0		
2	{A and B C	$\begin{cases} 30\\ 60\\ 90\\ 30\\ 60\\ 90 \end{cases}$	1.2 1.5 1.9 1.0 1.2 1.5	2.7 3.4 4.5 2.2 2.7 3.3	5.0 6.2 8.3 4.0 4.9 6.0	$12.3 \\ 15.7 \\ 20.9 \\ 9.5 \\ 11.5 \\ 14.4$	$\begin{array}{c} 25.\ 3\\ 32.\ 3\\ 42.\ 6\\ 18.\ 4\\ 22.\ 3\\ 28.\ 2\end{array}$	47. 0 59. 7 75. 0 31. 8 39. 1 49. 2		
1	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1.2 1.5 2.0 1.0 1.2 1.5	2.7 3.4 4.5 2.2 2.7 3.3	$\begin{array}{c} 4.9\\ 6.2\\ 8.2\\ 4.0\\ 4.8\\ 6.0 \end{array}$	12.0 15.2 20.2 9.5 11.4 14.2	23. 9 30. 4 39. 8 17. 9 21. 7 27. 2	$\begin{array}{r} 42.\ 7\\ 54.\ 0\\ 68.\ 4\\ 30.\ 3\\ 36.\ 9\\ 46.\ 1\end{array}$	113 133 153 73.4 88.7 107	298 322 344 206 232 258
0	A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \\ 90 \\ \end{cases}$	1.2 1.5 2.0 1.0 1.1 1.4	2.7 3.3 4.4 2.2 2.6 3.3	5.0 6.0 8.0 4.0 4.8 5.9	11.7 14.7 19.4 9.3 11.1 13.9	22. 6 28. 4 37. 1 17. 3 20. 9 26. 0	39. 1 49. 2 62. 5 28. 9 34. 8 43. 4	97.8 117 138 66.4 80.0 97.0	259 284 308 178 204 230
00	A and B	<pre>     30     60     90     30     60     90     90 </pre>	1.2 1.4 2.0 1.0 1.1 1.4	2.7 3.3 4.4 2.2 2.6 3.3	4.9 6.0 7.9 4.0 4.8 5.9	11. 3 14. 2 18. 6 9. 1 10. 9 13. 6	21. 5 27. 0 35. 0 16. 9 20. 2 25. 1	$\begin{array}{r} 36.5\\ 45.7\\ 57.9\\ 27.7\\ 33.2\\ 41.2 \end{array}$	86. 9 105 125 61. 3 73. 7 89. 2	226 252 277 157 181 207
000	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1.2 1.4 1.9 1.0 1.1 1.4	2.6 3.3 4.3 2.2 2.6 3.3	4.8 5.9 7.8 3.9 4.6 5.8	11. 2 13. 9 18. 2 8. 8 10. 8 13. 5	20. 9 26. 1 33. 7 16. 7 19. 8 24. 5	34. 9 43. 2 54. 7 26. 9 32. 4 39. 8	79. 2 96. 3 115 58. 2 69. 4 84. 0	201 227 253 142 165 190
0000	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1.2 1.5 1.9 1.0 1.1 1.4	2.6 3.3 4.3 2.2 2.6 3.2	4.7 5.9 7.7 3.9 4.7 5.8	11. 1 13. 7 17. 8 8. 8 10. 7 13. 3	20. 4 25. 2 32. 5 16. 4 19. 6 24. 0	$\begin{array}{c} 33.\ 5\\ 41.\ 3\\ 52.\ 3\\ 26.\ 3\\ 31.\ 4\\ 38.\ 6\end{array}$	73. 8 89. 3 108 55. 7 66. 0 79. 7	180 206 232 131 152 176

### TENSIONS FOR HARD COPPER

# Table 58.—Stringing Tensions for Medium and Hard-Drawn Bare Solid Copper Wire

HEAVY LOADING DISTRICT

[The tensions being such that when loaded at  $0^{\circ}$  F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B and 60 per cent for grade C]

Size	Grade of	Tem-		Tensio	ns (in p	ounds)	for span	length	s (in fee	et) of—	
A.W.G. No.	construc- tion	pera- ture	100	125	150	175	200	250	300	400	500
8		$egin{array}{c} {}^{\circ}F. \\ {30} \\ {60} \\ {90} \end{array}$	$168 \\ 116 \\ 77$	76 57 48	46 41 38						
6	{A and B . C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$268 \\185 \\124 \\478 \\385 \\297$	$152 \\ 111 \\ 87 \\ 367 \\ 277 \\ 196$	97 82 72 251 183 137	161 128 105			• • • • • • • • • • • • • • • • • • •		
4	{A and B. (C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \\ 90 \end{cases}$	640 496 355 891 748 597	$525 \\ 391 \\ 274 \\ 823 \\ 676 \\ 535$	$\begin{array}{r} 401 \\ 293 \\ 215 \\ 721 \\ 581 \\ 447 \end{array}$	$297 \\ 233 \\ 184 \\ 614 \\ 483 \\ 359$	$228 \\ 192 \\ 166 \\ 502 \\ 387 \\ 300$	$179 \\ 163 \\ 146 \\ 320 \\ 264 \\ 228$	$156 \\ 148 \\ 140 \\ 240 \\ 218 \\ 197$		
2	{A and B. C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1, 104 \\ 875 \\ 639 \\ 1, 448 \\ 1, 216 \\ 976$	$1,023 \\788 \\577 \\1,377 \\1,143 \\913$	911 700 511 1, 305 1, 080 851	$791 \\ 590 \\ 449 \\ 1,226 \\ 997 \\ 794$	$\begin{array}{r} 678 \\ 522 \\ 409 \\ 1, 122 \\ 903 \\ 705 \end{array}$	496 417 349 896 723 572	$\begin{array}{r} 412 \\ 365 \\ 331 \\ 700 \\ 584 \\ 491 \end{array}$	$339 \\ 323 \\ 311 \\ 496 \\ 454 \\ 418$	313 305 295 417 397 378
1	A and B.	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1, 379 1, 080 803 1, 788 1, 486 1, 191	1, 304 1, 008 753 1, 742 1, 435 1, 149	$1, 205 \\944 \\688 \\1, 676 \\1, 386 \\1, 100$	$1, 113 \\ 852 \\ 642 \\ 1, 575 \\ 1, 290 \\ 1, 021$	988 754 590 1, 500 1, 228 970	780 622 518 1, 277 1, 035 812	636 544 484 1, 080 878 731	$518 \\ 481 \\ 452 \\ 780 \\ 684 \\ 615$	$\begin{array}{r} 472 \\ 455 \\ 432 \\ 645 \\ 602 \\ 563 \end{array}$
0	A and B.	90	1, 732 1, 375 1, 007 2, 221 1, 848 1, 476	1, 657 1, 276 954 2, 171 1, 795 1, 434	1, 566 1, 214 896 2, 080 1, 699 1, 351	$1, 471 \\1, 131 \\854 \\1, 994 \\1, 645 \\1, 302$	1, 350 1, 056 808 1, 919 1, 566 1, 247	$1, 143 \\900 \\750 \\1, 740 \\1, 409 \\1, 135$	954 812 692 1, 521 1, 243 1, 018	$\begin{array}{c c} 771 \\ 700 \\ 646 \\ 1, 168 \\ 1, 011 \\ 892 \end{array}$	692 655 622 979 892 825
00	{A and B. {C	90	$\begin{array}{c} 2,128\\ 1,654\\ 1,215\\ 2,731\\ 2,243\\ 1,796 \end{array}$	2, 055 1, 596 1, 178 2, 670 2, 198 1, 743	$\begin{array}{c} 1,982\\ 1,549\\ 1,142\\ 2,608\\ 2,145\\ 1,696 \end{array}$	$\begin{array}{c} 1,878\\ 1,456\\ 1,095\\ 2,513\\ 2,066\\ 1,639 \end{array}$	$1,763 \\1,382 \\1,058 \\2,430 \\1,967 \\1,587$	$\begin{array}{c} 1,538\\ 1,236\\ 1,001\\ 2,231\\ 1,827\\ 1,456 \end{array}$	$1, 366 \\ 1, 142 \\ 960 \\ 2, 042 \\ 1, 696 \\ 1, 383$	1, 116 996 908 1, 669 1, 420 1, 242	$1,001 \\934 \\882 \\1,434 \\1,289 \\1,170$
0000	A and B. C	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right. $	3, 171 2, 426 1, 735 4, 001 3, 270 2, 521	3, 107 2, 392 1, 718 3, 960 3, 238 2, 514	3,080 2,342 1,718 3,928 3,188 2,508	2, 948 2, 292 1, 726 3, 850 3, 129 2, 456	2, 890 2, 250 1, 735 3, 792 3, 070 2, 456	2, 658 2, 083 1, 694 3, 593 2, 948 2, 322	2, 432 2, 010 1, 676 3, 430 2, 831 2, 307	2, 168 1, 885 1, 694 3, 053 2, 581 2, 215	1, 985 1, 810 1, 676 2, 721 2, 390 2, 140

# Table 58.—Stringing Tensions for Medium and Hard-Drawn Bare Solid Copper Wire—Continued

MEDIUM LOADING DISTRICT

[The tensions being such that when loaded at 15° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B and 60 per cent for grade C]

Size	Grade of I	Tem-	2	rensic	ons (ir	ı pour	nds) fe	or spa	n len	gths (	in fee	t) of -	-
A. W. G. No.	construction	pera- ture	100	125	150	175	200	250	300	400	500	700	1, 000
8	∫ <sup>B</sup>	$ \begin{cases} {}^{\circ}F. \\ {}^{30}\\ {}^{60}\\ {}^{90} \end{cases} $	284 225 169	229 175 125	124 89								
0	lc	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	395 338 277	357 299 242									
6	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \end{cases}$	513 421 327 664	470 375 291 634	418 330 247 597	281 212	- 4						
	lc	60     90     90	$571 \\ 477$	542 449	504 414	468 379							
4	A and B	( 90 ( 30		544 1, 050	639 502 1, 018	742 595 470 983	546 424 949	468 377 874	386 326 770	314 285 562			
	(A and B	$\begin{cases} 60 \\ 90 \\ 30 \\ 60 \end{cases}$	922 768 1, 344	1. 330		840 702 1, 230	672 1. 195		533 984	411 794		574	
2	C	$\begin{cases} 90 \\ 30 \\ 60 \end{cases}$	877 1, 659 1, 420	869 1, 642 1, 407		796 1, 571 1, 342	770 1, 540 1, 310	721 1, 477 1, 253	661 1, 382 1, 161	595 1, 184 997	561 1, 010 877	527 786 731	
1	A and B	{ 60   90 [ 30	1,343 1,057 2,022	1, 333 1, 040 2, 012	1, 585 1, 283 1, 005 1, 975	1, 254 990 1, 942	1, 228 973 1, 922	1, 155 914 1, 840	1,080 878 1,755	940 813 1. 588	858 773 1.398	773 734 1, 126	
	(A and B	$\begin{cases} 30 \\ 60 \end{cases}$	2,013 1,636	1,997 1,620	1, 690 1, 392 1, 935 1, 575	1,915	1, 890 1, 536	1,798 1,471	1,700 1,400	1,483 1,251	1,335 1,168	1,152 1,076	
0	{  c	$\begin{cases} 90 \\ 30 \\ 60 \end{cases}$	1,268 2,450 2,089	1,260 2,445 2,072	$ \begin{array}{c} 1,226\\2,433\\2,060\\1,691\end{array} $	1, 223 2, 400 2, 022	1, 223 2, 384 2, 028	1, 165 2, 292 1, 961	1, 148 2, 220 1, 878	1,081 2,055 1.754	1,056 1,844 1,608	1,020 1,567 1,430	
00	A and B	90	1.503	1.508	2, 410 1, 946 1, 508 2, 982 2, 515	1.503	1.482	1.460	1.440	(1.398)	1.388	11.362	1.340
	lc	L 90	2,070	2,070	2,060	2,050	2,019	1, 997	1,940	1,873	1,816	1,732	1, 658
0000	A and B	30	4, 460 3, 728	4, 427 3, 679	3, 570 2, 840 2, 167 4, 400 3, 652 2, 930	4, 360 3, 644	$\frac{4}{3}, \frac{332}{620}$	4, 319 3, 628	4,200 3,552	4, 100 3, 488	3,920 3,388	3, 593	3, 230

#### TENSIONS FOR HARD COPPER

# Table 58.—Stringing Tensions for Medium and Hard-Drawn Bare Solid Copper Wire—Continued

#### LIGHT LOADING DISTRICT

[The tensions being such that when loaded at 30° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B and 60 per cent for grade C]

Size	Grade of	Tem-	,	Fensio	ons (ii	n pou	nds) f	or spa	an len	gths	(in fee	et) of-	
A. W. G. No,	construction	pera- ture	100	125	150	175	200	250	300	400	500	700	1,000
8	ſ <sup>B</sup>	$\circ F. \\ \begin{cases} 30 \\ 60 \\ 90 \end{cases}$	405 345 287	341 282	395 338 281								
	lo	30     60     90     90	488 428 371	486 428 369	484 423 365	479 418 363							
6	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 20 \end{cases}$	628 539 443 758	533 438	618 528 437	434							
	lc	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	662 570	752 658 564	748 656 564		646 554						
4	A and B	$   \begin{cases}     30 \\     60 \\     90 \\     30   \end{cases} $	978 835 684	970 830 683 1, 175	962 820 672	$957 \\ 815 \\ 672 \\ 1 157$	950 805 670	941 796 667	647	738 624	701 603		
	lc	{ 60 90	1, 032 877	1, 025 882	1, 017 871	$1,005 \\ 861$	1, 004 860	992 856	983 845	957 829	928 803		
2	A and B	60     90     90	1,258 1,030	1, 492 1, 255 1, 023 1, 790	1,255 1,028	1,240 1,020	1, 234 1, 013	1,229 1,010	1,203 1,004	1, 169 985	1, 135 979	1, 073 976	
1	lc	{ 60 90	1,557 1,328	1, 545 1, 318	1, 545 1, 313	1, 540 1, 310	1, 540 1, 310	1, 521 1, 292	1,513 1,286	1, 474 1, 279	1,443 1,260	1,372 1,217	
1	A and B	60 90 30	1, 526 1, 231 2, 208	1, 820 1, 523 1, 231 2, 192	1, 523 1, 235 2, 184	1, 506 1, 231 2, 178	1, 506 1, 227 2, 170	1, 504 1, 231 2, 154	1, 465 1, 227 2, 129	1, 445 1, 225 2, 086	1, 412 1, 211 2, 034	1,343 1,218 1,910	1,294 1,211 1,760
-	lc	[ 90	1, 605	1, 890 1, 595	1, 592	1, 589	1, 589	1, 599	1, 569	1, 566	1, 556	1, 526	1, 507
0	A and B	{ 60 90	1, 878 1, 487	2, 230 1, 862 1, 492 2, 680	1, 854 1, 492	1, 845 1, 487	1, 854 1, 496	1,816 1,496	1, 811 1, 500	1, 790 1, 520	1,750 1,512	1, 703 1, 534	1,650 1,546
*	lc	{ 60 90	2, 317 1, 940	2, 300 1, 928	2, 296 1, 928	2, 300 1, 932	2, 283 1, 928	2, 275 1, 940	2, 270 1, 932	2, 238 1, 919	2, 192 1, 915	2, 153 1, 923	2, 051 1, 898
00	A and B	1 90	1,785	2, 702 2, 230 1, 770 3, 270	1,785	1,790	1,810	1,822	1.810	1,867	1,884	1.946	1,946
	lo	{ 60 90	2, 808 2, 351	2, 800 2, 335	2, 782 2, 325	2, 780 2, 320	2, 782 2, 335	2, 780 2, 335	2, 773 2, 331	2, 718 2, 346	2, 711 2, 346	2, 643 2, 372	2, 575 2, 388
0000	A and B	60 90 30 60	3, 320 2, 563 4, 850 4, 100	4,085	3, 303 2, 590 4, 800 4, 052	3, 295 2, 598 4, 790 4, 060	3, 288 2, 590 4, 800 4, 093	3, 279 2, 656 4, 818 4, 070	3, 279 2, 713 4, 790 4, 093	3, 338 2, 780 4, 740 4, 100	3, 295 2, 855 4, 632 4, 038	3, 295 2, 980 4, 550 4, 052	3, 303 3, 097 4, 334 3, 979
		1 90	3, 352	3, 343	3, 329	3, 343	3, 388	3, 402	3, 429	3, 479	3, 492	3, 629	3, 710

# Table 59.—Stringing Tensions for Medium and Hard-Drawn Bare Stranded Copper Wire

#### HEAVY LOADING DISTRICT

[The tensions being such that when loaded at 0° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B and 60 per cent for grade C]

Size	Grade of	Tem-	۲	Tension	ns (in p	ounds)	for span	length	s (in fee	et) of—	
A.W.G. No.	construc- tion	pera- ture	100	125	150	200	250	350	500	700	1,000
4	{A and B C	$ \begin{cases} {}^{\circ}F. \\ {}^{30} \\ {}^{60} \\ {}^{90} \\ {}^{30} \\ {}^{60} \\ {}^{90} \end{cases} $	650 506 368 909 765 621	538 403 288 835 692 550	400 294 218 730 589 454	230 195 170 506 390 301	$176 \\ 160 \\ 147 \\ 323 \\ 269 \\ 228$				
	A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1, 149 915 692 1, 508 1, 274 1, 040	$1,061\\832\\619\\1,440\\1,206\\978$	941 728 536 1, 368 1, 139 910	712 546 426 1, 175 957 759	$525 \\ 432 \\ 374 \\ 957 \\ 764 \\ 614$	$374 \\ 343 \\ 322 \\ 604 \\ 520 \\ 458$	$322 \\ 312 \\ 302 \\ 432 \\ 411 \\ 395$		
1	A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1,439\\1,142\\858\\1,960\\1,564\\1,267$	$1,360 \\ 1,069 \\ 799 \\ 1,802 \\ 1,505 \\ 1,208$	$1, 195 \\983 \\726 \\1, 729 \\1, 432 \\1, 148$	$1,030 \\785 \\614 \\1,551 \\1,267 \\1,010$	$772 \\ 653 \\ 541 \\ 1, 340 \\ 1, 010 \\ 865$	574 515 475 917 779 673	482 462 442 673 627 587	449 442 429 574 554 541	535 528 521
0	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1, 884 1, 511 1, 145 2, 407 2, 034 1, 660	1, 801 1, 436 1, 087 2, 349 1, 975 1, 610	1,710 1,353 1,013 2,274 1,909 1,544	$\begin{array}{c} 1,519\\ 1,204\\ 921\\ 2,117\\ 1,760\\ 1,419 \end{array}$	$1,278 \\1,013 \\822 \\1,926 \\1,486 \\1,287$	$938 \\805 \\722 \\1,519 \\1,262 \\1,013$	764 714 681 1,096 988 905	681 664 896 863 830	647 639 631 805 789 772
00	{A and B {C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	2, 352 1, 869 1, 418 2, 972 2, 489 2, 016	2, 258 1, 806 1, 365 2, 908 2, 436 1, 974	2, 195 1, 733 1, 323 2, 867 2, 394 1, 932	1,9851,5651,1972,7722,3001,869	$\begin{array}{c} 1,775\\ 1,418\\ 1,145\\ 2,531\\ 2,100\\ 1,701 \end{array}$	1,3861,1871,0192,1111,7431,460	$1, 124 \\ 1, 008 \\ 966 \\ 1, 628 \\ 1, 449 \\ 1, 302$	998 966 935 1,323 1,250 1,176	$\begin{array}{r} 935\\924\\914\\1,176\\1,145\\1,113\end{array}$
0000	{A and B C	$\left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right.$	3,752 2,988 2,258 4,665 3,918 3,171	3, 685 2, 955 2, 241 4, 631 3, 884 3, 137	3, 602 2, 888 2, 224 4, 598 3, 851 3, 104	3, 420 2, 756 2, 141 4, 465 3, 735 3, 038	3, 220 2, 590 2, 058 4, 233 3, 552 2, 888	2, 805 2, 341 1, 992 3, 868 3, 270 2, 706	$\begin{array}{c} 2,407\\ 2,158\\ 1,942\\ 3,503\\ 2,905\\ 2,556\end{array}$	$\begin{array}{c} 2,125\\ 1,975\\ 1,876\\ 2,988\\ 2,722\\ 2,523\end{array}$	$1,942 \\1,892 \\1,859 \\2,490 \\2,374 \\2,291$

## TENSIONS FOR HARD COPPER

# Table 59.—Stringing Tensions for Medium and Hard-Drawn Bare Stranded Copper Wire—Continued

#### MEDIUM LOADING DISTRICT

[The tensions being such that when loaded at 15° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B and 60 per cent for grade C]

Size	Grade of	Tem-		Tensior	ns (in po	ounds) i	for span	length	s (in fee	t) of—	
A.W.G. No.	construc- tion	pera- ture	100 .	125	150	200	250	350	500	700	1,000
4	{A and B C	$ \begin{cases} {}^{\circ}F. \\ 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \\ 90 \\ \end{cases} $	866 722 578 1,085 938 794	821 677 534 1,056 910 768	790 650 512 1, 030 883 742	691 557 438 957 816 678	570 454 390 864 726 598	378 326 288 650 544 451			
2	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	1, 383 1, 149 915 1, 700 1, 472 1, 232	1, 352 1, 113 889 1, 685 1, 451 1, 217	1, 316 1, 087 858 1, 659 1, 425 1, 193	1, 217 998 796 1, 586 1, 360 1, 131	1, 128 926 738 1, 513 1, 290 1, 074	910 738 629 1, 323 1, 123 946	692 624 580 1, 040 902 796	580 551 530 796 744 692	528 520 510 681 655 640
1	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1, 709 1, 406 1, 115 2, 086 1, 789 1, 485	1, 670 1, 373 1, 082 2, 066 1, 769 1, 472	1, 637 1, 346 1, 063 2, 039 1, 749 1, 452	1, 558 1, 274 1, 016 1, 987 1, 696 1, 406	1, 452 1, 195 950 1, 894 1, 617 1, 346	1, 261 1, 049 878 1, 709 1, 459 1, 221	983 871 785 1,432 1,241 1,089	838 799 746 1,162 1,049 983	759 739 719 977 937 898
0	A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	2, 170 1, 793 1, 419 2, 656 2, 283 1, 909	2, 158 1, 776 1, 411 2, 639 2, 266 1, 892	2, 100 1, 735 1, 374 2, 598 2, 233 1, 859	2, 034 1, 677 1, 345 2, 565 2, 204 1, 838	1, 930 1, 594 1, 282 2, 473 2, 117 1, 768	1, 726 1, 444 1, 179 2, 324 2, 000 1, 681	$\begin{array}{c} 1,436\\ 1,270\\ 1,129\\ 2,042\\ 1,776\\ 1,536\end{array}$	1, 257 1, 145 1, 071 1, 702 1, 544 1, 403	$1, 112 \\1, 071 \\1, 046 \\1, 444 \\1, 361 \\1, 299$
00	A and B.	$\left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right.$	2, 672 2, 189 1, 727 3, 287 2, 804 2, 331	2, 667 2, 184 1, 722 3, 266 2, 788 2, 315	2, 625 2, 158 1, 701 3, 213 2, 751 2, 279	2, 541 2, 090 1, 670 3, 166 2, 709 2, 252	2, 457 2, 037 1, 638 3, 108 2, 646 2, 205	2, 247 1, 880 1, 565 2, 930 2, 520 2, 121	$\begin{array}{c} 1,953\\ 1,712\\ 1,523\\ 2,657\\ 2,310\\ 2,006 \end{array}$	1, 717 1, 575 1, 470 2, 300 2, 079 1, 880	1, 586 1, 502 1, 449 2, 037 1, 911 1, 827
0000	A and B C	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ .30 \\ 60 \\ 90 \end{array}\right. $	4, 183 3, 436 2, 689 5, 113 4, 366 3, 619	4, 158 3, 420 2, 681 5, 063 4, 334 3, 586	4, 117 3, 386 2, 673 5, 046 4, 316 3, 586	4, 067 3, 353 2, 673 5, 030 4, 299 3, 586	4, 001 3, 320 2, 673 4, 980 4, 266 3, 569	3, 768 3, 204 2, 673 4, 764 4, 100 3, 469	3, 511 3, 046 2, 673 4, 631 3, 951 3, 420	3, 204 2, 922 2, 673 4, 183 3, 768 3, 370	2, 955 2, 805 2, 673 3, 801 3, 519 3, 303

25804°-27-18

# Table 59.—Stringing Tensions for Medium and Hard-Drawn Bare Stranded Copper Wire—Continued

#### LIGHT LOADING DISTRICT

[The tension being such that when loaded at 30° F. the wire will be stressed to 50 per cent of their ultimate strength for grades A and B and 60 per cent for grade C]

Size,	Grade of	Tem-		Tensior	ns (in p	ounds) i	for span	lengths	s (in fee	t) of—	
A.W.Ġ. No.	construc- tion	pera- ture	100	125	150	200	250	350	500	700	1,000
4	{A and B C	$ \begin{cases} {}^{\circ}F. \\ 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \\ 90 \\ \end{cases} $	986 842 698 1, 194 1, 043 899	976 835 692 1, 184 1, 037 893	973 832 688 1, 181 1, 032 890	957 816 678 1, 173 1, 029 883	931 794 662 1, 152 1, 008 869	914 741 626 1, 104 966 832	772 669 582 1,030 902 787		
2	{A and B {C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	1, 537 1, 310 1, 071 1, 851 1, 612 1, 378	1, 534 1, 305 1, 066 1, 846 1, 607 1, 373	1, 521 1, 292 1, 061 1, 841 1, 599 1, 368	1, 503 1, 274 1, 050 1, 812 1, 570 1, 342	1, 477 1, 253 1, 040 1, 794 1, 562 1, 342	1, 417 1, 204 1, 019 1, 752 1, 534 1, 321	1, 310 1, 144 988 1, 680 1, 477 1, 284	1, 160 - 1, 050 946 1, 524 1, 362 1, 217	
1	A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$\begin{array}{c} 1,888\\ 1,591\\ 1,294\\ 2,270\\ 1,960\\ 1,667\end{array}$	1, 881 1, 584 1, 290 2, 264 1, 957 1, 663	1, 868 1, 577 1, 287 2, 254 1, 954 1, 660	$\begin{array}{c} 1,848\\ 1,558\\ 1,277\\ 2,231\\ 1,934\\ 1,643 \end{array}$	$\begin{array}{c} 1,815\\ 1,535\\ 1,271\\ 2,218\\ 1,921\\ 1,637 \end{array}$	$\begin{array}{c} 1,762\\ 1,495\\ 1,267\\ 2,158\\ 1,884\\ 1,620 \end{array}$	1, 643 1, 429 1, 234 2, 072 1, 815 1, 584	1, 492 1, 343 1, 214 1, 921 1, 716 1, 538	1, 350 1, 274 1, 195 1, 736 1, 597 1, 485
0	A and B	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	2, 390 2, 013 1, 635 2, 872 2, 494 2, 121	2, 374 2, 004 1, 631 2, 864 2, 482 2, 117	2, 370 2, 000 1, 631 2, 855 2, 478 2, 112	2, 349 1, 992 1, 631 2, 847 2, 473 2, 108	2, 320 1, 967 1, 631 2, 822 2, 449 2, 092	$\begin{array}{c} 2,258\\ 1,921\\ 1,631\\ 2,764\\ 2,415\\ 2,075 \end{array}$	2, 129 1, 868 1, 619 2, 681 2, 357 2, 050	$\begin{array}{c} 1,975\\ 1,772\\ 1,602\\ 2,523\\ 2,258\\ 2,021 \end{array}$	1, 801 1, 683 1, 594 2, 324 2, 150 1, 975
00	A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$\begin{array}{c} 2,945\\ 2,462\\ 1,995\\ 3,528\\ 3,056\\ 2,573\end{array}$	2, 930 2, 457 1, 995 3, 518 3, 045 2, 573	2, 924 2, 452 1, 995 3, 512 3, 035 2, 573	2, 919 2, 447 1, 995 3, 507 3, 024 2, 573	2, 877 2, 426 1, 995 3, 497 3, 014 2, 573	2, 793 2, 378 2, 011 3, 423 2, 982 2, 557	$\begin{array}{c} 2,667\\ 2,326\\ 2,011\\ 3,339\\ 2,930\\ 2,557\end{array}$	2, 520 2, 263 2, 037 3, 192 2, 856 2, 557	2, 342 2, 184 2, 048 2, 982 2, 741 2, 520
0000	A and B C	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right. $	4, 590 3, 843 3, 088 5, 528 4, 772 4, 034	4, 573 3, 835 3, 088 5, 503 4, 748 4, 017	4, 565 3, 826 3, 088 5, 486 4, 739 4, 000	4, 548 3, 818 3, 121 5, 461 4, 731 4, 000	4, 532 3, 810 3, 154 5, 445 4, 714 4, 000	4, 432 3, 777 3, 204 5, 395 4, 681 4, 009	4, 333 3, 760 3, 254 5, 279 4, 631 4, 034	4, 150 3, 702 3, 337 5, 146 4, 598 4, 117	3, 951 3, 677 3, 428 4, 930 4, 548 4, 178

