NBS TECHNICAL NOTE

352

The Viscosity and Thermal Conductivity Coefficients of Dilute Neon, Krypton, and Xenon

H. J. M. HANLEY AND G. E. CHILDS



U.S. DEPARTMENT OF COMMERCE National Bureau of Standards

THE NATIONAL BUREAU OF STANDARDS

The National Bureau of Standards1 provides measurement and technical information services essential to the efficiency and effectiveness of the work of the Nation's scientists and engineers. The Bureau serves also as a focal point in the Federal Government for assuring maximum application of the physical and engineering sciences to the advancement of technology in industry and commerce. To accomplish this mission, the Bureau is organized into three institutes covering broad program areas of research and services:

THE INSTITUTE FOR BASIC STANDARDS ... provides the central basis within the United States for a complete and consistent system of physical measurements, coordinates that system with the measurement systems of other nations, and furnishes essential services leading to accurate and uniform physical measurements throughout the Nation's scientific community, industry, and commerce. This Institute comprises a series of divisions, each serving a classical subject matter area:

-Applied Mathematics-Electricity-Metrology-Mechanics-Heat-Atomic Physics-Physical Chemistry-Radiation Physics-Laboratory Astrophysics²-Radio Standards Laboratory,² which includes Radio Standards Physics and Radio Standards Engineering-Office of Standard Reference Data.

THE INSTITUTE FOR MATERIALS RESEARCH ... conducts materials research and provides associated materials services including mainly reference materials and data on the properties of materials. Beyond its direct interest to the Nation's scientists and engineers, this Institute yields services which are essential to the advancement of technology in industry and commerce. This Institute is organized primarily by technical fields:

-Analytical Chemistry-Metallurgy-Reactor Radiations-Polymers-Inorganic Materials-Cryogenics²---Materials Evaluation Laboratory---Office of Standard Reference Materials.

THE INSTITUTE FOR APPLIED TECHNOLOGY ... provides technical services to promote the use of available technology and to facilitate technological innovation in industry and government. The principal elements of this Institute are:

-Building Research—Electronic Instrumentation—Textile and Apparel Technology Center— Technical Analysis-Center for Computer Sciences and Technology-Office of Weights and Measures-Office of Engineering Standards Services-Office of Invention and Innovation-Clearinghouse for Federal Scientific and Technical Information.³

¹ Headquarters and Laboratories at Gaithersburg, Maryland, unless otherwise noted; mailing address Washington, D. C., 20234.

 ² Located at Boulder, Colorado, 80302.
 ³ Located at 5285 Port Royal Road, Springfield, Virginia, 22151.

UNITED STATES DEPARTMENT OF COMMERCE • Alexander B. Trowbridge, Acting Secretary NATIONAL BUREAU OF STANDARDS • A. V. Astin, Director



THE VISCOSITY AND THERMAL CONDUCTIVITY COEFFICIENTS OF DILUTE NEON, KRYPTON, AND XENON

H. J. M. HANLEY AND G. E. CHILDS

Cryogenics Division Institute for Materials Research National Bureau of Standards Boulder, Colorado

NBS Technical Notes are designed to supplement the Bureau's regular publications program. They provide a means for making available scientific data that are of transient or limited interest. Technical Notes may be listed or referred to in the open literature.

For sale by the Superintendent of Documents, U.S. Government Printing Office, Washington, D.C., 20402 Price: 25 cents



CONTENTS

Lis	st of Figures	iv					
Lis	st of Tables	v					
Abs	stract	1					
1.	Introduction	1					
2.	The Potential Functions	5					
3.	Kinetic Theory Transport Expressions	б					
4.	Experimental Data						
5.	Method of Calculation and Results	8					
	5.1 Viscosity	8					
	5.1.1 Neon	9					
	5.1.2 Krypton and Xenon	10					
	5.2 Thermal Conductivity	12					
б.	Conclusion	12					
7.	Acknowledgment	13					
8.	References	21					

LIST OF FIGURES

1.	Argon percent deviation curves $\left[\frac{\eta_{exp} - \eta_{calc}}{\eta_{exp}}\right] \times 100$.
	Curve a is reproduced from Fig. 2 of Ref. 2 and was
	calculated from the Kinara function with $\gamma = 0.1$, $\varepsilon/k = 139.8^{\circ}K$, and $\sigma = 3.35^{\circ}A$. Curve b was calcula-
	ted with the m-6 function, m = 17, ε/k = 151.5°K, and σ = 3.31Å.
2	Neon percent deviation curve $\left[\left(\frac{\eta_{exp} - \eta_{calc}}{2}\right) \times 100\right]$
<i>L</i> .	Meale (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)
	calculated from the Kihara potential function with $\gamma = 0.1$, $\varepsilon/k = 53.2^{\circ}$ K, and $\sigma = 2.67$ Å 11
3.	Krypton and xenon percent deviation curves $\left[\left(\frac{\eta_{exp} - \eta_{calc}}{\eta_{calc}}\right) \times 100\right]$
	calculated from the m-6 potential. For krypton,
	m = 17, ε/k = 226.0°K, and σ = 3.50Å. For xenon, m = 24, ε/k = 382.3°K, and σ = 3.73Å 14
4.	Neon percent deviation curve $\left[\left(\frac{\lambda_{exp} - \lambda_{calc}}{\lambda_{calc}}\right) \times 100\right]$
	calculated from the Kihara potential function,
	$\gamma = 0.1, \epsilon/k = 53.2^{\circ}K, \text{ and } \sigma = 2.67\text{\AA}.$ 15
5.	Krypton percent deviation curve $\left[\left(\frac{\lambda_{exp} - \lambda_{calc}}{\lambda_{calc}}\right) \times 100\right]$
	calculated from the m-6 potential function, m = 17, $\epsilon/k = 226.0$ °K, and $\sigma = 3.50$ Å
,	$\Gamma(\lambda_{\rm exp} - \lambda_{\rm exp}) = 1$
ь.	Xenon percent deviation curve $\left[\frac{exp}{\lambda_{calc}} \right] \times 100$
	calculated from the m-6 potential function, $m = 24$,
	$\sigma = 3.73$ and $\sigma = 3.73$ 17

LIST OF TABLES

I.	Best values of the Lennard-Jones parameters obtained for neon, krypton, and xenon	9
II.	Best functions and the parameters for neon, krypton, and xenon	10
III.	Viscosity and thermal conductivity of gaseous neon	18
IV.	Viscosity and thermal conductivity of gaseous krypton	19
V.	Viscosity and thermal conductivity of gaseous xenon	20

