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Spectroradiometry and Conventional Photometry
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## An Interlaboratory Comparison

# UNITED STATES DEPARTMENT OF COMMERCE Maurice H. Stans, Secretary 

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# Spectroradiometry and Conventional Photometry An Interlaboratory Comparison 

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| 2 | 8805 | 4.34 | 79 | 4.35 | 81 | 4.58 | 127 |
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|  | 8909 | 4.46 | 103 | 4.47 | 105 | 4.66 | 143 |
| 4 | 8809 | 4.38 | 87 | 4.39 | 89 | 4.60 | 131 |
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|  | 8911 | 4.48 | 107 | 4.49 | 109 | 4.67 | 145 |
| 5 | 8801 | 4.30 | 71 | 4.31 | 73 | 4.56 | 123 |
|  | 8802 | 4.32 | 75 | 4.33 | 77 | 4.57 | 125 |
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Relative spectral flux distribution (sphere)


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This report summarizes the results of a fluorescent lamp intercomparison carried out under the aegis of the National Bureau of Standards Photometry Section. The purpose of the intercomparison was to evaluate the interlaboratory precision obtainable in photometric and spectroradiometric measurements. The tests were also designed to disclose suspected systematic errors in measurement techniques.

The intercomparison consisted of five parts: (1) A homochromatic, photometric measurement of cool white fluorescent lamps and a heterochromatic, photometric measurement of a daylight fluorescent lamp and an incandescent lamp utilizing cool white fluorescent lamps as standards, all within an integrating sphere. (2) Spectroradiometric measurement of the above mentioned lamps in an integrating sphere. (3) Spectroradiometric measurement of a 25 cm section of the fluorescent lamps in a baffled enclosure. (4) An experiment designed to reveal systematic errors in heterochromatic photometry. (5) Measurement of the $x$ and $y$ chromaticity coordinates with a Barnes colorimeter.

Key words: Photometry, heterochromatic photometry, spectroradiometry, luminous flux, correlated color temperature, chromaticity coordinate, Barnes colorimeter, cool white fluorescent lamp, daylight fluorescent lamp, integrating sphere, color correction, intercomparison.

## 1. INTRODUCTION

### 1.1. Background information

From time to time the Lamp Testing Engineers Conference (LTEC) and the National Bureau of Standards (NBS) have conducted intercomparisons to compare the bases for luminous flux and color parameters used by lamp manufacturers and other members of the lamp industry.

In 1967 the National Bureau of Standards spectroradiometrically calibrated a set of eleven 40 watt, cool white fluorescent lamps by comparing their luminous flux output to those of a set of 200 watt, luminous flux standard incandescent lamps calibrated at $2854 \mathrm{~K} . * *$ Five of these fluorescent standards were retained at NBS and six were sent to the Electrical Testing Laboratories (ETL) where they were used in a statistically designed procedure to assign total luminous flux values to a group of eighty lamps of the same manufacturer and type. These lamps were sent in groups of six to some of the participating laboratories as new luminous flux standards. This intercomparison was conducted to see whether the use of these new standards would unify the base for total luminous flux throughout the lamp industry, and to compare it to the NBS base.

[^0]This intercomparison was conducted among some of the member laboratories of the Lamp Testing Engineers Conference and other interested laboratories. The participating laboratories were (in alphabetical order):

Duro-Test Corporation, North Bergen, New Jersey.
Electrical Testing Laboratories, Inc., New York, New York.
El-Tronics Inc., Warren, Pennsylvania.
General Electric Company, Cleveland, Ohio.
International Telephone and Telegraph Corporation, Lynn, Massachusetts.
National Research Council, Ottawa, Canada.
Sylvania Electric Products Inc., Danvers, Massachusetts.
University of California, Richmond, California.
Westinghouse Electric Corporation, Bloomfield, New Jersey.
Each laboratory was randomly assigned a code number for use in all references to that laboratory.

### 1.2. Description of intercomparison

The intercomparison consisted of five parts:

1) A photometric intercomparison of 40 watt fluorescent lamps by conventional substitution photometry in an integrating sphere
2) A spectroradiometric study of 40 watt fluorescent lamps in an integrating sphere;
3) A spectroradiometric study of a 25 cm (10 inch) section of 40 watt fluorescent lamps;
4) A statistically designed check on systematic errors in conventional sphere photometry; and
5) A Barnes Colorimeter determination of the $x$ any $y$ chromaticity coordinates of 40 watt fluorescent lamps.

The National Bureau of Standards supplied the participating laboratories with the following:

1) Two type F40T12 cool white lamps,
2) One type F40Tl2 daylight lamp,
3) One 200 watt incandescent lamp calibrated for total flux at 2854 K , and
4) One fixed inductance choke-ballast on which the fluorescent lamps (items 1 and 2) were to be operated.

The fluorescent lamps had been seasoned by the manufacturers for 500 burning hours and the operating conditions were specified (see appendix A).

Since several different types of standard and test lamps will be referred to in this report, it will be convenient to identify them here.

NBS Incandescent Standards: The 200 watt incandescent flux standards that are used at NBS in spectroradiometric work.

NBS CW Standards: The eleven type F40Tl2 cool white (CW) fluorescent lamps spectroradiometrically calibrated for luminous flux by using the NBS Incandescent Standards. These are the lamps referred to in section 1.1.

ETL CW Standards: The eighty lamps of type F40Tl2 CW, also referred to in section 1.1 , that were assigned luminous flux values on the basis of the NBS CW Standards by ETL.

Intercomparison CW Lamps: The two cool white fluorescent lamps supplied directly by NBS to the participating laboratories for this intercomparison.

Intercomparison Daylight Lamps: The daylight fluorescent lamps supplied by NBS.

Intercomparison Incandescent Lamps: The 200 watt incandescent lamps supplied by NBS.

Choke-Ballast: The fixed inductance choke-ballast that was supplied by NBS for use with the Intercomparison CW Lamps and the Intercomparison Daylight Lamp.

The genealogy of these lamps is given in figure l.l. The calibration on most of the lamps that were a part of this intercomparison can be traced back to the NBS 6807 group of incandescent luminous flux standards. This does not apply to the two laboratories in which ETL CW Standards were not used as a base, Laboratories 6 and 9.

Together with the incandescent and fluorescent intercomparison lamps and the choke-ballast, each participating laboratory was supplied with the experimental design and data sheets for each part of the intercomparison. A copy of the instructions and data sheets sent to each laboratory is attached as appendix A. Each participating laboratory also filled out a questionnaire on the type of equipment and procedures that were used. Appendix $B$ is $a$ copy of the questionnaire.

The intercomparison lamps were first measured at NBS by using both spectroradiometry and conventional substitution photometry. They were then measured at the participating laboratories where the fluorescent lamps were set up in the same lamp and choke-ballast combinations. The data and the lamps were returned to NBS, where the lamps were measured again. Measurements were made according to a statistical design.

The measurements taken at NBS before the lamps were sent out will be hereafter referred to as the "Initial" measurements; those taken at the laboratories will be referred to as "Laboratory" measurements; and those taken at NBS after the lamps were returned will be called "Repeat" measurements. Only Initial and Laboratory spectroradiometric measurements were taken on a 25 cm section of the fluorescent lamps. The data from the participating laboratories were to be returned untreated to NBS so that they could be reduced in a similar manner for all the laboratories. Unfortunately, due to the many different forms in which the data were received, the analysis of the data was different for each laboratory.


### 2.1. Conventional photometric measurements

The fluorescent lamps, that is, the cool white and daylight lamps, were measured photometrically at NBS in a 2 meter ( 80 inch) sphere by using the NBS Incandescent Standards and the NBS CW Standards. A circuit diagram is given in figure 2.1. A high impedance, true RMS differential voltmeter was used for measuring lamp voltage. The "restoration of light" method (ref. l) was, therefore, not required for lamp voltage measurements. Readings were taken both with and without an external color correcting filter. The ETL CW Standard lamps were operated on a Sylvania reference ballast and the fluorescent intercomparison lamps were operated on the choke-ballast. The same lamp and ballast combination was maintained throughout the period of the intercomparison.

During the Initial and Repeat measurements at NBS, NBS Incandescent Standards were used for the spectroradiometric transfers and the NBS CW Standards were used for the conventional photometric transfers.

### 2.2. Spectrcradiometric measurements

A block diagram of the spectroradiometer is given in figure 2.2. The spectroradiometer consisted of a 20 cm diameter sphere connected to the entrance slit of the monochromator. The inside of this sphere was coated with about 0.5 mm of barium sulphate powder which contained no binder, since binders tend to absorb radiation in the blue region of the spectrum. A 7.5 cm diameter aperture served to admit light from the measurement source into the sphere, perpendicular to the optical axis of the monochromator. The measurement source in this case was a lamp inside a 2 meter integrating sphere. The light was diffused inside the smaller collecting sphere and thus depolarized. The use of a collecting sphere minimized problems of alignment. Filters were inserted between the collecting sphere and the monochromator to eliminate second order spectra. However, this procedure was not followed in the 25 cm section measurements.

The monochromator used was a double grating instrument. Baffling along the optical path inside the monochromator served to reduce scattered radiation. The scattered radiation was further reduced by controlling the entrance slit height so that the radiation coming through the slit barely filled the first mirror in the monochromator. The entrance and exit slits were about equal and were approximately 5 nm in spectral bandpass.

The wavelength scale of the monochromator was calibrated against a set of standard emission lines to within an estimated uncertainty of $\pm 0.1 \mathrm{~nm}$. The photonultiplier tube used in the spectroradiometer had an $S-20$ cathōde and was selected for high sensitivity in the $600-800 \mathrm{~nm}$ region of the spectrum. The current from this photomultiplier tube was measured by a picoammeter that employed a cathode-follower type of amplifier for currents greater than $10^{-8} \mathrm{~A}$, and an operational amplifier for currents less than $10^{-8}$ A. Since the picoammeter did not modulate the incoming signal to amplify it, problems arising from phase-difference effects between the source (if operated on power other than direct current) and the modulating signal of the amplifier were eliminated. The output of the picoammeter was connected to a stable resistor and the voltage drop across this resistor was measured by a digital voltmeter.

In order to monitor the drift in the electronics and photomultiplier tube sensitivity, a 200 watt quartz halogen lamp set at constant voltaqe was referenced by the spectroradiometer simply by rotating the collecting sphere. During the course of a run, readings were taken of the monitor lamp at 560 nm before, after, and during a run. If the difference was more than about $0.2 \%$ the run was aborted. The gain on the picoammeter was adjusted for each run so that the voltmeter reading for the monitor lamp was 0.8 of full scale. All the spectroradiometric data were reduced by using the following assumptions:

1) The conditions were the same for both the test and standard sources (that is, no change in monochromator, sphere, detector, background, gain, instrument bandwidth, etc.).

CIRCUIT USED FOR OPERATING FLUORESCENT LAMPS
FIGURE 2.1


## SPECTRORADIOMETRIC measurements at nbs

FIGURE 2.2
2) The relative spectral distribution of the incandescent standard is the same as the relative spectral distribution of a Planckian radiator at 2854 K .
3) Differences in beam geometry and polarization are eliminated by the entrance sphere.
4) The system response is linear at any given wavelength.

The last assumption leads to the conclusion that at a particular dial setting, $\Lambda_{1}$, the instrument reading, $R\left(\Lambda_{1}\right)$, is proportional to the spectral radiant flux admitted by the entrance aperture. That is,

$$
\begin{equation*}
R\left(\Lambda_{1}\right)=K \int_{\left(\lambda_{i}-b / 2\right)}^{\left(\lambda_{1}+b / 2\right)} \Phi_{\lambda} D(\lambda) \tau\left(\Lambda_{i}, \lambda\right) d \lambda \tag{2.1}
\end{equation*}
$$

where $D(\lambda)$ is the relative system response as a function of wavelength (detector response and sphere or background absorption), $\tau\left(\Lambda_{1}, \lambda\right)$ is the instrument transmittance as a function of $\lambda$ at the $\Lambda_{1}$ dial setting, $\phi_{\lambda}$ is the spectral radiant flux per wavelength interval of the source and $K$ is the instrument proportionality constant. The limits of integration are set by the instrument bandpass, b: outside these limits the instrument transmittance is effectively zero.

For an incandescent lamp (the standard source) or the continuum of a fluorescent lamp (the test source), $\phi_{\lambda}$ is a slowly varying function of $\lambda$. (The problem of the measurement of the mercury lines in a fluorescent lamp output will be treated separately.) It is also usually true that $D(\lambda)$ is a slowly varying function of $\lambda$. Within reasonable limits of accuracy these two functions may be assumed constant over the bandpass of the instrument. Therefore, eq. 2.1 becomes,

$$
R\left(\Lambda_{i}\right)=K \phi_{\lambda}\left(\lambda_{1}\right) D\left(\lambda_{1}\right) \int_{\left(\lambda_{1}-b / 2\right)}^{\left(\lambda_{1}+b / 2\right)} \tau\left(\Lambda_{1}, \lambda\right) d \lambda
$$

Let $R^{t}\left(\Lambda_{1}\right), R^{s}\left(\Lambda_{1}\right)$, and $\phi_{\lambda}^{t}\left(\lambda_{1}\right), \phi_{\lambda}^{S}\left(\lambda_{1}\right)$ be the instrument readings and fluxes for the test and standard sources respectively. Within the approximations used to derive eq. 2.2, therefore, the spectral radiant flux ratio is equal to the ratio of the instrument readings.

$$
\begin{equation*}
\frac{R^{t}\left(\Lambda_{1}\right)}{R^{s}\left(\Lambda_{1}\right)}=\frac{\phi_{\lambda}^{t}\left(\lambda_{1}\right)}{\phi_{\lambda}^{s}\left(\lambda_{1}\right)} \tag{2.3}
\end{equation*}
$$

If $\phi_{\lambda}^{S}\left(\lambda_{i}\right)$ is known for each dial setting $\Lambda_{1}$, then the spectral radiant flux of the source can be evaluated. Although $\phi_{\lambda}$ is not known directly, it can be obtained from the total luminous flux, $\Phi s$ which is known by comparison to the NBS luminous flux standards, and from the assumption that the standard source has the same relative spectral distribution, $B(\lambda)$, as a Planckian radiator at 2854 K. That is,

$$
\begin{equation*}
\phi_{\lambda}^{s}=K_{1} B(\lambda) \tag{2.4}
\end{equation*}
$$

The total luminous flux, $\Phi$, is defined in general as,

$$
\begin{equation*}
\Phi=K_{m} \int_{380}^{760} \phi_{\lambda} v(\lambda) d \lambda \tag{2.5}
\end{equation*}
$$

where $\mathrm{K}_{\mathrm{m}}$ is the maximum value of the spectral luminous efficacy ( 680 lumens per watt) and $V(A)$ is the CIE luminous efficiency function. The limits of integration are given in nanometers and are set by the definition of $V(\lambda)$. For the standard source the total luminous flux is, therefore,

$$
\begin{equation*}
\Phi^{s}=K_{1} K_{m} \int_{380}^{760} V(\lambda) B(\lambda) d \lambda \tag{2.6}
\end{equation*}
$$

This yields a value for $K_{1}$, so that eq. 2.4 becomes,

$$
\begin{equation*}
\phi_{\lambda}^{s}\left(\lambda_{1}\right)=\frac{B\left(\lambda_{1}\right) \Phi^{s}}{K_{m} \int V(\lambda) B(\lambda) d \lambda} \tag{2.7}
\end{equation*}
$$

Here $B\left(\lambda_{f}\right)$ is the value of $B(\lambda)$ (in relative power per wavelength interval) at the dial setting $\Lambda_{1}$. Using this result in eq. 2.3 the radiant flux per unit wavelength for the test source is:

$$
\begin{equation*}
\phi_{\lambda}^{t}\left(\lambda_{1}\right)=\frac{R^{t}\left(\Lambda_{1}\right)}{R^{s}\left(\Lambda_{1}\right)} \frac{B\left(\lambda_{1}\right) \Phi^{s}}{K_{m} \int V(\lambda) B(\lambda) d \lambda} \tag{2.8}
\end{equation*}
$$

In order to compute the total luminous flux of the test source from eq. 2.5, the integration over $\lambda$ (the wavelength) may be approximated by a summation over $\Lambda_{1}$, (the wavelength dial setting). The total luminous flux of the test source is, therefore,

$$
\begin{equation*}
\Phi^{t}=K_{m} \sum_{380}^{760} \phi_{\lambda}^{t}\left(\lambda_{1}\right) V\left(\lambda_{1}\right) \Delta \Lambda \tag{2.9a}
\end{equation*}
$$

Combined with eq. 2.8 , it becomes:

$$
\begin{equation*}
\Phi^{t}=\sum_{380}^{760} \frac{R^{t}\left(\Lambda_{1}\right)}{R^{s}\left(\Lambda_{1}\right)} \frac{V\left(\lambda_{1}\right) B\left(\lambda_{1}\right) \Phi^{s}}{\int V(\lambda) B(\lambda) d \lambda} \Delta \Lambda \tag{2.9b}
\end{equation*}
$$

The limits of summation in nanometers are again set by the definition of $V\left(\lambda_{1}\right)$, the value of $V(\lambda)$ at $\Lambda_{i}$. The summation interval, $\Delta \Lambda$, which is the analog of di, remains to be chosen. This interval does not have to be the same as the instrument bandpass; in fact, for this intercomparison it was chosen to be about twice as big: the summation interval was 10 nm , and the bandpass was
approximately 5 nm . The same assumption, however, applies to both: the wavelength dependent instrument response and spectral radiant flux are assumed constant over the interval of summation and the bandpass. Choosing the summation interval fixes the dimensions of the $\phi_{\lambda}$ values to be used. In this case the dimensions of $\phi \sum_{\lambda}^{( }\left(\lambda_{i}\right)$ and $\phi f\left(\lambda_{i}\right)$ are watts per 10 nm .

Note once again that the approximations which led up to eq. 2.9b were for a source without narrow lines. In order to treat the mercury lines present in the output of a fluorescent lamp, eq. 2.1 must be re-examined. For a dial setting at one of the mercury lines, $\Lambda_{m}$, the equation becomes:

$$
\begin{equation*}
R^{t}\left(\Lambda_{m}\right)=k \int_{\left(\lambda_{m}-b / 2\right)}^{\left(\lambda_{m}+b / 2\right)} D(\lambda) \tau\left(\Lambda_{m}, \lambda\right) d \lambda \tag{2.10}
\end{equation*}
$$

Since the mercury lines are much narrower than the instrument bandpass, the integrand is zero everywhere except at one wavelength, $\lambda_{\text {II }}$. Equation 2.10 can be rewritten as,

$$
\begin{equation*}
R^{t}\left(\Lambda_{m}\right)=K \phi^{t}\left(\lambda_{m}\right) D\left(\lambda_{m}\right) \tau\left(\Lambda_{m}, \lambda_{m}\right) \tag{2.11}
\end{equation*}
$$

Note that $\phi t\left(\lambda_{m}\right)$ has been written without a subscript since it no longer is flux per wavelength interval--it is flux per mercury line. Dividing this by eq. 2.2 (written for a standard incandescent source) will obviously not yield the same cancellation that led to eq. 2.3. An additional experiment is necessary to evaluate the spectral radiant flux of a mercury line.

The experiment was performed as follows: By using the spectroradiometer, an analog plot of instrument reading versus dial setting was made of the output of a lamp having no continuum, only mercury line emission. The area under each plot of a mercury line was measured graphically. This area measurement is the value of the integral of the instrument reading as a function of the dial setting over the limits of the wavelength interval through which the mercury line is transmitted. That is,

$$
\begin{align*}
& \left(\Lambda_{m}+b / 2\right) \\
& \left.\int_{\left(R_{m}^{t}(\Lambda) d \Lambda=\right.} \int_{m}+b / 2\right)  \tag{2.12}\\
& \\
& \left.\Lambda_{m}-b / 2\right)\left(\Lambda_{m}\right) D\left(\lambda_{m}\right) \tau\left(\Lambda, \lambda_{m}\right) d \Lambda \\
& \left(\Lambda_{m}-b / 2\right)
\end{align*}
$$

In the integral on the right side of eq. 2.12 only the transmittance function, $\tau\left(\Lambda, \lambda_{m}\right)$, is a function of $\Lambda$. The transmittance function is a function of two variables: the wavelength of the radiation and the instrument dial setting. Furthermore, it is a slowly varying function of the dial setting. If the transmittance function is assumed to remain unchanged within small variations of the dial setting, then for a line source of variable wavelength the following equation is true:

$$
\int_{\left(\Lambda_{i}-b / 2\right)}^{\left(\Lambda_{i}+b / 2\right)} T\left(\Lambda_{i}\right) d \Lambda=\int_{\left(\lambda_{i}-b / 2\right)}^{\left(\lambda_{i}+b / 2\right)} t\left(\Lambda_{i}, \lambda\right) d \lambda
$$

That is, the integral of the transmittance function obtained by holding the line source wavelength fixed and varying the dial position is equal to the integral obtained by fixing the dial setting and varying the wavelength of the line source. With this assumption eq. 2.12 becomes

$$
\begin{array}{ll}
\left(\Lambda_{m}+b / 2\right) & \left(\lambda_{m}+b / 2\right) \\
\int_{R^{t}(\Lambda) d \Lambda=K \phi^{t}\left(\lambda_{m}\right) D\left(\lambda_{m}\right)} \int_{\left(\Lambda_{m}-b / 2\right)}^{\tau\left(\Lambda_{m}, \lambda\right) d \lambda}  \tag{2.14}\\
\left(\lambda_{m}-b / 2\right)
\end{array}
$$

Since the left side of this equation represents an area, it can be approximated by the product of two numbers. Choosing a specific instrument reading, for instance, $\mathrm{R}^{t}\left(\Lambda_{\mathrm{m}}\right)$, the reading at the mercury line wavelength, determines the value of the multiplicative constant to be used to obtain an area measurement from a single instrument reading. This factor, beff, termed the effective bandpass, will be unique for each mercury line and can now be used in the approximation of the integral on the left side of eq. 2.14 for any source containing mercury lines. This is, of course, only true if the characteristics of the instrument remain constant between the two experiments.

In order to compare eq. 2.14 to eq. 2.2 written for the standard incandescent source, the units of $\phi^{t}\left(\lambda_{m}\right)$ must be adjusted to the summation interval chosen for $\phi_{\lambda}^{S}\left(\lambda_{\mathrm{m}}\right)$. Dividing both sides of eq. 2.14 by $\Delta \Lambda$ will change the flux per mercury line to flux per wavelength interval, or $\phi f_{\lambda}\left(\lambda_{m}\right)$. Division of the adjusted version of eq. 2.14 by eq. 2.2 leads to:

$$
\begin{equation*}
\frac{R^{t}\left(\Lambda_{m}\right) b_{\text {eff }}}{R^{s}\left(\Lambda_{m}\right) \Delta \Lambda}=\frac{\phi_{\lambda}^{t}\left(\lambda_{m}\right)}{\phi_{\lambda}^{s}\left(\lambda_{m}\right)} \tag{2.15}
\end{equation*}
$$

Every term in this equation, except for the spectral radiant flux of the mercury line, has a known value. The $\phi \delta\left(\lambda_{m}\right)$ values in eq. 2.15 can now be included in the summation of eq. 2.9a as additional $\phi \underset{\lambda}{t}\left(\lambda_{1}\right)$ values.
For the NBS spectroradiometer, the effective bandpass. beff, was measured for each mercury line and found to be: 5.84 nm at 405.0 nm (doublet); 5.53 nm at $435.8 \mathrm{~nm} ; 5.48 \mathrm{~nm}$ at 546.1 nm ; and 5.93 nm at 578.0 nm (doublet). The mercury line spectral radiant flux values listed in the tables in section 4 were adjusted to a 10 mm interval.

In the measurement of the mercury line flux above the continuum of a fluorescent lamp, the instrument reading produced by the continuum at that point was interpolated by fitting a quadratic polynomial to three instrument readings in the vicinity of the line. The instrument reading produced by the mercury line was calculated by subtracting the interpolated continuum value from the experimental instrument reading at the mercury line wavelength setting.

As indicated above, two of the four mercury lines in a fluorescent lamp output are actually double lines. The treatment of these doublets is a simple extension of the previous discussion. When eq. 2.12 is rewritten for two mercury lines at $\lambda_{j}$ and $\lambda_{k}$ it becomes:

$$
\begin{aligned}
& \int_{(A+C)}^{(A-C)} R^{t}(\Lambda) d \Lambda=K \int_{(A-C)}^{(A+C)}\left[\phi^{t}\left(\lambda_{j}\right) D\left(\lambda_{j}\right) \tau\left(\Lambda, \lambda_{j}\right)+\phi^{t}\left(\lambda_{k}\right) D\left(\lambda_{k}\right) \tau\left(\Lambda, \lambda_{k}\right)\right] d \Lambda, ~
\end{aligned}
$$

$$
A=\left(\Lambda_{j}+\Lambda_{k}\right) / 2
$$

and

$$
c=\left(b+\Lambda_{j}-\Lambda_{k}\right) / 2
$$

Since the mercury line separation is less than the instrument bandpass, the assumptions that have been made about the behavior of the functions can be applied in eq. 2.16. Namely,

$$
D\left(\lambda_{j}\right)=D\left(\lambda_{k}\right)
$$

and

$$
\tau\left(\Lambda, \lambda_{j}\right)=\tau\left(\Lambda, \lambda_{k}\right)
$$

Equation 2.16 reduces to

$$
\begin{align*}
& \int_{(A-C)}^{(A+C)} R^{t}(\Lambda) d \Lambda=R D\left(\lambda_{j}\right)\left[\phi^{t}\left(\lambda_{j}\right)+\phi^{t}\left(\lambda_{k}\right)\right] \int_{(a-c)}^{(a+c)} \tau\left(\Lambda_{j}, \lambda\right) d \lambda
\end{align*}
$$

where $a$ and $c$ are defined with respect to $\lambda$ in the same manner as $A$ and $C$ were defined with respect to $\Lambda$. By choosing a specific instrument reading (not necessarily at the wavelength of either mercury line)an effective bandpass is determined and an equation similar to eq. 2.15 can be derived where the unknown flux will be the sum of the spectral radiant fluxes of the two mercury lines.

In order to check the validity of measuring the mercury doublets as a single line, the spectroradiometric measurements were repeated with a smaller instrument bandpass (narrower slits). This resolved the doublets and allowed them to be treated as single lines. The results of these two measurements were identical within the uncertainty of the measurement.

### 2.3. Analysis of the NBS measurements

The photocell data were reduced by using the five NBS Cool White Standards which were retained at NBS. For the spectroradiometric measurements, NBS Incandescent Standards were used. First the data were analyzed to determine if the luminous flux of the lamps remained constant throughout the intercomparison. The results are listed in table 2.1 .

Initial minus Repeat luminous flux measurements at NBS


Table 2.3
Precision (standard deviation) of an NBS measurement of luminous flux

|  | Photocell <br> Without Filter <br> (lumens) | Photocell With Filter (lumens) | Spectroradiometer (lumens) |
| :---: | :---: | :---: | :---: |
| Initial | 19.1 | 21.7 | 26.5 |
| Repeat | 14.1 | 13.6 | 12.6 |
| F-Test | 1.83 | 2.5 | 4.4 |
| ```Significant* (s}\mp@subsup{}{}{2}\mathrm{ Before/s }\mp@subsup{}{}{2}\mathrm{ After)``` | ) Yes** | Yes | Yes |

*Significant at the $95 \%$ confidence level (F-test).
**Both numerator and denominator had more than 40 degress of freedom.

Next the data were analyzed to determine if any difference exists among the methods used. These results are given in table 2.2. In table 2.3, the results of a statistical analysis are given which determine the precision of each method for Initial and Repeat measurements. The final values assigned to the lamps were an average of the spectroradiometric and photocell-filter Initial and Repeat values equally weighted.

Note that in table 2.1 there appears a significant drift in cool white lamps in all the three measurement methods. This could be due to some change in the characteristic of the lamp in the time between the Initial and the Repeat measurements. The daylight lamps, however, appear to change only when measured by a photocell without an additional color correcting filter. This may be due to a change in the spectral characteristics of either the sphere or photocell in the interim between measurements.

Table 2.2 compares the different methods used. Since the standards used for conventional photometry were cool white lamps, it is understandable that for daylight lamps the photocell values are significantly different from the photocell with filter values. The close agreement between the spectroradiometric and photocell with filter values lends further credence to the claim that a sphere can be spectrally corrected by using a color correcting filter. A small but significant difference was detected between the photocell and the photocell with filter values for cool white lamps. This could be due to the fact that the original standards used were of one manufacturer and the test lamps were of another manufacturer. Though they are all cool white lamps, there may be some spectral difference between them. It may also be noted that the original standards were mixed gas lamps and the test lamps are argon filled. Although the ambient temperature was maintained at $25 \pm 1^{\circ} \mathrm{C}$, mixed gas lamps are believed to be more sensitive to changes in ambient temperature than argon filled lamps. This might be a contributing factor.

The standard deviations given in table 2.3 are calculated estimates of the standard deviation of a single measurement. The difference in the precision between the Initial and Repeat measurements may be due to the level of experience of the different operators for the two cases.

In addition to the spectroradiometer measurements made on the entire lamp operated inside an integrating sphere, measurements were also made on a 25 cm section of the lamp operated inside a half-cylindrical enclosure. The enclosure was double shielded against drafts by wire nets. The base of this enclosure was baffled to enable the collecting sphere of the spectroradiometer to sample a 25 cm section of the lamp. Figure 2.3 is a diagram of this enclosure.

The spectroradiometric data were analyzed to yield values for of color temperature*, the $x$ and $y$ chromaticity coordinates, and, for the sphere measurements, total luminous flux.

Statistical tests were conducted to check whether there were significant differences between Initial and Repeat values for color temperature and chromaticity coordinates. Table 2.4 gives the Initial minus Repeat values for the measurements of color temperature and the $x$ and $y$ chromaticity coordinates for both cool white and daylight lamps. As in table 2.1, where the Initial and Repeat total luminous flux differed more for cool white lamps than for the daylight lamps, the cool white lamps seems to have changed significantly in the three color parameters. The daylight lamps have changed significantly in two: the $x$ chromaticity coordinate and color temperature. A change in the characteristics of the lamp and ballast combination resulting in a spectral change in lamp output could account for both the color change and the change in total luminous flux.

The NBS values for color parameters were assigned from the average of both the Initial and Repeat spectroradiometric sphere measurements. The 25 cm section values were not used for this purpose. Because only the Initial measurements were performed, the 25 cm section values were not included in the average.

[^1]
ENCLOSURE FOR MEASUREMENTS ON A 25 cm SECTION OF A
FLUORESCENT LAMP.
FIGURE 2.3

Table 2.4
Initial minus Repeat values of color parameter sphere measurements at NBS

| Parameter | Cool White |  | Daylight |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Difference | $\begin{gathered} \text { Significant* } \\ \text { Yes No } \end{gathered}$ | Difference | $\begin{gathered} \text { Significant* } \\ \text { Yes No } \end{gathered}$ |
| Color Temp. | 29.9K | x | 35.4 K | x |
| x | -0.0009 | x | -0.0006 | x |
| Y | 0.0009 | x | -0.0003 | x |

Table 2.5
Initial sphere measurements minus Initial 25 cm section measurements of color parameters at NBS

| Parameter | Cool White |  | Daylight |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Difference | $\begin{aligned} & \text { Significant* } \\ & \text { Yes No } \end{aligned}$ | Difference | $\begin{gathered} \text { Significant* } \\ \text { Yes No } \end{gathered}$ |
| Color Temp. | 16.0K | x | -5.4K | x |
| x | -0.0003 | x | 0.00002 | x |
| Y | 0.0013 | x | 0.0009 | X |

*Significance at the $95 \%$ confidence level (t-test). Note that the number of cool white lamps tested was twice that of the daylight lamps.

Their use would, of course, have weighted the final averages in favor of the Initial measurements.

Table 2.5 gives the Initial readings inside an integrating sphere minus the 25 cm section readings. The purpose of this comparison is to determine whether color temperature and chromaticity coordinate determined by a total flux measurement are comparable with their determination from a 25 cm section measurement. (At many laboratories measurement of chromaticity coordinates is typically performed with a Barnes Colorimeter which utilizes a 25 cm section of the lamp.) Table 2.5 indicates that the color parameters obtained by the two methods did not differ significantly for daylight lamps, but that the opposite was true for cool white lamps.

### 3.1. Comparison of the photometric and spectroradiometric equipment used

Though the general photometric setup was similar in most laboratories, there still were some significant differences in both the equipment and the measurement procedures. The differences were more marked in the spectroradiometric equipment and methods among the various laboratories. In this section the photometric equipment used by participating laboratories will be described. A brief description will then be given of each of the spectroradiometers.

Tables 3.1 to 3.3 sumarize the equipment used at the various laboratories for the measurements in part 1 of the intercomparison. Laboratories 2 and 4 have reported using external color correcting filters to correct for the wavelength dependence of sphere reflectivity and window absorption. The effects of using these filters will be more clearly brought out in the discussion of the results.

Laboratory 1 normally applies a mathematical correction to their data. The method is based on a separate determination of the wavelength dependence of sphere reflectivity, window absorption, the emission of the source, and the detector response. They did not apply this correction to any of the data submitted for this intercomparison, however, since the correction was relatively small.

All except Laboratory 1 used Weston photocells as detectors; five used the model 856 V (hermetically sealed) and two used model 594V. All Weston cells were equipped with Viscor filters. It should be noted that hermetically sealed photocells are not sensitive to humidity variations and are less sensitive to temperature variation (ref. 2).

Photocell output was read at most laboratories by a potentiometer device. Laboratory 5 used an operational amplifier and digital voltmeter combination. Only Laboratory 6 applied any linearity corrections to their photocell data.

All except Laboratory 6 warmed up the lamps for at least 15 minutes. All the laboratories measured the ambient temperature periodically, though the locations at which this was measured varied from laboratory to laboratory. Only Laboratories 2 and 3 indicate having temperature control. The location at which ambient temperature should be measured and the extent to which it should be controlled still constitute problems. Different types of lamps behave differently with a change in ambient temperature and it is not clear what is meant by the ambient temperature inside an integrating sphere. Most spheres, particularly larger ones, will have a temperature gradient even when the temperature at the sensor is controlled. The light output of a fluorescent lamp is a function of the wall temperature at the coldest point on the bulb. No completely satisfactory measurement has been made of this parameter.

Detailed descriptions of spectroradiometric equipment and techniques can be found in the papers of Thorington, et al., (ref. 3), and Sanders and Gaw (ref. 4). The spectroradiometric equipment that was used for this intercomparison by each of the laboratories participating in the spectroradiometric intercomparison will now be described briefly.

LABORATORY 1: This laboratory used two different monochromators in making measurements for this intercomparison. Measurements for part 2 of the intercomparison were made by using a custom built czerny-Turner type monochromator. In measurements for part 3 of the intercomparison, the lines in the spectrum were measured by using the custom made monochromator and the continuum was measured with a Leiss double prism monochromator with flint glass prisms. Wavelength calibration was performed before every run with the 435.8 nm and 546.1 nm mercury lines. Both monochromators employed a photomultiplier with an S-20 response (EMI-9558Q) as the detector. The detector ouptut for the custom made grating monochromator was amplified and displayed on an $L \& N$ type G, series 6000 recorder and amplifier. For the Leiss monochromator the detector output was amplified by a Keithley 610 electrometer and read on a Vidar 610 digital voltmeter and recorded on punched paper tape.

Sphere equipment used in the participating laboratories for photometric measurements.

| Laboratory | Diameter | Coating | Date Coated (See Note) | External Color Correcting $\qquad$ | Window |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1.5 meter | G.E. Paint* | July 1968 | None $* * * *$ | 1.5 mm ground glass |
| 2 | 3 meter | Burch** | July 1968 | Wratten 78C | None*** |
| 3 | 3 meter | Burch | Nov. 1967 | None | 3 mm pot opal |
| 4 | 1.5 meter | Burch | Oct. 1968 | Corning 5900 | 3 mm flashed opal |
| 5 | 2 meter | Burch | Aug. 1968 | None | Opal |
| 6 | 2.1 meter | Mg 0 | 1967 | None | Depolished opal |
| 7 | 1.8 meter | Burch | Aug. 1968 | None | 3 mmg ground glass |
| 8 | 3 meter | Burch | Aug. 1967 | None | None*** |

[^2]Table 3.2
Photocells used in the participating laboratories for photometric measurements

| Laboratory | Type | Linearity Correction | Dectector Read Out |
| :---: | :---: | :---: | :---: |
| 1 | GE-PV-1 | None | Standard Current Balance |
| 2 | Weston 856 V | None | Operational Amplifier \& Digital Voltmeter |
| 3 | Weston 856V | None | Rubicon Bridge |
| 4 | Weston 856 V | None | Rubicon Bridge |
| 5 | Weston 594V | None | ```Operational Ampli- fier & Digital Voltmeter``` |
| 6 | Weston 594V | Yes | K-2 Potentiometer |
| 7 | Weston 856 V | None | Rubicon Bridge |
| 8 | Weston 856V | None | Rubicon Bridge |

Table 3.3
Lamp operation and temperature control during photometric measurements at the participating laboratories

| Laboratory | Lamp Operation |  | Temperature |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Power | Ballast for | Sensor |  | Control |
|  | Regulation | Standards | Type | Location |  |
| 1 | 0.1\% | Sylvania Reference | Hg -thermometer | $10 \mathrm{~cm} \text { from wall on }$ lamp axis | -- |
| 2 | 1\% | Sylvania Reference | Hg-thermometer \& thermocouple | $\begin{aligned} & 30 \mathrm{~cm} \text { below lamp } \\ & 45 \mathrm{~cm} \text { above lamp } \end{aligned}$ | $\pm 0.5^{\circ} \mathrm{C}$ |
| 3 | 0.1\% | Sylvania Reference | Hg-thermometer \& thermocouple | 45 cm below at one end | $\pm 0.2{ }^{\circ} \mathrm{C}$ |
| 4 | 0.15\% | Sylvania Reference | Hg -thermometer | 5 cm from sphere wall in central plane | -- |
| 5 | 0.25\% | Sylvania Reference | Hg-thermometer | 15 cm above lamp at end | - - |
| 6 | 1\% | Sylvania Reference | Hg -thermometer | 45 cm below lamp from center | - - |
| 7 | 0.1\% | Sylvania Reference | Hg-thermometer | 20 cm above lamp at one end | - - |
| 8 | - - | Sylvania Reference | - - | - - | - - |

LABORATORY 2: The basic dispersing unit used by this laboratory is an Ebert type monochromator (Perkin Elmer model E-l) with a 10 cm diameter diffusing sphere at the entrance slit. NBS standard filters were used to calibrate the wavelength. The last calibration took place about a year before this intercomparison. A photomultiplier tube with an $S-20$ response (EMI-9558Q) was used as the detector. The signal from the detector was amplified and integrated over 2 nm intervals and recorded on punched paper tape.

LABORATORY 4: In this laboratory a Hilger Watts model D-300 quartz double monochromator with a variable speed wavelength drive was used as the basic dispersing unit. The manufacturer's wavelength calibration was checked by using $\mathrm{Hg}, \mathrm{Cd}, \mathrm{He}, \mathrm{Ne}$, and Rb line sources. A 9.3 cm diameter sphere was used before the entrance slit of the monochromator to collect and diffuse the light. A photomultiplier with a quartz window and an $S-20$ response (RCA-7265) was used as the detector. The incoming light was chopped at 90 Hz and the signal from the detector after a-c preamplification and amplification was recorded on an $x-y$ chart recorder.

LABORATORY 5: This laboratory used a Bausch and Lomb model 33-86-45 Ebert type grating monochromator. A 25 cm integrating box, coated with $3 M$ "Velvet White", was placed before the entrance slit of the monochromator. The wavelength scale was calibrated to within 1 nm by using mercury lines. A photomultiplier tube with an S-20 response (EMI-9558QB) was used as the detector. The output signal from the photomultiplier was amplified by using a Keithley model 610 DC electrometer and displayed on an Esterline - Augus Ellols chart recorder.

LABORATORY 7: This laboratory used a single prism monochromator (Beckman model DK-1) which was wavelength calibrated at the time of measurement by using the 546.1 nm mercury line. A photomultiplier tube with an $\mathrm{S}-10$ response (RCA 6217) was used as the detector. The signal from the detector was amplified by a Keithley model 6l0A DC electrometer and displayed on a chart recorder.

LABORATORY 9: In this laboratory a quartz prism Hilger Watts model D-300 monochromator was used with an S-20 response photomultiplier tube (EMI-9558QB). The wavelength scale was calibrated to $\pm 0.2 \mathrm{~nm}$ by using 60 lines of the $\mathrm{Ru}, \mathrm{Hg}$, Cs, Kr, Ar, and Ne spectra. The current output from the photomultiplier was amplified by a Dymec type 2411 A amplifier, the output of which was measured by a digital voltmeter (Dymec, type 2401B). The voltmeter then sent a BCD output to a card punch.

### 3.2. Comparison of the measurement procedures used

PART 1: Photometric intercomparison of 40 watt fluorescent lamps by conventional methods.

In order to standardize the experimental methods in the various participating laboratories, each laboratory was supplied with an experimental design and the necessary data sheets (appendix A). Fart 1 of the interlaboratory check involved three days of measurements at each laboratory. Over the course of a day six ETL CW standards (or other lamps held as standards by the laboratory) were measured against the two cool white and one daylight fluorescent, and the 200 watt incandescent intercomparison lamps. Each intercomparison lamp was measured twice in the course of a day. Over a period of three days, therefore, the fluoresent intercomparison lamps and the incandescent intercomparison lamp had each been measured six times. The data were analyzed in blocks of one day's run. A calibration factor was obtained by taking the ratio of the instrument reading and the assigned luminous flux of the six ETL CW Standards for substitutes). An average of these calibration factors was used to compute the luminous flux of the other test lamps that were measured that day. The data from all the participating laboratories were analyzed in the same manner. Only Laboratory 6 submitted linearity corrections for their photocell. These corrections, which were on the order of $2.5 \%$, were used in the analysis of their data.

In order to check for any drifts that might be present during the course of a day's run all the data were corrected for linear drift in the sphere factors. Only in the case of Laboratory 3 did drift corrections improve precision--and then only for the daylight lamp. This one result was judged to be insignificant and it was, therefore, concluded that no appreciable linear drift existed at any of the participating laboratories. Linear drift corrections were not applied to any of the reported data.

PART 2: Spectroradiometric study of 40 watt fluorescent lamps inside an integrating sphere

This test was intended to give the maximum amount of information for the minimum amount of work. The procedure was to be as follows.

1) The data were to be taken at 10 nm intervals from 380 nm to 760 nm . These data were to be reported unreduced.
2) Data were to be taken at $405.0 \mathrm{~nm}, 435.8 \mathrm{~nm}, 546.1 \mathrm{~nm}$, and 578.0 nm . These data were to be reported with the appropriate effective bandpass.
3) The lamps were to be run in the order specified on the data sheets supplied with the lamps.

Because of variations in laboratory, equipment, and technique, this test procedure was not uniformly followed. Therefore, the data from each participating laboratory had to be modified in order to conform to the designed test.

LABORATORY 1: The data received were completely reduced. Data for all the wavelengths of interest were not taken, however, because of equipment limitations. A missing point at 490 nm was interpolated by using a quadratic polynominal fit to the points around this wavelength. The points missing from each end of the spectrum were set equal to zero. Since the fluorescent and the incandescent standard lamps were compared against the same set of reference lamps, the reduced data were treated as though they were unreduced. The mercury lines had already been adjusted for a 10 nm interval and were, therefore, treated in the same manner as the continuum.

LABORATORY 2: These data were the most difficult to reduce. The reported data were already reduced and the photometric flux (Y) had been normalized to 1000 lumens. The $Y$ values were subsequently obtained from this laboratory for each set of measurements. By using $Y$, the magnitude of the data was adjusted and the data were reduced again at NBS.

LABORATORY 4: These data were reported unreduced. The mercury line doublets which were supposed to be reported as a single measurement were reported as two separate lines. These separate measurements were combined to single values and then all the data were reduced at NBS. Corrections were also applied for apparent discrete changes in the gain factor within one standard lamp - test lamp run.

LABORATORY 5: Unreduced data were reported by this laboratory. The datum reported for a mercury line, however, was the area under an analog plot of the line minus that of the continuum. Since the data of interest were the instrument readings adjusted to a 10 nm interval, the reported data for the mercury lines were divided by 10 times the instrument reading for the continuum and then multiplied by the radiant flux of the continuum. The data were then reduced at NBS.

LABORATORY 7: These data were reported in three parts. The first part was the dark current of the photomultiplier, the second part was the relative reflectance of a reflecting plaque used only for the incandescent standards, and the third part included the first two parts plus the spectral radiant flux of the source. Therefore, the data from all three parts were combined to solve for the unreduced data and then reduced at NBS.

LABORATORY 9: This laboratory reported irradiance values relative to a quartz-halogen lamp. Since the same reference had been used for all measurements, these data were reduced at NBS in the same manner as untreated data.

PART 3: Spectroradiometric study of color on a 25 cm section of 40 watt fluorescent lamps

The 25 cm section data were treated the same way as the spectroradiometric data of Part 2. However, values were computed only for the color temperature and the $x$ and $y$ chromaticity coordinates.

PART 4: Check on systematic errors in conventional sphere photometry.
This part of the intercomparison was designed to provide information about the performance of the photometric equipment. This was obtained by using an additive design experiment (See sample data sheets for this part in appendix A). One block of data was to consist of five sphere measurements performed according to the following procedure:

| 1. | $C$ |
| :--- | :--- |
| 2. | $C+(I)$ |
| 3. | $C+I$ |
| 4. | (C) $+I$ |
| 5. | $I$ |

Where C refers to a cool white fluorescent lamp and I to an incandescent 200 watt lamp, both of which had been calibrated for total luminous flux by NBS. The parentheses refer to the presence of an unlighted lamp in the sphere. For example, the second step represents a measurement taken with a lighted cool white fluorescent lamp and an unlighted incandescent lamp in the integrating sphere.

PART 5: Barnes Colorimeter determination of the $x$ and $y$ chromaticity coordinates of 40 watt fluorescent lamps.

Barnes Colorimeter measurements were not made at NBS, nor was an experimental design established for this test. The purpose of these measurements was to compare this method to the spectroradiometric method of determining the $x$ and $y$ chromaticity coordinates.
4. RESULTS OF THE INTERCOMPARISON
4.1. Results and comparison of the luminous flux measurements

In this section, the data obtained from the participating laboratories for each part of the intercomparison are compared against the assignments made at NBS. First a comparison is made of the parameters that were obtained from the conventional photometric measurements and those obtained spectroradiometrically. The differences in spectral distribution of the intercomparison lamps as measured at NBS and at the participating laboratories are then discussed.

Total luminous flux of the test lamps was obtained both from the photocell readings and from the spectral distribution measurements. Table 4.1 gives a summary of the conventional photometric luminous flux measurements at each laboratory averaged for each day. Tables 4.2 through 4.9 give the detailed results obtained from each laboratory and the differences between the laboratory and NBS values. Table 4.10 gives the final average total luminous flux measurements obtained at each laboratory and the calculated estimate of standard deviation.

Figure 4.1 is a combined plot of the percent difference between the daily laboratory average and the NBS assignment of total luminous flux. The plots of all differences for each laboratory are given in figures 4.2 through 4.9.

