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Spectroradiometry and Conventional Photometry

An Interlaboratory Comparison

D. A. McSparron, K. Mohan, R. C. Raybold, R. D. Saunders, and E. F. Zalewski

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	Average relative spectral flux (sphere)		Average absolute flux (sphere)		Average relative spectral irradianc (25 cm section)		
Laboratory	Lamp	Figure	Page	Figure	Page	Figure	Page
1	8797	4.18	64	4.19	66	4.44	116
	8798	4.20	68	4.21	70	4.45	118
	8906	4.34	96	4.35	98	4.55	138
2	8805	4.26	80	4.27	82	4.50	128
	8806	4.28	84	4.29	86	4.51	130
	8909	4.38	104	4.39	106	4.58	144
4	8809	4.30	88	4.31	90	4.52	132
	8810	4.32	92	4.33	94	4.53	134
	8911	4.40	108	4.41	110	4.59	146
5	8801	4.22	72	4.23	74	4.48	124
	8802	4.24	76	4.25	78	4.49	126
	8908	4.36	100	4.37	102	4.57	142
7	8795 8796 8905					4.42 4.43 4.54	112 114 136
9	8799 8800 8907					4.46 4.47 4.56	120 122 140

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			Table Desc	ription			
	Relative flux dist (sph Table ratory Lamp <u>Number</u>		e spectral stribution where)	Absolute spectra flux distributio (sphere)		Relative irradianc bution (25 c	spectral e distri- m section)
Laboratory			Page	Table Number	Page	Table Number	Page
1	8797	4.26	63	4.27	65	4.52	115
	8798	4.28	67	4.29	69	4.53	117
	8906	4.42	95	4.43	97	4.63	137
2	8805	4.34	79	4,35	81	4.58	127
	8806	4.36	83	4.37	85	4.59	129
	8909	4.46	103	4.47	105	4.66	143
4	8809	4.38	87	4.39	89	4.60	131
	8810	4.40	91	4.41	93	4.61	133
	8911	4.48	107	4.49	109	4.67	145
5	8801	4.30	71	4.31	73	4,56	123
	8802	4.32	75	4.33	77	4.57	125
	8908	4.44	9.9	4,45	101	4.65	141
7	8795					4:50	111
	8796					4.51	113
	8905					4.62	135
9	8799					4.54	119
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Spectroradiometry and Conventional Photometry An Interlaboratory Comparison

D.A. McSparron, K. Mohan*, R.C. Raybold, R.D. Saunders, and E.F. Zalewski

This report summarizes the results of a fluorescent lamp intercomparison carried out under the aegis of the National Bureau of Standards Photometry Section. The purpose of the intercomparison was to evaluate the interlaboratory precision obtainable in photometric and spectroradiometric measurements. The tests were also designed to disclose suspected systematic errors in measurement techniques.

The intercomparison consisted of five parts: (1) A homochromatic, photometric measurement of cool white fluorescent lamps and a heterochromatic, photometric measurement of a daylight fluorescent lamp and an incandescent lamp utilizing cool white fluorescent lamps as standards, all within an integrating sphere. (2) Spectroradiometric measurement of the above mentioned lamps in an integrating sphere. (3) Spectroradiometric measurement of a 25 cm section of the fluorescent lamps in a baffled enclosure. (4) An experiment designed to reveal systematic errors in heterochromatic photometry. (5) Measurement of the x and y chromaticity coordinates with a Barnes colorimeter.

Key words: Photometry, heterochromatic photometry, spectroradiometry, luminous flux, correlated color temperature, chromaticity coordinate, Barnes colorimeter, cool white fluorescent lamp, daylight fluorescent lamp, integrating sphere, color correction, intercomparison.

1. INTRODUCTION

1.1. Background information

From time to time the Lamp Testing Engineers Conference (LTEC) and the National Bureau of Standards (NBS) have conducted intercomparisons to compare the bases for luminous flux and color parameters used by lamp manufacturers and other members of the lamp industry.

In 1967 the National Bureau of Standards spectroradiometrically calibrated a set of eleven 40 watt, cool white fluorescent lamps by comparing their luminous flux output to those of a set of 200 watt, luminous flux standard incandescent lamps calibrated at 2854K.** Five of these fluorescent standards were retained at NBS and six were sent to the Electrical Testing Laboratories (ETL) where they were used in a statistically designed procedure to assign total luminous flux values to a group of eighty lamps of the same manufacturer and type. These lamps were sent in groups of six to some of the participating laboratories as new luminous flux standards. This intercomparison was conducted to see whether the use of these new standards would unify the base for total luminous flux throughout the lamp industry, and to compare it to the NBS base.

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**Color temperatures quoted in this intercomparison are based on the 1949 Color Temperature Scale. This scale is based on the 1948 International Practical Temperature Scale (IPTS). For a discussion of the 1970 Color Temperature Scale (1968 IPTS), see the NBS Technical News Bulletin, September, 1970. This intercomparison was conducted among some of the member laboratories of the Lamp Testing Engineers Conference and other interested laboratories. The participating laboratories were (in alphabetical order):

Duro-Test Corporation, North Bergen, New Jersey.

Electrical Testing Laboratories, Inc., New York, New York.

El-Tronics Inc., Warren, Pennsylvania.

General Electric Company, Cleveland, Ohio.

International Telephone and Telegraph Corporation, Lynn, Massachusetts.

National Research Council, Ottawa, Canada.

Sylvania Electric Products Inc., Danvers, Massachusetts.

University of California, Richmond, California.

Westinghouse Electric Corporation, Bloomfield, New Jersey.

Each laboratory was randomly assigned a code number for use in all references to that laboratory.

1.2. Description of intercomparison

The intercomparison consisted of five parts:

- 1) A photometric intercomparison of 40 watt fluorescent lamps by conventional substitution photometry in an integrating sphere
- A spectroradiometric study of 40 watt fluorescent lamps in an integrating sphere;
- A spectroradiometric study of a 25 cm (10 inch) section of 40 watt fluorescent lamps;
- A statistically designed check on systematic errors in conventional sphere photometry; and
- A Barnes Colorimeter determination of the x any y chromaticity coordinates of 40 watt fluorescent lamps.

The National Bureau of Standards supplied the participating laboratories with the following:

- 1) Two type F40T12 cool white lamps,
- 2) One type F40T12 daylight lamp,
- One 200 watt incandescent lamp calibrated for total flux at 2854K, and
- One fixed inductance choke-ballast on which the fluorescent lamps (items 1 and 2) were to be operated.

The fluorescent lamps had been seasoned by the manufacturers for 500 burning hours and the operating conditions were specified (see appendix A).

Since several different types of standard and test lamps will be referred to in this report, it will be convenient to identify them here.

NBS Incandescent Standards: The 200 watt incandescent flux standards that are used at NBS in spectroradiometric work.

NBS CW Standards: The eleven type F40Tl2 cool white (CW) fluorescent lamps spectroradiometrically calibrated for luminous flux by using the NBS Incandescent Standards. These are the lamps referred to in section 1.1.

ETL CW Standards: The eighty lamps of type F40T12 CW, also referred to in section 1.1, that were assigned luminous flux values on the basis of the NBS CW Standards by ETL.

Intercomparison CW Lamps: The two cool white fluorescent lamps supplied directly by NBS to the participating laboratories for this intercomparison.

Intercomparison Daylight Lamps: The daylight fluorescent lamps supplied by NBS.

Intercomparison Incandescent Lamps: The 200 watt incandescent lamps supplied by NBS.

Choke-Ballast: The fixed inductance choke-ballast that was supplied by NBS for use with the Intercomparison CW Lamps and the Intercomparison Daylight Lamp.

The genealogy of these lamps is given in figure 1.1. The calibration on most of the lamps that were a part of this intercomparison can be traced back to the NBS 6807 group of incandescent luminous flux standards. This does not apply to the two laboratories in which ETL CW Standards were not used as a base, Laboratories 6 and 9.

Together with the incandescent and fluorescent intercomparison lamps and the choke-ballast, each participating laboratory was supplied with the experimental design and data sheets for each part of the intercomparison. A copy of the instructions and data sheets sent to each laboratory is attached as appendix A. Each participating laboratory also filled out a questionnaire on the type of equipment and procedures that were used. Appendix B is a copy of the questionnaire.

The intercomparison lamps were first measured at NBS by using both spectroradiometry and conventional substitution photometry. They were then measured at the participating laboratories where the fluorescent lamps were set up in the same lamp and choke-ballast combinations. The data and the lamps were returned to NBS, where the lamps were measured again. Measurements were made according to a statistical design.

The measurements taken at NBS before the lamps were sent out will be hereafter referred to as the "Initial" measurements; those taken at the laboratories will be referred to as "Laboratory" measurements; and those taken at NBS after the lamps were returned will be called "Repeat" measurements. Only Initial and Laboratory spectroradiometric measurements were taken on a 25 cm section of the fluorescent lamps. The data from the participating laboratories were to be returned untreated to NBS so that they could be reduced in a similar manner for all the laboratories. Unfortunately, due to the many different forms in which the data were received, the analysis of the data was different for each laboratory.



2. NBS PROCEDURES FOR ASSIGNMENT OF LAMP PARAMETERS

2.1. Conventional photometric measurements

The fluorescent lamps, that is, the cool white and daylight lamps, were measured photometrically at NBS in a 2 meter (80 inch) sphere by using the NBS Incandescent Standards and the NBS CW Standards. A circuit diagram is given in figure 2.1. A high impedance, true RMS differential voltmeter was used for measuring lamp voltage. The "restoration of light" method (ref. 1) was, therefore, not required for lamp voltage measurements. Readings were taken both with and without an external color correcting filter. The ETL CW Standard lamps were operated on a Sylvania reference ballast and the fluorescent intercomparison lamps were operated on the choke-ballast. The same lamp and ballast combination was maintained throughout the period of the intercomparison.

During the Initial and Repeat measurements at NBS, NBS Incandescent Standards were used for the spectroradiometric transfers and the NBS CW Standards were used for the conventional photometric transfers.

2.2. Spectrcradiometric measurements

A block diagram of the spectroradiometer is given in figure 2.2. The spectroradiometer consisted of a 20 cm diameter sphere connected to the entrance slit of the monochromator. The inside of this sphere was coated with about 0.5 mm of barium sulphate powder which contained no binder, since binders tend to absorb radiation in the blue region of the spectrum. A 7.5 cm diameter aperture served to admit light from the measurement source into the sphere, perpendicular to the optical axis of the monochromator. The measurement source in this case was a lamp inside a 2 meter integrating sphere. The light was diffused inside the smaller collecting sphere and thus depolarized. The use of a collecting sphere minimized problems of alignment. Filters were inserted between the collecting sphere and the monochromator to eliminate second order spectra. However, this procedure was not followed in the 25 cm section measurements.

The monochromator used was a double grating instrument. Baffling along the optical path inside the monochromator served to reduce scattered radiation. The scattered radiation was further reduced by controlling the entrance slit height so that the radiation coming through the slit barely filled the first mirror in the monochromator. The entrance and exit slits were about equal and were approximately 5 nm in spectral bandpass.

The wavelength scale of the monochromator was calibrated against a set of standard emission lines to within an estimated uncertainty of ± 0.1 nm. The photomultiplier tube used in the spectroradiometer had an S-20 cathode and was selected for high sensitivity in the 600-800 nm region of the spectrum. The current from this photomultiplier tube was measured by a picoammeter that employed a cathode-follower type of amplifier for currents greater than 10^{-8} A, and an operational amplifier for currents less than 10^{-8} A. Since the picoammeter did not modulate the incoming signal to amplify it, problems arising from phase-difference effects between the source (if operated on power other than direct current) and the modulating signal of the amplifier were eliminated. The output of the picoammeter was connected to a stable resistor and the voltage drop across this resistor was measured by a digital voltmeter.

In order to monitor the drift in the electronics and photomultiplier tube sensitivity, a 200 watt quartz halogen lamp set at constant voltage was referenced by the spectroradiometer simply by rotating the collecting sphere. During the course of a run, readings were taken of the monitor lamp at 560 nm before, after, and during a run. If the difference was more than about 0.2% the run was aborted. The gain on the picoammeter was adjusted for each run so that the voltmeter reading for the monitor lamp was 0.8 of full scale. All the spectroradiometric data were reduced by using the following assumptions:

1) The conditions were the same for both the test and standard sources (that is, no change in monochromator, sphere, detector, back-ground, gain, instrument bandwidth, etc.).



CIRCUIT USED FOR OPERATING FLUORESCENT LAMPS





SPECTRORADIOMETRIC MEASUREMENTS AT NBS

FIGURE 2.2

2) The relative spectral distribution of the incandescent standard is the same as the relative spectral distribution of a Planckian radiator at 2854K.

3) Differences in beam geometry and polarization are eliminated by the entrance sphere.

4) The system response is linear at any given wavelength.

The last assumption leads to the conclusion that at a particular dial setting, Λ_1 , the instrument reading, $R(\Lambda_1)$, is proportional to the spectral radiant flux admitted by the entrance aperture. That is,

$$R(\Lambda_{i}) = K \int_{\lambda_{i}}^{\lambda_{i}+b/2} \varphi_{\lambda} D(\lambda) \tau(\Lambda_{i},\lambda) d\lambda$$
(2.1)
$$(\lambda_{i}-b/2)$$

where $D(\lambda)$ is the relative system response as a function of wavelength (detector response and sphere or background absorption), $\tau(\Lambda_1, \lambda)$ is the instrument transmittance as a function of λ at the Λ_1 dial setting, ϕ_{λ} is the spectral radiant flux per wavelength interval of the source and K is the instrument proportionality constant. The limits of integration are set by the instrument bandpass, b: outside these limits the instrument transmittance is effectively zero.

For an incandescent lamp (the standard source) or the continuum of a fluorescent lamp (the test source), ϕ_{λ} is a slowly varying function of λ . (The problem of the measurement of the mercury lines in a fluorescent lamp output will be treated separately.) It is also usually true that $D(\lambda)$ is a slowly varying function of λ . Within reasonable limits of accuracy these two functions may be assumed constant over the bandpass of the instrument. Therefore, eq. 2.1 becomes,

$$\mathbf{R}(\Lambda_{\underline{i}}) = \mathbf{K} \phi_{\lambda}(\Lambda_{\underline{i}}) D(\Lambda_{\underline{i}}) \int \tau(\Lambda_{\underline{i}}, \lambda) d\lambda$$

$$(\lambda_{\underline{i}} - b/2)$$
($\lambda_{\underline{i}} - b/2$)
($\lambda_{\underline{i}} - b/2$)

Let R^t(Λ_1), R^s(Λ_1), and $\phi_{\lambda}^{t}(\lambda_1)$, $\phi_{\lambda}^{s}(\lambda_1)$ be the instrument readings and fluxes for the test and standard sources respectively. Within the approximations used to derive eq. 2.2, therefore, the spectral radiant flux ratio is equal to the ratio of the instrument readings.

$$\frac{R^{L}(\Lambda_{1})}{R^{S}(\Lambda_{1})} = \frac{\phi_{\lambda}^{L}(\lambda_{1})}{\phi_{\lambda}^{S}(\lambda_{1})}$$
(2.3)

If $\phi_{\lambda}^{S}(\lambda_{1})$ is known for each dial setting Λ_{1} , then the spectral radiant flux of the source can be evaluated. Although ϕ_{λ}^{S} is not known directly, it can be obtained from the total luminous flux, Φ^{S} which is known by comparison to the NBS luminous flux standards, and from the assumption that the standard source has the same relative spectral distribution, $B(\lambda)$, as a Planckian radiator at 2854K. That is,

$$\phi_{\lambda}^{S} = K_{1} B(\lambda)$$
 (2.4)

The total luminous flux, 9, is defined in general as,

$$\Phi = K_{\rm m} \int_{380}^{760} \phi_{\lambda} V(\lambda) \, d\lambda$$
(2.5)

where K_m is the maximum value of the spectral luminous efficacy (680 lumens per watt) and $\mathbb{V}(\lambda)$ is the CIE luminous efficiency function. The limits of integration are given in nanometers and are set by the definition of $\mathbb{V}(\lambda)$. For the standard source the total luminous flux is, therefore,

$$v^{S} = K_{1}K_{m} \int V(\lambda) B(\lambda) d\lambda \qquad (2.6)$$

This yields a value for K1, so that eq. 2.4 becomes,

$$\phi_{\lambda}^{\mathfrak{s}}(\lambda_{1}) = \frac{B(\lambda_{1})}{K_{m} \int V(\lambda) B(\lambda) d\lambda}$$
(2.7)

Here $B(\lambda_1)$ is the value of $B(\lambda)$ (in relative power per wavelength interval) at the dial setting Λ_1 . Using this result in eq. 2.3 the radiant flux per unit wavelength for the test source is:

$$\phi_{\lambda}^{t}(\lambda_{1}) = \frac{R^{t}(\Lambda_{1})}{R^{s}(\Lambda_{1})} \frac{B(\lambda_{1}) \Phi^{s}}{K_{m} f V(\lambda) B(\lambda) d\lambda}$$
(2.8)

In order to compute the total luminous flux of the test source from eq. 2.5, the integration over λ (the wavelength) may be approximated by a summation over Λ_1 , (the wavelength dial setting). The total luminous flux of the test source is, therefore,

$$\Phi^{\mathbf{t}} = K_{m} \sum_{\lambda = 0}^{760} \phi_{\lambda}^{\mathbf{t}}(\lambda_{1}) \nabla(\lambda_{1}) \Delta \Lambda$$
(2.9a)

Combined with eq. 2.8, it becomes:

$$\Phi^{\mathsf{t}} = \sum_{380}^{760} \frac{R^{\mathsf{t}}(\Lambda_{1})}{R^{\mathsf{s}}(\Lambda_{1})} \frac{\nabla(\lambda_{1}) B(\lambda_{1}) \Phi^{\mathsf{s}}}{\int \nabla(\lambda) B(\lambda) d\lambda} \Delta\Lambda$$
(2.9b)

The limits of summation in nanometers are again set by the definition of $V(\lambda_1)$, the value of $V(\lambda)$ at Λ_1 . The summation interval, $\Delta\Lambda$, which is the analog of d λ , remains to be chosen. This interval does not have to be the same as the instrument bandpass; in fact, for this intercomparison it was chosen to be about twice as big: the summation interval was 10 nm, and the bandpass was

approximately 5 nm. The same assumption, however, applies to both: the wavelength dependent instrument response and spectral radiant flux are assumed constant over the interval of summation and the bandpass. Choosing the summation interval fixes the dimensions of the ϕ_λ values to be used. In this case the dimensions of $\phi^{*}_{\lambda}(\lambda_1)$ and $\phi^{*}_{\lambda}(\lambda_1)$ are watts per 10 nm.

Note once again that the approximations which led up to eq. 2.9b were for a source without narrow lines. In order to treat the mercury lines present in the output of a fluorescent lamp, eq. 2.1 must be re-examined. For a dial setting at one of the mercury lines, Λ_m , the equation becomes:

$$R^{t}(\Lambda_{m}) = K \int \phi_{\lambda}^{t} D(\lambda) \tau(\Lambda_{m}, \lambda) d\lambda$$

$$(2.10)$$

$$(\lambda_{m}-b/2)$$

Since the mercury lines are much narrower than the instrument bandpass, the integrand is zero everywhere except at one wavelength, λ_m . Equation 2.10 can be rewritten as,

$$R^{\mathsf{L}}(\Lambda_{\mathrm{m}}) = K \phi^{\mathsf{L}}(\lambda_{\mathrm{m}}) D(\lambda_{\mathrm{m}}) \tau(\Lambda_{\mathrm{m}}, \lambda_{\mathrm{m}})$$
(2.11)

Note that $\phi^{t}(\lambda_{m})$ has been written without a subscript since it no longer is flux per wavelength interval--it is flux per mercury line. Dividing this by eq. 2.2 (written for a standard incandescent source) will obviously not yield the same cancellation that led to eq. 2.3. An additional experiment is necessary to evaluate the spectral radiant flux of a mercury line.

The experiment was performed as follows: By using the spectroradiometer, an analog plot of instrument reading versus dial setting was made of the output of a lamp having no continuum, only mercury line emission. The area under each plot of a mercury line was measured graphically. This area measurement is the value of the integral of the instrument reading as a function of the dial setting over the limits of the wavelength interval through which the mercury line is transmitted. That is,

In the integral on the right side of eq. 2.12 only the transmittance function, $\tau(\Lambda, \lambda_m)$, is a function of Λ . The transmittance function is a function of two variables: the wavelength of the radiation and the instrument dial setting. Furthermore, it is a slowly varying function of the dial setting. If the transmittance function is assumed to remain unchanged within small variations of the dial setting, then for a line source of variable wavelength the following equation is true:

That is, the integral of the transmittance function obtained by holding the line source wavelength fixed and varying the dial position is equal to the integral obtained by fixing the dial setting and varying the wavelength of the line source. With this assumption eq. 2.12 becomes

$$(\Lambda_{m}^{+b}/2) \qquad (\lambda_{m}^{+b}/2)$$

$$\int \mathbb{R}^{t}(\Lambda) \ d\Lambda = K \ \phi^{t}(\lambda_{m}) \ D(\lambda_{m}) \ \int \tau(\Lambda_{m}, \lambda) \ d\lambda \qquad (2.14)$$

$$(\Lambda_{m}^{-b}/2) \qquad (\lambda_{m}^{-b}/2)$$

Since the left side of this equation represents an area, it can be approximated by the product of two numbers. Choosing a specific instrument reading, for instance, $R^t(\Lambda_m)$, the reading at the mercury line wavelength, determines the value of the multiplicative constant to be used to obtain an area measurement from a single instrument reading. This factor, b_{eff} , termed the effective bandpass, will be unique for each mercury line and can now be used in the approximation of the integral on the left side of eq. 2.14 for any source containing mercury lines. This is, of course, only true if the characteristics of the instrument remain constant between the two experiments.

In order to compare eq. 2.14 to eq. 2.2 written for the standard incandescent source, the units of $\phi^{\sharp}(\lambda_m)$ must be adjusted to the summation interval chosen for $\phi^{\chi}_{\lambda}(\lambda_m)$. Dividing both sides of eq. 2.14 by AA will change the flux per mercury line to flux per wavelength interval, or $\phi^{\chi}_{\lambda}(\lambda_m)$. Division of the adjusted version of eq. 2.14 by eq. 2.2 leads to:

 $\frac{\mathbb{R}^{\mathsf{t}}(\Lambda_{\mathrm{m}}) \quad \mathsf{b}_{\mathrm{eff}}}{\mathbb{R}^{\mathsf{s}}(\Lambda_{\mathrm{m}}) \quad \Delta\Lambda} = \frac{\phi_{\lambda}^{\mathsf{t}}(\lambda_{\mathrm{m}})}{\phi_{\lambda}^{\mathsf{s}}(\lambda_{\mathrm{m}})}$

(2.15)

Every term in this equation, except for the spectral radiant flux of the mercury line, has a known value. The $\phi_{\lambda}^{\dagger}(\lambda_m)$ values in eq. 2.15 can now be included in the summation of eq. 2.9a as additional $\phi_{\lambda}^{\dagger}(\lambda_1)$ values.

For the NBS spectroradiometer, the effective bandpass, b_{eff} , was measured for each mercury line and found to be: 5.84 nm at 405.0 nm (doublet); 5.53 nm at 435.8 nm; 5.48 nm at 546.1 nm; and 5.93 nm at 578.0 nm (doublet). The mercury line spectral radiant flux values listed in the tables in section 4 were adjusted to a 10 nm interval.

In the measurement of the mercury line flux above the continuum of a fluorescent lamp, the instrument reading produced by the continuum at that point was interpolated by fitting a quadratic polynomial to three instrument readings in the vicinity of the line. The instrument reading produced by the mercury line was calculated by subtracting the interpolated continuum value from the experimental instrument reading at the mercury line wavelength setting.

As indicated above, two of the four mercury lines in a fluorescent lamp output are actually double lines. The treatment of these doublets is a simple extension of the previous discussion. When eq. 2.12 is rewritten for two mercury lines at λ_1 and λ_k it becomes:

$$\begin{array}{ll} (A+C) & (A+C) \\ & \int \mathbb{R}^{t}(\Lambda) \ d\Lambda = \mathcal{K} \int \left[\phi^{t}(\lambda_{j}) \ \mathbb{D}(\lambda_{j}) \ \tau(\Lambda,\lambda_{j}) + \phi^{t}(\lambda_{k}) \ \mathbb{D}(\lambda_{k}) \ \tau(\Lambda,\lambda_{k})\right] \ d\Lambda \qquad (2.16) \\ & (A-C) & (A-C) \end{array}$$

The limits of integration are defined by:

$$A = (\Lambda_1 + \Lambda_k)/2$$

and

$$C = (b + \Lambda_i - \Lambda_k)/2$$

Since the mercury line separation is less than the instrument bandpass, the assumptions that have been made about the behavior of the functions can be applied in eq. 2.16. Namely,

$$D(\lambda_j) = D(\lambda_k)$$

and

$$\tau(\Lambda,\lambda_{j}) = \tau(\Lambda,\lambda_{k})$$

Equation 2.16 reduces to

$$\begin{array}{l} (A+C) & (a+c) \\ \int \mathbb{R}^{t}(\Lambda) \ d\Lambda = \mathbb{K} \ \mathbb{D}(\lambda_{j}) \ \left[\phi^{t}(\lambda_{j}) + \phi^{t}(\lambda_{k})\right] \int \tau(\Lambda_{j},\lambda) \ d\lambda \end{array}$$

$$(2.17)$$

$$(A-C) & (a-c) \end{array}$$

where a and c are defined with respect to λ in the same manner as A and C were defined with respect to Λ . By choosing a specific instrument reading (not necessarily at the wavelength of either mercury line)an effective bandpass is determined and an equation similar to eq. 2.15 can be derived where the unknown flux will be the sum of the spectral radiant fluxes of the two mercury lines.

In order to check the validity of measuring the mercury doublets as a single line, the spectroradiometric measurements were repeated with a smaller instrument bandpass (narrower slits). This resolved the doublets and allowed them to be treated as single lines. The results of these two measurements were identical within the uncertainty of the measurement.

2.3. Analysis of the NBS measurements

The photocell data were reduced by using the five NBS Cool White Standards which were retained at NBS. For the spectroradiometric measurements, NBS Incandescent Standards were used. First the data were analyzed to determine if the luminous flux of the lamps remained constant throughout the intercomparison. The results are listed in table 2.1.

Table 2.1

	Day	light	Cool White	
Measurement Method	Change (lumens)	Significant* Yes No	Change (lumens)	Significant* Yes No
Photocell (P)	13.5	х	33.2	х
Photocell + Filter (PF)	8.4	х	31.9	х
Spectroradio- meter (SR)	- 2.8	х	12.9	х

Initial minus Repeat luminous flux measurements at NBS

*Significance at the 95% confidence level (t+test).

Table 2.2

Differences between NBS measurement methods of luminous flux

	Da	ylight	Cool White		
Methods Compared	Difference (lumens)	Significant* Yes No	Difference (lumens)	Significant* Yes No	
			<u> </u>		
P-PF**	-43.3	х	7.0	х	
SR-PF	- 4.4	х	3.5	х	
SR-P	38.9	х	-3,5	х	

*Significance at the 95% confidence level (t-test). **See table 2.1 for a definition of these symbols.

Table 2.3

Precision (standard deviation) of an NBS measurement of luminous flux

	Photocell Without Filter (lumens)	Photocell With Filter (lumens)	Spectro- radiometer (lumens)
Initial	19.1	21.7	26.5
Repeat	14.1	13.6	12.6
F-Test Significant*	1.83	2.5	4.4
(s ² Before/s ² After) Yes**	Yes	Yes

*Significant at the 95% confidence level (F-test).

**Both numerator and denominator had more than 40 degress of freedom.

Next the data were analyzed to determine if any difference exists among the methods used. These results are given in table 2.2. In table 2.3, the results of a statistical analysis are given which determine the precision of each method for Initial and Repeat measurements. The final values assigned to the lamps were an average of the spectroradiometric and photocell-filter Initial and Repeat values equally weighted.

Note that in table 2.1 there appears a significant drift in cool white lamps in all the three measurement methods. This could be due to some change in the characteristic of the lamp in the time between the Initial and the Repeat measurements. The daylight lamps, however, appear to change only when measured by a photocell without an additional color correcting filter. This may be due to a change in the spectral characteristics of either the sphere or photocell in the interim between measurements.

Table 2.2 compares the different methods used. Since the standards used for conventional photometry were cool white lamps, it is understandable that for daylight lamps the photocell values are significantly different from the photocell with filter values. The close agreement between the spectroradiometric and photocell with filter values lends further credence to the claim that a sphere can be spectrally corrected by using a color correcting filter. A small but significant difference was detected between the photocell and the photocell with filter values for cool white lamps. This could be due to the fact that the original standards used were of one manufacturer and the test lamps were of another manufacturer. Though they are all cool white lamps, there may be some spectral difference between the test lamps are argon filled. Although the ambient temperature was maintained at $25 \pm 1^{\circ}$ c, mixed gas lamps are believed to be more sensitive to changes in ambient temperature than argon filled lamps.

The standard deviations given in table 2.3 are calculated estimates of the standard deviation of a single measurement. The difference in the precision between the Initial and Repeat measurements may be due to the level of experience of the different operators for the two cases.

In addition to the spectroradiometer measurements made on the entire lamp operated inside an integrating sphere, measurements were also made on a 25 cm section of the lamp operated inside a half-cylindrical enclosure. The enclosure was double shielded against drafts by wire nets. The base of this enclosure was baffled to enable the collecting sphere of the spectroradiometer to sample a 25 cm section of the lamp. Figure 2.3 is a diagram of this enclosure.

The spectroradiometric data were analyzed to yield values for of color temperature*, the x and y chromaticity coordinates, and, for the sphere measurements, total luminous flux.

Statistical tests were conducted to check whether there were significant differences between Initial and Repeat values for color temperature and chromaticity coordinates. Table 2.4 gives the Initial minus Repeat values for the measurements of color temperature and the x and y chromaticity coordinates for both cool white and daylight lamps. As in table 2.1, where the Initial and Repeat total luminous flux differed more for cool white lamps than for the daylight lamps, the cool white lamps seems to have changed significantly in the three color parameters. The daylight lamps have changed significantly in two: the x chromaticity coordinate and color temperature. A change in the characteristics of the lamp and ballast combination resulting in a spectral change in lamp output could account for both the color change and the change in total luminous flux.

The NBS values for color parameters were assigned from the average of both the Initial and Repeat spectroradiometric sphere measurements. The 25 cm section values were not used for this purpose. Because only the Initial measurements were performed, the 25 cm section values were not included in the average.

^{*}The common use of the term "color temperature" in reference to a fluorescent lamp is, in a strict sense, incorrect. The prescribed terminology is "correlated color temperature". However, in deference to familiarity and simplicity "color temperature" will be used throughout.



ENCLOSURE FOR MEASUREMENTS ON A 25 cm SECTION OF A FLUORESCENT LAMP.

FIGURE 2.3

Table 2.4

	Cool	White	Daylight		
Parameter	Difference	Significant* Yes No	Difference	Significant* Yes No	
Color Temp.	29.9K	x	35.4K	x	
x	-0.0009	x	-0.0006	х	
У	0.0009	x	-0.0003	x	

Initial minus Repeat values of color parameter sphere measurements at NBS

*Significance at the 95% confidence level (t-test).

Table	2.	5
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Initial sphere measurements minus Initial 25 cm section measurements of color parameters at NBS

	Cool	l White	Daylight		
Parameter	Difference	Significant* Yes No	Difference	Significant* Yes No	
Color Temp. x y	16.0K -0.0003 0.0013	x x x	-5.4K 0.00002 0.0009	x x x	

*Significance at the 95% confidence level (t-test). Note that the number of cool white lamps tested was twice that of the daylight lamps.

Their use would, of course, have weighted the final averages in favor of the Initial measurements.

Table 2.5 gives the Initial readings inside an integrating sphere minus the 25 cm section readings. The purpose of this comparison is to determine whether color temperature and chromaticity coordinate determined by a total flux measurement are comparable with their determination from a 25 cm section measurement. (At many laboratories measurement of chromaticity coordinates is typically performed with a Barnes Colorimeter which utilizes a 25 cm section of the lamp.) Table 2.5 indicates that the color parameters obtained by the two methods did not differ significantly for daylight lamps, but that the opposite was true for cool white lamps.

3. PARTICIPATING LABORATORY MEASUREMENT PROCEDURES

3.1. Comparison of the photometric and spectroradiometric equipment used

Though the general photometric setup was similar in most laboratories, there still were some significant differences in both the equipment and the measurement procedures. The differences were more marked in the spectroradiometric equipment and methods among the various laboratories. In this section the photometric equipment used by participating laboratories will be described. A brief description will then be given of each of the spectroradiometers.

Tables 3.1 to 3.3 summarize the equipment used at the various laboratories for the measurements in part 1 of the intercomparison. Laboratories 2 and 4 have reported using external color correcting filters to correct for the wavelength dependence of sphere reflectivity and window absorption. The effects of using these filters will be more clearly brought out in the discussion of the results.

Laboratory 1 normally applies a mathematical correction to their data. The method is based on a separate determination of the wavelength dependence of sphere reflectivity, window absorption, the emission of the source, and the detector response. They did not apply this correction to any of the data submitted for this intercomparison, however, since the correction was relatively small.

All except Laboratory 1 used Weston photocells as detectors; five used the model 856V (hermetically sealed) and two used model 594V. All Weston cells were equipped with Viscor filters. It should be noted that hermetically sealed photocells are not sensitive to humidity variations and are less sensitive to temperature variation (ref. 2).

Photocell output was read at most laboratories by a potentiometer device. Laboratory 5 used an operational amplifier and digital voltmeter combination. Only Laboratory 6 applied any linearity corrections to their photocell data.

All except Laboratory 6 warmed up the lamps for at least 15 minutes. All the laboratories measured the ambient temperature periodically, though the locations at which this was measured varied from laboratory to laboratory. Only Laboratories 2 and 3 indicate having temperature control. The location at which ambient temperature should be measured and the extent to which it should be controlled still constitute problems. Different types of lamps behave differently with a change in ambient temperature and it is not clear what is meant by the ambient temperature inside an integrating sphere. Most spheres, particularly larger ones, will have a temperature gradient even when the temperature at the sensor is controlled. The light output of a fluorescent lamp is a function of the wall temperature at the coldest point on the bulb. No completely satisfactory measurement has been made of this parameter.

Detailed descriptions of spectroradiometric equipment and techniques can be found in the papers of Thorington, et al., (ref. 3), and Sanders and Gaw (ref. 4). The spectroradiometric equipment that was used for this intercomparison by each of the laboratories participating in the spectroradiometric intercomparison will now be described briefly.

LABORATORY 1: This laboratory used two different monochromators in making measurements for this intercomparison. Measurements for part 2 of the intercomparison were made by using a custom built Czerny-Turner type monochromator. In measurements for part 3 of the intercomparison, the lines in the spectrum were measured by using the custom made monochromator and the continuum was measured with a Leiss double prism monochromator with flint glass prisms. Wavelength calibration was performed before every run with the 435.8 nm and 546.1 nm mercury lines. Both monochromators employed a photomultiplier with an S-20 response (EMI-9558Q) as the detector. The detector ouptut for the custom made grating monochromator was amplified and displayed on an L & N type G, series 6000 recorder and amplifier. For the Leiss monochromator the detector output was amplified by a Keithley 610 electrometer and read on a Vidar 610 digital voltmeter and recorded on punched paper tape.

Table 3.1

Sphere equipment used in the participating laboratories for photometric measurements.

Laboratory	Diameter	Coating	Date Coated _(See Note)	External Color Correcting Filter	Window
1	1.5 meter	G.E. Paint*	July 1968	None****	1.5 mm ground glass
2	3 meter	Burch**	July 1968	Wratten 78C	None***
3	3 meter	Burch	Nov. 1967	None	3 mm pot opal
4	1.5 meter	Burch	Oct. 1968	Corning 5900	3 mm flashed opal
5	2 meter	Burch	Aug. 1968	None	Opal
6	2.1 meter	MgO	1967	None	Depolished opal
7	1.8 meter	Burch	Aug. 1968	None	3 mm ground glass
8	3 meter	Burch	Aug. 1967	None	None***

*General Electric Sphere Paint **Burch Sphere Paint ***Cells mounted inside sphere facing sphere wall ****A different method is normally used for color correction (See text)

Note: Measurements at all the laboratories were made in October and November 1968.

Table 3.2

Photocells used in the participating laboratories for photometric measurements

Laboratory	Туре	Linearity Correction	Dectector Read Out
1	GE-PV-1	None	Standard Current Balance
2	Weston 856V	None	Operational Ampli- fier & Digital
3	Weston 856V	None	Rubicon Bridge
4	Weston 856V	None	Rubicon Bridge
5	Weston 594V	None	Operational Ampli- fier & Digital Voltmeter
6	Weston 594V	Yes	K-2 Potentiometer
7	Weston 856V	None	Rubicon Bridge
8	Weston 856V	None	Rubicon Bridge

Table 3.3

Lamp operation and temperature control during photometric measurements at the participating laboratories

	Control	і і	+ 0.5°C	+ 0.2°C	I I	I I	I I	I I	I I
Temperature	ensor Location	10 cm from wall o lamp axis	30 cm below lamp 45 cm above lamp	45 cm below at one end	5 cm from sphere wall in central plane	15 cm above lamp at end	45 cm below lamp from center	20 cm above lamp at one end	I I
	S	Hg-thermometer	Hg-thermometer & thermocouple	Hg-thermometer & thermocouple	Hg-thermometer	Hg-thermometer	Hg-thermometer	Hg-thermometer	1
Operation	Ballast for Standards	Sylvania Reference	Sylvania Reference	Sylvania Reference	Sylvania Reference	Sylvania Reference	Sylvania Reference	Sylvania Reference	Sylvania Reference
Lamp	<u>Power</u> Regulation	0.1%	1%	0.1%	0.15%	0.25%	1%	0.1%	1
Laboratory		1	7	e	4	Ŋ	9	2	8

LABORATORY 2: The basic dispersing unit used by this laboratory is an Ebert type monochromator (Perkin Elmer model E-1) with a 10 cm diameter diffusing sphere at the entrance slit. NBS standard filters were used to calibrate the wavelength. The last calibration took place about a year before this intercomparison. A photomultiplier tube with an S-20 response (EMI-9558Q) was used as the detector. The signal from the detector was amplified and integrated over 2 nm intervals and recorded on punched paper tape.