# Table 60.—Stringing Tensions for Medium and Hard-Drawn T. B. W. P. Solid Copper Wire

HEAVY LOADING DISTRICT

[The tensions being such that when loaded at 0° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B and 60 per cent for grade C]

Size, A. W.G.	Grade of	Tem-	Tensions (in pounds) for span lengths (in feet) of-									
A. W.G. No.	construction	pera- ture	100	125	150	175	200	250	300			
8	с	$\left\{\begin{array}{c}{}^\circ F.\\ 30\\ 60\\ 90\end{array}\right.$	$\begin{array}{c} 114\\ 86\\ 66\end{array}$	63 57 50	50 47 44							
6	A and B	$     \begin{cases}             30 \\             60 \\             90 \\             30             30          $	$194 \\ 138 \\ 107 \\ 408$	$116 \\ 100 \\ 89 \\ 272$	$     \begin{array}{r}       101 \\       85 \\       79 \\       169     \end{array} $	132						
	(C	{ 60 90	315 240	209 158	$\begin{array}{c} 138\\119\end{array}$	115 107						
4	A and B	$     \begin{cases}             30 \\             60 \\             90             90          $	$554 \\ 414 \\ 301$	$     \begin{array}{r}       411 \\       310 \\       231 \\       231     \end{array} $	301 238 195	225 197 174	$     \begin{array}{r}       195 \\       178 \\       168     \end{array} $					
	lc	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	$     \begin{array}{r}       840 \\       692 \\       551     \end{array} $	$738 \\ 592 \\ 465$	$     \begin{array}{r}       602 \\       481 \\       365     \end{array} $	$476 \\ 375 \\ 297$	$362 \\ 300 \\ 251$					
2	A and B	$     \begin{cases}             30 \\             60 \\             90 \\             30             30          $	$1,044 \\ 810 \\ 608 \\ 1,391$	932 716 538 1, 318	786 592 467 1, 198	$\begin{array}{r} 660 \\ 517 \\ 420 \\ 1,093 \end{array}$	559 459 391 978	443 402 363 739	386 355 334 590			
	(C	{ 60 90	1, 160 928	1, 083 875	976 776	870 694	783 629	618 522	522 470			
1	A and B	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \end{array}\right. $	1,327 1,038 773 1,749	1,217 953 694 1,660	$1,090 \\ 845 \\ 642 \\ 1,562$	964 744 600 1, 454	$845 \\ 682 \\ 557 \\ 1,356$	$     \begin{array}{r}       678 \\       573 \\       511 \\       1,097     \end{array} $	586 527 485 917			
	lc	{ 60 90	1, 454 1, 160	1, 363 1, 090	1, 294 1, 022	1, 198 930	1, 087 882	888 753	780 685			
0	A and B	$     \begin{cases}         30 \\         60 \\         90 \\         30     \end{cases} $	$1,686 \\ 1,325 \\ 979 \\ 2,180$	$1,566 \\ 1,230 \\ 900 \\ 2,098$	1, 488 1, 148 880 1, 990	$1, 322 \\ 1, 053 \\ 812 \\ 1, 920$	1, 201 974 783 1, 807	996 858 730 1, 575	871 767 704 1, 334			
	lc	$\begin{cases} 60 \\ 90 \end{cases}$	$1,804 \\ 1,438$	$1,729 \\ 1,372$	1, 645 1, 293	$1,562 \\ 1,256$	1, 496 1, 185	1, 272 1, 077	1, 135 978			
00	A and B	1 90	2,108 1,643 1,221 2,709	1,977 1,549 1,132	1, 883 1, 481 1, 116	$1,754 \\ 1,372 \\ 1,064$	1,657 1,288 1,064	1, 404 1, 190 1, 001	$     \begin{array}{r}       1,252 \\       1,095 \\       970     \end{array}   $			
	lc	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	2, 709 2, 228 1, 774	2,609 2,139 1,706	2, 490 2, 060 1, 617	2, 425 1, 977 1, 586	2, 295 1, 899 1, 492	2, 081 1, 727 1, 403	1, 872 1, 550 1, 335			
0000	A and B	$\left\{\begin{array}{c} 30 \\ 60 \\ 90 \end{array}\right.$	$3,130 \\ 2,408 \\ 1,751$	3, 021 2, 340 1, 717	2, 957 2, 290 1, 735	2, 858 2, 216 1, 735	2,715 2,190 1,726	2, 508 2, 073 1, 701	2, 309 1, 950 1, 710			
	lc	$\left\{\begin{array}{c}30\\60\\90\end{array}\right $	3, 969 3, 238 2, 513	3, 918 3, 187 2, 498	3, 842 3, 120 2, 463	3, 751 3, 052 2, 422	3, 679 3, 029 2, 407	3, 461 2, 847 2, 331	3, 252 2, 680 2, 290			

# Table 60.—Stringing Tensions for Medium and Hard-Drawn T. B. W. P. Solid Copper Wire—Continued

## MEDIUM LOADING DISTRICT

[The tensions being such that when loaded at 15° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B, and 60 per cent for grade C]

Size	Grade of	Tem-	Tensions (in pounds) for span lengths (in feet) of-								
A.W.G. No.	construction	pera- ture	100	125	150	175	200	250	300		
8	{ <sup>B</sup>	$ \begin{cases} {}^{\circ} F. \\ {}^{60} \\ {}^{90} \\ {}^{30} \\ {}^{60} \\ {}^{90} \end{cases} $	$232 \\ 160 \\ 111 \\ 364 \\ 305 \\ 350 $	182 121 94 300 243	133 97 79 237 188						
6	{A and B C		250 469 379 293 628 540 446	194 410 322 246 590 496	148 331 260 200 532 446 265	$264 \\ 215 \\ 173 \\ 465 \\ 384 \\ 306$					
4	{^A and B C	( 30	820 677 533 1,043 892 748	410 766 626 492 1,010 864 720	365 703 572 440 956 809 674	641 514 406 916 771 638	571 456 372 862 718 595				
2	{A and B C	( 30	1, 315 1, 078 856 1, 628 1, 388 1, 161	1, 262 1, 035 812 1, 589 1, 359 1, 127	1, 208 984 788 1, 552 1, 323 1, 094	1, 148 948 742 1, 515 1, 286 1, 075	1, 085 877 713 1, 453 1, 240 1, 025	950 792 648 1, 356 1, 148 958	841 713 616 1,225 1,048 877		
1	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1, 611 1, 326 1, 031 1, 981 1, 694 1, 405	1, 552 1, 271 996 1, 965 1, 676 1, 385	1, 523 1, 235 984 1, 938 1, 651 1, 365	1, 465 1, 195 941 1, 896 1, 598 1, 340	1, 415 1, 153 921 1, 844 1, 576 1, 291	1, 278 1, 051 862 1, 742 1, 484 1, 235	1, 163 960 839 1, 638 1, 385 1, 173		
0	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1, 977 1, 616 1, 248 2, 459 2, 078 1, 704	1, 944 1, 592 1, 244 2, 425 2, 051 1, 691	$1,906 \\1,555 \\1,227 \\2,402 \\2,022 \\1,683$	1,853 1,517 1,194 2,354 1,990 1,654	1, 811 1, 496 1, 190 2, 291 1, 952 1, 596	1, 671 1, 389 1, 135 2, 218 1, 866 1, 563	1, 509 1, 276 1, 065 2, 092 1, 783 1, 484		
00	{A and B C	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right. $	2, 405 1, 946 1, 497 3, 011 2, 537 2, 089	2, 384 1, 941 1, 514 2, 991 2, 520 2, 067	2, 352 1, 910 1, 492 2, 950 2, 472 2, 034	2, 290 1, 878 1, 461 2, 880 2, 437 1, 988	2, 242 1, 826 1, 445 2, 830 2, 400 1, 956	2, 139 1, 774 1, 440 2, 765 2, 332 1, 946	2,030 1,701 1,440 2,671 2,280 1,920		
0000	{ <sup>A</sup> and B C	( 30	3, 601 2, 870 2, 158 4, 415 3, 693 2, 954	3, 552 2, 862 2, 165 4, 391 3, 651 2, 939	3, 544 2, 830 2, 165 4, 359 3, 651 2, 930	3, 470 2, 771 2, 173 4, 341 3, 635 2, 947	3, 460 2, 789 2, 232 4, 300 3, 585 2, 961	3, 329 2, 755 2, 232 4, 200 3, 542 2, 921	3, 252 2, 689 2, 300 4, 118 3, 452 2, 930		

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#### TENSIONS FOR HARD COPPER

# Table 60.—Stringing Tensions for Medium and Hard-Drawn T. B. W. P. Solid Copper Wire—Continued

### LIGHT LOADING DISTRICT

[The tensions being such that when loaded at 30° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B and 60 per cent for grade C]

Size	Grade of	Tem-	Tensions (in pounds) for span lengths (in feet) of								
A.W.G. No.	construction	pera- ture	100	125	150	175	200	250	300		
8	{ <sup>B</sup>	$ \begin{cases} ^{\circ}F. \\                                    $	378 319 261 470	359 303 248 455	336 281 230 443	422					
		{ 60 90 ( 30	410 352 634	395 341 584	384 328 562	366 312 539	512				
6	A and B	60 90	$544 \\ 449$	493 405	477 387	451 373	432 352				
	lc	$     \begin{cases}         30 \\         60 \\         90         \end{bmatrix}     $	747 649 554	727 633 543	709 618 5 <b>2</b> 8	696 605 515	674 584 479				
4	A and B	1 90	951 799 657	940 790 649	920 776 639	890 757 613	860 722 597				
	lo	$     \begin{cases}             30 \\             60 \\             90             90          $	$1,157 \\ 1,014 \\ 864$	$1,144 \\ 992 \\ 847$	1, 133 983 839	1, 122 971 831	1,091 952 805				
2	A and B	1 80	1,476 1,226 1,007	1,460 1,232 1,001	$1,435 \\1,211 \\987$	1,425 1,205 982	$1,383 \\ 1,164 \\ 966$	1,331 1,132 929	1, 284 1, 091 924		
	lc	$     \begin{cases}             30 \\             60 \\             90             90          $	1, 790 1, 545 1, 320	1,779 1,534 1,307	$1,764 \\ 1,529 \\ 1,299$	1,737 1,513 1,278	1, 714 1, 495 1, 271	$1,685 \\ 1,466 \\ 1,255$	$ \begin{array}{c c} 1,633\\ 1,424\\ 1,213 \end{array} $		
1	A and B	1 90	1,808 1,513 1,218	1,792 1,500 1,212	1,781 1,496 1,212	1,755 1,473 1,212	1, 726 1, 441 1, 189	1,686 1,434 1,179	1,644 1,382 1,172		
	lc	{ 30 60 90	2, 188 1, 886 1, 592	2, 170 1, 873 1, 585	2,145 1,864 1,572	2,038 1,847 1,562	2,118 1,815 1,559	2,070 1,801 1,526	2,040 1,778 1,526		
	A and B	{ 30 60 90	2, 230 1, 858 1, 497	2, 198 1, 850 1, 485	2, 185 1, 824 1, 476	2, 163 1, 800 1, 485	2, 152 1, 792 1, 494	2,098 1,792 1,476	2,052 1,734 1,468		
0	lo	{ 30 60 90	2, 682 2, 297 1, 935	2,662 2,297 1,932	2, 650 2, 280 1, 925	2, 638 2, 277 1, 915	2, 623 2, 269 1, 920	2, 575 2, 230 1, 900	2, 529 2, 198 1, 882		
00	A and B	1 90	2,702 2,229 1,774	2,682 2,219 1,774	2,678 2,211 1,790	2, 670 2, 208 1, 800	2,655 2,232 1,795	2, 588 2, 180 1, 800	2,568 2,165 1,832		
	lo	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right. $	3, 271 2, 795 2, 335	3, 267 2, 785 2, 331	3, 232 2, 785 2, 314	3, 232 2, 780 2, 336	3, 209 2, 770 2, 310	3, 171 2, 728 2, 310	3, 140 2, 702 2, 314		
0000	A and B	30     60     90     90     1	4,019 3,288 2,558	4, 010 3, 270 2, 564	4, 010 3, 295 2, 605	4,000 3,303 2,614	3, 960 3, 260 2, 672	3, 884 3, 245 2, 672	3, 850 3, 303 2, 698		
	lc	30 60 90	4, 830 4, 060 3, 343	4, 708 4, 068 3, 320	4, 708 4, 040 3, 338	4, 780 4, 068 3, 370	4, 798 4, 083 3, 402	4, 740 4, 050 3, 387	4, 690 4, 050 3, 379		

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# Table 61 .- Stringing Tensions for T. B. W. P. Solid Soft Copper Wire

### HEAVY LOADING DISTRICT

[The tensions being such that when loaded at 0° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B and 60 per cent for grade C].

Size A. W. G.	Grade of construction	Tem- pera-	Tensions (in pounds) for span lengths (in feet) of—							
No.		ture	100	125	150	175	200			
		° <i>F</i> .								
6	C	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	$58 \\ 54 \\ 49$	$54 \\ 51 \\ 47$	$49 \\ 49 \\ 48$					
	A and B	$\left\{\begin{array}{c} 30 \\ 60 \\ 90 \end{array}\right.$	109 96 88	98 90 85	$91 \\ 88 \\ 81$					
4	.{c	$     \begin{cases}             30 \\             60 \\             90             90          $	$171 \\ 138 \\ 116$	137 121 109	121 112 103					
	A and B	{ 30 60	$324 \\ 248 \\ 201$	$269 \\ 224 \\ 100$	$235 \\ 209 \\ 109$	224 209	219 206			
2	.{	$   \begin{cases}     90 \\     30 \\     60 \\     90   \end{cases} $	$201 \\ 543 \\ 391 \\ 276$	$     \begin{array}{r}       198 \\       433 \\       329 \\       266     \end{array} $	193 349 290 253	196 308 274 248	$     \begin{array}{r}       196 \\       287 \\       261 \\       248     \end{array} $			
	{Λ and B	{ 30 60	$491 \\ 360 \\ 670$	416 328	367 318	334 301	$324 \\ 295 \\ 275$			
1	.} [C	$     \begin{cases}         90 \\         30 \\         60 \\         90     \end{cases}    $	$278 \\ 810 \\ 580 \\ 406$	282 682 507 383	$285 \\ 576 \\ 449 \\ 376$	278 485 416 354	442 393 350			
	{A and B	$\begin{cases} 30 \\ 60 \\ 90 \end{cases}$	783 551	663 497	$588 \\ 485 \\ 414$	534 456	$506 \\ 456 \\ 431$			
0	-{c	$   \begin{cases}     30 \\     60 \\     90   \end{cases} $	$     \begin{array}{r}       414 \\       1,156 \\       824 \\       592     \end{array} $	$     \begin{array}{r}       414 \\       1,024 \\       746 \\       568     \end{array} $	892 680 551	414 787 630 538	713 605 526			
	A and B.	$\begin{cases} 30 \\ 60 \\ 90 \end{cases}$	$1,080 \\ 772 \\ 548$	$991 \\ 731 \\ 574$	898 699 584	798 673 579	757 662 584			
00	[c	$\begin{cases} 30 \\ 60 \\ 90 \end{cases}$	$1,539 \\ 1,120 \\ 782$	$1,424 \\ 1,043 \\ 772$	1, 304 976 778	$1,190 \\ 944 \\ 761$	1,085 887 757			
	A and B	$\begin{cases} 30 \\ 60 \\ 90 \end{cases}$	2,001 1,410 1,020	1,876 1,353 1,020	1,768 1,360 1,062	1,634 1,319 1,070	1,618 1,303 1,136			
0000	-{c	$     \begin{cases}             30 \\             60 \\             90             90          $	2, 622 1, 942 1, 335	2, 522 1, 868 1, 353	2, 422 1, 817 1, 410	2, 273 1, 776 1, 394	2, 233 1, 726 1, 435			

#### TENSIONS FOR SOFT COPPER

# Table 61.—Stringing Tensions for T. B. W. P. Solid Soft Copper Wire— Continued

#### MEDIUM LOADING DISTRICT

[The tensions being such that when loaded at  $15^{\circ}$  F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B and 60 per cent for grade C]

Size	Grade of	Tem-	Tensions (in pounds) for span lengths (in feet) of-								
A. W. G. No.	construction	pera- ture	100	125	150	175	200	250			
6	с	$ \begin{cases} {}^{\circ}F. \\ {}^{30} \\ {}^{60} \\ {}^{90} \end{cases} $	190 137 106	$134 \\ 111 \\ 96$	111 100 91						
4	{A and B	$     \begin{cases}             30 \\             60 \\             90 \\             30             30          $	$298 \\ 212 \\ 161 \\ 461 \\ 0.000 \\ 0.00$	230 183 150 388	193 168 147 309	$     181 \\     161 \\     147 \\     267 \\     267 $					
	(0	{ 60 90	329 235	282 218	244 196	220 196					
2	{A and B	30 60 90 30 60	663 483 336 906 678	590 438 334 820 618	519 407 329 756 572	449 375 318 689 530	$ \begin{array}{c c} 423 \\ 360 \\ 318 \\ 611 \\ 496 \end{array} $				
		1 90	491	462	446	433	417				
1	{A and B C		$\begin{array}{r} 888\\ 632\\ 445\\ 1,160\\ 885\\ 632\end{array}$	$806 \\ 579 \\ 439 \\ 1, 107 \\ 838 \\ 625$	$738 \\ 570 \\ 449 \\ 1,035 \\ 803 \\ 609$	655 537 435 990 753 609	612 518 439 895 702 589	$556 \\ 488 \\ 449 \\ 774 \\ 662 \\ 566$			
0	$ \begin{cases} A \text{ and } B \\ C \end{bmatrix} $	30 60 90 30 60 90	$1,172 \\834 \\601 \\1,508 \\1,152 \\821$	$1,090 \\ 812 \\ 596 \\ 1,450 \\ 1,110 \\ 816$	$1,031 \\775 \\613 \\1,384 \\1,074 \\816$	954 775 613 1, 322 1, 040 812	912 746 618 1,251 995 812	$\begin{array}{r} 804 \\ 708 \\ 622 \\ 1, 123 \\ 958 \\ 800 \end{array}$			
60	{A and B	30 60 90 30 60 90	1, 518 1, 095 772 1, 930 1, 493 1, 069	1,482 1,080 804 1,868 1,461 1,064	1, 393 1, 075 819 1, 836 1, 420 1, 085	1, 351 1, 033 850 1, 806 1, 403 1, 100	1, 278 1, 038 845 1, 696 1, 352 1, 080	1, 185 986 871 1, 581 1, 320 1, 100			
0000	{A and B	<pre>     30     60     90     30     60     90 </pre>	2, 490 1, 826 1, 269 3, 112 2, 390 1, 717	2, 458 1, 801 1, 320 3, 090 2, 408 1, 760	2, 423 1, 801 1, 394 3, 030 2, 373 1, 777	2, 315 1, 801 1, 403 2, 988 2, 341 1, 835	2, 290 1, 809 1, 469 2, 988 2, 350 1, 892	2, 165 1, 809 1, 527 2, 808 2, 291 1, 900			
0000	1	30 60 90 30 60	2, 490 1, 826 1, 269 3, 112 2, 390	2, 458 1, 801 1, 320 3, 090 2, 408	2, 423 1, 801 1, 394 3, 030 2, 373	2, 315 1, 801 1, 403 2, 988 2, 341	2, 290 1, 809 1, 469 2, 988 2, 350				

# Table 61.—Stringing Tensions for T. B. W. P. Solid Soft Copper Wire— Continued

## LIGHT LOADING DISTRICT

[The tensions being such that when loaded at 30° F. the wires will be stressed to 50 per cent of their ultimate strength for grades A and B and 60 per cent for grade C]

Size A. W. G.	Grade of construction	Tem- pera-	Tension	s (in pou	nds) for s	span leng	gths (in f	III leet) oi—		
No.	construction	ture	100	125	150	175	200	250		
6	{A and B	$ \left\{ \begin{array}{c} \circ \ F, \\ 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array} \right. $	279 202 148 384 303 224	239 181 142 342 262 199	206 167 135 314 239 190					
4	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	514 383 269 648 508 381	469 347 266 619 491 362	434 334 258 594 463 355	381 311 248 554 438 342	346 290 241 508 404 332			
2	{A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{r} 882\\ 663\\ 480\\ 1,106\\ 880\\ 653\end{array}$	$846 \\ 650 \\ 475 \\ 1,078 \\ 848 \\ 647$	$809 \\ 619 \\ 475 \\ 1,044 \\ 833 \\ 640$	$772 \\ 600 \\ 485 \\ 1,010 \\ 802 \\ 624$	731 584 485 969 783 629	658 558 480 904 736 619		
1	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1,136\\852\\608\\1,375\\1,087\\813$	$1,081 \\ 826 \\ 609 \\ 1,362 \\ 1,087 \\ 819$	$1,055\\822\\619\\1,340\\1,054\\816$	$1,028\\800\\619\\1,304\\1,035\\816$	983 780 638 1, 267 1, 041 813	894 750 622 1, 199 982 813		
0	{A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1,450 \\1,090 \\783 \\1,745 \\1,396 \\1,040$	1,409 1,069 787 1,712 1,360 1,032	1,3671,0698081,7071,3601,056	1, 359 1, 060 812 1, 683 1, 355 1, 060	$1,310 \\ 1,027 \\ 842 \\ 1,637 \\ 1,360 \\ 1,056$	1, 214 1, 019 871 1, 567 1, 277 1, 060		
00	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1,830 \\1,387 \\981 \\2,211 \\1,764 \\1,315$	1,800 1,366 1,012 2,207 1,757 1,330	1, 778 1, 382 1, 064 2, 180 1, 747 1, 352	$1,742 \\1,387 \\1,064 \\2,140 \\1,711 \\1,357$	$1,721 \\1,387 \\1,095 \\2,150 \\1,726 \\1,394$	$1,622 \\1,345 \\1,121 \\2,070 \\1,706 \\1,394$		
0000	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 2,962\\ 2,281\\ 1,610\\ 3,538\\ 2,822\\ 2,090 \end{array}$	2, 952 2, 273 1, 676 3, 543 2, 848 2, 159	2, 898 2, 232 1, 693 3, 520 2, 822 2, 159	2, 862 2, 250 1, 760 3, 494 2, 839 2, 190	2, 798 2, 265 1, 768 3, 452 2, 789 2, 232	2, 771 2, 258 1, 867 3, 403 2, 807 2, 282		

# Table 62 .-- Stringing Tensions for Ordinary Grade Steel Wire

#### HEAVY LOADING DISTRICT

[At 30, 60, and 90° F. without load, the tensions being such that when loaded at 0° F. the wire will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

Steel wire Grade of		Tem-		Tensions (in pounds) for span lengths (in feet) of-											
gage No.	construction	pera- ture	100	125	150	175	200	250	300	400	500				
8	c	${f \circ}_{F.}^{\circ} F. \\ \left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	260 165 110	130 99 83	89 79 70										
6	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	320 200 135 580 430 280	190 140 115 450 300 210	$135 \\ 120 \\ 105 \\ 300 \\ 220 \\ 160$	210 170 145	170 150 130	140 130 125	125 120 115	115 110 110	110 110 110 110				
4	A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	640 430 270 970 740 530	480 330 230 850 630 440	$360 \\ 260 \\ 210 \\ 710 \\ 510 \\ 360$	$280 \\ 230 \\ 195 \\ 560 \\ 410 \\ 310$	$240 \\ 210 \\ 185 \\ 450 \\ 340 \\ 280$	200 185 175 310 270 240	185 180 170 260 240 220	$175 \\ 170 \\ 165 \\ 220 \\ 220 \\ 210$	$     \begin{array}{r}       165 \\       165 \\       210 \\       210 \\       200 \\       \end{array} $				

MEDIUM LOADING DISTRICT

[At 30, 60, and 90° F. without load, the tensions being such that when loaded at  $15^{\circ}$  F. the wire will be stressed to 50 per cent of ultimate strength for Grades A and B, and to 60 per cent for grade C]

8	С	$\Big\{\begin{array}{c} 30 \\ 60 \\ 90 \end{array}$	580 460 340	520 400 300	450 340 240						
6	A and B C	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right. $	670 500 360 880 710	610 450 310 830 660	530 380 270 780 610	710	640 490	500 390	380 320	280 260	230 220
4	{A and B C	$   \begin{cases}     90 \\     60 \\     90 \\     30 \\     60 \\     90   \end{cases} $	550 980 760 550 1, 250 1, 030 800	500 930 710 510 1, 220 990 770	460 870 650 470 1, 170 950 730	410 790 600 430 1, 110 890 680	370 720 540 410 1,050 840 640	310 590 460 370 920 730 570	270 480 400 340 780 630 510	230 370 340 310 550 480 420	210 340 320 300 480 440 400

## Table 62.—Stringing Tensions for Ordinary Grade Steel Wire— Continued

#### LIGHT LOADING DISTRICT

[At 30, 60, and 90° F. without load, the tensions being such that when loaded at 30° F. the wire will be stressed to 50 per cent of ultimate strength for grades A and B and to 60 per cent for grade C]

Steel wire	Grade of	Tem-	Tensions (in pounds) for span lengths (in feet) of-										
gage No.	construction	pera- ture	100	125	150	175	200	250	300	400	500		
8	C	$ \begin{array}{c} ^{\circ}F.\\ 30\\ 60\\ 90\\ \end{array} $	730 610 490 850	720 610 490 840	710 600 480 830								
6	A and B C	$ \begin{cases}     60 \\     90 \\     30 \\     60 \\     90 \end{cases} $	680 520 1, 030 870 700	670 520 1, 030 860 690	$ \begin{array}{r}     660 \\     510 \\     1,020 \\     850 \\     690 \\   \end{array} $	$1,010 \\ 850 \\ 680$	$1,000 \\ 840 \\ 680$	970 820 660	$940 \\ 790 \\ 640$	870 730 610	800 680 580		
4	{A and B {C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1, 180 \\950 \\720 \\1, 420 \\1, 190 \\970$	$1, 170 \\940 \\720 \\1, 420 \\1, 190 \\960$	1, 160 930 720 1, 410 1, 180 960	$1, 150 \\920 \\720 \\1, 400 \\1, 170 \\950$	$1, 140 \\910 \\710 \\1, 390 \\1, 170 \\950$	1, 110 890 700 1, 370 1, 150 930	$1,070 \\ 860 \\ 690 \\ 1,340 \\ 1,120 \\ 910$	$970 \\ 810 \\ 680 \\ 1,260 \\ 1,060 \\ 880$	$\begin{array}{r} 860 \\ 760 \\ 660 \\ 1, 180 \\ 1, 010 \\ 860 \end{array}$		

# Table 63 .- Stringing Tensions for Siemens-Martin Steel Wire

#### HEAVY LOADING DISTRICT

[At 30, 60, and 90° F., without load, the tensions being such that when loaded at 0 °F., the wire will be stressed to 50 per cent of ultimate strength for grades A and B and to 60 per cent for grade C]

Steel wire	Grade of construc-	Tein-	Ten	sions (i	n poune	ls) for s	pan len	gths (in	feet) o	f—
gage No.	tion	pera- ture	200	250	300	400	500	600	700	1,000
6	c	${ { 8 F. \\ 30 \\ 60 \\ 90 } }$	$440 \\ 330 \\ 250$	260 220 190	200 185 170	$160 \\ 155 \\ 150$	$150 \\ 150 \\ 145$	$145 \\ 145 \\ 140$	140 140 140	
4	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	530 400 310 1,000 780 590	$350 \\ 290 \\ 260 \\ 730 \\ 570 \\ 440$	$280 \\ 260 \\ 240 \\ 520 \\ 420 \\ 360$	$240 \\ 230 \\ 220 \\ 340 \\ 320 \\ 300 \\ 300$	$\begin{array}{c} 220 \\ 220 \\ 210 \\ 300 \\ 290 \\ 280 \end{array}$	$210 \\ 210 \\ 210 \\ 270 \\ 270 \\ 260$	$210 \\ 210 \\ 200 \\ 270 \\ 260 \\ 260 \\ 260$	$260 \\ 260 \\ 260 \\ 260$