Total luminous flux was also determined from spectroradiometric measurements. The spectroradiometric flux determinations are given in table 4.11. Plots of the differences of these values from the NBS assignments are given in figure 4.10, and on an expanded scale in figure 4.11.
Table 4.1

| Lab | $\underline{\text { Lamp }}$ | Lamp <br> Type | $\begin{gathered} \text { NBS } \\ \text { (lumens) } \\ \hline \end{gathered}$ | $\begin{gathered} \text { Lab } \\ \text { (1umens) } \end{gathered}$ | Difference | Per Cent Difference | Lab | Lamp | Lamp Type | $\begin{gathered} \text { NBS } \\ \text { (lumens) } \end{gathered}$ | $\begin{gathered} \text { Lab } \\ \text { (1umens) } \end{gathered}$ | Difference | Per Cent Difference |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 8797 | CWl | 2826.6 | 2797.8 | -28.9 | -1.0 | 5 | 8801 | CW1 | 2750.5 | 2791.0 | 40.5 | 1.5 |
|  |  |  |  | 2801.8 | -24.8 | -0.9 |  |  |  |  | 2788.0 | 37.5 | 1.4 |
|  |  |  |  | 2811.9 | -14.6 | -0.5 |  |  |  |  | 2787.5 | 37.0 | 1.3 |
|  | 8798 | CW2 | 2838.1 | 2861.1 | 23.0 | 0.8 |  | 8802 | CW2 | 2805.7 | 2839.5 | 33.8 | 1.2 |
|  |  |  |  | 2849.5 | 11.4 | 0.4 |  |  |  |  | 2844.5 | 38.8 | 1.4 |
|  |  |  |  | 2857.6 | 19.5 | 0.7 |  |  |  |  | 2846.5 | 40.8 | 1.5 |
|  | 8906 | D | 2473.7 | 2488.2 | 14.5 | 0.6 |  | 8908 | D | 2450.9 | 2409.5 | -41.4 | -1.7 |
|  |  |  |  | 2491.8 | 18.1 | 0.7 |  |  |  |  | 2414.0 | -36.9 | -1.5 |
|  |  |  |  | 2489.5 | 15.9 | 0.6 |  |  |  |  | 2410.0 | -40.9 | -1.7 |
| 2 | 8805 | CWl | 2794.8 | 2793.5 | - 1.3 | 0.0 | 6 | 8813 | CW1 | 2804.9 | 2298.5 | -506.4 | -18.1 |
|  |  |  |  | 2795.0 | 0.2 | 0.0 |  |  |  |  | 2256.6 | -548.3 | -19.5 |
|  |  |  |  | 2802.0 | 7.2 | 0.3 |  |  |  |  | 2252.2 | -552.7 | -19.7 |
|  | 8806 | CW2 | 2863.1 | 2864.0 | 0.9 | 0.0 |  | 8814 | CW2 | 2847.5 | 2265.5 | -582.0 | -20.4 |
|  |  |  |  | 2872.5 | 9.4 | 0.3 |  |  |  |  | 2249.7 | -597.8 | -21.0 |
|  |  |  |  | 2847.0 | -16.1 | -0.6 |  |  |  |  | 2257.1 | -590.4 | -20.7 |
|  | 8909 | D | 2479.7 | 2449.5 | -30.2 | -1.2 |  | 8913 | D | 2460.9 | 2062.9 | -398.0 | -16.2 |
|  |  |  |  | 2448.0 | -31.7 | -1.3 |  |  |  |  | 2041.2 | -419.7 | -17.1 |
|  |  |  |  | 2459.5 | -20.2 | -0.8 |  |  |  |  | 2054.1 | -406.8 | -16.5 |
| 3 | 8807 | CW1 | 2917.1 | 2912.3 | - 4.9 | -0.2 | 7 | 8795 | CW1 | 2902.5 | 2914.5 | 11.9 | 0.4 |
|  |  |  |  | 2923.9 | 6.9 | 0.2 |  |  |  |  | 2888.1 | -14.4 | -0.5 |
|  |  |  |  | 2929.8 | 12.7 | 0.4 |  |  |  |  | 2887.6 | -14.9 | -0.5 |
|  | 8808 | CW2 | 2897.8 | 2887.5 | -10.2 | -0.4 |  | 8796 | CW2 | 2505.2 | 2522.2 | 17.0 | 0.7 |
|  |  |  |  | 2907.6 | 9.8 | 0.3 |  |  |  |  | 2513.8 | 8.6 | 0.3 |
|  |  |  |  | 2912.5 | 14.7 | 0.5 |  |  |  |  | 2512.7 | 7.5 | 0.3 |
|  | 8910 | D | 2465.9 | 2392.9 | -73.1 | -3.0 |  | 8905 | D | 2472.5 | 2441.5 | -31.0 | -1.3 |
|  |  |  |  | 2390.7 | -75.2 | -3.1 |  |  |  |  | 2409.2 | -63.3 | -2.6 |
|  |  |  |  | 2392.0 | -73.9 | -3.0 |  |  |  |  | 2397.6 | -74.9 | -3.0 |
| 4 | 8809 | CW1 | 2783.2 | 2754.0 | -29.2 | -1.0 | 8 | 8803 | CW1 | 2836.1 | 2849.9 | 13.8 | 0.5 |
|  |  |  |  | 2773.3 | - 9.9 | -0.4 |  |  |  |  | 2816.6 | -19.5 | -0.7 |
|  |  |  |  | 2779.2 | - 4.0 | -0.1 |  |  |  |  | 2853.2 | 17.1 | 0.6 |
|  | 8810 | CW2 | 2841.9 | 2804.9 | -37.0 | -1.3 |  | 8804 | CW2 | 2858.3 | 2875.6 | 17.3 | 0.6 |
|  |  |  |  | 2834.1 | - 7.8 | -0.3 |  |  |  |  | 2861.6 | 3.3 | 0.1 |
|  |  |  |  | 2824.9 | -17.0 | -0.6 |  |  |  |  | 2864.3 | 6.0 | 0.2 |
|  | 8911 | D | 2481.5 | 2462.1 | -19.5 | -0.8 |  | 8908A | D | 2476.2 | 2442.2 | -34.0 | -1.4 |
|  |  |  |  | 2471.8 | - 9.7 | -0.4 |  |  |  |  | 2433.6 | -42.6 | -1.7 |
|  |  |  |  | 2470.7 | -10.8 | -0.4 |  |  |  |  | 2439.9 | -36.3 | -1. 5 |

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Table 4.2

Photometric measurement of total luminous flux--Laboratory 1.

| Lamp | $\begin{gathered} \text { NBS } \\ \text { (lumens) } \end{gathered}$ | $\begin{gathered} \text { Lab } \\ \text { (lumens) } \end{gathered}$ | Difference | Per Cent Difference |
| :---: | :---: | :---: | :---: | :---: |
| 8797 | 2826.3 | 2781.3 | -45.3 | -1.6 |
|  |  | 2814.2 | -12.4 | -0.4 |
|  |  | 2796.3 | -30.3 | -1.1 |
|  |  | 2807.3 | -19.3 | -0.7 |
|  |  | 2824.0 | - 2.6 | -0.1 |
|  |  | 2799.9 | -26.7 | -0.9 |
| 8798 | 2838.1 | 2890.1 | 52.0 | 1.8 |
|  |  | 2832.2 | - 5.9 | -0.2 |
|  |  | 2868.6 | 30.5 | 1.1 |
|  |  | 2830.4 | - 7.7 | -0.3 |
|  |  | 2848.0 | 9.9 | 0.3 |
|  |  | 2867.1 | 29.0 | 1.0 |
| 8906 | 2473.7 | 2491.7 | 18.0 | 0.7 |
|  |  | 2484.7 | 11.0 | 0.4 |
|  |  | 2486.8 | 13.1 | 0.5 |
|  |  | 2496.8 | 23.1 | 0.9 |
|  |  | 2505.1 | 31.4 | 1.3 |
|  |  | 2474.0 | 0.3 | 0.0 |

Table 4.3
Photometric measurement of total luminous flux--Laboratory 2.

| Lamp | $\begin{gathered} \text { NBS } \\ (1 \text { umens }) \end{gathered}$ | $\begin{gathered} \text { Lab } \\ \text { (1 lumens) } \end{gathered}$ | Difference | Per Cent Difference |
| :---: | :---: | :---: | :---: | :---: |
| 8805 | 2794.8 | 2795 | 0 | 0.0 |
|  |  | 2792 | - 3 | -0.1 |
|  |  | 2792 | - 3 | -0.1 |
|  |  | 2798 | 3 | 0.1 |
|  |  | 2800 | 5 | 0.2 |
|  |  | 2804 | 9 | 0.3 |
| 8806 | 2863.1 | 2887 | 24 | 0.8 |
|  |  | 2841 | - 22 | -0.8 |
|  |  | 2905 | 42 | 1.5 |
|  |  | 2840 | - 23 | -0.8 |
|  |  | 2844 | - 19 | -0.7 |
|  |  | 2850 | - 13 | -0.5 |
| 8909 | 2479.7 | 2449 | - 31 | -1.2 |
|  |  | 2450 | - 30 | -1.2 |
|  |  | 2442 | - 38 | -1.5 |
|  |  | 2454 | - 26 | -1.0 |
|  |  | 2462 | - 18 | -0.7 |
|  |  | 2457 | - 23 | -0.9 |


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Table 4.4
Photometric measurement of total luminous flux--Laboratory 3.

| Lamp | $\begin{gathered} \text { NBS } \\ \text { (1umens) } \end{gathered}$ | $\begin{gathered} \text { Lab } \\ \text { (lumens) } \end{gathered}$ | Difference | Per Cent Difference |
| :---: | :---: | :---: | :---: | :---: |
| 8807 | 2917.1 | 2919.8 | 2.7 | 0.1 |
|  |  | 2904.7 | -12.4 | -0.4 |
|  |  | 2927.0 | 9.9 | 0.3 |
|  |  | 2920.9 | 3.8 | 0.1 |
|  |  | 2936.9 | 19.8 | 0.7 |
|  |  | 2922.7 | 5.6 | 0.2 |
| 8808 | 2897.8 | 2889.6 | -8.2 | -0.3 |
|  |  | 2885.5 | -12.3 | -0.4 |
|  |  | 2892.6 | -5.2 | -0.2 |
|  |  | 2922.7 | 24.9 | 0.9 |
|  |  | 2922.7 | 24.9 | 0.9 |
|  |  | 2902.3 | 4.5 | 0.2 |
| 8910 | 2465.9 | 2400.4 | -65.5 | -2. 7 |
|  |  | 2385.3 | -80.6 | -3.3 |
|  |  | 2385.6 | -80.3 | -3.3 |
|  |  | 2395.7 | -70.2 | -2.8 |
|  |  | 2388.9 | -77.0 | -3.1 |
|  |  | 2395.1 | -70.8 | -2.9 |

Table 4.5
Photometric measurement of total luminous flux--Laboratory 4.

| Lamp | $\begin{gathered} \text { NBS } \\ \text { (1umens) } \end{gathered}$ | $\begin{gathered} \text { Lab } \\ \text { (1umens) } \end{gathered}$ | Difference | Per Cent Difference |
| :---: | :---: | :---: | :---: | :---: |
| 8809 | 2783.2 | 2751.2 | -32.0 | -1.1 |
|  |  | 2756.8 | -26.4 | -0.9 |
|  |  | 2775.7 | -7.5 | -0.3 |
|  |  | 2771.0 | -12.2 | -0.4 |
|  |  | 2781.1 | -2.1 | -0.1 |
|  |  | 2777.4 | -5.8 | -0.2 |
| 8810 | 2841.9 | 2831.3 | -10.6 | -0.4 |
|  |  | 2778.5 | -63.4 | -2.2 |
|  |  | 2833.7 | -8.2 | -0.3 |
|  |  | 2834.6 | -7.3 | -0.3 |
|  |  | 2823.1 | -18.8 | -0.7 |
|  |  | 2826.8 | -15.1 | -0.5 |
| 8911 | 2481.5 | 2461.1 | -20.4 | -0.8 |
|  |  | 2463.0 | -18.5 | -0.7 |
|  |  | 2476.5 | -5.0 | -0.2 |
|  |  | 2467.2 | -14.3 | -0.6 |
|  |  | 2472.6 | -8.9 | -0.4 |
|  |  | 2468.9 | -12.6 | -0.5 |

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Table 4.6
Photometric measurement of total luminous flux--Laboratory 5.

| Lamp | $\begin{gathered} \text { NBS } \\ \text { (1umens) } \end{gathered}$ | $\begin{gathered} \text { Lab } \\ \text { (1umens) } \\ \hline \end{gathered}$ | Difference | Per Cent Difference |
| :---: | :---: | :---: | :---: | :---: |
| 8801 | 2750.5 | 2794 | 43 | 1.6 |
|  |  | 2788 | 37 | 1.4 |
|  |  | 2788 | 37 | 1.4 |
|  |  | 2788 | 37 | 1.4 |
|  |  | 2787 | 36 | 1.3 |
|  |  | 2788 | 37 | 1.4 |
| 8802 | 2805.7 | 2835 | 29 | 1.0 |
|  |  | 2844 | 38 | 1.4 |
|  |  | 2846 | 40 | 1.4 |
|  |  | 2843 | 37 | 1.3 |
|  |  | 2852 | 46 | 1.7 |
|  |  | 2841 | 35 | 1.3 |
| 8908 | 2450.9 | 2411 | -40 | -1.6 |
|  |  | 2408 | -43 | -1.8 |
|  |  | 2418 | -33 | -1.3 |
|  |  | 2410 | -41 | -1.7 |
|  |  | 2411 | -40 | -1.6 |
|  |  | 2409 | -42 | -1.7 |

Table 4.7
Photometric measurement of total lumínous flux--Laboratory 6 .

| Lamp | NBS <br> (1umens) | Lab <br> (1umens) | Difference <br> 8813 | 2804.9 |
| :--- | :---: | :---: | :---: | :---: |

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Table 4.8
Photometric measurement of total luminous flux--Laboratory 7.

| Lamp | $\begin{gathered} \text { NBS } \\ \text { (lumens) } \end{gathered}$ | $\begin{gathered} \text { Lab } \\ \text { (lumens) } \end{gathered}$ | Difference | Per Cent Difference |
| :---: | :---: | :---: | :---: | :---: |
| 8795 | 2902.5 | 2918.5 | 16.0 | 0.6 |
|  |  | 2910.4 | 7.9 | 0.3 |
|  |  | 2895.1 | - 7.4 | -0.3 |
|  |  | 2881.1 | -21.4 | -0.7 |
|  |  | 2887.1 | -15.4 | -0.5 |
|  |  | 2888.1 | -14.4 | -0.5 |
| 8796 | 2505.2 | 2492.7 | -12.5 | -0.5 |
|  |  | 2551.8 | 46.6 | 1.9 |
|  |  | 2506.4 | 1.2 | 0.0 |
|  |  | 2521.3 | 16.1 | 0.6 |
|  |  | 2512.7 | 7.5 | 0.3 |
|  |  | 2512.7 | 7.5 | 0.3 |
| 8905 | 2472.5 | 2459.6 | -49.0 | -2.0 |
|  |  | 2459.6 | -12.9 | -0.5 |
|  |  | 2412.7 | -59.8 | -2.4 |
|  |  | 2405.7 | -66.8 | -2.7 |
|  |  | 2402.6 | -69.9 | -2.8 |
|  |  | 2392.6 | -79.9 | -3.2 |

Table 4.9
Photometric measurement of total luminous flux--Laboratory 8.

| Lamp | $\begin{gathered} \text { NBS } \\ \text { (1umens) } \end{gathered}$ | $\begin{gathered} \text { Lab } \\ (1 \text { umens }) \end{gathered}$ | Difference | Per Cent Difference |
| :---: | :---: | :---: | :---: | :---: |
| 8803 | 2836.1 | 2836.9 | 0.8 | 0.0 |
|  |  | 2862.9 | 26.8 | 0.9 |
|  |  | 2812.7 | -23.4 | -0.8 |
|  |  | 2820.6 | -15.5 | -0.5 |
|  |  | 2856.2 | 20.1 | 0.7 |
|  |  | 2850.3 | 14.2 | 0.5 |
| 8804 | 2858.3 | 2878.3 | 20.0 | 0.7 |
|  |  | 2872.9 | 14.6 | 0.5 |
|  |  | 2866.9 | 8.6 | 0.3 |
|  |  | 2856.2 | - 2.1 | -0.1 |
|  |  | 2850.3 | -8.0 | -0.3 |
|  |  | 2878.3 | 20.0 | 0.7 |
| 8908A | 2476.2 | 2440.2 | -36.0 | -1. 5 |
|  |  | 2444.2 | -32.0 | -1.3 |
|  |  | 2434.6 | -41.6 | -1.7 |
|  |  | 2432.6 | -43.6 | -1.8 |
|  |  | 2434.9 | -41.3 | -1.7 |
|  |  | 2444.9 | -31.3 | -1. 3 |

Table 4.10
Photometric measurement of total luminous flux-comprehensive average and standard deviation. for each participating laboratory.

| Laboratory | Lamp | Average <br> (lumens) | Standard Deviation (lumens) |
| :---: | :---: | :---: | :---: |
| 1 | CW1 - 8797 | 2804 | 14.9 |
|  | CW2 - 8798 | 2856 | 23.4 |
|  | D - 8906 | 2490 | 10.7 |
| 2 | CW1 - 8805 | 2797 | 4.8 |
|  | CW2 - 8806 | 2861 | 27.8 |
|  | D - 8909 | 2452 | 6.9 |
| 3 | CW1 - 8807 | 2922 | 10.5 |
|  | CW2 - 8808 | 2903 | 16.6 |
|  | D - 8910 | 2392 | 6.2 |
| 4 | CW1 - 8809 | 2769 | 12.1 |
|  | CW2 - 8810 | 2821 | 21.4 |
|  | D - 8911 | 2468 | 5.8 |
| 5 | CW1 - 8801 | 2789 | 2.6 |
|  | CW2 - 8802 | 2844 | 5.6 |
|  | D - 8908 | 2411 | 3.5 |
| 6 | CW1 - 8813 | 2269 | 23.5 |
|  | CW2 - 8814 | 2258 | 13.8 |
|  | D - 8913 | 2053 | 11.1 |
| 7 | CW1 - 8795 | 2897 | 14.7 |
|  | CW2 - 8796 | 2516 | 19.8 |
|  | D - 8905 | 2416 | 23.7 |
| 8 | CW1 - 8803 | 2840 | 20.1 |
|  | CW2 - 8804 | 2867 | 11.7 |
|  | D - 8908 | 2439 | 5.3 |

Spectroradiometeric, integrating sphere measurement of total luminous flux

| Laboratory | Lamp | $\begin{gathered} \text { NBS } \\ \text { (lumens) } \end{gathered}$ | Lab (lumens) | Difference | Per Cent Difference |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 8797 | 2827 | 2770 | - 57 | - 2.0 |
|  |  |  | 2808 | - 19 | - 0.7 |
|  |  |  | 2825 | - 2 | - 0.1 |
|  | 8798 | 2838 | 2851 | 13 | 0.5 |
|  |  |  | 2830 | - 8 | - 0.3 |
|  |  |  | 2823 | - 15 | - 0.5 |
|  | 8906 | 2474 | 2407 | - 67 | - 2.7 |
|  |  |  | 2424 | - 50 | - 2.0 |
|  |  |  | 2427 | - 47 | - 1.9 |
| 2 | 8805 | 2795 | 2611 | -184 | - 6.6 |
|  |  |  | 2587 | -208 | - 7.4 |
|  |  |  | 2604 | -191 | - 6.8 |
|  | 8806 | 2863 | 2685 | -178 | -6.2 |
|  |  |  | 2671 | -192 | - 6.7 |
|  |  |  | 2629 | -234 | -8.2 |
|  | 8909 | 2480 | 2341 | -139 | - 5.6 |
|  |  |  | 2337 | -143 | - 5.8 |
|  |  |  | 2305 | -175 | - 7.0 |
| 4 | 8809 | 2783 | 3183 | 400 | 14.4 |
|  |  |  | 3189 | 406 | 14.6 |
|  |  |  | 3183 | 400 | 14.4 |
|  | 8810 | 2842 | 3311 | 469 | 16.5 |
|  |  |  | 3321 | 479 | 16.9 |
|  |  |  | 3315 | 473 | 16.6 |
|  | 8911 | 2481 | 2914 | 432 | 17.4 |
|  |  |  | 2922 | 440 | 17.8 |
|  |  |  | 2913 | 431 | 17.4 |
| 5 | 8801 | 2750 | 2737 | - 13 | - 0.5 |
|  |  |  | 2748 | - 3 | - 0.1 |
|  |  |  | 2752 | 1 | 0.1 |
|  | 8802 | 2806 | 2782 | - 24 | - 0.8 |
|  |  |  | 2775 | - 31 | - 1.1 |
|  |  |  | 2800 | - 6 | - 0.2 |
|  | 8908 | 2451 | 2393 | - 58 | - 2.4 |
|  |  |  | $2394$ | - 57 | - 2.3 |
|  |  |  | 2548 | 97 | 4.0 |

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Fig. 4.10 NBS assignments compared to the spectroradiometric, integrating sphere measurements of total luminous
4.2. Results and comparison of the measurements of color
temperature and the $x$ and $y$ chromaticity coordinates

Color temperature and the $x$ and $y$ chromaticity coordinates were evaluated from the data obtained in parts 2 and 3 of the intercomparison; that is, from the spectroradiometric measurements of the lamp in an integrating sphere and of a 25 cm section of the lamp. The $x$ and $y$ chromaticity coordinates were also measured with a Barnes Colorimeter in part 5 of the intercomparison. Tables 4.12 through 4.21 contain the results of these three tests.

Table 4.12 gives the laboratory sphere determinations of color temperature and compares these with the NBS assignments. Figure 4.12 is a plot of this data.

The $x$ and $y$ chromaticity coordinates measured in the participating laboratories and assigned at NBS, as well as the differences between the two, are given in tables 4.13, 4.14, and figures 4.13, and 4.14.

Tables 4.15 and 4.16 present summaries of the precision of the spectroradiometric sphere measurements of total luminous flux, color temperature, and the $x$ and $y$ chromaticity coordinates.

Table 4.17 gives the laboratory evaluation of color temperature and the NBS assignment based on measurements of a 25 cm section of the lamps (part 3). Figure 4.15 gives a plot of the percent deviation of the laboratory values from the NBS values. Tables 4.18 and 4.19 and figures 4.16 and 4.17 present the same information for the $x$ and $y$ chromaticity coordinates. Tables 4.20 and 4.21 are summaries of the precision of 25 cm section measurements of color temperature and $x$ and $y$ chromaticity coordinates in the different laboratories. Table 4.22 gives a summary of the luminous flux measurements obtained by both the spectroradiometric and conventional photometric techniques.

Finally, tables $4.23,4.24$ and 4.25 give a summary of the average values obtained at NBS and at the participating laboratories for the color parameters measured in the intercomparison and the methods used to obtain them. These tables also contain the results of the Barnes Colorimeter measurements.

Table 4.12
Spectroradiometric, integrating sphere measurement of color temperature

| Laboratory | Lamp | $\begin{gathered} \text { NBS } \\ \text { (kelvins) } \end{gathered}$ | $\begin{gathered} \text { Lab } \\ \text { (kelvins) } \end{gathered}$ | Difference |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 8797 | 4059 | 4076 | 17 |
|  |  |  | 4066 | 7 |
|  |  |  | 4109 | 50 |
|  | 8798 | 4086 | 4127 | 41 |
|  |  |  | 4133 | 47 |
|  |  |  | 4061 | - 25 |
|  | 8906 | 6443 | 6584 | 141 |
|  |  |  | 6518 | 75 |
|  |  |  | 6527 | 84 |
| 2 | 8805 | 4110 | 4075 | - 35 |
|  |  |  | 3986 | -124 |
|  |  |  | 4095 | - 15 |
|  | 8806 | 4125 | 4100 | - 25 |
|  |  |  | 4097 | - 28 |
|  |  |  | 4093 | - 32 |
|  | 8909 | 6436 | 6351 | - 85 |
|  |  |  | 6319 | -117 |
|  |  |  | 6278 | -158 |
| 4 | 8809 | 4101 | 4175 | 74 |
|  |  |  | 4185 | 84 |
|  |  |  | 4184 | 83 |
|  | 8810 | 4085 | 4101 | 16 |
|  |  |  | 4104 | 19 |
|  |  |  | 4095 | 10 |
|  | 8911 | 6450 | 6413 | $-37$ |
|  |  |  | 6456 | 6 |
|  |  |  | 6446 | - 4 |
| 5 | 8801 | 4092 | 4144 | 52 |
|  |  |  | 4129 | 37 |
|  |  |  | 4134 | 42 |
|  | 8802 | 4100 | 4111 | 11 |
|  |  |  | 4144 | 44 |
|  |  |  | 4142 | 42 |
|  | 8908 | 6402 | 6291 | -111 |
|  |  |  | 6272 | -130 |
|  |  |  | 6457 | 55 |

Spectroradiometric, integrating sphere measurement of the $x$ chromaticity coordinate

| Laboratory | Lamp | NBS x | Lab x | Difference |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 8797 | 0.3800 | 0.3786 | -0.0014 |
|  |  |  | 0.3794 | -0.0006 |
|  |  |  | 0.3777 | -0.0023 |
|  | 8798 | 0.3794 | 0.3769 | -0.0025 |
|  |  |  | 0.3770 | -0.0024 |
|  |  |  | 0.3796 | 0.0002 |
|  | 8906 | 0.3131 | 0.3106 | -0.0025 |
|  |  |  | 0.3118 | -0.0013 |
|  |  |  | 0.3119 | -0.0012 |
| 2 | 8805 | 0.3783 | 0.3806 | 0.0023 |
|  |  |  | 0.3835 | 0.0052 |
|  |  |  | 0.3797 | 0.0014 |
|  | 8806 | 0.3774 | 0.3787 | 0.0013 |
|  |  |  | 0.3790 | 0.0016 |
|  |  |  | 0.3796 | 0.0022 |
|  | 8909 | 0.3133 | 0.3147 | 0.0014 |
|  |  |  | 0.3152 | 0.0019 |
|  |  |  | 0.3158 | 0.0025 |
| 4 | 8809 | 0.3786 | 0.3768 | -0.0018 |
|  |  |  | 0.3760 | -0.0026 |
|  |  |  | 0.3762 | -0.0024 |
|  | 8810 | 0.3794 | 0.3795 | 0.0001 |
|  |  |  | 0.3792 | -0.0002 |
|  |  |  | 0.3797 | 0.0003 |
|  | 8911 | 0.3131 | 0.3132 | 0.0001 |
|  |  |  | 0.3128 | -0.0003 |
|  |  |  | 0.3130 | -0.0001 |
| 5 | 8801 | 0.3790 | 0.3783 | -0.0007 |
|  |  |  | 0.3795 | 0.0005 |
|  |  |  | 0.3794 | 0.0004 |
|  | 8802 | 0.3787 | 0.3800 | 0.0013 |
|  |  |  | 0.3788 | 0.0001 |
|  |  |  | 0.3790 | 0.0003 |
|  | 8908 | 0.3137 | 0.3153 | 0.0016 |
|  |  |  | 0.3159 | 0.0022 |
|  |  |  | 0.3124 | -0.0013 |

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Spectroradiometric, integrating sphere measurement of the $y$ chromaticity coordinate

| Laboratory | Lamp | NBS y | $\underline{L a b} y$ | Difference |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 8797 | 0.3837 | 0.3805 | -0.0032 |
|  |  |  | 0.3820 | -0.0017 |
|  |  |  | 0.3816 | -0.0021 |
|  | 8798 | 0.3850 | 0.3811 | -0.0039 |
|  |  |  | 0.3824 | -0.0026 |
|  |  |  | 0.3822 | -0.0028 |
|  | 8906 | 0.3358 | 0.3329 | -0.0029 |
|  |  |  | 0.3341 | -0.0017 |
|  |  |  | 0.3326 | -0.0032 |
| 2 | 8805 | 0.3844 | 0.3881 | 0.0037 |
|  |  |  | 0.3865 | 0.0021 |
|  |  |  | 0.3880 | 0.0036 |
|  | 8806 | 0.3830 | 0.3845 | 0.0015 |
|  |  |  | 0.3852 | 0.0022 |
|  |  |  | 0.3869 | 0.0039 |
|  | 8909 | 0.3356 | 0.3370 | 0.0014 |
|  |  |  | 0.3380 | 0.0024 |
|  |  |  | 0.3395 | 0.0039 |
| 4 | 8809 | 0.3842 | 0.3870 | 0.0028 |
|  |  |  | 0.3856 | 0.0014 |
|  |  |  | 0.3865 | 0.0023 |
|  | 8810 | 0.3851 | 0.3879 | 0.0028 |
|  |  |  | 0.3870 | 0.0019 |
|  |  |  | 0.3878 | 0.0027 |
|  | 8911 | 0.3351 | 0.3381 | 0.0030 |
|  |  |  | 0.3370 | 0.0019 |
|  |  |  | 0.3373 | 0.0022 |
| 5 | 8801 | 0.3844 | 0.3899 | 0.0055 |
|  |  |  | 0.3919 | 0.0075 |
|  |  |  | 0.3922 | 0.0078 |
|  | 8802 | 0.3844 | 0.3909 | 0.0065 |
|  |  |  | 0.3922 | 0.0078 |
|  |  |  | 0.3917 | 0.0073 |
|  | 8908 | 0.3357 | 0.3424 | 0.0067 |
|  |  |  | 0.3433 | 0.0076 |
|  |  |  | 0.3410 | 0.0053 |

new


Spectroradiometric, integrating sphere measurement of luminous flux and color temperature--comprehensive average and standard deviation for each participating laboratory

| Laboratory | Lamp | $\begin{gathered} \text { Luminous } \\ \text { Flux } \\ \hline \end{gathered}$ | Standard Deviation | Color <br> Temperature | Standard Deviation |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 8797 | 2801 | 28 | 4084 | 23 |
|  | 8798 | 2835 | 15 | 4107 | 40 |
|  | 8906 | 2419 | 11 | 6543 | 36 |
| 2 | 8805 | 2601 | 12 | 4052 | 58 |
|  | 8806 | 2662 | 29 | 4097 | 4 |
|  | 8909 | 2328 | 20 | 6316 | 37 |
| 4 | 8809 | 3185 | 3 | 4181 | 6 |
|  | 8810 | 3316 | 5 | 4100 | 5 |
|  | 8911 | 2916 | 5 | 6438 | 23 |
| 5 | 8801 | 2746 | 8 | 4136 | 8 |
|  | 8802 | 2786 | 13 | 4132 | 19 |
|  | 8908 | 2445 | 89 | 6340 | 102 |

Table 4.16
Spectroradiometeric, integrating sphere measurement of the $x$ and $y$ chromaticity coordinates - comprehensive average and standard deviation for each participating laboratory

| Laboratory | Lamp | $\underline{x}$ | Standard Deviation | $y$ | Standard Deviation |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 8797 | 0.3786 | 0.0009 | 0.3814 | 0.0008 |
|  | 8798 | 0.3778 | 0.0015 | 0.3819 | 0.0007 |
|  | 8906 | 0.3114 | 0.0007 | 0.3332 | 0.0008 |
| 2 | 8805 | 0.3813 | 0.0020 | 0.3875 | 0.0009 |
|  | 8806 | 0.3791 | 0.0005 | 0.3855 | 0.0012 |
|  | 8909 | 0.3152 | 0.0006 | 0.3382 | 0.0013 |
| 4 | 8809 | 0.3763 | 0.0004 | 0.3864 | 0.0007 |
|  | 8810 | 0.3795 | 0.0003 | 0.3876 | 0.0005 |
|  | 8911 | 0.3130 | 0.0002 | 0.3375 | 0.0006 |
| 5 | 8801 | 0.3791 | 0.0007 | 0.3913 | 0.0013 |
|  | 8802 | 0.3793 | 0.0006 | 0.3916 | 0.0007 |
|  | 8908 | 0.3145 | 0.0019 | 0.3422 | 0.0012 |

Table 4.17
Spectroradiometric, 25 cm lamp section measurement of color temperature

| Laboratory | Lamp | $\begin{gathered} \text { NBS } \\ \text { (kelvins) } \end{gathered}$ | $\begin{gathered} \text { Lab } \\ \text { (kelvins) } \end{gathered}$ | Difference |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 8797 | 4080 | 3987 | - 93 |
|  |  |  | 3990 | - 90 |
|  |  |  | 4033 | - 47 |
|  | 8798 | 4070 | 3990 | - 80 |
|  |  |  | 3982 | - 88 |
|  |  |  | 4002 | - 68 |
|  | 8906 | 6507 | 6193 | - 314 |
|  |  |  | 6476 | - 31 |
|  |  |  | 6492 | - 15 |
| 2 | 8805 | 4093 | 4099 | 6 |
|  |  |  | 4098 | 5 |
|  |  |  | 4093 | 0 |
|  | 8806 | 4107 | 4122 | 15 |
|  |  |  | 4114 | 7 |
|  |  |  | 4116 | 9 |
|  | 8909 | 6457 | 6419 | - 38 |
|  |  |  | 6372 | - 85 |
|  |  |  | 6450 | - 8 |
| 4 | 8809 | 4111 | 4129 | 18 |
|  |  |  | 4090 | - 21 |
|  |  |  | 4070 | - 41 |
|  | 8810 | 4073 | 4083 | 9 |
|  |  |  | 4101 | 27 |
|  |  |  | 4128 | 54 |
|  | 8911 | 6467 | 6280 | - 187 |
|  |  |  | 6271 | - 196 |
|  |  |  | 6374 | - 93 |
| 5 | 8801 | 4091 | 4139 | 48 |
|  |  |  | 4145 | 54 |
|  |  |  | 4141 | 50 |
|  | 8802 | 4118 | 4186 | 68 |
|  |  |  | 4141 | 23 |
|  |  |  | 4138 | 20 |
|  | 8908 | 6412 | 6383 | - 29 |
|  |  |  | 6377 | - 35 |
|  |  |  | 6305 | - 107 |
| 7 | 8795 | 4111 | 3773 | - 338 |
|  |  |  | 3758 | - 353 |
|  |  |  | 3711 | - 400 |
|  | 8796 | 3996 | 3658 | - 338 |
|  |  |  | 3693 | - 303 |
|  |  |  | 3606 | - 390 |
|  | 8905 | 6465 | 5269 | -1196 |
|  |  |  | 5381 | $-1084$ |
|  |  |  | 5151 | -1314 |
| 9 | 8799 | 4089 | 4075 | - 14 |
|  |  |  | 4080 | - 9 |
|  |  |  | 4089 | 0 |
|  | 8800 | 4071 | 4083 | 12 |
|  |  |  | 4075 | 4 |
|  |  |  | 4089 | 18 |
|  | 8907 | 6435 | 6433 | - 2 |
|  |  |  | 6446 | 11 |
|  |  |  | 6442 | 7 |

Table 4.18
Spectroradiometric, 25 cm lamp section measurement of the x chromaticity coordinate

| Laboratory | Lamp | NBS x | Lab $x$ | Difference |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 8797 | 0.3788 | 0.3837 | 0.0049 |
|  |  |  | 0.3837 | 0.0049 |
|  |  |  | 0.3823 | 0.0035 |
|  | 8798 | 0.3801 | 0.3843 | 0.0042 |
|  |  |  | 0.3843 | 0.0042 |
|  |  |  | 0.3835 | 0.0034 |
|  | 8906 | 0.3120 | 0.3171 | 0.0051 |
|  |  |  | 0.3122 | 0.0002 |
|  |  |  | 0.3124 | 0.0004 |
| 2 | 8805 | 0.3786 | 0.3788 | 0.0002 |
|  |  |  | 0.3787 | 0.0001 |
|  |  |  | 0.3792 | 0.0006 |
|  | 8806 | 0.3778 | 0.3775 | -0.0003 |
|  |  |  | 0.3780 | 0.0002 |
|  |  |  | 0.3779 | 0.0001 |
|  | 8909 | 0.3132 | 0.3135 | 0.0003 |
|  |  |  | 0.3144 | 0.0012 |
|  |  |  | 0.3131 | -0.0001 |
| 4 | 8809 | 0.3780 | 0.3780 | 0.0000 |
|  |  |  | 0.3803 | 0.0023 |
|  |  |  | 0.3810 | 0.0030 |
|  | 8810 | 0.3800 | 0.3803 | 0.0003 |
|  |  |  | 0.3793 | -0.0007 |
|  |  |  | 0.3791 | -0.0009 |
|  | 8911 | 0.3129 | 0.3157 | 0.0028 |
|  |  |  | 0.3160 | 0.0031 |
|  |  |  | 0.3142 | 0.0013 |
| 5 | 8801 | 0.3789 | 0.3786 | -0.0003 |
|  |  |  | 0.3784 | -0.0005 |
|  |  |  | 0.3785 | -0.0004 |
|  | 8802 | 0.3778 | 0.3766 | -0.0012 |
|  |  |  | 0.3783 | 0.0005 |
|  |  |  | 0.3788 | 0.0010 |
|  | 8908 | 0.3137 | 0.3138 | 0.0001 |
|  |  |  | 0.3138 | 0.0001 |
|  |  |  | 0.3150 | 0.0013 |
| 7 | 8795 | 0.3776 | 0.3994 | 0.0218 |
|  |  |  | 0.4002 | 0.0226 |
|  |  |  | 0.4031 | 0.0255 |
|  | 8796 | 0.3832 | 0.4059 | 0.0227 |
|  |  |  | 0.4049 | 0.0217 |
|  |  |  | 0.4103 | 0.0271 |
|  | 8905 | 0.3129 | 0.3392 | 0.0263 |
|  |  |  | 0.3364 | 0.0235 |
|  |  |  | 0.3426 | 0.0297 |
| 9 | 8799 | 0.3787 | 0.3793 | 0.0006 |
|  |  |  | 0.3791 | 0.0004 |
|  |  |  | 0.3785 | -0.0002 |
|  | 8800 | 0.3792 | 0.3793 | 0.0001 |
|  |  |  | 0.3794 | 0.0002 |
|  |  |  | 0.3789 | -0.0003 |
|  | 8907 | 0.3134 | 0.3134 | 0.0000 |
|  |  |  | 0.3132 | -0.0002 |
|  |  |  | 0.3133 | -0.0001 |

Table 4.19
Spectroradiometric, 25 cm lamp section measurement of the $y$ chromaticity coordinate

| Laboratory | Lamp | NBS y | Lab y | Difference |
| :---: | :---: | :---: | :---: | :---: |
| 1 | 8797 | 0.3819 | 0.3874 | 0.0055 |
|  |  |  | 0.3877 | 0.0058 |
|  |  |  | 0.3876 | 0.0057 |
|  | 8798 | 0.3852 | 0.3897 | 0.0045 |
|  |  |  | 0.3887 | 0.0035 |
|  |  |  | 0.3887 | 0.0035 |
|  | 8906 | 0.3347 | 0.3405 | 0.0058 |
|  |  |  | 0.3350 | 0.0003 |
|  |  |  | 0.3352 | 0.0005 |
| 2 | 8805 | 0.3823 | 0.3850 | 0.0027 |
|  |  |  | 0.3844 | 0.0021 |
|  |  |  | 0.3855 | 0.0032 |
|  | 8806 | 0.3821 | 0.3825 | 0.0004 |
|  |  |  | 0.3835 | 0.0014 |
|  |  |  | 0.3833 | 0.0012 |
|  | 8909 | 0.3342 | 0.3353 | 0.0011 |
|  |  |  | 0.3366 | 0.0024 |
|  |  |  | 0.3353 | 0.0011 |
| 4 | 8809 | 0.3830 | 0.3860 | 0.0030 |
|  |  |  | 0.3891 | 0.0061 |
|  |  |  | 0.3887 | 0.0057 |
|  | 8810 | 0.3856 | 0.3881 | 0.0025 |
|  |  |  | 0.3870 | 0.0014 |
|  |  |  | 0.3902 | 0.0046 |
|  | 8911 | 0.3342 | 0.3400 | 0.0058 |
|  |  |  | 0.3394 | 0.0052 |
|  |  |  | 0.3380 | 0.0038 |
| 5 | 8801 | 0.3837 | 0.3898 | 0.0061 |
|  |  |  | 0.3900 | 0.0063 |
|  |  |  | 0.3903 | 0.0066 |
|  | 8802 | 0.3823 | 0.3885 | 0.0062 |
|  |  |  | 0.3888 | 0.0065 |
|  |  |  | 0.3904 | 0.0081 |
|  | 8908 | 0.3350 | 0.3405 | 0.0055 |
|  |  |  | 0.3409 | 0.0059 |
|  |  |  | 0.3421 | 0.0071 |
| 7 | 8795 | 0.3817 | 0.4092 | 0.0275 |
|  |  |  | 0.4096 | 0.0279 |
|  |  |  | 0.4133 | 0.0316 |
|  | 8796 | 0.3865 | 0.4126 | 0.0261 |
|  |  |  | 0.4154 | 0.0289 |
|  |  |  | 0.4185 | 0.0320 |
|  | 8905 | 0.3336 | 0.3692 | 0.0356 |
|  |  |  | 0.3692 | 0.0356 |
|  |  |  | 0.3759 | 0.0423 |
| 9 | 8799 | 0.3828 | 0.3827 | -0.0001 |
|  |  |  | 0.3832 | 0.0004 |
|  |  |  | 0.3820 | -0.0008 |
|  | 8800 | 0.3826 | 0.3842 | 0.0016 |
|  |  |  | 0.3835 | 0.0009 |
|  |  |  | 0.3834 | 0.0008 |
|  | 8907 | 0.3349 | 0.3358 | 0.0009 |
|  |  |  | 0.3351 | 0.0002 |
|  |  |  | 0.3352 | 0.0003 |



Spectroradiometric, 25 cm lamp section measurement of color temperature -- comprehensive average and standard deviation for each participating laboratory

| Laboratory | Lamp | Average <br> (kelvins) | Standard <br> Deviation |
| :---: | :---: | :---: | :---: |
| 1 | 8797 | 4003 | 26 |
|  | 8798 | 3991 | 10 |
|  | 8906 | 6387 | 168 |
| 2 | 8805 | 4097 | 3 |
|  | 8806 | 4117 | 4 |
|  | 8909 | 6414 | 39 |
| 4 | 8809 | 4096 | 30 |
|  | 8810 | 4104 | 23 |
|  | 8911 | 6308 | 57 |
|  | 8801 | 4142 | 3 |
|  | 8802 | 4155 | 43 |
|  | 8908 | 6355 | 32 |
|  | 8795 | 3747 | 44 |
|  | 8796 | 5267 | 115 |
|  | 8905 | 4081 | 7 |
|  | 8799 | 4082 | 7 |
|  | 8800 | 6440 | 7 |

Table 4.21

Spectroradiometric, 25 cm lamp section measurement of the $x$ and $y$ chromaticity coordinates -comprehensive average and standard deviation for each participating laboratory

| Laboratory | Lamp | Average x | Standard Deviation | Average y | Standard Deviation |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 8797 | 0.3832 | 0.0008 | 0.3876 | 0.0002 |
|  | 8798 | 0.3840 | 0.0005 | 0.3890 | 0.0006 |
|  | 8906 | 0.3139 | 0.0028 | 0.3369 | 0.0031 |
| 2 | 8805 | 0.3789 | 0.0003 | 0.3850 | 0.0006 |
|  | 8806 | 0.3778 | 0.0003 | 0.3831 | 0.0005 |
|  | 8909 | 0.3137 | 0.0007 | 0.3357 | 0.0008 |
| 4 | 8809 | 0.3798 | 0.0016 | 0.3879 | 0.0017 |
|  | 8810 | 0.3796 | 0.0006 | 0.3884 | 0.0016 |
|  | 8911 | 0.3153 | 0.0010 | 0.3391 | 0.0010 |
| 5 | 8801 | 0.3785 | 0.0001 | 0.3900 | 0.0003 |
|  | 8802 | 0.3779 | 0.0012 | 0.3892 | 0.0010 |
|  | 8908 | 0.3142 | 0.0007 | 0.3412 | 0.0008 |
| 7 | 8795 | 0.4009 | 0.0019 | 0.4107 | 0.0023 |
|  | 8796 | 0.4070 | 0.0029 | 0.4155 | 0.0030 |
|  | 8905 | 0.3394 | 0.0031 | 0.3714 | 0.0039 |
| 9 | 8799 | 0.3790 | 0.0004 | 0.3826 | 0.0006 |
|  | 8800 | 0.3792 | 0.0003 | 0.3837 | 0.0004 |
|  | 8907 | 0.3133 | 0.0001 | 0.3354 | 0.0004 |

Comparison of the photometric and spectroradiometric measurements of total luminous flux.

| Laboratory | Lamp | Lamp type | NBS (lumens) |  | Lab (lumens) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Photometric | Spectroradiometric | Photometric | Spectroradiometric |
| 1 | 8797 | CW1 | 2820 | 2833 | 2804 | 2801 |
|  | 8798 | CW2 | 2833 | 2842 | 2856 | 2835 |
|  | 8906 | D | 2464 | 2482 | 2490 | 2419 |
| 2 | 8805 | CW1 | 2792 | 2798 | 2797 | 2601 |
|  | 8806 | CW2 | 2863 | 2864 | 2861 | 2662 |
|  | 8909 | D | 2485 | 2474 | 2452 | 2328 |
| 3 | 8807 | CW1 | 2911 | 2924 | 2922 | -- |
|  | 8808 | CW2 | 2895 | 2902 | 2903 | -- |
|  | 8910 | D | 2472 | 2460 | 2392 | -- |
| 4 | 8809 | CW1 | 2777 | 2789 | 2769 | 3185 |
|  | 8810 | CW2 | 2840 | 2844 | 2821 | 3316 |
|  | 8911 | D | 2485 | 2478 | 2468 | 2916 |
| 5 | 8801 | CW1 | 2751 | 2750 | 2789 | 2746 |
|  | 8802 | CW2 | 2808 | 2804 | 2844 | 2786 |
|  | 8908 | D | 2452 | 2450 | 2411 | 2445 |
| 6 | 8813 | CW1 | 2797 | 2812 | 2269 | -- |
|  | 8814 | CW2 | 2847 | 2848 | 2258 | -- |
|  | 8913 | D | 2469 | 2454 | 2053 | -- |
| 7 | 8795 | CW1 | 2946 | 2936 | 2897 | -- |
|  | 8796 | CW2 | 2514 | 2499 | 2516 | -- |
|  | 8905 | D | 2478 | 2467 | 2416 | -- |
| 8 | 8803 | CWI | 2834 | 2838 | 2840 | -- |
|  | 8804 | CW2 | 2857 | 2860 | 2867 | -- |
|  | 8908A | D | 2480 | 2473 | 2439 | -- |

Comparison of the integrating sphere and the 25 cm lamp section spectroradiometric measurements of color temperature.

| Laboratory | Lamp | Lamp <br> type | NBS (kelvins) |  | Lab (kelvins) |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Sphere | 25 cm section | Sphere | $\begin{gathered} 25 \mathrm{~cm} \\ \text { section } \end{gathered}$ |
| 1 | 8797 | CW1 | 4059 | 4080 | 4084 | 4003 |
|  | 8798 | CTV2 | 4086 | 4070 | 4107 | 3991 |
|  | 8906 | D | 6443 | 6507 | 6543 | 6387 |
| 2 | 8805 | CW1 | 4110 | 4093 | 4052 | 4097 |
|  | 8806 | CN2 | 4125 | 4107 | 4097 | 4117 |
|  | 8909 | D | 6436 | 6457 | 6316 | 6414 |
| 4 | 8809 | CW1 | 4101 | 4111 | 4181 | 4096 |
|  | 8810 | CW2 | 4085 | 4073 | 4100 | 4104 |
|  | 8911 | D | 6450 | 6461 | 6438 | 6308 |
| 5 | 8801 | CW1 | 4092 | 4091 | 4136 | 4142 |
|  | 8802 | CW2 | 4100 | 4118 | 4132 | 4155 |
|  | 8908 | D | 6402 | 6412 | 6340 | 6355 |
| 7 | 8795 | CW1 | 4130 | 4111 | -- | 3747 |
|  | 8796 | CW2 | 3996 | 3996 | -- | 3652 |
|  | 8905 | D | 6431 | 6465 | -- | 5267 |
| 9 | 8799 | CW1 | 4073 | 4089 | -- | 4081 |
|  | 8800 | CW2 | 4067 | 4071 | -- | 4082 |
|  | 8907 | D | 6427 | 6435 | -- | 6440 |

Comparison of the integrating sphere and the 25 cm lamp section spectroradiometric measurements, and the Barnes colorimetric measurement of the x chromaticity coordinate.

| Laboratory | Lamp | Lamp <br> type | NBS x |  | Lab $\times$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Sphere | $\begin{array}{r} 25 \mathrm{~cm} \\ \text { section } \end{array}$ | Sphere | $\qquad$ | Barnes |
| 1 | 8797 | CW1 | 0.3800 | 0.3788 | 0.3786 | 0.3832 | 0.3845 |
|  | 8798 | CW2 | 0.3794 | 0.3801 | 0.3778 | 0.3840 | 0.3845 |
|  | 8906 | D | 0.3131 | 0.3120 | 0.3114 | 0.3139 | 0.3178 |
| 2 | 8805 | CW 1 | 0.3783 | 0.3786 | 0.3813 | 0.3789 | 0.3832 |
|  | 8806 | CW2 | 0.3774 | 0.3778 | 0.3791 | 0.3778 | 0.3825 |
|  | 8909 | D | 0.3133 | 0.3132 | 0.3152 | 0.3137 | 0.3148 |
| 3 | 8807 | CW1 | 0.3776 | 0.3778 | - | - | 0.3784 |
|  | 8808 | CW2 | 0.3766 | 0.3768 | - | - | 0.3776 |
|  | 8910 | D | 0.3133 | 0.3134 | - | - | 0.3151 |
| 4 | 8809 | CW1 | 0.3786 | 0.3780 | 0.3763 | 0.3798 | 0.3824 |
|  | 8810 | CW2 | 0.3794 | 0.3800 | 0.3795 | 0.3796 | 0.3842 |
|  | 8911 | D | 0.3131 | 0.3130 | 0.3130 | 0.3153 | 0.3169 |
| 5 | 8801 | CW1 | 0.3790 | 0.3789 | 0.3791 | 0.3785 | 0.3730 |
|  | 8802 | CW2 | 0.3787 | 0.3776 | 0.3793 | 0.3779 | 0.3730 |
|  | 8908 | D | 0.3137 | 0.3137 | 0.3145 | 0.3142 | 0.3150 |
| 7 | 8795 | CW1 | 0.3773 | 0.3776 | - | 0.4009 | 0.3820 |
|  | 8796 | CW2 | 0.3833 | 0.3832 | - | 0.4070 | 0.3875 |
|  | 8905 | D | 0.3134 | 0.3129 | - | 0.3394 | 0.3161 |
| 8 | 8803 | CW1 | 0.3798 | 0.3800 | - | - | 0.3854 |
|  | 8804 | CW2 | 0.3798 | 0.3798 | - | - | 0.3851 |
|  | 8908A | D | 0.3134 | 0.3136 | - | - | 0.3137 |
| 9 | 8799 | CW1 | 0.3794 | 0.3787 | - | 0.3790 | - |
|  | 8800 | CW2 | 0.3794 | 0.3792 | - | 0.3792 | - |
|  | 8907 | D | 0.3134 | 0.3134 | - | 0.3133 | - |

Comparison of the integrating sphere and the 25 cm lamp section spectroradiometric measurements, and the Barnes colorimetric measurement of the y chromaticity coordinate.

| Laboratory | Lamp | Lamp <br> type | NBS y |  | Lab y |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Sphere | $\begin{array}{r} 25 \mathrm{~cm} \\ \text { section } \end{array}$ | Sphere | $\begin{gathered} 25 \mathrm{~cm} \\ \text { section } \end{gathered}$ | Barnes |
| 1 | 8797 | CW1 | 0.3837 | 0.3819 | 0.3814 | 0.3876 | 0.3895 |
|  | 8798 | CW2 | 0.3850 | 0.3852 | 0.3819 | 0.3890 | 0.3905 |
|  | 8906 | D | 0.3358 | 0.3347 | 0.3332 | 0.3369 | 0.3410 |
| 2 | 8805 | CW1 | 0.3844 | 0.3832 | 0.3875 | 0.3850 | 0.3895 |
|  | 8806 | CW2 | 0.3830 | 0.3821 | 0.3855 | 0.3831 | 0.3878 |
|  | 8909 | D | 0.3356 | 0.3342 | 0.3382 | 0.3357 | 0.3401 |
| 3 | 8807 | CW1 | 0.3827 | 0.3818 | - | - | 0.3857 |
|  | 8808 | CW2 | 0.3811 | 0.3792 | - | - | 0.3843 |
|  | 8910 | D | 0.3351 | 0.3344 | - | - | 0.3401 |
| 4 | 8809 | CW1 | 0.3842 | 0.3830 | 0.3864 | 0.3879 | 0.3885 |
|  | 8810 | CW2 | 0.3851 | 0.3856 | 0.3876 | 0.3884 | 0.3897 |
|  | 8811 | D | 0.3351 | 0.3340 | 0.3375 | 0.3391 | 0.3402 |
| 5 | 8801 | CW1 | 0.3844 | 0.3837 | 0.3913 | 0.3900 | 0.3850 |
|  | 8802 | CW2 | 0.3844 | 0.3823 | 0.3916 | 0.3892 | 0.3850 |
|  | 8908 | D | 0.3357 | 0.3350 | 0.3422 | 0.3412 | 0.3370 |
| 7 | 8795 | CW1 | 0.3831 | 0.3817 | - | 0.4107 | 0.3863 |
|  | 8796 | CW2 | 0.3870 | 0.3865 | - | 0.4155 | 0.3907 |
|  | 8905 | D | 0.3350 | 0.3336 | - | 0.3714 | 0.3395 |
| 8 | 8803 | CW1 | 0.3842 | 0.3837 | - | - | 0.3913 |
|  | 8804 | CW2 | 0.3843 | 0.3834 | - | - | 0.3916 |
|  | 8908A | D | 0.3352 | 0.3345 | - | - | 0.3416 |
| 9 | 8799 | CW1 | 0.3830 | 0.3828 | - | 0.3826 | - |
|  | 8800 | CW2 | 0.3836 | 0.3826 | - | 0.3837 | - |
|  | 8907 | D | 0.3357 | 0.3349 | - | 0.3354 | - |

4.3. Results and comparison of the spectral distribution measurements

The spectral distribution data from each laboratory are given in tables 4.26 through 4.67 and plotted in figures 4.18 through 4.59. These data include both the spectroradionetric measurement of the total lamp output in an integrating sphere and that of a 25 cm section of the lamp. Summarization and compilation of these results are included in the tables and figures listed in the previous section.