LABORATORY 4: In this laboratory a Hilger Watts model D-300 quartz double monochromator with a variable speed wavelength drive was used as the basic dispersing unit. The manufacturer's wavelength calibration was checked by using Hg, Cd, He, Ne, and Rb line sources. A 9.3 cm diameter sphere was used before the entrance slit of the monochromator to collect and diffuse the light. A photomultiplier with a quartz window and an S-20 response (RCA-7265) was used as the detector. The incoming light was chopped at 90 Hz and the signal from the detector after a-c preamplification and amplification was recorded on an x-y chart recorder.

LABORATORY 5: This laboratory used a Bausch and Lomb model 33-86-45 Ebert type grating monochromator. A 25 cm integrating box, coated with 3M "Velvet White", was placed before the entrance slit of the monochromator. The wavelength scale was calibrated to within 1 nm by using mercury lines. A photomultiplier tube with an S-20 response (EMI-9558QB) was used as the detector. The output signal from the photomultiplier was amplified by using a Keithley model 610 DC electrometer and displayed on an Esterline - Augus EllOIS chart recorder.

LABORATORY 7: This laboratory used a single prism monochromator (Beckman model DK-1) which was wavelength calibrated at the time of measurement by using the 546.1 nm mercury line. A photomultiplier tube with an S-10 response (RCA 6217) was used as the detector. The signal from the detector was amplified by a Keithley model 610A DC electrometer and displayed on a chart recorder.

LABORATORY 9: In this laboratory a quartz prism Hilger Watts model D-300 monochromator was used with an S-20 response photomultiplier tube (EMI-9558QB). The wavelength scale was calibrated to ± 0.2 nm by using 60 lines of the Ru, Hg, Cs, Kr, Ar, and Ne spectra. The current output from the photomultiplier was amplified by a Dymec type 2411A amplifier, the output of which was measured by a digital voltmeter (Dymec, type 2401B). The voltmeter then sent a BCD output to a card punch.

3.2. Comparison of the measurement procedures used

PART 1: Photometric intercomparison of 40 watt fluorescent lamps by conventional methods.

In order to standardize the experimental methods in the various participating laboratories, each laboratory was supplied with an experimental design and the necessary data sheets (appendix A). Part 1 of the interlaboratory check involved three days of measurements at each laboratory. Over the course of a day six ETL CW standards (or other lamps held as standards by the laboratory) were measured against the two cool white and one daylight fluorescent, and the 200 watt incandescent intercomparison lamps. Each intercomparison lamp was measured twice in the course of a day. Over a period of three days, therefore, the fluoresent intercomparison lamps and the incandescent intercomparison lamp had each been measured six times. The data were analyzed in blocks of one day's run. A calibration factor was obtained by taking the ratio of the instrument reading and the assigned luminous flux of the six ETL CW Standards (or substitutes). An average of these calibration factors was used to compute the luminous flux of the other test lamps that were measured that day. The data from all the participating laboratories were analyzed in the same manner. Only Laboratory 6 submitted linearity corrections for their photocell. These corrections, which were on the order of 2.5%, were used in the analysis of their data.

In order to check for any drifts that might be present during the course of a day's run all the data were corrected for linear drift in the sphere factors. Only in the case of Laboratory 3 did drift corrections improve precision--and then only for the daylight lamp. This one result was judged to be insignificant and it was, therefore, concluded that no appreciable linear drift existed at any of the participating laboratories. Linear drift corrections were not applied to any of the reported data.

PART 2: Spectroradiometric study of 40 watt fluorescent lamps inside an integrating sphere

This test was intended to give the maximum amount of information for the minimum amount of work. The procedure was to be as follows.

1) The data were to be taken at 10 nm intervals from 380 nm to 760 nm. These data were to be reported unreduced.

2) Data were to be taken at 405.0 nm, 435.8 nm, 546.1 nm, and 578.0 nm. These data were to be reported with the appropriate effective bandpass.

3) The lamps were to be run in the order specified on the data sheets supplied with the lamps.

Because of variations in laboratory, equipment, and technique, this test procedure was not uniformly followed. Therefore, the data from each participating laboratory had to be modified in order to conform to the designed test.

LABORATORY 1: The data received were completely reduced. Data for all the wavelengths of interest were not taken, however, because of equipment limitations. A missing point at 490 nm was interpolated by using a quadratic polynominal fit to the points around this wavelength. The points missing from each end of the spectrum were set equal to zero. Since the fluorescent and the incandescent standard lamps were compared against the same set of reference lamps, the reduced data were treated as though they were unreduced. The mercury lines had already been adjusted for a 10 nm interval and were, therefore, treated in the same manner as the continuum.

LABORATORY 2: These data were the most difficult to reduce. The reported data were already reduced and the photometric flux (Y) had been normalized to 1000 lumens. The Y values were subsequently obtained from this laboratory for each set of measurements. By using Y, the magnitude of the data was adjusted and the data were reduced again at NBS.

LABORATORY 4: These data were reported unreduced. The mercury line doublets which were supposed to be reported as a single measurement were reported as two separate lines. These separate measurements were combined to single values and then all the data were reduced at NBS. Corrections were also applied for apparent discrete changes in the gain factor within one standard lamp - test lamp run.

LABORATORY 5: Unreduced data were reported by this laboratory. The datum reported for a mercury line, however, was the area under an analog plot of the line minus that of the continuum. Since the data of interest were the instrument readings adjusted to a 10 nm interval, the reported data for the mercury lines were divided by 10 times the instrument reading for the continuum and then multiplied by the radiant flux of the continuum. The data were then reduced at NES.

LABORATORY 7: These data were reported in three parts. The first part was the dark current of the photomultiplier, the second part was the relative reflectance of a reflecting plaque used only for the incandescent standards, and the third part included the first two parts plus the spectral radiant flux of the source. Therefore, the data from all three parts were combined to solve for the unreduced data and then reduced at NBS.

LABORATORY 9: This laboratory reported irradiance values relative to a quartz-halogen lamp. Since the same reference had been used for all measurements, these data were reduced at NBS in the same manner as untreated data.

PART 3: Spectroradiometric study of color on a 25 cm section of 40 watt fluorescent lamps

The 25 cm section data were treated the same way as the spectroradiometric data of Part 2. However, values were computed only for the color temperature and the x and y chromaticity coordinates.

PART 4: Check on systematic errors in conventional sphere photometry.

This part of the intercomparison was designed to provide information about the performance of the photometric equipment. This was obtained by using an additive design experiment (See sample data sheets for this part in appendix A). One block of data was to consist of five sphere measurements performed according to the following procedure:

1. C 2. C + (I) 3. C + I 4. (C) + I 5. I

Where C refers to a cool white fluorescent lamp and I to an incandescent 200 watt lamp, both of which had been calibrated for total luminous flux by NBS. The parentheses refer to the presence of an unlighted lamp in the sphere. For example, the second step represents a measurement taken with a lighted cool white fluorescent lamp and an unlighted incandescent lamp in the integrating sphere.

PART 5: Barnes Colorimeter determination of the x and y chromaticity coordinates of 40 watt fluorescent lamps.

Barnes Colorimeter measurements were not made at NBS, nor was an experimental design established for this test. The purpose of these measurements was to compare this method to the spectroradiometric method of determining the x and y chromaticity coordinates.

4. RESULTS OF THE INTERCOMPARISON

4.1. Results and comparison of the luminous flux measurements

In this section, the data obtained from the participating laboratories for each part of the intercomparison are compared against the assignments made at NBS. First a comparison is made of the parameters that were obtained from the conventional photometric measurements and those obtained spectroradiometrically. The differences in spectral distribution of the intercomparison lamps as measured at NBS and at the participating laboratories are then discussed.

Total luminous flux of the test lamps was obtained both from the photocell readings and from the spectral distribution measurements. Table 4.1 gives a summary of the conventional photometric luminous flux measurements at each laboratory averaged for each day. Tables 4.2 through 4.9 give the detailed results obtained from each laboratory and the differences between the laboratory and NBS values. Table 4.10 gives the final average total luminous flux measurements obtained at each laboratory and the calculated estimate of standard deviation.

Figure 4.1 is a combined plot of the percent difference between the daily laboratory average and the NBS assignment of total luminous flux. The plots of all differences for each laboratory are given in figures 4.2 through 4.9.

Total luminous flux was also determined from spectroradiometric measurements. The spectroradiometric flux determinations are given in table 4.11. Plots of the differences of these values from the NBS assignments are given in figure 4.10, and on an expanded scale in figure 4.11.

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Photometric measurement of total luminous flux -- summary of the daily averages for all participating laboratories

Per Cent Difference	1.5 1.4 1.3	1.2 1.4 1.5	-1.7 -1.5 -1.7	-18.1 -19.5 -19.7	-20.4 -21.0 -20.7	-16.2 -17.1 -16.5	0.4 -0.5 -0.5	0.7 0.3 0.3	-1.3 -2.6 -3.0	0.5 0.7 0.6	0.6	-1.4 -1.7 -1.5
Difference	40.5 37.5 37.0	33.8 38.8 40.8	-41.4 -36.9 -40.9	-506.4 -548.3 -552.7	-582.0 -597.8 -590.4	-398.0 -419.7 -406.8	11.9 -14.4 -14.9	17.0 8.6 7.5	-31.0 -63.3 -74.9	13.8 -19.5 17.1	17.3 3.3 6.0	-34.0 -42.6 -36.3
Lab (lumens)	2791.0 2788.0 2787.5	2839.5 2844.5 2846.5	2409.5 2414.0 2410.0	2298.5 2256.6 2252.2	2265.5 2249.7 2257.1	2062.9 2041.2 2054.1	2914.5 2888.1 2887.6	2522.2 2513.8 2512.7	2441.5 2409.2 2397.6	2849.9 2816.6 2853.2	2875.6 2861.6 2864.3	2442.2 2433.6 2439.9
NBS (lumens)	2750.5	2805.7	2450.9	2804.9	2847.5	2460.9	2902.5	2505.2	2472.5	2836.1	2858.3	2476.2
Lamp Type	CW1	CW2	Q	CWI	CW2	A	CW1	CW2	Q	CW1	CW2	A
Lamp	8801	8802	8908	8813	8814	8913	8795	8796	8905	8803	8804	8908A
Lab	2			9			7			80		
Per Cent Difference	-1.0 -0.9	0.7	0.6 0.7 0.6	0.0	0.0	-1.2 -1.3 -0.8	-0.2 0.2 0.4	-0.4 0.3 0.5	-3.0 -3.1 -3.0	-1.0 -0.4 -0.1	-1.3 -0.3 -0.6	-0.8 -0.4 4.0-
Per Cent Difference Difference	-28.9 -1.0 -24.8 -0.9 -14.6 -0.5	23.0 0.8 11.4 0.4 19.5 0.7	14.5 0.6 18.1 0.7 15.9 0.6	- 1.3 0.0 0.2 0.0 7.2 0.3	0.9 0.0 9.4 0.3 -16.1 -0.6	-30.2 -1.2 -31.7 -1.3 -20.2 -0.8	- 4.9 -0.2 6.9 0.2 12.7 0.4	-10.2 -0.4 9.8 0.3 14.7 0.5	-73.1 -3.0 -75.2 -3.1 -73.9 -3.0	-29.2 -1.0 - 9.9 -0.4 - 4.0 -0.1	-37.0 -1.3 - 7.8 -0.3 -17.0 -0.6	-19.5 -0.8 - 9.7 -0.4 -10.8 -0.4
Lab Per Cent (<u>lumens)</u> Difference Difference	2797.8 -28.9 -1.0 2801.8 -24.8 -0.9 2811.9 -14.6 -0.5	2861.1 23.0 0.8 2849.5 11.4 0.4 2857.6 19.5 0.7	2488.2 14.5 0.6 2491.8 18.1 0.7 2489.5 15.9 0.6	2793.5 - 1.3 0.0 2795.0 0.2 0.0 2802.0 7.2 0.3	2864.0 0.9 0.0 2872.5 9.4 0.3 2847.0 -16.1 -0.6	2449.5 -30.2 -1.2 2448.0 -31.7 -1.3 2459.5 -20.2 -0.8	2912.3 - 4.9 -0.2 2923.9 6.9 0.2 2929.8 12.7 0.4	2887.5 -10.2 -0.4 2907.6 9.8 0.3 2912.5 14.7 0.5	2392.9 -73.1 -3.0 2390.7 -75.2 -3.1 2392.0 -73.9 -3.0	2754.0 -29.2 -1.0 2773.3 - 9.9 -0.4 2779.2 - 4.0 -0.1	2804.9 -37.0 -1.3 2834.1 - 7.8 -0.3 2824.9 -17.0 -0.6	2462.1 -19.5 -0.8 2471.8 -9.7 -0.4 2470.7 -10.8 -0.4
NBS Lab Per Cent (lumens) (lumens) Difference Difference	2826.6 2797.8 -28.9 -1.0 2801.8 -24.8 -0.9 2811.9 -14.6 -0.5	2838.1 2861.1 23.0 0.8 2849.5 11.4 0.4 2857.6 19.5 0.7	2473.7 2488.2 14.5 0.6 2491.8 18.1 0.7 2499.5 15.9 0.6	2794.8 2793.5 - 1.3 0.0 2795.0 0.2 0.0 2802.0 7.2 0.3	2863.1 2864.0 0.9 0.0 2872.5 9.4 0.3 2847.0 -16.1 -0.6	2479.7 2449.5 -30.2 -1.2 2479.7 2448.0 -31.7 -1.3 2459.5 -20.2 -0.8	2917.1 2912.3 - 4.9 -0.2 2923.9 6.9 0.2 2929.8 12.7 0.4	2897.8 2887.5 -10.2 -0.4 2907.6 9.8 0.3 2912.5 14.7 0.5	2465.9 2392.9 -73.1 -3.0 2390.7 -75.2 -3.1 2392.0 -73.9 -3.0	2783.2 2754.0 -29.2 -1.0 2773.3 - 9.9 -0.4 2779.2 - 4.0 -0.1	2841.9 2804.9 -37.0 -1.3 2834.1 - 7.8 -0.3 2824.9 -17.0 -0.6	2481.5 2462.1 -19.5 -0.8 2471.8 - 9.7 -0.4 2470.7 -10.8 -0.4
Lamp NBS Lab Per Cent Type (lumens) 01fference Difference	CWI 2826.6 2797.8 -28.9 -1.0 2801.8 -24.8 -0.9 2811.9 -14.6 -0.5	CW2 2838.1 2861.1 23.0 0.8 2849.5 11.4 0.4 2857.6 19.5 0.7	D 2473.7 2488.2 14.5 0.6 2491.8 18.1 0.7 2489.5 15.9 0.6	CW1 2794.8 2793.5 - 1.3 0.0 2795.0 0.2 0.0 2802.0 7.2 0.3	CW2 2863.1 2864.0 0.9 0.0 2872.5 9.4 0.3 2847.0 -16.1 -0.6	D 2479.7 2449.5 -30.2 -1.2 2448.0 -31.7 -1.3 2459.5 -20.2 -0.8	CW1 2917.1 2912.3 - 4.9 -0.2 2923.9 6.9 0.2 2929.8 12.7 0.4	CW2 2897.8 2887.5 -10.2 -0.4 29.8 0.3 2912.5 14.7 0.5	D 2465.9 2392.9 -73.1 -3.0 2390.7 -75.2 -3.1 2392.0 -73.9 -3.0	CWI 2783.2 2754.0 -29.2 -1.0 2773.3 - 9.9 -0.4 2779.2 - 4.0 -0.1	CW2 2841.9 2804.9 -37.0 -1.3 2834.1 - 7.8 -0.3 2824.9 -17.0 -0.6	D 2481.5 2462.1 -19.5 -0.8 2471.8 -9.7 -0.4 2470.7 -10.8 -0.4
Lamp Type (lumens) (lumens) Difference Difference	8797 CW1 2826.6 2797.8 -28.9 -1.0 2801.8 -24.8 -0.9 2811.9 -14.6 -0.5	8798 CW2 2838.1 2861.1 23.0 0.8 2849.5 11.4 0.4 2857.6 19.5 0.7	8906 D 2473.7 2488.2 14.5 0.6 2491.8 18.1 0.7 2489.5 15.9 0.6	8805 CW1 2794.8 2793.5 - 1.3 0.0 2795.0 0.2 0.0 2802.0 7.2 0.3	8806 CW2 2863.1 2864.0 0.9 0.0 2872.5 9.4 0.3 2847.0 -16.1 -0.6	8909 D 2479.7 2449.5 -30.2 -1.2 2448.0 -31.7 -1.3 2459.5 -20.2 -0.8	8807 CW1 2917.1 2912.3 - 4.9 -0.2 2923.9 6.9 0.2 2929.8 12.7 0.4	8808 CW2 2897.8 2887.5 -10.2 -0.4 2907.6 9.8 0.3 2912.5 14.7 0.5	8910 D 2465.9 2392.9 -73.1 -3.0 2390.7 -75.2 -3.1 2392.0 -73.9 -3.0	8809 CW1 2783.2 2754.0 -29.2 -1.0 2773.3 - 9.9 -0.4 2779.2 - 4.0 -0.1	8810 CW2 2841.9 2804.9 -37.0 -1.3 2834.1 - 7.8 -0.3 2824.9 -17.0 -0.6	8911 D 2481.5 2462.1 -19.5 -0.8 2471.8 -9.7 -0.4 2470.7 -10.8 -0.4

1



participating laboratories.

	NBS	Lab		Per Cent
Lamp	(lumens)	(lumens)	Difference	Difference
8797	2826.3	2781.3	-45.3	-1.6
		2814.2	-12.4	-0.4
		2796.3	-30.3	-1.1
		2807.3	-19.3	-0.7
		2824.0	- 2.6	-0.1
		2799.9	-26.7	-0.9
8798	2838.1	2890.1	52.0	1.8
0, 50	205011	2832 2	- 5.9	-0.2
		2868 6	30 5	1 1
		2830 /	- 7 7	-0.3
		2000.4	- /./	-0.5
		2040.0	20.0	1.0
		2007.1	29.0	1.0
8906	2473.7	2491.7	18.0	0.7
		2484.7	11.0	0.4
		2486.8	13.1	0.5
		2496.8	23.1	0.9
		2505.1	31.4	1.3
		2474.0	0.3	0.0
			0.00	0.0

Photometric measurement of total luminous flux--Laboratory 1.

Table 4.3

Photometric measurement of total luminous flux--Laboratory 2.

	NBS	Lab		Per Cent
Lamp	(lumens)	(lumens)	Difference	Difference
8805	2794.8	2795	0	0.0
		2792	- 3	-0.1
		2792	- 3	-0.1
		2798	3	0.1
		2800	5	0.2
		2804	9	0.3
8806	2863.1	2887	24	0.8
		2841	- 22	-0.8
		2905	42	1.5
		2840	- 23	-0.8
		2844	- 19	-0.7
		2850	- 13	-0.5
8909	2479.7	2449	- 31	-1.2
		2450	- 30	-1.2
		2442	- 38	-1.5
		2454	- 26	-1.0
		2462	- 18	-0.7
		2457	- 23	-0.9




Lamp	NBS (lumens)	Lab (lumens)	Difference	Per Cent Difference
8807	2917.1	2919.8	2.7	0.1
		2904.7	-12.4	-0.4
		2927.0	9.9	0.3
		2920.9	3.8	0.1
		2936.9	19.8	0.7
		2922.7	5.6	0.2
8808	2897.8	2889.6	-8.2	-0.3
		2885.5	-12.3	-0.4
		2892.6	-5.2	-0.2
		2922.7	24.9	0.9
		2922.7	24.9	0.9
		2902.3	4.5	0.2
8910	2465.9	2400.4	-65.5	-2.7
		2385.3	-80.6	-3.3
		2385.6	-80.3	-3.3
		2395.7	-70.2	-2.8
		2388.9	-77.0	-3.1
		2395.1	-70.8	-2.9

Photometric measurement of total luminous flux--Laboratory 3.

Table 4.5

Photometric measurement of total luminous flux--Laboratory 4.

	NBS	Lab		Per Cent
Lamp	(lumens)	(lumens)	Difference	Difference
0.000	0.000			
8809	2783.2	2751.2	-32.0	-1.1
		2756.8	-26.4	-0.9
		2775.7	-7.5	-0.3
		2771.0	-12.2	-0.4
		2781.1	-2.1	-0.1
		2777.4	-5.8	-0.2
8810	2841.9	2831.3	-10.6	-0.4
		2778.5	-63.4	-2 2
		2833.7	-8.2	-0.3
		2834.6	-7.3	-0.3
		2823.1	-18.8	-0.7
		2826.8	-15.1	-0.5
8911	2481.5	2461.1	-20.4	-0.8
		2463.0	-18.5	-0.7
		2476.5	-5.0	-0.2
		2467.2	-14.3	-0.6
		2472.6	-8.9	-0.4
		2468.9	-12.6	-0.5



Fig. 4.4 NBS assignments compared to the photometric measurements of total luminous flux at Laboratory 3.



Fig. 4. 5 NBS assignments compared to the photometric measurements of total luminous flux at Laboratory 4.

hotometric meas	urement of	total	luminous	fluxLa	aboratory	5.
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	MRC	Lab		Per Cent
Tomo	(lumone)	(lumone)	Difforence	Difference
Lamp	(Tumens)	(Tumens)	Difference	Difference
8801	2750.5	2794	43	1.6
		2788	37	1.4
		2788	37	1.4
		2788	37	1.4
		2787	36	1.3
		2788	37	1.4
8802	2805.7	2835	29	1.0
0002	200317	2844	38	1.4
		2846	40	1.4
		2843	37	1.3
		2852	46	1 7
		2052	25	1.2
		2041	22	1.5
8908	2450.9	2411	-40	-1.6
		2408	-43	-1.8
		2418	-33	-1.3
		2410	-41	-1.7
		2411	-40	-1.6
		2409	-42	-1.7

Photometric measurement of total luminous flux--Laboratory 6.

	NBS	Lab		Per Cent
Lamp	(lumens)	(lumens)	Difference	Difference
8813	2804.9	2293.5	-511.4	-18.2
		2303.5	-501.4	-17.9
		2263.6	-541.3	-19.3
		2249.7	-555.2	-19.8
		2253.2	-551.7	-19.7
		2251.2	-553.7	-19.7
8814	2847.5	2277.5	-570.0	-20.0
		2253.6	-593.9	-20.9
		2263.6	-583.9	-20.5
		2235.8	-611.7	-21.5
		2261.1	-586.4	-20.6
		2253.2	-594.3	-20.9
8913	2460.9	2069.9	-391.0	-15.9
		2056.0	-404.9	-16.5
		2043.2	-417.7	-17.0
		2039.2	-421.7	-17.1
		2058.1	-402.8	-16.4
		2050.2	-410.7	-16.7



Fig. 4.6 NBS assignments compared to the photometric measurements of total luminous flux at Laboratory 5.





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	NBS	Lab		Per Cent
Lamp	(lumens)	(lumens)	Difference	Difference
8795	2902.5	2918.5	16.0	0.6
		2910.4	7.9	0.3
		2895.1	- 7.4	-0.3
		2881.1	-21.4	-0.7
		2887.1	-15.4	-0.5
		2888.1	-14.4	-0.5
8796	2505.2	2492.7	-12.5	-0.5
		2551.8	46.6	1.9
		2506.4	1.2	0.0
		2521.3	16.1	0.6
		2512.7	7.5	0.3
		2512.7	7.5	0.3
8905	2472.5	2459.6	-49.0	-2.0
		2459.6	-12.9	-0.5
		2412.7	-59.8	-2.4
		2405.7	-66.8	-2.7
		2402.6	-69.9	-2.8
		2392.6	-79.9	-3.2

Photometric measurement of total luminous flux--Laboratory 7.

Table 4.9

Photometric measurement of total luminous flux--Laboratory 8.

	NID O			
	NBS	Lab		Per Cent
Lamp	(lumens)	(lumens)	Difference	Difference
8803	2836.1	2836.9	0.8	0.0
		2862.9	26.8	0.9
		2812.7	-23.4	-0.8
		2820.6	-15.5	-0.5
		2856.2	20.1	0.7
		2850.3	14.2	0.5
8804	2858.3	2878.3	20.0	0.7
		2872.9	14.6	0.5
		2866.9	8.6	0.3
		2856.2	- 2.1	-0.1
		2850.3	- 8.0	-0.3
		2878.3	20.0	0.7
8908A	2476.2	2440.2	-36.0	-1.5
		2444.2	-32.0	-1.3
		2434.6	-41.6	-1.7
		2432.6	-43.6	-1.8
		2434.9	-41.3	-1.7
		2444.9	-31.3	-1.3



Fig. 4.8 NBS assignments compared to the photometric measurements of total luminous flux at Laboratory 7.



Fig. 4.9 NBS assignments compared to the photometric measurements of total luminous flux at Laboratory 8.

Laboratory	Lamp	Average (lumens)	Standard Deviation (lumens)
1	CW1 - 8797	2804	14.9
	CW2 - 8798	2856	23.4
	D - 8906	2490	10.7
2	CW1 - 8805	2797	4.8
	CW2 - 8806	2861	27.8
	D - 8909	2452	6.9
3	CW1 - 8807	2922	10.5
	CW2 - 8808	2903	16.6
	D - 8910	2392	6.2
4	CW1 - 8809	2769	12.1
	CW2 - 8810	2821	21.4
	D - 8911	2468	5.8
5	CW1 - 8801	2789	2.6
	CW2 - 8802	2844	5.6
	D - 8908	2411	3.5
6	CW1 - 8813	2269	23.5
	CW2 - 8814	2258	13.8
	D - 8913	2053	11.1
7	CW1 - 8795	2897	14.7
	CW2 - 8796	2516	19.8
	D - 8905	2416	23.7
8	CW1 - 8803	2840	20.1
	CW2 - 8804	2867	11.7
	D - 8908	2439	5.3

Photometric measurement of total luminous flux--comprehensive average and standard deviation. for each participating laboratory.

Table 4.10

Spectroradiometeric, i	Integrating	s sphere	measurement	of
total	l luminous	flux		

		NBS	Lah		Par Cont
Laboratory	Lamp	(<u>lumens</u>)	(<u>lumens</u>)	Difference	Difference
1	8797	2827	2770	- 57	- 2.0
-	0777	2027	2808	- 19	- 0.7
			2825	- 2	- 0.1
	8798	2838	2851	13	0.5
			2830	- 8	- 0.3
			2823	- 15	- 0.5
	8906	2474	2407	- 67	- 2.7
			2424	- 50	- 2.0
			2427	- 47	- 1.9
2	8805	2795	2611	-184	- 6.6
			2587	-208	- 7.4
			2604	-191	- 6.8
	8806	2863	2685	-178	- 6.2
			2671	-192	- 6.7
			2629	-234	- 8.2
	8909	2480	2341	-139	- 5.6
			2337	-143	- 5.8
			2305	-175	- 7.0
4	8809	2783	3183	400	14.4
			3189	406	14.6
			3183	400	14.4
	8810	2842	3311	469	16.5
			3321	479	16.9
			3315	473	16.6
	8911	2481	2914	432	17.4
			2922	440	17.8
			2913	431	17.4
5	8801	2750	2737	- 13	- 0.5
			2748	- 3	- 0.1
			2752	1	0.1
	8802	2806	2782	- 24	- 0.8
			2775	- 31	- 1.1
			2800	- 6	- 0.2
	8908	2451	2393	- 58	- 2.4
			2394	- 57	- 2.3
			2548	97	4.0







4.2. Results and comparison of the measurements of color temperature and the x and y chromaticity coordinates

Color temperature and the x and y chromaticity coordinates were evaluated from the data obtained in parts 2 and 3 of the intercomparison; that is, from the spectroradiometric measurements of the lamp in an integrating sphere and of a 25 cm section of the lamp. The x and y chromaticity coordinates were also measured with a Barnes Colorimeter in part 5 of the intercomparison. Tables 4.12 through 4.21 contain the results of these three tests.

Table 4.12 gives the laboratory sphere determinations of color temperature and compares these with the NBS assignments. Figure 4.12 is a plot of this data.

The x and y chromaticity coordinates measured in the participating laboratories and assigned at NBS, as well as the differences between the two, are given in tables 4.13, 4.14, and figures 4.13, and 4.14.

Tables 4.15 and 4.16 present summaries of the precision of the spectroradiometric sphere measurements of total luminous flux, color temperature, and the x and y chromaticity coordinates.

Table 4.17 gives the laboratory evaluation of color temperature and the NBS assignment based on measurements of a 25 cm section of the lamps (part 3). Figure 4.15 gives a plot of the percent deviation of the laboratory values from the NBS values. Tables 4.18 and 4.19 and figures 4.16 and 4.17 present the same information for the x and y chromaticity coordinates. Tables 4.20 and 4.21 are summaries of the precision of 25 cm section measurements of color temperature and x and y chromaticity coordinates in the different laboratories. Table 4.22 gives a summary of the luminous flux measurements obtained by both the spectroradiometric and conventional photometric techniques.

Finally, tables 4.23, 4.24 and 4.25 give a summary of the average values obtained at NBS and at the participating laboratories for the color parameters measured in the intercomparison and the methods used to obtain them. These tables also contain the results of the Barnes Colorimeter measurements.

Spectroradiometric, integrating sphere measurement of color temperature

		NBS	Lab	
Laboratory	Lamp	(Kelvins)	<u>(kelvins)</u>	Difference
1	8797	4059	4076	17
-			4066	7
			4109	50
	8798	4086	4127	41
			4133	47
			4061	- 25
	8906	6443	6584	141
			6518	75
			6527	84
2	8805	4110	4075	- 35
			3986	-124
			4095	- 15
	8806	4125	4100	- 25
			4097	- 28
			4093	- 32
	8909	6436	6351	- 85
			6319	-117
			6278	-158
4	8809	4101	4175	74
			4185	84
			4184	83
	8810	4085	4101	16
			4104	19
			4095	10
	8911	6450	6413	- 37
			6456	6
			6446	- 4
5	8801	4092	4144	52
-			4129	37
			4134	42
	8802	4100	4111	11
			4144	44
			4142	42
	8908	6402	6291	-111
			6272	-130
			6457	55



Spectroradiometric,	integrating	sphere	measurement	of	the	x
	chromaticity	coordin	ate			

Laboratory	Lamp	NES x	Lab x	Difference
1	8797	0.3800	0.3786	-0.0014
			0.3794	-0.0006
			0.3777	-0.0023
	8798	0.3794	0.3769	-0.0025
			0.3770	-0.0024
			0.3796	0.0002
	8906	0.3131	0.3106	-0.0025
			0.3118	-0.0013
			0.3119	-0.0012
2	8805	0.3783	0.3806	0.0023
			0.3835	0.0052
			0.3797	0.0014
	8806	0.3774	0.3787	0.0013
			0.3790	0.0016
			0.3796	0.0022
	8909	0.3133	0.3147	0.0014
			0.3152	0.0019
			0.3158	0.0025
4	8809	0.3786	0.3768	-0.0018
			0.3760	-0.0026
			0.3762	-0.0024
	8810	0.3794	0.3795	0.0001
			0.3792	-0.0002
			0.3797	0.0003
	8911	0.3131	0.3132	0.0001
			0.3128	-0.0003
			0.3130	-0.0001
5	8801	0.3790	0.3783	-0.0007
			0.3795	0.0005
			0.3794	0.0004
	8802	0.3787	0.3800	0.0013
			0.3788	0.0001
			0.3790	0.0003
	8908	0.3137	0.3153	0.0016
			0.3159	0.0022
			0.3124	-0.0013





Laboratory	Lamp	NBS y	Lab y	Difference
1	8797	0.3837	0.3805	-0.0032
			0.3820	-0.0017
			0.3816	-0.0021
	8798	0.3850	0.3811	-0.0039
			0.3824	-0.0026
			0.3822	-0.0028
	8906	0.3358	0.3329	-0.0029
			0.3341	-0.0017
			0.3326	-0.0032
2	8805	0.3844	0.3881	0.0037
			0.3865	0.0021
			0.3880	0.0036
	8806	0.3830	0.3845	0.0015
			0.3852	0.0022
			0.3869	0.0039
	8909	0.3356	0.3370	0.0014
			0.3380	0.0024
			0.3395	0.0039
4	8809	0.3842	0.3870	0.0028
			0.3856	0.0014
			0.3865	0.0023
	8810	0.3851	0.3879	0.0028
			0 <mark>.387</mark> 0	0.0019
			0.3878	0.0027
	8911	0.3351	0.3381	0.0030
			0.3370	0.0019
			0.3373	0.0022
5	8801	0.3844	0.3899	0.0055
			0.3919	0.0075
			0.3922	0.0078
	8802	0.3844	0.3909	0.0065
			0.3922	0.0078
			0.3917	0.0073
	8908	0.3357	0.3424	0.0067
			0.3433	0.0076
			0.3410	0.0053

Spectroradiometric, integrating sphere measurement of the y chromaticity coordinate



NBS assignments compared to the spectroradiometric, integrating sphere measurements of the y chromaticity coordinate at each participating laboratory. Fig. 4.14

Spectroradiometric, integrating sphere measurement of luminous flux and color temperature--comprehensive average and standard deviation for each participating laboratory

Laboratory	Lamp	Luminous Flux	Standard Deviation	Color Temperature	Standard Deviation
1	8797	2801	28	4084	23
	8798	2835	15	4107	40
	890 6	2419	11	6543	36
2	8805	2601	12	4052	58
	8806	2662	29	4097	4
	8909	2328	20	6316	37
4	8809	3185	3	4181	6
	8810	3316	5	4100	5
	8911	2916	5	6438	23
5	8801	2746	8	4136	8
	8802	2786	13	4132	19
	8908	2445	89	6340	102

Table 4.16

Spectroradiometeric, integrating sphere measurement of the x and y chromaticity coordinates - comprehensive average and standard deviation for each participating laboratory

Laboratory	Lamp	<u>x</u>	Standard Deviation	<u>y</u>	Standard Deviation
_	0707	0.270/	0.0000	0 201/	0 0008
1	8/9/	0.3780	0.0009	0.3814	0.0008
	8798	0.3778	0.0015	0.3819	0.0007
	8906	0.3114	0.0007	0.3332	0.0008
2	8805	0.3813	0.0020	0.3875	0.0009
	8806	0.3791	0.0005	0.3855	0.0012
	8909	0.3152	0.0006	0.3382	0.0013
4	8809	0.3763	0.0004	0.3864	0.0007
	8810	0.3795	0.0003	0.3876	0.0005
	8911	0.3130	0.0002	0.3375	0.0006
5	8801	0.3791	0.0007	0.3913	0,0013
-	8802	0.3793	0.0006	0.3916	0.0007
	0002	0.01/5	0.0010	0.0/00	0.0010
	8908	0.3145	0.0019	0.3422	0.0012

		NBS	Lab	
Laboratory	Lamp	(kelvins)	(kelvins)	Difference
1	8797	4080	3987	- 93
-	0151	1000	3990	- 90
			4033	- 47
	8798	4070	3990	- 80
			3982	- 88
			4002	- 68
	8906	6507	6193	- 314
			6476	- 31
			6492	- 15
2	8805	4093	4099	6
2	0005	4000	4098	5
			4093	0
	8806	4107	4122	15
	6666	4107	4114	7
			4116	, 0
	8000	6/57	6/10	- 38
	8909	0407	6272	- 50
			6450	- 05
			0450	- 0
4	8809	4111	4129	18
			4090	- 21
			4070	- 41
	8810	4073	4083	9
			4101	27
			4128	54
	8911	6467	6280	- 187
	0,11	0.07	6271	- 196
			6374	- 93
5	8801	4091	4139	/18
5	6601	4001	4135	54
			4141	50
	8802	6118	4141	68
	8802	4110	4161	23
			/138	20
	8908	6/12	6383	- 29
	8900	0412	6377	- 35
			6305	- 107
			0000	- 107
7	8795	4111	3773	- 338
			3758	- 353
			3711	- 400
	8796	3996	3658	- 338
			3693	- 303
			3606	- 390
	8905	6465	5269	-1196
			5381	-1084
			5151	-1314
9	8700	4089	4075	- 1/
9	0799	4009	4075	- 14
			4080	- 9
	8800	4071	4003	10
	0000	4071	4003	12
			4075	4
	8007	64.35	4089	18
	8907	6435	0433	- 2
			0440	11
			6442	/





Table 4	4.18
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Laboratory	Lamp	<u>NBS x</u>	Lab x	Difference
1	8797	0.3788	0 3837	0 0049
-			0.3837	0.0049
			0.3823	0.0035
	8798	0.3801	0.3843	0.0042
		010001	0.3843	0.0042
			0.3835	0 0034
	8906	0.3120	0.3171	0 0051
		010120	0.3122	0,0002
			0.3124	0.0004
2	8805	0.3786	0.3788	0.0002
			0.3787	0.0001
			0.3792	0.0006
	8806	0.3778	0.3775	-0.0003
			0.3780	0.0002
			0,3779	0.0001
	8909	0.3132	0,3135	0.0003
			0.3144	0.0012
			0.3131	-0.0001
4	8809	0.3780	0.3780	0.0000
			0.3803	0.0023
			0.3810	0.0030
	8810	0.3800	0.3803	0.0003
		010000	0.3793	-0.0007
			0.3791	-0.0009
	8911	0 3129	0 3157	0.0028
		0.13127	0 3160	0.0031
			0.3142	0.0013
5	8801	0 3789	0.3786	-0.0003
J	0001	0.3789	0.3786	-0.0003
			0.3784	-0.0005
	8802	0 3779	0.3765	-0.0004
	8802	0.3778	0.3766	-0.0012
			0.3763	0.0003
	8008	0 2127	0.3700	0.0010
	8908	0.3137	0.3138	0.0001
			0.3130	0.0001
			0.3150	0.0013
7	8795	0.3776	0.3994	0.0218
			0.4002	0.0226
			0.4031	0.0255
	8796	0.3832	0.4059	0.0227
			0.4049	0.0217
			0.4103	0.0271
	8905	0.3129	0.3392	0.0263
			0.3364	0.0235
			0.3426	0.0297
9	8799	0.3787	0.3793	0.0006
			0.3791	0.0004
			0.3785	-0.0002
	8800	0.3792	0.3793	0.0001
			0.3794	0.0002
			0.3789	-0.0003
	8907	0.3134	0.3134	0.0000
			0.3132	-0.0002
			0.3133	-0.0001
				0.0001





Table	4.	19
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Laboratory	Lamp	NBS y	Lab y	Difference
1	8797	0.3819	0.3874	0.0055
			0.3877	0.0058
			0.3876	0.0057
	8798	0.3852	0.3897	0.0045
			0.3887	0.0035
			0.3887	0.0035
	8906	0.3347	0.3405	0.0058
			0.3350	0.0003
			0.3352	0.0005
2	8805	0.3823	0.3850	0.0027
			0.3844	0.0021
			0.3855	0.0032
	8806	0.3821	0.3825	0.0004
			0.3835	0.0014
			0.3833	0.0012
	8909	0.3342	0.3353	0.0011
			0.3366	0.0024
			0.3353	0.0011
4	8809	0.3830	0.3860	0.0030
			0.3891	0.0061
			0.3887	0.0057
	8810	0.3856	0.3881	0.0025
			0.3870	0.0014
			0.3902	0.0046
	8911	0.3342	0.3400	0.0058
		0.000.1	0.3394	0.0052
			0.3380	0.0038
5	8801	0 3837	0 3898	0.0061
2	0001	0.3037	0.3900	0,0063
			0.3903	0.0065
	8802	0 3823	0.3885	0.0062
	0002	0.5025	0.3888	0.0065
			0.3904	0.0081
	8908	0 3350	0 3405	0.0055
	0,00	0.0000	0 3409	0.0059
			0.3421	0.0071
			0.0721	010071
7	8795	0.3817	0.4092	0.0275
			0.4096	0.0279
			0.4133	0.0316
	8796	0.3865	0.4126	0.0261
			0.4154	0.0289
			0.4185	0.0320
	8905	0.3336	0.3692	0.0356
			0.3692	0.0356
			0.3759	0.0423
9	8799	0.3828	0.3827	-0.0001
			0.3832	0.0004
			0.3820	-0.0008
	8800	0.3826	0.3842	0.0016
			0.3835	0.0009
			0.3834	0.0008
	8907	0.3349	0.3358	0.0009
			0.3351	0.0002
			0.3352	0.0003





Laboratory	Lamp	Average (kelvins)	Standard Deviation
1	8797	4003	26
	8798	3991	10
	8906	6387	168
2	8805	4097	3
	8806	4117	4
	8909	6414	39
4	8809	4096	30
	8810	4104	23
	8911	6308	57
5	8801	4142	3
	8802	4155	27
	8908	6355	43
7	8795	3747	32
	8796	3652	44
	8905	5267	115
9	8799	4081	7
	8800	4082	7
	8907	6440	7

and standard deviation for each participating laboratory

Table 4.21

Spectroradiometric, 25 cm lamp section measurement of the x and y chromaticity coordinates --

comprehensive average and standard deviation for each participating laboratory

Laboratory	Lamp	<u>Average x</u>	Standard Deviation	<u>Average y</u>	Standard Deviation
1	8797	0.3832	0.0008	0.3876	0.0002
	8798	0.3840	0.0005	0.3890	0.0006
	8906	0.3139	0.0028	0.3369	0.0031
2	8805	0.3789	0.0003	0.3850	0.0006
	8806	0.3778	0.0003	0.3831	0.0005
	8909	0.3137	0.0007	0.3357	0.0008
4	8809	0.3798	0.0016	0.3879	0.0017
	8810	0.3796	0.0006	0.3884	0.0016
	8911	0.3153	0.0010	0.3391	0.0010
5	8801	0.3785	0.0001	0.3900	0.0003
	8802	0.3779	0.0012	0.3892	0.0010
	8908	0.3142	0.0007	0.3412	0.0008
7	8795	0.4009	0.0019	0.4107	0.0023
	8796	0.4070	0.0029	0.4155	0.0030
	8905	0.3394	0.0031	0.3714	0.0039
9	8799	0.3790	0.0004	0:3826	0.0006
	8800	0.3792	0.0003	0:3837	0.0004
	8907	0.3133	0.0001	0:3354	0.0004

			NBS (lu	mens)	Lab (lumens)		
		Lamp		Spectro-		Spectro-	
Laboratory	Lamp	type	Photometric	radiometric	Photometric	radiometric	
1	8797	CW1	2820	2833	2804	2801	
	8798	CW2	2833	2842	2856	2835	
	8906	D	2464	2482	2490	2419	
2	8805	CW1	2792	2798	2797	2601	
	8806	CW2	2863	2864	2861	2662	
	8909	D	2485	2474	2452	2328	
3	8807	CW1	2911	2924	2922		
	8808	CW2	2895	2902	2903		
	8910	D	2472	2460	2392		
4	8809	CW1	2777	2789	2 76 9	3185	
	8810	CW2	2840	2844	2821	3316	
	8911	D	2485	2478	2468	2916	
5	8801	CW1	2751	2750	2789	2746	
	8802	CW2	2808	2804	2844	2786	
	8908	D	2452	2450	2411	2445	
6	8813	CW1	2797	2812	2269		
	8814	CW2	2847	2848	2258		
	8913	D	2469	2454	2053		
7	8795	CW1	2946	2936	2897		
	8796	CW2	2514	2499	2516	1980 1980 1	
	8905	D	2478	2467	2416		
8	8803	CW1	2834	2838	2840		
	8804	CW2	2857	2860	2867		
	8908A	D	2480	2473	2439		

Comparison of the photometric and spectroradiometric measurements of total luminous flux.

