

NATIONAL BUREAU OF STANDARDS REPORT

9098

A THEOREM ON OPTIMAL LOCATIONS

by

A.J. Goldman and P.R. Meyers

Technical Report

to

U.S. Post Office Department

and

Office of High Speed Ground Transportation

Department of Commerce



U.S. DEPARTMENT OF COMMERCE
NATIONAL BUREAU OF STANDARDS

THE NATIONAL BUREAU OF STANDARDS

The National Bureau of Standards is a principal focal point in the Federal Government for assuring maximum application of the physical and engineering sciences to the advancement of technology in industry and commerce. Its responsibilities include development and maintenance of the national standards of measurement, and the provisions of means for making measurements consistent with those standards; determination of physical constants and properties of materials; development of methods for testing materials, mechanisms, and structures, and making such tests as may be necessary, particularly for government agencies; cooperation in the establishment of standard practices for incorporation in codes and specifications; advisory service to government agencies on scientific and technical problems; invention and development of devices to serve special needs of the Government; assistance to industry, business, and consumers in the development and acceptance of commercial standards and simplified trade practice recommendations; administration of programs in cooperation with United States business groups and standards organizations for the development of international standards of practice; and maintenance of a clearinghouse for the collection and dissemination of scientific, technical, and engineering information. The scope of the Bureau's activities is suggested in the following listing of its three Institutes and their organizational units.

Institute for Basic Standards. Applied Mathematics. Electricity. Metrology. Mechanics. Heat. Atomic Physics. Physical Chemistry. Laboratory Astrophysics.* Radiation Physics. Radio Standards Laboratory.* Radio Standards Physics; Radio Standards Engineering. Office of Standard Reference Data.

Institute for Materials Research. Analytical Chemistry. Polymers. Metallurgy. Inorganic Materials. Reactor Radiations. Cryogenics.* Materials Evaluation Laboratory. Office of Standard Reference Materials.

Institute for Applied Technology. Building Research. Information Technology. Performance Test Development. Electronic Instrumentation. Textile and Apparel Technology Center. Technical Analysis. Office of Weights and Measures. Office of Engineering Standards. Office of Invention and Innovation. Office of Technical Resources. Clearinghouse for Federal Scientific and Technical Information.**

*Located at Boulder, Colorado, 80301.

**Located at 5285 Port Royal Road, Springfield, Virginia, 22171.

NATIONAL BUREAU OF STANDARDS REPORT

NBS PROJECT

4235450
2050456

March 30, 1966

NBS REPORT

9098

A THEOREM ON OPTIMAL LOCATIONS

by

A.J. Goldman and P.R. Meyers

Operations Research Section

Applied Mathematics Division

For

U.S. Post Office Department

and

Office of High Speed Ground Transportation

Department of Commerce

IMPORTANT NOTICE

NATIONAL BUREAU OF STANDARDS
for use within the Government. Before
and review. For this reason, the report
whole or in part, is not authorized
Bureau of Standards, Washington, D.C.
the Report has been specifically prepared

Approved for public release by the
director of the National Institute of
Standards and Technology (NIST)
on October 9, 2015

Counting documents intended
to additional evaluation
of this Report, either in
ce of the Director, National
Government agency for which
for its own use.



U.S. DEPARTMENT OF COMMERCE

NATIONAL BUREAU OF STANDARDS

A THEOREM ON OPTIMAL LOCATION

A.J. Goldman and P.R. Meyers

National Bureau of Standards

ABSTRACT

The problem studied concerns the location of a facility (e.g. a mail-sorting installation or a transport terminal) so as to minimize the sum of transport costs for the "source"-to-facility and facility-to-"sink" flows. Movements are assumed to occur along least costly paths in a network of roads or other conduits. The only assumption on cost structure is that marginal cost is a non-increasing function of trip length, this function possibly changing from trip segment to trip segment. The distributions of sources and sinks along the roads can be arbitrary, as can the network topology. Under further mild hypotheses, it is shown that the search for an optimal facility location can be confined to endpoints of roads and interchanges between roads. A detailed study is made of a radially symmetric circular-disk model in which only radial and circumferential movement is permitted (each with a constant unit cost), and the "density" of sources and sinks drops exponentially as a function of distance from the center of the disk.