•

THE VISCOSITY AND THERMAL CONDUCTIVITY COEFFICIENTS OF DILUTE NEON, KRYPTON, AND XENON

H. J. M. Hanley and G. E. Childs

The coefficients of viscosity and thermal conductivity for dilute neon, krypton, and xenon were examined by a method already proved successful for dilute argon, oxygen, and nitrogen. This method selects a suitable potential function, and its parameters, which is then used to correlate theory with experimental data, given the kinetic theory expressions for the transport coefficients. The method has recently been expanded and generalized and the results of this general study are applied in this note. The potential functions examined were members of the m-6, Kihara, Exp: 6, and Morse families. It was found that the Kihara was most suitable for neon, and the m-6, with m = 17 and m = 24, was most suitable for krypton and xenon, respectively. Viscosity and thermal conductivities were calculated from these functions and tables are given between 100 and 1000°K.

Key Words: dilute gases, neon, krypton, xenon, transport coefficients, correlations, m-6, Kihara, Exp: 6, Morse, potential functions.

1. INTRODUCTION

In this note we correlate transport coefficients of dilute neon, krypton, and xenon by applying a method which has been discussed and shown to be successful in previous publications for argon $[1, 2]^{\dagger}$ and for oxygen and nitrogen [3]. Experimental transport coefficients for these gases were correlated by means of the rigorous kinetic theory expressions and a suitable intermolecular potential function. Recently this method has been considerably expanded and can now be generalized for <u>any</u> given potential function and for <u>any</u> property [4], provided that theoretical tables for the potential and the property can be calculated.

Numbers in brackets refer to references.

(Specifically, the properties second virial coefficient, Joule-Thomson coefficient, viscosity and diffusion coefficients; and the families m-6, Kihara, Exp: 6, and Morse were considered). The general study is not yet complete but three conclusions have resulted from it which are relevent to this note because they enable the correlation procedure to be considerably simplified. The conclusions are taken to be correct.

We first define a reduced temperature T^* by the relation $T^* = T/(\varepsilon/k)$, where T is the absolute temperature, ε is the value of the maximum energy of attraction between two molecules for a given potential function, and k is Boltzmann's constant. We frequently refer to the temperature reduced with respect to the 12-6 (Lennard-Jones) potential, T^*_{12-6} ; this choice is a matter of convenience because values of $(\varepsilon/k)_{12-6}$ are known for most common substances, at least to a first approximation.

The conclusions from the general study can be stated: 1. It appears impossible to distinguish between one reasonable intermolecular potential function and another in the reduced temperature range of about 2.0 < T_{12-6}^{*} < 5.0[‡].

2. If a potential function of one family correlates data in a particular manner, it appears that a member of another family can always be chosen that will correlate the data in a similar manner. This is especially true for the temperature range $1.5 < T_{12-6}^* < 10.0$. This conclusion obviously includes the result of conclusion 1 above.

+

By "reasonable" we mean that the function is based on a model believed to approximate the real situation. The conclusions, therefore, may not be valid for such relatively simple models as the square well, triangular well, and so on.

3. It seems that it is impossible to find a three-parameter function that will satisfactorily correlate transport data over the temperature range of approximately $1.0 < T_{12-6}^* < 20.0$. This is a very wide range; for argon, for example, it is $125 < T^{\circ}K < 2,500$.

Also, preliminary calculations have indicated that the ability to distinguish between one function and another, which is already negligible between $2.0 < T_{12-6}^* < 5.0$, is further reduced over a wider temperature range if the data have a random error of about 0.5% or more.

It is not intended to discuss the general validity of these conclusions in this article, but we indicate the validity of 1 and 2 for transport processes by considering results from our previous investigations [1, 2, 3]. Consider first conclusion 2 for the special case of argon. Curve a, Fig. 1, shows the deviation curve obtained when the viscosity coefficient was correlated with the Kihara function [1]. We have now found that this deviation curve is essentially duplicated when a member of the m-6 family was used, m = 17 in this case (curve b). Undoubtedly a similar curve would have been obtained with a member of the Exp: 6 family. In other words, there most probably exists a value of α (the characteristic parameter of the Exp: 6 family) which will enable argon to be correlated in a similar manner; however, the necessary theoretical calculations for the Exp: 6 family are not yet complete.

With regard to conclusion 1 we can clearly demonstrate [Fig. 1 shown here; Fig. 2 of Ref. 1, and Figs. 5, 6, and 7 of Ref. 3] that in the range $2.0 < T_{12-6}^{*} < 5.0$, the m-6, Kihara, Exp: 6, and Morse functions all satisfactorily, and in like manner, correlate the data for argon, oxygen, and nitrogen.

The point we wish to emphasize is that in the range $1.5 < T_{12-6}^*$ < 10.0, there is a lack of uniqueness in the choice of the three-parameter function investigated [4]. So before starting to investigate



Fig. 1. Argon percent deviation curves $\left[\left(\frac{\eta_{exp} - \eta_{calc}}{\eta_{calc}}\right) \times 100\right]$. Curve a

is reproduced from Fig. 2 of Ref. 2 and was calculated from the Kihara function with $\gamma = 0.1$, $\varepsilon/k = 139.8^{\circ}K$ and $\sigma = 3.35\text{\AA}$. Curve b was calculated with the m-6 function, m = 17, $\varepsilon/k = 151.5^{\circ}K$ and $\sigma = 3.31\text{\AA}$. neon, krypton, or xenon, we can say that should we find that a particular potential function satisfactorily correlates the transport data in the temperature range $1.5 < T_{12-6}^* < 10.0$, we can be reasonably sure that this function is as suitable as any other function we might select. As mentioned above, this statement is based on studies of the m-6, Kihara, Exp: 6, and Morse functions—about all the common three-parameter functions in use at the present time.

The comment on the experimental requirements reinforces the decision made previously that it is best to study experimental viscosity data in order to determine a potential function and its parameters. Any attempt to select a potential function from experimental thermal conductivity data is not likely to be successful because thermal conductivity data are known to be less accurate.

2. THE POTENTIAL FUNCTIONS

The discussion in this note is restricted to the functions of four families: the m-6, the Kihara, the Exp: 6, and the Morse. The Kihara, in particular, has received much attention in the literature recently [5, 6,7], as has the Morse function which has been described by several authors [8,9]. The usage of the m-6 family is not as common as the others (although it contains the Lennard-Jones function) because of the difficulties in obtaining the tables of the collision integrals. Recently, however, these tables have become available [10].

