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**A CALIBRATION SERVICE FOR
COAXIAL REFERENCE STANDARDS
FOR MICROWAVE POWER**

Fred R. Clague

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TRADE NAME DISCLAIMER

Certain commercial components used in the calibration system are identified in this report in order to adequately document the design. Such use and identification do not imply recommendation or endorsement by NIST, nor do they imply that the identified items are necessarily the best available for the purpose.

A CALIBRATION SERVICE FOR COAXIAL REFERENCE STANDARDS FOR MICROWAVE POWER

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A calibration service at the National Institute of Standards and Technology (NIST) for coaxial microwave power reference standards is described. The service provides measurements of a reference standard's effective efficiency from 50 MHz to 18 GHz at a power of 10 mW. The NIST microwave power standards consist of both a microcalorimeter and an associated reference standard. The reference standard is a bolometric power detector (a thermistor mount). The only thermistor mounts accepted for measurement are those constructed to NIST specifications. These thermistor mounts and the automated microcalorimeter are described. A detailed error analysis with an estimate of the calibration uncertainties and their sources is included. The calibration uncertainty, which is quoted as a function of frequency, ranges from about 0.2 percent at 50 MHz to 0.4 percent at 18 GHz.

Key words: coaxial microwave power standard; microcalorimeter; microwave; microwave microcalorimeter; microwave power measurement; microwave power standard

1. INTRODUCTION

1.1 NIST Microwave Power Standards

The microwave power standards in use at the National Institute of Standards and Technology (NIST) consist of microcalorimeters and associated reference standards [1-4]. Each power standard is made up of both a microcalorimeter and a reference standard. The reference standards are substitution type bolometric power detectors. These detectors are generally called bolometer mounts or simply mounts. In this document the terms "reference standard," "bolometer mount," and "mount" are used interchangeably. Commercial bolometer mounts, especially coaxial units, are generally not suitable for use as a reference standard that is measured by the microcalorimeter. While they have been used by NIST in the past, the resulting calibration uncertainties were higher because of their use.

To meet the need in the microwave community for lower calibration uncertainty, a reference standard designed for use with the microcalorimeter is required. Figure 1.1 shows the coaxial microcalorimeter and the Type N thermistor mount used as the reference standard. This document includes a brief description of the microcalorimeter and the reference standard. Additional design and construction details for both the coaxial microcalorimeters and the bolometer mounts used as the reference standards are available as NIST Technical Notes [5, 6]. These references and those noted previously all include descriptions of the microcalorimeter and bolometer mount operation. However, for convenience a brief summary follows.

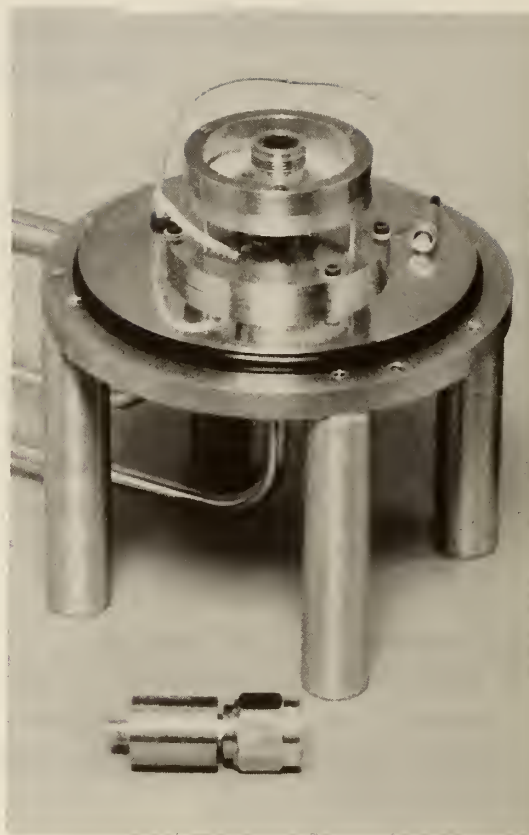


Figure 1.1 Coaxial microcalorimeter and coaxial reference standard.

1.2 Bolometer Mount-Microcalorimeter Operation

The bolometric power detector uses a heat sensitive resistor (bolometer) which terminates the transmission line and absorbs the microwave energy. Two types of bolometers are used: a platinum wire with a positive temperature coefficient called a barretter, and a thermistor bead with a negative temperature coefficient. The detectors are biased by an external source of dc current (power meter) to an operating resistance that produces a match with the characteristic impedance of the transmission line. Coaxial mounts typically use two bolometer elements which are connected in series for the dc bias, but are in parallel for the rf. Thus, to match the $50\ \Omega$ characteristic impedance of a coaxial transmission line, the pair is maintained at a series resistance of $200\ \Omega$. When microwave energy is applied to the mount, the dc bias supplied by the power meter is automatically reduced to maintain a constant operating resistance [7]. If all the microwave energy incident on the mount were absorbed by the bolometer elements, and if the elements were heated identically by equal amounts of dc and rf power, then the microwave power would be equal to the amount by which the dc power is reduced. This is called a substitution type power meter, because the rf power replaces a portion of the dc bias power. The substituted dc power (also called the bolometric power) is calculated using the equation

$$P_{dc} = \frac{V_1^2 - V_2^2}{R_0}, \quad (1-1)$$

where V_1 is the power meter output voltage (the dc voltage across the bolometer elements) with no rf, V_2 is the power meter output voltage with rf, and R_0 is the dc operating resistance of the bolometer pair (200 Ω for a coaxial mount).

The microwave energy incident on a mount is not all absorbed by the bolometer elements. The dielectric and conductor losses in the input connector, the input transmission line, and the bolometer mounting structure, plus any leakage from the mount result in a measurement error characterized by a correction factor called the mount efficiency. This efficiency is always less than 1. In addition, the bolometer elements are not heated identically by equal amounts of rf and dc power. This is known as the rf-dc substitution error. The combination of these two effects, which is measured by the microcalorimeter, is a correction factor defined as the effective efficiency η_e . The rf power absorbed at the input of the mount is calculated by dividing the substituted dc power by the effective efficiency. The mount's effective efficiency is independent of mismatch corrections, which are treated separately at the time of calibration transfer to an unknown mount.

The bolometer elements used in the reference standards are thermistors. Thermistors are rugged and resist burnout in the event of an rf overload. They are available commercially as a conveniently usable subassembly. Disadvantages to using thermistors include a continuous drift in the bias current even in a constant temperature environment. Also, thermistors are not usable in an alternative efficiency measurement technique known as the impedance method [8].

The microcalorimeter essentially measures the temperature rise of the bolometer mount connected to it. In the coaxial microcalorimeter, the mount's temperature increase is measured with a thermopile. During the measurement, the microcalorimeter is immersed in a stable temperature-controlled water bath [9, 10] to minimize the effect of external temperature changes. The measurement procedure determines the following at each frequency of interest: the power meter and thermopile output voltages (V_1 and e_1) with only dc applied to the mount, and then again (V_2 and e_2) with both rf and dc applied. The effective efficiency η_e is calculated at each frequency using the equation

$$\eta_e = g \frac{1 - \left(\frac{V_2}{V_1} \right)^2}{\frac{e_2}{e_1} - \left(\frac{V_2}{V_1} \right)^2}. \quad (1-2)$$

The g term is a frequency dependent correction factor for the microcalorimeter-bolometer mount combination. It is also known as the calorimetric equivalence correction. The uncertainty of the η_e measurement is determined primarily by the uncertainty in g . The determination of g is a major effort that is described in section 6 of this document.

A typical reference standard calibration is done at approximately 125 frequencies from 50 MHz to 18 GHz. Even with the automated system described in section 4, the measurement takes about 40 h. Figure 1.2 shows a typical thermopile output at a few frequencies. The value of η_e for one the reference standards, measured at 125 frequencies, is shown in figure 1.3. The expanded uncertainty in the η_e measurement as a function of frequency is shown in figure 1.4. The basis for determining the uncertainty and the method for combining the different components are also described in section 6.

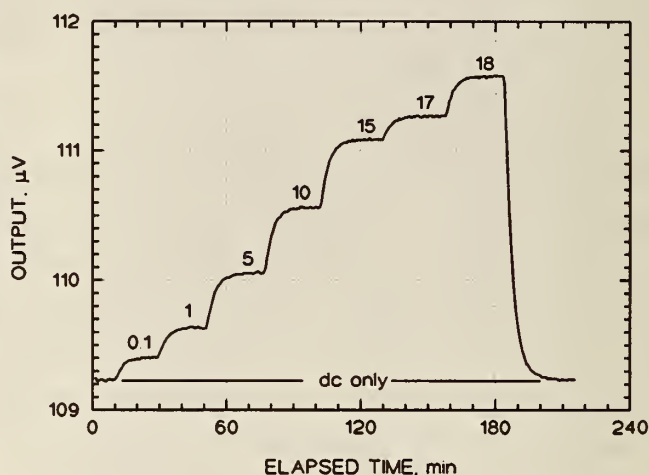


Figure 1.2 Thermopile output versus time for seven frequencies (in GHz).

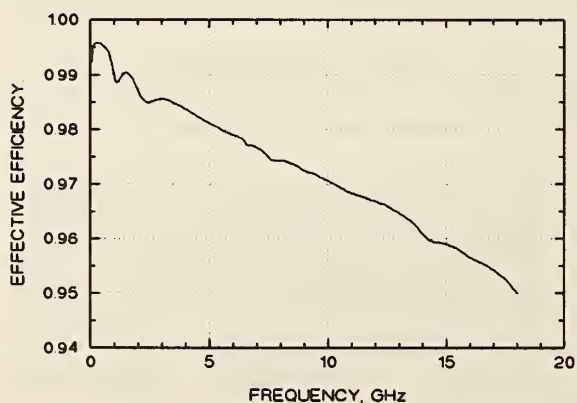


Figure 1.3 Effective efficiency of a Type N mount measured at 125 frequencies.

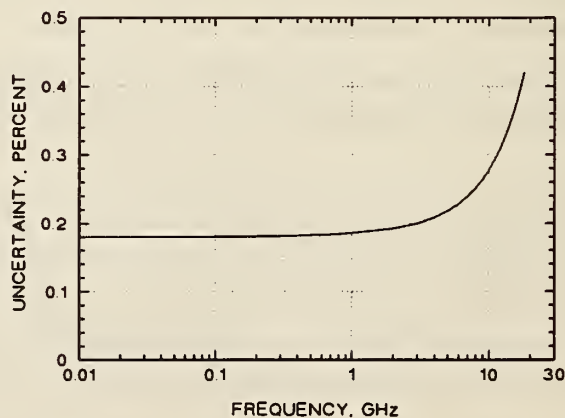


Figure 1.4 Expanded uncertainty for the Type N coaxial microcalorimeter when measuring the effective efficiency of a NIST Type N mount.

2. TYPE N AND APC-7 REFERENCE STANDARD DESIGN

The features of the bolometer mount described below are both desirable and necessary for the mount to be used as an optimum reference standard. The body of the mount and the internal thermistor bead assembly are both considered. Complete design and construction details are available in reference [5].

2.1 Mount Body Design

As noted in the introduction, the primary function of the microcalorimeter is to measure the effect of all microwave energy dissipated in the mount. To best accomplish this, there should be minimal thermal resistance between the heat sources and the measuring thermopile. Thus, the mount should be constructed of a material with a high thermal conductivity, and the thermal paths should be short as possible. Typical commercial mounts are constructed of nickel-plated or gold-plated brass and might also have stainless steel parts in the thermal path.

The transfer standard should have a high effective efficiency. This means a low rf-loss input transmission line made of high electrical conductivity material with low surface roughness ($\approx 0.5 \mu\text{m}$).

To meet these requirements, the mount body is constructed of tellurium copper, while the parts of the mount that involve the input transmission line (the outer conductor) are made of electroformed copper. The electrical conductivity of copper is nearly 3 times higher than brass and 30 times higher than stainless steel. The thermal conductivity is about 2.5 times higher than either brass or beryllium copper and 26 times higher than stainless steel. The electroformed parts provide a better outer conductor surface finish than can be obtained by machining.

The disadvantage of these two materials is that they are softer than beryllium copper or brass. This is more of a liability for the Type N mount (because of the vulnerable outer conductor of the connector) than for the APC-7 design. With careful handling, it is not a major problem with either design. Experience with one of the Type N mounts reveals no visible connector damage after more than 100 connections. All parts of the mount are gold plated to prevent deterioration of the surface characteristics, primarily thermal emissivity and electrical conductivity.

Valid measurements of the thermopile output and the power meter voltage cannot be made until the microcalorimeter and mount are in thermal equilibrium with the water bath, a condition indicated by a stable thermopile output. The time to reach stability may be lengthy: an average of 50 min per

measurement frequency (a typical calibration at 108 points can take about 90 h) on the commercial mounts because of their long thermal time constant. To minimize the effect of external temperature changes, all commercial mounts are typically massive and seek to thermally isolate the thermistor bead structures. Such design objectives are the opposite of those desired for use in the microcalorimeter. An effective way to speed the measurements is to minimize the thermal mass (heat capacity) of the bolometer mount by reducing the size and to eliminate the thermal isolation.

Both techniques are used in the mounts. For example, the mass of the new Type N mount is approximately one-third that of the commercial version previously used (53 g versus 142 g). The average measurement time per frequency for the new design is less than 30 min (see section 4).

The rf leakage from the bolometer mount is a first-order source of error in the measurement. The leakage energy, because it is not dissipated in the mount, is not detected by the bolometer elements or by the microcalorimeter thermopile. Leakage may radiate or conduct through mechanical joints in the mount body, the dc bias leads, or the rf input connector. Commercial mounts, which are adequate for their intended use, generally do not have low enough leakage for this application, where errors on the order of 0.01 percent are of concern.

The effort to minimize leakage has focused on rf containment by the mount body and the dc bias circuit. The shielding is accomplished by totally enclosing the mount and minimizing any gap that might allow leakage at a mechanical joint. Residual leakage from threaded joints can be further reduced by painting the seam with conductive epoxy or paint. Because of the thin wall of the mount body, the cap is not threaded. It is designed to be a tight press fit in the body; in fact, a special fixture is needed to remove the cap. Once it is determined that a newly constructed mount is operating properly, the cap seam can also be sealed with conductive epoxy or paint.

The internal rf bypass structure consists of a tubular pi-section (a pair of capacitors with a ferrite inductor) low-pass filter with an added external ferrite bead in each of four leads. A cross section of the dc feed-through structure is shown later as part of figure 2.1 and 2.2. The dc connection to the thermistor beads is through a miniature connector to allow the mount cap to be removed.

2.2 Thermistor Bead Assembly

As described earlier, the substitution type power meter measures power in terms of a change in the dc bias power. Any uncertainty in the bolometer dc resistance will be reflected as an error in the power

calculation. Lead or contact resistance in the dc bias circuit will generate such an error. The solution to this problem is a four-wire connection from the bolometer elements to a power meter which uses external sense leads such as the NIST Type IV power meter (made commercially by several manufacturers). The thermistor bead assembly used in the mount does have the required four-wire connection.

Coaxial bolometer mounts typically use a dual bolometer configuration. The elements are connected in series for the dc bias and in parallel for the rf. This simplifies the dc bias connection and also provides a good rf match to the 50 Ω transmission line. However, if the electrical characteristics of the two elements are not identical, a dc-rf substitution error in the power measurement results. For thermistor mounts, the error increases nonlinearly with rf power. The error is restricted to coaxial mounts since, in general, waveguide designs use a single element. The effect can be minimized by proper matching of the element pair. The beads in the assembly used are matched to 0.05 Ω at 165°C. The details of the dual-element error are presented in reference [11].

Another performance parameter for the mount, which is a function of the bead assembly, is the input reflection coefficient. A low reflection coefficient (less than 0.1) is not necessary for the microcalorimeter measurement, but it is important for reducing the uncertainty in the calibration transfer and for reducing the minimum power requirement on the microwave source.

Another desirable feature of the mount is that the η_e be a smooth function of frequency. Most thermistor mounts display resonances, or sharp narrow dips in η_e . Because η_e is changing very rapidly with frequency at these points, the random uncertainty is greater and interpolation between measured points is not possible. The resonance effect is the result of microwave leakage past the thermistor beads into the space that forms a cavity behind the thermistor bulkhead. The effect can be reduced or eliminated by filling the cavity with two layers of magnetic microwave absorber. The filling material is fastened in place to prevent movement which could change the η_e .

The thermistor bead structure with its unique four-wire connection is a commercial product. This greatly simplifies the construction of the mount. The choice of the particular commercial part does not represent an endorsement of the vendor or the product or imply that it is the best in this application.

2.3 Final Design

The final mechanical and electrical design features are indicated in the following two figures. Figure 2.1 is a cross sectional view of the Type N mount with the major parts identified. The same view of the APC-7 mount design is shown in figure 2.2.

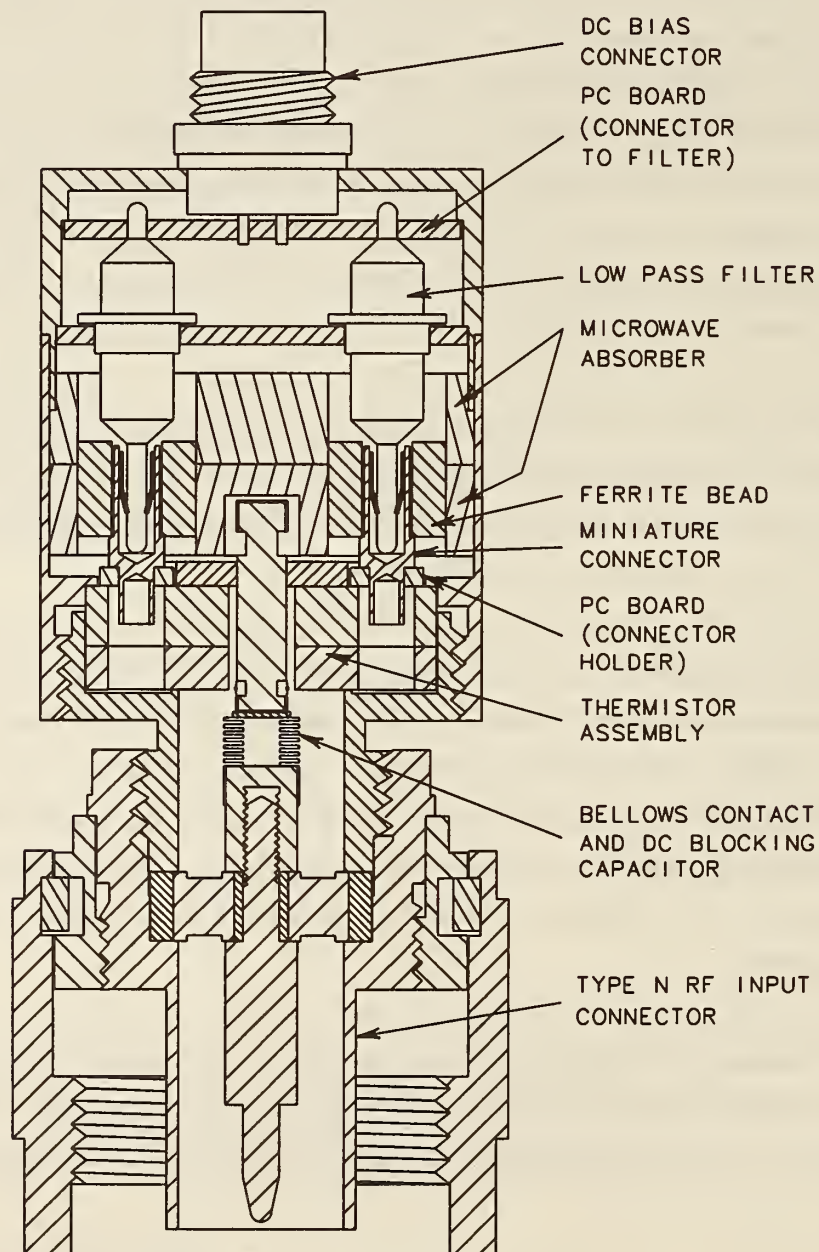


Figure 2.1. Cross section of the Type N thermistor mount.

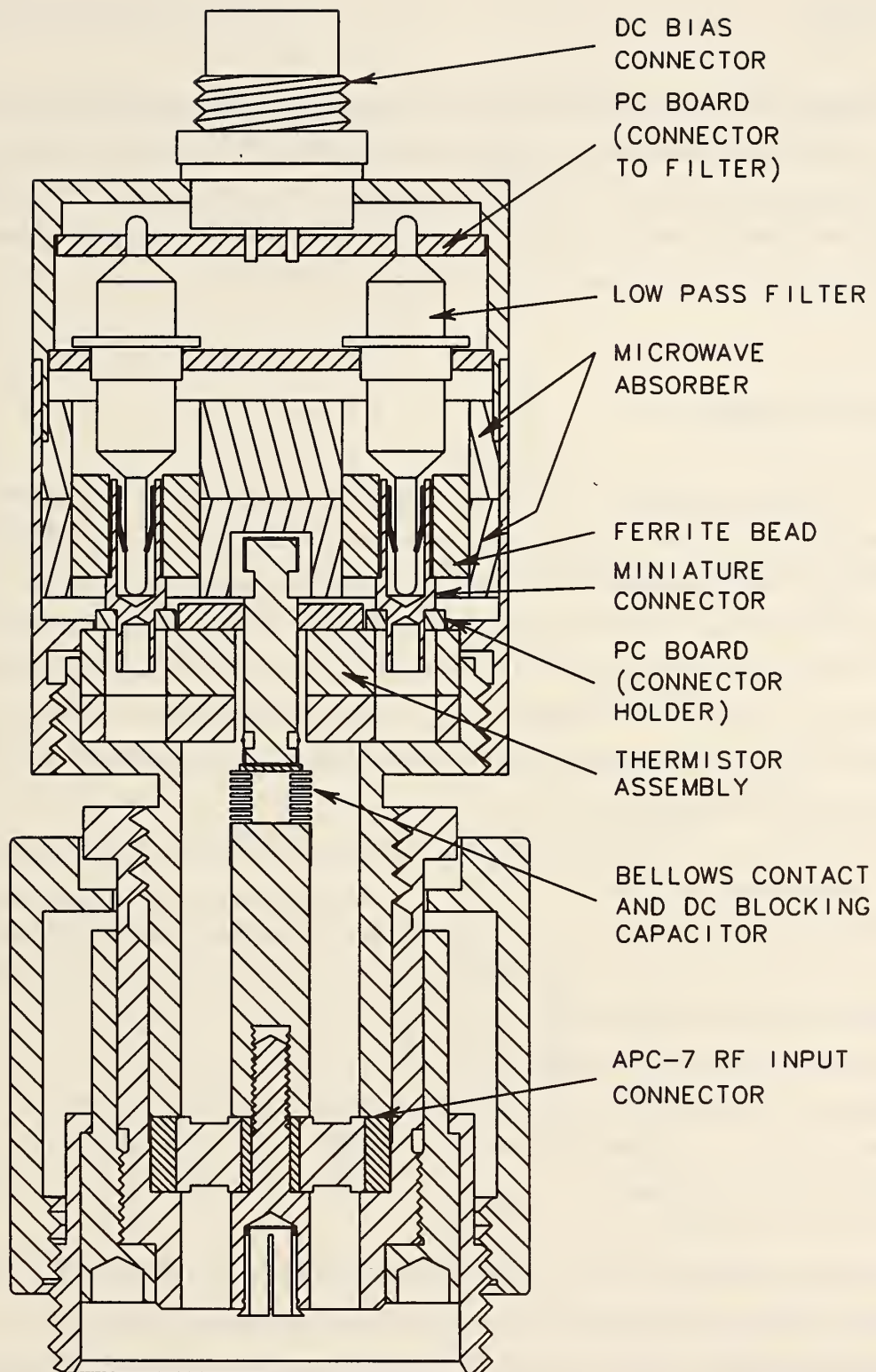


Figure 2.2 Cross section of the APC-7 mount.

2.4 Performance

Material presented in this section reports the measured performance of several samples of the Type N mount only. At the time of this publication, customer interest in an APC-7 service has not been sufficient to warrant constructing the mounts or evaluating the calorimeter. The parts, however, are in hand and can be assembled and evaluated if needed in the future. These measurements are thought to be typical and thus representative of future units. The basis of these performance measures was presented earlier in section 2.1.

2.4.1 Microwave Leakage

Detection of microwave leakage is relatively easy; accurate measurement of its magnitude is not. Development of special techniques and facilities such as the reverberation chamber and the TEM cell make such measurements potentially possible [12]. A reverberation chamber can be used to measure the energy above about 300 MHz (the low frequency limit is determined by the size of the available chamber) that is radiated from the mount and its connected dc bias cable. Energy that is conducted from the mount on the connecting dc bias cable can be measured using a vector voltmeter and a spectrum analyzer. Measurements on early prototype mounts show that most of the energy escaping from the mount is conducted away on the connecting cable, rather than radiated. Therefore, measurements were not made in the reverberation chamber.

Results shown in figure 2.3 were obtained from measurements on the mount using a vector voltmeter at the low frequencies and a spectrum analyzer above 1 GHz. The objective is to keep total leakage from the mount more than 40 dB below the input (less than 0.01 percent of the input). The figure indicates that this was achieved.

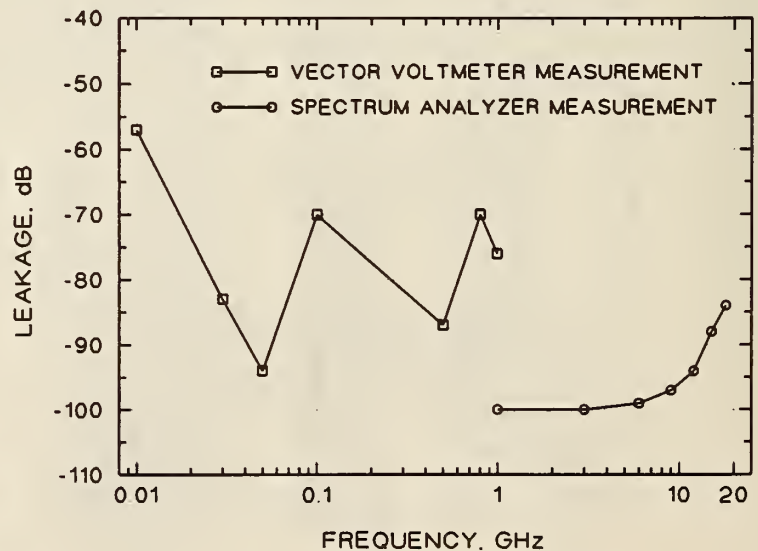


Figure 2.3. Microwave leakage in decibels below the input.

2.4.2 Input Reflection Coefficient

As previously indicated, it is desirable for the magnitude of the input reflection coefficient to be small. The measurements made by an automatic vector network analyzer (45 MHz to 18 GHz) and by a six-port network analyzer (10 MHz to 50 MHz) on a typical Type N mount are shown in figure 2.4. The magnitude is under 0.1 from about 20 MHz to 16.5 GHz.

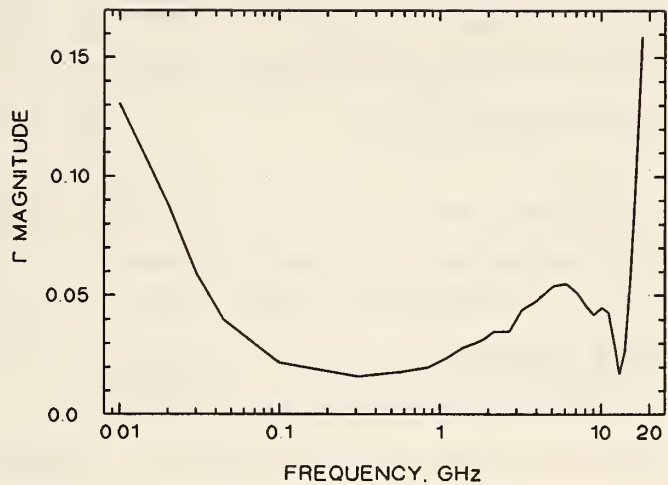


Figure 2.4. Type N mount reflection coefficient.

2.4.3 Dual Element Error

First, we note that if the mount is used at 10 mW, where it was calibrated, there is no error. However, if the mount is used as a reference standard to calibrate another system at a different power, say 1 mW, then there may well be an additional uncertainty in the measurement.

The only way to determine the magnitude of the dual-element error is by direct measurement. In theory, one possible measurement method is to connect the coaxial mount to one arm of a nominally equal power splitter (such as a 3 dB hybrid or a waveguide "magic tee"), and a single-element waveguide mount to the other arm. The ratio of the two bolometric powers is determined at 10 mW and again at a randomly selected power between 10 mW and 0.1 mW. The change in the ratios as determined at the two powers is a measure of the dual-element error. The process is repeated enough times to give a curve showing the nonlinearity as a function of power up to 10 mW.

The test of the procedure is to place identical model waveguide mounts on each arm of the power splitter to verify the linearity of the splitter and associated instrumentation. Figure 2.5 shows results of such a measurement with two identical model waveguide mounts at 9.1 GHz. The increased spread of the data as the power decreases is typical of bolometric measurements because of the small change in dc power that occurs at low microwave power.

The result for a commercial coaxial mount compared with one of the waveguide mounts is shown in figure 2.6. The error is very small at low power and increases to about 0.035 percent at 10 mW.

Unfortunately, most of the data taken using this technique do not give results comparable to figures 2.5 and 2.6. Considerable time has been put into the effort to reduce this approach to a reliable measurement technique. Thus far, it has not been successful. Generally, the results of the power splitter linearity tests have not provided the desired verification, so the comparisons between the coaxial mount and a waveguide mount are not too meaningful. The difficulty seems to be that when looking for deviations on the order of 0.01 percent, instrumentation problems such as the inability to locate the ground precisely where it should be in the dc measurement circuit are of the same order. At best, the comparison between the coaxial and waveguide mounts is in error by the amount of the apparent nonlinearity seen when comparing a waveguide mount to a waveguide mount.

Another way to determine the dual-element error is to measure the effective efficiency as

a function of power. Figure 2.7 shows that measurement on a Type N mount. The significant nonlinearity above about 12 mW is largely due to the dual-element error. At the lower powers the measurement uncertainty becomes large, so the shape of the curve is not necessarily accurate. A line fitted to the measured data between 5 mW and 12 mW is shown in figure 2.8. Based on this linear fit, the change in efficiency for this mount between 10 mW and 1 mW is less than 0.01 percent. This is a better estimate of the dual-element error than the power splitter method provides.

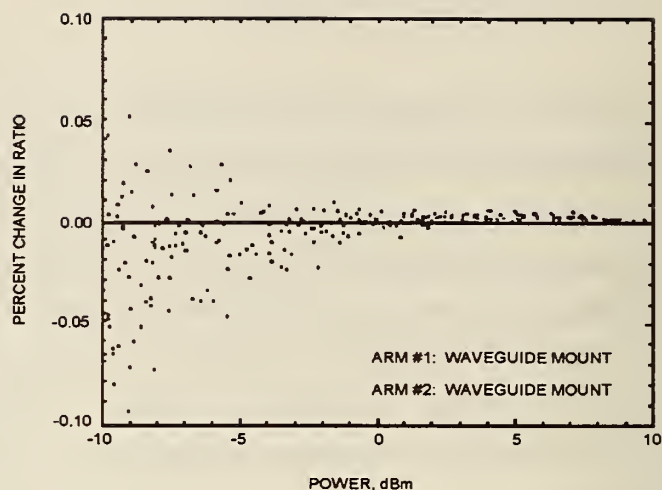


Figure 2.5. Change in the power ratio of two waveguide mounts versus power.

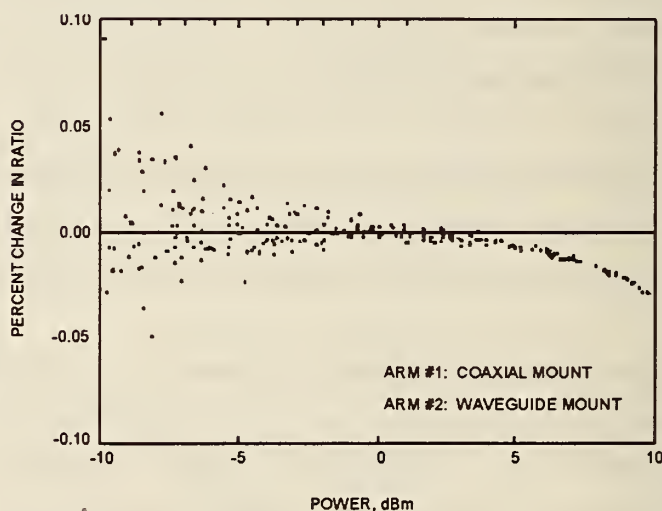


Figure 2.6. Change in the power ratio of a coaxial mount to a waveguide mount versus power.

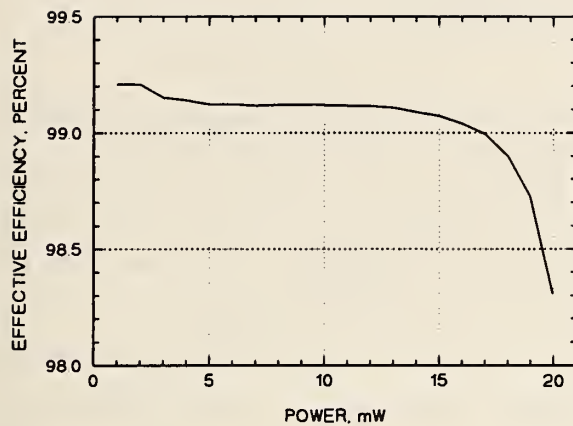


Figure 2.7. Effective efficiency as a function of power.

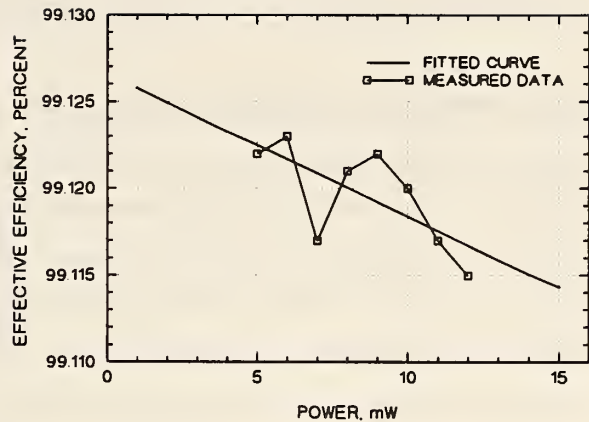


Figure 2.8. Linear fit to data of figure 2.7 from 5 to 12 mW.

2.4.4 Mount Settling Time

In figure 2.9, the upper trace is the output of a crystal detector monitoring a 10 GHz source as the rf is turned on for about 6 ms and then turned off. The lower trace is the power meter voltage of the coaxial thermistor mount as it measures the same output. Note the large "overshoot" excursions that occur for about 2 ms until a steady state is reached. These excursions may occur because the current distribution in the thermistor beads changes when rf is applied, so the heat distribution must also change. It takes a few milliseconds for a new thermal steady state to be reached. Thus the measurement of the power meter voltages should not be made until after the overshoot has subsided. The effect decreases with power and is independent of frequency.

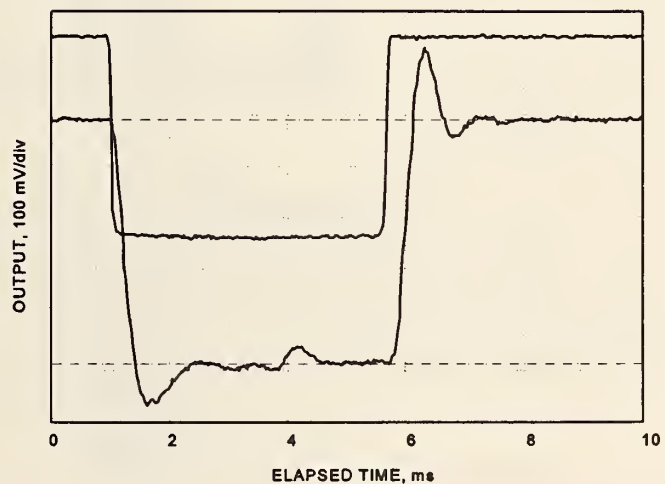


Figure 2.9. Crystal detector and mount output as rf power is switched on and off. The source output is 10 mW.

2.4.5 Effective Efficiency

A plot of the effective efficiency of one of the Type N mounts is shown in figure 1.3. The efficiency is well above 90 percent and decreases smoothly with frequency. Figure 2.10 is a plot of the effective efficiency of a mount before and after suppression of the resonant behavior with microwave absorber as described earlier.

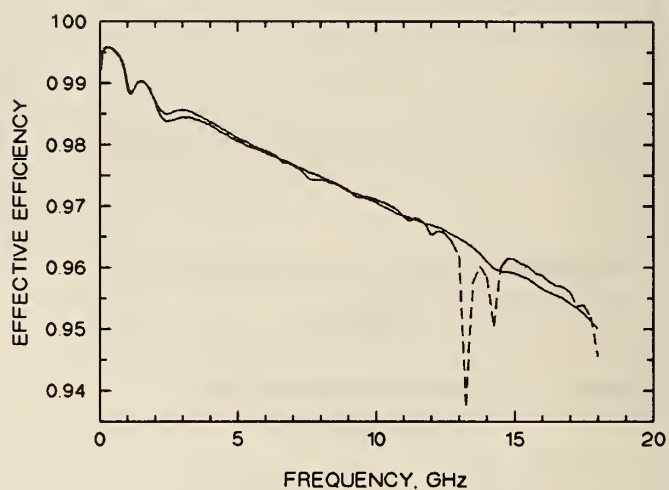


Figure 2.10. Effective efficiency of a Type N mount before (dashed line) and after resonance suppression.

3. MICROCALORIMETER DESIGN

As noted in section 1, the primary function of the microcalorimeter is to measure the effect of all microwave energy dissipated in the reference standard bolometer mount. This is accomplished by using a thermopile to measure the temperature rise of an attached bolometer mount with respect to a thermal reference ring under two conditions. The first condition is with dc only dissipated in the bolometer mount and the second condition is with both dc and rf dissipated in the mount. Because the temperature changes are very small (on the order of 0.05°C), the microcalorimeter is also designed to be immersed in a stable temperature-controlled water bath [9, 10] during the measurement to minimize the effect of external temperature changes. The water bath is controlled to about $\pm 20\ \mu^{\circ}\text{C}$ at near room temperature. Figure 3.1 is a cross sectional view of the base of the microcalorimeter with the major parts labeled. Complete design and construction details are available as reference [6].

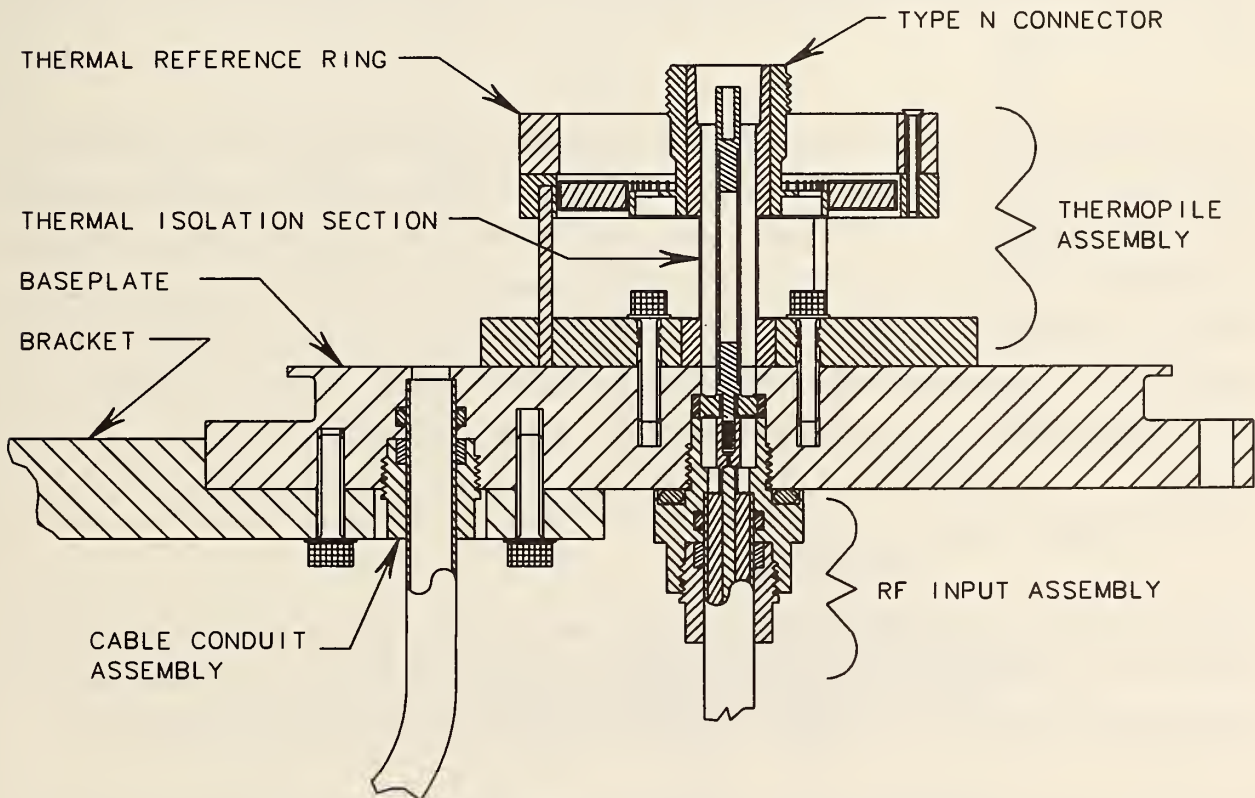


Figure 3.1. Cross section of the Type N microcalorimeter.

3.1 Thermopile Assembly

This part contains a thermal isolation section as well as the thermopile itself. The thermal isolation section, which is between the baseplate (in close contact with the water bath) and the bolometer mount, allows the mount temperature to rise with respect to the baseplate. The isolation section is a short length of coaxial transmission line made with a thin-wall copper outer conductor and a hollow thin-wall gold-plated stainless steel inner conductor.

The thermopile is a ring made of 66 equally spaced radial turns of Constantan wire; the lower half of the ring is copper plated giving 66 copper/Constantan junctions around both inner and outer circumferences. The ring of inner thermocouple junctions is in thermal contact with (but electrically insulated from) the 7 mm coaxial outer conductor just below the coaxial connector. The circle of outer thermocouple junctions is in contact with a thermal reference ring which approximates the thermal characteristics of the dummy reference standard used in the earlier twin-joule microcalorimeter design as described in references [1] and [2].

The thermocouples in the thermopile are connected in series, so the thermopile output can be increased by increasing the number of junctions. The number of thermocouples in the original thermopile was limited by the input range, 100 μV , of the potentiometer used to measure the thermopile output. Since the microcalorimeter described here uses the original thermopile assembly, it has less thermocouple junctions than it would otherwise. A thermopile with many more junctions and made of finer wire would be a better match to the 2 mV range of the modern electronic nanovoltmeter now used. A typical thermopile output at a few frequencies for one of the reference standards is shown in figure 1.2.

3.2 Other Design Features

The rf input leads, the mount's dc bias leads, and the thermopile's output leads are brought in through the bottom of the microcalorimeter. This provides a more convenient arrangement for removing the top cover and also keeps the leads in the water bath for a greater distance to provide better thermal tempering.