A THEOREM ON OPTIMAL LOCATION⁽¹⁾

by

A.J. Goldman and P.R. Meyers

National Bureau of Standards

1. INTRODUCTION

Suppose given a collection of "customers" for the services of a central facility (mail sorting installation, transport terminal, firehouse, library, school, food distribution point, etc.). The common feature of the class of applications we have in mind is that performance of the service involves the movement of something between the customer location and the central facility --- e.g. of mail from patrons to sorting installation and from sorting installation to recipients, or of travellers from initial origins to transport terminal, or from terminal to final destinations.

Thus each customer location can act either as a source of flow to the facility, or a sink of flow from the facility, or both. We can weight each source location according to the amount of flow emanating from it, and each sink location according to how much flow it receives, thus giving rise to two mass distributions, denoted μ (for the sources) and μ^* (for the sinks).

The flow is required to move along a least costly among the "allowable paths"; the latter will be called roads for concreteness, though interpretations as pipelines, pneumatic tubes or other types of conduit are equally in order. We use the notation equally in order.

$c(P, L)$ = cost of transporting⁽²⁾ one unit from source location P to facility location L ,

$c^*(L, P^*)$ = cost of transporting one unit from facility location L to sink location P^* .

Then the total transport cost, including both incoming (to the facility) and outgoing flow, is

$$f(L) = \sum_P c(P, L) \mu(P) + \sum_{P^*} c^*(L, P^*) \mu^*(P^*) . \quad (1)$$

(1) Supported by the Post Office Department and by the Department of Commerce's High Speed Ground Transportation Project. No official endorsement is implied.

(2) Transport costs are considered exclusive of the costs at the central facility of unloading, processing (servicing) and loading. These costs are assumed independent of the location of the facility.

The "optimal location problem" for a single facility can be defined, for present purposes, as that of choosing the facility's location L so as to minimize $f(L)$. It may be useful to "smear out" the representation of small customers to a continuous mass distribution, retaining some discrete mass-points or mass-curves as required to represent extra-large customers or concentrations of them. Thus (1) will be replaced by

$$f(L) = \int c(P, L) d\mu(P) + \int c^*(L, P^*) d\mu^*(P^*) . \quad (2)$$

In recent (unpublished) work⁽³⁾, C. Witzgall discussed a number of topics relating to this problem. As one of several concrete illustrative models, he considered the case of identical uniform distributions of sources and sinks over a circular disk. Only radial and circumferential movements were permitted, a situation suggestive of a city which has a radial web of major streets and is surrounded by a beltway. The two parameters of the model were both costs of transporting a unit over a unit distance, namely the costs for radial and for peripheral movements, which will be denoted c_r and c_p respectively. Witzgall showed that the condition for a peripheral location of the facility to be better than a central one is

$$c_p/c_r < 0.216 , \text{ or } c_p/c_r < 2/3\pi = 0.212 , \quad (3)$$

according as short-cuts through the center of town to a peripheral facility are or are not permitted.

No proof was given, however, that the optimum had to occur for one of these extreme cases (location at center or on circumference) rather than at an intermediate position along a radius. This certainly seemed plausible (and turned out to be true) for the simple disk model, but its main interest lay in the likelihood that it represented a special case of some general principle.

The present paper records our current understanding of this principle. As will be seen, it admits arbitrary mass distributions μ and μ^* , and road networks much more general than that of the disk model. The unit (per mile) transport cost along a road need not be constant; indeed, the critical assumption describing the principle's range of validity appears to be that transport cost along a road (per unit carried) is a concave function (perhaps differing from road to road) of the distance travelled. That is, long-haul costs no more per mile than does short-haul⁽⁴⁾.

(3) C. Witzgall, "Optimal Location of a Central Facility; Mathematical Models and Concepts," 1964.

(4) This statement about average costs should really be replaced by the corresponding one about marginal costs.

In the following Section 2, we formulate the present version of the principle as a theorem, which is then proved in Section 3. Some extensions are described in Section 4. Section 5 contains an analysis of a more general "circular disk" model with radial symmetry; advantage is taken of the theorem, in that the search for an optimal location for the central facility is confined to the center and periphery of the disk.