In examining the detailed data compiled in this section, one should note that the intercomparison was statistically designed to use the data acquired at NBS as a base. Therefore, data from the spectroradiometric equipment at the participating laboratories will be evaluated against the NBS base. Consistent differences from the NBS base in all the data would indicate, of course, that the problem may be at NBS itself.

From an examination of all of the spectral distribution curves it appears that most of the curves do not match in the regions of the mercury lines. The largest deviations are in the region near 580 nm . Since the curvature of the continuum is greatest at this mercury line, the efficiency of the fit of a quadratic polynominal may be in question. Perhaps a better interpolation procedure at NBS would have eliminated this problem. No other consistent deviations were observed between NBS and the other laboratories. The individual laboratory deviations will now be examined.

If the data from each laboratory (see also the tables and figures in section 4.2) are different from NBS or from the overall laboratory average, this could be indicative of problems in experimental technique. Effects of system nonlinearity, improper sphere size, inadequate or improperly arranged baffling, scattered light within the monochromator, inadequate (or the absence of) filtering of second-order spectra and, of course, the individualism of each operator will contribute to differences in the measurement of the color parameters and total luminous flux.

LABORATORY l: Agreement between this laboratory's spectroradiometric measurement of total luminous flux and that of NBS was close. The small difference may be attributable to system non-linearity either at this laboratory or at NBS. This point cannot be checked, of course, without additional experiments.

LABORATORY 2: The spectroradiometric values of total luminous flux obtained in this laboratory's sphere were low compared to the other participating laboratories. Small sphere size and the arrangement of lamps and baffling within the sphere are suspected as the principal reasons for these low values. However, the difficulties encountered in the data analysis may have introduced discrepancies and would, of course, obscure the identification of problems in experimental technique.

LABORATORY 4: This laboratory's sphere measurements of total luminous flux were extremely high and may have been caused by inadequate baffling of the lamps. Difficulties were encountered in the analysis of the data from this laboratory and may have obfuscated the identification of problems in experimental technique. The relative spectral flux distribution curves for this laboratory appear to be higher than those of NBS in the 440 to 520 nm region. This laboratory used synchronous amplification and, therefore, chopped the light output at 90 Hz . Because the various phosphors used in the lamp do not have the same decay time, the light output from each phosphor was probably sampled to a different extent. The spectral flux in the region around 590 nm is also considerably different from that of NBS. Since this laboratory used a prism monochromator and did not indicate frequent wavelength calibration checks, the cam in the wavelength drive of the instrument may have been off calibration in this region.

LABORATORY 5: This laboratory's sphere measurements of total luminous flux were close to those of NBS. However, a spurious line appears at 700 nm and the spectral flux distribution curves exhibit a decrease from the NBS curves toward the red region of the spectrum. The line may be due to an emission from the coating used on their integrating box but this does not explain the relative decrease in this region. If this is not an effect produced by the $3 M$ "Velvet

White" coating, then it is suspected either that the sensitivity of their photomultiplier has decreased in this spectral region or that the gain and/or the sensitivity of their electronics consistently drifted during the course of a single run.

LABORATORY 7: Data from Laboratory 7 agreed very poorly with those of all of the other participating laboratories. Their spectroradiometric equipment appeared to have most of the problems that afflict spectroradiometry.

LABORATORY 9: This laboratory submitted only relative spectral irradiance measurements, and these agreed closely with those made at NBS.

NATIONAL BUREAU OF STANDARDS: Careful analysis of the NBS Initial and Repeat spectroradiometric measurements indicates that a small wavelength shift occurred in the interim between measurements. The shift was definitely less than the instrument bandpass and much too small to be detected in a data comparison with the other laboratories.

RELATIVE SPECTRAL FLUX DISTRIBUTION IN SPHERE-NORMALIZFD TO AREA LAMP NUMBER NBS8797

|  | NBS INITIAL |  |  | LABORATORY 1 |  |  | NBS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 |
| 380.0 | 3.8 | 4.2 | 3.9 | . 0 | . 0 | . 0 | 3.6 | 3.6 | 3.7 |
| 390.0 | $5 \cdot 8$ | 6.2 | 6.0 | 6.6 | 6.1 | 7.3 | 5.7 | 5.6 | 5.8 |
| 400.0 | 8.5 | 8.6 | 8.6 | 8.9 | 9.2 | 8.8 | 8.2 | 8.1 | 8.3 |
| 410.0 | 10.8 | 10.8 | 10.8 | 11.1 | 10.5 | 10.8 | 10.6 | 10.4 | 10.6 |
| 420.0 | 13.1 | 13.2 | 13.2 | 13.5 | 13.0 | 13.5 | 13.0 | 12.9 | 13.0 |
| 430.0 | 15.9 | 16.1 | 16.0 | 16.1 | 16.7 | 16.9 | 15.8 | 15.9 | 15.8 |
| 440.0 | 18.4 | 18.6 | 18.5 | 19.3 | 18.8 | 19.4 | 18.4 | 18.4 | 18.3 |
| 450.0 | 20.7 | 20.6 | 20.7 | 21.5 | 20.8 | 21.0 | 20.7 | 20.8 | 20.6 |
| 460.0 | 22.4 | 22.3 | 22.5 | 22.7 | 22.7 | 21.7 | 22.5 | 22.5 | 22.4 |
| 470.0 | 23.5 | 23.4 | 23.5 | 23.9 | 23.6 | 23.9 | 23.5 | 23.6 | 23.6 |
| 480.0 | 23.8 | 23.8 | 23.9 | 24.0 | 24.0 | 23.8 | 23.9 | 24.0 | 23.9 |
| 490.0 | 23.8 | 23.8 | 23.9 | 23.7 | 23.8 | 23.4 | 23.9 | 23.9 | 23.9 |
| 500.0 | 22.8 | 22.8 | 22.9 | 22.9 | 22.9 | 22.7 | 23.0 | 23.1 | 23.0 |
| 510.0 | 22.4 | 22.4 | 22.5 | 22.8 | 22.5 | 22.5 | 22.5 | 22.6 | 22.5 |
| 520.0 | 23.4 | 23.4 | 23.2 | 23.6 | 23.7 | 23.5 | 23.5 | 23.4 | 23.4 |
| 530.0 | 27.5 | 27.4 | 27.6 | 27.7 | 27.9 | 28.3 | 27.4 | 27.2 | 27.2 |
| 540.0 | 35.5 | 35.4 | 35.6 | 34.8 | 35.1 | 35.7 | 35.1 | 34.9 | 35.0 |
| 550.0 | 45.6 | 45.4 | 45.7 | 44.9 | 45.2 | 45.6 | 45.3 | 45.0 | 45.1 |
| 560.0 | 58.3 | 58.0 | 58.5 | 58.0 | 58.3 | 58.1 | 58.1 | 57.9 | 57.9 |
| 570.0 | 66.4 | 66.1 | 66.7 | 65.4 | 65.2 | 64.9 | 66.4 | 66.3 | 66.2 |
| 580.0 | 69.0 | 68.7 | 69.4 | 67.8 | 67.5 | 67.0 | 69.3 | 69.2 | 69.1 |
| 590.0 | 65.0 | 64.6 | $65 \cdot 1$ | 65.3 | 65.1 | 64.4 | 65.5 | 65.5 | 65.5 |
| 600.0 | 57.1 | 56.8 | 57.4 | 57.8 | 58.1 | 57.1 | 57.7 | 57.6 | 57.6 |
| 610.0 | $47 \cdot 2$ | 47.0 | 47.4 | 48.8 | 48.4 | 47.7 | 48.0 | 47.9 | 48.1 |
| 620.0 | 37.0 | 36.8 | 37.1 | 39.1 | 38.4 | 37.7 | 37.7 | 37.9 | 37.9 |
| 630.0 | 28.4 | 28.4 | 28.5 | 29.0 | 29.7 | 28.9 | 28.9 | 28.9 | 29.0 |
| 640.0 | 21.2 | 21.2 | 21.2 | 21.6 | 22.0 | 22.0 | 21.7 | 22.0 | 21.7 |
| 650.0 | 15.5 | 15.7 | 15.6 | 16.1 | 16.6 | 16.8 | 16.0 | 16.0 | 16.0 |
| 660.0 | 11.4 | 11.5 | 11.4 | 12.0 | 12.8 | 12.7 | 11.6 | 11.6 | 11.6 |
| 670.0 | 8.4 | 8.6 | 8.4 | 9.4 | $10 \cdot 1$ | 10.0 | 8.5 | 8.5 | 8.7 |
| 680.0 | 6.2 | 6.4 | 6.0 | 7.2 | 7.5 | 7.8 | 6.2 | 6.4 | 6.4 |
| 690.0 | 5.0 | 5.0 | 4.7 | 5.2 | $5 \cdot 4$ | 5.9 | $5 \cdot 0$ | 5.0 | 5.0 |
| 700.0 | 3.6 | 3.7 | 3.3 | 4.1 | 4.5 | 4.5 | 3.6 | 3.6 | 3.6 |
| 710.0 | 3.0 | 3.2 | 2.7 | 3.1 | 3.3 | 4.3 | 2.9 | 3.0 | 3.0 |
| 720.0 | 2.3 | 2.7 | 2.0 | 3.2 | 3.1 | 3.0 | 2.3 | 2.3 | 2.3 |
| 730.0 | 3.2 | 3.5 | 3.2 | . 0 | . 0 | . 0 | 1.9 | 1.8 | 2.0 |
| 740.0 | 2.1 | 2.4 | 1.6 | - 0 | - 0 | . 0 | 2.0 | 2.1 | 2.1 |
| 750.0 | 2.5 | 2.8 | 1.9 | . 0 | - 0 | . 0 | 2.2 | 2.0 | 2.3 |
| 760.0 | 2.4 | 2.7 | 1.6 | . 0 | - 0 | . 0 | 1.5 | 1.5 | 1.6 |

## MERCURY LINES

| 405.0 | 23.1 | 23.0 | 23.4 | 23.2 | 23.5 | 22.2 | 23.3 | 23.8 | 23.2 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 57.7 | 56.9 | 57.5 | 59.4 | 58.2 | 59.4 | 56.8 | 57.7 | 57.3 |
| 546.0 | 26.8 | 26.6 | 27.0 | 27.8 | 27.5 | 27.8 | 27.0 | 27.1 | 26.9 |
| 578.0 | 9.3 | 9.2 | 9.3 | 8.6 | 8.3 | 8.9 | 9.1 | 9.0 | 9.0 |



FIGURE 4.18 AVERAGE RELATIVE SPECTRAL FLUX (SPHERE MEASUREMENTS) NORMALIZED TO AREA

SPECTRAL FLUX DISTRIBUTION (WATTS) IN SPHERE LAMP NUMBER NBS8797

|  | NBS INITIAL |  |  | LABORATORY 1 |  |  | NIRS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 |
| 380.0 | . 0320 | . 0354 | . 0328 | . 0000 | . 0000 | . 0000 | . 0295 | . 0297 | . 0302 |
| 390.0 | . 0482 | . 0521 | . 0497 | . 0537 | . 0505 | . 0604 | . 0468 | . 0467 | . 0477 |
| 400.0 | . 0708 | . 0723 | . 0714 | . 0722 | . 0758 | . 0733 | . 0672 | . 0670 | . 0679 |
| 410.0 | . 0899 | . 0908 | . 0903 | . 0900 | . 0861 | . 0900 | . 0863 | . 0863 | . 0872 |
| 420.0 | . 1097 | . 1107 | . 1099 | . 1096 | . 1066 | . 1123 | . 1066 | . 1076 | . 1073 |
| 430.0 | . 1329 | . 1356 | . 1331 | . 1309 | . 1374 | . 1403 | . 1293 | . 1319 | . 1298 |
| 440.0 | . 1535 | . 1559 | . 1539 | . 1567 | . 1546 | . 1607 | . 1501 | . 1531 | . 1508 |
| 450.0 | .1726 | . 1734 | . 1727 | . 1746 | . 1710 | . 1741 | . 1691 | . 1726 | . 1699 |
| 460.0 | . 1868 | . 1875 | . 1871 | . 1848 | . 1867 | . 1805 | . 1839 | . 1868 | . 1842 |
| 470.0 | .1959 | . 1970 | . 1955 | . 1939 | . 1942 | . 1985 | . 1926 | . 1961 | . 1939 |
| 480.0 | . 1988 | . 1996 | . 1993 | . 1947 | . 1977 | . 1972 | . 1958 | . 1995 | . 1970 |
| 490.0 | . 1983 | . 1996 | . 1987 | . 1921 | . 1959 | . 1940 | . 1955 | . 1984 | . 1963 |
| 500.0 | . 1903 | . 1918 | . 1908 | . 1861 | . 1887 | . 1887 | . 1881 | . 1919 | . 1891 |
| 510.0 | .1873 | . 1882 | . 1874 | . 1850 | . 1853 | . 1872 | . 1845 | . 1878 | . 1852 |
| 520.0 | . 1955 | . 1964 | . 1936 | . 1920 | . 1950 | . 1950 | . 1919 | . 1947 | . 1922 |
| 530.0 | . 2297 | . 2304 | - 2298 | - 2251 | . 2297 | - 2348 | - 2240 | - 2263 | . 2241 |
| 540.0 | . 2964 | . 2971 | . 2962 | . 2827 | . 2887 | . 2960 | . 2875 | . 2899 | . 2881 |
| 550.0 | . 3807 | . 3818 | . 3807 | . 3647 | . 3721 | . 3786 | . 3703 | . 3740 | . 3712 |
| 560.0 | . 4863 | . 4876 | . 4870 | . 4711 | . 4799 | . 4826 | . 4752 | . 4815 | . 4765 |
| 570.0 | . 5538 | . 5555 | . 5556 | . 5310 | . 5370 | . 5390 | . 5434 | . 5513 | . 5445 |
| 580.0 | . 5761 | . 5774 | . 5783 | . 5507 | . 5559 | . 5563 | . 5669 | . 5755 | . 5688 |
| 590.0 | . 5423 | . 5424 | . 5426 | . 5302 | . 5364 | . 5346 | . 5361 | . 5453 | . 5387 |
| 600.0 | . 4765 | . 4773 | . 4781 | . 4697 | . 4786 | . 4739 | . 4718 | . 4791 | . 4736 |
| 610.0 | . 3944 | - 3946 | . 3950 | . 3960 | . 3981 | . 3960 | . 3929 | . 3986 | . 3961 |
| 620.0 | . 3090 | . 3095 | . 3093 | . 3178 | . 3164 | . 3129 | . 3088 | . 3151 | . 3120 |
| 630.0 | . 2367 | . 2383 | . 2377 | . 2355 | . 2443 | . 2399 | . 2361 | . 2408 | . 2387 |
| 640.0 | . 1770 | . 1785 | . 1766 | . 1754 | . 1812 | . 1827 | . 1779 | . 1834 | . 1784 |
| 650.0 | . 1297 | . 1318 | . 1296 | . 1309 | . 1370 | . 1393 | . 1310 | . 1327 | . 1320 |
| 660.0 | . 0950 | . 0967 | . 0949 | . 0972 | . 1058 | . 1055 | . 0951 | . 0965 | . 0953 |
| 670.0 | . 0704 | . 0725 | . 0703 | . 0763 | . 0829 | . 0832 | . 0697 | . 0708 | . 0712 |
| 680.0 | . 0521 | . 0536 | . 0500 | . 0581 | . 0620 | . 0646 | . 0511 | . 0529 | . 0524 |
| 690.0 | . 0415 | . 0422 | . 0392 | . 0424 | . 0445 | . 0493 | . 0409 | . 0417 | . 0411 |
| 700.0 | . 0302 | . 0311 | . 0277 | . 0330 | . 0370 | . 0373 | . 0295 | . 0301 | . 0293 |
| 710.0 | . 0254 | . 0266 | . 0226 | . 0254 | . 0275 | . 0359 | . 0240 | . 0246 | . 0248 |
| 720.0 | . 0195 | . 0225 | . 0163 | . 0256 | . 0253 | . 0251 | . 0187 | . 0191 | . 0192 |
| $730 \cdot 0$ | . 0264 | . 0298 | . 0264 | . 0000 | . 0000 | . 0000 | . 0158 | . 0147 | . 0163 |
| 740.0 | . 0177 | . 0197 | . 0133 | . 0000 | . 0000 | . 0000 | . 0167 | . 0172 | . 0173 |
| 750.0 | . 0212 | . 0235 | . 0160 | . 0000 | . 0000 | . 0000 | . 0179 | . 0164 | . 0186 |
| 760.0 | . 0197 | . 0228 | . 0132 | . 0000 | . 0000 | . 0000 | . 0123 | . 0127 | . 0128 |

## MERCURY LINES

| 405.0 | .1929 | .1930 | .1948 | .1888 | .1937 | .1843 | .1903 | .1984 | .1911 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 436.0 | .4819 | .4781 | .4788 | .4821 | .4788 | .4932 | .4650 | .4796 | .4713 |
| 546.0 | .2240 | .2235 | .2251 | .2258 | .2267 | .2311 | .2210 | .2254 | .2214 |
| 578.0 | .0779 | .0775 | .0772 | .0696 | .0685 | .0740 | .0745 | .0751 | .0739 |



FIGURE 4.19 AVERAGE SPECTRAL FLUX (SPHERE MEASUREMENTS)

RELATIVE SPECTRAL FLUX OISTRIBUTION IN SPHERE-NORMALIZED TO AREA LAMP NUMBER NBS8798

|  | NBS INITIAL |  |  | LABORATORY 1 |  |  | NBS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 |
| 380.0 | 3.7 | 3.7 | 3.9 | . 0 | . 0 | . 0 | 3.6 | 3.5 | 3.9 |
| 390.0 | 5.9 | $5 \cdot 9$ | 6.0 | 6.2 | 6.9 | 6.1 | 5.7 | 5.8 | $5 \cdot 8$ |
| 400.0 | 8.5 | 8.5 | 8.6 | 7.9 | 9.8 | 8.8 | 8.2 | 8.3 | 8.3 |
| 410.0 | 10.7 | 10.7 | 10.8 | 10.8 | 11.2 | 10.3 | 10.6 | 10.6 | 10.6 |
| 420.0 | 13.0 | 13.0 | 13.2 | 13.5 | 13.4 | 13.0 | 13.1 | 13.1 | 13.0 |
| 430.0 | 15.9 | 15.9 | 16.0 | 16.1 | 16.3 | 16.7 | 15.9 | 15.9 | 15.7 |
| 440.0 | 18.3 | 18.3 | 18.5 | 19.3 | 19.0 | 19.0 | 18.4 | 18.4 | 18.2 |
| 450.0 | 20.6 | 20.6 | 20.7 | 21.6 | 21.2 | 21.0 | 20.7 | 20.7 | 20.5 |
| 460.0 | 22.3 | 22.3 | 22.4 | 23.2 | 22.9 | 22.5 | 22.5 | 22.5 | 22.4 |
| 470.0 | 23.4 | 23.4 | 23.6 | 24.2 | 23.5 | 23.7 | 23.6 | 23.6 | 23.4 |
| 480.0 | 23.8 | 23.8 | 23.9 | 24.1 | 24.1 | 24.1 | 24.0 | 24.0 | 23.9 |
| 490.0 | 23.8 | 23.1 | 23.8 | 23.7 | 23.9 | 23.8 | 24.0 | 23.9 | 23.8 |
| 500.0 | 22.8 | 22.9 | 22.9 | 22.9 | 23.0 | 22.9 | 23.1 | 23.0 | 22.9 |
| 510.0 | 22.5 | 22.5 | 22.5 | 22.7 | 22.6 | 23.2 | 22.6 | 22.6 | 22.5 |
| 520.0 | 23.6 | 23.6 | 23.6 | 23.9 | 23.5 | 23.6 | 23.7 | 23.6 | 23.5 |
| 530.0 | 27.8 | 27.8 | 27.7 | 28.5 | 28.6 | 28.0 | 27.7 | 27.4 | 27.4 |
| 540.0 | 35.9 | 35.8 | 35.9 | 35.9 | 36.1 | 35.2 | 35.7 | 35.2 | 35.1 |
| 550.0 | 46.1 | 46.0 | 46.1 | 46.2 | 46.1 | 45.3 | 45.9 | 45.4 | 45.2 |
| 560.0 | 58.6 | 58.7 | 58.7 | 59.3 | 58.5 | 58.2 | 58.7 | 58.3 | 58.0 |
| 570.0 | 66.6 | 66.8 | 66.8 | 66.0 | 65.0 | 65.5 | 66.9 | 66.4 | 66.1 |
| 580.0 | 69.2 | 69.3 | 69.4 | 68.0 | 66.9 | 67.9 | 69.6 | 69.1 | 68.9 |
| 590.0 | $64 \cdot 8$ | $65 \cdot 0$ | 64.9 | 65.2 | 64.1 | 65.7 | 65.7 | $65 \cdot 2$ | 64.8 |
| 600.0 | 56.9 | 57.1 | 57.1 | 57.5 | 56.8 | 58.6 | 57.7 | 57.3 | 57.1 |
| 610.0 | 47.3 | 47.1 | 47.1 | 48.3 | 47.5 | 48.6 | 47.9 | 47.6 | 47.6 |
| 620.0 | 36.9 | 37.0 | 36.9 | 37.9 | 37.7 | 38.7 | 37.6 | 37.5 | 37.5 |
| 630.0 | 28.3 | 28.3 | 28.4 | 29.2 | 29.0 | 29.3 | 28.8 | 28.7 | 28.8 |
| 640.0 | 21.2 | 21.3 | 21.2 | 21.2 | 21.8 | 21.9 | 18.1 | 21.9 | 21.9 |
| 650.0 | 15.6 | 15.6 | 15.6 | 16.0 | 16.2 | 16.8 | 15.9 | 16.1 | 16.1 |
| 660.0 | 11.4 | 11.4 | 11.3 | 11.8 | 12.7 | 12.1 | 11.6 | 11.7 | 11.8 |
| 670.0 | 8.6 | 8.5 | 8.4 | 8.9 | 9.0 | 9.0 | 8.6 | 8.5 | 8.8 |
| 680.0 | 6.3 | 6.3 | 6.1 | 6.7 | 6.5 | 7.1 | 6.3 | 6.3 | 6.6 |
| 690.0 | 5.0 | 5.0 | 4.8 | 5.1 | 5.6 | 5.5 | 5.0 | 5.0 | 5.3 |
| 700.0 | 3.6 | 3.6 | 3.5 | 3.7 | 4.5 | 4.4 | 3.6 | 3.7 | 4.0 |
| 710.0 | 3.1 | 3.1 | 2.9 | 3.0 | 3.1 | 3.5 | 2.9 | 3.1 | 3.2 |
| 720.0 | 2.6 | 2.4 | 2.1 | 2.4 | 2.7 | 3.0 | 2.3 | 2.3 | 2.6 |
| 730.0 | 3.2 | 3.2 | 2.9 | . 0 | - 0 | . 0 | 1.9 | 1.9 | 2.3 |
| 740.0 | 2.1 | 2.1 | 1.9 | - 0 | - 0 | . 0 | 2.0 | 2.1 | $2 \cdot 5$ |
| 750.0 | 2.5 | 2.6 | 2.2 | . 0 | - 0 | . 0 | 2.2 | 1.8 | 2.7 |
| 760.0 | 2.4 | 2.4 | 1.6 | . 0 | . 0 | . 0 | 1.5 | 1.5 | 2.2 |

## MERCURY LINES

| 405.0 | 22.7 | 23.0 | 23.2 | 21.8 | 25.0 | 23.0 | 23.2 | 23.4 | 22.8 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 56.2 | 56.3 | 56.6 | 61.0 | 58.6 | 58.0 | 56.7 | 57.2 | 56.6 |
| 546.0 | 27.0 | 27.0 | 27.0 | 27.7 | 28.1 | 27.2 | 27.3 | 27.1 | 26.8 |
| 578.0 | 9.2 | 9.2 | 9.1 | 9.0 | 8.9 | 8.7 | 9.1 | 9.1 | 9.0 |



SPECTRAL FLUX DISTRIBUTION (WATTS) IN SPHERE
LAMP NUMBER NBS8798

|  | NBS INITIAL |  |  | LABORATORY 1 |  |  | NBS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUIN 9 |
| 380.0 | . 0313 | . 0305 | . 0328 | . 0000 | . 0000 | . 0000 | . 0295 | . 0293 | . 0326 |
| 390.0 | . 0490 | . 0494 | . 0497 | . 0511 | . 0572 | . 0503 | . 0468 | . 0479 | . 0486 |
| 400.0 | . 0708 | . 0708 | . 0714 | . 0655 | . 0813 | . 0729 | . 0672 | . 0688 | . 0692 |
| 410.0 | . 0898 | . 0886 | . 0903 | . 0891 | . 0929 | . 0852 | . 0865 | . 0877 | . 0885 |
| 420.0 | . 1091 | . 1083 | . 1099 | . 1117 | . 1108 | . 1068 | . 1070 | . 1084 | . 1085 |
| 430.0 | . 1329 | . 1321 | . 1331 | . 1334 | . 1350 | . 1376 | . 1301 | . 1318 | . 1309 |
| 440.0 | . 1531 | . 1524 | . 1538 | . 1596 | . 1577 | . 1569 | . 1509 | . 1525 | . 1518 |
| 450.0 | . 1719 | . 1709 | . 1723 | . 1791 | . 1759 | . 1728 | . 1697 | . 1720 | . 1708 |
| 460.0 | . 1867 | . 1854 | . 1864 | . 1919 | . 1899 | . 1853 | . 1845 | . 1866 | . 1865 |
| 470.0 | . 1960 | . 1945 | . 1963 | - 2004 | . 1952 | -1957 | . 1938 | . 1957 | - 1950 |
| 480.0 | . 1992 | . 1976 | . 1990 | . 1996 | . 1996 | . 1988 | . 1969 | . 1990 | . 1989 |
| 490.0 | . 1988 | . 1922 | . 1984 | . 1960 | . 1981 | . 1964 | . 1963 | . 1981 | . 1982 |
| 500.0 | . 1910 | . 1901 | . 1908 | . 1897 | . 1905 | . 1884 | . 1892 | . 1912 | . 1909 |
| 510.0 | . 1877 | . 1868 | . 1874 | . 1878 | . 1871 | -1912 | . 1855 | . 1876 | . 1874 |
| 520.0 | . 1972 | -1960 | . 1968 | -1977 | . 1950 | -1944 | . 1942 | . 1955 | -1957 |
| 530.0 | . 2322 | . 2311 | . 2309 | - 2359 | . 2369 | . 2309 | . 2275 | - 2274 | - 2284 |
| 540.0 | . 3000 | - 2976 | . 2993 | - 2974 | . 2992 | - 2906 | . 2923 | - 2922 | - 2928 |
| 550.0 | . 3851 | . 3818 | . 3843 | - 3825 | . 3819 | - 3736 | . 3760 | -3767 | - 3768 |
| 560.0 | . 4902 | . 4882 | . 4892 | . 4911 | . 4849 | . 4799 | . 4812 | . 4837 | . 4833 |
| 570.0 | . 5569 | - 5550 | . 5566 | . 5471 | - 5390 | - 5397 | . 5480 | . 5511 | - 5514 |
| 580.0 | . 5780 | - 5761 | . 5778 | . 5634 | - 5547 | - 5602 | . 5702 | . 5730 | - 5742 |
| 590.0 | . 5415 | . 5399 | . 5404 | - 5400 | . 5319 | . 5414 | . 5381 | . 5406 | . 5407 |
| 600.0 | . 4759 | . 4744 | . 4758 | . 4769 | . 4708 | . 4832 | . 4729 | . 4750 | . 4763 |
| 610.0 | . 3956 | - 3915 | . 3924 | - 3998 | . 3939 | . 4006 | . 3923 | - 3948 | - 3973 |
| 620.0 | . 3081 | . 3074 | . 3072 | - 3138 | - 3129 | - 3192 | . 3082 | -3112 | - 3126 |
| 630.0 | . 2365 | . 2349 | . 2361 | . 2420 | . 2407 | . 2416 | . 2361 | . 2378 | . 2400 |
| 640.0 | . 1774 | . 1770 | . 1766 | - 1759 | . 1804 | . 1809 | . 1481 | -1819 | - 1828 |
| 650.0 | . 1306 | . 1299 | . 1295 | - 1325 | . 1341 | -1384 | . 1302 | . 1336 | . 1345 |
| 660.0 | . 0956 | . 0948 | . 0938 | . 0977 | . 1055 | . 0997 | . 0952 | . 0971 | . 0980 |
| 670.0 | . 0718 | . 0703 | . 0703 | . 0737 | . 0744 | . 0740 | . 0705 | . 0708 | . 0730 |
| 680.0 | . 0524 | . 0522 | . 0510 | . 0551 | . 0535 | . 0584 | . 0520 | . 0522 | . 0550 |
| 690.0 | . 0418 | . 0415 | . 0404 | . 0422 | . 0468 | . 0456 | . 0409 | . 0412 | . 0438 |
| 700.0 | . 0304 | . 0303 | . 0290 | . 0309 | . 0372 | . 0363 | . 0295 | . 0307 | . 0333 |
| 710.0 | . 0256 | . 0255 | . 0240 | . 0251 | . 0254 | . 0288 | . 0240 | . 0253 | . 0270 |
| 720.0 | . 0213 | . 0196 | . 0179 | . 0202 | . 0226 | . 0248 | . 0187 | . 0188 | . 0218 |
| 730.0 | . 0265 | . 0265 | . 0246 | . 0000 | . 0000 | . 0000 | . 0158 | . 0160 | . 0193 |
| 740.0 | . 0178 | . 0178 | . 0156 | . 0000 | . 0000 | . 0000 | . 0167 | . 0170 | . 0208 |
| 750.0 | . 0213 | . 0213 | . 0186 | . 0000 | . 0000 | . 0000 | . 0179 | . 0152 | . 0227 |
| 760.0 | . 0198 | . 0198 | . 0132 | . 0000 | . 0000 | . 0000 | . 0123 | . 0126 | . 0179 |

## MERCURY LINES

| 405.0 | .1897 | .1908 | .1931 | .1806 | .2072 | .1897 | .1903 | .1943 | .1903 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 436.0 | .4696 | .4681 | .4713 | .5054 | .4856 | .4785 | .4651 | .4743 | .4722 |
| 546.0 | .2255 | .2242 | .2252 | .2298 | .2330 | .2240 | .2236 | .2245 | .2233 |
| 578.0 | .0769 | .0761 | .0761 | .0746 | .0737 | .0721 | .0748 | .0752 | .0751 |



FIGURE 4.21 AVERAGE SPECTRAL FLUX (SPHERE MEASUREMENTS)

RELATIVE SPECTRAL FLUX DISTRIBUTION IN SPHERE-NORMALIZED TO AREA LAMP NUMBER NBS8801

|  | NBS INITIAL |  |  | LABORATORY 5 |  |  | MBS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 |
| 380.0 | 4.0 | 3.8 | 4.1 | 3.7 | 3.3 | 3.4 | 3.8 | 3.7 | 3.8 |
| 390.0 | 5.9 | 6.0 | 5.9 | 5.9 | 5.4 | 5.5 | 5.7 | 5.7 | 5.9 |
| 400.0 | 8.4 | 8.4 | 8.5 | 9.1 | 8.9 | 9.0 | 8.3 | 8.3 | 8.2 |
| 410.0 | 10.7 | 10.7 | 10.8 | 10.8 | 10.6 | 10.5 | 10.7 | 10.7 | 10.6 |
| 420.0 | 13.1 | 13.1 | 13.2 | 13.9 | 13.8 | 13.8 | 13.1 | 13.1 | 12.9 |
| 430.0 | 16.0 | 16.1 | 16.0 | 16.3 | 16.2 | 16.3 | 15.9 | 15.8 | 15.9 |
| 440.0 | 18.6 | 18.6 | 18.6 | 18.8 | 18.8 | 18.7 | 18.4 | 18.4 | 18.5 |
| 450.0 | 20.8 | 20.8 | 20.9 | 21.7 | 21.6 | 21.6 | 20.7 | 19.4 | 20.9 |
| 460.0 | 22.5 | 22.6 | 22.6 | 23.2 | 23.0 | 23.2 | 22.6 | 22.6 | 22.6 |
| 470.0 | 23.6 | 23.7 | 23.7 | 24.3 | 24.4 | 24.3 | 23.6 | 23.7 | 23.8 |
| 480.0 | 24.0 | 24.0 | 24.0 | 24.5 | 24.6 | 24.6 | 24.1 | 24.2 | 24.0 |
| $490 \cdot 0$ | 23.9 | 24.0 | 24.0 | 24.4 | 24.4 | 24.4 | 24.0 | 24.1 | 23.9 |
| 500.0 | 23.0 | 23.0 | 23.0 | 24.1 | 24.0 | 24.0 | 23.1 | 23.2 | 23.1 |
| 510.0 | 22.6 | 22.6 | 22.7 | 23.6 | 23.7 | 24.2 | 22.7 | 22.7 | 22.6 |
| 520.0 | 23.7 | 23.7 | 23.8 | 24.8 | 24.9 | 24.8 | 23.6 | 23.9 | 23.6 |
| 530.0 | 27.8 | 27.8 | 28.0 | 29.4 | 29.7 | 29.8 | 27.6 | 27.7 | 27.6 |
| 540.0 | 35.9 | 36.0 | 36.0 | 38.3 | 38.7 | 38.6 | 35.5 | 35.1 | 35.4 |
| 550.0 | 46.0 | 46.1 | 46.2 | 49.5 | 50.4 | 49.9 | 45.6 | 45.7 | 45.4 |
| 560.0 | 58.6 | 58.7 | 58.8 | 61.8 | 62.0 | 61.8 | 58.3 | 58.4 | 58.0 |
| 570.0 | 66.5 | 66.6 | 66.8 | 68.1 | 66.9 | 67.4 | 66.4 | 66.6 | 66.3 |
| 580.0 | 68.9 | 69.1 | 69.3 | 68.5 | 67.6 | 68.4 | 69.2 | 69.4 | 69.0 |
| 590.0 | 64.6 | $64 \cdot 6$ | 65.0 | 67.2 | 67.2 | 67.3 | 65.4 | 65.5 | 65.1 |
| 600.0 | 56.9 | 56.9 | 57.1 | 59.0 | 59.6 | 59.5 | 57.4 | 57.5 | 57.3 |
| 610.0 | 47.1 | 46.9 | 47.1 | 47.7 | 48.5 | 48.5 | 47.7 | 47.9 | 47.7 |
| 620.0 | 36.9 | 36.7 | 36.8 | 37.6 | 37.6 | 37.4 | 37.5 | 37.8 | 37.9 |
| 630.0 | 28.4 | 28.2 | 28.4 | 28.1 | 28.2 | 28.0 | 28.6 | 28.9 | 28.9 |
| 640.0 | 21.2 | 21.1 | 21.2 | 20.2 | 20.7 | 20.3 | 21.5 | 21.6 | 21.6 |
| 650.0 | 15.5 | 15.5 | 15.5 | 13.5 | 13.8 | 13.6 | 15.9 | 15.8 | 15.8 |
| 660.0 | 11.2 | 11.3 | 11.2 | 9.8 | 9.8 | 9.8 | 11.4 | 11.5 | 11.6 |
| 670.0 | 8.4 | 8.3 | 8.4 | 5.6 | 5.7 | 5.7 | 8.6 | 8.6 | 8.5 |
| 680.0 | 6.2 | 6.1 | 5.9 | 3.1 | 3.2 | 3.2 | 6.2 | 6.2 | 6.3 |
| 690.0 | 4.8 | 4.8 | 4.6 | 2.5 | 2.1 | 1.8 | 4.9 | 4.9 | 4.9 |
| 700.0 | 3.4 | 3.5 | 3.4 | 2.0 | 2.0 | 2.4 | 3.6 | 3.6 | 3.6 |
| 710.0 | 3.1 | 2.9 | 2.8 | . 0 | . 4 | . 4 | 3.0 | 3.1 | 3.1 |
| 720.0 | 2.4 | 2.4 | 2.0 | . 0 | - 0 | . 0 | 2.4 | 2.3 | 2.2 |
| 730.0 | $3 \cdot 3$ | 3.2 | 2.8 | . 0 | . 0 | . 0 | 2.0 | 1.8 | 1.8 |
| 740.0 | 2.2 | 2.2 | 1.6 | . 0 | . 0 | . 0 | 2.1 | $2 \cdot 1$ | 2.2 |
| 750.0 | 2.6 | 2.6 | 2.0 | . 0 | . 0 | . 0 | 2.5 | 2.2 | 2.3 |
| 760.0 | 2.4 | 2.0 | 1.6 | . 0 | - 0 | . 0 | 1.9 | 1.5 | 1.6 |

## MERCURY LINES

| 405.0 | 22.7 | 22.9 | 22.9 | 19.7 | 18.8 | 19.6 | 22.8 | 22.9 | 23.2 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 56.7 | 56.9 | 56.9 | 55.0 | 53.0 | 52.3 | 56.4 | 56.7 | 57.1 |
| 546.0 | 26.4 | 26.5 | 26.7 | 28.0 | 28.4 | 28.8 | 26.5 | 26.3 | 26.5 |
| 578.0 | 9.1 | 9.1 | 9.1 | 16.2 | 18.2 | 17.1 | 8.9 | 8.9 | 8.9 |



FIGURE 4.22 GVERAGE RELATIVE SPECTRAL FLUX (SPHERE MEASUREMENTS) NORMALIZED TO AREA

NBS INITIAL

| WAVELENGTH RUN 1 |  |
| :---: | :---: |
| 380.0 | .0320 |

4

|  |
| :---: |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |
|  |  |



FIGURE 4.23 GVERAGE SPECTRAL fLUX (SPHERE MEASUREMENTS)

RELATIVE SPECTRAL FLUX DISTRIBUTION IN SPHERE-NORMALIZED TO AREA LAMP NUMBER NBS8802

|  | NBS INITIAL |  |  | LABORATORY 5 |  |  | NBS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 |
| 380.0 | 4.0 | 3.9 | 4.0 | 3.6 | 3.4 | 3.5 | 3.5 | 3.6 | 3.9 |
| 390.0 | 5.9 | $6 \cdot 1$ | 6.0 | 5.7 | 5.7 | 5.8 | 5.7 | 5.7 | 6.0 |
| 400.0 | 8.4 | 8.7 | 8.7 | 9.0 | 9.0 | 9.0 | 8.3 | 8.3 | 8.5 |
| 410.0 | 10.7 | 10.9 | 11.0 | 10.9 | 10.8 | 6.0 | 10.6 | 10.7 | $10 \cdot 8$ |
| 420.0 | 13.1 | 13.2 | 13.4 | 13.7 | 13.7 | 13.8 | 13.1 | 13.1 | 13.1 |
| 430.0 | 16.2 | 16.1 | 16.2 | 16.6 | 16.4 | 16.5 | 16.0 | 15.9 | 16.1 |
| 440.0 | 18.7 | 18.6 | 18.7 | 18.8 | 18.7 | 19.0 | 18.5 | 18.5 | 18.6 |
| 450.0 | 21.0 | 20.9 | 21.0 | 21.6 | 21.5 | 21.9 | 20.9 | 19.5 | 21.0 |
| 460.0 | 22.6 | 22.6 | 22.8 | 23.0 | 23.3 | 23.5 | 22.6 | 22.8 | 22.7 |
| 470.0 | 23.7 | 23.7 | 23.8 | 24.1 | 24.2 | 24.2 | 23.8 | 23.8 | 23.8 |
| 480.0 | 24.0 | 24.0 | 24.2 | 24.7 | 24.7 | 24.8 | 24.2 | 24.2 | 24.1 |
| 490.0 | 23.9 | 23.3 | 24.0 | 24.5 | 24.3 | 24.7 | 23.5 | 24.1 | 24.1 |
| 500.0 | 23.0 | 23.0 | 23.1 | 23.8 | 23.8 | 23.9 | 23.2 | 23.3 | 23.1 |
| 510.0 | 22.6 | 22.6 | 22.6 | 23.3 | 24.1 | 24.4 | 22.8 | 22.8 | 22.6 |
| 520.0 | 23.7 | 23.7 | 23.7 | 24.8 | 25.1 | 25.0 | 23.7 | 23.9 | 23.6 |
| 530.0 | 27.8 | 27.9 | 27.9 | 29.5 | 29.7 | 29.7 | 27.7 | 27.7 | 27.6 |
| 540.0 | 36.0 | 35.9 | 36.0 | 38.3 | 38.9 | 39.0 | 35.6 | 35.0 | 35.4 |
| 550.0 | 46.1 | 46.0 | 46.2 | 49.5 | 50.1 | 50.2 | 45.8 | 45.6 | 45.5 |
| 560.0 | 58.5 | 58.6 | 58.7 | 61.7 | 62.1 | 62.3 | 58.4 | 58.5 | 58.0 |
| 570.0 | 66.4 | 66.5 | 66.7 | 67.4 | 67.4 | 67.4 | 66.6 | 66.7 | 66.2 |
| 580.0 | 68.8 | 68.9 | 69.2 | 68.1 | 67.9 | 68.2 | 69.3 | 69.3 | 68.8 |
| 590.0 | 64.5 | 64.6 | 64.8 | 67.2 | 67.4 | 67.6 | 65.3 | 65.4 | 64.9 |
| 600.0 | 57.1 | 56.7 | 56.7 | 59.3 | 59.0 | 59.3 | 57.5 | 57.6 | 57.1 |
| 610.0 | 46.8 | 47.0 | 47.0 | 48.3 | 48.0 | 48.0 | 47.6 | 47.8 | 47.6 |
| 620.0 | 36.6 | 36.8 | 36.8 | 37.7 | 37.4 | 37.8 | 37.4 | 37.7 | 37.8 |
| 630.0 | 28.2 | 28.1 | 28.3 | 28.4 | 27.9 | 28.7 | 28.6 | 28.7 | 28.5 |
| 640.0 | 21.1 | 21.1 | 21.1 | 21.0 | 20.4 | 20.8 | 21.5 | 21.5 | 21.4 |
| 650.0 | 15.4 | 15.5 | 15.3 | 14.6 | 13.8 | 14.5 | 15.7 | 15.8 | 16.2 |
| 660.0 | 11.3 | 11.3 | 11.3 | 9.9 | 9.7 | 9.9 | 11.5 | 11.5 | 11.7 |
| 670.0 | 8.4 | 8.5 | 8.3 | 5.8 | 5.6 | 5.9 | 8.4 | 8.5 | 8.5 |
| 680.0 | 6.2 | 6.2 | 6.1 | 3.1 | 3.1 | 3.1 | 6.2 | 6.2 | 6.2 |
| 690.0 | 4.9 | 4.9 | 4.8 | 2.8 | 2.1 | 2.8 | 4.9 | 4.9 | 4.9 |
| 700.0 | 3.7 | 3.5 | 3.4 | 3.1 | 1.6 | 2.7 | 3.5 | 3.6 | 3.6 |
| 710.0 | 3.1 | 3.1 | 2.8 | - 8 | . 4 | . 8 | 3.0 | 2.9 | 2.9 |
| 720.0 | 2.4 | 2.4 | 2.0 | . 4 | - 0 | . 0 | 2.2 | 2.1 | 2.2 |
| 730.0 | 3.2 | 3.2 | 2.8 | - 0 | - 0 | . 0 | 1.8 | 1.9 | 1.8 |
| 740.0 | 2.2 | 2.1 | 1.6 | . 0 | - 0 | . 0 | 2.1 | 2.1 | 2.1 |
| 750.0 | 2.6 | 2.6 | 1.9 | . 0 | - 0 | . 0 | 2.5 | 2.4 | 2.5 |
| 760.0 | 2.4 | 2.4 | 1.6 | . 0 | - 0 | . 0 | 1.5 | 1.5 | 1.6 |

## MERCURY LINES

| 405.0 | 22.8 | 22.9 | 23.2 | 19.8 | 20.1 | 15.2 | 23.0 | 23.1 | 23.2 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 56.1 | 56.3 | 56.8 | 52.2 | 52.8 | 53.7 | 56.2 | 56.8 | 56.7 |
| 546.0 | 26.6 | 26.6 | 26.6 | 26.9 | 28.8 | 28.7 | 26.6 | 26.3 | 26.4 |
| 578.0 | 9.2 | 9.2 | 9.2 | 16.2 | 17.1 | 17.4 | 9.0 | 9.0 | 9.0 |



FIGURE 4.24 AVERAGE RELATIVE SPECTRAL FLUX (SPhERE MEASUREMENTS) NORMALIZED TO AREA

SPECTRAL FLUX DISTRIBUTION (WATTS) IN SPHERE
LAMP NUMBER NBS8802

|  | NBS INITIAL |  |  | LABORATORY 5 |  |  | NBS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 |
| 380.0 | . 0328 | . 0320 | . 0328 | . 0282 | . 0260 | . 0269 | . 0285 | . 0292 | . 0320 |
| 390.0 | . 0490 | . 0505 | . 0497 | . 0442 | . 0441 | . 0450 | . 0456 | . 0462 | . 0492 |
| 400.0 | . 0696 | . 0720 | . 0714 | . 0705 | . 0696 | . 0699 | . 0666 | . 0678 | . 0697 |
| 410.0 | . 0886 | . 0900 | . 0903 | . 0846 | . 0833 | . 0468 | . 0858 | . 0872 | . 0891 |
| 420.0 | . 1085 | . 1098 | . 1099 | . 1068 | . 1055 | . 1069 | . 1057 | . 1067 | . 1081 |
| 430.0 | . 1334 | . 1339 | . 1331 | . 1291 | . 1262 | . 1276 | . 1287 | . 1293 | . 1322 |
| 440.0 | . 1541 | . 1545 | . 1539 | . 1465 | . 1445 | . 1473 | . 1492 | . 1506 | . 1531 |
| 450.0 | .1731 | . 1731 | . 1726 | . 1680 | - 1659 | . 1696 | . 1685 | . 1588 | . 1728 |
| 460.0 | . 1867 | . 1872 | . 1871 | . 1793 | . 1797 | . 1822 | . 1824 | . 1857 | . 1867 |
| 470.0 | .1956 | . 1963 | . 1956 | . 1879 | . 1866 | . 1878 | . 1917 | . 1939 | . 1962 |
| 480.0 | . 1984 | . 1994 | . 1986 | . 1921 | . 1903 | . 1919 | . 1949 | . 1972 | . 1986 |
| 490.0 | .1977 | . 1936 | . 1973 | . 1908 | . 1872 | . 1911 | . 1890 | . 1966 | . 1981 |
| 500.0 | . 1899 | . 1908 | . 1901 | . 1857 | . 1839 | . 1856 | . 1869 | . 1896 | . 1903 |
| 510.0 | . 1867 | . 1875 | . 1859 | . 1812 | . 1860 | . 1894 | . 1834 | . 1856 | . 1861 |
| 520.0 | . 1953 | . 1964 | - 1950 | -1931 | . 1935 | -1937 | . 1913 | . 1951 | . 1942 |
| 530.0 | . 2295 | . 2315 | . 2290 | - 2299 | . 2292 | . 2305 | . 2233 | - 2256 | - 2268 |
| 540.0 | . 2968 | . 2979 | - 2961 | - 2983 | . 3000 | - 3023 | - 2868 | - 2853 | . 2916 |
| 550.0 | - 3805 | . 3815 | . 3796 | - 3856 | - 3861 | - 3894 | - 3688 | - 3721 | - 3742 |
| 560.0 | . 4831 | . 4863 | . 4826 | - 4803 | . 4787 | . 4829 | . 4709 | . 4769 | . 4779 |
| 570.0 | . 5479 | . 5512 | . 5481 | - 5252 | - 5198 | . 5224 | - 5366 | . 5434 | - 5448 |
| 580.0 | . 5684 | . 5715 | - 5689 | - 5305 | . 5234 | . 5283 | . 5583 | . 5653 | . 5668 |
| 590.0 | . 5327 | . 5360 | . 5328 | - 5233 | - 5200 | - 5238 | - 5265 | - 5329 | - 5345 |
| 600.0 | . 4711 | . 4702 | . 4663 | . 4617 | . 4549 | -4593 | . 4631 | - 4698 | . 4701 |
| 610.0 | . 3865 | - 3895 | . 3860 | - 3760 | . 3701 | - 3724 | . 3836 | . 3896 | . 3917 |
| 620.0 | . 3024 | - 3053 | - 3022 | . 2940 | . 2884 | - 2931 | . 3016 | - 3070 | - 3110 |
| 630.0 | . 2325 | . 2333 | . 2330 | - 2214 | . 2151 | - 2228 | . 2306 | - 2339 | - 2349 |
| 640.0 | . 1739 | . 1752 | . 1731 | . 1636 | . 1577 | . 1613 | . 1735 | - 1750 | . 1759 |
| 650.0 | . 1275 | . 1289 | - 1255 | . 1134 | . 1067 | -1120 | - 1268 | - 1285 | . 1332 |
| 660.0 | . 0934 | . 0937 | . 0927 | . 0768 | . 0750 | . 0770 | . 0926 | . 0938 | . 0959 |
| 670.0 | . 0697 | . 0703 | . 0682 | . 0452 | . 0432 | . 0454 | . 0679 | . 0690 | . 0703 |
| 680.0 | . 0513 | . 0511 | . 0500 | . 0240 | . 0241 | . 0241 | . 0502 | . 0503 | . 0514 |
| 690.0 | . 0406 | . 0404 | . 0392 | - 0216 | . 0162 | . 0216 | . 0391 | . 0401 | . 0401 |
| 700.0 | . 0304 | . 0290 | . 0278 | . 0243 | . 0122 | . 0212 | . 0285 | . 0295 | . 0292 |
| 710.0 | . 0256 | . 0255 | . 0226 | . 0061 | . 0031 | . 0061 | . 0240 | . 0240 | . 0236 |
| $720 \cdot 0$ | . 0197 | . 0196 | . 0163 | -0033 | . 0000 | . 0000 | . 0174 | . 0174 | . 0180 |
| 730.0 | . 0265 | . 0265 | . 0227 | . 0000 | . 0000 | . 0000 | . 0144 | . 0158 | . 0149 |
| 740.0 | . 0178 | . 0178 | . 0133 | . 0000 | . 0000 | . 0000 | . 0168 | . 0167 | . 0173 |
| 750.0 | . 0213 | . 0213 | . 0160 | . 0000 | . 0000 | . 0000 | . 0199 | . 0199 | -0207 |
| 760.0 | . 0198 | . 0198 | . 0132 | . 0000 | . 0000 | -0000 | . 0122 | . 0123 | . 0128 |