The entire assembly, including the cover, is gold plated for corrosion protection. The gold-plated interior of the cover is polished to provide a high infrared reflectivity. Figure 3.2 is a partial cross sectional view of the entire calorimeter with the cover raised. When in use the unit is suspended in the temperature-controlled water bath by the rod extending from the top of the cover. The actual water level when in the bath is indicated.

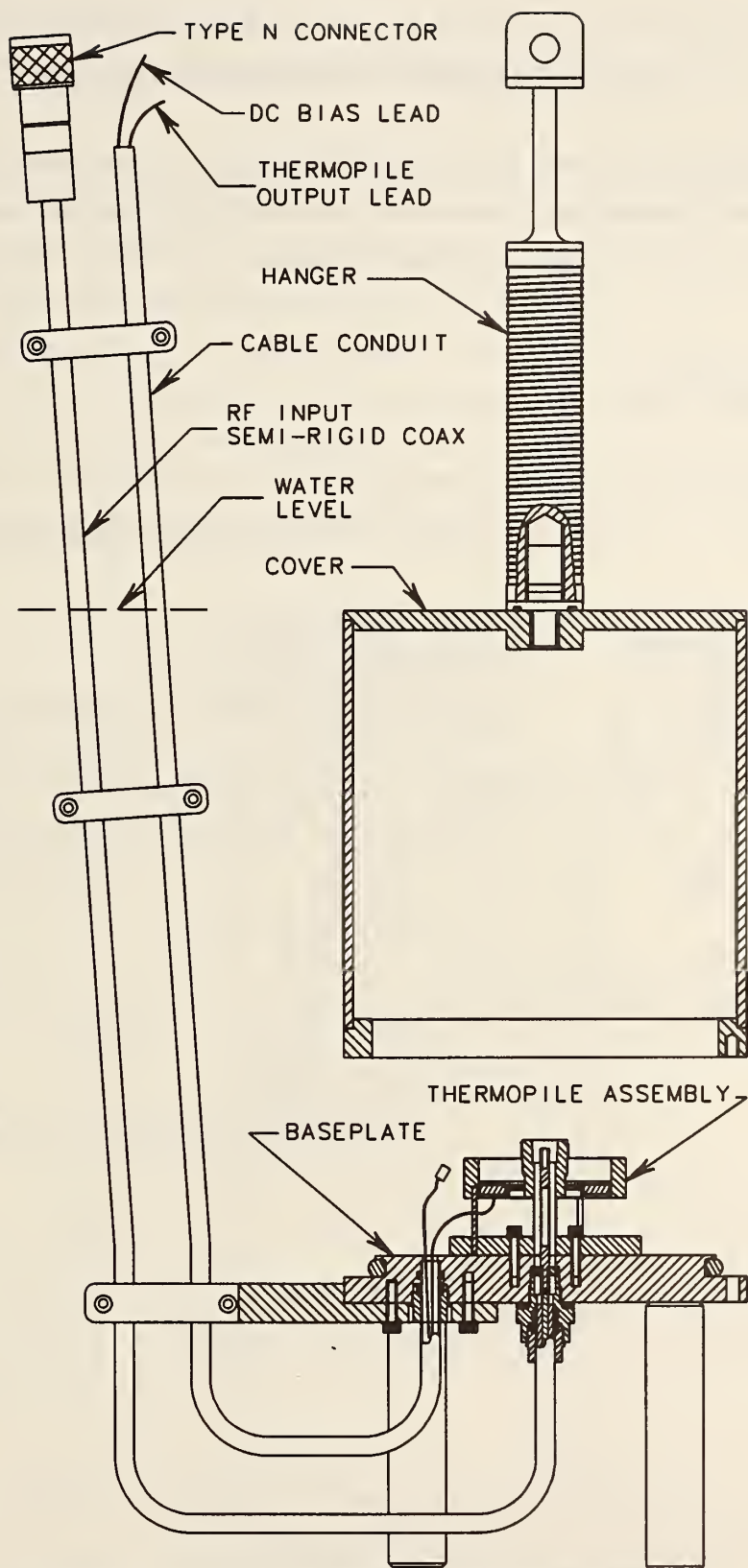


Figure 3.2. View of the entire microcalorimeter assembly.

4. AUTOMATED CALIBRATION SYSTEM

The automated system provides a completely unattended measurement of the effective efficiency once the reference standard and microcalorimeter are connected and placed in the temperature controlled water bath. The automation is accomplished using off-the-shelf computer controlled GPIB instrumentation and custom software.

4.1 SYSTEM HARDWARE

The measurement console containing two automated systems, one in each rack, is shown in figure 4.1. Except for items 7 and 9 each system has an identical set of instruments. The right-hand rack is intended

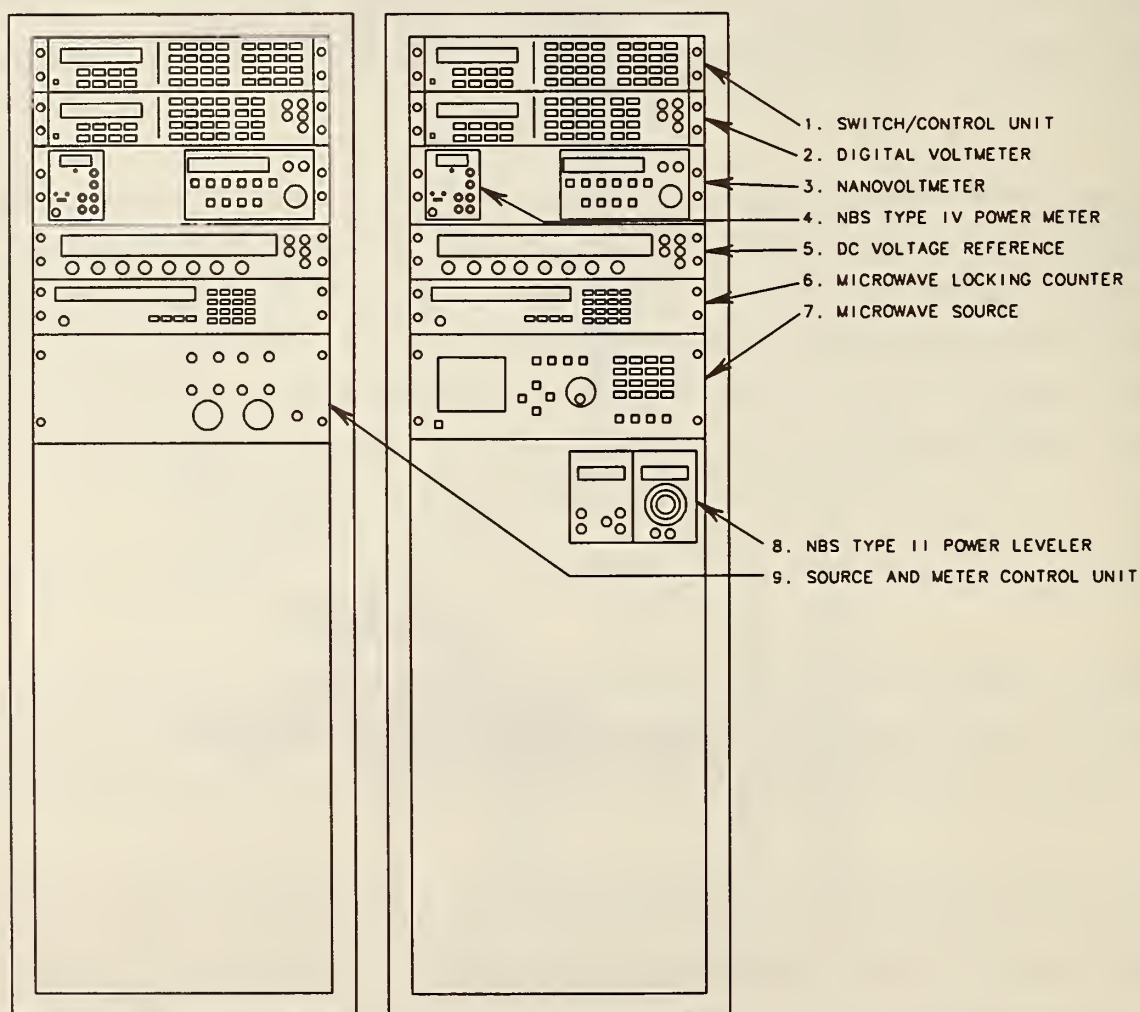


Figure 4.1. Automated calibration system instrument rack.

primarily for coaxial calibrations because the microwave source, item 6, has a 10 MHz to 20 GHz frequency range. The system in the left-hand rack is used with the waveguide microcalorimeters.

Item 1, the switch control unit, provides bus control for the different connections required as the measurement is made. Item 2, the digital voltmeter, measures the output from item 4, the Type IV power meter. Item 3 is a nanovoltmeter used to measure the thermopile output. A precision dc source, item 5, is used as the reference voltage for instrument 8, the NBS Type II power leveler. Item 6 is a locking counter which phase locks the microwave source, unit 7. Item 9 is a custom control unit for the individual YIG tuned FET oscillators used as sources for the waveguide microcalorimeters. Not shown in figure 4.1 are the two instrument controllers. The actual instruments used are identified by item in Appendix F.

A schematic diagram of the instrument connections is shown in figure 4.2.

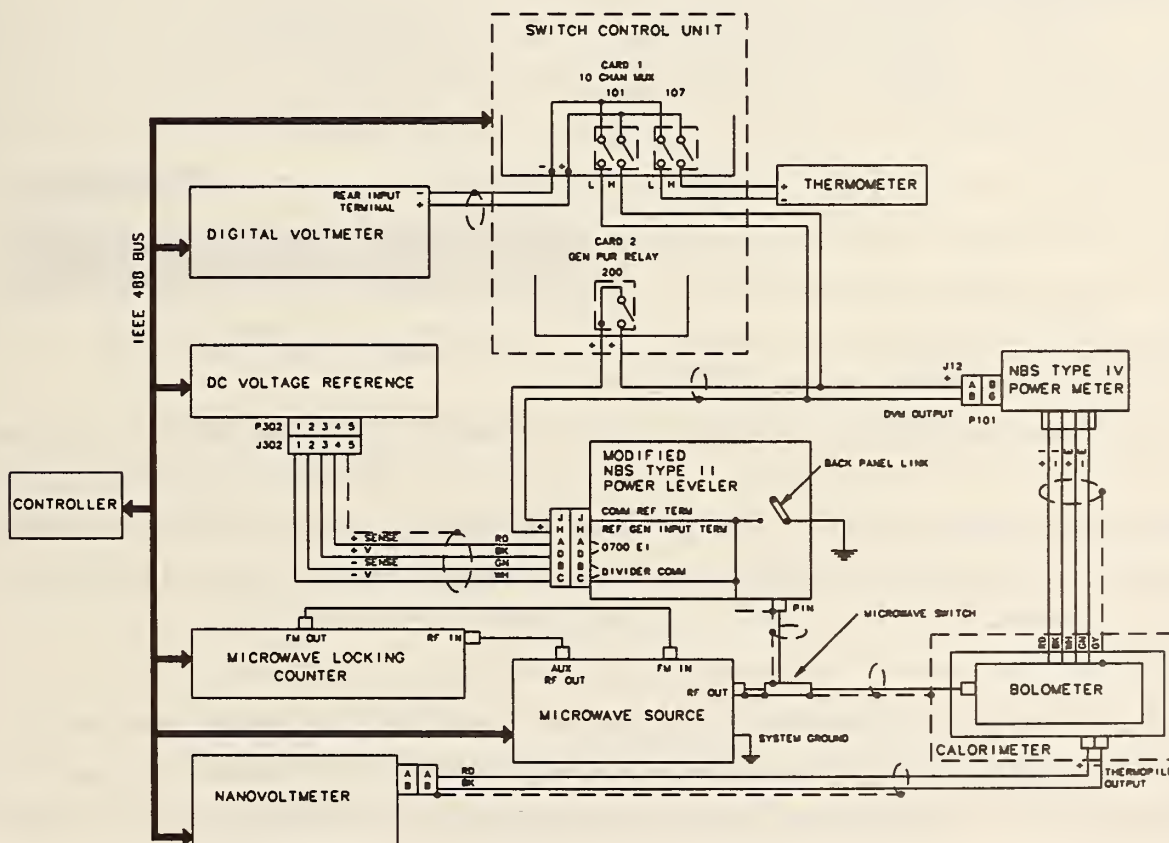


Figure 4.2. Automated calibration system schematic diagram.

4.2 SYSTEM SOFTWARE

The measurement program, called MICRO_CxAP, is written in HP BASIC (also known as Rocky Mountain BASIC or RMB). The program controls the measurement and does the post-measurement processing needed to compute the effective efficiency. A post-measurement computation is required because of the need to correct for the effect of drift in the reference standard bias voltage during the measurement.

4.2.1 Program Features

The program is menu driven, with soft keys used for much of the input. The first menu encountered in running the program is shown in figure 4.3. The reverse video items at the bottom of the screen are soft key definitions. When item 1 is selected, a series of screens is presented that set the initial conditions by asking for the measurement frequencies, the serial number of the reference standard, the scale factors for the real time graph, the desired time delay before starting the measurement, and whether a nanovoltmeter zero offset measurement will be included. One of the initial screens sets up the program to measure at five test frequencies when a mount is first connected to the microcalorimeter. After these results are entered into the program, the mount is removed, reconnected, and measured again at the five test frequencies. If the two sets of measurements agree within established limits, the program automatically continues the measurements over the full set of desired frequencies.

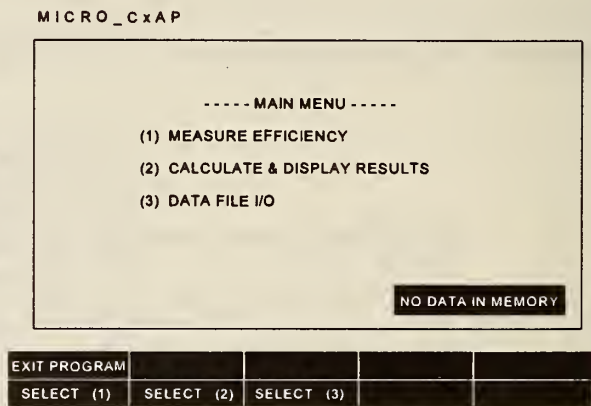


Figure 4.3. First program menu.

During the measurement a real-time graph is displayed on the monitor that shows the thermopile output and other information. Figure 4.4 is an example of the real-time display as the program is measuring the five test frequencies. Information about the program appears in the three windows at the top. The center and right windows can each be toggled to display additional information in another window. The information found in the left-hand window labeled "HEADER INFO" is self explanatory. The center window labeled "LAST READING" gives the total time since the measurement started, the elapsed time since switching to the frequency presently being measured, the total count of data points measured since the start, a countdown that gives the time remaining until the next reading and directions for switching to

the alternate window. The right-hand window labeled "THERMOPILE OUTPUT & TEMP" shows the most recent nanovoltmeter reading of the thermopile output, the average of the last 18 thermopile voltage readings, two spaces for possible future readings of the room and water bath temperatures, and directions for switching to the alternate window. Figure 4.5 shows the real-time display with the alternate center and right windows. The center window labeled "SYSTEM PARAMETERS" shows the present measurement frequency, the last voltage reading from the power meter, the setting of the reference voltage for the power leveler, a calculated value for the substituted dc power in the reference standard, a countdown that gives the time remaining until the next reading, and directions for switching back to the original window. The alternate right window labeled "STATISTICS" shows variables related to the stability algorithm which is explained in section 4.2.2 and Appendix C.

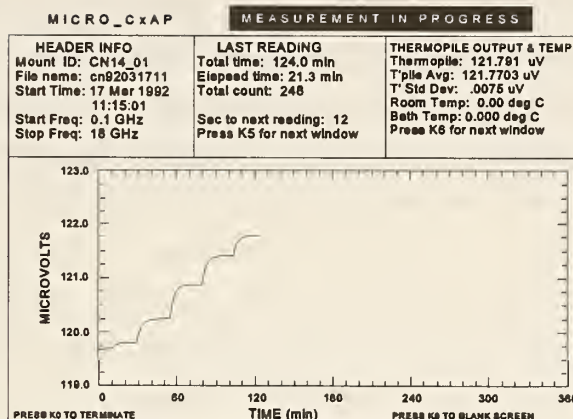


Figure 4.4. Real-time display.

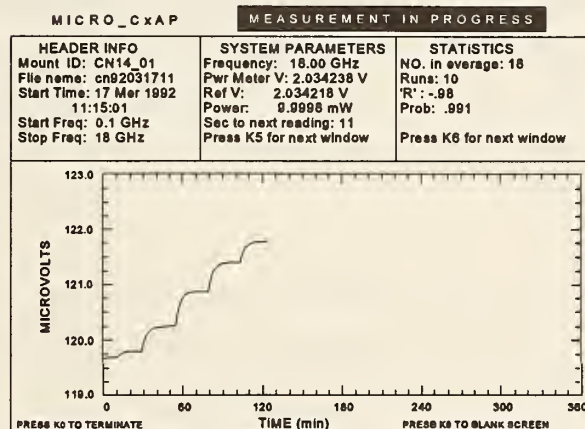


Figure 4.5. Alternate real-time display.

During the measurement the data are taken as the frequency is incremented (tests have shown no difference in results if the frequency is stepped incrementally, or if it is changed randomly) from 50 MHz to 18 GHz. The frequency range is broken into four segments: 50 MHz to 2 GHz in steps of 50 MHz, 2.1 to 4 GHz in steps of 100 MHz, 4.2 to 12.4 GHz in steps of 200 MHz, and 12.5 to 18 GHz in steps of 250 MHz. All of the measured data for each frequency segment are automatically saved to disk individually, with a name that includes the date and time at the beginning of the measurement. An example of the file name is shown under "HEADER INFO" in figure 4.4. The "cn" indicates the reference standard is a Model CN coax mount and "92031711" indicates the measurement was started between 1100 and 1200 h on Mar. 17, 1992. The program completes all four segments automatically without operator intervention.

After completing the entire measurement sequence, the program will return to the main menu. The data from the last set of measured frequencies will still be in memory. Item 2, "CALCULATE & DISPLAY

RESULTS", is selected. This produces the menu shown in figure 4.6 with options to plot the power meter voltage, plot the thermopile voltage, calculate the efficiency, plot the rf power, plot the temperature (if it had been measured), and calculate the standard deviation of any selected set of data points. The plots are useful to get a quick overview of the measurement results to see that the data looks reasonable before calculating the efficiency.

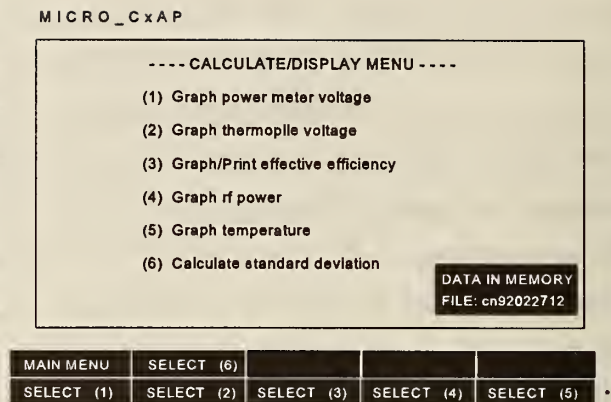


Figure 4.6. Calculation and display menu.

When the program calculates the effective efficiency, four plots at each frequency are optionally available. Examples of these plots for a measurement made at 15 GHz are shown in figures 4.7, 4.8, 4.9, and 4.10.

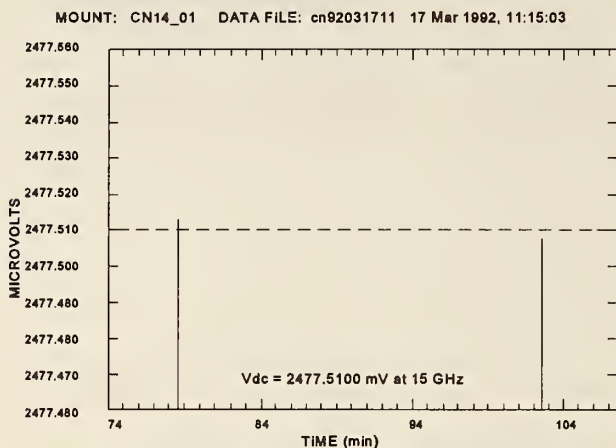


Figure 4.7. Power meter voltage with rf off.

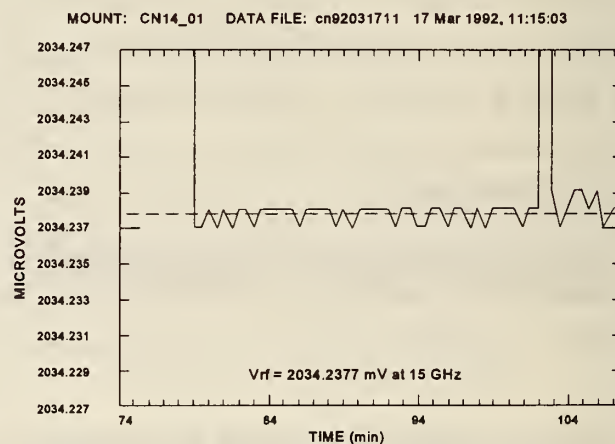


Figure 4.8. Power meter voltage with rf on.

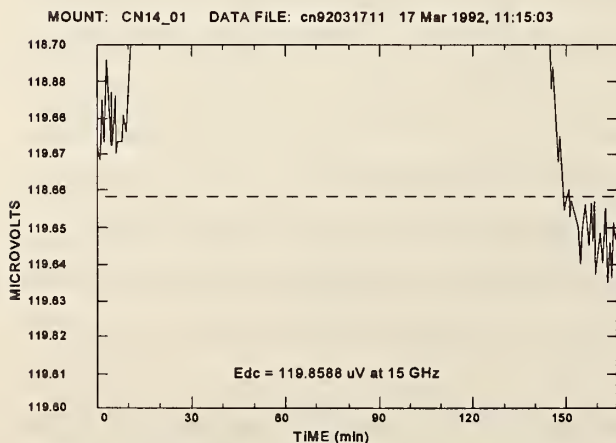


Figure 4.9. Thermopile output with rf off.

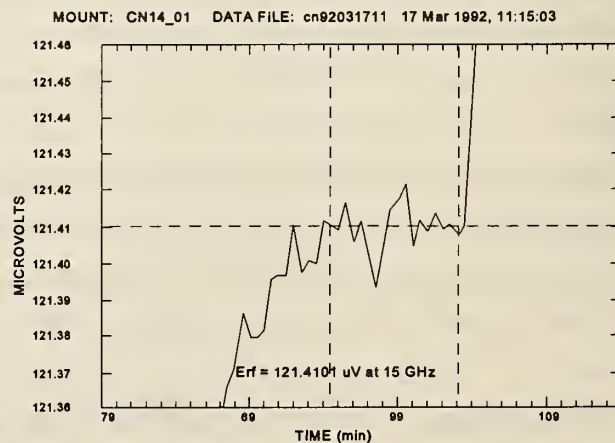


Figure 4.10. Thermopile output with rf on.

The horizontal dashed line in each plot shows the value calculated by the program for each variable. The exact numerical value is displayed at the bottom of the plot. Refer to section 6.1 for a description of the variables and equation used to calculate the effective efficiency. There is a change of variable between these figures and eq (6.1.20): V_{dc} , V_{rf} , E_{dc} , and E_{rf} in the figures equal V_1 , V_2 , e_1 , and e_2 , respectively, in the equation.

In figure 4.7, note that the rf is off only for the initial and final readings and the calculated V_{dc} is the average of the two readings. In figure 4.8, the calculated V_{rf} is the average of all the readings taken while the rf is on. Note that the power leveler keeps the power meter voltage constant within a single count of the DVM. In figure 4.9, the calculated E_{dc} is taken from a linear fit between the average of the initial readings (taken while the rf is off) and the average of the final readings (again while the rf is off) at the time corresponding to the center of the stabilized thermopile output when the rf is on (about 99 min from figure 4.10). In figure 4.10, the value of E_{rf} is the average of the 18 readings between the 2 vertical dashed lines. The decision that stability had been reached in the thermopile output was made by the stability algorithm described in section 4.2.2. The program determines these variables and then calculates and plots the effective efficiency for each frequency measured.

Figure 4.11 is an example how the screen looks when the effective efficiency is plotted. The X and Y axis can be changed to scale the graph and the numerical values can be listed to the screen or printed.

Figure 4.12 shows the screen listing (only a portion of the listing is shown, the rest can be scrolled). The effective efficiency values are now part of the original data file, and the file is saved to disk as described in the next paragraph.

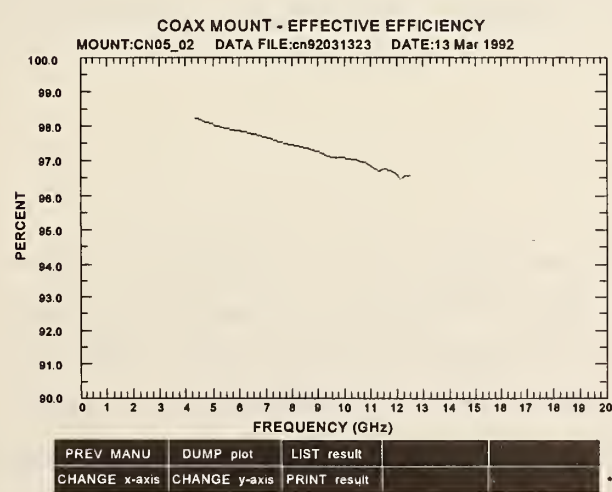


Figure 4.11. Effective efficiency plot.

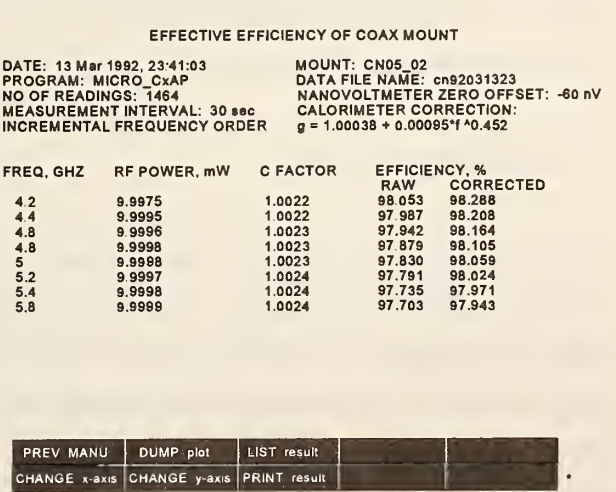


Figure 4.12. Screen listing.

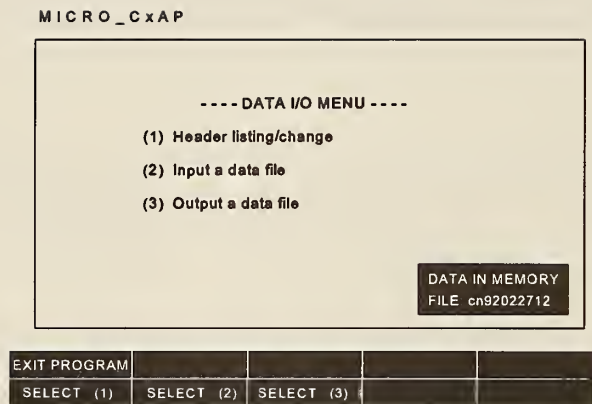


Figure 4.13. Data I/O menu.

HEADER LISTING FOR: A Previous Measurement

Option Array #

(1)	----	Data file name:	cn82031323
(2)	----	Mount ID:	CN05_02
(3)	----	Measurement program:	MICRO_CxAP
(4)	[1]	Revision #:	8202031348
(5)	[2]	Test date:	13 Mar 1992, 23:41:03
(6)	[3]	Band ID:	Coax
(7)	[4]	Effective efficiency flag:	1
(8)	[5]	No. of measurement frequencies:	42
(9)	[6]	Start frequency:	4.2 GHz
(10)	[7]	Stop frequency:	12.4 GHz
(11)	[8]	Step frequency:	.2 GHz
(12)	[9]	Number of measurements:	1464
(13)	[10]	Measurement duration:	12.20 hr
(14)	[11]	Measurement interval:	30 sec
(15)	[12]	Nominal power:	10.0 mW
(16)	[13]	Voltage reference:	0 volts
(17)	[14]	Mount operating resistance:	200 ohms
(18)	[15]	Nanovoltmeter zero correction:	-8.E-8
(19)	[16]	Mount pre_bale flag:	0
(20)	[17]	Room temperature:	0
(21)	[18]	Bath temperature:	0
(22)	[19]	Zero correction flag:	0
(23)	[20]	Auto meas flag:	1
(24)	[21]	Random freq order flag:	0

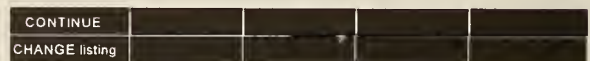


Figure 4.14. Header listing.

To save the data file (or input the data file for the next frequency segment), return to the main menu (figure 4.3), and select option 3, "DATA FILE I/O". This produces the screen shown in figure 4.13. The first item is an option to list the header that is part of each data file. The header, which contains information about the measurement, is shown as it lists to the screen in figure 4.14 (all of the header is shown in the figure, but the actual screen has to be scrolled). As indicated by the soft key options, it may be changed if needed. The item to input a data file also has the option to catalogue any mass storage unit on the system to obtain or check the file name if needed. Once the name is typed in, soft key options input the file from any mass storage unit connected to the controller. The data file output choice includes the option to change the file name, as well as save to any mass storage unit.

Once the efficiencies for all the measured frequencies have been calculated and saved, another program is used to collect them into a single file (which does not contain any of the raw data). This file is used to generate the final calibration report.

4.2.2 Stability Algorithm

One of the critical points in the measurement is the determination of when the thermopile output has reached equilibrium or stability. This is especially difficult because the bias voltage for the reference standard essentially never stops changing; in other words, an aging process is always going on. This means there is always a drift in the thermopile output, aside from the effect of the microwave loss. In addition, the nanovoltmeter reading is fairly noisy because the measurement is being made at about 100 μV , which is just 5 percent of the lowest range (2 mV) on the instrument. An algorithm to determine when stability

has been reached under these conditions has been developed by the NIST Statistical Engineering Division. The algorithm is described in detail in Appendix C. Refer back to figure 4.10 as an example of the thermopile output when it was determined that stability had been achieved. The dashed line is taken to be the thermopile output and is the average of 18 successive measurements between the 2 vertical lines. The right vertical line is the point at which the algorithm decided the output was stable.

5. CALIBRATION PROCEDURES

This section describes the process followed in performing the effective efficiency measurement. Since the measurement is automated, the manual part of connecting the standard, setting up the software, and producing the measurement report are the primary things described. The description is appropriate for a new operator's training and thus detailed.

5.1 STEP-BY-STEP DESCRIPTION

The following steps are carried out in performing the calibration of a reference standard.

1. The Type N connector on the reference standard is inspected closely (under a microscope) for dirt and physical damage. The connector is cleaned if necessary. This is a precaution taken to avoid damaging the microcalorimeter connector, since the effective efficiency measurement is not affected to first order by the mount's reflection coefficient. The critical Type N connector dimension is measured (and compared with previous measurements if this is not the first calibration). This ensures that there will not be a destructive interference when the standard is mated to the microcalorimeter.
2. Any moisture retention by the reference standard or in the microcalorimeter has proven to give erroneous, nonrepeatable results in the efficiency measurement. Be sure your hands are clean and dry before handling the standard and that no water drops are in the microcalorimeter when the cover is replaced. An effective means of being certain that excess moisture is not present in the reference standard is to place the standard in a vacuum for a few hours.
3. The reference standard is connected to a power meter and biased with dc for a period of two to three days. This reduces the bias drift that occurs when the unit is placed in the microcalorimeter.
4. The reference standard is connected to the microcalorimeter using a Type N torque wrench (approximately $1.13 \text{ N} \cdot \text{m}$ ($10 \text{ lbf} \cdot \text{in}$)). The cover is placed on the microcalorimeter, the total unit is placed in the water bath, the Type IV power meter and nanovoltmeter leads are connected, the dc bias is turned on, and the entire unit is allowed to temperature stabilize for at least 1 h. If at that point the power meter and thermopile outputs are fairly stable (an operator's judgement call learned by experience—actually the program will not start the measurement if the drift rate is too high) the first of the measurements can be started. Section 6.4.1 describes a first-order drift correction made when the effective efficiency is calculated.

5. The program called "MICRO_CxAP" is loaded and set up to run the five check frequencies. Information about the program and how to use it can be found in section 4.2. When the program is run, a 3.5 in diskette with sufficient space must be in drive 0 (the left side) of the dual 3.5 in drive. The effective efficiency is measured at five check frequencies, 0.1, 3, 5, 10, 15, and 18 GHz. This takes four to five hours, and the data are saved to disk. The program is run again to compute the results.
6. The microcalorimeter is then disconnected from the power meter and nanovoltmeter, removed from the water bath, the cover removed, and the standard disconnected. The calorimeter is left open for at least 15 to 30 min and then the mount is replaced for a second connect, and the process described by step 5 is repeated, except the results from step 5 are entered into the program before it is run again.
7. If the second five-frequency check result repeats within ± 0.06 percent, the program automatically runs the full frequency set. (The measurement is made without disconnecting the mount.) Again, a 3.5 in diskette with sufficient space must be in drive 0 (the left side) of the dual 3.5 in drive. The effective efficiency is measured at 124 frequencies, 0.05 to 18 GHz. This takes about 40 h, with the data saved to disk in four files. As described in section 4.2, the program is run again to compute and save the results.
8. A program called "MICRO_DMA" is used to extract the effective efficiency from the four data files saved in the last step. The program combines the four segments and saves the results as a single ASCII file which is converted to a DOS file and used to produce the final test report.
9. As described in step 6, the microcalorimeter is removed from the water bath, and the mount removed. This completes the measurement.

5.2 MEASUREMENT RESULTS

The results in the Report of Calibration are listed in a table that gives the effective efficiency, Type B uncertainty, and expanded uncertainty for each frequency. An example of the report can be found in Appendix E.

6. MEASUREMENT CORRECTIONS AND EVALUATION OF UNCERTAINTIES

The factors listed below all contribute to the measurement uncertainty and are included or mentioned in the analysis. A correction is determined for the combined effect. The standard uncertainty for the correction factor and for the remaining uncertainty components is determined by either a Type A or a Type B evaluation [13] as appropriate.

1. Nonlinearity of thermopile and nanovoltmeter.
2. Instrumentation errors (voltmeters and dc-substitution power meter).
3. External temperature stability.
4. Microcalorimeter microwave transmission line loss.
5. Microcalorimeter microwave connector loss.
6. Bolometer mount microwave leakage.
7. Bolometer mount internal dc lead resistance.
8. Bolometer mount microwave transmission line loss.
9. Bolometer mount microwave connector loss.
10. Bolometer mount dc lead filter.
11. Microwave connector repeatability.

6.1 MICROCALORIMETER OPERATION THEORY

This section is based in part on formulations by both Engen [1] and Weidman [2]. Figure 6.1 is a cross section of the reference standard connected to the calorimeter isolation section and the thermopile. The figure may be helpful in understanding the following derivation and equations.

Recall that the thermopile measures the temperature rise of the attached bolometer mount when the mount is biased with dc alone, or with dc plus rf. The expression for the thermopile output voltage with only dc bias applied to the mount may be written as

$$e_1 = k_1 P_{dcl} = \frac{k_1 V_1^2}{R_0}, \quad (6-1)$$

where k_1 is a proportionality factor characteristic of the thermal transfer path from the mount to the thermopile and is a constant unless the thermopile output is nonlinear. The other terms were originally defined in section 1.2. P_{dcl} is the dc bias power dissipated in the mount, V_1 is the power meter output

voltage (equal to the voltage across the bolometer elements) when P_{dc1} is applied, and R_0 is the bolometer element dc operating resistance maintained by the power meter.

With both dc and rf applied to the mount, the new thermopile output voltage is given by

$$e_2 = k_2 (P_{dc2} + aP_t + bP_{mi} + cP_{ci} + dP_{mb}), \quad (6-2)$$

where k_2 does not equal k_1 because of the thermopile nonlinearity, P_{dc2} is the dc bias power dissipated in the mount, P_t is the rf dissipation in and near the thermistor beads, P_{mi} is the rf loss in the mount input section transmission line including the connector, P_{ci} is the rf loss in the calorimeter isolation section transmission line including the connector, P_{mb} is the rf loss in the mount rf low-pass filters, and a , b , c , and d are constants that account for thermal paths that are different than the one described by k_2 . Equation (6-2) may also be written as

$$e_2 = k_2 \left[P_{dc2} + P_{rf} \left(a \frac{P_t}{P_{rf}} + b \frac{P_{mi}}{P_{rf}} + c \frac{P_{ci}}{P_{rf}} + d \frac{P_{mb}}{P_{rf}} \right) \right], \quad (6-3)$$

where P_{rf} is the total rf power delivered to the mount. Letting

$$q = P_t / P_{rf}, \quad (6-4)$$

$$r = P_{mi} / P_{rf}, \quad (6-5)$$

$$s = P_{ci} / P_{rf}, \quad (6-6)$$

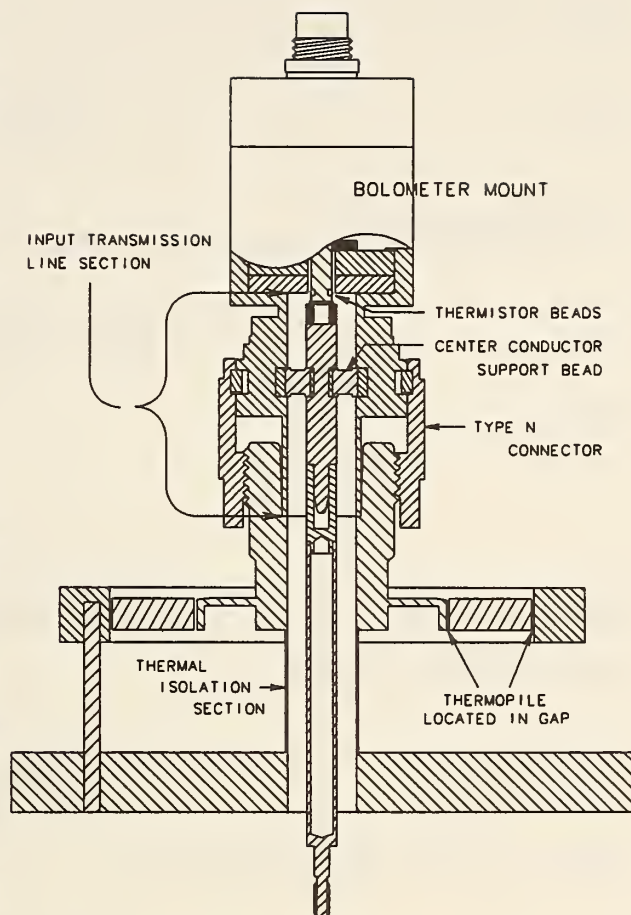


Figure 6.1 Cross section of mount and calorimeter.

and

$$t = P_{mb} / P_{rf}, \quad (6-7)$$

we can write eq (6-3) as

$$e_2 = k_2[P_{dc2} + P_{rf}(aq + br + cs + dt)]. \quad (6-8)$$

Note that

$$q + r + t = 1 \quad (6-9)$$

because each term represents a fraction of the total rf power absorbed in the mount.

Then eq (6-8) can be written as

$$e_2 = k_2(P_{dc2} + gP_{rf}), \quad (6-10)$$

where g is the correction factor given by

$$g = aq + br + cs + dt. \quad (6-11)$$

Writing eq (6-10) in terms of V_2 gives

$$e_2 = k_2 \left(\frac{V_2^2}{R_0} + gP_{rf} \right). \quad (6-12)$$

Solving for P_{rf} , we find

$$P_{rf} = \frac{1}{g} \left(\frac{e_2}{k_2} - \frac{V_2^2}{R_0} \right). \quad (6-13)$$

From eq (6-1), k_1 is given by

$$k_1 = \frac{e_1 R_0}{V_1^2}. \quad (6-14)$$

Let

$$k_2 = c_n k_1 = c_n \frac{e_1 R_0}{V_1^2}, \quad (6-15)$$

where c_n is a correction factor for the thermopile nonlinearity. Using eq (6-15), eq (6-13) becomes

$$P_{rf} = \frac{1}{g} \left[\left(\frac{e_2}{e_1} \right) \frac{V_1^2}{R_0 c_n} - \frac{V_2^2}{R_0} \right] \quad (6-16)$$

or

$$P_{rf} = \frac{1}{g} \left(\frac{V_1^2}{R_0} \right) \left[\left(\frac{e_2}{e_1} \right) \frac{1}{c_n} - \left(\frac{V_2}{V_1} \right)^2 \right]. \quad (6-17)$$

The definition of effective efficiency is

$$\eta_e = \frac{P_b}{P_{rf}}, \quad (6-18)$$

where P_b is the bolometric substituted power given by

$$P_b = \frac{1}{R_0} (V_1^2 - V_2^2) = \frac{V_1^2}{R_0} \left[1 - \left(\frac{V_2}{V_1} \right)^2 \right], \quad (6-19)$$

and P_{rf} is the total rf power delivered to the mount.

Using eqs (6-17) and (6-19), eq (6-18) becomes

$$\eta_e = g \frac{1 - \left(\frac{V_2}{V_1} \right)^2}{\frac{e_2}{e_1} \frac{1}{c_n} - \left(\frac{V_2}{V_1} \right)^2}. \quad (6-20)$$

Equation (6-20) can be simplified by letting

$$F_v = \frac{V_2}{V_1} \quad (6-21)$$

and

$$f_e = \frac{e_2}{e_1} \frac{1}{c_n}, \quad (6-22)$$

so eq (6-20) becomes

$$\eta_e = g \frac{1 - F_v^2}{f_e - F_v^2}. \quad (6-23)$$

Taking the total differential of eq (6-23) gives an expression for the uncertainty $\Delta\eta_e$ in η_e due to uncertainties in g , F_v , and f_e .

$$|\Delta\eta_e| = \frac{1 - F_v^2}{f_e - F_v^2} |\Delta g| + g \left| \frac{2 F_v (1 - f_e)}{(f_e - F_v^2)^2} \right| |\Delta F_v| + g \frac{1 - F_v^2}{(f_e - F_v^2)^2} |\Delta f_e|, \quad (6-24)$$

where the absolute value of each uncertainty term is used to obtain the maximum uncertainty. The relative uncertainty is given by

$$\left| \frac{\Delta\eta_e}{\eta_e} \right| = \left| \frac{\Delta g}{g} \right| + \frac{2 F_v^2 (f_e - 1)}{(1 - F_v^2)(f_e - F_v^2)} \left| \frac{\Delta F_v}{F_v} \right| + \frac{f_e}{f_e - F_v^2} \left| \frac{\Delta f_e}{f_e} \right|. \quad (6-25)$$

The determination of the terms g , F_v , and f_e , and their uncertainties, is described in the following sections.