Comparison of the integrating sphere and the 25 cm lamp section spectroradiometric measurements of color temperature.

Lamp 25 cm 25 Laboratory Lamp type Sphere section Sphere sec 1 8797 CW1 4059 4080 4084 4 8798 CW2 4086 4070 4107 3 8906 D 6443 6507 6543 6 2 8805 CW1 4110 4093 4052 4 8906 D 6443 6507 6543 6 2 8805 CW1 4110 4093 4052 4 8909 D 6436 6457 6316 6 4 8809 CW1 4101 4111 4181 4 8810 CW2 4085 4073 4100 4 8911 D 6450 6461 6438 6 5 8801 CW1 4092 4091 4136 4	cm ction 003 991 387 097
Laboratory Lamp type Sphere section Sphere section 1 8797 CW1 4059 4080 4084 4 8798 CW2 4086 4070 4107 3 8906 D 6443 6507 6543 6 2 8805 CW1 4110 4093 4052 4 8906 D 6436 6457 6316 6 2 8805 CW1 4110 4093 4052 4 8909 D 6436 6457 6316 6 4 8809 CW1 4101 4111 4181 4 8810 CW2 4085 4073 4100 4 8911 D 6450 6461 6438 6 5 8801 CW1 4092 4091 4136 4	003 991 387 097
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4003 1991 5387 6097
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3991 387 097
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	5387 1097
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	097
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	117
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	
4 8809 CW1 4101 4111 4181 4 8810 CW2 4085 4073 4100 4 8911 D 6450 6461 6438 6 5 8801 CW1 4092 4091 4136 4 8802 CW2 4100 4118 4132 4	5414
8810 CW2 4085 4073 4100 4 8911 D 6450 6461 6438 6 5 8801 CW1 4092 4091 4136 4 6450 6410 6438 6 6 6 6 6	4096
8911 D 6450 6461 6438 6 5 8801 CW1 4092 4091 4136 4 8802 CW2 6100 6118 6132 6	+104
5 8801 CW1 4092 4091 4136 4	308
8802 CH2 (100 (118 (132 (142
	155
8908 D 6402 6412 6340 6	5355
7 8795 CW1 4130 4111 3	3747
8796 CW2 3996 3996 3	3652
8905 D 6431 6465 5	5267
9 8799 CW1 4073 4089 4	081
8800 CW2 4067 4071 4	082
8907 D 6427 6435 6	6440

Comparison of the integrating sphere and the 25 cm lamp section spectroradiometric measurements, and the Barnes colorimetric measurement of the x chromaticity coordinate.

			NBS x		Lab x			
		Lamp		25 cm		25 cm		
Laboratory	Lamp	type	Sphere	section	Sphere	section	Barnes	
1	8797	CW1	0.3800	0.3788	0.3786	0.3832	0.3845	
	8798	CW2	0.3794	0.3801	0.3778	0.3840	0.3845	
	8906	D	0.3131	0.3120	0.3114	0.3139	0.3178	
2	8805	CW1	0.3783	0.3786	0.3813	0.3789	0.3832	
	8806	CW2	0.3774	0.3778	0.3791	0.3778	0.3825	
	8909	D	0.3133	0.3132	0.3152	0.3137	0.3148	
3	8807	CW 1	0.3776	0.3778	-	_	0.3784	
Ū.	8808	CW2	0.3766	0.3768	-	-	0.3776	
	8910	D	0.3133	0.3134	-	-	0.3151	
		_						
4	8809	CW1	0.3786	0.3780	0.3763	0.3798	0.3824	
	8810	CW2	0.3794	0.3800	0.3795	0.3796	0.3842	
	8911	D	0.3131	0.3130	0.3130	0.3153	0.3169	
5	8801	CW 1	0.3790	0.3789	0.3791	0.3785	0.3730	
	8802	CW2	0.3787	0.3776	0.3793	0.3779	0.3730	
	8908	D	0.3137	0.3137	0.3145	0.3142	0.3150	
7	8795	CUI	0 3773	0 3776		0 /009	0 3820	
'	8796	CP12	0.3773	0.3770	-	0.4070	0.3875	
	8905	D D	0.3134	0.3129	-	0.4070	0.3161	
	0905	D	0.5154	0.5129	-	0.5594	0.5101	
8	8803	CW1	0.3798	0.3800	-	-	0.3854	
	8804	CW2	0.3798	0.3798	-	-	0.3851	
	8908A	D	0.3134	0.3136	-	-	0.3137	
9	8799	CW 1	0 3794	0.3787	-	0 3790	_	
-	8800	CW2	0.3794	0.3792	_	0.3792	_	
	8907	D	0.3134	0.3134	-	0.3133	_	
	0.07	-	0.0104	0.0101		0.0100		

Comparison of the integrating sphere and the 25 cm lamp section spectroradiometric measurements, and the Barnes colorimetric measurement of the y chromaticity coordinate.

			NBS y		Lab y		
		Lamp		25 cm		25 cm	
Laboratory	Lamp	type	Sphere	section	Sphere	section	Barnes
1	8797	CW1	0.3837	0.3819	0.3814	0.3876	0.3895
	8798	CW2	0.3850	0.3852	0.3819	0.3890	0,3905
	8906	D	0.3358	0.3347	0.3332	0.3369	0.3410
2	8805	CW1	0.3844	0.3832	0.3875	0.3850	0.3895
	8806	CW2	0.3830	0.3821	0.3855	0.3831	0.3878
	8909	D	0.3356	0.3342	0.3382	0.3357	0.3401
3	8807	CW1	0.3827	0.3818	-	-	0.3857
	8088	CW2	0.3811	0.3792	-	-	0.3843
	8910	D	0.3351	0.3344	-	-	0.3401
4	8809	CW1	0.3842	0.3830	0.3864	0.3879	0.3885
	8810	CW2	0.3851	0.3856	0.3876	0.3884	0.3897
	8811	D	0.3351	0.3340	0.3375	0.3391	0.3402
							0 0050
5	8801	CW1	0.3844	0.3837	0.3913	0.3900	0,3850
	8802	CW2	0.3844	0.3823	0.3916	0.3892	0,3850
	8908	D	0,3357	0.3350	0.3422	0.3412	0.3370
7	8795	CW1	0.3831	0.3817	-	0.4107	0.3863
	8796	CW2	0.3870	0.3865	-	0.4155	0.3907
	8905	D	0.3350	0.3336	-	0.3714	0.3395
8	8803	CW1	0.3842	0.3837	-	-	0.3913
	8804	CW2	0.3843	0.3834	-	-	0.3916
	8908A	D	0.3352	0.3345	-	-	0.3416
0	8799	CW1	0 3830	0 3828		0 3826	
2	8800	CU12	0.3836	0.3826		0.3837	
	8007	D	0.3357	0.3340		0.335/	
	0907	D	1,0,001	0.0047	-	0.0004	

4.3. Results and comparison of the spectral distribution measurements

The spectral distribution data from each laboratory are given in tables 4.26 through 4.67 and plotted in figures 4.18 through 4.59. These data include both the spectroradiometric measurement of the total lamp output in an integrating sphere and that of a 25 cm section of the lamp. Summarization and compilation of these results are included in the tables and figures listed in the previous section.

In examining the detailed data compiled in this section, one should note that the intercomparison was statistically designed to use the data acquired at NBS as a base. Therefore, data from the spectroradiometric equipment at the participating laboratories will be evaluated against the NBS base. Consistent differences from the NBS base in all the data would indicate, of course, that the problem may be at NBS itself.

From an examination of all of the spectral distribution curves it appears that most of the curves do not match in the regions of the mercury lines. The largest deviations are in the region near 580 nm. Since the curvature of the continuum is greatest at this mercury line, the efficiency of the fit of a quadratic polynominal may be in question. Perhaps a better interpolation procedure at NBS would have eliminated this problem. No other consistent deviations were observed between NBS and the other laboratories. The individual laboratory deviations will now be examined.

If the data from each laboratory (see also the tables and figures in section 4.2) are different from NBS or from the overall laboratory average, this could be indicative of problems in experimental technique. Effects of system nonlinearity, improper sphere size, inadequate or improperly arranged baffling, scattered light within the monochromator, inadequate (or the absence of) filtering of second-order spectra and, of course, the individualism of each operator will contribute to differences in the measurement of the color parameters and total luminous flux.

LABORATORY 1: Agreement between this laboratory's spectroradiometric measurement of total luminous flux and that of NBS was close. The small difference may be attributable to system non-linearity either at this laboratory or at NBS. This point cannot be checked, of course, without additional experiments.

LABORATORY 2: The spectroradiometric values of total luminous flux obtained in this laboratory's sphere were low compared to the other participating laboratories. Small sphere size and the arrangement of lamps and baffling within the sphere are suspected as the principal reasons for these low values. However, the difficulties encountered in the data analysis may have introduced discrepancies and would, of course, obscure the identification of problems in experimental technique.

LABORATORY 4: This laboratory's sphere measurements of total luminous flux were extremely high and may have been caused by inadequate baffling of the lamps. Difficulties were encountered in the analysis of the data from this laboratory and may have obfuscated the identification of problems in experimental technique. The relative spectral flux distribution curves for this laboratory appear to be higher than those of NBS in the 440 to 520 nm region. This laboratory used synchronous amplification and, therefore, chopped the light output at 90 Hz. Because the various phosphors used in the lamp do not have the same decay time, the light output from each phosphor was probably sampled to a different extent. The spectral flux in the region around 590 nm is also considerably different from that of NBS. Since this laboratory used a prism monochromator and did not indicate frequent wavelength calibration checks, the cam in the wavelength drive of the instrument may have been off calibration in this region.

LABORATORY 5: This laboratory's sphere measurements of total luminous flux were close to those of NBS. However, a spurious line appears at 700 nm and the spectral flux distribution curves exhibit a decrease from the NBS curves toward the red region of the spectrum. The line may be due to an emission from the coating used on their integrating box but this does not explain the relative decrease in this region. If this is not an effect produced by the 3M "Velvet White" coating, then it is suspected either that the sensitivity of their photomultiplier has decreased in this spectral region or that the gain and/or the sensitivity of their electronics consistently drifted during the course of a single run.

LABORATORY 7: Data from Laboratory 7 agreed very poorly with those of all of the other participating laboratories. Their spectroradiometric equipment appeared to have most of the problems that afflict spectroradiometry.

LABORATORY 9: This laboratory submitted only relative spectral irradiance measurements, and these agreed closely with those made at NBS.

NATIONAL BUREAU OF STANDARDS: Careful analysis of the NBS Initial and Repeat spectroradiometric measurements indicates that a small wavelength shift occurred in the interim between measurements. The shift was definitely less than the instrument bandpass and much too small to be detected in a data comparison with the other laboratories.
	NB	S INITI	AL	LA	BORATOR	Y 1	M	BS REPE	AT
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8	RUN 9
380.0	3.8	4.2	3.9	•0	0	0	3.6	3.6	3.7
390.0	5.8	6.2	6.0	6•6	6.1	7.3	5.7	5.6	5.8
400.0	8.5	8.6	8.6	8.9	9.2	8.8	8.2	8.1	8.3
410.0	10.8	10.8	10.8	11.1	10.5	10.8	10.6	10.4	10.6
420.0	13.1	13.2	13.2	13.5	13.0	13.5	13.0	12.9	13.0
430.0	15.9	16.1	16.0	16.1	16.7	16.9	15.8	15.9	15.8
440.0	18.4	18.6	18.5	19.3	18.8	19.4	18.4	18.4	18.3
450.0	20.7	20•6	20.7	21.5	20.8	21.0	20.7	20.8	20.6
460.0	22.4	22•3	22.5	22.7	22.7	21.7	22.5	22.5	22.4
470.0	23.5	23•4	23.5	23.9	23.6	23.9	23.5	23.6	23.6
480.0	23.8	23•8	23.9	24.0	24.0	23.8	23.9	24.0	23.9
490.0	23.8	23•8	23.9	23.7	23.8	23.4	23.9	23.9	23.9
500.0	22.8	22.8	22.9	22.9	22.9	22.7	23.0	23.1	23.0
510.0	22.4	22.4	22.5	22.8	22.5	22.5	22.5	22.6	22.5
520.0	23.4	23.4	23.2	23.6	23.7	23.5	23.5	23.4	23.4
530.0	27.5	27.4	27.6	27.7	27.9	28.3	27.4	27.2	27.2
540.0	35.5	35.4	35.6	34.8	35.1	35.7	35.1	34.9	35.0
550.0	45.6	45.4	45.7	44.9	45.2	45.6	45.3	45.0	45.1
570.0 580.0 590.0	58.5 66.4 69.0 65.0	66 • 1 68 • 7 64 • 6	66.7 69.4 65.1	65.4 67.8 65.3	58.3 65.2 67.5 65.1	58.1 64.9 67.0 64.4	66.4 69.3 65.5	66.3 69.2 65.5	57.9 66.2 69.1 65.5
600.0	57.1	56.8	57.4	57.8	58.1	57.1	57.7	57.6	57.6
610.0	47.2	47.0	47.4	48.8	48.4	47.7	48.0	47.9	48.1
620.0	37.0	36.8	37.1	39.1	38.4	37.7	37.7	37.9	37.9
630.0	28.4	28.4	28.5	29.0	29.7	28.9	28.9	28.9	29.0
640.0	21.2	21.2	21.2	21.6	22.0	22.0	21.7	22.0	21.7
650.0	15.5	15.7	15.6	16.1	16.6	16.8	16.0	16.0	16.0
660.0	11.4	11.5	11.4	12.0	12.8	12.7	11.6	11.6	11.6
670.0	8•4	8•6	8.4	9.4	10•1	10.0	8.5	8.5	8.7
680.0	6•2	6•4	6.0	7.2	7•5	7.8	6.2	6.4	6.4
690.0	5•0	5•0	4.7	5.2	5•4	5.9	5.0	5.0	5.0
700.0 710.0 720.0 730.0 740.0 750.0 760.0	3.6 3.0 2.3 3.2 2.1 2.5 2.4	3.7 3.2 2.7 3.5 2.4 2.8 2.7	3.3 2.7 2.0 3.2 1.6 1.9	4.1 3.1 3.2 .0 .0 .0	4.5 3.3 3.1 .0 .0 .0	4.5 4.3 3.0 .0 .0	3.6 2.9 2.3 1.9 2.0 2.2 1.5	3.6 3.0 2.3 1.8 2.1 2.0 1.5	3.6 3.0 2.3 2.0 2.1 2.3 1.6
10000	2.04	2 • 1	1.0	ME	ERCURY L	.INES	100	1+3	100
405.0	23•1	23.0	23.4	23.2	23•5	22.2	23.3	23.8	23.2
436.0	57•7	56.9	57.5	59.4	58•2	59.4	56.8	57.7	57.3
546.0	26•8	26.6	27.0	27.8	27•5	27.8	27.0	27.1	26.9
578.0	9•3	9.2	9.3	8.6	8•3	8.9	9.1	9.0	9.0



NORMALIZED TO AREA

	NBS INITIAL			LABORATORY 1		Y 1	NBS REPEAT		
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8	RUN 9
380.0	.0320	•0354	•0328	•0000	.0000	•0000	•0295	•0297	•0302
390.0	.0482	•0521	•0497	•0537	.0505	•0604	•0468	•0467	•0477
400.0	.0708	.0723	.0714	0722	.0758	.0733	.0672	.0670	.0679
410.0	.0899	.0908	.0903	0900	.0861	.0900	.0863	.0863	.0872
420.0	.1097	.1107	.1099	1096	.1066	.1123	.1066	.1076	.1073
430.0	.1329	.1356	.1331	1309	.1374	.1403	.1293	.1319	.1298
440.0	.1535	.1559	.1539	1567	.1546	.1607	.1501	.1531	.1508
450.0	.1726	.1734	.1727	1746	.1710	.1741	.1691	.1726	.1699
460.0	.1868	.1875	.1871	1848	.1867	.1805	.1839	.1868	.1842
470.0	.1959	.1970	.1955	1939	.1942	.1985	.1926	.1961	.1939
480•0	•1988	•1996	•1993	•1947	•1977	•1972	•1958	•1995	•1970
490•0	•1983	•1996	•1987	•1921	•1959	•1940	•1955	•1984	•1963
500.0 510.0 520.0 530.0 550.0 550.0 560.0 570.0 580.0 590.0	.1903 .1873 .1955 .2297 .2964 .3807 .4863 .5538 .5761 .5423	 1918 1882 1964 2304 2971 3818 4876 5555 5774 5424 	.1908 .1874 .1936 .2298 .2962 .3807 .4870 .5556 .5783 .5426	•1861 •1850 •1920 •2251 •2827 •3647 •4711 •5310 •5507 •5302	.1887 .1853 .1950 .2297 .2887 .3721 .4799 .5370 .5559 .5364	 1887 1872 1950 2348 2960 3786 4826 5390 5563 5346 	.1881 .1845 .1919 .2240 .2875 .3703 .4752 .5434 .5669 .5361	.1919 .1878 .1947 .2263 .2899 .3740 .4815 .5513 .5755 .5453	.1891 .1852 .2241 .2881 .3712 .4765 .5445 .5688 .5387
600.0 610.0 620.0 640.0 650.0 660.0 670.0 680.0 690.0	.4765 .3944 .3090 .2367 .1770 .1297 .0950 .0704 .0521 .0415	.4773 .3946 .2383 .1785 .1318 .0967 .0725 .0536 .0422	.4781 .3950 .2377 .1766 .1296 .0949 .0703 .0500 .0392	.4697 .3960 .3178 .2355 .1754 .1309 .0972 .0763 .0581 .0424	.4786 .3981 .3164 .2443 .1812 .1370 .1058 .0829 .0620 .0445	.4739 .3960 .3129 .2399 .1827 .1393 .1055 .0832 .0646 .0493	.4718 .3929 .3088 .2361 .1779 .1310 .0951 .0697 .0511 .0409	.4791 .3986 .3151 .2408 .1834 .1327 .0965 .0708 .0529 .0417	.4736 .3961 .3120 .2387 .1784 .1320 .0953 .0712 .0524 .0411
700.0	.0302	.0311	.0277	0330	.0370	.0373	.0295	•0301	.0293
710.0	.0254	.0266	.0226	0254	.0275	.0359	.0240	•0246	.0248
720.0	.0195	.0225	.0163	0256	.0253	.0251	.0187	•0191	.0192
730.0	.0264	.0298	.0264	0000	.0000	.0000	.0158	•0147	.0163
740.0	.0177	.0197	.0133	0000	.0000	.0000	.0167	•0172	.0173
750.0	.0212	.0235	.0160	0000	.0000	.0000	.0179	•0164	.0186
760.0	.0197	.0228	.0132	0000	.0000	.0000	.0123	•0127	.0128
405.0	•1929	•1930	•1948	•1888	•1937	•1843	•1903	•1984	•1911
436.0	•4819	•4781	•4788	•4821	•4788	•4932	•4650	•4796	•4713
546.0	•2240	•2235	•2251	•2258	•2267	•2311	•2210	•2254	•2214
578.0	•0779	•0775	•0772	•0696	•0685	•0740	•0745	•0751	•0739



RELATIVE SPECTRAL FLUX DISTRIBUTION IN SPHERE-NORMALIZED TO AREA LAMP NUMBER NBS8798

	NB	S INITI	AL	LA	BORATOR	Y 1	N	BS REPE	AT
WAVELENGTH 380.0	RUN 1 3.7	RUN 2 3.7	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7 3.6	RUN 8 3.5	RUN 9 3.9
390•0 400•0	5.9	5.9	8.6	7.9	9.8	8.8	5.7	5.8	5•8 8•3
410.0	10.7	10.7	10.8	10.8	11.2	10.3	10.6	10.6	10.6
420.0	13.0	13.0	13.2	13.5	13.4	13.0	13.1	13.1	13.0
430.0	15.9	15.9	16.0	16.1	16.3	16.7	15.9	15.9	15.7
440.0	20.6	20.6	20.7	21.6	21.2	21.0	20.7	20.7	20.5
460.0	22.3	22.3	22.4	23.2	22.9	22.5	22.5	22.5	22.4
470.0	23.4	23.4	23.6	24.2	23.5	23.7	23.6	23.6	23.4
480.0	23.8	23.8	23.9	24.1	24.1	24.1	24.0	24.0	23.9
490.0	23.8	23•1	23.8	23.7	23.9	23.8	24.0	23.9	23.8
500.0	22.8	22.9	22.9	22.9	23.0	22.9	23.1	23.0	22.9
510.0	22.5	22.5	22.5	22.7	22.6	23.2	22.6	22.6	22.5
520.0	23.6	23.6	23.6	23.9	23.5	23.6	23.7	23.6	23.5
540.0	35.9	35.8	35.9	35.9	36.1	35.2	35.7	35.2	35.1
550.0	46.1	46.0	46.1	46.2	46.1	45.3	45.9	45.4	45.2
560.0	58.6	58.7	58.7	59.3	58.5	58.2	58.7	58.3	58.0
570.0	66.6	66•8	66.8	66.0	65.0	65.5	66.9	66.4	66.1
580•0 590•0	69•2	69•3 65•0	69.4 64.9	65.2	64.1	67.9	65.7	65.2	64.8
				-7 -	=	50 (-7.7		
600.0	56.9	5/+1	5/+1	5/+5	56.8	58.0	5/•/ 47.9	57.5	5/01
620+0	36.9	37.0	36.9	37.9	37.7	38.7	37.6	37.5	37.5
630.0	28.3	28.3	28.4	29.2	29.0	29.3	28.8	28.7	28.8
640.0	21.2	21.3	21.2	21.2	21.8	21.9	18.1	21.9	21.9
650.0	15.6	15.6	15.6	16.0	16.2	16.8	15.9	16.1	16.1
660•0 670 0	11.4	11+4	11.5	8.9	12•7	12+1	8.6	11+7	11.0
680.0	6.3	6.3	6.1	6.7	6.5	7.1	6.3	6.3	6.6
690.0	5.0	5.0	4.8	5.1	5.6	5 <mark>.</mark> 5	5.0	5.0	5.3
700.0	3.6	3.6	3.5	3.7	4.5	4.4	3.6	3.7	4.0
710.0	3.1	3.1	2.9	3.0	3.1	3.5	2.9	3.1	3.2
720.0	2.6	2.4	2.1	2.4	2.7	3.0	2.3	2+3	2.5
740.0	2.1	2.1	2.9	•0	•0	.0	2.0	2.1	2.5
750.0	2.5	2.6	2.2	• 0	• 0	.0	2.2	1.8	2.7
760.0	2.4	2.4	1.6	• 0	• 0	• 0	1.5	1.5	2.2
				ME	ERCURY 1	INES			
405.0	22.7	23.0	23.2	21.8	25.0	23.0	23.2	23.4	22.8
436.0	56.2	56.3	56.6	61.0	58.6	58.0	56.7	57.2	56.6
546.0	27.0	27.0	27.0	27.7	28.1	27.2	27.3	27.1	26.8
5/8+0	9.2	9.2	9.1	9.0	8+9	8.1	9.1	9+1	9.0



INCIZED TO HKEH

<u></u>	NBS INITIAL			LABORATORY 1		Y 1	NBS REPEAT		
wAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8	RUN 9
380•0	.0313	•0305	.0328	•0000	•0000	•0000	•0295	•0293	.0326
390•0	.0490	•0494	.0497	•0511	•0572	•0503	•0468	•0479	.0486
400.0	.0708	.0708	.0714	•0655	•0813	•0729	•0672	•0688	.0692
410.0	.0898	.0886	.0903	•0891	•0929	•0852	•0865	•0877	.0885
420.0	.1091	.1083	.1099	•1117	•1108	•1068	•1070	•1084	.1085
430.0	.1329	.1321	.1331	•1334	•1350	•1376	•1301	•1318	.1309
440.0	.1531	.1524	.1538	•1596	•1577	•1569	•1509	•1525	.1518
450.0	•1719	•1709	•1725	•1791	•1759	•1728	•1897	•1720	•1708
460.0	•1867	•1854	•1864	•1919	•1899	•1853	•1845	•1866	•1865
470.0	•1960	•1945	•1963	•2004	•1952	•1957	•1938	•1957	•1950
480.0	•1992	•1976	•1990	•1996	•1996	•1988	•1969	•1990	•1989
490.0	•1988	•1922	•1984	•1960	•1981	•1964	•1963	•1981	•1982
500.0 510.0 520.0 530.0 540.0 550.0 560.0	 1910 1877 1972 2322 3000 3851 4902 5560 	 1901 1868 1960 2311 2976 3818 4882 550 	.1908 .1874 .1968 .2309 .2993 .3843 .4892	 1897 1878 1977 2359 2974 3825 4911 5471 	.1905 .1871 .1950 .2369 .2992 .3819 .4849	 1884 1912 1944 2309 2906 3736 4799 5307 	 1892 1855 1942 2275 2923 3760 4812 	 1912 1876 1955 2274 2922 3767 4837 	.1909 .1874 .1957 .2284 .2928 .3768 .4833
570.0 580.0 590.0 600.0	•5569 •5780 •5415 •4759	•5350 •5761 •5399 •4744	•5566 •5778 •5404 •4758	•5471 •5634 •5400 •4769	•5390 •5547 •5319 •4708	•5597 •5602 •5414 •4832	•5702 •5381 •4729	•5730 •5406 •4750	•5742 •5747 •5407
610.0	.3956	• 3915	.3924	•3998	.3939	.4006	.3923	•3948	.3973
620.0	.3081	• 3074	.3072	•3138	.3129	.3192	.3082	•3112	.3126
630.0	.2365	• 2349	.2361	•2420	.2407	.2416	.2361	•2378	.2400
640.0	.1774	• 1770	.1766	•1759	.1804	.1809	.1481	•1819	.1828
650.0	.1306	• 1299	.1295	•1325	.1341	.1384	.1302	•1336	.1345
660.0	.0956	• 0948	.0938	•0977	.1055	.0997	.0952	•0971	.0980
670.0	.0718	• 0703	.0703	•0737	.0744	.0740	.0705	•0708	.0730
680.0	.0524	• 0522	.0510	•0551	.0535	.0584	.0520	•0522	.0550
690.0	.0418	• 0415	.0404	•0422	.0468	.0456	.0409	•0412	.0438
700.0	.0304	•0303	.0290	•0309	.0372	.0363	.0295	.0307	.0333
710.0	.0256	•0255	.0240	•0251	.0254	.0288	.0240	.0253	.0270
720.0	.0213	•0196	.0179	•0202	.0226	.0248	.0187	.0188	.0218
730.0	.0265	•0265	.0246	•0000	.0000	.0000	.0158	.0160	.0193
740.0	.0178	•0178	.0156	•0000	.0000	.0000	.0167	.0170	.0208
750.0	.0213	•0213	.0186	•0000	.0000	.0000	.0179	.0152	.0227
760.0	.0198	•0198	.0132	•0000	.0000	.0000	.0123	.0126	.0179
405.0	•1897	•1908	•1931	•1806	.2072	•1897	•1903	•1943	•1903
436.0	•4696	•4681	•4713	•5054	.4856	•4785	•4651	•4743	•4722
546.0	•2255	•2242	•2252	•2298	.2330	•2240	•2236	•2245	•2233
578.0	•0769	•0761	•0761	•0746	.0737	•0721	•0748	•0752	•0751



	NBS INITIAL			LA	BORATOR	Y 5	Ν	BS REPE	AT
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8	RUN 9
380.0	4.0	3.8	4.1	3.7	3.3	3.4	3.8	3.7	3.8
390.0	5.9	6.0	5.9	5.9	5•4	5.5	5.7	5.7	5.9
400.0	8.4	8.4	8.5	9.1	8.9	9.0	8.3	8.3	8.2
410.0	10.7	10.7	10.8	10.8	10.6	10.5	10.7	10.7	10.6
420.0	13+1	13.1	13.2	13.9	13.8	13.8	13.1	13.1	12.9
430.0	16.0	16.1	16.0	16.3	16.2	16.3	15.9	15.8	15.9
440.0	18.6	18.6	18.6	18.8	18•8	18.7	18.4	18.4	18.5
450.0	20.8	20.8	20.9	21.7	21.6	21.6	20.7	19.4	20.9
460.0	22.5	22.6	22.6	23.2	23.0	23.2	22.6	22.6	22.6
470.0	23.6	23.1	23.7	24.3	24.4	24.3	23.6	23.7	23.8
480.0	24.0	24.0	24.0	24.5	24.6	24.6	24.1	24.2	24.0
490.0	23.9	24•0	24.0	24.4	24.4	24.4	24.0	24•1	23.9
500.0	23.0	23.0	23.0	24.1	24.0	24.0	23.1	23.2	23.1
510.0	22.6	22.6	22.7	23.6	23.7	24.2	22.7	22.7	22.6
520.0	23.7	23.7	23.8	24.8	24.9	24.8	23.6	23.9	23.6
530.0	27.8	27.8	28.0	29.4	29.7	29.8	27.6	27.7	27.6
540.0	35.9	36.0	36.0	38.3	38•7	38.6	35.5	35.1	35.4
550.0	46.0	46.1	46.2	49.5	50.4	49.9	45.6	45.7	45.4
560.0	58.6	58.7	58.8	61.8	62.0	61.8	58.3	58.4	58.0
570.0	66.5	66•6	66.8	68.1	66•9	67.4	66•4	66.6	66.3
580.0	68.9	69•1	69.3	68.5	67•6	68.4	69•2	69.4	69.0
590.0	64•6	64•6	65.0	67.2	67•2	67.3	65.4	65.5	65.1
600.0	56.9	56.9	57.1	59.0	59.6	59.5	57.4	57.5	57.3
610.0	47.1	46.9	47.1	47.7	48.5	48.5	47.7	47.9	47.7
620.0	36.9	36.7	36.8	37.6	37.6	37.4	37.5	37.8	37.9
630.0	28.4	28.2	28.4	28.1	28.2	28.0	28.6	28.9	28.9
640.0	21.2	21.1	21.2	20.2	20.7	20.3	21.5	21.6	21.6
650.0	15.5	15.5	15.5	13.5	13.8	13.6	15.9	15.8	15.8
660.0	11.2	11.3	11.2	9.8	9•8	9.8	11.4	11.5	11.6
670.0	8.4	8.3	8.4	5.6	5.7	5.7	8 <mark>•6</mark>	8.6	8.5
680.0	6.2	6.1	5.9	3.1	3.2	3.2	6.2	6.2	6.3
690.0	4.8	4•8	4.6	2.5	2.1	1.8	4.9	4.9	4.9
700.0	3.4	3.5	3.4	2.0	2.0	2.4	3.6	3.6	3.6
710.0	3.1	2.9	2.8	• 0	• 4	.4	3.0	3.1	3.1
720.0	2.4	2.4	2.0	• 0	• 0	• 0	2.4	2.3	2.2
730.0	3.3	3.2	2.8	• 0	• 0	• 0	2.0	1.8	1.8
740.0	2.2	2.2	1.6	• 0	• 0	• 0	2.1	2.1	2.2
750.0	2.6	2.6	2.0	• 0	• 0	• 0	2.5	2.2	2.3
760.0	2.4	2.0	1.6	• 0	• 0	• 0	1.9	1.5	1.6
				ME	RCURY L	INES			
405.0	22.7	22.9	22.9	19.7	18.8	19.6	22.8	22.9	23.2
436.0	56.7	56.9	56.9	55.0	53.0	52.3	56.4	56.7	57.1
546.0	26.4	26.5	26.7	28.0	28.4	28.8	26.5	26.3	26.5
578.0	9.1	9.1	9.1	16.2	18.2	17.1	8.9	8.9	8.9





SPECTRAL	FLUX	DISTRIBUTION	(WATTS)	IN	SPHERE
		LAMP NUMB	ER NBS880	01	

		NBS INITIAL			LABORATORY 5		NBS REPEAT			
W	AVELENGIH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8	RUN 9
	300.0	+0320	0/100	0/17/	•0282	•0250	0260	.0298	.0292	.0307
	390.0		• 0 + 0 0	•0474	•0452	•0412	•0421	•0456	•0453	•0473
	400.0	.0683	.0679	.0690	•0696	.0678	.0690	.0659	• 0664	.0665
	410.0	•086 7	•0859	.0876	.0825	.0805	.0802	.0845	.0852	.0854
	420.0	.1065	•1056	.1068	•1061	•1055	.1054	•1039	•1041	.1043
	430.0	•1301	•1302	.1295	.1248	.1233	•1248	.1264	•1259	.1286
	440.0	•1504	•1503	.1501	•1437	•1431	•1431	•1462	•1465	•1491
	450.0	.1823	+10/0	• 1009	• 1060 1770	•1652	•1653	•1646	•1544	•1682
	470.0	.1915	1912	.1920	•1774	+1/5Z 1960	•1//2 1053	•1/91	+1802	•1823
	480.0	.1945	•1937	.1944	.1874	1876	1878	•10/0	•1009	•1910
	490.0	•1935	•1935	.1939	.1866	•1865	•1868	•1902	•1920	•1932
	500 0	1061	105(1040						
	510.0	.1931	+1800 1920	• 1860	•1843	•1831	•1834	•1831	•1848	•1863
	520.0	.1919	1908	.1922	-1005	•1809	•1850	•1/99	+1810	•1826
	530.0	.2252	.2246	.2261	.2246	•1901	*1099 .2274	+18//	•190Z	• 1901
	540.0	.2909	.2901	.2914	.2926	.2950	.2948	•2109	• 2205 • 279/i	.2857
	550+0	•3730	• 3721	.3736	• 3786	•3843	•3812	• 3623	• 3641	•2007
	560.0	•4748	.4733	•4756	•4721	.4730	•4724	.4625	•4656	•4677
	570.0	•5388	•5375	.5398	•5204	.5107	•5153	•5274	•5311	.5347
	580.0	•5586	•5571	• 5603	•5233	•5159	•5229	•5494	•5531	•5570
	290.0	• 5238	•5215	•5252	•5134	•5131	•5147	•5192	•5220	•5252
	600.0	•4611	•4587	•4616	•4510	.4549	•4544	.4560	• 4584	.4624
	610.0	.3814	•3787	.3809	•3646	•3701	• 3710	.3785	•3817	.3849
	620.0	.2990	•2962	.2979	•2872	·2870	·2862	.2979	•3015	.3061
	630.0	.2304	•2275	.2299	•2145	•2151	•2143	•2273	•2306	•2329
	640.0	•1/1/	•1699	•1713	•1548	•1577	•1549	•1706	•1721	•1744
	660.0	•1257	+1248	•1255	•1034	•1050	+103/	•1260	•1260	•1273
	670.0	.0682	•0917	.0505	•0/49 •0430	0/30	+0/51	•0908 06 7 0	•0920	•0933
	680.0	.0499	•0493	.0478	.0240	.0241	·0433	.0493	•000Z	•0000
	690.0	.0392	.0387	.0369	•0189	.0162	.0135	•0391	•0392	.0391
	700 0	0077	0005							
	710.0	· U 2 7 7	+U280 - 0238	022//	+0152	•0152	+0182	•0285	•0285	•0293
	720.0	.0196	.0193	.0163	•0000	00001	+0000	+0240	• 0251	• 0247
	730.0	.0264	.0261	.0227	•0000	•0000	•0000	•0107	•0187	.0148
	740.0	•0177	•0175	.0133	•0000	.0000	.0000	.0167	•0167	.0174
	750.0	.0212	•0209	.0160	.0000	.0000	•0000	.0199	.0179	.0187
	760.0	•0197	•0162	.0132	•0000	•0000	•0000	.0147	•0123	.0128
					ME	RCURY L	INES			
	405.0	1840	.1844	.1855	.1509	1/136	1/108	1906	1925	1074
	436.0	.4598	•4587	•4603	.4205	.4045	•1498	• 1000	.4521	.4606
	546.0	.2143	•2137	.2159	.2141	.2171	.2202	.2101	.2099	.21.34
	578.0	•0740	.0738	.0737	.1241	.1390	.1303	.0709	.0707	.0717