If U(r) is the interaction potential of two molecules separated by a distance r, and ε is the maximum energy of attraction, or energy minimum, the potentials of the families are written:

m-6

$$U(r) = \varepsilon \left[\left(\frac{\sigma}{r} \right)^{m} - \left(\frac{\sigma}{r} \right)^{6} \right] / \left[\left(\frac{6}{m} \right)^{\frac{6}{m-6}} - \left(\frac{6}{m} \right)^{\frac{m}{m-6}} \right], \quad (1)$$

where σ is the value of r at U(r) = 0.

Kihara

$$U(r) = 4\varepsilon \left[\left(\frac{\sigma - a}{r - a} \right)^{12} - \left(\frac{\sigma - a}{r - a} \right)^{6} \right], r > a$$
 (2)

$$U(r) = \infty$$
, $r \leq a$;

here the finite size of the molecule is taken into consideration by including a core diameter, a. The reduced parameter γ , defined as a/σ , is the parameter characteristic of this family.

Exp: 6

$$U(r) = \frac{\varepsilon}{1 - 6/\alpha} \left[\frac{6}{\alpha} e^{\alpha (1 - r/r_m)} - (r_m/r)^6 \right], \quad (3)$$

where r_m is the value of r at the energy minimum, and α the family parameter which represents the steepness of the repulsive part of the function.

Morse

$$U(\mathbf{r}) = \varepsilon \left\{ \exp\left[-2\left(\frac{c}{\sigma}\right)\left(\mathbf{r} - \mathbf{r}_{m}\right)\right] - 2 \exp\left[-\left(\frac{c}{\sigma}\right)\left(\mathbf{r} - \mathbf{r}_{m}\right)\right] \right\}, (4)$$

where c is related to the curvature of the potential at $r = r_m$, and is the family parameter in this case.

3. KINETIC THEORY EXPRESSIONS FOR THE VISCOSITY AND THERMAL CONDUCTIVITY COEFFICIENTS

The kinetic theory for a dilute gas is formally complete[11,12]; the Chapman-Enskog treatment of the Boltzmann equation gives the viscosity and thermal conductivity coefficients in terms of collision integrals which are functions of the gas dynamics and thus of the intermolecular potential. It is the lack of knowledge of the latter which restricts the applicability of the kinetic theory expressions. These expressions are:

Viscosity (η)

$$\eta \, 10^{6} = \frac{26.693 \, (MT)^{\frac{1}{2}}}{R^{2} \Omega^{(2,2)} (T^{*})} f_{\eta} \qquad \text{g cm}^{-1} \, \text{sec}^{-1}, \qquad (5)$$

Thermal Conductivity (λ)

$$\lambda \ 10^{6} = \frac{832.24 \ (T/M)^{\frac{1}{2}}}{R^{2} \Omega^{(2,2)} (T^{*})} f_{\lambda} \qquad J \ cm^{-1} \ sec^{-1} \ deg^{-1}, \qquad (6)$$

where: M = molecular weight. (M = 20.183 for neon, M = 83.80 for krypton, M = 131.30 for xenon.)

R = a distance parameter, i.e.,
$$R \equiv \sigma$$
 for the m-6,
Kihara and Morse; and $R \equiv r_m$ for the Exp: 6.

$$T = the absolute temperature, °K.$$

 $\Omega^{(2,2)*}(T^*)$ = the reduced collision integrals (reduced by dividing by the integrals for the rigid sphere case) at the reduced temperature T^* , where $T^* = T/(\varepsilon/k)$ with k the Boltzmann constant.

The terms f_{η} and f_{λ} account for higher mathematical approximations to η and λ and are slowly varying functions of T^* which seldom differ from unity by more than about 0.5%. To be consistent with the accuracy of the experimental viscosity and thermal conductivity data especially at extreme temperatures, the terms can be omitted from Eqs (5) and (6) without significant error.

Appropriate tables of the collision integrals as a function of T^{*} for each of the families were taken from Refs. 7, 10, 12, and 13. The numerical values of the integrals depend on the method of integration which varies from one procedure to another, but it was verified that the choice of any particular set of tables made no significant difference to the results presented here.

4. EXPERIMENTAL DATA FOR NEON, KRYPTON, AND XENON

The experimental data were taken from the following references:

Neon, viscosity, Refs. 16, 17, 20, 22-26; temperature range 80 - 1100°K.

Krypton, viscosity, Refs. 22, 25, 27, 28; temperature range 283 - 972°K.

Xenon, viscosity, Refs. 22, 25, 28-30; temperature range 288 - 972°K.

Neon, thermal conductivity, Refs. 31-37; temperature range 90 - 579°K.

Krypton, thermal conductivity, Refs. 32, 33, 38; temperature range 171 - 579°K.

Xenon, thermal conductivity, Refs. 30, 32, 33, 38; temperature range 155 - 579°K.

5. METHOD OF CALCULATION AND RESULTS

5.1 VISCOSITY

The method for selecting a function and its parameters which will suitably correlate experimental data in conjunction with Eq (5) has been explained in detail in Refs. 1, 2, and 3. We investigated a particular function by first observing the variation of ϵ/k with T at a fixed R, then observing any subsequent changes caused by varying R. To do this, experimental values of η and the corresponding temperatures for a given gas were substituted in Eq (5) together with a sensible value for R, hence obtaining $\Omega^{(2,2)}^*$ as a function of T. An interpolation computer routine then generated T^{*} by inserting the calculated $\Omega^{(2,2)}^*$ into a given set of $\Omega^{(2,2)}^*$ (T^{*}) for the function. From T^{*} and the expression $\epsilon/k = T/T^*$, ϵ/k was then computed as a function of T. This procedure

was repeated for several values of R, varying R by about 10% overall. The same experimental data were used for all functions of the four families. The procedure was repeated for all the gases.

The best value of R was that value associated with the curve having the least variation of ϵ/k over the widest temperature range, allowing for the approximate 1% experimental and interpolation error. Values of ϵ/k were chosen to obtain agreement at 293°K for neon[20] and krypton[25] and 298°K for xenon[25]. We estimated ϵ/k to about 1% and R to about 0.2% for neon, but for krypton and xenon the estimation is about 2% and 1%, for ϵ/k and R, respectively. The higher possibility for error is due to the lack of data for these two gases. Table I gives the values of the Lennard-Jones parameters for each gas.