2. FORMULATION OF THEOREM

We consider two systems Σ and Σ^* of roads; the first carries the source-to-facility flow, and the second the flow from facility to sinks. Some roads, or segments of roads, may be common to Σ and Σ^* . The set of points covered by the roads of Σ will for simplicity be identified with the set of possible locations of sources⁽⁵⁾ (the distinction between $u > 0$ and $u=0$ implicitly sorting out the "actual" locations among the possible ones), and this point-set is assumed compact⁽⁶⁾; similarly for Σ^* and the possible locations of sinks. It is assumed that each possible source location is connected within Σ to each possible location of the facility, and similarly for the facility-to-sink flow.

Each road is taken to be a continuous rectifiable curve in the usual mathematical sense; this implies an orientation⁽⁷⁾, and a running "path length parameter" which increases from zero at the beginning of the road to some finite maximum value (the length of the road) at its end. Some roads may be closed curves, i.e. their beginning point and ending point coincide (as for a beltway).

As noted earlier, transport cost along any one road (per unit carried) is assumed a concave function of the road-length traversed, this function possibly differing from road to road. While this seems plausible when expressed as a comparison of long-haul per mile transport cost with that for short-haul (the former not exceeding the latter), it may introduce a bias into the choice between central or peripheral location for the facility. Flow from an outlying source to a central location may in its progress encounter successively more congested zones, and therefore successively higher per mile costs; our concavity hypothesis in effect assumes that this effect is at least counter-balanced by the economies of long-haul operations. On the other hand, the reverse holds true for flow from central facility to outlying sink. Roughly speaking, the bias is likely to be for or against a central location according as μ or μ^* is more concentrated about the "center" of the region under study.

(5) This evades any need to provide a more or less arbitrary description of how flow from off- Σ sources moves toward Σ . Such a description can be guided by reality for any specific application.

(6) The desire to encompass idealized models with infinitely many customers and roads and special points requires more technical mathematics than would be needed for discrete models. Readers unfamiliar with these concepts (e.g. compactness) can ignore them without serious loss.

(7) A bidirectional road can be represented as two oppositely oriented roads.

Certain special points on the roads of the two systems are distinguished. These are required to include the beginning and ending points of all roads which are not closed curves, and of all segments shared by any specific set of roads. (Thus the "focus" of a radial web of roads would be a special point.) They are also required to include all interchanges, i.e. points where two roads intersect and transition from one to the other is permitted. (For the simple disk model described earlier, this means that all points on the beltway are special.) The set of special points is assumed compact.

From this last assumption we see that an allowed location for the central facility is either a special point, or else⁽⁸⁾ lies on a road segment free of special points. In the first case the special point must be an interchange from a road of Σ to one of Σ^* , while in the second case the road segment must be common to a road of Σ and one of Σ^* . The set of allowed locations L is supposed compact; thus $f(L)$, if continuous, does actually attain a minimum value. The continuity of $f(L)$ is ensured by requiring $c(P,L)$ and $c^*(L,P^*)$ to be continuous.

As noted earlier, flow is assumed to move along a least costly of the allowed paths. More precisely, if $c(P,\alpha,L)$ is the transport cost for unit flow along the allowed route α in Σ from P to L , then

$$c(P,L) = \inf_{\alpha} c(P,\alpha,L) ; \quad (4)$$

similarly for $c^*(L,P^*)$.

The remaining assumption is that all flow, whether to or from the facility, must be routed so as to pass through at least one special point. This suggests viewing the special points as seats of some recording or check-in operation, or perhaps of consolidation and break-bulk operations. The hypothesis is automatically satisfied when the facility is itself at a special point. It is automatically satisfied for flow from or to a customer location on a road not containing the central facility, since such flow must pass through at least one interchange. Thus the assumption is restrictive only if the facility's location L is on a road segment free of special points except for its endpoints, and even then it requires "unnatural" routing only for the (presumably small) fraction of flow originating or terminating on that particular segment.

(8) The point is that an allowed location, if not itself a special point, cannot be a limit of special points.

THEOREM. Under the above hypotheses, at least one special point is an optimal location.

The important implication is that when seeking to determine an optimal location, one can simplify the task by restricting attention to special points. This may be useful not only in placing new facilities, but also in explaining historic patterns of location of "central places". In connection with this last remark, it should be noted that cities can be regarded (in part) as "service facilities" for the "customers" of their surrounding areas.