	NB	S INITI	AL	LA	BORATOR	Y 5	N	BS REPE	AT
WAVELENGTH 380.0 390.0	RUN 1 4.0 5.9	RUN 2 3.9 6.1	RUN 3 4.0 6.0	RUN 4 3.6 5.7	RUN 5 3.4 5.7	RUN 6 3.5 5.8	RUN 7 3.5 5.7	RUN 8 3.6 5.7	RUN 9 3.9 6.0
400.0 410.0 420.0 430.0 440.0 450.0 460.0	8.4 10.7 13.1 16.2 18.7 21.0 22.6 23.7	8.7 10.9 13.2 16.1 18.6 20.9 22.6 23.7	8.7 11.0 13.4 16.2 18.7 21.0 22.8 23.8	9.0 10.9 13.7 16.6 18.8 21.6 23.0	9.0 10.8 13.7 16.4 18.7 21.5 23.3 24.2	9.0 6.0 13.8 16.5 19.0 21.9 23.5 24.2	8.3 10.6 13.1 16.0 18.5 20.9 22.6 23.8	8.3 10.7 13.1 15.9 18.5 19.5 22.8 23.8	8.5 10.8 13.1 16.1 18.6 21.0 22.7 23.8
480•0 490•0	24.0 23.9	24.0 23.3	24.2 24.0	24.7 24.5	24.7 24.3	24.8 24.7	24.2 23.5	24.2 24.1	24.1 24.1
500.0 510.0 520.0 530.0 540.0 550.0 550.0 560.0 570.0 580.0 590.0	23.0 22.6 23.7 27.8 36.0 46.1 58.5 66.4 68.8 64.5	23.0 22.6 23.7 27.9 35.9 46.0 58.6 66.5 68.9 64.6	23.1 22.6 23.7 27.9 36.0 46.2 58.7 66.7 69.2 64.8	23.8 23.3 24.8 29.5 38.3 49.5 61.7 67.4 68.1 67.2	23.8 24.1 25.1 29.7 38.9 50.1 62.1 67.4 67.9 67.4	23.9 24.4 25.0 29.7 39.0 50.2 62.3 67.4 68.2 67.6	23.2 22.8 23.7 35.6 45.8 58.4 66.6 69.3 65.3	23.3 22.8 23.9 27.7 35.0 45.6 58.5 66.7 69.3 65.4	23.1 22.6 23.6 27.6 35.4 45.5 58.0 66.2 68.8 64.9
600.0 610.0 620.0 630.0 640.0 650.0 660.0 670.0 680.0 680.0 690.0	57.1 46.8 36.6 28.2 21.1 15.4 11.3 8.4 6.2 4.9	56.7 47.0 36.8 28.1 21.1 15.5 11.3 8.5 6.2 4.9	56.7 47.0 36.8 28.3 21.1 15.3 11.3 8.3 6.1 4.8	59.3 48.3 37.7 28.4 21.0 14.6 9.9 5.8 3.1 2.8	59.0 48.0 37.4 20.4 13.8 9.7 5.6 3.1 2.1	59.3 48.0 37.8 28.7 20.8 14.5 9.9 5.9 3.1 2.8	57.5 47.6 37.4 28.6 21.5 15.7 11.5 8.4 6.2 4.9	57.6 47.8 37.7 28.7 21.5 15.8 11.5 8.5 6.2 4.9	57.1 47.6 37.8 28.5 21.4 16.2 11.7 8.5 6.2 4.9
700.0 710.0 720.0 730.0 740.0 750.0 760.0	3.7 3.1 2.4 3.2 2.2 2.6 2.4	3.5 3.1 2.4 3.2 2.1 2.6 2.4	3.4 2.8 2.0 2.8 1.6 1.9 1.6	3.1 .8 .4 .0 .0 .0	1.6 .4 .0 .0 .0 .0	2.7 .8 .0 .0 .0 .0	3.5 3.0 2.2 1.8 2.1 2.5 1.5	3.6 2.9 2.1 1.9 2.1 2.4 1.5	3.6 2.9 2.2 1.8 2.1 2.5 1.6
405•0 436•0 546•0 578•0	22.8 56.1 26.6 9.2	22•9 56•3 26•6 9•2	23•2 56•8 26•6 9•2	19.8 52.2 26.9 16.2	20•1 52•8 28•8 17•1	15.2 53.7 28.7 17.4	23.0 56.2 26.6 9.0	23.1 56.8 26.3 9.0	23.2 56.7 26.4 9.0



NORMALIZED TO AREA

	NBS INITIAL			LABORATORY 5		Y 5	NBS REPEAT		
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8	RUN 9
380.0	•0328	•0320	•0328	•0282	•0260	•0269	•0285	•0292	•0320
390.0	•0490	•0505	•0497	•0442	•0441	•0450	•0456	•0462	•0492
400.0	•0696	•0720	•0714	•0705	•0696	•0699	•0666	•0678	•0697
410.0	•0886	•0900	•0903	•0846	•0833	•0468	•0858	•0872	•0891
420.0	•1085	•1098	•1099	•1068	•1055	•1069	•1057	•1067	•1081
430.0 440.0 450.0 460.0	 1334 1541 1731 1867 	•1339 •1545 •1731 •1872	.1331 .1539 .1726 .1871	 1291 1465 1680 1793 	 1262 1445 1659 1797 	 1276 1473 1696 1822 	 1287 1492 1685 1824 	<pre>.1293 .1506 .1588 .1857</pre>	 1322 1531 1728 1867
470.0	•1956	•1963	•1956	•1879	•1866	•1878	•1917	•1939	•1962
480.0	•1984	•1994	•1986	•1921	•1903	•1919	•1949	•1972	•1986
490.0	•1977	•1936	•1973	•1908	•1872	•1911	•1890	•1966	•1981
500.0 510.0 520.0 530.0	•1899 •1867 •1953	•1908 •1875 •1964	.1901 .1859 .1950	•1857 •1812 •1931	•1839 •1860 •1935	•1856 •1894 •1937	•1869 •1834 •1913	•1896 •1856 •1951	•1903 •1861 •1942
540.0	•2968	•2979	•2961	•2983	•3000	• 3023	•2868	•2853	•2916
550.0	•3805	•3815	•3796	•3856	•3861	• 3894	•3688	•3721	•3742
560.0	•4831	•4863	•4826	•4803	•4787	• 4829	•4709	•4769	•4779
570.0 580.0 590.0	•5479 •5684 •5327	•5715 •5360	•5481 •5689 •5328	•5252 •5305 •5233	•5234 •5200	•5283 •5238	•5583 •5265	•5454 •5653 •5329	• 5668 • 5345
600.0	.4711	•4702	•4663	•4617	.4549	•4593	•4631	•4698	.4701
610.0	.3865	•3895	•3860	•3760	.3701	•3724	•3836	•3896	.3917
620.0	.3024	•3053	•3022	•2940	.2884	•2931	•3016	•3070	.3110
630.0	.2325	•2333	•2330	•2214	.2151	•2228	•2306	•2339	.2349
640.0 650.0 660.0 670.0	•1739 •1275 •0934 •0697	•1752 •1289 •0937 •0703	•1751 •1255 •0927 •0682	•1636 •1134 •0768 •0452	•1067 •0750 •0432	•1613 •1120 •0770 •0454	•1735 •1268 •0926 •0679	•1750 •1285 •0938 •0690	•1759 •1332 •0959 •0703
680.0	•0513	•0511	.0500	•0240	.0241	•0241	•0502	•0503	.0514
690.0	•0406	•0404	.0392	•0216	.0162	•0216	•0391	•0401	.0401
700.0	•0304	•0290	.0278	•0243	.0122	•0212	•0285	•0295	.0292
710.0	•0256	•0255	.0226	•0061	•0031	•0061	.0240	•0240	.0236
720.0	•0197	•0196	.0163	•0033	•0000	•0000	.0174	•0174	.0180
730.0	•0265	•0265	.0227	•0000	•0000	•0000	.0144	•0158	.0149
740.0	•0178	•0178	.0133	•0000	•0000	•0000	.0168	•0167	.0173
750•0 760•0	•0213 •0198	•0213 •0198	.0160 .0132	•0000 •0000 ME	•0000 •0000	•0000 •0000	•0199 •0122	•0199 •0123	.0207 .0128
405.0	.1885	•1901	•1906	•1544	•1552	•1176	•1854	•1882	•1912
436.0	.4633	•4667	•4665	•4064	•4071	•4164	•4527	•4627	•4672
546.0	.2195	•2203	•2190	•2097	•2223	•2228	•2140	•2143	•2170
578.0	.0759	•0766	•0752	•1260	•1318	•1349	•0727	•0732	•0737



	NE	S INITI	AL	LA	BORATOR	Y 2	N	IBS REPE	AT
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8	RUN 9
380.0	3.9	3.8	3.8	•0	•0	.0	3.8	3.8	3.7
390.0	5.9	6.0	5.9	6.3	4.7	4.1	5.9	5.7	5.8
400.0	8.7	8.4	8.5	8.3	7.6	7.4	8.5	8.3	8.3
410.0	11.0	10.6	10.7	10.8	10.3	10.4	10.8	10.7	10.7
420.0	13.3	14.0	13.2	13.1	12.9	13.1	13.3	13.1	13.1
430.0	16.0	16.0	16.1	16.0	15.8	16.2	16.1	16.1	16.0
440.0	18.5	18•6	18.6	18.6	18.4	18.9	18.7	18.5	18.5
450.0	20.9	20.8	20.9	20.6	20.5	20.8	21.0	20.9	20.9
400.0	23.8	22.0	22.2	22.4	22.0	22.0	22.1	22.6	22.0
480.0	24.2	24.2	24.1	24.0	23.8	24.1	24.3	23.0	23.0
490.0	24.0	24.0	23.9	23.9	23.8	24.0	24.1	24.1	24.0
500.0	23.1	23.1	23.1	23.2	23.0	23.3	23.2	23.2	23.2
510.0	22.7	22.7	22.7	22.9	22.7	23.0	22.8	22.8	22.7
520.0	23.7	23.8	23.7	24.2	24.0	24.3	23.7	23.7	23.8
530.0	27.9	27.9	27.9	28.4	28.1	28.6	27.7	27.7	27.7
540.0	36.0	36.0	36.0	36.9	36.6	37.1	35.6	35.6	35.5
550.0	46+1	46.2	46.2	47.2	46.7	47.4	45.7	45.7	45.6
570.0	66.5	56+9	66.7	67.0	50.0	59.4 47 4	58+4	58+4	50+3 66 //
580.0	68.9	69.1	69.1	69.3	68.7	69.6	69.1	69.1	69.1
590.0	64.5	64.7	64.8	65.5	64.9	65.6	65.1	65+1	65.1
600.0	56.7	56•9	56.8	57.6	57.2	57.5	57.2	57.2	57.3
610.0	46.8	47.0	46.9	47.8	47.6	47.5	47.4	47.5	47.5
620.0	36.6	36.7	36.8	37.8	37•4	37.6	37.3	37.3	37.2
630.0	28.0	28.3	28.3	28.9	28.7	28.8	28.5	28.4	28.4
640.0	21.0	21.1	20.9	21.7	21.5	21.6	21.4	21.4	21.5
650.0	15+4	15.0	15+5	16.1	15+9	16.0	15.6	15.7	15.6
670.0	8.4	8.2	8.2	8.7	11.0	11/	11+4	11+4	11+4
680.0	6.1	6.0	6.0	6.4	6.3	6.3	6.1	6.3	6.2
690.0	4.8	4.7	4.8	4.9	4.8	4.8	4.8	4.9	5.0
700.0	3.4	3.3	3.4	3.7	3.6	3.6	3.5	3.5	3.6
710.0	3.1	2.7	2.7	2.8	2.8	2.8	2.8	2.9	3.1
720.0	2.4	2.4	2.4	2.1	2.0	2.0	2.2	2.4	2.4
730.0	3.2	3.2	3.2	1.7	1.6	1.7	1.8	1.9	1.9
740.0	2.2	2.1	2.1	1.6	1.4	1.5	1.9	2.3	2.3
750.0	2.0	1.6	2.0	1.4	1.5	1.5	2+2	2.2	2.4
/00+0	2.04	1+0	1.0	•0	•0	•0	1.0	1.0	1.0
				ME	RCURY L	INES			
405.0	22.7	22.7	23.1	24.2	23.8	24.3	23.0	22.9	22.9
436.0	56.5	56.4	56.4	53.4	54.3	53.9	56.4	56.5	56.8
546.0	26.5	26.6	26.9	26.3	25.9	27.0	26.7	26.5	26.5
578.0	9.0	9.1	9.1	9.9	$10 \cdot 0$	10.2	8.8	8.9	8.8



	NBS INITIAL			LABORATORY 2			NBS REPEAT		
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8	RUN 9
380.0	.0320	•0315	.0316	•0000	.0000	•0000	.0311	•0308	•0304
390.0	.0482	•0490	.0489	•0473	.0354	•0308	.0478	•0467	•0476
400.0	.0708	.0691	.0701	.0623	.0565	.0553	.0690	.0673	.0679
410.0	.0895	.0870	.0884	.0813	.0771	.0781	.0882	.0867	.0876
420.0	.1086	.1149	.1088	.0989	.0959	.0982	.1081	.1067	.1072
430.0	.1310	.1317	.1330	.1203	.1181	.1212	.1310	.1305	.1306
440.0	.1515	.1526	.1538	.1398	.1373	.1412	.1520	.1507	.1513
450.0	.1711	.1710	.1721	.1552	.1527	.1558	.1710	.1697	.1707
460.0	.1853	.1861	.1828	.1684	.1659	.1691	.1851	.1839	.1847
470.0	.1944	.1958	.1957	.1770	.1741	.1773	.1945	.1935	.1944
480.0	.1973	.1984	.1987	.1804	.1771	.1804	.1982	.1971	.1980
490.0	.1963	.1968	.1974	.1801	.1771	.1798	.1961	.1960	.1964
500.0 510.0 520.0 530.0 540.0 550.0 560.0 560.0 570.0 580.0 590.0	•1888 •1852 •1940 •2282 •2940 •3766 •4792 •5435 •5629 •5270	 1899 1862 1950 2288 2955 3794 4835 5481 5671 5311 	.1906 .1872 .1957 .2301 .2969 .3811 .4855 .5503 .5699 .5343	 1745 1724 1823 2142 2782 3554 4456 5047 5217 4937 	 1713 1694 1787 2097 2724 3482 4365 4952 5121 4836 	<pre>.1740 .1722 .1815 .2136 .2774 .3544 .4445 .5042 .5042 .5208 .4907</pre>	.1892 .1858 .1935 .2260 .2904 .3727 .4755 .5417 .5633 .5307	 1886 1853 1927 2252 2891 3712 4743 5399 5614 5290 	 1894 1855 1941 2264 2904 3728 4761 5425 5645 5321
600.0	.4635	.4673	.4687	.4342	.4265	.4302	.4664	.4652	.4683
610.0	.3827	.3857	.3871	.3598	.3526	.3556	.3861	.3864	.3879
620.0	.2990	.3011	.3036	.2844	.2788	.2812	.3037	.3030	.3040
630.0	.2289	.2322	.2330	.2177	.2138	.2152	.2319	.2311	.2320
640.0	.1717	.1735	.1723	.1633	.1602	.1613	.1740	.1740	.1754
650.0	.1256	.1282	.1274	.1211	.1184	.1194	.1273	.1275	.1279
660.0	.0907	.0920	.0937	.0889	.0883	.0875	.0927	.0924	.0929
670.0	.0682	.0676	.0680	.0658	.0639	.0644	.0678	.0688	.0691
680.0	.0499	.0494	.0498	.0483	.0467	.0475	.0500	.0511	.0505
690.0	.0392	.0388	.0392	.0369	.0358	.0361	.0395	.0399	.0410
700.0 710.0 720.0 730.0 740.0 750.0 760.0	•0277 •0254 •0196 •0264 •0176 •0212 •0196	.0275 .0224 .0194 .0262 .0176 .0158 .0135	.0277 .0226 .0196 .0265 .0177 .0212 .0132	0275 0213 0159 0128 0123 0105 0000 ME	.0265 .0207 .0151 .0118 .0107 .0099 .0000 RCURY L	.0270 .0207 .0151 .0126 .0112 .0101 .0000	.0289 .0231 .0175 .0145 .0152 .0181 .0124	0285 0240 0198 0157 0183 0178 0147	.0296 .0251 .0199 .0158 .0184 .0199 .0148
405.0	•1854	•1866	•1908	•1826	•1775	•1817	•1876	•1862	•1871
436.0	•4612	•4628	•4655	•4024	•4049	•4027	•4597	•4588	•4639
546.0	•2164	•2182	•2219	•1981	•1931	•2021	•2176	•2157	•2165
578.0	•0737	•0746	•0754	•0749	•0742	•0763	•0720	•0722	•0722



	NB	S INITI	AL	LA	LABORATORY 2 NBS REPEAT				
WAVELENGTH 380.0 390.0	RUN 1 4.0	RUN 2 4.1 6.1	RUN 3 3.9 6.1	RUN 4	RUN 5	RUN 6	RUN 7 3.9	RUN 8 3.8	RUN 9 3.9
400.0	8.8	8.8	8.7	8.0	8.0	7.8	8.5	8.5	8.5
410.0	11.1	11.2	11.0	10.7	10.8	10.8	10.9	10.9	10.9
420.0	13.4	14.3	13.5	13.3	13.3	13.3	13.4	13.3	13.3
430.0	16.3	16•4	16.4	16.3	16.3	16.3	16.3	16.3	16.2
440.0	18.8	18•9	18.9	19.0	18.9	18.9	18.9	18.8	18.8
450.0	21.2	21•6	21.2	21.0	21.1	21.0	21.2	21.1	21.2
460.0	22.9	22•6	22.9	22.8	22.8	22.8	23.0	22.9	22.9
470.0	24.0	24.0	24•1	23.8	23.9	23.8	24•2	24•1	24.1
480.0	24.3	24.3	24•4	24.2	24.3	24.2	24•6	24•5	24.5
490.0	24.3	24.2	24•3	24.2	24.3	24.2	24•4	24•4	24.3
500.0	23.3	23.3	23.4	23.4	23•4	23.4	23.5	23.5	23.4
510.0	22.8	22.8	22.9	23.0	23•1	23.1	23.0	23.0	22.9
520.0	23.8	23.8	23.9	24.2	24•2	24.2	23.8	23.8	23.8
530.0	27.8	27.8	27.8	28.2	27•7	28.4	27.6	27.6	27.6
540.0	35.7	35 • 7	35.7	36.4	36 • 6	36 • 7	35•3	35•2	35.3
550.0	45.7	45 • 7	45.8	46.5	46 • 9	46 • 8	45•2	45•2	45.2
560.0	58.1	58 • 2	58.3	58.3	58 • 5	58 • 8	57•7	57•7	57.7
570.0	65.9	66 • 1	66.2	66.2	66 • 4	66 • 8	65•8	65•8	65.9
580.0	68.4	68 • 6	68.7	68.6	68 • 8	69 • 1	68•6	68•5	68.7
590.0	64.2	64•4	64.5	65.1	65•1	65.4	64•7	64.7	64•9
600.0	56.5	56•6	56.8	57.4	57•4	57.5	57•0	57.0	57•0
610.0	46.8	46•8	46.9	47.6	47•5	47.6	47•2	47.3	47•4
620.0	36.6	36.7	36.8	37.7	37.7	37.7	37.2	37.4	37.3
630.0	28.1	28.1	28.3	28.9	28.9	29.0	28.5	28.4	28.5
640.0	21.4	20.9	21.0	21.7	21.7	21.7	21.4	21.4	21.4
650.0	15.4	15.3	15.5	16.1	16.1	16.1	15.7	15.8	15.8
660•0	11.3	11.2	11.2	11.8	11•9	11.9	11.5	11.5	11.5
670•0	8.5	8.3	8.3	8.7	8•8	8.7	8.5	8.7	8.5
680•0	6.2	6.0	6.0	6.4	6•4	6.4	6.2	6.3	6.3
690•0	4.9	4.8	4.8	4.9	4•9	4.9	4.9	5.0	5.0
700.0	3.6	3.4	3.4	3.7	3.7	3.7	3.6	3.6	3.5
710.0	3.0	2.8	2.8	2.9	2.9	2.8	2.9	2.9	2.9
720.0	2.5	2.3	2.3	2.1	2.1	2.1	2.2	2.4	2.4
730.0	3.4	3.1	3.1	1.7	1.7	1.7	1.9	1.9	1.9
750.0 760.0	2•1 2•2 2•3	1.9	1.9 1.6	1.5 .0 ME	1.5 .0 ERCURY L	1.4 .0	1.9 1.5	2.1 1.7	1.9
405.0	22.6	23.1	23.0	24.3	24.5	23.8	23.3	23.0	23•2
436.0	56.3	56.4	56.4	55.9	54.8	53.6	56.7	56.6	56•6
546.0	26.4	26.6	26.7	26.1	26.2	27.1	26.8	26.6	26•7
578.0	9.0	9.0	9.0	9.9	9.8	10.2	8.9	8.8	8•9



NORMALIZEO TO AREA

	NB	S INITI	AL	LA	BORATOR	Y 2	NBS REPEAT		
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8	RUN 9
380•0	•0340	•0343	.0330	•0000	•0000	•0000	•0325	•0322	•0331
390•0	•0508	•0512	.0511	•0447	•0400	•0350	•0498	•0496	•0505
400.0	.0742	.0745	.0735	.0624	.0623	.0596	.0712	.0710	.0717
410.0	.0931	.0941	.0930	.0838	.0839	.0820	.0912	.0912	.0921
420.0	.1130	.1203	.1134	.1037	.1035	.1013	.1122	.1120	.1124
430.0	.1374	.1380	.1380	.1276	.1267	.1234	.1365	.1366	.1366
440.0	.1583	.1591	.1591	.1484	.1468	.1436	.1584	.1577	.1581
450.0	.1784	.1823	.1785	.1637	.1633	.1595	.1781	.1775	.1783
460.0	.1927	.1905	.1931	.1777	.1766	.1729	.1929	.1927	.1931
490.0 490.0	•2020 •2046 •2042	•2023 •2052 •2043	•2029 •2052 •2044	•1893 •1886	•1833 •1884 •1881	•1840 •1836	•2029 •2062 •2048	•2022 •2061 •2051	•2064 •2048
500.0	.1960	 1962 1926 2009 2347 3007 3852 4907 5573 5783 5428 	.1970	•1826	.1817	.1775	.1970	.1973	.1975
510.0	.1919		.1928	•1797	.1790	.1751	.1927	.1929	.1932
520.0	.2004		.2011	•1888	.1879	.1840	.1993	.2318	.2005
530.0	.2339		.2346	•2202	.2147	.2154	.2315	.2318	.2327
540.0	.3002		.3012	•2844	.2839	.2785	.2959	.2962	.2977
550.0	.3841		.3857	•3630	.3638	.3555	.3790	.3797	.3813
560.0	.4885		.4910	•4555	.4536	.4461	.4836	.4849	.4864
570.0	.5545		.5576	•5171	.5150	.5070	.5517	.5529	.5552
580.0	.5753		.5789	•5356	.5333	.5248	.5746	.5760	.5788
590.0	.5397		.5438	•5082	.5050	.4960	.5427	.5440	.5471
600.0 610.0 620.0 630.0 640.0 650.0 660.0 670.0 680.0 690.0	.4752 .3935 .2366 .1796 .1299 .0950 .0714 .0521 .0415	.4770 .3941 .3096 .2370 .1765 .1288 .0944 .0699 .0507 .0401	.4783 .3952 .3097 .2383 .1774 .1306 .0941 .0702 .0509 .0403	.4479 .3716 .2941 .2255 .1695 .1260 .0925 .0682 .0502 .0386	.4449 .3687 .2922 .2243 .1683 .1250 .0919 .0679 .0496 .0382	.4363 .3612 .2861 .2197 .1650 .1222 .0900 .0662 .0488 .0373	.4780 .3959 .3118 .2386 .1792 .1315 .0962 .0713 .0517 .0413	.4794 .3977 .3145 .2390 .1799 .1325 .0968 .0731 .0528 .0418	.4804 .3993 .3144 .2400 .1805 .1329 .0973 .0717 .0531 .0420
700.0 710.0 720.0 730.0 740.0 750.0 760.0	•0302 •0254 •0212 •0283 •0177 •0185 •0196	.0288 .0239 .0195 .0263 .0154 .0158 .0164	.0289 .0240 .0195 .0264 .0155 .0159 .0132	0292 0227 0166 0135 0126 0118 0000	.0288 .0228 .0166 .0135 .0126 .0118 .0000 RCURY L	.0278 .0215 .0158 .0127 .0121 .0107 .0000	0299 0242 0188 0159 0152 0161 0124	0304 0240 0198 0157 0167 0178 0147	.0296 .0240 .0199 .0158 .0167 .0160 .0123
405.0	•1903	•1943	•1939	•1897	•1899	•1810	•1957	•1936	•1952
436.0	•4733	•4752	•4749	•4366	•4253	•4065	•4749	•4760	•4769
546.0	•2223	•2241	•2246	•2035	•2033	•2057	•2244	•2238	•2255
578.0	•0755	•0762	•0760	•0773	•0761	•0772	•0746	•0740	•0747



	NBS INITIAL			LA	BORATOR	Y 4	N	NBS REPEAT			
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8	RUN 9		
380.0	4.0	3.9	3.9	4.3	4.3	4.3	3.6	3.9	3.9		
390.0	5.9	5.9	6.0	6.5	6.5	6.5	5.8	5.9	6.0		
400.0	8.5	8.6	8.4	8.9	8.9	8.9	8.3	8.3	8.4		
410.0	10.7	10.7	10.6	11.5	11.5	11.5	10.7	10.6	10.8		
420.0	13.1	14.0	13.2	14.4	14.4	14.4	13.2	13.1	13.3		
430.0	16.1	15.9	16.2	17.1	17.1	17.1	16.0	16.0	16.1		
440.0	18.5	18.4	18.7	19.7	19.7	19.7	18.5	18.5	18.6		
450.0	20.8	20.8	20.8	22.3	22.5	22.2	20.9	20.8	20.8		
460.0	22.6	22.6	22.1	24.1	24.1	24.1	22.6	22.6	22.5		
470.0	23.7	23.7	23.7	25.0	25.1	25.0	23.7	23.7	23.7		
480.0	23.9	24.0	24.0	25.2	25.2	25.4	24.1	24.0	24.1		
490.0	24.0	23.9	23.9	24.7	24.8	25.0	24.1	24.0	24.0		
500.0 510.0 520.0 530.0 540.0 550.0	23.1 22.6 23.7 27.8 35.9 46.1 58.7	23.1 22.6 23.7 27.9 35.8 46.0 58.7	23.1 22.6 23.8 27.9 36.0 46.2 58.9	23.8 23.3 24.4 28.6 36.8 48.1 59.3	23.7 23.1 24.4 28.4 36.6 48.0	23.9 23.3 24.4 28.5 36.8 48.2 59.3	23.2 22.7 23.7 27.7 35.6 45.7	23.1 22.7 23.7 27.7 35.5 45.5	23.0 22.6 23.6 27.5 35.4 45.5 58.0		
570.0	66•5	66•6	66 • 8	67.0	66.7	66.7	66.4	66.4	66•1		
580.0	69•0	69•0	69 • 2	70.8	71.4	70.7	69.1	69.1	68•7		
590.0	64•7	64•7	64 • 9	65.2	65.0	65.0	65.1	65.1	64•7		
600.0	57.1	57.0	57.0	56.9	56.7	56.7	57.3	57.3	57.0		
610.0	46.9	47.1	47.1	46.7	46.5	46.6	47.4	47.5	47.3		
620.0	36.7	36.9	36.9	36.8	36.7	36.7	37.3	37.4	37.2		
630.0	28.2	28.3	28.3	28.2	28.1	28.2	28.5	28.6	28.5		
640.0	21.0	21.0	21.0	21.1	20.9	21.0	21.4	21.5	21.3		
650.0	15.5	15.5	15.4	15.6	15.5	15.6	15.8	15.9	15.8		
660.0	11.2	11.3	11.3	11.5	11.4	11.5	11.5	11.6	11.6		
670.0	8.4	8.4	8.4	8.4	8.4	8.5	8.5	8.5	8.6		
680.0	6.2	6.1	6.1	6.1	6.0	6.0	6.2	6.3	6.3		
690.0 710.0 720.0 730.0 740.0 750.0 760.0	4 • 8 3 • 4 2 • 8 2 • 4 3 • 3 2 • 2 2 • 6 2 • 4	4.9 3.5 2.9 2.2 3.0 1.9 2.2 2.1	4.8 3.4 2.8 2.0 3.3 2.2 2.6 1.6	4.9 3.5 2.9 2.0 1.8 1.8 1.6 1.0	4.8 3.5 2.9 1.9 1.6 1.6 1.4 1.3	4.7 3.1 1.9 1.6 1.6 1.4 1.3	4.8 3.5 3.0 2.3 1.9 2.1 2.5 1.8	4.9 3.6 3.1 2.4 2.1 2.3 2.4 1.8	5.0 3.8 3.1 2.4 2.3 2.2 2.9 2.1		
				ME	RCURY L	INES					
405.0	22.8	22.7	22.9	11.6	11.9	11.8	22.8	22.6	22.9		
436.0	56.4	56.4	56.5	50.8	52.5	51.5	57.0	56.8	57.5		
546.0	26.6	26.6	26.5	28.6	28.5	28.5	26.2	26.2	26.1		
578.0	9.3	9.7	9.1	7.4	7.4	7.5	8.9	9.0	8.9		



	NBS INITIAL			LA	BORATOR	Y 4	NBS REPEAT		
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8	RUN 9
380•0	.0327	•0314	•0316	•0396	•0398	•0399	•0298	•0317	•0324
390•0	.0482	•0479	•0489	•0597	•0600	•0599	•0472	•0485	•0490
400.0	.0692	.0699	.0685	.0812	.0821	.0815	.0681	.0680	.0695
410.0	.0872	.0876	.0863	.1052	.1057	.1055	.0874	.0869	.0888
420.0	.1066	.1144	.1067	.1318	.1326	.1321	.1081	.1071	.1093
430.0	.1307	.1295	.1312	.1563	.1569	.1568	.1305	.1306	.1324
440.0	.1506	.1503	.1516	.1804	.1813	.1811	.1513	.1508	.1528
450.0	.1688	.1699	.1691	.2043	.2068	.2034	.1708	.1700	.1715
460.0	.1834	.1843	.1792	.2205	.2220	.2210	.1845	.1842	.1855
470.0	.1925	.1933	.1921	.2291	.2304	.2290	.1938	.1935	.1955
480.0	.1947	.1960	.1945	.2307	.2318	.2329	.1970	.1963	.1955
490.0 500.0 510.0 520.0 530.0 540.0 550.0 560.0 570.0 580.0 590.0	 .1949 .1875 .1841 .1929 .2263 .2918 .3747 .4769 .5408 .5260 	<pre>.1951 .1882 .1845 .1936 .2274 .2924 .3753 .4792 .5439 .5634</pre>	.1940 .1872 .1837 .1928 .2264 .2922 .3750 .4776 .5419 .5615 .5267	.2265 .2181 .2136 .2232 .2617 .3372 .4405 .5431 .6139 .6487 .5971	.2278 .2180 .2127 .2240 .2609 .3369 .4412 .5438 .6134 .6567 .5974	.2290 .2189 .2136 .2237 .2615 .3374 .4420 .5435 .6122 .6482 .5960	.1967 .1894 .1857 .1937 .2259 .2904 .3731 .4760 .5424 .5640	 1957 1886 1850 1931 2259 2898 3719 4751 56418 5638 5311 	 1974 1896 1866 1946 2267 2916 3744 4780 5443 5659 5326
600.0	.4644	•4650	.4628	•5212	.5210	•5201	.4679	.4676	.4694
610.0	.3811	•3844	.3819	•4281	.4279	•4279	.3874	.3881	.3897
620.0	.2983	•3011	.2993	•3373	.3373	•3365	.3048	.3050	.3062
630.0	.2295	•2307	.2298	•2587	.2585	•2589	.2329	.2338	.2348
640.0	.1706	•1718	.1705	•1930	.1926	•1924	.1751	.1756	.1758
650.0	.1263	•1262	.1254	•1427	.1429	•1428	.1292	.1302	.1304
660.0	.0909	•0920	.0915	•1051	.1045	•1052	.0939	.0944	.0954
670.0	.0683	•0687	.0680	•0769	.0770	•0778	.0697	.0697	.0707
680.0	.0501	•0494	.0498	•0559	.0551	•0551	.0509	.0511	.0521
690.0	.0393	•0400	.0392	•0446	.0437	•0427	.0396	.0400	.0410
700.0	.0278	0287	.0277	0324	.0324	.0335	0288	.0295	.0315
710.0	.0227	0238	.0226	0266	.0267	.0280	0242	.0251	.0251
720.0	.0196	0178	.0163	0186	.0171	.0171	0188	.0199	.0199
730.0	.0265	0242	.0265	0163	.0146	.0146	0159	.0172	.0186
740.0	.0178	0154	.0177	0169	.0149	.0149	0169	.0184	.0184
750.0	.0213	0154	.0212	0150	.0125	.0125	0200	.0199	.0239
760.0	.0198	0184	.0132	0089	.0119	.0118	0148	.0147	.0172
405•0	•1851	•1850	•1855	•1061	•1092	•1083	•1860	•1844	•1883
436•0	•4586	•4606	•4588	•4650	•4829	•4725	•4659	•4636	•4737
546•0	•2159	•2173	•2153	•2616	•2625	•2615	•2143	•2140	•2148
5 78•0	•0754	•0792	•0738	•0680	•0682	•0687	•0725	•0731	•0734



RELATIVE SPECTRAL FLUX DISTRIBUTION IN SPHERE-NORMALIZED TO AREA LAMP NUMBER NBS8810

	NB	S INITI	AL	LA	BORATOR	Y 4	NBS REPEAT		
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8	RUN 9
380•0	3.7	3.8	3.8	4.3	4.3	4.3	3.8	3.6	3.7
390•0	5.8	5.9	5.9	6.5	6.5	6.5	5.7	5.8	5.7
400.0 410.0 420.0 430.0 440.0 450.0 460.0 470.0 480.0	8.4 10.7 13.1 16.0 18.4 20.5 22.3 23.5 23.5 23.8	8.5 10.7 13.8 15.9 17.7 19.2 22.3 23.4 23.8	8.4 10.7 13.1 15.9 18.4 20.6 22.4 23.5 23.8 23.7	8.6 11.1 13.8 16.6 19.2 22.1 23.7 24.7 24.7	8.7 7.9 13.8 16.5 19.2 22.3 23.8 24.5 24.5	8.6 7.9 13.8 16.5 19.1 22.3 23.8 24.4 25.0	8.3 10.7 13.2 15.8 18.3 20.7 22.4 23.6 24.0	8.2 10.6 13.0 15.8 18.3 20.6 22.3 23.5 23.9	8.2 10.6 13.1 15.9 18.4 20.6 22.4 23.6 24.0
500.0 510.0 520.0 530.0 540.0 550.0 560.0 570.0 580.0 590.0	22.9 22.5 23.6 27.8 35.9 46.0 58.6 66.6 68.9 64.6	22.9 22.5 23.7 27.8 35.9 46.1 58.9 66.9 69.5 65.1	22.9 22.5 23.6 27.8 35.9 46.2 58.9 66.8 69.4 65.0	23.5 23.0 23.9 28.1 36.1 47.3 58.5 66.2 76.6 65.3	23.4 22.9 23.9 28.1 36.0 47.3 58.4 66.2 78.2 65.3	23.4 22.9 23.9 28.2 36.2 47.4 58.6 66.5 78.3 65.5	23.9 23.0 22.6 23.6 27.6 35.4 45.6 58.3 66.4 69.1 65.2	22.9 22.6 23.5 27.6 35.4 45.6 58.2 66.5 69.2 65.3	22.9 22.5 23.6 27.5 35.5 45.6 58.3 66.4 69.1 65.2
600.0	56.8	57.2	57.1	57.2	57.2	57.3	57.4	57.4	57.3
610.0	47.1	47.3	47.2	47.2	47.1	47.3	47.5	47.6	47.6
620.0	36.9	37.1	36.9	37.2	37.2	37.3	37.4	37.5	37.4
630.0	28.7	28.5	28.4	28.5	28.4	28.5	28.6	28.7	28.6
640.0	21.3	21.3	21.2	21.3	21.3	21.4	21.6	21.6	21.4
650.0	15.6	15.7	15.6	15.9	15.9	15.9	15.9	16.0	15.8
660.0	11.4	11.4	11.3	11.8	11.7	11.7	11.5	11.6	11.4
670.0	8.5	8.6	8.4	8.7	8.6	8.5	8.6	8.6	8.5
680.0	6.4	6.1	6.1	6.4	6.4	6.4	6.4	6.4	6.2
690.0	5.0	4.8	4.8	5.0	5.0	4.9	5.0	5.0	4.9
700.0	3.7	3.5	3.5	3.9	3.9	3.8	3.7	3.6	3.7
710.0	3.2	3.0	2.9	3.1	3.1	3.0	3.1	2.9	3.0
720.0	2.5	2.3	2.1	2.3	2.3	2.3	2.4	2.2	2.2
730.0	3.3	3.2	3.2	1.9	1.7	1.7	2.1	1.9	1.9
740.0	2.3	1.9	1.9	2.0	1.8	1.8	2.0	2.2	2.0
750.0	2.5	2.2	2.2	1.8	1.8	1.8	2.4	2.1	2.2
760.0	2.3	2.0	2.0	1.2	1.3	1.3	1.8	1.8	1.8
405•0	22.6	23.2	23.0	11.1	11.7	11.7	23•2	23.2	23.4
436•0	56.4	56.4	56.6	50.4	52.3	51.3	56•6	57.3	57.7
546•0	26.8	27.0	27.0	28.9	29.0	28.9	26•9	27.1	27.0
578•0	9.2	9.2	9.2	6.0	5.8	5.7	8•9	9.1	9.1