#### MEDIUM LOADING DISTRICT

[At 30, 60, and 90° F., without load, the tensions being such that when loaded at 15° F., the wire will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

6 C	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	$1,010 \\ 820 \\ 690$	890 730 580	760 620 490	$520 \\ 440 \\ 380$	390 350 320	330 310 300	300 290 280	$270 \\ 270 \\ 260$
4	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1, 130 910 700 1, 500 1, 280 1, 060	$1,020 \\810 \\640 \\1,410 \\1,180 \\970$	860 690 560 1, 300 1, 090 890	$640 \\ 550 \\ 470 \\ 1,060 \\ 880 \\ 730$	520 470 430 830 720 620	$\begin{array}{r} 450 \\ 430 \\ 400 \\ 670 \\ 610 \\ 550 \end{array}$	$\begin{array}{r} 430 \\ 410 \\ 390 \\ 590 \\ 550 \\ 520 \end{array}$	$390 \\ 380 \\ 370 \\ 490 \\ 480 \\ 470$

#### LIGHT LOADING DISTRICT

[At 30, 60, and 90° F., without load, the tensions being such that when loaded at 30° F., the wire will be stressed to 50 per cent of ultimate strength for grades A and B and to 60 per cent for grade C]

6	с	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	1, 280 1, 110 940	1, 260 1, 090 930	1, 240 1, 080 920	1, 190 1, 030 880	1, 130 980 840	1, 060 920 800	1,000 880 770	830 760 700
4	{A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1, 450 1, 230 1, 000 1, 770 1, 540 1, 310	$1, 430 \\1, 210 \\990 \\1, 750 \\1, 530 \\1, 300$	1,400 1,180 980 1,730 1,510 1,290	$\begin{array}{c} 1, 330 \\ 1, 130 \\ 950 \\ 1, 680 \\ 1, 460 \\ 1_{\psi} 260 \end{array}$	1, 260 1, 080 920 1, 620 1, 410 1, 220	1, 180 1, 020 890 1, 540 1, 350 1, 170	1, 110 980 870 1, 480 1, 300 1, 140	960 890 830 1, 280 1, 160 1; 060

# Table 64.-Stringing Tensions for High-Tension Steel Wire

### HEAVY LOADING DISTRICT

[At 30, 60, and 90° F., without load, the tensions being such that when loaded at 0° F., the wire will be stressed to 50 per cent of ultimate strength for grades A and B and to 60 per cent for grade C]

Steel wire	Grade of construc-	Tèm-	Ter	isions (i	n poun	ds) for s	pan len	gths (in	feet) of	í—
gage No.	tion	pera- ture	200	250	300	400	500	600	700	1,000
6	σ	$egin{pmatrix} {}^{\circ}F. \\ {30} \\ {60} \\ {90} \end{smallmatrix}$	1, 730 1, 570 1, 400	1, 590 1, 430 1, 260	1, 420 1, 260 1, 100	960 810 680	560 480 420	400 380 350	330 320 300	250 250 250
4	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1, 970 1, 730 1, 500 2, 560 2, 330 2, 100	1, 800 1, 570 1, 340 2, 430 2, 190 1, 960	1, 590 1, 370 1, 160 2, 280 2, 050 1, 820	$1, 110 \\930 \\770 \\1, 940 \\1, 720 \\1, 500$	710 620 550 1, 500 1, 290 1, 110	540 500 460 1,070 930 820	470 440 420 790 710 650	390 380 370 520 500 490

#### MEDIUM LOADING DISTRICT

[At 30, 60, and 90° F. without load, the tensions being such that when loaded at 15° F. the wire will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

6	с	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	2,000 1,820 1,660	1, 970 1, 800 1, 630	1, 920 1, 750 1, 580	1, 790 1, 620 1, 460	1, 640 1, 480 1, 320	1, 440 1, 290 1, 140	1,220 1,090 960	740 690 630
4	{A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	2, 290 2, 060 1, 830 2, 810 2, 580 2, 350	2, 240 2, 010 1, 780 2, 770 2, 540 2, 310	2, 180 1, 950 1, 720 2, 730 2, 500 2, 270	2,020 1,800 1,580 2,620 2,400 2,170	1, 830 1, 620 1, 420 2, 480 2, 250 2, 030	1, 620 1, 430 1, 250 2, 320 2, 100 1, 880	1, 400 1, 230 1, 080 2, 140 1, 930 1, 730	950 880 820 1, 540 1, 390 1, 260

#### LIGHT LOADING DISTRICT

[At 30, 60, and 90° F, without load, the tensions being such that when loaded at 30° F. the wire will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

6	с	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \end{array} \right.$	2, 160 1, 980 1, 820	2, 150 1, 980 1, 820	2, 140 1, 970 1, 810	2, 120 1, 950 1, 800	2, 100 1, 930 1, 770	2, <b>0</b> 80 1, 910 1, 750	2,060 1,890 1,720	1, 910 1, 750 1, 610
4	A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	2, 470 2, 240 2, 020 2, 980 2, 750 2, 530	2, 470 2, 230 2, 010 2, 970 2, 740 2, 520	2, 450 2, 220 1, 990 2, 960 2, 730 2, 510	2, 430 2, 200 1, 970 2, 940 2, 710 2, 490	2, 400 2, 180 1, 950 2, 920 2, 690 2, 470	2, 350 2, 140 1, 910 2, 890 2, 660 2, 440	2, 310 2, 090 1, 870 2, 860 2, 640 2, 420	2, 130 1, 940 1, 770 2, 730 2, 520 2, 320

# Table 65.—Stringing Tensions for Ordinary Grade Steel Cable

### HEAVY LOADING DISTRICT

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[At 30, 60, and 90° F. without load, the tensions being such that when loaded at 0° F. the cable will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

Cable diam-	Grade of	Tem-	ę	<b>Fension</b>	s (in po	ounds)	for spar	length	s (in fe	et) of—	
eter (inches)	construc- tion	pera- ture	100	125	150	175	200	250	300	400	500
1⁄4	A and B C	$ \begin{cases} {}^{\circ}F. \\ 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases} $	470 340 230 770 610 470	320 230 175 630 500 360	220 175 150 480 370 270	170 150 135 350 270 220	150 140 130 260 220 190	130 125 120 195 180 165	$125 \\ 125 \\ 120 \\ 170 \\ 160 \\ 155$	120 115 115 150 150 145	$     \begin{array}{r}       115 \\       115 \\       115 \\       145 \\       140 \\       135     \end{array} $
<mark>л</mark> е	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1, 140 \\900 \\670 \\1, 550 \\1, 290 \\1, 040$	$1,010 \\780 \\580 \\1,440 \\1,190 \\960$	880 670 500 1, 330 1, 100 870	740 560 450 1, 210 990 780	$\begin{array}{r} 610\\ 490\\ 410\\ 1,090\\ 880\\ 690\end{array}$	450 400 360 820 680 550	390 360 340 620 550 480	$340 \\ 330 \\ 320 \\ 480 \\ 450 \\ 420$	330 320 320 420 410 390
<sup>3</sup> ⁄8	{A and B C	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array} \right.$	1, 680 1, 350 1, 020 2, 200 1, 850 1, 510	$\begin{array}{c} 1,580\\ 1,260\\ 950\\ 2,130\\ 1,780\\ 1,460 \end{array}$	$1, 460 \\1, 150 \\870 \\2, 030 \\1, 690 \\1, 370$	$1,320 \\1,040 \\800 \\1,920 \\1,590 \\1,280$	$1,180 \\930 \\740 \\1,800 \\1,480 \\1,170$	920 770 660 1, 530 1, 260 1, 020	780 690 620 1, 280 1, 070 910	640 600 560 940 840 770	580 560 540 800 760 710
1 <del>7</del>	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	2, 570 2, 080 1, 600 3, 280 2, 780 2, 280	2, 480 2, 000 1, 540 3, 210 2, 710 2, 220	2, 370 1, 900 1, 480 3, 130 2, 640 2, 160	2, 260 1, 810 1, 420 3, 040 2, 560 2, 100	2, 140 1, 710 1, 360 2, 940 2, 470 2, 020	$\begin{array}{c} 1,870\\ 1,530\\ 1,250\\ 2,700\\ 2,250\\ 1,860 \end{array}$	$\begin{array}{c} 1, 630 \\ 1, 370 \\ 1, 170 \\ 2, 450 \\ 2, 060 \\ 1, 720 \end{array}$	1, 320 1, 180 1, 080 1, 990 1, 730 1, 510	1, 180 1, 110 1, 050 1, 690 1, 520 1, 390
¥	A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	3, 120 2, 520 1, 940 3, 970 3, 380 2, 780	3,020 2,460 1,910 3,900 3,300 2,720	2, 930 2, 380 1, 860 3, 830 3, 230 2, 660	2, 830 2, 290 1, 800 3, 740 3, 150 2, 590	2,720 2,180 1,730 3,640 3,070 2,520	2, 470 1, 980 1, 630 3, 420 2, 880 2, 380	2, 200 1, 840 1, 550 3, 180 2, 670 2, 240	1, 790 1, 590 1, 420 2, 720 2, 330 2, 030	$\begin{array}{c} 1,600\\ 1,480\\ 1,380\\ 2,320\\ 2,060\\ 1,860 \end{array}$
9 18	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	4, 210 3, 440 2, 670 5, 310 4, 500 3, 700	4, 150 3, 380 2, 630 5, 280 4, 470 3, 680	4,070 3,300 2,580 5,230 4,420 3,650	3, 960 3, 230 2, 530 5, 140 4, 350 3, 600	3, 840 3, 150 2, 480 5, 050 4, 280 3, 540	3,600 2,960 2,410 4,840 4,100 3,400	3, 380 2, 800 2, 350 4, 590 3, 900 3, 270	2,930 2,560 2,260 4,140 3,560 3,080	2, 620 2, 380 2, 180 3, 720 3, 290 2, 920
<u>5/8</u>	A and B C	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right. $	5, 250 4, 280 3, 340 6, 550 5, 570 4, 560	5, 160 4, 190 3, 290 6, 500 5, 530 4, 540	5,070 4,140 3,250 6,440 5,480 4,500	4, 980 4, 060 3, 220 6, 370 5, 410 4, 470	4, 880 3, 990 3, 180 6, 280 5, 340 4, 430	4, 660 3, 830 3, 140 6, 100 5, 190 4, 310	4, 390 3, 680 3, 080 5, 860 4, 980 4, 210	3, 960 3, 440 2, 980 5, 410 4, 660 4, 030	3, 590 3, 240 2, 930 4, 970 4, 380 3, 880

# Table 65.-Stringing Tensions for Ordinary Grade Steel Cable-Con.

MEDIUM LOADING DISTRICT

 $[A\,t\,30,\,60,\,and\,90^\circ$  F. without load, the tensions being such that when loaded at 15° F. the cable will be stressed to 50 per cent of ultimate strength for grades A and B and to 60 per cent for grade C]

Cable diam-	Grade of	Tem-	1	Tensi	ons (in j	pounds)	) for spa	n lengti	hs (in fe	et) of—	
eter (inches)	construc- tion	pera- ture	100	125	150	175	200	250	300	400	500
1⁄4	{A and B C	$ \begin{cases} {}^{\circ}F. \\ 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases} $	770 630 480 990 850 700	710 570 440 950 800 660	640 510 390 900 760 620	570 450 350 840 700 570	500 390 310 780 650 520	$370 \\ 310 \\ 270 \\ 640 \\ 530 \\ 430$	$300 \\ 260 \\ 240 \\ 520 \\ 440 \\ 370$	250 230 220 360 330 300	230 220 210 300 280 270
, 16	$\begin{cases} A and B_{-} \\ C_{-} \end{cases}$	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1, 420 1, 180 930 1, 790 1, 540 1, 320	$\begin{array}{c} 1,380\\ 1,140\\ 900\\ 1,760\\ 1,500\\ 1,270 \end{array}$	1, 330 1, 100 870 1, 730 1, 470 1, 230	$1,290 \\1,040 \\830 \\1,690 \\1,440 \\1,190$	$1,220 \\990 \\790 \\1,640 \\1,400 \\1,150$	$1,090 \\880 \\720 \\1,520 \\1,290 \\1,070$	950 800 670 1, 390 1, 190 990	750 670 590 1, 150 990 850	650 600 560 950 850 770
3⁄8	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	2,000 1,640 1,310 2,470 2,120 1,780	1,960 1,610 1,290 2,440 2,100 1,760	$\begin{array}{c} 1,910\\ 1,580\\ 1,260\\ 2,420\\ 2,070\\ 1,740 \end{array}$	$\begin{array}{c} 1,860\\ 1,550\\ 1,230\\ 2,380\\ 2,040\\ 1,710 \end{array}$	$\begin{array}{c} 1,810\\ 1,510\\ 1,200\\ 2,340\\ 2,000\\ 1,670 \end{array}$	$\begin{array}{c} 1, 690 \\ 1, 410 \\ 1, 140 \\ 2, 240 \\ 1, 910 \\ 1, 610 \end{array}$	$\begin{array}{c} 1,550\\ 1,300\\ 1,080\\ 2,120\\ 1,810\\ 1,520 \end{array}$	1, 320 1, 140 1, 010 1, 860 1, 610 1, 390	1, 150 1, 040 950 1, 640 1, 460 1, 280
<del>1</del> 6	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$\begin{array}{c} 2,940\\ 2,430\\ 1,940\\ 3,600\\ 3,100\\ 2,600 \end{array}$	2, 890 2, 400 1, 920 3, 580 3, 080 2, 580	2, 860 2, 370 1, 890 3, 560 3, 060 2, 560	2, 830 2, 330 1, 870 3, 530 3, 030 2, 540	2,780 2,300 1,860 3,490 3,000 2,520	2, 660 2, 220 1, 820 3, 400 2, 930 2, 470	2, 540 2, 140 1, 780 3, 310 2, 840 2, 410	2, 320 1, 990 1, 720 3, 080 2, 670 2, 310	2,090 1,840 1,660 2,830 2,500 2,190
1⁄2	{ A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3, 520 2, 920 2, 330 4, 310 3, 720 3, 120	3,500 2,900 2,320 4,300 3,710 3,110	3, 460 2, 860 2, 300 4, 290 3, 700 3, 100	3, 420 2, 830 2, 290 4, 260 3, 670 3, 080	$\begin{array}{c} 3,380\\ 2,800\\ 2,270\\ 4,220\\ 3,630\\ 3,060 \end{array}$	$\begin{array}{c} 3,260\\ 2,740\\ 2,230\\ 4,130\\ 3,560\\ 3,010 \end{array}$	$\begin{array}{c} 3,140\\ 2,640\\ 2,200\\ 4,050\\ 3,480\\ 2,950 \end{array}$	2,900 2,500 2,160 3,800 3,300 2,850	2,660 2,370 2,110 3,560 3,120 2,750
9 16	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	4, 720 3, 940 3, 160 5, 800 5, 000 4, 190	4, 700 3, 920 3, 150 5, 770 4, 970 4, 180	4, 670 3, 880 3, 140 5, 740 4, 940 4, 160	4, 630 3, 850 3, 130 5, 710 4, 920 4, 150	4, 580 3, 820 3, 120 5, 690 4, 900 4, 140	4, 470 3, 760 3, 100 5, 610 4, 850 4, 100	$\begin{array}{c} 4,360\\ 3,690\\ 3,080\\ 5,510\\ 4,790\\ 4,060\end{array}$	4, 110 3, 540 3, 060 5, 310 4, 630 3, 980	$\begin{array}{c} 3,900\\ 3,440\\ 3,040\\ 5,110\\ 4,470\\ 3,920 \end{array}$
<sup>5</sup> ⁄s	A and B C	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \\ 90 \end{array}\right. $	5,800 4,830 3,880 7,110 6,110 5,110	5,770 4,800 3,860 7,070 6,100 5,110	5, 740 4, 780 3, 860 7, 050 6, 090 5, 110	5,7104,7503,8707,0306,0805,110	5,670 4,730 3,880 7,000 6,060 5,110	5,560 4,670 3,880 6,940 6,000 5,110	5, 440 4, 620 3, 880 6, 870 5, 940 5, 970	5, 220 4, 540 3, 890 6, 680 5, 790 5, 000	4, 970 4, 400 3, 890 6, 400 5, 600 4, 940

# Table 65.-Stringing Tensions for Ordinary Grade Steel Cable-Con.

LIGHT LOADING DISTRICT

[At 30, 60, and 90° F. without load, the tensions being such that when loaded at 30° F. the cable will be stressed to 50 per cent of ultimate strength for grades A and B and to 60 per cent for grade C]

Cable diam-	Grade of	Tem-		Tensio	ns (in p	ounds)	for span	length	s (in fee	t) of	
eter (inches)	construc- tion	pera- ture	100	125	150	175	200	250	300	400	500
1/4	A and B C	$ \begin{cases} {}^{\circ}F. \\ {}^{60} \\ {}^{90} \\ {}^{30} \\ {}^{60} \\ {}^{90} \end{cases} $	930 790 640 1, 160 970 820	920 770 620 1, 140 960 810	900 760 620 1,120 950 800	890 740 600 1,100 940 790	870 720 590 1,080 930 780	820 690 570 1,050 900 760	770 660 540 1,010 870 730	690 590 510 930 800 690	$610 \\ 540 \\ 480 \\ 850 \\ 740 \\ 640$
<u>5</u> 16	{A and B (C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1, 620 1, 370 1, 120 1, 960 1, 710 1, 460	1,610 1,360 1,100 1,950 1,700 1,450	1,600 1,340 1,100 1,940 1,690 1,440	1, 580 1, 330 1, 090 1, 930 1, 680 1, 430	1, 550 1, 310 1, 080 1, 920 1, 670 1, 420	1, 520 1, 280 1, 070 1, 880 1, 640 1, 400	1,470 1,260 1,060 1,850 1,610 1,380	1, 380 1, 200 1, 030 1, 760 1, 540 1, 330	$\begin{array}{c} 1, 290 \\ 1, 140 \\ 1, 010 \\ 1, 670 \\ 1, 470 \\ 1, 270 \end{array}$
<sup>3</sup> ⁄8	{A and B {C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	2, 220 1, 870 1, 530 2, 680 2, 340 1, 990	2, 210 1, 860 1, 530 2, 670 2, 330 1, 980	2, 200 1, 850 1, 520 2, 660 2, 320 1, 970	2, 180 1, 840 1, 520 2, 650 2, 310 1, 960	2, 160 1, 830 1, 510 2, 640 2, 300 1, 950	2, 130 1, 810 1, 500 2, 600 2, 280 1, 940	2,080 1,770 1,480 2,580 2,260 1,930	1, 980 1, 710 1, 470 2, 490 2, 180 1, 890	1,870 1,650 1,450 2,380 2,100 1,850
<del>1</del> 6	A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3, 230 2, 730 2, 230 3, 890 3, 390 2, 890	3, 220 2, 720 2, 230 3, 880 3, 380 2, 880	3, 200 2, 710 2, 220 3, 870 3, 370 2, 880	3, 190 2, 700 2, 220 3, 860 3, 360 2, 880	3, 180 2, 680 2, 220 3, 850 3, 360 2, 870	3, 140 2, 660 2, 220 3, 820 3, 340 2, 860	3, 100 2, 640 2, 220 3, 780 3, 320 2, 830	3,000 2,600 2,230 3,710 3,260 2,840	2, 880 2, 530 2, 230 3, 620 3, 220 2, 820
1⁄2	A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3, 880 3, 270 2, 680 4, 660 4, 050 3, 460	$\begin{array}{c} 3,860\\ 3,260\\ 2,680\\ 4,660\\ 4,050\\ 3,460\end{array}$	$\begin{array}{c} 3,850\\ 3,260\\ 2,680\\ 4,650\\ 4,050\\ 3,460 \end{array}$	3, 840 3, 250 2, 680 4, 640 4, 040 3, 460	3, 820 3, 240 2, 680 4, 630 4, 030 3, 460	$\begin{array}{c} 3,770\\ 3,220\\ 2,680\\ 4,600\\ 4,000\\ 3,450 \end{array}$	3, 720 3, 180 2, 680 4, 550 3, 970 3, 440	$\begin{array}{c} 3,620\\ 3,120\\ 2,690\\ 4,450\\ 3,920\\ 3,420 \end{array}$	3, 500 3, 060 2, 700 4, 360 3, 870 3, 390
9 16	A and B C	$   \begin{cases}     90 \\     30 \\     60 \\     90   \end{cases} $	5, 160 4, 370 3, 580 6, 210 5, 410 4, 610		$5,140 \\ 4,350 \\ 3,580 \\ 6,190 \\ 5,390 \\ 4,600$	$\begin{array}{c} 5,120\\ 4,340\\ 3,580\\ 6,180\\ 5,380\\ 4,600 \end{array}$	$5,100\\4,330\\3,590\\6,170\\5,370\\4,600$	$\begin{bmatrix} 5,070\\ 4,300\\ 3,600\\ 6,150\\ 5,360\\ 4,610 \end{bmatrix}$	$\begin{array}{c} 5,040\\ 4,290\\ 3,620\\ 6,110\\ 5,350\\ 4,620 \end{array}$	4, 920 4, 250 3, 670 6, 030 5, 320 4, 630	4,800 4,210 3,710 5,940 5,260 4,640
5⁄8	{A and B C	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right. $	$\begin{array}{c} 6, 330 \\ 5, 360 \\ 4, 390 \\ 7, 620 \\ 6, 620 \\ 5, 650 \end{array}$	$\begin{array}{c} 6, 310 \\ 5, 350 \\ 4, 390 \\ 7, 610 \\ 6, 610 \\ 5, 640 \end{array}$	$\begin{array}{c} 6,300\\ 5,340\\ 4,390\\ 7,600\\ 6,610\\ 5,640 \end{array}$	$\begin{array}{c} 6, 290 \\ 5, 320 \\ 4, 400 \\ 7, 590 \\ 6, 610 \\ 5, 640 \end{array}$	$\begin{array}{c} 6,280\\ 5,310\\ 4,400\\ 7,580\\ 6,610\\ 5,650 \end{array}$	$\begin{array}{c} 6, 240 \\ 5, 300 \\ 4, 420 \\ 7, 560 \\ 6, 600 \\ 5, 680 \end{array}$	$\begin{array}{c} 6,200\\ 5,270\\ 4,450\\ 7,510\\ 6,590\\ 5,690 \end{array}$	$\begin{array}{c} 6,080\\ 5,250\\ 4,520\\ 7,410\\ 6,550\\ 5,700 \end{array}$	5, 980 5, 230 4, 590 7, 330 6, 500 5, 720
	-		1	1	i	1					

# Table 66 .- Stringing Tensions for Siemens-Martin Steel Cable

HEAVY LOADING DISTRICT

[At 30, 60, and 90° F. without load, the sags being such that when loaded at 0° F. the cable will be stressed to 50 per cent of ultimate strength for grades A and B and to 60 per cent for grade C]

Cable diam-	Grade of construc-	Tem-	, ''	Pensions	(in pour	ids) for s	pan leng	ths (in fe	et) of—	
eter (inches)	tion	pera- ture	200	250	300	400	500	600	700	1,000
18	{A and B C	$ \begin{array}{c} ^{\circ}F. \\ 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array} $	1,210 990 780 1,790 1,530 1,300	930 770 620 1, 520 1, 290 1, 070	720 620 530 1, 270 1, 080 980	520 480 450 870 760 680	450 440 430 650 610 570	420 410 400 570 550 520	410 400 390 530 520 500	410 400 390 480 470 460
• */8	A and B 0	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1, 940 1, 620 1, 310 2, 690 2, 360 2, 030	1, 700 1, 420 1, 150 2, 480 2, 140 1, 830	1,450 1,210 1,020 2,250 1,920 1,630	$1,070 \\950 \\860 \\1,750 \\1,520 \\1,310$	870 820 770 1, 360 1, 230 1, 100	770 740 710 1, 110 1, 040 970	730 720 700 1, 010 960 910	680 670 660 870 850 830
<del>7</del> 16	{ <b>A</b> and <b>B</b> C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3, 140 2, 650 2, 190 4, 090 3, 600 3, 110	2, 910 2, 440 2, 050 3, 920 3, 440 2, 960	2, 660 2, 250 1, 890 3, 740 3, 270 2, 810	$\begin{array}{c} 2,220\\ 1,910\\ 1,650\\ 3,260\\ 2,860\\ 2,470 \end{array}$	$\begin{array}{c} 1,840\\ 1,660\\ 1,500\\ 2,790\\ 2,460\\ 2,160 \end{array}$	1, 600 1, 490 1, 400 2, 400 2, 160 1, 950	1, 470 1, 420 1, 350 2, 120 1, 980 1, 830	1, 340 1, 300 1, 270 1, 730 1, 670 1, 610
1⁄2	A and B	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array} \right.$	3, 910 3, 340 2, 780 4, 950 4, 360 3, 770	$\begin{array}{c} 3, 660 \\ 3, 120 \\ 2, 580 \\ 4, 800 \\ 4, 220 \\ 3, 650 \end{array}$	$\begin{array}{c} 3,  390 \\ 2,  900 \\ 2,  410 \\ 4,  600 \\ 4,  040 \\ 3,  500 \end{array}$	2, 930 2, 550 2, 180 4, 150 3, 650 3, 160	$\begin{array}{c} 2,540\\ 2,250\\ 2,020\\ 3,660\\ 3,250\\ 2,840 \end{array}$	2, 240 2, 040 1, 900 3, 260 2, 930 2, 620	2,040 1,910 1,810 2,890 2,660 2,440	1, 790 1, 740 1, 690 2, 370 2, 280 2, 180
	{A and B {C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	5, 320 4, 550 3, 780 6, 750 5, 940 5, 130	5, 120 4, 360 3, 650 6, 600 5, 830 5, 050	$\begin{array}{c} 4,920\\ 4,180\\ 3,520\\ 6,410\\ 5,680\\ 4,960\end{array}$	4, 470 3, 840 3, 330 6, 010 5, 340 4, 680	4, 040 3, 550 3, 150 5, 590 4, 950 4, 320	3, 630 3, 270 2, 980 5, 100 4, 570 4, 070	3, 320 3, 070 2, 860 4, 670 4, 260 3, 850	2, 920 2, 810 2, 700 3, 880 3, 650 3, 470
<sup>5</sup> /8	A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	6, 630 5, 700 4, 770 8, 340 7, 370 6, 410	6, 460 5, 550 4, 630 8, 190 7, 250 6, 310	$\begin{array}{c} 6,230\\ 5,360\\ 4,500\\ 8,030\\ 7,110\\ 6,200 \end{array}$	5, 770 5, 030 4, 300 7, 660 6, 790 5, 950	5, 340 4, 700 4, 140 7, 250 6, 450 5, 670	4, 940 4, 420 4, 000 6, 800 6, 080 5, 420	4, 570 4, 180 3, 870 6, 320 5, 670 5, 150	4,030 3,840 3,660 5,330 5,000 4,670

### Table 66.-Stringing Tensions for Siemens-Martin Steel Cable-Con.

#### MEDIUM LOADING DISTRICT

[At 30, 60, and 90° F., without load, the tensions being such that when loaded at 15° F., the cable will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