MERCURY LINES

| 405.0 | .1885 | .1901 | .1906 | .1544 | .1552 | .1176 | .1854 | .1882 | .1912 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 436.0 | .4633 | .4667 | .4665 | .4064 | .4071 | .4164 | .4527 | .4627 | .4672 |
| 546.0 | .2195 | .2203 | .2190 | .2097 | .2223 | .2228 | .2140 | .2143 | .2170 |
| 578.0 | .0759 | .0766 | .0752 | .1260 | .1318 | .1349 | .0727 | .0732 | .0737 |



FIGURE 4.25 AVERAGE SPECTRAL FLUX (SPHERE MEASUREMENTS)

RELATIVE SPECTRAL FLUX DISTRIBUTION IN SPHERE-NORMALIZED TO AREA LAMP NUMBER NBS8805

|  | NBS INITIAL |  |  | LABORATORY 2 |  |  | NBS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 |
| 380.0 | 3.9 | 3.8 | 3.8 | . 0 | . 0 | . 0 | 3.8 | 3.8 | 3.7 |
| 390.0 | 5.9 | 6.0 | 5.9 | 6.3 | 4.7 | 4.1 | 5.9 | 5.7 | 5.8 |
| 400.0 | 8.7 | 8.4 | 8.5 | 8.3 | 7.6 | 7.4 | 8.5 | 8.3 | 8.3 |
| 410.0 | 11.0 | 10.6 | 10.7 | 10.8 | 10.3 | 10.4 | 10.8 | 10.7 | 10.7 |
| 420.0 | 13.3 | 14.0 | 13.2 | 13.1 | 12.9 | 13.1 | 13.3 | 13.1 | 13.1 |
| 430.0 | 16.0 | 16.0 | 16.1 | 16.0 | 15.8 | 16.2 | 16.1 | 16.1 | 16.0 |
| 440.0 | 18.5 | 18.6 | 18.6 | 18.6 | 18.4 | 18.9 | 18.7 | 18.5 | 18.5 |
| 450.0 | 20.9 | 20.8 | 20.9 | 20.6 | 20.5 | 20.8 | 21.0 | 20.9 | 20.9 |
| 460.0 | 22.7 | 22.7 | 22.2 | 22.4 | 22.3 | 22.6 | 22.7 | 22.6 | 22.6 |
| 470.0 | 23.8 | 23.9 | 23.7 | 23.5 | 23.4 | 23.7 | 23.9 | 23.8 | 23.8 |
| 480.0 | 24.2 | 24.2 | 24.1 | 24.0 | 23.8 | 24.1 | 24.3 | 24.2 | 24.2 |
| 490.0 | 24.0 | 24.0 | 23.9 | 23.9 | 23.8 | 24.0 | 24.1 | 24.1 | 24.0 |
| 500.0 | 23.1 | 23.1 | 23.1 | 23.2 | 23.0 | 23.3 | 23.2 | 23.2 | 23.2 |
| 510.0 | 22.7 | 22.7 | 22.7 | 22.9 | 22.7 | 23.0 | 22.8 | 22.8 | 22.7 |
| 520.0 | 23.7 | 23.8 | 23.7 | 24.2 | 24.0 | 24.3 | 23.7 | 23.7 | 23.8 |
| 530.0 | 27.9 | 27.9 | 27.9 | 28.4 | 28.1 | 28.6 | 27.7 | 27.7 | 27.7 |
| 540.0 | 36.0 | 36.0 | 36.0 | 36.9 | 36.6 | 37.1 | 35.6 | 35.6 | 35.5 |
| 550.0 | 46.1 | 46.2 | 46.2 | 47.2 | 46.7 | 47.4 | 45.7 | 45.7 | 45.6 |
| 560.0 | 58.7 | 58.9 | 58.9 | 59.2 | 58.6 | 59.4 | 58.4 | 58.4 | 58.3 |
| 570.0 | 66.5 | 66.8 | 66.7 | 67.0 | 66.4 | 67.4 | 66.5 | 66.4 | 66.4 |
| 580.0 | 68.9 | 69.1 | 69.1 | 69.3 | 68.7 | 69.6 | 69.1 | 69.1 | 69.1 |
| 590.0 | 64.5 | 64.7 | 64.8 | 65.5 | 64.9 | 65.6 | 65.1 | 65.1 | 65.1 |
| 600.0 | 56.7 | 56.9 | 56.8 | 57.6 | 57.2 | 57.5 | 57.2 | 57.2 | 57.3 |
| 610.0 | 46.8 | 47.0 | 46.9 | 47.8 | 47.6 | 47.5 | 47.4 | 47.5 | 47.5 |
| 620.0 | 36.6 | 36.7 | 36.8 | 37.8 | 37.4 | 37.6 | 37.3 | 37.3 | 37.2 |
| 630.0 | 28.0 | 28.3 | 28.3 | 28.9 | 28.7 | 28.8 | 28.5 | 28.4 | 28.4 |
| 640.0 | 21.0 | 21.1 | 20.9 | 21.7 | 21.5 | 21.6 | 21.4 | 21.4 | 21.5 |
| 650.0 | 15.4 | 15.6 | 15.5 | 16.1 | 15.9 | 16.0 | 15.6 | 15.7 | 15.6 |
| 660.0 | 11.1 | 11.2 | 11.4 | 11.8 | 11.8 | 11.7 | 11.4 | 11.4 | 11.4 |
| 670.0 | 8.4 | 8.2 | 8.2 | 8.7 | 8.6 | 8.6 | 8.3 | 8.5 | 8.5 |
| 680.0 | 6.1 | 6.0 | 6.0 | 6.4 | 6.3 | 6.3 | 6.1 | 6.3 | 6.2 |
| 690.0 | 4.8 | 4.7 | $4 \cdot 8$ | 4.9 | $4 \cdot 8$ | 4.8 | 4.8 | 4.9 | 5.0 |
| 700.0 | 3.4 | 3.3 | 3.4 | 3.7 | 3.6 | 3.6 | 3.5 | 3.5 | 3.6 |
| 710.0 | 3.1 | 2.7 | 2.7 | 2.8 | 2.8 | 2.8 | 2.8 | 2.9 | 3.1 |
| 720.0 | 2.4 | 2.4 | 2.4 | 2.1 | 2.0 | 2.0 | 2.2 | 2.4 | 2.4 |
| 730.0 | 3.2 | 3.2 | 3.2 | 1.7 | 1.6 | 1.7 | 1.8 | 1.9 | 1.9 |
| 740.0 | 2.2 | 2.1 | 2.1 | 1.6 | 1.4 | 1.5 | 1.9 | 2.3 | 2.3 |
| 750.0 | 2.6 | 1.9 | 2.6 | 1.4 | 1.3 | 1.3 | 2.2 | 2.2 | 2.4 |
| 760.0 | 2.4 | 1.6 | 1.6 | . 0 | . 0 | . 0 | 1.5 | 1.8 | 1.8 |

## MERCURY LINES

| 405.0 | 22.7 | 22.7 | 23.1 | 24.2 | 23.8 | 24.3 | 23.0 | 22.9 | 22.9 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 56.5 | 56.4 | 56.4 | 53.4 | 54.3 | 53.9 | 56.4 | 56.5 | 56.8 |
| 546.0 | 26.5 | 26.6 | 26.9 | 26.3 | 25.9 | 27.0 | 26.7 | 26.5 | 26.5 |
| 578.0 | 9.0 | 9.1 | 9.1 | 9.9 | 10.0 | 10.2 | 8.8 | 8.9 | 8.8 |



FIGURE 4.26 AVERAGE RELATIVE SPECTRAL FLUX (SPHERE MEASUREMENTS) NORMALIZED TO AREA

|  | NBS INITIAL |  |  | LABORATORY 2 |  |  | NBS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 |
| 380.0 | . 0320 | . 0315 | . 0316 | . 0000 | . 0000 | . 0000 | . 0311 | . 0308 | . 0304 |
| 390.0 | . 0482 | . 0490 | . 0489 | . 0473 | . 0354 | . 0308 | . 0478 | . 0467 | . 0476 |
| 400.0 | . 0708 | . 0691 | . 0701 | . 0623 | . 0565 | . 0553 | . 0690 | . 0673 | . 0679 |
| 410.0 | . 0895 | . 0870 | . 0884 | . 0813 | . 0771 | . 0781 | . 0882 | . 0867 | . 0876 |
| 420.0 | . 1086 | -1149 | . 1088 | . 0989 | . 0959 | . 0982 | . 1081 | . 1067 | . 1072 |
| 430.0 | .1310 | . 1317 | . 1330 | . 1203 | . 1181 | . 1212 | . 1310 | . 1305 | . 1306 |
| 440.0 | . 1515 | . 1526 | . 1538 | . 1398 | . 1373 | . 1412 | . 1520 | . 1507 | .1513 |
| 450.0 | . 1711 | . 1710 | . 1721 | . 1552 | . 1527 | . 1558 | . 1710 | . 1697 | . 1707 |
| 460.0 | .1853 | . 1861 | . 1828 | . 1684 | . 1659 | . 1691 | . 1851 | . 1839 | . 1847 |
| 470.0 | . 1944 | - 1958 | . 1957 | . 1770 | . 1741 | . 1773 | . 1945 | . 1935 | . 1944 |
| 480.0 | .1973 | . 1984 | . 1987 | . 1804 | . 1771 | . 1804 | . 1982 | . 1971 | . 1980 |
| 490.0 | . 1963 | . 1968 | . 1974 | . 1801 | .1771 | . 1798 | . 1961 | . 1960 | . 1964 |
| 500.0 | . 1888 | . 1899 | . 1906 | . 1745 | . 1713 | .1740 | . 1892 | . 1886 | . 1894 |
| 510.0 | . 1852 | -1862 | . 1872 | . 1724 | . 1694 | . 1722 | . 1858 | . 1853 | . 1855 |
| 520.0 | . 1940 | . 1950 | . 1957 | . 1823 | .1787 | . 1815 | . 1935 | . 1927 | . 1941 |
| 530.0 | . 2282 | - 2288 | . 2301 | . 2142 | . 2097 | . 2136 | . 2260 | . 2252 | . 2264 |
| 540.0 | . 2940 | - 2955 | . 2969 | . 2782 | . 2724 | . 2774 | . 2904 | . 2891 | . 2904 |
| 550.0 | . 3766 | . 3794 | . 3811 | . 3554 | . 3482 | . 3544 | . 3727 | . 3712 | . 3728 |
| 560.0 | . 4792 | . 4835 | . 4855 | . 4456 | . 4365 | . 4445 | . 4755 | . 4743 | . 4761 |
| 570.0 | . 5435 | . 5481 | . 5503 | . 5047 | . 4952 | . 5042 | . 5417 | . 5399 | . 5425 |
| 580.0 | . 5629 | . 5671 | . 5699 | . 5217 | . 5121 | . 5208 | . 5633 | . 5614 | . 5645 |
| 590.0 | . 5270 | . 5311 | . 5343 | . 4937 | . 4836 | . 4907 | . 5307 | . 5290 | . 5321 |
| 600.0 | . 4635 | . 4673 | . 4687 | . 4342 | . 4265 | . 4302 | . 4664 | . 4652 | . 4683 |
| 610.0 | . 3827 | - 3857 | - 3871 | - 3598 | - 3526 | - 3556 | . 3861 | . 3864 | . 3879 |
| 620.0 | . 2990 | - 3011 | . 3036 | . 2844 | . 2788 | - 2812 | . 3037 | - 3030 | . 3040 |
| 630.0 | . 2289 | . 2322 | . 2330 | . 2177 | . 2138 | . 2152 | . 2319 | . 2311 | . 2320 |
| 640.0 | . 1717 | -1735 | . 1723 | . 1633 | . 1602 | . 1613 | . 1740 | . 1740 | . 1754 |
| 650.0 | . 1256 | -1282 | . 1274 | . 1211 | . 1184 | . 1194 | . 1273 | . 1275 | . 1279 |
| 660.0 | . 0907 | . 0920 | . 0937 | . 0889 | . 0883 | . 0875 | . 0927 | . 0924 | . 0929 |
| 670.0 | . 0682 | . 0676 | . 0680 | . 0658 | . 0639 | . 0644 | . 0678 | . 0688 | . 0691 |
| 680.0 | .0499 | . 0494 | . 0498 | . 0483 | . 0467 | . 0475 | . 0500 | . 0511 | . 0505 |
| 690.0 | . 0392 | . 0388 | . 0392 | . 0369 | . 0358 | . 0361 | . 0395 | . 0399 | . 0410 |
| 700.0 | . 0277 | -0275 | . 0277 | . 0275 | . 0265 | . 0270 | . 0289 | . 0285 | . 0296 |
| 710.0 | . 0254 | . 0224 | . 0226 | . 0213 | . 0207 | . 0207 | . 0231 | . 0240 | . 0251 |
| 720.0 | . 0196 | . 0194 | . 0196 | . 0159 | . 0151 | . 0151 | . 0175 | . 0198 | . 0199 |
| $730 \cdot 0$ | . 0264 | - 0262 | . 0265 | . 0128 | . 0118 | . 0126 | . 0145 | . 0157 | . 0158 |
| 740.0 | . 0176 | . 0176 | . 0177 | . 0123 | . 0107 | . 0112 | . 0152 | . 0183 | . 0184 |
| 750.0 | . 0212 | . 0158 | . 0212 | . 0105 | . 0099 | . 0101 | . 0181 | . 0178 | . 0199 |
| 760.0 | .0196 | . 0135 | . 0132 | . 0000 | . 0000 | . 0000 | . 0124 | . 0147 | . 0148 |

## MERCURY LINES

| 405.0 | .1854 | .1866 | .1908 | .1826 | .1775 | .1817 | .1876 | .1862 | .1871 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 436.0 | .4612 | .4628 | .4655 | .4024 | .4049 | .4027 | .4597 | .4588 | .4639 |
| 546.0 | .2164 | .2182 | .2219 | .1981 | .1931 | .2021 | .2176 | .2157 | .2165 |
| 578.0 | .0737 | .0746 | .0754 | .0749 | .0742 | .0763 | .0720 | .0722 | .0722 |



FIGURE 4.27 GVERAGE SPECTRAL FLUX (SPHERE MEASUREMENTS)

RELATIVE SPECTRAL FLUX DISTRIBUTION IN SPHERE-NORMALIZED TO AREA LAMP NUMBER NBS8806

|  | NBS INITIAL |  |  | LABORATORY 2 |  |  | NBS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 |
| 380.0 | 4.0 | 4.1 | 3.9 | . 0 | . 0 | . 0 | 3.9 | 3.8 | 3.9 |
| 390.0 | 6.0 | 6.1 | 6.1 | 5.7 | $5 \cdot 2$ | 4.6 | 5.9 | 5.9 | 6.0 |
| 400.0 | 8.8 | 8.8 | 8.7 | 8.0 | 8.0 | 7.8 | 8.5 | 8.5 | 8.5 |
| 410.0 | 11.1 | 11.2 | 11.0 | 10.7 | 10.8 | 10.8 | 10.9 | 10.9 | 10.9 |
| 420.0 | 13.4 | 14.3 | 13.5 | 13.3 | 13.3 | 13.3 | 13.4 | 13.3 | 13.3 |
| 430.0 | 16.3 | 16.4 | 16.4 | 16.3 | 16.3 | 16.3 | 16.3 | 16.3 | 16.2 |
| 440.0 | 18.8 | 18.9 | 18.9 | 19.0 | 18.9 | 18.9 | 18.9 | 18.8 | 18.8 |
| 450.0 | 21.2 | 21.6 | 21.2 | 21.0 | 21.1 | 21.0 | 21.2 | 21.1 | 21.2 |
| 460.0 | 22.9 | 22.6 | 22.9 | 22.8 | 22.8 | 22.8 | 23.0 | 22.9 | 22.9 |
| 470.0 | 24.0 | 24.0 | 24.1 | 23.8 | 23.9 | 23.8 | 24.2 | 24.1 | 24.1 |
| 480.0 | 24.3 | 24.3 | 24.4 | 24.2 | 24.3 | 24.2 | 24.6 | 24.5 | 24.5 |
| 490.0 | 24.3 | 24.2 | 24.3 | 24.2 | 24.3 | 24.2 | 24.4 | 24.4 | 24.3 |
| 500.0 | 23.3 | 23.3 | 23.4 | 23.4 | 23.4 | 23.4 | 23.5 | 23.5 | 23.4 |
| 510.0 | 22.8 | 22.8 | 22.9 | 23.0 | 23.1 | 23.1 | 23.0 | 23.0 | 22.9 |
| 520.0 | 23.8 | 23.8 | 23.9 | 24.2 | 24.2 | 24.2 | 23.8 | 23.8 | 23.8 |
| 530.0 | 27.8 | 27.8 | 27.8 | 28.2 | 27.7 | 28.4 | 27.6 | 27.6 | 27.6 |
| 540.0 | 35.7 | 35.7 | 35.7 | 36.4 | 36.6 | 36.7 | 35.3 | 35.2 | 35.3 |
| 550.0 | 45.7 | 45.7 | 45.8 | 46.5 | 46.9 | 46.8 | 45.2 | 45.2 | 45.2 |
| 560.0 | 58.1 | 58.2 | 58.3 | 58.3 | 58.5 | 58.8 | 57.7 | 57.7 | 57.7 |
| 570.0 | 65.9 | 66.1 | 66.2 | 66.2 | 66.4 | 66.8 | 65.8 | 65.8 | 65.9 |
| 580.0 | 68.4 | 68.6 | 68.7 | 68.6 | 68.8 | 69.1 | 68.6 | 68.5 | 68.7 |
| 590.0 | 64.2 | 64.4 | 64.5 | 65.1 | 65.1 | 65.4 | 64.7 | 64.7 | 64.9 |
| 600.0 | 56.5 | 56.6 | 56.8 | 57.4 | 57.4 | 57.5 | 57.0 | 57.0 | 57.0 |
| 610.0 | 46.8 | 46.8 | 46.9 | 47.6 | 47.5 | 47.6 | 47.2 | 47.3 | 47.4 |
| 620.0 | 36.6 | 36.7 | 36.8 | 37.7 | 37.7 | 37.7 | 37.2 | 37.4 | 37.3 |
| 630.0 | 28.1 | 28.1 | 28.3 | 28.9 | 28.9 | 29.0 | 28.5 | 28.4 | 28.5 |
| 640.0 | 21.4 | 20.9 | 21.0 | 21.7 | 21.7 | 21.7 | 21.4 | 21.4 | 21.4 |
| 650.0 | 15.4 | 15.3 | 15.5 | 16.1 | 16.1 | 16.1 | 15.7 | 15.8 | 15.8 |
| 660.0 | 11.3 | 11.2 | 11.2 | 11.8 | 11.9 | 11.9 | 11.5 | 11.5 | 11.5 |
| 670.0 | 8.5 | 8.3 | 8.3 | 8.7 | 8.8 | 8.7 | 8.5 | 8.7 | 8.5 |
| 680.0 | 6.2 | 6.0 | 6.0 | 6.4 | $6 \cdot 4$ | 6.4 | 6.2 | 6.3 | 6.3 |
| 690.0 | 4.9 | 4.8 | 4.8 | 4.9 | 4.9 | 4.9 | 4.9 | 5.0 | 5.0 |
| 700.0 | 3.6 | 3.4 | 3.4 | 3.7 | 3.7 | 3.7 | 3.6 | 3.6 | 3.5 |
| 710.0 | 3.0 | 2.8 | 2.8 | 2.9 | $2 \cdot 9$ | 2.8 | 2.9 | 2.9 | 2.9 |
| 720.0 | 2.5 | 2.3 | 2.3 | 2.1 | $2 \cdot 1$ | 2.1 | 2.2 | 2.4 | 2.4 |
| 730.0 | 3.4 | 3.1 | 3.1 | 1.7 | 1.7 | 1.7 | 1.9 | 1.9 | 1.9 |
| 740.0 | 2.1 | 1.8 | 1.8 | 1.6 | 1.6 | 1.6 | 1.8 | 2.0 | 2.0 |
| 750.0 | 2.2 | 1.9 | 1.9 | 1.5 | 1.5 | 1.4 | 1.9 | 2.1 | 1.9 |
| 760.0 | $2 \cdot 3$ | 1.9 | 1.6 | . 0 | . 0 | . 0 | 1.5 | 1.7 | 1.5 |

## MERCURY LINES

| 405.0 | 22.6 | 23.1 | 23.0 | 24.3 | 24.5 | 23.8 | 23.3 | 23.0 | 23.2 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 56.3 | 56.4 | 56.4 | 55.9 | 54.8 | 53.6 | 56.7 | 56.6 | 56.6 |
| 546.0 | 26.4 | 26.6 | 26.7 | 26.1 | 26.2 | 27.1 | 26.8 | 26.6 | 26.7 |
| 578.0 | 9.0 | 9.0 | 9.0 | 9.9 | 9.8 | 10.2 | 8.9 | 8.8 | 8.9 |



FIGURE 4.28 AVERAGE RELATIVE SPECTRAL FLUX (SPHERE MEASUREMENTS) NORMALIZEO TO AREA

SPECTRAL FLUX DISTRIBUTION (WATTS) IN SPHERE
LAMP NUMBER NBS8806

|  | NBS INITIAL |  |  | LABORATORY 2 |  |  | NBS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 |
| 380.0 | . 0340 | . 0343 | . 0330 | . 0000 | . 0000 | . 0000 | . 0325 | . 0322 | . 0331 |
| 390.0 | . 0508 | . 0512 | . 0511 | . 0447 | . 0400 | . 0350 | . 0498 | . 0496 | . 0505 |
| 400.0 | . 0742 | . 0745 | . 0735 | . 0624 | . 0623 | . 0596 | . 0712 | . 0710 | . 0717 |
| 410.0 | . 0931 | . 0941 | . 0930 | . 0838 | . 0839 | . 0820 | . 0912 | . 0912 | . 0921 |
| 420.0 | . 1130 | . 1203 | . 1134 | . 1037 | . 1035 | . 1013 | . 1122 | . 1120 | . 1124 |
| 430.0 | . 1374 | . 1380 | . 1380 | . 1276 | . 1267 | . 1234 | . 1365 | . 1366 | . 1366 |
| 440.0 | .1583 | . 1591 | . 1591 | . 1484 | . 1468 | . 1436 | . 1584 | . 1577 | . 1581 |
| 450.0 | . 1784 | . 1823 | . 1785 | . 1637 | . 1633 | . 1595 | -1781 | . 1775 | . 1783 |
| 460.0 | . 1927 | . 1905 | . 1931 | . 1777 | . 1766 | . 1729 | . 1929 | -1927 | . 1931 |
| 470.0 | . 2020 | . 2023 | - 2029 | . 1861 | . 1853 | . 1809 | - 2029 | - 2022 | - 2031 |
| 480.0 | . 2046 | . 2052 | . 2052 | .1893 | . 1884 | .1840 | . 2062 | . 2061 | . 2064 |
| 490.0 | . 2042 | . 2043 | . 2044 | .1886 | . 1881 | .1836 | - 2048 | - 2051 | . 2048 |
| 500.0 | .1960 | . 1962 | . 1970 | . 1826 | . 1817 | . 1775 | .1970, | . 1973 | . 1975 |
| 510.0 | . 1919 | . 1926 | . 1928 | . 1797 | .1790 | . 1751 | . 1927 | . 1929 | . 1932 |
| 520.0 | . 2004 | - 2009 | . 2011 | . 1888 | . 1879 | . 1840 | . 1993 | . 1998 | . 2005 |
| 530.0 | . 2339 | . 2347 | . 2346 | . 2202 | . 2147 | . 2154 | . 2315 | . 2318 | . 2327 |
| 540.0 | . 3002 | - 3007 | . 3012 | . 2844 | . 2839 | . 2785 | - 2959 | - 2962 | - 2977 |
| 550.0 | . 3841 | . 3852 | . 3857 | . 3630 | - 3638 | - 3555 | - 3790 | . 3797 | . 3813 |
| 560.0 | . 4885 | . 4907 | . 4910 | . 4555 | . 4536 | . 4461 | . 4836 | . 4849 | . 4864 |
| 570.0 | . 5545 | . 5573 | . 5576 | . 5171 | - 5150 | . 5070 | . 5517 | . 5529 | . 5552 |
| 580.0 | . 5753 | - 5783 | . 5789 | . 5356 | . 5333 | . 5248 | - 5746 | . 5760 | - 5788 |
| 590.0 | . 5397 | . 5428 | . 5438 | . 5082 | - 5050 | . 4960 | - 5427 | . 5440 | - 5471 |
| 600.0 | . 4752 | . 4770 | . 4783 | . 4479 | . 4449 | . 4363 | . 4780 | . 4794 | . 4804 |
| 610.0 | . 3935 | . 3941 | . 3952 | . 3716 | - 3687 | . 3612 | . 3959 | . 3977 | - 3993 |
| 620.0 | . 3075 | - 3096 | . 3097 | - 2941 | - 2922 | . 2861 | - 3118 | - 3145 | - 3144 |
| 630.0 | . 2366 | - 2370 | . 2383 | - 2255 | - 2243 | - 2197 | . 2386 | . 2390 | . 2400 |
| 640.0 | .1796 | . 1765 | . 1774 | . 1695 | . 1683 | . 1650 | . 1792 | . 1799 | -1805 |
| 650.0 | . 1299 | . 1288 | . 1306 | -1260 | . 1250 | . 1222 | . 1315 | -1325 | . 1329 |
| 660.0 | . 0950 | . 0944 | . 0941 | . 0925 | . 0919 | . 0900 | . 0962 | . 0968 | . 0973 |
| 670.0 | . 0714 | . 0699 | . 0702 | . 0682 | . 0679 | . 0662 | . 0713 | . 0731 | . 0717 |
| 680.0 | . 0521 | . 0507 | . 0509 | . 0502 | . 0496 | . 0488 | . 0517 | . 0528 | . 0531 |
| 690.0 | . 0415 | . 0401 | . 0403 | . 0386 | . 0382 | .0373 | . 0413 | . 0418 | . 0420 |
| 700.0 | . 0302 | . 0288 | . 0289 | . 0292 | . 0288 | . 0278 | . 0299 | . 0304 | . 0296 |
| 710.0 | . 0254 | . 0239 | . 0240 | . 0227 | . 0228 | . 0215 | . 0242 | . 0240 | . 0240 |
| 720.0 | . 0212 | . 0195 | . 0195 | . 0166 | . 0166 | . 0158 | . 0188 | . 0198 | . 0199 |
| 730.0 | . 0283 | . 0263 | . 0264 | . 0135 | . 0135 | . 0127 | . 0159 | . 0157 | . 0158 |
| 740.0 | . 0177 | . 0154 | . 0155 | . 0126 | . 0126 | . 0121 | . 0152 | . 0167 | . 0167 |
| 750.0 | . 0185 | . 0158 | . 0159 | . 0118 | . 0118 | . 0107 | . 0161 | . 0178 | . 0160 |
| 760.0 | . 0196 | . 0164 | . 0132 | . 0000 | . 0000 | . 0000 | . 0124 | . 0147 | . 0123 |

## MERCURY LINES

| 405.0 | .1903 | .1943 | .1939 | .1897 | .1899 | .1810 | .1957 | .1936 | .1952 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 436.0 | .4733 | .4752 | .4749 | .4366 | .4253 | .4065 | .4749 | .4760 | .4769 |
| 546.0 | .2223 | .2241 | .2246 | .2035 | .2033 | .2057 | .2244 | .2238 | .2255 |
| 578.0 | .0755 | .0762 | .0760 | .0773 | .0761 | .0772 | .0746 | .0740 | .0747 |



FIGURE 4.29 AVERAGE SPECTRAL FLUX (SPHERE MEASUREMENTS)

|  | NBS INITIAL |  |  | LABORATORY 4 |  |  | NBS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 |
| 380.0 | 4.0 | 3.9 | 3.9 | 4.3 | 4.3 | 4.3 | 3.6 | 3.9 | 3.9 |
| 390.0 | 5.9 | 5.9 | 6.0 | 6.5 | 6.5 | 6.5 | 5.8 | 5.9 | 6.0 |
| 400.0 | 8.5 | 8.6 | 8.4 | 8.9 | 8.9 | 8.9 | 8.3 | 8.3 | 8.4 |
| 410.0 | 10.7 | 10.7 | 10.6 | 11.5 | 11.5 | 11.5 | 10.7 | 10.6 | 10.8 |
| 420.0 | 13.1 | 14.0 | 13.2 | 14.4 | 14.4 | 14.4 | 13.2 | 13.1 | 13.3 |
| 430.0 | 16.1 | 15.9 | 16.2 | 17.1 | 17.1 | 17.1 | 16.0 | 16.0 | 16.1 |
| 440.0 | 18.5 | 18.4 | 18.7 | 19.7 | 19.7 | 19.7 | 18.5 | 18.5 | 18.6 |
| 450.0 | 20.8 | 20.8 | 20.8 | 22.3 | 22.5 | 22.2 | 20.9 | 20.8 | 20.8 |
| 460.0 | 22.6 | 22.6 | 22.1 | 24.1 | 24.1 | 24.1 | 22.6 | 22.6 | 22.5 |
| 470.0 | 23.7 | 23.7 | 23.7 | 25.0 | 25.1 | 25.0 | 23.7 | 23.7 | 23.7 |
| 480.0 | 23.9 | 24.0 | 24.0 | 25.2 | 25.2 | 25.4 | 24.1 | 24.0 | 24.1 |
| 490.0 | 24.0 | 23.9 | 23.9 | 24.7 | 24.8 | 25.0 | 24.1 | 24.0 | 24.0 |
| 500.0 | 23.1 | 23.1 | 23.1 | 23.8 | 23.7 | 23.9 | 23.2 | 23.1 | 23.0 |
| 510.0 | 22.6 | 22.6 | 22.6 | 23.3 | 23.1 | 23.3 | 22.7 | 22.7 | 22.6 |
| 520.0 | 23.7 | 23.7 | 23.8 | 24.4 | 24.4 | 24.4 | 23.7 | 23.7 | 23.6 |
| 530.0 | 27.8 | 27.9 | 27.9 | 28.6 | 28.4 | 28.5 | 27.7 | 27.7 | 27.5 |
| 540.0 | 35.9 | 35.8 | 36.0 | 36.8 | 36.6 | 36.8 | 35.6 | 35.5 | 35.4 |
| 550.0 | 46.1 | 46.0 | 46.2 | 48.1 | 48.0 | 48.2 | 45.7 | 45.5 | 45.5 |
| 560.0 | 58.7 | 58.7 | 58.9 | 59.3 | 59.1 | 59.3 | 58.3 | 58.2 | 58.0 |
| 570.0 | 66.5 | 66.6 | 66.8 | 67.0 | 66.7 | 66.7 | 66.4 | 66.4 | 66.1 |
| 580.0 | 69.0 | 69.0 | 69.2 | 70.8 | 71.4 | 70.7 | 69.1 | 69.1 | 68.7 |
| 590.0 | 64.7 | 64.7 | 64.9 | 65.2 | 65.0 | 65.0 | 65.1 | 65.1 | 64.7 |
| 600.0 | 57.1 | 57.0 | 57.0 | 56.9 | 56.7 | 56.7 | 57.3 | 57.3 | 57.0 |
| 610.0 | 46.9 | 47.1 | 47.1 | 46.7 | 46.5 | 46.6 | 47.4 | 47.5 | 47.3 |
| 620.0 | 36.7 | 36.9 | 36.9 | 36.8 | 36.7 | 36.7 | 37.3 | 37.4 | 37.2 |
| 630.0 | 28.2 | 28.3 | 28.3 | 28.2 | 28.1 | 28.2 | 28.5 | 28.6 | 28.5 |
| 640.0 | 21.0 | 21.0 | 21.0 | 21.1 | 20.9 | 21.0 | 21.4 | 21.5 | 21.3 |
| 650.0 | 15.5 | 15.5 | 15.4 | 15.6 | 15.5 | 15.6 | 15.8 | 15.9 | 15.8 |
| 660.0 | 11.2 | 11.3 | 11.3 | 11.5 | 11.4 | 11.5 | 11.5 | 11.6 | 11.6 |
| 670.0 | 8.4 | 8.4 | 8.4 | 8.4 | 8.4 | 8.5 | 8.5 | 8.5 | 8.6 |
| 680.0 | 6.2 | 6.1 | 6.1 | 6.1 | 6.0 | 6.0 | 6.2 | 6.3 | 6.3 |
| 690.0 | 4.8 | 4.9 | 4.8 | 4.9 | 4.8 | 4.7 | 4.8 | 4.9 | 5.0 |
| 700.0 | 3.4 | 3.5 | 3.4 | 3.5 | $3 \cdot 5$ | 3.7 | 3.5 | 3.6 | 3.8 |
| 710.0 | 2.8 | 2.9 | 2.8 | 2.9 | 2.9 | 3.1 | 3.0 | 3.1 | 3.1 |
| 720.0 | 2.4 | 2.2 | 2.0 | 2.0 | 1.9 | 1.9 | $2 \cdot 3$ | 2.4 | 2.4 |
| 730.0 | 3.3 | 3.0 | 3.3 | 1.8 | 1.6 | 1.6 | 1.9 | 2.1 | 2.3 |
| 740.0 | 2.2 | 1.9 | 2.2 | 1.8 | 1.6 | 1.6 | 2.1 | 2.3 | 2.2 |
| 750.0 | 2.6 | 2.2 | 2.6 | 1.6 | 1.4 | 1.4 | 2.5 | 2.4 | 2.9 |
| 760.0 | 2.4 | $2 \cdot 1$ | 1.6 | 1.0 | 1.3 | 1.3 | 1.8 | 1.8 | 2.1 |

## MERCURY LINES

| 405.0 | 22.8 | 22.7 | 22.9 | 11.6 | 11.9 | 11.8 | 22.8 | 22.6 | 22.9 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 56.4 | 56.4 | 56.5 | 50.8 | 52.5 | 51.5 | 57.0 | 56.8 | 57.5 |
| 546.0 | 26.6 | 26.6 | 26.5 | 28.6 | 28.5 | 28.5 | 26.2 | 26.2 | 26.1 |
| 578.0 | 9.3 | 9.7 | 9.1 | 7.4 | 7.4 | 7.5 | 8.9 | 9.0 | 8.9 |



FIGURE 4.30 AVERAGE RELATIVE SPECTRAL FLUX (SPHERE MEASUREMENTS) NORMALIEED TO AREA

SPECTRAL FLUX DISTRIBUTION (WATTS) IN SPHERE LAMP NUMBER NBS8809

|  | NBS INITIAL |  |  | LABORATORY 4 |  |  | NBS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 |
| 380.0 | . 0327 | . 0314 | . 0316 | . 0396 | . 0398 | . 0399 | . 0298 | . 0317 | . 0324 |
| 390.0 | . 0482 | . 0479 | . 0489 | . 0597 | . 0600 | . 0599 | . 0472 | . 0485 | . 0490 |
| 400.0 | . 0692 | . 0699 | . 0685 | . 0812 | . 0821 | . 0815 | . 0681 | . 0680 | . 0695 |
| 410.0 | . 0872 | . 0876 | . 0863 | . 1052 | . 1057 | . 1055 | . 0874 | . 0869 | . 0888 |
| 420.0 | . 1066 | . 1144 | . 1067 | . 1318 | . 1326 | . 1321 | . 1081 | . 1071 | -1093 |
| 430.0 | . 1307 | . 1295 | . 1312 | -1563 | . 1569 | . 1568 | . 1305 | - 1306 | - 1324 |
| 440.0 | .1506 | . 1503 | . 1516 | . 1804 | . 1813 | . 1811 | . 1513 | - 1508 | . 1528 |
| 450.0 | . 1688 | - 1699 | . 1691 | - 2043 | . 2068 | . 2034 | . 1708 | . 1700 | . 1715 |
| 460.0 | . 1834 | . 1843 | . 1792 | - 2205 | . 2220 | - 2210 | . 1845 | - 1842 | - 1855 |
| 470.0 | . 1925 | -1933 | . 1921 | - 2291 | . 2304 | - 2290 | . 1938 | . 1935 | . 1955 |
| 480.0 | . 1947 | . 1960 | . 1945 | - 2307 | . 2318 | . 2329 | . 1970 | . 1963 | . 1985 |
| 490.0 | . 1949 | - 1951 | . 1940 | - 2265 | - 2278 | - 2290 | . 1967 | . 1957 | . 1974 |
| 500.0 | . 1875 | . 1882 | . 1872 | . 2181 | . 2180 | . 2189 | . 1894 | . 1886 | . 1896 |
| 510.0 | . 1841 | . 1845 | . 1837 | - 2136 | . 2127 | . 2136 | . 1857 | . 1850 | . 1866 |
| 520.0 | . 1929 | . 1936 | . 1928 | - 2232 | . 2240 | - 2237 | . 1937 | . 1931 | . 1946 |
| 530.0 | . 2263 | . 2274 | . 2264 | - 2617 | - 2609 | - 2615 | . 2259 | - 2259 | - 2267 |
| 540.0 | . 2918 | - 2924 | - 2922 | - 3372 | . 3369 | . 3374 | . 2904 | - 2898 | - 2916 |
| 550.0 | . 3747 | - 3753 | . 3750 | . 4405 | . 4412 | . 4420 | . 3731 | -3719 | . 3744 |
| 560.0 | . 4769 | . 4792 | . 4776 | . 5431 | . 5438 | . 5435 | . 4760 | . 4751 | . 4780 |
| 570.0 | . 5408 | . 5439 | . 5419 | -6139 | . 6134 | -6122 | . 5424 | . 5418 | . 5443 |
| 580.0 | . 5608 | . 5634 | . 5615 | . 6487 | . 6567 | - 6482 | . 5640 | - 5638 | . 5659 |
| 590.0 | . 5260 | - 5284 | . 5267 | . 5971 | . 5974 | - 5960 | . 5315 | . 5311 | - 5326 |
| 600.0 | . 4644 | . 4650 | . 4628 | . 5212 | . 5210 | . 5201 | . 4679 | . 4676 | . 4694 |
| 610.0 | . 3811 | . 3844 | . 3819 | - 4281 | . 4279 | . 4279 | - 3874 | - 3881 | - 3897 |
| 620.0 | . 2983 | . 3011 | . 2993 | . 3373 | . 3373 | . 3365 | . 3048 | - 3050 | - 3062 |
| 630.0 | . 2295 | . 2307 | . 2298 | - 2587 | . 2585 | - 2589 | - 2329 | - 2338 | - 2348 |
| 640.0 | . 1706 | . 1718 | . 1705 | . 1930 | . 1926 | . 1924 | . 1751 | . 1756 | . 1758 |
| 650.0 | . 1263 | . 1262 | . 1254 | . 1427 | . 1429 | . 1428 | - 1292 | . 1302 | . 1304 |
| 660.0 | . 0909 | . 0920 | . 0915 | . 1051 | . 1045 | - 1052 | . 0939 | . 0944 | . 0954 |
| 670.0 | . 0683 | . 0687 | . 0680 | . 0769 | . 0770 | . 0778 | . 0697 | . 0697 | . 0707 |
| 680.0 | . 0501 | . 0494 | . 0498 | . 0559 | . 0551 | . 0551 | . 0509 | . 0511 | . 0521 |
| 690.0 | . 0393 | . 0400 | . 0392 | . 0446 | . 0437 | -0427 | . 0396 | . 0400 | . 0410 |
| 700.0 | . 0278 | . 0287 | . 0277 | . 0324 | . 0324 | . 0335 | . 0288 | . 0295 | . 0315 |
| 710.0 | . 0227 | . 0238 | . 0226 | . 0266 | . 0267 | . 0280 | . 0242 | . 0251 | . 0251 |
| 720.0 | . 0196 | . 0178 | . 0163 | . 0186 | . 0171 | . 0171 | . 0188 | . 0199 | . 0199 |
| 730.0 | . 0265 | . 0242 | . 0265 | . 0163 | . 0146 | . 0146 | . 0159 | . 0172 | . 0186 |
| 740.0 | . 0178 | . 0154 | . 0177 | . 0169 | . 0149 | . 0149 | . 0169 | . 0184 | . 0184 |
| 750.0 | . 0213 | . 0184 | . 0212 | . 0150 | . 0125 | . 0125 | -0200 | . 0199 | . 0239 |
| 760.0 | . 0198 | . 0169 | . 0132 | . 0089 | . 0119 | . 0118 | . 0148 | . 0147 | . 0172 |

## MERCURY LINES

| 405.0 | .1851 | .1850 | .1855 | .1061 | .1092 | .1083 | .1860 | .1844 | .1883 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 436.0 | .4586 | .4606 | .4588 | .4650 | .4829 | .4725 | .4659 | .4636 | .4737 |
| 546.0 | .2159 | .2173 | .2153 | .2616 | .2625 | .2615 | .2143 | .2140 | .2148 |
| 578.0 | .0754 | .0792 | .0738 | .0680 | .0682 | .0687 | .0725 | .0731 | .0734 |



FIGURE 4.31 AVERAGE SPECTRAL FLUX (SPHERE MEASUREMENTS)

RELATIVE SPECTRAL FLUX DISTRIBUTION IN SPHERE-NORMALIZED TO AREA LAMP NUMBER NBS8810

|  | NBS INITIAL |  |  | LABORATORY 4 |  |  | NBS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 |
| 380.0 | 3.7 | 3.8 | 3.8 | 4.3 | 4.3 | 4.3 | 3.8 | 3.6 | 3.7 |
| 390.0 | 5.8 | 5.9 | 5.9 | 6.5 | 6.5 | 6.5 | 5.7 | 5.8 | 5.7 |
| 400.0 | 8.4 | 8.5 | 8.4 | 8.6 | 8.7 | 8.6 | 8.3 | 8.2 | 8.2 |
| 410.0 | 10.7 | 10.7 | 10.7 | 11.1 | 7.9 | 7.9 | 10.7 | 10.6 | 10.6 |
| 420.0 | 13.1 | 13.8 | 13.1 | 13.8 | 13.8 | 13.8 | 13.2 | 13.0 | 13.1 |
| 430.0 | 16.0 | 15.9 | 15.9 | 16.6 | 16.5 | 16.5 | 15.8 | 15.8 | 15.9 |
| 440.0 | 18.4 | 17.7 | 18.4 | 19.2 | 19.2 | 19.1 | 18.3 | 18.3 | 18.4 |
| 450.0 | 20.5 | 19.2 | 20.6 | 22.1 | 22.3 | 22.3 | 20.7 | 20.6 | 20.6 |
| 460.0 | 22.3 | 22.3 | 22.4 | 23.7 | 23.8 | 23.8 | 22.4 | 22.3 | 22.4 |
| 470.0 | 23.5 | 23.4 | 23.5 | 24.7 | 24.5 | 24.4 | 23.6 | 23.5 | 23.6 |
| 480.0 | 23.8 | 23.8 | 23.8 | 24.7 | 24.8 | 25.0 | 24.0 | 23.9 | 24.0 |
| 490.0 | 23.7 | 23.7 | 23.7 | 24.4 | 24.2 | 24.3 | 23.9 | 23.8 | 23.8 |
| 500.0 | 22.9 | 22.9 | 22.9 | 23.5 | 23.4 | 23.4 | 23.0 | 22.9 | 22.9 |
| 510.0 | 22.5 | 22.5 | 22.5 | 23.0 | 22.9 | 22.9 | 22.6 | 22.6 | 22.5 |
| 520.0 | 23.6 | 23.7 | 23.6 | 23.9 | 23.9 | 23.9 | 23.6 | 23.5 | 23.6 |
| 530.0 | 27.8 | 27.8 | 27.8 | 28.1 | 28.1 | 28.2 | 27.6 | 27.6 | 27.5 |
| 540.0 | 35.9 | 35.9 | 35.9 | 36.1 | 36.0 | 36.2 | 35.4 | 35.4 | 35.5 |
| 550.0 | 46.0 | 46.1 | 46.2 | 47.3 | 47.3 | 47.4 | 45.6 | 45.6 | 45.6 |
| 560.0 | 58.6 | 58.9 | 58.9 | 58.5 | $58 \cdot 4$ | 58.6 | 58.3 | 58.2 | 58.3 |
| 570.0 | 66.6 | 66.9 | 66.8 | 66.2 | 66.2 | 66.5 | 66.4 | 66.5 | 66.4 |
| 580.0 | 68.9 | 69.5 | 69.4 | 76.6 | 78.2 | 78.3 | 69.1 | 69.2 | 69.1 |
| 590.0 | $64 \cdot 6$ | $65 \cdot 1$ | 65.0 | 65.3 | $65 \cdot 3$ | 65.5 | 65.2 | 65.3 | 65.2 |
| 600.0 | 56.8 | 57.2 | 57.1 | 57.2 | 57.2 | 57.3 | 57.4 | 57.4 | 57.3 |
| 610.0 | 47.1 | 47.3 | 47.2 | 47.2 | 47.1 | 47.3 | 47.5 | 47.6 | 47.6 |
| 620.0 | 36.9 | 37.1 | 36.9 | 37.2 | 37.2 | 37.3 | 37.4 | 37.5 | 37.4 |
| 630.0 | 28.7 | 28.5 | 28.4 | 28.5 | 28.4 | 28.5 | 28.6 | 28.7 | 28.6 |
| 640.0 | 21.3 | 21.3 | 21.2 | 21.3 | 21.3 | 21.4 | 21.6 | 21.6 | 21.4 |
| 650.0 | 15.6 | 15.7 | 15.6 | 15.9 | 15.9 | 15.9 | 15.9 | 16.0 | 15.8 |
| 660.0 | 11.4 | 11.4 | 11.3 | 11.8 | 11.7 | 11.7 | 11.5 | 11.6 | 11.4 |
| 670.0 | 8.5 | 8.6 | 8.4 | 8.7 | 8.6 | 8.5 | 8.6 | 8.6 | 8.5 |
| 680.0 | 6.4 | 6.1 | 6.1 | 6.4 | 6.4 | 6.4 | 6.4 | 6.4 | 6.2 |
| 690.0 | 5.0 | 4.8 | 4.8 | 5.0 | 5.0 | 4.9 | 5.0 | 5.0 | 4.9 |
| 700.0 | 3.7 | 3.5 | 3.5 | 3.9 | 3.9 | 3.8 | 3.7 | 3.6 | 3.7 |
| 710.0 | 3.2 | 3.0 | 2.9 | 3.1 | 3.1 | 3.0 | 3.1 | 2.9 | 3.0 |
| 720.0 | 2.5 | 2.3 | 2.1 | 2.3 | 2.3 | 2.3 | 2.4 | 2.2 | 2.2 |
| 730.0 | $3 \cdot 3$ | 3.2 | 3.2 | 1.9 | 1.7 | 1.7 | 2.1 | 1.9 | 1.9 |
| 740.0 | $2 \cdot 3$ | 1.9 | 1.9 | 2.0 | 1.8 | 1.8 | 2.0 | 2.2 | 2.0 |
| 750.0 | 2.5 | 2.2 | 2.2 | 1.8 | 1.8 | 1.8 | 2.4 | 2.1 | 2.2 |
| 760.0 | 2.3 | 2.0 | 2.0 | 1.2 | 1.3 | 1.3 | 1.8 | 1.8 | 1.8 |

## MERCURY LINES

| 405.0 | 22.6 | 23.2 | 23.0 | 11.1 | 11.7 | 11.7 | 23.2 | 23.2 | 23.4 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 56.4 | 56.4 | 56.6 | 50.4 | 52.3 | 51.3 | 56.6 | 57.3 | 57.7 |
| 546.0 | 26.8 | 27.0 | 27.0 | 28.9 | 29.0 | 28.9 | 26.9 | 27.1 | 27.0 |
| 578.0 | 9.2 | 9.2 | 9.2 | 6.0 | 5.8 | 5.7 | 8.9 | 9.1 | 9.1 |