6.2 DETERMINATION OF CORRECTION FACTOR g

Figure 6.2 is a cross section of a special measurement configuration used to determine g . The setup contains two thermopile assemblies and is symmetrical about the indicated horizontal center line. The microwave losses and the thermal conditions in each half are nearly equal, so the effect on the thermopiles is as if the other half were not present. (An analogy is the method of images employed with electromagnetic field problems.) Each half of the center adapter section is made of the same material and length as the input transmission line section of the mount (see figure 6.1), so that each half is thermally and electrically the same as a mount connector and input section. Although not shown, the transmission line is terminated (at the top of the figure) by one of the reference standards. The arrangement is fed by a nominal 10 mW (with the power leveled by the terminating mount) from the bottom, and the output of both thermopiles is noted. Assuming adequate symmetry, either thermopile reading is an indication of the heating due to loss in the calorimeter thermal isolation section and the mount input section. In the same way, then, as eqs (6-1) and (6-2) were developed, one of the thermopile outputs (say the lower) can be written as

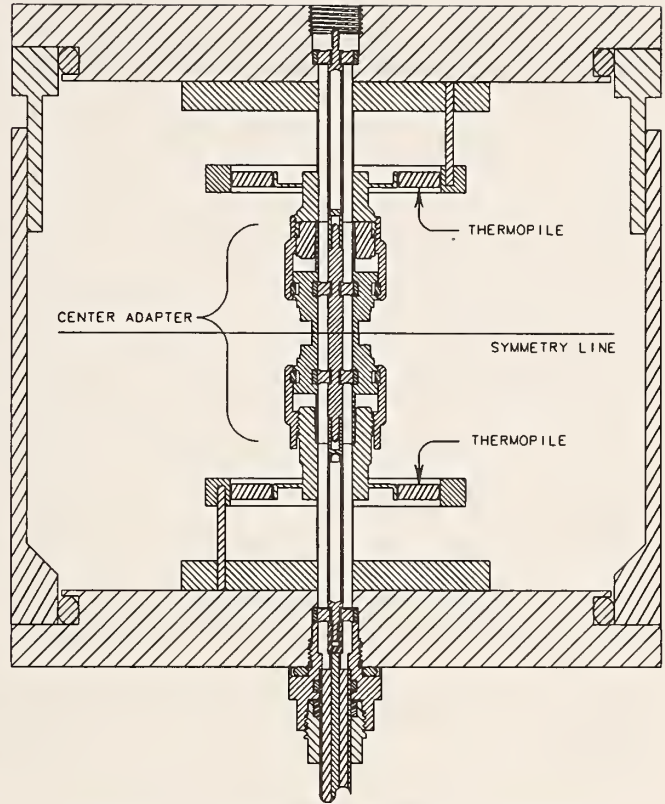


Figure 6.2 Arrangement used to determine the correction factor g .

$$e_B = k_B (b' P_{mi} + c' P_{ci}). \quad (6-26)$$

As before, P_{mi} is the loss in the mount input section, and P_{ci} is the loss of the calorimeter thermal isolation section, and k_B , b' , and c' are equivalent to k_i , b , and c , the constants characteristic of the different thermal transfer paths. Note that although the total loss in this measurement configuration is approximately double that of the configuration of figure 6.1, it does not result in added heating because there is also an additional identical thermal path to the temperature-controlled external environment.

In terms of the power ratios of eqs (6-5) and (6-6), eq (6-26) becomes

$$e_B = k_B P_{rf} (b' r + c' s). \quad (6-27)$$

Because of the adapter material and size, we assume that

$$k_B \approx k_1. \quad (6-28)$$

The factor b' is associated with the loss in the mount input section. In the mount, the heat due to center conductor loss is transmitted to the thermopile primarily by the center conductor support bead rather than by the thermistor bead structure, because the dc blocking capacitor and bellows contact provide good thermal isolation. This was verified experimentally by measuring the thermopile output with the bellows and capacitor removed from a mount. For a representative mount with a dc bias of about 30 mW, the thermopile output with the bellows is $116 \mu\text{V}$, and without the bellows the output is $118 \mu\text{V}$, a less than 2 percent change. Thus the thermal effect should be nearly the same in the adapter and

$$b' \approx b. \quad (6-29)$$

The factor c' is associated with the loss of the calorimeter isolation section, and for the same reasons noted above,

$$c' \approx c. \quad (6-30)$$

With these substitutions eq (6-27) becomes

$$e_B \approx k_1 P_{rf} (b r + c s), \quad (6-31)$$

so

$$b r + c s \approx \frac{e_B}{k_1 P_{rf}}. \quad (6-32)$$

Recall that

$$g = a q + b r + c s + d t. \quad (6-11)$$

The loss in the low pass filters is given by t . It will be zero only if there is no rf leakage past the internal thermistor bead structure. It is assumed that t is negligible, since its effect can be absorbed in the other loss term q , and it is not susceptible to direct measurement. The approximation that $a \approx 1$ can be made

because q is the power ratio associated with the dissipation in the thermistor beads and k_1 is the thermal constant associated with that same heating. Then, with (6-32) substituted into (6-11), the expression for g becomes

$$g = q + \frac{e_B}{k_1 P_{rf}}. \quad (6-33)$$

From eq (6-9), with $t = 0$,

$$q = 1 - r. \quad (6-34)$$

Recall that r is the fractional loss in the input section and connector of the mount. An approximation for this is half the loss of the adapter section shown in figure 6.2. If the total loss is α_L , then

$$q \approx 1 - \frac{\alpha_L}{2}. \quad (6-35)$$

That loss is given by (see appendix A)

$$\alpha_L \approx 1 - |S_{21}|^2, \quad (6-36)$$

so the expression for g becomes

$$g \approx \frac{1 + |S_{21}|^2}{2} + \frac{e_B}{k_1 P_{rf}}. \quad (6-37)$$

Measured and calculated values for $|S_{21}|$ in decibels are shown in figure 6.3. The basis for the "theoretical plated line loss" curve is given in appendix B. The curve labeled "adjusted plated line loss" is a calculated loss obtained by changing the value of the conductivity of the gold plating and the joint loss factors (including the exponent of the frequency term) so the curve approximately fits the measured values. Table 6.1 lists the parameter values that were changed to obtain the adjusted curve

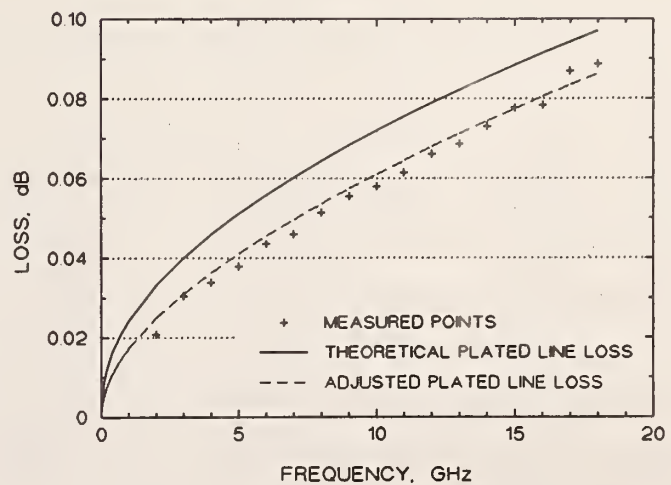


Figure 6.3 Type N male-to-male coax adapter loss.

Table 6.1 Values used in calculating the adjusted loss.

Parameter	Layer 1 (Au) thickness	Layer 1 (Au) conductivity	Layer 2 (Cu) conductivity	Joint loss factors		
	d μm	σ_1 S/m	σ_2 S/m	A_0	B dB/(GHz) ^E	E
Inner conductor loss calculation	1.27 (nc)	2.5×10^7	8.00×10^6 (nc)	—	—	—
Outer conductor loss calculation	1.27 (nc)	2.5×10^7	5.75×10^7 (nc)	—	—	—
Type N joint loss calculation	—	—	—	0 (nc)	0.004	0.65
Bead joint loss calculation	—	—	—	0 (nc)	0.0022	0.65

(compare with table B1 in appendix B) using the equations derived in appendix B. An (nc) indicates the values have not changed from those listed in table B1.

The adjusted curve provides reasonable low frequency values for $|S_{21}|$ below 2 GHz where it was not possible to measure it. These values are used in eq (6-37) at all frequencies below 2 GHz. Above 2 GHz the measured values of $|S_{21}|$ are used.

Measurements of e_B , which were made over the frequency range of 10 MHz to 18 GHz, are shown in figure 6.4. The dashed line is a curve fitted to the bottom thermopile output. It shows that the output has a \sqrt{f} dependence. The e_B values from the bottom thermopile are used in the calculation of g using eq (6-37).

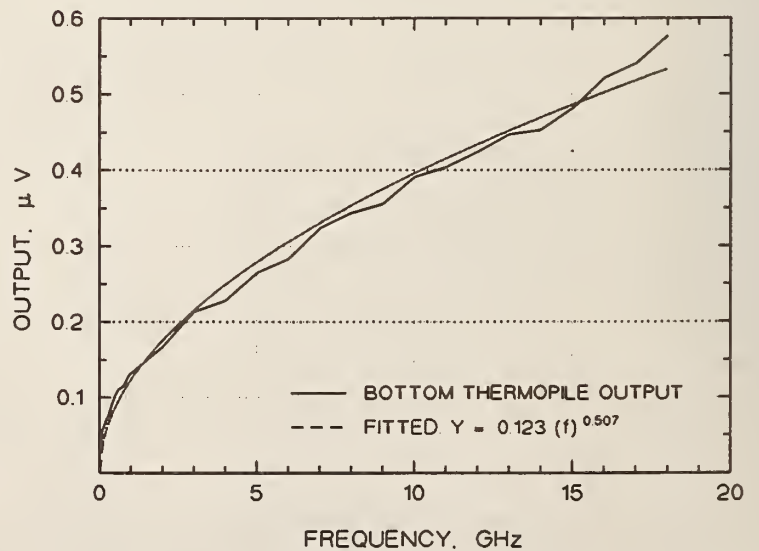


Figure 6.4 Measured thermopile output.

The value used for P_T in eq (6-37) can reasonably be the nominal 10 mW power at which e_B was measured.

Values for g as a function of frequency from 10 MHz to 18 GHz are shown in figure 6.5. The fitted curve is proposed as the operational expression for g . A numerical listing of the values for g is included as table 6.2.

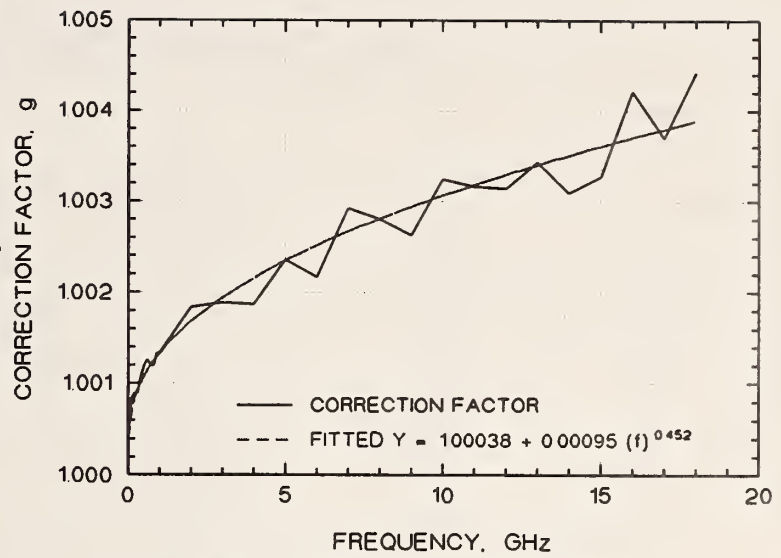


Figure 6.5 Microcalorimeter correction factor, g .

It is mathematically possible for g to be less than 1 if

$$\frac{\alpha_L}{2} > \frac{e_B}{k_1 P_{rf}}. \quad (6-38)$$

Physically, this can happen because the heating effect of the center conductor loss is relatively isolated from the thermopile. In a waveguide calorimeter there is not an equivalent thermal path that is fairly well isolated from the thermopile, so g must always be 1 or greater.

Table 6.2 Tabulated values for g .

FREQ GHz	q	$\frac{e_B}{k_1 P_{rf}}$	g	g fitted
0.01	0.99983	0.00063	1.00046	1.00050
0.02	0.99975	0.00073	1.00048	1.00054
0.03	0.99969	0.00084	1.00052	1.00057
0.04	0.99964	0.00099	1.00063	1.00060
0.05	0.99960	0.00111	1.00071	1.00063
0.06	0.99955	0.00119	1.00074	1.00065
0.07	0.99951	0.00124	1.00075	1.00067

Table 6.2 (continued) Tabulated values for g .

FREQ GHz	q	$\frac{e_B}{k_1 P_{rf}}$	g	g fitted
0.08	0.99947	0.00129	1.00076	1.00068
0.09	0.99944	0.00134	1.00078	1.00070
0.10	0.99941	0.00142	1.00083	1.00072
0.20	0.99915	0.00175	1.00090	1.00084
0.30	0.99894	0.00195	1.00089	1.00093
0.40	0.99877	0.00230	1.00107	1.00101
0.50	0.99861	0.00258	1.00119	1.00107
0.60	0.99847	0.00278	1.00126	1.00113
0.70	0.99834	0.00286	1.00121	1.00119
0.80	0.99823	0.00296	1.00119	1.00124
0.90	0.99812	0.00322	1.00133	1.00129
1.00	0.99801	0.00332	1.00133	1.00133
2.00	0.99763	0.00423	1.00186	1.00186
3.00	0.99654	0.00539	1.00193	1.00194
4.00	0.99615	0.00577	1.00192	1.00216
5.00	0.99570	0.00671	1.00241	1.00235
6.00	0.99507	0.00716	1.00224	1.00252
7.00	0.99481	0.00820	1.00301	1.00267
8.00	0.99421	0.00871	1.00292	1.00281
9.00	0.99378	0.00901	1.00279	1.00294
10.0	0.99347	0.00990	1.00337	1.00307
11.0	0.99307	0.01023	1.00330	1.00319
12.0	0.99258	0.01073	1.00332	1.00330
13.0	0.99227	0.01132	1.00358	1.00341
14.0	0.99179	0.01147	1.00326	1.00351
15.0	0.99128	0.01218	1.00346	1.00361
16.0	0.99119	0.01319	1.00438	1.00371
17.0	0.99022	0.01367	1.00389	1.00380
18.0	0.99008	0.01461	1.00469	1.00389

6.3 UNCERTAINTY IN CORRECTION FACTOR g

From the preceding section

$$g \approx \frac{1 + |S_{21}|^2}{2} + \frac{e_B}{k_1 P_{rf}}. \quad (6-37)$$

Taking the total differential of eq (6-37) gives the following expression for the absolute uncertainty in g due to uncertainties in the independent variables.

$$|\Delta g| = |S_{21}|^2 \left| \frac{\Delta S_{21}}{S_{21}} \right| + \frac{1}{k_1 P_{rf}} |\Delta e_B| + \frac{e_B}{k_1 P_{rf}} \left| \frac{\Delta k_1}{k_1} \right| + \frac{e_B}{k_1 P_{rf}} \left| \frac{\Delta P_{rf}}{P_{rf}} \right|, \quad (6-39)$$

where the absolute value of each uncertainty term is used to obtain the maximum uncertainty.

In the measurement of both e_B and k_1 a correction for the zero offset is made. In terms of the measured quantities these are given by

$$e_B = (e_B)_1 - (e_B)_0 \quad (6-40)$$

and

$$k_1 = \frac{(e_{k_1})_1 - (e_{k_1})_0}{P_{dcl}}, \quad (6-41)$$

where the subscript $_0$ denotes the zero correction value and the subscript $_1$ the measured value. The variable P_{dcl} is the dc power dissipated in the thermistor mount. Thus the ratio of e_B to k_1 includes a ratio of zero-corrected nanovoltmeter readings.

$$\frac{e_B}{k_1} = \frac{(e_B)_1 - (e_B)_0}{(e_{k_1})_1 - (e_{k_1})_0} P_{dcl}. \quad (6-42)$$

As will be explained in the next section, under these circumstances only the random part of the nanovoltmeter error contributes to the uncertainty.

Rather than using analytical differentiation, the uncertainty in g has been evaluated numerically. The contribution of each variable is determined by first calculating g with no change in the variable, and then again with the variable at its uncertainty limit, all other variables held constant. The difference between these two values of g gives the uncertainty due to the effect of that variable. This process is repeated for each variable, with the total uncertainty given by the sum of these individual contributions. As eq (6-25) shows, the relative uncertainty in η_e due to g is just the relative uncertainty in g .

Table 6.3 gives the uncertainty used for each variable along with the basis for the choice. The value shown is either the equivalent of one standard deviation of a normal distribution (as indicated by an SD) or the half-width limit of a rectangular distribution (as indicated by an R).

Table 6.3. Variable uncertainty values.

Uncertainty	Value	Basis
$ \Delta e_B $	6 nV (SD)	Random error of two e measurements (each is average of 18, see section 6.4)
$\left \frac{\Delta k_1}{k_1} \right $	0.01 (R)	Approximation $k_1 \approx k_B$ plus measurement error
$\left \frac{\Delta P_{rf}}{P_{rf}} \right $	0.01 (R)	Bolometric power measurement plus power level instability
$\left \frac{\Delta S_{21}}{S_{21}} \right $	1 (SD)	Below 0.2 GHz ($ S_{21} $ from fitted curve)
$ \Delta S_{21} $	0.0076 dB (SD)	For 0.3 through 1 GHz ($ S_{21} $ from fitted curve)
$ \Delta S_{21} $	Function of frequency (SD) (see figure 6.6)	<p>Above 1 GHz: 6-port measurement uncertainty given by:</p> $u_{S_{21}} = \sqrt{\Delta^2/3 + S_{NIST}^2 + S_c^2/6}$ <p>where</p> $\Delta = 0.0006\sqrt{f} + 0.0011$ $S_{NIST} = 10^{-2.17 + 0.024f}$ $S_c = 10^{-3.22 + 0.034f}$

The contribution of the individual factors to the uncertainty in g as a function of frequency is shown in figure 6.6. The contribution from the level instability is identical to that of k_1 . That the end points of the curves seem to meet is only coincidence. By far the largest uncertainty is from the 6-port measurement of the adapter loss. These components are combined as part of the expanded uncertainty as described in section 6.9.

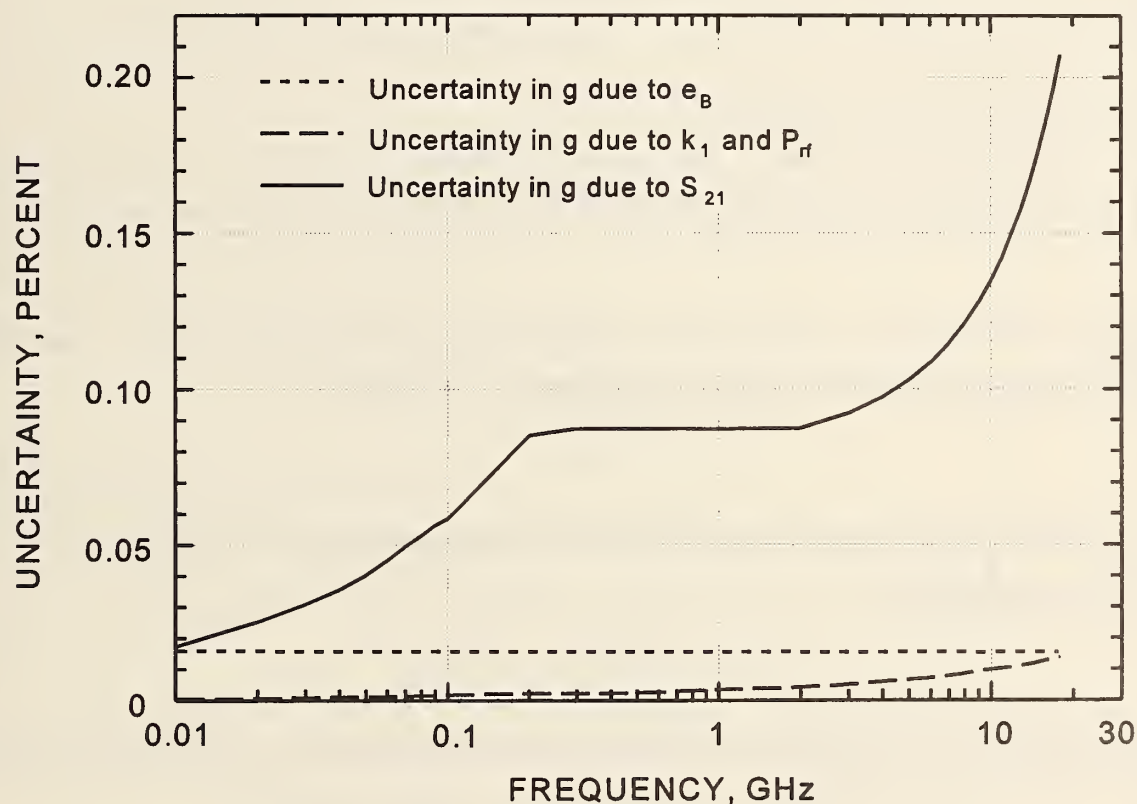


Figure 6.6 Contribution of each factor to the uncertainty in g .

6.4 UNCERTAINTY DUE TO VOLTAGE RATIOS

6.4.1 Power Meter Voltage Ratio

From section 6.1, the expression for F_V is

$$F_V = \frac{V_2}{V_1}. \quad (6-21)$$

The absolute value of the uncertainty in F_V is

$$|\Delta F_V| = \frac{V_2}{V_1^2} |\Delta V_1| + \frac{1}{V_1} |\Delta V_2|. \quad (6-43)$$

Because of mount drift, V_1 does not remain constant during the measurement, so V_1 is actually an interpolated value between two end point measurements. V_1 is given by

$$V_1 = V_{1i} + F(V_{1f} - V_{1i}), \quad (6-44)$$

where V_{1i} and V_{1f} are the initial and final values of the V_1 measurements and F is a fraction between 0 and 1. The uncertainty in V_1 is

$$|\Delta V_1| = (1-F) |\Delta V_{1i}| + F |\Delta V_{1f}|. \quad (6-45)$$

If both the initial and final values are measured on the same range, $|\Delta V_{1i}| \approx |\Delta V_{1f}|$. Then by eq (6-45), $|\Delta V_1| \approx |\Delta V_{1i}|$, so the uncertainty in V_1 is the same as for a single measurement.

For both the power meter voltages (V), and the nanovoltmeter readings (e), the desired quantity is a ratio. The error in a voltmeter reading is generally specified as a percent of reading factor (alpha) plus a percent of full scale (beta). The alpha factor comes from the error of the internal reference, while the beta factor is due to random and zero correction errors and nonlinearity. In a ratio measurement, if the two voltages are measured on the same scale, the alpha factor can be neglected. In addition, if the zero drift is explicitly corrected (as in the f_e case), the only contribution to the uncertainty is from the random part of the beta factor.

A calculation of the uncertainty in η_e due to ΔF_V , which is a function of η_e and P_{rf} , can be made using eqs (6-25) and (6-43). If the voltmeter manufacturer's one-year beta specification is used, the result is a value

well under 0.001 percent for all reasonable values of η_e .

6.4.2 Thermopile Voltage Ratio

The expression for f_e is

$$f_e = \frac{e_2}{e_1} \frac{1}{c_n}. \quad (6-22)$$

In measuring f_e , a correction for the zero offset must be made. This involves measuring e_0 before measuring the dc bias term e_1 or the dc-plus-rf term e_2 . When we take e_0 into consideration, eq (6.1.22) becomes

$$f_e = \frac{1}{c_n} \frac{e_2 - e_0}{e_1 - e_0}. \quad (6-46)$$

The absolute uncertainty in f_e is given by

$$|\Delta f_e| = \frac{e_2 - e_1}{c_n (e_1 - e_0)^2} |\Delta e_0| + \frac{e_2 - e_0}{c_n (e_1 - e_0)^2} |\Delta e_1| + \frac{1}{c_n (e_1 - e_0)} |\Delta e_2| + \frac{e_2 - e_0}{c_n^2 (e_1 - e_0)} |\Delta c_n|. \quad (6-47)$$

Like V_1 , e_1 is obtained by linear interpolation, so the uncertainty Δe_1 is also that of a single measurement.

The calculation of the uncertainty in η_e due to Δf_e is based on the applicable parts of eq (6-25) and eq (6-47). To determine the error in f_e it is necessary to know the random error in the nanovoltmeter measurement. This random error beta factor is determined by making repeated measurements on the actual setup and thus includes the effects of variations in the dc bias as supplied by the power meter, in the microwave power leveling, in the external temperature, and in the room air pressure. These measurements were made under three conditions: with no dc bias, with dc bias, and with dc bias plus rf at 18 GHz. The largest standard deviation seen was 3.65 nV for the dc-plus-rf case, and that result is shown in figure 6.7. The three-sigma limit is therefore about ± 11 nV.

In the actual efficiency measurement routine, each data point is the average of 18 separate measurements, so the value for Δf_e can be further decreased as a result of the averaging. This reduces the three-sigma limit by a factor of $1/\sqrt{18}$ to approximately ± 3 nV. Using a value of ± 3 nV for Δe_o and Δe_i in eq (6-47) and then using that result in eq (6-25) gives the uncertainty in η_e due to Δf_e shown in figure 6.8. The uncertainty is a function of η_e and P_f but not of frequency. The maximum is about 0.016 percent when η_e is 1. That value is used as the thermopile voltage ratio uncertainty.

An additional factor that may add to Δf_e is the uncertainty in knowing when the thermopile has reached equilibrium. This is a critical element in the measurement. A software algorithm determines when equilibrium has been reached at each measurement frequency. The algorithm is described in appendix C. It has been tested by letting the measurement continue for several minutes beyond the point the algorithm indicates stability has been reached and noting that the result essentially does not change. While it has not been possible to detect any systematic uncertainty in the process, there is a random component and that is included in the random uncertainty number.

6.4.3 Thermopile and Nanovoltmeter Nonlinearity

The linearity correction factor c_n has been determined from a series of measurements on the Type N microcalorimeter using a mount with a resistor in place of the thermistor beads. Figure 6.9 shows the measured k as a function of the thermopile output e . Note that these results include the effect of both thermopile and nanovoltmeter nonlinearity.

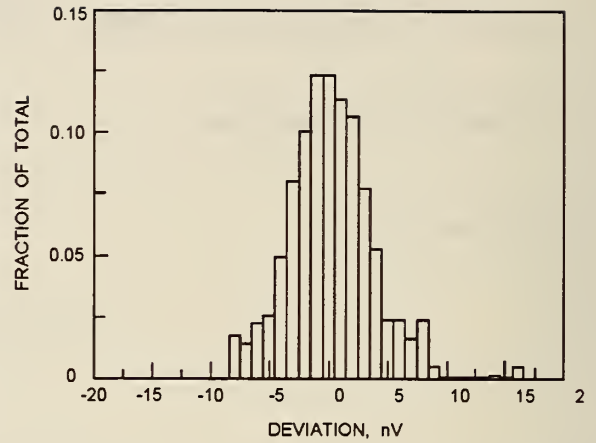


Figure 6.7. Histogram of the variation in 1000 nanovoltmeter readings. The average is $115.916 \mu\text{V}$ with a standard deviation of 3.65 nV.

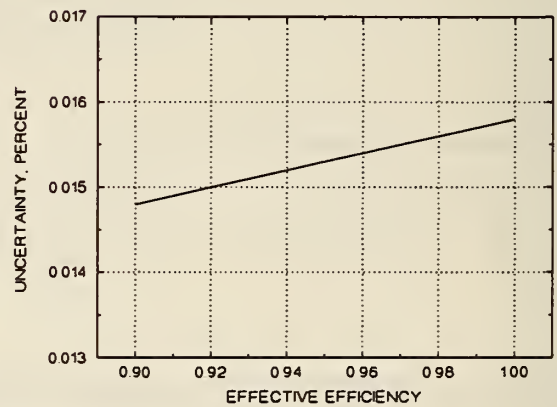


Figure 6.8. Uncertainty in η_e due to the thermopile voltage ratio uncertainty as a function of η_e .

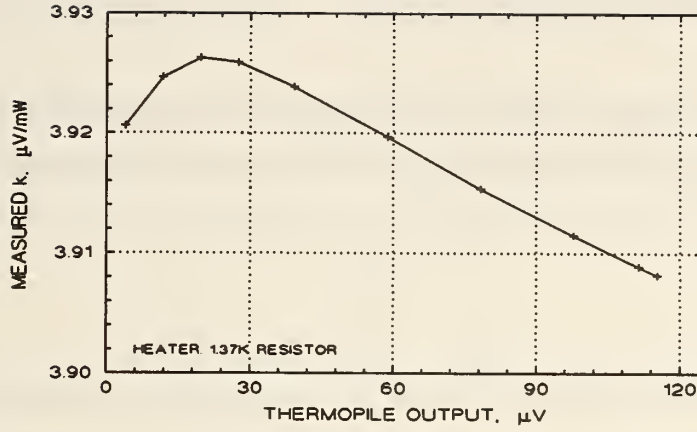


Figure 6.9. k factor vs thermopile output.

From equation (6-15),

$$k_2 = k_1 c_n. \quad (6-48)$$

k_2 can also be expressed as

$$k_2 = k_1 + \Delta k. \quad (6-49)$$

If S is the slope of the curve (from 30 μV and above) in figure 6.9,

$$\Delta k \approx S (e_2 - e_1). \quad (6-50)$$

Then

$$k_2 \approx k_1 \left(1 + \frac{S}{k_1} (e_2 - e_1) \right), \quad (6-51)$$

so

$$c_n \approx 1 + \frac{S}{k_1} (e_2 - e_1). \quad (6-52)$$

Based on experimental evidence ($e_2 - e_1 \leq 5 \mu\text{V}$ and $k_1 \approx 3.90$) and figure 6.9 ($S \approx -0.00016$), c_n could vary between 1 and 0.9998. Thus the maximum correction would be on the order of 0.02 percent. Rather than make a correction, we will assume $c_n = 1$ and include the 0.02 percent as a Type B uncertainty.

6.5 MOUNT MICROWAVE POWER LEAKAGE

Microwave power leakage from the mount essentially reduces the effective efficiency because the leakage energy is not detected by the mount thermistor beads. The expression for effective efficiency is

$$\eta_e = \frac{P_b}{P_{rf}}, \quad (6-18)$$

where P_b is the dc bolometric power, and P_{rf} is the net rf power delivered to the mount. Since P_{rf} is the total power dissipated in the mount plus any microwave power leakage, η_e includes the effect of leakage. However the microcalorimeter measures only the effect of the total power dissipated in the mount because the thermopile does not sense the leakage power. Thus the microcalorimeter measurement of η_e is in error if there is any leakage. To account for leakage, let the measured η_e be denoted by η_{eL} . It is given by

$$\eta_{eL} = \frac{P_b}{P_{rf} - P_L}, \quad (6-53)$$

where P_L is the leakage power. Factoring out P_{rf} gives

$$\eta_{eL} = \frac{P_b}{P_{rf} \left(1 - \frac{P_L}{P_{rf}} \right)}. \quad (6-54)$$

Substituting from eq (6-18) and solving for η_e gives

$$\eta_e = \eta_{eL} \left(1 - \frac{P_L}{P_{rf}} \right), \quad (6-55)$$

so the error in η_e due to P_L is P_L/P_{rf} . The ratio P_L/P_{rf} for the prototype mount was measured as described in section 2.4.1. with the result shown in figure 2.3. The ratio is less than -40 dB from 5 MHz through 18 GHz. Thus the error is less than 0.0001 or 0.01 percent over that range.

6.6 BOLOMETER LEAD RESISTANCE

Lead resistance that is beyond the four-wire connection to the mount (in the form of any final short leads to the thermistor beads) does not cause an error in the measurement of efficiency, but does cause an error when the transfer standard is used to measure power. To determine the effect let r_L be the lead resistance. Then

$$R_0' = R_0 - r_L = R_0 \left(1 - \frac{r_L}{R_0} \right), \quad (6-56)$$

and

$$V' = V \left(1 - \frac{r_L}{R_0} \right). \quad (6-57)$$

V' is the actual voltage across the beads, V is the power meter voltage (known), R_0' is the actual bead resistance, and R_0 is the resistance (known) being maintained by the power meter.

For the efficiency measurement the ratio of V_1' to V_2' is desired. In terms of V_1 and V_2 this is given by

$$\frac{V_1'}{V_2'} = \frac{V_1 \left(1 - \frac{r_L}{R_0} \right)}{V_2 \left(1 - \frac{r_L}{R_0} \right)} \quad (6-58)$$

which reduces to

$$\frac{V_1'}{V_2'} = \frac{V_1}{V_2} \quad (6-59)$$

and there is no error.

For the power measurement the desired expression is

$$P_b = \frac{1}{R_0'} (V_1'^2 - V_2'^2). \quad (6-60)$$

In terms of V_1 and V_2 ,

$$P_b = \frac{1}{R_0} (V_1^2 - V_2^2) \left(1 - \frac{r_L}{R_0} \right). \quad (6-61)$$

The measurement is in error by the factor $1 - r_L / R_0$. Values of r_L for a commercial mount have been measured as high as 400 m Ω (including connector contact resistance because the four leads are not brought through the connector), giving an uncertainty in the power measurement of about 0.2 percent. For the transfer standard, the residual lead resistance beyond the four-wire connection has not been measured, but is estimated as less than 10 m Ω . The error is less than 0.005 percent.

6.7 TYPE IV POWER METER ERRORS

The uncertainty due to the measurement of V_1 and V_2 was addressed in section 6.4. The additional uncertainty due to limitations of the operational amplifiers and reference resistor within the Type IV power meter is also very small. The uncertainty is under 0.001 percent and will be neglected.

6.8 RANDOM EFFECTS

The Type A evaluation of standard uncertainty for the measurement process reported in this document is based on repeated measurements of a single reference standard which will continue to be used as a check standard. Ideally, standard uncertainty for the bolometer mounts should be determined through repeat measurements for each individual mount. However, this is impractical due to the time required for a complete set of measurements. Therefore, we will assume that the standard uncertainty inherent in all mounts behaves in basically the same fashion so that the standard uncertainty we derive for the check standard mount will apply to the population of mounts as well. Although the actual measurements for the check standard mount are quite repeatable, the observed standard deviations are different for each frequency. Thus, a single value of standard uncertainty which is valid for all frequencies was calculated based on a "worst" case standard deviation.

The standard uncertainty, determined through Type A evaluation, in the measured effective efficiency for customer mounts at any individual frequency is 0.00014, which is the worst case (among frequencies) computed standard deviation based on ten degrees of freedom.

The Type A evaluation of standard uncertainty for the measured effective efficiency for the check standard mount CN05 at any individual frequency is 0.000041, which is the worst case (among frequencies) computed standard error of the mean effective efficiency, $0.00014/\sqrt{11}$ based on ten degrees of freedom.

6.9 COMBINED STANDARD AND EXPANDED UNCERTAINTY

Table 6.4 is a summary of the results at 18 GHz for all the uncertainty evaluations described earlier. The section describing the uncertainty is listed in the table. Definitions for the variables and terms used are found in reference [13]. The expanded uncertainty value is for a customer standard.

Table 6.4. Value of uncertainty components in percent at 18 GHz.

Uncertainty factor (evaluation type)	Section reference	Half-width interval (a)	Distribution	Conversion formula	Standard uncertainty
Adapter loss meas. (B)	6.3	0.207	Normal	$u_j = a$	0.207
Nanovoltmeter, e_B (A)	6.3	-	Normal	-	0.015
k_1 (B)	6.3	0.014	Rectangular	$u_j = a/\sqrt{3}$	8.1×10^{-3}
Power leveling & meas. (B)	6.3	0.014	Rectangular	$u_j = a/\sqrt{3}$	8.1×10^{-3}
V ratio, F_V (B)	6.4.1	0.001	Rectangular	$u_j = a/\sqrt{3}$	5.8×10^{-4}
e ratio, f_e (A)	6.4.2	-	Normal	-	0.016
Linearity, c_n (B)	6.4.3	0.02	Rectangular	$u_j = a/\sqrt{3}$	0.012
Mount leakage (B)	6.5	0.01	Rectangular	$u_j = a/\sqrt{3}$	5.8×10^{-3}
Lead resistance (B)	6.6	0.005	Rectangular	$u_j = a/\sqrt{3}$	2.9×10^{-3}
Type IV power meter (B)	6.7	0.001	Rectangular	$u_j = a/\sqrt{3}$	5.8×10^{-4}
Random effects (A)	6.8	-	Normal	-	0.014
Combined standard uncertainty (RSS)					0.209
Expanded uncertainty ($k = 2$)					0.419

The first factor on the list is the largest, and because of the RSS combination, dominates the combined uncertainty. It is also the only uncertainty that is a strong function of frequency.

Figure 6.10 shows the expanded uncertainty as a function of frequency. It also shows a fitted curve with the equation that is the operational expression for the expanded uncertainty. The uncertainty at any frequency is calculated using the equation. The higher value it gives in the range 50 to 200 MHz is intentional and accounts for low frequency dissipation in the mount that occurs in the low pass filter behind

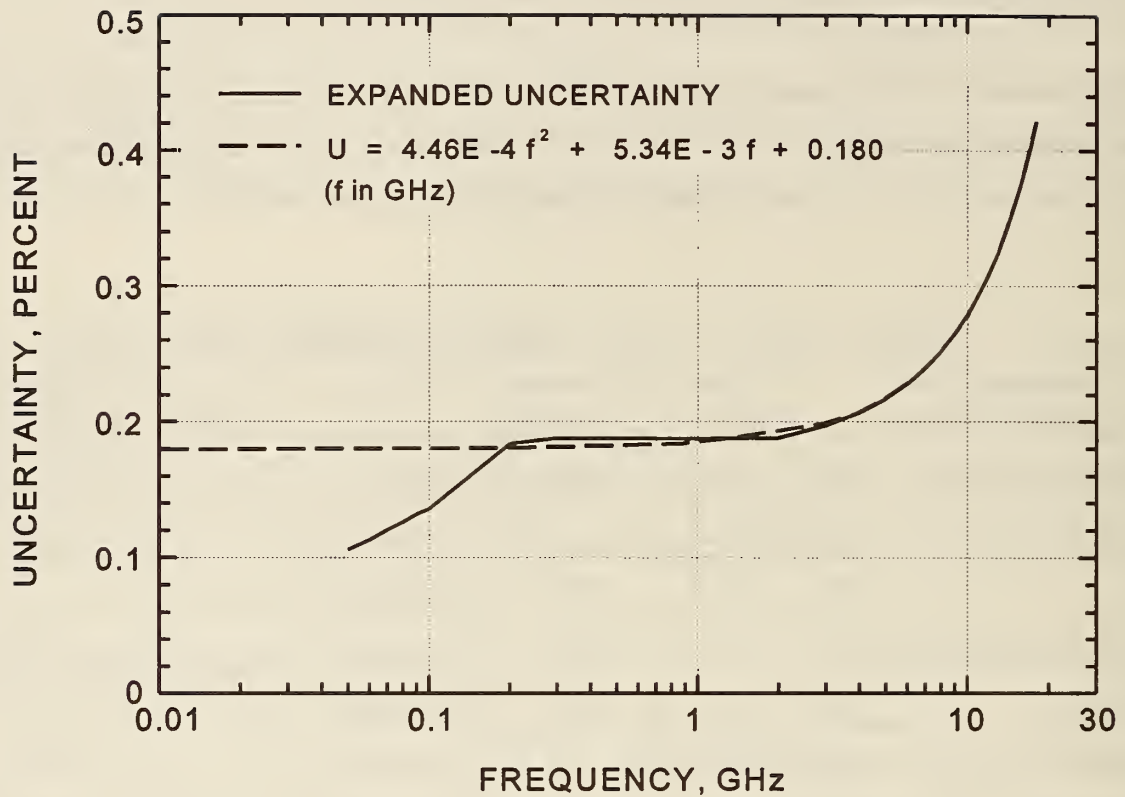


Figure 6.10 The expanded uncertainty ($k = 2$) for the Type N coaxial microcalorimeter when measuring the effective efficiency of a NIST CN coaxial transfer standard.

the thermistor beads. This process has become apparent in using and comparing the CN mount with other transfer standards, but we have not been able to come up with any way evaluate it directly.

A sample Report of Calibration is found in appendix E.

7. MEASUREMENT ASSURANCE

One of the most important aspects of maintaining the coaxial microcalorimeter system is measurement assurance. Since individual mounts cannot be measured repeatedly, it becomes even more important to ensure that the system is behaving as it should. Several techniques are currently being employed to monitor the system and assure measurement quality.

To monitor the long-term behavior of the microcalorimeter system, a check standard mount is measured on a regular basis at all 125 frequencies. Each new set of measurements is compared to the historical data to determine if the system is performing as expected. Figure 7.1 summarizes the behavior of the latest observation in relation to past data. The solid dots in Figure 7.1 represent the latest observation, the diamonds denote historical data, and three standard deviation limits are indicated by a solid, vertical line at each frequency.

A second chart is used to monitor system variability at each frequency through the use of moving ranges. A moving range is defined to be the absolute value of the difference between the two most recent observations. Figure 7.2 displays the moving range, indicated by a dot, and the associated control limits based on moving ranges for the historical data, represented by a solid vertical line. If the computed moving range for the latest observation is higher than the control limit, then the process variability is greater than the acceptable amount determined by the historical data, and the cause of the increased variability should be investigated. Figures 7.1 and 7.2 indicate that the system is behaving in a reasonable fashion relative to the historical data.

Although the control charts allow us to examine the behavior of new data in comparison to past data, other methods must be used to monitor the system over time. It is impractical to generate separate control charts to monitor all 125 frequencies; however, control charts for five check frequencies are used as an additional tool for signaling potential problems, such as drift [14]. An example of the type of control charts used to monitor a check frequency is shown in figure 7.3. The top chart, called an individuals chart, monitors the nominal effective efficiency, while the bottom chart, the moving range chart, monitors variability. Although it is possible to interpret patterns in the individuals control chart, patterns observed in the moving range chart are meaningless because adjacent points are related [15]. The variability observed in the moving range chart of figure 7.3 does not exceed the upper control limit, and the newest observation on the individuals chart lies within the control limits and does not reveal any patterns or drift, so we can

conclude that the effective efficiency at a frequency of 0.1 GHz is "in control."

The five check frequencies are also used to determine the quality of mount connection before each measurement occasion using the following procedure. After each bolometer mount is connected to the coaxial calibration system, the five check frequencies are measured and the mount is disconnected. Then the same mount is reconnected to the system and the same five check frequencies are measured again. If the difference between the first and second set of measurements is small, then all 125 frequencies are measured before the mount is disconnected a second time, otherwise, the mount is disconnected, and the procedure is repeated until it can be determined that the connection is "good." The measurement assurance tools used to monitor this calibration system are quite extensive and provide confidence that the system is functioning properly.