TABLE I

Best values of the Lennard-Jones parameters obtained for neon, krypton, and xenon

Gas	€/k, °K	• σ,Å
neon	47.0	2.72
krypton	182.8	3.62
xenon	249.5	3.96

We report that the variation of ε/k and R obtained here for neon, krypton, and xenon was essentially the same as that obtained in Refs. 1 and 3. We also report a marked lack of sensitivity in choosing a function in the temperature range 2.0 < T_{12-6}^* < 5.0 for all gases which is as it should be in view of conclusion 1 in the introductory remarks.

5.1.1 NEON

The experimental data are in the range 80 < T °K < 1100 which is equivalent to a reduced range of $1.7 < T_{12-6}^* < 23.4$. We repeat that a marked lack of sensitivity characterized the choice of a potential func-

tion in the range 2.3 < T_{12-6}^* < 5.0, where all functions essentially behave similarly. However, the functions behaved differently and gave different results in the range 5.0 < T_{12-6}^* < 27.0, but in view of conclusion 3 we did not expect to find a function that resulted in good agreement between experiment and theory over the <u>entire</u> temperature range. It was felt that the Kihara function with $\gamma = 0.1$ (Table II) was the best possible. The deviation curve is plotted in Fig. 2.

TABLE II

Best functions and the parameters for neon, krypton, and xenon

Gas	Function	€/k,°K	σ , Å
neon	Kihara (Y = 0.1)	53.2	2.67
krypton	m-6 (m = 17)	226.0	3.50
xenon	m-6 (m = 24)	382.3	3.73

It is assumed that functions of the m-6, Exp: 6, and possibly the Morse families also exist that could be used to obtain a similar deviation curve. At present we do not have complete tables of collision integrals for the values of α (Exp: 6) or c (Morse) that can completely verify this point, but application of the 16-6 member of the m-6 family ($\varepsilon/k = 68.4^{\circ}$ K, $\sigma = 2.60$ Å) gives a deviation curve which is practically identical with Fig. 2.

5.1.2 KRYPTON AND XENON

For these gases the experimental viscosity data lie between 280 and 975°K. In terms of reduced temperatures, therefore, the range for krypton is $1.5 < T_{12-6}^* < 5.3$, and for xenon $1.1 < T_{12-6}^* < 3.9$. It is at once clear that the problem is not so much the choice of a function which correlates the data, because we have an embarassment of choices, but rather to find a function that can predict data outside the present



Neon percent deviation curve $\left[\left(\frac{\eta_{exp} - \eta_{calc}}{\eta_{calc}}\right) \times 100\right]$ calculated from the Kihara potential function with $\gamma = 0.1$, $\varepsilon/k = 53.2^{\circ}K$ and $\sigma = 2.67$ Å. Fig. 2.

experimental range. The problem can be simplified because (conclusion 3) if a suitable function of a particular family can be found, then it is unlikely that the correlation can be satisfactorily improved upon considering another family from those for which collision integrals are available. Thus it is only really necessary to work with one family and the m-6 was selected for this purpose. We have shown that m = 16 is a suitable parameter for neon, and m = 17 for argon. If it is assumed that m increases with molecular weight, it can be expected that a value of at least m = 17 would be required for krypton and a higher value for xenon. From the collision integral tables available we selected m = 17 for krypton and m = 24 for xenon. Deviation curves are plotted in Fig. 3.

5.2 THERMAL CONDUCTIVITY

Thermal conductivities were calculated from Eq (6) using the functions and parameters determined from viscosity data as outlined above. Deviation curves are given in Figs. 4, 5, and 6 for neon, krypton, and xenon, respectively. It is well known that the scatter in experimental thermal conductivity coefficients between the results of different workers is large (about 5%) and the graphs indicate that the correlation is satisfactory.

6. CONCLUSION

The deviation curves verify that the kinetic theory expressions adequately correlate the experimental data available above 100°K, allowing for the estimated error in the data. The data for krypton and xenon are in a temperature range which does not allow us to choose a potential function that can be proved to be satisfactory over the complete temperature range considered, 100 to 1000°K. Although a sensible guess was made when selecting the function used for these latter gases, there must, of course, be some uncertainty in the theoretical transport coefficients calculated for temperatures outside the range of the data.

Tables of the viscosity and thermal conductivity in the temperature range 100 to 1000°K were computed for all gases, and they are given in Tables III, IV, and V for neon, krypton, and xenon, respectively. The viscosity tables are estimated to be accurate to 2% and the thermal conductivity tables accurate to 5%.

7. ACKNOWLEDGMENT

We would like to thank Dr. Max Klein for valuable discussions. This work was supported by a grant from NASA, Contract Number R-06-006-046.















TABLE III VISCOSITY AND THERMAL CONDUCTIVITY OF GASEOUS NEON[†]

TEMPERATURE	VISCOSITY	THERMAL	TEMPERATURE	VISCOSITY	THERMAL
к	G/CM-SEC 7106	J/CM-SEC-DEG X106	к	G/CM-SEC η106	J/CM-SEC-DEC λιο ⁶
			500	441.8	682.6
			510	447.5	691.3
			520	458.7	708.5
			540	464.1	716.9
			550	469.6	725.4
			570	480.4	742.1
			580	485.7	750.4
			540	491.1	/58+6
100	140.6	217.2	600	496.4	766.8
120	152+2	235+1	620	506.8	783.0
130	174.0	268.7	630	512.0	791.0
140	184.4	284.8	640	517.2	798.9
150	194.3	300.2	650	522.2	806.7
160	204.0	315.1	660	527.4	814.7
180	222.4	343.5	680	537.4	830.2
190	231.2	357.2	690	542.4	837.9
200	239.8	370.4	700	547.4	845.6
210	248.2	383.4	710	552.3	853.3
230	264.5	408.6	720	562.2	868.4
240	272.4	420.8	740	567.0	876.0
250	280.1	432.6	750	571.8	883.4
260	287.6	444.4	760	576.6	890.7
280	302.4	467.1	780	586.2	905.6
c90	309.5	478.2	790	590.9	912.9
300	316.7	489.2	800	595.7	920.2
310	323.7	500.0	810	600.4	927.4
330	337.4	521.2	830	609.7	941.9
340	344.1	531.5	840	614.3	949.0
350	350.7	541.7	850	619.0	956 • 2
360	357.2	551.9	860	623.5	963.2
380	370.0	571.6	870	632.7	977.3
39(1	376.4	581.4	890	637.2	984.3
400	382.6	591.1	900	641.7	991.3
410	388.8	600.6	910	646.2	998.3
420	401.0	619.1 619.4	920	655.2	1005+2
440	407.0	628.7	940	659.6	1018.9
450	412.9	637.9	950	664.0	1025.8
460	418.8	647.0	960	668.4	1032.6
480	424.1	656.0	970	672.7	1039.2
490	436.2	673.8	990	681.5	1052.7
			1000	684.9	1058.0

† Calculated for the dilute gas by the Kihara potential with $\gamma = 0.1$, $\sigma = 2.67$ Å, $\varepsilon/k = 53.2$ °K.