FIGURE 4.32 AVERAGE RELATIVE SPECTRAL FLUX (SPHERE MEASUREMENTS) NORMALIZED TO ЯREA

|  | NBS INITIAL |  |  | LABORATORY 4 |  |  | NBS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 |
| $380 \cdot 0$ | . 0308 | . 0312 | . 0315 | . 0408 | . 0408 | . 0408 | . 0311 | . 0304 | . 0311 |
| 390.0 | . 0481 | . 0490 | . 0489 | . 0616 | . 0619 | . 0617 | . 0472 | . 0485 | . 0471 |
| 400.0 | . 0690 | . 0705 | . 0702 | . 0821 | . 0825 | . 0819 | . 0687 | . 0690 | . 0684 |
| 410.0 | . 0878 | . 0891 | . 0892 | . 1052 | . 0756 | . 0752 | . 0882 | . 0885 | . 0884 |
| 420.0 | .1080 | . 1144 | . 1088 | . 1313 | . 1314 | . 1312 | . 1089 | . 1089 | . 1093 |
| 430.0 | .1317 | . 1318 | . 1327 | . 1576 | . 1576 | . 1569 | . 1311 | . 1325 | . 1328 |
| 440.0 | . 1514 | . 1468 | . 1531 | . 1826 | . 1830 | . 1817 | . 1519 | . 1530 | . 1533 |
| 450.0 | . 1691 | . 1591 | . 1718 | . 2102 | . 2127 | . 2113 | . 1715 | . 1725 | . 1718 |
| 460.0 | . 1837 | . 1850 | . 1862 | . 2253 | . 2270 | . 2258 | . 1854 | . 1870 | . 1864 |
| 470.0 | . 1933 | . 1945 | . 1954 | . 2347 | . 2332 | . 2318 | . 1950 | . 1968 | . 1967 |
| 480.0 | . 1960 | . 1976 | . 1983 | . 2355 | . 2365 | . 2376 | . 1984 | . 1999 | . 2000 |
| 490.0 | . 1955 | . 1969 | . 1976 | . 2317 | . 2309 | . 2301 | . 1978 | . 1995 | .1983 |
| 500.0 | . 1884 | . 1898 | . 1908 | . 2236 | . 2226 | . 2216 | . 1905 | . 1919 | . 1913 |
| 510.0 | . 1856 | . 1867 | . 1873 | . 2185 | . 2177 | - 2169 | . 1870 | . 1888 | . 1879 |
| 520.0 | . 1947 | . 1963 | . 1965 | - 2277 | . 2277 | - 2267 | . 1951 | . 1970 | . 1963 |
| 530.0 | . 2289 | . 2306 | . 2316 | . 2673 | . 2678 | . 2677 | . 2285 | - 2307 | . 2293 |
| 540.0 | . 2954 | . 2976 | . 2993 | . 3436 | . 3434 | . 3432 | . 2933 | . 2966 | . 2958 |
| 550.0 | - 3791 | . 3826 | . 3845 | . 4502 | .4509 | . 4499 | . 3772 | . 3813 | . 3805 |
| 560.0 | . 4828 | . 4881 | . 4902 | . 5570 | . 5566 | . 5562 | . 4823 | . 4874 | . 4864 |
| 570.0 | . 5482 | . 5550 | . 5567 | . 6302 | . 6307 | . 6307 | - 5501 | . 5563 | . 5539 |
| 580.0 | . 5675 | . 5760 | . 5776 | . 7292 | . 7453 | . 7428 | . 5724 | .5793 | . 5763 |
| 590.0 | . 5317 | . 5402 | . 5417 | . 6215 | . 6217 | . 6215 | . 5396 | . 5462 | . 5435 |
| 600.0 | . 4675 | . 4747 | . 4753 | . 5440 | . 5449 | . 5440 | . 4748 | . 4802 | . 4777 |
| 610.0 | - 3880 | . 3923 | . 3933 | . 4490 | . 4488 | . 4487 | . 3936 | . 3984 | . 3965 |
| 620.0 | . 3039 | - 3076 | . 3076 | . 3537 | . 3544 | . 3541 | . 3093 | . 3135 | . 3117 |
| 630.0 | . 2364 | . 2362 | . 2368 | . 2712 | . 2709 | . 2708 | . 2366 | . 2398 | . 2388 |
| 640.0 | . 1752 | . 1765 | . 1765 | . 2031 | . 2033 | . 2026 | . 1785 | . 1808 | . 1788 |
| 650.0 | . 1282 | . 1298 | . 1296 | . 1515 | . 1517 | . 1510 | . 1315 | . 1335 | . 1320 |
| 660.0 | . 0940 | . 0944 | . 0941 | . 1118 | . 1119 | . 1111 | . 0955 | . 0970 | . 0954 |
| 670.0 | . 0700 | . 0710 | . 0702 | . 0826 | . 0819 | . 0810 | . 0713 | . 0723 | . 0707 |
| 680.0 | . 0525 | . 0507 | . 0509 | . 0613 | . 0614 | . 0605 | . 0534 | . 0537 | . 0521 |
| 690.0 | . 0413 | . 0402 | . 0403 | . 0477 | . 0478 | . 0468 | . 0413 | . 0419 | . 0410 |
| 700.0 | . 0305 | . 0288 | . 0289 | . 0370 | . 0371 | . 0359 | . 0308 | . 0305 | . 0305 |
| 710.0 | . 0260 | . 0253 | . 0240 | . 0293 | . 0293 | . 0280 | . 0253 | . 0240 | . 0251 |
| 720.0 | . 0205 | . 0195 | . 0179 | . 0217 | . 0218 | . 0218 | . 0200 | . 0186 | . 0187 |
| 730.0 | . 0273 | . 0263 | . 0264 | . 0182 | . 0165 | . 0165 | . 0173 | . 0157 | . 0158 |
| 740.0 | . 0193 | . 0154 | . 0155 | . 0191 | . 0170 | . 0170 | . 0169 | . 0184 | . 0167 |
| $750 \cdot 0$ | . 0203 | . 0185 | . 0186 | . 0175 | . 0175 | . 0175 | . 0200 | . 0179 | . 0179 |
| 760.0 | . 0190 | . 0164 | . 0165 | . 0119 | . 0119 | . 0119 | .0148 | . 0147 | . 0148 |

## MERCURY LINES

| 405.0 | .1862 | .1926 | .1915 | .1053 | .1115 | .1108 | .1920 | .1940 | .1951 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 436.0 | .4643 | .4680 | .4717 | .4793 | .4979 | .4867 | .4682 | .4794 | .4807 |
| 546.0 | .2208 | .2241 | .2249 | .2752 | .2762 | .2746 | .2231 | .2265 | .2248 |
| 578.0 | .0755 | .0759 | .0766 | .0567 | .0549 | .0542 | .0739 | .0764 | .0762 |



FIGURE 4.33 gVERaGE SPECTRAL FLUX (SPHERE MEASUREMENTS)

|  | NBS INITIAL |  |  | LABORATORY 1 |  |  | NBS REPEAT |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 | RUN 10 |
| 380.0 | 5.1 | 5.0 | 5.1 | 5.3 | . 0 | . 0 | . 0 | 4.8 | 5.0 | 5.0 |
| 390.0 | 8.8 | 8.8 | 8.8 | 8.8 | 7.7 | 9.3 | 10.0 | 8.5 | $8 \cdot 3$ | 8.4 |
| 400.0 | 14.2 | 13.5 | 14.0 | 13.7 | 14.8 | 13.8 | 13.4 | 13.2 | 13.4 | 13.5 |
| 410.0 | 18.5 | 17.9 | 18.4 | 17.9 | 18.7 | 18.4 | 17.9 | 17.8 | 17.9 | 17.9 |
| 420.0 | 23.1 | 22.6 | 22.8 | 22.6 | 23.5 | 23.4 | 23.1 | 22.5 | 22.5 | 22.5 |
| 430.0 | 28.3 | 28.2 | 28.2 | 28.1 | 29.3 | 28.9 | 28.9 | 27.9 | 27.8 | 27.7 |
| 440.0 | 32.7 | 32.6 | 32.5 | 32.4 | 33.1 | 33.4 | 33.5 | 32.4 | 32.2 | 32.2 |
| 450.0 | 36.3 | 36.2 | 36.2 | 36.1 | 36.5 | 36.8 | 36.9 | 36.2 | 36.1 | 36.0 |
| 460.0 | 38.6 | 38.5 | 38.6 | 37.7 | 39.6 | 39.1 | 39.0 | 38.6 | 38.5 | 38.4 |
| 470.0 | 39.7 | 39.7 | 39.7 | 39.6 | 40.4 | 40.1 | 40.0 | 39.7 | 39.7 | 39.5 |
| 480.0 | 39.3 | 39.4 | $39 \cdot 3$ | 39.2 | 39.0 | 39.3 | 38.3 | 39.5 | 39.4 | 39.4 |
| 490.0 | 38.0 | 38.0 | 38.0 | 37.9 | 37.5 | 37.9 | 36.9 | 38.2 | 38.1 | 38.0 |
| 500.0 | 35.6 | 35.7 | 35.7 | 35.7 | 35.9 | 35.9 | 35.7 | 35.9 | 35.8 | 35.7 |
| 510.0 | 33.3 | 33.3 | 33.3 | 33.4 | 33.5 | 33.4 | $33 \cdot 3$ | 33.6 | 33.6 | 33.4 |
| 520.0 | 31.6 | 31.6 | 31.6 | 31.7 | 31.7 | 32.0 | 31.5 | 31.9 | 31.8 | 31.6 |
| 530.0 | 31.8 | 31.8 | 31.9 | 31.9 | 32.7 | 32.8 | 32.5 | 31.9 | 31.9 | 31.7 |
| 540.0 | 34.7 | 34.5 | 34.5 | 34.6 | 35.2 | 35.2 | 35.1 | 34.6 | 34.4 | 34.3 |
| 550.0 | 38.8 | 38.6 | 38.6 | 38.7 | 39.2 | 39.2 | 39.1 | 38.7 | 38.6 | 40.5 |
| 560.0 | 44.5 | 44.5 | 44.4 | 44.6 | 44.8 | 44.8 | 44.7 | 44.5 | 44.4 | 51.0 |
| 570.0 | 47.9 | 47.8 | 47.9 | 48.0 | 47.2 | 47.1 | 47.1 | 48.0 | 48.0 | 47.6 |
| 580.0 | 48.2 | 48.2 | 48.2 | 48.3 | 47.1 | 47.0 | 47.0 | 48.4 | 48.4 | 45.4 |
| 590.0 | 44.7 | 44.8 | 44.6 | 44.7 | 44.4 | 44.5 | 44.5 | 45.0 | 45.0 | 44.7 |
| 600.0 | 38.8 | 39.1 | 39.0 | 39.1 | 39.1 | 39.6 | 39.5 | 39.5 | 39.4 | 39.1 |
| 610.0 | 32.3 | 32.6 | 32.2 | 32.3 | 32.4 | 32.8 | 33.4 | 32.8 | 32.7 | 32.5 |
| 620.0 | 25.2 | 25.5 | 25.4 | 27.0 | 25.6 | 26.2 | 26.0 | 25.9 | 25.9 | 25.7 |
| 630.0 | 19.6 | 20.0 | 19.8 | 19.8 | 19.9 | 20.1 | 20.2 | 20.1 | 20.1 | 19.8 |
| 640.0 | 14.6 | 15.0 | 14.9 | 15.0 | 15.4 | 15.4 | 15.4 | 15.2 | 15.3 | 15.1 |
| 650.0 | 10.7 | 11.1 | 11.1 | 11.1 | 11.4 | 11.4 | 11.6 | 11.4 | 11.4 | 11.2 |
| 660.0 | 7.7 | 8.2 | 8.2 | 8.3 | 8.5 | 8.6 | 9.0 | 8.4 | 8.5 | $8 \cdot 3$ |
| 670.0 | 5.8 | 6.4 | 6.2 | 6.1 | 6.1 | 7.0 | 7.3 | 6.4 | 6.4 | 6.2 |
| 680.0 | 4.1 | 4.7 | 4.6 | 4.7 | 4.8 | 5.1 | 5.1 | 4.6 | 4.8 | 4.6 |
| 690.0 | 3.4 | 3.9 | 3.8 | 3.6 | 4.3 | 4.2 | 4.2 | 3.8 | 3.9 | 3.8 |
| 700.0 | 2.5 | 3.0 | 2.8 | 2.9 | $3 \cdot 3$ | 3.2 | 3.2 | 2.8 | 2.9 | 2.8 |
| 710.0 | 1.9 | 2.4 | 2.3 | 2.4 | 2.5 | 2.5 | 3.0 | 2.3 | 2.5 | 2.3 |
| 720.0 | 1.5 | 1.9 | 1.9 | 1.9 | 2.4 | 2.4 | 2.4 | 1.9 | 2.1 | 1.8 |
| 730.0 | 2.1 | 2.7 | 2.7 | 2.7 | . 0 | . 0 | . 0 | 1.5 | 1.7 | 1.4 |
| 740.0 | 1.0 | 1.6 | 1.6 | 1.6 | . 0 | . 0 | - 0 | 1.6 | 1.6 | 1.4 |
| 750.0 | . 6 | 1.9 | 1.9 | 1.9 | . 0 | . 0 | . 0 | 1.4 | 1.9 | 1.7 |
| 760.0 | . 4 | 1.6 | 1.9 | 1.6 | . 0 | . 0 | . 0 | 1.2 | 1.5 | 1.2 |

## MERCURY LINES

| 405.0 | 22.8 | 21.1 | 21.1 | 21.2 | 23.9 | 22.7 | 21.1 | 21.3 | 21.1 | 21.2 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 55.2 | 52.0 | 52.1 | 51.7 | 54.5 | 52.5 | 55.5 | 51.9 | 51.6 | 51.8 |
| 546.0 | 26.9 | 25.8 | 25.8 | 25.7 | 26.9 | 26.4 | 26.9 | 25.8 | 25.6 | 25.1 |
| 578.0 | 9.2 | 8.4 | 8.5 | 8.5 | 7.4 | 7.7 | 7.8 | 8.3 | 8.2 | 8.5 |



FIGURE 4.34 AVERAGE RELATIVE SPECTRAL FLUX (SPHERE MEASUREMENTS) NORMALIZED TO AREA

NBS INITIAL

| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 | RUN 10 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 380.0 | . 0461 | . 0417 | . 0431 | . 0443 | . 0000 | . 0000 | . 0000 | . 0403 | 0421 | . 0424 |
| 390.0 | . 0796 | . 0735 | . 0744 | . 0735 | . 0636 | . 0769 | . 0836 | . 0712 | . 0699 | . 0718 |
| 400.0 | . 1277 | . 1134 | . 1182 | . 1146 | . 1225 | . 1146 | . 1117 | . 1112 | . 1124 | . 1144 |
| 410.0 | . 1668 | . 1505 | . 1552 | . 1502 | . 1547 | . 1524 | .1493 | . 1493 | . 1507 | . 1526 |
| 420.0 | . 2075 | . 1900 | . 1927 | . 1893 | . 1944 | . 1941 | . 1921 | . 1895 | . 1896 | . 1915 |
| 430.0 | . 2550 | - 2365 | . 2379 | . 2350 | . 2416 | . 2395 | . 2401 | . 2343 | . 2339 | . 2355 |
| 440.0 | . 2939 | . 2733 | . 2743 | - 2716 | . 2733 | - 2770 | . 2786 | - 2721 | . 2710 | . 2735 |
| 450.0 | . 3267 | - 3039 | - 3056 | . 3019 | . 3016 | . 3054 | . 3068 | . 3039 | . 3041 | - 3062 |
| 460.0 | . 3474 | - 3231 | . 3259 | . 3159 | . 3267 | . 3247 | . 3248 | . 3246 | . 3242 | - 3265 |
| 470.0 | . 3572 | . 3330 | . 3353 | . 3319 | . 3335 | - 3323 | . 3325 | - 3340 | - 3342 | -3359 |
| 480.0 | . 3538 | - 3306 | - 3319 | . 3284 | - 3217 | . 3259 | . 3187 | . 3321 | . 3321 | - 3351 |
| 490.0 | . 3421 | - 3186 | . 3211 | . 3175 | - 3094 | . 3144 | - 3069 | . 3215 | . 3210 | - 3229 |
| 500.0 | . 3207 | . 2995 | . 3016 | . 2988 | . 2968 | . 2978 | . 2971 | - 3019 | . 3017 | - 3039 |
| 510.0 | . 2994 | . 2795 | . 2812 | . 2793 | . 2764 | - 2767 | . 2770 | . 2822 | . 2826 | - 2838 |
| 520.0 | . 2840 | . 2652 | . 2668 | - 2652 | . 2617 | - 2655 | . 2619 | . 2678 | . 2675 | - 2690 |
| 530.0 | . 2865 | . 2672 | . 2691 | . 2673 | . 2698 | . 2720 | . 2706 | - 2685 | - 2684 | - 2699 |
| 540.0 | . 3118 | - 2896 | . 2916 | - 2894 | . 2905 | . 2919 | . 2918 | . 2905 | . 2898 | . 2915 |
| 550.0 | . 3490 | . 3241 | - 3262 | . 3241 | . 3237 | . 3250 | . 3255 | . 3250 | . 3246 | - 3445 |
| 560.0 | . 4004 | . 3732 | - 3749 | - 3734 | . 3696 | . 3716 | . 3718 | - 3738 | . 3736 | . 4337 |
| 570.0 | . 4306 | . 4015 | . 4040 | . 4020 | . 3901 | . 3910 | - 3916 | . 4037 | . 4037 | . 4047 |
| 580.0 | . 4333 | . 4045 | . 4066 | . 4040 | . 3891 | . 3903 | . 3910 | . 4072 | . 4074 | - 3862 |
| 590.0 | . 4022 | . 3764 | . 3762 | -3738 | . 3667 | - 3694 | . 3701 | -3785 | . 3788 | - 3800 |
| 600.0 | . 3492 | - 3282 | . 3291 | - 3273 | - 3227 | . 3284 | . 3289 | - 3316 | . 3317 | - 3329 |
| 610.0 | . 2903 | . 2735 | . 2720 | . 2707 | . 2672 | . 2724 | . 2778 | - 2756 | . 2755 | . 2761 |
| 620.0 | . 2263 | . 2142 | . 2142 | . 2261 | . 2116 | . 2176 | . 2163 | - 2177 | . 2184 | - 2189 |
| 630.0 | . 1759 | . 1679 | .1667 | . 1659 | . 1647 | . 1665 | . 1677 | - 1686 | . 1692 | - 1683 |
| 640.0 | . 1310 | - 1263 | . 1260 | . 1254 | . 1268 | . 1276 | . 1283 | . 1278 | . 1292 | . 1284 |
| 650.0 | . 0965 | . 0933 | . 0940 | . 0931 | . 0938 | . 0949 | - 0966 | . 0955 | . 0963 | . 0956 |
| 660.0 | . 0697 | . 0692 | . 0692 | . 0698 | . 0701 | . 0715 | . 0753 | . 0705 | . 0715 | . 0704 |
| 670.0 | . 0518 | . 0534 | . 0526 | . 0510 | . 0500 | . 0583 | . 0606 | . 0534 | . 0542 | . 0531 |
| 680.0 | . 0372 | . 0391 | . 0386 | . 0390 | . 0400 | . 0420 | . 0421 | . 0390 | . 0407 | . 0395 |
| 690.0 | . 0303 | . 0323 | . 0319 | . 0300 | . 0352 | . 0352 | . 0351 | . 0319 | . 0327 | . 0322 |
| 700.0 | . 0229 | . 0252 | . 0236 | . 0239 | . 0272 | . 0262 | . 0264 | . 0236 | . 0246 | . 0239 |
| 710.0 | .0171 | . 0198 | . 0196 | . 0198 | . 0207 | -0207 | . 0250 | . 0197 | . 0208 | . 0198 |
| 720.0 | . 0132 | . 0163 | .0161 | . 0163 | . 0198 | . 0198 | . 0200 | . 0162 | . 0174 | . 0150 |
| 730.0 | . 0191 | . 0227 | . 0224 | -0227 | . 0000 | . 0000 | . 0000 | . 0129 | . 0144 | . 0116 |
| 740.0 | . 0090 | . 0132 | . 0132 | . 0133 | . 0000 | . 0000 | . 0000 | . 0134 | . 0134 | . 0118 |
| 750.0 | . 0054 | . 0159 | . 0157 | . 0159 | . 0000 | . 0000 | . 0000 | . 0120 | . 0159 | . 0141 |
| 760.0 | . 0033 | .0131 | . 0163 | . 0132 | . 0000 | . 0000 | . 0000 | . 0098 | . 0123 | . 0099 |

## MERCURY LINES

| 405.0 | .2054 | .1770 | .1780 | .1778 | .1977 | .1882 | .1753 | .1791 | .1780 | .1807 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 436.0 | .4963 | .4366 | .4402 | .4331 | .44 .97 | .4352 | .4618 | .4363 | .4342 | .4410 |
| 546.0 | .2417 | .2163 | .2181 | .2154 | .2223 | .2193 | .2241 | .2172 | .2159 | .2138 |
| 578.0 | .0830 | .0703 | .0714 | .0708 | .0610 | .0642 | .0649 | .0700 | .0692 | .0721 |



FIGURE 4.35 gVERgGE SPECTRAL FLUX (SPHERE MEGSUREMENTS)

RELATIVE SPECTRAL FLUX DISTRIBUTION IN SPHERE-NORMALIZED TO AREA LAMP NUMBER NBS8908

|  | NBS INITIAL |  |  | LABORATORY 5 |  |  | NBS REPEAT |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 |
| 380.0 | 5.0 | 5.2 | 4.9 | 4.6 | 4.9 | 5.2 | 4.9 | 5.1 |
| 390.0 | 8.7 | 8.7 | 8.8 | 8.4 | $9 \cdot 1$ | 8.7 | 8.3 | 8.7 |
| 400.0 | 13.8 | 13.8 | 14.8 | 14.6 | 15.1 | 13.8 | 13.4 | 13.4 |
| 410.0 | 18.2 | 17.9 | 18.5 | 18.2 | 18.6 | 18.1 | 17.9 | 17.9 |
| 420.0 | 22.5 | 24.0 | 23.7 | 23.6 | 23.9 | 22.6 | 22.7 | 22.6 |
| 430.0 | 27.8 | 27.6 | 28.5 | 27.9 | 28.3 | 27.9 | 27.7 | 27.8 |
| 440.0 | 32.1 | 32.0 | 32.3 | 32.0 | 32.3 | 32.2 | 32.1 | 32.2 |
| 450.0 | 36.0 | 35.8 | 36.8 | 36.7 | 37.0 | 35.9 | 36.0 | 35.8 |
| 460.0 | 38.3 | 38.2 | 38.8 | 38.4 | 39.1 | 38.2 | 38.3 | 38.2 |
| 470.0 | 39.3 | 39.5 | 39.9 | 40.1 | 39.9 | 39.3 | 39.4 | 39.4 |
| 480.0 | 39.0 | 39.1 | 39.7 | 39.7 | 39.7 | 39.0 | 39.3 | 39.2 |
| $490 \cdot 0$ | 37.7 | 37.8 | 38.3 | 38.4 | 38.3 | 37.8 | 38.0 | 37.8 |
| 500.0 | 35.4 | 35.5 | 36.6 | 36.8 | 36.3 | 35.5 | 35.7 | 35.5 |
| 510.0 | 33.1 | 33.1 | 34.0 | 34.1 | 34.7 | 33.3 | 33.5 | 33.3 |
| 520.0 | 31.4 | 31.5 | 33.0 | 33.2 | 32.7 | 31.5 | 31.7 | 31.6 |
| 530.0 | 31.7 | 31.8 | 33.4 | 33.5 | 33.4 | 31.8 | 31.8 | 31.7 |
| 540.0 | 34.4 | 34.5 | 37.4 | 37.0 | 37.3 | 34.5 | 34.4 | 34.3 |
| 550.0 | 38.6 | 38.7 | 42.3 | 42.2 | 42.2 | 38.7 | 38.6 | 38.4 |
| 560.0 | 44.5 | 44.5 | 47.5 | 47.1 | 47.0 | 44.6 | 44.5 | 44.3 |
| 570.0 | 47.9 | 48.0 | 50.0 | 50.1 | 49.2 | 48.1 | 48.1 | 47.8 |
| 580.0 | 48.2 | 48.4 | 49.1 | 49.3 | 48.6 | 48.4 | 48.5 | 48.3 |
| 590.0 | 44.6 | 44.9 | 47.2 | 47.6 | 46.4 | 44.8 | 45.2 | 44.9 |
| 600.0 | 39.0 | 39.4 | 41.7 | 41.6 | 40.4 | 39.2 | 39.6 | 39.4 |
| 610.0 | 32.6 | 32.6 | 33.4 | 33.3 | $32 \cdot 3$ | 32.6 | 32.8 | 32.8 |
| 620.0 | 26.0 | 25.7 | 25.7 | 26.1 | 24.9 | 25.8 | 26.0 | 25.9 |
| 630.0 | 19.9 | 19.9 | 19.6 | 19.7 | 19.0 | 19.9 | 20.0 | 20.0 |
| 640.0 | 15.2 | 15.1 | 14.5 | 14.6 | 13.6 | 15.1 | 15.2 | 15.3 |
| 650.0 | 11.2 | 11.0 | 9.0 | 9.0 | $8 \cdot 4$ | 11.2 | 11.3 | 11.4 |
| 660.0 | 8.4 | 8.1 | 6.2 | 6.4 | $5 \cdot 5$ | 8.2 | 8.4 | 8.5 |
| 670.0 | 6.4 | $6 \cdot 3$ | 3.0 | 3.1 | 2.9 | 6.2 | 6.4 | 6.4 |
| 680.0 | 4.7 | 4.6 | 1.2 | 1.2 | 1.2 | 4.6 | 4.7 | 4.8 |
| 690.0 | 3.9 | 3.5 | . 7 | . 7 | - 6 | 3.7 | 3.7 | 3.9 |
| 700.0 | 2.9 | 2.7 | 1.2 | 1.2 | - 7 | 2.8 | 2.9 | 2.9 |
| 710.0 | 2.5 | 2.3 | - 4 | - 0 | - 0 | 2.4 | 2.4 | 2.5 |
| 720.0 | 1.9 | 1.9 | - 0 | - 0 | - 0 | 1.7 | 1.8 | 2.1 |
| 730.0 | 2.9 | 2.7 | - 0 | - 0 | - 0 | 2.7 | 1.6 | 1.7 |
| 740.0 | 1.8 | 1.6 | - 0 | . 0 | . 0 | 1.6 | 1.6 | 1.8 |
| 750.0 | 1.9 | 1.3 | . 0 | - 0 | - 0 | 1.6 | 1.7 | 1.9 |
| 760.0 | 2.0 | 1.6 | - 0 | - 0 | - 0 | 1.6 | 1.2 | 1.7 |

## MERCURY LINES

| 405.0 | 21.3 | 21.5 | 17.7 | 17.8 | 19.6 | 21.6 | 21.5 | 21.5 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 52.6 | 53.0 | 51.0 | 51.1 | 54.3 | 52.8 | 52.7 | 53.1 |
| 546.0 | 26.2 | 26.2 | 26.0 | 27.0 | 28.2 | 26.0 | 25.9 | 25.7 |
| 578.0 | 8.7 | 8.7 | 13.4 | 13.8 | 14.4 | 8.6 | 8.4 | 8.5 |


figure 4.36 gVErage relative spectral flux (SPhere measurements) NORMALIZED TO AREA

|  | NBS INITIAL |  |  | LABORATORY 5 |  |  | NBS REPEA |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUNT 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 |
| 380.0 | . 0423 | . 0441 | . 0384 | . 0357 | . 0405 | . 0441 | . 0406 | . 0433 |
| 390.0 | . 0730 | . 0736 | . 0688 | . 0657 | . 0757 | . 0734 | . 0694 | . 0732 |
| 400.0 | . 1161 | - 1158 | . 1152 | . 1137 | . 1259 | . 1157 | . 1117 | . 1133 |
| 410.0 | . 1529 | -1509 | . 1443 | . 1419 | . 1549 | . 1525 | . 1498 | . 1513 |
| 420.0 | . 1895 | - 2019 | . 1846 | . 1835 | . 1992 | . 1898 | . 1895 | . 1909 |
| 430.0 | . 2338 | - 2325 | - 2222 | - 2168 | . 2362 | . 2344 | . 2316 | . 2350 |
| 440.0 | . 2701 | - 2694 | - 2520 | . 2488 | . 2695 | - 2705 | . 2684 | . 2715 |
| 450.0 | . 3027 | - 3013 | . 2875 | - 2855 | . 3081 | - 3020 | . 3010 | . 3027 |
| 460.0 | . 3219 | - 3218 | . 3028 | - 2990 | - 3259 | - 3210 | . 3203 | . 3222 |
| 470.0 | . 3305 | - 3322 | . 3111 | - 3123 | . 3325 | . 3306 | . 3295 | - 3327 |
| 480.0 | . 3280 | - 3288 | . 3097 | . 3091 | . 3309 | . 3281 | . 3281 | . 3308 |
| 490.0 | . 3175 | - 3180 | . 2988 | - 2988 | . 3194 | . 3175 | . 3177 | . 3191 |
| 500.0 | . 2978 | . 2984 | . 2858 | . 2861 | . 3028 | - 2985 | . 2985 | . 2999 |
| 510.0 | . 2784 | - 2787 | . 2656 | - 2655 | . 2896 | - 2795 | . 2796 | - 2808 |
| 520.0 | . 2641 | - 2649 | . 2573 | - 2583 | . 2723 | . 2643 | . 2652 | - 2666 |
| 530.0 | . 2670 | - 2673 | . 2609 | . 2610 | . 2786 | . 2673 | . 2659 | - 2674 |
| 540.0 | - 2896 | - 2904 | . 2919 | - 2877 | - 3112 | - 2903 | . 2875 | - 2895 |
| 550.0 | . 3247 | - 3255 | . 3303 | - 3280 | . 3520 | - 3255 | . 3223 | - 3244 |
| 560.0 | . 3741 | - 3747 | . 3703 | - 3666 | . 3917 | - 3751 | . 3717 | - 3740 |
| 570.0 | . 4031 | . 4043 | . 3900 | - 3897 | . 4105 | . 4042 | . 4018 | . 4039 |
| 580.0 | . 4060 | . 4073 | - 3828 | . 3838 | . 4048 | . 4070 | . 4055 | . 4077 |
| 590.0 | . 3756 | -3781 | - 3682 | - 3704 | - 3868 | - 3768 | . 3773 | - 3795 |
| 600.0 | . 3285 | . 3313 | - 3254 | - 3240 | - 3368 | - 3296 | . 3305 | - 3324 |
| 610.0 | . 2740 | - 2740 | . 2604 | - 2594 | . 2696 | . 2736 | . 2740 | - 2771 |
| 620.0 | . 2192 | . 2159 | - 2003 | - 2030 | . 2077 | - 2168 | . 2171 | - 2188 |
| 630.0 | . 1673 | . 1674 | . 1529 | . 1534 | . 1581 | . 1674 | . 1670 | . 1693 |
| 640.0 | . 1281 | . 1268 | . 1130 | . 1133 | . 1132 | - 1268 | . 1270 | . 1293 |
| 650.0 | . 0940 | . 0922 | . 0701 | . 0701 | . 0703 | . 0943 | . 0948 | . 0964 |
| 660.0 | . 0707 | . 0685 | . 0480 | . 0500 | . 0463 | . 0685 | . 0706 | . 0716 |
| 670.0 | . 0537 | . 0529 | . 0237 | . 0238 | . 0238 | . 0521 | . 0531 | . 0543 |
| 680.0 | . 0394 | . 0387 | . 0096 | . 0096 | . 0096 | . 0390 | . 0394 | . 0408 |
| 690.0 | . 0325 | -0297 | . 0054 | . 0054 | . 0054 | . 0311 | . 0312 | . 0328 |
| 700.0 | . 0241 | . 0225 | . 0091 | . 0091 | . 0061 | . 0239 | . 0238 | . 0246 |
| 710.0 | . 0213 | . 0196 | . 0031 | . 0000 | . 0000 | . 0198 | . 0198 | . 0208 |
| 720.0 | . 0164 | . 0162 | . 0000 | . 0000 | . 0000 | . 0147 | . 0151 | . 0174 |
| 730.0 | . 0247 | . 0224 | .0000 | . 0000 | . 0000 | . 0227 | . 0130 | . 0143 |
| $740 \cdot 0$ | . 0156 | . 0132 | . 0000 | . 0000 | . 0000 | . 0133 | . 0135 | . 0151 |
| 750.0 | . 0160 | . 0105 | . 0000 | . 0000 | . 0000 | . 0133 | . 0140 | . 0159 |
| 760.0 | . 0165 | . 0135 | .0000 | . 0000 | . 0000 | . 0132 | . 0099 | . 0148 |

## MERCURY LINES

| 405.0 | .1791 | .1809 | .1383 | .1381 | .1633 | .1814 | .1799 | .1819 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 436.0 | .4423 | .4459 | .3982 | .3976 | .4525 | .4434 | .4401 | .4481 |
| 546.0 | .2205 | .2202 | .2025 | .2103 | .2351 | .2187 | .2168 | .2172 |
| 578.0 | .0732 | .0733 | .1045 | .1071 | .1203 | .0719 | .0705 | .0716 |



FIGURE 4.37 AVERAGE SPECTRAL FLUX (SPHERE MEASUREMENTS)

RELATIVE SPECTRAL FLUX OISTRIBUTION IN SPHERE-NORMALIZED TO AREA LAMP NUMBER NBS8909

|  | NBS INITIAL |  |  | LABORATORY 2 |  |  | NBS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 |
| 380.0 | 5.1 | 5.2 | 5.2 | . 0 | . 0 | . 0 | 5.1 | 5.1 | 5.0 |
| 390.0 | 8.8 | 8.8 | 7.6 | 9.7 | 8.0 | 6.2 | 8.6 | 8.7 | 8.5 |
| 400.0 | 13.9 | 13.8 | 13.8 | 13.8 | 13.4 | 12.4 | 13.4 | 13.6 | 13.9 |
| 410.0 | 18.3 | 18.0 | 18.3 | 18.6 | 18.4 | 18.0 | 17.9 | 18.2 | 18.2 |
| 420.0 | 22.6 | 24.2 | 22.7 | 22.9 | 22.8 | 22.7 | 22.5 | 22.5 | 22.6 |
| 430.0 | 27.9 | 27.9 | 27.9 | 27.9 | 27.9 | 27.9 | 27.8 | 27.9 | 27.5 |
| 440.0 | 32.2 | 32.3 | 32.2 | 32.4 | 32.3 | 32.4 | 32.1 | 32.2 | 30.7 |
| 450.0 | 36.1 | 36.0 | 36.0 | 35.7 | 35.8 | 35.8 | 35.9 | 36.0 | 32.8 |
| 460.0 | 38.3 | 38.4 | 38.6 | 38.0 | 38.1 | 38.2 | 38.4 | 38.5 | 38.4 |
| 470.0 | 39.4 | 39.6 | 39.5 | 39.1 | 39.2 | 39.3 | 39.5 | 39.7 | 39.8 |
| 480.0 | 39.1 | 39.2 | 39.1 | 38.9 | 39.0 | 39.1 | 39.4 | 39.3 | 39.5 |
| 490.0 | 37.8 | 37.8 | 37.9 | 37.8 | 37.9 | 38.1 | 38.1 | 38.0 | 38.2 |
| $500 \cdot 0$ | 35.5 | 35.5 | 35.5 | 35.6 | 35.6 | 35.8 | 35.8 | 35.8 | 35.9 |
| 510.0 | 33.2 | 33.1 | 33.2 | 33.4 | 33.5 | 33.6 | 33.4 | 33.5 | 33.5 |
| 520.0 | 32.2 | 31.5 | 31.5 | 32.0 | 32.1 | 32.3 | 31.7 | 31.7 | 31.8 |
| 530.0 | 31.7 | 32.7 | 31.9 | 32.3 | 32.4 | 32.6 | 31.8 | 31.7 | 31.9 |
| 540.0 | 34.4 | 34.4 | 34.7 | 35.3 | 35.5 | 35.8 | 34.4 | 34.3 | 34.4 |
| 550.0 | 38.5 | 38.2 | 38.7 | 39.5 | 39.8 | 40.1 | 38.5 | 38.4 | 38.5 |
| 560.0 | 44.3 | 44.4 | 44.7 | 44.9 | 45.1 | 45.6 | 44.3 | 44.1 | 44.5 |
| 570.0 | 47.7 | 47.8 | 48.0 | 48.3 | 48.6 | 49.0 | 47.9 | 47.7 | 48.0 |
| 580.0 | 48.0 | 48.0 | 48.2 | 48.5 | 48.8 | 49.2 | 48.3 | 48.2 | 48.5 |
| 590.0 | 44.5 | 44.5 | 44.7 | 45.3 | 45.5 | 45.9 | 44.9 | 44.8 | 45.1 |
| 600.0 | 38.8 | 39.0 | 39.3 | 39.7 | 39.9 | 40.2 | 39.4 | 39.2 | 39.5 |
| 610.0 | 32.3 | 32.1 | 32.4 | 33.0 | 33.1 | 33.4 | 32.7 | 32.7 | 32.8 |
| 620.0 | 25.4 | 25.3 | 25.6 | 26.2 | 26.4 | 26.6 | 25.8 | 26.1 | 26.0 |
| 630.0 | 19.7 | 19.8 | 19.7 | 20.3 | 20.5 | 20.6 | 19.9 | 19.9 | 20.5 |
| 640.0 | 15.1 | 14.9 | 15.4 | 15.5 | 15.5 | 15.7 | 15.2 | 15.3 | 15.3 |
| 650.0 | 11.1 | 11.1 | 11.2 | 11.6 | 11.7 | 11.7 | 11.4 | 11.4 | 11.5 |
| 660.0 | 8.4 | 8.3 | 7.9 | 8.7 | 8.7 | 8.8 | 8.3 | 8.4 | 8.5 |
| 670.0 | 6.3 | 6.2 | 6.2 | 6.5 | 6.5 | 6.5 | 6.3 | 6.4 | 6.4 |
| 680.0 | 4.7 | 4.5 | 4.6 | 4.9 | 4.8 | 4.8 | 4.8 | 4.8 | 4.9 |
| 690.0 | 3.8 | 3.5 | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 | 3.8 | 4.0 |
| 700.0 | 3.0 | 2.6 | 2.7 | 2.8 | 2.8 | 2.8 | 2.9 | 2.8 | 3.0 |
| 710.0 | 2.5 | 2.3 | 2.4 | 2.2 | 2.2 | 2.1 | 2.5 | 2.4 | 2.5 |
| 720.0 | 1.9 | 1.9 | 2.0 | 1.6 | 1.6 | 1.6 | 1.9 | 1.8 | 2.0 |
| 730.0 | 2.9 | 2.6 | 2.8 | 1.3 | 1.2 | 1.2 | 1.7 | 1.6 | 1.7 |
| 740.0 | 1.8 | 1.5 | 1.6 | 1.1 | 1.1 | 1.1 | 1.8 | 1.6 | 1.8 |
| 750.0 | 1.9 | 1.9 | 2.0 | . 9 | 1.0 | . 8 | 1.9 | 1.7 | 1.9 |
| 760.0 | 1.9 | 1.6 | 1.6 | - 0 | . 0 | . 0 | 1.5 | 1.2 | 1.5 |

## MERCURY LINES

| 405.0 | 21.3 | 21.4 | 21.3 | 23.4 | 23.3 | 22.5 | 21.6 | 21.8 | 21.2 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 53.1 | 53.1 | 52.9 | 52.4 | 51.8 | 50.9 | 52.9 | 53.2 | 53.6 |
| 546.0 | 26.0 | 26.2 | 26.0 | 25.2 | 25.5 | 26.3 | 25.9 | 25.7 | 26.0 |
| 578.0 | 8.6 | 8.7 | 8.7 | 8.9 | 9.0 | 9.0 | 8.4 | 8.4 | 8.4 |



FIGURE 4.38 AVERAGE RELATIVE SPECTRAL FLUX (SPHERE MEASUREMENTS) NORMALIZED TO AREA

SPECTRAL FLUX DISTRIBUTION (WATTS) IN SPHERE LAMP NUMBER NBS8909

NBS INITIAL
WAVELENGTH RUN 1 RUN 2 RUN 380.0
390.0 400.0 410.0 420.0 430 440.0 450.0 460.0 470.0 480.0
490.0 500.0 510.0 520.0 530.0 $540 \cdot 0$ 550.0 560.0 570.0 580.0 $590 \cdot 0$ 600.0 620.0 630.0 640.0 650 . 0 $660 \cdot 0$ 670.0 680.0 $690 \cdot 0$
700.0 710.0 720.0 730.0 740.0 750.0 760.0
.1190
.1178 $\begin{array}{ll}.1564 & .1539 \\ .1937 & .2062\end{array}$ $\begin{array}{ll}.2388 & .2379 \\ .2758 & .2753\end{array}$ $\begin{array}{ll}.3089 & .3069 \\ .3276 & .3272\end{array}$

$$
.3065
$$ $\begin{array}{ll}.3371 & .3376 \\ .3340 & .3343\end{array}$

$$
\begin{array}{r}
.3282 \\
.3360
\end{array}
$$ .3234 . 3224

.3033 . 3028 . 3026 $\begin{array}{lll}.2843 & .2821 & .2828 \\ .2753 & .2685 & .2685\end{array}$ $\begin{array}{lll}.2711 & .2791 & .2712 \\ .2944 & .2935 & .2952\end{array}$ .3297 . 3256 . 3294 $\begin{array}{lll}.3790 & .3782 & .3803 \\ .4078 & .4072 & .4088\end{array}$ $\begin{array}{lll}.4107 & .4093 & .4105 \\ .3805 & .3792 & .3805\end{array}$ $.3805 \cdot 3792 \cdot 3805$ .3315 . 3325 . 3342 .2759
.2170

$$
\begin{aligned}
& .2759 \\
& .2177
\end{aligned}
$$ .1681 .1690 . 1290 .0950 .0943

$$
\begin{array}{r}
.1929 \\
.2373 \\
.2737 \\
.3065
\end{array}
$$

$$
.1681
$$

$$
.1314
$$

$$
.0953
$$ .0717 .0707

$$
.0676
$$ $\begin{array}{ll}.0537 & .0529 \\ .0405 & .0387\end{array}$

$$
.0524
$$ .0325 .0297

$$
\begin{array}{r}
.0392 \\
.0326
\end{array}
$$

$$
.0254 \quad .0
$$

$$
.0232
$$

$$
.0213
$$

$$
.0164
$$

$$
\text { . } 0204
$$

$$
.0247
$$

$$
.0169
$$

$$
.0156
$$

$$
.0160
$$

$$
\begin{array}{r}
.0139 \\
.0169
\end{array}
$$

.0165

$$
.0169
$$

## LABORATORY 2

| RUN 4 | RUN 5 | RUN 6 |
| :--- | :--- | :--- |
| .0000 | .0000 | .0000 |
| .0771 | .0632 | .0482 |

$\begin{array}{llll}.1177 & .1101 & .1056 & .0959 \\ .1556 & .1479 & .1453 & .1388\end{array}$
NBS REPEAT
RUN 7 RUN 8 RUN 9
$.1511 \quad .1549 .1535$

$$
\begin{array}{lll}
.1821 & .1804 & .1752 \\
.2221 & .2207 & .2154
\end{array}
$$

$$
.1896 .1918 \quad .1909
$$

$$
\begin{array}{lll}
.2521 & .2201 & .2154 \\
.2576 & .2553 & .2507 \\
\hline 2026 & 2771
\end{array}
$$

$$
\begin{array}{lll}
.2345 & .2376 & .2318 \\
.2710 & .2747 & .2588
\end{array}
$$

$$
\begin{array}{lll}
.2843 & .2826 & .2771 \\
.3028 & .3015 & .2956
\end{array}
$$

$$
\begin{array}{lll}
.2710 & .2747 & .2588 \\
.3034 & .3075 & .2769
\end{array}
$$

$$
\begin{array}{rrr}
.3028 & .3015 & .2956 \\
.3111 & .3096 & .3040 \\
.3097 & .3080 & .3023
\end{array}
$$

$$
\begin{array}{lll}
.3034 & .3075 & .2769 \\
.3238 & .3285 & .3245
\end{array}
$$

$$
\begin{array}{rr}
.3238 & .3285 \\
.3334 & .3389 \\
.3358
\end{array}
$$

$$
\begin{array}{llll}
.3328 & .3097 & .3080 & .3023 \\
.3225 & .3005 & .2993 & .2942
\end{array}
$$

$$
\begin{array}{lll}
.3334 & .3389 & .3358 \\
.3326 & .3355 & .3331 \\
.3221 & .3245 & .3226
\end{array}
$$

$\cdot 3005 \cdot 2993 \cdot 2942$

$$
.3221
$$

| .2833 | .2816 | .2767 |
| :--- | :--- | :--- |
| .2660 | .2645 | .2602 |
| .2549 | .2537 | .2494 |
| .2569 | .2560 | .2524 |
| .2806 | .2806 | .2766 |
| .3141 | .3143 | .3099 |
| .3571 | .3566 | .3522 |
| .3844 | .3840 | .3787 |
| .3863 | .3858 | .3803 |
| .3606 | .3596 | .3546 |

$$
\begin{aligned}
& .3019 \\
& .2822
\end{aligned}
$$

$$
\begin{array}{lll}
.2822 & .2856 & .2832 \\
.2677 & .2705 & .2681
\end{array}
$$

$$
\text { . } 2686 \text {. } 2705 \cdot 2690
$$

$$
.2903 \cdot 2929.2902
$$

$$
.3248 \quad .3273 \quad .3247
$$

$$
.3738 \quad .3760 \quad .3753
$$

$$
.4041 \quad .4071 \quad .4053
$$

$$
.4079 .4110 \quad .4092
$$

$$
.3791 .3820 .3806
$$

$$
.3161 \cdot 3154 \quad \cdot 3107
$$

$$
.2625 \quad .2618 \quad .2579
$$

$$
.2089 .2086 \quad .2056
$$

$$
.1618 \quad .1617 \quad .1590
$$

$$
.1231 \quad .1227 \quad .1211
$$

$$
.0926 \quad .0922 .0908
$$

$$
.0693 \quad .0690 \quad .0677
$$

$$
.0520 \quad .0515 \quad .0506
$$

$$
.0389 \quad .0383 \quad .0375
$$

$$
.0302 .0298 \quad .0291
$$

$$
.0225 .0220 .02
$$

$$
.0176 \quad .0174 \quad .01
$$

$$
.0130 \quad .0125 \quad .01
$$

$$
.0102 .0095
$$

$$
.3330 \quad .3342 \quad .3337
$$

2758

$$
.2182 \quad .2224 \quad .2193
$$

$$
.1679 \quad .1697 \quad .1728
$$

$$
.1283 .1304 \quad .1296
$$

$$
.0962 .0973 .0972
$$

$$
.0705 \quad .0718 \quad .0716
$$

$$
.0534 .0545 \quad .0543
$$

$$
.0407 .0408 \quad .0415
$$

$$
.0318 \quad .0327 \quad .0334
$$

$$
.0246 .0243 .0251
$$

$$
.0207 .0203 .0212
$$

$$
.0161 .0154 \quad .0166
$$

$$
.0143 .0134 \quad .0148
$$

$$
.0150 \quad .0139 \quad .0155
$$

$$
.0159 .0145 \quad .0164
$$

$$
.0123 \quad .0103 \quad .0127
$$

## MERCURY LINES

| 405.0 | .1818 | .1827 | .1817 | .1862 | .1840 | .1738 | .1822 | .1856 | .1793 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 436.0 | .4541 | .4524 | .4506 | .4174 | .4093 | .3938 | .4467 | .4539 | .4524 |
| 546.0 | .2219 | .2235 | .2216 | .2006 | .2017 | .2031 | .2185 | .2194 | .2194 |
| 578.0 | .0736 | .0744 | .0740 | .0710 | .0710 | .0694 | .0712 | .0716 | .0707 |



FIGURE 4.39 AVERAGE SPECTRAL FLUX (SPHERE MEASUREMENTS)

RELATIVE SPECTRAL FLUX DISTRIBUTION IN SPHERE-NORMALIZED TO AREA LAMP NUMBER NBS8911

NBS INITIAL

WAVELEN
380.0 380.0
390.0

| 400.0 | 14.0 | 13.9 | 14.0 |
| :--- | :--- | :--- | :--- |
| 410.0 | 18.3 | 18.3 | 18.4 |
| 420.0 | 22.7 | 23.9 | 22.8 |
| 430.0 | 28.0 | 27.8 | 28.1 |
| 440.0 | 32.2 | 32.0 | 32.4 |
| 450.0 | 36.0 | 36.5 | 36.2 |
| 460.0 | 38.4 | 38.2 | 38.6 |
| 470.0 | 39.4 | 39.4 | 39.6 |
| 480.0 | 39.1 | 39.1 | 39.2 |
| 490.0 | 37.8 | 37.9 | 38.0 |

500.0 510.0 520.0 530.0 540.0 550.0 560.0 570.0 580.0 590.0
600.0 610.0 620.0 630.0 640.0 650.0 660.0 670.0 680.0 690.0
700.0 710.0 720.0 730.0 740.0
750.0
$760 \cdot 0$
RUN 1 RUN 2 RUN 3

| 5.2 | 5.1 | 5.2 |
| :--- | :--- | :--- |
| 8.7 | 8.6 | 8.7 |

LABORATORY 4

| RUN 4 | RUN 5 | RUN 6 |
| ---: | ---: | ---: |
| 5.6 | 5.6 | 5.6 |
| 9.0 | 9.0 | 9.0 |

$13.1 \quad 13.2 \quad 13.2$
$18.0 \quad 18.0 \quad 18.1$ $23.4 \quad 23.3 \quad 23.4$ $29.2 \quad 29.1 \quad 29.4$ $33.9 \quad 34.0 \quad 34.1$ $\begin{array}{lll}38.3 & 38.4 & 38.3 \\ 40.4 & 40.5 & 40.5\end{array}$ $41.2 \quad 41.2 \quad 41.6$ $\begin{array}{lll}40.5 & 40.4 & 40.6 \\ 38.7 & 38.7 & 38.8\end{array}$ $38.7 \quad 38.7$ 38.8 36.0
33.5
31.9
31.8
34.4
39.2
44.2
47.3
57.8
44.3 44. 36.
33.
31
32
34
39
44
47
57
44

| 36.0 | 36.0 |
| :--- | :--- |
| 33.5 | 33.5 |
| 31.8 | 31.9 |
| 31.8 | 31.8 |
| 34.4 | 34.4 |
| 39.1 | 39.2 |
| 44.0 | 44.2 |
| 47.1 | 47.3 |
| 58.4 | 57.8 |
| 44.2 | 44.3 |

$38.6 \quad 38.4 \quad 38.6$
$31.9 \quad 31.7 \quad 31.8$
$25.2 \quad 25.1 \quad 25.2$
$19.5 \quad 19.4 \quad 19.5$
$14.8 \quad 14.7 \quad 14.8$
$11.1 \quad 11.0 \quad 11.1$

## 8.

6.3
4.8
3.8
$2.9 \quad 2.9 \quad 2.8$
$2.3 \quad 2.3 \quad 2.3$
1.7
1.5
1.5
1.5
1.2

NBS REPEAT

| RUN 7 | RUN 8 | RUN 9 |
| ---: | ---: | ---: |
| 4.9 | 5.0 | 5.0 |
| 8.4 | 8.3 | 8.5 |
| 13.4 | 13.4 | 13.6 |
| 18.0 | 18.0 | 18.0 |
| 22.6 | 22.5 | 22.7 |
| 27.8 | 27.6 | 28.0 |
| 32.3 | 32.1 | 32.3 |
| 33.6 | 35.9 | 36.1 |
| 38.7 | 38.4 | 38.6 |
| 39.8 | 39.5 | 39.7 |
| 39.6 | 39.4 | 39.4 |
| 38.3 | 38.1 | 38.1 | $33.6 \quad 33.4$ $\begin{array}{ll}32.2 & 31.7\end{array}$ $32.0 \quad 31.7$ 34. 44.

48. 

48.5
45.2
39.
32.
26.
20.

15

## 11

8. 
9. 
10. 
11. 