3. PROOF OF THEOREM

As observed above, the hypotheses of the theorem ensure the existence of at least one optimal location L_0 . We assume that L_0 is an ordinary (i.e., non-special) point, and prove the theorem by showing that this implies the existence of an optimal special point.

Because L_0 is ordinary and the set of special points is compact, L_0 must lie on some road segment σ_0 whose interior contains only ordinary points, and which lies both on at least one road of Σ and on at least one road of Σ^* . Consider the continuation of σ_0 through L_0 in one of the two possible directions. A "branch-point" may be reached at which σ_0 loses its identity because some road containing it diverges, or some new road portion merges with it; such a point is a special point. The beginning or end of a road may be encountered, or an interchange may be reached; again a special point must be present. If none of these occurs, then we must eventually return to L_0 ; in this case σ_0 is a closed curve consisting of ordinary points only. Since this curve has no interchanges, and all customer locations must be connectable with L_0 , it follows that all possible customer locations lie on σ_0 , i.e. the points of all roads lie on σ_0 . This is impossible because all flow must pass through a special point, whereas σ_0 lacks special points. The conclusion is that the maximal continuation of σ_0 through L_0 in either direction ends in a special point.

From now on we reserve the symbol σ_0 for the maximal segment of ordinary points containing L_0 , including its (special) end-points E_0 and E_1 . (The possibility of a closed curve with $E_0 = E_1$ as its sole special point offers no difficulty.) The points of σ_0 will be denoted $L(\lambda)$, where λ is the arc-length parameter along σ_0 measured from E_0 , i.e. $L(0) = E_0$ and $L(\lambda_{\max}) = E_1$, where

$$\lambda_{\max} = \text{length of } \sigma_0.$$

It will be shown that either E_0 or E_1 is optimal. This will be done by proving that the function

$$g(\lambda) = f(L(\lambda)) , \quad (5)$$

defined for $0 \leq \lambda \leq \lambda_{\max}$, attains its minimum at an endpoint of this interval. Since L_0 lies on σ_0 , we have

$$\min_L f(L) \leq \min_{\lambda} g(\lambda) = \min_{L \in \sigma_0} f(L) \leq f(L_0) = \min_L f(L) ,$$

from which the optimality of E_0 or E_1 will follow.

Let Q be the set of all special points on all roads of Σ which contain σ_0 , and assume $0 < \lambda < \lambda_{\max}$. Consider any possible location P . If the flow from P to $L(\lambda)$ would move wholly along a single road of Σ , then the last special point it would encounter is either E_0 or E_1 , which both lie in Q . If not, the flow enters the last road it traverses at some interchange which is a point of Q . So eq(4) becomes

$$c(P, L(\lambda)) = \inf_{q \in Q} \{c(P, q) + c(q, L(\lambda))\} . \quad (6)$$

We will use the abbreviations

$$c_q(\lambda) = c(q, L(\lambda)) ,$$

$$\bar{c}_q(\lambda, P) = c(P, q) + c_q(\lambda) .$$

The appearance of $c_q(\lambda)$ in (6) refers to movement along a single road, and so by hypothesis this function is concave in λ . That is, for each triple $(\lambda^-, \lambda^+, t)$ with

$$0 < \lambda^- < \lambda^+ < \lambda_{\max} , \quad 0 < t < 1 , \quad (7)$$

the equality

$$c_q(t\lambda^- + (1-t)\lambda^+) \geq tc_q(\lambda^-) + (1-t)c_q(\lambda^+) \quad (8)$$

is valid. Since $c(P, q)$ is independent of λ , it follows that for each $q \in Q$ and each P , $\bar{c}_q(\lambda, P)$ is concave in λ .