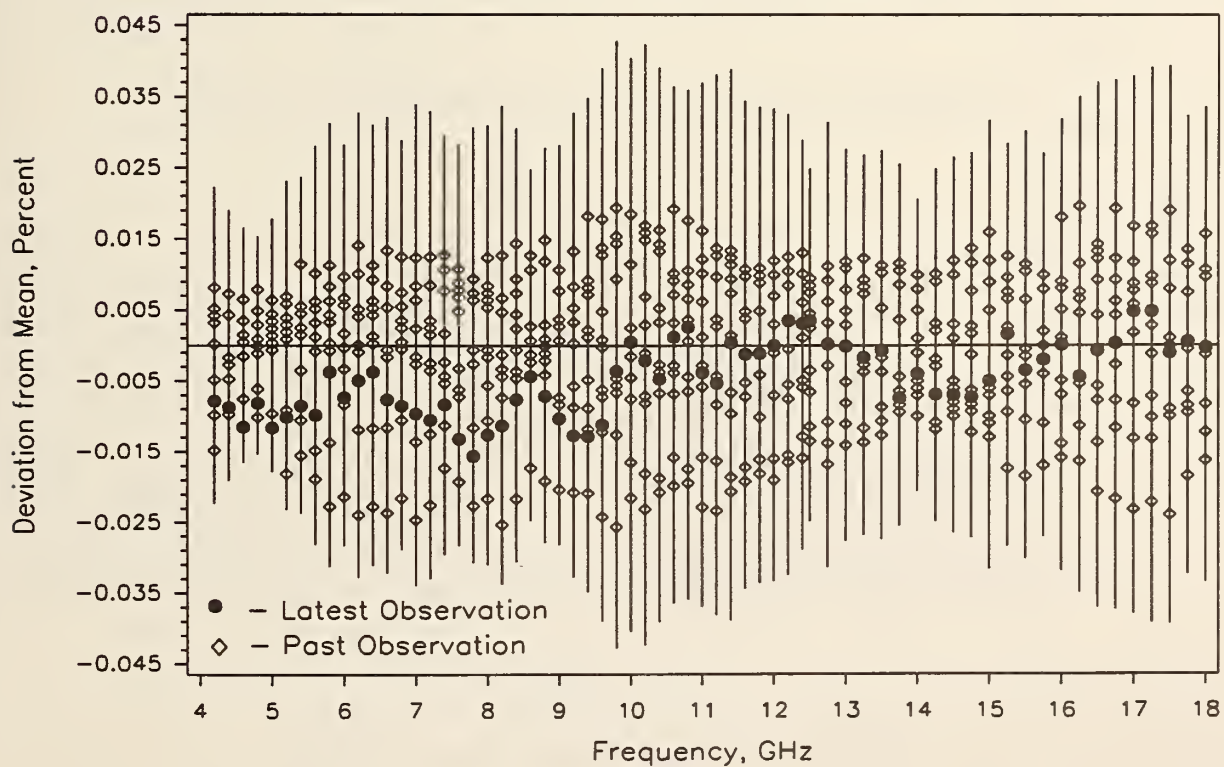
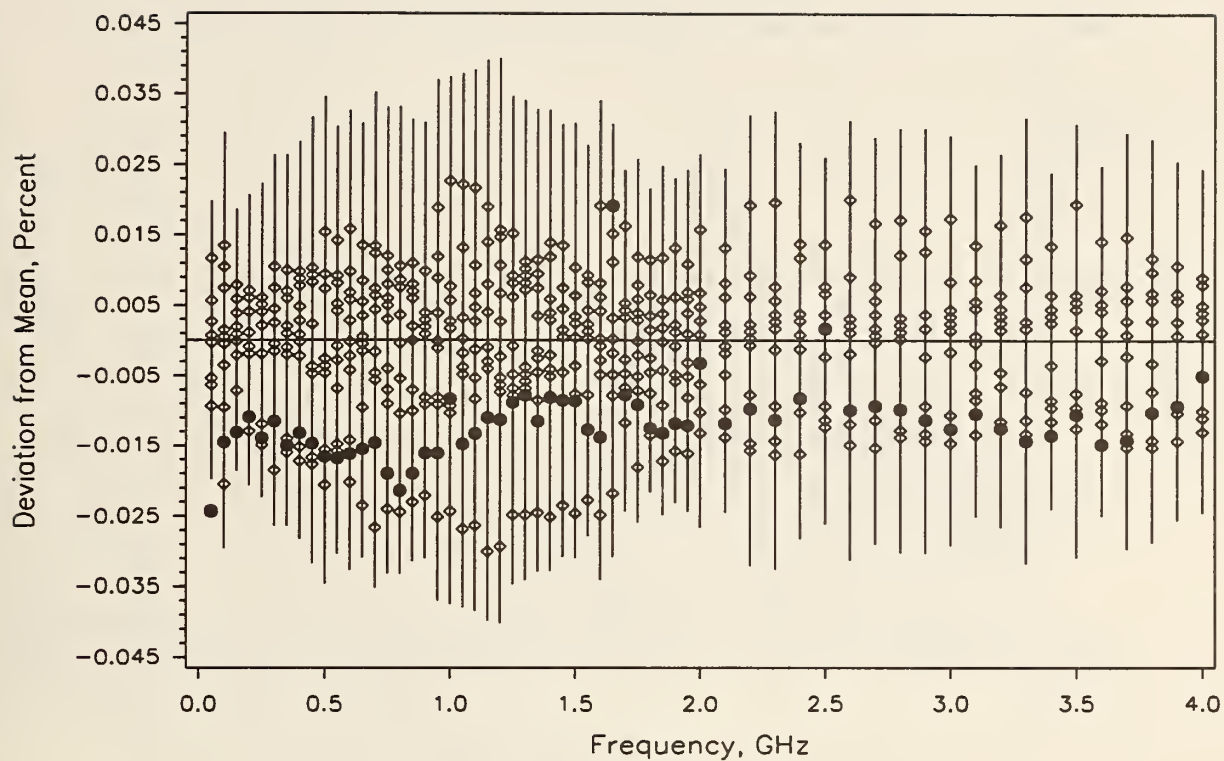


Figure 7.1. Three standard deviation limits for CN05.

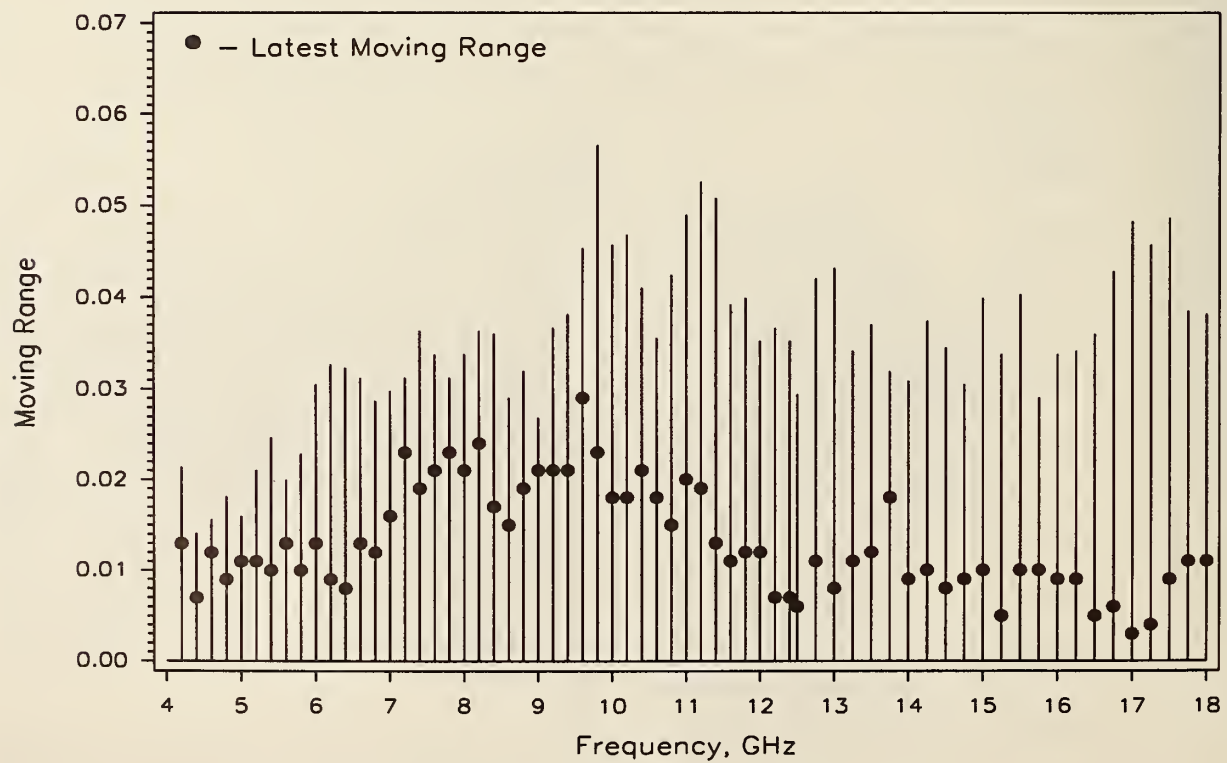
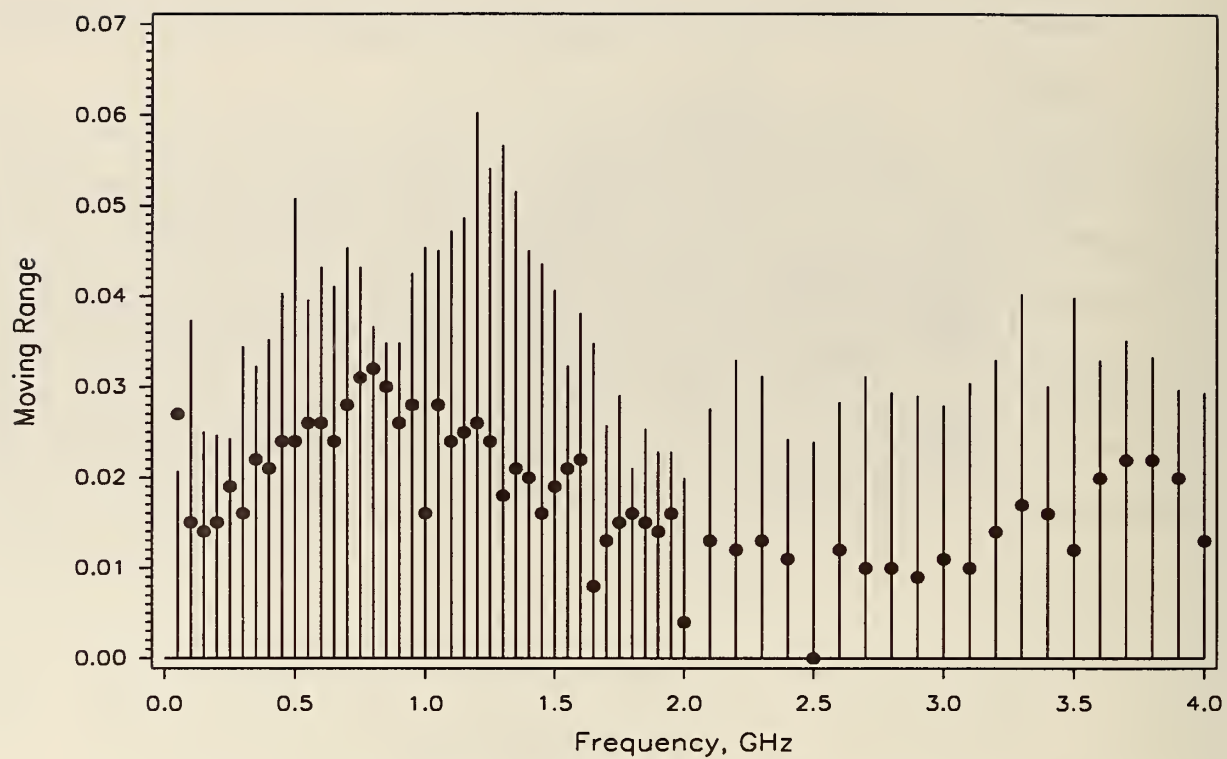


Figure 7.2. Moving range control chart for CN05.

Check Standard Mount CN05, Check Frequency = 0.1 GHz

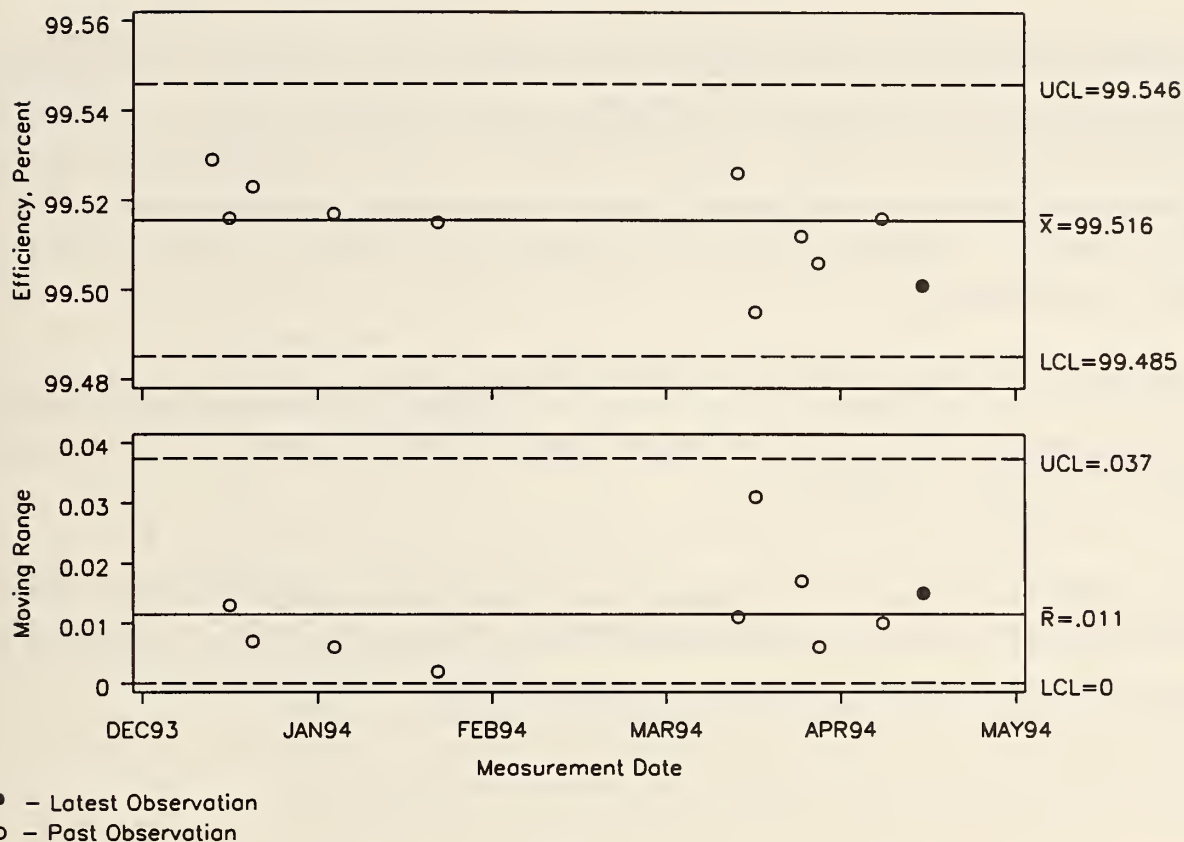


Figure 7.3. Control chart for the first of the five check frequencies.

8. FUTURE CHANGES

Inevitably, in the future the calibration system will not remain exactly as described in this document. Software will be modified or even completely rewritten to improve operating efficiency or implement new measurement requirements. Hardware changes will range from the simple replacement of an obsolete or defective microwave source to a completely new way of determining the temperature change of the reference standard. Additional uncertainty or measurement assurance factors may become apparent and will have to be addressed.

The majority of the modifications will be minor. The changes will be noted and kept in an active documentation file on the system. While the details may no longer be completely accurate, this report should still adequately describe the service.

Major changes, such as a new reference standard, a new microcalorimeter design, significantly different operating procedures, large changes in uncertainty (to say one-half the present value), or changes in the frequency range, may require the preparation of a new document.

If up-to-date information is critical, contact NIST for the current documentation.

9. ACKNOWLEDGEMENTS

The designs of both the coax reference standard and the coax microcalorimeter are based on the early work and ideas of Morris E. Harvey. Thanks also to Mr. Harvey for the review of his work plus his suggestions at the beginning of this project. The author is particularly indebted to Neil T. Larsen for his support, suggestions, and many helpful discussions. Special thanks to Dominic F. Veccia and Jolene D. Splett for help with the statistical analysis and experimental design contained in sections 6.8, 7, and appendix C, to Robert M. Judish for help with the uncertainty analysis and helpful comments on section 6, and also to Manly P. Weidman for his helpful suggestions on section 6.

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APPENDIX A. Measured Adapter Loss

Chapter 6 describes the determination of the calorimetric equivalence correction factor g for the microcalorimeter. The procedure uses a special type N male-to male adapter (made in the same way and of the same material as the reference standard bolometer mount) that connects two thermopile assemblies. The analysis requires a knowledge of the adapter loss (which is small). This appendix derives an expression for the loss in terms of the measurable S parameters.

The adapter is gold plated with an electroformed copper outer conductor and a beryllium copper inner conductor supported by a pair of dielectric beads. Figure A.1 is a cross section view of the adapter. The connector on the bottom is a type N male while the top connector is a type N male modified to allow mating with the APC-7 connector on the top thermopile (see figure 6.2).

The desired result is the ratio of the total power dissipated in the adapter to the net power entering the adapter. The adapter is a 2-port junction as shown in figure A.2. The input incident and reflected powers at port 1 are P_{i1} and P_{r1} , the output incident and reflected powers at port 2 are P_{i2} and P_{r2} . The net input power P_1 at port 1 is

$$P_1 = P_{i1} - P_{r1}, \quad (\text{A-1})$$

and the net output power P_2 at port 2 is

$$P_2 = P_{i2} - P_{r2}. \quad (\text{A-2})$$

The total power, P_D , dissipated in the adapter is given by the change in the incident power plus the change in the reflected power

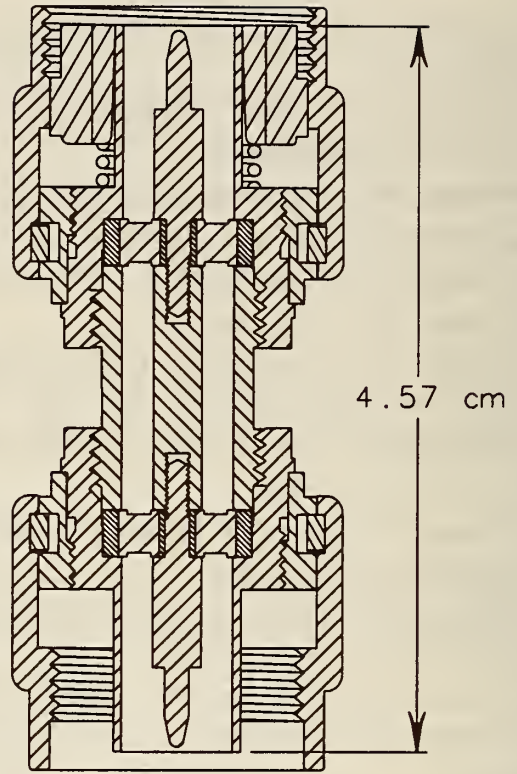


Figure A.1. Adapter cross section.

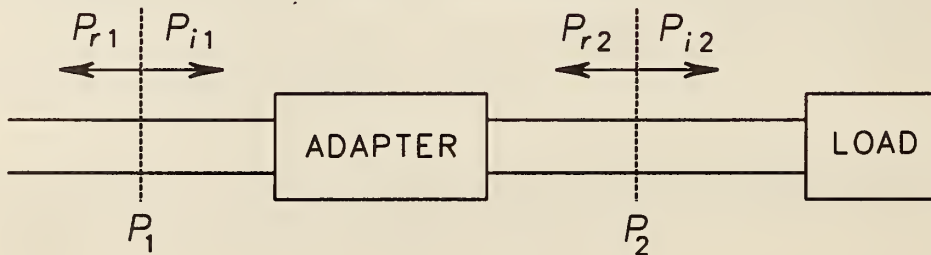


Figure A.2. The adapter as a 2-port junction.

$$P_D = (P_{i1} - P_{i2}) + (P_{r2} - P_{r1}). \quad (\text{A-3})$$

Rearranging terms gives

$$P_D = (P_{i1} - P_{r1}) - (P_{i2} - P_{r2}), \quad (\text{A-4})$$

which by eqs (A-1) and (A-2) is just the difference $P_1 - P_2$ in the net powers. The desired fractional loss then is given by

$$\frac{P_D}{P_1} = \frac{P_1 - P_2}{P_1} = 1 - \frac{P_2}{P_1}. \quad (\text{A-5})$$

The ratio of P_2 to P_1 is defined as the efficiency, η of the junction when energy is fed into port 1. Assuming unit normalization, it is given by reference [A1]

$$\eta_1 = \frac{|S_{21}|^2 (1 - |\Gamma_L|^2)}{|1 - S_{22}\Gamma_L|^2 - |(S_{12}S_{21} - S_{11}S_{22})\Gamma_L + S_{11}|^2}. \quad (\text{A-6})$$

The S parameters are those of the adapter, and Γ_L is the reflection coefficient of the terminating load. If both Γ_L and S_{11} are sufficiently small, η_1 reduces to

$$\eta_1 \approx |S_{21}|^2, \quad (\text{A-7})$$

and eq (A-5) becomes simply

$$\frac{P_D}{P_1} \approx 1 - |S_{21}|^2. \quad (\text{A-8})$$

The S parameters of the adapter and Γ_L of the terminating load were measured using the NIST 6-port network analyzer, and the efficiency calculated. The result is shown in figure A.3. The curve labeled "exact" was obtained using eq (A-6) and the curve labeled "approximate" using eq (A-7). The differences are small, with the largest at 7 and 18 GHz. A change of just 2° in the phase of Γ_L (using eq (A-6)) eliminates the difference at either frequency. Because the amplitude of Γ_L is small, the uncertainty in the phase measurement is 20° . The "approximate" values are adequate in this case, and eq (A-8) is used as the expression for the adapter loss.

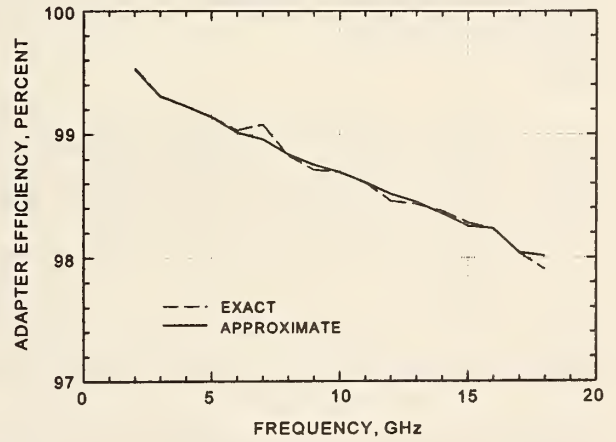


Figure A.3. Adapter efficiency.

References

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APPENDIX B. Theoretical Adapter Loss

Appendix A derives an expression for the loss of a special type N male-to-male adapter used in the determination of a correction factor g for the microcalorimeter. The result is in terms of measurable S parameters. The accuracy with which a small loss can be measured is limited at best, so additional support for the measurement in the form of a calculated result is useful.

The adapter is gold plated with an electroformed copper outer conductor and a beryllium copper inner conductor supported by a pair of dielectric beads. A cross sectional view of the adapter is shown in appendix A as figure A.1.

Calculation of the conductor loss for a plated coaxial transmission line is based on theory found in reference [B1]. Table 8.09 in the reference gives the attenuation due to the conductor as

$$\alpha_c = \frac{R}{2 Z_0}, \quad (\text{B-1})$$

where R is the conductor resistance and Z_0 is the transmission line characteristic impedance. R can be written in terms of the skin effect surface resistivity R_s as

$$R = \frac{R_s}{2 \pi} \left(\frac{1}{a} + \frac{1}{b} \right). \quad (\text{B-2})$$

The radius of the inner conductor is a and the inner radius of the outer conductor is b . The surface resistivity is given by

$$R_s = \frac{1}{\sigma \delta}, \quad (\text{B-3})$$

where σ is the conductivity of the conductor and δ is the skin depth. The skin depth is

$$\delta = \frac{1}{\sqrt{\pi f \mu \sigma}}, \quad (\text{B-4})$$

where f is the frequency and μ is the conductor permeability.

The conductors, being gold plated, are actually made up of two layers. Layer 1 is gold and layer 2 is beryllium copper for the inner conductor and copper for the outer conductor. Using the results found in section 5.19 of reference [B1] for two-layer conductors, the expression for the equivalent surface resistivity R_s of the combination for either the inner or outer conductor is

$$R_s = \Re \left(R_{s1} (1 + j) \left[\frac{\sinh \tau_1 d + (R_{s2}/R_{s1}) \cosh \tau_1 d}{\cosh \tau_1 d + (R_{s2}/R_{s1}) \sinh \tau_1 d} \right] \right). \quad (\text{B-5})$$

The subscripts 1 and 2 refer to the layers, d is the thickness of layer 1,

$$\tau_1 = \frac{(1 + j)}{\delta_1} = (1 + j) \sqrt{\pi f \mu_1 \sigma_1}, \quad (\text{B-6})$$

$$R_{S1} = \sqrt{\frac{\pi f \mu_1}{\sigma_1}}, \quad (\text{B-7})$$

and

$$R_{S2} = \sqrt{\frac{\pi f \mu_2}{\sigma_2}}. \quad (\text{B-8})$$

Finally then, the total coaxial line conductor loss A_C (in dB) is

$$A_C = 20 \ln \frac{L}{4 \pi Z_0} \left(\frac{R_{Si}}{a} + \frac{R_{So}}{b} \right), \quad (\text{B-9})$$

where L is the total line length, and R_{Si} and R_{So} are the results of applying eq (B-5) to the inner and outer conductors, respectively.

The loss due to joints at the connector and at the center conductor support beads is calculated using the experimental results found in reference [B2]. (Loss in the dielectric of the center conductor support bead is not included.) A general expression for the joint loss in dB is

$$A_J = A_0 + B f^E, \quad (\text{B-10})$$

where f is the frequency in GHz, A_0 and B are small experimentally determined constants (≈ 0.01), and E is a constant with a value between 0.5 and 1.

The work reported in reference [B2] gives A_0 a value of 0, B a value of 0.0088 for the type N joint and 0.0047 for a center conductor support bead joint, and E as 0.5 in both cases. Another investigator has found A_0 to be approximately 0.005, C approximately 0.007, and E very likely somewhat larger than 0.5.

Figure B.1 shows the calculated curves for the conductor (A_C), joint (A_J), and total adapter loss as a function of frequency. Table B.1 gives the values chosen for the different parameters used in the calculations.

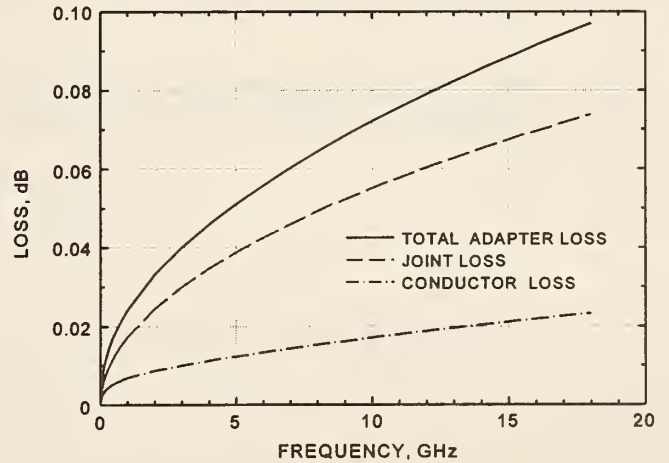


Figure B.1. Calculated adapter loss.

Table B.1. Values used in calculating adapter loss.

Fixed for all calculations:						
Parameter	Line length	Layer 1 (Au) permeability	Layer 2 (Cu) permeability	Inner cond. radius	Outer cond. radius	
	L	μ_1	μ_2	a	b	
	cm	H/m	H/m	cm	cm	
Values	4.57	$4\pi \times 10^{-7}$	$4\pi \times 10^{-7}$	0.1521	0.3500	
Changed in different calculations:						
Parameter	Layer 1 (Au) thickness	Layer 1 (Au) conductivity	Layer 2 (Cu) conductivity	Joint loss factors		
	d μm	σ_1 S/m	σ_2 S/m	A_0	B dB/(GHz) ^E	E
Inner conductor loss calculation	1.27	4.61×10^7	8.00×10^6	–	–	–
Outer conductor loss calculation	1.27	4.61×10^7	5.75×10^7	–	–	–
Type N joint loss calculation	–	–	–	0	0.008	0.5
Bead joint loss calculation	–	–	–	0	0.0047	0.5

REFERENCES

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APPENDIX C. Thermopile Stability Testing

This appendix describes statistical methods and algorithms for detecting "stable" periods in thermopile voltages as they evolve in time. The statistical methods that have been used essentially search for two types of instability: nonrandomness and trend. None of the statistical methods makes assumptions about the particular distributional properties of the data. Since they are not linked to variability, the methods should not have the shortcomings of variance-based criteria that cannot be successfully tuned to handle unpredictable changes in variability that may occur in the system. The methods that have been implemented are discussed briefly below.

RUNS TEST

A sequence of voltage readings $\{v_1, v_2, \dots, v_n\}$ may be analyzed for randomness by considering the magnitude of each element relative to that of the immediately preceding element in the time sequence. If the next element is larger, a run up is started; if smaller, a run down. We observe when the sequence increases, and for how long, when it decreases, and for how long. A decision concerning randomness is then based on the number of runs, R . Long runs, leading to a small value of R , should not occur in a set of stable, random voltage readings. A runs analysis should be sensitive to either trends or other low frequency periodicities in the data.

The runs test calculation is a simple function of the difference sequence $d_j = v_{j+1} - v_j$, for $j = 1, \dots, n - 1$. Under the assumption of randomness, the expected number of runs, μ_R , and the standard deviation, σ_R , of the number of runs for a sequence of length n are

$$\mu_R = \frac{2n - 1}{3}, \quad (C-1)$$

$$\sigma_R = \sqrt{\frac{16n - 29}{90}}. \quad (C-2)$$

If, for a given sequence of readings, R denotes the observed number of runs, the quantity

$$Z_R = \frac{R - \mu_R}{\sigma_R} \quad (C-3)$$

is used to test for nonrandomness. If the acceptable number of stable readings is n , then the value Z_R is calculated sequentially after each new voltage reading starting with the n th value obtained

after a change of frequency. Successive values of Z_R each are based on the preceding n readings, ending with the latest value. A threshold (or critical value) of Z_R , denoted by R_{CV} , determines if Z_R passes the test for stability based on the runs analysis. The criterion for RUNS stability is that $Z_R \geq R_{CV}$ be satisfied. The particular value R_{CV} may be chosen to provide any desired sensitivity to detecting excessively long runs. Currently, the value $R_{CV} = -2.5$ is being used.

KENDALL'S TEST FOR TREND

The following test is useful to detect a particular type of nonrandomness: namely, a monotonic trend in the sequence $\{v_1, v_2, \dots, v_n\}$. The procedure is complementary to the runs test. It seems to be more sensitive to the types of voltage drifts seen in the system, probably because it considers the relative magnitude of each voltage reading relative to every preceding measurement.

Kendall's test is derived from

$$\tau = \frac{S}{\sqrt{D n (n - 1) / 2}}, \quad (C-4)$$

where

$$S = \sum_{i=1}^{n-1} \sum_{j=i+1}^n \text{sign}(v_j - v_i), \quad (C-5)$$

$$D = \sum_{i=1}^{n-1} \sum_{j=i+1}^n [\text{sign}(v_j - v_i)]^2, \quad (C-6)$$

and $\text{sign}(d)$ is simply the sign of the voltage difference, or 0 if $v_i = v_j$. The value of τ is a measure of association between the voltage sequence and "time," and hence is indicative of trend. Its interpretation is similar to the usual correlation coefficient, for instance, it takes values between -1 and 1 .

To use Kendall's test for trend, we compute the test statistic

$$Z_S = \frac{S}{\sqrt{\text{Var}(S)}}, \quad (C-7)$$

where

$$\text{Var}(S) = [n(n-1)(2n+5) - T_v] / 18, \quad (C-8)$$

and $T_v = 0$ if there are no common voltages (i.e., ties) in the data sequence. Otherwise, T_v is computed by sorting the sequence and computing the multiplicity of each group of tied values. Then,

$$T_v = \sum t(t-1)(2t+5), \quad (C-9)$$

where the summation is over the number of sets of tied values. For a given set, t is the corresponding number of tied values ($t \geq 2$).

The software computes a probability (p) associated with Z_S , where a small value (say $p < 0.25$) would show an increasing trend and a large value (say $p > 0.75$) shows a significant decreasing trend. The particular values used to compare to p are arbitrary tuning constants that have been set by experience with the algorithm on the system. As the algorithm is refined and tested, the particular values of the tuning constants may be revised. Currently, the TREND criterion for accepting a sequence of n voltage readings as stable is that $0.25 < p < 0.75$.

STABILITY ALGORITHM

Suppose that n_a successive voltage readings are required for stability. Let μ_R and σ_R be the expected runs and standard deviation in equations (C-1) and (C-2) for sample size n_a . Following a change of frequency the algorithm is entered with an initial data set $\{v_1, v_2, \dots, v_n\}$ such that $n \geq n_a$.

- (A) $j \leftarrow n - n_a + 1$; Data = $\{v_j, v_{j+1}, \dots, v_n\}$
- (B) Compute: $R, Z_R; S, Z_S, p$ from n_a readings in Data.
- (C) If ($Z_R \geq -2.5$) and ($0.25 < p < 0.75$) then: compute $\bar{v} = \text{Average (Data)}$; $S_v = \text{Standard Deviation (Data)}$; EXIT: Data is stable. Otherwise, GOTO (D).
- (D) $n \leftarrow n + 1$; $v_n \leftarrow \{\text{next voltage}\}$; GOTO (A).

EXAMPLES

Figure C.1 shows the thermopile output for measurements at five frequencies on mount CN27_04. Graphical illustrations of the stability testing results at the first three frequencies are shown in figures C.2 - C.4. In each of the three figures, the vertical dashed lines represent endpoints of the region found to be acceptably stable, while the horizontal dashed line is plotted at the average voltage of readings in the stable region.

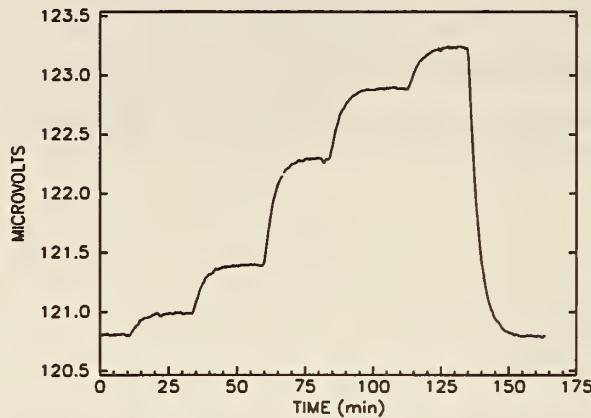


Figure C.1. Thermopile output versus time for CN27 at five check frequencies.

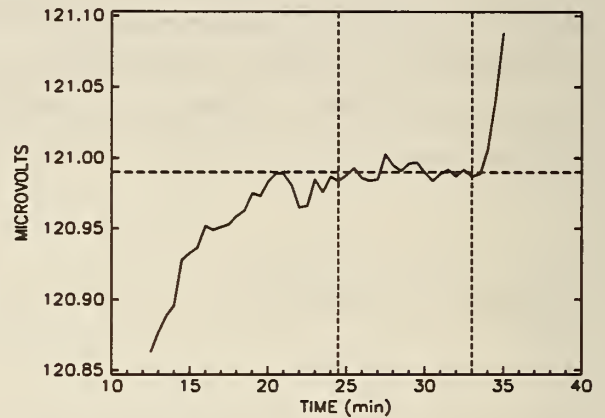


Figure C.2. Thermopile output versus time for CN27 at 100 MHz.

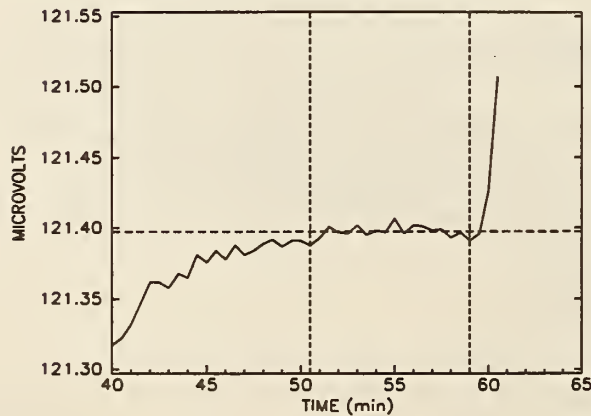


Figure C.3. Thermopile output versus time for CN27 at 3 GHz.

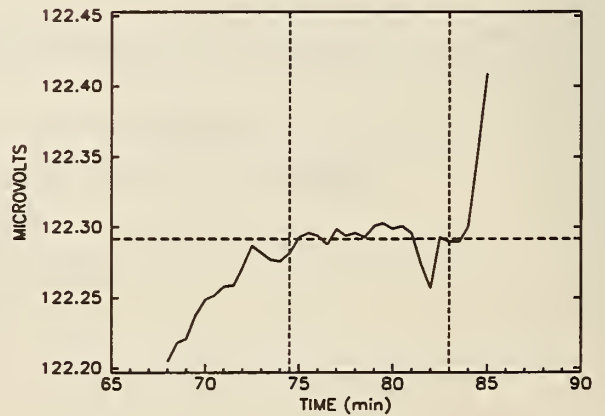


Figure C.4. Thermopile output versus time for CN27 at 10 GHz.

To illustrate the calculations, the sequence of numerical results at 10 GHz are listed in Tables C.1 and C.2. Since the required number of stable readings was $n_a = 18$, Table C.1 simply shows the sequential average and standard deviation calculated after each of the initial 17 readings. Stability checking (see Table C.2) began after the 18th reading, with the initial test results $Z_R = -6.29$ and $Z_S = 5.80$ with $p = 0.00$. The entries following Z_R and p show the respective test conclusions, indicating if the prior 18 readings passed (P) or failed (F) the RUNS and TREND stability tests, respectively, based on the criteria at step (C) of the algorithm. As the table shows, both procedures successfully passed tests after the 47th reading, thereby indicating that $\{v_{30}, v_{31}, \dots, v_{47}\}$ was an acceptable data set. The resulting average, $\bar{v} = 122.2916 \mu\text{V}$, was used in calculating the effective efficiency at 10 GHz.