Cable diam-	Grade of	Tem-	1	Censions	(in pour	ds) for s	pan leng	ths (in fe	et) of—	
eter (inches)	construc- tion	pera- ture	200	250	300	400	500	600	700	1,000
5 16	{A and B C	$ \left\{ \begin{array}{c} \circ \ F. \\ 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array} \right. $	$\begin{array}{c} 1,730\\ 1,480\\ 1,240\\ 2,190\\ 1,940\\ 1,690 \end{array}$	1, 610 1, 380 1, 150 2, 120 1, 880 1, 630	1, 500 1, 290 1, 080 2, 020 1, 800 1, 560	$\begin{array}{c} 1,260\\ 1,090\\ 950\\ 1,830\\ 1,610\\ 1,400 \end{array}$	$1,030 \\920 \\830 \\1,590 \\1,400 \\1,230$	900 830 770 1, 350 1, 220 1, 100	820 770 730 1, 190 1, 090 1, 020	710 690 680 940 900 870
3⁄8	$\begin{cases} A and B_{-} \\ C_{-} \end{cases}$	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 2,460\\ 2,120\\ 1,780\\ 3,070\\ 2,720\\ 2,380 \end{array}$	$\begin{array}{c} 2,370\\ 2,040\\ 1,710\\ 3,010\\ 2,670\\ 2,330 \end{array}$	$\begin{array}{c} 2,260\\ 1,930\\ 1,630\\ 2,940\\ 2,590\\ 2,260 \end{array}$	2,020 1,760 1,500 2,750 2,440 2,130	1, 770 1, 570 1, 390 2, 520 2, 240 1, 960	1, 560 1, 410 1, 290 2, 280 2, 630 1, 800	$\begin{array}{c} 1,440\\ 1,330\\ 1,230\\ 2,060\\ 1,870\\ 1,680 \end{array}$	1,220 1,180 1,140 1,660 1,560 1,490
1 <del>7</del>	{A and B C	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right. $	$\begin{array}{c} 3,670\\ 3,180\\ 2,700\\ 4,530\\ 4,030\\ 3,540 \end{array}$	$\begin{array}{c} 3,600\\ 3,120\\ 2,650\\ 4,480\\ 3,990\\ 3,500 \end{array}$	3, 490 3, 040 2, 590 4, 410 3, 940 3, 460	3, 290 2, 880 2, 470 4, 240 3, 790 3, 340	$\begin{array}{c} 3,070\\ 2,720\\ 2,370\\ 4,050\\ 3,620\\ 3,200 \end{array}$	2, 860 2, 540 2, 290 3, 830 3, 440 3, 050	$\begin{array}{c} 2,660\\ 2,410\\ 2,210\\ 3,600\\ 3,260\\ 2,920 \end{array}$	2,280 2,160 2,060 3,060 2,860 2,660
1⁄2	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{r} 4,380\\ 3,800\\ 3,230\\ 5,440\\ 4,840\\ 4,250\end{array}$	$\begin{array}{c} 4,330\\ 3,760\\ 3,200\\ 5,400\\ 4,800\\ 4,200 \end{array}$	$\begin{array}{c} 4,260\\ 3,700\\ 3,150\\ 5,340\\ 4,750\\ 4,160\end{array}$	4, 050 3, 540 3, 040 5, 180 4, 620 4, 060	$\begin{array}{c} 3,810\\ 3,360\\ 2,940\\ 4,990\\ 4,450\\ 3,950\end{array}$	3, 580 3, 200 2, 860 4, 760 4, 270 3, 820	3, 390 3, 070 2, 800 4, 530 4, 090 3, 680	2,940 2,770 2,630 3,910 3,640 3,390
9 16	A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	5,960 5,180 4,400 7,300 6,470 5,650	$\begin{array}{c} 5,880\\ 5,130\\ 4,360\\ 7,240\\ 6,430\\ 5,630 \end{array}$	$\begin{array}{c} 5,800\\ 5,060\\ 4,320\\ 7,180\\ 6,390\\ 5,610 \end{array}$	$\begin{array}{c} 5,610\\ 4,920\\ 4,230\\ 7,030\\ 6,280\\ 5,540 \end{array}$	5,380 4,760 4,150 6,860 6,140 5,450	$\begin{array}{c} 5,150\\ 4,590\\ 4,090\\ 6,650\\ 5,980\\ 5,340 \end{array}$	$\begin{array}{c} 4,940\\ 4,470\\ 4,030\\ 6,410\\ 5,800\\ 5,220 \end{array}$	4, 460 4, 170 3, 920 5, 900 5, 440 5, 030
5⁄8	{A:and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	7, 340 6, 380 5, 420 8, 990 8, 010 7, 030	7, 260 6, 330 5, 400 8, 930 7, 960 6, 990	$\begin{array}{c} 7,160\\ 6,270\\ 5,380\\ 8,860\\ 7,900\\ 6,950 \end{array}$	6, 990 6, 160 5, 330 8, 710 7, 790 6, 880	$\begin{array}{c} 6,800\\ 6,030\\ 5,260\\ 8,520\\ 7,660\\ 6,800 \end{array}$	6, 580 5, 880 5, 220 8, 320 7, 520 6, 720	6, 340 5, 710 5, 160 8, 120 7, 370 6, 630	5, 750 5, 370 5, 030 7, 450 6, 880 6, 360

25804°-27-19

# Table 66.-Stringing Tensions for Siemens-Martin Steel Cable-Con.

#### LIGHT LOADING DISTRICT

[At 30, 60, and  $90^{\circ}$  F. without load, the tensions being such that when loaded at  $30^{\circ}$  F. the cable will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

Cable diam-	Grade of construc-	Tem- pera-	1 ]	<b>Fensions</b>	(in pour	ids) for s	pan leng	ths (in fe	eet) of—	
eter (inches)	tion	ture	200	250	300	400	500	600	700	1,000
1 <sup>5</sup>	{A and B_ C	${ { 8 \\                                $	2,000 1,750 1,510 2,420 2,170 1,920	1, 970 1, 720 1, 480 2, 400 2, 150 1, 910	1, 940 1, 700 1, 460 2, 380 2, 140 1, 890	1, 860 1, 640 1, 420 2, 330 2, 090 1, 850	1, 780 1, 570 1, 370 2, 270 2, 040 1, 820	1, 690 1, 510 1, 340 2, 190 1, 980 1, 770	1, 610 1, 460 1, 310 2, 100 1, 910 1, 710	1, 410 1, 320 1, 230 1, 870 1, 730 1, 590
• 3⁄8	$\begin{cases} A and B \\ C \\ \end{bmatrix}$	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$\begin{array}{c} 2,760\\ 2,420\\ 2,080\\ 3,350\\ 3,010\\ 2,670 \end{array}$	2, 750 2, 410 2, 070 3, 330 2, 990 2, 650	2, 710 2, 380 2, 060 3, 300 2, 960 2, 620	2, 620 2, 320 2, 020 3, 240 2, 910 2, 580	2, 510 2, 240 1, 960 3, 160 2, 850 2, 540	2, 430 2, 180 1, 930 3, 080 2, 790 2, 490	2,350 2,130 1,910 2,990 2,710 2,440	2, 090 1, 960 1, 820 2, 710 2, 510 2, 310
7 16	A and B. C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$\begin{array}{c} 4,030\\ 3,540\\ 3,050\\ 4,850\\ 4,340\\ 3,840 \end{array}$	4, 000 3, 520 3, 040 4, 840 4, 330 3, 830	3, 970 3, 500 3, 030 4, 820 4, 320 3, 820	3, 900 3, 450 3, 000 4, 770 4, 290 3, 800	3, 810 3, 390 2, 980 4, 700 4, 240 3, 780	3, 710 3, 330 2, 950 4, 620 4, 180 3, 750	3, 620 3, 270 2, 930 4, 540 4, 130 3, 730	3, 370 3, 110 2, 900 4, 250 3, 940 3, 630
<sup>1</sup> ⁄2	{A and B. {C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$\begin{array}{r} 4,840\\ 4,250\\ 3,670\\ 5,830\\ 5,220\\ 4,620\end{array}$	4, 810 4, 230 3, 660 5, 810 5, 210 4, 610	$\begin{array}{c} 4,770\\ 4,200\\ 3,640\\ 5,780\\ 5,190\\ 4,600 \end{array}$	$\begin{array}{c} 4,680\\ 4,140\\ 3,610\\ 5,720\\ 5,150\\ 4,580 \end{array}$	$\begin{array}{c} 4,560\\ 4,070\\ 3,580\\ 5,640\\ 5,090\\ 4,550\end{array}$	$\begin{array}{c} 4,450\\ 4,000\\ 3,560\\ 5,550\\ 5,030\\ 4,510 \end{array}$	4, 330 3, 930 3, 560 5, 480 4, 960 4, 450	4, 090 3, 800 3, 510 5, 350 4, 850 4, 360
9 16	A and B.	$\left\{ \begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array} \right.$	6, 440 5, 660 4, 870 7, 760 6, 930 6, 100	6, 420 5, 650 4, 870 7, 740 6, 920 6, 100	6, 390 5, 640 4, 870 7, 700 6, 900 6, 090	6, 300 5, 600 4, 870 7, 650 6, 860 6, 080	$\begin{array}{c} 6,180\\ 5,540\\ 4,870\\ 7,580\\ 6,820\\ 6,070\\ \end{array}$	6, 080 5, 470 4, 870 7, 500 6, 780 6, 070	6, 000 5, 430 4, 870 7, 400 6, 730 6, 050	5, 880 5, 380 4, 870 7, 110 6, 550 5, 980
5⁄8	A and B.	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	7, 900 6, 940 5, 990 9, 510 8, 500 7, 490	7, 880 6, 930 5, 990 9, 490 8, 480 7, 480	7, 850 6, 920 5, 990 9, 460 8, 460 7, 460	7, 780 6, 890 6, 000 9, 410 8, 430 7, 460	7, 680 6, 840 6, 010 9, 350 8, 400 7, 480	7, 570 6, 800 6, 030 9, 250 8, 370 7, 480	7, 470 6, 750 6, 050 9, 160 8, 330 7, 480	7, 140 6, 620 6, 100 8, 890 8, 190 7, 490

### TENSIONS FOR STEEL CABLE

# Table 67.-Stringing Tensions for High-Tension Steel Cable

### HEAVY LOADING DISTRICT

[At 30, 60, and 90° F. without load, the tensions being such that when loaded at 0° F. the cable will be stressed to 50 per cent of ultimate strength for grades A and B and to 60 per cent for grade C]

Cable diam-	Grade of	Tem-	т	ensions	(in poun	ds) for sp	oan lengt	hs (in fe	et) of—	
eter (inches)	construc- tion	pera- ture	200	250	300	400	500	600	700	1,000
5 18	{A and B C	$ \begin{cases} {}^{\circ}F. \\ {}^{30} \\ {}^{60} \\ {}^{90} \\ {}^{30} \\ {}^{60} \\ {}^{90} \end{cases} $	2, 990 2, 700 2, 420 3, 670 3, 410 3, 160	2, 840 2, 570 2, 310 3, 590 3, 340 3, 080	2, 660 2, 420 2, 180 3, 500 3, 240 2, 990	2, 250 2, 040 1, 830 3, 240 2, 990 2, 750	1, 850 1, 650 1, 450 2, 860 2, 640 2, 420	1, 420 1, 270 1, 140 2, 430 2, 220 2, 000	1, 130 1, 040 960 2, 060 1, 860 1, 670	800 770 740 1,230 1,160 1,090
3⁄8	A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	4, 160 3, 810 3, 460 5, 150 4, 800 4, 440	4,050 3,690 3,340 5,060 4,710 4,350	$\begin{array}{c} 3,920\\ 3,560\\ 3,210\\ 4,970\\ 4,620\\ 4,270 \end{array}$	3, 590 3, 260 2, 920 4, 740 4, 400 4, 050	3, 210 2, 890 2, 580 4, 460 4, 120 3, 780	2, 760 2, 480 2, 220 4, 110 3, 790 3, 460	2, 340 2, 110 1, 900 3, 640 3, 330 3, 030	1, 560 1, 490 1, 420 2, 630 2, 500 2, 360
7 16	{A and B (C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	6, 130 5, 630 5, 120 7, 500 7, 000 6, 490	$\begin{array}{c} 6,020\\ 5,530\\ 5,030\\ 7,450\\ 6,950\\ 6,450 \end{array}$	5, 910 5, 420 4, 940 7, 380 6, 880 6, 380	5, 640 5, 170 4, 680 7, 200 6, 700 6, 200	5, 320 4, 870 4, 390 6, 950 6, 470 5, 980	4, 960 4, 510 4, 060 6, 670 6, 210 5, 710	4, 550 4, 140 3, 730 6, 350 5, 890 5, 430	3, 400 3, 140 2, 930 5, 260 4, 850 4, 440
⅓	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	7, 380 6, 770 6, 160 9, 050 8, 440 7, 840	7, 300 6, 700 6, 100 8, 990 8, 330 7, 780	7, 200 6, 600 6, 000 8, 920 8, 320 7, 710	6, 920 6, 350 5, 750 8, 750 8, 150 7, 550	6, 600 6, 040 5, 460 8, 490 7, 900 7, 310	6, 230 5, 700 5, 150 8, 210 7, 630 7, 050	5, 860 5, 350 4, 850 7, 910 7, 330 6, 750	$\begin{array}{c} 4,620\\ 4,270\\ 3,940\\ 6,840\\ 6,340\\ 5,850 \end{array}$
9	A and B.	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	9,900 9,100 8,300 12,080 11,280 10,440	9, 830 9, 030 8, 240 12, 020 11, 210 10, 390	9,750 8,940 8,150 11,960 11,150 10,330	9, 510 8, 710 7, 930 11, 800 10, 990 10, 180	9, 200 8, 440 7, 670 11, 600 10, 800 10, 000	8,850 8,120 7,370 11,310 10,520 9,750	8, 500 7, 790 7, 080 11, 020 10, 250 9, 500	7, 310 6, 750 6, 210 10, 110 9, 420 8, 710
5/8	$\begin{cases} A and B \\ C \\ \end{bmatrix}$	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$12, 150 \\ 11, 160 \\ 10, 200 \\ 14, 800 \\ 13, 820 \\ 12, 850$	12,070 11,090 10,140 14,750 13,780 12,800	11, 980 11, 010 10, 060 14, 700 13, 720 12, 730	$\begin{array}{c} 11,780\\ 10,820\\ 9,880\\ 14,570\\ 13,580\\ 12,600 \end{array}$	11, 520 10, 580 9, 640 14, 380 13, 380 12, 420	11, 150 10, 240 9, 350 14, 100 13, 140 12, 180	10, 780 9, 890 9, 060 13, 820 12, 890 11, 940	9,700 8,950 8,240 13,000 12,100 11,280

# Table 67.-Stringing Tensions for High-Tension Steel Cable-Contd.

### MEDIUM LOADING DISTRICT

[At 30, 60, and  $90^{\circ}$ F. without load, the tensions being such that when loaded at  $15^{\circ}$ F. the cable will be stressed to 50 per cent of ultimate strength for grades A and B, and 60 per cent for grade C]

Cable diam-	Grade of	Tem-	, Те	ensions (i	in pound	s) for spa	an lengtl	ns (in fee	t) of —	
ete <b>r</b> (inches)	construc- tion	pera- ture	200	250	300	400	500	600	700	1, 000
5 16	{A and B C	$ \begin{cases} {}^{\circ}F. \\ {}^{30}\\ {}^{60}\\ {}^{90}\\ {}^{30}\\ {}^{60}\\ {}^{90} \end{cases} $	3, 200 2, 960 2, 720 3, 920 3, 670 3, 410	3, 170 2, 920 2, 670 3, 890 3, 630 3, 380	3, 120 2, 870 2, 630 3, 850 3, 590 3, 340	3,000 2,760 2,520 3,770 3,510 3,250	2, 850 2, 610 2, 370 3, 650 3, 400 3, 150	2, 680 2, 450 2, 220 3, 520 3, 270 3, 030	2, 490 2, 280 2, 060 3, 370 3, 130 2, 900	1, 860 1, 720 1, 590 2, 870 2, 650 2, 440
3/8	$\begin{cases} A and B \\ C \end{bmatrix}$	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	4, 450 4, 100 3, 760 5, 400 5, 050 4, 690	4, 420 4, 060 3, 730 5, 380 5, 030 4, 680	4, 370 4, 030 3, 690 5, 350 5, 000 4, 660	4, 260 3, 930 3, 600 5, 270 4, 930 4, 580	4, 140 3, 810 3, 480 5, 190 4, 850 4, 500	3, 980 3, 660 3, 340 5, 060 4, 720 4, 380	3,790 3,490 3,180 4,900 4,560 4,220	3, 120 2, 920 2, 720 4, 230 3, 920 3, 640
7 16	$\begin{cases} A and B \\ C \\ \end{cases}$	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	6, 470 5, 980 5, 490 7, 840 7, 320 6, 810	6, 440 5, 940 5, 450 7, 820 7, 310 6, 800	6, 400 5, 900 5, 420 7, 800 7, 290 6, 780	6, 310 5, 820 5, 330 7, 740 7, 240 6, 730	6, 200 5, 710 5, 230 7, 650 7, 150 6, 650	6, 060 5, 590 5, 120 7, 550 7, 060 6, 570	5, 870 5, 430 4, 940 7, 450 6, 960 6, 470	5, 340 4, 940 4, 540 7, 000 6, 560 6, 120
1⁄2	A and B. C	$\begin{cases} 30\\ 60\\ 90\\ 30\\ 60\\ 90 \end{cases}$	7, 770 7, 180 6, 580 9, 410 8, 800 8, 190	7, 740 7, 150 6, 540 9, 390 8, 780 8, 180	7,700 7,120 6,500 9,360 8,750 8,150	$\begin{array}{c} 7,610\\ 7,030\\ 6,430\\ 9,290\\ 8,690\\ 8,100 \end{array}$	7, 500 6, 900 6, 320 9, 200 8, 610 8, 010	7, 330 6, 760 6, 190 9, 090 8, 520 7, 920	7, 170 6, 620 6, 070 8, 960 8, 380 7, 810	6, 690 6, 190 5, 700 8, 550 8, 000 7, 460
9 16	$ \left\{ \begin{matrix} A \text{ and } B \\ C \end{matrix} \right\} $	$     \begin{cases}         90 \\         30 \\         60 \\         90     \end{cases} $	10, 370 9, 590 8, 780 12, 530 11, 700 10, 910	$10, 340 \\ 9, 550 \\ 8, 740 \\ 12, 510 \\ 11, 680 \\ 10, 880$	$\begin{array}{c} 10,310\\ 9,520\\ 8,710\\ 12,500\\ 11,660\\ 10,860 \end{array}$	$10,230 \\ 9,450 \\ 8,650 \\ 12,440 \\ 11,620 \\ 10,810$	10, 120 9, 350 8, 550 12, 370 11, 570 10, 770	9, 980 9, 220 8, 460 12, 270 11, 490 10, 700	9, 820 9, 080 8, 350 12, 140 11, 360 10, 580	9, 370 8, 690 8, 030 11, 780 11, 000 10, 260
5⁄8	{A and B_ C	$\left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right.$	$\begin{array}{c} 12,700\\ 11,710\\ 10,740\\ 15,380\\ 14,380\\ 13,380 \end{array}$	12, 680 11, 700 10, 720 15, 350 14, 350 13, 370	$\begin{array}{c} 12,650\\ 11,690\\ 10,700\\ 15,320\\ 14,330\\ 13,350 \end{array}$	$\begin{array}{c} 12,560\\ 11,600\\ 10,640\\ 15,250\\ 14,280\\ 13,320 \end{array}$	$\begin{array}{c} 12,440\\ 11,500\\ 10,540\\ 15,200\\ 14,200\\ 13,250 \end{array}$	$\begin{array}{c} 12,320\\ 11,390\\ 10,440\\ 15,100\\ 14,130\\ 13,170 \end{array}$	$\begin{array}{c} 12,190\\ 11,260\\ 10,330\\ 15,000\\ 14,040\\ 13,100 \end{array}$	$11,720 \\ 10,890 \\ 10,060 \\ 14,550 \\ 13,660 \\ 12,780$

5/

# Table 67.-Stringing Tensions for High-Tension Steel Cable-Contd.

### LIGHT LOADING DISTRICT

[At 30, 60, and 90° without load the tensions being such that when loaded at 30° F. the cable will be stressed to 50 per cent of ultimate strength for grades A and B, and to 60 per cent for grade C]

Cable diam-	Grade of	Tem-		Tension	s (in pou	nds) for	span len	gths (in	feet) of—	
eter (inches)	construc- tion	pera- ture	200	250	300	400	500	600	700	1,000
5 16	A and B. C		3, 390 3, 140 2, 880 4, 080 3, 820 3, 560	3, 380 3, 130 2, 870 4, 070 3, 810 3, 560	3, 370 3, 120 2, 860 4, 060 3, 800 3, 550	3, 340 3, 090 2, 840 4, 040 3, 790 3, 540	3, 300 3, 050 2, 810 4, 020 3, 760 3, 510	3, 260 3, 020 2, 780 3, 980 3, 730 3, 480	3, 200 2, 960 2, 740 3, 950 3, 700 3, 450	3, 030 2, 810 2, 590 3, 800 3, 560 3, 330
3⁄8	A and B. C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	4, 660 4, 310 3, 970 5, 610 5, 250 4, 900	4, 650 4, 310 3, 960 5, 600 5, 250 4, 900	4, 650 4, 300 3, 960 5, 600 5, 240 4, 890	4, 620 4, 280 3, 940 5, 570 5, 220 4, 880	4, 580 4, 240 3, 910 5, 550 5, 200 4, 860	4, 540 4, 210 3, 880 5, 510 5, 170 4, 840	4, 470 4, 150 3, 840 5, 470 5, 140 4, 820	4, 280 3, 990 3, 710 5, 320 4, 990 4, 670
<del>1</del> 6	A and B. C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	6,770 6,260 5,760 8,130 7,620 7,100	6, 760 6, 250 5, 750 8, 120 7, 600 7, 090	6, 730 6, 230 5, 740 8, 100 7, 590 7, 080	6, 710 6, 220 5, 730 8, 080 7, 580 7, 080	6, 670 6, 180 5, 700 8, 050 7, 560 7, 060	6, 610 6, 130 5, 660 8, 020 7, 530 7, 040	6, 550 6, 100 5, 630 7, 980 7, 490 7, 000	6, 380 5, 960 5, 540 7, 840 7, 360 6, 870
	A and B.		8, 110 7, 510 6, 910 9, 740 9, 130 8, 510	8, 100 7, 500 6, 900 9, 730 9, 120 8, 500	8, 090 7, 490 6, 890 9, 720 9, 110 8, 490	8, 060 7, 470 6, 870 9, 690 9, 090 8, 480	8,010 7,430 6,840 9,670 9,080 8,470	7, 960 7, 380 6, 810 9, 650 9, 060 8, 460	7, 900 7, 330 6, 770 9, 590 9, 000 8, 410	7,650 7,160 6,650 9,420 8,850 8,280
<u>9</u> 16	$\begin{cases} A and B \\ C \\ \end{bmatrix}$	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$\begin{array}{c} 10,790\\ 10,010\\ 9,190\\ 12,970\\ 12,150\\ 11,320 \end{array}$	10, 780 9, 990 9, 180 12, 960 12, 140 11, 320	10, 770 9, 980 9, 170 12, 940 12, 130 11, 310	10, 750 9, 950 9, 150 12, 930 12, 110 11, 300	$\begin{array}{c} 10,710\\ 9,920\\ 9,140\\ 12,900\\ 12,090\\ 11,300 \end{array}$	10, 650 9, 860 9, 100 12, 880 12, 080 11, 290	$\begin{array}{c} 10,600\\ 9,800\\ 9,050\\ 12,850\\ 12,060\\ 11,280 \end{array}$	10, 300 9, 630 8, 940 12, 670 11, 900 11, 160
5⁄8	A and B. C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$13,230 \\ 12,280 \\ 11,280 \\ 15,890 \\ 14,890 \\ 13,890$	13, 220 12, 280 11, 280 15, 880 14, 880 13, 880	13, 210 12, 280 11, 280 15, 870 14, 870 13, 880	$\begin{array}{c} 13,200\\ 12,250\\ 11,260\\ 15,840\\ 14,850\\ 13,860 \end{array}$	$\begin{array}{c} 13,150\\ 12,210\\ 11,240\\ 15,830\\ 14,830\\ 13,850 \end{array}$	$\begin{array}{c} 13,100\\ 12,180\\ 11,220\\ 15,800\\ 14,810\\ 13,840 \end{array}$	13, 020 12, 120 11, 200 15, 770 14, 780 13, 820	12, 800 11, 960 11, 130 15, 600 14, 670 13, 730

# 270

### APPENDIX B

# Table 68.—Stringing Tensions for Bare Copper-Covered Steel Wire (Ordinary Grade)

### HEAVY LOADING DISTRICT

[The tensions being such that when loaded at 0° F. the wires will be stressed to 50 per cent of their ultimate strength]

Size	Grade of	Tem-	Tensions (in pounds) for span lengths (in feet) of-									
A.W.G. No.	construction	pera- ture	100	125	150	175	200	250	300			
6	A and B	° <i>F</i> . 30 60 90	637 548 460	$530 \\ 441 \\ 352$	424 341 264	310 246 197						
4	A and B	30 60 90	1, 037 901 764	964 822 685	863 729 594	$752 \\ 620 \\ 495$	635 507 400	400 314 275	274 244 222			

### MEDIUM LOADING DISTRICT

[The tensions being such that when loaded at 15° F. the wires will be stressed to 50 per cent of their ultimate strength]

Size	Grade of	Tem-											
A. W. G. No.	Grade of construction	pera- ture	100	125	150	175	200	250	300	400			
8	В	° F. 30 60 90	$511 \\ 455 \\ 400$	$479 \\ 423 \\ 368$	437 384 327								
6	A and B	30 60 90	807 719 629	780 691 602	747 660 570	$706 \\ 619 \\ 532$							
4	A and B	30 60 90	1, 210 1, 070 933	1, 190 1, 050 910	1, 160 1, 020 881	1, 130 988 850	1, 087 949 826	998 860 734	894 767 648	670 572 484			

TENSIONS FOR COPPER-COVERED STEEL

# Table 68.—Stringing Tensions for Bare Copper-Covered Steel Wire (Ordinary Grade)—Continued

### LIGHT LOADING DISTRICT

[The tensions being such that when loaded at 30° F. the wires will be stressed to 50 per cent of their ultimate strength]

A. W. G.		Tem-	Tensions (in pounds) for span lengths (in feet) of-								
A. W. G. No.	Grade of construction	pera- ture	100	150	200	300	400	500			
8	B	° F. 30 60 90	595 540 484	590 534 478							
6	A and B	30 60 90	893 805 718	886 799 711	877 790 702						
4	A and B	30 60 90	$\substack{1,323\\1,180\\1,038}$	1, 302 1, 162 1, 024	1, 300 1, 160 1, 022	$\substack{1,287\\1,152\\996}$	1, 225 1, 093 967	1, 176 1, 052 931			

# Table 69.—Stringing Tensions for Bare Copper-Covered Steel Cable HEAVY LOADING DISTRICT

[The tensions being such that when loaded at 0° F. the cable will be stressed to 50 per cent of its ultimate strength]

Size (inch)	Grade of	Tem-	Tensions (in pounds) for span lengths (in feet) of-									
(inch)	construction	pera- ture	200	250	300	400	500	600	800	1,000		
<del>5</del> 16	A and B	° F. 30 60 90	2, 260 2, 020 1, 790	2, 105 1, 870 1, 605	1, 885 1, 660 1, 440	1, 455 1, 260 1, 105	1, 065 940 840					
3/8	A and B	30 60 90	3, 600 3, 240 2, 885	3, 435 3, 080 2, 740	3, 285 2, 940 2, 595	2, 920 2, 600 2, 290	2, 505 2, 220 1, 970	2, 100• 1, 887 1, 700	1, 586 1, 490 1, 405			
<del>7</del> 8	A and B	30 60 90	4, 309 3, 960 3, 530	4, 280 3, 850 3, 425	4, 110 3, 700 3, 285	3, 760 3, 360 2, 985	3, 350 2, 990 2, 665	2, 930 2, 640 2, 380	2, 320 2, 160 2, 010	1, 995 1, 910 1, 835		
1⁄2	A and B	30 60 90	5, 585 5, 060 4, 560	5, 480 4, 960 4, 465	5, 330 4, 820 4, 325	5, 015 4, 520 4, 055	4, 625 4, 180 3, 745	4, 230 3, 830 3, 460	3, 485 3, 210 2, 960	2, 985 2, 830 2, 685		
9 16	A and B	30 60 90	6, 845 6, 280 5, 650	6, 790 6, 180 5, 570	6, 660 6, 050 5, 460	6, 380 5, 800 5, 220	6, 020 5, 470 4, 940	5, 635 5, 130 4, 660	4, 875 4, 480 4, 140	4, 260 4, 010 3, 810		

# Table 69.—Stringing Tensions for Bare Copper-Covered Steel Cable— Continued

### MEDIUM LOADING DISTRICT

[The tensions being such that when loaded at 15° F. the cable will be stressed to 50 per cent of its ultimate strength]