This will be used to prove⁽⁹⁾ that for each P ,

$$c(P, L(\lambda)) = \inf \{ \bar{c}_q(\lambda, P) : q \in Q \} \quad (9)$$

is concave in λ . Let $(\lambda^-, \lambda^+, t)$ be as in (7). For any $\delta > 0$, there is a $q \in Q$ such that

$$c(P, L(t\lambda^- + (1-t)\lambda^+)) + \delta > \bar{c}_q(t\lambda^- + (1-t)\lambda^+, P). \quad (10)$$

From (8) and (9), we have

$$\bar{c}_q(t\lambda^- + (1-t)\lambda^+, P) \geq tc(P, L(\lambda^-)) + (1-t)c(P, L(\lambda^+)). \quad (11)$$

Combining (10) and (11), and recalling that δ was arbitrary, we have

$$c(P, L(t\lambda^- + (1-t)\lambda^+)) \geq tc(P, L(\lambda^-)) + (1-t)c(P, L(\lambda^+)), \quad (12)$$

and so (by definition) $c(P, L(\lambda))$ is concave in λ .

(9) For completeness, the proofs of known properties of concave functions are incorporated.

Inequality (12) can be rewritten as

$$c(P, L(t\lambda^- + (1-t)\lambda^+)) - tc(P, L(\lambda^-)) - (1-t) c(P, L(\lambda^+)) \geq 0 . \quad (13)$$

A non-negative integrand yields a non-negative integral with respect to any mass distribution μ ; applying this to (13), we obtain

$$\begin{aligned} \int c(P, L(t\lambda^- + (1-t)\lambda^+)) d\mu(P) &\geq t \int c(P, L(\lambda^-)) d\mu(P) \\ &\quad + (1-t) \int c(P, L(\lambda^+)) d\mu(P) . \end{aligned}$$

This is simply the assertion that the function

$$g_1(\lambda) = \int c(P, L(\lambda)) d\mu(P)$$

is concave in λ . By eqs(2) and (5), $g(\lambda)$ is the sum of $g_1(\lambda)$ and a similar term for the facility-to-sinks flow. The latter can be proved concave by similar arguments, and so $g(\lambda)$ is itself concave. Thus, for $(\lambda^-, \lambda^+, t)$ as in (7),

$$\begin{aligned} g(t\lambda^- + (1-t)\lambda^+) &\geq tg(\lambda^-) + (1-t)g(\lambda^+) \\ &\geq t \min(g(\lambda^-), g(\lambda^+)) + (1-t) \min(g(\lambda^-), g(\lambda^+)) \\ &= \min(g(\lambda^-), g(\lambda^+)) . \end{aligned}$$

That is

$$g(\lambda) \geq \min(g(\lambda^-), g(\lambda^+)) \quad \text{for } \lambda^- \leq \lambda \leq \lambda^+ .$$

By continuity this remains true for $\lambda^- = 0$ and $\lambda^+ = \lambda_{\max}$ so that, as desired,

$$\min \{g(\lambda) : 0 \leq \lambda \leq \lambda_{\max}\} = \min \{g(0), g(\lambda_{\max})\} ,$$

from which it follows as shown above that E_0 or E_1 is an optimal location.

4. SOME EXTENSIONS

One extension of the theorem arises if its hypotheses are weakened to require concavity of transport costs along only some roads and road segments. The preceding proof can easily be adapted to establish the existence of at least one optimal location which is not an ordinary point on any of those roads and segments for which concavity is postulated.

The description of a second extension requires another definition. A function $h(\lambda)$, defined (say) on an interval $0 \leq \lambda \leq \lambda_{\max}$, is called strictly concave in λ if for all $(\lambda^-, \lambda^+, t)$ obeying (7), the strict inequality

$$h(t\lambda^- + (1-t)\lambda^+) > th(\lambda^-) + (1-t)h(\lambda^+)$$

holds.

If $g(\lambda)$ is strictly concave in λ , the last part of the preceding proof can be modified to show that the minimum of $g(\lambda)$ occurs only for $\lambda = 0$ or $\lambda = \lambda_{\max}$. It would follow that only special points can be optimal.

One might hope that the strict concavity of $g(\lambda)$ could be inferred if the hypothesis of concavity of transport costs along any road were strengthened to strict concavity. This will not always work. The functions $\bar{c}_q(\lambda, P)$ will each be strictly concave, but the infimum of an infinite collection of strictly concave functions need not be strictly concave (it can for example be linear), so that "strictness" can be lost in the transition to the function $c(P, L(\lambda))$ defined in (9).