Table C.1. Initial readings for mount CN27_04 at 10 GHz.

n	Time,s	μV	Average	S.D.
1	3600.1	121.426	121.4260	0.0000
2	3630.1	121.507	121.4665	0.0573
3	3660.1	121.598	121.5103	0.0860
4	3690.1	121.679	121.5525	0.1098
5	3720.1	121.764	121.5948	0.1341
6	3750.1	121.839	121.6355	0.1560
7	3780.1	121.912	121.6750	0.1766
8	3810.1	121.957	121.7103	0.1915
9	3840.1	122.004	121.7429	0.2042
10	3870.1	122.046	121.7732	0.2150
11	3900.1	122.081	121.8012	0.2241
12	3930.1	122.107	121.8267	0.2312
13	3960.1	122.132	121.8502	0.2370
14	3990.1	122.153	121.8718	0.2417
15	4020.1	122.177	121.8921	0.2458
16	4050.1	122.196	121.9111	0.2494
17	4080.1	122.205	121.9284	0.2517

Table C.2. Stability checking at 10 GHz: Average and S.D. of last 18 readings.

n	Time, s	μV	Average	S.D.	Z_R	Z_S	p
18	4110.1	122.218	121.9445	0.2536	-6.29 F	5.80	0.00 F
19	4140.1	122.221	121.9887	0.2257	-6.29 F	5.80	0.00 F
20	4170.1	122.238	122.0293	0.1980	-6.29 F	5.80	0.00 F
21	4200.1	122.249	122.0654	0.1723	-6.29 F	5.80	0.00 F
22	4230.1	122.252	122.0973	0.1480	-6.29 F	5.80	0.00 F
23	4260.1	122.258	122.1247	0.1268	-6.29 F	5.80	0.00 F
24	4290.1	122.259	122.1481	0.1084	-6.29 F	5.80	0.00 F
25	4320.1	122.272	122.1681	0.0947	-6.29 F	5.80	0.00 F
26	4350.1	122.287	122.1864	0.0826	-6.29 F	5.80	0.00 F
27	4380.1	122.282	122.2018	0.0717	-5.70 F	5.72	0.00 F
28	4410.1	122.277	122.2147	0.0623	-5.70 F	5.57	0.00 F
29	4440.1	122.276	122.2255	0.0541	-5.70 F	5.34	0.00 F
30	4470.1	122.282	122.2352	0.0467	-5.11 F	5.23	0.00 F
31	4500.1	122.293	122.2442	0.0409	-5.11 F	5.23	0.00 F
32	4530.1	122.296	122.2521	0.0357	-5.11 F	5.23	0.00 F
33	4560.1	122.294	122.2586	0.0316	-4.52 F	5.16	0.00 F
34	4590.1	122.288	122.2637	0.0281	-4.52 F	4.93	0.00 F
35	4620.1	122.299	122.2689	0.0251	-3.93 F	4.93	0.00 F
36	4650.1	122.294	122.2732	0.0223	-3.34 F	4.74	0.00 F
37	4680.1	122.296	122.2773	0.0187	-2.75 F	4.63	0.00 F
38	4710.1	122.293	122.2804	0.0162	-2.16 P	4.22	0.00 F
39	4740.1	122.301	122.2833	0.0149	-1.57 P	4.22	0.00 F
40	4770.1	122.303	122.2861	0.0134	-1.57 P	4.22	0.00 F
41	4800.1	122.299	122.2884	0.0117	-0.98 P	4.03	0.00 F
42	4830.1	122.301	122.2907	0.0094	-0.39 P	3.92	0.00 F
43	4860.1	122.296	122.2921	0.0083	-0.39 P	3.47	0.00 F
44	4890.1	122.274	122.2913	0.0092	-0.39 P	2.48	0.01 F
45	4920.1	122.257	122.2899	0.0121	-0.39 P	1.45	0.07 F
46	4950.1	122.293	122.2908	0.0117	-0.39 P	0.84	0.20 F
47	4980.1	122.290	122.2916	0.0111	0.20 P	0.00	0.50 P

APPENDIX D. Software Listing

```

7100 File$="MICRO_CXAP"
105 Rev$="9204061454" ! FRC, BFR
110 !
115 !
120 ! This program is a modification of MICRO_CAL. Its application is the
125 ! effective efficiency measurement of a thermistor mount using the
130 ! coax microcalorimeter. Default menu choices and the correction factor
135 ! are set for coax; waveguide microcalorimeter measurements can also
140 ! can also be made by choosing the appropriate menu item and changing
145 ! the correction factor. The correction factor is changed by changing
150 ! the four lines labeled G, G1, G2, and G3, and the RF subprogram.
155 ! Thermopile output (using the Keithley 181 nanovoltmeter),
160 ! and power meter voltage are the measured parameters.
165 ! Provision for temperature measurement is made but not implemented in
170 ! this version. It controls the instrumentation, does the calculations,
175 ! and outputs the results.
180 !
185 ! NOTES: This version can turn dc bias on & off, checking the nanovoltmeter
190 ! and thermopile zero.
195 ! This version is saving & looking for the temperature array, Tp,
200 ! even though it is not measured.
205 ! This version can run the entire frequency range of the coax
210 ! mounts, automatically.
215 !
220 ! INSTRUMENTS CONTROLLED:
225 ! 1. HP3457A DVM
230 ! 2. HP3488A SWITCH CONTROL UNIT
235 ! 3. EIP 578 LOCKING COUNTER
240 ! 4. KEITHLEY 181 DIGITAL NANOVOLTMETER
245 ! 5. EIP 931 0.01 - 18.6 GHz SOURCE
250 ! 6. DATA PRECISION 8200 DC SOURCE
255 !
260 ! DESCRIPTION OF THE MAIN VARIABLES:
265 !
270 ! These are in the labeled common /Data/.
275 !
280 ! * Dfile$ is the name of the data file (may include drive extension).
285 ! File name code example:
290 !
295 ! Waveguide: WR-90 Date (year, mo, day, hour)
300 ! (Coax: Type N = cn, APC-7 = c7)
305 !
310 ! * File1$ is the name of the program that generated the data file.
315 ! * Mount_id$ is the identifier of the mount calibrated.
320 !
325 ! --- The following are real arrays with TWO dimensions. -----
330 ! * V, an array containing in Col 1: the time of measurement;
335 ! in Col 2: the measured power meter voltages.
340 !
345 ! * E, an array containing in Col 1: the time of measurement;
350 ! in Col 2: the measured thermopile output voltage.
355 ! * AF, an array containing in each row of three columns the Start, Stop,
360 ! and Step sequences for each measurement set.
365 ! * F, an array containing in Col 1: the frequencies; in Col 2:
370 ! the beginning measurement No. for that frequency.
375 ! * Ne, an array containing in Col 1: the frequency; in Col 2:
380 ! the effective efficiency.
385 !
390 ! --- The following is a real array with ONE dimension. -----
395 ! * Header, an array with 27 elements, containing the housekeeping
400 ! information.
405 ! Each element is defined as follows:
410 ! (1) - Rev$, revision No., yr-mo-day-hour-min-sec format.
415 ! (2) - Test date, in "timedate" format.
420 ! (3) - Band Id, ie. "90" for WR-90.
425 ! (4) - Efficiency flag, indicates data set includes Ne,
430 ! the effective efficiency result array.
435 !
440 ! (5) - Total number of measurement frequencies
445 ! (6) - Starting measurement frequency
450 ! (7) - Final measurement frequency
455 ! (8) - Step frequency size (the first step may be different)
460 ! (9) - Total No. of measurements
465 ! (10) - Elapsed time for measurement series, sec
470 ! (11) - Measurement interval, sec
475 ! (12) - Nominal rf power level, mW
480 ! (13) - Reference voltage, volts
485 ! (14) - Mount operating resistance, ohms
490 ! (15) - Nanovoltmeter zero correction, volts
495 ! (16) - Pre-bias flag, mount dc biased before run
500 ! (17) - Room temperature
505 ! (18) - Bath temperature
510 ! (19) - zero correction flag, data includes dc OFF
515 ! (20) - Auto measure flag, indicates full data set taken
520 ! and stored automatically
525 ! (21) - Random frequency order flag
530 ! (22) -
535 ! (23) -
540 ! (24) -
545 ! (25) -
550 ! (26) -
555 ! (27) -
560 !
565 ! --- The following is an integer array with ONE dimension. -----
570 ! * Tp, an array containing the temperature measurements.
575 !
580 ! ***** INITIALIZATION *****
585 !
590 ! OPTION BASE 1
595 ! KEY LABELS OFF
600 ! Default graphics parameters
605 ! PLOTTER IS CRT, "INTERNAL", COLOR MAP
610 ! !Print color white
615 !
620 ! Common:
625 ! COM /Data/ Dfile$(20), File1$(16), Mount_id$(16)
630 ! COM /Data/ V(3000,2), E(3000,2), F(500,2), Ne(100,2), Header(27)
635 ! COM /Init_stats/ Tcv,Rcv,Enr,Sdnr,Volts(100), INTEGER Mode,Lss
640 ! COM /Flags/ Manual_freqs
645 ! COM /Xy_coordinates/ T_min,T_max,Vpmin,Vpmax
650 !
655 ! T_max=43200
660 ! T_min=0
665 ! Vpmax=1.21E-4
670 ! Vpmin=1.17E-4
675 ! Lss=18
680 !
685 ! Mcontrol: ! ***** MAIN MENU AND CONTROL *****
690 !
695 ! IF V(1,2) OR E(1,2) THEN CALL New_size !If data still in common, re_dim
700 ! Sys_ptr=VAL(SYSTEM$( "SYSTEM PRIORITY" )) !Determine system priority
705 ! Lcl_ptr=Sys_ptr+1 !Set local priority 1 higher for ON KEY
710 ! Softkey interrupts:
715 ! FOR N=0 TO 19
720 ! ON KEY N LABEL " " GOTO Top
725 ! NEXT N
730 ! ON KEY 0 LABEL " EXIT PROGRAM " ,Lcl_ptr GOTO End
735 ! ON KEY 5 LABEL " SELECT (1) " ,Lcl_ptr GOSUB Measure
740 ! ON KEY 6 LABEL " SELECT (2) " ,Lcl_ptr GOSUB Calcdisp
745 ! ON KEY 7 LABEL " SELECT (3) " ,Lcl_ptr GOSUB Iodfile
750 ! ON KEY 9,Lcl_ptr CALL Blank !Turn CRT back on after meas
755 ! M_flg=1 !Set flag to display menu
760 ! KEY LABELS ON
765 ! Top:LOOP

```



```

770 IF M_flg THEN GOSUB Main_menu
775 END LOOP
780 !
785 Measure:
790 INTEGER Counter
795 CALL Soft_init(Z_flg)
800 File$=File$
805 Header(1)=VAL(Rev$)
810 IF Mount_id$="" THEN CALL Mount_id !To get the mount identifier
815 ! CALL Hard_init
820 Counter=0
825 Wk1: !
830 LOOP
835 EXIT IF Nomore_f
840 Counter=Counter+1
845 IF Counter=1 THEN
850 CALL Generate_freq(Nomore_f,Counter)!Produces start, stop, step freq
855 CALL Freq_change_pts(1) !Set up frequency list & display
860 CALL New_size !Resize after any possible changes
865 CALL Display_data !Init the voltage/time parameters
870 ELSE
875 CALL Re_set !Partial software init
880 CALL Generate_freq(Nomore_f,Counter)!Produces start, stop, step freq
885 CALL New_size !Resize arrays
890 CALL Freq_change_pts(0) !Set up frequency list, no display
895 END IF
900 IF Counter=1 AND Header(16) THEN CALL Pre_bias(1) !To set up for
pre_bias
905 IF Counter=1 THEN CALL Delay_start !Wait until start time
910 IF Counter=1 AND Header(16) THEN CALL Pre_bias(0) !To do the pre_bias
915 CALL File_name !To set up the file name
920 CALL Meas_disp !To set up screen display for Meas
925 IF NOT Header(19) THEN CALL Dc(1,2) !Be sure bias is on, if no zero
check
930 CALL Meas !Do the measurement
935 IF Header(20) THEN CALL Save_data(1) !If auto mode, save the meas
940 EXIT IF NOT Header(20) !Once thru if manual or ball out
945 END LOOP
950 M_flg=1
955 RETURN
960 !
965 Calcdisp:
970 IF V(1,2) OR E(1,2) THEN
975 CALL Calc_disp
980 M_flg=1
985 ELSE
990 CALL Flash(" NO DATA IN MEMORY ")
995 M_flg=1
1000 END IF
1005 RETURN
1010 !
1015 Iodfile:
1020 CALL Io_dfile
1025 M_flg=1
1030 RETURN
1035 !
1040 Main_menu:
1045 OUTPUT KBD;"K";
1050 PRINT TABXY(5,2),CHR$(137)&"M I C R O - C X A P"&CHR$(136)
1055 Crt_id$=SYSTEM$( "CRT ID" )
1060 IF Crt_id$(4,5)="" THEN
1065 CLIP 10,11,24,84
1070 ELSE
1075 CLIP 4,74,62,92
1080 END IF
1085 PEN 5
1090 FRAME

```

```

1095 PRINT TABXY(25,7)," - - - - - MAIN MENU - - - - -"
1100 PRINT TABXY(25,10),"(1) MEASURE EFFICIENCY"
1105 PRINT TABXY(25,12),"(2) CALCULATE & DISPLAY RESULTS"
1110 PRINT TABXY(25,14),"(3) DATA FILE I/O"
1115 IF V(1,2) OR E(1,2) THEN
1120 PRINT TABXY(59,18),CHR$(129)&" DATA IN MEMORY "&CHR$(128)
1125 IF Dfile$="" THEN
1130 PRINT TABXY(59,19),CHR$(129)&" (NO FILE NAME) "&CHR$(128)
1135 ELSE
1140 PRINT TABXY(59,19),CHR$(129)&" FILE:"&Dfile$&CHR$(128)
1145 END IF
1150 ELSE
1155 PRINT TABXY(56,19),CHR$(129)&" NO DATA IN MEMORY "&CHR$(128)
1160 END IF
1165 M_flg=0 !Lower menu flag
1170 RETURN
1175 !
1180 END: CLEAR SCREEN
1185 END: MICRO_Ck??
1190!* * * * * S U B P R O G R A M S * * * * *
1195 Io_dfile: !
1200 SUB Io_dfile
1205 OPTION BASE 1
1210 COM /Data/ Dfile$(20),File$(16),Mount_id$(16)
1215 COM /Data/ V(3000,2),E(3000,2),P(500,2),Ne(100,2),Header(27)
1220 COM /Data/ Af(10,3),INTEGER Tp(3000)
1225 M_flg=1 !Set flag to print menu
1230 No-Header(9) !Total measurement #
1235 Sys_ptr=VAL(SYSTEM$( "SYSTEM PRIORITY" )) !Determine system priority
1240 Lcl_ptr=Sys_ptr+1 !Set local priority 1 higher for ON KEY
1245 FOR N=0 TO 19
1250 ON KEY N LABEL " " GOTO Top
1255 NEXT N
1260 ON KEY 0 LABEL " MAIN MENU ",Lcl_ptr GOTO Exit
1265 ON KEY 5 LABEL " SELECT (1) ",Lcl_ptr GOSUB Disphdr
1270 ON KEY 6 LABEL " SELECT (2) ",Lcl_ptr GOSUB Get_data
1275 ON KEY 7 LABEL " SELECT (3) ",Lcl_ptr GOSUB Save_data
1280 KEY LABELS ON
1285 Top: LOOP
1290 IF M_flg THEN GOSUB Menu
1295 END LOOP
1300 !
1305 Disphdr:
1310 IF Header(1) THEN
1315 CALL Disp_hdr
1320 M_flg=1 !To restore menu
1325 ELSE
1330 CALL Flash(" NO HEADER DATA IN MEMORY ")
1335 M_flg=1 !Because no data in memory
1340 END IF
1345 RETURN
1350 !
1355 Save_data:
1360 IF V(1,2) OR E(1,2) THEN
1365 CALL Save_data(0)
1370 M_flg=1 !To restore menu
1375 ELSE
1380 CALL Flash(" NO DATA IN MEMORY ")
1385 M_flg=1 !Because no data in memory
1390 END IF
1395 RETURN
1400 !
1405 Get_data:
1410 CALL Get_data
1415 M_flg=1 !Retrieve BDATA file
1420 RETURN
1425 !

```

```

1430 Menu:
1435 OUTPUT KBD,"K";
1440 PRINT TABXY(5,2),CHR$(137)&"M I C R O _ C X A P"&CHR$(136)
1445 PEN 1
1450 FRAME
1455 PRINT CHR$(138)
1460 PRINT TABXY(25,7)," - - - DATA I/O MENU - - -"
1465 PRINT TABXY(25,10),"(1) Header listing/change"
1470 PRINT TABXY(25,12),"(2) Input a data file"
1475 PRINT TABXY(25,14),"(3) Output a data file"
1480 IF V(1,2) OR E(1,2) THEN
1485 PRINT TABXY(59,18),CHR$(129)&" DATA IN MEMORY "&CHR$(128)
1490 IF Dfiles="" THEN
1495 PRINT TABXY(59,19),CHR$(129)&" (NO FILE NAME) "&CHR$(128)
1500 ELSE
1505 PRINT TABXY(59,19),CHR$(129)&" FILE:"&Dfiles&CHR$(128)
1510 END IF
1515 ELSE
1520 PRINT TABXY(56,19),CHR$(129)&" NO DATA IN MEMORY "&CHR$(128)
1525 END IF
1530 M_flg=0
1535 RETURN
1540 !
1545 Exit-OPF KEY
1550 SUBEND ! Io_dfile
1555 ! * * * * *
1560 Disp_hdr: !
1565 SUB Disp_hdr
1570 OPTION BASE 1
1575 COM /Data/ Dfiles[20],File1[16],Mount_id[16]
1580 COM /Data/ V(3000,2),F(3000,2),F(500,2),Ne(100,2),Header(27)
1585 COM /Data/ Af(10,3),INTEGER Tp(3000)
1590 INTEGER Ans
1595 Disp_hdr: !Print out the header items
1600 OUTPUT KBD,"K";
1605 IF V(1,1) THEN
1610 PRINT TABXY(17,1),CHR$(138),CHR$(132),"HEADER LISTING
FOR: ",CHR$(128),CHR$(136)," A Previous Measurement";CHR$(138)
ELSE
1615 PRINT TABXY(17,1),CHR$(138),CHR$(132),"HEADER LISTING
FOR: ",CHR$(128),CHR$(136)," A New Measurement";CHR$(138)
END IF
1625 PRINT
1630 PRINT "Option Array #"
1635 PRINT " (1) - - - - Data file name: ";CHR$(136),Dfiles;CHR$(138)
1640 PRINT " (2) - - - - Mount ID: ";CHR$(136),Mount_id;CHR$(138)
1645 PRINT " (3) - - - - Measurement program: ";CHR$(136),File1;CHR$(138)
1650 IMAGE " (4) [1] Revision #: ";CHR$(136),A
1655 PRINT USING 1655;CHR$(136),Header(1);CHR$(138)
1660 IF Header(2) THEN
1665 PRINT " (5) [2] Test date: ";CHR$(136),DATE$(Header(2)),",
",TIME$(Header(2)),CHR$(138)
ELSE
1675 PRINT " (5) [2] Test date: ";CHR$(136),"NA";CHR$(138)
END IF
1685 IF Header(3) THEN
1690 PRINT " (6) [3] Band ID: WR-";CHR$(136),Header(3);CHR$(138)
ELSE
1700 PRINT " (6) [3] Band ID: ";CHR$(136),"Coax";CHR$(138)
END IF
1710 PRINT " (7) [4] Effective efficiency flag:
";CHR$(136),Header(4);CHR$(138)
1715 PRINT " (8) [5] No. of measurement frequencies:
";CHR$(136),Header(5);CHR$(138)
1720 PRINT " (9) [6] Start frequency:
";CHR$(136),Header(6);CHR$(138);"GHz"
1725 PRINT " (10) [7] Stop frequency:
";CHR$(136),Header(7);CHR$(138);"GHz"
1730 PRINT " (11) [8] Step frequency:
";CHR$(136),Header(8);CHR$(138);"GHz"
1735 PRINT " (12) [9] Number of measurements:
";CHR$(136),Header(9);CHR$(138)
1740 IMAGE " (13) [10] Measurement duration: ";A,22,DD,A," hr"
1745 PRINT USING 1745;CHR$(136),Header(10)/3600;CHR$(138)
1750 PRINT " (14) [11] Measurement interval:
";CHR$(136),Header(11);CHR$(138);"sec"
1755 IMAGS " (15) [12] Nominal power: ";A,DD,D,A," mW"
1760 PRINT USING 1760;CHR$(136),Header(12);CHR$(138)
1765 PRINT " (16) [13] Voltage reference:
";CHR$(136),Header(13);CHR$(138);"volts"
1770 PRINT " (17) [14] Mount operating resistance:
";CHR$(136),Header(14);CHR$(138);"ohms"
1775 PRINT " (18) [15] Nanovoltmeter zero correction:
";CHR$(136),Header(15);CHR$(138)
1780 PRINT " (19) [16] Mount pre_bias flag:
";CHR$(136),Header(16);CHR$(138)
1785 PRINT " (20) [17] Room temperature:
";CHR$(136),Header(17);CHR$(138)
1790 PRINT " (21) [18] Bath temperature:
";CHR$(136),Header(18);CHR$(138)
1795 PRINT " (22) [19] Zero correction flag:
";CHR$(136),Header(19);CHR$(138)
1800 PRINT " (23) [20] Auto meas flag: ";CHR$(136),Header(20);CHR$(138)
1805 PRINT " (24) [21] Random freq order flag:
";CHR$(136),Header(21);CHR$(138)
1810 PRINT CHR$(128)
1815 CONTROL CRT,12,2 !Turn on key labels
1820 Sys_ptrty=VAL(SYSTEM$( "SYSTEM PRIORITY" )) !Determine System priority
1825 Lcl_ptrty=Sys_ptrty+1 !Set local priority 1 higher for ON KEY
1830 FOR N=0 TO 19
1835 ON KEY N LABEL " " GOTO Top
NEXT N
1840 ON KEY 5 LABEL "CHANGE listing",Lcl_ptrty GOTO Edit
1845 ON KEY 0 LABEL " CONTINUE " Lcl_ptrty GOTO Disp_exit
1850 Top: LOOP
1855 END LOOP
1860 Edit:
1865 CONTROL CRT,12,1 !Turn off labels
1870 INPUT "Input item number to change: ",Ans
1875 SELECT Ans
1880 CASE 1
1885 INPUT "Input new data file name: ",Dfiles
1890 CASE 2
1895 INPUT "Input mount ID: ",Mount_id
1900 CASE 3
1905 INPUT "Input measurement program name: ",File1
1910 CASE 4
1915 INPUT "Input revision number: ",Header(1)
1920 CASE 5
1925 INPUT "Input band ID: ",Header(3)
1930 CASE 6
1935 GOTO Disp_hdr
1940 CASE 7
1945 INPUT "Input effective efficiency flag: ",Header(4)
1950 CASE 8
1955 INPUT "Input start frequency: ",Header(6)
1960 CASE 9
1965 INPUT "Input stop frequency: ",Header(7)
1970 CASE 10
1975 INPUT "Input step frequency: ",Header(8)
1980 CASE 11
1985 INPUT "Input no. of measurement frequencies: ",Header(5)
1990 CASE 12
2000 INPUT "Input no. of measurements: ",Header(9)
2005

```



```

2010 CALL New_size
2015 CASE 14
2020 INPUT "Input measurement interval: ",Header(11)
2025 CASE 15
2030 INPUT "Input power: ",Header(12)
2035 CASE 16
2040 GOTO Disp_hdr
2045 CASE 17
2050 INPUT "Input mount resistance: ",Header(14)
2055 CASE 18
2060 INPUT "Nanovoltmeter zero correction: ",Header(15)
2065 CASE 19
2070 INPUT "Mount pre-bias flag: ",Header(16)
2075 CASE 20
2080 INPUT "Room temperature: ",Header(17)
2085 CASE 21
2090 INPUT "Bath temperature: ",Header(18)
2095 CASE 22
2100 INPUT "Zero correction flag: ",Header(19)
2105 CASE 23
2110 INPUT "Auto meas flag: ",Header(20)
2115 CASE 24
2120 INPUT "Random freq order flag: ",Header(21)
2125 CASE ELSE
2130 GOTO Disp_hdr
2135 END SELECT
2140 GOTO Disp_hdr
2145 Disp_exit:
2150 OFF KEY
2155 SUBEND
2160 ! * * * * *
2165 Calc_disp:
2170 SUB Calc_disp
2175 OPTION BASE 1
2180 COM /Data/ Drive$(20),File$(16),Mount_id$(16)
2185 COM /Data/ V(3000,2),E(3000,2),F(3000,2),Ne(100,2),Header(27)
2190 COM /Data/ Af(10,3),INTEGER Tp(3000)
2195 COM /Grph_prt/ Pwr(100,2)
2200 DIM B$(60)
2205 Sys_prt=VAL(SYSTEM$( "SYSTEM PRIORITY" )) !Determine system priority
2210 Lcl_prt=Sys_prt+1 !Set local priority 1 higher for ON KEY
2215 !
2220 FOR N=0 TO 19
2225 ON KEY N LABEL " " GOTO Top
2230 NEXT N
2235 ON KEY 0 LABEL " MAIN MENU " ,Lcl_prt GOTO Exit
2240 ON KEY 5 LABEL " SELECT (1) " ,Lcl_prt GOSUB Grphv
2245 ON KEY 6 LABEL " SELECT (2) " ,Lcl_prt GOSUB Grphe
2250 ON KEY 7 LABEL " SELECT (3) " ,Lcl_prt GOSUB Grphn
2255 ON KEY 8 LABEL " SELECT (4) " ,Lcl_prt GOSUB Grphp
2260 ON KEY 9 LABEL " SELECT (5) " ,Lcl_prt GOSUB Grpht
2265 ON KEY 1 LABEL " SELECT (6) " ,Lcl_prt GOSUB Calc_sd
2270 M_flg=1
2275 Top:LOOP
2280 IF M_flg THEN GOSUB Menu
2285 END LOOP
2290 !
2295 Grphv:
2300 IF V(1,1)=0 THEN
2305 CALL Flash(" NO DATA ")
2310 ELSE
2315 Ptf1g=1
2320 B$="MOUNT VOLTAGE CHANGE VS TIME"
2325 CALL Graph_v(Ptf1g,B$)
2330 END IF
2335 M_flg=1
2340 RETURN

```

```

2345 !
2350 Grphe:
2355 Ptf1g=2
2360 B$="THERMOPILE VOLTAGE CHANGE VS TIME"
2365 CALL Graph_v(Ptf1g,B$)
2370 M_flg=1
2375 RETURN
2380 !
2385 Grpht:
2390 IF Tp(1)=0 THEN
2395 CALL Flash(" NO DATA ")
2400 ELSE
2405 Ptf1g=3
2410 B$="TEMPERATURE CHANGE VS TIME"
2415 CALL Graph_v(Ptf1g,B$)
2420 END IF
2425 M_flg=1
2430 RETURN
2435 !
2440 Grphn:
2445 OUTPUT KBD;"K";
2450 IF NOT Header(4) THEN CALL Eff_calc !Do power calculation if not done
2455 Ptf1g=0
2460 CALL Graph_n_p(Pf1g)
2465 M_flg=1
2470 RETURN
2475 !
2480 Grpht:
2485 OUTPUT KBD;"K";
2490 IF NOT Pwr(1,1) THEN CALL Eff_calc !Do power calculation if not done
2495 Ptf1g=1
2500 CALL Graph_n_p(Pf1g)
2505 M_flg=1
2510 RETURN
2515 !
2520 Calc_sd:
2525 OUTPUT KBD;"K";
2530 CALL Std_dev
2535 M_flg=1
2540 RETURN
2545 Menu:
2550 OUTPUT KBD;"K";
2555 PRINT TABXY(5,2),CHR$(137)&"M I C R O _ C x A P"&CHR$(136)
2560 Crt_id$=SYSTEM$( "CRT ID" ) !To find out the # of CRT col.
2565 IF Crt_id$(4,5)="80" THEN
2570 CLIP 10,117,24,84
2575 ELSE
2580 CLIP 4,74,62,92
2585 END IF
2590 PEN 1
2595 FRAME
2600 PRINT CHR$(140)
2605 PRINT TABXY(20,6)," - - - CALCULATE/DISPLAY MENU - - - "
2610 PRINT TABXY(25,8)," (1) Graph power meter voltage"
2615 PRINT TABXY(25,10)," (2) Graph thermopile voltage"
2620 PRINT TABXY(25,12)," (3) Graph/Print effective efficiency"
2625 PRINT TABXY(25,14)," (4) Graph Rf Power"
2630 PRINT TABXY(25,16)," (5) Graph Temperature"
2635 PRINT TABXY(25,18)," (6) Calculate standard deviation"
2640 IF V(1,2) OR B(1,2) THEN
2645 PRINT TABXY(59,18),CHR$(129)&" DATA IN MEMORY "&CHR$(128)
2650 IF Dfile$="" THEN
2655 PRINT TABXY(59,19),CHR$(129)&" (NO FILE NAME) "&CHR$(128)
2660 ELSE
2665 PRINT TABXY(59,19),CHR$(129)&" FILE:"&Dfile$&CHR$(128)
2670 END IF
2675 ELSE

```

```

2680 PRINT TABXY(56,19),CHR$(129)&" NO DATA IN MEMORY "&CHR$(128)
2685 END IF
2690 M_flg=0
2695 RETURN
2700 Exit:OFF KEY
2705 SUBEND
2710 !*****
2715 Graph_v:
2720 SUB Graph_v(Ptflg,B$)
2725 ! For Ptflg=1 : Graph power meter voltage
2730 ! For Ptflg=2 : Graph thermopile output
2735 ! For Ptflg=3 : Graph temperature probe output
2740 ! B$ passes the plot title
2745 OPTION BASE 1
2750 COM /Data/ dfiles[20],Mount_id$[16]
2755 COM /Data/ V(3000,2),F(3000,2),Ne(100,2),Header(27)
2760 COM /Data/ Af(10,3),INTEGER Tp(3000)
2765 No-Header(9)
2770 ALLOCATE A$(80)
2775 ALLOCATE P(No,2)
2780 Sys_prtv=VAL(SYSTEM$("SYSTEM PRIORITY")) !Determine system priority
2785 !cl_prtv=Sys_prtv+1
2790 G_flg=1
2795 FOR N=0 TO 19
2800 ON KEY N LABEL " " GOTO Top
2805 NEXT N
2810 ON KEY 0 LABEL " PREV MENU ",!cl_prtv GOTO Exit
2815 ON KEY 1 LABEL " DUMP plot ",!cl_prtv GOSUB Dump
2820 ON KEY 5 LABEL "CHANGE x-axis ",!cl_prtv GOSUB Chg_x
2825 ON KEY 6 LABEL "CHANGE y-axis ",!cl_prtv GOSUB Chg_y
2830 Top:LOOP
2835 IF G_flg THEN GOSUB Graph
2840
2845 IF Chg_flg THEN GOSUB Graph_xy
2850 !
2855 Chg_x:
2860 Ans$=""
2865 DISP "New Tmin <";Tmin/60;"> "; !Ask if change for Tmin
2870 INPUT Ans$ !Get response
2875 IF Ans$<>" THEN Tmin=60.*VAL(Ans$)
2880 Ans$=""
2885 DISP "New Tmax <";Tmax/60;"> "; !Ask if change for Tmax
2890 INPUT Ans$ !Get response
2895 IF Ans$<>" THEN Tmax=60.*VAL(Ans$)
2900 Ans$=""
2905 Chg_flg=1
2910 RETURN
2915 !
2920 Chg_y:
2925 DISP "New Vmin <";Vpmin;"> "; !Ask if change for Vmin
2930 INPUT Ans$ !Get response
2935 IF Ans$<>" THEN Vpmin=VAL(Ans$)
2940 Ans$=""
2945 DISP "New Vmax <";Vpmax;"> "; !Ask if change for Vmax
2950 INPUT Ans$ !Get response
2955 IF Ans$<>" THEN Vpmax=VAL(Ans$)
2960 Chg_flg=1
2965 RETURN
2970 !
2975 Dump:
2980 OUTPUT KBD;"K";
2985 CONTROL 1,12;1
2990 GOSUB Graph_xy
2995 OUTPUT KBD;"N";
3000 CONTROL 1,12;0
3005 RETURN
3010 !

```

```

3015 Graph:
3020 SELECT Ptflg
3025 CASE 1
3030 MAT P= V
3035 CASE 2
3040 MAT P= E
3045 CASE 3
3050 MAT P= E
3055 FOR N=1 TO No
3060 P(N,2)=Tp(N)
3065 NEXT N
3070 END SELECT
3075 IF P(No,1)>1.E+6 THEN
3080 FOR N=1 TO No
3085 P(N,1)=P(N,1)-Header(2)
3090 NEXT N
3095 END IF
3100 Tmax=P(No,1)
3105 Tmin=0
3110 Vpmax=P(1,2)
3115 Vpmin=P(1,2)
3120 FOR N=2 TO No
3125 IF Vpmax<P(N,2) THEN Vpmax=P(N,2)
3130 IF Vpmin>P(N,2) THEN Vpmin=P(N,2)
3135 NEXT N
3140 Vpmax=Vpmax+.05*ABS(Vpmax-Vpmin) !Find the plot max + 5%
3145 Vpmin=Vpmin-.05*ABS(Vpmax-Vpmin) !Find the plot min - 5%
3150 Graph_xy:
3155 OUTPUT KBD;"K";
3160 GINIT
3165 LONG 6
3170 PEN 5
3175 MOVE 75,100
3180 CSIZE 3.0
3185 A$=DATES(TIMEDATE)&","&TIMES(TIMEDATE)
3190 A$=B$&" "
3195 LABEL A$
3200 MOVE 75,95
3205 A$="MOUNT: "&Mount_id$&" PROGRAM: "&Filei$&" DATA FILE: "&dfile$
3210 LABEL A$
3215 CSIZE 4.0
3220 MOVE 70,12
3225 LABEL "TIME (min)"
3230 MOVE 0,55
3235 LDIR PI/2
3240 SELECT Ptflg
3245 CASE 1
3250 LABEL "MILLIVOLTS"
3255 CASE 2
3260 LABEL "MICROVOLTS"
3265 CASE 3
3270 LABEL "DEGREES C "
3275 END SELECT
3280 LDIR 0
3285 PEN 1
3290 VIEWPORT 20,125,16,90
3295 MOVE 0,0
3300 WINDOW Tmin,Tmax,Vpmin,Vpmax !Scale factors
3305 ! Set up x-axis tic and label spacing
3310 Range=Tmax-Tmin
3315 SELECT Range
3320 CASE <=5400
3325 X=60
3330 Xtic=10
3335 Stp=600
3340 CASE <=18000
3345 X=600