	NBS INITIAL			LA	BORATOR	Y 4	NBS REPEAT		
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8	RUN 9
380.0	•0308	•0312	.0315	•0408	•0408	•0408	•0311	•0304	.0311
390.0	•0481	•0490	.0489	•0616	•0619	•0617	•0472	•0485	.0471
400.0	.0690	•0705	•0702	•0821	•0825	•0819	•0687	•0690	•0684
410.0	.0878	•0891	•0892	•1052	•0756	•0752	•0882	•0885	•0884
420.0	.1080	•1144	•1088	•1313	•1314	•1312	•1089	•1089	•1093
430.0 440.0 450.0 460.0	 1317 1514 1691 1837 	•1318 •1468 •1591 •1850	•1327 •1531 •1718	•1576 •1826 •2102	•1576 •1830 •2127	•1569 •1817 •2113	•1311 •1519 •1715	•1325 •1530 •1725	•1328 •1533 •1718
470.0	•1933	•1945	•1954	•2347	•2332	•2318	•1950	•1968	•1967
480.0	•1960	•1976	•1983	•2355	•2365	•2376	•1984	•1999	•2000
490.0	•1955	•1969	•1976	•2317	•2309	•2301	•1978	•1995	•1983
500.0	•1884	•1898	•1908	•2236	•2226	•2216	•1905	•1919	.1913
510.0	•1856	•1867	•1873	•2185	•2177	•2169	•1870	•1888	.1879
520.0	•1947	•1963	•1965	•2277	•2277	•2267	•1951	•1970	.1963
530.0	•2289	•2508	•2316	•2673	•2678	•2677	•2285	•2307	•2293
540.0	•2954	•2976	•2993	•3436	•3434	•3432	•2933	•2966	•2958
550.0	•3791	•3826	•3845	•4502	•4509	•4499	•3772	•3813	•3805
560.0	•4828	•4881	•4902	•5570	•5566	•5562	•4823	•4874	•4864
570•0	•5482	•5550	•5567	•6302	•6307	•6307	•5501	•5563	•5539
580•0	•5675	•5760	•5776	•7292	•7453	•7428	•5724	•5793	•5763
590•0	•5317	•5402	•5417	•6215	•6217	•6215	•5396	•5462	•5435
600.0	•4675	•4747	•4753	•5440	•5449	•5440	•4748	•4802	•4777
610.0	•3880	•3923	•3933	•4490	•4488	•4487	•3936	•3984	•3965
620.0	•3039	•3076	•3076	•3537	•3544	•3541	•3093	•3135	•3117
630.0	•2364	•2362	•2368	•2712	•2709	•2708	•2366	•2398	•2388
650.0 660.0 670.0 680.0	•1752 •1282 •0940 •0700	•1765 •1298 •0944 •0710	•1765 •1296 •0941 •0702	•2031 •1515 •1118 •0826 •0613	•2033 •1517 •1119 •0819	•2028 •1510 •1111 •0810	•1785 •1315 •0955 •0713	•1808 •1335 •0970 •0723	•1788 •1320 •0954 •0707
690.0 700.0 710.0	•0305 •0305	•0402 •0288	•0403 •0289	•0477 •0370	•0478 •0371	•0468 •0359	•0308	•0305 •0305	•0305 •0305
720.0 730.0 740.0	•0205 •0273 •0193	•0195 •0263 •0154	•0240 •0179 •0264 •0155	•0293 •0217 •0182 •0191	•0293 •0218 •0165 •0170	•0286 •0218 •0165 •0170	•0200 •0173 •0169	•0186 •0157 •0184	•0187 •0158 •0167
760.0	•0190	•0164	.0165	•0119 ME	.0119 RCURY L	•0119	•0148	•0147	.0148
405•0	•1862	•1926	•1915	•1053	•1115	•1108	•1920	•1940	•1951
436•0	•4643	•4680	•4717	•4793	•4979	•4867	•4682	•4794	•4807
546•0	•2208	•2241	•2249	•2752	•2762	•2746	•2231	•2265	•2248
578•0	•0755	•0759	•0766	•0567	•0549	•0542	•0739	•0764	•0762



NBS INITIAL				LA	BORATOR	Y 1	NBS REPEAT				
W.	AVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8	RUN 9	RUN 10
	380.0	5.1	5.0	5.1	5.3	• 0	•0	• 0	4.8	5.0	5.0
	390.0	8•8	8.8	8.8	8.8	7 •7	9.3	10.0	8.5	8.3	8.4
	400.0	14.2	13.5	14.0	13.7	14.8	13.8	13.4	13.2	13.4	13.5
	410.0	18.5	17.9	18.4	17.9	18.7	18.4	17.9	17.8	17.9	17.9
	420.0	23.1	22.6	22.8	22.6	23.5	23.4	23.1	22.5	22.5	22.5
	430.0	28.3	28.2	28.2	28.1	29.3	28.9	28.9	27.9	27.8	27.7
	440.0	32.7	32.6	32.5	32.4	33+1	33.4	33.5	32.4	32.2	32+2
	450.0	36+3	36+2	36.2	30.1	36.5	36.8	36.9	30+2	30.5	30.0
	460.0	30.7	38.3	30.0	30 6	39.0	09.1	39.0	30.0	30.7	30.5
	470.0	39.7	39.4	30.3	30.2	30.0	30.3	39.3	39.5	39.4	30.4
	490.0	38.0	38.0	38.0	37.9	37.5	37.9	36.9	38.2	38.1	38.0
}	500.0	35.6	35.7	35.7	35.7	35.9	35.9	35.7	35.9	35.8	35.7
	510.0	33.3	33.3	33.3	33.4	33.5	33.4	33.3	33.6	33.6	33.4
	520.0	31.6	31.6	31.6	31.7	31.7	32.0	31.5	31.9	31.8	31.6
	530.0	31.8	31.8	31.9	31.9	32.7	32.8	32.5	31.9	31.9	31.7
	540.0	34.7	34.5	34.5	34.6	35.2	35.2	35+1	34.6	34.4	34.3
	550.0	38.8	38.6	38.6	38.7	39.2	39.2	39.1	38•7	38+6	40.5
	560.0	44.5	44.5	44.4	44.6	44.8	44.8	44•7	44.5	44.4	51.0
	570+0	47.9	4/•8	4/•9	48.0	47.02	4/•1	4/+1	48.0	40.0	4/+0
	590.0	48•2	44.8	44.6	44.7	44.4	44.5	44.5	45.0	45.0	44.7
	600.0	38.8	39.1	39.0	39.1	39.1	39.6	39.5	39.5	39.4	39•1
	610.0	32.3	32.6	32.2	32.3	32.4	32.8	33.4	32.8	32.7	32.5
	620.0	25.2	25.5	25.4	27.0	25.6	26.2	26.0	25.9	25.9	25.7
	630.0	19.6	20.0	19.8	19.8	19.9	20.1	20.2	20.1	20.1	19.8
	640.0	14.6	15.0	14.9	15.0	15.4	15.4	15.4	15.2	15.3	15.1
	650.0	10.7	11+1	11.1	$11 \cdot 1$	11.4	11.4	11.6	11•4	11.4	11.2
	660.0	7.7	8.2	8.2	8.3	8.5	8.6	9.0	8.4	8.5	8.3
	670.0	5.8	6.4	6.2	6.1	6.1	7.0	7.3	6.4	6.4	6.2
	680.0	4.1	4.7	4.6	4.7	4.8	5.1	5+1	4.6	4.8	4.0
	690.0	3.4	3.9	3.8	3.6	4.5	4.2	4•2	3.8	2.7	3.8
	700.0	2.5	3.0	2.8	2.9	3.3	3.2	3.2	2.8	2.9	2.8
	710.0	1.9	2.4	2.3	2.4	2.5	2.5	3.0	2.3	2.5	2.3
	720.0	1.5	1.9	1.9	1.9	2.4	2.4	2.4	1.9	2.1	1.8
	730.0	2.1	2.7	2.7	2.7	•0	.0	•0	1.5	1.7	1.4
	740.0	1.0	1.6	1.6	1.6	•0	•0	•0	1.6	1.0	1 4
	750.0	•6	1.9	1.9	1.9	• U	.0	• 0	1.2	1.5	1.2
	100+0	• 4	1.0	1.9	1.0	•0	•0	•0	1.5	1.5	1.42
					ME	ERCURY L	INES				
	405.0	22.8	21.1	21.1	21.2	23.9	22.7	21.1	21.3	21.1	21.2
	436.0	55.2	52.0	52.1	51.7	54.5	52.5	55.5	51.9	51.6	51.8
	546.0	26.9	25.8	25.8	25.7	26.9	26.4	26.9	25.8	25.6	25.1
	578.0	9.2	8.4	8.5	8.5	7.4	7.7	7.8	8.3	8.2	8.5



NORMALIZED TO AREA

	NB	S INITI	AL	LA	BORATOR	Y 1	NBS REPEAT			
WAVELENGTH 380.0 390.0	RUN 1 .0461	RUN 2 •0417	RUN 3 •0431	RUN 4 •0443	RUN 5 •0000	RUN 6 •0000	RUN 7 •0000	RUN 8 •0403	RUN 9 .0421	RUN 10 •0424
400.0	•1277	•1134	•1182	•1146	•1225	•1146	•1117	•1112	•1124	•1144
410.0 420.0 430.0	•2075 •2550	•1900 •2365	•1927 •2379	•1893 •2350	•1944 •2416	•1524 •1941 •2395	•1921 •2401	•1495 •1895 •2343	•1896 •2339	•1915 •2355
440.0 450.0	•2939 •3267	•2733 •3039	.2743 .3056	•2716 •3019	•2733 •3016	•2770 •3054	•2786 •3068	•2721 •3039	•2710 •3041	•2735 •3062
460•0 470•0 480•0	• 3474 • 3572 • 3538	• 3231 • 3330 • 3306	• 3259 • 3353 • 3319	• 3159 • 3319 • 3284	• 3267 • 3335 • 3217	• 324 / • 3323 • 3259	• 3248 • 3325 • 3187	• 3246 • 3340 • 3321	• 3242 • 3342 • 3321	• 3265 • 3359 • 3351
490.0	.3421	•3186	.3211	•3175	• 3094	•3144	• 3069	• 3215	.3210	• 3229
500.0 510.0 520.0	•3207 •2994 •2840	•2995 •2795 •2652	•3016 •2812 •2668	•2988 •2793 •2652	•2968 •2764 •2617	•2978 •2767 •2655	•2971 •2770 •2619	• 3019 • 2822 • 2678	• 2826 • 2675	•2838 •2690
530.0 540.0	•2865 •3118	•2672 •2896	•2691 •2916	•2673 •2894	•2698 •2905	•2720 •2919	•2706 •2918	•2685 •2905	•2684 •2898	•2699 •2915
560.0 570.0	•4004 •4306	•3732 •4015	• 3749 • 4040	•3734 •4020	•3696 •3901	• 3716 • 3910	• 3718 • 3916	•3738 •4037	·3736 ·4037	•4337 •4047
580•0 590•0	•4333 •4022	•4045 •3764	•4066 •3762	•4040 •3738	•3891 •3667	•3903 •3694	•3910 •3701	•4072 •3785	•4074 •3788	•3862 •3800
600.0 610.0	•3492 •2903	• 3282 • 2735	•3291 •2720	• 3273 • 2707	• 3227 • 2672	• 3284 • 2724	• 3289 • 2778	• 3316 • 2756	• 3317 • 2755	• 3329 • 2761
630.0 640.0	•1759 •1310	•2142 •1679 •1263	•2142 •1667 •1260	•2261 •1659 •1254	•1647 •1268	•1665 •1276	•1677 •1283	•1686 •1278	•1692 •1292	•1683 •1284
650.0 660.0 670.0	•0965 •0697 •0518	•0933 •0692 •0534	•0940 •0692	•0931 •0698 •0510	•0938 •0701 •0500	•0949 •0715 •0583	•0966 •0753 •0606	•0955 •0705 •0534	•0963 •0715 •0542	•0956 •0704 •0531
680•0 690•0	•0372 •0303	•0391 •0323	•0386 •0319	•0390 •0300	•0400 •0352	• 0420 • 0352	•0421 •0351	•0390 •0319	•0407 •0327	•0395 •0322
700•0 710•0	•0229 •0171	•0252 •0198	•0236 •0196	•0239 •0198	•0272 •0207	•0262 •0207	•0264 •0250	•0236 •0197	•0246 •0208	•0239 •0198
720•0 730•0 740•0	•0132 •0191	•0163 •0227	•0161 •0224	•0163 •0227	.0198 .0000	•0198 •0000 •0000	•0200 •0000 •0000	•0162 •0129 •0134	•0174 •0144 •0134	•0150 •0116 •0118
750.0 760.0	•0054 •0033	•0159 •0131	.0157 .0163	•0159 •0132	•0000	•0000	•0000 •0000	•0120 •0098	•0159 •0123	•0141 •0099
				ME	ERCURY L	INES				
405•0 436•0 546•0	•2054 •4963 •2417	•1770 •4366 •2163	•1780 •4402 •2181	•1778 •4331 •2154	•1977 •44 <u>9</u> 7 •2223	•1882 •4352 •2193	•1753 •4618 •2241	•1791 •4363 •2172	•1780 •4342 •2159	•1807 •4410 •2138
578.0	.0830	.0703	.0714	•0708	.0610	•0642	•0649	•0700	.0692	•0721


RELATIVE SPECTRAL FLUX DISTRIBUTION IN SPHERE-NORMALIZED TO AREA LAMP NUMBER NBS8908

	NB	S INITI	AL	LABORATORY 5			NBS REPEAT		
WAVELENGTH 380•0 390•0	RUN 1 5.0 8.7	RUN 2 5.2 8.7	RUN 3 4.9 8.8	RUN 4 4.6 8.4	RUN 5 4.9 9.1	RUN 6 5.2 8.7	RUN 7 4.9 8.3	RUN 8 5.1 8.7	
400.0 410.0 420.0 430.0 440.0 450.0 460.0 470.0 480.0 490.0	13.8 18.2 22.5 27.8 32.1 36.0 38.3 39.3 39.0 37.7	13.8 17.9 24.0 27.6 32.0 35.8 38.2 39.5 39.1 37.8	14.8 18.5 23.7 28.5 32.3 36.8 38.8 39.9 39.7 38.3	14.6 18.2 23.6 27.9 32.0 36.7 38.4 40.1 39.7 38.4	15.1 18.6 23.9 28.3 32.3 37.0 39.1 39.9 39.7 38.3	13.8 18.1 22.6 27.9 32.2 35.9 38.2 39.3 39.0 37.8	13.4 17.9 22.7 32.1 36.0 38.3 39.4 39.3 38.0	13.4 17.9 22.6 27.8 32.2 35.8 38.2 39.4 39.2 37.8	
500.0 510.0 520.0 530.0 540.0 550.0 560.0 570.0 580.0 580.0	35.4 33.1 31.4 31.7 34.4 38.6 44.5 47.9 48.2 44.6	35.5 33.1 31.5 31.8 34.5 38.7 44.5 48.0 48.4 48.4	36.6 34.0 33.0 37.4 42.3 47.5 50.0 49.1 47.2	36.8 34.1 33.2 37.0 42.2 47.1 50.1 49.3 47.6	36 • 3 34 • 7 32 • 7 33 • 4 37 • 3 42 • 2 47 • 0 49 • 2 48 • 6 46 • 4	35.5 33.3 31.5 31.8 34.5 38.7 44.6 48.1 48.4 48.4	35.7 33.5 31.7 31.8 34.4 38.6 44.5 48.1 48.5 45.2	35.5 33.3 31.6 31.7 34.3 38.4 44.3 47.8 48.3 48.3 44.9	
600.0 610.0 620.0 630.0 640.0 650.0 660.0 670.0 680.0 680.0 690.0	39.0 32.6 26.0 19.9 15.2 11.2 8.4 6.4 4.7 3.9	39.4 32.6 25.7 19.9 15.1 11.0 8.1 6.3 4.6 3.5	41.7 33.4 25.7 19.6 14.5 9.0 6.2 3.0 1.2 .7	41.6 33.3 26.1 19.7 14.6 9.0 6.4 3.1 1.2 .7	40.4 32.3 24.9 19.0 13.6 8.4 5.5 2.9 1.2 .6	39.2 32.6 25.8 19.9 15.1 11.2 6.2 4.6 3.7	39.6 32.8 26.0 20.0 15.2 11.3 8.4 6.4 4.7 3.7	39.4 32.8 25.9 20.0 15.3 11.4 8.5 6.4 4.8 3.9	
700.0 710.0 720.0 730.0 740.0 750.0 760.0	2.9 2.5 1.9 2.9 1.8 1.9 2.0	2.7 2.3 1.9 2.7 1.6 1.3 1.6	1.2 .4 .0 .0 .0 .0	1.2 .0 .0 .0 .0 .0 .0	•7 •0 •0 •0 •0 •0 •0	2.8 2.4 1.7 2.7 1.6 1.6 1.6	2.9 2.4 1.8 1.6 1.6 1.7 1.2	2.9 2.5 2.1 1.7 1.8 1.9 1.7	
405•0 436•0 546•0 578•0	21.3 52.6 26.2 8.7	21.5 53.0 26.2 8.7	17.7 51.0 26.0 13.4	17.8 51.1 27.0 13.8	19•6 54•3 28•2 14•4	21.6 52.8 26.0 8.6	21.5 52.7 25.9 8.4	21.5 53.1 25.7 8.5	



SPECTRAL FLUX DISTRIBUTION (WATTS) IN SPHERE LAMP NUMBER NBS8908

	NBS INITIAL			LA	BORATOR	Y 5	И	BS REPEAT
WAVELENGTH 380•0 390•0	RUN 1 •0423 •0730	RUN 2 •0441 •0736	RUN 3 •0384 •0688	RUN 4 •0357 •0657	RUN 5 •0405 •0757	RUN 6 •0441 •0734	RUN 7 •0406 •0694	RUN 8 •0433 •0732
400.0 410.0 420.0 430.0 440.0 450.0	•1161 •1529 •1895 •2338 •2701 •3027	 1158 1509 2019 2325 2694 3013 	 1152 1443 1846 2222 2520 2875 	 1137 1419 1835 2168 2488 2855 	 1259 1549 1992 2362 2695 3081 	•1157 •1525 •1898 •2344 •2705 •3020	 1117 1498 1895 2316 2684 3010 	•1133 •1513 •1909 •2350 •2715 •3027
460.0 470.0 480.0 490.0	•3219 •3305 •3280 •3175	•3218 •3322 •3288 •3180	•3028 •3111 •3097 •2988	•2990 •3123 •3091 •2988	•3259 •3325 •3309 •3194	•3210 •3306 •3281 •3175	•3203 •3295 •3281 •3177	•3222 •3327 •3308 •3191
500.0 510.0 520.0 530.0 540.0 550.0 560.0 570.0 580.0	.2978 .2784 .2641 .2670 .2896 .3247 .3741 .4031 .4060 .3756	.2984 .2787 .2649 .2673 .2904 .3255 .3747 .4043 .4073 .3781	.2858 .2656 .2573 .2609 .2919 .3303 .3703 .3703 .3900 .3828 .3682	•2861 •2655 •2583 •2610 •2877 •3280 •3666 •3897 •3838 •3704	.3028 .2896 .2723 .2786 .3112 .3520 .3917 .4105 .4048 .3868	.2985 .2795 .2643 .2673 .2903 .3255 .3751 .4042 .4070	.2985 .2796 .2652 .2659 .2875 .3223 .3717 .4018 .4055	•2999 •2808 •2666 •2674 •2895 •3244 •3740 •4039 •4077 •3795
600.0 610.0 620.0 630.0 640.0 650.0 660.0 670.0 680.0 690.0	• 3756 • 3285 • 2740 • 2192 • 1673 • 1281 • 0940 • 0707 • 0537 • 0394 • 0325	.3781 .3313 .2740 .2159 .1674 .1268 .0922 .0685 .0529 .0387 .0297	.3254 .2604 .2003 .1529 .1130 .0701 .0480 .0237 .0096 .0054	.3704 .3240 .2594 .2030 .1534 .1133 .0701 .0500 .0238 .0096 .0054	.3368 .2696 .2077 .1581 .1132 .0703 .0463 .0238 .0096 .0054	.3768 .3296 .2736 .2168 .1674 .1268 .0943 .0521 .0390 .0311	•3305 •2740 •2171 •1670 •1270 •0948 •0706 •0531 •0394 •0312	•3795 •3324 •2771 •2188 •1693 •1293 •0964 •0716 •0543 •0408 •0328
700.0 710.0 720.0 730.0 740.0 750.0 760.0	.0241 .0213 .0164 .0247 .0156 .0160 .0165	.0225 .0196 .0162 .0224 .0132 .0105 .0135	0091 0031 0000 0000 0000 0000 0000	.0091 .0000 .0000 .0000 .0000 .0000	.0061 .0000 .0000 .0000 .0000 .0000	.0239 .0198 .0147 .0227 .0133 .0133 .0132	.0238 .0198 .0151 .0130 .0135 .0140 .0099	.0246 .0208 .0174 .0143 .0151 .0159 .0148
405•0 436•0 546•0 578•0	•1791 •4423 •2205 •0732	•1809 •4459 •2202 •0733	•1383 •3982 •2025 •1045	•1381 •3976 •2103 •1071	•1633 •4525 •2351 •1203	•1814 •4434 •2187 •0719	•1799 •4401 •2168 •0705	•1819 •4481 •2172 •0716



RELATIVE SPECTRAL FLUX DISTRIBUTION IN SPHERE-NORMALIZED TO AREA LAMP NUMBER NBS8909

	NBS INITIAL			LA	BORATOR	Y 2	NBS REPEAT		
WAVELENGTH 380.0 390.0	RUN 1 5.1 8.8	RUN 2 5.2 8.8	RUN 3 5.2 7.6	RUN 4 .0 9.7	RUN 5 0 8.0	RUN 6 .0 6.2	RUN 7 5.1 8.6	RUN 8 5.1 8.7	RUN 9 5.0 8.5
400.0 410.0 420.0 430.0 440.0 450.0 460.0 470.0	13.9 18.3 22.6 27.9 32.2 36.1 38.3 39.4	13.8 18.0 24.2 27.9 32.3 36.0 38.4 39.6	13.8 18.3 22.7 27.9 32.2 36.0 38.6 39.5	13.8 18.6 22.9 27.9 32.4 35.7 38.0 39.1	13.4 18.4 22.8 27.9 32.3 35.8 38.1 39.2	12.4 18.0 22.7 27.9 32.4 35.8 38.2 39.3	13.4 17.9 22.5 27.8 32.1 35.9 38.4 39.5	13.6 18.2 22.5 27.9 32.2 36.0 38.5 39.7	13.9 18.2 22.6 27.5 30.7 32.8 38.4 39.8
490.0 500.0 510.0	37.8 35.5 33.2	37.8 35.5 33.1	37.9 35.5 33.2	37.8 35.6 33.4	35.6 33.5	39.1 38.1 35.8 33.6	39•4 38•1 35•8 33•4	39.3 38.0 35.8 33.5	35.9 33.5
520.0 530.0 540.0 550.0 560.0 570.0 580.0	32.2 31.7 34.4 38.5 44.3 47.7 48.0	31.5 32.7 34.4 38.2 44.4 47.8 48.0	31.5 31.9 34.7 38.7 44.7 48.0 48.2	32.0 32.3 35.3 39.5 44.9 48.3 48.5	32 • 1 32 • 4 35 • 5 39 • 8 45 • 1 48 • 6 48 • 8	32.3 32.6 35.8 40.1 45.6 49.0 49.2	31.7 31.8 34.4 38.5 44.3 47.9 48.3	31.7 31.7 34.3 38.4 44.1 47.7 48.2	31.8 31.9 34.4 38.5 44.5 48.0 48.5
600.0 610.0 620.0 630.0 640.0 650.0 660.0 670.0 680.0	38.8 32.3 25.4 19.7 15.1 11.1 8.4 6.3 4.7	39.0 32.1 25.3 19.8 14.9 11.1 8.3 6.2 4.5	39.3 32.4 25.6 19.7 15.4 11.2 7.9 6.2 4.6	39.7 33.0 26.2 20.3 15.5 11.6 8.7 6.5 4.9	39.9 33.1 26.4 20.5 15.5 11.7 8.7 6.5 4.8	40.2 33.4 26.6 20.6 15.7 11.7 8.8 6.5 4.8	39.4 32.7 25.8 19.9 15.2 11.4 8.3 6.3 4.8	39.2 32.7 26.1 19.9 15.3 11.4 8.4 6.4 4.8	39.5 32.8 26.0 20.5 15.3 11.5 8.5 6.4 4.9
690.0 710.0 720.0 730.0 740.0 750.0 760.0	3.8 3.0 2.5 1.9 2.9 1.8 1.9 1.9	3.5 2.6 2.3 1.9 2.6 1.5 1.9 1.6	3.8 2.7 2.4 2.0 2.8 1.6 2.0 1.6	3.8 2.2 1.6 1.3 1.1 .9 .0	3.8 2.2 1.6 1.2 1.1 1.0 .0	3.8 2.8 2.1 1.6 1.2 1.1 .8 .0	3.8 2.9 2.5 1.9 1.7 1.8 1.9 1.5	3.8 2.8 2.4 1.8 1.6 1.6 1.7 1.2	4.0 3.0 2.5 2.0 1.7 1.8 1.9 1.5
405•0 436-0	21.3	21.4	21.3	ME 23.4	23.3	22.5	21.6	21.8	21.2
546 • 0 578 • 0	26•0 8•6	26•2 8•7	26.0 8.7	25.2 8.9	25+8 25+5 9+0	26.3 9.0	25.9 8.4	25.7 8.4	26.0 8.4



SPECTRAL FLUX DISTRIBUTION (WATTS) IN SPHERE LAMP NUMBER NBS8909

	NBS INITIAL			LA	BORATOR	Y 2	NBS REPEAT		
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8	RUN 9
380.0	.0438	•0441	•0438	•0000	.0000	•0000	•0430	•0436	.0425
390.0	.0753	•0747	•0643	•0771	.0632	•0482	•0726	•0738	.0719
400.0 410.0 420.0 430.0 440.0 450.0 460.0 470.0 480.0 490.0	 1190 1564 1937 2388 2758 3089 3276 3371 3340 3234 	 1178 1539 2062 2379 2753 3069 3272 3376 3343 3224 	.1177 .1556 .1929 .2373 .2737 .3065 .3282 .3360 .3328 .3225	<pre>.1101 .1479 .1821 .2221 .2576 .2843 .3028 .3111 .3097 .3005</pre>	 1056 1453 1804 2207 2553 2826 3015 3096 3080 2993 	.0959 .1388 .1752 .2154 .2507 .2771 .2956 .3040 .3023 .2942	 1133 1511 1896 2345 2710 3034 3238 3334 3326 3221 	 1163 1549 1918 2376 2747 3075 3285 3389 3355 3245 	 1172 1535 1909 2318 2588 2769 3245 3358 3331 3226
500.0	.3033	.3028	.3026	•2833	.2816	•2767	.3019	.3055	3028
510.0	.2843	.2821	.2828	•2660	.2645	•2602	.2822	.2856	2832
520.0	.2753	.2685	.2685	•2549	.2537	•2494	.2677	.2705	2681
530.0	.2711	.2791	.2712	•2569	.2560	•2524	.2686	.2705	2690
540.0	.2944	.2935	.2952	•2806	.2806	•2766	.2903	.2929	2902
550.0	.3297	.3256	.3294	•3141	.3143	•3099	.3248	.3273	3247
560.0	.3790	.3782	.3803	•3571	.3566	•3522	.3738	.3760	3753
570.0	.4078	.4072	.4088	•3844	.3840	•3787	.4041	.4071	4053
580.0	.4107	.4093	.4105	•3863	.3858	•3803	.4079	.4110	4092
590.0	.3805	.3792	.3805	•3606	.3596	•3546	.3791	.3820	3806
600.0	•3315	•3325	.3342	•3161	.3154	•3107	•3330	•3342	.3337
610.0	•2759	•2740	.2759	•2625	.2618	•2579	•2758	•2793	.2770
620.0	•2170	•2159	.2177	•2089	.2086	•2056	•2182	•2224	.2193
630.0	•1681	•1690	.1681	•1618	.1617	•1590	•1679	•1697	.1728
640.0	•1290	•1268	.1314	•1231	.1227	•1211	•1283	•1304	.1296
650.0	•0950	•0943	.0953	•0926	.0922	•0908	•0962	•0973	.0972
660.0	•0717	•0707	.0676	•0693	.0690	•0677	•0705	•0718	.0716
670.0	•0537	•0529	.0524	•0520	.0515	•0506	•0534	•0545	.0543
680.0	•0405	•0387	.0392	•0389	.0383	•0375	•0407	•0408	.0415
690.0	•0325	•0297	.0326	•0302	.0298	•0291	•0318	•0327	.0334
700 • 0	.0254	.0225	.0232	.0225	.0220	.0215	.0246	.0243	.0251
710 • 0	.0213	.0196	.0204	.0176	.0174	.0163	.0207	.0203	.0212
720 • 0	.0164	.0162	.0169	.0130	.0125	.0121	.0161	.0154	.0166
730 • 0	.0247	.0224	.0236	.0102	.0095	.0094	.0143	.0134	.0148
740 • 0	.0156	.0132	.0139	.0090	.0087	.0084	.0150	.0139	.0155
750 • 0	.0160	.0158	.0169	.0073	.0078	.0064	.0159	.0145	.0164
760 • 0	.0165	.0135	.0137	.0000	.0000	.0000	.0123	.0103	.0127
405.0	•1818	•1827	•1817	•1862	•1840	•1738	•1822	•1856	•1793
436.0	•4541	•4524	•4506	•4174	•4093	•3938	•4467	•4539	•4524
546.0	•2219	•2235	•2216	•2006	•2017	•2031	•2185	•2194	•2194
578.0	•0736	•0744	•0740	•0710	•0710	•0694	•0712	•0716	•0707



RELATIVE SPECTRAL FLUX DISTRIBUTION IN SPHERE-NORMALIZED TO AREA LAMP NUMBER NBS8911

	NBS INITIAL			LABORATORY 4			NBS REPEAT		
WAVELENGTH 380•0 390•0	RUN 1 5•2 8•7	RUN 2 5.1 8.6	RUN 3 5.2 8.7	RUN 4 5.6 9.0	RUN 5 5.6 9.0	RUN 6 5.6 9.0	RUN 7 4.9 8.4	RUN 8 5.0 8.3	RUN 9 5.0 8.5
400.0 410.0 420.0 430.0 440.0 450.0 460.0 470.0 480.0	14.0 18.3 22.7 28.0 32.2 36.0 38.4 39.4 39.1 37.8	13.9 18.3 23.9 27.8 32.0 36.5 38.2 39.4 39.1 37.9	14.0 18.4 22.8 28.1 32.4 36.2 38.6 39.6 39.2 38.0	13.1 18.0 23.4 29.2 33.9 38.3 40.4 41.2 40.5 38.7	13.2 18.0 23.3 29.1 34.0 38.4 40.5 41.2 40.4 38.7	13.2 18.1 23.4 34.1 38.3 40.5 41.6 40.6 38.8	13.4 18.0 22.6 32.3 33.6 38.7 39.8 39.6 38.3	13.4 18.0 22.5 27.6 32.1 35.9 38.4 39.5 39.4 38.1	13.6 18.0 22.7 28.0 32.3 36.1 38.6 39.7 39.4 38.1
500.0 510.0 520.0 530.0 540.0 550.0 560.0 570.0 580.0 590.0	35.5 33.1 31.4 31.7 34.3 38.4 44.3 47.6 47.9 44.4	35.6 33.2 31.5 31.7 34.4 38.5 44.3 47.7 48.1 44.6	35.7 33.2 31.6 31.8 34.5 38.7 44.5 47.9 48.2 44.6	36.2 33.7 31.9 32.0 34.6 39.2 44.2 47.3 57.4 44.4	36.0 33.5 31.8 31.8 34.4 39.1 44.0 47.0 58.4 44.2	36.0 33.5 31.9 31.8 34.4 39.2 44.2 47.3 57.8 44.3	36.0 33.6 32.2 32.0 34.1 38.7 44.5 48.1 48.5 45.2	35.7 33.4 31.7 31.7 34.3 38.4 44.1 47.7 48.1 45.5	35.9 33.5 31.7 31.8 34.3 38.4 44.2 47.7 48.2 45.0
600.0 610.0 620.0 630.0 640.0 650.0 660.0 670.0 680.0 680.0 690.0	38.8 32.2 25.5 19.7 15.0 11.2 8.2 6.3 4.6 3.9	39.1 32.7 25.4 19.8 14.9 11.1 8.1 6.2 4.6 3.8	39.1 32.3 25.4 19.8 14.8 10.9 8.0 6.2 4.6 3.7	38.6 31.9 25.2 19.5 14.8 11.1 8.3 6.3 4.8 3.8	38.4 31.7 25.1 19.4 14.7 11.0 8.2 6.2 4.8 3.7	38.6 31.8 25.2 19.5 14.8 11.1 8.2 6.1 4.7 3.6	39.5 32.9 26.1 20.0 15.2 11.4 8.3 6.4 4.6 3.8	39.2 32.6 26.0 20.1 15.4 11.4 8.5 6.5 4.9 4.0	39.1 32.6 25.9 19.8 15.2 11.3 6.3 4.7 3.8
700.0 710.0 720.0 730.0 740.0 750.0 760.0	2.9 2.4 2.8 1.8 1.8 1.9	2.8 2.3 1.9 2.7 1.6 1.9 1.5	2.8 2.3 1.7 2.7 1.6 1.6 1.5	2.9 2.3 1.7 1.5 1.5 1.5 1.2	2.9 2.3 1.7 1.5 1.5 1.5 1.2	2.8 2.3 1.7 1.3 1.3 1.3 1.2	2.8 2.3 1.8 1.4 1.4 1.4 1.4	3.0 2.6 1.9 1.7 1.8 1.9 1.5	2.8 2.5 1.8 1.5 1.6 1.7 1.2
405•0 436•0 546•0 578•0	21.6 53.7 26.2 8.8	21.5 52.7 26.0 8.7	21.6 53.1 26.0 8.6	10.1 45.0 28.8 6.9	10.3 46.5 28.8 6.8	10.3 45.6 28.8 6.9	21.8 53.1 25.8 8.5	21.4 52.8 25.6 8.3	21.8 53.2 25.8 8.3



SPECTRAL FLUX DISTRIBUTION (WATTS) IN SPHERE LAMP NUMBER NBS8911

	NBS INITIAL			LA	LABORATORY 4			NBS REPEAT		
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8	RUN 9	
380.0	•0450	•0438	.0441	•0550	•0552	.0552	•0413	•0425	.0427	
390.0	.0757	•0736	•0746	•0884	•0889	•0885	•0708	•0702	•0720	
400.0	.1217	•1186	•1190	•1285	.1299	.1293	.1128	•1141	•1151	
410.0	•1590	•1558	•1566	•1761	.1773	•1771	•1514	•1532	•1529	
420+0	• 1972	•2034	• 1944	•2290	.2296	•2291	•1900	• 1911	.1929	
430.0	.2796	.2728	.2760	•2000 •3323	.3345	• 2884	02342	·2349	• 2373 2742	
450.0	.3121	.3111	.3084	.3761	• 3786	• 3761	.2830	.3047	.3066	
460.0	.3329	.3256	.3287	• 3964	.3993	.3974	.3259	•3266	.3273	
470.0	.3420	• 3356	.3374	•4040	.4062	.4076	.3352	•3360	.3367	
480.0	•3390	•3330	.3343	• 3972	.3978	• 3978	• 3332	•3351	.3347	
490.0	.3280	• 3223	• 3236	• 3798	.3809	•3803	• 3223	•3236	.3235	
500.0	.3077	• 3032	.3040	• 3552	• 3547	• 3530	.3027	•3036	.3045	
510.0	•2869	•2830	.2830	•3301	•3297	•3284	•2829	•2840	•2843	
520.0	27/20	•2684	• 2089 2710	• 3127	• 31 34	• 31 31	•2709	• 2696	•2690	
540.0	.2978	• 2926	.2942	.3380	+3131	.3373	.2868	.2097	. 2013	
550.0	•3335	.3278	.3296	•3846	.3851	.3849	.3254	.3259	.3259	
560.0	•3839	• 3776	.3795	•4335	.4339	•4337	• 3748	.3749	•3751	
570.0	.4127	•4066	.4084	•4643	.4642	.4638	.4045	•4052	.4052	
580.0	•4152	•4095	.4108	•5629	•5754	.5673	•4083	•4087	.4090	
590.0	•3848	• 3799	•3800	•4355	•4350	•4344	• 3799	• 3864	•3815	
600.0	•3365	• 3332	•3331	•3785	•3786	•3785	• 3323	•3331	.3321	
610.0	•2792	•2784	.2755	•3126	•3119	•3120	.2765	•2769	.2767	
620.0	•2213	•2166	•2161	•2474	.2472	.2471	.2195	•2213	.2198	
630.0	.1710	•1688	•1690	•1909	•1911	• 1911	•1685	•1711	•1684	
640.0	• 1299	•12/1	•1259	•1448	•1449	•1449	•1278	•1308	•1291	
660.0	0713	•0947	0932	•1090	0011	•1085	0963	0722	0937	
670.0	.0544	•0531	.0532	•0616	•0611	•0604	•0033	•0722	.0536	
680.0	.0402	0389	.0390	.0469	.0470	.0461	.0391	.0417	.0401	
690.0	.0335	.0322	.0311	.0376	.0367	.0356	.0319	.0339	.0321	
700.0	.0252	.0238	.0239	•0289	.0290	•0278	•0236	•0258	•0238	
710.0	•0212	•0197	.0198	.0227	.0227	•0227	•0197	•0220	.0210	
720.0	.0179	.0162	.0146	•0171	.0171	•0171	.0150	•0164	.0151	
730.0	•0245	•0226	•0227	•0146	.0146	•0128	.0115	•0145	•0131	
740+0	•0155	•0133	•0133	•0149	+0149	•0128	•0117	• 0153	•0136	
750.0	0159	+0139	0172	+0150	0110	+0120	•0120	•0103	• 0142	
/00+0	*0104	+0131	.0152	•0119	+0119	+0119	•0099	+0120	•0101	
				ME	RCURY L	INES				
405.0	.1877	•1834	.1843	.0986	.1015	.1006	•1833	•1815	.1851	
436.0	.4657	•4491	.4524	.4414	•4584	.4475	•4467	.4483	•4511	
546.0	•2276	•2216	.2217	.2823	.2833	•2824	•2167	•2179	.2193	
578.0	•0766	•0743	.0733	•0675	•0667	•0673	•0713	•0709	.0706	



RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION (25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8795

		NBS		LABORA	TORY 7	
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6
380.0	3.9	3.7	4.0	2.9	12.9	1.9
390.0	6.0	5.8	5.9	3.4	3.9	2.9
400.0 410.0 420.0 430.0 440.0 450.0	8.2 10.7 13.3 16.3 18.9 21.0 22.8	8.0 10.5 13.0 15.8 18.5 20.9	8.1 10.5 13.2 16.0 18.5 21.0 22.7	4.7 6.4 8.9 11.3 14.0 16.6 18.3	5.0 6.6 9.0 11.4 14.1 15.4	4.2 5.9 8.4 10.5 13.6 15.4
480.0 470.0 480.0 490.0	24.0 24.3 24.3	23.9 24.4 24.1	23.8 24.2 24.2	20.3 20.2 20.6	19.2 20.8 20.4	19.7 20.9 21.5
500.0	23.3	23.3	23.2	20.9	20.6	21.0
510.0	22.8	22.6	22.6	20.7	20.1	20.8
520.0	23.7	23.6	23.7	21.3	20.9	21.8
530.0	27.6	27.3	27.5	24.4	24.0	24.6
540.0	35.3	35.0	35.2	31.4	31.1	32.0
550.0	45.3	44.9	45.1	40.7	40.4	41.3
560.0	57.9	57.6	57.6	52.5	52.5	53.8
570.0	65.9	65.7	65.7	59.6	60.2	61.5
580.0	68.6	68.5	68.4	62.1	63.0	64.0
590.0	64.3	64.3	64.3	58.6	60.9	61.2
600.0	56.4	57.2	56.6	52.9	53.3	54.6
610.0	46.8	47.6	47.0	44.0	45.7	45.0
620.0	36.7	37.5	36.7	35.1	36.3	36.5
630.0	28.6	29.4	28.5	28.8	29.3	30.1
640.0	21.1	21.5	21.2	21.5	22.7	22.1
650.0	15.4	15.6	15.6	16.9	18.2	17.8
660.0	11.3	11.4	11.4	13.5	14.0	14.0
670.0	8.5	8.8	8.5	12.0	12.0	11.6
680.0	6.2	6.4	6.3	10.8	8.1	10.1
690.0	4.8	4.8	5.1	10.9	10.3	9.9
700.0	3.5	3.7	3.8	11.2	10.6	9.8
710.0	2.9	3.2	3.3	12.5	11.9	11.2
720.0	2.5	2.6	2.9	14.5	13.3	13.2
730.0	4.8	5.1	5.6	17.3	16.7	15.9
740.0	2.0	2.1	2.5	20.4	20.1	19.7
750.0	2.1	2.0	2.5	25.1	23.2	22.4
760.0	2.1	2.0	2.9	28.4	26.5	24.5
405.0	22•5	21•5	21.9	5.9	6.9	6.2
436.0	58•5	58•6	58.0	28.7	29.7	28.6
546.0	25•9	25•9	25.6	25.0	24.6	26.3
578.0	8•8	8•8	8.9	24.7	25.0	25.8



RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION (25CM SECTION) -NORMALIZED TO AREA LAMP NUMBER NBS8796

		NBS		LABORA	TORY 7	
₩AVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6
380•0	3.5	3.4	3.6	2.2	12.6	1.7
390•0	5.5	5.3	5.4	2.8	3.8	2.6
400.0	7.6	7.4	7.5	4.1	5.0	3.9
410.0	10.0	9.7	9.9	5.9	6.7	5.5
420.0	12.5	12.3	12.4	8.3	8.7	7.7
430.0	15.4	15.1	15.0	10.6	10.6	9.5
440.0	17.9	17.6	17.5	13.1	13.1	12.3
450.0	20.0	19.8	19.8	15.4	14.4	14.0
460.0	21.8	21.6	21.5	17.3	16.7	16.4
470.0	23.0	22.8	22.8	19.2	18.0	17.8
480.0	23.5	23.4	23.2	19.2	19.5	19.6
490.0 510.0 520.0 530.0 540.0 550.0 560.0 570.0 580.0 580.0 590.0	22.7 22.3 23.3 27.5 35.5 45.9 58.9 67.2 70.1 66.1	23.3 22.5 22.1 23.1 27.1 35.2 45.5 58.4 67.0 70.2 66.5	22.4 22.0 23.2 27.2 35.3 45.5 58.5 58.5 66.9 69.8 65.8	20.5 20.4 21.0 24.3 30.5 40.0 52.8 61.2 64.8 61.8	19.5 19.9 21.0 24.5 32.0 41.7 54.1 61.9 64.5 62.0	20.2 20.0 19.7 20.7 23.9 32.0 41.5 53.9 61.7 65.6 65.6
600.0	58.4	58.6	58.1	53.7	54.5	54.4
610.0	48.6	48.4	48.3	45.3	47.0	46.3
620.0	37.8	38.4	37.8	37.5	37.9	37.6
630.0	29.4	29.7	29.7	30.7	29.8	29.8
640.0	21.7	22.2	21.9	24.0	24.5	23.0
650.0	16.0	16.5	16.2	18.3	18.4	17.8
660.0	11.7	12.0	11.8	14.9	14.4	14.8
670.0	8.6	8.9	9.1	12.1	11.9	12.2
680.0	6.3	6.3	6.5	10.5	10.4	10.2
690.0	5.0	5.1	5.3	10.4	10.1	10.0
700.0 710.0 720.0 730.0 740.0 750.0 760.0	3.7 3.1 2.4 4.6 1.8 1.7 2.1	4 • 1 3 • 2 2 • 7 4 • 9 2 • 4 2 • 4 2 • 4 2 • 3	4 • 1 3 • 5 3 • 0 5 • 3 2 • 8 2 • 8 2 • 8	10.5 11.6 13.2 15.4 18.3 22.6 25.7	10.0 11.1 12.4 15.5 19.0 21.8 25.2	9.4 10.9 25.1 14.9 18.2 20.8 23.2
405.0	21.7	20•8	21.1	5.8	6.5	5.9
436.0	56.2	56•7	56.4	29.0	28.8	27.6
546.0	26.1	25•9	25.8	27.1	25.3	26.8
578.0	9.2	9•0	9.0	26.4	24.9	25.4



RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION (25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8797

	_	NBS		LABORA	TORY 1	
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6
380•0	3.5	3.5	3.8	.0	.0	.0
390•0	5.7	5.6	5.8	5.4	5.5	5.9
400.0	8.0	7.9	7.9	7.5	7.5	7.7
410.0	10.5	10.3	10.3	10.0	10.1	10.1
420.0	13.0	12.8	12.9	12.7	12.8	12.7
430.0	15.8	15.5	15.7	15.6	15.6	15.5
440.0	18.3	18.1	18.1	18.2	18.3	18.2
450.0	20.5	20.3	20.5	20.5	20.6	20.4
460.0	22.3	22.1	22.3	22.4	22.5	22.3
470.0	23.5	23.3	23.3	23.6	23.8	23.5
480.0	23.9	23.8	23.7	24.0	24.2	23.9
490.0	23.9	23.6	23.7	23.7	23.9	23.8
500.0	23.0	22.8	22.8	22.6	22.8	23.2
510.0	22.5	22.3	22.3	22.3	22.4	22.8
520.0	23.3	23.3	23.3	23.4	23.5	23.9
530.0	27.4	27.1	27.3	27.9	27.9	28.3
540.0	35.4	35.1	35.2	35.4	35.4	35.7
550.0	45.6	45.1	45.3	46.0	46.1	46.2
560.0	58.4	57.7	58.1	59.7	59.9	59.7
570.0	66.6	65.7	66.3	67.8	68.2	67.6
580.0	69.5	68.6	69.0	70.5	70.9	70.1
590.0	65.3	65.0	65.0	67.7	68.0	67.2
$600 \cdot 0$	57.3	57.2	57.0	59.5	59.5	58.8
$610 \cdot 0$	47.5	47.3	47.3	49.1	49.2	48.6
$620 \cdot 0$	37.1	37.6	37.1	39.7	39.6	39.2
$630 \cdot 0$	28.6	29.7	29.0	29.9	29.9	29.5
$640 \cdot 0$	21.2	21.4	21.5	21.8	21.8	21.7
$650 \cdot 0$	15.4	15.8	15.5	16.2	16.1	16.2
$660 \cdot 0$	11.4	11.7	11.5	11.9	11.8	12.1
$670 \cdot 0$	8.5	8.6	8.7	8.7	8.5	8.9
$680 \cdot 0$	6.1	6.1	6.3	6.5	6.3	6.8
$690 \cdot 0$	4.7	4.9	4.9	5.0	4.8	5.3
700.0 710.0 720.0 730.0 740.0 750.0 760.0	3.5 2.8 2.4 4.6 1.6 1.9 1.5	3.8 3.1 2.4 4.9 2.1 2.1 2.0	4.0 3.4 2.8 5.2 2.2 2.6 2.0 MERCURY	3.8 2.9 2.3 .0 .0 .0 .0 LINES	3.6 2.8 2.0 .0 .0 .0	4.1 3.2 2.6 .0 .0 .0
405•0	22.5	22.5	21.0	24.1	21•1	21.1
436•0	60.5	61.6	61.0	54.4	54•4	55.7
546•0	25.7	26.1	25.8	28.1	28•4	28.4
578•0	9.3	9.7	9.0	9.5	10•3	9.1



RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION (25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8798

		MRC		LABODA	TODY 1	· · · · · ·
		NBS		LABORA	TORT I	
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6
380.0	3.5	3.5	3.7	.0	.0	.0
390.0	5 • 7	2+2	2.8	5.8	5•/	5.8
400.0	7.9	7.6	7.8	7.8	7.7	7.6
410.0	10.4	10.0	10.2	10.1	10.1	9.9
420.0	13.0	12.6	12.9	12.7	12.7	12.5
430+0	18.5	15+4	15.7	15+5	15+5	15.3
450.0	20.6	20.4	18.6	20.4	20.4	20.4
460.0	22.4	22.2	22.4	22.2	22.2	22.2
470.0	23.7	23.3	23.4	23.4	23.6	23.4
480.0	23.9	23.8	23.9	23.8	23.8	23.9
49000	2349	23.1	2349	2017	2300	23.0
500+0	22.9	22.8	22.9	23.1	23.1	23.1
510.0	22.6	22.5	22.5	22.7	22.6	22.7
520.0	23.6	23+4	23.6	23.9	23+7	23.9
540.0	35.8	35.4	35.9	35.9	35.7	35.8
550.0	46.1	45.5	46.1	46.4	46.2	46.3
560.0	58.9	58.0	58.9	60.1	59.7	59.9
570+0	66+9	66+5	6/•1	68.0 70 F	6/•7	68.0
590.0	64.9	65+5	65.3	67.6	67.6	67.7
600.0	57.0	57.3	57.2	59.1	59+4	59.2
620.0	36.7	38.2	47.4	49.0	49+1 39-8	40.9
630.0	28.4	30.2	29.0	29.9	29.9	29.8
640.0	21.0	21.7	21.4	21.9	22.0	21.9
650.0	15.5	15.9	16.0	16.5	16.5	16.4
670.0	11+5	11+9	11.5	12.2	12+2	12.1
680.0	6.4	6.3	6.5	6.8	6.8	6.7
690.0	4.7	5.0	4.9	5.3	5.3	5.2
700.0	3.5	3.8	2.2	4.1	4.1	4.0
710.0	2.8	3.2	3.5	3.3	3.3	3.2
720.0	2.4	• 3	2.8	2.6	2.6	2.5
730.0	4.6	4.8	5.6	•0	• 0	•0
740.0	1.0	2.2	2.8	• 0	•0	.0
760.0	1.5	2.6	3.1	•0	•0	.0
			MERCHINY			
			MERCURY	LINES		
405.0	22.7	21.9	22.1	20.4	20.8	21.5
436.0	58.5	58.9	58.1	52.5	53.4	54.3
546+0	26+2	25+9	25.6	27.6	2/.7	27.9
510+0	202	0	0.7	1002	TOAT	0.9



RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION (25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8799

							and the second	
		NBS		LABORA	TORY 9			
₩AVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6	RUN 7	RUN 8
380•0	3.6	3.7	3.8	3.7	3.7	3.7	3.7	3.6
390•0	5.8	5.9	5.9	6.5	6.6	5.8	5.8	5.6
400.0	7.9	8.1	7.9	7.8	7.8	7.9	7.9	7.8
410.0	10.5	10.6	10.4	10.5	10.4	10.5	10.4	10.3
420.0	13.1	13.1	13.1	13.0	13.0	13.1	13.0	13.1
430.0	16.2	15.8	16.1	15.8	15.8	15.8	15.9	15.9
440.0	18.8	18.5	18.6	18.5	18.5	18.6	18.6	18.5
450.0	21.0	21.0	20.9	20.9	20.8	20.8	20.9	20.9
460.0	22.7	22.9	22.7	22.8	22.5	22.7	22.8	22.7
470.0	23.9	24.0	23.7	23.9	23.8	23.7	23.7	23.9
480.0	24.2	24.6	24.0	24.4	24.1	24.2	24.2	24.2
490.0	24.2	24.3	24.1	24.2	24.1	24.1	24.2	24.3
500.0 510.0 520.0 530.0 550.0 550.0 560.0 570.0 580.0 590.0	23.1 22.7 23.5 27.5 35.3 45.5 58.3 66.5 69.2 65.0	23.5 22.9 23.8 27.7 35.1 45.2 58.6 67.2 70.3 66.2	23.0 22.6 23.1 27.5 35.5 45.6 58.3 66.4 69.0 65.0	23.1 22.6 23.5 27.5 35.5 46.8 58.1 65.7 67.1 65.6	23 • 1 22 • 4 23 • 4 27 • 5 35 • 0 46 • 4 58 • 0 65 • 5 66 • 8 65 • 0	23.2 22.6 23.6 27.5 35.5 46.9 58.4 65.7 67.0 65.5	23.2 22.5 23.7 27.5 35.6 46.7 58.6 65.8 67.1 65.6	23.2 22.7 23.7 35.4 47.1 58.4 65.9 67.4 65.6
600.0	57.2	58.3	57.0	58.0	58.1	57.8	57.7	57.9
610.0	47.9	48.2	47.1	48.2	47.8	46.9	47.4	48.0
620.0	37.1	37.8	37.3	37.7	37.8	37.9	37.7	38.1
630.0	28.9	30.0	28.6	28.6	28.8	28.9	28.8	28.4
640.0	21.3	22.4	21.1	21.3	21.4	21.4	21.5	20.9
650.0	15.9	16.1	15.7	15.7	15.9	15.8	15.2	15.9
660.0	11.5	11.9	11.5	11.6	11.6	11.6	11.5	11.7
670.0	8.6	8.9	8.6	8.6	8.5	8.5	8.5	8.6
680.0	6.0	6.5	6.3	6.3	6.2	6.2	6.3	6.4
690.0	4.6	5.1	5.1	4.9	5.0	4.9	4.8	5.0
700.0 710.0 720.0 730.0 740.0 750.0 760.0	3.5 2.8 2.4 4.5 1.6 1.9 1.5	4.0 3.2 2.5 4.7 2.2 2.2 2.1	3.8 3.3 2.7 5.0 2.1 2.5 3.0 MERCURY	3.8 3.0 2.4 1.9 1.6 1.5 1.3	3.8 3.0 2.3 1.9 1.6 1.5 1.3	3.7 3.0 2.3 1.9 1.6 1.4 1.3	3.7 3.0 2.3 1.9 1.7 1.4 1.2	3.7 3.0 2.4 2.0 1.6 1.4 1.4
405•0	22.4	22.2	21.6	19.4	20.0	20.0	20.8	19.9
436•0	57.9	58.2	56.7	58.8	59.0	60.4	59.6	58.3
546•0	25.2	26.1	25.0	25.1	27.5	24.9	25.0	25.7
578•0	9.0	9.0	8.8	12.5	12.9	12.9	12.4	12.1



MEASUREMENTS NORMALIZED TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION (25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8800

		NBS		LABORA	TORY 9	
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6
380.0	3.5	3.6	3.8	3.6	3.5	3.6
390.0	5.7	5.7	5.7	6.5	5.6	5.6
400.0	7.9	7.6	7.7	7.7	7.7	7.6
410.0	10.4	10.0	10.1	10.2	10.2	10.3
420.0	13.0	12.7	12.9	12.8	12.7	12.9
430.0	16.0	15.8	15.8	15.7	15.7	15.6
440.0	18.6	18.5	18.3	18.4	18.4	18.3
450.0	20.8	20.7	20.6	20.8	20.7	20.6
460.0	22.5	22.5	22.5	22.6	22.7	22.7
470.0	23.8	23.7	23.6	23.9	23.8	23.8
480.0	24.2	24.1	24.0	24.2	24.2	24.2
490.0 500.0 510.0 520.0 530.0 540.0 550.0 560.0 570.0 580.0 590.0	24 • 2 23 • 3 22 • 8 23 • 6 27 • 4 35 • 5 58 • 2 66 • 5 69 • 4 65 • 2	23.1 22.6 23.6 27.3 34.9 44.8 57.5 66.3 69.6 65.6	23.0 22.6 23.5 27.5 35.4 45.4 58.0 66.2 68.9 64.8	24.2 23.2 22.7 23.7 27.6 35.6 46.9 58.6 65.7 67.1 65.6	24.2 23.3 22.7 23.7 27.7 35.6 47.0 58.4 66.0 67.3 65.9	24.2 23.2 22.7 23.6 27.5 35.6 46.7 58.3 65.7 66.8 65.5
600.0	57.5	58.0	56.9	57.8	58.1	57.8
610.0	47.5	48.1	47.1	47.1	47.8	48.0
620.0	37.0	38.3	36.9	37.5	37.3	37.5
630.0	28.7	30.3	28.5	28.7	28.9	28.9
640.0	21.4	21.6	21.4	21.6	21.4	21.0
650.0	15.7	16.0	15.7	15.7	16.0	15.9
660.0	11.4	11.4	11.5	11.8	11.6	11.7
670.0	8.5	8.6	8.7	8.6	8.5	8.5
680.0	6.1	6.1	6.3	6.4	6.3	6.3
690.0	4.7	4.8	5.1	5.0	5.0	5.0
700.0	3.5	3.5	3.8	3.8	3.7	3.8
710.0	2.8	2.9	3.3	3.1	3.0	2.9
720.0	2.4	2.2	2.7	2.4	2.4	2.4
730.0	4.6	4.4	5.3	1.9	2.0	2.0
740.0	1.6	2.2	2.8	1.6	1.6	1.6
750.0	1.9	1.7	2.9	1.4	1.5	1.4
760.0	1.5	2.1	3.0	1.3	1.4	1.3
405.0	22•2	20.7	21.7	20.7	20•1	20.1
436.0	58•8	58.6	58.1	57.7	58•9	59.6
546.0	25•6	25.7	25.3	25.6	25•0	27.0
578.0	8•7	8.8	9.0	12.7	12•7	12.3



MEASUREMENTS NORMALIZED TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION (25CM SECTION) -NORMALIZED TO AREA LAMP NUMBER NBS8801

		NBS		LABURA	TORY 5	
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6
380.0	3.6	3.6	3.6	•0	1.1	.0
390.0	5.8	5.5	5.7	•0	1.2	1.2
400.0	8.0	7.9	7.9	15.9	17.8	16.9
410.0	10.4	10.4	10.4	15.9	13.3	12.7
420.0	13.0	12.8	13.1	13.6	13.7	13.5
430.0	16.0	15.4	15.9	15.7	15.9	15.5
440.0	18.6	18.0	18.4	18.4	18.3	18.1
450.0	20.8	20.5	20.8	21.2	21.5	22.0
460.0	22.6	22.4	22.5	22.7	23.3	23.3
470.0	23.8	23.4	23.6	24.3	24.0	24.1
480.0	24.2	24.0	23.9	24.7	24.7	24.9
490.0	24.1	23.8	24.0	24.6	24.7	24.8
500.0 510.0 520.0 530.0 540.0 550.0 560.0 570.0 580.0 590.0	23.2 22.7 23.6 27.8 35.9 46.1 58.8 66.8 69.4 64.9	23.0 22.5 23.5 27.2 35.5 45.6 57.9 66.4 69.4 69.4	23.0 22.6 23.7 27.8 36.0 46.1 58.6 66.8 69.3 64.7	24.1 23.9 24.6 29.4 37.8 49.4 61.2 66.9 68.0 66.8	24.6 24.9 29.2 38.2 49.4 61.0 65.9 66.8 66.8	24.1 24.3 24.9 29.6 38.1 48.9 60.6 66.4 68.3 67.1
600.0	57.3	58.6	56.7	58.0	59.0	58.5
610.0	47.1	48.0	47.0	47.5	47.0	48.0
620.0	36.7	37.8	36.8	37.8	37.6	37.4
630.0	28.5	29.5	28.4	28.0	28.9	28.3
640.0	21.1	21.9	21.1	21.5	21.0	20.7
650.0	15.4	15.7	15.6	14.4	14.2	14.0
660.0	11.3	11.4	11.3	9.4	9.6	9.5
670.0	8.4	8.6	8.5	6.2	5.6	5.6
680.0	6.0	6.1	6.0	4.8	4.4	4.5
690.0	4.7	4.8	5.2	4.8	2.5	1.9
700.0 710.0 720.0 730.0 740.0 750.0 760.0	3.5 2.8 2.2 4.6 1.9 1.9	3.5 2.9 2.2 4.4 2.2 1.7 2.0	3.9 3.3 2.7 5.1 2.1 2.5 2.0 MERCURY	2.0 1.4 .7 9.5 2.6 1.6 .0 LINES	1.4 .7 .8 7.8 2.8 1.7 .0	1.4 1.6 7.8 2.8 1.7
405.0	22•4	21•5	21.5	5.5	5.0	5.6
436.0	58•2	58•7	57.4	54.6	54.7	55.0
546.0	25•8	25•7	25.7	26.8	27.7	28.7
578.0	8•4	8•7	8.9	13.8	16.8	16.3



RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION (25CM SECTION) -NORMALIZED TO AREA LAMP NUMBER NBS8802

		NBS		LABORA	TORY 5	
WAVELENGTH 380.0	RUN 1 3.8	RUN 2 3.6	RUN 3 3.8	RUN 4	RUN 5 1.0	RUN 6
390.0	5.9	5.7	5.9	1.1	1•1	1.1
400.0	7•9	7.9	7.8	17.6	21.8	16.3
420.0	13.0	12.8	13.0	13.9	13.8	13.4
430.0	16.1	15.6	16.0	15.3	16.0	15.5
450.0	20.7	20.7	20.8	21.5	21.7	21.6
460.0	22.4	22.4	22.6	23.0	23.0	23.2
480.0	23.9	24.1	23.9	24.9	23.9	24.4
490.0	23.9	23.9	24.0	24.7	24.5	24.8
500.0	22.9	23.1	22.9	24.4	24.2	24.4
510+0	22.4	22.7	22.5	24.5	24.2	24.1
530.0	27.6	27.5	27.7	29.7	29.3	29.5
540.0	35+5 45+6	35+1 45+1	35•8 45•9	38.4 49.8	37•6 49•0	38.1 49.1
560.0	58.2	58.1	58.4	61.4	60.2	61.5
570+0	66.0 68.4	66•4 69•4	66.6	66•1 66•9	66•4 67•6	66.7
590.0	64.0	65+8	64.6	66.7	66•2	67.0
600.0	56.0	57.3	56.5	58,7	59•1	59,2
610•0 620•0	46.3	47•4 37•6	46.7	47.0	46.8	47.4
630.0	28.3	28.9	28.1	28.0	27.9	27.8
640•0 650•0	20.8	21.2	21.2	20.6	21.3	21.4
660.0	11.0	11.5	11.1	9.0	9.3	9.1
670.0 680.0	8•3 6•0	8.5	8.4	5.3	5•2 4•1	5.4
690.0	4.7	5.0	5.1	1.8	4.1	3.1
700.0	3.4	3.7	3.8	1.4	2.7	1.4
710.0	2.8	3.1	3.3	•7	1.4	<u>1.4</u> 1.5
730.0	4.7	4.7	5.0	6.4	8.3	8.6
740•0 750•0	1.7	2.2	2.1	2.7	2.6	2.7
760.0	2.0	2.0	3.0	• 0	• 0	.0
			MERCURY	LINES		
405.0	24.2	22.0	22.2	5.5	5.3	4.8
436+0 546+0	63•3 26•7	25.9	25.6	26.9	26.6	27.7
578.0	10.1	8.6	8.9	17.2	14.2	16.0



RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION (25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8805

		NBS		LABORA	TORY 2	
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6
380•0	3.5	3.6	3.7	.0	0	.0
390•0	5.6	5.7	5.7	5.4	4.8	5.3
400.0	7.8	7.7	7.7	7.6	7.3	7.6
410.0	10.3	10.1	10.2	10.2	10.0	10.2
420.0	12.9	12.8	13.0	13.0	12.9	12.9
430.0	15.8	15.8	16.0	16.1	16.1	16.1
440.0	18.4	18.4	18.6	18.8	18.8	18.9
450.0	20.7	20.6	20.9	20.9	20.9	21.0
460.0	22.5	22.5	22.6	22.8	22.8	22.8
470.0	23.6	23.6	23.7	23.9	24.0	23.9
480.0	24.1	24.1	24.0	24.4	24.4	24.4
490.0 500.0 510.0 520.0 530.0 540.0 550.0 560.0 570.0 580.0 590.0	24 • 1 23 • 2 22 • 7 23 • 5 27 • 6 35 • 7 45 • 8 58 • 3 66 • 5 69 • 2 64 • 9	23.1 22.6 23.6 23.6 35.3 45.5 58.4 66.4 69.1 64.8	24.2 23.0 22.7 23.8 27.9 35.9 46.1 58.8 66.8 69.2 64.9	24.3 23.5 23.1 24.2 28.4 36.9 47.3 59.4 67.7 69.7 66.0	23.5 23.1 24.2 28.5 37.0 47.5 59.8 68.0 70.2 66.3	24.3 23.5 23.1 24.3 28.4 37.0 47.4 59.6 67.7 69.8 66.0
600.0	58.0	57.0	56.9	57.9	58.3	58.2
610.0	47.5	48.3	46.7	47.8	48.1	48.0
620.0	37.1	37.2	36.7	37.7	37.9	37.8
630.0	29.6	29.2	28.3	28.7	28.9	28.9
640.0	21.4	21.1	21.3	21.4	21.5	21.5
650.0	15.7	15.7	15.2	15.8	15.7	15.8
660.0	11.2	11.2	11.2	11.5	11.4	11.5
670.0	8.5	8.6	8.3	8.3	8.2	8.3
680.0	6.1	6.1	6.2	6.0	5.8	6.0
690.0	4.6	5.0	4.9	4.6	4.3	4.5
700.0 710.0 720.0 730.0 740.0 750.0 760.0	3.4 2.9 2.3 4.5 1.6 1.6	3.7 3.2 2.5 4.7 2.2 2.1 2.6	2.2 3.4 2.8 5.2 2.2 2.6 2.6 2.6 MERCURY	3.3 2.6 2.0 1.6 1.3 .9 .0	3.0 2.1 1.5 1.0 .8 .1 .0	3.3 2.5 1.8 1.4 1.2 .6 .0
405.0	22.3	22.0	21.8	22.0	22•1	21.7
436.0	59.3	58.2	57.8	57.7	59•4	57.2
546.0	25.4	25.5	25.5	25.2	25•2	25.5
578.0	8.8	8.8	8.7	10.2	10•1	10.1



MEASUREMENTS NORMALIZED TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8806

		NBS		LABORA	TORY 2	
VAVELENGTH 380•0 390•0	RUN 1 3.7 5.9	RUN 2 3.7 5.9	RUN 3 3.8 5.9	RUN 4 .0 5.8	RUN 5 0 5.7	RUN 6 .0 5.6
400.0 410.0 420.0 430.0 440.0 450.0 460.0	8.3 10.9 13.4 16.1 18.7 21.0 22.8 23.9	11.1 13.2 13.2 11.7 14.5 20.9 22.8	7.9 10.4 13.2 16.2 18.8 21.1 22.8 23.8	8.0 10.4 13.2 16.3 19.1 21.2 23.0	7.9 10.5 13.3 16.4 19.1 21.3 23.1	7.8 10.4 13.2 16.3 19.2 21.3 23.1
480•0 490•0	24.5 24.4	24.4	24.2 24.3	24.2 24.6 24.5	24•5 24•7 24•6	24.5 24.7 24.5
500.0 510.0 520.0 540.0 550.0 550.0 560.0 570.0 580.0 590.0	23.5 22.9 23.7 27.5 35.1 45.1 57.6 65.9 68.8 64.6	23.3 22.8 23.7 27.4 35.1 45.0 57.6 65.9 68.7 64.4	23.3 22.6 23.7 27.7 35.5 45.4 57.9 65.7 68.3 64.2	23.6 23.2 24.2 28.2 36.4 46.6 58.5 66.9 68.9 65.3	23.6 23.2 24.2 36.5 46.7 58.7 66.8 69.1 65.5	23.7 23.2 24.2 28.2 36.6 46.8 58.8 67.0 69.3 65.7
$600 \cdot 0$ $610 \cdot 0$ $620 \cdot 0$ $630 \cdot 0$ $640 \cdot 0$ $650 \cdot 0$ $660 \cdot 0$ $670 \cdot 0$ $680 \cdot 0$ $690 \cdot 0$	57.8 47.6 37.2 29.4 21.4 15.6 11.4 8.6 6.0 4.7	56.6 47.4 37.2 29.0 21.6 15.8 11.2 8.7 6.2 4.9	56.5 46.4 36.6 28.3 21.0 15.5 11.4 8.7 6.2 4.9	57.4 47.6 37.6 28.7 21.5 15.8 11.5 8.4 6.1 4.7	57.6 47.7 37.7 28.8 21.5 15.9 11.6 8.5 6.2 4.7	57.7 47.6 37.6 28.8 21.5 15.8 11.5 8.4 6.0 4.6
700.0 710.0 720.0 730.0 740.0 750.0 760.0	3.5 2.8 2.2 4.4 1.6 1.6 1.5	2.1 3.1 2.7 5.3 2.1 2.1 2.5	3.9 3.3 3.0 5.4 2.5 2.5 3.0	3.4 2.6 2.1 1.7 1.4 1.2 .0	3.4 2.7 2.1 1.5 1.7 .5 .0	3.3 2.6 1.9 1.5 1.2 .8 .0
405.0 436.0 546.0 578.0	21.7 58.7 25.9 8.7	19.5 64.2 25.6 8.7	MERCURY 21.9 57.8 25.3 8.8	22.0 58.9 25.2 10.1	22•2 57•1 25•5 9•9	22.1 57.7 25.4 9.9



MEASUREMENTS NORMALIZED TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION (25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8809

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		NBS		LABORA	TORY 4	
VAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6
380.0	3.6	3.6	3.9	4.2	3.8	4.0
390.0	5.8	4.2	5.8	6.2	6.3	5.5
400.0	8.1	6.7	7.9	8.5	8.0	8.2
410.0	10.5	8.9	10.3	11.5	10.6	10.2
420.0	13.1	10.9	13.0	13.6	13.3	13.1
430.0	15.9	12.9	16.0	16.5	15.7	16.1
440.0	18+4	19+/	18.5	19+2	18+3	18.0
450+0	22.5	20+0	22.6	21.4	20.3	20.4
470.0	23.6	21.9	23.6	24.3	22.0	21.01
480.0	24.1	22.3	24.1	25.0	25.5	24.0
490.0	24.0	22.4	24.1	24.2	23.9	23.3
500.0	23.2	22.4	23.1	24.2	23.7	23.4
510.0	22.7	21.9	22.6	23.2	23.0	22.9
520.0	23.6	22.1	23.7	24.5	23.7	24.0
530.0	27.7	24.4	27.9	29.1	28.7	28.4
540.0	35.4	30.2	35.9	37.4	36•9	36.7
550.0	40.5	41.0	45.9	40.5	47.9	47.9
570.0	56.3	61.1	56.4	64.6	50.5	59.1
580.0	69.1	65.0	68.8	76.5	76.1	74.8
590.0	65.2	69.5	64.4	63.1	64.8	65.5
600.0	57.4	61.9	56.6	55.7	56.9	57.4
610.0	47.5	53+5	46.6	45 .7	46.8	47.2
620.0	36.9	43.6	36.6	37.2	36.9	37.4
630.0	29.2	34.6	28.2	28.5	28.3	28.6
640.0	21+2	26.6	21.2	21.6	21.6	21.5
650.0	11.0	20+5	10+4	12 0	15+9	15.9
670.0	8.3	10.0	8.6	8.8	8.6	8.7
680.0	6.2	7.3	6.1	6.5	6.4	6.4
690.0	4.8	5.6	5.1	5.1	5.1	5.2
700.0	3.6	4.3	2.2	3.8	3.7	3.7
710.0	2.9	3.6	3.4	3.1	2.9	3.0
720.0	2.0	3.1	2.8	2.4	2.2	2.3
730.0	4.7	3.5	4.9	1.9	1.9	2.0
740.0	1.6	3+1	2.5	1.6	1.5	1.7
750.0	1+9	2.4	2.6	1.4	1+4	1.5
/60+0	1.5	2 • 4	2.1	1.2	1.0	1.0
			MERCURY	LINES		
405.0	22.5	14.8	22.1	20.8	20.8	19.5
436.0	59.1	54.7	58.3	52.2	52.9	54.1
546.0	25.9	21.6	25.6	24.8	25.7	25.5
578.0	8.9	6.6	8.9	7.2	6.9	7.2



RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION (25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8810

		NBS		LABORA	TORY 4	
₩AVELENGTH 380•0 390•0	RUN 1 3.7 5.7	RUN 2 3•4 4•0	RUN 3 3.9 5.6	RUN 4 4.0 6.5	RUN 5 3.6 5.9	RUN 6 4.2 6.2
400.0 410.0 420.0 430.0 450.0 450.0 460.0 470.0 480.0	7.9 10.4 12.9 15.8 18.4 20.5 22.3 23.6 23.9 23.9	9.5 12.3 13.3 13.2 18.3 20.5 21.9 21.4 21.9	7.8 10.3 13.0 15.8 18.3 20.6 20.3 23.5 23.9 23.9	8.2 10.4 13.2 15.8 18.4 20.6 23.2 23.4 24.7 22.5	8 • 2 11 • 2 13 • 0 15 • 9 18 • 6 20 • 7 22 • 0 24 • 5 24 • 8 23 • 9	7.9 10.5 12.8 15.7 18.5 20.0 22.3 23.4 24.0
500.0 510.0 520.0 530.0 540.0 550.0 560.0 570.0 580.0 590.0	23.0 22.7 23.6 27.6 35.7 45.9 58.6 66.6 69.4 65.3	22.0 21.7 21.9 24.1 30.1 40.7 57.1 61.1 65.2 69.3	23.0 22.5 23.5 27.8 35.9 46.1 58.8 66.9 69.5 65.2	23.7 22.9 23.7 27.5 35.9 47.1 58.2 66.2 78.0 64.0	22 • 8 22 • 6 24 • 6 28 • 2 35 • 6 46 • 3 58 • 4 66 • 1 74 • 4 64 • 8	23.1 22.0 24.1 28.4 36.4 47.8 58.9 66.8 76.5 64.9
600.0 610.0 620.0 630.0 640.0 650.0 660.0 670.0 680.0 690.0	57.6 47.9 37.3 29.1 21.6 15.7 11.3 8.7 6.3 4.9	61.1 53.1 42.9 34.5 27.1 21.0 14.4 10.4 7.7 5.9	57.0 47.0 28.6 21.2 15.6 11.3 8.5 6.1 5.2	56.6 46.7 36.7 28.0 21.5 15.9 11.9 8.8 6.5 5.2	56.7 46.7 36.9 28.4 21.4 15.9 11.9 8.7 6.6 5.2	57.0 47.1 37.3 28.5 21.5 16.1 11.8 8.9 6.5 5.1
700.0 710.0 720.0 730.0 740.0 750.0 760.0	3.5 2.8 2.4 4.5 1.6 1.9 1.5	4.6 3.8 3.3 3.4 3.3 2.7 2.8	3.9 3.4 2.7 5.1 2.2 2.5 3.0 MERCURY	3.7 3.0 2.4 1.9 1.5 1.3 1.1	3.7 3.0 2.3 2.0 1.6 1.3 1.0	3.8 3.1 2.4 1.8 1.5 1.4 1.0
405•0 436•0 546•0 578•0	22•1 56•9 26•2 9•0	13.4 52.5 24.3 6.1	22.1 56.4 26.1 9.0	21.2 53.2 27.6 7.4	21.5 54.3 27.8 7.0	20.7 53.0 26.4 7.3


RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION (25CM SECTION) -NORMALIZED TO AREA LAMP NUMBER NBS8905

		NBS		LABORA	TORY 7	
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6
380.0	4.9	4.8	4.9	3.2	14.7	2.5
390.0	8•4	8.2	8.1	4 • 1	5.0	4.0
400.0	12.8	12.6	12.5	6.2	7.2	6.3
410.0	17.6	17.3	17.2	9.3	10.3	9.3
420.0	22.4	22.1	22.1	13.8	14.7	13.6
430.0	2/./	2/+4	21.3	10.0	19.0	1/02
440.0	36.0	35.6	35.8	27.4	24+0	26.0
460.0	38.4	38.0	38.1	28.3	30.0	29.2
470.0	39.5	39.1	39.1	32.7	31.9	31.0
480.0	39.3	39.1	39.0	32.8	33.6	32.6
490.0	38.2	37.7	37.9	34.0	32•6	33.1
500.0	35.7	35.5	35.4	31.9	31.8	32.3
510.0	33.3	33.3	33.0	30.7	29.9	30.8
520.0	31.6	31.6	31.5	29.1	28+5	29.5
540.0	34.4	34.2	34.3	31.2	31.6	32.5
550.0	38.6	38.2	38.3	35.1	35.6	36.3
560.0	44.4	44.0	44.2	40.9	41.4	42.4
570.0	47.9	47.7	47.8	45.6	46.2	46.5
580.0	48.3	48.3	48.2	46.7	46.7	46.8
590.0	44.6	44.7	44.7	42.9	43.0	43.1
600.0	39.1	39.2	39.1	37.1	30.9	38.7
610.0	32.2	32.5	32.4	32.3	31.6	33.3
620.0	25.3	26.0	25.4	25.7	26.0	25.7
630.0	19.8	21.4	20.2	21.4	21.1	21.2
640.0	14+8	11.2	11.3	13.9	14.1	14.1
660.0	8.2	8.2	8.4	11.9	11.7	12.0
670.0	6.3	6.5	6.5	10.7	10.2	10.6
680.0	4.5	4.7	4.8	9.8	9.1	9.5
690.0	3.6	4.0	3.9	10.2	9.5	10.1
700.0	2.7	3.1	2.9	10.1	9.7	10.3
710.0	2.4	2.5	2.8	12.3	11.3	12.1
720.0	1.9	2.1	2.1	14.3	12.8	14.6
730.0	3.9	4.4	4.9	1/.1	16.0	22.0
750.0	1.8	2.1	2.4	25.6	23.5	24.6
760.0	1.4	1.9	2.9	28.3	26.9	27.7
			MERCURY	LINES		
405.0	21.2	20.7	20.8	6.1	7.0	6.1
436.0	56.9	56.2	55.9	31.1	30.4	28.3
546.0	25.0	24.8	24.8	25.3	25.6	25.1
578.0	8.6	8.4	8.6	21.2	22.0	21.4



MEASUREMENTS NORMALIZED TO AREA

RELATIVE	SPECTRAL	IRRADIANCE	DISTRIBUTION (25CM	SECTION) -NORMALIZED	ΤO	AREA
			LAMP NUMBER NBS	3906		

	_	NBS		LABORA	TORY 1	
AVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6
380.0	4.9	4.9	5.1	.0	.0	.0
390.0	8.5	8.2	8.4	8.2	8.9	8.7
0,,,,,		• • • •			0.7	
400.0	13.1	12.9	12.9	12.0	12.8	12.9
410.0	17.8	17.5	17.6	16.9	18.0	18.0
420.0	22.6	22.2	22.6	22.0	23.2	23.2
430.0	27.8	27.1	27.7	27.3	28.6	28.6
440.0	32.4	31.7	32.2	32.1	33.5	33.5
450.0	36.3	35.8	36.4	35.9	37.2	37.1
460.0	38.6	38.4	38.8	38.6	39•7	39.6
470.0	39.9 30 E	39.5	39.7	39.7	40+7	40.0
480.0	38.3	38.1	38.5	38.6	4002 38.8	40.1 38.8
490.0	20.2	30.1	J0 • J	20.0	2000	30.0
500.0	36.0	35•8	36.0	36.5	36.6	36.5
510.0	33.5	33.4	33.7	34.1	34.0	34.0
520.0	31.8	31.6	31.7	32.4	32.3	32.2
530.0	31.9	31.8	31.9	32.7	32.5	32.4
540+0	34.5	34+4	34.6	30.0	34 • /	34.7
550.0	50+7	00.4	44.7	15.9	J900 45 4	09.0 05.4
570.0	47.9	44.5	48.3	4 9 .4	43.4	45.7
580.0	48.3	48.4	48.6	49.7	48.6	48.9
590.0	44.7	45.1	44.8	46.8	45.6	45.8
600.0	38.9	39.3	38.6	40.7	39.5	39.4
610.0	32.3	33.2	32.4	33.7	32.6	32.6
620.0	25.4	25.9	25.7	27.3	26+1	26.1
630.0	19.9	20+7	20.1	20.8	19.9	19.9
640.0	11 2	11.4	11 3	11 0	11.2	11 1
660.0	8.3	8.2	8.4	9.0	8.4	8.2
670.0	6.3	6.5	6.6	6.7	6.3	6.2
680.0	4.4	4.8	5.0	5.3	4.8	4.8
690.0	3.8	4.0	4.2	4.2	3.7	3.8
				-		• •
700.0	2.9	3.1	3.3	3.4	2.9	2.9
710.0	2.5	2.7	2.9	2.1	2+3	2.4
720.0	2.0	202	2 • D	2.2	1.0	1.0
740.0	4+1	1.8	2.5	.0	•0	.0
750.0	1.9	2.1	2.5	.0	.0	.0
760.0	1.5	2.1	3.1	• 0	• 0	.0
			MERCURY	LINES		
405.0	20.5	19.7	20.2	19.2	20.4	20.6
436.0	53.5	53.1	53.1	49.6	51.7	51.7
546.0	24.7	24.8	24.5	26.4	26.2	26.2
578.0	8.3	8.1	8.0	8.6	8.6	8.0



RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION (25CM SECTION)-NOPMALIZED TO AREA LAMP NUMBER NBS8907

		NBS		LABORA	TORY 9	
VAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6
380•0	5.1	4.7	5.2	4.9	4.9	4.6
390•0	8.5	8.2	8.4	9.2	8.2	8.1
400 • 0	12.9	12.2	12.7	12.3	12.2	12.2
410 • 0	17.6	16.9	17.4	17.2	17.1	16.9
420 • 0	22.5	21.9	22.4	22.6	22.4	22.3
430 • 0	27.9	27.7	27.7	27.8	27.7	27.7
440 • 0	32.4	32.4	32.1	32.4	32.6	32.5
450.0	36•1	35.9	36.0	36.2	36.4	36.3
460.0	38•6	38.4	38.5	39.0	38.8	38.7
470.0	39•7	39.5	39.4	40.1	39.9	39.9
480.0	39•4	39.4	39.1	39.7	39.8	39.8
490.0	38•2	38.0	38.0	38.5	38.5	38.5
500.0	35.9	35.7	35.6	36.0	36.2	36.1
510.0	33.4	33.3	33.3	33.6	33.5	33.6
520.0	31.8	31.7	31.6	31.7	31.9	31.8
530.0	31.9	31.8	31.8	32.0	32.3	32.2
540.0	34.6	34.3	34.6	34.7	34.9	34.8
550.0	38.7	38.4	38.8	39.5	39.9	39.7
560.0 570.0 580.0 590.0	44.6 48.1 48.4 44.6	44.4 47.9 48.3 44.9	44.7 48.1 48.3 44.7 39.0	44.9 47.8 47.3 45.1 39.5	45.0 48.0 47.4 45.1 39.6	44.8 47.8 47.3 45.2 39.7
610.0 620.0 630.0 640.0 650.0	32.5 25.5 20.1 15.1 11.2 8.4	32.7 26.0 21.7 14.9 11.3 8.3	32.3 25.6 19.9 15.0 11.4 8.5	32.5 25.9 20.1 15.2 11.3 8.5	32.8 26.2 20.0 14.9 11.3 8.5	32.7 26.0 20.3 14.7 11.4 8.6
670.0	6.3	6.6	6.3	6.4	6 • 3	6.4
680.0	4.7	4.7	4.6	4.8	4 • 8	4.8
690.0	3.9	4.0	4.1	3.9	3 • 8	3.9
700.0	3.0	2.9	3.3	3.0	3 • 0	2.9
710.0	2.3	2.5	2.7	2.4	2.4	2.4
720.0	1.9	2.1	2.0	1.9	2.0	2.0
730.0	4.1	4.2	4.8	1.6	1.6	1.6
740.0	1.8	1.7	2.0	1.4	1.3	1.3
750.0	1.8	2.0	2.4	1.2	1.2	1.3
405-0	20.0	20.2	MERCURY	LINES	17.5	18.9
436.0	52.3	54.0	52.8	52.5	54.3	54.0
546.0	24.2	24.7	24.6	25.2	24.3	24.8
578.0	8.4	8.2	8.3	10.4	10.4	10.4



RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8908

		NBS		LABORA	TORY 5	
WAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5	RUN 6
380.0	4.9	4.8	5.0	.0	1.0	.0
390.0	8.4	8.2	8.2	1.1	1.2	2.3
400.0	12.6	12.4	12.5	28.9	30.0	24.5
410.0	17.2	17.0	17.2	26.0	22.4	20.7
420.0	21.9	21.9	22.2	23.2	23.4	23.1
430.0	27.3	27.2	27.5	26.7	26.9	26.6
440+0	35.0	31+8	31.8	30.1	30.9	31.0
450+0	38.2	38.1	38.2	37.3	38.5	38.8
470.0	39.4	39.3	39.1	38.7	39.4	39.7
480.0	39.3	39.1	38.9	38.6	39.7	40.0
490.0	38.1	38.0	37.9	37.4	38.4	38.7
500.0	35.8	35.7	35.4	35.8	36+6	36.9
510.0	33.5	33.2	33.0	33.3	34.7	34.4
520.0	31 0	31.7	31 6	32+1	32+3	32.9
50.0	34.5	34.4	34.4	36.0	36.8	33.3
550.0	38.6	38.6	38.6	40.8	41.6	42.0
560.0	44.5	44.5	44.6	45.8	46.8	47.1
570.0	48.3	48.3	48.2	48.0	48.9	49.0
580.0	48.8	49.0	48.5	47.4	48.3	48.2
590.0	44.9	45.6	44.9	45.9	46.0	46.1
600.0	39.7	40.0	39.2	40.0	40.9	41.0
610.0	33.1	32.5	32.4	32.0	33.1	33.2
620.0	25.7	26.0	25.5	24.5	25+5	26.8
630.0	19.9	20.1	19.9	18.5	18.9	19.5
640.0	15.1	15+1	15.0	14.0	14.1	14.8
650.0	11.2	11+3	11.5	9.2	8.0	9.5
650+0	8+4	8.4	8.5	0.4	4.8	5.1
680.0	4.6	4.8	4.8	4.5	2.5	1.7
690.0	3.6	3.9	3.9	1.2	•6	1.9
0,0,0		••••				
700.0	2.9	3.0	3.4	•7	• 0	•7
710.0	2.3	2.6	2.8	•7	• 0	•7
720.0	1+8	2.1	2.1	1.5	• 0	8.
730+0	3.9	4.3	5.0	8.4	4+3	9.0
740.0	1.6	2.1	2.5	4.0	1+4	2.7
760.0	1.5	2.0	3.0	.0	.0	.0
10010		200	000	••	•0	••
			MERCURY	LINES		
405.0	21.1	20.3	20.5	23.6	22.2	2.6
436.0	54.7	54.2	53.4	50.9	52.0	53.5
546.0	25.0	24.9	24.9	24.5	24.8	25.6
578.0	8+4	8.3	8.4	10.7	12.7	14.1





RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION (25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8909

		NBS		LABORA	TORY 2
VAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5
380•0	4.8	5.1	.0	.0	.0
390•0	8.3	8.3	8.2	8.3	7.7
400.0 410.0 420.0 430.0 440.0 450.0 460.0 470.0 480.0 490.0	12.9 17.7 22.4 27.5 32.0 35.8 38.4 39.5 39.3 38.2	12.8 17.5 22.5 27.7 32.1 36.0 38.4 39.4 39.1 38.0	12.6 17.4 22.4 27.9 32.6 36.1 38.6 39.8 39.8 39.6 38.4	12.5 17.2 22.1 27.5 32.2 35.9 38.5 39.8 39.5 38.4	12.3 17.3 22.5 27.9 32.8 36.5 39.0 40.2 40.0 38.7
500.0	35.8	35.6	36 • 1	36 • 1	36.3
510.0	33.5	33.1	33 • 7	33 • 7	34.0
520.0	31.8	31.5	32 • 1	32 • 1	32.4
530.0	31.8	31.8	32 • 3	32 • 4	32.6
540.0	34.3	34.5	35 • 3	35 • 3	35.6
550.0	38.4	38.5	39 • 5	39 • 7	39.9
560.0	44.2	44.2	45 • 0	45 • 2	45.4
570.0	47.8	47.8	48 • 6	48 • 7	48.8
580.0	48.4	48.2	48 • 6	48 • 9	49.0
590.0	44.9	44.7	45 • 4	45 • 6	45.7
600.0	39.4	39.1	39.8	40.0	40.0
610.0	33.0	32.2	32.9	33.1	33.1
620.0	25.8	25.5	26.2	26.3	26.2
630.0	20.8	20.0	20.2	20.3	20.2
640.0	15.1	15.0	15.3	15.4	15.2
650.0	11.3	11.3	11.4	11.5	11.3
660.0	8.2	8.4	8.5	8.6	8.3
670.0	6.3	6.4	6.3	6.3	6.1
680.0	4.6	4.9	4.6	4.7	4.4
690.0	3.7	4.2	3.6	3.7	3.4
700.0	2.8	3.3	2.7	2.8	2.5
710.0	2.2	2.8	2.2	2.3	1.8
720.0	1.7	.3	1.7	1.8	1.3
730.0	3.8	4.9	1.4	1.4	.9
740.0	1.5	2.1	1.1	1.6	.5
750.0	1.5	2.4	1.0	.5	.2
760.0	1.5	2.9	.0	.0	.0
405•0 436•0 546•0 578•0	20.9 55.0 24.8 8.2	20•3 54•3 24•5 8•2	MERCURY 21.1 55.3 25.1 9.4	21.0 54.5 25.1 9.3	20•7 55•4 24•9 9•0



RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION (25CM SECTION) - NORMALIZED TO AREA LAMP NUMBER NBS8911

	_	NBS		LABORA	TORY 4
VAVELENGTH	RUN 1	RUN 2	RUN 3	RUN 4	RUN 5
380•0	5.0	5.0	5.3	5.1	4•9
390•0	8.3	8.3	8.4	8.6	8•9
400.0	12.5	9.4	14.0	12.1	13.0
410.0	17.1	16.0	17.3	16.9	17.7
420.0	22.0	21.8	22.3	22.3	22.2
430.0	27.6	27.1	27.7	27.4	27.8
440.0	32.2	31.4	31.0	31.9	32.3
450.0	36.1	35.1	34.9	35.0	37.0
460.0	38.5	37.5	37.4	38.1	38.4
470.0	39.6	38.5	39.2	39.4	41.1
480.0	39.4	38.3	38.8	39.3	38.6
490.0 500.0 510.0 520.0 530.0 540.0 550.0 560.0 570.0 580.0	38.2 35.9 33.5 31.8 31.9 34.4 38.5 44.2 47.9 48.5 44.8	37.1 34.7 32.5 30.8 31.1 31.9 34.4 43.4 46.7 47.0	37.5 35.6 33.0 31.8 31.5 35.2 40.0 45.1 48.6 53.6 44.7	37.2 35.8 33.7 32.3 32.1 34.8 39.5 44.6 48.2 53.0 45.4	37.4 35.9 33.6 32.0 34.7 39.9 45.0 48.4 50.7
600.0	39.5	38 • 1	39.0	39.8	39.3
610.0	32.4	31 • 6	32.2	32.8	32.5
620.0	25.7	25 • 1	26.0	25.9	25.8
630.0	20.5	19 • 6	20.1	20.1	20.0
640.0	15.0	14 • 6	15.3	15.4	15.1
650.0	11.1	11 • 1	11.4	11.6	11.5
660.0	8.3	8 • 1	8.5	8.6	8.5
670.0	6.4	6 • 5	6.4	6.6	6.4
680.0	4.6	4 • 8	4.9	4.9	4.9
690.0	3.7	4 • 2	4.0	4.1	4.1
700.0	2.8	3.3	2.9	2.9	3.0
710.0	2.4	2.7	2.4	2.4	2.4
720.0	1.9	2.3	1.9	1.9	1.9
730.0	4.0	4.9	1.5	1.6	1.5
740.0	1.5	2.4	1.4	1.3	1.3
750.0	1.8	2.4	1.1	1.0	1.2
760.0	1.5	2.9	.9	1.0	1.0
405•0	21.3	20.8	20.4	20.3	19.8
436•0	54.6	52.9	52.6	51.6	49.5
546•0	24.8	9.7	26.7	26.2	26.2
578•0	8.2	8.3	7.3	7.6	7.5



4.4. Results of the check on systematic errors in conventional sphere photometry

In section 3.2 the experimental design for this part of the intercomparison was briefly discussed. Each experiment was to consist of five measurements performed in a prescribed manner. For example, the first step was to be the measurement of the total luminous flux of a cool white fluorescent lamp without other lamps in the sphere. The photocell reading in this case is proportional to the total luminous flux of the lamp, C, minus a fraction, A_c , of the light which is absorbed by the lamp. That is,

$$R_1 = K_1 C(1 - A_c)$$
(4.1)

where K_1 is the proportionality factor for the spectral distribution of a cool white fluorescent lamp.

In the second step of the experiment the above measurement was repeated with an unlighted incandescent lamp present in the sphere. If the fraction of light absorbed by the incandescent lamp is ${\rm A}_{\rm I}$, the equation describing this step of the experiment is:

$$R_2 = K_1 C(1-A_c) (1-A_I)$$
(4.2)

Multiplication of the two factors enclosed by parenthesis yields four terms, one of which is the product of the two absorption fractions. Since the fraction of light absorbed by each bulb is much less than unity, their product may be neglected. Equation 4.2 becomes

$$R_2 = K_1 C(1 - A_c - A_I)$$
(4.3)

If the change in the lamp absorption due to the different spectral distributions of the sources is assumed to be negligible, then the equation representing the photocell readout of a lighted incandescent and an unlighted fluorescent lamp is:

$$\mathbf{R}_{4} = \mathbf{K}_{2} \mathbf{I} \left(\mathbf{I} - \mathbf{A}_{\mathbf{C}} - \mathbf{A}_{\mathbf{I}} \right) \tag{4-4}$$

In this equation, I is the total luminous flux of the incandescent lamp and K_2 is the proportionality factor for an incandescent spectral distribution. In summary, the equations representing all five steps in this experiment are:

 $\begin{array}{l} R_1 &= K_1 \ C(1-A_C \) \\ R_2 &= K_1 \ C(1-A_C \ -A_I \) \\ R_3 &= K_1 \ C(1-A_C \ -A_I \) \\ R_4 &= K_2 \ I(1-A_C \ -A_I \) \\ R_5 &= K_2 \ I(1-A_I \) \end{array}$

In the third equation listed above, a term has been introduced to represent all the effects in the system that preclude closure. The two major effects included in W are the non-linearity of the system and the change of fluorescent lamp output caused by heat from the incandescent lamp nearby. These two effects cannot be separately determined from the data of this limited experiment. However, if such a separate determination is desired in future experiments, it is suggested that the experiment be expanded to include another lamp of the same spectral distribution as either of the two used in the present test. That is, a second fluorescent lamp in the sphere would test linearity without introducing a heating effect. Furthermore, if four lamps were tested (two of each type) in a series of single and double lamp measurements, then the assumption that lamp absorption is independent of spectral distribution would be unnecessary. In this case the fractional absorption of each source by the same bulb could be determined separately. For the present intercomparison it was decided to forgo completeness for the sake of simplicity. Since the total luminous flux of both the fluorescent and incandescent lamps was assigned at NBS, the five equations listed above can be solved for the fractional absorption A_I and A_c , the sphere factors K_1 and K_2 , and the closure term W. The absorption terms are:

$$A_{I} = \frac{R_{4} (R_{1} - R_{2})}{R_{2}R_{5} + R_{1}R_{4} - R_{2}R_{4}}$$
(4.5)

and

$$A_{c} = \frac{R_{2} (R_{5} - R_{2})}{R_{2}R_{5} + R_{1}R_{4} - R_{2}R_{4}}$$
(4.6)

The sphere factors are:

 $K_1 = R_1 / C(1 - A_c)$ (4.7)

and

 $K_2 = R_5 / I(1 - A_I)$ (4.8)

And the closure term is:

$$W = R_3 - R_2 - R_4 \tag{4.9}$$

By using the photocell readings supplied by the various laboratories, the values of each of these terms were calculated and are presented in tables 4.68 to 4.74. Table 4.75 is a summary of the results of these experiments. This table also lists the sphere size, paint, and color correction used by each laboratory. The "Percent Color Deviation" in the last line of the table is the difference between the two calculated sphere factors. That is,

Percent Color Deviation =
$$100(K_1 - K_2)/K_2$$
 (4.10)

For perfectly color corrected spheres, this quantity would, of course, be zero.

It is readily seen from table 4.75 that the fraction of light absorbed by the fluorescent lamps can be closely correlated with the sphere diameter. These data and the data from the incandescent lamps are presented graphically in figure 4.60. The absolute value of the closure term can also be correlated to a small extent with the sphere diameter. This may mean that heating of the fluorescent lamp in smaller spheres is the slightly dominant effect. As discussed previously, an expanded experiment would be necessary actually to determine this.

The extent of color correction attempted by each laboratory and the calculated color deviation are related except in the case of Laboratories 1 and 5. Laboratory 1 is apparently correct in saying that any color corrections to their system are relatively small, however, an explanation for this apparent anomaly in the case of Laboratory 5 is not discernable from the available data. (See tables 3.1 to 3.3 and section 3.1)

The negative absorption observed by Laboratories 2 and 5 deserves some mention. In both cases it is quite close to the standard deviation of a single measurement and may not be meaningfully different from zero. It can be argued that inadequate baffling, leading to a direct reflection from the unlighted bulb to the detector, would appear as a negative absorption. There are, however, insufficient data to support this hypothesis.

SYSTEMATIC ERROR CHECK OF PHOTOMETRIC EQUIPMENT

LABORATORY	LABORATORY 1 C = 2826.6 LUMENS I = 2906.0 LUMENS									
RUN 1										
OBS. LAMP	FLUORESCENT LAMP VOLT CUR(SET)	INCANDESCENT VOLT(SET)	LAMP CUR	TIME	TEMP	PHOTOCELL READING				
1 C 2 C +(I) 3 C + I 4 (C) + I 5 I	102.20 430 102.20 430 102.30 430	117.70 117.70 117.70	1.57 1.57 1.57	10.00 10.02 10.10 10.12 10.13	76.90 77.10 77.40 78.00 78.40	2800.0 2783.0 5664.0 2856.0 2906.0				
RUN 2										
OBS. LAMP	FLUORESCENT LAMP VOLT CUR(SET)	INCANDESCENT VOLT(SET)	LAMP CUR	TIME	TEMP	PHOTOCELL READING				
6 C 7 C +(I) 8 C + I 9 (C)+ I 10 I	102.30 430 102.40 430 102.40 430	117.70 117.70 117.70	1.57 1.57 1.57	10.35 10.36 10.37 10.38 10.39	77.00 77.20 77.60 78.00 78.40	2807.0 2790.0 5666.0 2853.0 2909.0				
RUN 3										
OBS. LAMP	FLUORESCENT LAMP VOLT CUR(SET)	INCANDESCENT VOLT(SET)	LAMP CUR	TIME	TE™P	PHOTOCELL READING				
11 C 12 C +(I) 13 C + I 14 (C)+ I 15 I	102.60 430 102.60 430 102.40 430	117.70 117.70 117.70	1.57 1.57 1.57	11.02 11.03 11.05 11.06 11.07	77.20 77.20 77.70 78.00 78.60	2811.0 2800.0 5667.0 2848.0 2898.0				
ABSORPTION 1 ABSORPTION C CLOSURE SPH FACTOR P SPH FACTOR P	RUN 1 RU I .60 C 1.71 1 .44 (1 1.0078 1.0 (2 1.0060 1.0	IN 2 RUN 3 •59 •38 •91 1•72 •41 •34 0124 1•0119 0070 1•0011	N 1.0 1.0	1EAN •53 •78 •40 0107 0047	S.D. .12 .12 .05 .0025 .0032	PERCENT PERCENT PERCENT				

SYSTEMATIC ERROR CHECK OF PHOTOMETRIC EQUIPMENT

LAB	DRATORY	2	C = 2794.	8 LUME	เทร	I = 2753.	0 LUM	IENS		
RUN	1									
OBS.	LAMP	-	FLUORESCENT VOLT CUR	LAMP (SET)	11 /	NCANDESCENT	LAMP CUR	TIME	TEMP	PHOTOCELL READING
1 2 3 4 5	C C +(I) C + I (C)+ I I		101.40 101.20 101.20	430 430 430		109.00 109.00 109.00	1.59 1.59 1.59	•00 •00 •00 •00 •00	77.40 77.20 77.30 77.80 77.30	2845.0 2836.0 5544.0 2725.0 2708.0
RUN	2									
085.	LAMP		FLUORESCENT VOLT CUP	LAMP (SET)	I	NCANDESCENT VOLT(SET)	LAMP CUR	TIME	TEMP	PHOTOCELL READING
6 7 8 9 10	C C +(1) C + 1 (C) + 1 I	•	100.80 101.00 100.60	430 430 430	_	109.00 109.00 109.00	1.59 1.59 1.59	•00 •00 •00 •00 •00	77.60 77.30 77.70 77.80 78.20	2828.0 2819.0 5544.0 2722.0 2713.0
RUN	3									
ors.	LAMP		FLUORESCENT VOLT CUP	LAMP	I	NCANDESCENT VOLT(SET)		TIME	TEMP	PHOTOCELL READING
11 12 13 14 15	C C +(I) C + I (C)+ I I	•	100.90 100.80 100.80	430 430 430		109.00 109.00 109.00	1.59 1.59 1.59	• 00 • 00 • 00 • 00 • 00	77.40 77.40 78.00 78.00 78.00	2840.0 2834.0 5604.0 2731.0 2734.0
ABSC ABSC CLOS SPH SPH	RPTION RPTION SURE FACTOR FACTOR	I C K1 K2	RUN 1 .32 63 31 1.0116 .9868	R(UN 2 • 32 • • 33 • 05 0085 9886	RUN 3 •21 •11 •70 1•0173 •9952	1.	MEAN •28 •28 •15 0125 9902	S.D. .06 .37 .51 .0044 .0044	PERCENT PERCENT PERCENT

SYSTEMATIC ERROR CHECK OF PHOTOMETRIC EQUIPMENT

LABORATORY	3	C =	2917.1	LUMENS	I = 270	1.0 LUMENS
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RUN	1
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OBS. LAMP	FLUORESCENT VOLT CUR	LAMP (SET)	INCANDESCENT VOLT(SET)	LAMP CUR	TIME	TEMP	PHOTOCELL READING
1 C 2 C +(I) 3 C + I 4 (C)+ I 5 I	102.80 102.80 102.80	430 430 430	108.60 108.60 108.60	1.60 1.60 1.60	13.10 13.12 13.15 13.17 13.19	76.90 76.90 77.90 78.00 78.20	2970.0 2970.0 5823.0 2863.0 2865.0
RUN 2							
OBS. LAMP	FLUORESCENT VOLT CUR	LAMP (SET)	INCANDESCENT VOLT(SET)	LAMP Cur	TIME	TE ^M P	PHOTOCELL READING
6 C 7 C +(I) 8 C + I 9 (C)+ I 10 I	101.80 101.80 101.80	430 430 430	108.60 108.60 108.60	1.60 1.60 1.60	13.35 13.37 13.40 13.42 13.43	76.50 76.50 77.50 77.50 77.80	2930.0 2°20.0 5765.0 2850.0 2855.0
RUN 3							
OBS. LAMP	FLUORESCENT VOLT CUP	LAMP (SET)	INCANDESCENT VOLT(SET)	LAMP CUR	TIME	TEMP	PHOTOCELL READING
11 C 12 C +(I) 13 C + I 14 (C)+ I 15 I	101.80 101.80 101.80	430 430 430	108.60 108.60 108.60	1.60 1.60 1.60	14.25 14.27 14.29 14.33 14.34	76.40 76.40 76.90 77.20 77.50	2915.0 2916.0 5755.0 2860.0 2865.0
ABSORPTION I ABSORPTION C CLOSURE SPH FACTOR K SPH FACTOR K	RUN 1 •00 •07 -•17 1 1•0188 2 1•0607	RUN • 3' • 1 • 0' 1•006 1•060	2 RUN 3 403 7 .17 936 2 1.0010 6 1.0604	1.	MEAN •10 •14 -•21 0087 0606	S.D. .21 .06 .14 .0092	PERCENT PERCENT PERCENT

SYSTEMATIC ERROR CHECK OF PHOTOMETRIC EQUIPMENT

LABORATORY 4 C = 2783.2 LUMENS I = 2633.0 LUMENS											
RUN 1											
OBS. LAMP	FLUORESCENT VOLT CUR	LAMP IN (SET) V	CANDESCENT OLT(SET)	LAMP CUR	TIME	TEMP	PHOTOCELL READING				
1 C 2 C +(I) 3 C + I 4 (C)+ I 5 I	101.50 101.50 101.50	+30 +30 +30	107.10 107.10 107.10	1.58 1.58 1.58	17.26 17.32 17.37 17.43 17.48	76•20 76•20 78•20 78•20 82•00	2937.0 2922.0 5622.0 2732.0 2780.0				
RUN 2											
OBS. LAMP	FLUORESCENT VOLT CUR	LAMP IN (SET) V	CANDESCENT	L AMP CUR	TIME	TEMP	PHOTOCELL READING				
6 C 7 C +(I) 8 C + I 9 (C)+ 1 10 I	101.90 101.90 101.90	430 430 430	107.10 107.10 107.10	1.58 1.58 1.58	15.45 15.47 15.52 15.57 16.00	76.40 76.40 80.00 80.00 80.00	2973.0 2961.0 5711.0 2768.0 2821.0				
RUN 3											
OBS. LAMP	FLUORESCENT VOLT CUR	LAMP IN	ICANDESCENT	LAMP CUR	TIME	TEMP	PHOTOCELL READING				
11 C 12 C +(I) 13 C + I 14 (C) + I 15 I	101.50 101.50 101.40	430 430 430	107.10 107.10 107.10	1.58 1.58 1.58	16.27 16.28 16.35 16.36 16.37	76.20 76.20 79.00 80.00 80.00	3001.0 2984.0 5747.0 2774.0 2834.0				
ABSORPTION I ABSORPTION C CLOSURE SPH FACTOR K	RUN 1 •50 1•72 -•57 1 1•0737	RUN 2 •40 1•87 -•31 1•0886	RUN 3 •55 2•11 -•19 1•1014	1.	MEAN •48 1•90 -•36 0879	5.D. .08 .20 .19 .0139	PERCENT PERCENT PERCENT				

SYSTEMATIC ERROR CHECK OF PHOTOMETRIC EQUIPMENT

LABORATORY 5 C = 2750.5 LUMENS I = 2680.0 LUMENS

RUN	1								
овг.	LAMP	FLUORESCEN VOLT CU	IT LAMP	INC VO	ANDESCENT LT(SET)	LAMP CUR	TIME	TEMP	PHOTOCELL READING
1 2 3 4 5	C C +(I) C + I (C) + I I	101.00 101.00 101.00	430 430 430	1 1 1	07•90 07•90 07•90	1.58 1.58 1.58	4 • 44 4 • 45 4 • 47 4 • 48 4 • 49	24.70 24.70 25.20 25.50 25.60	3025•0 3029•0 5978•0 2945•0 2974•0
RUN	2								
085.	LAMP	FLUORESCEN VOLT CU	IT LAMP JR(SET)	INC VO	ANDESCENT LT(SET)	LAMP CUR	TIME	TEMP	PHOTOCELL READING
6 7 8 9 10	C C +(I) C + I (C)+ I I	100.50 100.50 101.00	430 430 430	1 1 1	07.90 07.90 07.90	1.58 1.58 1.58	4.21 4.22 4.25 4.26 4.27	24.80 24.80 24.80 25.00 25.20	3012.0 3014.0 6000.0 2962.0 2990.0
RUN	3								
OBS.	LAMP	FLUORESCEN VOLT CU	JR (SET)	INC VO	ANDESCENT LT(SET)	LAMP CUR	TIME	TE ^M P	PHOTOCELL READING
11 12 13 14 15	C C + (I) C + I (C)+ I I	101.00 101.00 101.20	430 430 430	1	•00 07•90 07•90	•00 1•58 1•58	4.17 4.18 4.21 4.22 4.23	24.20 24.20 24.40 24.60 24.80	3028.0 3034.0 6004.0 2955.0 2983.0
ABSC ABSC CLOS SPH SPH	DRPTION DRPTION SURE FACTOR FACTOR	RUN I1 C -99 K1 1.1100 K2 1.108	1 RI 3 - 6 1. 3 1.	JN 2 07 .94 .40 1054 1149	RUN 3 20 .94 .25 1.1113 1.1109	1.	MEAN - 13 - 95 - 24 1091 1114	5.D. .07 .02 .17 .0032 .0034	PERCENT PERCENT PERCENT

SYSTEMATIC ERROR CHECK OF PHOTOMETRIC EQUIPMENT

LABORATORY	6	с =	2804.9	LUMENS	I =	2646.0	LUMENS

KUN 1						
OBS. LAMP	FLUORESCENT LAMP VOLT CUR(SET)	INCANDESCENT VOLT(SET)	L AMP CUR	TIME	TEMP	PHOTOCELL READING
$ \begin{array}{cccc} 1 & C \\ 2 & C + (I) \\ 3 & C + I \\ 4 & (C) + I \\ 5 & I \\ \end{array} $	234.00 430 234.00 430 234.00 430	107.50 107.50 107.50	1.59 1.59 1.59	9.05 9.10 9.15 9.20 9.23	14.80 14.80 16.00 16.30 16.40	1167.0 1158.0 2507.0 1350.0 1358.0
RUN 2						
OBS. LAMP	FLUORESCENT LAMP VOLT CUR(SET)	INCANDESCENT VOLT(SET)	LAMP CUR	TIME	TEMP	PHOTOCELL READING
6 C 7 C +(I) 8 C + I 9 (C)+ I 10 I	235.00 430 235.00 430 235.00 430	107.50 107.50 107.50	1.59 1.59 1.59	11.10 11.15 11.20 11.22 11.25	15.80 16.00 17.00 17.50 17.50	1165.0 1162.0 2507.0 1346.0 1354.0
RUN 3 OBS• LAMP	FLUORESCENT LAMP VOLT CUR(SET)	INCANDESCENT VOLT(SET)	LAMP CUR	TIME	TEMP	PHOTOCELL READING
11 C 12 C +(I) 13 C + I 14 (C)+ I 15 I	234.00 430 234.00 430 234.00 430	107.50 107.50 107.50	1.59 1.59 1.59	12.05 12.10 12.15 12.17 12.25	17.30 16.40 17.60 18.00 18.00	1165.0 1158.0 2505.0 1344.0 1352.0
ABSORPTION I ABSORPTION C CLOSURE SPH FACTOR K SPH FACTOR K	RUN 1 R •77 •58 ••04 1 •4185 • 2 •5172 •	UN 2 RUN 3 •26 •60 •59 •59 •04 •12 4178 •4178 5130 •5140	۹ د د 5	4EAN •54 •59 •01 •180 5148	S.D. .26 .00 .09 .0004 .0022	PERCENT PERCENT PERCENT

TABLE 4.74											
	SYSTEMATIC ERROR	CHECK OF PHOTO	METRI	C EQUI	PMENT						
LABORATORY 7	C = 2902.5 LUME	NS I = 2769.	O LUM	ENS							
RUN 1											
DBS. LAMP	FLUORESCENT LAMP VOLT CUR(SET)	INCANDESCENT VOLT(SET)	LAMP CUR	TIME	TEMP	PHOTOCELL READING					
1 C 2 C +(I) 3 C + I 4 (C) + I 5 I	102.30 430 102.40 430 103.10 430	109.10 109.10 109.10	•00 •00 •00	10.16 10.19 10.23 10.25 10.27	24.90 25.00 26.30 27.40 27.60	2900.0 2886.0 6000.0 3105.0 3118.0					
RUN 2											
OBS. LAMP	FLUORESCENT LAMP VOLT CUR(SET)	INCANDESCENT VOLT(SET)	CUR	TIME	TEMP	PHOTOCELL READING					
6 C 7 C +(I) 8 C + I 9 (C)+ I 10 I	102.70 430 102.70 430 102.70 430	109.10 109.10 109.10	•00 •00 •00	10.55 10.57 11.01 11.03 11.05	25.00 25.10 26.50 27.20 27.40	2910.0 2890.0 5981.0 3124.0 3143.0					
RUN 3											
OBS. LAMP	FLUORESCENT LAMP VOLT CUR(SET)	INCANDESCENT VOLT(SET)	LAMP CUR	TIME	TEMP	PHOTOCELL READING					
11 C 12 C +(I) 13 C + I 14 (C)+ I 15 I	103.00 430 103.00 430 103.00 430	109.10 109.10 109.10	•00 •00 •00	11.32 11.34 11.37 11.39 11.42	25.00 25.00 26.50 27.20 27.40	2910.0 2891.0 5974.0 3085.0 3165.0					
ABSORPTION I ABSORPTION C CLOSURE SPH FACTOR K	RUN 1 RU -48 -41 -15 1 1.0033 1.0	N 2 RUN 3 •68 •64 •60 2•51 •55 -03 1086 1•0284	1.1	MEAN •60 1•18 -•14 0135	S.D. .11 1.16 .36 .0132	PERCENT PERCENT PERCENT					

OBS.

OBS.

SPH FACTOR K2

1.1315

1.1429

1.1503

1.1416

.0095

Table 4.75

1.8 meter Burch None 0.6 1.2 -0.1 -11.2 2.1 meter None Mg0 0.5 0°0 0°0 -18.8 9 2 meter Burch None 1.0 -0.1 0.2 -0.2 Sol 1 1.5 meter Corning 5900 Burch 0.5 1.9 -0.4 1.4 1 3 meter Burch None 0.1 0.1 -4.9 -0.2 3 3 meter Burch** Wratten 78C 0.3 -0°3 0.2 2.3 2 1.5 meter None *** G. Е.* 0.5 1.8 0.4 0°0 Percent Absorption Percent Absorption Color Correcting (Incandescent) Sphere Diameter (Fluorescent) Percent Closure Percent Color Sphere Paint Filter Deviation Laboratory

Systematic error check of photometric equipment summarization of results

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*General Electric Sphere Paint **Burch Sphere Paint ***See Section 3.1



5. DUSCUSSION AND CONCLUSIONS

5.1. The status of substitutional photometry

In the introduction it was stated that this intercomparison was conducted primarily to determine whether the use of a uniform set of cool white fluorescent lamps standardized at one laboratory would improve the agreement among the values of total luminous flux measured in laboratories throughout the lamp industry. The purpose of this intercomparison has not, however, been limited to just this. This was the first interlaboratory intercomparison to attempt an experimental design that would answer the more general question: what is the present capability of the lamp industry in the fields of photometry and spectroradiometry? The tests were also designed so that many specific questions could be answered about the performance of the equipment and the experimental techniques of the laboratories taking part in this intercomparison. Some of these specific conclusions have already been presented in section 4.