39.239 .1
$32.6 \quad 32.6$
$26.0 \quad 25.9$
$20.1 \quad 19.8$
$15.4 \quad 15.2$

$$
20
$$ 2. 1. 1. 1. 1.2

34.3
38.4 44.1 47.7 48.1 $45 \cdot 5$
11.411 .3
$8.5 \quad 8.3$

## MERCURY LINES

21.6
53.7 26.2 $8 \cdot 8$
$\begin{array}{rr}21.5 & 21.6 \\ 52.7 & 53.1 \\ 26.0 & 26.0 \\ 8.7 & 8.6\end{array}$
10.1
45.0
28.8
6.9
10.3
46.5
28.8
6.8
10.3
45.6
28.8
6.9
21.8
53.1
25.8
8.5
21.4
52.8
25.6
8.3
21.8
53.2
25.8


FIGURE 4.40 AVERAGE RELATIVE SPECTRAL FLUX (SPHERE MEASUREMENTS) NORMALIZED TO AREA

## TABLE 4.49

SPECTRAL FLUX DISTRIBUTION (WATTS) IN SPHERE
LAMP NUMBER NBS8911

|  | NBS INITIAL |  |  | LABORATORY 4 |  |  | NBS REPEAT |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 | RUN 9 |
| 380.0 | . 0450 | . 0438 | . 0441 | . 0550 | . 0552 | . 0552 | . 0413 | . 0425 | . 0427 |
| 390.0 | . 0757 | . 0736 | . 0746 | . 0884 | . 0889 | . 0885 | . 0708 | . 0702 | . 0720 |
| 400.0 | . 1217 | . 1186 | . 1190 | . 1285 | . 1299 | . 1293 | .1128 | . 1141 | . 1151 |
| 410.0 | . 1590 | . 1558 | . 1566 | . 1761 | . 1773 | . 1771 | . 1514 | . 1532 | . 1529 |
| 420.0 | . 1972 | - 2034 | . 1944 | . 2290 | . 2296 | . 2291 | . 1900 | . 1911 | . 1929 |
| 430.0 | . 2432 | . 2363 | . 2393 | . 2866 | . 2871 | - 2884 | . 2342 | . 2349 | . 2375 |
| 440.0 | . 2796 | . 2728 | . 2760 | . 3323 | . 3345 | . 3342 | . 2718 | . 2725 | . 2742 |
| 450.0 | . 3121 | - 3111 | . 3084 | . 3761 | . 3786 | . 3761 | . 2830 | . 3047 | . 3066 |
| 460.0 | . 3329 | . 3256 | . 3287 | . 3964 | . 3993 | . 3974 | . 3259 | . 3266 | . 3273 |
| 470.0 | . 3420 | - 3356 | . 3374 | . 4040 | . 4062 | . 4076 | . 3352 | . 3360 | . 3367 |
| 480.0 | . 3390 | -3330 | . 3343 | . 3972 | . 3978 | - 3978 | - 3332 | - 3351 | . 3347 |
| 490.0 | . 3280 | - 3223 | . 3236 | . 3798 | . 3809 | . 3803 | . 3223 | . 3236 | . 3235 |
| 500.0 | . 3077 | . 3032 | . 3040 | . 3552 | - 3547 | - 3530 | . 3027 | . 3036 | . 3045 |
| 510.0 | . 2869 | . 2830 | . 2830 | . 3301 | . 3297 | . 3284 | . 2829 | . 2840 | . 2843 |
| 520.0 | . 2726 | - 2684 | . 2689 | . 3127 | . 3134 | - 3131 | . 2709 | - 2696 | . 2690 |
| 530.0 | . 2748 | - 2702 | . 2710 | . 3138 | - 3131 | - 3118 | - 2690 | - 2697 | - 2698 |
| 540.0 | . 2978 | . 2926 | . 2942 | . 3389 | . 3387 | . 3373 | . 2868 | . 2913 | . 2913 |
| 550.0 | . 3335 | - 3278 | . 3296 | . 3846 | - 3851 | - 3849 | - 3254 | - 3259 | - 3259 |
| 560.0 | . 3839 | - 3776 | . 3795 | . 4335 | . 4339 | . 4337 | . 3748 | . 3749 | - 3751 |
| 570.0 | . 4127 | . 4066 | . 4084 | . 4643 | . 4642 | . 4638 | . 4045 | . 4052 | . 4052 |
| 580.0 | . 4152 | . 4095 | . 4108 | . 5629 | . 5754 | . 5673 | . 4083 | . 4087 | . 4090 |
| 590.0 | . 3848 | . 3799 | . 3800 | . 4355 | . 4350 | . 4344 | . 3799 | - 3864 | . 3815 |
| 600.0 | . 3365 | . 3332 | . 3331 | . 3785 | .3786 | . 3785 | . 3323 | . 3331 | . 3321 |
| 610.0 | . 2792 | . 2784 | . 2755 | . 3126 | - 3119 | - 3120 | . 2765 | - 2769 | - 2767 |
| 620.0 | . 2213 | . 2166 | . 2161 | . 2474 | . 2472 | . 2471 | . 2195 | . 2213 | . 2198 |
| 630.0 | . 1710 | . 1688 | . 1690 | . 1909 | . 1911 | . 1911 | . 1685 | . 1711 | . 1684 |
| 640.0 | . 1299 | . 1271 | . 1259 | . 1448 | . 1449 | . 1449 | . 1278 | -1308 | . 1291 |
| 650.0 | . 0975 | . 0947 | . 0932 | . 1090 | . 1085 | . 1085 | . 0963 | . 0971 | . 0957 |
| 660.0 | . 0713 | . 0687 | . 0685 | . 0818 | . 0811 | . 0804 | . 0699 | . 0722 | . 0707 |
| 670.0 | . 0544 | . 0531 | . 0532 | . 0616 | . 0609 | . 0600 | . 0536 | . 0552 | . 0536 |
| 680.0 | . 0402 | . 0389 | . 0390 | . 0469 | . 0470 | . 0461 | . 0391 | . 0417 | . 0401 |
| 690.0 | . 0335 | . 0322 | . 0311 | . 0376 | . 0367 | . 0356 | . 0319 | . 0339 | . 0321 |
| 700.0 | . 0252 | . 0238 | . 0239 | . 0289 | . 0290 | - 0278 | . 0236 | . 0258 | . 0238 |
| 710.0 | . 0212 | . 0197 | . 0198 | . 0227 | . 0227 | . 0227 | . 0197 | . 0220 | . 0210 |
| 720.0 | .0179 | .0162 | . 0146 | . 0171 | . 0171 | . 0171 | . 0150 | . 0164 | . 0151 |
| 730.0 | . 0245 | . 0226 | . 0227 | . 0146 | . 0146 | . 0128 | . 0115 | . 0145 | . 0131 |
| 740.0 | . 0155 | . 0133 | . 0133 | . 0149 | . 0149 | . 0128 | . 0117 | . 0153 | . 0136 |
| 750.0 | . 0159 | . 0159 | . 0133 | . 0150 | . 0150 | . 0125 | . 0120 | . 0163 | . 0142 |
| $760 \cdot 0$ | . 0164 | .0131 | . 0132 | . 0119 | . 0119 | .0119 | . 0099 | . 0126 | . 0101 |

## MERCURY LINES

| 405.0 | .1877 | .1834 | .1843 | .0986 | .1015 | .1006 | .1833 | .1815 | .1851 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 436.0 | .4657 | .4491 | .4524 | .4414 | .4584 | .4475 | .4467 | .4483 | .4511 |
| 546.0 | .2276 | .2216 | .2217 | .2823 | .2833 | .2824 | .2167 | .2179 | .2193 |
| 578.0 | .0766 | .0743 | .0733 | .0675 | .0667 | .0673 | .0713 | .0709 | .0706 |



FIGURE 4.41 AVERAGE SPECTRAL FLUX (SPHERE MEASUREMENTS)

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8795

| WAVELENGTH380.0 | NBS |  |  | LABORATORY 7 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 |
|  | 3.9 | 3.7 | 4.0 | 2.9 | 12.9 | 1.9 |
| 390.0 | 6.0 | 5.8 | 5.9 | 3.4 | 3.9 | 2.9 |
| 400.0 | 8.2 | 8.0 | 8.1 | 4.7 | 5.0 | 4.2 |
| 410.0 | 10.7 | 10.5 | 10.5 | 6.4 | 6.6 | 5.9 |
| 420.0 | 13.3 | 13.0 | 13.2 | 8.9 | 9.0 | 8.4 |
| 430.0 | 16.3 | 15.8 | 16.0 | 11.3 | 11.4 | 10.5 |
| 440.0 | 18.9 | 18.5 | 18.5 | 14.0 | 14.1 | 13.6 |
| 450.0 | 21.0 | 20.9 | 21.0 | 16.6 | 15.4 | 15.4 |
| 460.0 | 22.8 | 22.7 | 22.7 | 18.3 | 17.6 | 17.9 |
| 470.0 | 24.0 | 23.9 | 23.8 | 20.3 | 19.2 | 19.7 |
| 480.0 | 24.3 | 24.4 | 24.2 | 20.2 | 20.8 | 20.9 |
| 490.0 | 24.3 | 24.1 | 24.2 | 20.6 | 20.4 | 21.5 |
| 500.0 | 23.3 | 23.3 | 23.2 | 20.9 | 20.6 | 21.0 |
| 510.0 | 22.8 | 22.6 | 22.6 | 20.7 | 20.1 | 20.8 |
| 520.0 | 23.7 | 23.6 | 23.7 | 21.3 | 20.9 | 21.8 |
| 530.0 | 27.6 | 27.3 | 27.5 | 24.4 | 24.0 | 24.6 |
| 540.0 | 35.3 | 35.0 | 35.2 | 31.4 | 31.1 | 32.0 |
| 550.0 | 45.3 | 44.9 | 45.1 | 40.7 | $40 \cdot 4$ | 41.3 |
| 560.0 | 57.9 | 57.6 | 57.6 | 52.5 | $52 \cdot 5$ | 53.8 |
| 570.0 | 65.9 | 65.7 | 65.7 | 59.6 | 60.2 | 61.5 |
| 580.0 | 68.6 | 68.5 | 68.4 | 62.1 | 63.0 | 64.0 |
| 590.0 | 64.3 | 64.3 | 64.3 | 58.6 | 60.9 | 61.2 |
| 600.0 | 56.4 | 57.2 | 56.6 | 52.9 | 53.3 | 54.6 |
| 610.0 | 46.8 | 47.6 | 47.0 | 44.0 | 45.7 | 45.0 |
| 620.0 | 36.7 | 37.5 | 36.7 | 35.1 | 36.3 | 36.5 |
| 630.0 | 28.6 | 29.4 | 28.5 | 28.8 | 29.3 | 30.1 |
| 640.0 | 21.1 | 21.5 | 21.2 | 21.5 | 22.7 | 22.1 |
| 650.0 | 15.4 | 15.6 | 15.6 | 16.9 | 18.2 | 17.8 |
| 660.0 | 11.3 | 11.4 | 11.4 | 13.5 | 14.0 | 14.0 |
| 670.0 | 8.5 | 8.8 | 8.5 | 12.0 | 12.0 | 11.6 |
| 680.0 | 6.2 | 6.4 | 6.3 | 10.8 | 8.1 | 10.1 |
| 690.0 | 4.8 | 4.8 | 5.1 | 10.9 | 10.3 | 9.9 |
| 700.0 | 3.5 | 3.7 | 3.8 | 11.2 | 10.6 | 9.8 |
| 710.0 | 2.9 | 3.2 | 3.3 | 12.5 | 11.9 | 11.2 |
| 720.0 | 2.5 | 2.6 | 2.9 | 14.5 | 13.3 | 13.2 |
| 730.0 | 4.8 | 5.1 | 5.6 | 17.3 | 16.7 | 15.9 |
| 740.0 | 2.0 | 2.1 | 2.5 | 20.4 | 20.1 | 19.7 |
| 750.0 | 2.1 | 2.0 | 2.5 | 25.1 | 23.2 | 22.4 |
| 760.0 | 2.1 | 2.0 | 2.9 | 28.4 | 26.5 | 24.5 |

MERCURY LINES

| 405.0 | 22.5 | 21.5 | 21.9 | 5.9 | 6.9 | 6.2 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 58.5 | 58.6 | 58.0 | 28.7 | 29.7 | 28.6 |
| 546.0 | 25.9 | 25.9 | 25.6 | 25.0 | 24.6 | 26.3 |
| 578.0 | 8.8 | 8.8 | 8.9 | 24.7 | 25.0 | 25.8 |



FIGURE 4.42 AVERAGE RELATIVE SPECTRAL IRRADIANCE ( 25 CM SECTION) MEASUREMENTS NORMALIZED TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8796

| WAVELENGTH | NBS |  |  | LABORATORY 7 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 |
| 380.0 | 3.5 | 3.4 | 3.6 | 2.2 | 12.6 | 1.7 |
| 390.0 | 5.5 | $5 \cdot 3$ | 5.4 | 2.8 | 3.8 | 2.6 |
| 400.0 | 7.6 | 7.4 | 7.5 | 4.1 | 5.0 | 3.9 |
| 410.0 | 10.0 | 9.7 | 9.9 | 5.9 | 6.7 | 5.5 |
| 420.0 | 12.5 | 12.3 | 12.4 | 8.3 | 8.7 | 7.7 |
| 430.0 | 15.4 | 15.1 | 15.0 | 10.6 | 10.6 | 9.5 |
| 440.0 | 17.9 | 17.6 | 17.5 | 13.1 | 13.1 | 12.3 |
| 450.0 | 20.0 | 19.8 | 19.8 | 15.4 | 14.4 | 14.0 |
| 460.0 | 21.8 | 21.6 | 21.5 | 17.3 | 16.7 | 16.4 |
| 470.0 | 23.0 | 22.8 | 22.8 | 19.2 | 18.0 | 17.8 |
| 480.0 | 23.5 | 23.4 | 23.2 | 19.9 | 19.5 | 19.6 |
| 490.0 | 23.4 | 23.3 | 23.3 | 20.9 | 19.5 | 20.2 |
| $500 \cdot 0$ | 22.7 | 22.5 | 22.4 | 20.5 | 19.9 | 20.0 |
| 510.0 | 22.3 | 22.1 | 22.0 | 20.4 | 19.9 | 19.7 |
| 520.0 | 23.3 | 23.1 | 23.2 | 21.0 | 21.0 | 20.7 |
| 530.0 | 27.5 | 27.1 | 27.2 | 24.3 | 24.5 | 23.9 |
| 540.0 | 35.5 | 35.2 | 35.3 | 30.5 | 32.0 | 32.0 |
| 550.0 | 45.9 | 45.5 | 45.5 | 40.0 | 41.7 | 41.5 |
| 560.0 | 58.9 | 58.4 | 58.5 | 52.8 | 54.1 | 53.9 |
| 570.0 | 67.2 | 67.0 | 66.9 | 61.2 | 61.9 | 61.7 |
| 580.0 | 70.1 | $70 \cdot 2$ | 69.8 | 64.8 | 64.5 | 65.6 |
| 590.0 | 66.1 | 66.5 | 65.8 | 61.8 | 62.0 | 65.6 |
| 600.0 | 58.4 | 58.6 | 58.1 | 53.7 | 54.5 | 54.4 |
| 610.0 | 48.6 | 48.4 | 48.3 | 45.3 | 47.0 | 46.3 |
| 620.0 | 37.8 | 38.4 | 37.8 | 37.5 | 37.9 | 37.6 |
| 630.0 | 29.4 | 29.7 | 29.7 | 30.7 | 29.8 | 29.8 |
| 640.0 | 21.7 | 22.2 | 21.9 | 24.0 | 24.5 | 23.0 |
| $650 \cdot 0$ | 16.0 | 16.5 | 16.2 | 18.3 | 18.4 | 17.8 |
| 660.0 | 11.7 | 12.0 | 11.8 | 14.9 | 14.4 | 14.8 |
| 670.0 | 8.6 | 8.9 | 9.1 | 12.1 | 11.9 | 12.2 |
| 680.0 | 6.3 | 6.3 | 6.5 | 10.5 | 10.4 | 10.2 |
| 690.0 | 5.0 | $5 \cdot 1$ | $5 \cdot 3$ | 10.4 | 10.1 | 10.0 |
| 700.0 | 3.7 | 4.1 | 4.1 | 10.5 | 10.0 | 9.4 |
| 710.0 | 3.1 | 3.2 | 3.5 | 11.6 | 11.1 | 10.9 |
| 720.0 | 2.4 | 2.7 | 3.0 | 13.2 | 12.4 | 25.1 |
| 730.0 | 4.6 | 4.9 | 5.3 | 15.4 | 15.5 | 14.9 |
| 740.0 | 1.8 | 2.4 | 2.8 | 18.3 | 19.0 | 18.2 |
| 750.0 | 1.7 | 2.4 | 2.8 | 22.6 | 21.8 | 20.8 |
| 760.0 | 2.1 | 2.3 | 2.8 | 25.7 | 25.2 | 23.2 |

MERCURY LINES

| 405.0 | 21.7 | 20.8 | 21.1 | 5.8 | 6.5 | 5.9 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 56.2 | 56.7 | 56.4 | 29.0 | 28.8 | 27.6 |
| 546.0 | 26.1 | 25.9 | 25.8 | 27.1 | 25.3 | 26.8 |
| 578.0 | 9.2 | 9.0 | 9.0 | 26.4 | 24.9 | 25.4 |



FIGURE 4.43 AVERAGE RELATIVE SPECTRAL IRRADIANCE $(25$ CM SECTION) MEASUREMENTS NORMALIZED TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8797

| WAVELENGTH | NBS |  |  | LABORATORY 1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 |
| 380.0 | 3.5 | 3.5 | 3.8 | . 0 | . 0 | . 0 |
| 390.0 | 5.7 | 5.6 | 5.8 | 5.4 | 5.5 | 5.9 |
| 400.0 | 8.0 | 7.9 | 7.9 | 7.5 | 7.5 | 7.7 |
| 410.0 | 10.5 | $10 \cdot 3$ | 10.3 | 10.0 | 10.1 | 10.1 |
| 420.0 | 13.0 | 12.8 | 12.9 | 12.7 | 12.8 | 12.7 |
| 430.0 | 15.8 | 15.5 | 15.7 | 15.6 | 15.6 | 15.5 |
| 440.0 | 18.3 | 18.1 | 18.1 | 18.2 | 18.3 | 18.2 |
| 450.0 | 20.5 | 20.3 | 20.5 | 20.5 | 20.6 | 20.4 |
| 460.0 | 22.3 | 22.1 | 22.3 | 22.4 | 22.5 | 22.3 |
| 470.0 | 23.5 | 23.3 | 23.3 | 23.6 | 23.8 | 23.5 |
| 480.0 | 23.9 | 23.8 | 23.7 | 24.0 | 24.2 | 23.9 |
| 490.0 | 23.9 | 23.6 | 23.7 | 23.7 | 23.9 | 23.8 |
| 500.0 | 23.0 | 22.8 | 22.8 | 22.6 | 22.8 | 23.2 |
| 510.0 | 22.5 | 22.3 | 22.3 | 22.3 | 22.4 | 22.8 |
| 520.0 | 23.3 | 23.3 | 23.3 | 23.4 | 23.5 | 23.9 |
| 530.0 | 27.4 | 27.1 | 27.3 | 27.9 | 27.9 | 28.3 |
| 540.0 | 35.4 | 35.1 | 35.2 | 35.4 | 35.4 | 35.7 |
| 550.0 | 45.6 | 45.1 | 45.3 | 46.0 | 46.1 | 46.2 |
| 560.0 | 58.4 | 57.7 | 58.1 | 59.7 | 59.9 | 59.7 |
| 570.0 | 66.6 | 65.7 | 66.3 | 67.8 | 68.2 | 67.6 |
| 580.0 | 69.5 | 68.6 | 69.0 | 70.5 | 70.9 | 70.1 |
| 590.0 | 65.3 | 65.0 | 65.0 | 67.7 | 68.0 | 67.2 |
| 600.0 | 57.3 | 57.2 | 57.0 | 59.5 | 59.5 | 58.8 |
| 610.0 | 47.5 | 47.3 | 47.3 | 49.1 | 49.2 | 48.6 |
| 620.0 | 37.1 | 37.6 | 37.1 | 39.7 | 39.6 | 39.2 |
| 630.0 | 28.6 | 29.7 | 29.0 | 29.9 | 29.9 | 29.5 |
| 640.0 | 21.2 | 21.4 | 21.5 | 21.8 | 21.8 | 21.7 |
| 650.0 | 15.4 | 15.8 | 15.5 | 16.2 | 16.1 | 16.2 |
| 660.0 | 11.4 | 11.7 | 11.5 | 11.9 | 11.8 | 12.1 |
| 670.0 | 8.5 | 8.6 | 8.7 | 8.7 | 8.5 | 8.9 |
| 680.0 | 6.1 | 6.1 | 6.3 | 6.5 | 6.3 | 6.8 |
| 690.0 | 4.7 | 4.9 | 4.9 | 5.0 | $4 \cdot 8$ | 5.3 |
| 700.0 | 3.5 | 3.8 | 4.0 | 3.8 | 3.6 | 4.1 |
| 710.0 | 2.8 | 3.1 | 3.4 | 2.9 | 2.8 | 3.2 |
| 720.0 | 2.4 | 2.4 | 2.8 | 2.3 | 2.0 | 2.6 |
| 730.0 | 4.6 | 4.9 | 5.2 | . 0 | . 0 | . 0 |
| 740.0 | 1.6 | 2.1 | 2.2 | . 0 | . 0 | . 0 |
| 750.0 | 1.9 | 2.1 | 2.6 | . 0 | . 0 | . 0 |
| 760.0 | 1.5 | $2 \cdot 0$ | 2.0 | . 0 | - 0 | . 0 |

MERCURY LINES

| 405.0 | 22.5 | 22.5 | 21.0 | 24.1 | 21.1 | 21.1 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 60.5 | 61.6 | 61.0 | 54.4 | 54.4 | 55.7 |
| 546.0 | 25.7 | 26.1 | 25.8 | 28.1 | 28.4 | 28.4 |
| 578.0 | 9.3 | 9.7 | 9.0 | 9.5 | 10.3 | 9.1 |



FIGURE 4.44 AVERAGE RELATIVE SPECTRAL IRRAOIANCE ( 25 CM SECTION) MEASUREMENTS NORMALIZEO TO RREA

|  | NBS |  |  | LABORATORY 1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 |
| 380.0 | 3.5 | 3.5 | 3.7 | . 0 | . 0 | . 0 |
| 390.0 | 5.7 | $5 \cdot 5$ | 5.8 | 5.8 | 5.7 | 5.8 |
| 400.0 | 7.9 | 7.6 | 7.8 | 7.8 | 7.7 | 7.6 |
| 410.0 | 10.4 | 10.0 | 10.2 | 10.1 | 10.1 | 9.9 |
| 420.0 | 13.0 | 12.6 | 12.9 | 12.7 | 12.7 | 12.5 |
| 430.0 | 16.0 | 15.4 | 15.7 | 15.5 | 15.5 | 15.3 |
| 440.0 | 18.5 | 18.1 | 16.8 | 18.1 | 18.2 | 18.1 |
| 450.0 | 20.6 | 20.4 | 18.6 | 20.4 | 20.4 | 20.4 |
| 460.0 | 22.4 | 22.2 | 22.4 | 22.2 | 22.2 | 22.2 |
| 470.0 | 23.7 | 23.3 | 23.4 | 23.4 | 23.6 | 23.4 |
| 480.0 | 23.9 | 23.8 | 23.8 | 23.8 | 23.8 | 23.9 |
| 490.0 | 23.9 | 23.7 | 23.9 | 23.7 | 23.6 | 23.8 |
| 500.0 | 22.9 | 22.8 | 22.9 | 23.1 | 23.1 | 23.1 |
| 510.0 | 22.6 | 22.5 | 22.5 | 22.7 | 22.6 | 22.7 |
| 520.0 | 23.6 | 23.4 | 23.6 | 23.9 | 23.7 | 23.9 |
| 530.0 | 27.8 | 27.4 | 27.7 | 28.3 | 28.2 | 28.3 |
| 540.0 | 35.8 | 35.4 | 35.9 | 35.9 | 35.7 | 35.8 |
| 550.0 | 46.1 | 45.5 | 46.1 | 46.4 | 46.2 | 46.3 |
| 560.0 | 58.9 | 58.0 | 58.9 | 60.1 | 59.7 | 59.9 |
| 570.0 | 66.9 | 66.5 | 67.1 | 68.0 | 67.7 | 68.0 |
| 580.0 | 69.5 | 69.5 | 69.7 | 70.5 | 70.4 | 70.6 |
| 590.0 | 64.9 | 65.5 | 65.3 | 67.6 | 67.6 | 67.7 |
| 600.0 | 57.0 | 57.3 | 57.2 | 59.1 | 59.4 | 59.2 |
| 610.0 | 47.1 | 47.3 | 47.4 | 49.0 | 49.1 | 48.9 |
| 620.0 | 36.7 | 38.2 | 37.3 | 39.5 | 39.8 | 39.5 |
| 630.0 | 28.4 | 30.2 | 29.0 | 29.9 | 29.9 | 29.8 |
| 640.0 | 21.0 | 21.7 | 21.4 | 21.9 | 22.0 | 21.9 |
| 650.0 | 15.5 | 15.9 | 16.0 | 16.5 | 16.5 | 16.4 |
| 660.0 | 11.3 | 11.9 | 11.5 | 12.2 | 12.2 | 12.1 |
| 670.0 | 8.4 | 8.7 | 8.8 | 8.9 | 8.9 | 8.9 |
| 680.0 | 6.4 | 6.3 | 6.5 | 6.8 | 6.8 | 6.7 |
| 690.0 | 4.7 | $5 \cdot 0$ | 4.9 | 5.3 | $5 \cdot 3$ | 5.2 |
| 700.0 | 3.5 | 3.8 | 2.2 | 4.1 | 4.1 | 4.0 |
| 710.0 | 2.8 | 3.2 | 3.5 | 3.3 | 3.3 | 3.2 |
| 720.0 | 2.4 | - 3 | 2.8 | 2.6 | 2.6 | 2.5 |
| 730.0 | 4.6 | 4.8 | 5.6 | . 0 | - 0 | . 0 |
| 740.0 | 1.6 | 2.2 | 2.6 | . 0 | - 0 | . 0 |
| 750.0 | 1.9 | 2.2 | 2.8 | . 0 | - 0 | . 0 |
| 760.0 | 1.5 | 2.6 | 3.1 | . 0 | . 0 | . 0 |

MERCURY LINES

| 405.0 | 22.7 | 21.9 | 22.1 | 20.4 | 20.8 | 21.5 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 58.5 | 58.9 | 58.1 | 52.5 | 53.4 | 54.3 |
| 546.0 | 26.2 | 25.9 | 25.6 | 27.6 | 27.7 | 27.9 |
| 578.0 | 9.2 | 8.9 | 8.9 | 10.2 | 10.1 | 8.9 |



FIGURE 4.45 AVERAGE RELATIVE SPECTRAL IRRADIANCE ( 25 CM SECTION) MEASUREMENTS NORMALIZED TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8799

|  | NBS |  |  | LABORATORY 9 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 | RUN 7 | RUN 8 |
| 380.0 | 3.6 | 3.7 | 3.8 | 3.7 | 3.7 | 3.7 | 3.7 | 3.6 |
| 390.0 | 5.8 | 5.9 | 5.9 | 6.5 | 6.6 | 5.8 | 5.8 | 5.6 |
| 400.0 | 7.9 | 8.1 | 7.9 | 7.8 | 7.8 | 7.9 | 7.9 | 7.8 |
| 410.0 | 10.5 | 10.6 | 10.4 | 10.5 | $10 \cdot 4$ | 10.5 | 10.4 | $10 \cdot 3$ |
| 420.0 | 13.1 | 13.1 | 13.1 | 13.0 | 13.0 | 13.1 | 13.0 | 13.1 |
| 430.0 | 16.2 | 15.8 | 16.1 | 15.8 | 15.8 | 15.8 | 15.9 | 15.9 |
| 440.0 | 18.8 | 18.5 | 18.6 | 18.5 | 18.5 | 18.6 | 18.6 | 18.5 |
| 450.0 | 21.0 | 21.0 | 20.9 | 20.9 | 20.8 | 20.8 | 20.9 | 20.9 |
| 460.0 | 22.7 | 22.9 | 22.7 | 22.8 | 22.5 | 22.7 | 22.8 | 22.7 |
| 470.0 | 23.9 | 24.0 | 23.7 | 23.9 | 23.8 | 23.7 | 23.7 | 23.9 |
| 480.0 | 24.2 | 24.6 | 24.0 | 24.4 | 24.1 | 24.2 | 24.2 | 24.2 |
| 490.0 | 24.2 | 24.3 | 24.1 | 24.2 | 24.1 | 24.1 | 24.2 | 24.3 |
| 500.0 | 23.1 | 23.5 | 23.0 | 23.1 | 23.1 | 23.2 | 23.2 | 23.2 |
| 510.0 | 22.7 | 22.9 | 22.6 | 22.6 | 22.4 | 22.6 | 22.5 | 22.7 |
| 520.0 | 23.5 | 23.8 | 23.1 | 23.5 | 23.4 | 23.6 | 23.7 | 23.7 |
| 530.0 | 27.5 | 27.7 | 27.5 | 27.5 | 27.5 | 27.5 | 27.5 | 27.5 |
| 540.0 | 35.3 | 35.1 | 35.5 | 35.5 | 35.0 | 35.5 | 35.6 | 35.4 |
| 550.0 | 45.5 | $45 \cdot 2$ | 45.6 | 46.8 | 46.4 | 46.9 | 46.7 | 47.1 |
| 560.0 | 58.3 | 58.6 | 58.3 | 58.1 | 58.0 | 58.4 | 58.6 | 58.4 |
| 570.0 | 66.5 | 67.2 | 66.4 | 65.7 | 65.5 | 65.7 | 65.8 | 65.9 |
| 580.0 | 69.2 | $70 \cdot 3$ | 69.0 | 67.1 | 66.8 | 67.0 | 67.1 | 67.4 |
| 590.0 | 65.0 | 66.2 | 65.0 | 65.6 | 65.0 | 65.5 | $65 \cdot 6$ | 65.6 |
| 600.0 | 57.2 | $58 \cdot 3$ | 57.0 | 58.0 | 58.1 | 57.8 | 57.7 | 57.9 |
| 610.0 | 47.9 | 48.2 | 47.1 | 48.2 | 47.8 | 46.9 | 47.4 | 48.0 |
| 620.0 | 37.1 | 37.8 | 37.3 | 37.7 | 37.8 | 37.9 | 37.7 | 38.1 |
| 630.0 | 28.9 | 30.0 | 28.6 | 28.6 | 28.8 | 28.9 | 28.8 | 28.4 |
| 640.0 | 21.3 | 22.4 | 21.1 | 21.3 | 21.4 | 21.4 | 21.5 | 20.9 |
| 650.0 | 15.9 | 16.1 | 15.7 | 15.7 | 15.9 | 15.8 | 15.2 | 15.9 |
| 660.0 | 11.5 | 11.9 | 11.5 | 11.6 | 11.6 | 11.6 | 11.5 | 11.7 |
| 670.0 | 8.6 | 8.9 | 8.6 | 8.6 | 8.5 | 8.5 | 8.5 | 8.6 |
| 680.0 | 6.0 | 6.5 | 6.3 | 6.3 | 6.2 | 6.2 | 6.3 | 6.4 |
| 690.0 | 4.6 | 5.1 | 5.1 | 4.9 | 5.0 | 4.9 | 4.8 | 5.0 |
| 700.0 | 3.5 | 4.0 | 3.8 | 3.8 | 3.8 | 3.7 | 3.7 | 3.7 |
| 710.0 | 2.8 | 3.2 | 3.3 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| 720.0 | 2.4 | 2.5 | 2.7 | 2.4 | 2.3 | 2.3 | $2 \cdot 3$ | 2.4 |
| 730.0 | 4.5 | 4.7 | 5.0 | 1.9 | 1.9 | 1.9 | 1.9 | 2.0 |
| 740.0 | 1.6 | 2.2 | 2.1 | 1.6 | 1.6 | 1.6 | 1.7 | 1.6 |
| 750.0 | 1.9 | 2.2 | 2.5 | 1.5 | 1.5 | 1.4 | 1.4 | 1.4 |
| 760.0 | 1.5 | 2.1 | 3.0 | 1.3 | 1.3 | 1.3 | 1.2 | 1.4 |

## MERCURY LINES

| 405.0 | 22.4 | 22.2 | 21.6 | 19.4 | 20.0 | 20.0 | 20.8 | 19.9 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 57.9 | 58.2 | 56.7 | 58.8 | 59.0 | 60.4 | 59.6 | 58.3 |
| 546.0 | 25.2 | 26.1 | 25.0 | 25.1 | 27.5 | 24.9 | 25.0 | 25.7 |
| 578.0 | 9.0 | 9.0 | 8.8 | 12.5 | 12.9 | 12.9 | 12.4 | 12.1 |



FIGURE 4.46 AVERAGE RELATIVE SPECTRAL IRRADIANCE ( 25 CM SECTION) MEASUREMENTS NORMALIZED TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8800

|  | NBS |  |  | LABORATORY 9 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 |
| 380.0 | 3.5 | 3.6 | 3.8 | 3.6 | 3.5 | 3.6 |
| 390.0 | 5.7 | 5.7 | 5.7 | 6.5 | 5.6 | 5.6 |
| 400.0 | 7.9 | 7.6 | 7.7 | 7.7 | 7.7 | 7.6 |
| 410.0 | 10.4 | 10.0 | 10.1 | 10.2 | 10.2 | 10.3 |
| 420.0 | 13.0 | 12.7 | 12.9 | 12.8 | 12.7 | 12.9 |
| 430.0 | 16.0 | 15.8 | 15.8 | 15.7 | 15.7 | 15.6 |
| 440.0 | 18.6 | 18.5 | 18.3 | 18.4 | 18.4 | 18.3 |
| 450.0 | 20.8 | 20.7 | 20.6 | 20.8 | 20.7 | 20.6 |
| 460.0 | 22.5 | 22.5 | 22.5 | 22.6 | 22.7 | 22.7 |
| 470.0 | 23.8 | 23.7 | 23.6 | 23.9 | 23.8 | 23.8 |
| 480.0 | 24.2 | 24.1 | 24.0 | 24.2 | 24.2 | 24.2 |
| 490.0 | $24 \cdot 2$ | 24.0 | 24.0 | 24.2 | 24.2 | 24.2 |
| 500.0 | 23.3 | 23.1 | 23.0 | 23.2 | 23.3 | 23.2 |
| 510.0 | $22 \cdot 8$ | 22.6 | 22.6 | 22.7 | 22.7 | 22.7 |
| 520.0 | 23.6 | 23.6 | 23.5 | 23.7 | 23.7 | 23.6 |
| 530.0 | 27.4 | 27.3 | 27.5 | 27.6 | 27.7 | 27.5 |
| 540.0 | 35.3 | 34.9 | 35.4 | 35.6 | 35.6 | 35.6 |
| 550.0 | 45.5 | 44.8 | 45.4 | 46.9 | 47.0 | 46.7 |
| 560.0 | 58.2 | 57.5 | 58.0 | 58.6 | 58.4 | 58.3 |
| 570.0 | 66.5 | 66.3 | 66.2 | 65.7 | 66.0 | 65.7 |
| 580.0 | 69.4 | 69.6 | 68.9 | 67.1 | 67.3 | 66.8 |
| 590.0 | 65.2 | $65 \cdot 6$ | 64.8 | 65.6 | 65.9 | 65.5 |
| 600.0 | 57.5 | 58.0 | 56.9 | 57.8 | 58.1 | 57.8 |
| 610.0 | 47.5 | 48.1 | 47.1 | 47.1 | 47.8 | 48.0 |
| 620.0 | 37.0 | 38.3 | 36.9 | 37.5 | 37.3 | 37.5 |
| 630.0 | 28.7 | 30.3 | 28.5 | 28.7 | 28.9 | 28.9 |
| 640.0 | 21.4 | 21.6 | 21.4 | 21.6 | 21.4 | 21.0 |
| 650.0 | 15.7 | 16.0 | 15.7 | 15.7 | 16.0 | 15.9 |
| 660.0 | 11.4 | 11.4 | 11.5 | 11.8 | 11.6 | 11.7 |
| 670.0 | 8.5 | 8.6 | 8.7 | 8.6 | 8.5 | 8.5 |
| 680.0 | 6.1 | 6.1 | 6.3 | 6.4 | 6.3 | 6.3 |
| 690.0 | 4.7 | $4 \cdot 8$ | 5.1 | 5.0 | 5.0 | 5.0 |
| 700.0 | 3.5 | 3.5 | 3.8 | 3.8 | 3.7 | 3.8 |
| 710.0 | 2.8 | 2.9 | 3.3 | 3.1 | 3.0 | 2.9 |
| 720.0 | 2.4 | 2.2 | 2.7 | 2.4 | 2.4 | 2.4 |
| 730.0 | 4.6 | 4.4 | 5.3 | 1.9 | 2.0 | 2.0 |
| 740.0 | 1.6 | 2.2 | 2.8 | 1.6 | 1.6 | 1.6 |
| 750.0 | 1.9 | 1.7 | 2.9 | 1.4 | 1.5 | 1.4 |
| 760.0 | 1 | 2.1 | 3.0 | 1.3 | 1.4 | 1. |

MERCURY LINES

| 405.0 | 22.2 | 20.7 | 21.7 | 20.7 | 20.1 | 20.1 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 58.8 | 58.6 | 58.1 | 57.7 | 58.9 | 59.6 |
| 546.0 | 25.6 | 25.7 | 25.3 | 25.6 | 25.0 | 27.0 |
| 578.0 | 8.7 | 8.8 | 9.0 | 12.7 | 12.7 | 12.3 |



FIGURE 4.47 gVERAGE RELATIVE SPECTRAL IRRADIANCE $(25$ CM SECTION) MEASUREMENTS NORMALIZED TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8801

|  | NBS |  |  | LABURATORY 5 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 |
| 380.0 | 3.6 | 3.6 | 3.6 | . 0 | 1.1 | . 0 |
| 390.0 | 5.8 | 5.5 | 5.7 | . 0 | 1.2 | 1.2 |
| 400.0 | 8.0 | 7.9 | 7.9 | 15.9 | 17.8 | 16.9 |
| 410.0 | 10.4 | 10.4 | 10.4 | 15.9 | 13.3 | 12.7 |
| 420.0 | 13.0 | 12.8 | 13.1 | 13.6 | 13.7 | 13.5 |
| 430.0 | 16.0 | 15.4 | 15.9 | 15.7 | 15.9 | 15.5 |
| 440.0 | 18.6 | 18.0 | 18.4 | 18.4 | 18.3 | 18.1 |
| 450.0 | 20.8 | 20.5 | 20.8 | 21.2 | 21.5 | 22.0 |
| 460.0 | 22.6 | 22.4 | 22.5 | 22.7 | 23.3 | 23.3 |
| 470.0 | 23.8 | 23.4 | 23.6 | 24.3 | 24.0 | 24.1 |
| 480.0 | 24.2 | 24.0 | 23.9 | 24.7 | 24.7 | 24.9 |
| 490.0 | 24.1 | 23.8 | 24.0 | 24.6 | 24.7 | 24.8 |
| 500.0 | 23.2 | 23.0 | 23.0 | 24.1 | 24.6 | 24.1 |
| 510.0 | 22.7 | 22.5 | 22.6 | 23.9 | 24.2 | 24.3 |
| 520.0 | 23.6 | 23.5 | 23.7 | 24.6 | 24.9 | 24.9 |
| 530.0 | 27.8 | 27.2 | 27.8 | 29.4 | 29.2 | 29.6 |
| 540.0 | 35.9 | 35.5 | 36.0 | 37.8 | 38.2 | 38.1 |
| 550.0 | 46.1 | 45.6 | 46.1 | 49.4 | 49.4 | 48.9 |
| 560.0 | 58.8 | 57.9 | 58.6 | 61.2 | 61.0 | 60.6 |
| 570.0 | 66.8 | 66.4 | 66.8 | 66.9 | 65.9 | 66.4 |
| 580.0 | 69.4 | 69.4 | 69.3 | 68.0 | 66.8 | 68.3 |
| 590.0 | 64.9 | 65.2 | 64.7 | 66.8 | 66.8 | 67.1 |
| 600.0 | $57 \cdot 3$ | 58.6 | 56.7 | 58.0 | 59.0 | 58.5 |
| 610.0 | 47.1 | 48.0 | 47.0 | 47.5 | 47.0 | 48.0 |
| 620.0 | 36.7 | 37.8 | 36.8 | 37.8 | 37.6 | 37.4 |
| 630.0 | 28.5 | 29.5 | 28.4 | 28.0 | 28.9 | 28.3 |
| 640.0 | 21.1 | 21.9 | 21.1 | 21.5 | 21.0 | 20.7 |
| 650.0 | 15.4 | 15.7 | 15.6 | 14.4 | 14.2 | 14.0 |
| 660.0 | 11.3 | 11.4 | 11.3 | 9.4 | 9.6 | 9.5 |
| 670.0 | 8.4 | 8.6 | 8.5 | 6.2 | $5 \cdot 6$ | 5.6 |
| 680.0 | 6.0 | 6.1 | 6.0 | 4.8 | 4.4 | 4.5 |
| 690.0 | 4.7 | $4 \cdot 8$ | 5.2 | 4.8 | 2.5 | 1.9 |
| 700.0 | 3.5 | 3.5 | 3.9 | 2.0 | 1.4 | 1.4 |
| 710.0 | 2.8 | 2.9 | 3.3 | 1.4 | . 7 | 1.4 |
| 720.0 | 2.2 | 2.2 | 2.7 | . 7 | - 8 | 1.6 |
| 730.0 | 4.6 | 4.4 | 5.1 | 9.5 | $7 \cdot 8$ | 7.8 |
| 740.0 | 1.9 | 2.2 | 2.1 | 2.6 | 2.8 | 2.8 |
| 750.0 | 1.9 | 1.7 | 2.5 | 1.6 | 1.7 | 1.7 |
| 760.0 | 1.9 | 2.0 | 2.0 | - 0 | - 0 | . 0 |

## MERCURY LINES

| 405.0 | 22.4 | 21.5 | 21.5 | 5.5 | 5.0 | 5.6 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 58.2 | 58.7 | 57.4 | 54.6 | 54.7 | 55.0 |
| 546.0 | 25.8 | 25.7 | 25.7 | 26.8 | 27.7 | 28.7 |
| 578.0 | 8.4 | 8.7 | 8.9 | 13.8 | 16.8 | 16.3 |



FIGURE 4.48 AVERAGE RELATIVE SPECTRAL IRRADIANCE ( 25 CM SECTION) MEASUREMENTS NORMALIZED TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8802

| WAVELENGTH | NBS |  |  | LABORATORY 5 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 |
| 380.0 | 3.8 | 3.6 | 3.8 | . 0 | 1.0 | . 0 |
| 390.0 | 5.9 | 5.7 | 5.9 | 1.1 | 1.1 | 1.1 |
| 400.0 | 7.9 | 7.9 | 7.8 | 17.6 | 21.8 | 16.3 |
| 410.0 | 10.4 | 10.3 | 10.3 | 16.4 | 13.6 | 12.6 |
| 420.0 | 13.0 | 12.8 | 13.0 | 13.9 | 13.8 | 13.4 |
| 430.0 | 16.1 | 15.6 | 16.0 | 15.3 | 16.0 | 15.5 |
| 440.0 | 18.6 | 18.3 | 18.5 | 18.3 | 18.1 | 18.4 |
| 450.0 | 20.7 | 20.7 | 20.8 | 21.5 | 21.7 | 21.6 |
| 460.0 | 22.4 | 22.4 | 22.6 | 23.0 | 23.0 | 23.2 |
| 470.0 | 23.6 | 23.6 | 23.6 | 24.4 | 23.9 | 24.4 |
| 480.0 | 23.9 | 24.1 | 23.9 | 24.9 | 24.6 | 24.9 |
| 490.0 | 23.9 | 23.9 | 24.0 | 24.7 | 24.5 | 24.8 |
| 500.0 | 22.9 | 23.1 | 22.9 | 24.4 | 24.2 | 24.4 |
| 510.0 | 22.4 | 22.7 | 22.5 | 24.3 | 24.2 | 24.1 |
| 520.0 | 23.5 | 23.5 | 23.6 | 24.7 | 24.4 | 24.9 |
| 530.0 | 27.6 | 27.5 | 27.7 | 29.7 | 29.3 | 29.5 |
| 540.0 | 35.5 | 35.1 | 35.8 | 38.4 | 37.6 | 38.1 |
| 550.0 | 45.6 | 45.1 | 45.9 | 49.8 | 49.0 | 49.1 |
| 560.0 | 58.2 | 58.1 | 58.4 | 61.4 | 60.2 | 61.5 |
| 570.0 | 66.0 | 66.4 | 66.6 | 66.1 | 66.4 | 66.7 |
| 580.0 | 68.4 | 69.4 | 69.2 | 66.9 | 67.6 | 67.7 |
| 590.0 | 64.0 | 65.8 | 64.6 | 66.7 | 66.2 | 67.0 |
| 600.0 | 56.0 | $57 \cdot 3$ | 56.5 | 58.7 | 59.1 | 59.2 |
| 610.0 | 46.3 | 47.4 | 46.7 | 47.0 | 46.8 | 47.4 |
| 620.0 | 36.2 | 37.6 | 36.6 | 36.7 | 37.6 | 38.1 |
| 630.0 | 28.3 | 28.9 | 28.1 | 28.0 | 27.9 | 27.8 |
| 640.0 | 20.8 | 21.2 | 21.2 | 20.6 | 21.3 | 21.4 |
| 650.0 | 15.1 | 15.3 | 15.7 | 14.2 | 14.2 | 14.7 |
| 660.0 | 11.0 | 11.5 | 11.1 | 9.0 | 9.3 | 9.1 |
| 670.0 | $8 \cdot 3$ | 8.5 | 8.4 | 5.3 | 5.2 | 5.4 |
| 680.0 | 6.0 | 6.0 | 6.3 | 3.8 | 4.1 | 4.3 |
| 690.0 | 4.7 | 5.0 | 5.1 | 1.8 | $4 \cdot 1$ | 3.1 |
| 700.0 | 3.4 | 3.7 | 3.8 | 1.4 | 2.7 | 1.4 |
| 710.0 | 2.8 | 3.1 | 3.3 | - 7 | 1.4 | 1.4 |
| 720.0 | 2.3 | 2.5 | 2.7 | . 7 | - 7 | 1.5 |
| 730.0 | 4.7 | 4.7 | 5.0 | 6.4 | $8 \cdot 3$ | 8.6 |
| 740.0 | 1.7 | 2.2 | 2.1 | 2.7 | 2.6 | 2.7 |
| 750.0 | 1.7 | $2 \cdot 1$ | 2.5 | 1.7 | 1.6 | 1.7 |
| 760.0 | 2.0 | $2 \cdot 0$ | 3.0 | . 0 | . 0 | . 0 |

MERCURY LINES

| 405.0 | 24.2 | 22.0 | 22.2 | 5.5 | 5.3 | 4.8 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 63.3 | 59.0 | 57.5 | 58.3 | 54.7 | 54.6 |
| 546.0 | 26.7 | 25.9 | 25.6 | 26.9 | 26.6 | 27.7 |
| 578.0 | 10.1 | 8.6 | 8.9 | 17.2 | 14.2 | 16.0 |



FIGURE 4.49 gVERage relative spectral Irraoiance ( 25 cm section) MEASUREMENTS NORMALIZEO TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8805

| WAVELENGTH | NBS |  |  | LABORATORY 2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 |
| 380.0 | 3.5 | 3.6 | 3.7 | . 0 | . 0 | . 0 |
| 390.0 | 5.6 | 5.7 | 5.7 | 5.4 | 4.8 | 5.3 |
| 400.0 | 7.8 | 7.7 | 7.7 | 7.6 | 7.3 | 7.6 |
| 410.0 | 10.3 | 10.1 | 10.2 | 10.2 | 10.0 | 10.2 |
| 420.0 | 12.9 | 12.8 | 13.0 | 13.0 | 12.9 | 12.9 |
| 430.0 | 15.8 | 15.8 | 16.0 | 16.1 | 16.1 | 16.1 |
| 440.0 | 18.4 | 18.4 | 18.6 | 18.8 | 18.8 | 18.9 |
| 450.0 | 20.7 | 20.6 | 20.9 | 20.9 | 20.9 | 21.0 |
| 460.0 | 22.5 | 22.5 | 22.6 | 22.8 | 22.8 | 22.8 |
| 470.0 | 23.6 | 23.6 | 23.7 | 23.9 | 24.0 | 23.9 |
| 480.0 | 24.1 | 24.1 | 24.0 | 24.4 | 24.4 | 24.4 |
| 490.0 | 24.1 | 24.0 | 24.2 | 24.3 | 24.4 | 24.3 |
| 500.0 | 23.2 | 23.1 | 23.0 | 23.5 | 23.5 | 23.5 |
| 510.0 | 22.7 | 22.6 | 22.7 | 23.1 | 23.1 | 23.1 |
| 520.0 | 23.5 | 23.6 | 23.8 | 24.2 | 24.2 | 24.3 |
| 530.0 | 27.6 | 27.3 | 27.9 | 28.4 | 28.5 | 28.4 |
| 540.0 | 35.7 | 35.3 | 35.9 | 36.9 | 37.0 | 37.0 |
| 550.0 | 45.8 | 45.5 | 46.1 | $47 \cdot 3$ | 47.5 | 47.4 |
| 560.0 | 58.3 | 58.4 | 58.8 | 59.4 | 59.8 | 59.6 |
| 570.0 | 66.5 | 66.4 | 66.8 | 67.7 | 68.0 | 67.7 |
| 580.0 | 69.2 | 69.1 | 69.2 | 69.7 | 70.2 | 69.8 |
| 590.0 | 64.9 | $64 \cdot 8$ | 64.9 | 66.0 | 66.3 | 66.0 |
| 600.0 | 58.0 | 57.0 | 56.9 | 57.9 | $58 \cdot 3$ | 58.2 |
| 610.0 | 47.5 | $48 \cdot 3$ | 46.7 | 47.8 | 48.1 | 48.0 |
| 620.0 | 37.1 | 37.2 | 36.7 | 37.7 | 37.9 | 37.8 |
| 630.0 | 29.6 | 29.2 | 28.3 | 28.7 | 28.9 | 28.9 |
| 640.0 | 21.4 | 21.1 | 21.3 | 21.4 | 21.5 | 21.5 |
| 650.0 | 15.7 | 15.7 | 15.2 | 15.8 | 15.7 | 15.8 |
| 660.0 | 11.2 | 11.2 | 11.2 | 11.5 | 11.4 | 11.5 |
| 670.0 | 8.5 | 8.6 | 8.3 | 8.3 | 8.2 | 8.3 |
| 680.0 | 6.1 | 6.1 | 6.2 | 6.0 | 5.8 | 6.0 |
| 690.0 | 4.6 | 5.0 | $4 \cdot 9$ | 4.6 | $4 \cdot 3$ | 4.5 |
| 700.0 | 3.4 | 3.7 | 2.2 | 3.3 | 3.0 | 3.3 |
| 710.0 | 2.9 | 3.2 | 3.4 | 2.6 | 2.1 | 2.5 |
| 720.0 | $2 \cdot 3$ | 2.5 | 2.8 | 2.0 | 1.5 | 1.8 |
| 730.0 | 4.5 | 4.7 | 5.2 | 1.6 | 1.0 | 1.4 |
| 740.0 | 1.6 | 2.2 | 2.2 | 1.3 | - 8 | 1.2 |
| 750.0 | 1.6 | 2.1 | 2.6 | - 9 | . 1 | . 6 |
| 760.0 | 1.5 | 2.6 | 2.6 | . 0 | . 0 | . 0 |

MERCURY LINES

| 405.0 | 22.3 | 22.0 | 21.8 | 22.0 | 22.1 | 21.7 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 59.3 | 58.2 | 57.8 | 57.7 | 59.4 | 57.2 |
| 546.0 | 25.4 | 25.5 | 25.5 | 25.2 | 25.2 | 25.5 |
| 578.0 | 8.8 | 8.8 | 8.7 | 10.2 | 10.1 | 10.1 |