TABLE IV

VISCOSITY AND THERMAL CONDUCTIVITY OF GASEOUS KRYPTON[†]

TEMPERATURE	VISCOSITY	THERMAL CONDUCTIVITY	TEMPERATURE	VISCOSITY	THERMAL CONDUCTIVITY
к	G/CM-SEC 7106	J/CM+SEC=DEG λιο ⁶	к	G/CM-SEC ηι0 ⁶	J/CM-SEC-DEG λιο ⁶
			Eas	202 6	146-1
			510	398.8	148+4
			520	404.9	150.7
			530	411.0	152.9
			540	417.0	155.1
			550	422.9	157.3
			560	428.8	159.5
			570	434.6	161.7
			500	440.4	165.8
			590		100+0
100*	90.3	33.6	600	451.8	168.1
110*	98.6	36.7	610	457.4	170.2
120*	105.9	39.0	620	40J.U 469 5	174.7
140*	123.6	46.0	640	473.9	176.3
150*	132.1	49.1	650	479.4	178.4
160*	140.5	52.3	660	484.9	180.4
190+	148.9	55+4	670	490.2	186.4
190*	165.8	61.7	690	500.8	186.3
500*	174.2	64.8	700	506.1	188.3
210*	182.6	67.9	710	511.3	190.2
220*	191.0	71.0	720	516.5	192.1
240*	207.3	74.1	730	526.7	194.0
240	207.05		.40	528.7	17000
250*	215.4	80.1	750	531.8	197.8
260*	223.4	83.1	760	536.8	199.7
270	231.4	86.1	770	. 541.8	201.6
280	239.3	89.0	780	546.7	203.4
590	247.1	91.9	790	551.7	205+2
300	254.9	94.8	800	556.6	207.1
310	262.5	97.7	810	561.4	208.9
320	270.1	100.5	820	566.3	210.7
330	277.5	103.4	830	571.1	212+5
	20417	10010	040	51549	21403
350	292.2	108.7	850	580.6	216.0
360	299.4	111.4	860	585.4	217.8
370	306.5	114.0	870	590.0	219.5
380	313.6	116.7	880	594.7	221+3
340	320+5	114.3	040	577.4	223.0
400	327.5	121.8	900	604.0	224 • 7
410	334.3	124.4	910	608.5	226 • 4
420	341.0	126.9	920	613.0	228 • 1
430	34/0/	129.4	930	622.2	229.8
~~0	55404	19142	740		20100
450	360.9	134.3	950	626.7	233.2
460	367.4	136.7	960	631.1	234 · B
470	373.8	139+1	970	635.6	236.5
480	380.2	141.4	980*	644-4	239.8
, U	20010				
			1000*	647.7	241.0

[†] Calculated for the dilute gas by the m-6 potential with m = 17, $\sigma = 3.50$ Å, $\varepsilon/k = 226.0$ °K.

^{*} There is some uncertainty in these transport coefficients because they have been extrapolated outside the range of the experimental data.

TABLE V

VISCOSITY AND THERMAL CONDUCTIVITY OF GASEOUS XENON[†]