Size (inch)	Grade of construction	Tem- pera-	Tensions (in pounds) for span lengths (in feet) of—								
(/		ture	100	250	400	600	800	1,000			
<u>5</u> 16	A and B	° F. 30 60 90	2, 660 2, 420 2, 180	2, 540 2, 309 2, 070	2, 330 2, 100 1, 880	1, 940 1, 750 1, 570					
³⁄8	A and B	30 60 90	4,000 3,630 3,270	3, 890 3, 540 3, 180	3, 710 3, 370 3, 020	3, 330 3, 040 2, 730	2, 940 2, 710 2, 470				
<del>7</del> 16	A and B	30 60 90	4, 830 4, 400 3, 960	4, 750 4, 320 3, 890	4, 560 4, 150 3, 760	4, 230 3, 850 3, 490	3, 850 3, 530 3, 240	3, 490 3, 250 3, 030			
1⁄2	A and B	30 60 90	6, 030 5, 500 4, 970	5, 930 5, 410 4, 900	5, 760 5, 260 4, 770	5, 450 4, 990 4, 530	5, 080 4, 690 4, 320	4, 710 4, 390 4, 090			
9 16	A and B	30 60 90	7, 370 6, 740 6, 120	7, 280 6, 660 6, 050	7, 150 6, 520 5, 930	6, 820 6, 270 5, 740	6, 470 5, 980 5, 520	6, 110 5, 690 5, 310			

### LIGHT LOADING DISTRICT

[The tensions being such that when loaded at 30° F. the cable will be stressed to 50 per cent of its ultimate strength]

5 A and B	30 60 90	2, 800 2, 560 2, 320	2, 760 2, 530 2, 290	2, 710 2, 480 2, 220	2, 610 2, 390 2, 180	2, 460 2, 260 2, 070	
3/8 A and B	30	4, 190	4, 170	4, 105	4, 000	3, 900	3, 720
	60	3, 830	3, 810	3, 755	3, 670	3, 570	3, 490
	90	3, 470	3, 440	3, 400	3, 350	3, 270	3, 190
78 A and B	30	5, 030	5, 020	4, 970	4, 880	4, 740	4, 590
	60	4, 640	4, 610	4, 570	4, 480	4, 380	4, 270
	90	4, 200	4, 180	4, 150	4, 090	4, 020	3, 960
1/2 A and B	30	6, 300	6, 270	6, 200	6, 100	5, 960	5, 810
	60	5, 780	5, 750	5, 700	5, 620	5, 520	5, 420
	90	5, 260	5, 230	5, 210	5, 160	5, 100	5, 040
<sup>9</sup> / <sub>18</sub> A and B	30	7, 700	7, 660	7, 660	7, 490	7, 360	7, 210
	60	7, 070	7, 040	7, 000	6, 920	6, 830	6, 730
	90	6, 450	6, 430	6, 410	6, 370	6, 320	6, 280

# Table 70 .- Stringing Tensions for Bare Stranded Aluminum

HEAVY LOADING DISTRICT

[The tensions being such that when loaded at 0° F. the conductor will be stressed to 50 per cent of the ultimate strength for grades A and B and 60 per cent for grade C]

Size	Grade of	Tem-	Ten	isions (i	n poun	ds) for s	pan len	gths (ir	ı feet) o	f —
A. W. G. No.	construction	pera- ture	100	125	150	200	250	300	400	600
1	{A and B C	$\begin{cases} {}^{\circ}F. \\ {}^{60} \\ {}^{90} \\ {}^{30} \\ {}^{60} \\ {}^{90} \end{cases}$	96 66 53 267 125 73	73 59 50 149 89 69	66 53 50 99 79 66					
0	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	199 108 79 527 273 116	125 91 75 315 162 104	108 91 75 216 133 104	95 87 75 133 112 100	87 83 75 112 104 100	87 83 75 108 104 95	83 79 75 104 100 91	 
00	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	378 173 121 709 378 173	263 152 116 593 305 168	$200 \\ 142 \\ 116 \\ 420 \\ 231 \\ 158$	$152 \\ 131 \\ 121 \\ 252 \\ 189 \\ 158$	147 131 121 194 173 152	$137 \\ 131 \\ 126 \\ 179 \\ 163 \\ 152$	$131 \\ 126 \\ 126 \\ 168 \\ 158 \\ 147$	152 147 147
000	A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	640 304 165 1,030 601 277	488 251 165 871 482 244	370 231 172 759 409 251	$251 \\ 205 \\ 172 \\ 455 \\ 304 \\ 231$	$218 \\ 198 \\ 178 \\ 330 \\ 264 \\ 224$	$211 \\ 191 \\ 185 \\ 290 \\ 251 \\ 224$	198     191     185     264     244     224	$     185 \\     185 \\     231 \\     224 \\     224    $
0000	A and B	$ \left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90 \end{array}\right. $	938 448 232 1, 370 772 374	747 415 232 1, 295 722 374	623 349 241 1, 104 631 340	398 299 249 780 465 332	349 291 257 589 415 332	$324 \\ 291 \\ 266 \\ 452 \\ 365 \\ 332$	291 274 266 365 349 324	$ \begin{array}{c c} 282 \\ 266 \\ 266 \\ 349 \\ 340 \\ 324 \\ \end{array} $

# Table 70.-Stringing Tensions for Bare Stranded Aluminum-Contd.

### MEDIUM LOADING DISTRICT

[The tensions being such that when loaded at 15° F. the conductor will be stressed to 50 per cent of the ultimate strength for grades A and B and 60 per cent for grade C]

Size	Grade of		1	Tensior	ıs (in po	unds) f	or span	lengths	(in feet	;) of—	
A. W. G. No.	construc- tion	pera- ture	100	125	150	200	250	300	400	500	600
1	$\begin{cases} A and B_{-} \\ C_{} \end{cases}$	$\left\{\begin{array}{c} {}^\circ F,\\ {}^{30}\\ {}^{60}\\ {}^{90}\\ {}^{30}\\ {}^{60}\\ {}^{90}\end{array}\right.$	426 224 102 620 399 198	$337 \\ 172 \\ 99 \\ 535 \\ 317 \\ 162$	$254 \\ 137 \\ 96 \\ 472 \\ 277 \\ 152$						
0	A and B. C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	598 336 149 822 531 282	523 274 145 768 498 253	$\begin{array}{r} 427 \\ 237 \\ 145 \\ 697 \\ 427 \\ 237 \end{array}$	$261 \\ 174 \\ 137 \\ 552 \\ 315 \\ 203$	199 162 137 374 249 187	$174 \\ 154 \\ 137 \\ 274 \\ 216 \\ 183$	$154 \\ 145 \\ 137 \\ 208 \\ 187 \\ 174$	145 141 137 191 178 170	141 133 137 183 174 170
00	{A and B. C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	830 473 221 1,087 735 399	$746 \\ 425 \\ 210 \\ 1,040 \\ 683 \\ 382$	$672 \\ 373 \\ 210 \\ 982 \\ 646 \\ 352 \\ $	467 289 205 824 625 310	$347 \\ 252 \\ 205 \\ 641 \\ 410 \\ 278$	284 236 205 494 347 273	$\begin{array}{c} 247 \\ 226 \\ 205 \\ 352 \\ 299 \\ 263 \end{array}$	$226 \\ 215 \\ 205 \\ 305 \\ 278 \\ 257$	$\begin{array}{c} 221 \\ 210 \\ 205 \\ 278 \\ 263 \\ 252 \end{array}$
000	$\begin{cases} A and B \\ C \\ \end{bmatrix}$	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1,089\\640\\304\\1,412\\964\\528$	$1,010 \\ 587 \\ 297 \\ 1,360 \\ 911 \\ 502$	937 548 297 1,294 865 482	$746 \\ 442 \\ 297 \\ 1,142 \\ 746 \\ 442$	$581 \\ 396 \\ 297 \\ 990 \\ 647 \\ 422$	$\begin{array}{r} 455 \\ 350 \\ 297 \\ 812 \\ 542 \\ 403 \end{array}$	442 337 297 568 455 383	$343 \\ 317 \\ 297 \\ 469 \\ 416 \\ 376$	323 310 297 429 396 370
0000	{A and B_ C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1,411\\855\\407\\1,785\\1,220\\681$	$\begin{array}{c c}1,328\\789\\407\\1,743\\1,179\\664\end{array}$	1,2627474071,5941,162647	$1,038\\614\\407\\1,552\\1,038\\614$	896 581 415 1,378 896 581	706 523 415 1, 187 797 573	589 490 432 921 689 564	$515 \\ 465 \\ 432 \\ 739 \\ 614 \\ 540$	490- 457 432 656 589 540

# Table 70.-Stringing Tensions for Bare Stranded Aluminum-Contd.

LIGHT LOADING DISTRICT

[The tensions being such that when loaded at 30° F., the conductor will be stressed to 50 per cent of the ultimate strength for grades A and B and 60 per cent for grade C]

Size	Grade of	ade of Tem-		Tensio	ns (in p	ounds)	for spar	ı length	s (in fee	et) of—	
A .W.G. No.	tion	ture	100	125	150	200	250	300	400	500	600
1	{A and B C	90	660 436 228 828 597 380	634 409 218 812 574 353	$597 \\ 383 \\ 208 \\ 776 \\ 551 \\ 340$						
0	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$838 \\ 564 \\ 303 \\ 1,042 \\ 751 \\ 477 \\$	$813 \\ 535 \\ 291 \\ 1,021 \\ 739 \\ 465$	$780 \\ 510 \\ 278 \\ 988 \\ 668 \\ 440$	$714 \\ 465 \\ 278 \\ 934 \\ 660 \\ 411$	606 423 257 855 598 390	$506 \\ 340 \\ 253 \\ 784 \\ 549 \\ 361$	$361 \\ 286 \\ 241 \\ 593 \\ 427 \\ 328$	$303 \\ 270 \\ 232 \\ 452 \\ 361 \\ 307$	274 253 232 378 332 295
00	$\begin{cases} A and B_{-} \\ C_{-} \end{cases}$	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$1,087 \\730 \\399 \\1,323 \\966 \\614$	1,0556983831,302940599	$1,024 \\ 677 \\ 378 \\ 1,292 \\ 914 \\ 578$	$935 \\ 614 \\ 373 \\ 1,218 \\ 872 \\ 557$	$845 \\ 557 \\ 362 \\ 1, 145 \\ 809 \\ 536$	$719 \\ 478 \\ 347 \\ 1,045 \\ 730 \\ 494$	$536 \\ 415 \\ 336 \\ 840 \\ 609 \\ 452$	452 378 336 683 525 431	$\begin{array}{r} 404 \\ 368 \\ 336 \\ 572 \\ 483 \\ 425 \end{array}$
000	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$1, 366 \\ 917 \\ 502 \\ 1, 663 \\ 1, 214 \\ 772$	$1, 360 \\904 \\502 \\1, 650 \\1, 201 \\766$	$1, 313 \\ 878 \\ 502 \\ 1, 630 \\ 1, 175 \\ 752$	$1,214\\865\\482\\1,577\\1,135\\733$	$1,129\\746\\482\\1,511\\1,089\\713$	$1,010 \\ 680 \\ 469 \\ 1,406 \\ 1,003 \\ 680$	818 601 469 1, 214 878 634	640 535 455 997 759 601	$581 \\ 515 \\ 455 \\ 858 \\ 700 \\ 594$
0000	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	$1,735 \\ 1,170 \\ 639 \\ 2,108 \\ 1,544 \\ 988$	$1, 693 \\ 1, 145 \\ 639 \\ 2, 075 \\ 1, 519 \\ 963$	$1,668 \\ 1,121 \\ 639 \\ 2,067 \\ 1,511 \\ 963$	$1,594 \\ 1,071 \\ 639 \\ 2,017 \\ 1,461 \\ 955$	1, 486 996 639 1, 934 1, 403 930	$1, 370 \\930 \\639 \\1, 834 \\1, 320 \\905$	$1, 137 \\ 822 \\ 631 \\ 1, 627 \\ 1, 204 \\ 863$	930 755 631 1, 411 1, 054 830	830 706 631 1, 204 963 797

# Table 71.—Stringing Tensions for Bare Stranded Aluminum, Steel-Reinforced

### HEAVY LOADING DISTRICT

[The tensions being such that when loaded at 0° F. the cable will be stressed to 50 per cent of the ultimate strength for grades A and B and 60 per cent for grade C]

Size A. W. G. No.	Grade of construction	Tem-	Te	nsions (	in poun	ds) for :	span ler	igths (ii	n feet) of—				
		pera- ture	100	150	200	300	400	500	700	1,000			
4	{A and B C	$\begin{cases} {}^{\circ}F.\\ {}^{60}\\ {}^{90}\\ {}^{30}\\ {}^{60}\\ {}^{90} \end{cases}$	$282 \\ 155 \\ 81 \\ 528 \\ 385 \\ 246$	80 64 55 258 153 98	57 53 49 98 81 70	49 47 46 64 61 59	46 46 45 58 57 56	45 45 45 56 55 55					
2	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	732 507 296 1,043 815 588	454 274 170 840 618 407	219 163 133 570 380 248	$132 \\ 122 \\ 115 \\ 212 \\ 180 \\ 159$	$117 \\ 113 \\ 109 \\ 158 \\ 149 \\ 141$	112 109 107 143 139 134	127 126 124				
1	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1,005 \\720 \\446 \\1,365 \\1,077 \\792$	756 494 29 <b>3</b> 1, 188 904 629	$\begin{array}{r} 462 \\ 303 \\ 220 \\ 946 \\ 678 \\ 447 \end{array}$	226 199 180 435 329 267	$188 \\ 178 \\ 169 \\ 273 \\ 246 \\ 225$	$182 \\ 169 \\ 165 \\ 233 \\ 221 \\ 211$	165 163 161 207 203 199	161 160 159 197 194 194			
0	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1, 345 \\984 \\633 \\1, 777 \\1, 414 \\1, 052$	1, 127 781 479 1, 610 1, 251 898	841 554 365 1, 408 1, 059 734	411 334 284 865 619 457	$307 \\ 282 \\ 262 \\ 499 \\ 418 \\ 364$	276 264 252 387 355 330	$255 \\ 249 \\ 245 \\ 326 \\ 315 \\ 305$	245 243 241 302 297 294			
00	A and B	<pre>     30     60     90     30     60     90 </pre>	1, 768 1, 310 865 2, 290 1, 832 1, 376	1, 575 1, 134 722 2, 155 1, 712 1, 253	1, 316 911 588 1, 968 1, 522 1, 093	768 567 451 1, 466 1, 079 772	521 454 405 948 734 596	445 411 387 677 588 523	393 384 372 523 496 473	$372 \\ 369 \\ 366 \\ 468 \\ 458 \\ 449$			
	A and B	<pre>     30     60     90     30     60     90     90 </pre>	2, 275 1, 698 1, 137 2, 916 2, 335 1, 762	2, 106 1, 545 1, 007 2, 793 2, 218 1, 652	1, 875 1, 337 876 2, 624 2, 058 1, 510	1, 299 930 692 2, 162 1, 642 1, 187	884 722 615 1, 616 1, 220 942	715 638 584 1, 173 960 814	607 576 553 834 772 718	561 553 538 714 692 672			
0000	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	2, 938 2, 210 1, 483 3, 740 3, 010 2, 283	2, 782 2, 065 1, 386 3, 632 2, 909 2, 190	2, 569 1, 881 1, 270 3, 482 2, 767 2, 069	2,026 1,464 1,057 3,068 2,384 1,762	1, 493 1, 154 940 2, 539 1, 950 1, 480	1, 192 1, 008 882 2, 007 1, 589 1, 287	950 892 834 1, 379 1, 228 1, 110	863 834 805 1, 118 1, 068 1, 023			

# Table 71.—Stringing Tensions for Bare Stranded Aluminum, Steel-Reinforced—Continued

### MEDIUM LOADING DISTRICT

[The tensions being such that when loaded at 15° F. the cable will be stressed to 50 per cent of the ultimate strength for grades A and B and 60 per cent for grade C]

Size A. W. G. No.	Grade of construction	Ten-	Ter	isions (i	n poun	ds) for a	span ler	ngths (i	n feet)	of—
		pera- ture	100	150	200	300	400	500	700	1,000
4	{A and B C	$ \begin{cases} {}^{\circ}F. \\ {}^{60}\\ {}^{90}\\ {}^{30}\\ {}^{60}\\ {}^{90} \end{cases} $	579 435 294 759 614 471	457 320 198 673 530 390	301 195 132 555 417 288	126 109 97 272 197 153	99 93 88 150 133 120	91 88 85 123 116 110		
2	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	$1,079\\851\\624\\1,268\\1,039\\810$	913 688 472 1,203 975 749	786 571 381 1,112 887 667	$\begin{array}{r} 477 \\ 344 \\ 261 \\ 862 \\ 655 \\ 474 \end{array}$	295 251 220 573 435 342	240 220 205 385 327 286		
1	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1, 290 999 715 1, 617 1, 328 1, 040	$1,203 \\919 \\643 \\1,549 \\1,262 \\977$	$1,088\\812\\558\\1,467\\1,183\\903$	$788 \\ 569 \\ 411 \\ 1, 240 \\ 970 \\ 720$	$519 \\ 413 \\ 343 \\ 953 \\ 728 \\ 554$	$396 \\ 349 \\ 314 \\ 687 \\ 552 \\ 458$	$321 \\ 305 \\ 291 \\ 453 \\ 414 \\ 383$	292 286 280 375 362 351
0	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1,6461,2839232,0421,6781,314	$1,570 \\ 1,211 \\ 861 \\ 1,990 \\ 1,626 \\ 1,267$	1,4661,1157831,9161,5561,202	$1, 187 \\878 \\629 \\1, 711 \\4, 363 \\1, 035$	879 670 529 1, 441 1, 127 857	$\begin{array}{r} 665\\ 555\\ 480\\ 1,149\\ 904\\ 721 \end{array}$	504 468 439 754 663 595	444 430 418 583 555 530
00	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	2,099 1,641 1,187 2,593 2,133 1,675	$\begin{array}{c} 2,031\\ 1,577\\ 1,134\\ 2,545\\ 2,088\\ 1,633 \end{array}$	$1,937 \\1,491 \\1,065 \\2,478 \\2,024 \\1,576$	$1,680 \\ 1,267 \\ 915 \\ 2,292 \\ 1,850 \\ 1,426$	$\begin{array}{c} 1,370\\ 1,039\\ 795\\ 2,043\\ 1,627\\ 1,253 \end{array}$	$1,086 \\872 \\723 \\1,755 \\1,393 \\1,097$	797 718 655 1, 232 1, 042 901	674 646 620 914 850 797
000	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	2, 657 2, 079 1, 507 3, 271 2, 691 2, 113	2, 594 2, 021 1, 462 3, 227 2, 650 2, 076	$\begin{array}{c} 2,507\\ 1,943\\ 1,403\\ 3,165\\ 2,591\\ 2,026 \end{array}$	2, 270 1, 738 1, 268 2, 994 2, 433 1, 893	$\begin{array}{c} 1,969\\ 1,508\\ 1,142\\ 2,763\\ 2,227\\ 1,734 \end{array}$	$\begin{array}{c} 1,660\\ 1,310\\ 1,056\\ 2,487\\ 1,998\\ 1,575 \end{array}$		1, 014 957 907 1, 413 1, 283 1, 178
0000	A and B	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	3, 382 2, 653 1, 929 4, 154 3, 424 2, 694	$\begin{array}{c} 3,324\\ 2,601\\ 1,892\\ 4,114\\ 3,385\\ 2,662 \end{array}$	3, 244 2, 530 1, 844 4, 057 3, 334 2, 620	3, 023 2, 344 1, 728 3, 899 3, 190 2, 503	2, 740 2, 125 1, 611 3, 685 3, 002 2, 361	2, 429 1, 915 1, 517 3, 426 2, 784 2, 210	1, 904 1, 615 1, 401 3, 025 2, 501 2, 069	1, 537 1, 420 1, 325 2, 177 1, 931 1, 737

# Table 71.—Stringing Tensions for Bare Stranded Aluminum, Steel-Reinforced—Continued

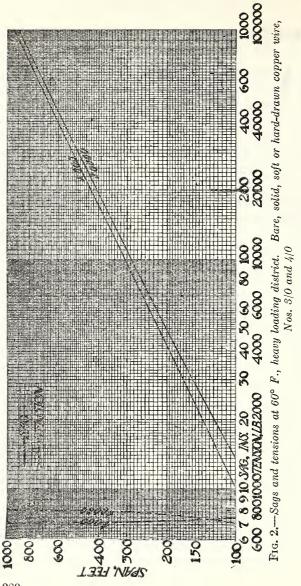
### LIGHT LOADING DISTRICT

[The tensions being such that when loaded at 30° F. the cable will be stressed to 50 per cent of the ultimate strength for grades A and B and 60 per cent for grade C]

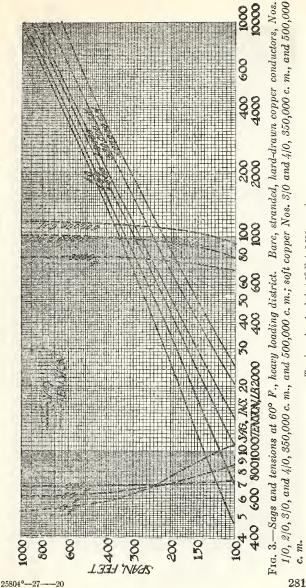
Size A.W.G. No.	Grade of con- struction	Tem-	Tensions (in pounds) for span lengths (in feet) of-								
		pera- ture	100	150	200	300	400	500	700	1,000	
4	{A and B C	$ \begin{cases} {}^{\circ}F. \\ {}^{60}\\ {}^{90}\\ {}^{30}\\ {}^{60}\\ {}^{90} \end{cases} $	729 585 441 885 741 597	702 559 418 870 723 579	666 525 388 842 698 556	$565 \\ 434 \\ 316 \\ 769 \\ 629 \\ 493$	442 336 256 673 540 419	$331 \\ 260 \\ 222 \\ 560 \\ 445 \\ 350$			
2	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1, 176 947 719 1, 422 1, 192 963	1, 150 922 697 1, 403 1, 174 947	1, 114 888 668 1, 377 1, 150 924	$1,012 \\796 \\595 \\1,306 \\1,082 \\863$	$\substack{882\\686\\521\\1,208\\992\\787}$	739 581 463 1,090 887 705			
1	{A and B C	$\left\{\begin{array}{c} 30\\ 60\\ 90\\ 30\\ 60\\ 90\end{array}\right.$	1,479 1,190 903 1,785 1,496 1,208	1,452 1,165 882 1,766 1,478 1,192	1,4151,1318541,7411,4541,170	1, 313 1, 039 783 1, 668 1, 386 1, 110	1, 179 919 707 1, 570 1, 296 1, 034	$1,027\\812\\642\\1,449\\1,189\\951$	766 648 562 1, 174 970 804	592 550 514 853 758 683	
0	{A and B C	$\begin{cases} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{cases}$	1, 869 1, 505 1, 142 2, 253 1, 888 1, 524	$\begin{array}{c} 1,842\\ 1,480\\ 1,122\\ 2,235\\ 1,871\\ 1,509 \end{array}$	1, 805 1, 447 1, 097 2, 209 1, 847 1, 483	$\begin{array}{c} 1,703\\ 1,356\\ 1,028\\ 2,136\\ 1,779\\ 1,430 \end{array}$	1, 568 1, 242 953 2, 037 1, 689 1, 356	$1,410 \\1,121 \\883 \\1,916 \\1,582 \\1,274$	1, 107 923 786 1, 628 1, 350 1, 116	856 781 720 1, 241 1, 085 962	
00	A and B	$\left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right.$	2, 364 1, 904 1, 448 2, 847 2, 387 1, 928	2, 337 1, 880 1, 429 2, 829 2, 370 1, 913	2, 301 1, 848 1, 404 2, 803 2, 347 1, 893	2, 198 1, 758 1, 341 2, 731 2, 280 1, 838	2,061 1,646 1,269 2,631 2,191 1,768	$\begin{array}{c} 1,901\\ 1,521\\ 1,198\\ 2,509\\ 2,084\\ 1,687 \end{array}$	$\begin{array}{c} 1,568\\ 1,297\\ 1,091\\ 2,214\\ 1,844\\ 1,524 \end{array}$	$\begin{array}{c} 1,232\\ 1,106\\ 1,007\\ 1,774\\ 1,535\\ 1,345 \end{array}$	
C00	{Λ and B C	$\left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right.$	2, 977 2, 398 1, 821 3, 583 3, 003 2, 424	2, 949 2, 375 1, 804 3, 564 2, 985 2, 409	2, 913 2, 342 1, 783 3, 537 2, 962 2, 390	2, 810 2, 256 1, 725 3, 465 2, 896 2, 339	2, 673 2, 144 1, 660 3, 366 2, 810 2, 272	$\begin{array}{c} 2,510\\ 2,018\\ 1,591\\ 3,242\\ 2,705\\ 2,196 \end{array}$	2, 152 1, 779 1, 479 2, 942 2, 461 2, 035	$1,742 \\1,542 \\1,385 \\2,461 \\2,120 \\1,841$	
0000	A and B	$ \left\{\begin{array}{c} 30 \\ 60 \\ 90 \\ 30 \\ 60 \\ 90 \end{array}\right. $	3, 774 3, 043 2, 316 4, 540 3, 807 3, 077	3, 747 3, 021 2, 303 4, 521 3, 791 3, 065	3, 710 2, 990 2, 283 4, 495 3, 768 3, 047	3, 608 2, 906 2, 234 4, 423 3, 705 3, 001	3, 471 2, 796 2, 176 4, 323 3, 620 2, 939	3, 306 2, 674 2, 116 4, 200 3, 517 2, 870	2, 934 2, 424 2, 012 3, 897 3, 275 2, 715	2, 453 2, 147 1, 908 3, 387 2, 912 2, 517	

# Appendix C.—SAGS FOR LINE CONDUCTORS STRUNG TO THE 2,000-POUND LIMITATION

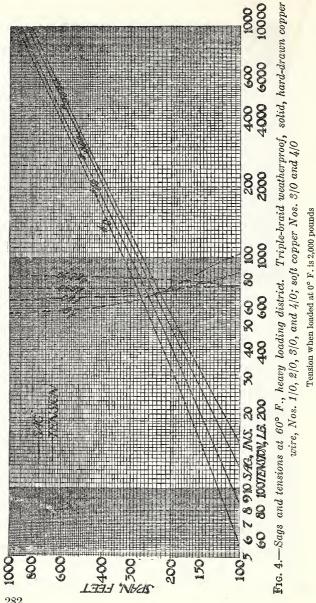
By stringing conductors so that, under the worst assumed condition of loading, the tension in the conductor does not exceed 2,000 pounds, the required strength of cross arms and pins is similarly limited. (See rules 261, D, 3, and 261, E, 1.) Values of sag at a stringing temperature of  $60^{\circ}$  F. which will keep the tension when loaded within this limit are given for conductor sizes having an ultimate strength in excess of 4,000 pounds. Figures 2 to 13 give the sag values for copper, and Figures 14, 15, and 16 for aluminum cable with steel core.

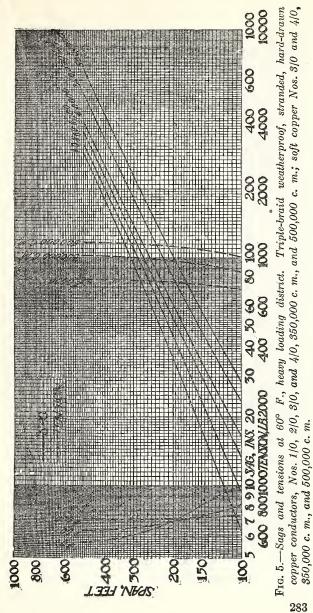


Tension when loaded at 0° F. is 2,000 pounds

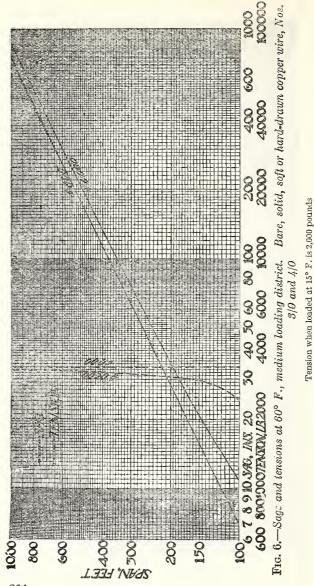


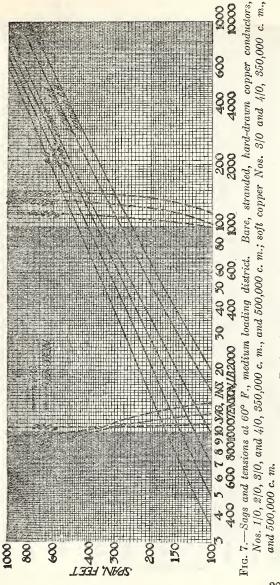
Tension when loaded at 0° F. is 2,000 pounds c. m.