FIGURE 4.50 AVERAGE RELATIVE SPECTRAL IRRADIANCE ( 25 CM SECTION) MEASUREMENTS NORMALIZED TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NRS8806

|  | NBS |  |  | LABORATORY 2 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 |
| 380.0 | 3.7 | 3.7 | 3.8 | . 0 | . 0 | . 0 |
| 390.0 | 5.9 | 5.9 | 5.9 | 5.8 | 5.7 | 5.6 |
| 400.0 | 8.3 | 11.1 | 7.9 | 8.0 | 7.9 | 7.8 |
| 410.0 | 10.9 | 13.2 | $10 \cdot 4$ | 10.4 | 10.5 | 10.4 |
| 420.0 | 13.4 | 13.2 | 13.2 | 13.2 | 13.3 | 13.2 |
| 430.0 | 16.1 | 11.7 | 16.2 | 16.3 | 16.4 | 16.3 |
| 440.0 | 18.7 | 14.5 | 18.8 | 19.1 | 19.1 | 19.2 |
| 450.0 | 21.0 | 20.9 | 21.1 | 21.2 | 21.3 | 21.3 |
| 460.0 | 22.8 | 22.8 | 22.8 | 23.0 | 23.1 | 23.1 |
| 470.0 | 23.9 | 23.9 | 23.8 | 24.2 | 24.3 | 24.3 |
| 480.0 | 24.5 | 24.4 | 24.2 | 24.6 | 24.7 | 24.7 |
| 490.0 | 24.4 | 24.2 | 24.3 | 24.5 | 24.6 | 24.5 |
| 500.0 | 23.5 | 23.3 | 23.3 | 23.6 | 23.6 | 23.7 |
| 510.0 | 22.9 | 22.8 | 22.6 | 23.2 | 23.2 | 23.2 |
| 520.0 | 23.7 | 23.7 | 23.7 | 24.2 | 24.2 | 24.2 |
| 530.0 | 27.5 | 27.4 | 27.7 | 28.2 | 28.2 | 28.2 |
| 540.0 | 35.1 | 35.1 | 35.5 | 36.4 | 36.5 | 36.6 |
| 550.0 | 45.1 | 45.0 | 45.4 | 46.6 | 46.7 | 46.8 |
| 560.0 | 57.6 | 57.6 | 57.9 | 58.5 | 58.7 | 58.8 |
| 570.0 | 65.9 | 65.9 | 65.7 | 66.9 | 66.8 | 67.0 |
| 580.0 | 68.8 | 68.7 | 68.3 | 68.9 | 69.1 | 69.3 |
| 590.0 | $64 \cdot 6$ | 64.4 | 64.2 | 65.3 | 65.5 | 65.7 |
| 600.0 | 57.8 | 56.6 | 56.5 | 57.4 | 57.6 | 57.7 |
| 610.0 | 47.6 | 47.4 | 46.4 | 47.6 | 47.7 | 47.6 |
| 620.0 | 37.2 | 37.2 | 36.6 | 37.6 | 37.7 | 37.6 |
| 630.0 | 29.4 | 29.0 | 28.3 | 28.7 | 28.8 | 28.8 |
| 640.0 | 21.4 | 21.6 | 21.0 | 21.5 | 21.5 | 21.5 |
| 650.0 | 15.6 | 15.8 | 15.5 | 15.8 | 15.9 | 15.8 |
| 660.0 | 11.4 | 11.2 | 11.4 | 11.5 | 11.6 | 11.5 |
| 670.0 | 8.6 | 8.7 | 8.7 | 8.4 | 8.5 | 8.4 |
| 680.0 | 6.0 | 6.2 | 6.2 | 6.1 | 6.2 | 6.0 |
| 690.0 | 4.7 | 4.9 | 4.9 | 4.7 | 4.7 | 4.6 |
| 700.0 | 3.5 | 2.1 | 3.9 | 3.4 | 3.4 | 3.3 |
| 710.0 | 2.8 | 3.1 | 3.3 | 2.6 | 2.7 | 2.6 |
| 720.0 | 2.2 | 2.7 | 3.0 | 2.1 | 2.1 | 1.9 |
| 730.0 | 4.4 | $5 \cdot 3$ | 5.4 | 1.7 | 1.5 | 1.5 |
| 740.0 | 1.6 | 2.1 | 2.5 | 1.4 | 1.7 | 1.2 |
| 750.0 | 1.6 | 2.1 | 2.5 | 1.2 | . 5 | . 8 |
| 760.0 | 1.5 | 2.5 | 3.0 | . 0 | . 0 | . 0 |

MERCURY LINES

| 405.0 | 21.7 | 19.5 | 21.9 | 22.0 | 22.2 | 22.1 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 58.7 | 64.2 | 57.8 | 58.9 | 57.1 | 57.7 |
| 546.0 | 25.9 | 25.6 | 25.3 | 25.2 | 25.5 | 25.4 |
| 578.0 | 8.7 | 8.7 | 8.8 | 10.1 | 9.9 | 9.9 |



FIGURE 4.51 AVERAGE RELATIVE SPECTRAL IRRADIRNCE ( 25 CM SECTION) MEASUREMENTS NORMALIZED TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8809

|  | NBS |  |  | LABORATORY 4 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 |
| 380.0 | 3.6 | 3.6 | 3.9 | 4.2 | 3.8 | 4.0 |
| 390.0 | $5 \cdot 8$ | 4.2 | 5.8 | 6.2 | 6.3 | 5.5 |
| 400.0 | 8.1 | 6.7 | 7.9 | 8.5 | 8.0 | 8.2 |
| 410.0 | 10.5 | 8.9 | 10.3 | 11.5 | 10.6 | 10.2 |
| 420.0 | 13.1 | 10.9 | 13.0 | 13.6 | 13.3 | 13.1 |
| 430.0 | 15.9 | 12.9 | 16.0 | 16.5 | 15.7 | 16.1 |
| 440.0 | 18.4 | 19.7 | 18.5 | 19.2 | 18.3 | 18.6 |
| 450.0 | 20.8 | 20.8 | 20.8 | 21.4 | 20.3 | 20.4 |
| 460.0 | 22.5 | 22.8 | 22.6 | 22.6 | 22.7 | 21.1 |
| 470.0 | 23.6 | 21.9 | 23.6 | 24.3 | 22.8 | 23.8 |
| 480.0 | 24.1 | 22.3 | 24.1 | 25.0 | 25.5 | 24.0 |
| 490.0 | 24.0 | 22.4 | 24.1 | 24.2 | 23.9 | 23.3 |
| 500.0 | 23.2 | 22.4 | 23.1 | 24.2 | 23.7 | 23.4 |
| 510.0 | 22.7 | 21.9 | 22.6 | 23.2 | 23.0 | 22.9 |
| 520.0 | 23.6 | 22.1 | 23.7 | 24.5 | 23.7 | 24.0 |
| 530.0 | 27.7 | 24.4 | 27.9 | 29.1 | 28.7 | 28.4 |
| 540.0 | 35.4 | 30.2 | 35.9 | 37.4 | 36.9 | 36.7 |
| 550.0 | 45.5 | 41.0 | 45.9 | 45.5 | 47.9 | 47.9 |
| 560.0 | 58.3 | 57.7 | 58.5 | 57.0 | 58.5 | 59.1 |
| 570.0 | 66.3 | 61.1 | 66.4 | 64.6 | 66.5 | 66.9 |
| 580.0 | 69.1 | 65.0 | 68.8 | 76.5 | 76.1 | 74.8 |
| 590.0 | $65 \cdot 2$ | 69.5 | 64.4 | 63.1 | $64 \cdot 8$ | 65.5 |
| 600.0 | 57.4 | 61.9 | 56.6 | 55.7 | 56.9 | 57.4 |
| 610.0 | 47.5 | 53.5 | 46.6 | 45.7 | 46.8 | 47.2 |
| 620.0 | 36.9 | 43.6 | 36.6 | 37.2 | 36.9 | 37.4 |
| 630.0 | 29.2 | 34.6 | 28.2 | 28.5 | 28.3 | 28.6 |
| 640.0 | 21.2 | 26.6 | 21.2 | 21.6 | 21.6 | 21.5 |
| 650.0 | 15.6 | 20.5 | 15.4 | 16.3 | 15.9 | 15.9 |
| 660.0 | 11.0 | 14.2 | 11.4 | 12.0 | 11.7 | 11.8 |
| 670.0 | 8.3 | 10.0 | 8.6 | 8.8 | 8.6 | 8.7 |
| 680.0 | 6.2 | 7.3 | 6.1 | 6.5 | 6.4 | 6.4 |
| 690.0 | 4.8 | $5 \cdot 6$ | 5.1 | 5.1 | $5 \cdot 1$ | 5.2 |
| 700.0 | 3.6 | 4.3 | 2.2 | 3.8 | 3.7 | 3.7 |
| 710.0 | 2.9 | 3.6 | 3.4 | 3.1 | 2.9 | 3.0 |
| 720.0 | 2.0 | 3.1 | 2.8 | 2.4 | 2.2 | 2.3 |
| 730.0 | 4.7 | 3.5 | 4.9 | 1.9 | 1.9 | 2.0 |
| 740.0 | 1.6 | 3.1 | 2.5 | 1.6 | 1.5 | 1.7 |
| 750.0 | 1.9 | $2 \cdot 4$ | 2.6 | 1.4 | 1.4 | 1.5 |
| 760.0 | 1.5 | 2.4 | 3.1 | 1.2 | 1.0 | 1.3 |

MERCURY LINES

| 405.0 | 22.5 | 14.8 | 22.1 | 20.8 | 20.8 | 19.5 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 59.1 | 54.7 | 58.3 | 52.2 | 52.9 | 54.1 |
| 546.0 | 25.9 | 21.6 | 25.6 | 24.8 | 25.7 | 25.5 |
| 578.0 | 8.9 | 6.6 | 8.9 | 7.2 | 6.9 | 7.2 |



FIGURE 4.52 AVERAGE RELATIVE SPECTRAL IRRAOIANCE ( 25 CM SECTION) MEASUREMENTS NORMALIZEO TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8810

| WAVELENGTH | NBS |  |  | LABORATORY 4 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN |
|  | 3.7 | 3.4 | 3.9 | 4.0 | 3.6 | 4.2 |
| 390.0 | $5 \cdot 7$ | 4.0 | 5.6 | 6.5 | 5.9 | 6.2 |
| 400.0 | 7.9 | 9.5 | 7.8 | 8.2 | $8 \cdot 2$ | 7.9 |
| 410.0 | 10.4 | 12.3 | 10.3 | 10.4 | 11.2 | 10.5 |
| 420.0 | 12.9 | 13.3 | 13.0 | 13.2 | 13.0 | 12.8 |
| 430.0 | 15.8 | 13.2 | 15.8 | 15.8 | 15.9 | 15.7 |
| 440.0 | 18.4 | 18.3 | 18.3 | 18.4 | 18.6 | 18.5 |
| 450.0 | 20.5 | 20.5 | 20.6 | 20.6 | 20.7 | 20.0 |
| 460.0 | 22.3 | 21.9 | 20.3 | 23.2 | 22.0 | 22.3 |
| 470.0 | 23.6 | 21.4 | 23.5 | 23.4 | 24.5 | 23.4 |
| 480.0 | 23.9 | 21.9 | 23.9 | 24.7 | 24.8 | 24.0 |
| 490.0 | 23.9 | 22.0 | 23.9 | 22.5 | 23.9 | 23.5 |
| 500.0 | 23.0 | 22.0 | 23.0 | 23.7 | 22.8 | 23.1 |
| 510.0 | 22.7 | 21.7 | 22.5 | 22.9 | 22.6 | 22.0 |
| 520.0 | 23.6 | 21.9 | 23.5 | 23.7 | 24.6 | 24.1 |
| 530.0 | 27.6 | 24.1 | 27.8 | 27.5 | 28.2 | 28.4 |
| 540.0 | 35.7 | $30 \cdot 1$ | 35.9 | 35.9 | 35.6 | 36.4 |
| 550.0 | 45.9 | 40.7 | 46.1 | 47.1 | $46 \cdot 3$ | 47.8 |
| 560.0 | 58.6 | 57.1 | 58.8 | 58.2 | 58.4 | 58.9 |
| 570.0 | 66.6 | 61.1 | 66.9 | 66.2 | 66.1 | 66.8 |
| 580.0 | 69.4 | 65.2 | 69.5 | 78.0 | 74.4 | 76.5 |
| 590.0 | 65.3 | $69 \cdot 3$ | 65.2 | 64.0 | 64.8 | 64.9 |
| 600.0 | 57.6 | 61.1 | 57.0 | 56.6 | 56.7 | 57.0 |
| 610.0 | 47.9 | 53.1 | 47.0 | 46.7 | 46.7 | 47.1 |
| 620.0 | 37.3 | 42.9 | 37.0 | 36.7 | 36.9 | 37.3 |
| 630.0 | 29.1 | 34.5 | 28.6 | 28.0 | 28.4 | 28.5 |
| 640.0 | 21.6 | 27.1 | 21.2 | 21.5 | 21.4 | 21.5 |
| 650.0 | 15.7 | 21.0 | 15.6 | 15.9 | 15.9 | 16.1 |
| 660.0 | 11.3 | 14.4 | 11.3 | 11.9 | 11.9 | 11.8 |
| 670.0 | 8.7 | 10.4 | 8.5 | 8.8 | 8.7 | 8.9 |
| 680.0 | $6 \cdot 3$ | 7.7 | 6.1 | 6.5 | 6.6 | 6.5 |
| 690.0 | 4.9 | $5 \cdot 9$ | 5.2 | 5.2 | $5 \cdot 2$ | 5.1 |
| 700.0 | 3.5 | 4.6 | 3.9 | 3.7 | 3.7 | 3.8 |
| 710.0 | 2.8 | 3.8 | 3.4 | 3.0 | 3.0 | 3.1 |
| 720.0 | 2.4 | 3.3 | 2.7 | 2.4 | $2 \cdot 3$ | 2.4 |
| 730.0 | 4.5 | 3.4 | 5.1 | 1.9 | 2.0 | 1.8 |
| 740.0 | 1.6 | 3.3 | 2.2 | 1.5 | 1.6 | 1.5 |
| 750.0 | 1.9 | 2.7 | 2.5 | 1.3 | 1.3 | 1.4 |
| 760.0 | 1.5 | 2.8 | 3.0 | 1.1 | 1.0 | 1.0 |

MERCURY LINES

| 405.0 | 22.1 | 13.4 | 22.1 | 21.2 | 21.5 | 20.7 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 56.9 | 52.5 | 56.4 | 53.2 | 54.3 | 53.0 |
| 546.0 | 26.2 | 24.3 | 26.1 | 27.6 | 27.8 | 26.4 |
| 578.0 | 9.0 | 6.1 | 9.0 | 7.4 | 7.0 | 7.3 |


figure 4.53 average relative spectral irradiance ( 25 cm section) MEASUREMENTS NORMALIZED TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8905

|  | NBS |  |  | LABORATORY 7 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 |
| 380.0 | 4.9 | 4.8 | 4.9 | 3.2 | 14.7 | 2.5 |
| 390.0 | 8.4 | 8.2 | 8.1 | 4.1 | 5.0 | 4.0 |
| 400.0 | 12.8 | 12.6 | 12.5 | 6.2 | 7.2 | 6.3 |
| 410.0 | 17.6 | 17.3 | 17.2 | 9.3 | 10.3 | 9.3 |
| 420.0 | 22.4 | 22.1 | 22.1 | 13.8 | 14.7 | 13.6 |
| 430.0 | 27.7 | 27.4 | 27.3 | 18.8 | 19.0 | 17.2 |
| 440.0 | 32.2 | 31.9 | 31.7 | 23.6 | 24.0 | 22.6 |
| 450.0 | 36.0 | 35.6 | 35.8 | 27.4 | 26.5 | 26.0 |
| 460.0 | 38.4 | 38.0 | 38.1 | 28.3 | 30.0 | 29.2 |
| 470.0 | 39.5 | 39.1 | 39.1 | 32.7 | 31.9 | 31.0 |
| 480.0 | 39.3 | 39.1 | 39.0 | 32.8 | 33.6 | 32.6 |
| 490.0 | 38.2 | 37.7 | 37.9 | 34.0 | 32.6 | 33.1 |
| 500.0 | 35.7 | 35.5 | 35.4 | 31.9 | 31.8 | 32.3 |
| 510.0 | 33.3 | 33.3 | 33.0 | 30.7 | 29.9 | 30.8 |
| 520.0 | 31.6 | 31.6 | 31.5 | 29.1 | 28.5 | 29.5 |
| 530.0 | 31.8 | 31.5 | 31.6 | 29.2 | 29.0 | 29.7 |
| 540.0 | 34.4 | 34.2 | 34.3 | 31.2 | 31.6 | 32.5 |
| 550.0 | 38.6 | 38.2 | 38.3 | 35.1 | 35.6 | 36.3 |
| 560.0 | 44.4 | 44.0 | 44.2 | 40.9 | 41.4 | 42.4 |
| 570.0 | 47.9 | 47.7 | 47.8 | 45.6 | 46.2 | 46.5 |
| 580.0 | 48.3 | 48.3 | 48.2 | 46.7 | 46.7 | 46.8 |
| 590.0 | 44.6 | 44.7 | 44.7 | 42.9 | 43.0 | 43.1 |
| 600.0 | 39.1 | 39.2 | 39.1 | 37.1 | 30.9 | 38.7 |
| 610.0 | 32.2 | 32.5 | 32.4 | 32.3 | 31.6 | 33.3 |
| 620.0 | 25.3 | 26.0 | 25.4 | 25.7 | 26.0 | 25.7 |
| 630.0 | 19.8 | 21.4 | 20.2 | 21.4 | 21.1 | 21.2 |
| 640.0 | 14.8 | 15.3 | 15.2 | 17.3 | 16.8 | 17.0 |
| 650.0 | 10.9 | 11.2 | 11.3 | 13.9 | 14.1 | 14.1 |
| 660.0 | 8.2 | 8.2 | 8.4 | 11.9 | 11.7 | 12.0 |
| 670.0 | 6.3 | 6.5 | 6.5 | 10.7 | 10.2 | 10.6 |
| 680.0 | 4.5 | 4.7 | 4.8 | 9.8 | 9.1 | 9.5 |
| 690.0 | 3.6 | 4.0 | 3.9 | 10.2 | 9.5 | 10.1 |
| 700.0 | 2.7 | 3.1 | 2.9 | 10.1 | 9.7 | 10.3 |
| 710.0 | 2.4 | 2.5 | 2.8 | 12.3 | 11.3 | 12.1 |
| 720.0 | 1.9 | 2.1 | 2.1 | 14.3 | 12.8 | 14.6 |
| 730.0 | 3.9 | 4.4 | 4.9 | 17.1 | 16.0 | 17.9 |
| 740.0 | 1.5 | 2.1 | 2.1 | 20.7 | 20.4 | 22.0 |
| 750.0 | 1.8 | 2.0 | 2.4 | 25.6 | 23.5 | 24.6 |
| 760.0 | 1.4 | 1.9 | 2.9 | 28.3 | 26.9 | 27.7 |

MERCURY LINES

| 405.0 | 21.2 | 20.7 | 20.8 | 6.1 | 7.0 | 6.1 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 56.9 | 56.2 | 55.9 | 31.1 | 30.4 | 28.3 |
| 546.0 | 25.0 | 24.8 | 24.8 | 25.3 | 25.6 | 25.1 |
| 578.0 | 8.6 | 8.4 | 8.6 | 21.2 | 22.0 | 21.4 |



FIGURE 4.54 AVERAGE RELATIVE SPECTRAL IRRADIANCE ( 25 CM SECTION) MEASUREMENTS NORMALIZED TO AREA

| WAVELENGTH | NBS |  |  | LABORATORY 1 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RIJN 6 |
| 380.0 | 4.9 | 4.9 | 5.1 | . 0 | . 0 | . 0 |
| 390.0 | 8.5 | 8.2 | 8.4 | 8.2 | 8.9 | 8.7 |
| 400.0 | 13.1 | 12.9 | 12.9 | 12.0 | 12.8 | 12.9 |
| 410.0 | 17.8 | 17.5 | 17.6 | 16.9 | 18.0 | 18.0 |
| 420.0 | 22.6 | 22.2 | 22.6 | 22.0 | 23.2 | 23.2 |
| 430.0 | 27.8 | 27.1 | 27.7 | 27.3 | 28.6 | 28.6 |
| 440.0 | 32.4 | 31.7 | 32.2 | 32.1 | 33.5 | 33.5 |
| 450.0 | 36.3 | 35.8 | 36.4 | 35.9 | 37.2 | 37.1 |
| 460.0 | 38.6 | 38.4 | 38.8 | 38.6 | 39.7 | 39.6 |
| 470.0 | 39.9 | 39.5 | 39.7 | 39.7 | 40.7 | 40.5 |
| 480.0 | 39.5 | 39.5 | 39.6 | 39.7 | 40.2 | 40.1 |
| 490.0 | $38 \cdot 3$ | 38.1 | 38.5 | 38.6 | $38 \cdot 8$ | 38.8 |
| 500.0 | 36.0 | 35.8 | 36.0 | 36.5 | 36.6 | 36.5 |
| 510.0 | 33.5 | 33.4 | 33.7 | 34.1 | 34.0 | 34.0 |
| 520.0 | 31.8 | 31.6 | 31.7 | 32.4 | 32.3 | 32.2 |
| 530.0 | 31.9 | 31.8 | 31.9 | 32.7 | 32.5 | 32.4 |
| 540.0 | 34.5 | 34.4 | 34.6 | 35.0 | 34.7 | 34.7 |
| 550.0 | 38.7 | 38.4 | 38.7 | 39.4 | 39.0 | 39.0 |
| 560.0 | 44.4 | 44.3 | 44.7 | 45.8 | 45.4 | 45.4 |
| 570.0 | 47.9 | 47.8 | 48.3 | 49.4 | 48.6 | 48.7 |
| 580.0 | 48.3 | 48.4 | 48.6 | 49.7 | 48.6 | 48.9 |
| 590.0 | 44.7 | $45 \cdot 1$ | 44.8 | 46.8 | $45 \cdot 6$ | 45.8 |
| 600.0 | 38.9 | 39.3 | 38.6 | 40.7 | 39.5 | 39.4 |
| 610.0 | 32.3 | 33.2 | 32.4 | 33.7 | 32.6 | 32.6 |
| 620.0 | 25.4 | 25.9 | 25.7 | 27.3 | 26.1 | 26.1 |
| 630.0 | 19.9 | 20.7 | 20.1 | 20.8 | 19.9 | 19.9 |
| 640.0 | 14.8 | 15.3 | 15.2 | 15.5 | 14.7 | 14.6 |
| 650.0 | 11.2 | 11.4 | 11.3 | 11.9 | 11.2 | 11.1 |
| 660.0 | 8.3 | 8.2 | 8.4 | 9.0 | 8.4 | 8.2 |
| 670.0 | 6.3 | 6.5 | 6.6 | 6.7 | $6 \cdot 3$ | 6.2 |
| 680.0 | 4.4 | 4.8 | 5.0 | 5.3 | 4.8 | 4.8 |
| 690.0 | 3.8 | 4.0 | 4.2 | 4.2 | 3.7 | 3.8 |
| 700.0 | 2.9 | 3.1 | 3.3 | 3.4 | $2 \cdot 9$ | 2.9 |
| 710.0 | 2.5 | 2.7 | 2.9 | 2.7 | $2 \cdot 3$ | 2.4 |
| 720.0 | 2.0 | 2.2 | 2.5 | 2.2 | 1.8 | 1.9 |
| 730.0 | 4.1 | 4.4 | 4.8 | - 0 | . 0 | . 0 |
| 740.0 | 1.6 | 1.8 | 2.5 | . 0 | - 0 | . 0 |
| 750.0 | 1.9 | 2.1 | 2.5 | . 0 | . 0 | . 0 |
| 760.0 | 1.5 | 2.1 | 3.1 | . 0 | . 0 | . 0 |

## MERCURY LINES

| 405.0 | 20.5 | 19.7 | 20.2 | 19.2 | 20.4 | 20.6 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 53.5 | 53.1 | 53.1 | 49.6 | 51.7 | 51.7 |
| 546.0 | 24.7 | 24.8 | 24.5 | 26.4 | 26.2 | 26.2 |
| 578.0 | 8.3 | 8.1 | 8.0 | 8.6 | 8.6 | 8.6 |



Figure 4.55 fVERage relative spectral IRRAOIANCE (25 cm SECtion) MEASUREMENTS NORMALIZEO TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8907

|  | NBS |  |  | LABORATORY 9 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 |
| 380.0 | 5.1 | 4.7 | 5.2 | 4.9 | 4.9 | 4.6 |
| 390.0 | 8.5 | 8.2 | 8.4 | 9.2 | 8.2 | 8.1 |
| 400.0 | 12.9 | 12.2 | 12.7 | 12.3 | 12.2 | 12.2 |
| 410.0 | 17.6 | 16.9 | 17.4 | 17.2 | 17.1 | 16.9 |
| 420.0 | 22.5 | 21.9 | 22.4 | 22.6 | 22.4 | 22.3 |
| 430.0 | 27.9 | 27.7 | 27.7 | 27.8 | 27.7 | 27.7 |
| 440.0 | 32.4 | 32.4 | 32.1 | 32.4 | 32.6 | 32.5 |
| 450.0 | 36.1 | 35.9 | 36.0 | 36.2 | 36.4 | 36.3 |
| 460.0 | 38.6 | 38.4 | 38.5 | 39.0 | 38.8 | 38.7 |
| 470.0 | 39.7 | 39.5 | 39.4 | 40.1 | 39.9 | 39.9 |
| 480.0 | 39.4 | 39.4 | 39.1 | 39.7 | 39.8 | 39.8 |
| 490.0 | 38.2 | 38.0 | 38.0 | 38.5 | 38.5 | 38.5 |
| 500.0 | 35.9 | 35.7 | 35.6 | 36.0 | 36.2 | 36.1 |
| 510.0 | 33.4 | 33.3 | 33.3 | 33.6 | 33.5 | 33.6 |
| 520.0 | 31.8 | 31.7 | 31.6 | 31.7 | 31.9 | 31.8 |
| 530.0 | 31.9 | 31.8 | 31.8 | 32.0 | 32.3 | 32.2 |
| 540.0 | 34.6 | $34 \cdot 3$ | 34.6 | 34.7 | 34.9 | 34.8 |
| 550.0 | 38.7 | 38.4 | 38.8 | 39.5 | 39.9 | 39.7 |
| 560.0 | 44.6 | 44.4 | 44.7 | 44.9 | 45.0 | 44.8 |
| 570.0 | 48.1 | 47.9 | 48.1 | 47.8 | 48.0 | 47.8 |
| 580.0 | 48.4 | 48.3 | 48.3 | 47.3 | 47.4 | 47.3 |
| 590.0 | 44.6 | 44.9 | 44.7 | 45.1 | 45.1 | 45.2 |
| 600.0 | 39.1 | 39.2 | 39.0 | 39.5 | 39.6 | 39.7 |
| 610.0 | 32.5 | 32.7 | 32.3 | 32.5 | 32.8 | 32.7 |
| 620.0 | 25.5 | 26.0 | 25.6 | 25.9 | 26.2 | 26.0 |
| 630.0 | 20.1 | 21.7 | 19.9 | 20.1 | 20.0 | 20.3 |
| 640.0 | 15.1 | 14.9 | 15.0 | 15.2 | 14.9 | 14.7 |
| 650.0 | 11.2 | 11.3 | 11.4 | 11.3 | 11.3 | 11.4 |
| 660.0 | 8.4 | 8.3 | 8.5 | 8.5 | 8.5 | 8.6 |
| 670.0 | 6.3 | 6.6 | 6.3 | 6.4 | $6 \cdot 3$ | 6.4 |
| 680.0 | 4.7 | 4.7 | 4.6 | 4.8 | $4 \cdot 8$ | 4.8 |
| 690.0 | 3.9 | 4.0 | 4.1 | 3.9 | 3.8 | 3.9 |
| 700.0 | 3.0 | 2.9 | 3.3 | 3.0 | 3.0 | 2.9 |
| 710.0 | $2 \cdot 3$ | 2.5 | 2.7 | 2.4 | 2.4 | 2.4 |
| 720.0 | 1.9 | 2.1 | 2.0 | 1.9 | 2.0 | 2.0 |
| 730.0 | 4.1 | 4.2 | 4.8 | 1.6 | 1.6 | 1.6 |
| 740.0 | 1.8 | 1.7 | 2.0 | 1.4 | 1.3 | 1.3 |
| 750.0 | 1.8 | 2.0 | 2.4 | 1.2 | 1.2 | 1.3 |
| 760.0 | 1.8 | 1.9 | 1.9 | 1.0 | 1.1 | 1.1 |
|  |  |  | MERCURY | LINES |  |  |
| 405.0 | 20.8 | 20.2 | 20.2 | 19.0 | 17.5 | 18.9 |
| 436.0 | 52.3 | 54.0 | 52.8 | 52.5 | $54 \cdot 3$ | 54.0 |
| 546.0 | 24.2 | 24.7 | 24.6 | 25.2 | 24.3 | 24.8 |
| 578.0 | 8.4 | 8.2 | 8.3 | 10.4 | 10.4 | 10.4 |



FIGURE 4.56 AVERAGE RELATIVE SPECTRAL IRRADIANCE ( 25 CM SECTION) MEASUREMENTS NORMALIZED TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8908

|  | NBS |  |  | LABORATORY 5 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WAVELENGTH | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 | RUN 6 |
| 380.0 | 4.9 | 4.8 | 5.0 | . 0 | 1.0 | . 0 |
| 390.0 | 8.4 | 8.2 | 8.2 | 1.1 | 1.2 | 2.3 |
| 400.0 | 12.6 | 12.4 | 12.5 | 28.9 | 30.0 | 24.5 |
| 410.0 | 17.2 | 17.0 | 17.2 | 26.0 | 22.4 | 20.7 |
| 420.0 | 21.9 | 21.9 | 22.2 | 23.2 | 23.4 | 23.1 |
| 430.0 | 27.3 | 27.2 | 27.5 | 26.7 | 26.9 | 26.6 |
| 440.0 | 31.9 | 31.8 | 31.8 | 30.7 | 30.9 | 31.0 |
| 450.0 | 35.9 | 35.4 | 35.7 | 35.4 | 36.6 | 36.7 |
| 460.0 | 38.2 | 38.1 | 38.2 | 37.3 | 38.5 | 38.8 |
| 470.0 | 39.4 | 39.3 | 39.1 | 38.7 | 39.4 | 39.7 |
| 480.0 | 39.3 | 39.1 | 38.9 | 38.6 | 39.7 | 40.0 |
| 490.0 | 38.1 | 38.0 | 37.9 | 37.4 | 38.4 | 38.7 |
| 500.0 | 35.8 | 35.7 | 35.4 | 35.8 | 36.6 | 36.9 |
| 510.0 | 33.5 | 33.2 | 33.0 | 33.3 | 34.7 | 34.4 |
| 520.0 | 31.6 | 31.6 | 31.4 | 32.1 | $32 \cdot 3$ | 32.9 |
| 530.0 | 31.9 | 31.7 | 31.6 | 32.3 | 32.8 | 33.5 |
| 540.0 | 34.5 | 34.4 | 34.4 | 36.0 | 36.8 | 37.1 |
| 550.0 | 38.6 | 38.6 | 38.6 | 40.8 | 41.6 | 42.0 |
| 560.0 | 44.5 | 44.5 | 44.6 | 45.8 | 46.8 | 47.1 |
| 570.0 | 48.3 | 48.3 | 48.2 | 48.0 | 48.9 | 49.0 |
| 580.0 | 48.8 | 49.0 | 48.5 | 47.4 | 48.3 | 48.2 |
| 590.0 | 44.9 | $45 \cdot 6$ | 44.9 | 45.9 | $46 \cdot 0$ | 46.1 |
| 600.0 | 39.7 | 40.0 | 39.2 | 40.0 | 40.9 | 41.0 |
| 610.0 | 33.1 | 32.5 | 32.4 | 32.0 | 33.1 | 33.2 |
| 620.0 | 25.7 | 26.0 | 25.5 | 24.5 | 25.5 | 26.8 |
| 630.0 | 19.9 | 20.1 | 19.9 | 18.5 | 18.9 | 19.5 |
| 640.0 | 15.1 | 15.1 | 15.0 | 14.0 | 14.1 | 14.8 |
| 650.0 | 11.2 | 11.3 | 11.5 | 9.2 | 8.0 | 9.5 |
| 660.0 | 8.4 | 8.4 | 8.5 | 6.4 | 4.8 | 5.7 |
| 670.0 | 6.4 | 6.6 | 6.5 | 4.3 | 2.5 | 4.5 |
| 680.0 | 4.6 | 4.8 | 4.8 | 1.6 | 1.1 | 1.7 |
| 690.0 | 3.6 | 3.9 | 3.9 | 1.2 | . 6 | 1.9 |
| 700.0 | 2.9 | 3.0 | 3.4 | . 7 | - 0 | . 7 |
| 710.0 | 2.3 | 2.6 | 2.8 | . 7 | . 0 | . 7 |
| 720.0 | 1.8 | 2.1 | 2.1 | 1.5 | . 0 | . 8 |
| 730.0 | 3.9 | 4.3 | 5.0 | 8.4 | 4.3 | 9.8 |
| 740.0 | 1.6 | 1.8 | 2.1 | 4.0 | 1.4 | 2.7 |
| 750.0 | 1.6 | 2.1 | 2.5 | 1.6 | - 0 | 1.7 |
| 760.0 | 1.5 | 2.0 | 3.0 | . 0 | - 0 | . 0 |

MERCURY LINES

| 405.0 | 21.1 | 20.3 | 20.5 | 23.6 | 22.2 | 2.6 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 54.7 | 54.2 | 53.4 | 50.9 | 52.0 | 53.5 |
| 546.0 | 25.0 | 24.9 | 24.9 | 24.5 | 24.8 | 25.6 |
| 578.0 | 8.4 | 8.3 | 8.4 | 10.7 | 12.7 | 14.1 |



FIGURE 4.57 AVERAGE RELATIVE SPECTRAL IRRADIANCE ( 25 CM SECTION) MEASUREMENTS NORMALIZED TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8909

| WAVELENGTH | NBS |  |  | LABORATORY 2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 |
| 380.0 | 4.8 | 5.1 | . 0 | . 0 | . 0 |
| 390.0 | 8.3 | 8.3 | 8.2 | 8.3 | 7.7 |
| 400.0 | 12.9 | 12.8 | 12.6 | 12.5 | 12.3 |
| 410.0 | 17.7 | 17.5 | 17.4 | 17.2 | 17.3 |
| 420.0 | 22.4 | 22.5 | 22.4 | 22.1 | 22.5 |
| 430.0 | 27.5 | 27.7 | 27.9 | 27.5 | 27.9 |
| 440.0 | 32.0 | 32.1 | 32.6 | 32.2 | 32.8 |
| 450.0 | 35.8 | 36.0 | 36.1 | 35.9 | 36.5 |
| 460.0 | 38.4 | 38.4 | 38.6 | 38.5 | 39.0 |
| 470.0 | 39.5 | 39.4 | 39.8 | 39.8 | 40.2 |
| 480.0 | 39.3 | 39.1 | 39.6 | 39.5 | 40.0 |
| 490.0 | 38.2 | 38.0 | 38.4 | 38.4 | 38.7 |
| 500.0 | 35.8 | 35.6 | 36.1 | 36.1 | 36.3 |
| 510.0 | 33.5 | 33.1 | 33.7 | 33.7 | 34.0 |
| 520.0 | 31.8 | 31.5 | 32.1 | 32.1 | 32.4 |
| 530.0 | 31.8 | 31.8 | 32.3 | 32.4 | 32.6 |
| 540.0 | $34 \cdot 3$ | 34.5 | $35 \cdot 3$ | 35.3 | 35.6 |
| 550.0 | $38 \cdot 4$ | 38.5 | 39.5 | 39.7 | 39.9 |
| 560.0 | 44.2 | 44.2 | 45.0 | 45.2 | 45.4 |
| 570.0 | 47.8 | 47.8 | 48.6 | 48.7 | 48.8 |
| 580.0 | 48.4 | 48.2 | 48.6 | 48.9 | 49.0 |
| 590.0 | 44.9 | 44.7 | 45.4 | 45.6 | 45.7 |
| 600.0 | 39.4 | 39.1 | 39.8 | 40.0 | 40.0 |
| 610.0 | 33.0 | 32.2 | 32.9 | 33.1 | 33.1 |
| 620.0 | 25.8 | 25.5 | 26.2 | 26.3 | 26.2 |
| 630.0 | 20.8 | 20.0 | 20.2 | 20.3 | 20.2 |
| 640.0 | 15.1 | 15.0 | 15.3 | 15.4 | 15.2 |
| 650.0 | 11.3 | 11.3 | 11.4 | 11.5 | 11.3 |
| 660.0 | 8.2 | 8.4 | 8.5 | 8.6 | 8.3 |
| 670.0 | 6.3 | 6.4 | 6.3 | 6.3 | 6.1 |
| 680.0 | 4.6 | 4.9 | 4.6 | 4.7 | 4.4 |
| 690.0 | 3.7 | 4.2 | 3.6 | 3.7 | 3.4 |
| 700.0 | 2.8 | 3.3 | 2.7 | 2.8 | 2.5 |
| 710.0 | 2.2 | 2.8 | 2.2 | 2.3 | 1.8 |
| 720.0 | 1.7 | . 3 | 1.7 | 1.8 | 1.3 |
| 730.0 | 3.8 | 4.9 | 1.4 | 1.4 | - 9 |
| 740.0 | 1.5 | 2.1 | 1.1 | 1.6 | . 5 |
| 750.0 | 1.5 | 2.4 | 1.0 | - 5 | - 2 |
| 760.0 | 1.5 | 2.9 | . 0 | - 0 | . 0 |

MERCURY LINES

| 405.0 | 20.9 | 20.3 | 21.1 | 21.0 | 20.7 |
| ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 55.0 | 54.3 | 55.3 | 54.5 | 55.4 |
| 546.0 | 24.8 | 24.5 | 25.1 | 25.1 | 24.9 |
| 578.0 | 8.2 | 8.2 | 9.4 | 9.3 | 9.0 |



FIGURE 4.58 AVERAGE RELATIVE SPECTRAL IRRADIANCE ( 25 CM SECTION) MEASUREMENTS NORMALIZED TO AREA

RELATIVE SPECTRAL IRRADIANCE DISTRIBUTION(25CM SECTION)-NORMALIZED TO AREA LAMP NUMBER NBS8911

| WAVELENGTH380.0 | NBS |  |  | LABORATORY 4 |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | RUN 1 | RUN 2 | RUN 3 | RUN 4 | RUN 5 |
|  | 5.0 | 5.0 | 5.3 | 5.1 | 4.9 |
| 390.0 | 8.3 | $8 \cdot 3$ | 8.4 | 8.6 | 8.9 |
| 400.0 | 12.5 | 9.4 | 14.0 | 12.1 | 13.0 |
| 410.0 | 17.1 | 16.0 | 17.3 | 16.9 | 17.7 |
| 420.0 | 22.0 | 21.8 | 22.3 | 22.3 | 22.2 |
| 430.0 | 27.6 | 27.1 | 27.7 | 27.4 | 27.8 |
| 440.0 | 32.2 | 31.4 | 31.0 | 31.9 | $32 \cdot 3$ |
| 450.0 | 36.1 | 35.1 | 34.9 | 35.0 | 37.0 |
| 460.0 | 38.5 | 37.5 | 37.4 | 38.1 | 38.4 |
| 470.0 | 39.6 | 38.5 | 39.2 | 39.4 | 41.1 |
| 480.0 | 39.4 | 38.3 | 38.8 | 39.3 | 38.6 |
| 490.0 | 38.2 | 37.1 | 37.5 | 37.2 | 37.4 |
| 500.0 | 35.9 | 34.7 | 35.6 | 35.8 | 35.9 |
| 510.0 | 33.5 | 32.5 | 33.0 | 33.7 | 33.6 |
| 520.0 | 31.8 | 30.8 | 31.8 | 32.3 | 32.0 |
| 530.0 | 31.9 | 31.1 | 31.5 | 32.1 | 32.0 |
| 540.0 | 34.4 | 31.9 | 35.2 | 34.8 | 34.7 |
| 550.0 | 38.5 | 34.4 | 40.0 | 39.5 | 39.9 |
| 560.0 | 44.2 | 43.4 | 45.1 | 44.6 | 45.0 |
| 570.0 | 47.9 | 46.7 | 48.6 | 48.2 | 48.4 |
| 580.0 | 48.5 | 47.0 | 53.6 | 53.0 | 50.7 |
| 590.0 | 44.8 | 43.5 | 44.7 | 45.4 | 45.1 |
| 600.0 | 39.5 | 38.1 | 39.0 | 39.8 | $39 \cdot 3$ |
| 610.0 | 32.4 | 31.6 | 32.2 | 32.8 | 32.5 |
| 620.0 | 25.7 | 25.1 | 26.0 | 25.9 | 25.8 |
| 630.0 | 20.5 | 19.6 | 20.1 | 20.1 | 20.0 |
| 640.0 | 15.0 | 14.6 | 15.3 | 15.4 | 15.1 |
| 650.0 | 11.1 | 11.1 | 11.4 | 11.6 | 11.5 |
| 660.0 | 8.3 | 8.1 | 8.5 | 8.6 | 8.5 |
| 670.0 | 6.4 | 6.5 | 6.4 | 6.6 | 6.4 |
| 680.0 | 4.6 | 4.8 | 4.9 | 4.9 | 4.9 |
| 690.0 | 3.7 | 4.2 | 4.0 | 4.1 | $4 \cdot 1$ |
| 700.0 | 2.8 | 3.3 | 2.9 | 2.9 | 3.0 |
| 710.0 | 2.4 | 2.7 | 2.4 | 2.4 | 2.4 |
| 720.0 | 1.9 | $2 \cdot 3$ | 1.9 | 1.9 | 1.9 |
| 730.0 | 4.0 | 4.9 | 1.5 | 1.6 | 1.5 |
| 740.0 | 1.5 | 2.4 | 1.4 | 1.3 | 1.3 |
| 750.0 | 1.8 | 2.4 | 1.1 | 1.0 | 1.2 |
| 760.0 | 1.5 | 2.9 | - 9 | 1.0 | 1.0 |

MERCURY LINES

| 405.0 | 21.3 | 20.8 | 20.4 | 20.3 | 19.8 |
| ---: | ---: | ---: | ---: | ---: | ---: |
| 436.0 | 54.6 | 52.9 | 52.6 | 51.6 | 49.5 |
| 546.0 | 24.8 | 9.7 | 26.7 | 26.2 | 26.2 |
| 578.0 | 8.2 | 8.3 | 7.3 | 7.6 | 7.5 |



FIGURE 4.59 AVERAGE RELATIVE SPECTRAL [RRAD[ANCE ( 25 CM SECTION) MEASUREMENTS NORMALIZED TO AREA
4.4. Results of the check on systematic errors in conventional sphere photometry

In section 3.2 the experimental design for this part of the intercomparison was briefly discussed. Each experiment was to consist of five measurements performed in a prescribed manner. For example, the first step was to be the measurement of the total luminous flux of a cool white fluorescent lamp without other lamps in the sphere. The photocell reading in this case is proportional to the total luminous flux of the lamp, $C$, minus a fraction, $A_{c}$, of the light which is absorbed by the lamp. That is,

$$
\begin{equation*}
\mathrm{R}_{1}=\mathrm{K}_{1} \mathrm{C}\left(1-\mathrm{A}_{\mathrm{c}}\right) \tag{4.1}
\end{equation*}
$$

where $\mathrm{Kl}_{1}$ is the proportionality factor for the spectral distribution of a cool white fluorescent lamp.

In the second step of the experiment the above measurement was repeated with an unlighted incandescent lamp present in the sphere. If the fraction of light absorbed by the incandescent lamp is $A_{I}$, the equation describing this step of the experiment is:

$$
\begin{equation*}
R_{2}=K_{1} C\left(1-A_{c}\right)\left(1-A_{I}\right) \tag{4.2}
\end{equation*}
$$

Multiplication of the two factors enclosed by parenthesis yields four terms, one of which is the product of the two absorption fractions. Since the fraction of light absorbed by each bulb is much less than unity, their product may be neglected. Equation 4.2 becomes

$$
\begin{equation*}
R_{2}=K_{1} C\left(1-A_{c}-A_{I}\right) \tag{4.3}
\end{equation*}
$$

If the change in the lamp absorption due to the different spectral distributions of the sources is assumed to be negligible, then the equation representing the photocell readout of a lighted incandescent and an unlighted fluorescent lamp is:

$$
\begin{equation*}
R_{4}=K_{2} I\left(I-A_{c}-A_{I}\right) \tag{4.4}
\end{equation*}
$$

In this equation, $I$ is the total luminous flux of the incandescent lamp and $K_{2}$ is the proportionality factor for an incandescent spectral distribution. In summary, the equations representing all five steps in this experiment are:

$$
\begin{aligned}
& R_{1}=K_{1} C\left(1-A_{c}\right) \\
& R_{2}=K_{1} C\left(1-A_{c}-A_{I}\right) \\
& R_{3}=K_{1} C\left(1-A_{c}-A_{I}\right)+K_{2} I\left(1-A_{c}-A_{I}\right)+W \\
& R_{4}=K_{2} I\left(1-A_{c}-A_{I}\right) \\
& R_{5}=K_{2} I\left(1-A_{I}\right)
\end{aligned}
$$

In the third equation listed above, a term has been introduced to represent all the effects in the system that preclude closure. The two major effects included in $W$ are the non-linearity of the system and the change of fluorescent lamp output caused by heat from the incandescent lamp nearby. These two effects cannot be separately determined from the data of this limited experiment. However, if such a separate determination is desired in future experiments, it is suggested that the experiment be expanded to include another lamp of the same spectral distribution as either of the two used in the present test. That is, a second fluorescent lamp in the sphere would test linearity without introducing a heating effect. Furthermore, if four lamps were tested (two of each type) in a series of single and double lamp measurements, then the assumption that lamp absorption is independent of spectral distribution would be unnecessary. In this case the fractional absorption of each source by the same bulb could be determined separately. For the present intercomparison it was decided to forgo completeness for the sake of simplicity.

Since the total luminous flux of both the fluorescent and incandescent lamps was assigned at NBS, the five equations listed above can be solved for the fractional absorption $A_{I}$ and $A_{c}$, the sphere factors $K_{1}$ and $K_{2}$, and the closure term W. The absorption terms are:

$$
\begin{equation*}
A_{I}=\frac{R_{4}\left(R_{1}-R_{2}\right)}{R_{2} R_{5}+R_{1} R_{4}-R_{2} R_{4}} \tag{4.5}
\end{equation*}
$$

and

$$
\begin{equation*}
A_{c}=\frac{R_{2}\left(R_{5}-R_{2}\right)}{R_{2} R_{5}+R_{1} R_{4}-R_{2} R_{4}} \tag{4.6}
\end{equation*}
$$

The sphere factors are:

$$
\begin{equation*}
K_{1}=R_{1} / C\left(1-A_{c}\right) \tag{4.7}
\end{equation*}
$$

and

$$
\begin{equation*}
\mathrm{K}_{2}=\mathrm{R}_{5} / \mathrm{I}\left(1-\mathrm{A}_{\mathrm{I}}\right) \tag{4.8}
\end{equation*}
$$

And the closure term is:

$$
\begin{equation*}
W=R_{3}-R_{2}-R_{4} \tag{4.9}
\end{equation*}
$$

By using the photocell readings supplied by the various laboratories, the values of each of these terms were calculated and are presented in tables 4.68 to 4.74. Table 4.75 is a summary of the results of these experiments. This table also lists the sphere size, paint, and color correction used by each laboratory. The "Percent Color Deviation" in the last line of the table is the difference between the two calculated sphere factors. That is,

$$
\begin{equation*}
\text { Percent Color Deviation }=100\left(\mathrm{~K}_{1}-\mathrm{K}_{2}\right) / \mathrm{K}_{2} \tag{4.10}
\end{equation*}
$$

For perfectly color corrected spheres, this quantity would, of course, be zero. It is readily seen from table 4.75 that the fraction of light absorbed by the fluorescent lamps can be closely correlated with the sphere diameter. These data and the data from the incandescent lamps are presented graphically in figure 4.60. The absolute value of the closure term can also be correlated to a small extent with the sphere diameter. This may mean that heating of the fluorescent lamp in smaller spheres is the slightly dominant effect. As discussed previously, an expanded experiment would be necessary actually to determine this.

The extent of color correction attempted by each laboratory and the calculated color deviation are related except in the case of Laboratories 1 and 5 . Laboratory $l$ is apparently correct in saying that any color corrections to their system are relatively small, however, an explanation for this apparent anomaly in the case of Laboratory 5 is not discernable from the available data. (See tables 3.1 to 3.3 and section 3.1)

The negative absorption observed by Laboratories 2 and 5 deserves some mention. In both cases it is quite close to the standard deviation of a single measurement and may not be meaningfully different from zero. It can be argued that inadequate baffling, leading to a direct reflection from the unlighted bulb to the detector, would appear as a negative absorption. There are, however, insufficient data to support this hypothesis.