Considering the first question asked above: Did the use of the ETL CW Standards improve the agreement among the many laboratories that utilize conventional substitution photometry? If the results of the previous intercomparison* are used as an example of past performance, the answer is no. The range of agreement in the measurement of total luminous flux of cool white 40 watt fluorescent lamps by the laboratories participating in the 1964 Intercomparison** was l.6%. That is, the individual measurements were all within + 0.8% of the average. In the present intercomparison this range was 2.0%, if the results of Laboratory 6 are excluded. Laboratory 6 did not use the ETL CW Standards; and, although their measurements were precise, their results were far outside the range quoted above. This could be used as an argument for the use of one source for fluorescent lamp standards. The argument is further bolstered by the lack of agreement of the lamp industry's average measurement of total luminous flux with that of NBS** in the 1964 Intercomparison. In spite of the close agreement among the laboratories, their average was 2.6% above the NBS base. In the present intercomparison the agreement of the industry average with the NBS base is +0.2%, which is not significantly different from zero at the 95% confidence level.

One conclusion drawn from this part of the present intercomparison is that the use of a single source of fluorescent lamp standards would indeed form a uniform base among all the laboratories measuring luminous flux. However, the use of one source for standard lamps has not served to improve the range of agreement among these laboratories. This can only be accomplished by the improvement of photometric measuring techniques and equipment, and by developing sources that are more stable.

Each laboratory also measured, by conventional substitution photometry, a daylight fluorescent lamp against the ETL CW Standards in order to test agreement in heterochromatic photometry. The range of agreement among all, except Laboratory 6, was 3.6% and the difference of the industry average from the NBS base*** was -1.4%. In the 1964 Intercomparison the standards to be used in measuring daylight lamps were unspecified: a daylight lamp base was probably used. The range of agreement was 4.1% and the difference of the industry average from the NBS base was +0.1%. Thus it may be concluded that the 'present's the standard's the 'present's the 'present's the standard's the 'present's the 'present's the standard's the 'present's the 'pr

*The results of the 1964 Intercomparison were the subject of a National Bureau of Standards report to members of the Lamp Testing Engineers Conference (LTEC) and, as such, are not available for general circulation except by permission of LTEC.

**This includes the measurements made by the Electrical Testing Laboratories which were not included in the report since they were received at NBS after publication. The NBS measurements were also not included as part of the published form of the 1964 Intercomparison.

***A degree of confidence in the NBS measurements can be estimated by comparing the results of two different measurements on the same lamps. The results of the measurement of luminous flux of daylight and cool white fluorescent lamps by spectroradiometry and color corrected substitutional photometry, given in table 2.2, agree to within 0.2% for the daylight lamps and 0.1% for the cool white lamps. status of heterochromatic photometry is at the same level as that of daylight lamp homochromatic photometry in 1964.

From the data gathered for this intercomparison it can be seen that the increased lack of agreement in the measurements of daylight fluorescent lamps is directly traceable to the extent of the color correction applied at each laboratory. Laboratory 4 applied a suitable color correction filter for both their sphere and sphere window. Laboratory 1 reported their color correction to be relatively small. (See sections 3.1 and 4.4.) The difference between the average of their measurements of the daylight fluorescent lamp and the NBS base was -0.1%, whereas the average of their measurements of the col white fluorescent lamps differed from NBS by -0.4%. Laboratory 2 achieved partial color correction by using Wratten filters and eliminating the sphere window. Laboratory 8 did not apply color corrections to its sphere but did not use a sphere window; they had, in a sense, a partial color correction. Their average difference from NBS for daylight lamps was -1.3% and for cool white lamps, +0.1%. The remaining three laboratories, Laboratories 3, 5 and 7, used sphere windows and did not apply any color corrections. Their average difference from NBS have 2.3% and for cool white lamps, +0.5%.

The value of color correction in heterochromatic substitutional photometry has been clearly demonstrated by the results of this intercomparison.

5.2. The status of spectroradiometry and color parameter measurement.

Evaluation of the present status of spectroradiometry is based on the data supplied by four laboratories: Laboratories 1, 2, 4, and 5. Since their measurements were made with standards supplied by NBS and since they submitted data for all parts of the intercomparison, the relative merit of the two techniques for measuring total luminous flux (conventional substitution photometry and spectroradiometry) and the three techniques for measuring color parameters (spectroradiometry of the entire lamp in a sphere, spectroradiometry of a 25 cm section in a baffled enclosure, and the Barnes Colorimeter measurements) could be evaluated.

Conventional photometry and spectroradiometry were compared by measuring total luminous flux by using both techniques. Measurements of the total luminous flux of a 200 watt incandescent lamp against a set of 40 watt cool white standards by conventional substitution photometry are summarized in table 5.1. It would be well to note once again that only Laboratories 1 and 4 achieved suitable color correction, while Laboratory 5 did not color correct at all. The percent differences between the average of their measurements and the NBS assignments were: -1.4% and -1.3% for Laboratory 5. These percent differences can be compared with the differences found from the average of their spectroradiometric measurements of luminous flux of two 40 watt cool white fluorescent lamps versus a 200 watt incandescent lamp (see Table 4.11). They are as follows: -0.5% for Laboratory 1; -7.0% for Laboratory 2; +15.6% for Laboratory 4; and -0.4% for Laboratory 5. The range of agreement among the reported spectroadiometric measurements averaged for each laboratory is 22.6% and their average differences from the NBS base is +1.9%. Using conventional photometry the same laboratories reported a range of agreement of 5.1% and an average difference from the NBS base of -0.8%.

It appears, therefore, that overall spectroradiometric capability has to be developed much further before the agreement between the spectroradiometric measurement of total luminous flux made at different laboratories will be comparable to the agreement presently attainable by substitutional photometry. The experimental difficulties that Laboratories 2 and 4 may have encountered have been described in Section 4.4. The causes of the present lack of agreement are probably to be found there. The results achieved at NBS, where a comparison (see table 2.2) of spectroradiometry and color corrected substitutional photometry showed differences of at most 0.2% demonstrate that a significant improvement in spectroradiometric technique can be achieved. It should be noted that only since the introduction of automatic data acquisition systems has

Laboratory	Lamp	NBS (lumens)	Lab (lumens)
1	8757	2906	2865.2 2865.2 2866.6 2861.6 2867.1 2863.1 Avg. 2864.7
2	8758	2753	2673.0 2671.0 2674.0 2676.0 2687.3 <u>2687.3</u> Avg. 2678.1
4	8759	2633	2586.4 2595.8 2593.4 2607.4 2605.9 <u>2609.7</u> Avg. 2599.7
5	8756	2680	2740.9 2739.1 2743.3 2743.3 2746.3 <u>2750.0</u> Avg. 2743.8

Luminous flux of a 200 watt incandescent lamp by conventional photometry using 40 watt cool white fluorescent lamps as standards spectroradiometry become a feasible routine measurement and that for most laboratories it is a very new technique. It is hoped that we may finally be in a position to fulfill the prediction made by Parry Moon (ref. 5) in the 1930's:

"Evidently, we are getting rapidly to a place where our antiquated photometric notions must be discarded, and it seems advisable to analyze our concepts and see what can be done to replace them. In the present book, the entire development has been based not on the eighteenth century intuitive concept of 'light' but upon the firmly established concept of the spectroradiometric curve. It is true that the precision obtainable in radiometric measurements is still disappointingly low, so that actual photometry may be forced to stick to the old methods for a few years longer. But this does not appear to be an adequate reason why we should continue to force our minds into an eighteenth century mold as regards photometric concepts."

Turning now to the question of color measurement: What is the precision attainable in the measurement of the color parameters of a fluorescent lamp? This includes the agreement between different methods employed at the same laboratory and the agreement between different laboratories employing the same method. Table 5.2 is a comparison of the three techniques used to measure the x and y chromaticity coordinates. Since the color temperature of a lamp can be derived from the x and y chromaticity coordinates (ref. 6), this discussion will be limited to the measurement of these coordinates.

At NBS the x and y chromaticity coordinates were measured by using only the two spectroradiometric techniques. One technique samples the entire lamp in an integrating sphere and the other samples a 25 cm section of the lamp in a baffled enclosure. The first pair of columns in table 5.2 lists the differences observed between these two measurements on the same lamp (these are listed as differences in the fourth place). The second pair lists the same information for the x and y chromaticity coordinates measured at the four reporting laboratories. These two pairs of columns are an indication of the agreement between these two separate measurements made at the same laboratory. At NBS the internal range of agreement of the two methods of measurement was, therefore, -0.0021 to +0.0012, or 0.0033; and at the four reporting laboratories it was -0.0025 to +0.0071, or 0.0096.

The absolute value of the differences reported for Laboratory 1 are about twice those reported for the other laboratories. Four of these differences are much larger than the combined value of the standard deviations of each measurement. The reason for the internal disagreement in the case of Laboratory 1 is not clearly evident. Disagreement in the x and y chromaticity coordinates is not a diagnostic check on spectroradiometric performance: it merely indicates that a problem exists. It has already been pointed out that Laboratory 1 used two different monochromators for these measurements and that they reported their data in reduced form. They also failed to report data at several points in the spectrum, notably at the red and blue extremities. None of these factors can be cited as the primary cause of the internal disagreement. Their spectral distribution curves are in good agreement with those of NBS, as are their spectroradiometric values of total luminous flux. In the third pair of columns of table 5.2, it is evident that their sphere measurements of color parameters are also in good agreement with those of NBS. One may possibly conclude, therefore, that there is a systematic error in their measurements on a 25 cm section of a lamp that does not exist in their sphere measurements.

The last three pairs of columns of table 5.2 are an indication of the status of interlaboratory agreement in the measurement of color parameters. The third pair of columns compares the sphere measurements made on the same lamps at NBS and the four reporting laboratories. The range of agreement was from -0.0031 to +0.0072. The fourth pair is a comparison of the laboratory Barnes measurements and the NBS sphere measurement: range, -0.0060 to +0.0058. The last pair, which is a comparison of laboratory and NBS 25 cm section measurements, indicates a range of -0.0004 to +0.0069.

In the comparison of the sphere and 25 cm section measurements of Laboratory 5 in Table 5.2, there appears to be a large disagreement with the NBS measurements of the y chromaticity coordinate. From an examination of their spectral distribution curves it is clear that their match with the NBS points become poorer at Table 5.2

																		re,	lon
	(25)	λ	+57	+38	+60	+18	+10	+15	07+	A CT	071	+51	+63	+69	+62	o f		sphe	sect
	12)-N			•	•		_		~		_	_		-		sct for		ating	5 C B
	L (3	×	744	+30	+19	+	0	+	+	. 1		+23	1	+	+	CH S6		tegra	n a 2
	(L]	A	-58	-55	-52	-51	-48	-45	57-	24	1	-51	9 -	9 -	-13	a 25		an İr	ent c
	-N (S		Ŧ	+	+	+	+	+	-1		F	+	Ŧ	+	+	ų		ln	uren
	L(B)	×	+45	+51	447	+49	+51	+15	+38		0 + +	+38	-60	-57	+13	ement		ement	meas
10*																asur		asur	rf¢
Tab	(SP)	δ	-23	-31	-26	+31	-25	+26	+22		1 1 1	+24	+69	+72	+65	E		ше	omet
ance	N-(tric		ric	radi
fere	L(S)	×	-14	-16	-17	+30	+17	+19	-22	, - , -	⊣ ⊦	-	+	9 +	∞ +	ome		Lome	troi
Fe Fe																radi		radi	spec.
	SP)	5	+62	+71	+37	-25	-24	-25	۲ ۲		o F	+16	-13	-24	-10	ctro	e d	ctro	ory lamp
)-L(spe	lam	spe	orat the
	.(25	×	₽46	H62	F25	-24	-13	-15	7	55		F23	9	-14	ŝ	NBS	the	NBS	Lab
		1 1	Ŧ	т	т	'	•	'	7		r	т		'				-	
	P)		18	2	11	12	6	14	10	1 1	n	11	7	21	2	N (25		N (SP	L(25
	-N (S		1	+	1	1	I	1	1	- 1	F	1	1	1	1				
	(25)	2	L2	7	=	ŝ	4	-	ų	b v	Þ	-	ч	⊒	0	lon			
	z		+	ł	Ŧ	1	1	+	-	-	I	+	+	Ŧ		Inf			
2	4	e l	_	-		_					_		-	-		deb			
rato	pu	Typ	CM	5 G	Q	CW	5 C	Q	10	5 5	ځ	р	CF	ð	Q	- odm			
odel	5 0	Lamp	ч			2			4	٢			ŝ			^S*	2		

Note that all the differences in x and y have been mulitplied by 10,000.

L(SP) - Laboratory spectroradiometric measurement in an integrating

- Laboratory measurement using a Barnes Colorimeter.

sphere.

L(B)

Fourth place differences in the x and y chromaticity coordinates

the red end of the spectrum. As noted in section 4.4, this may be due to reduced photomultiplier sensitivity in this spectral region or to a systematic drift in the gain and/or sensitivity of their electronics.

The above discussion on agreement of color parameters is, of course. not at all rigorous. Since x and y are non-linear parameters, it is extremely difficult to obtain a statistical comparison of several measurements. However, from table 5.2 several conclusions are apparent:

1) In the most favorable case it is possible to obtain agreement to about ± 0.002 between two different spectroradiometric measurements of the same chromaticity coordinate made at the same laboratory. The present capability within three of the laboratories under consideration is, however, only about ± 0.003 in the best cases. (Note that the intralaboratory difference is as high as 0.007 for one of the laboratories.)

2) The level of agreement among measurements of chromaticity coordinates between three of the laboratories and NBS in performing the same spectroradiometric measurement on the same lamp is about ± 0.003 . (Note that the difference from NBS is as high as 0.007 for one of the laboratories.)

3) Agreement between a spectroradiometric measurement at one laboratory and a Barnes Colorimetric measurement at another is on the order of ± 0.006 .

4) The agreement between the four reporting laboratories and NBS in spectroradiometric measurement of chromaticity coordinates seems to be uncorrelated with the agreement in spectroradiometric measurement of total luminous flux.

It is expected that with improvements in spectroradiometric techniques throughout the lamp industry, agreement between laboratories in the measurement of color parameters will improve and spectroradiometry will become more important as a primary means of measuring these parameters.

5.3. Summary and conclusions

For the measurement of total luminous flux the most precise method presently in use is homochromatic substitutional photometry (range of agreement, 2%). The measurements are fast and relatively simple to perform; however, a standard of each type of lamp to be measured must be available in order to achieve maximum precision. Comparison of the luminous flux of two lamps with different spectral distributions, heterochromatic substitutional photometry, is considerably less precise unless the spectral response of the entire photometric system matches the CIE luminous efficiency function; that is, unless the system is fully color corrected. (Range of agreement: daylight versus coolwhite fluorescent, 3.6%; fluorescent versus incandescent, 5.1%.)

Although the range of agreement among the participating laboratories was found to be 22.6%, at NBS spectroradiometric and heterochromatic photometric measurements agreed within 0.2%. Therefore, with proper spectroradiometric techniques it should be possible to compare the total luminous flux of two lamps with very different spectral distributions to a precision close to that of homochromatic substitutional photometry. Furthermore, it would be unnecessary to correct for the spectral response of the system. Since it is difficult to produce and maintain reliably stable standard sources, the expense and effort necessary to set up and maintain a fully color corrected photometric system for all possible sources would be comparable to or might possibly exceed that of a single spectroradiometer. In addition to heterochromatic measurement of total luminous flux, the spectroradiometer data acquired in a single spectral flux distribution measurement permit the calculation of all the color parameters (chromaticity coordinates, color temperature, color rendering, flattery index, etc.), thereby replacing all other color measuring instruments. We may look forward to a time when a well developed spectroradiometric laboratory would need only a few highly stable standards of flux and spectral distribution from which to derive accurate (though not necessarily stable or precise) secondary standards of each lamp in production. These secondary standards would then be used in homochromatic substitutional photometry for routine quality control testing and other intralaboratory needs.

5.4. Acknowledgement

The authors would like to express their sincere thanks to Dr. Frank Studer for his guidance in the development of NBS spectroradiometric photometry and his assistance in the early stages of this intercomparison.

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Appendix A

Procedures for interlaboratory intercomparison of fluorescent lamps

Part 1

The intercomparison of T12F40 cool-white and daylight lamps for luminous flux will be conducted by having each laboratory make a set of three runs. The runs are statistically designed and involve measurements on the cool-white, and one daylight fluorescent lamps and one incandescent lamp, all supplied by NBS. These lamps are designated as C1, C2, D and I respectively. The six T12F40 CW lumen standards supplied by ETL last Spring to the industry are to be used as reference standards for this intercomparison by the laboratories that have them; the other laboratories will use their customary reference standards. These are designated as S_1 through S_6 in the data sheets. A reference ballast is being supplied and should be used with the three fluorescent lamps being supplied by NBS. The ETL standards should be run on the Sylvania reference ballast, and should be operated according to the instructions sent out with them (see Appendix A of the minutes of the May 14, 1968 meeting of LTEC). The lamps being supplied by NBS should be run with the NBS supplied ballast in the same manner. The USASI circuitry (II1. Eng. 62, 552-523, Sept. 1967) should be used and all fluorescent lamps should be operated by holding current at 430 mA. The incandescent lamp should be held at the specified voltage and should be in the sphere, but not lit during the fluorescent lamp runs. Similarly a fluorescent lamp should be in the sphere, but not lit, during the measurements on the incandescent lamp. Each run should be completed in the course of a day, and linearity corrections, if any, in the photometric equipment should be noted.

Part 2

The spectroradiometric intercomparison is designed to determine the uncertainty between measurements and between participating laboratories. The test will consist of three runs on each of the fluorescent lamps sent by NES, and one run on each of the ETL standards. The incandescent lamp sent by the Bureau and one of the fluorescent lamps will be in the sphere at all times to eliminate the effect of absorption. The incandescent lamp will be measured at the beginning of each set of runs and after each fluorescent lamp is measured. The lamps should be operated in the same manner as they were for Part 1 (substitution method). Since one of the purposes of this test is to transfer lumen values from the incandescent lamp to the fluorescent lamp, it will be important to hold the temperature at the center of the sphere to 25° C ± .2°C during the measurement of each fluorescent lamp. Uncorrected data points will be recorded at every 10 nm and at the mercury peaks. Any applicable correction curve will be recorded separately.

Part 3

This part of the intercomparison is the same as part 2 except that the flux of a fluorescent lamp from a 25-cm section of the fluorescent lamp rather than that from the entire lamp is measured. As in part 2 there will be three runs on each fluorescent lamp supplied and one run on each of the ETL standards, in each case by using the incandescent lamps supplied as a reference source. If the relative spectral distribution of the fluorescent lamp is to be made without reference to the incandescent lamp during the run, the 560 nm reading shall be recorded at the beginning and the end of each run. It is important that the reading does not change during the run. Although the temperature requirements are not strict, the fluorescent lamp should be free of drafts that will cause the output of the lamp to change during the run. Uncorrected data will be recorded at every 10 nm and at the mercury lines. Any appreciable correction curve will be recorded separately.

Part 4

In this part of the intercomparison the linearity of the system will be checked and the effects of absorption of the incandescent lamp and the fluorescent lamps will be measured. This part of the intercomparison will be used only in conjunction with part 1 (substitution method). The "I" notation stands for the incandescent lamp and the " C_1 " notation for the first cool-white fluorescent lamp in the intercomparison group. The I or C_1 enclosed in parentheses means the lamp is in the sphere but is not lit. There should be approximately 15 minutes between the shutting off of I and the lighting of C_1 . Since the incandescent lamp heats the sphere, time between readings $C_1^+(I)$ and C_1^+I should be as short as possible; <u>uncorrected</u> data will be recorded together with the time it was taken. Any correction factor will also be recorded separately.

Part 5

The main purpose of this part of the intercomparison is to determine if any discrepancies exist between spectroradiometric and Barnes colorimeter determinations of chromaticity coordinates. The intercomparison lamps, C_1 , C_2 and D, will be operated in accordance with the electrical procedures listed for part 1. Each participating laboratory will use the standards and test procedures it normally uses with the Barnes colorimeter. Each laboratory will report the CIE chromaticity coordinates for both the standards used and intercomparison fluorescent lamps. Any applicable correction factors will be recorded separately.

N85 506-Analysis paper

GPO - 1962 OF-	640466		Т	est 1 R	Run 1 Date 901-10					
					photo		Corre	ction		
	Current				cell		Linearit	y Other		
Lamp	(mA)	Voltage	Time	Temp.	reading			(if any)		
S ₁	430									
с ₁	430									
D	430									
S	430									
<u> </u>	430									
-S										
<u>-3</u>	430									
<u> </u>	430									
C,	430									
S.	430									
<u>_</u>	430									
I	450									
s ₆	//30									
	450									
							<u> </u>			
						-				

NBS 506—Analysis paper

GPO : 1962 OF-	840466		1	Test 1 Run 2 Date						
Lamp	Current (mA)	Voltage	Time	Тетр	photo cell reading		<u>Correc</u> Linearit	tion y Other		
S	420				leading			(II ally)		
- C ₁	430			<u> </u>						
n	430									
S ₅	430									
C ₂	430	·								
I	450								<u> </u>	
	430									
53	430							-		
C2	430									
C1	430									
S ₂	430									
D	430									
I										
S ₁	430									
										L

										<u> </u>

GPO : 1982 OF-	- 640468		Test 1 Run 3 Date				901-102					
					photo		Corre	ction				
	Current				cell		Linearit	y Other				
Lamp	(mA)	Voltage	Time	Temp.	reading			(if any)				
<u>s</u> 3	430											
<u> </u>	430											
<u> </u>	430											
<u></u>	430											
D	430											
I												
1	_430											
<u>6</u>	430											
- <u>I</u>												
<u>1</u>	430											
5	430											
<u>D</u>	430											
	430											
4	.430											
<u> </u>												
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										-		

NBS 506-Analysis paper

GP	0 · 1962 OF-	640466		I	Test 2 Run 1 Date							
Wave length	I	c ₁	I	s ₁	I	D	I	C ₂	I	s ₂		
3800												
3900												
4000				<u> </u>								
4100				<u> </u>								
4200												
4300												
4400												
4500												
4600												
4700												
4800												
4900												
5000												
5100												
5200												
5300												
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5600			1									
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5800												
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6000												
6100												
6200												
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6400												
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6700												
6800												
6900												
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7100												
7200												
7300												
7400												
7500												
7600												
4050												
4050												
5461												
5790												
5780												
	Tempe	rature Be	fore									
~		A	ter									
-	Volta	ge Before	2									
		After										

NBS 506—Analysis paper

GP	0 : 1962 OF-	640466		Test 2 Run 2 Date						,	01-102
Wave											
length	I	53	I	D	I	^U 2	I	s ₄	I	с ₁	
3800											
3900											
4000											
4100											
4200											
4300											
4400											
4500											
4600											
4000											
4800											
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7200											
7300											-
7400											
7500											
/600	ļ										
4050											
4300	h										-
5461											-
5780											
	Tempe	tature Be	fore								
	177-1-	A:	ter								
	volta	ge Before									
		Aiter									
NBS 506-Analysis paper

Temperature Before

Voltage Before After

After

GP	GPD: 1962 07-440466 Test 2 Run 3 Date 901-102										
Wave length	I	D	I	s ₆	I	c ₁	I	s ₅	I	c ₂	,
3800								-			
3900						1					
4000											
4100											
4200											
4300											
4400						1					
4500											
4600											
4700											
4800											
4900											
_5000											
5100											
5200											
5300											
5400											
_5500			_								
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6400											
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6700											L
6800											
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7000											
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7300											
7400											
7500											

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Test 4

tion y Other (if any)		
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Photo- cell reading		
Tempera-		
Time		
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Incandesc Voltage (set)		
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/oltage		
$\begin{array}{c} \frac{Lamp}{C} \\ \frac{C}{C} \\ \frac{C}{1} + I \\ 1 \\ 1 \\ 1 \end{array}$	$\begin{array}{c} c_1 \\ c_1 + t \end{array}$	
r Bun	3	

GPO : 1982 OF-640466			for C_1 , C_2 and D on a Barnes colorimeter							0 1- 10
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Appendix B

Questionnaire on equipment and procedures used for the NBS intercomparison of October, 1968 Please fill in the following questionnaire for all portions of the intercomparison in which your laboratory participated.

General

Α.	Laboratory		National Bureau of Standards*	_
Β.	For further	informationcontact	R. D. Saunders	
		Telephone	(301) 921-2113	

C. Our laboratory participated in:

X 40-W, cool-white, direct substitution intercomparison.

- X Spectroradiometric determination of the lumen outputs of 40-W fluorescent lamps.
- X Spectroradiometric determination of chromaticity coordinates on 10" sections of 40-W fluorescent lamps.

_____ Check of photometric equipment.

Barnes colorimeter determinations of chromaticity coordinates on 40-W fluorescent lamps.

Test 1: Cool-White, Direct Substitution Intercomparison

- A. Sphere
 - 1. Size 2m diameter
 - 2. Coating (please append spectral reflectance curve if available)

Type BaSO₄ - see figure B-1 following this section.

Last renewed April, 1966.

3. Color correcting (blue) filter (please append spectral transmittance curve if available)

not used

X used

Type Corning 5900

Thickness 1.55 mm

- Sphere window (please append spectral transmittance curve if available) Material <u>White plexiglass - see figure B-2 following this section</u>. Thickness <u>0.5 cm</u>
- Geometry: please append a sketch of the sphere used showing lamp location, receiver location, baffle location and size, etc. - see figure B-3.

^{*}Certain commercial instruments or materials are identified in this appendix in order to adequately specify the experimental procedure. In no case does such identification imply recommendation or endorsement by the National Bureau of Standards, nor does it imply that the material or equipment identified is necessarily the best available for the purpose.

B. Photoc	el	1
-----------	----	---

- 1. Manufacturer Weston
- 2. Model ____856 V
- 3. Color corrected X yes _____no

(please append spectral response curve if available)

- 4. Measuring circuit (please append circuit diagram) see figure B-4 following this section.
- 5. Linearity corrections
 - X Not applied
 - _____ Applied

```
Method of determining linearity correction (specify)
```

- C. Lamp Operation-Fluorescent (please append complete circuit diagram) see figure 2.1 in text.
 - 1. Power source
 - 0.015 % distortion
 - _____ AC line (regulated to ____%)
 - X Power supply (Manufacturer Elgar

Model 6000)

Other (specify)_____

- 2. Reference ballast for ETL C-W standards
 - Type variable reactance reference ballast

Manufacturer Sylvania

3. Power factor of reference ballast 7.5%

How determined (specify) by using a low power factor wattmeter, a true RMS voltmeter, and an ammeter.

- 4. Lamp voltage X measured _____set How measured by using a high impedance voltmeter (Fluke Model 931)______ Voltmeter input impedance 10 meg_ ohms
- 5. Current _____ measured X set How measured by using a Weston Model 904 AC ammeter
- Stabilization time <u>20</u> minutes in sphere <u>zero</u> minutes prestabilization. The lamp (was/was not) turned off after prestabilization.
- D. Lamp operation-incandescent (please append complete circuit diagram)
 - 1. Power source

AC Power

	volts
	amperes
	Hertz
	% Distortion
	AC line (regulated to%)
	AC power supply (manufacturer
	model)
	Other (specify)
	<u>X</u> DC power
	Batteries
	X DC power supply (manufacturer N.J.E. (2 units in series)
	modelSY_60-12)
2.	Voltage
	measured
	<u>X</u> set
	How determinedby using a differential voltmeter (Keithley model 660)
3.	Current
	<u>X</u> measured
	set
	How determined by measuring the drop across a 1 ohm shunt with the above mentioned differential
	voltmeter
4.	Warm-up time <u>5</u> minutes
	(If not in place in the sphere during warmup please give details)
5.	The incandescent lamp (was/was not) in the sphere when the fluorescent lamps were measured.
Amb	ient temperature
1.	not measured
2.	_X_measured
	Method of measurement <u>Digitec model 251 thermometer</u>
	Location of measurement 3 locations: 18 inches above center of lamp and 1 inch from each end
Oth	er
1.	Test was conducted by technicianX_ professional
2.	Treated as a routine test?yesno
3.	If no, please detail the special precautions used This was an experiment of special design.
	In addition, the equipment was checked out before these tests.
Cor	ments

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Ε.

F.

G.

Test 2: Spectroradiometric Determination of the Lumen Output of 40-W Fluorescent Lamps

A. Sphere

1.	X_The	information	supplied	for	Test	1,	Section A	is	applicable.	(If	so,	skip	2,	3,	4,	5,
	& 6)															

- 2. Size _____diameter
- 3. Coating (please append spectral reflectance curve if available)
 - Туре _____
 - Last renewed
- Color correcting (blue) filter (please append spectral transmittance curve if available) not used
 - used

Туре_____

Thickness_____

- 5. Sphere window (please append spectral transmittance curve if available)
 - Material_____

Thickness_____

- Geometry: Please append a sketch of the sphere used showing lamp location, receiver location, baffle location and size, etc.
- B. Lamp operation-Fluorescent (please append complete circuit diagram)
 - X The information supplied for Test 1, Section C, is applicable. (If so, skip 2, 3, 4, 5, 6, & 7)
 - 2. Power source
 - % Distortion

____AC line (regulated to _____%)

Power supply (Manufacturer

Model_____)

Other (specify)_____

3. Reference ballast for ETL C-W standards

Туре_____

Manufacturer_____

- 4. Power factor of reference ballast ____% How determined (specify)______%
- 5. Lamp voltage ____measured _____set

How measured

Voltmeter input impedance _____ ohms

- Current <u>measured</u> set
 How measured
- 7. Stabilization time _____minutes in sphere _____minutes prestabilization. The lamp (was/was not) turned off after prestabilization.
- C. Lamp operation-Incandescent (please append complete circuit diagram)
 - <u>x</u> The information supplied for Test 1, Section D, is applicable. (If so, skip 2, 3, 4, 5 & 6)
 - 2. Power source

	AC power
	volts
	amperes
	Hertz
	% Distortion
	AC line (regulated to%)
	AC power supply (manufacturer
	mode1)
	Other (specify)
	DC power
	Batteries
	DC power supply (manufacturer
	mode1)
Vo	ltage
	measured
	set
Ho	w determined
Cu	rrent
	measured
	set
Hor	w determined
	rm up time minutes
Wa	

D. Ambient temperature

	1.	X The information supplied for Test 1, Section E is applicable (if so, skip to the next
		section)
	2.	Not measured
	3.	Measured
		Method of measurement
		Location of measurement
Е.	Spe	ctroradiometer (Please append a block diagram of the instrument showing light path, major
	com	ponents, entrance and auxiliary optics, detector location, etc.) - see figure 2.2 of text.
	1.	Monochromator
		a. <u>Bauschand Lomb</u> Manufacturer <u>505</u> model
		Prism X grating
		Combination (specify)
		b. Effective spectral bandpass (Please append slit width correction curve if available)
		4050Å <u>5.84 nm</u>
		4358Å <u>5.53 nm</u>
		5461Å <u>5.48 nm</u>
		5780Å <u>5.93 nm</u>
		How determined (specify) from an analog plot of instrument reading versus dial setting and
		subsequent graphical area measurement.
	2.	Wavelength Calibration
		Last calibrated before each series of measurements
		Method (Specify spectral lines used) Hg and Cd emission lines
	3.	Detector (please append spectral response curve if available)
		EMI Manufacturer 9558QB Model
		<u>PM</u> Type (Photomultiplier, thermopile, etc.) <u>S-20</u> response type
	4.	Readout electronics (please append block circuit diagram) - see figure 2.2 of text.
		Integrating time approximately 0.1 sec
		Light chopped? X No Yes (Hertz)
		Other special features
	5.	System checks
		a. Linearity <u>X</u> checkednot checked
		Method by using sector discs and neutral density filters
		b. Scattered light X checkednot checked
		Method by using narrow band interference filters
		c. Other (specify)

	6.	Data reduction method normally used in your laboratory see section 2.2 of text
		a. Calibration
		Reference source used
		Procedure
		b. Line spectra (please describe method of evaluation)
		c. Other reduction procedures (specify)
F.	Oth	er
	1.	Test was conducted bytechnician
		X professional
	2.	Treated as a routine test? Yes X No
	3.	If No, please detail the special precautions used This was an experiment of special design.
		In addition, the equipment was checked out before these tests.
G.	Com	ments
Tes	t 3:	Spectroradiometric Determination of Chromaticity Coordinates on 10" Section of 40-W
Flu	ores	cent Lamps
Α.	Geo	metry (Please append a sketch of the setup used) - see figure 2.3 in text.
	X	_The 10" section specified by NBS was used.
		_A 10" section other than specified by NBS was used (specify)
	Met	hod of isolating a 10" section for investigation (Please describe baffling, baffling material,
	baf	fling coating, etc.)
В.	Lam	p Operation-Fluorescent (Please append complete circuit diagram)
	1.	X The information supplied for
		(Test 1, Section C or Test 2, Section B) is applicable
		(If so, state which and skip 2, 3, 4, 5, 6 & 7)
	2.	Power source
		% Distortion
		AC line (regulated to%)
		Power supply (Manufacturer
		Mode 1)
		Other (specify)

3.	Reference ballast for ETL C-W standards
	Туре
	Manufacturer
4.	Power factor of Reference ballast%
	How determined
5.	Voltagemeasuredset
	How measured
	Voltmeter input impedanceohms
6.	Currentmeasuredset
	Row measured
7.	Stabilization timeminutes in placeminutes prestabilization. The lamp (was/was
	not) turned off after prestabilization.
Lam	p operation-Incandescent (please append complete circuit diagram)
1.	X The information supplied for (Test 1, Section D or Test 2, Section D) is applicable. (If
	so, state which and skip 2, 3, 4, & 5).
2.	Power source
	AC power
	volts
	amperes
	hertz
	% distortion
	AC line (regulated to%)
	AC power supply (manufacturer
	model)
	Other (specify)
	DC power
	Batteries
	DC power supply (manufacturer
	model)
3.	Lamp voltage
	measured
	set
	How determined
4.	Current
	maacurad

С

_set

How determined

5. Warm-up time _____minutes

(If not in place please give details______

- D. Ambient temperature
 - The information supplied for (Test 1, Section E or Test 2, Section D) is applicable (if so, state which and skip to the next Section)
 - 2. X Not measured.
 - Measured.

Method of measurement_____

Location of measurement_____

E. Spectroradiometer

- 1. X The spectroradiometer described for Test 2, Section E, was used without modification.
- 2. ____The spectroradiometer described for Test 2, Section E, was modified as follows
- 3. ____Our laboratory did not participate in the spectroradiometric determination of the lumen output of 40-W fluorescent lamps. (Please fill in Test 2, Section E, above to describe the instrument used for the present test.)
- F. Other
 - 1. Test was conducted by _____technician ____X_professional
 - 2. Treated as a routine test? Yes X No
 - If no, please detail the special precautions used <u>This was an experiment of special design</u>. In addition, the equipment was checked out before these tests.
- G. Comments

Test 4: Check of Photometric Equipment (Test not performed at NBS)

A. Sphere

- The information supplied for (Test 1, Section A or Test 2, Section A) is applicable. (If so, state which and skip 2, 3, 4, 5 & 6)
- 2. Size _____diameter
- 3. Coating (please append spectral reflectance curve if available)
 - Туре

Last renewed_____

Color correcting (blue) filter (please append spectral transmitting curve if available)
 _____not used

____used

	Туре
	Thickness
5.	Sphere window (please append spectral transmittance curve if available)
	Material
	Thickness
б.	Geometry: Please append a sketch of the sphere used showing lamp location, receiver location,
	baffle location and size, etc.
Phot	tocell
1.	The information supplied for Test 1, Section B, is applicable. (If so, skip 2, 3, 4, & 5)
2.	Manufacturer Model
3.	Color correctedYesNo
	(please append spectral response curve if available)
4.	Measuring circuit (please append circuit diagram)
5.	Linearity corrections
	Not applied
	Applied
	Method of determining linearity correction (specify)
Lam	p Operation-Fluorescent (Please append complete circuit diagram)
1.	The information supplied for (Test 1, Section C, Test 2, Section B or Test 3, Section B) is
	applicable. (If so, state which and skip 2, 3, 4, 5, 6 & 7)
2.	Power source
	% distortion
	AC line (regulated to%)
	Power supply (Manufacturer
	Mode1)
	Other (specify)
3.	Ballast for Fluorescent Lamp
	Type
	Manufacturer
4.	Power factor of ballast%
	How determined
5.	Lamp voltagemeasuredset
	How measured
	Voltmeter input impedanceohms.

В

С

- 6. Current ______measured ______set How measured
- 7. Stabilization time _____minutes in sphere _____minutes prestabilization. The lamp (was/was not) turned off after prestabilization.
- D. Lamp Operation-Incandescent (please append complete circuit diagram)
 - 1. _____The information supplied for (Test 1, Section D, Test 2, Section C or Test 3, Section C) is applicable. (If so, state which and skip 2, 3, 4 & 5)
 - 2. Power source

Е. A

	AC power
	volts
	amperes
	hertz
	% distortion
	AC line (regulated to%)
	AC power supply (manufacturer
	mode1)
	Other (specify)
	DC Power
	Batteries
	DC power supply (manufacturer
	mode1)
3.	Voltage
	measured
	set
	Row determined
4.	Current
	measured
	set
	Row determined
5.	Warm-up timeminutes
	(If not in place in the sphere please give details)
Amb	ient temperature
1.	The information supplied for (Test 1, Section E, Test 2, Section D or Test 3, Section D)
	is applicable. (If so, state which and skip 2 & 3)
2.	Not measured

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3. ____Measured

Method of measurement_____

Location of measurement_____

- F. Other
 - 1. Test was conducted by technician professional

2. Treated as a routine test? Yes____ No____

3. If No, please detail the special precuations used

G. Comments

Test 5: Barnes Colorimeter Determinations of Chromaticity Coordinates on 40-W Fluorescent Lamps (Test not performed at NBS)

- A. Lamp Geometry: Please give details of the geometric setup used including a sketch:______
- B. Lamp Operation: Please give details of the lamp operation including warmup time, voltage and current measurements, ballasts, power factor, etc.:
- C. Standards: Please describe the standards used to calibrate the colorimeter as to lamp type, where and when calibrated, etc.:_____
- D. Calibration Procedure: Please describe in detail the calibration procedure used, including the data reduction for a test lamp:
- E. Photocells: Please describe the photocells in the colorimeter as to type, number, aperture, filters, hermetic sealing, etc.:
- F. Readout Equipment: Please describe the equipment used to read the photocell outputs:

G. Other

Test was conducted by _____technician _____professional

2. Treated as a routine test? ____Yes ____No

3. If no, please detail the special precautions used______

H. Comments











FIGURE B-4

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