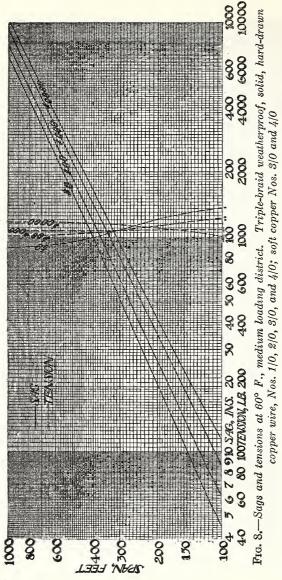


Tension when loaded at 0° F. is 2,000 pounds

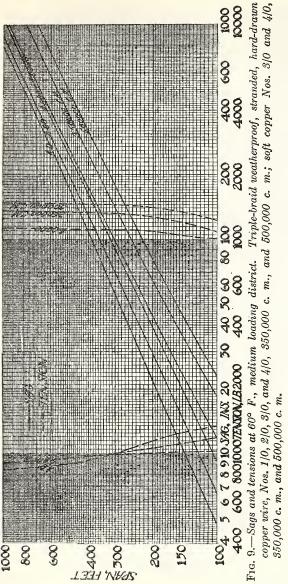




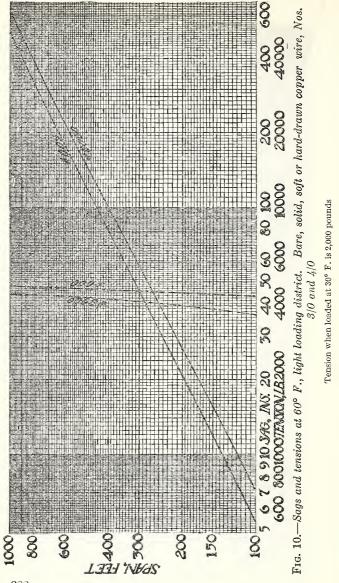
Tension when loaded at 15° F. is 2,000 pounds

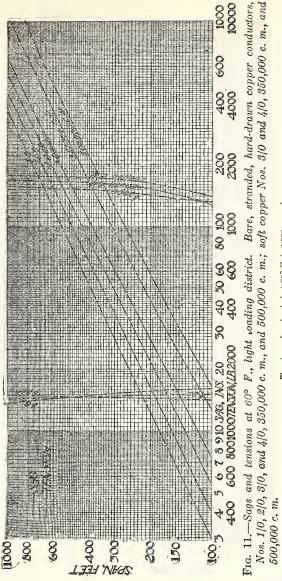


Tension when loaded at 15° F. is 2,000 pounds

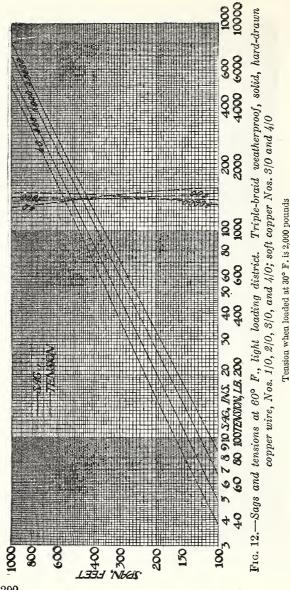


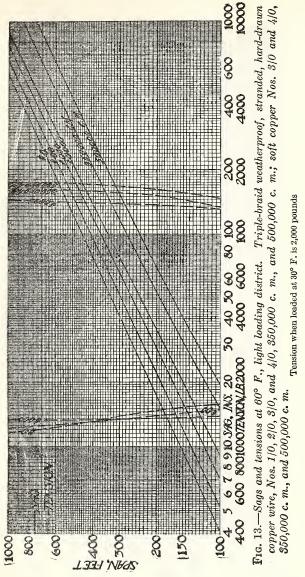
Tension when loaded at 15° F. is 2,000 pounds

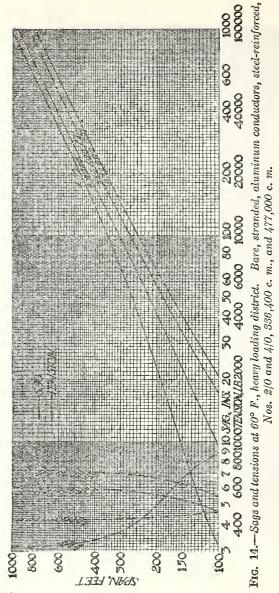




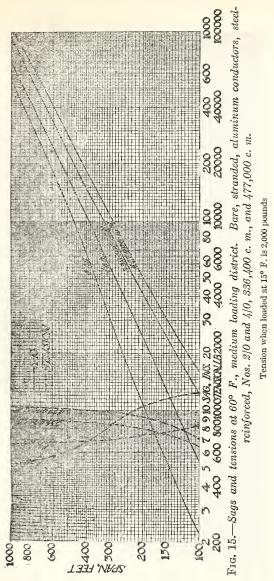
Tension when loaded at 30° F. is 2,000 pounds

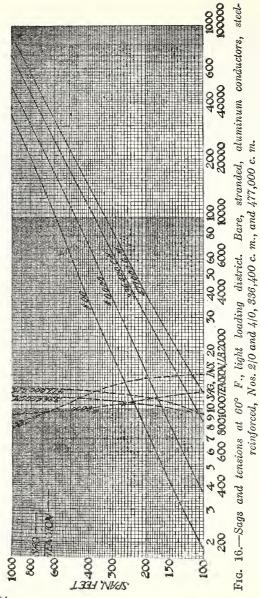






Tension when loaded at 0° F. is 2,000 pounds





Tension when loaded at 30° F. is 2,000 pounds

# Appendix D.—MECHANICAL DATA FOR WIRES AND CABLES

## Copper.

The following tables give the mechanical characteristics of copper wire and cable and are based on the standard specifications of the American Society for Testing Materials.

Hard-drawn copper manufactured in accordance with these specifications has an elastic limit of approximately 55 per cent of the ultimate strength given. Soft copper has no definite elastic limit, but it is below 5,000 pounds per square inch. It is not customarily stressed in excess of half its ultimate stress.

For purposes of calculation of sags and stresses, medium hard-drawn wire conforming with the A. S. T. M. specifications is considered as hard-drawn. The breaking load of stranded cable has been taken as 90 per cent of the sum of the breaking loads of the individual strands.

The modulus of elasticity has been taken at 16,000,000 pounds per square inch for all grades of copper. The coefficient of linear thermal expansion per degree Fahrenheit has been taken as  $9.6 \times 10^{-6}$ . The weight of bare solid copper conductors has been taken as 3.854 pounds per square inch of cross section per foot of length; and of stranded conductors as 3.931 pounds. The weights of covered conductors are given in Table 81.

## APPENDIX D

		Area of	Hard-dra	awn wire	Soft wire	
Size A. W. G. No.	Diameter	conduc- tor	Ultimate stress	Breaking load	Ultimate stress	Breaking load
0000	Inch 0.460 .410 .365 .325 .229 .249 .249 .244 .162 .128 .114 .102 .081 .064	$\begin{array}{c} Sg.\ in.\\ 0.\ 166\\ .\ 132\\ .\ 083\\ .\ 066\\ .\ 052\\ .\ 041\\ .\ 033\\ .\ 021\\ .\ 010\\ .\ 0082\\ .\ 0051\\ .\ 0032\\ \end{array}$	Lbs./in. <sup>2</sup> 49,000 51,000 52,800 54,500 56,100 57,600 57,600 59,000 60,100 62,100 63,700 64,300 64,300 65,700 66,200	$\begin{array}{c} Pounds \\ 8,100 \\ 6,700 \\ 5,500 \\ 4,500 \\ 3,700 \\ 2,400 \\ 2,000 \\ 1,300 \\ 830 \\ 660 \\ 530 \\ 340 \\ 210 \end{array}$	Lbs./in.2 36,000 36,000 36,000 37,000 37,000 37,000 37,000 37,000 37,000 37,000 37,000 37,000	Pounds         6,000         4,700         3,800         3,000         2,400         1,900         1,500         1,200         760         480         370         310

## Table 72 .- Solid Copper Wire

# Table 73.-Stranded Copper Conductors

•	Teterral	ĥ	Area of	Breaki	ng load
	External diameter	Stranding	conduc- tors	Hard- drawn	Soft
Circular mills: 1,000,000 500,000 450,000 350,000 350,000 350,000 200,000 20	.813 .772 .728	$\begin{array}{c} 61\times 0.128\\ 37\times .116\\ 37\times .104\\ 37\times .104\\ 37\times .097\\ 19\times .126\\ 37\times .092\\ 19\times .126\\ 37\times .082\\ 19\times .126\\ 37\times .082\\ 19\times .115\\ 19\times .064\\ 7\times .174\\ 19\times .004\\ 7\times .138\\ 19\times .075\\ 19\times .075\\ 7\times .123\\ 19\times .066\\ 7\times .097\\ 7\times .067\\ 7\times .067\\ 7\times .069\\ 7\times .061\\ 7\times .059\\ 7\times .069\\ 7\times .061\\ 7\times .059\\ 7\times .069\\ 7\times .0$	$\begin{array}{c} Sg.\ in.\\ 0.785\\ .392\\ .353\\ .314\\ .275\\ .236\\ .236\\ .26\\ .196\\ .196\\ .196\\ .166\\ .162\\ .132\\ .132\\ .132\\ .132\\ .104\\ .083\\ .066\\ .052\\ .052\\ .041\\ .033\\ .026\\ .041\\ .033\\ .026\\ .021\\ .016\\ .016\\ .016\end{array}$	$\begin{array}{c} Pounds \\ 45,000 \\ 22,700 \\ 22,700 \\ 22,700 \\ 20,500 \\ 13,900 \\ 13,900 \\ 13,900 \\ 13,900 \\ 11,300 \\ 11,300 \\ 11,300 \\ 9,700 \\ 9,200 \\ 7,700 \\ 7,409 \\ 6,100 \\ 4,900 \\ 4,900 \\ 4,900 \\ 4,900 \\ 3,050 \\ 2,450 \\ 1,550 \\ 1,230 \\ 980 \\ 780 \end{array}$	$\begin{array}{c} Pounds \\\hline 13,000 \\ 11,700 \\ 10,500 \\ 9,500 \\ 9,500 \\ 9,500 \\ 8,200 \\ 6,800 \\ 6,800 \\ 6,800 \\ 6,500 \\ 5,500 \\ 5,500 \\ 5,500 \\ 4,600 \\ 3,600 \\ 3,600 \\ 2,850 \\ 2,750 \\ 2,300 \\ 2,200 \\ 2,200 \\ 1,300 \\ 1,431 \\ 1,131 \\ 1,131 \\ 900 \\ 710 \\ 556 \\ 454 \end{array}$

296

Steel.

Tables 74 and 75 give the mechanical characteristics of steel wire and cable of three grades, ordinary, Siemens-Martin, and high-tension. The ultimate stresses of the three are taken as 60,000, 75,000, and 125,000 pounds per square inch, respectively. The breaking load of stranded cable has in all cases been taken as 90 per cent of the sum of the breaking loads of the individual strands.

The coefficient of linear thermal expansion for steel has been taken as  $6.7 \times 10^{-6}$  per ° F. The modulus of elasticity has been taken as 29,000,000 pounds per square inch for solid wires and 21,000,000 pounds per square inch for cables. The weight of conductor per square inch of cross section is taken as 3.39 pounds per foot of length.

Steel from different sources may differ in physical properties, and when materials are used having properties different from those assumed, loads and sags should be computed from the actual values.

Size Stl. W. G. No.	Diameter	8	Breaking load		
		Area	Ordinary	Siemens- Martin	High- tension steel
4 6 8	Inch 0. 225 . 192 . 162	$Sq. in. \\ 0.0400 \\ .0290 \\ .0206$	Pounds 2,400 1,740 1,240	Pounds 3,000 2,170 1,560	Pounds 5,000 3,620 2,570

Table 74 .- Bare Solid Steel Wires

	Table	75.—Stranded	Bare Steel	Conductors
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	Diameter		Breaking load			
Nominal size (inches)		Area	Ordinary	Siemens- Martin	High- tension steel	
5%	Inch 0. 625 . 562 . 500 . 437 . 375 . 312 . 250	$\begin{array}{c} Sq. in. \\ 0.2356 \\ .1922 \\ .1443 \\ .1204 \\ .0832 \\ .0606 \\ .0352 \end{array}$	Pounds 12, 720 10, 380 7, 790 6, 500 4, 490 3, 270 1, 900	Pounds 15, 900 13, 000 9, 740 8, 130 5, 620 4, 090 2, 380	Pounds 26, 500 21, 620 16, 230 13, 540 9, 360 6, 820 3, 960	

25804°-27-21

## Copper-Covered Steel.

Tables 76, 77, and 78 give the mechanical characteristics of copper-covered steel conductors of standard tensile grade and extra-high-tensile grade. The tables were submitted by the Copperweld Steel Co. for copperweld wire, with supporting data. The breaking load of stranded conductors has been taken as 90 per cent of the sum of the breaking loads of the individual strands.

Sags have been computed for standard tensile grade only. The coefficient of linear thermal expansion for these conductors has been taken as  $7.2 \times 10^{-6}$  per ° F. The modulus of elasticity for solid wires has been taken as 20,000,000 pounds per square inch. For stranded cables, the value of the modulus varies with size as follows:

5% inch diameter, 15,600,000 pounds per square inch.

 $\frac{9}{16}$  inch diameter, 16,100,000 pounds per square inch.

 $\frac{1}{2}$  inch diameter, 17,000,000 pounds per square inch.

 $\frac{7}{16}$  inch diameter, 17,800,000 pounds per square inch.

3% inch diameter, 18,600,000 pounds per square inch.

 $\frac{5}{16}$  inch diameter, 19,500,000 pounds per square inch.

The weight of conductor per square inch of cross section is taken as 3.53 pounds per foot of length.

	D: /		Breaking load		
Size A. W. G. No.	Diameter	Area	Standard	Extra-high tensile	
0000	Inch 0.460	Square inch 0. 166	Pounds 9,850	Pounds	
00000	.410 .365	.132 .104	8, 280 6, 850		
0	.325 .289	.083	5, 700 4, 800		
2	. 258	.052	4,000	7, 300	
3	.229 .204	.041 .033	3,200 2,650	5,780 4,600	
56	.182 .162	. 026 . 021	2,200 1,800	3, 640 2, 880	
7	.144 .128	.016 .013	1,450 1,200	2, 290 1, 820	
89 10	.120 .114 .102	.013	1, 200 970 800		
10-aa	. 102	.0082	800		

Table 76 .- Solid Bare Copper-Covered Steel Conductors

Table 77.—Stranded Bare	Copper-Covered	Steel	Conductors-
Standa	rd Tensile Grad	9	

Size A. W. G. No.	Nominal diameter	Stranding	Area	Breaking load
0000 000 00 0	Inch 5% 16 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2 1/2	7 No. 4 7 No. 5 7 No. 6 7 No. 6 7 No. 7 7 No. 8 7 No. 8 7 No. 9 7 No. 10	.182 .166 .144 .132 .114 .105 .091 .0829	Pounds 18, 550 15, 400 14, 300 12, 600 11, 640 10, 160 9, 460 8, 400 7, 780 6, 790 5, 600

\* Means special size wire, not an A.W.G. size.

## Table 78.—Stranded Bare Copper-Covered Steel Conductors—Extra-High Tensile Grade

Size A. W. G. No.	Nominal diameter	Stranding	Area	Breaking load
	Inch $\frac{7/8}{\frac{13}{16}}$	19 No. 5 19 No. 6 19 <sup>*</sup> 19 No. 7	Square inch 0. 495 . 392 . 354 . 311	Pounds 62, 240 49, 250 44, 600 39, 160
	11 16 5/8 5/8 <u>9</u> 16	19 <sup>x</sup> 19 No. 8 7 No. 4 7 No. 5	.275 .246 .229 .182	$34,800 \\ 31,120 \\ 28,980 \\ 22,930$
0000		7± 7 No. 6	$\begin{smallmatrix}&166\\&144\end{smallmatrix}$	20,940 18,200
000		7* 7 No. 7 7*	$.132 \\ .114 \\ .105$	16,600 14,420 13,160
	3⁄8	7 No. 8	. 091	11, 460

<sup>z</sup> Means special size wire, not an A.W.G. size.

## Aluminum.

Table 79 gives the mechanical characteristics of stranded aluminum conductors. The coefficient of linear thermal expansion for aluminum has been taken as  $12.8 \times 10^{-6}$  per degree Fahrenheit, and the modulus of elasticity as 9,000,000 pounds per square inch. The weight of conductor is 1.194 pounds per square inch of cross section for a length of 1 foot.

Table 80 gives the mechanical characteristics of aluminum cable having a steel core. The virtual coefficient of expansion, the modulus of elasticity, and the weight per unit length vary with the size of cable. For cables of sizes 4/0to 6, A. W. G., the coefficient of thermal expansion has been taken as  $10.5 \times 10^{-6}$  per degree Fahrenheit; the modulus of elasticity as 12,000,000 pounds per square inch; and the weight per unit cross section as 1.52 pounds per foot of length.

Size	Diam- eter	Area	Usual stranding	Copper equivalent	Elastic limit	Breaking load
Circular mils: 874, 500 795, 000 750, 000	Inches 1.077 1.026 .994	Square inch 0.687 .624 .589	$37 \times 0.154$ $37 \times .146$ $37 \times .142$	c. m. 550, 000 500, 000 472, 000	Pounds 9,600 8,750 8,250	Pounds 14, 800 13, 500 12, 700
715, 500 636, 000	.974 .918	. 562 . 500	37×.139 37×.131	450, 000 400, 000	7, 870 7, 000	12,100 10,800
556, 500 500, 000 477, 000 397, 500 300, 000	.856     .810     .793     .724     .621	. 437 . 393 . 375 . 312 . 236	$\begin{array}{c} 19 \times .171 \\ 19 \times .162 \\ 19 \times .158 \\ 19 \times .145 \\ 19 \times .126 \end{array}$	350,000 314,500 300,000 250,000 188,800	$\begin{array}{c} 6,120\\ 5,500\\ 5,240\\ 4,370\\ 3,300 \end{array}$	9,450 8,500 8,100 6,750 5,100
336, 400 266, 800	. 657 . 586	.264 .209	19× .133 7× .195	A. W. G. No. 4/0 3/0	3, 700 2, 940	5, 700 4, 550
A. W. G. No.: 4/0	.522 .464 .414 .368 .328	.166 .132 .104 .083 .066	$7 \times .174$ $7 \times .155$ $7 \times .138$ $7 \times .123$ $7 \times .109$	$2/0 \\ 0 \\ 1 \\ 2 \\ 3$	2,330 1,845 1,465 1,160 920	3, 570 2, 860 2, 270 1, 790 1, 420

Table 79 .- Stranded Aluminum Conductors

Size	Equivalent	Diam-	Stran	ding	Total	Breaking
5120	copper	eter	Aluminum	Steel	area	load
Circular mils: 795,000- 715,500- 636,000- 477,000- 397,500-	$\begin{array}{c} c. \ m. \\ 500, \ 000 \\ 450, \ 000 \\ 400, \ 000 \\ 300, \ 000 \\ 250, \ 000 \end{array}$	Inches 1. 093 1. 036 . 977 . 883 . 806	$54 \times 0.\ 1214$ $54 \times .\ 1151$ $54 \times .\ 1085$ $30 \times .\ 1261$ $30 \times .\ 1151$	$7 \times 0.1214$ $7 \times .1151$ $7 \times .1085$ $7 \times .1261$ $7 \times .1151$	Square inch 0.7060 .6350 .5640 .4620 .3850	Pounds 25, 150 22, 680 20, 060 20, 700 17, 250
336, 400 266, 800 <b>A.</b> W. G. No.: 0000 000 000 1	000	.741 .633 .564 .501 .447 .398 .355	$\begin{array}{c} 30 \times .1059 \\ 6 \times .2108 \\ 6 \times .1830 \\ 6 \times .1670 \\ 6 \times .1490 \\ 6 \times .1327 \\ 6 \times .1182 \end{array}$	$\begin{array}{c} 7\times .1059 \\ 7\times .0705 \\ 1\times .1830 \\ 1\times .1670 \\ 1\times .1490 \\ 1\times .1327 \\ 1\times .1182 \end{array}$	. 3260 . 2370 . 1939 . 1537 . 1219 . 0967 . 0766	14, 580 8, 450 7, 590 5, 995 4, 770 3, 780 3, 000
2 3 4 5 6	4 5 6 7 8	.316 .281 .250 .223 .198	$\begin{array}{c} 6\times .1052 \\ 6\times .0938 \\ 6\times .0834 \\ 6\times .0743 \\ 6\times .0661 \end{array}$	$\begin{array}{c} 1\times .1052 \\ 1\times .0938 \\ 1\times .0834 \\ 1\times .0743 \\ 1\times .0661 \end{array}$	. 0608 . 0482 . 0383 . 0303 . 0240	2, 394 1, 890 1, 500 1, 183 940

Table 80.-Aluminum Cables, Steel-Reinforced

The values given in these tables were submitted by the Aluminum Co. of America with supporting data. The breaking load of stranded conductors has been taken as 90 per cent of the sum of the breaking loads of the individual strands, including the steel core where used.

### APPENDIX E

# Appendix E.—LOADS UPON CONDUCTORS AND SUPPORTS

Table 81 gives the weights of conductors of various sizes and materials, with and without ice loading. Table 82 gives the transverse and resultant loads of the same conductors based on the assumed loadings of section 25. The over-all diameters of covered wires supplied by different manufacturers are not the same and hence average values have been chosen. This is also true of the sizes of strands which make up steel cables.

		Weight of-				
Size of conductor	Diameter over all	Conductor +0.5 inch of ice= heavy	Conductor +0.25 inch of ice= medium	Conductor only= light		
Bare solid copper: A. W. G. No.—	Inch	Lbs./ft.	Lbs./jt.	Lbs./ft.		
12	0.081	0.381	0.122	0.020		
108	.102 .128	. 406 . 440	$.141 \\ .168$	.031		
6	. 128	.440	. 103	.030		
V	. 102	. 101	. 201	.015		
4	. 204	. 564	. 268	.126		
3	. 229	. 612	. 308	.159		
2	. 258	. 672	. 359	.201		
1	. 289	. 744	. 421	. 253		
0	. 325	.832	. 498	.319		
00	.365	. 943	. 596	. 405		
000	. 410	1.075	.714	. 509		
0000	. 460	1.237	. 861	. 640		
Bare stranded copper:						
A. W. G. No	10	FOF	010	000		
6	. 18	. 505	. 216	. 083		
4	. 23	. 580	. 275	. 126		
3	. 26	. 634	. 320	. 161		
2	. 29	. 696	. 372	. 204		
1	. 33	.775	. 440	. 259		
0	. 37	. 867	. 519	. 326		
00	.41	. 979	. 618	. 413		
000	.46	1, 116	.740	. 519		
0000	. 52	1. 287	. 892	. 652		

Table 81.-Vertical Loads on Conductor Supports

# Table 81.---Vertical Loads on Conductor Supports-Continued

			Weight of-	
Size of conductor	Diameter over all	Conductor +0.5 inch of ice= heavy	Conductor +0.25 inch of ice= medium	Conductor only= light
Bare stranded copper—Continued. Cir. mils— 250,000	Inch 0.57 .63 .68 .73	$Lbs./ft. \\ 1.436 \\ 1.630 \\ 1.815 \\ 1.992$	Lbs./ft 1.025 1.201 1.370 1.539	Lbs./ft. 0.770 .928 1.081 1.234
450,000 500,000 1,000,000 T. B. W. P. solid copper: A. W. G. No	. 77 . 81 1. 15	$\begin{array}{c} 2.\ 177\\ 2.\ 355\\ 4.\ 112 \end{array}$	1. 705 1. 870 3. 521	1. 388 1. 541 3. 086
12. 10. 8. 6.	$21 \\ 25 \\ 26 \\ 32$	.476 .519 .547 .622	.178 .208 .234 .289	.035 .053 .075 .112
4 3 1	.38 .41 .44 .47	.711 .760 .840 .919	.370 .405 .474 .540	.164 .200 .260 .316
000 0000000 T. B. W. P. stranded copper: A. W. G. No.—	. 50 . 53 . 62 . 65	$\begin{array}{c} 1.\ 029\\ 1.\ 143\\ 1.\ 326\\ 1.\ 482 \end{array}$	. 640 . 745 . 900 1. 047	. 407 . 502 . 630 . 767
A. W. G. No 2	.444 .518 .620 .662 .734 .785	. 857      . 961      1. 120      1. 245      1. 421      1. 599	. 486     . 567     . 694     . 806     . 960     1.122	270 328 424 522 654 800
Cir. mils— 250,000 350,000 500,000 750,000 1,000,000 Bare solid steel:	.862 .978 1.108 1.343 1.531	1. 832 2. 264 2. 894 3. 968 4. 937	$\begin{array}{c} 1.\ 331\\ 1.\ 727\\ 2.\ 316\\ 3.\ 317\\ 4.\ 228 \end{array}$	. 985 1. 345 1. 894 2. 822 3. 674
Stl. W. G. No.— 8 6 4	.162 .192 .225	.482 .528 .586	. 198 . 235 . 283	. 070 . 098 . 135
Bare stranded steel: '4-inch '5-inch '5-inch '5-inch '5-inch '5-inch '5-inch '5-inch '5-inch '5-inch '5-inch '5-inch	$\begin{array}{r} .\ 250\\ .\ 312\\ .\ 375\\ .\ 437\\ .\ 500\\ .\ 562\\ .\ 625\end{array}$	586 .711 .826 .991 1.111 1.312 1.498	$\begin{array}{r} .\ 275\\ .\ 380\\ .\ 476\\ .\ 622\\ .\ 722\\ .\ 904\\ 1.\ 071\end{array}$	$\begin{array}{c} .119 \\ .205 \\ .282 \\ .408 \\ .489 \\ .652 \\ .799 \end{array}$

	-	Weight of—				
Size of conductor	Diameter over all	Conductor +0.5 inch of ice = heavy	Conductor +0.25 inch of ice= medium	Conductor only= light		
Solid bare copper-covered steel: A. W. G. No.— 10	$\begin{array}{c} Inch \\ 0, 102 \\ .128 \\ .162 \\ .204 \\ .306 \\ .384 \\ .432 \\ .436 \\ .546 \\ .546 \\ .546 \\ .293 \\ .328 \\ .328 \\ .368 \\ .414 \\ .464 \\ .522 \\ \end{array}$	$\begin{array}{c} Lbs./ft.\\ 0.402\\ .437\\ .485\\ .554\\ .710\\ .882\\ .998\\ 1.139\\ 1.313\\ 1.313\\ .554\\ .592\\ .637\\ .692\\ .756\\ .832\\ \end{array}$	$\begin{array}{c} Lbs./ft.\\ 0.138\\ .163\\ .201\\ .257\\ .382\\ .529\\ .630\\ .755\\ .910\\ .230\\ .230\\ .331\\ .379\\ .437\\ \end{array}$	$\begin{array}{c} Lbs.//t.\\ 0.029\\ 0.046\\ .073\\ .116\\ .209\\ .332\\ .418\\ .526\\ .663\\ .663\\ .663\\ .062\\ .079\\ .099\\ .125\\ .158\\ .198\\ .198\end{array}$		
A. W. G. No.— 4 2 1 0 000	$\begin{array}{r} .\ 250\\ .\ 316\\ .\ 355\\ .\ 398\\ .\ 447\\ .\ 501\\ .\ 564\\ .\ 741\\ .\ 883\\ \end{array}$	$\begin{array}{r} .523\\ .598\\ .647\\ .704\\ .772\\ .853\\ .954\\ 1.297\\ 1.605\\ \end{array}$	$\begin{array}{r} .\ 213\\ .\ 268\\ .\ 305\\ .\ 348\\ .\ 401\\ .\ 465\\ .\ 547\\ .\ 834\\ 1.\ 098 \end{array}$	$\begin{array}{c} .058\\ .092\\ .117\\ .147\\ .185\\ .232\\ .294\\ .527\\ .747\end{array}$		

Table	81Vertical	Loads	on	Conductor	Sup	ports—Continued
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## Table 82.—Transverse and Resultant Loads on Conductors and Supports in Three Loading Districts

[Pounds per conductor per linear foot]

Size of conductor		se force on o e covering		Resultant force on conductor due to weight and wind		
	Heavy	Medium	Light	Heavy	Medium	Light
Bare solid copper: A. W. G. No.— 12 10 8 6	0. 721 . 735 . 752 . 775	$0.387 \\ .401 \\ .419 \\ .442$	$\begin{array}{c} 0.\ 081 \\ .\ 102 \\ .\ 128 \\ .\ 162 \end{array}$	0.815 .840 .872 .918	$0.\ 406 \\ .\ 425 \\ .\ 451 \\ .\ 467$	0.084 .107 .137 .180

T.