It is however true that the minimum of a finite collection of strictly concave functions is strictly concave. If u is discrete, then the passage from $c(P, L(\lambda))$ to $g_1(\lambda)$ also preserves strict concavity. So for discrete models, only special points can be optimal if transport costs are strictly concave.

5. APPLICATION TO A CIRCULAR DISC MODEL

In this section we illustrate the previous material by examining in some detail a generalization of the circular disc model mentioned in Section 1. The mass distributions μ (for sources) and μ^* (for sinks) are assumed to coincide, as are the road systems Σ and Σ^* and the associated transport costs. Thus, for any location of the facility, the cost of the sources-to-facility flow will be exactly half that of the total (two-way) flow.

Polar coordinates (r, θ) , with origin at the center of the disc, will be employed. The disc itself is characterized by $0 \leq r \leq 1$, i.e. its radius is (for simplicity) chosen as the unit of length. The mass density is assumed to fall off exponentially from the disc-center in a radially symmetric way ⁽¹⁰⁾, i.e.

$$d\mu(r, \theta) = K \exp(-ar) r dr d\theta$$

where K is a normalization constant, $r dr d\theta$ is the element of area in polar coordinates, and $a > 0$ is a parameter representing the degree of central concentration of the distribution. The limiting case $a=0$ corresponds to the uniform distribution studied by Witzgall (op cit), and our study generalizes his precisely in permitting $a > 0$.

The system of available roads is taken to consist of the periphery of the disk and (initially) all of its radii, regarded as bidirectional.

(10) This assumption is a fairly common one. See for example H.K. Weiss, The Distribution of Urban Population and an Application to a Servicing Problem, Operations Research 9 (1961), pp. 860-874.

The intersection of each radial road with the periphery is taken as a transfer point and also as an end-point of that road, the other end-point being the center of the disk. Unit costs of peripheral and radial travel are assumed to be constants (c_p and c_r , respectively); thus the transport cost along any road is a linear (hence, concave) function of distance travelled. It follows that our general principle indeed applies, to show that the optimal location for the facility is either at the center of the disc or on the periphery. By symmetry, we need consider only one among the peripheral locations, and we choose the one given by $\theta=0$.

First suppose the facility is located at the center of the disc. Then the least costly path from any point to the facility consists of a single radial segment, and so the total cost (for the two-way flow) is

$$\begin{aligned} f_c &= 2 \int_0^1 \int_{-\pi}^{\pi} c_r r d\mu(r, \theta) \\ &= 4 \pi K c_r \int_0^1 r^2 \exp(-ar) dr \\ &= 4 \pi K c_r a^{-3} [2 - (2 + 2a + a^2) \exp(-a)] . \end{aligned}$$

Second, suppose the facility is located on the periphery, at the point given by $\theta=0$. There are really two cases to consider, depending on whether or not short-cuts through the central district are permitted, i.e. whether or not the center of the disc is assumed to be an interchange point between distinct radial roads. We assume for the moment that such short-cuts are forbidden, so that the least costly path from any point consists of a radial trip to the periphery, followed by a trip to the

facility along a minor arc of the periphery. The corresponding total cost is

$$\begin{aligned}
 f_p &= 2 \int_0^1 \int_{-\pi}^{\pi} [c_r(1-r) + c_p |\theta|] d\mu(r, \theta) \\
 &= 4 Kc_r \int_0^1 (1-r)r \exp(-ar) dr \\
 &\quad + 4Kc_p \int_0^1 r \exp(-ar) \int_0^{\pi} \theta d\theta dr \\
 &= 4\pi Kc_r a^{-3} [(a-2) + (a+2) \exp(-a)] \\
 &\quad + 2\pi^2 Kc_p a^{-2} [1-(1+a) \exp(-a)] .
 \end{aligned}$$

Our objective is to determine the "critical value" $\tau^* = \tau^*(a)$,
of the ratio

$$\tau = c_p / c_r , \quad (14)$$

which divides the cases for which the peripheral location of the facility is optimal from those for which the central location is optimal, i.e.

$$f_p < f_c \quad \text{if} \quad \tau < \tau^*(a) ,$$

$$f_p > f_c \quad \text{if} \quad \tau > \tau^*(a) .$$

Thus τ^* can be found by equating f_p to f_c , and solving for τ .