```

!Main graph routine

!For power meter

!For thermopile

!For temperature - thermo time in Col 1

!Temp into Col 2

!Check for elapsed or absolute time

!Change to elapsed

!Find Max time

!Find the plot max/min

!Find the plot max + 5%

!Find the plot min - 5%

!Alternate entry point

!Clear screen

!All labels ref. top center

!Move to top for title label

!Smaller letters

!Add date to title

!Write title

!Move for sub title

PROGRAM: "&Filei\$&" DATA FILE: "&dfile\$

!Write title

!Little larger letters

!For horizontal axes label

!Write label

!For vertical axis label

!Rotate 90

!For power meter

!For thermopile

!For temperature

!Back to horizontal

!Subset of screen area

!Cure for WINDOW error

!Scale factors

!Horizontal scale range in seconds

!For Range <= 90 min

!X-tics every 1 min

!10 tics/major div

!Labels every 10 min

!For 300 min >=Range> 120 min

!X-tics every 10 min


```

4015 !
4020 D_1400: !Save on 360 hard drive
4025 N_name$="\\USERS\\FRC\\&file$":1400"
4030 GOSUB Save
4035 Msg_flg=1
4040 RETURN
4045 !
4050 D_2: !Save on vol ? of the hard drive
4055 INPUT "What hard volume ?","Vq$
4060 N_name$=Dfile$&":700,0,"&Vq$
4065 GOSUB Save
4070 Msg_flg=1
4075 RETURN
4080 !
4085 C_name: !To change file name
4090 INPUT "Input the new file name",Dfile$
4095 Msg_flg=1
4100 RETURN
4105 !
4110 Save: !Save the data
4115 DISP "File name:",N_name$ !Print the name
4120 CALL New_size
4125 IF Header(4) THEN !Indicates ER array to be saved
4130 Rec_no=(LEN(Test_dates)-LEN(File$)+8*27*34*No-32*(No1+2))/256+1
4135 CREATE BDAT N_name$,Rec_no !Create it
4140 ASSIGN @Path1 TO N_name$ !Open & set file pointer at beginning
4145 Output all test information and files
4150 OUTPUT @Path1;File$,Mount_id$,Header(*)
4155 OUTPUT @Path1;8(*),V(*),P(*),Tp(*),Ne(*),END
4160 ELSE !ER array not saved
4165 Rec_no=(LEN(Test_dates)-LEN(File$)+8*27*34*No-16*(No1+2))/256+1
4170 CREATE BDAT N_name$,Rec_no !Create it
4175 ASSIGN @Path1 TO N_name$ !Open & set file pointer at beginning
4180 Output all test information and files
4185 OUTPUT @Path1;File$,Mount_id$,Header(*)
4190 OUTPUT @Path1;8(*),V(*),P(*),Tp(*),END
4195 END IF
4200 ASSIGN @Path1 TO * !Close file
4205 RETURN
4210 Exit:OFF KEY
4215 SUBEND
4220 ! * * * * *
4225 Get_data: !
4230 SUB Get_data !Retrieve BDAT data file
4235 OPTION BASE 1
4240 COM /Data/ Dfile$(20),File$(16),Mount_id$(16)
4245 COM /Data/ V(3000,2),E(3000,2),P(500,2),Ne(100,2),Header(27)
4250 COM /Data/ Af(10,3),INTEGER Tp(3000)
4255 Msg_flg=1
4260 ALLOCATE N_name$(20),D14files(30)
4265 Sys_prtv=VAL(SYSTEM$( "SYSTEMS PRIORITY" )) !Determine system priority
4270 Lcl_prtv=Sys_prtv+1 !Set local priority 1 higher for ON KEY
4275 FOR N=0 TO 15
4280 ON KEY N LABEL " " GOTO Top
4285 NEXT N
4290 ON KEY 0 LABEL " PREV MENU " ,Lcl_prtv GOTO Exit
4295 ON KEY 1 LABEL " CAT 700,1 " ,Lcl_prtv GOSUB Cat_3_5
4300 ON KEY 2 LABEL " CAT 702,0 " ,Lcl_prtv GOSUB Cat_3_5_0
4305 ON KEY 3 LABEL " CAT 702,1 " ,Lcl_prtv GOSUB Cat_3_5_1
4310 ON KEY 4 LABEL " CAT 1400 " ,Lcl_prtv GOSUB Cat_1400
4315 ON KEY 5 LABEL " INPUT name " ,Lcl_prtv GOSUB C_name
4320 ON KEY 6 LABEL " LOAD 700,1 " ,Lcl_prtv GOSUB Ld_3_5
4325 ON KEY 7 LABEL " LOAD 702,0 " ,Lcl_prtv GOSUB Ld_3_5_0
4330 ON KEY 8 LABEL " LOAD 702,1 " ,Lcl_prtv GOSUB Ld_3_5_1
4335 ON KEY 9 LABEL " LOAD 1400 " ,Lcl_prtv GOSUB Ld_1400
4340 KEY LABELS ON
4345 Top:LOOP

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4350 IF Msg_flg THEN GOSUB Msg1
4355 END LOOP
4360 !
4365 Msg1: !Put message on screen
4370 OUTPUT KBD;"K"; !Clear screen
4375 PRINT TABXY(30,14),"DATA FILE INPUT "
4380 IF Dfile$="" THEN
4385 PRINT TABXY(5,16),"File in memory: ";CHR$(136),"NONE";CHR$(138)
4390 ELSE
4395 PRINT TABXY(5,16),"File in memory: ";CHR$(136);Dfile$;CHR$(138)
4400 END IF
4405 IF N_name$="" THEN
4410 PRINT TABXY(5,18),CHR$(140),"Select softkey option.";CHR$(138)
4415 ELSE
4420 PRINT TABXY(5,18),"Requested file name: ";CHR$(136);N_name$;CHR$(140)
4425 PRINT TABXY(5,19),"(Select soft key option to load the file.)"
4430 END IF
4435 Msg_flg=0
4440 RETURN
4445 !
4450 Cat_3_5: !Cat 3.5" drive
4455 CAT ":700,1"
4460 RETURN
4465 !
4470 Ld_3_5: !Load from 3.5" drive
4475 IF N_name$="" THEN
4480 DISP "Have not been given a file name."
4485 WAIT 1
4490 DISP ""
4495 GOTO R35
4500 END IF
4505 Dfile$=N_name$&":700,1"
4510 N_name$=""
4515 GOSUB Get_data
4520 GOTO Exit
4525 R35:RETURN
4530 !
4535 Cat_3_5_0: !Cat dual 3.5", drive 0
4540 CAT ":702,0"
4545 RETURN
4550 !
4555 Ld_3_5_0: !Load from dual 3.5", drive 0
4560 IF N_name$="" THEN
4565 DISP "Have not been given a file name."
4570 WAIT 1
4575 DISP ""
4580 GOTO R350
4585 END IF
4590 Dfile$=N_name$&":702,0"
4595 N_name$=""
4600 GOSUB Get_data
4605 GOTO Exit
4610 R350:RETURN
4615 !
4620 Cat_3_5_1: !Cat dual 3.5", drive 1
4625 CAT ":702,1"
4630 RETURN
4635 !
4640 Ld_3_5_1: !Load from dual 3.5", drive 1
4645 IF N_name$="" THEN
4650 DISP "Have not been given a file name."
4655 WAIT 1
4660 DISP ""
4665 GOTO R351
4670 END IF
4675 Dfile$=N_name$&":702,1"
4680 N_name$=""

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```

4685 GOSUB Get_data
4690 GOTO Exit
4695 R351:RETURN
4700 !
4705 Cat_1400: !Cat /USERS/FRC:,1400
4710 Cat "/USERS/FRC:,1400"
4715 RETURN
4720 !
4725 !
4730 Ld_1400: !Load from /USERS/FRC:,1400
4735 IF N_names$="" THEN
4740 DISP "Have not been given a file name."
4745 WAIT 1
4750 DISP ""
4755 GOTO R1400
4760 END IF
4765 D14files$="/USERS/FRC/."&N_names$&":1400"
4770 N_names$=""
4775 GOSUB Get_14data
4780 GOTO Exit
4785 R1400:RETURN
4790 !
4795 C_name: !Change to another file name
4800 KEY LABELS OFF
4805 INPUT "Input the new file name",N_names$
4810 Msg_flg=1
4815 KEY LABELS ON
4820 RETURN
4825 !
4830 Get_data: !Retrieve data file
4835 MAT B= (0) !Clear the data arrays
4840 MAT V= (0)
4845 MAT F= (0)
4850 MAT Tp= (0)
4855 ASSIGN @Path1 TO Dfiles !Open & set file pointer at beginning
4860 ! Input all test information and all files
4865 ENTER @Path1,File1$,Mount_id$,Header(*)
4870 CALL New_size !Redim arrays to fit data
4875 IF Header(4) THEN !The EE array is present
4880 ENTER @Path1,E(*),V(*),F(*),Tp(*),Ne(*)
4885 ELSE !EE array not present
4890 ENTER @Path1,E(*),V(*),F(*),Tp(*)
4895 END IF
4895 ASSIGN @Path1 TO * !Close file
4900 Dfiles=Dfiles[1,10] !Strip off the drive extension
4905 Header(4)=0 !Problem with Pwr(*) - force recalc
4910 !of EE & thus Pwr(*)
4915 RETURN
4920 !
4925 !
4930 Get_14data: !Special Retrieve data file for 1400 drive
4935 MAT B= (0) !Clear the data arrays
4940 MAT V= (0)
4945 MAT F= (0)
4950 MAT Tp= (0)
4955 ASSIGN @Path1 TO D14files !Open & set file pointer at beginning
4960 ! Input all test information and all files
4965 ENTER @Path1,File1$,Mount_id$,Header(*)
4970 CALL New_size !Redim arrays to fit data
4975 IF Header(4) THEN !The EE array is present
4980 ENTER @Path1,E(*),V(*),F(*),Tp(*),Ne(*)
4985 ELSE !EE array not present
4990 ENTER @Path1,E(*),V(*),F(*),Tp(*)
4995 END IF
4995 ASSIGN @Path1 TO * !Close file
5000 Dfiles=D14files[12,21] !Strip off the drive extension
5005 Header(4)=0 !Problem with Pwr(*) - force recalc
5010 !of EE & thus Pwr(*)
5015
5020 RETURN
5025 !
5030 Exit:OFF KEY
5035 SUBEND
5040 ! *****
5045 Ef: !
5050 Bff_calc: !Calculates effective efficiency
5055 SUB Bff_calc
5060 OPTION BASE 1
5065 COM /Data/ Dfiles[20],File1$(16),Mount_id$(16)
5070 COM /Data/ V(3000,2),E(3000,2),F(500,2),Ne(100,2),Header(27)
5075 COM /Data/ Af(10,3),INTEGER Tp(3000)
5080 COM /Grph_prt/ P(100,2) !Set up power array
5085 No_freq=Header(5) !Get No. of frequencies
5090 Chk_e0=Header(19) !Set flag if E0 check is in data set
5095 REDIM P(No_freq,2) !Change size to match
5100 DISP "Do you wish to visually check the computed values of Vdc and Vrf
? "
5105 Sys_prt=VAL(SYSTEM$( "SYSTEM PRIORITY" )) !Determine system priority
5110 Lcl_prt=Sys_prt+1 !Set local priority 1 higher for ON KEY
5115 ! Softkey interrupts:
5120 FOR N=0 TO 19
5125 ON KEY N LABEL " " GOTO Top
5130 NEXT N
5135 ON KEY 0 LABEL " PREV MENU ",Lcl_prt GOTO Exit
5140 ON KEY 5 LABEL "YES, all freq ",Lcl_prt GOTO Yes1
5145 ON KEY 6 LABEL " YES, 1 freq ",Lcl_prt GOTO Yes2
5150 ON KEY 7 LABEL " NO ",Lcl_prt GOTO No
5155 Top:LOOP
5160 END LOOP
5165 Yes1:Chk_flg=1 !Set the check flag (for visually
5170 GOTO Y_n_end !reasonable results-all freq)
5175 Yes2:Chk_flg=-1 !Set single freq flag
5180 IF Chk_flg<0 THEN !What frequency ?
5185 FOR N=1+Chk_e0 TO Header(5)+Chk_e0
5190 PRINT "No. ",N;" ",F(N,1);" GHz"
5195 NEXT N
5195 KEY LABELS OFF
5200 INPUT "Input the frequency you wish to see in GHz: ",Chk_freq
5205 KEY LABELS ON
5210 END IF
5215 GOTO Y_n_end !
5220 No: Chk_flg=0 !Lower the check flag
5225 Y_n_end: !End of Y/N
5230 IF Chk_flg<=0 THEN !
5235 KEY LABELS OFF !Turn off key labels
5240 DISP "" !Clear display area
5245 END IF
5250 FOR N=1+Chk_e0 TO No_freq+Chk_e0 ! +1 if checking E0
5255 CALL V_avg(Chk_flg,Chk_freq,N,Vdc,Vrf)
5260 CALL E_avg(Chk_flg,Chk_freq,N,Edc,Erf)
5265 GOSUB Pwr_calc !Get the frequency
5270 Freq=F(N,1)
5275 P(N-Chk_e0,1)=Freq
5280 P(N-Chk_e0,2)=Pwr
5285 GOSUB Bff_calc !Calculate EE
5290 Ne(N-Chk_e0,1)=Freq !Fill array
5295 Ne(N-Chk_e0,2)=Bff
5300 NEXT N
5310 Header(4)=1 !Set EE flag
5315 GOTO Exit
5320 !
5325 Pwr_calc: !Calculates rf power level
5330 Vref=Header(13) !Get the reference voltage (if any)
5335 R0=Header(14) !Get the mount operating resistance
5340 V1=Vref+Vdc !V1 for power calculation
5345 V2=Vref+Vrf !V2 for power calc

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5350 Pwr=1000*(V1*V1-V2*V2)/R0      !Rf power in milliwatts
5355 RETURN
5360 !
5365 Bff_calc:
5370 G: G=1.00038*.00095*Freq^.452  !Calculates effective efficiency
5375 Ra2=(V2/V1)^2                    !Calorimeter correction constant
5380 Eff=G*(1-Ra2)/(Erf/Edc-Ra2)     !Ratio of V2 to V1, squared
5385 PRINT Freq                      !Effective efficiency
5390 PRINT Ra2,Edc,Erf,Eff
5395 RETURN
5400 !
5405 Exit:CONTROL 1,12,0
5410 SUBEND
5415 ! * * * * *
5420 V_avg:
5425 SUB V_avg(Chk_flg,Chk_freq,Freq_no,Vdc,Vrf) !Average V's from raw data
5430 !
5435 ! Chk_flg: 1 = Displays the data and results for a visual check
5440 !           at ALL frequencies.
5445 ! " : 0 = Computes average without displaying result(s).
5450 ! " : -1 = Displays the data and results for a visual check
5455 !           at ONE frequency.
5460 ! Chk_freq: The single frequency for a visual check.
5465 ! Freq_no: No. of freq (place in the series of frequencies) for which
5470 !           the average is to be determined.
5475 ! Vdc: The returned calculated average value of Vdc.
5480 ! Vrf: The returned calculated average value of Vrf.
5485 !
5490 ! OPTION BASE 1
5495 COM /Data/ Dfile$(20),File$(16),Mount_id$(16)
5500 COM /Data/ V(3000,2),E(3000,2),F(500,2),Ne(100,2),Header(27)
5505 COM /Data/ Af(10,3),INTEGER Tp(3000)
5510 DIM B$(60)
5515 !
5520 Vdc=0      !Zero out variable
5525 Vrf=0      !Zero out variable
5530 Freq=INT(F(Freq_no,1)*1.E+3)/1.E+3 !Get the frequency in GHz
5535 N1=F(1,2)  !Meas No. at start of freq
5540 Vst=V(N1-1,2) !Vdc at start of freq
5545 FOR N=N1 TO Header(9)
5550 IF V(N,2)>.9*Vst AND V(N,2)<1.1*Vst THEN GOTO Jump_out
5555 Vrf=Vrf+V(N,2)
5560 NEXT N
5565 Jump_out:N2=N
5570 Vsp=V(N2,2)
5575 Vdc=(Vst+Vsp)/2
5580 Pltflg=1
5585 Vflg=1
5590 OUTPUT Vdc$ USING "#,DDDD,DDDD",Vdc*1.E+3
5595 B$="Vdc="+Vdc$&" mV at " &VAL$(Freq)&" GHz"
5600 IF Chk_flg=0 THEN CALL Graph_check(Pltflg,Vflg,B$,Vdc,N1,N2,0,0,S_flg)
5605 IF Chk_flg=0 AND Freq=Chk_freq THEN CALL
5610 Graph_check(Pltflg,Vflg,B$,Vdc,N1,N2,0,0,S_flg)
5615 Vrf=Vrf/(N2-N1)
5620 Vflg=0
5625 B$="Vrf="+Vrf$&" mV at " &VAL$(Freq)&" GHz"
5630 IF Chk_flg=0 THEN CALL Graph_check(Pltflg,Vflg,B$,Vrf,N1,N2,0,0,S_flg)
5635 IF Chk_flg=0 AND Freq=Chk_freq THEN CALL
5640 Graph_check(Pltflg,Vflg,B$,Vrf,N1,N2,0,0,S_flg)
5645 OFF KEY
5650 SUBEND
5655 E_avg:
5660 SUB E_avg(Chk_flg,Chk_freq,Freq_no,Edc,Erf) !Determine avg E's
5665 !
5670 ! Chk_flg: 1 = Displays the data and results for a visual check

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```

6010 X1=INT((Nsp+Nst)/2) !X1 for linear thermopile correction
6015 Y1=Bdc1 !Y1 for linear thermopile correction
6020 ! ***** Second end point for Edc average
6025 Nf=Header(9) !Total No. of measurement points
6030 IF Chk_e0 THEN NF=F(Nf_freq+3,2) !Meas pts at end of rf off
6035 Nst=Nf-Lss !Start average back Lss/2 min from end
6040 Nsp=Nst+Lss-1 !Average for Lss points (Lss/2 min)
6045 FOR N=Nst TO Nsp !Start and stop as indicated above
6050 Edc2=Edc2+E(N,2)
6055 NEXT N
6060 Edc2=Edc2/(Nsp-Nst+1)
6065 X2=INT((Nsp+Nst)/2) !Average
6070 Y2=Bdc2 !X2 for linear thermopile correction
6075 Edc=(Y1+Y2)/2 !Avg without linear correction
6080 A=(Y2-Y1)/(X2-X1) !A - slope for linear correction
6085 B=(X2*Y1-X1*Y2)/(X2-X1) !B - intercept for a+bx correction
6090 ! ***** Get Erf value
6095 N1=F(Freq_no,2) !Meas No. at start of freq
6100 N2=F(Freq_no+1,2) !Meas No. at end of freq
6105 CALL Settle_1(N1,N2,Erf,Nmid,Nst,Nsp,S_flg) !Rtns avg Erf, mid, start, stop
6110 NF=Header(9) !Total No. of measurement points
6115 P1flg=0 !Plot E
6120 V1flg=1 !For Edc
6125 IF Chk_e0 THEN !For calculated E0
6130 E0=A0*Nmid+B0 !Linear slope correction
6135 OUTPUT E0$ USING "#,DDD.DDDD":E0*1.E+6
6140 B$="E0="&E0$&" vV at "&AVAL$(Freq)&" Ghz"
6145 IF Chk_flg>0 THEN CALL Graph_check(P1flg,V1flg,B$,E0,1,Nf,0,0,S_flg)
6150 IF Chk_flg<0 AND Freq=Chk_freq THEN CALL
Graph_check(P1flg,V1flg,B$,E0,1,Nf,0,0,S_flg)
END IF
6155 Edc=A*Nmid+B !Linear correction for thermopile drift
6160 OUTPUT Edc$ USING "#,DDD.DDDD":Edc*1.E+6
6165 B$="Edc="&Edc$&" vV at "&AVAL$(Freq)&" Ghz"
6170 B$="Edc="&Edc$&" vV at "&AVAL$(Freq)&" Ghz"
6175 IF Chk_flg>0 THEN CALL Graph_check(P1flg,V1flg,B$,E0,1,Nf,0,0,S_flg)
6180 IF Chk_flg<0 AND Freq=Chk_freq THEN CALL
Graph_check(P1flg,V1flg,B$,Edc,1,Nf,0,0,S_flg)
V1flg=0 !For Erf
6185 OUTPUT Erf$ USING "#,DDD.DDDD":Erf*1.E+6
6190 B$="Erf="&Erf$&" vV at "&AVAL$(Freq)&" Ghz"
6200 IF Chk_flg>0 THEN CALL
Graph_check(P1flg,V1flg,B$,Erf,N1,N2,Nst,Nsp,S_flg)
IF Chk_flg<0 AND Freq=Chk_freq THEN CALL
Graph_check(P1flg,V1flg,B$,Erf,N1,N2,Nst,Nsp,S_flg)
E0=Header(15) !Get the 181 zero correction
6210 Edc=Edc-E0 !Make the dc zero correction
6215 Erf=Erf-E0 !Make the rf zero correction
6220 OFF KEY
6225 SUBEND
6230 ! * * * * *
6235 ! * * * * *
6240 Graph check: !
6245 SUB Graph_check(P1flg,V1flg,B$,Vavg,N1,N2,Nst,Nsp,S_flg) !Visual check
6250 !
6255 ! P1flg: set = plot power meter voltages (Vdc & Vrf)
6260 ! : down = plot thermopile output (Bdc & Erf)
6265 ! S_flg: set = step thru stability test routine
6270 ! V1flg: set = plot the dc values
6275 ! : down = plot the rf values
6280 ! B$: Title string
6285 ! Vavg: Average value of Vdc,Vrf,Edc, or Erf to be indicated on graph
6290 ! N1: Meas No. for start (left edge) of the plot
6295 ! N2: Meas No. for end (right edge) of the plot (+10 min)
6300 ! Nst: Meas No. for start of data points used in average
6305 ! Nsp: Meas No. for end of data points used in average
6310 !
6315 OPTION BASE 1
6320 COM /Data/ Dfile$(20),File$(16),Mount_id$(16)

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6325 COM /Data/ V(3000,2),E(3000,2),F(500,2),Ne(100,2),Header(27)
6330 COM /Data/ Af(10,3),INTEGER Tp(3000)
6335 !Total # of measurements (array size)
6340 !String for title
6345 !Plotting array
6350 Sys_prt=VAL(SYSTEM$("SYSTEM PRIORITY")) !Determine system priority
6355 !Set local priority 1 higher for ON KEY
6360 !Set flag to display graph
6365 !Lower flag for stepping stability test
6370 !Turn on user soft key labels
6375 !
6380 FOR N=0 TO 9
6385 ON KEY N LABEL " " GOTO Top
6390 NEXT N
6395 ON KEY 0 LABEL " CONTINUE " ,Lcl_prt GOTO Exit
6400 ON KEY 1 LABEL " STEP CONTINUE " ,Lcl_prt GOTO Sexit
6405 ON KEY 5 LABEL "CHANGE x axis " ,Lcl_prt GOSUB Chg_x
6410 ON KEY 6 LABEL "CHANGE y axis " ,Lcl_prt GOSUB Chg_y
6415 ON KEY 7 LABEL "CHANGE V avg " ,Lcl_prt GOSUB Chg_v
6420 ON KEY 8 LABEL " DUMP plot " ,Lcl_prt GOSUB Dump
6425 Top:LOOP
6430 IF G_flg THEN GOSUB Graph_setup
6435 IF Chg_flg THEN GOSUB Graph_xy
6440 END LOOP
6445 !
6450 Vavg:
6455 Delt=Header(11) !Show avg V
6460 IF P1flg THEN !Measurement interval in sec
6465 Timin=N1*Delt-300 !For V
6470 Timax=N2*Delt+300 !Beginning point minus 5 min
6475 IF V1flg THEN !End point plus 5 min
6480 Vpmin=Vavg-5.E-5 !Sets up range for y axis
6485 Vpmin=INT(Vpmin*1.E+6)*1.E-6 !Vdc minus 50 uV
6490 Vpmax=Vpmin+1.E-4 !Vpmin+100uV
6495 ELSE
6500 Vpmin=Vavg-1.E-5 !Vrf minus 10 uV
6505 Vpmin=INT(Vpmin*1.E+6)*1.E-6 !Start at an integer division
6510 Vpmax=Vpmin+2.E-5 !Vpmin+20uV
6515 END IF
6520 ELSE !For E
6525 Timin=INT(N1*Delt/60)*60 !Beginning point
6530 Timax=Timin+2100 !End point plus 30 min
6535 Vpmin=Vavg-5.E-8 !Edc minus 50 nV
6540 Vpmin=INT(Vpmin*1.E+8)*1.E-8 !Start at an integer division
6545 Vpmax=Vpmin+1.E-7 !Vmin+100nV (Edc plus 50 nV)
6550 IF V1flg THEN !Sets up range for y axis
6555 Timin=0 !Beginning point
6560 Timax=N2*Delt !End point
6565 END IF
6570 END IF !Indicate the change
6575 Chg_flg=1
6580 RETURN
6585 !
6590 Chg_x:
6595 Ans$="" !Change x axis range
6600 DISP "New Tmin <";Timin/60;" "; !Make sure dummy is empty
6605 INPUT Ans$ !Ask if change for Tmin
6610 IF Ans<>" " THEN Timin=60.*VAL(Ans$) !Get response
6615 Ans$="" !Make sure dummy is empty
6620 DISP "New Tmax <";Timax/60;" "; !Ask if change for Tmax
6625 INPUT Ans$ !Get response
6630 IF Ans<>" " THEN Timax=60.*VAL(Ans$) !Make sure dummy is empty
6635 Ans$="" !Indicate the change
6640 Chg_flg=1
6645 RETURN
6650 !
6655 Chg_y:

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7330 RETURN
7335 !
7340 Setit: S_flg=1 !Set the step flag
7345 Exit: OFF KEY
7350 KEY LABELS OFF
7355 GINIT
7360 SUBEND
7365 ! * * * * *
7370 Settle_2: !
7375 SUB Settle_2 (N1,N2,Erf,Nmid,Nst,Nsp,S_flg)
7380 !
7385 ! N1: Frequency starting point
7390 ! N2: Frequency stopping point
7395 ! Nst: Beginning of settled run
7400 ! Nsp: End of settled run
7405 ! Erf: is the final settled value
7410 ! Nmid: is the mid point of the array range from which Erf came
7415 ! S_flg: A flag to pause after every call to Find_trend subprogram
7420 !
7425 OPTION BASE 1
7430 INTEGER I,N
7435 COM /Data/ Dfile$(20),File1$(16),Mount_id$(16)
7440 COM /Data/ V(3000,2),E(3000,2),F(500,2),Ne(100,2),Header(27)
7445 COM /Data/ Af(10,3),INTEGER Tp(3000)
7450 COM /Init_stats/ Tcv,Rcv,Ent,Sdnt,Volts(100),INTEGER Mode,Lss
7455 !
7460 Erf=0 !Initialize
7465 Mode=1 !Initialize
7470 N=N1 !Initialize
7475 WHILE N=Lss-1<N2 AND Stable_run=0 !Either
7480 FOR I=1 TO Lss !Data for "Find_trend"
7485 Volts(I)=1.0E+6*E(I-1+N,2) !Data to microvolts
7490 NEXT I
7495 CALL Find_trend(Stable_run) !Dom's routine
7500 IF S_flg THEN PAUSE !So we can follow Find_trend variables
7505 N=N+1
7510 END WHILE
7515 Nst=N-1
7520 Nsp=N-Lss-2
7525 FOR N=Lst TO Nsp
7530 Erf=Erf+E(N,2) !Sum
7535 NEXT N
7540 Erf=Erf/(Nsp-Nst+1) !Average
7545 Nmid=INT((Nst+Nsp)/2) !Mid-point
7550 SUBEND
7555 ! * * * * *
7560 Graph_n_p: !
7565 SUB Graph_n_p(P_flg) !Graph efficiency or power
7570 OPTION BASE 1
7575 COM /Data/ Dfile$(20),File1$(16),Mount_id$(16)
7580 COM /Data/ V(3000,2),E(3000,2),F(500,2),Ne(100,2),Header(27)
7585 COM /Data/ Af(10,3),INTEGER Tp(3000)
7590 COM /Grph_prt/ Pwr(100,2) !Power array
7595 No-Header(5) !Total # of frequencies (array size)
7600 ALLOCATE AS[90] !String for title
7605 ALLOCATE P[No,2] !Plotting array
7610 REDIM Pwr(No,2) !In case it hasn't been done
7615 Bid=Header(3) !Band ID
7620 Bid=VAL$(Bid)
7625 Sys_prt=VAL$(SYSTEM$("SYSTEM PRIORITY")) !Determine system priority
7630 Lcl_prt=Sys_prt+1 !Set local priority 1 higher for ON KEY
7635 G_flg=1 !Set flag=1
7640 CONTROL 1,12:0
7645 FOR N=0 TO 19
7650 ON KEY N LABEL " " GOTO Top
7655 NEXT N
7660 ON KEY 0 LABEL " PREV MENU ",Lcl_prt GOTO Exit

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7665 ON KEY 5 LABEL "CHANGE X-axis ",Lcl_prt GOSUB Chg_x
7670 ON KEY 6 LABEL "CHANGE Y-axis ",Lcl_prt GOSUB Chg_y
7675 ON KEY 1 LABEL " DUMP plot ",Lcl_prt GOSUB Dump
7680 ON KEY 2 LABEL " LIST result ",Lcl_prt GOSUB List
7685 ON KEY 7 LABEL " PRINT result ",Lcl_prt GOSUB Print
7690 Top: LOOP
7695 IF G_flg THEN GOSUB Graph_setup
7700 IF Chg_flg THEN GOSUB Graph_xy
7705 END LOOP
7710 !
7715 Chg_x:
7720 Ans$="" !Change x axis range
7725 DISP "New Xmin <";Xmin;"> "; !Make sure dummy is empty
7730 INPUT Ans$ !Ask if change for Xmin
7735 IF Ans$<>" THEN Xmin=VAL(Ans$) !Get response
7740 Ans$="" !Make sure dummy is empty
7745 DISP "New Xmax <";Xmax;"> "; !Ask if change for Xmax
7750 INPUT Ans$ !Get response
7755 IF Ans$<>" THEN Xmax=VAL(Ans$) !Make sure dummy is empty
7760 Ans$="" !Indicate the change
7765 Chg_flg=1
7770 RETURN
7775 !
7780 Chg_y:
7785 DISP "New Ymin <";Ymin;"> "; !Graphs thermopile nanovolt output
7790 INPUT Ans$ !Ask if change for Ymin
7795 IF Ans$<>" THEN Ymin=VAL(Ans$) !Get response
7800 Ans$="" !Make sure dummy is empty
7805 DISP "New Ymax <";Ymax;"> "; !Ask if change for Ymax
7810 INPUT Ans$ !Get response
7815 IF Ans$<>" THEN Ymax=VAL(Ans$) !Make sure dummy is empty
7820 Chg_flg=1 !Indicate the change
7825 RETURN
7830 !
7835 Dump:
7840 OUTPUT KBD;"K"; !Graphs calculated effective efficiency
7845 CONTROL 1,12:1 !Clear screen
7850 GOSUB Graph_xy !Turn off user soft key labels
7855 OUTPUT KBD;"N"; !Go to alternate entry point
7860 CONTROL 1,12:0 !Dump graphics
7865 RETURN !Turn on user soft key labels
7870 !
7875 List:
7880 P_flg=0 !List effective efficiency to screen
7885 CALL Print_ne(P_flg) !
7890 RETURN
7895 !
7900 Print:
7905 P_flg=1 !Print effective efficiency
7910 CALL Print_ne(P_flg) !Set print flag
7915 RETURN
7920 !
7925 Graph_setup:
7930 IF P_flg THEN !Setup routine
7935 MAT P= Pwr !POWER
7940 IF Header(21) THEN MAT SORT P(*,1) !If random freq order
7945 Xmin=0 !Beginning point: x axis
7950 Ymin=9.9 !End point: x axis
7955 Ymax=10.1 !Beginning point: y axis
7960 ELSE !End point: y axis
7965 MAT P= Ne
7970 IF Header(21) THEN MAT SORT P(*,1) !If random freq order
7975 Xmin=0 !Beginning point: x axis
7980 Ymax=20 !End point: x axis
7985 Ymin=.90 !Beginning point: y axis
7990 Ymax=1.0 !End point: y axis
7995

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8000 END IF
8005 Chg_flg=1
8010 RETURN
8015 !
8020 Graph_xy:
8025 OUTPUT KBD;"K";
8030 GINIT
8035 LONG 6
8040 PEN 5
8045 !
8050 CSIZE 5.0
8055 MOVE 64,100
8060 IF Pflg THEN
8065 LABEL "COAX MOUNT - RF POWER LEVEL"
8070 ELSE
8075 LABEL "COAX MOUNT - EFFECTIVE EFFICIENCY"
8080 END IF
8085 !
8090 CSIZE 3.5
8095 MOVE 64,94
8100 TImedate1=Header(2)
8105 A$=DATE$(TImedate1)
8110 A$="MOUNT:"&Mount_id$&" DATA FILE:"&File$&" DATE:"&A$
8115 LABEL A$
8120 !
8125 CSIZE 4.5
8130 MOVE 70,12
8135 LABEL "FREQUENCY (GHz)"
8140 MOVE 0,55
8145 LDIR PI/2
8150 IF Pflg THEN
8155 LABEL "POWER (mW)"
8160 ELSE
8165 LABEL "PERCENT"
8170 END IF
8175 LDIR 0
8180 PEN 1
8185 IF Pflg THEN
8190 VIEWPORT 18,125,16,88
8195 ELSE
8200 VIEWPORT 14,125,16,88
8205 END IF
8210 WINDOW Xmin,Xmax,Ymin,Ymax
8215 ! Set up x-axis tic and label spacing
8220 X=-25
8225 Xtic=4
8230 Stpx=1
8235 Y=(Ymax-Ymin)/20
8240 AXES X,Y,Xmin,Ymin,Xtic,2,4
8245 AXES X,Y,Xmax,Ymax,Xtic
8250 CLIP OFF
8255 CSIZE 3.5
8260 FOR I=0 TO Xmax-Xmin STEP Stpx
8265 MOVE Xmin+I,Ymin-Y/10
8270 LABEL USING "#,DD";(Xmin+I)
8275 NEXT I
8280 LONG 8
8285 IF Pflg THEN
8290 FOR I=Ymin TO Ymax STEP 2*Y
8295 MOVE Xmin-.01,I
8300 LABEL USING "#,DD,DDD";I
8305 NEXT I
8310 ELSE
8315 FOR I=Ymin TO Ymax STEP 2*Y
8320 MOVE Xmin-.01,I
8325 LABEL USING "#,DDD.D";100*I;100*CR/LF - percent
8330 NEXT I
8335 !
8340 CLIP ON
8345 !Keep plot inside viewport
8350 FOR Count=1 TO No
8355 PLOT P(Count,1),P(Count,2)
8360 NEXT Count
8365 PENUP
8370 PEN 3
8375 G_flg=0
8380 Chg_flg=0
8385 RETURN
8390 !
8395 Exit:OFF KEY
8400 GINIT
8405 SUBEND
8410 ! * * * * *
8415 Print_ne:
8420 SUB Print_ne(P_flg)
8425 OPTION BASE 1
8430 COM /Data/ Dfiles(20),File$(16),Mount_id$(16)
8435 COM /Data/ V(3000,2),E(3000,2),P(500,2),Ne(100,2),Header(27)
8440 COM /Data/ Af(10,3),INTEGER Tp(3000)
8445 COM /Grph prt/ Pwr(100,2)
8450 No1=Header(5)
8455 ALLOCATE Nei(No1,2)
8460 ALLOCATE Pwr1(No1,2)
8465 MAT Nei= Ne
8470 MAT Pwr1= Pwr
8475 IF Header(21) THEN
8480 MAT SORT Nei(*,1)
8485 MAT SORT Pwr1(*,1)
8490 END IF
8495 FOR N=1 TO No1
8500 IF N=1 THEN
8505 GOSUB Print_e
8510 ELSE
8515 GOSUB Print_e2
8520 END IF
8525 NEXT N
8530 GOTO Exit
8535 Print_e:
8540 OUTPUT KBD;"K";
8545 IF P_flg THEN PRINTER IS PRT
8550 PRINT TAB(22),"EFFECTIVE EFFICIENCY OF COAX MOUNT"
8555 PRINT
8560 PRINT TAB(4),"DATE: ";DATE$(Header(2));";";TIME$(Header(2));
8565 PRINT TAB(45),"MOUNT: ";Mount_id$
8570 !
8575 PRINT TAB(4),"PROGRAM: ";File$;
8580 PRINT TAB(45),"DATA FILE NAME: ";Dfiles$
8585 !
8590 PRINT TAB(4),"NO OF READINGS: ";Header(9);
8595 PRINT TAB(45),"NANOVOLTMETER ZERO OFFSET: ";
8600 PRINT USING "#,DDDD";Header(15)*1.E+9
8605 PRINT " nV"
8610 !
8615 PRINT TAB(4),"MEASUREMENT INTERVAL: ";Header(11);" sec"; 14
8620 PRINT TAB(45),"CALORIMETER CORRECTION: "
8625 IF Header(21) THEN PRINT TAB(4),"RANDOM FREQUENCY ORDER";
8630 IF NOT Header(21) THEN PRINT TAB(4),"INCREMENTAL FREQUENCY ORDER";
8635 G1: PRINT TAB(48),"g = 1.00038 + 0.00095*f*0.452"
8640 !
8645 ! PRINT TAB(5),"BATH TEMPERATURE: N.A.";
8650 ! PRINT TAB(45),"ELAPSED TIME: "; How long?
8655 ! PRINT USING "#,DDD.DD";Header(10)/60
8660 ! PRINT " min"
8665 PRINT

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9340 Header(3)=62 !Band ID
9345 Header(6)=12.4 !Start frequency
9350 Header(7)=18 !Stop frequency
9355 Header(8)=.25 !Step frequency
9360 Header(14)=100 !Mount operating resistance
9365 SUBEND
9370 ! * * * * *
9375 Default4: !
9380 SUB Default4 !Sets up defaults for WR-42
9385 OPTION BASE 1
9390 COM /Data/ Dfiles[20],Fileid[16],Mount_id[16]
9395 COM /Data/ V(3000,2),E(3000,2),F(500,2),Ne(100,2),Header(27)
9400 COM /Data/ Af(10,3),INTEGER Tp(3000)
9405 COM /Menu/ INTEGER Men(17,20)
9410 COM /Maxmin/ REAL Maxf,Minf
9415 Maxf=26
9420 Minf=18
9425 Header(3)=42 !Band ID
9430 Header(6)=18 !Start frequency
9435 Header(7)=26 !Stop frequency
9440 Header(8)=.25 !Step frequency
9445 Header(14)=200 !Mount operating resistance
9450 SUBEND
9455 ! * * * * *
9460 Default5: !
9465 SUB Default5 !Sets up defaults for WR-28
9470 OPTION BASE 1
9475 COM /Data/ Dfiles[20],Fileid[16],Mount_id[16]
9480 COM /Data/ V(3000,2),E(3000,2),F(500,2),Ne(100,2),Header(27)
9485 COM /Data/ Af(10,3),INTEGER Tp(3000)
9490 COM /Menu/ INTEGER Men(17,20)
9495 COM /Maxmin/ REAL Maxf,Minf
9500 Maxf=40
9505 Minf=26
9510 Header(3)=28 !Band ID
9515 Header(6)=37.5 !Start frequency
9520 Header(7)=41.5 !Stop frequency
9525 Header(8)=0 !Step frequency
9530 Header(14)=200 !Mount operating resistance
9535 SUBEND
9540 ! * * * * *
9545 Default6: !
9550 SUB Default6 !Sets up defaults for WR-22
9555 OPTION BASE 1
9560 COM /Data/ Dfiles[20],Fileid[16],Mount_id[16]
9565 COM /Data/ V(3000,2),E(3000,2),F(500,2),Ne(100,2),Header(27)
9570 COM /Data/ Af(10,3),INTEGER Tp(3000)
9575 COM /Menu/ INTEGER Men(17,20)
9580 COM /Maxmin/ REAL Maxf,Minf
9585 Maxf=50
9590 Minf=33
9595 Header(3)=22 !Band ID
9600 Header(6)=33 !Start frequency
9605 Header(7)=50 !Stop frequency
9610 Header(8)=.25 !Step frequency
9615 Header(14)=200 !Mount operating resistance
9620 SUBEND
9625 ! * * * * *
9630 Default7: !
9635 SUB Default7 !Sets up defaults for WR-15
9640 OPTION BASE 1
9645 COM /Data/ Dfiles[20],Fileid[16],Mount_id[16]
9650 COM /Data/ V(3000,2),E(3000,2),F(500,2),Ne(100,2),Header(27)
9655 COM /Data/ Af(10,3),INTEGER Tp(3000)
9660 COM /Menu/ INTEGER Men(17,20)
9665 COM /Maxmin/ REAL Maxf,Minf
9670 Maxf=75

9675 Minf=50
9680 Header(3)=15 !Band ID
9685 Header(6)=50 !Start frequency
9690 Header(7)=75 !Stop frequency
9695 Header(8)=.25 !Step frequency
9700 Header(14)=200 !Mount operating resistance
9705 SUBEND
9710 ! * * * * *
9715 Default8: !
9720 SUB Default8 !Sets up defaults for WR-10
9725 OPTION BASE 1
9730 COM /Data/ Dfiles[20],Fileid[16],Mount_id[16]
9735 COM /Data/ V(3000,2),E(3000,2),F(500,2),Ne(100,2),Header(27)
9740 COM /Data/ Af(10,3),INTEGER Tp(3000)
9745 COM /Menu/ INTEGER Men(17,20)
9750 COM /Maxmin/ REAL Maxf,Minf
9755 Maxf=110
9760 Minf=75
9765 Header(3)=10 !Band ID
9770 Header(6)=75 !Start frequency
9775 Header(7)=110 !Stop frequency
9780 Header(8)=.25 !Step frequency
9785 Header(14)=200 !Mount operating resistance
9790 SUBEND
9795 ! * * * * *
9800 Scrno: !
9805 SUB Scrno(Label$(*))
9810 ! Sets up the options of the first screen menu
9815 OPTION BASE 1
9820 DATA " COAX " !Label menu items
9825 DATA " WR-90 "
9830 DATA " WR-62 "
9835 DATA " WR-42 "
9840 DATA " WR-28 "
9845 DATA " WR-22 "
9850 DATA " WR-15 "
9855 DATA " WR-10 "
9860 READ Label$(*)
9865 SUBEND
9870 ! * * * * *
9875 Scrni: !
9880 SUB Scrni(Label$(*))
9885 ! Sets up the options of the second screen menu
9890 OPTION BASE 1
9895 COM /Data/ Dfiles[20],Fileid[16],Mount_id[16]
9900 COM /Data/ V(3000,2),E(3000,2),F(500,2),Ne(100,2),Header(27)
9905 COM /Data/ Af(10,3),INTEGER Tp(3000)
9910 COM /Menu/ INTEGER Men(17,20)
9915 Startf=Header(6) !Start frequency
9920 Stopf=Header(7) !Stop frequency
9925 Stepf=Header(8) !Step frequency
9930 Interval=Header(11) !Measurement interval in sec
9935 Pwr=Header(12) !Power level
9940 Zero=Header(19) !Zero meas flag
9945 Prebias=Header(16) !Pre-bias flag
9950 Label$(1,1)=" COMPLETE FREQ SET (auto) "
9955 Label$(2,1)=" START FREQ = "&VAL$(Startf)&" GHZ "
9960 Label$(3,1)=" STOP FREQ = "&VAL$(Stopf)&" GHZ "
9965 Label$(4,1)=" STEP FREQ = "&VAL$(Stepf)&" GHZ "
9970 Label$(5,1)=" POWER LEVEL = "&VAL$(Pwr)&" MW "
9975 Label$(6,1)=" MEAS. INTERVAL = "&VAL$(Interval)&" sec "
9980 IF Zero THEN
9985 Label$(7,1)=" ZERO DETERMINATION "
9990 ELSE
9995 Label$(7,1)=" NO ZERO DETERMINATION "
10000 END IF
10005 IF Prebias THEN

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10010 Label$(8,1)=" MOUNT PRE-BIAS ON "
10015 ELSE
10020 Label$(8,1)=" MOUNT PRE-BIAS OFF "
10025 END IF
10030 SUBEND
10035 ! * * * * *
10040 Menu: !
10045 SUB Menu(Menu_no,No_rows,No_cols)
10050 Rev$="8609051427"! 8606240839, 8606121528, 8606111827, 8606100948
10055 Dis$=""
10060 ! General menu program written by NTL.
10065 ! 8606240839. Added 300 keyboard compatibility code.
10070 ! 8609051427. Added code to slow knob. (NTL)
10075 ! " Removed 300 kbd compatibility and changed code to use 300
10080 ! softkey layout. (FRC)
10085 OPTION BASE 1
10090 COM /Menu/ INTEGER Men(17,20)
10095 COM /Data/ Data$(20),File$(16),Mount_id$(16)
10100 COM /Data/ V(3000,2),F(3000,2),Ne(100,2),Header(27)
10105 COM /Data/ Af(10,3),INTEGER Tp(3000)
10110 COM /Flags/ Manual_freqs
10115 DIM A$(80),B$(90),C_sum(20),Screen$(17,20)[80]
10120 Para: !
10125 Spacing=2
10130 Wrap=2
10135 No_rows=MAX(1,No_rows)
10140 No_rows=MIN(17,No_rows)
10145 No_cols=MAX(1,No_cols)
10150 No_cols=MIN(40,No_cols)
10155 REDIM
Screen$(1,No_rows,1,No_cols),Men(1,No_rows,1,No_cols),C_sum(1,1,No_cols)
Ptr$=CHR$(129)&CHR$(136)&"="&CHR$(138)&CHR$(128)
Clear$=""
GOSUB Defaults
10175 CLEAR SCREEN
10180 GOSUB Scrn_print
10185 Sys_ptr=VAL(SYSTEM$( "SYSTEM PRIORITY" )) !Determine system priority
10190 Lcl_ptr=Sys_ptr+1 !Set local priority 1 higher for ON KEY
10195 ON KNOB .03,Lcl_ptr GOSUB Knob_service
10200 WAIT .05
10205 FOR N=0 TO 19
10210 ON KEY N LABEL "",Lcl_ptr GOTO Idle
10215 NEXT N
10220 ON KEY 0 LABEL " CONTINUE ",Lcl_ptr GOTO Exit
10225 IF Menu_no=0 THEN
10230 ON KEY 5 LABEL "SELECT OPTION",Lcl_ptr GOSUB Check
10235 ELSE
10240 ON KEY 5 LABEL "CHANGE DEFAULT",Lcl_ptr GOSUB Check
10245 END IF
10250 ON KBD Lcl_ptr GOSUB Kbd_service
10255 KEY LABELS ON
10260 Idle:LOOP
10265 END LOOP
10270 !
10275 Defaults:
10280 SELECT Menu_no
10285 CASE =1
!Coax
10290 CALL Default1
10295 CASE =2
!WR-90
10300 CALL Default2
10305 CASE =3
!WR-62
10310 CALL Default3
10315 CASE =4
!WR-42
10320 CALL Default4
10325 CASE =5
!WR-28
10330 CALL Default5
10335 CASE =6
!WR-22

```

```

10670 END IF
10675 CALL Sc(0,0,Spacing*(Row-1)+1,(Stl+2)*(Col-1)+1,Ptr$)
10680 RETURN
10685 !
10690 Knob_service: !
10695 Slowdown=10
10700 Kx=KNOBX*Kx
10705 Ky=KNoby*Ky
10710 IF ABS(Kx)<Slowdown AND ABS(Ky)<Slowdown THEN 10775
10715 IF No_cols=1 THEN Ky=Kx
10720 IF Kx>0 THEN Col=Col+1
10725 IF Kx<0 THEN Col=Col-1
10730 IF Ky>0 THEN Row=Row+1
10735 IF Ky<0 THEN Row=Row-1
10740 GOSUB Rc_check
10745 CALL Sc(0,0,Spacing*(Old_row-1)+1,(Stl+2)*(Old_col-1)+1,Clear$) ! Clear
10750 CALL Sc(0,0,Spacing*(Row-1)+1,(Stl+2)*(Col-1)+1,Ptr$) ! Print
10755 Old_row=Row
10760 Old_col=Col
10765 Kx=0
10770 Ky=0
10775 RETURN !

10780 !
10785 Kbd_service: !
10790 K$=KBD$
10795 CALL Sc(0,0,Spacing*(Old_row-1)+1,(Stl+2)*(Old_col-1)+1,Clear$)
10800 IF LEN(K$)<2 THEN 10935
10805 IF NUM(K$(1,1))<>255 THEN 10935
10810 SELECT NUM(K$(2,2))
10815 CASE =60
10820 Col=Col-1
10825 GOSUB Rc_check
10830 CASE =62
10835 Col=Col+1
10840 GOSUB Rc_check
10845 CASE =71
10850 Col=No_cols
10855 CASE =72
10860 Col=1
10865 CASE =84
10870 Row=No_rows
10875 CASE =86
10880 Row=Row+1
10885 GOSUB Rc_check
10890 CASE =87
10895 Row=1
10900 CASE =94
10905 Row=Row-1
10910 GOSUB Rc_check
10915 END SELECT
10920 CALL Sc(0,0,Spacing*(Row-1)+1,(Stl+2)*(Col-1)+1,Ptr$)
10925 Old_row=Row
10930 Old_col=Col
10935 RETURN !

10940 Rc_check: !
10945 SELECT Wrap
10950 CASE =1
10955 IF Col<1 THEN Col=1
10960 IF Col>No_cols THEN Col=No_cols
10965 IF Row<1 THEN Row=1
10970 IF Row>No_rows THEN Row=No_rows
10975 CASE =2
10980 IF Col<1 THEN Col=No_cols

```

```

10985 IF Col>No_cols THEN Col=1
10990 IF Row<1 THEN Row=No_rows
10995 IF Row>No_rows THEN Row=1
11000 CASE =3
11005 IF Col<1 THEN
11010 Col=No_cols
11015 Row=Row-1
11020 IF Row<1 THEN Row=No_rows
11025 END IF
11030 IF Col>No_cols THEN
11035 Col=1
11040 Row=Row+1
11045 IF Row>No_rows THEN Row=1
11050 END IF
11055 IF Row<1 THEN
11060 Row=No_rows
11065 Col=Col-1
11070 IF Col<1 THEN Col=No_cols
11075 END IF
11080 IF Row>No_rows THEN
11085 Row=1
11090 Col=Col+1
11095 IF Col>No_cols THEN Col=1
11100 END IF
11105 END SELECT
11110 RETURN !

11115 Check: !Check for disallowed selections before Accept is executed
11120 IF Menu_no>0 THEN
11125 CALL New_default(Row)
11130 GOSUB Scrn_print
11135 ELSE
11140 CALL Check0(Row,Old_row)
11145 GOSUB Accept
11150 Row=Row
11155 GOSUB Reject
11160 Row=Old_row
11165 END IF
11170 RETURN
11175 Accept: !
11180 B$="q" & Screen$(Row,Col) & "c"
11185 CALL Sc(0,0,Spacing*(Row-1)+1,(Stl+2)*(Col-1)+3,B$) ! Inverse on
11190 Men(Row,Col)=1
11195 IF Array_printed THEN GOSUB Array_print
11200 RETURN !

11205 Reject: !
11210 B$="c" & Screen$(Row,Col)
11215 CALL Sc(0,0,Spacing*(Row-1)+1,(Stl+2)*(Col-1)+3,B$) ! Inverse off
11220 Men(Row,Col)=0
11225 IF Array_printed THEN GOSUB Array_print
11230 RETURN !

11235 Set_wrap: !
11240 INPUT "No wrap with hard limits (1), normal wraparound (2), or raster
(3)?",Wrap
11245 Wrap=MIN(3,Wrap)
11250 Wrap=MAX(1,Wrap)
11255 RETURN !

11260 Array_print: !
11265 FOR R=1 TO No_rows
11270 FOR C=1 TO No_cols

```

```

11275 PRINT TABXY(59+2*C,R);Men(R,C)
11280 NEXT C
11285 NEXT R
11290 Array_printed=1
11295 RETURN
11300 Exit:KEY LABELS OFF
11305 SUBEND
11310 ! * * * * *
11315 SUB Sc(Blank_Center,Row,Col,String$)
11320 IF Blank THEN OUTPUT KBD;CHR$(255)&CHR$(75);
11325 IF NOT Center THEN 11335
11330 Col=40-INT(LEN(String$)/2+.5)
11335 PRINT TABXY(Col+25,Row+2);String$;
11340 SUBEND
11345 ! * * * * *
11350 New_default: !
11355 SUB New_default(Row) !Checks for parameter change, does it
11360 OPTION BASE 1
11365 COM /Data/ Dfiles$(20),Files$(16),Mount_id$(16)
11370 COM /Data/ V(3000,2),F(3000,2),Ne(100,2),Header(27)
11375 COM /Data/ Af(10,3),INTEGER Tp(3000)
11380 COM /Menu/ INTEGER Men(17,20)
11385 COM /Maxmin/ REAL Maxf,Minf
11390 KEY LABELS OFF
11395 SELECT Row
11400 CASE =1 !Row 1
11405 Header(20)=ABS(Header(20)-1) !Toggle auto freq flag
11410 CASE =2
11415 DISP "What is the new starting frequency in GHz";
11420 INPUT Startf
11425 IF Startf<Minf THEN
11430 BEEP 2000,.1
11435 DISP "MINIMUM ALLOWED FREQ IS ",Minf;" GHz"
11440 WAIT 1.5
11445 GOTO 11415
11450 END IF
11455 IF Startf>Maxf THEN
11460 BEEP 2000,.1
11465 DISP "MAXIMUM ALLOWED FREQ IS ",Maxf;" GHz"
11470 WAIT 1.5
11475 GOTO 11415
11480 END IF
11485 IF Stopf<Startf AND Stepf>0 THEN Stepf=-Stepf
11490 Header(6)=Startf
11495 CASE =3
11500 DISP "What is the new stop frequency in GHz";
11505 INPUT Stopf
11510 IF Stopf<Minf THEN
11515 BEEP 2000,.1
11520 DISP "MINIMUM ALLOWED FREQ IS ",Minf;" GHz"
11525 WAIT 1.5
11530 GOTO 11500
11535 END IF
11540 IF Stopf>Maxf THEN
11545 BEEP 2000,.1
11550 DISP "MAXIMUM ALLOWED FREQ IS ",Maxf;" GHz"
11555 WAIT 1.5
11560 GOTO 11500
11565 END IF
11570 IF Stopf<Startf AND Stepf>0 THEN Stepf=-Stepf
11575 Header(7)=Stopf
11580 CASE =4
11585 DISP "What is the new step frequency in GHz";
11590 INPUT Stepf
11595 IF Stopf<Startf AND Stepf>0 THEN Stepf=-Stepf
11600 Header(8)=Stepf
11605 CASE =5

```



```

11945 Init_source: !
11950 SUB Init_source
11955 OUTPUT 720,"RF OFF"
11960 OUTPUT 720,"CW"
11965 SUBEND
11970 ! * * * * *
11975 File_name: !
11980 SUB File_name
11985 OPTION BASE 1
11990 COM /Data/ Dfiles$[20],Fileid$[16],Mount_id$[16]
11995 COM /Data/ V(3000,2),E(3000,2),F(500,2),Ne(100,2),Header(27)
12000 COM /Data/ Af(10,3),INTEGER Tp(3000)
12005 ALLOCATE TS[11],Mos[16]
12010 Mos$="JanFebMarAprMayJunJulAugSepOctNovDec"
12015 !
12020 IF Header(3) THEN
12025 Pre$="w"&VAL$(Header(3))
12030 ELSE
12035 Pre$="cn"
12040 END IF
12045 !
12050 DS=DATE$(TIMEDATE)
12055 IF DS[1,1]=" " THEN DS[1,1]="0"
12060 M=POS((Mos$), (DS[4,6]))
12065 M=1+(M-1)/3
12070 OUTPUT MS USING "#,22";M
12075 TS=TIME$(TIMEDATE)
12080 TS=TS[1,2]
12085 Dtg$=DS[10,11]&MS&DS[1,2]&TS
12090 Dfiles=Pre$&Dtg$
12095 SUBEND
12100 ! * * * * *
12105 Mount_id: !
12110 SUB Mount_id
12115 OPTION BASE 1
12120 COM /Data/ Dfiles$[20],Fileid$[16],Mount_id$[16]
12125 COM /Data/ V(3000,2),E(3000,2),F(500,2),Ne(100,2),Header(27)
12130 COM /Data/ Af(10,3),INTEGER Tp(3000)
12135 CLEAR SCREEN
12140 CONTROL 1,12:1
12145 PRINT TABXY(25,16) "BOLOMETER MOUNT IDENTIFICATION"
12150 PRINT TABXY(25,18) "Maximum length: 16 characters."
12155 INPUT "Enter the mount identifier: ",Mount_id$
12160 SUBEND
12165 ! * * * * *
12170 Meas: !
12175 SUB Meas
12180 OPTION BASE 1
12185 COM /Data/ Dfiles$[20],Fileid$[16],Mount_id$[16]
12190 COM /Data/ V(3000,2),E(3000,2),F(500,2),Ne(100,2),Header(27)
12195 COM /Data/ Af(10,3),INTEGER Tp(3000)
12200 COM /Init_stats/ Tcv,Rcv,Enr,Sdnr,Volts(100),INTEGER Mode,Lss
12205 COM /Pwr Lev_set_in/ P_rf,R_0
12210 COM /Io path names/ @Eip_578,@Eip_931,@P_8200,@Hp_3457
12215 COM /Initial value/ V_ref 0,V_rf off
12220 COM /Intr parameters/ Desired_freq,INTEGER No_of_intrs
12225 COM /Window flags/ Window_cs[1],Window_rs[1]
12230 COM /Screen update/ Count,Cftime,Freq,Pwr
12235 COM /Stats_2/ R,Prob,INTEGER Nruns
12240 !
12245 INTEGER Hpbib
12250 DIM New_windows[2]
12255 !
12260 Hpbib=7
12265 ASSIGN @Eip_578 TO 719
12270 ASSIGN @Eip_931 TO 720
12275 ASSIGN @P_8200 TO 714

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12280 ASSIGN @Hp_3457 TO 722
12285 !
12290 P_rf=Header(12)
12295 R_0=Header(14)
12300 Cycle_time=Header(11)
12305 Stop_freq=Header(7)
12310 Max_count=Header(9)
12315 N=1
12320 Starting_freq
12325 Rf on=0
12330 Desired_freq=0
12335 New_window$="XX"
12340 Window_cs="A"
12345 Window_rs="A"
12350 Na=Lss
12355 !
12360 Sys_prty=VAL(SYSTEMS("SYSTEM PRIORITY"))
12365 Lcl_prty=Sys_prty+1
12370 !
12375 Meas_control:
12380 Header(2)=TIMEDATE
12385 Cftime=TIMEDATE
12390 Cycle_start=TIMEDATE
12400 !
12405 Set_interrupts: !
12410 ON INTR Hpbib,Lcl_prty CALL Intr7
12415 OUTPUT @Eip_578,"SR02"
12420 !
12425 ENABLE INTR Hpbib;2
12430 ON CYCLE Cycle_time,Lcl_prty GOSUB E_meas
12435 !
12440 ON KEY 0 LABEL " ",Lcl_prty GOTO Bail_out
12445 ON KEY 1 LABEL " ",Lcl_prty GOSUB Man_freq_chg
12450 ON KEY 5,Lcl_prty GOSUB View_c
12455 ON KEY 6,Lcl_prty GOSUB View_r
12460 ON KEY 9,Lcl_prty CALL Blank
12465 !
12470 Wait:
12475 LOOP
12480 GOSUB Time
12485 IF Count=Max_count THEN End_meas
12490 IF Freq=Stop_freq THEN End_meas
12495 END LOOP
12500 !
12505 !The following 4 subroutines set flags that are used by the Window
12510 !subprograms to output the correct data displays; it was necessary
12515 !to accomplish that task using this code in order to avoid a problem
12520 !created during interrupt service while the display screens were
12525 !being updated.
12530 !
12535 View_c: !
12540 IF Window_cs="A" THEN
12545 New_window$="CB"
12550 ELSE
12555 New_window$="CA"
12560 END IF
12565 RETURN
12570 View_r: !
12575 IF Window_rs="A" THEN
12580 New_window$="RB"
12585 ELSE
12590 New_window$="RA"
12595 END IF
12600 RETURN
12605 !
12610 ! MAIN MEASUREMENT ROUTINE -----