## Table 82.—Transverse and Resultant Loads on Conductors and Supports in Three Loading Districts—Continued

[Pounds per conductor per linear foot]

Size of conductor		se force on a e covering (		Resultant force on conductor due to weight and wind		
	Heavy	Medium	Light	Heavy	Medium	Light
Bare solid copper-Contd.						
A. W. G. No	0.803	0.470	0.204	0. 986	0.540	0.240
3	. 820	.486	. 229	1. 023	. 576	. 279
2	. 839	. 506	. 258	1.075	. 620	. 327
1	. 860	. 526	. 289	1.137	. 674	. 384
0	. 884	. 550	. 325	1.214	. 742	. 456
00	. 910	. 577	. 365	1.310	. 829	. 545
000	. 940	. 607	. 410	1.428	. 937	. 653
0000	. 974	. 640	. 460	1.574	1.073	. 788
Bare stranded copper: A, W, G, No.—						
6	. 787	. 454	. 180	. 935	. 503	. 198
4	. 820	.487	. 230	1.005	• . 559	. 262
3	. 840	. 507	. 260	1.053	. 599	. 306
2	. 860	. 527	. 290	1.106	. 645	. 355
1	. 887	. 554	. 330	1.178	. 707	. 420
0	. 914	. 580	.370	1.260	. 779	. 493
00	. 940	. 607	. 410	1.357	. 866	. 582
000	. 974	. 640	. 460	1.481	. 978	. 693
0000	1.014	. 680	. 520	1.638	1.122	.834
Cir. mils— 250,000	1.047	.714	. 570	1.777	1.294	059
300,000	1.047	.754	. 630	1. 960	1. 294	.958 1.121
350,000		.787	. 680	2, 133	1. 580	1.271 1.277
400,000		. 820	. 730	2.308	1.744	1. 434
450,000	1.181	.847	.770	2.477	1.904	1.587
500,000	1.207	.874	. 810	2.646	2.064	1.741
1,000,000	1.434	1.100	1.150	4.355	3.822	3.293
T. B. W. P. solid copper: A. W. G. No	1					
12	. 807	. 474	. 210	. 937	. 506	.213
10	. 834	. 500	. 250	. 987	. 542	. 255
8	. 840	. 507	. 260	1.003	. 558	. 270
6		. 547	. 320	1.078	. 619	. 339
4		. 587	. 380	1.163	.694	. 414
3	. 940	.607 .627	.410 .440	$1.213 \\ 1.276$	.730	. 456
2	. 900	. 647	. 440	1. 276	. 768 . 843	.511 .566
		0.00				
0	1.000 1.020	.667	. 500	1.435 1.532	. 924 1. 013	. 645 . 730
000	1.020	. 747	. 620	1. 532	1. 013	. 730
0000	1,100	.767	. 650	1.846	1. 286	1.005
T. B. W. P. stranded copper:					1.200	** 500
A. W. G. No						
2	. 961	. 630	. 444	1.289	. 796	. 520
1		. 679	. 518	1.396	.884	.613
0	1.080 1.109	.747 .775	. 620 . 662	1.557 1.667	1.020	.751
00	1. 109	. 823	. 002	1. 832	1.118	.843
0000	1, 191	.857	,785	1.994	1. 412	1. 121

### APPENDIX E

## Table 82.—Transverse and Resultant Loads on Conductors and Supports in Three Loading Districts—Continued

Pounds	per	conductor	per	linear	foot]
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Size of conductor		e force on co e covering (		Resultant force on conductor due to weight and wind		
Dize of conductor	Heavy	Medium	Light	Heavy	Medium	Light
T. B. W. P. stranded cop-						
per-Continued.						
Cir. mils—	1.041	0.000	0.000	0.010	1 011	
250,000	1.241 1.319	0.908	0.862 .978	2.213 2.620	1.611 1.988	1.309
500.000	1. 319	1.072	1.108	3. 217	2. 552	1.663 2.194
750,000	1. 563	1. 229	1. 343	4. 265	3. 538	2.194
1,000,000	1.688	1.355	1.531	5.218	4.439	3, 980
Bare solid steel:						0.000
Stl. W. G. No						
8	.775	.442	.162	. 912	. 484	. 176
6	. 795	.462	.192	, 955	. 518	. 216
4	.817	. 484	. 225	1.006	. 560	. 263
Bare stranded steel:	000	500	050	1 010		
<sup>1</sup> / <sub>4</sub> •inch	. 833	. 500	. 250	1.018	. 570	. 277
5-inch %-inch	.875	.542 .583	.312 .375	$1.126 \\ 1.234$	.661 .753	. 374
$\frac{7}{16}$ -inch	. 958	. 625	. 437	1. 234	. 882	. 469
16-inch	1.000	. 667	. 500	1. 495	. 983	. 699
-inch	1.042	.708	. 562	1.675	1,149	.861
9 16-inch 5/8-inch	1.083	.750	. 625	1.849	1.307	1.014
Solid bare copper-covered steel:						
A. W. G. No						
10	. 735	. 401	. 102	. 838	. 425	. 106
8	.752	. 419	.128	. 870	. 450	.136
6	.775	. 442	. 162	.914	. 485	. 178
4	. 803	. 470	. 204	. 975	. 535	. 235
stranded bare copper-cov-		1				
ered steel:	. 871	. 538	. 306	1, 124	. 659	070
%-inch	. 923	. 590	. 305	$1.124 \\ 1.276$	. 659	. 370
76-inch		.622	. 432	1.381	. 885	. 601
16-inch	. 991	.658	.486	1.510	1.001	.716
<sup>9</sup> -inch	1.031	. 698	. 546	1.670	1.147	.859
Bare stranded aluminum: A. W. G. No.—						
2	, 862	. 529	. 293	1.020	. 577	.300
1		. 552	. 328	1.065	. 609	. 337
0		. 579	.368	1.113	. 647	. 380
00	. 943	. 610	.414	1.170	. 693	. 432
000	. 976	. 643	.464	1.234	.746	. 489
0000	1, 015	. 682	. 522	1.312	.810	. 557
Bare stranded aluminum						
steel-reinforced: A. W. G. No.—				1		
A. W. G. NO	, 834	. 500	.250	. 984	. 544	. 257
2	.878	.544	. 316	1.062	.607	. 329
1		.570	.355	1.112	.646	. 374
0	. 932	. 599	. 398	1. 168	. 693	. 424
00	. 965	.632	. 447	1.236	.748	. 484
000	1.001	. 668	. 501	1.315	.814	. 552
0000	1.043	.710	. 564	1.414	. 896	. 636
Cir. mils—						
336,400		. 828	. 741	1.741	1.175	. 909
477,000	1.256	. 922	. 883	2.038	1.434	1.157

# Appendix F.-WOOD POLES

# Moments of Resistance of Poles.

The resisting moments of wood poles of various groundline circumferences are given in the accompanying tables for each value of allowable fiber stress recognized in Table 21 (rule 261A, 4) for poles when installed. Table 83 gives the values for dense southern yellow pine; Table 84 for other pine, chestnut, western cedar, cypress, etc., having a recognized ultimate fiber stress of 5,000 pounds per square inch; and Table 85 for woods having an ultimate fiber stress of 3,600 pounds per square inch, such as redwood and eastern cedar (northern white cedar).

Southern yellow pine should not be used for supporting structures unless first given a preservative treatment, as otherwise the rapid deterioration will require early replacement.

The following formula has been used in calculating the moments:

 $M = 0.0002638 f C^3 =$  moment in pound-feet; where

f = allowable fiber stress in pounds per square inch, and

C=circumference of the pole at ground line in inches. While the ground-line section may not be the most stressed section in poles with considerable taper, it is so regarded here. Since the wood usually deteriorates most rapidly at this point, it is here that sufficient strength must be provided.

### APPENDIX F

## Table 83.—Resisting Moments for Poles of Woods Having Ultimate Fiber Stress of 6,500 Pounds per Square Inch (Dense Southern Yellow Pine)

Circumference at ground line	Resisting moments for fiber stress of (pounds per square inch)						
(inches)	2,170	2,600	3,250	3,900	4,870	6,500	
24 25 26 27	$\begin{array}{c} Lb.\text{-}ft.\\7,900\\8,950\\10,050\\11,250\end{array}$	$\begin{array}{c} Lbft.\\ 9,500\\ 10,700\\ 12,050\\ 13,500 \end{array}$	$\begin{array}{c} \textit{Lbft.}\\ 11,850\\ 13,400\\ 15,050\\ 16,900 \end{array}$	Lbft. 14, 200 16, 100 18, 100 20, 250	Lbft. 17, 750 20, 050 22, 600 25, 300	Lbft. 23, 700 26, 800 30, 150 33, 750	
28 29 30	$\begin{array}{c} 12,550\\ 13,950\\ 15,450\\ 17,050 \end{array}$	15, 050 16, 750 18, 500 20, 450	$\begin{array}{c} 18,800\\ 20,900\\ 23,150\\ 25,550 \end{array}$	22,600 25,100 27,800 30,650	$28, 200 \\ 31, 350 \\ 34, 700 \\ 38, 250$	$\begin{array}{c} 37,650\\ 41,800\\ 46,300\\ 51,100 \end{array}$	
32 33 34 35	$\begin{array}{c} 18,750\\ 20,550\\ 22,500\\ 24,550\end{array}$	22, 500 24, 650 26, 950 29, 400	$\begin{array}{c} 28,100\\ 30,800\\ 33,700\\ 36,750 \end{array}$	33,700 36,950 40,450 44,100	42, 100 46, 150 50, 500 55, 100	56,200 61,600 67,400 73,500	
36	$\begin{array}{c} 26,700\\ 29,000\\ 31,400\\ 33,950 \end{array}$	32,000 34,750 37,650 40,700	40, 000 43, 400 47, 050 50, 850	48,000 52,100 56,450 61,050	59, 950 65, 050 70, 500 76, 200	80,000 86,850 94,100 101,700	
40 41 42 43	36, 650 39, 450 42, 400 45, 500	43, 900 47, 250 50, 800 54, 550	$54,850 \\ 59,100 \\ 63,500 \\ 68,150$	65, 850 70, 900 76, 200 81, 800	82, 200 88, 550 95, 200 102, 150	109, 750 118, 200 127, 050 136, 350	
44	48, 750 52, 150 55, 700 59, 450	58,450 62,500 66,750 71,200	73,05078,15083,45089,000	87, 650 93, 750 100, 150 106, 800	$109, 450 \\117, 050 \\125, 050 \\133, 400$	$146,050\\156,250\\166,900\\178,000$	
48 49 50 51	63,300 67,350 71,550 75,950	75, 850 80, 700 85, 750 91, 000	94, 800 100, 850 107, 150 113, 750	$113,800 \\121,050 \\128,600 \\136,450$	142, 100 151, 150 160, 600 170, 400	$189, 650 \\ 201, 750 \\ 214, 350 \\ 227, 450$	
52 53 54 55	80, 500 85, 200 90, 150 95, 250	$\begin{array}{r} 96,450\\ 102,100\\ 108,000\\ 114,100 \end{array}$	$\begin{array}{c} 120,550\\ 127,650\\ 135,000\\ 142,650\end{array}$	$\begin{array}{c} 144,650\\ 153,150\\ 162,000\\ 171,150\end{array}$	180, 650 191, 250 202, 300 213, 750	$\begin{array}{c} 241,100\\ 255,300\\ 270,000\\ 285,300 \end{array}$	
56	$100, 550 \\ 106, 000 \\ 111, 700 \\ 117, 550$	$\begin{array}{c} 120,450\\ 127,000\\ 133,800\\ 140,850 \end{array}$	$\begin{array}{c} 150,550\\ 158,800\\ 167,300\\ 176,100 \end{array}$	180, 700 190, 550 200, 750 211, 300	$\begin{array}{c} 225,600\\ 237,900\\ 250,650\\ 263,850 \end{array}$	$\begin{array}{c} 301,150\\ 317,550\\ 334,550\\ 352,150 \end{array}$	
60 61 62 63	123, 650 129, 950 136, 450 143, 150	$\begin{array}{c} 148, 150 \\ 155, 700 \\ 163, 450 \\ 171, 500 \end{array}$	$\begin{array}{c} 185,200\\ 194,600\\ 204,350\\ 214,400 \end{array}$	$\begin{array}{c} 222,200\\ 233,500\\ 245,200\\ 257,250 \end{array}$	277, 500 291, 600 306, 200 321, 250	370, 400 389, 200 408, 650 428, 750	

# 308

# Table 83.—Resisting Moments for Poles of Woods Having Ultimate Fiber Stress of 6,500 Pounds per Square Inch (Dense Southern Yellow Pine—Continued)

Circumference at ground line (inches)	Resisting moments for fiber stress of (pounds per square inch)						
	2,170	2,600	3,250	3,900	4,870	6,500	
64         65           65         66           66         67           68         69           70         71           71         72           73         74           75         5	<i>Lbft.</i> 150,050 157,200 164,600 172,150 180,000 188,050 196,350 204,900 213,650 222,700 231,950 241,500	<i>Lbft.</i> 179,800 188,350 197,200 206,300 215,050 225,300 235,250 245,500 256,000 266,800 277,950 289,350	Lbft. 224,750 235,450 246,500 257,850 281,650 294,050 306,850 320,000 335,500 347,400 361,700	Lbft. 269,700 282,550 295,800 309,450 338,000 352,900 368,250 384,000 400,250 416,900 434,050	Lbft. 336, 800 352, 800 369, 350 386, 400 403, 950 422, 050 440, 650 459, 800 479, 500 499, 750 520, 600 542, 000	$\begin{array}{c} Lbft.\\ 449,500\\ 470,900\\ 492,950\\ 515,700\\ 539,150\\ 563,300\\ 588,150\\ 613,700\\ 640,000\\ 667,050\\ 694,850\\ 723,400 \end{array}$	

## Table 84.—Resisting Moments for Poles of Woods with Ultimate Fiber Stress of 5,000 Pounds per Square Inch (Pine, Chestnut, Western Cedar, Cypress, etc.)

Resisting moments for fiber stress of (pounds per square inch)-							
1,250	1,670	2,000	2,500	3,000	3,750	5,000	
$\begin{array}{c} Lbft.\\ 4,550\\ 5,150\\ 5,800\\ 6,500\\ 7,250\\ 8,050\\ 8,900\\ 9,800\\ \end{array}$	$\begin{array}{c} Lbft.\\ 6,100\\ 6,900\\ 7,750\\ 8,650\\ 9,650\\ 10,750\\ 11,900\\ 13,100\\ \end{array}$	$\begin{matrix} Lbft.\\7,300\\8,250\\9,250\\10,400\\11,600\\12,850\\14,250\\15,700 \end{matrix}$	<i>Lbft.</i> 9, 100 10, 300 11, 600 13, 000 14, 500 16, 100 17, 800 19, 650	$\begin{array}{c} Lbft.\\ 10, 950\\ 12, 350\\ 13, 900\\ 15, 600\\ 17, 350\\ 19, 300\\ 21, 350\\ 23, 600\\ \end{array}$	$\begin{array}{c} Lb.\text{-ft.}\\ 13,700\\ 15,450\\ 17,400\\ 19,450\\ 21,700\\ 24,150\\ 26,700\\ 29,450\\ \end{array}$	$\begin{matrix} Lbft.\\ 18,250\\ 20,600\\ 23,200\\ 25,950\\ 28,950\\ 32,150\\ 35,600\\ 39,300 \end{matrix}$	
10, 800 11, 850 12, 950 14, 150 15, 400 16, 700 18, 100	14, 450 15, 850 17, 300 18, 900 20, 550 22, 300 24, 150	$17, 300 \\ 18, 950 \\ 20, 750 \\ 22, 600 \\ 24, 600 \\ 26, 700 \\ 28, 950 \\ 17, 100 \\ 18, 100 \\ 18, 100 \\ $	$\begin{array}{c} 21,600\\ 23,700\\ 25,900\\ 28,300\\ 30,750\\ 33,400\\ 36,200\\ \end{array}$	25,95028,45031,10033,95036,90040,10043,450	$\begin{array}{c} 32,400\\ 35,550\\ 38,900\\ 42,400\\ 46,150\\ 50,100\\ 54,300\\ \end{array}$	$\begin{array}{r} 43,200\\ 47,400\\ 51,850\\ 56,550\\ 61,550\\ 66,800\\ 72,400\\ \end{array}$	
	1,250 <i>Lbft.</i> 4,550 5,150 6,500 7,250 8,050 8,050 9,800 10,800 11,850 12,950 14,150 15,400 16,700	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	

### APPENDIX F

## Table 84.—Resisting Moments for Poles of Woods with Ultimate Fiber Stress of 5,000 Pounds per Square Inch (Pine, Chestnut, Western Cedar, Cypress, etc.)—Continued

Circumference at ground line	Resisting moments for fiber stress of (pounds per square inch)-							
(inches)	1,250	• 1,670	2,000	2,500	3,000	3,750	5,000	
40 41 42 43	$\begin{array}{c} Lbft.\\ 21,100\\ 22,750\\ 24,450\\ 26,200 \end{array}$	Lbft. 28, 200 30, 350 32, 650 35, 050	$\begin{array}{c} Lbft.\\ 33,750\\ 36,350\\ 39,100\\ 41,950\end{array}$	$\begin{array}{c} Lbft.\\ 42,200\\ 45,450\\ 48,850\\ 52,450\end{array}$	Lbft. 50, 650 54, 550 58, 650 62, 900	Lbft. 63, 300 68, 200 73, 300 78, 650	Lbft. 84, 400 90, 900 97, 700 104, 850	
44 45 46 47	$\begin{array}{c} 28,100\\ 30,050\\ 32,100\\ 34,250 \end{array}$	37, 550 40, 150 42, 900 45, 750	44, 950 48, 100 51, 350 54, 800	56, 200 60, 100 64, 200 68, 500	67, 400 72, 100 77, 050 82, 150	84, 250 90, 150 96, 300 102, 700	$\begin{array}{c} 112, 350 \\ 120, 200 \\ 128, 400 \\ 136, 950 \end{array}$	
48 49 50 51	36, 450 38, 800 41, 200 43, 750	$\begin{array}{r} 48,700\\ 51,850\\ 55,050\\ 58,450\end{array}$	58, 350 62, 050 65, 950 70, 000	72, 950 77, 600 82, 450 87, 500	87, 500 93, 100 98, 900 105, 000	$\begin{array}{c} 109,400\\ 116,400\\ 123,650\\ 132,200 \end{array}$	$145, 850 \\ 155, 200 \\ 164, 900 \\ 174, 950$	
52 53 54 55	46, 350 49, 100 51, 900 54, 850	61, 950 65, 600 69, 350 73, 300	74, 200 78, 550 83, 100 87, 800	92, 750 98, 200 103, 850 109, 700	$\begin{array}{c} 111,300\\ 117,800\\ 124,600\\ 131,650 \end{array}$	$\begin{array}{c} 139,100\\ 147,300\\ 155,750\\ 164,600 \end{array}$	185, 450 196, 350 207, 700 219, 450	
56 57 58 59	57, 900 61, 050 64, 350 67, 700	77, 350 81, 600 85, 950 90, 500	92, 650 97, 700 102, 950 108, 350	$\begin{array}{c} 115,800\\ 122,150\\ 128,700\\ 135,450 \end{array}$	$\begin{array}{c} 139,000\\ 146,550\\ 154,400\\ 162,550\end{array}$	$173,750\\183,200\\193,000\\203,150$	231, 650 244, 250 257, 350 270, 900	
60 61 62 63	$71, 250 \\74, 850 \\78, 600 \\82, 450$	95, 150 100, 000 104, 500 110, 150	113, 900 119, 750 125, 750 131, 900	$\begin{array}{c} 142,450\\ 149,700\\ 157,200\\ 164,900 \end{array}$	$170, 950 \\ 179, 650 \\ 188, 600 \\ 197, 900$	213, 700 224, 550 235, 750 247, 350	284, 900 299, 40 <b>0</b> 314, 350 329, 800	
64 65 66 67	86, 450 90, 550 94, 800 99, 200	$\begin{array}{c} 115,500\\ 121,000\\ 126,650\\ 132,500 \end{array}$	138, 300 144, 900 151, 700 158, 700	172, 900 181, 100 189, 600 198, 350	$\begin{array}{c} 207,450\\ 217,350\\ 227,500\\ 238,000 \end{array}$	$259, 350 \\ 271, 650 \\ 284, 400 \\ 297, 550$	345,750 362,250 379,200 396,700	
68 69 70 71	$\begin{array}{c} 103,700\\ 108,350\\ 113,100\\ 118,000 \end{array}$	$\begin{array}{c} 138,500\\ 144,700\\ 151,100\\ 157,700 \end{array}$	165, 900 173, 300 180, 950 188, 850	$\begin{array}{c} 207,350\\ 216,650\\ 226,200\\ 236,050 \end{array}$	$\begin{array}{c} 248,850\\ 260,000\\ 271,450\\ 283,250 \end{array}$	311,050 325,000 339,300 354,050	414, 750 433, 300 452, 400 472, 100	
72 73 74 75	$\begin{array}{c} 123,100\\ 128,250\\ 133,600\\ 139,100 \end{array}$	164, 450 171, 400 178, 500 185, 850	$\begin{array}{c} 196,950\\ 205,250\\ 213,800\\ 222,600 \end{array}$	$\begin{array}{c} 246,150\\ 256,550\\ 267,250\\ 278,250 \end{array}$	295, 400 307, 850 320, 700 333, 850	369, 250 384, 850 400, 850 417, 300	$\begin{array}{c} 492,300\\ 513,100\\ 534,500\\ 556,450\end{array}$	

## Table 85.—Resisting Moments for Poles of Woods Having Ultimate Fiber Stress of 3,600 Pounds per Square Inch (Eastern Cedar, Redwood, etc.)

Circumference at	Resisting moment for fiber stress of (pounds per square inch)								
ground line (inches)	900	1,200	1,440	1,800	2,160	2,700	3,600		
24 25 26 27	Lb -ft. 3,300 3,700 4,150 4,650	$\begin{array}{c} Lbft.\\ 4,400\\ 4,950\\ 5,550\\ 6,250\end{array}$	Lbft. 5, 250 5, 950 6, 700 7, 500	Lbft. 6, 550 7, 400 8, 350 9, 350	Lbft. 7, 900 8, 900 10, 000 11, 200	Lbft. 9,850 11,150 12,500 14,000	Lbft. 13, 150 14, 850 16, 700 18, 700		
28 29 30 31	5, 200 5, 800 6, 400 7, 050	6, 950 7, 700 8, 550 9, 450	8, 350 9, 250 10, 250 11, 300	$10,400 \\ 11,600 \\ 12,800 \\ 14,150$	12, 500 13, 900 15, 400 17, 000	$15,650 \\ 17,350 \\ 19,250 \\ 21,200$	20, 850 23, 150 25, 650 28, 300		
32 33 34 35	7, 800 8, 550 9, 350 10, 200	$10,350 \\ 11,400 \\ 12,450 \\ 13,550$	$\begin{array}{c} 12,450\\ 13,650\\ 14,950\\ 16,300 \end{array}$	15, 550 17, 050 18, 650 20, 350	$18,650 \\ 20,500 \\ 22,400 \\ 24,450$	$\begin{array}{c} 23,350\\ 25,600\\ 28,000\\ 30,550 \end{array}$	$31, 100 \\ 34, 150 \\ 37, 350 \\ 40, 700$		
36 37 38 39	11, 100 12, 050 13, 050 14, 100	$\begin{array}{c} 14,750\\ 16,050\\ 17,350\\ 18,800 \end{array}$	17, 700 19, 250 20, 850 22, 550	22, 150 24, 050 26, 050 28, 150	26, 600 28, 850 31, 250 33, 800	$\begin{array}{c} 33,250\\ 36,100\\ 39,100\\ 42,250\end{array}$	$\begin{array}{r} 44,300\\ 48,100\\ 52,100\\ 56,350\end{array}$		
40 41 42 43	15, 200 16, 350 17, 600 18, 900	20, 250 21, 800 23, 450 25, 150	24, 300 26, 200 28, 150 30, 200	30, 400 32, 750 35, 200 37, 750	36, 450 39, 250 42, 200 45, 300	45, 600 49, 100 52, 750 56, 650	60, 800 65, 450 70, 350 75, 500		
44 45 46 47	20, 200 21, 650 23, 100 24, 650	26, 950 28, 850 30, 800 32, 850	32, 350 34, 600 37, 000 39, 450	40, 450 43, 250 46, 200 49, 300	48, 550 51, 900 55, 450 59, 150	60, 650 64, 900 69, 350 73, 950	80, 900 86, 550 92, 450 98, 600		
48 49 50 51	26, 250 27, 950 29, 700 31, 500	$35,000 \\ 37,250 \\ 39,550 \\ 42,000$	42,000 44,700 47,500 50,400	52, 500 55, 850 59, 350 63, 000	$\begin{array}{c} 63,000\\ 67,050\\ 71,250\\ 75,600 \end{array}$	78, 750 83, 800 89, 050 94, 500	$\begin{array}{c} 105,050\\ 111,750\\ 118,700\\ 126,000 \end{array}$		
52 53 54 55	33, 400 35, 350 37, 400 39, 500	44, 500 47, 150 49, 850 52, 650	53,400 56,550 59,800 63,200	66, 750 70, 700 74, 750 79, 000	80, 100 84, 850 89, 700 94, 800	100, 150 106, 050 112, 150 118, 500	$133,550\\141,400\\149,550\\158,000$		
56 57 58 59	41, 700 43, 950 46, 300 48, 750	55, 600 58, 600 61, 750 65, 000	66, 700 70, 350 74, 100 78, 000	83, 400 87, 950 92, 650 97, 500	100, 050 105, 500 111, 200 117, 500	$\begin{array}{c} 125,100\\ 131,900\\ 138,950\\ 146,300 \end{array}$	166,800 175,850 185,300 195,050		
60 61 62 63	51, 300 53, 900 56, 600 59, 350	68, 400 71, 850 75, 450 79, 150	82, 050 86, 200 90, 550 95, 000	$\begin{array}{c} 102,550\\ 107,800\\ 113,150\\ 118,750 \end{array}$	$\begin{array}{c} 123,100\\ 129,350\\ 135,800\\ 142,500 \end{array}$	$\begin{array}{c} 153,850\\ 161,650\\ 169,750\\ 178,100 \end{array}$	$\begin{array}{c} 205,150\\ 215,550\\ 226,350\\ 237,450 \end{array}$		
64 65 66 67	62, 250 65, 200 68, 250 71, 400	83,000 86,950 91,000 95,200	99,600 104,300 109,200 114,250	$\begin{array}{c} 124,500\\ 130,400\\ 136,500\\ 142,800 \end{array}$	149, 350 156, 900 163, 800 171, 400	186, 700 195, 600 204, 750 214, 200	$\begin{array}{c} 248,950\\ 260,800\\ 273,050\\ 285,650\end{array}$		

### APPENDIX F

Circumference at	Resisti	ng momen	t for fiber	stress of (p	ounds per	square inc	h)—
ground line (inches)	900	1,200	1,440	1,800	2,160	2,700	3,600
68 69 70 71 72 73 74 75	$\begin{array}{c} Lbft.\\ 74, 650\\ 78, 000\\ 81, 450\\ 85, 000\\ \\ 88, 600\\ 92, 350\\ 96, 200\\ 100, 150\\ \end{array}$	$\begin{array}{c} Lbft.\\ 99,550\\ 104,000\\ 108,600\\ 113,300\\ 118,150\\ 123,150\\ 128,300\\ 133,550\\ \end{array}$	$\begin{array}{c} Lbft.\\ 119, 450\\ 124, 800\\ 130, 300\\ 135, 950\\ 141, 800\\ 147, 800\\ 153, 950\\ 160, 250\\ \end{array}$	$\begin{array}{c} Lbft.\\ 149,300\\ 156,000\\ 162,850\\ 169,950\\ 177,250\\ 184,700\\ 192,400\\ 200,300 \end{array}$	$\begin{array}{c} Lbft.\\ 179, 150\\ 187, 200\\ 195, 450\\ 203, 950\\ 212, 700\\ 221, 650\\ 230, 900\\ 240, 400\\ \end{array}$	$\begin{array}{c} Lbft.\\ 223,950\\ 234,000\\ 244,300\\ 255,000\\ 265,850\\ 277,100\\ 288,600\\ 300,500\\ \end{array}$	$\begin{array}{c} Lbft.\\ 298,600\\ 312,000\\ 325,750\\ 339,900\\ 354,450\\ 369,450\\ 384,850\\ 400,650\\ \end{array}$

Table 85.—Resisting Moments for Poles of Woods Having Ultimate Fiber Stress of 3,600 Pounds per Square Inch (Eastern Cedar, Redwood, etc.)—Continued

# Depreciation of Wood Poles.

Rule 261, A, 4 stipulates that wood poles shall be of such material and dimensions that the loading specified in section 25 will not cause the fiber stresses given in Table 20 to be exceeded. The allowable fiber stresses vary with the grade of construction, and even with a stated grade of construction vary according to the situation and according to whether the pole has had previous preservative treatment. When the pole has deteriorated to such an extent that the fiber stress reaches another specified value, the pole must be replaced. The percentage of depreciation varies with the con-Table 86 gives the minimum permissible depreditions. ciated ground-line circumference for poles which have just met the requirements when installed. Table 88 gives the same information in terms of the permissible reduction in the radius of the cross section of the pole taken at the ground line. Table 87 shows the situations to which the various values in Tables 86 and 88 apply.