κ $6/CM-SEC$ $J/CM-SEC-DEG$ κ $0/CM-SEC$ $J/CM-SEC$ 500 $573, 6$ $86, 1$ 510 $573, 6$ $86, 1$ 520 $372, 6$ $86, 1$ 520 $372, 6$ $86, 1$ 520 $376, 1$ $86, 1$ $90, 1$ 560 $364, 7$ $90, 1$ 510 $575, 0$ $166, 7$ $90, 1$ $223, 0$ 610 $428, 7$ 100 100^+ $89, 4$ $21, 2$ 6000 $428, 7$ 100 100^+ $89, 4$ $21, 2$ 6000 $428, 7$ 100 100^+ $89, 4$ $21, 2$ 6000 $428, 7$ 100 120^+ $103, 9$ $224, 7$ 6200 $450, 7$ 100 120^+ $1325, 2$ $29, 7$ 6600 $457, 7$ 100 110^+ $1325, 2$ $31, 6$ $600, 7$ 1111 100^+ 110^+ 110^+ 120^+ 110^+	TEMPERATURE	V15COS1TY	THERMAL CONDUCTIVITY	TEMPERATURE	VISCOSITY	THERMAL CONDUCTIVITY
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	к	G/CM-SEC	J/CM-SEC-DEG	к	G/CM-SEC	J/CM-SEC-DEG
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		7 ¹⁰⁰	λ10°		7100	y 106
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				500	367.3	87.2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				510	373.6	88.7
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				520	379.9	90.2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				530	386.1	91.7
$\begin{array}{c c c c c c c c c c c c c c c c c c c $				540	392.3	93.7
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				55.0	398.5	94.6
$\begin{array}{c c c c c c c c c c c c c c c c c c c $				560	404.7	96.1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				570	410.8	97.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				580	416.8	99.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				590	422.8	100.4
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	100*	89.4	21.2	600	428.7	101.8
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	110*	96.7	23.0	610	434.6	103.2
136* 111.1 26.4 636 446.2 106 $140*$ 118.2 28.1 640 452.0 107 $150*$ 125.4 31.4 650 457.7 106 $160*$ 132.4 33.1 670 460.0 111 $190*$ 153.7 36.5 690 490.2 114 $200*$ 160.9 38.2 700 484.8 115 $210*$ 180.9 39.9 710 491.2 116 $220*$ 195.2 41.3 720 590.7 119 $230*$ 186.6 46.7 750 512.9 121 $260*$ 203.8 46.4 760 518.2 120 $270*$ 231.8 46.4 760 518.2 120 $270*$ 231.8 50.1 770 534.0 126 300 232.4 55.2	120*	103.9	24.7	620	440.4	104.6
140° 118.2 28.1 640 452.0 107 150° 125.2 29.7 650 457.7 108 160° 132.4 31.4 660 463.4 110 180° 132.4 31.4 660 463.4 110 180° 146.6 34.8 660 474.7 112 190° 153.7 36.5 690 486.8 115 210° 168.0 39.9 710 491.2 116 220° 175.2 41.6 720 496.7 119 240° 189.5 45.0 740 507.5 120 250° 196.6 46.7 750 518.2 121 70° 231.0 55.2 810 544.3 126 70° 225.3 53.5 790 534.0 126 70° 226.4	130*	111.1	26.4	630	446.2	106.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	140*	118.2	28.1	640	452.0	107.3
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	150*	125.2	29.7	650	457.7	108.7
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	160*	132.4	31.4	660	463.4	110.0
180^{*} 146.6 34.8 660 474.7 112 190^{*} 153.7 36.5 690 480.2 114 200^{*} 160.9 38.2 700 485.8 115 210^{*} 160.9 39.9 710 491.2 116 220^{*} 175.2 41.6 720 496.7 118 239^{*} 182.4 43.3 730 502.1 119 240^{*} 199.5 45.0 740 507.5 120 250^{*} 203.8 48.4 760 512.9 121 260^{*} 203.8 48.4 760 518.2 123 270^{*} 211.0 50.1 770 523.5 124 280 218.2 51.4 780 528.8 125 300 232.4 55.2 800 539.2 128 310 239.4 56.8 410 544.3 129 320 22	170*	139.5	33.1	670	469.0	111.4
190* 153.7 36.5 690 480.2 114 200* 160.9 38.2 700 485.8 115 210* 168.0 39.9 710 491.2 116 720* 175.2 41.6 720 496.7 118 720* 175.2 41.6 720 496.7 118 720* 195.5 45.0 740 507.5 120 760* 203.8 48.4 760 518.2 123 70* 21.9 50.1 770 523.5 124 70* 21.9 51.4 770 523.5 124 700 225.3 53.5 790 534.0 126 300 232.4 55.2 800 544.3 129 310 239.4 56.8 410 544.3 129 320 26.5 61.9 840 559.7 132 350 267.4 63.5	180*	146.6	34.8	680	474.7	112+7
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	190*	153.7	36.5	690	480.2	114.0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	200*	160.9	38.2	700	485.8	115.3
220^{+} 175.2 41.6 720 496.7 118 230^{+} 189.5 43.3 730 502.1 119 240^{+} 189.5 45.0 740 507.5 120 250^{+} 203.8 48.4 760 518.2 123 270^{+} 211.0 50.1 770 523.5 124 280 218.2 51.4 780 528.6 125 290 222.4 55.2 800 539.2 128 300 232.4 55.2 800 539.2 128 310 239.4 56.8 810 544.3 129 320 246.4 58.5 820 544.5 130 330 253.5 60.2 830 554.6 131 340 260.5 61.9 840 559.7 132 350 267.4 63.5 850 564.6 134 360 274.3 65.1 860 569.7 135 370 281.3 66.8 870 579.6 137 390 295.0 70.0 890 584.6 138 400 301.8 71.7 910 599.5 140 410 306.6 73.3 910 599.5 140 420 315.3 74.9 920 599.1 142 430 321.9 76.4 930 613.5 145 460 328.5 78.0 940	210*	168.0	39.9	710	491.2	116.7
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	720*	175.2	41.6	720	496.7	118.0
240^{+-} 189.5 45.0 740 507.5 120 250^{+-} 196.6 46.7 750 512.9 121 260^{+-} 203.8 484.4 760 518.2 123 270^{+-} 211.0 50.1 770 523.5 124 280 218.2 51.3 780 528.8 125 290 222.3 53.5 790 534.0 126 310 239.4 56.8 810 544.3 129 320 246.4 58.5 820 549.5 130 330 253.5 60.2 830 554.6 131 340 260.5 61.9 840 559.7 132 350 267.4 63.5 850 564.6 134 360 274.3 65.1 860 569.7 135 370 281.3 66.8 870 574.7 136 380 28	230*	182.4	43.3	730	502.1	119.2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	240*	189.5	45.0	740	507.5	120.5
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	250*	196.6	46.7	750	512.9	121.8
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	260*	203.8	48.4	760	518.2	123+1
280 218.2 51.8 780 528.8 125 290 225.3 53.5 790 534.0 126 300 232.4 55.2 800 539.2 128 310 239.4 56.8 810 544.3 129 320 244.4 58.5 820 549.5 130 330 253.5 60.2 830 554.6 131 340 260.5 61.9 840 559.7 132 350 267.4 63.5 850 564.6 134 360 274.3 65.1 860 569.7 135 370 281.3 66.8 870 574.7 136 380 288.1 68.4 880 579.6 137 390 295.0 70.0 890 584.6 138 400 301.8 71.7 900 589.5 140 410 308.6 73.3 910 594.3 141 420 315.3 74.9 920 599.1 142 430 328.5 78.0 940 608.7 144 450 335.1 79.6 950 613.5 145 460 341.6 81.1 960 613.5 145 460 354.5 8.2 980^* 622.9 147 480 354.5 8.2 980^* 622.6 149 490 360.9 85.7 990^* 622.2	270*	211.0	50.1	770	523.5	124.3
290 225.3 53.5 790 534.0 126 300 232.4 55.2 800 539.2 128 310 239.4 56.8 810 544.3 129 320 246.4 58.5 820 549.5 130 330 253.5 60.2 830 554.6 131 340 260.5 61.9 840 559.7 132 350 267.4 63.5 850 564.6 134 360 274.3 65.1 860 579.6 137 370 281.3 66.8 870 574.7 136 380 288.1 68.4 890 579.6 137 390 295.0 70.0 890 584.6 138 400 301.8 71.7 900 589.5 140 410 308.6 73.3 910 594.3 141 420 315.3 74.9	280	218.2	51.8	780	528.8	125.6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	290	225.3	53.5	790	534.0	126.8
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	300	232.4	55.2	800	539.2	128.0
320 246.4 58.5 820 549.5 130 330 253.5 60.2 830 554.6 131 340 260.5 61.9 840 559.7 132 350 267.4 63.5 850 564.6 134 360 274.3 65.1 860 569.7 135 370 281.3 66.8 870 574.7 136 380 288.1 66.8 870 574.7 136 390 295.0 70.0 890 584.6 138 400 301.8 71.7 900 589.5 140 410 308.6 73.3 910 594.3 141 420 315.3 74.9 920 599.5 140 440 328.5 78.0 940 608.7 144 450 341.6 81.1 960 613.5 145 460 341.6 81.1 <t< td=""><td>310</td><td>239.4</td><td>56.8</td><td>810</td><td>544.3</td><td>129.3</td></t<>	310	239.4	56.8	810	544.3	129.3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	320	246.4	58.5	820	549.5	130.5
340 260.5 61.9 840 559.7 132 350 267.4 63.5 850 564.6 134 360 274.3 65.1 860 569.7 135 370 281.3 66.8 870 574.7 136 380 288.1 68.4 880 579.6 137 390 295.0 70.0 890 584.6 138 400 301.8 71.7 900 589.5 140 410 308.6 73.3 910 594.3 141 420 315.3 74.9 920 599.1 142 430 328.5 78.0 940 608.7 144 450 335.1 79.6 950 613.5 145 460 341.6 81.1 960 618.2 146 450 335.1 79.6 950 613.5 145 460 341.6 81.1 <t< td=""><td>330</td><td>253.5</td><td>60.2</td><td>830</td><td>554.6</td><td>131+7</td></t<>	330	253.5	60.2	830	554.6	131+7
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$.340	260.5	61.9	840	559.7	132.9
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	350	267.4	63.5	850	564.6	134.1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	360	274.3	65.1	860	569.7	135+3
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	370	281.3	66.8	870	574.7	136.5
390 295.0 70.0 890 584.6 138 400 301.8 71.7 900 589.5 140 410 308.6 73.3 910 594.3 141 420 315.3 74.9 920 599.1 142 430 321.9 76.4 930 604.0 143 440 328.5 78.0 940 608.7 144 450 335.1 79.6 950 613.5 145 460 341.6 81.1 960 618.2 146 470 348.1 82.7 970 622.9 147 480 354.5 84.2 $980*$ 627.6 149 490 360.9 85.7 $980*$ 627.6 149	380	288.1	68.4	880	579.6	137+6
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	390	295.0	70.0	890	584.6	138.A
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	400	301.8	71.7	900	589.5	140.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	410	308.6	73.3	910	594.3	141+1
430 321.9 76.4 930 604.0 143 440 328.5 78.0 940 608.7 144 450 335.1 79.6 950 613.5 145 460 341.6 81.1 960 618.2 145 460 341.6 81.1 960 618.2 145 480 354.5 84.2 980* 622.9 147 480 354.5 84.2 980* 627.6 149 490 360.9 85.7 990* 632.2 150	+20	315.3	74.9	920	599.1	142+3
440 328.5 78.0 940 608.7 144 450 335.1 79.6 950 613.5 145 460 341.6 81.1 960 618.2 146 470 348.1 82.7 970 622.9 147 480 354.5 84.2 980* 627.6 149 490 360.9 85.7 990* 632.2 150	430	321.9	76.4	930	604.0	143.4
450 335.1 79.6 950 613.5 145 460 341.6 81.1 960 618.2 146 470 348.1 82.7 970 622.9 147 480 354.5 84.2 980* 627.6 149 490 360.9 85.7 990* 632.2 150	440	328.5	78.0	940	608.7	144.5
460 341.6 81.1 960 618.2 146 470 348.1 82.7 970 622.9 147 480 354.5 84.2 980* 627.6 149 490 360.9 85.7 990* 632.2 150	450	335+1	79.6	950	613.5	145.7
470 348.1 82.7 970 622.9 147 480 354.5 84.2 980.* 627.6 149 490 360.9 85.7 990.* 632.2 150	460	341.6	81.1	960	610.2	146.8
480 354,5 84,2 980* 627,6 149 490 360,9 85,7 990* 632,2 150	470	348.1	82.7	970	622.9	147.9
490 360.9 85.7 990* 632.2 150	480	354.5	84.2	980*	627.6	149.0
	490	360.9	85.7	990*	632.2	150.1
1000* 635.4 150				1000*	635.4	150.9