```



```

12615 !
12620 E_meas:
12625 Count=Count+1
12630 Cycle_start=TIMEDATE
12635 !
12640 ! ***** Change Frequency ? *****
12645 ! IF P(N,2)+119=Count THEN Next_freq=1 ! Max time at any freq (60 min)
12650 IF Next_freq THEN
12655 CALL Rf(0,Freq,11,Rf_on)
12660 END IF
12665 !
12670 ! ***** Power Meter
12675 CALL Dvm(Sread)
12680 V(Count,1)=TIMEDATE
12685 V(Count,2)=Sread
12690 ! ***** Thermopile
12695 CALL Dnm(Nread)
12700 E(Count,1)=TIMEDATE
12705 E(Count,2)=Nread
12710 IF NOT Rf ON THEN
12715 V_rf_off=Sread
12720 END IF
12725 IF Rf ON THEN
12730 CALL Power_lev_chk(V_ref,Sread,Pwr)
12735 END IF
12740 ! ***** Temperature
12745 ! OUTPUT 709,"CHAN 107"
12750 ! WAIT 1
12755 ! CALL Dvm(Sread)
12760 ! Sread=Sread+1.E+5
12765 ! IF Sread>3.2E+4 THEN
12770 ! Sread=2.6E+4
12775 ! BEEP 2200,.01
12780 ! END IF
12785 ! Tp(Count)=Sread
12790 !
12795 ! OUTPUT 709,"CHAN 101"
12800 ! ***** Finish freq change ? *****
12805 Next_freq:
12810 IF Next_freq THEN
12815 Freq=F(N,1)
12820 Desired_freq=F(N,1)
12825 F(N,2)=Count+1
12830 SELECT Freq
12835 CASE --3
12840 GOTO End_meas
12845 CASE --2
12850 CALL Dc(0,2)
12855 CASE --1
12860 CALL Dc(1,2)
12865 CASE =0
12870 CALL Rf(0,Freq,15,Rf_on)
12875 Cftime=TIMEDATE
12880 CASE ELSE
12885 CALL Power_lev_set(V_ref,Sread)
12890 V_ref=V_ref
12895 CALL Rf(1,Freq,15,Rf_on)
12895 Cftime=TIMEDATE
12900 END SELECT
12905 N=N+1
12910 Nruns=0
12915 R=0
12920 Prob=0
12925 Next_freq=0
12930 END IF
12940 !
12945 CALL Screen_update
!Effective eff. measurement
!Count the measurements
!Start time for wait until cycle_time
! *****
! IF P(N,2)+119=Count THEN Next_freq=1 ! Max time at any freq (60 min)
! Frequency change requested
! First, turn off rf
CALL Rf(0,Freq,11,Rf_on)
END IF
! ***** Power Meter
CALL Dvm(Sread)
V(Count,1)=TIMEDATE
V(Count,2)=Sread
! ***** Thermopile
CALL Dnm(Nread)
E(Count,1)=TIMEDATE
E(Count,2)=Nread
IF NOT Rf ON THEN
V_rf_off=Sread
END IF
IF Rf ON THEN
CALL Power_lev_chk(V_ref,Sread,Pwr)
END IF
! ***** Temperature
OUTPUT 709,"CHAN 107"
WAIT 1
CALL Dvm(Sread)
Sread=Sread+1.E+5
IF Sread>3.2E+4 THEN
Sread=2.6E+4
BEEP 2200,.01
END IF
Tp(Count)=Sread
!
OUTPUT 709,"CHAN 101"
! ***** Finish freq change ? *****
Next_freq:
IF Next_freq THEN
Freq=F(N,1)
Desired_freq=F(N,1)
F(N,2)=Count+1
SELECT Freq
CASE --3
GOTO End_meas
CASE --2
CALL Dc(0,2)
CASE --1
CALL Dc(1,2)
CASE =0
CALL Rf(0,Freq,15,Rf_on)
Cftime=TIMEDATE
CASE ELSE
CALL Power_lev_set(V_ref,Sread)
V_ref=V_ref
CALL Rf(1,Freq,15,Rf_on)
Cftime=TIMEDATE
END SELECT
N=N+1
Nruns=0
R=0
Prob=0
Next_freq=0
END IF
CALL Screen_update
!Do the plotting
!Lift pen between points - dotted line
!To reset a counter in Stats
***** Check for Stability & Calculate Statistics *****
CALL Stats(Na,E(Count,2),Next_freq)
END MAIN MEASUREMENT ROUTINE
-----
13010 Time:
13015 Cycle_stop=Cycle_start+Cycle_time
13020 T=TIMEDATE
13025 Count_down=INT(Cycle_stop-T)
13030 PRINT TABXY(49,8);
13035 IF Count_down<Cycle_time-1 THEN
13040 PRINT USING "#,ZZ,X",Count_down!
13045 END IF
13050 SELECT New_window$
13055 CASE "CA"
13060 CALL Window_c_a
13065 New_window$="XX"
13070 CASE "CB"
13075 CALL Window_c_b
13080 New_window$="XX"
13085 CASE "RA"
13090 CALL Window_r_a
13095 New_window$="XX"
13100 CASE "RB"
13105 CALL Window_r_b
13110 New_window$="XX"
13115 END SELECT
13120 RETURN
13125 !
13130 Man_freq_chg:
13135 Next_freq=1
13140 RETURN
13145 !
13150 Bail_out:
13155 Header(20)=0
13160 CALL Rf(0,Freq,15,Rf_on)
13165 OUTPUT 722;"TRIG AUTO"
13170 !
13175 End_meas:
13180 Header(9)=Count
13185 CALL New_size
13190 !
13195 OFF CYCLE
13200 Stop_time=TIMEDATE
13205 Header(10)=Stop_time-Header(2)
13210 OUTPUT 722;"TRIG AUTO"
13215 GOSUB Dvm_status
13220 CALL Rf(0,Freq,15,Rf_on)
13225 VIEWPORT 0,128,0,100
13230 WINDOW 0,128,0,100
13235 !
13240 IF Header(20) THEN SUBEXIT
13245 !
13250 CSIZE 3.4
13255 MOVE 115,3
13260 LABEL "PROGRAM PAUSED"
13265 PAUSE
13270 STATUS 1,20,B1
13275 IF B1=0 THEN CALL Blank
13280 !

```

```

13285 Exit:
13290 GINOT
13295 KEY LABELS ON
13300 SUBEND ! SUB Meas
13305 ! *****
13310 Delay_start: !
13315 SUB Delay_start
13320 Sys_prt=VAL(SYSTEMS("SYSTEM PRIORITY")) !Determine system priority
13325 Lcl_prt=Sys_prt+1
13330 OUTPUT KBD;"K";
13335 Enter:KEY LABELS OFF
13340 PRINT TABXY(27,16),"DELATED PROGRAM START"
13345 TS=TIMES(TIMEDATE)
13350 PRINT TABXY(27,18),"Present time"
13355 INPUT "Enter the desired starting time. (1832 for 6:32 PM, 0215 for 2:15 AM, etc).";Start$(1,4)
13360 ST$=Start$(1,2)&" "&Start$(3,4)&" ":00"
13365 PRINT TABXY(27,18)," "
13370 ON KEY 0 LABEL " START meas " Lcl_prt GOTO Exit
13375 ON KEY 1 LABEL " CHANGE time " Lcl_prt GOTO Enter
13380 FOR N=2 TO 8
13385 ON KEY N LABEL " " GOTO Top
13390 NEXT N
13395 ON KEY 9 LABEL " BLANK CRT " Lcl_prt CALL Blank !To blank CRT
13400 !
13405 KEY LABELS ON
13410 Top:LOOP
13415 TS=TIMES(TIMEDATE)
13420 TS$=TS(1,2)&TS(4,5)
13425 DISP " Starting time: " TS$," Present time: " TS$
13430 IF TS$=Start$ THEN Exit
13435 END LOOP
13440 Exit:
13445 SUBEND
13450 ! *****
13455 Rf: !
13460 SUB Rf(On,Freq,Pwr,Rf_on)
13465 OFF CYCLE
13470 OFF KEY
13475 IF On THEN
13480 Rf_on:
13485 DISABLE INTR 7
13490 BEEP 1500,.01
13495 Rf_on=1
13500 OUTPUT 709,"CLOSE 200"
13505 IF Freq<1 THEN
13510 OUTPUT 719;"B2"
13515 ELSE
13520 OUTPUT 719;"B3"
13525 END IF
13530 OUTPUT 720,"FR "&VAL$(Freq)&" GH,PO "&VAL$(Pwr)&" DB" !Set 931 f & p
13535 OUTPUT 720;"RF ON"
13540 WAIT 4
13545 ENTER 719;F
13550! Delt=Freq-F*1.E-9
13555! Nfreq=Freq*Delta
13560! OUTPUT 720 USING "2A,X,2D,2A":"FR",Nfreq,"GH" !Correct it
13565! WAIT 2
13570 OUTPUT 719;"PF "&VAL$(Freq)&" G" !Set EIP to lock at desired freq.
13575 WAIT 6
13580 ENABLE INTR 7;2
13585 ELSE
13590 Rf_off:
13595 DISABLE INTR 7
13600 OUTPUT 720;"RF OFF"
13605 OUTPUT 719;"BFG"
13610 OUTPUT 709;"OPEN 200"

```

```

13950 FOR I=Vpmin TO Vpmax STEP 4*Y      !Label every 10*Y on Y axis
13955 MOVE Timin-.01,I                  !To the left of X axis
13960 LABEL USING "#,DDD.D",I,E+6*I      !NO CR/LF - microvolts
13965 NEXT I
13970 PEN 2
13975 CLIP ON
13980 PENUP
13985 SUBEND ! Rtime_graph
13990 ! *****
13995 Stats: !
14000 SUB Stats(Na,E,Next_freq)          !Statistics to determine when to change
14005                                     !to next frequency
14010 OPTION BASE 1
14015 COM /Stats/ Eavg(100,2),Ecal(100),INTEGER N
14020 COM /init_stats/ Tcv,Rcv,Enr,SdNr,Volts(100),INTEGER Mode,Lss
14025 COM /Window_flags/ Window_CS(11),Window_rS(11)
14030 COM /Screen_updates/ Avg,Sd
14035 INTEGER Ta
14040 !
14045 ! Na - number of data points in the average & SD calculation
14050 ! E - latest thermopile reading (received parameter)
14055 ! Next_freq - flag indicating switch to next frequency (returned
14060 !           parameter) and flag to reset average counter
14065 ! Eavg - In Col 1: freq; in Col 2: Avg thermopile V
14070 ! Ecal - scratch array for avg
14075 ! N - keep track of No. of measurement values added
14080 ! Ecal - scratch array for avg
14085 !
14090 REDIM Ecal(Na)
14095 ALLOCATE D(Na)
14100 IF Next_freq THEN
14105   N=0
14110   MAT Ecal= (0)
14115   Next_freq=0
14120 END IF
14125 N=N+1
14130 SELECT N
14135 CASE <Na
14140   Ecal(N)=E
14145 GOTO Exit
14150 CASE =Na
14155   Ecal(Na)=E
14160 CASE >Na
14165   FOR K=1 TO Na-1
14170     Ecal(K)=Ecal(K-1)
14175   NEXT K
14180 END SELECT
14185 Ecal(Na)=E
14190 MAT Volts=Ecal
14195 CALL Find_trend(Next_freq)
14200 IF Next_freq THEN
14205   N=0
14210   MAT Ecal= (0)
14215 END IF
14220 GOSUB Calc_sd
14225 GOTO Exit
14230 Calc_sd:
14235   Avg=SUM(Ecal)/Na
14240   MAT D= Ecal-(Avg)
14245   MAT D= D . D
14250   Sd=SQR(SUM(D)/(Na-1))
14255   IF Sd<.3 E-9 THEN BEEP 2200,.01 !Signal when SD below threshold
14260 RETURN
14265 Exit:
14270 SUBEND
14275 ! *****
14280 Dnmv: !

```

```

14285 SUB Dnmv(Nread)
14290 ENTER 712,Nread
14295 SUBEND
14300 ! *****
14305 Dvm: !
14310 SUB Dvm(Sread)
14315 ENTER 722,Sread
14320 SUBEND
14325 ! *****
14330 Dc: !
14335 SUB Dc(On,Unit)
14340
14345 DISABLE
14350 SELECT Unit
14355 CASE =1
14360 IF On THEN
14365 OUTPUT 709,"CLOSE 207"
14370 ELSE
14375 OUTPUT 709,"OPEN 207"
14380 END IF
14385 CASE =2
14390 IF On THEN
14395 OUTPUT 709,"CLOSE 209"
14400 ELSE
14405 OUTPUT 709,"OPEN 209"
14410 END IF
14415 END SELECT
14420 ENABLE
14425 SUBEND
14430 ! *****
14435 Std_dev: !
14440 SUB Std_dev
14445
14450 OPTION BASE 1
14455 COM /Data/ Ffile$(20),File$(16),Mount_id$(16)
14460 COM /Data/ V(3000,2),F(3000,2),Ne(100,2),Header(27)
14465 COM /Data/ Af(10,3),INTEGER Tp(3000)
14470 INTEGER N,Na,N1,N2
14475 N1=1
14480 N2=100
14485 !
14490 Sys_prt=VAL(SYSTEM$("SYSTEM PRIORITY")) !Determine system priority
14495 Lcl_prt=Sys_prt+1 !Set local priority 1 higher for ON KEY
14500 ! Softkey interrupts:
14505 CONTROL 2,2,1
14510 CONTROL 1,12,0
14515 FOR N=0 TO 19
14520 ON KEY N LABEL " = GOTO Top
14525 NEXT N
14530 ON KEY 0 LABEL " PREV MENU " ,Lcl_prt GOTO Exit
14535 ON KEY 5 LABEL " CHANGE N1 " ,Lcl_prt GOSUB N_one
14540 ON KEY 6 LABEL " CHANGE N2 " ,Lcl_prt GOSUB N_two
14545 ON KEY 7 LABEL " CALCULATE SD " ,Lcl_prt GOSUB Calc_sd
14550 S_flg=1
14555 Top:LOOP
14560 IF S_flg THEN GOSUB Screen
14565 END LOOP
14570 !
14575 GOTO Exit
14580 !
14585 N_one:
14590 INPUT "Calculation starting point # ? ",N1
14595 S_flg=1
14600 RETURN
14605 !
14610 N_two:
14615 INPUT "Calculation stopping point # ? ",N2

```



```

14620 S_flg=2
14625 RETURN
14630 !
14635 Calc_sd:
14640 Na=N2-N1+1
14645 ALLOCATE Ecal(Na),D(Na)
14650 MAT Ecal= (0)
14655 MAT D= (0)
14660 FOR N=N1 TO N2
14665 Ecal(N+1-N1)=E(N,2)
14670 NEXT N
14675 Avg=SUM(Ecal)/Na
14680 MAT D= Bcal-(Avg)
14685 MAT D= D - D
14690 Sd=SQR(SUM(D)/(Na-1))
14695 PRINT TABXY(20,1),CHR$(136); !Move cursor for average
14700 PRINT USING "6D.1D,X.2A";Avg*1.E+9,"nv" !Erf
14705 PRINT TABXY(30,16); !Move cursor for SD
14710 PRINT USING "4D.2D,X.2A";Sd*1.E+9,"nv"
14715 DEALLOCATE Ecal(*),D(*)
14720 RETURN
14725 Screen:
14730 T1=(E(N1,1)-Header(2))/60
14735 T2=(E(N2,1)-Header(2))/60
14740 OUTPUT KBD,"K";
14745 PRINT TABXY(5,2),CHR$(137)&"M I C R O _ S D T"&CHR$(136)
14750 CLIP 0,80,62,100
14755 PEN 1
14760 FRAME
14765 PRINT CHR$(140)
14770 PRINT TABXY(18,6)," - - - CALCULATE STANDARD DEVIATION - - - "
14775 PRINT TABXY(10,8),"Starting point (N1): ";CHR$(136);N1;CHR$(140)
14780 PRINT TABXY(45,8),"Time: ";CHR$(136);
14785 OUTPUT CRT USING "32.D,3A";T1;CHR$(140);"min"
14790 PRINT TABXY(10,10),"Stopping point (N2): ";CHR$(136);N2;CHR$(140)
14795 PRINT TABXY(45,10),"Time: ";CHR$(136);
14800 OUTPUT CRT USING "32.D,3A";T2;CHR$(140);"min"
14805 PRINT TABXY(10,12),"Total points: ";CHR$(136);N2-N1+1;CHR$(140)
14810 PRINT TABXY(10,14),"Average: "
14815 PRINT TABXY(10,16),"Standard Deviation:"
14820 IF V(1,2) OR E(1,2) THEN
14825 PRINT TABXY(59,17),CHR$(129)&" DATA IN MEMORY "&CHR$(128)
14830 IF Dfile$="" THEN
14835 PRINT TABXY(59,18),CHR$(129)&" (NO FILE NAME) "&CHR$(128)
14840 ELSE
14845 PRINT TABXY(59,18),CHR$(129)&" FILE: "&Dfile$&CHR$(128)
14850 END IF
14855 ELSE
14860 PRINT TABXY(56,18),CHR$(129)&" NO DATA IN MEMORY "&CHR$(128)
14865 END IF
14870 S_flg=0
14875 RETURN
14880 Exit:
14885 SUBEND
14890 !
14895 Freq_change_pts: !
14900 SUB Freq_change_pts(Display)
14905 OPTON BASE 1
14910 COM /data/ Dfile$[20],File$[16],Mount_id$[16]
14915 COM /Data/ V(3000,2),E(3000,2),F(500,2),Ne(100,2),Header(27)
14920 COM /data/ Af(10,3),INTEGER Tp(3000)
14925 COM /Matrix_var/ Insert_Matrix(50),Choice$[1]
14930 COM /Matrix_var/ INTEGER Lower_index,No_of_inserts
14935 !
14940 INTEGER N,No1,Start,Finish,X,Y,Z
14945 !
14950 IF NOT Display THEN !No display or manual input
!For auto mode
!Random freq flag
!Put freq in random order
GOSUB Update_screen
IF Header(21) THEN
CALL Random_f
END IF
SUBEXIT
ELSE
CLEAR SCREEN
GOSUB Update_screen
IF Header(21) THEN
CALL Random_f
END IF
GOSUB Update_screen
END IF
!
Update_values: !
15030 Sys_ptty=VAL(SYSPTTY$("SYSTEM PRIORITY"))
15035 Lcl_ptty=Sys_ptty+1
15040 !
FOR Nn=0 TO 19
ON KEY Nn LABEL " ",Lcl_ptty GOTO Wait_loop
NEXT Nn
15055
15060 ON KEY 5 LABEL " CHANGE FREQ ",Lcl_ptty GOSUB Change_freq
15065 ON KEY 6 LABEL " ADD FREQ'S ",Lcl_ptty GOSUB Add_freqs
15070 ON KEY 0 LABEL " CONTINUE ",Lcl_ptty GOTO Sub_exit
!
15075
GOSUB Update_screen
IF Header(21) THEN
CALL Random_f
!Random freq flag
!Put freq in random order
GOSUB Update_screen
END IF
!
Wait_loop:
15115
15120 GOTO Wait_loop
!
15125
Update_screen: !
15130
15135 No1=Header(5)
15140 IF Header(19) THEN
F(1,1)=1
15145
F(Noi+2,1)=0
15150
F(Noi+3,1)=-2
15155
F(Noi+4,1)=-3
15160
Start=2
15165
Finish=Noi+1
15170
ELSE
15175
F(Noi+1,1)=0
15180
F(Noi+2,1)=-3
15185
Start=1
15190
Finish=Noi
15195
END IF
15200
X=1
15205
Y=3
15210
Z=3
15215
FOR N=Start TO Finish
!Input freq. & starting points
IF F(N,1)<1 AND Nc=No_elements THEN
OUTPUT F$ USING "XX.Z.DDD";F(N,1)
15235
ELSE
15240
OUTPUT F$ USING "3D.DDD";F(N,1)
15245
END IF
15250
IF Start=1 THEN
PRINT TABXY(X,Y);N;TABXY(X+5,Y);F$
15260
ELSE
15265
PRINT TABXY(X,Y);N-1;TABXY(X+5,Y);F$
15270
END IF
15275
Y=Y+1
15280
SELECT Y
15285

```



```

15290 CASE =19,-39,-59
15295 X=X+20
15300 Y=Z
15305 PRINT TABXY(X,1),"No.",TABXY(X+5,1),"Freq (GHz)"
15310 END SELECT
15315 NEXT N
15320 RETURN ! Update_screen
15325 !
15330 Add freqs: !
15335 Lcl_prty_2=VAL(SYSTEMS("SYSTEM PRIORITY"))+2
15340 MAT Insert_matrix= (0)
15345 !
15350 FOR M=1 TO 7
15355 ON KEY M LABEL " ",Lcl_prty_2 GOTO Wait_loop_2
15360 NEXT M
15365 ON KEY 5 LABEL "BEFORE FREQ #1",Lcl_prty_2 GOSUB Insert_before
15370 ON KEY 6 LABEL "AFTER LAST FREQ",Lcl_prty_2 GOSUB Insert_after
15375 ON KEY 7 LABEL "INSERT BETWEEN",Lcl_prty_2 GOSUB Insert_between
15380 ON KEY 0 LABEL "CONTINUE ",Lcl_prty_2 GOTO Update_values
15385 !
15390 Wait_loop_2: ! Wait for ON KEY interrupt.
15395 GOTO Wait_loop_2
15400 !
15405 Insert_before: !
15410 KEY LABELS OFF
15415 INPUT "No. of frequencies to be added: ",No_of_inserts
15420 FOR I=1 TO No_of_inserts
15425 INPUT "New frequency: ",Insert_matrix(I)
15430 NEXT I
15435 Choice$="B" ! Flag for "Before first frequency"
15440 CALL Insert_array
15445 GOSUB Update_screen
15450 KEY LABELS ON
15455 RETURN ! Insert_before
15460 !
15465 Insert_between: !
15470 KEY LABELS OFF
15475 INPUT "No. of frequencies to be added: ",No_of_inserts
15480 INPUT "No. of lower frequency (from display): ",Lower_index
15485 FOR I=1 TO No_of_inserts
15490 INPUT "New frequency: ",Insert_matrix(I)
15495 NEXT I
15500 Choice$="I" ! Flag for "In-between frequencies"
15505 CALL Insert_array
15510 GOSUB Update_screen
15515 KEY LABELS ON
15520 RETURN ! Insert_between
15525 !
15530 Insert_after: !
15535 KEY LABELS OFF
15540 INPUT "No. of frequencies to be added: ",No_of_inserts
15545 FOR I=1 TO No_of_inserts
15550 INPUT "New frequency: ",Insert_matrix(I)
15555 NEXT I
15560 Choice$="A" ! Flag for "After last frequency"
15565 CALL Insert_array
15570 GOSUB Update_screen
15575 KEY LABELS ON
15580 RETURN ! Insert_after
15585 !
15590 RETURN ! Add_freqs
15595 !
15600 Change_freq: !
15605 KEY LABELS OFF
15610 INPUT "No. of frequency to be changed: ",N_screen
15615 INPUT "Frequency (GHz): ",New_freq
15620 IF Header(19) THEN

```

```

15625 GOSUB Zero_flag_on
15630 ELSE
15635 GOSUB Zero_flag_off
15640 END IF
15645 KEY LABELS ON
15650 RETURN ! Change_freq
15655 !
15660 Zero_flag_off: !
15665 N=N_screen
15670 F(N,1)=New_freq
15675 IF F(N,1)<1 THEN
15680 OUTPUT F$ USING "XX,Z.DD";F(N,1)
15685 ELSE
15690 OUTPUT F$ USING "3D.DD";F(N,1)
15695 END IF
15700 SELECT N
15705 CASE <=16
15710 X=1
15715 Y=N+2
15720 CASE <=32
15725 X=21
15730 Y=N-14
15735 CASE <=48
15740 X=41
15745 Y=N-30
15750 END SELECT
15755 PRINT TABXY(X,Y);N,TABXY(X+5,Y);F$
15760 RETURN ! Zero_flag_off
15765 !
15770 Zero_flag_on: !
15775 N=N_screen+1
15780 F(N,1)=New_freq
15785 IF F(N,1)<1 THEN
15790 OUTPUT F$ USING "XX,Z.DD";F(N,1)
15795 ELSE
15800 OUTPUT F$ USING "3D.DD";F(N,1)
15805 END IF
15810 SELECT N_screen
15815 CASE <=16
15820 X=1
15825 Y=N_screen+2
15830 CASE <=32
15835 X=21
15840 Y=N_screen-14
15845 CASE <=48
15850 X=41
15855 Y=N_screen-30
15860 END SELECT
15865 PRINT TABXY(X,Y);N_screen,TABXY(X+5,Y);F$
15870 RETURN ! Zero_flag_on
15875 !
15880 Sub_exit: KEY LABELS OFF
15885 SUBEND ! Freq_change_pts
15890 ! * * * * *
15895 Runs: !
15900 SUB Runs(X(*), INTEGER N,Nruns)
15905 !This subroutine Runs determines the number of successive "runs"
15910 !that occurs in the data array "X", and returns the result in "Nruns".
15915 !
15920 OPTION BASE 1
15925 INTEGER I,J
15930 Nruns=0
15935 I=1
15940 Segment_1: !
15945 IF (I+1)>N THEN GOTO Segment_2
15950 Olddiff=X(I+1)-X(I)
15955 IF (Olddiff>0.) THEN

```

```

15960 Oldiff=FNSign(1.0,Oldiff)
15965 GOTO Segment_2
15970 END IF
15975 I=I+1
15980 GOTO Segment_1
15985 Segment_2:
15990 FOR J=I+1 TO N-1
15995   Diff=X(J+1)-X(J)
16000   IF (Diff<0.) THEN
16005     Diff=FNSign(1.0,Diff)
16010   IF (Diff<>Oldiff) THEN
16015     Nrns=Nrns+1
16020     Oldiff=Diff
16025   END IF
16030 NEXT J
16035 Nrns=Nrns+1
16040 SUBEND ! Runs
16045 ! *****
16050 ! *****
16055 Taub:
16060 SUB Taub(X(*),INTEGER N,REAL Tau,Prob)
16065 !This subroutine Taub computes the probability "Prob" from the data
16070 !array contained in "X".
16075 !
16080 OPTION BASE 1
16085 INTEGER I,J
16090 REAL U,S,Susq,Tx,Tiechk,Xtmp,T,Vars
16095 !
16100 S=0.
16105 Susq=0.
16110 FOR I=1 TO N-1
16115   FOR J=I+1 TO N
16120     U=X(J)-X(I)
16125     IF (U<>0.) THEN U=FNSign(1.,U)
16130     S=S+U
16135     Susq=Susq+U*U
16140   NEXT J
16145 NEXT I
16150 Tau=S/SQR(Susq*N*(N-1)/2)
16155 Tx=0.
16160 Tiechk=Susq-(N*(N-1))/2
16165 IF Tiechk<0. THEN
16170   MAT SORT X(*)
16175   Xtmp=X(1)
16180   T=1.
16185 FOR I=2 TO N
16190   IF X(I)-Xtmp THEN
16195     T=X(I)-Xtmp
16200   GOTO End_of_taubloop
16205 ELSE
16210   Xtmp=X(I)
16215 END IF
16220 IF T>1.0 THEN
16225   Tx=Tx+T*(T-1)*(2.*T*5.)
16230   T=1.0
16235 END IF
16240 End_of_taubloop:
16245 NEXT I
16250 END IF
16255 Vars=(N*(N-1)*(2*N+5)-Tx)/18.0
16260 Z=S/SQR(Vars)
16265 CALL Errf(Z,Prob)
16270 SUBEND ! Taub
16275 ! *****
16280 Fnsign:
16285 DEF FNSign(A,B)
16290 !This function "SIGN" returns:

```

```

16295 ! ABS(A) if B>0
16300 ! -ABS(A) if B<0
16305 !
16310 IF B<0 THEN
16315 RETURN -ABS(A)
16320 ELSE
16325 RETURN ABS(A)
16330 END IF
16335 FNEnd ! Sign
16340 ! *****
16345 Errf:
16350 SUB Errf(X,P)
16355 ! From FORTRAN code supplied by D. Vecchia,870929.
16360 ! This subroutine computes the error function for the value X,
16365 ! and returns the answer in the variable P. The answer is not
16370 ! the standard result, but is computed on the basis of the last
16375 ! three conditional statements at the end of the subroutine.
16380 !
16385 DATA
0.319381530,-0.356563782,1.781477937,-1.8212515978,1.330274429,0.2316419
0.319381530,-0.356563782,1.781477937,-1.8212515978,1.330274429,0.2316419
16390 READ B1,B2,B3,B4,B5,P
16395 Z=ABS(X)
16400 T=1/(1+P*Z)
16405 Cdf=1-(((.39894228040143)*EXP(-.5*Z*Z))*)
(B1*T+B2*T*T+B3*T*T*T+B4*T*T*T*T+B5*T*T*T*T*T)
16410 IF X<0 THEN P=1-Cdf
16415 IF X=0 THEN P=.5
16420 IF X>0 THEN P=Cdf
16425 SUBEND ! errf
16430 ! *****
16435 Find_trend:
16440 SUB Find_trend(Stable_run)
16445 ! The purpose of this of subroutine is to determine if
16450 ! stability exist in a given set of data points. This
16455 ! is determined by computing two statistical values,
16460 ! denoted by R and Prob, and comparing these values to
16465 ! pre-determined constants. A decision is based on the
16470 ! results of this comparison as follows:
16475 ! R > Rcv or Prob > (1 - Tcv)
16480 ! If either of these conditions are met, then the sub-
16485 ! routine returns Stable_run=1, which means stability
16490 ! exist. If stability does not exist, then Stable_run=0.
16495 !
16500 OPTION BASE 1
16505 COM /Init_stats/ Tcv,Rcv,Enr,Sdnr,Volts(100),INTEGER Mode,Lss
16510 COM /State_2/ R,Prob,INTEGER Nrns
16515 REAL Vwork(100)
16520 INTEGER I,N
16525 !
16530 !Compute the statistics of the number of runs, R:
16535 CALL Runs(Volts(*),Lss,Nrns)
16540 R=(Nrns-Enr)/Sdnr
16545 !
16550 !Copy vector Volts into vector Vwork for use in SUB Taub;
16555 !Taub computes the probability Prob:
16560 MAT Vwork=Volts
16565 CALL Taub(Vwork(*),Lss,Tau,Prob)
16570 !
16575 ! - - -Nrns,R,Prob printed by Screen_update
16580 !
16585 ! Check for monotonically increasing/decreasing data.
16590 IF R>Rcv AND Prob>Tcv AND Prob<(1-Tcv) THEN
16595   Stable_run=1
16600 ELSE
16605   !Data is not stable; fetch new data point and re-compute the
16610   !statistics.
16615   GOTO Sub_exit

```

```

16620      END IF
16625 Sub Exit: !
16630 SUBEND ! Find trend
16635 ! *****
16640 Settle_1: !
16645 SUB Settle_1(N1,N2,Erf,Nmid,Nst,Nsp,S_flg)
16650 !
16655 ! N1: Frequency starting point
16660 ! N2: Frequency stopping point
16665 ! Nst: Beginning of settled run
16670 ! Nsp: End of settled run
16675 ! Erf: is the final settled value
16680 ! Nmid: is the mid point of the array range from which Erf came
16685 ! S_flg: A flag to pause after every call to Find_trend subprogram
16690 !
16695 !
16700 !
16705 !
16710 !
16715 !
16720 !
16725 !
16730 !
16735 !
16740 !
16745 !
16750 !
16755 !
16760 !
16765 !
16770 !
16775 !
16780 !
16785 !
16790 !
16795 !
16800 !
16805 !
16810 !
16815 !
16820 !
16825 !
16830 !
16835 !
16840 !
16845 !
16850 !
16855 !
16860 !
16865 !
16870 !
16875 !
16880 !
16885 !
16890 !
16895 !
16900 !
16905 !
16910 !
16915 !
16920 !
16925 !
16930 !
16935 !
16940 !
16945 !
16950 !

COM /Io_path_names/ @Eip_578,@Eip_931,@Dp_8200,@Hp_3457
COM /Initial_value/ V_ref_0,V_rf_off

DIM Sign$(1),Range$(1)
INTEGER No_dec_digits

Software_lockout: !
Min_voltage=1.6! 1.9 V originally
Max_current=100! 100 mA

! Copy initial values into reference variables:
Value=ABS(Value_0) ! Absolute value required.
Mode$=UPC$(Mode_0$) ! Force uppercase letters.

IF Mode$="V" THEN
  IF Value<Min_voltage THEN
    Present_max=Min_voltage
    Unit$=" V"
  GOSUB Error_lockout
  BEEP 1500,.05
  Value_0=V_ref_0
  Value=ABS(V_ref_0)
  END IF
  END IF ! Mode$="V"
IF Mode$="A" THEN
  IF Value>Max_current THEN
    Present_max=Max_current
    Unit$=" mA"
  GOSUB Error_lockout
  Value=Max_current
  END IF
  END IF ! Mode$="A"
IF Mode$="A" THEN
  IF Value>Max_current THEN
    Present_max=Max_current
    Unit$=" mA"
  GOSUB Error_lockout
  Value=Max_current
  END IF
  END IF ! Mode$="A"
IF Value_0<0 THEN
  Sign$="-"
  ELSE
  Sign$="+"
  END IF ! Value_0<0
  END IF ! Mode$="V" THEN
  SELECT Value
  CASE <=1.0485758-1
    Range$="0" ! 100 mV range; max value= 104.8575 mV
    No_dec_digits=4 ! Format required: NNND
    N = integer numbers D = decimal numbers
  CASE <=10.48575
    Range$="1" ! 10 V range; max value= 10.48575 V
    No_dec_digits=5 ! Format required: NNDDDD
  CASE <=104.8575
    Range$="2" ! 100 V range; max value= 104.8575 V
    No_dec_digits=5 ! Format required: NNDDDD
  END SELECT ! Value
  END IF ! Mode$="V"
  END IF ! Mode$="A" THEN
  Range$="3" ! Format required: NNDDDD
  No_dec_digits=3
  END IF ! Mode$="A"
  New_value=Value*10^No_dec_digits! Move decimal point over.
  ! The following code writes alphanumeric data into the string
  ! variable "Dp_output$".
  IF Mode$="V" THEN
    OUTPUT Dp_output$ USING "3A,72",Mode$&Range$&Sign$,New_value
  ELSE

```



```

17290 OUTPUT Dp_output$ USING "2A, 6Z"; Mode$&Sign$, New_value
17295 END IF; Mode$="V"
17300 !
17305 GOTO Set_output! Set output of DP 8200 and SUBEND.
17310 !
17315 Error_lockout: !
17320 BEEP
17325 PRINT
17330 PRINT USING "K"; "Output requested ", Value, Unit$, " exceeds maximum
      allowed."
17335 PRINT USING "K"; "Present maximum: ", Present_max, Unit$
17340 PRINT "Program is PAUSED in subroutine DP_8200_source."
17345 PRINT
17350 PAUSE
17355 RETURN ! Error_lockout
17360 !
17365 Set_output: !
17370 BEEP 1500, .05
17375 OUTPUT @Dp_8200; Dp_output$
17380 !
17385 SUBEND ! Dp_8200
17390 !
17395 Power_lever_set: !
17400 !*****
17405 SUB Power_lever_set (V_ref, Sread)
17410 !*****
17415 !
17420 INPUT(S) : Sread - power meter voltage, RF is off.
17425 ! OUTPUT(S) : V_ref - reference voltage for the DP 8200.
17430 !
17435 COM /Pwr_lever_set in/ P_rf, R_0
17440 COM /Initial_value/ V_ref_0, V_rf_off
17445 !
17450 V_rf_off=Sread ! Power meter voltage, RF is off.
17455 V_ref=SQR(V_rf_off*V_rf_off-(P_rf/1000*R_0))
17460 CALL Dp_8200(V_ref, "V") ! Set the voltage reference to initial value.
17465 !
17470 SUBEND ! Power_lever_set
17475 !
17480 Intr7: !
17485 !*****
17490 SUB Intr7
17495 !*****
17500 !
17505 COM /Io_path_names/ @Eip_578, @Eip_931, @Dp_8200, @Hp_3457
17510 COM /Intr_parameters/ Desired_freq, INTEGER No_of_intrs
17515 !
17520 No_of_intrs=No_of_intrs+1
17525 Source_freq=Desired_freq
17530 !
17535 !
17540 OUTPUT @Eip_931 USING "2A, X, 2D, X, 2A": "PR", Source_freq, "GH"
17545 WAIT 2
17550 !
17555 OUTPUT @Eip_578, "RS" ! Reset the counter to allow a measurement.
17560 WAIT 2
17565 ENTER @Eip_578; Freq_m ! Measure the EIP uWave Source frequency with
      ! the EIP counter.
17570 !
17575 !
17580 Measured_freq=Freq_m/1.E+9 ! Convert to GHz.
17585 Offset=ROUND(Desired_freq-Measured_freq, 5) ! Units are GHz.
17590 IF Offset<=.2*Desired_freq THEN Offset=.2*Desired_freq
17595 Source_freq=Source_freq+Offset
17600 !
17605 OUTPUT @Eip_931 USING "2A, X, 2D, X, 2A": "PR", Source_freq, "GH"
17610 WAIT 2
17615 OUTPUT @Eip_578; "PF " & VAL$(Desired_freq) & " G"

```

```

17620 !
17625 OUTPUT @Eip_931, "CLEARST" ! Clear the status register of the 931
      ! source to prevent an interrupt from it.
17630 ENABLE INTR 7; 2 ! Re-enable the interrupts (2=SRQ bit).
17640 OUTPUT @Eip_578, "SR02" ! SRQ on bit 2, "counter searching", enabled.
17645 !
17650 SUBEND ! SUB Intr7
17655 !
17660 Power_lever_chk: !
17665 !*****
17670 SUB Power_lever_chk(V_ref, V_rf_on, Pwr)
17675 !*****
17680 !
17685 INPUT(S) : V_ref - reference voltage for DP 8700.
17690 ! OUTPUT(S) : V_rf_on - power meter voltage, RF is on.
      ! V_ref - may be changed as determined by code.
17695 ! Pwr - calculated from last V_rf_off & V_rf_on
17700 ! COM /Pwr_lever_set in/ P_rf, R_0
17710 COM /Initial_value/ V_ref_0, V_rf_off
17715 !
17720 Delta_v=ROUND(V_ref-V_rf_on, 5) ! Difference: Ref-present reading
17725 SELECT Delta_v
17730 CASE <-.0001 ! Leveler out of control - reset
      V_ref=ROUND(V_rf_on, 5)+.0001 ! Compute new value
      CALL Dp_8200(V_ref, "V") ! Set 8200 to new value
17740 CASE >.05 ! 8200 has probably set itself to zero
      CALL Dp_8200(V_ref_0, "V") ! Reset 8200 to original value
17750 END SELECT
17755 !
17760 ! Pwr=1000*(V_rf_off-V_rf_on-V_rf_on)/R_0 ! Power calc
17765 !
17770 SUBEND ! Power_lever_chk
17775 !
17780 !
17785 Display_data: !
17790 !*****
17795 SUB Display_data
17800 !*****
17805 !
17810 COM /Xy_coordinates/ T_min, T_max, V_min, V_max
17815 !
17820 CLEAR SCREEN
17825 !
17830 PRINT CHR$(136)
17835 PRINT TABXY(15, 4); "The current real-time graph parameters are:"
17840 PRINT CHR$(138)
17845 PRINT TABXY(15, 7); "(1) Minimum Time (hours)"
17850 PRINT TABXY(50, 7); CHR$(136); T_min/3600; CHR$(138)
17855 PRINT TABXY(15, 10); "(2) Maximum Time (hours)"
17860 PRINT TABXY(50, 10); CHR$(136); T_max/3600; CHR$(138)
17865 PRINT TABXY(15, 13); "(3) Minimum Voltage (microvolts)"
17870 PRINT TABXY(50, 13); CHR$(136); V_min*10^6; CHR$(138)
17875 PRINT TABXY(15, 16); "(4) Maximum Voltage (microvolts)"
17880 PRINT TABXY(50, 16); CHR$(136); V_max*10^6; CHR$(138)
17885 !
17890 Sys_prtty=VAL(SYSTEM$( "SYSTEM PRIORITY" ))
17895 Lcl_prtty=Sys_prtty+1
17900 FOR N=0 TO 19
17905 ON KEY N LABEL " ", Lcl_prtty GOTO Wait_loop
17910 NEXT N
17915 ON KEY 5 LABEL "CHANGE DEFAULT", Lcl_prtty GOSUB Change_param
17920 ON KEY 0 LABEL " CONTINUE ", Lcl_prtty GOTO Sub_exit
17925 KEY LABELS ON
17930 !
17935 Wait_loop: ! Wait for ON KEY interrupt.
17940 GOTO Wait_loop
17945 !
17950 Change_param: !