TABLE 4.69

SYSTEMATIC ERROR CHECK OF PHOTOMETRIC EQUIPMENT

```
LABORATORY 2 C = 2794.8 LUMENS I = 2753.0 LUMENS
```


## RUN 1

| OBS. | LAMP | FLUORESCENT LAMP VOLT CUR(SET) |  | INCANDESCENT VOLT(SET) | LAMP CUR | TIME | TEMP | PHOTOCELL READING |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | $c$ | 101.40 | 430 |  |  | . 00 | 77.40 | 2845.0 |
| 2 | $C+(I)$ | 101.20 | 430 |  |  | - 00 | 77.20 | 2836.0 |
| 3 | C +I | 101.20 | 430 | 109.00 | 1.59 | . 00 | $77 \cdot 30$ | 5544.0 |
| 4 | $(\mathrm{C})+\mathrm{I}$ |  |  | 109.00 | 1.59 | . 00 | 77.80 | 2725.0 |
| 5 | I |  |  | 109.00 | 1.59 | . 00 | $77 \cdot 30$ | 2708.0 |

KUN 2


LABORATORY $3 \quad C=2917.1$ LUMENS $I=2701.0$ LUMENS

| RUN | 1 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | FLUORESCENT LAMP |  | INCANDESCENT VOLT(SET) | $\begin{aligned} & \text { LAMP } \\ & \text { CUR } \end{aligned}$ | TIME | TEMP | $\begin{aligned} & \text { PHOTOCELL } \\ & \text { READING } \end{aligned}$ |
| OBS. | Lainp | VOLT | (SE.T) |  |  |  |  |  |
| 1 | C | 102.80 | 430 |  |  | 13.10 | 76.90 | 2970.0 |
| 2 | C + ( I) | 102.80 | 430 |  |  | 13.12 | 76.90 | 2970.0 |
| 3 | $C+I$ | $102 \cdot 80$ | 430 | 108.60 | 1.60 | 13.15 | $77 \cdot 90$ | 58.23 .0 |
| 4 | $(\mathrm{C})+\mathrm{I}$ |  |  | 108.60 | 1.60 | 13.17 | 78.00 | 2963.0 |
| 5 | I |  |  | 108.60 | 1.60 | 13.19 | $78 \cdot 20$ | 2865.0 |

RUN 2


SYSTEMATIC ERROR CHECK OF PHOTOMETRIC EQUIPMFNT

```
LABORATORY 4 C = 2783.2 LUMENS I = 2633.0 LUMENS
```

RUN 1

| OBS. | LAMP | FLUOHESCENT LAMP VOLT CUR(SET) |  | INCANDESCENT VOLT(SET) | LAMP CUR | TIME | TEMP | PHOTOCELL READIIvG |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | C | 101.50 | 430 |  |  | 17.26 | 76.20 | 2937.0 |
| 2 | $C+(I)$ | 101.50 | 430 |  |  | 17.32 | $76 \cdot 20$ | 2922.0 |
| 3 | C +1 | 101.50 | 430 | 107.10 | 1.58 | 17.37 | 78.20 | 5622.0 |
| 4 | (C) +I |  |  | 107.10 | 1.58 | 17.43 | $78 \cdot 20$ | 2732.0 |
| 5 | I |  |  | 107.10 | 1.58 | 17.48 | $82 \cdot 00$ | 2780.0 |

RUN 2

| OBS. | LAMP | FLUORESC VOLT | ENT LAMP CUR (SET) | INCANDESCENT VOLT(SET) | LAMP CUR | TIME | TEMP | PHOTOCELL <br> READIING |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | C | 101.90 | - 430 |  |  | 15.45 | 76.40 | 2973.0 |
| 7 | $C+(I)$ | 101.90 | 430 |  |  | 15.47 | 76.40 | 2961.0 |
| E | $C+I$ | 101.90 | 430 | 107.10 | 1.58 | 15.52 | 80.00 | 5711.0 |
| 9 | (C) +1 |  |  | 107.10 | 1.58 | 15.57 | 80.00 | 2768.0 |
| 10 | I |  |  | 107.10 | 1.58 | 16.00 | 80.00 | 2821.0 |

RUN 3

| OBS. | LAMP | FLUORESCENT LAMP |  | INCANDESCENT VOLT(SET) | LAMP CUR | TIME | TEMP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | VOLT | CUR(SET) |  |  |  |  |
| 11 | C | 101.50 | 430 |  |  | 16.27 | $76 \cdot 20$ |
| 12 | $C+(I)$ | 101.50 | 430 |  |  | 16.28 | 76.20 |
| 13 | $C+I$ | 101.40 | 430 | 107.10 | 1.58 | 16.35 | 79.00 |
| 14 | (C) +I |  |  | 107.10 | 1.58 | 16.36 | 80.00 |
| 15 | I |  |  | 107.10 | 1.58 | $16 \cdot 37$ | 80.00 |

PHOTOCELL
READING
3001.0
2984.0 5747.0 2774.0 2834.0

|  | RUN 1 | RUN 2 | RUN 3 | MEAN | S.D. |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| ABSORPTION I | .50 | .40 | .55 | .48 | .08 | PERCENT |
| ABSORPTION C | 1.72 | 1.87 | 2.11 | 1.90 | .20 | PERCENT |
| CLOSUFE | -.57 | -.31 | -.19 | -.36 | .19 | PERCENT |
| SPH FACTOR K1 | 1.0737 | 1.0886 | 1.1014 | 1.0879 | .0139 |  |
| SPH FACTOK K2 | 1.0612 | 1.0757 | 1.0823 | 1.0731 | .0108 |  |

```
LABOKATORY 5 C = 2750.5 LUMENS I = 2680.0 LUNENS
```

| RUN 1 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBS. | LAMP | FLUORESCENT LAMP VOLT CUR(SET) |  | INCANDESCENT VOLT (SET) | LAMP CUR | TIME | TEMP | PHOTOCELL READIIG |
| 1 | C | 101.00 | 430 |  |  | 4.44 | 24.70 | 3025.0 |
| 2 | $C+(I)$ | 101.00 | 430 |  |  | 4.45 | 24.70 | 3029.0 |
| 3 | $C+I$ | 101.00 | 430 | 107.90 | 1.58 | 4.47 | 25.20 | 5978.0 |
| 4 | $(C)+I$ |  |  | 107.90 | 1.58 | 4.48 | 25.50 | 2945.0 |
| 5 | I |  |  | 107.90 | 1.58 | 4.49 | 25.60 | 2974.0 |

RUN 2

| OBS. | LAMP | FLUURESCENT LAMF VOLT CUR (SET) |  | INCANDESCENT VOLT(SET) | LAMP CUR | TIME | TEMP | PHOTOCELL READIIVG |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | C | 100.50 | 430 |  |  | 4.21 | 24.80 | 3012.0 |
| 7 | $C+(1)$ | 100.50 | 430 |  |  | 4.22 | 24.80 | 3014.0 |
| 8 | $C+I$ | 101.00 | 430 | 107.90 | 1.58 | 4.25 | 24.80 | 6000.0 |
| 9 | $(\mathrm{C})+\mathrm{I}$ |  |  | 107.90 | 1.58 | 4.26 | 25.00 | 2962.0 |
| 10 | I |  |  | 107.90 | 1.58 | $4 \cdot 27$ | 25.20 | 2990.0 |

PHOTOCELL

READING
3028.0
3034.0
6004.0
2955.0
2983.0

ABSORPTION I ABSORPTION C CLOSURE
SPH FACTOR K1 SPH FACTOR K2

| RUN 1 | RUN 2 |
| ---: | ---: |
| -.13 | -.07 |
| .98 | .94 |
| .07 | .40 |
| 1.1106 | 1.1054 |
| 1.1083 | 1.1149 |


| RUN 3 | MEAN | S.D. |
| ---: | ---: | ---: |
| $=.20$ | -.13 | .07 |
| .94 | .95 | .02 |
| .25 | .24 | .17 |
| 1.1113 | 1.1091 | .0032 |
| 1.1109 | 1.1114 | .0034 |


| INCANDESCENT VOLT (SET) | $\begin{aligned} & \text { LAMP } \\ & \text { CUR } \end{aligned}$ | TIME | TEMP |
| :---: | :---: | :---: | :---: |
|  |  | 4.17 | 24.20 |
|  |  | 4.18 | 24.20 |
| . 00 | . 00 | 4.21 | 24.40 |
| 107.90 | 1.58 | 4.22 | 24.60 |
| 107.90 | 1.58 | 4.23 | $24 \cdot 80$ |

SYSTEMATIC ERROR CHECK OF PHOTOMETRIC EQUIPMENT

```
LABORATORY 6 C = 2804.9 LUMENS I = 2646.0 LUMENS
```

| kUN 1 |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OBS. | LAMP | FLUORESCENT LAMP VOLT CUR(SET) |  | INCANDESCENT VOLT(SET) | LAMP CIJR | TIME | TEMP | PHOTOCELL |
|  |  |  |  | READING |  |  |  |
| 1 | C | 234.00 | 430 |  |  |  | 9.05 | 14.80 | 1167.0 |
| 2 | $C+(I)$ | 234.00 | 430 |  |  | 9.10 | 14.80 | 1158.0 |
| 3 | $C+I$ | 234.00 | 430 | 107.50 | 1.59 | 9.15 | 16.00 | 2507.0 |
|  | $(\mathrm{C})+\mathrm{I}$ |  |  | 107.50 | 1.59 | 9.20 | 16.30 | 1350.0 |
| 5 | I |  |  | 107.50 | 1.59 | 9.23 | 16.40 | 1358.0 |

RUN 2

| OBS. | LAMP | FLUORESCENT LAMP VOLT CUR(SET) |  | INCANDESCENT VOLT(SET) | LAMP CUR | TIM ${ }^{\text {E }}$ | TENP | PHOTOCELL REALING |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6 | $C$ | 235.00 | 430 |  |  | 11.10 | 15.80 | 1165.0 |
| 7 | $C+(I)$ | 235.00 | 430 |  |  | 11.15 | 16.00 | 1162.0 |
| 8 | $C+I$ | 235.00 | 430 | 107.50 | 1.59 | 11.20 | 17.00 | 2507.0 |
| 9 | $(C)+I$ |  |  | 107.50 | 1.59 | 11.22 | 17.50 | 1346.0 |
| 10 | I |  |  | 107.50 | 1.59 | 11.25 | $17 \cdot 50$ | 1354.0 |

RUN 3

| ObS. | LAMP |  | FLUURESCENT LAMP VOLT CUR(SET) |  |  | INCANDESCENT VOLT(SET) | $\begin{aligned} & \text { LAMP } \\ & \text { CUR } \end{aligned}$ | TIME | TEMP | PHOTOCELL READING |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 11 | C |  | 234.00 | 430 |  |  |  | 12.05 | 17.30 | 1165.0 |
|  | $C+(\mathrm{I})$ |  | 234.00 | 430 |  |  |  | 12.10 | 16.40 | 1158.0 |
| 13 | C + I |  | 234.00 | 430 |  | 107.50 | 1.59 | 12.15 | 17.60 | 2505.0 |
|  | $(C)+I$ |  |  |  |  | 107.50 | 1.59 | 12.17 | 18.00 | 1344.0 |
| 15 |  |  |  |  |  | 107.50 | 1.59 | 12.25 | 18.00 | 1352.0 |
|  |  |  | RUN 1 |  | RUN 2 | 2 RUN 3 |  | MEAN | S.D. |  |
| ABSO | ORPTION | I | . 77 |  | - 26 | 6 .60 |  | . 54 | - 26 | PERCENT |
| ABSO | ORPTION | C | - 58 |  | . 59 | 9.59 |  | - 59 | . 00 | PERCENT |
| CLOS | UKE |  | -. 04 |  | -. 04 | 4 . 12 |  | . 01 | . 09 | PERCENT |
| SPH | FACTOR | K1 | . 4185 |  | . 4178 | $8 \quad .4178$ |  | 4180 | . 0004 |  |
| SPH | FACTOR | K2 | . 5172 |  | . 5130 | 0.5140 |  | 5148 | . 0022 |  |

```
LABORATORY 7 C = 2902.5 LUMENS I = 2769.0 LUMENS
```

| RUN | 1 |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | FLUORESCENT LAMP |  | INCANDESCENT VOLT(SET) | LAMP CUR | TIME | TEMP | $\begin{aligned} & \text { PHOTOCELL } \\ & \text { READIWG } \end{aligned}$ |
| OBS. | LAMP | VOLT | CUR (SET) |  |  |  |  |  |
| 1 | $c$ | 102.30 | 430 |  |  | 10.16 | 24.90 | 2900.0 |
| 2 | $C+(1)$ | 102.40 | 430 |  |  | 10.19 | 25.00 | 2886.0 |
| 3 | $C+I$ | 103.10 | 430 | 109.10 | . 00 | 10.23 | $26 \cdot 30$ | 6000.0 |
| 4 | (C) +I |  |  | 109.10 | . 00 | 10.25 | 27.40 | 3105.0 |
| 5 | I |  |  | 109.10 | . 00 | 10.27 | 27.60 | 3118.0 |

RUN 2

| OBS. | LAMP |
| ---: | :--- |
| 6 $C$ <br> 7 $C+(I)$ <br> 8 $C+I$ <br> 9 $(C)+I$ <br> 10 $I$ |  |

FLUORESCENT LAMP INCANDESCENT LAMP
Table 4.75
Systematic error check of photometric equipment summarization of results $\begin{array}{lll}2 & 3 & 4 \\ \begin{array}{ll}3 \text { meter } & 3 \text { meter }\end{array} & 1.5 \text { meter } \\ \text { Burch** } & \text { Burch } & \text { Burch } \\ \begin{array}{c}\text { Wratten } \\ 78 C\end{array} & \text { None } & \begin{array}{c}\text { Corning } \\ 5900\end{array}\end{array}$
0.1
0.1
$-0.2$
$-4.9$


.
$\begin{array}{llll}n & \cdots & N & m \\ 0 & 0 & 0 & N\end{array}$

Laboratory
Sphere Diameter
Sphere Paint
Color Correcting
Filter
Percent Absorption
(Incandescent)
Percent Absorption
(Fluorescent)
Percent Closure
Percent Color
Deviation
*General Electric Sphere Paint **Burch Sphere Paint
***See Section 3.1


## 5. DUSCUSSION AND CONCLUSIONS

### 5.1. The status of substitutional photometry

In the introduction it was stated that this intercomparison primarily to determine whether the use of a uniform set fluorescent lamps standardized at one laboratory would improve among the values of total luminous flux measured in laboratories lamp industry. The purpose of this intercomparison has not,
 limited to just this. This was the first interlaboratory intercomparison to attempt an experimental design that would answer the more general question: What is the present capability of the lamp industry in the fields of photometry and spectroradiometry? The tests were also designed so that many specific questions could be answered about the performance of the equipment and the experimental techniques of the laboratories taking part in this intercomparison. Some of these specific corclusions have already been presented in section 4 .

Considering the first question asked above: Did the use of the ETL CW Standards improve the agreement among the many laboratories that utilize conventional substitution photometry? If the results of the previous intercomparison* are used as an example of past performance, the answer is no. The range of agreement in the measurement of total luminous flux of cool white 40 watt fluorescent lamps by the laboratories participating in the 1964 Intercomparison** was 1.6\%. That is, the individual measurements were all within $+0.8 \%$ of the average. In the present intercomparison this range was $2.0 \%$, if the results of Laboratory 6 are excluded. Laboratory 6 did not use the ETL CW Standards; and, although their measurements were precise, their results were far outside the range quoted above. This could be used as an argument for the use of one source for fluorescent lamp standards. The argument is further bolstered by the lack of agreement of the lamp industry's average measurement of total luminous flux with that of NBS** in the 1964 Intercomparison. In spite of the close agreement among the laboratories, their average was $2.6 \%$ above the NBS base. In the present intercomparison the agreement of the industry average with the NBS base is $+0.2 \%$, which is not significantly different from zero at the $95 \%$ confidence level.

One conclusion drawn from this part of the present intercomparison is that the use of a single source of fluorescent lamp standards would indeed form a uniform base among all the laboratories measuring luminous flux. However, the use of one source for standard lamps has not served to improve the range of agreement among these laboratories. This can only be accomplished by the improvement of photometric measuring techniques and equipment, and by developing sources that are more stable.

Each laboratory also measured, by conventional substitution photometry, a daylight fluorescent lamp against the ETL CW Standards in order to test agreement in heterochromatic photometry. The range of agreement among all, except Laboratory 6, was $3.6 \%$ and the difference of the industry average from the NBS base*** was $-1.4 \%$. In the 1964 Intercomparison the standards to be used in measuring daylight lamps were unspecified: a daylight lamp base was probably used. The range of agreement was $4.1 \%$ and the difference of the industry average from the NBS base was $+0.1 \%$. Thus it may be concluded that the present
*The results of the 1964 Intercomparison were the subject of a National Bureau of Standards report to members of the Lamp Testing Engineers Conference (LTEC) and, as such, are not available for general circulation except by permission of LTEC.
**This includes the measurements made by the Electrical Testing Laboratories which were not included in the report since they were received at NBS after publication. The NBS measurements were also not included as part of the published form of the 1964 Intercomparison.
***A degree of confidence in the NBS measurements can be estimated by comparing the results of two different measurements on the same lamps. The results of the measurement of luminous flux of daylight and cool white fluorescent lamps by spectroradiometry and color corrected substitutional photometry, given in table 2.2, agree to within $0.2 \%$ for the daylight lamps and $0.1 \%$ for the cool white lamps.
status of heterochromatic photometry is at the same level as that of daylight lamp homochromatic photometry in 1964.

From the data gathered for this intercomparison it can be seen that the increased lack of agreement in the measurements of daylight fluorescent lamps is directly traceable to the extent of the color correction applied at each laboratory. Laboratory 4 applied a suitable color correction filter for both their sphere and sphere window. Laboratory 1 reported their color correction to be relatively small. (See sections 3.1 and 4.4.) The difference between the average of their measurements of the daylight fluorescent lamp and the NBS base was $-0.1 \%$, whereas the average of their measurements of the cool white fluorescent lamps differed from NBS by $-0.4 \%$. Laboratory 2 achieved partial color correction by using Wratten filters and eliminating the sphere window. Laboratory 8 did not apply color corrections to its sphere but did not use a sphere window; they had, in a sense, a partial color correction. Their average difference from NBS for daylight lamps was $-1.3 \%$ and for cool white lamps, +0.1\%. The remaining three laboratories, Laboratories 3, 5 and 7, used sphere windows and did not apply any color corrections. Their average difference from NBS for daylight lamps was $-2.3 \%$ and for cool white lamps, $40.5 \%$.

The value of color correction in heterochromatic substitutional photometry has been clearly demonstrated by the results of this intercomparison.

> 5.2. The status of spectroradiometry and color parameter measurement.

Evaluation of the present status of spectroradiometry is based on the data supplied by four laboratories: Laboratories 1, 2, 4, and 5. Since their measurements were made with standards supplied by NBS and since they submitted data for all parts of the intercomparison, the relative merit of the two techniques for measuring total luminous flux (conventional substitution photometry and spectroradiometry) and the three techniques for measuring color parameters (spectroradiometry of the entire lamp in a sphere, spectroradiometry of a 25 cm section in a baffled enclosure, and the Barnes Colorimeter measurements) could be evaluated.

Conventional photometry and spectroradiometry were compared by measuring total luminous flux by using both techniques. Measurements of the total luminous flux of a 200 watt incandescent lamp against a set of 40 watt cool white standards by conventional substitution photometry are summarized in table 5.1. It would be well to note once again that only Laboratories 1 and 4 achieved suitable color correction of their equipment. Laboratory 2 attempted only a partial color correction, while Laboratory 5 did not color correct at all. The percent differences between the average of their measurements and the NBS assignments were: $-1.4 \%$ and $-1.3 \%$ for Laboratories 1 and 4 respectively; $-2.7 \%$ for Laboratory 2; and $+2.4 \%$ for Laboratory 5. These percent differences can be compared with the differences found from the average of their spectroradiometric measurements of luminous flux of two 40 watt cool white fluorescent lamps versus a 200 watt incandescent lamp (see Table 4.11). They are as follows: $-0.5 \%$ for Laboratory 1; $-7.0 \%$ for Laboratory 2; $+15.6 \%$ for Laboratory $4 ;$ and $-0.4 \%$ for Laboratory 5. The range of agreement among the reported spectroradiometric measurements averaged for each laboratory is $22.6 \%$ and their average difference from the NBS base is $+1.9 \%$. Using conventional photometry the same laboratories reported a range of agreement of $5.1 \%$ and an average difference from the NBS base of $-0.8 \%$.

It appears, therefore, that overall spectroradiometric capability has to be developed much further before the agreement between the spectroradiometric measurement of total luminous flux made at different laboratories will be comparable to the agreement presently attainable by substitutional photometry. The experimental difficulties that Laboratories 2 and 4 may have encountered have been described in Section 4.4. The causes of the present lack of agreement are probably to be found there. The results achieved at NBS, where a comparison (see table 2.2) of spectroradiometry and color corrected substitutional photometry showed differences of at most $0.2 \%$, demonstrate that a significant improvement in spectroradiometric technique can be achieved. It should be noted that only since the introduction of automatic data acquisition systems has

Luminous flux of a 200 watt incandescent lamp by conventional photometry using 40 watt cool white fluorescent lamps as standards

| Laboratory | Lamp | $\begin{gathered} \text { NBS } \\ \text { (lumens) } \\ \hline \end{gathered}$ | $\begin{gathered} \text { Lab } \\ \text { (lumens) } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| 1 | 8757 | 2906 | 2865.2 |
|  |  |  | 2865.2 |
|  |  |  | 2866.6 |
|  |  |  | 2861.6 |
|  |  |  | 2867.1 |
|  |  |  | 2863.1 |
|  |  |  | Avg. 2864.7 |
| 2 | 8758 | 2753 | 2673.0 |
|  |  |  | 2671.0 |
|  |  |  | 2674.0 |
|  |  |  | 2676.0 |
|  |  |  | 2687.3 |
|  |  |  | 2687.3 |
|  |  |  | Avg. 2678.1 |
| 4 | 8759 | 2633 | 2586.4 |
|  |  |  | 2595.8 |
|  |  |  | 2593.4 |
|  |  |  | 2607.4 |
|  |  |  | 2605.9 |
|  |  |  | 2609.7 |
|  |  |  | Avg. 2599.7 |
| 5 | 8756 | 2680 | 2740.9 |
|  |  |  | 2739.1 |
|  |  |  | 2743.3 |
|  |  |  | 2743.3 |
|  |  |  | 2746.3 |
|  |  |  | 2750.0 |
|  |  |  | Avg. 2743.8 |

spectroradiometry become a feasible routine measurement and that for most laboratories it is a very new technique. It is hoped that we may finally be in a position to fulfill the prediction made by Parry Moon (ref. 5) in the 1930's:
"Evidently, we are getting rapidly to a place where our antiquated photometric notions must be discarded, and it seems advisable to analyze our concepts and see what can be done to replace them. In the present book, the entire development has been based not on the eighteenth century intuitive concept of 'light' but upon the firmly established concept of the spectroradiometric curve. It is true that the precision obtainable in radiometric measurements is still disappointingly low, so that actual photometry may be forced to stick to the old methods for a few years longer. But this does not appear to be an adequate reason why we should continue to force our minds into an eighteenth century mold as regards photometric concepts.n

Turning now to the question of color measurement: What is the precision attainable in the measurement of the color parameters of a fluorescent lamp? This includes the agreement between different methods employed at the same laboratory and the agreement between different laboratories employing the same method. Table 5.2 is a comparison of the three techniques used to measure the $x$ and $y$ chromaticity coordinates. Since the color temperature of a lamp can be derived from the $x$ and $y$ chromaticity coordinates (ref. 6), this discussion will be limited to the measurement of these coordinates.

At NBS the $x$ and $y$ chromaticity coordinates were measured by using only the two spectroradiometric techniques. One technique samples the entire lamp in an integrating sphere and the other samples a 25 cm section of the lamp in a baffled enclosure. The first pair of columns in table 5.2 lists the differences observed between these two measurements on the same lamp (these are listed as differences in the fourth place). The second pair lists the same information for the $x$ and $Y$ chromaticity coordinates measured at the four reporting laboratories. These two pairs of columns are an indication of the agreement between these two separate measurements made at the same laboratory. At NBS the internal range of agreement of the two methods of measurement was, therefore, -0.0021 to +0.0012 , or 0.0033 ; and at the four reporting laboratories it was -0.0025 to +0.0071 , or 0.0096 .

The absolute value of the differences reported for Laboratory 1 are about twice those reported for the other laboratories. Four of these differences are much larger than the combined value of the standard deviations of each measurement. The reason for the internal disagreement in the case of Laboratory 1 is not clearly evident. Disagreement in the $x$ and $y$ chromaticity coordinates is not a diagnostic check on spectroradiometric performance: it merely indicates that a problem exists. It has already been pointed out that Laboratory l used two different monochromators for these measurements and that they reported their data in reduced form. They also failed to report data at several points in the spectrum, notably at the red and blue extremities. None of these factors can be cited as the primary cause of the internal disagreement. Their spectral distribution curves are in good agreement with those of NBS, as are their spectroradiometric values of total luminous flux. In the third pair of columns of table 5.2 , it is evident that their sphere measurements of color parameters are also in good agreement with those of NBS. One may possibly conclude, therefore, that there is a systematic error in their measurements on a 25 cm section of a lamp that does not exist in their sphere measurements.

The last three pairs of columns of table 5.2 are an indication of the status of interlaboratory agreement in the measurement of color parameters. The third pair of columns compares the sphere measurements made on the same lamps at NBS and the four reporting laboratories. The range of agreement was from -0.0031 to +0.0072. The fourth pair is a comparison of the laboratory Barnes measurements and the NBS sphere measurement: range, -0.0060 to +0.0058 . The last pair, which is a comparison of laboratory and NBS 25 cm section measurements, indicates a range of -0.0004 to +0.0069 .

In the comparison of the sphere and 25 cm section measurements of Laboratory 5 in Table 5.2, there appears to be a large disagreement with the NBS measurements of the $y$ chromaticity coordinate. From an examination of their spectral distribution curves it is clear that their match with the NBS points become poorer at
Table 5.2
Fourth place differences in the x and y chromaticity coordinates

*Symbol definitions: $N(25)$ - NBS spectroradiometric measurement on a 25 cm section of $N(S P)$ - NBS spectroradiometric measurement in an integrating sphere. $L(25)$ - Laboratory spectroradiometric measurement on a 25 cm section
ol of the lamp. Laboratory
sphere.
sphere.
L(B) - Laboratory measurement using a Barnes Colorimeter. Note that all the differences in $x$ and $y$ have been mulitplied by 10,000 .
the red end of the spectrum. As noted in section 4.4, this may be due to reduced photomultiplier sensitivitv in this spectral region or to a systematic drift in the gain and/or sensitivity of their electronics.

The above discussion on agreement of color parameters is, of course. not at all rigorous. Since $x$ and $y$ are non-linear parameters, it is extremely difficult to obtain a statistical comparison of several measurements. However, from table 5.2 several conclusions are apparent:

1) In the most favorable case it is possible to obtain agreement to about $\pm 0.002$ between two different spectroradiometric measurements of the same chromaticity coordinate made at the same laboratory. The present capability within three of the laboratories under consideration is, however, only about +0.003 in the best cases. (Note that the intralaboratory difference is as high as 0.007 for one of the laboratories.)
2) The level of agreement among measurements of chromaticity coordinates between three of the laboratories and NBS in performing the same spectroradiometric measurement on the same lamp is about $\pm 0.003$. (Note that the difference from NBS is as high as 0.007 for one of the laboratories.)
3) Agreement between a spectroradiometric measurement at one laboratory and a Barnes Colorimetric measurement at another is on the order of $\pm 0.006$.
4) The agreement between the four reporting laboratories and NBS in spectroradiometric measurement of chromaticity coordinates seems to be uncorrelated with the agreement in spectroradiometric measurement of total luminous flux.

It is expected that with improvements in spectroradiometric technigues throughout the lamp industry, agreement between laboratories in the measurement of color parameters will improve and spectroradiometry will become more important as a primary means of measuring these parameters.

### 5.3. Summary and conclusions

For the measurement of total luminous flux the most precise method presently in use is homochromatic substitutional photometry (range of agreement, 2\%). The measurements are fast and relatively simple to perform; however, a standard of each type of lamp to be measured must be available in order to achieve maximum precision. Comparison of the luminous flux of two lamps with different spectral distributions, heterochromatic substitutional photometry, is considerably less precise unless the spectral response of the entire photometric system matches the CIE luminous efficiency function; that is, unless the system is fully color corrected. (Range of agreement: daylight versus coolwhite fluorescent, 3.6\%; fluorescent versus incandescent, 5.1\%.)

Although the range of agreement among the participating laboratories was found to be $22.6 \%$, at NBS spectroradiometric and heterochromatic photometric measurements agreed within 0.2\%. Therefore, with proper spectroradiometric techniques it should be possible to compare the total luminous flux of two lamps with very different spectral distributions to a precision close to that of homochromatic substitutional photometry. Furthermore, it would be unnecessary to correct for the spectral response of the system. Since it is difficult to produce and maintain reliably stable standard sources, the expense and effort necessary to set up and maintain a fully color corrected photometric system for all possible sources would be comparable to or might possibly exceed that of a single spectroradiometer. In addition to heterochromatic measurement of total luminous flux, the spectroradiometer data acquired in a single spectral flux distribution measurement permit the calculation of all the color parameters (chromaticity coordinates, color temperature, color rendering, flattery index, etc.), thereby replacing all other color measuring instruments.

We may look forward to a time when a well developed spectroradiometric laboratory would need only a few highly stable standards of flux and spectral distribution from which to derive accurate (though not necessarily stable or precise) secondary standards of each lamp in production. These secondary standards would then be used in homochromatic substitutional photometry for routine quality control testing and other intralaboratory needs.

### 5.4. Acknowledgement

The authors would like to express their sincere thanks to Dr. Frank Studer for his guidance in the development of NBS spectroradiometric photometry and his assistance in the early stages of this intercomparison.

References

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## Part 1

The intercomparison of T12F40 cool-white and daylight lamps for luminous $f 1 u x$ will be conducted by having each laboratory make a set of three runs. The runs are statistically designed and involve measurements on the cool-white, and one daylight fluorescent lamps and one incandescent lamp, all supplied by NBS. These lamps are designated as $C_{1}, C_{2}, D$ and $I$ respectively. The six T12F40 CW lumen standards supplied by ETL last Spring to the industry are to be used as reference standards for this intercomparison by the laboratories that have them; the other laboratories will use their customary reference standards. These are designated as $S_{1}$ through $S_{6}$ in the data sheets. A reference ballast is being supplied and should be used with the three fluorescent lamps being supplied by NBS. The ETL standards should be run on the Sylvania reference ballast, and should be operated according to the instructions sent out with them (see Appendix A of the minutes of the May 14, 1968 meeting of LTEC). The lamps being supplied by NBS should be run with the NBS supplied ballast in the same manner. The USASI circuitry (Il1. Eng. 62, 552-523, Sept. 1967) should be used and all fluorescent lamps should be operated by holding current at 430 mA . The incandescent lamp should be held at the specified voltage and should be in the sphere, but not lit during the fluorescent lamp runs. Similarly a fluorescent lamp should be in the sphere, but not lit, during the measurements on the incandescent lamp. Each run should be completed in the course of a day, and linearity corrections, if any, in the photometric equipment should be noted.

Part 2
The spectroradiometric intercomparison is designed to determine the uncertainty between measurements and between participating laboratories. The test will consist of three runs on each of the fluorescent lamps sent by NBS, and one run on each of the ETL standards. The incandescent lamp sent by the Bureau and one of the fluorescent lamps will be in the sphere at all times to eliminate the effect of absorption. The incandescent lamp will be measured at the beginning of each set of runs and after each fluorescent lamp is measured. The lamps should be operated in the same manner as they were for Part 1 (substitution method). Since one of the purposes of this test is to transfer lumen values from the incandescent lamp to the fluorescent lamp, it will be important to hold the temperature at the center of the sphere to $25^{\circ} \mathrm{C} \pm .2^{\circ} \mathrm{C}$ during the measurement of each fluorescent lamp. Uncorrected data points will be recorded at every 10 nm and at the mercury peaks. Any applicable correction curve will be recorded separately.

## Part 3

This part of the intercomparison is the same as part 2 except that the flux of a fluorescent lamp from a $25-\mathrm{cm}$ section of the fluorescent lamp rather than that from the entire lamp is measured. As in part 2 there will be three runs on each fluorescent lamp supplied and one run on each of the ETL standards, in each case by using the incandescent lamps supplied as a reference source. If the relative spectral distribution of the fluorescent lamps is to be made without reference to the incandescent lamp during the run, the 560 nm reading shall be recorded at the beginning and the end of each run. It is important that the reading does not change during the run. Although the temperature requirements are not strict, the fluorescent lamp should be free of drafts that will cause the output of the lamp to change during the run. Uncorrected data will be recorded at every 10 nm and at the mercury lines. Any appreciable correction curve will be recorded separately.

## Part 4

In this part of the intercomparison the linearity of the system will be checked and the effects of absorption of the incandescent lamp and the fluorescent lamps will be measured. This part of the intercomparison will be used only in conjunction with part 1 (substitution method). The "I" notation stands for the incandescent lamp and the " $C_{1}$ " notation for the first cool-white fluorescent lamp in the intercomparison group. The I or $C_{1}$ enclosed in parentheses means the lamp is in the sphere but is not lit. There should be approximately 15 minutes between the shutting off of $I$ and the lighting of $c_{1}$. Since the incandescent lamp heats the sphere, time between readings $C_{1}+(I)$ and $C_{1}+I$ should be as short as possible; uncorrected data will be recorded together with the time it was taken. Any correction factor will also be recorded separately.

## Part 5

The main purpose of this part of the intercomparison is to determine if any discrepancies exist between spectroradiometric and Barnes colorimeter determinations of chromaticity coordinates. The intercomparison lamps, $C_{1}, C_{2}$ and $D$, will be operated in accordance with the electrical procedures 1 isted for part 1. Each participating laboratory will use the standards and test procedures it normally uses with the Barnes colorimeter. Each laboratory will report the CIE chromaticity coordinates for both the standards used and intercomparison fluorescent lamps. Any applicable correction factors will be recorded separately.

Test 1 Run 2 Date


Test 1 Run 3 Date




NBS 506a-Analysis paper
Test 4



Questionnaire on equipment and procedures used for the NBS intercomparison of October, 1968 Please fill in the following questionnaire for all portions of the intercomparison in which your laboratory participated.

## General

A. Laboratory National Bureau of Standards*
B. For further informationcontact R. D. Saunders

Te lephone $\qquad$
(301) 921-2113
C. Our laboratory participated in:
$\square$ 40-W, cool-white, direct substitution intercomparison.

X
Spectroradiometric determination of the lumen outputs of $40-\mathrm{W}$ fluorescent lamps.
X. Spectroradiometric determination of chromaticity coordinates on $10^{\prime \prime}$ sections of $40-W$
fluorescent lamps.

Check of photometric equipment.
Barnes colorimeter determinations of chromaticity coordinates on $40-W$ fluorescent lamps.

## Test 1: Cool-White, Direct Substitution Intercomparison

A. Sphere

1. Size 2m diameter
2. Coating (please append spectral reflectance curve if available)

Type $\mathrm{BaSO}_{4}$ - see figure $\mathrm{B}-1$ following this section.
Last renewed April, 1966.
3. Color correcting (blue) filter (please append spectral transmittance curve if available)
___ not used
X
used

Type Corning 5900

Thickness 1.55 mm
4. Sphere window (please append spectral transmittance curve if available)

Material White plexiglass - see figure B-2 following this section.

Thickness 0.5 cm
5. Geometry: please append a sketch of the sphere used showing lamp location, receiver location, baffle location and size, etc. - see figure B-3.
*Certain commercial instruments or materials are identified in this appendix in order to adequately specify the experimental procedure. In no case does such identification imply recommendation or endorsement by the National Bureau of Standards, nor does it imply that the material or equipment identified is necessarily the best available for the purpose.
B. Photocell

1. Manufacturer Weston
2. Model 856 V
3. Color corrected X yes ___no
(please append spectral response curve if available)
4. Measuring circuit (please append circuit diagram) - see figure B-4 following this section.
5. Linearity corrections

X Not applied Applied

Method of determining linearity correction (specify)
c. Lamp Operation-Fluorescent (please append complete circuit diagram) - see figure 2.1 in text.

1. Power source

## $0.015 \%$ distortion

$\qquad$ AC line (regulated to $\qquad$ \%)

X Power supply (Manufacturer Elgar
Model $\qquad$ )
$\qquad$ Other (specify) $\qquad$
2. Reference ballast for ETL C-W standards

Type variable reactance reference ballast
Manufacturer Sylvania
3. Power factor of reference ballast 7.5\%

How determined (specify) by using a low power factor wattmeter, a true RMS voltmeter, and an ammeter.
4. Lamp voltage $\qquad$ X measured $\qquad$ set

How measured by using a high impedance voltmeter (Fluke Model 931)
Voltmeter input impedance 10 meg ohms
5. Current $\qquad$ measured $\qquad$ set

How measured by using a Weston Model 904 AC ammeter
6. Stabilization time 20 minutes in sphere zero minutes prestabilization. The lamp (was/was not) turned off after prestabilization.
D. Lamp operation-incandescent (please append complete circuit diagram)

1. Power source
$\qquad$ AC Power
___ amperes
$\qquad$ Hertz
___ Distortion
___ AC line (regulated to $\qquad$ $\%$ )
$\qquad$ AC power supply (manufacturer $\qquad$
mode1 $\qquad$
$\qquad$ Other (specify) $\qquad$
$\qquad$ DC power

## __ Batteries

X DC power supply (manufacturer N.J.E. (2 units in series) model SY 60-12
2. Voltage
$\qquad$ measured
$\qquad$ set

How determined by using a differential voltmeter (Keithley model 660)
3. Current

X measured
$\qquad$ set

How determined by measuring the drop across a 1 ohm shunt with the above mentioned differential voltmeter
4. Warm-up time $\qquad$ 5 minutes
(If not in place in the sphere during warmup please give details $\qquad$ )
5. The incandescent lamp (was/was not) in the sphere when the f1uorescent lamps were measured.
E. Ambient temperature

1. $\qquad$ not measured
2. $\qquad$ measured

Method of measurement Digitec model 251 thermometer
Location of measurement 3 locations: 18 inches above center of 1 amp and 1 inch from each end
F. Other

1. Test was conducted by ___ technician X_ professional
2. Treated as a routine test? $\qquad$ yes $\qquad$ X no
3. If no, please detail the special precautions used This was an experiment of special design.

In addition, the equipment was checked out before these tests.
G. Comments

## Test 2: Spectroradiometric Determination of the Lumen Output of 40-W Fluorescent Lamps

A. Sphere

1. X The information supplied for Test l, Section $A$ is applicable. (If so, skip 2, 3, 4, 5, \& 6)
2. Size $\qquad$ diameter
3. Coating (please append spectral reflectance curve if available)

Type $\qquad$
Last renewed $\qquad$
4. Color correcting (blue) filter (please append spectral transmittance curve if available)
$\qquad$ not used
$\qquad$ used Type $\qquad$ Thickness $\qquad$
5. Sphere window (please append spectral transmittance curve if available)

Material $\qquad$
Thickness $\qquad$
6. Geometry: Please append a sketch of the sphere used showing lamp location, receiver location, baffle location and size, etc.
B. Lamp operation-Fluorescent (please append complete circuit diagram)

1. X The information supplied for Test 1, Section C, is applicable. (If so, skip 2, 3, 4, 5, $6, \& 7$ )
2. Power source
$\qquad$ \% Distortion
AC line (regulated to $\qquad$ \%)

Power supply (Manufacturer
Model $\qquad$
$\qquad$ Other (specify) $\qquad$
3. Reference ballast for ETL C-W standards

Type $\qquad$
Manufacturer $\qquad$
4. Power factor of reference ballast $\qquad$ \%

How determined (specify)
5. Lamp voltage $\qquad$ measured $\qquad$ set

How measured $\qquad$

Voltmeter input impedance $\qquad$ ohms
6. Current $\qquad$ measured set

How measured
7. Stabilization time $\qquad$ minutes in sphere $\qquad$ minutes prestabilization. The lamp (was/was not) turned off after prestabilization.
C. Lamp operation-Incandescent (please append complete circuit diagram)

1. Z The information supplied for Test 1, Section D, is applicable. (If so, skip 2, 3, 4, 5 \& 6)
2. Power source

AC power
$\qquad$ volts
$\qquad$
__Hertz
$\qquad$ \% Distortion
___ AC line (regulated to $\qquad$ \%)
_ AC power supply (manufacturer $\qquad$
mode1 $\qquad$
$\qquad$ Other (specify) $\qquad$
$\qquad$ DC power
_ Batteries
$\qquad$ DC power supply (manufacturer $\qquad$
mode 1 $\qquad$
3. Voltage
$\qquad$ measured
$\qquad$ set

How determined $\qquad$
4. Current
$\qquad$ measured
$\qquad$ set

How determined $\qquad$
5. Warm-up time $\qquad$ minutes
(If not in place in the sphere during warmup please give details $\qquad$
$\qquad$
6. The incandescent lamp (was/was not) in the sphere when the fluorescent lamps were measured.
D. Ambient temperature

1. X
$\qquad$ The information supplied for Test 1, Section E is applicable (if so, skip to the next section)
2. $\qquad$ Not measured
3. $\qquad$
Method of measurement $\qquad$
Location of measurement $\qquad$
E. Spectroradiometer (Please append a block diagram of the instrument showing light path, major components, entrance and auxiliary optics, detector location, etc.) - see figure 2.2 of text.
4. Monochromator
a. Bauschand Lomb Manufacturer 505 model
___ Prism X___ grating

Combination (specify)
b. Effective spectral bandpass (Please append slit width correction curve if available)

$4050 \AA$| 5.84 nm |
| :---: |

$4358 \AA 5.53 \mathrm{~nm}$
$5461 \AA .48 \mathrm{~nm}$
$5780 \AA 5.93 \mathrm{~nm}$
How determined (specify) from an analog plot of instrument reading versus dial setting and subsequent graphical area measurement.
2. Wavelength Calibration

Last calibrated before each series of measurements
Method (Specify spectral lines used) Hg and Cd emission lines
3. Detector (please append spectral response curve if available)

EMI Manufacturer 9558 QB Mode 1
PM Type (Photomultiplier, thermopile, etc.) S-20 response type
4. Readout electronics (please append block circuit diagram) - see figure 2.2 of text.

Integrating time approximately 0.1 sec
Light chopped? X No $\qquad$ Yes $\qquad$
Other special features $\qquad$
$\qquad$ Hertz)
5. System checks
a. Linearity _X_checked $\qquad$
Method by using sector discs and neutral density filters
b. Scattered light X_checked not checked

Method by using narrow band interference filters
c. Other (specify) $\qquad$
6. Data reduction method normally used in your laboratory. - see section 2 , 2 of text
a. Calibration

Reference source used $\qquad$
Procedure $\qquad$
$\qquad$
b. Line spectra (please describe method of evaluation) $\qquad$
c. Other reduction procedures (specify) $\qquad$
F. Other

1. Test was conducted by $\qquad$ technician

X
X professional
2. Treated as a routine test? $\qquad$
3. If No, please detail the special precautions used This was an experiment of special design.

In addition, the equipment was checked out before these tests.
G. Comments

## Test 3: Spectroradiometric Determination of Chromaticity Coordinates on $10^{\prime \prime}$ Section of $40-W$

## Fluorescent Lamps

A. Geometry (Please append a sketch of the setup used) - see figure 2.3 in text.

X The $10^{\prime \prime}$ section specified by NBS was used.
A $10^{\prime \prime}$ section other than specified by NBS was used (specify) $\qquad$
Method of isolating a $10^{\prime \prime}$ section for investigation (Please describe baffling, baffling material, baffling coating, etc.) $\qquad$
B. Lamp Operation-Fluorescent (Please append complete circuit diagram)

1. $\qquad$ The information supplied for
(Test 1, Section C or Test 2, Section B) is applicable
(If so, state which and skip 2, 3, 4, 5, 6 \& 7)
2. Power source
$\qquad$ \% Distortion
$\qquad$ AC line (regulated to $\qquad$ \%)
$\qquad$ Power supply (Manufacturer $\qquad$

Mode 1 $\qquad$ )
$\qquad$ Other (specify) $\qquad$
$\qquad$
3. Reference ballast for ETL C-W standards

Type $\qquad$
Manufacturer $\qquad$
4. Power factor of Reference ballast $\qquad$ \%

How determined
5. Voltage $\qquad$ measured $\qquad$ set

How measured
Voltmeter input impedance $\qquad$ ohms
6. Current $\qquad$ measured $\qquad$ set

How measured
7. Stabilization time $\qquad$ minutes in place $\qquad$ minutes prestabilization. The lamp (was/was
not) turned off after prestabilization.
C. Lamp operation-Incandescent (please append complete circuit diagram)

1. X The information supplied for (Test 1, Section D or Test 2, Section D) is applicable. (If so, state which and skip $2,3,4, \& 5)$.
2. Power source

AC power
___volts
___ amperes
_hertz
\% distortion
__AC line (regulated to $\qquad$ $\%)$

AC power supply (manufacturer $\qquad$
model $\qquad$ )

Other (specify) $\qquad$

DC power
__ Batteries
_ DC power supply (manufacturer $\qquad$ model $\qquad$
3. Lamp voltage
___measured
$\qquad$ set
How determined
4. Current
$\qquad$
$\qquad$ set

How determined
5. Warm-up time $\qquad$ minutes
(If not in place please give details $\qquad$
D. Ambient temperature

1. $\qquad$ The information supplied for (Test 1, Section E or Test 2, Section D) is applicable (if so, state which and skip to the next Section)
2. $\qquad$ Not measured.
3. $\qquad$ Measured.

Method of measurement $\qquad$
Location of measurement $\qquad$
E. Spectroradiometer

1. X The spectroradiometer described for Test 2, Section $E$, was used without modification.
2. $\qquad$ The spectroradiometer described for Test 2 , Section $E$, was modified as follows
3. $\qquad$ Our laboratory did not participate in the spectroradiometric determination of the lumen output of $40-\mathrm{W}$ fluorescent lamps. (Please fill in Test 2, Section $E$, above to describe the instrument used for the present test.)
F. Other
4. Test was conducted by $\qquad$ technician X professional
5. Treated as a routine test? $\qquad$ Yes $\qquad$ No
6. If no, please detail the special precautions used This was an experiment of special design. In addition, the equipment was checked out before these tests.
G. Comments

Test 4: Check of Photometric Equipment (Test not performed at NBS)
A. Sphere

1. $\qquad$ The information supplied for (Test 1, Section A or Test 2, Section A) is applicable. (If so, state which and skip $2,3,4,5 \& 6$ )
2. Size $\qquad$ diameter
3. Coating (please append spectral reflectance curve if available)

Type $\qquad$
Last renewed $\qquad$
4. Color correcting (blue) filter (please append spectral transmitting curve if available)
$\qquad$ not used
$\qquad$ used

Type $\qquad$
Thickness $\qquad$
5. Sphere window (please append spectral transmittance curve if available)

Material $\qquad$
Thickness $\qquad$
6. Geometry: Please append a sketch of the sphere used showing lamp location, receiver location, baffle location and size, etc.
B. Photocell

1. $\qquad$ The information supplied for Test 1, Section B, is applicable. (If so, skip 2, 3, 4, \& 5)
2. Manufacturer $\qquad$ Model $\qquad$
3. Color corrected $\qquad$ Yes $\qquad$ No
(please append spectral response curve if available)
4. Measuring circuit (please append circuit diagram)
5. Linearity corrections
$\qquad$ Not applied
__Applied
Method of determining linearity correction (specify) $\qquad$
C. Lamp Operation-Fluorescent (Please append complete circuit diagram)
6. $\qquad$ The information supplied for (Test 1, Section C, Test 2, Section B or Test 3, Section B) is applicable. (If so, state which and skip 2, 3, 4, 5, $6 \& 7$ )
7. Power source
$\qquad$ \% distortion
$\ldots$ AC line (regulated to $\qquad$ \%)
___ Power supply (Manufacturer $\qquad$
Model $\qquad$
Other (specify) $\qquad$
8. Ballast for Fluorescent Lamp

Type $\qquad$
Manufacturer $\qquad$
4. Power factor of ballast $\qquad$ \%

How determined
5. Lamp voltage $\qquad$ measured $\qquad$ set

How measured
Voltmeter input impedance $\qquad$ ohms.
6. Current $\qquad$ measured $\qquad$ set

How measured
7. Stabilization time $\qquad$ minutes in sphere $\qquad$ minutes prestabilization. The lamp (was/was not) turned off after prestabilization.
D. Lamp Operation-Incandescent (please append complete circuit diagram)

1. $\qquad$ The information supplied for (Test 1, Section D, Test 2, Section C or Test 3, Section C)
is applicable. (If so, state which and skip 2, 3, 4 \& 5)
2. Power source
$\qquad$ AC power
$\qquad$
___amperes
___hertz
\% distortion
_ AC line (regulated to $\qquad$ \%)
$\qquad$ AC power supply (manufacturer $\qquad$
mode1 $\qquad$
$\qquad$ Other (specify) $\qquad$ DC Power
__Batteries
___ DC power supply (manufacturer $\qquad$ model $\qquad$ )
3. Voltage
$\qquad$ measured
$\qquad$ set

How determined $\qquad$
4. Current
$\qquad$ measured
$\qquad$ set

How determined $\qquad$
5. Warm-up time $\qquad$ minutes
(If not in place in the sphere please give details $\qquad$ )
E. Ambient temperature

1. $\qquad$ The information supplied for (Test 1, Section E, Test 2, Section D or Test 3, Section D)
is applicable. (If so, state which and skip $2 \& 3$ )
2. $\qquad$ Not measured
3. $\qquad$
Method of measurement $\qquad$
Location of measurement $\qquad$
F. Other
4. Test was conducted by technician $\qquad$ professional
5. Treated as a routine test? Yes $\qquad$ No $\qquad$
6. If No, please detail the special precuations used $\qquad$
G. Comments

Test 5: Barnes Colorimeter Determinations of Chromaticity Coordinates on 40-W Fluorescent Lamps (Test not performed at NBS)
A. Lamp Geometry: Please give details of the geometric setup used including a sketch: $\qquad$
B. Lamp Operation: Please give details of the lamp operation including warmup time, voltage and current measurements, ballasts, power factor, etc.: $\qquad$
C. Standards: Please describe the standards used to calibrate the colorimeter as to lamp type, where and when calibrated, etc.: $\qquad$
D. Calibration Procedure: Please describe in detail the calibration procedure used, including the data reduction for a test lamp: $\qquad$
E. Photocells: Please describe the photocells in the colorimeter as to type, number, aperture, filters, hermetic sealing, etc.: $\qquad$
F. Readout Equipment: Please describe the equipment used to read the photocell outputs: $\qquad$
G. Other

1. Test was conducted by $\qquad$ technician ___professional
2. Treated as a routine test? $\qquad$ Yes $\qquad$ No
3. If no, please detail the special precautions used $\qquad$
H. Comments


BAFFLE AND LAMP ARRANGEMENT IN THE NBS INTEGRATING SPHERE FIGURE B-3

FIGURE B-4

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PENALTY FOR PRIVATE USE, $\$ 300$


[^0]:    *Research Associate from the Electrical Testing Laboratories at the National Bureau of Standards.
    **Color temperatures quoted in this intercomparison are based on the 1949 Color Temperature Scale. This scale is based on the 1948 International Practical Temperature Scale (IPTS). For a discussion of the 1970 Color Temperature Scale (1968 IPTS), see the NBS Technical News Bulletin, September, 1970.

[^1]:    *The common use of the term "color temperature" in reference to a fluorescent lamp is, in a strict sense, incorrect. The prescribed terminology is "correlated color temperature". However, in deference to familiarity and simplicity "color temperature" will be used throughout.

[^2]:    *General Electric Sphere Paint
    **Burch Sphere Paint
    ***Cells mounted inside sphere facing sphere wall
    ****A different method is normally used for color correction (See text)
    Note: Measurements at all the laboratories were made in October and November 1968.