[†] Calculated for the dilute gas by the m-6 potential with m = 24, $\sigma = 3.73$ Å, $\varepsilon/k = 382.3$ °K.

* There is some uncertainty in these transport coefficients because they have been extrapolated outside the range of the experimental data.

- H. J. M. Hanley, Comparison of the Lennard-Jones, Exp: ó, and Kihara Potential Functions from Viscosity Data of Dilute Argon, J. Chem. Phys. 44, 4219-22 (1966).
- H. J. M. Hanley, The Viscosity and Thermal Conductivity Coefficients of Dilute Argon between 100 and 2000°K, Natl. Bur. Std. Tech. Note No. 333 (March 1966).
- G. E. Childs and H. J. M. Hanley, The Viscosity and Thermal Conductivity Coefficients of Dilute Nitrogen and Oxygen, Natl. Bur. Std. Tech. Note No. 350 (October 1966).
- M. Klein, Determination of Intermolecular Potential Functions from Macroscopic Measurements, J. Res. Nat. Bur. Std. 70A, No. 3, 259-269 (1966); M. Klein and H. J. M. Hanley, to be published.
- J. A. Barker, W. Fock, and F. Smith, Calculation of Gas Transport Properties and the Interaction of Argon Atoms, Phys. Fluids 7, 897-903 (1964).
- J. S. Rowlinson, A Test of Kihara's Intermolecular Potential, Mol. Phys. 9, No. 2, 197-98 (1965).
- J. P. O'Connell and J. M. Prausnitz, Applications of the Kihara Potential to Thermodynamic and Transport Properties of Gases, ADVANCES IN THERMOPHYSICAL PROPERTIES AT EXTREME TEMPERATURES AND PRESSURES, 19-31, Am. Soc. Mech. Engr., New York (1965).
- S. E. Lovell and J. O. Hirschfelder, Tables of Collision Integrals for Gases Obeying the Morse Potential, University of Wisconsin Theoretical Chemistry Laboratory, WIS-AF-21 (June 1962), Contr. No. AF 33(657)-7311.
- D. D. Konowalow and S. Carra, Determination and Assessment of Morse Potential Functions for Some Nonpolar Gases, Phys. Fluids 8, 1585-89 (1965).
- 10. M. Klein and F. J. Smith, to be published.