## Table 86.—Minimum Depreciated Ground-Line Circumference of Wood Poles

Ground-line circumference when installed (inches)	for rati				d-line circ to fiber st	
	2/3	3/5	5/9	1/2	4/9	2/5
24 25 26	Inches 21. 0 21. 8 22. 7 23. 6	Inches 20. 2 21. 1 21. 9 22. 8	Inches 19.7 20.6 21.5 22.2	Inches 19.0 19.8 20.6 21.4	Inches 18.3 19.1 19.8 20.6	Inches 17. 7 18. 4 19. 2 19. 9
28 29 30 31	24. 5 25. 3 26. 2 27. 1	23. 6 24. 5 25. 3 26. 1	23. 0 23. 8 24. 7 25. 5	22. 2 23. 0 23. 8 24. 6	21. 4 22. 1 22. 9 23. 7	20. 6 21. 4 22. 1 22. 8
32 33 34 35	$\begin{array}{c} 28.\ 0\\ 28.\ 8\\ 29.\ 7\\ 30.\ 6\end{array}$	27. 0 28. 0 28. 7 29. 5	$26.3 \\ 27.1 \\ 28.0 \\ 28.8 $	25. 4 26. 2 27. 0 27. 8	24. 4 25. 2 25. 9 26. 7	23. 6 24. 3 25. 0 25. 8
36 37 38 39	31. 4 32. 3 33. 2 34. 1	30. 4 31. 2 32. 0 32. 9	29.6 30.4 31.2 32.1	28.6 29.4 30.2 30.9	27.5 28.2 29.0 29.8	26. 5 27. 3 28. 0 28. 7
40 41 42 43	34. 9 35. 8 36. 7 37. 6	33. 7 34. 6 35. 4 36. 3	32.9 33.7 34.5 35.4	31. 7 32. 5 33. 3 34. 1	30. 5 31. 3 32. 1 32. 8	29.5 30.2 31.0 31.7
44 45 46 47	38, 4 39, 3 40, 2 41, 1	37. 1 38. 0 38. 8 39. 6	36. 2 37. 0 37. 8 38. 6	34. 9 35. 7 36. 5 37. 3	33.6 34.3 35.1 35.9	32. 4 33. 2 33. 9 34. 6
48 49 50 51	41. 9 42. 8 43. 7 44. 5	40. 5 41. 3 42. 4 43. 0	$39.5 \\ 40.3 \\ 41.1 \\ 41.9$	38. 1 38. 9 39. 7 40. 5	36. 6 37. 4 38. 2 38. 9	$\begin{array}{c} 35.\ 4\\ 36.\ 1\\ 36.\ 8\\ 37.\ 6\end{array}$
52	45. 4 46. 3 47. 2 48. 0	43. 7 44. 7 45. 5 46. 4	$\begin{array}{r} 42.\ 7\\ 43.\ 6\\ 44.\ 4\\ 45.\ 2\end{array}$	41. 3 42. 1 42. 9 43. 7	$\begin{array}{c} 39.\ 7\\ 40.\ 4\\ 41.\ 2\\ 42.\ 0\end{array}$	38. 3 39. 0 39. 8 40. 5
56	48. 9 49. 8 50. 7 51. 5	47. 2 48. 1 48. 9 49. 8	$\begin{array}{r} 46.\ 0\\ 46.\ 9\\ 47.\ 7\\ 48.\ 5\end{array}$	44. 4 45. 2 46. 0 46. 8	42. 7 43. 5 44. 3 45. 0	41. 3 42. 0 42. 7 43. 5
60 61 62 63	52.4 53.3 54.2 55.0	50. 6 51. 4 52. 3 53. 1	49. 3 50. 2 51. 0 51. 8	47. 6 48. 4 49. 2 50. 0	45. 8 46. 5 47. 3 48. 1	44. 2 44. 9 45. 7 46. 4
64 65 66 67	55. 9 56. 8 57. 7 58. 5	54. 0 54. 8 55. 7 56. 5	52.6 53.4 54.3 55.1	50. 8 51. 6 52. 4 53. 2	48. 8 49. 6 50. 4 51. 1	47. 2 47. 9 48. 6 49. 4

25804°-27-22

### APPENDIX F

## Table 86.—Minimum Depreciated Ground-Line Circumference of Wood Poles—Continued

Ground-line circumference when installed (inches)	for ratio	n allowabl o of fiber s ated of—	e deprecia tress wher	ted ground installed	d-line circ to fiber st	umference ress when
	, 2/3	3/5	5/9	1/2	4/9	2/5
68 69 70 71 72 73 74 75	$\begin{array}{c} Inches \\ 59, 4 \\ 60, 3 \\ 61, 2 \\ 62, 0 \\ 62, 9 \\ 63, 8 \\ 64, 6 \\ 65, 5 \end{array}$	$\begin{array}{c} In ches \\ 57. \ 4 \\ 58. \ 2 \\ 59. \ 0 \\ 59. \ 9 \\ 60. \ 7 \\ 61. \ 6 \\ 62. \ 4 \\ 63. \ 2 \end{array}$	Inches 55. 9 56. 7 57. 5 58. 4 59. 2 60. 0 60. 8 61. 7	<i>Inches</i> 54. 0 54. 8 55. 6 56. 4 57. 1 57. 9 58. 7 59. 5	$\begin{array}{c} In ches \\ 51.9 \\ 52.6 \\ 53.4 \\ 54.2 \\ 54.9 \\ 55.7 \\ 56.5 \\ 57.2 \end{array}$	Inches 50. 1 50. 8 51. 6 52. 3 53. 0 53. 8 54. 5 55. 3

## Table 37.—Allowable Depreciation of Wood Poles Under Vertical and Transverse Loading for Various Situations

[This table locates the situations to which the columns of Tables 86 and 88 apply]

	Ratio of maximum fiber stress when in stalled to maximum fiber stress when de preciated for—		
	Treated poles	Untreated poles	
At crossings: In lines of one grade of construction throughout— Grade A Grade B Grade C	2/3 2/3 1/2	2/3 2/3 1/2	
In isolated sections of higher grade of construction in lines of a lower grade of construction— Grade A Grade B Grade C	2/3 2/3 1/2	1/2 4/9 2/5	
Elsewhere than at crossings: Grade A Grade B Grade C	2/3 3/5 2/3	5/9 1/2 1/2	

314

# Table 88.—Maximum Radial Depreciation of Wood Poles

Ground-line circumference	Maximun whe	n allowable n installed	radial dep to fiber str	reciation for ress when d	or ratio of f lepreciated	iber stress of—
when installed (inches)	2/3	3/5	5/9	1/2	4/9	2/5
24	Inches 0.48 .50 .52 .54	Inches 0.60 .62 .66 .67	Inches 0.68 .71 .72 .76	Inches 0. 79 . 82 . 85 . 89	Inches 0.90 .94 .98 1.02	Inches 1.01 1.05 1.09 1.13
28	.56 .58 .60 .62	. 70 . 72 . 75 . 77	. 79 . 82 . 85 . 88	$\begin{array}{c} .92\\ .95\\ .99\\ 1.02\end{array}$	1.06 1.09 1.13 1.17	1. 17 1. 21 1. 26 1. 30
32 33 34 35	.64 .66 .68 .70	. 80 . 82 . 85 . 87	. 91 . 93 . 96 . 99	1.05 1.08 1.12 1.15	$\begin{array}{c} 1.\ 21 \\ 1.\ 24 \\ 1.\ 28 \\ 1.\ 32 \end{array}$	1.34 1.38 1.42 1.47
36 37 38 39	.72 .75 .76 .78	.90 .92 .95 .97	${ \begin{smallmatrix} 1. & 02 \\ 1. & 05 \\ 1. & 07 \\ 1. & 10 \\ \end{split} }$	${ \begin{array}{c} 1.\ 18\\ 1.\ 22\\ 1.\ 25\\ 1.\ 28 \end{array} } }$	1.36 1.40 1.43 1.47	1.51 1.55 1.59 1.63
40 41 42 43	. 80 . 82 . 85 . 86	1.00 1.02 1.05 1.07	1. 13 1. 16 1. 19 1. 22	$1.31 \\ 1.35 \\ 1.38 \\ 1.41$	$1.51 \\ 1.55 \\ 1.58 \\ 1.62$	1.68 1.72 1.76 1.80
44 45 46 47	. 88 . 90 . 93 . 95	1. 10 1. 12 1. 15 1. 17	1.25 1.27 1.30 1.33	1.44 1.48 1.51 1.54	1.66 1.70 1.74 1.77	1.84 1.88 1.93 1.97
48 49 50 51	.97 .99 1.01 1.03	$1.20 \\ 1.22 \\ 1.25 \\ 1.27$	$1.36 \\ 1.39 \\ 1.42 \\ 1.44$	$1.58 \\ 1.61 \\ 1.64 \\ 1.67$	$1.81 \\ 1.85 \\ 1.89 \\ 1.92$	2.01 2.05 2.09 2.14
52 53 54 55	1.05 1.07 1.09 1.11	$1.30 \\ 1.32 \\ 1.35 \\ 1.37$	$\begin{array}{c} 1.\ 47\\ 1.\ 50\\ 1.\ 53\\ 1.\ 56\end{array}$	1.71 1.74 1.77 1.81	1. 96 2. 00 2. 03 2. 07	2. 18 2. 22 2. 26 2. 30
56 57 58 59	1. 13 1. 15 1. 17 1. 19	$1.40 \\ 1.42 \\ 1.45 \\ 1.47$	$1.59 \\ 1.61 \\ 1.64 \\ 1.67$	1.84 1.87 1.90 1.94	2. 11 2. 15 2. 19 2. 23	2.35 2.39 2.43 2.47
60 61 62 63	1.23	$1.50 \\ 1.52 \\ 1.55 \\ 1.57$	1.70 1.73 1.76 1.78	1.96 2.00 2.03 2.07	2. 26 2. 30 2. 34 2. 37	2. 51 2. 55 2. 60 2. 64

Ground-line circumference when installed (inches)			radial dep to fiber stre			
when instaned (inches)	2/3	3/5	5/9	1/2	4/9	2/5
64	$     1.35 \\     1.37 \\     1.39 \\     1.41 \\     1.43 \\     1.45 $	Inches 1.60 1.62 1.65 1.67 1.70 1.72 1.74 1.77 1.79	Inches 1. 81 1. 84 1. 87 1. 90 1. 93 1. 93 1. 95 1. 98 2. 01 2. 04	Inches 2.10 2.14 2.17 2.20 2.23 2.26 2.30 2.33 2.36	Inches 2.41 2.45 2.49 2.53 2.56 2.60 2.64 2.68 2.71	Inches 2, 68 2, 72 2, 76 2, 81 2, 85 2, 89 2, 93 2, 97 3, 02
73 74 75	$1.47 \\ 1.49 \\ 1.51$	$1.82 \\ 1.84 \\ 1.87$	2.07 2.09 2.12	2.40 2.43 2.46	2, 75 2, 79 2, 83	3.06 3.10 3.14

Table 88.-Maximum Radial Depreciation of Wood Poles-Continued

# Allowable Number of Wires on a Given Pole With and Without Side Guys.

Table 89 gives the allowable number of No. 4 covered, solid, copper wires to be carried by a 35-foot pole of any wood having an ultimate fiber stress of 5,000 pounds per square inch. This number varies with the grade of construction and with the loading district. In this table it is assumed (1) that poles are set 6 feet in the ground; (2) that the cross arms are 2 feet apart; (3) that 6-pin cross arms are used up to 30 wires, and 8-pin arms for 31 or more wires; (4) that the placing of wires is begun at the top arm (wires 6 inches below the top of poles) and continues to lower cross arms after all wire positions are filled; (5) that the clearance of wires above ground is never less than 18 feet; (6) that the taper of poles amounts to 2 inches of circumference per 5 feet of length. Strengths are computed at the ground line. The values given apply to untreated poles in situations of conflict or joint use, or to poles either treated or untreated at crossings in a line of uniform construction. The values also hold for treated poles used at crossings where the construction differs from the remainder of the line.

Tables 90 and 91 are based upon the assumption (1) that the guys carry their loads with a factor of safety of 2; (2) that they are installed with a lead of 1 to 3; (3) that they are attached at the center of the load, thus making it unnecessary to take into account the height of the pole. The wind pressure on the pole itself has not been taken into account in these tables. This addition to the load is equivalent to that due to one or more wires, depending upon the size and height of the pole and length of span and deduction should be made in each case.

### Table 89.—Allowable Number of No. 4 Solid Copper T. B. W. P. Wires to be Carried by Untreated 35-Foot Poles of Woods Classed as of 5,000 Pounds per Square Inch Ultimate Fiber Stress (Pine, Chestnut, Western Cedar, Cypress, etc.)

[For grades A, B, and C (except at crossings in isolated sections of higher grade) in heavy, medium, and light loading districts]

Grade and loading	Maxi- mum	Span	Al	Allowable number of wires for ground-line circum- ference of—							
	stress in pole	opun	32 in.	24 in.	36 in.	38 in.	40 in.	42 in.	44 in.	46 in.	48 in.
- H	Lbs./in.2	Feet	a 4 a 3	$5\\4$	6 5	8	9 7	11 9	14 10	16     12	18 14
А. Н	1, 670	$\left\{ \begin{array}{c} 150\\ 200 \end{array} \right.$	a 3 a 2	$\frac{3}{2}$	4 3	5 4	6 4	7 5	9 6	10 7	11 8
В. Н.	2, 500	$ \left\{\begin{array}{c} 100 \\ 125 \\ 150 \\ 200 \end{array}\right. $	7 6 5 3	9 7 6 4	11 8 7 5		$     \begin{array}{c}       16 \\       12 \\       10 \\       7     \end{array} $	18     14     12     9	$     \begin{array}{c}       22 \\       17 \\       14 \\       10     \end{array} $	$26 \\ 20 \\ 16 \\ 12$	31 23 19 14
С. н	3, 750	$\left\{ \begin{array}{c} 100 \\ 125 \\ 150 \\ 200 \end{array} \right.$	$     \begin{array}{c}       11 \\       9 \\       7 \\       5     \end{array} $	$     \begin{array}{c}       14 \\       11 \\       9 \\       7     \end{array} $	17 13 11 8	$21 \\ 16 \\ 13 \\ 10$	$26 \\ 20 \\ 16 \\ 11$	$30 \\ 23 \\ 19 \\ 14$	$     \begin{array}{r}       35 \\       28 \\       22 \\       16     \end{array} $	<sup>b</sup> 40 32 27 19	<sup>b</sup> 40 37 29 23
A. M	1, 670	$\left\{ \begin{array}{c} 100 \\ 125 \\ 150 \\ 200 \end{array} \right.$	a 7 a 5 a 4 a 3	9 7 5 4	$     \begin{array}{c}       11 \\       9 \\       7 \\       5     \end{array} $	$     \begin{array}{c}       14 \\       10 \\       8 \\       6     \end{array} $	$     \begin{array}{c}       16 \\       12 \\       10 \\       7     \end{array} $	$19 \\ 15 \\ 12 \\ 9$	$23 \\ 17 \\ 14 \\ 10$	$27 \\ 20 \\ 16 \\ 12$	$30 \\ 24 \\ 19 \\ 14$
в. м	2, 500	$\left\{ \begin{array}{c} 100 \\ 125 \\ 150 \\ 200 \end{array} \right.$	$     \begin{array}{c}       12 \\       9 \\       7 \\       5     \end{array}   $	$     \begin{array}{c}       14 \\       11 \\       9 \\       7     \end{array} $	18 14 11 8	$22 \\ 17 \\ 14 \\ 10$	$26 \\ 20 \\ 16 \\ 12$	$30 \\ 24 \\ 19 \\ 14$	$36 \\ 30 \\ 23 \\ 16$	<sup>b</sup> 40 32 27 19	<sup>b</sup> 40 38 30 23
С. М	3, 750	$\left\{ \begin{array}{c} 100 \\ 125 \\ 150 \\ 200 \end{array} \right.$	$19 \\ 15 \\ 12 \\ 9$	$24 \\ 18 \\ 15 \\ 11$	30 23 18 13	$     \begin{array}{r}       34 \\       28 \\       22 \\       16     \end{array} $	<sup>b</sup> 40 32 27 19	$b 40 \\ 38 \\ 31 \\ 23$	<sup>b</sup> 40 <sup>b</sup> 40 37 27	<sup>b</sup> 40 <sup>b</sup> 40 <sup>b</sup> 40 30	<sup>b</sup> 40 <sup>b</sup> 40 <sup>b</sup> 40 36
A. L	1, 670	$\left\{ \begin{array}{c} 100 \\ 125 \\ 150 \\ 200 \end{array} \right.$	$     \begin{array}{c}       11 \\       9 \\       7 \\       5     \end{array}   $	$     \begin{array}{c}       14 \\       11 \\       9 \\       8     \end{array}   $	$17 \\ 13 \\ 11 \\ 8$	$21 \\ 17 \\ 14 \\ 10$	$26 \\ 20 \\ 16 \\ 12$	$30 \\ 24 \\ 19 \\ 14$	36 29 23 16	<sup>b</sup> 40 32 27 19	<sup>b</sup> 40 38 30 22
B. L	2, 500	$\left\{ \begin{array}{c} 100 \\ 125 \\ 150 \\ 200 \end{array} \right.$	$     \begin{array}{r}       19 \\       15 \\       12 \\       9     \end{array} $	$24 \\ 18 \\ 15 \\ 11$	30 23 18 13	$34 \\ 28 \\ 22 \\ 16$	<sup>b</sup> 40 32 27 19	<sup>b</sup> 40 39 31 23	<sup>b</sup> 40 <sup>b</sup> 40 37 27	<sup>b</sup> 40 <sup>b</sup> 40 <sup>b</sup> 40 31	<sup>b</sup> 40 <sup>b</sup> 40 <sup>b</sup> 40 36
C. L	3, 750	$\left\{ \begin{array}{c} 100 \\ 125 \\ 150 \\ 200 \end{array} \right.$	$30 \\ 25 \\ 20 \\ 14$	$38 \\ 30 \\ 25 \\ 18$	<sup>b</sup> 40 36 30 21	<sup>b</sup> 40 <sup>b</sup> 40 36 26	<sup>b</sup> 40 <sup>b</sup> 40 <sup>b</sup> 40 30	<sup>b</sup> 40 <sup>b</sup> 40 <sup>b</sup> 40 37	b 40 b 40 b 40 b 40 b 40	<sup>b</sup> 40 <sup>b</sup> 40 <sup>b</sup> 40 <sup>b</sup> 40 <sup>b</sup> 40	b 40 b 40 b 40 b 40 b 40

• For grade A in heavy and medium loading districts, 35-foot poles can not be used with so small a ground-line circumference, since pole top would be less than 7 inches. (See rule 261, A, 4, (g).) <sup>b</sup> These numbers of wires will fill all available pole space when carried on 8-pin cross arms,

<sup>b</sup> These numbers of wires will fill all available pole space when carried on 8-pin cross arms, but will not use up the available strength of the pole.

1

## Table 90.—Allowable Number of No. 4 Solid Copper T. B. W. P. Wires to be Carried on Poles Supported by Side Guys of Various Strengths under Various Grades of Construction (A, B, or C) and Loadings (Heavy, Medium, Light)

_ (1)		Number of wires to be carried by poles supported by the following numbers and strengths of guys							
Grade and loading	Span	One 4,000- pound	One 6,000- pound	One 10,000- pound	One 16,000- pound	Two 10,000- pound	One 10,000- pound, one 16,000- pound	Two 16,000- pound	
A. H. and B. H	$\begin{cases} Feet \\ 75 \\ 100 \\ 125 \\ 150 \\ 200 \end{cases}$	- 9 6 5 4 3		22 17 13 11 8	36 27 22 18 13	45 34 27 22 17	59 44 35 29 22	$73 \\ 55 \\ 44 \\ 36 \\ 27$	
с. н	$\left\{\begin{array}{c} 75\\ 100\\ 125\\ 150\\ 200\end{array}\right.$	$     \begin{array}{c}       13 \\       10 \\       8 \\       6 \\       5     \end{array} $	20 15 12 10 7	$     \begin{array}{r}       34 \\       25 \\       20 \\       17 \\       12     \end{array} $	55 41 33 27 20		89 67 53 44 33	$     \begin{array}{r}         & 110 \\             & 82 \\             & 66 \\             & 55 \\             & 41 \\         \end{array} $	
A. M. and B. M	$\left\{\begin{array}{c} 75\\ 100\\ 125\\ 150\\ 200\end{array}\right.$	14 10 8 7 5	$21 \\ 16 \\ 12 \\ 10 \\ 8$	$35 \\ 26 \\ 21 \\ 18 \\ 13$	$57 \\ 43 \\ 34 \\ 28 \\ 21$	$71 \\ 53 \\ 43 \\ 35 \\ 26$	$93 \\ 70 \\ 56 \\ 46 \\ 35$	$     \begin{array}{r}         & 115 \\             86 \\             68 \\           $	
с. м	$\left\{\begin{array}{c} 75\\ 100\\ 125\\ 150\\ 200\end{array}\right.$	21 16 12 10 8	$32 \\ 24 \\ 19 \\ 16 \\ 12$	53 40 32 27 20	$     \begin{array}{r}       86 \\       64 \\       51 \\       43 \\       32     \end{array} $	$107 \\ 80 \\ 64 \\ 53 \\ 40$	$140 \\ 105 \\ 84 \\ 70 \\ 52$	$172 \\ 129 \\ 103 \\ 86 \\ 64$	
A. L and B. L	$\left\{\begin{array}{c} 75\\ 100\\ 125\\ 150\\ 200\end{array}\right.$	$22 \\ 16 \\ 13 \\ 11 \\ 8$	$33 \\ 25 \\ 20 \\ 16 \\ 12$	$55 \\ 41 \\ 33 \\ 27 \\ 20$	88 66 53 44 33	$     \begin{array}{c}       111 \\       83 \\       66 \\       55 \\       41     \end{array} $	$     \begin{array}{r}       144 \\       108 \\       86 \\       72 \\       54     \end{array} $	$     \begin{array}{r}       177 \\       133 \\       106 \\       88 \\       66     \end{array} $	
C. <b>L</b>	$\left\{\begin{array}{c} 75\\ 100\\ 125\\ 150\\ 200\end{array}\right.$	$33 \\ 25 \\ 20 \\ 16 \\ 12$	49 37 30 25 18	$83 \\ 62 \\ 49 \\ 41 \\ 31$	133 99 79 66 49	$166 \\ 124 \\ 99 \\ 83 \\ 62$	$216 \\ 162 \\ 129 \\ 108 \\ 82$	$266 \\ 199 \\ 159 \\ 133 \\ 99$	

### APPENDIX F

Table 91.—Allowable Number of No. 8 B. W. G. Bare Iron Wires to be Carried on Poles Supported by Side Guys of Various Strengths under Various Grades of Construction (D or E) and Loading (Heavy, Medium, or Light)

Grade and loading	Span	One 4,000- pound	One 6,000- pound	One 10,000- pound	One 16,000- pound	<b>Two</b> 10,000- pound	One 10,000- pound, one 16,000- pound	Two 16,000- pound
D. н	$\begin{cases} 75 \\ 100 \\ 125 \\ 150 \end{cases}$	10 8 6 5	16 12 9 8	27 20 17 13	$43 \\ 32 \\ 26 \\ 21$	$54 \\ 40 \\ 32 \\ 29$	70 53 42 35	86 65 52 43
Е. H	$\left\{\begin{array}{c} 75 \\ 100 \\ 125 \\ 150 \end{array}\right.$	16 12 9 8	24 18 14 12	40 30 24 20	65 48 39 32	81 61 48 40	79 63 53	97 78 65
D. M	$\left\{\begin{array}{c} 75 \\ 100 \\ 125 \\ 150 \end{array}\right.$	19 14 11 9	28 21 17 14	47 35 28 23	76 57 45 38	95 71 57 47	92 74 61	91 76
E. M	$\left\{\begin{array}{c} 75 \\ 100 \\ 125 \\ 150 \end{array}\right.$	$28 \\ 21 \\ 17 \\ 14$	$42 \\ 32 \\ 25 \\ 21$	71 53 42 35	85 68 57	85 71	92	
D. L	$\left\{\begin{array}{c} 75 \\ 100 \\ 125 \\ 150 \end{array}\right.$	51 38 30 25	76 57 46 38	96 76 63				
E. L	$\left\{\begin{array}{c} 75\\ 100\\ 125\\ 150\end{array}\right.$	76 57 46 38	86 69 57	95				

NOTE.—The blank spaces in the above tables indicate that more than 100 wires can be carried by the size and number of guys in question under the indicated conditions of hazard, loading, and span length without exceeding one-half of the ultimate strength of the guys. Where the number of wires carried by a pole exceeds 80 it is good practice to install some of them in cable.

14

# Depth of Setting of Poles.

The values given in Table 92 are those recommended as the depth to which poles should be set under ordinary straight-line conditions in firm soil or rock. On corners or angles, or heavy dead-ends, these values should be increased by at least 6 inches. (See rule 262, B.)

Table 92.-Recommended Depth of Setting of Poles-Rule 262, B

Length of pole in feet	Setting in soil	Setting in rock
20 25 30 35 40	Feet 5.0 5.0 5.5 6.0 6.0	Feet 3.0 3.5 3.5 4.0 4.0
45	6.5 7.0 7.0 7.5 8.0	4.5 4.5 5.0 5.0 6.0
70 75 80	8.0 8.5 9.0	6.0 6.0 6.5

# Appendix G.—DEFINITION OF AMERICAN SOCIETY FOR TESTING MATERIALS OF DENSE SOUTHERN YELLOW PINE

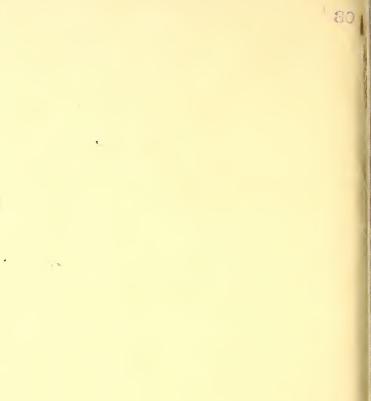
This term includes the species of yellow pine growing in the Southern States from Virginia to Texas; that is, the pines hitherto known as long-leaf pine (*Pinus palustris*), short-leaf pine (*Pinus echinata*), loblolly pine (*Pinus taeda*), Cuban pine (*Pinus heterophylla*), and pond pine (*Pinus serotina*).

Under this heading two classes of timber are designated: (a) Dense southern yellow pine and (b) sound southern yellow pine. It is understood that these two terms are descriptive of quality rather than of botanical species.

(a) Dense southern yellow pine shall show on either end an average of at least six annual rings per inch and at least one-third summer wood, or else the greater number of the rings shall show at least one-third summer wood, all as measured over the third, fourth, and fifth inches on a radial line from the pith. Wide-ringed material excluded by this rule will be acceptable, provided that the amount of summer wood as above measured shall be at least one-half.

The contrast in color between summer wood and spring wood shall be sharp and the summer wood shall be dark in color, except in pieces having considerably above the minimum requirement for summer wood.

(b) Sound southern yellow pine shall include pieces of southern pine without any ring or summer-wood requirement.





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