```

```

17955 KEY LABELS OFF
17960 INPUT "Number of parameter to be changed:",Parameter_no
17965 !
17970 PRINT CHR$(136)
17975 SELECT Parameter_no
17980 CASE =1
17985 INPUT "Minimum Time (hours)=",T_min
17990 PRINT TABXY(50,7),T_min,"
17995 T_min=T_min*3600 !Convert to seconds
18000 CASE =2
18005 INPUT "Maximum Time (hours)=",T_max
18010 PRINT TABXY(50,10),T_max,"
18015 T_max=T_max*3600 !Convert to seconds
18020 CASE =3
18025 INPUT "Minimum Voltage (microvolts)=",V_min_uv
18030 PRINT TABXY(50,13),V_min_uv,"
18035 V_min=V_min_uv/10^6 ! Convert from microvolts to volts.
18040 CASE =4
18045 INPUT "Maximum Voltage (microvolts)=",V_max_uv
18050 PRINT TABXY(50,16),V_max_uv,"
18055 V_max=V_max_uv/10^6 ! Convert from microvolts to volts.
18060 END SELECT
18065 PRINT CHR$(138)
18070 KEY LABELS ON
18075 RETURN ! Change_param
18080 !
18085 SUB exit:KEY LABELS OFF
18090 SUBEND! Display_data
18095 !
18100 Generate_freq:
18105 !*****
18110 SUB Generate_freq(Nomore_f,INTEGER Row)
18115 !*****
18120 !
18125 OPTION BASE 1
18130 COM /Data/ Dfiles[20],Files[16],Mount_id[16]
18135 COM /Data/ V(3000,2),E(3000,2),F(500,2),Header(27)
18140 COM /Data/ Af(10,3),INTEGER Tp(3000)
18145 !
18150 INTEGER I,No_of_freqs,Rowm
18155 Rowm=SIZE(Af,1)
18160 !
18165 IF Header(20) THEN
18170 Min_freq=Af(Row,1)
18175 Header(6)=Min_freq
18180 Max_freq=Af(Row,2)
18185 Header(7)=Max_freq
18190 Delta_freq=Af(Row,3)
18195 Header(8)=Delta_freq
18200 IF Row=Rowm THEN Nomore_f=1
18205 ELSE
18210 Min_freq=Header(6)
18215 Max_freq=Header(7)
18220 Delta_freq=INT(1.E+3*Header(8))/1.E+3 !Step, integer based
18225 Nomore_f=1
18230 END IF
18235 !
18240 IF Delta_freq=0 THEN
18245 No_of_freqs=(Max_freq-Min_freq)/Delta_freq+1
18250 Header(5)=No_of_freqs
18255 Next_freq=Min_freq
18260 !
18265 IF Header(19) THEN
18270 Start=2
18275 Finish=No_of_freqs+1
18280 ELSE
18285 Start=1
!Without zero correction

```

```

18290 Finish=No_of_freqs
18295 END IF
18300 !
18305 REDIM F(Finish+2,2)
18310 !
18315 FOR I=Start TO Finish
18320 F(I,1)=Next_freq
18325 Next_freq=Next_freq+Delta_freq
18330 NEXT I
18335 ELSE
18340 No_of_freq=7
18345 Header(5)=No_of_freq
18350 REDIM F(No_of_freq+2,2)
18355 FOR I=1 TO No_of_freq
18360 READ F(I,1)
18365 NEXT I
18370 DATA .1,1.5,10,15,17,18
18375 END IF
18380 !
18385 SUBEND ! Generate_freq
18390 !
18395 Insert_array: !
18400 !*****
18405 SUB Insert_array
18410 !*****
18415 !
18420 !This subroutine inserts a subarray into a larger array. It is designed
18425 specifically for the program MICRO_Cx??. and the large array is a two
18430 dimensional array with inserted items in the first column.
18435 !
18440 INPUT(S): Dest_matrix - the array that receives the inserted items
18445 ! Insert_matrix - the array that is to be inserted into
18450 ! Dest_matrix
18455 ! Choice$ - A character variable that flags a need to insert
18460 ! data before the first frequency ("B"), in-between
18465 ! two frequencies ("I"), or after the last frequency
18470 ! ("A").
18475 ! Lower_index - the lower index number of Dest_matrix
18480 ! Upper_index - the upper index number of Dest_matrix
18485 ! (e.g., if Insert_array needed to be inserted between items
18490 ! 3 and 4 of Dest_matrix, then Lower_index=3 and Upper_index=4)
18495 ! No_elements - total No. of elements in Dest_matrix (before
18500 ! Insert_array is inserted)
18505 ! No_of_inserts - No. of elements in Insert_array to be inserted
18510 ! into Dest_matrix
18515 ! (All variables are in COM /Matrix_var/)
18520 !
18525 !OUTPUT(S): Elements in Insert_array are inserted in the proper place
18530 ! in the array Dest_matrix, and elements in Dest_matrix are
18535 ! moved up accordingly (no elements are deleted).
18540 ! Variable "No_elements" updated to the size of the new, ex-
18545 ! panded array.
18550 !
18555 OPTION BASE 1
18560 COM /Data/ Dfiles[20],Files[16],Mount_id[16]
18565 COM /Data/ V(3000,2),E(3000,2),F(500,2),Header(27)
18570 COM /Data/ Af(10,3),INTEGER Tp(3000)
18575 !
18580 COM /Matrix_var/ Insert_matrix(50),Choices$
18585 COM /Matrix_var/ INTEGER Lower_index,No_of_inserts
18590 !
18595 ALLOCATE Temp_matrix(250),Dest_matrix(500)
18600 INTEGER A,B,Z
18605 !
18610 Total=Header(5)+No_of_inserts! Total No. of elements for new array.
18615 No_elements=Header(5)
18620 !

```

```

18625 MAT Dest_matrix= (0)
18630 MAT Temp_matrix= (0)
18635 !
18640 IF Header(19) THEN
18645 MAT Dest_matrix(1:No_elements+1)= F(1:No_elements+1,1)
18650 ELSE
18655 MAT Dest_matrix(1:No_elements)= F(1:No_elements,1)
18660 END IF
18665 !
18670 SELECT Choice$
18675 CASE ="B": Before first frequency
18680 IF Header(19) THEN
18685 A=2
18690 Z=No_elements+1
18695 Tot=Total+1
18700 ELSE
18705 A=1
18710 Z=No_elements
18715 Tot=Total
18720 END IF
18725 B=A-No_of_inserts
18730 MAT Temp_matrix= Dest_matrix(A:Z)
18735 MAT Dest_matrix(A:B-1)= Insert_matrix(1:No_of_inserts)
18740 MAT Dest_matrix(B:Tot)= Temp_matrix
18745 !
18750 CASE ="I": In-between frequencies
18755 IF Header(19) THEN
18760 A=Lower_index+2
18765 B=Lower_index+No_of_inserts+1
18770 Z=No_elements+1
18775 Tot=Total+1
18780 ELSE
18785 A=Lower_index+1
18790 B=Lower_index+No_of_inserts
18795 Z=No_elements
18800 Tot=Total
18805 END IF
18810 MAT Temp_matrix= Dest_matrix(A:Z)
18815 MAT Dest_matrix(A:B)= Insert_matrix(1:No_of_inserts)
18820 MAT Dest_matrix(B+1:Tot)= Temp_matrix
18825 !
18830 CASE ="A": After last frequency
18835 IF Header(19) THEN
18840 A=2
18845 Q=No_elements+2
18850 Tot=Total+1
18855 ELSE
18860 A=1
18865 Q=No_elements+1
18870 Tot=Total
18875 END IF
18880 MAT Dest_matrix(Q:Tot)= Insert_matrix(1:No_of_inserts)
18885 END SELECT
18890 !
18895 MAT F(A:Tot,1)= Dest_matrix(A:Tot)
18900 Header(5)=Total ! Update variable for new matrix size.
18905 !
18910 DEALLOCATE Temp_matrix(*), Dest_matrix(*)
18915 !
18920 SUBEND! Insert_array
18925 !
18930 Window_left: ! Left window
18935 !*****
18940 SUB Window_left
18945 !*****
18950 !
18955 OPTION BASE 1

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18960 !
18965 COM /Data/ Dfiles$[20], Files$[16], Mount_id$[16]
18970 COM /Data/ V(3000,2), F(3000,2), Ne(100,2), Header(27)
18975 COM /Data/ Af(10,3), INTEGER Tp(3000)
18980 !
18985 PRINT TABXY(7,3), "HEADER INFO"
18990 PRINT TABXY(1,4), "Mount ID: ", CHR$(136); " ", Mount_id$, " ", CHR$(140)
18995 PRINT TABXY(1,5), "File name: ", CHR$(136); Files$(140)
19000 PRINT TABXY(1,6), "Start Time: ", CHR$(136); DATES$(TIMEDATE)
19005 PRINT TABXY(14,7), CHR$(136); TIMES$(TIMEDATE); CHR$(140)
19010 PRINT TABXY(1,8), "Start Freq: ", CHR$(136); Header(6); "GHz ", CHR$(140)
19015 PRINT TABXY(1,9), "Stop Freq: ", CHR$(136); Header(7); "GHz ", CHR$(140)
19020 !
19025 SUBEND ! Window_left
19030 !
19035 Window_c_a: ! Center window
19040 !*****
19045 SUB Window_c_a
19050 !*****
19055 !
19060 OPTION BASE 1
19065 COM /Data/ Dfiles$[20], Files$[16], Mount_id$[16]
19070 COM /Data/ V(3000,2), F(3000,2), Ne(100,2), Header(27)
19075 COM /Data/ Af(10,3), INTEGER Tp(3000)
19080 COM /Window_flags/ Window_cs, Window_rs
19085 COM /Screen_update/ Count, Cftime, Freq, Pwr
19090 !
19095 Window_cs="A" !Flags which header info is displayed.
19100 FOR Row=3 TO 7
19105 PRINT TABXY(28,Row); " " !Clear previous info.
19110 NEXT Row
19115 !
19120 PRINT TABXY(34,3), CHR$(140); "LAST READING"
19125 PRINT TABXY(28,4), "Total time: "
19130 PRINT TABXY(28,5), "Elapsed time: "
19135 PRINT TABXY(28,6), "Total count: "
19140 PRINT TABXY(28,9), CHR$(136); "Press K5 for next window"; CHR$(128)
19145 PRINT CHR$(136)
19150 CALL Screen_update
19155 !
19160 SUBEND ! Window_c_a
19165 !
19170 Window_r_a: ! Right window
19175 !*****
19180 SUB Window_r_a
19185 !*****
19190 !
19195 OPTION BASE 1
19195 COM /Data/ Dfiles$[20], Files$[16], Mount_id$[16]
19200 COM /Data/ V(3000,2), F(3000,2), Ne(100,2), Header(27)
19205 COM /Data/ Af(10,3), INTEGER Tp(3000)
19210 COM /Window_flags/ Window_cs, Window_rs
19215 !
19220 Window_rs="A" !Flags which header info is displayed.
19225 FOR Row=3 TO 8
19230 PRINT TABXY(55,Row); " " !Clear previous info.
19235 NEXT Row
19240 !
19245 PRINT TABXY(56,3), CHR$(140); "THERMOPILE OUTPUT & TEMP"
19250 PRINT TABXY(55,4), "Thermopile: "
19255 PRINT TABXY(55,5), "T'pile Avg: "
19260 PRINT TABXY(55,6), "T' Std Dev: "
19265 PRINT TABXY(55,7), "Room Temp: "
19270 PRINT TABXY(55,8), "Bath Temp: "
19275 PRINT TABXY(55,9), CHR$(136); "Press K6 for next window"; CHR$(128)
19280 PRINT CHR$(136)
19285 !
19290 CALL Screen_update

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19295 !
19300 SUBEND ! Window_r_a
19305 !
19310 Window_c_b: !
19315 !*****
19320 SUB Window_c_b
19325 !*****
19330 !
19335 OPTION BASE 1
19340 COM /Data/ Dfiles[20], Files[16], Mount_id[16]
19345 COM /Data/ V(3000,2), F(500,2), Ne(100,2), Header(27)
19350 COM /Data/ Af(10,3), INTEGER Tp(3000)
19355 COM /Window_flags/ window_cs, Window_r[5]
19360 !
19365 Window_cs="B"
19370 FOR Row=3 TO 7
19375 PRINT TABXY(28, Row); " " !Clear previous info.
19380 NEXT Row
19385 !
19390 PRINT TABXY(32, 3), CHR$(136); "SYSTEM PARAMETERS"
19395 PRINT TABXY(28, 4), "Frequency: "
19400 PRINT TABXY(28, 5), "Pwr Meter V: "
19405 PRINT TABXY(28, 6), "Ref V: "
19410 PRINT TABXY(28, 7), "Power: "
19415 PRINT TABXY(28, 9), CHR$(136); "Press K5 for next window", CHR$(128)
19420 PRINT CHR$(136)
19425 CALL Screen_update
19430 !
19435 SUBEND ! Window_c_b
19440 !
19445 Window_r_b: !
19450 !*****
19455 SUB Window_r_b
19460 !*****
19465 !
19470 OPTION BASE 1
19475 COM /Data/ Dfiles[20], Files[16], Mount_id[16]
19480 COM /Data/ V(3000,2), F(500,2), Ne(100,2), Header(27)
19485 COM /Data/ Af(10,3), INTEGER Tp(3000)
19490 COM /Window_flags/ window_cs, Window_r[5]
19495 !
19500 Window_r[5]="B"
19505 FOR Row=3 TO 8
19510 PRINT TABXY(55, Row); " " !Clear previous info
19515 NEXT Row
19520 PRINT TABXY(64, 3), CHR$(140); "STATISTICS"
19525 PRINT TABXY(55, 4), "NO. in average: "
19530 PRINT TABXY(55, 5), "Runs: "
19535 PRINT TABXY(55, 6), "R: "
19540 PRINT TABXY(55, 7), "Prob: "
19545 PRINT TABXY(55, 9), CHR$(136); "Press K6 for next window", CHR$(128)
19550 PRINT CHR$(136)
19555 CALL Screen_update
19560 !
19565 SUBEND ! Window_r_b
19570 !
19575 Meas_disp: !
19580 !*****
19585 SUB Meas_disp
19590 !*****
19595 !
19600 OPTION BASE 1
19605 COM /Data/ Dfiles[20], Files[16], Mount_id[16]
19610 COM /Data/ V(3000,2), F(500,2), Ne(100,2), Header(27)
19615 COM /Data/ Af(10,3), INTEGER Tp(3000)
19620 COM /Window_flags/ window_cs[1], Window_r[1]
19625 COM /Screen_update/ Count, Cftime, Freq, Pwr

19630 !
19635 KEY LABELS OFF
19640 OUTPUT KBD; "K";
19645 PRINT TABXY(1,1), CHR$(137); "M I C R O - C x"&CHR$(136)
19650 PRINT TABXY(30,1), CHR$(136); CHR$(129); " M E A S U R E M E N T I N
P R O G R E S S "; CHR$(128)
19655 !
19660 CLIP 0,128,63,92
19665 FRAME
19670 !To draw a rectangle
19675 !Draw the rectangle
19680 !Map x,y to default GDU's
19685 !Draw a vertical line
19690 !
19695 !Draw a vertical line
19700 !
19705 !To draw a rectangle
19710 FRAME
19715 PRINT CHR$(140)
19720 !Set PEN color to Cyan.
19725 !Left header information
19730 !Center header information
19735 !Right header information
19740 !
19745 PRINT TABXY(28,8), CHR$(140); "Sec to next reading: "; CHR$(136)
19750 !
19755 CALL Rtime_graph
19760 SUBEND ! Meas_disp
19765 !
19770 Screen_update: !
19775 !*****
19780 SUB Screen_update
19785 !*****
19790 !
19795 OPTION BASE 1
19800 !
19805 COM /Data/ Dfiles[20], Files[16], Mount_id[16]
19810 COM /Data/ V(3000,2), F(500,2), Ne(100,2), Header(27)
19815 COM /Data/ Af(10,3), INTEGER Tp(3000)
19820 COM /Initial value/ V_ref 0, V_rf off
19825 COM /Init_state/ Tcv, Rcv, Enr, Sdnt, Volts(100), INTEGER Mode, Lss
19830 COM /State_2/ R, Prob, INTEGER Nrums
19835 COM /Window_flags/ Window_cs[1], Window_r[1]
19840 COM /Screen_update/ Count, Cftime, Freq, Pwr
19845 COM /Screen_update2/ Avg, Sd
19850 !
19855 IF Window_cs="A" THEN
19860 !LAST READING
19865 Total_time=(TIMEDATE-Header(2))/60 !Total time elapsed.
19870 IF Count<1 THEN Total_time=0 !Special first time thru
19875 PRINT TABXY(41,4), CHR$(136); !Move cursor for total time.
19880 PRINT USING "#,4D,2D,X,3A"; Total_time, "min"
19885 E_time=(TIMEDATE-Cftime)/60 !Elapsed time since last freq change
19890 IF Count<1 THEN E_time=0 !Special first time thru
19895 PRINT TABXY(41,5); !Move cursor for Elapsed time
19900 PRINT USING "#,4D,2D,X,3A"; E_time, "min"
19905 PRINT TABXY(42,6), Count; !Display the count
19910 GOTO Sub_exit
19915 END IF ! Window_cs="A"
19920 !
19925 IF Window_cs="B" THEN
19930 !SYSTEM PARAMETERS
19935 PRINT TABXY(41,4); !Move cursor for Freq
19940 PRINT USING "#,2D,2D,X,3A"; Freq, "GHz"
19945 Cnt=Count
19950 IF Count=0 THEN Cnt=1
19955 PRINT USING "#,M2,6D,X,1A"; V(Cnt,2), "V"
19960 PRINT TABXY(40,6); !Move cursor for reference voltage
19965 PRINT USING "#,M2,6D,X,1A"; V_ref_0, "V"

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19960 PRINT TABXY(40,7); !Move cursor for power
19965 PRINT USING "#,2D,4D,X,2A";Pwr,"mW"
19970 END IF ! Window_CS="B"
19975 !
19980 IF Window_r$="A" THEN !THERMOPILE OUTPUT & TEMPS
19985 PRINT TABXY(70,4); !Move cursor for thermopile voltage
19990 Cnt=Count
19995 IF Count=0 THEN Cnt=1
20000 PRINT USING "#,3D,3D,X,3A";E(Cnt,2)*1.E+6," uV"
20005 PRINT TABXY(70,5); !Move cursor for average
20010 PRINT USING "#,3D,4D,X,2A";Avg*1.E+6,"uV" !Erf
20015 PRINT TABXY(69,6); !Move cursor for SD
20020 PRINT USING "#,4D,4D,X,2A";Sd*1.E+6,"uV"
20025 PRINT TABXY(66,7); !Move cursor for room temperature
20030 Cnt=Count
20035 IF Count=0 THEN Cnt=1
20040 PRINT USING "#,2D,2D,X,6A";Tp(Cnt)*1.E-3," deg C"
20045 PRINT TABXY(66,8); !Move cursor for bath temperature.
20050 PRINT USING "#,2D,3D,X,5A";Header(18),"deg C"
20055 END IF ! Window_r$="A"
20060 !
20065 !
20070 IF Window_r$="B" THEN !STATISTICS
20075 PRINT TABXY(70,4);Lss !Print readings in average
20080 PRINT TABXY(61,5); !Move cursor for runs
20085 PRINT USING "#,2D",Nruns !No of runs
20090 PRINT TABXY(61,6); !Move cursor for R
20095 PRINT USING "#,2D,2D";R !R
20100 PRINT TABXY(62,7); !Move cursor for Prob
20105 PRINT USING "#,D,3D";prob !Prob
20110 END IF ! Window_r$="B"
20115 Sub_exit: !
20120 SUBEND ! Screen_update
20125 !
20130 Blank:SUB Blank
20135 COM /Blank/ INTEGER Off
20140 IF Off THEN !To blank or unblank crt
20145 SET DISPLAY MASK 15 !To keep track of CRT
20150 Off=0 !Turn all 4 planes on
20155 ELSE !Indicate CRT is ON
20160 SET DISPLAY MASK 0 !Turn all 4 planes off
20165 Off=1 !Indicate CRT is OFF
20170 END IF
20175 SUBEND ! Blank
20180 !
20185 Pre_bias:SUB Pre_bias(Setup) !To bias the mount for a time
20190 !Before the run
20195 OPTION BASE 1
20200 COM /Data/ Files$(20),Files$(16),Mount_id$(16)
20205 COM /Data/ V(3000,2),E(3000,2),F(3000,2),Me(100,2),Header(27)
20210 COM /Data/ Af(10,3),INTEGER Tp(3000)
20215 COM /Init_stats/ Tcv,Kcv,Enr,Snr,Volts(100),INTEGER Mode,Lss
20220 COM /Stats_2/ R,Prob,INTEGER Nruns
20225 COM /Screen_update2/ Avg,Sd
20230 COM /Prbias/ On_dur !Keep track of previous setting
20235 !
20240 Sys_prt=VAL(SYSTEM$( "SYSTEM PRIORITY" )) !Determine system priority
20245 Lcl_prt=Sys_prt+1 !Set local priority 1 higher for ON KEY
20250 CLEAR SCREEN !
20255 KEY LABELS OFF !Turn off user soft key labels
20260 !
20265 IF Setup THEN !To set up defaults
20270 IF Header(19) THEN On_dur=1 !Default, zero flag ON
20275 IF NOT Header(19) THEN On_dur=0 !Default, zero flag OFF
20280 END IF
20285 Cycle_time=Header(11) !Measurement interval
20290 Na=Lss !No. of points to use in stability test

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20295 !
20300 GOSUB Print
20305 !
20310 IF Setup THEN !For setup
20315 ON KEY 0 LABEL " Continue ",Lcl_prt GOTO Exit
20320 ON KEY 1 LABEL " Chng ON time ",Lcl_prt GOSUB Change_on
20325 FOR N=2 TO 9
20330 ON KEY N LABEL " " GOTO Top1
20335 NEXT N
20340 ELSE !For measurement
20345 ON KEY 0 LABEL " Start meas ",Lcl_prt GOTO Bailout
20350 FOR N=1 TO 8
20355 ON KEY N LABEL " " GOTO Top2
20360 NEXT N
20365 ON KEY 9 LABEL " BLANK CRT ",Lcl_prt CALL Blank !To blank CRT
20370 END IF
20375 !
20380 KEY LABELS ON
20385 IF Setup THEN
20390 Top1:LOOP !wait for input
20395 END LOOP
20400 ELSE
20405 Start$=TIME$(TIMEDATE) !Start time now
20410 GOSUB Calc
20415 IF On_dur>0 THEN !If On_dur=0 skip this
20420 CALL Dc(1,2) !Turn on the dc bias
20425 ON DELAY On_dur*3600,Lcl_prt GOSUB Dc_off !Turn off bias after delay
20430 ELSE
20435 GOSUB Dc_off !If NO bias be sure dc off
20440 END IF
20445 Top2:LOOP !Wait for interrupts
20450 Ts=TIME$(TIMEDATE) !Get the time
20455 Ts=Ts-[1,2]&Ts[4,5] !Format to compare with Stp$
20460 DISP "Pre-bias off: ",Stp1$," Present time: ",Ts
20465 IF Stable THEN Exit1 !finished
20470 END LOOP
20475 END IF
20480 !
20485 Calc: !Calculations
20490 Stp1$=TIME$(TIME(Start$)+On_dur*3600) !Time to shut off bias
20495 Stp1$=Stp1$[1,5]&"00" !Eliminate seconds
20500 Stp1$=Stp1$[1,2]&Stp1$[4,5] !Convert
20505 RETURN
20510 !
20515 Change_on: !To change duration
20520 KEY LABELS OFF
20525 INPUT "New ON time in hours? ",On_dur
20530 GOSUB Print
20535 KEY LABELS ON
20540 RETURN
20545 !
20550 Dc_off: !Turn off the dc bias
20555 CALL Dc(0,2)
20560 ON CYCLE Cycle_time,Lcl_prt GOSUB E0_meas !Turn on meas interrupt
20565 RETURN
20570 !
20575 E0_meas: !To determine E0
20580 CALL Dnmv(Nread) !Read nanovoltmeter (thermopile)
20585 Avg1=Avg !Save avg from previous meas
20590 CALL Stats(Na,Nread,Stable) !Check for stability of thermopile
20595 IF Stable THEN
20600 Nruns=0 !Reset some stats variables
20605 R=0 !Reset stat
20610 Prob=0 !Reset stat
20615 IF ABS(Nread)<1.E-6 THEN !If less than 1 uV, the bias is off
20620 Header(15)=Avg1 !Put E0 in Header (Avg=E0)
20625 IF NOT Header(19) THEN !No zero correction, then

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```

20630 Stable=0
20635 CALL Dc(1,2)
20640 END IF
20645 END IF
20650 END IF
20655 RETURN
20660 !
20665 Print:
20670 PRINT TABXY(27,4)," MOUNT PRE-BIAS "
20675 PRINT TABXY(27,6),"DC Bias ON For: ",On_dur," hrs. "
20680 RETURN
20685 !
20690 Bailout:
20695 IF Header(19) THEN CALL Dc(0,2)!Be sure bias is off if zero correction
20700 Exit1:
20705 OFF DELAY
20710 OFF CYCLE
20715 Exit:
20720 SUBEND !Pre_bias
20725 !
20730 Re_set:SUB Re_set
20735 OPTION BASE 1
20740 COM /Data/ Dfile$(20),File1$(16),Mount_id$(16)
20745 COM /Data/ V(3000,2),F(500,2),Ne(100,2),Header(27)
20750 COM /Data/ Af(10,3),INTEGER Tp(3000)
20755 COM /Init stats/ Tcv,Rcv,Bnr,Sdvr,Volts(100),INTEGER Mode,Lss
20760 COM /Screen update/ Count,Cftime,Freq,Pwr
20765 COM /Screen update2/ Avg,Sd
20770 COM /Stats_2/ R,Prob,INTEGER Nruns
20775 Dfile$="" !Clear data file name
20780 MAT V= (0) !Clear old data
20785 MAT B= (0)
20790 MAT F= (0)
20795 MAT Ne= (0)
20800 Count=0
20805 Header(9)=2400
20810
20815
20820 Lss=18
20825 Tcv=-2.5
20830 Rcv=.25
20835 Bnr=(2.0*Lss-1.0)/3.0
20840 Sdvr=SQR((16.0*Lss-29.0)/90.0)
20845 Mode=1
20850 R=0
20855 Prob=0
20860 Nruns=0
20865 Avg=0
20870 Sd=0
20875 Pwr=0
20880 !
20885 SUBEND !Re_set
20890 !
20895 Random_f:SUB Random_f
20900 OPTION BASE 1
20905 COM /Data/ Dfile$(20),File1$(16),Mount_id$(16)
20910 COM /Data/ V(3000,2),F(500,2),Ne(100,2),Header(27)
20915 COM /Data/ Af(10,3),INTEGER Tp(3000)
20920 !
20925 INTEGER Nr,Nol
20930 Nol=Header(5)
20935 !
20940 DIM Rm(50)
20945 DIM Rv(50)
20950 !
20955 RANDOMIZE
20960 FOR Nr=1 TO 50

!not finished and
!turn bias back on & wait for stability

Stable=0
CALL Dc(1,2)
END IF
END IF
END IF
RETURN
!
Print:
PRINT TABXY(27,4)," MOUNT PRE-BIAS "
PRINT TABXY(27,6),"DC Bias ON For: ",On_dur," hrs. "
RETURN
!
Bailout:
IF Header(19) THEN CALL Dc(0,2)!Be sure bias is off if zero correction
Exit1:
OFF DELAY
OFF CYCLE
Exit:
SUBEND !Pre_bias
!
Re_set:SUB Re_set
OPTION BASE 1
COM /Data/ Dfile$(20),File1$(16),Mount_id$(16)
COM /Data/ V(3000,2),F(500,2),Ne(100,2),Header(27)
COM /Data/ Af(10,3),INTEGER Tp(3000)
COM /Init stats/ Tcv,Rcv,Bnr,Sdvr,Volts(100),INTEGER Mode,Lss
COM /Screen update/ Count,Cftime,Freq,Pwr
COM /Screen update2/ Avg,Sd
COM /Stats_2/ R,Prob,INTEGER Nruns
Dfile$="" !Clear data file name
MAT V= (0) !Clear old data
MAT B= (0)
MAT F= (0)
MAT Ne= (0)
Count=0
Header(9)=2400
!
Lss=18
Tcv=-2.5
Rcv=.25
Bnr=(2.0*Lss-1.0)/3.0
Sdvr=SQR((16.0*Lss-29.0)/90.0)
Mode=1
R=0
Prob=0
Nruns=0
Avg=0
Sd=0
Pwr=0
!
SUBEND !Re_set
!
Random_f:SUB Random_f
OPTION BASE 1
COM /Data/ Dfile$(20),File1$(16),Mount_id$(16)
COM /Data/ V(3000,2),F(500,2),Ne(100,2),Header(27)
COM /Data/ Af(10,3),INTEGER Tp(3000)
!
INTEGER Nr,Nol
Nol=Header(5)
!
DIM Rm(50)
DIM Rv(50)
!
RANDOMIZE
FOR Nr=1 TO 50

```


APPENDIX E. Calibration Report

U.S. DEPARTMENT OF COMMERCE
NATIONAL INSTITUTE OF STANDARDS AND TECHNOLOGY
ELECTRONICS AND ELECTRICAL ENGINEERING LABORATORY
Boulder, Colorado

REPORT OF CALIBRATION

COAXIAL THERMISTOR MOUNT
NIST Model CN, Serial No. 05

Submitted by:

Customer's Name
Customer's Address
Customer's City, State and Zip

The measurements were performed under ambient environmental conditions of approximately 23°C and 40 percent relative humidity. The uncertainty of the calibration frequency is 1 ppm. The thermistor mount is operated at its designated resistance and is allowed to attain thermal equilibrium before beginning the test.

Effective efficiency η_e is defined as the ratio of the bolometrically substituted dc power in the thermistor mount to the net rf or microwave power delivered to the thermistor mount.

The effective efficiency of the thermistor mount was measured using the NIST automated coaxial microcalorimeter. Two connect-disconnect measurements were made in the microcalorimeter. On the first connect, measurements were made at five test frequencies. The frequencies are 0.1, 3, 10, 15 and 18 GHz. On the second connect the measurements at the five test frequencies were repeated. The results of the second series were compared with the first and found to agree to better than ± 0.1 percent. Then with the device still connected, the measurements were done at the full set of desired frequencies and these results are reported in Table 1. All the measurements were made at a power of 10 mW. Detailed descriptions of the calibration procedure, the system hardware, and the uncertainty evaluation process are found in references [1 - 3].

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The uncertainties associated with the measurement of η_e are grouped in two categories according to the method used to estimate their numerical values [4]. The Type A evaluations of standard uncertainty are based on a statistical analysis of measurement results. The Type B evaluations of standard uncertainty are based on other methods. The standard uncertainties obtained by either the Type A or the Type B evaluations are expressed as a standard deviation.

The Type A evaluation of standard uncertainty in the measurement process is based on repeated measurements of another identical Model CN used as a check standard. The random effects are due to voltmeter resolutions, connector nonrepeatability, long term system variations, and system noise. This standard uncertainty is estimated to be 0.032 percent, independent of frequency. The estimate is subject to change in the future as additional measurements are made on the check standard.

The Type B evaluation accounts for uncertainties in the microcalorimeter correction factor and the associated measurement instrumentation. These estimates of standard uncertainty are based on measurement results and manufacturer's instrument specifications.

A combined standard uncertainty is calculated as the RSS (square root of the sum of the squares) combination of all the uncertainty components from both categories. The expanded uncertainty given in Table 1 is obtained by multiplying the combined standard uncertainty by a coverage factor of 2 and can be calculated using the equation,

$$U = 4.46 \times 10^{-4} f^2 + 5.34 \times 10^{-3} f + 0.180,$$

where U is the uncertainty in percent and f is the frequency in GHz.

For the Director,
National Institute of
Standards and Technology

Approved by:

Robert M. Judish, Group Leader
Microwave Metrology Group
Electromagnetic Fields Division

Fred R. Clague
(303) 497-5778

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[1] Fred R. Clague, and Paul G. Voris, "Coaxial reference standard for microwave power," NIST Technical Note 1357, 1993. (U.S. Government Printing Office, Washington DC 20402-9325 or NTIS, Springfield, VA 22161).

[2] Fred R. Clague, "Microcalorimeter for 7 mm coaxial transmission line," NIST Technical Note 1358, 1993. (U.S. Government Printing Office, Washington DC, 20402-9325 or NTIS, Springfield, VA 22161).

[3] Fred R. Clague, "A calibration service for coaxial reference standards for microwave power," NIST Technical Note 1374, May 1995. (U. S. Government Printing Office, Washington DC 20402-9325 or NTIS, Springfield, VA 22161).

[4] Barry N. Taylor and Chris E. Kuyatt, "Guidelines for evaluating and expressing the uncertainty of NIST measurement results," NIST Technical Note 1297, 1993. (U.S. Government Printing Office, Washington DC 20402-9325 or NTIS, Springfield, VA 22161).

Coaxial Thermistor Mount
Model CN, Serial No. 05

Table 1.

Frequency (GHz)	Effective Efficiency	Type B Uncertainty (Percent)	Expanded Uncertainty (Percent)
0.05	0.9922	0.11	0.21
0.10	0.9951	0.13	0.23
0.15	0.9957	0.14	0.24
0.20	0.9959	0.16	0.26
0.25	0.9959	0.17	0.27
0.30	0.9959	0.18	0.28
0.35	0.9959	0.19	0.29
0.40	0.9958	0.20	0.30
0.45	0.9957	0.21	0.31
0.50	0.9956	0.22	0.32
0.55	0.9955	0.22	0.32
0.60	0.9953	0.23	0.33
0.65	0.9951	0.23	0.33
0.70	0.9949	0.24	0.34
0.75	0.9947	0.25	0.35
0.80	0.9942	0.25	0.35
0.85	0.9936	0.25	0.35
0.90	0.9926	0.25	0.35
0.95	0.9916	0.25	0.35
1.00	0.9905	0.25	0.35
1.05	0.9895	0.25	0.35
1.10	0.9889	0.25	0.35
1.15	0.9889	0.25	0.35
1.20	0.9892	0.25	0.35
1.25	0.9896	0.25	0.35
1.30	0.9900	0.25	0.35
1.35	0.9903	0.25	0.35
1.40	0.9906	0.25	0.35
1.45	0.9907	0.25	0.35
1.50	0.9907	0.25	0.35
1.55	0.9907	0.25	0.35
1.60	0.9906	0.25	0.35
1.65	0.9903	0.25	0.35
1.70	0.9901	0.25	0.35
1.75	0.9898	0.25	0.35
1.80	0.9894	0.25	0.35

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Table 1. (con't)

Frequency (GHz)	Effective Efficiency	Type B Uncertainty (Percent)	Expanded Uncertainty (Percent)
1.85	0.9889	0.25	0.35
1.90	0.9884	0.25	0.35
1.95	0.9879	0.25	0.35
2.00	0.9873	0.25	0.35
2.10	0.9863	0.25	0.35
2.20	0.9855	0.25	0.35
2.30	0.9851	0.25	0.35
2.40	0.9849	0.25	0.35
2.50	0.9849	0.25	0.35
2.60	0.9851	0.25	0.35
2.70	0.9852	0.25	0.35
2.80	0.9854	0.25	0.35
2.90	0.9855	0.25	0.35
3.00	0.9856	0.25	0.35
3.10	0.9855	0.25	0.35
3.20	0.9855	0.25	0.35
3.30	0.9853	0.25	0.35
3.40	0.9851	0.25	0.35
3.50	0.9849	0.25	0.35
3.60	0.9847	0.25	0.35
3.70	0.9845	0.25	0.35
3.80	0.9843	0.25	0.35
3.90	0.9840	0.25	0.35
4.00	0.9837	0.25	0.35
4.20	0.9831	0.26	0.36
4.40	0.9826	0.26	0.36
4.60	0.9821	0.26	0.36
4.80	0.9816	0.26	0.36
5.00	0.9811	0.26	0.36
5.20	0.9807	0.26	0.36
5.40	0.9802	0.26	0.36
5.60	0.9798	0.26	0.36
5.80	0.9793	0.26	0.36
6.00	0.9789	0.26	0.36
6.20	0.9785	0.26	0.36
6.40	0.9780	0.26	0.36

Coaxial Thermistor Mount
Model CN, Serial No. 05

Table 1. (con't)

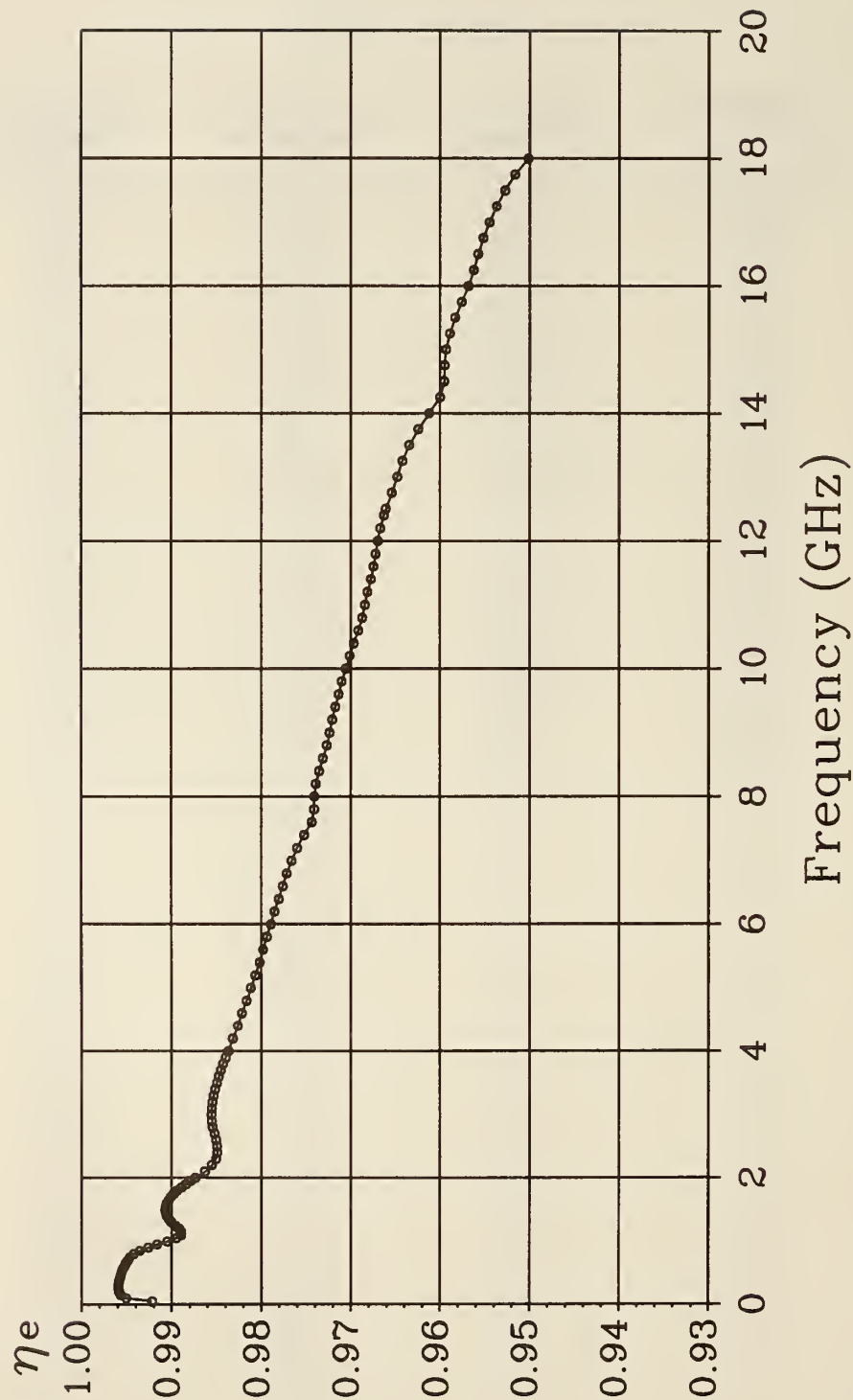
Frequency (GHz)	Effective Efficiency	Type B Uncertainty (Percent)	Expanded Uncertainty (Percent)
6.60	0.9776	0.26	0.36
6.80	0.9771	0.26	0.36
7.00	0.9766	0.26	0.36
7.20	0.9760	0.26	0.36
7.40	0.9752	0.26	0.36
7.60	0.9743	0.26	0.36
7.80	0.9741	0.26	0.36
8.00	0.9741	0.26	0.36
8.20	0.9739	0.26	0.36
8.40	0.9735	0.26	0.36
8.60	0.9731	0.26	0.36
8.80	0.9727	0.26	0.36
9.00	0.9724	0.26	0.36
9.20	0.9721	0.26	0.36
9.40	0.9717	0.26	0.36
9.60	0.9713	0.26	0.36
9.80	0.9710	0.26	0.36
10.00	0.9705	0.27	0.36
10.20	0.9701	0.27	0.37
10.40	0.9697	0.27	0.37
10.60	0.9691	0.27	0.37
10.80	0.9687	0.27	0.37
11.00	0.9684	0.27	0.37
11.20	0.9681	0.27	0.37
11.40	0.9677	0.27	0.37
11.60	0.9674	0.27	0.37
11.80	0.9672	0.27	0.37
12.00	0.9670	0.27	0.37
12.20	0.9667	0.27	0.37
12.40	0.9663	0.27	0.37
12.50	0.9661	0.27	0.37
12.75	0.9654	0.27	0.37
13.00	0.9648	0.27	0.37
13.25	0.9642	0.27	0.37
13.50	0.9634	0.27	0.37
13.75	0.9624	0.27	0.37

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Table 1. (con't)

Frequency (GHz)	Effective Efficiency	Type B Uncertainty (Percent)	Expanded Uncertainty (Percent)
14.00	0.9612	0.27	0.37
14.25	0.9600	0.27	0.37
14.50	0.9595	0.27	0.37
14.75	0.9595	0.27	0.37
15.00	0.9593	0.27	0.37
15.25	0.9589	0.27	0.37
15.50	0.9583	0.27	0.37
15.75	0.9576	0.27	0.37
16.00	0.9568	0.28	0.38
16.25	0.9562	0.28	0.38
16.50	0.9557	0.28	0.38
16.75	0.9552	0.28	0.38
17.00	0.9545	0.28	0.38
17.25	0.9537	0.28	0.38
17.50	0.9527	0.28	0.38
17.75	0.9516	0.28	0.38
18.00	0.9501	0.28	0.38

Coaxial Power Standard Microcalorimeter Measurements



APPENDIX F. Instrument Identification

Table F1 identifies the commercial instruments used in the automated calibration system at the time this report was prepared. Items are listed as shown in figure 4.1. This identification does not imply recommendation or endorsement by NIST, nor does it imply that the identified items are necessarily the best available for the purpose.

Table F.1. Commercial instrument identification.

Item	Manufacturer	Model
1. Switch/Control Unit	Hewlett-Packard	3488A
2. Digital Voltmeter	Hewlett-Packard	3457A
3. Nanovoltmeter	Keithley	181
4. NBS Type IV Power Meter	-	-
5. DC Voltage Reference	Data Precision	8200
6. Microwave Locking Counter	EIP	578
7. Microwave Source	EIP	931
8. NBS Type II Power Leveler	-	-
9. Source and Meter Control Unit	-	-
Microwave Switch (See figure 4.2)	Hewlett Packard	P/N 33102A

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