- 11. S. Chapman and T. G. Cowling, THE MATHEMATICAL THEORY OF NON UNIFORM GASES, Cambridge (1964) 7th Printing.
- 12. J. O. Hirschfelder, C. F. Curtiss, and R. B. Bird, MOLECULAR THEORY OF GASES AND LIQUIDS, John Wiley & Sons, New York (1964) Second Printing.
- E. A. Mason and W. E. Rice. The Intermolecular Potentials for Some Simple Non-polar Molecules, J. Chem. Phys. <u>22</u>, 843-51 (1954).
- A. Michels, A. Botzen, and W. Schuurman, The Viscosity of Argon at Pressures up to 2000 Atmospheres, Physica 20, 1141-48 (1954).
- A. Van Itterbeek and O. Van Paemel, Measurements on the Viscosity of Argon Gas at Room Temperature and Between 90° and 55°K, Physica 5, 1009-11 (1938).
- 16. H. L. Johnston and E. R. Grilly, Viscosities of Carbon Monoxide, Helium, Neon, and Argon Between 80° and 300°K, Coefficients of Viscosity, J. Phys. Chem. 46, 948-63 (1942).
- M. Trautz and R. Zink, Die Reibung, Wärmeleitung und Diffusion in Gasmischungen. XII. Gasreibung bei höheren Temperaturen, (The Viscosity, Heat Conduction and Diffusion of Gas Mixtures. XII. The Viscosity of Gases at Higher Temperatures), Ann. Physik 7, 427-52 (1930).
- V. Vasilesco, Recherches Experimentales sur la Viscosite des Gaz aux Temperatures Elevees, (Experimental Research on the Viscosity of Gas at Elevated Temperatures), Ann. Phys. (Paris) 20, 137-76 (1945).
- G. P. Filippova and I. P. Ishkin, The Viscosity of Air, Nitrogen, and Argon at Low Temperatures and at Pressures up to 150 Atmospheres, Inzh. Fiz. Zh. Akad. Nauk Belorussk SSR <u>4</u>, 105-09 (1961).
- 20. R. Wobser and F. Müller, Die innere Reibung von Gasen und Dämpfen und ihre Messung im Höppler-Viskosimeter, (The Viscosity of Gases and Vapors and their Measurement with the Hoppler Viscometer), Kolloid-Beih. 52, 165-276 (1941).

- F. G. Keyes, The Heat Conductivity, Viscosity, Specific Heat and Prandtl Numbers for Thirteen Gases, Mass. Inst. of Technol., Proj. Squid, Tech. Rept. No. 37 (1952), DDC ATI 167 173.
- 22. A. O. Rankine, Über die Anderung der inneren Reibung der Gase der Argongruppe mit der Temperatur, (On the Variation with Temperature of the Viscosities of the Gases of the Argon Group), Physik. Z. 11, 745-52 (1910).
- R. S. Edwards, The Effect of Temperature on the Viscosity of Neon, Proc. Roy. Soc. (London) A119, 578-90 (1928).
- 24. M. Trautz and H. E. Binkele, Die Reibung, Wärmeleitung und Diffusion in Gasmischungen. VIII. Die Reibung des H₂, He, Ne, Ar und ihrer binaren Gemische, (The Viscosity, Heat Conduction and Diffusion in Gas Mixtures. VIII. The Viscosity of H₂, He, Ne, Ar and their Binary Mixtures), Ann. Physik 5, 561-80 (1930).
- J. Kestin and W. Leidenfrost, An Absolute Determination of the Viscosity of Eleven Gases over a Range of Pressures, Physica 25, 1033-62 (1959).
- 26. N. J. Trappeniers, A. Botzen, H. R. Van den Berg and J. Van Oosten, The Viscosity of Neon Between 25°C and 75°C at Pressures up to 1800 Atmospheres. Corresponding States for the Viscosity of the Noble Gases up to High Densities, Physica 30, 985-96 (May 1964).
- A. Nasini and C. Rossi, Viscosita di miscele di gas rari, (Viscosity of Rare Gas Mixtures), Gazz. Chim. Ital. <u>58</u>, 898-912 (1928).
- M. Rigby and E. B. Smith, Viscosities of the Inert Gases, Trans. Faraday Soc. 62, 54-58 (1966).
- 29. M. Trautz and R. Heberling, Die Reibung, Wärmeleitung und Diffusion in Gasmischungen. XXV. Die Inhere Reibung von Xenon und Seinen Gemischen mit Wasserstoff und Helium, (The Viscosity, Thermal Conductivity and Diffusion in Gas Mixtures. XXV. The Viscosity of Xenon and its Mixtures with Hydrogen and Helium), Ann. Physik 20, 118-20 (1934).

- E. Thornton, Viscosity and Thermal Conductivity of Binary Gas Mixtures: Xenon-Krypton, Xenon-Argon, Xenon-Neon and Xenon-Helium, Proc. Phys. Soc (London) 76, 104-12 (1960).
- 31. S. Weber, Über die Wärmeleitfähigkeit der Gase, (The Thermal Conductivity of Gas), Ann. Physik 82, 479-503 (1927).
- M. Curie and A. Lepape, Conductibilite thermique des gaz rares, (Thermal Conductivity of Rare Gases), J. Phys. Radium 2, 392-97 (1931).
- 33. W. G. Kannuluik and E. H. Carman, The Thermal Conductivity of Rare Gases, Proc. Phys. Soc. (London) B65, 701-09 (1952).
- 34. F. G. Keyes, Thermal Conductivity of Gases, Trans. ASME <u>76</u>, 809-16 (1954).
- 35. L. B. Thomas and R. C. Golike, A Comparative Study of Accommodation Coefficients by the Temperature Jump and Low-Pressure Methods and Thermal Conductivities of He, Ne, and CO₂, J. Chem. Phys. 22, 300-05 (1954).
- B. N. Srivastava and A. K. Barua, Thermal Conductivity of Binary Mixtures of Diatomic and Monatomic Gases, J. Chem. Phys. 32, 427-35 (1960).
- 37. J. V. Sengers, W. T. Bolk, and C. J. Stigter, The Thermal Conductivity of Neon Between 25°C and 75°C at Pressures up to 2600 Atmospheres, Physica 30, 1018-26 (1964).
- 38. F. G. Keyes, Thermal Conductivity of Gases, Trans. ASME 77, 1395-96 (1955).

-

.

U.S. DEPARTMENT OF COMMERCE WASHINGTON, D.C. 20230

OFFICIAL BUSINESS

POSTAGE AND FEES PAID U.S. DEPARTMENT OF COMMERCE