The result (for the case of forbidden short-cuts) is

$$\tau^*(a) = (2/\pi) [(4-a)\exp(a) - (4+3a+a^2)] / a[\exp(a) - (1+a)] , \quad (15)$$

which for small a has the form

$$\tau^*(a) = (2/\pi)[1+o(a)]/[3+a+o(a)] .$$

Thus $\tau^*(0) = 2/3\pi = 0.212^+$, in conformance with Witzgall's result for the uniform distribution.

Increasing values of a correspond to greater central concentration, and therefore to a greater tendency for the central location to be optimal. We should therefore expect $\tau^*(a)$ to be a decreasing function. This can indeed be verified analytically (details omitted), and is also indicated by the second column of Table 1. It is especially interesting to note that $\tau^*(a)$ turns negative at roughly $a=2.7$, representing a degree of concentration at (and beyond) which subsidization of circumferential travel would be required to overcome the cost advantage of the central location.

Next we assume that short-cuts through the center are permitted. It is easily seen that the least-cost path from any point (r,θ) to the facility is either the same one assumed in the previous discussion, or the one involving a radial trip to the center followed by a radial trip along the ray $\theta=0$ to the periphery. The former is less costly than the latter if and only if

$$c_r(1-r) + c_p |\theta| < c_r (1+r) ,$$

i.e. if and only if

TABLE 1: Values^(*) of $\tau^*(a)$

a	$\tau^*(a)$	
	A. Short cuts through center forbidden	B. Short cuts through center permitted
0.05	.208	.214
0.1	.205	.210
0.2	.198	.202
0.3	.191	.194
0.4	.183	.186
0.5	.176	.179
0.6	.168	.171
0.7	.161	.163
0.8	.153	.155
0.9	.145	.147
1.0	.137	.139
1.2	.121	.123
1.4	.105	.106
1.6	.089	.090
1.8	.073	.073
2.0	.056	.057
2.3	.032	.032
2.6	.007	.007
2.7	-.001	.000

(*) Recall that $\tau^*(a)$ is the value of c_p/c_r for which the transport costs associated with peripheral and central facility locations are equal.

where

$$F(x,a) = ax + x(4+3a+a^2)\exp(-a) - x^2(1+a)\exp(-a) \\ - [6-6\exp(-x) - 2x\exp(-x)] . \quad (18)$$

Before considering this equation in detail, we will dispose of the remaining case $\tau > 2/\pi$, corresponding to $x > a$. In this case the short-cut fails to be best if and only if

$$\tau|\theta|/2 \leq r \leq 1 ,$$

which can only occur for $|\theta| \leq 2/\tau$. Thus the total cost is

$$\begin{aligned} f_p &= 2 \int_0^{2/\tau} \int_0^{\tau\theta/2} c_r(1+r) d\mu(r,\theta) \\ &+ 2 \int_0^{2/\tau} \int_{\tau\theta/2}^1 [c_r(1-r) + c_p\theta] d\mu(r,\theta) \\ &+ 2 \int_{2/\tau}^{\pi} \int_0^1 c_r(1+r) d\mu(r,\theta) \\ &= 2 K c_r \left\{ \int_0^{\pi} \int_0^1 r \exp(-ar) dr d\theta \right. \\ &+ \int_0^{2/\tau} \int_0^{\tau\theta/2} r^2 \exp(-ar) dr d\theta \\ &+ \int_0^{2/\tau} \int_{\tau\theta/2}^1 (\tau\theta r - r^2) \exp(-ar) dr d\theta \\ &\left. + \int_{2/\tau}^{\pi} \int_0^1 r^2 \exp(-ar) dr d\theta \right\} . \end{aligned}$$

We can also write

$$\begin{aligned}
 f_c = 2 Kc_r \{ & \int_0^{2/\tau} \int_0^{\tau\theta/2} r^2 \exp(-ar) dr d\theta \\
 & + \int_0^{2/\tau} \int_{\tau\theta/2}^1 r^2 \exp(-ar) dr d\theta \\
 & + \int_{2/\tau}^{\pi} \int_0^1 r^2 \exp(-ar) dr d\theta \} ,
 \end{aligned}$$

and so

$$\begin{aligned}
 (f_p - f_c)/2Kc_r = & \int_0^{\pi} \int_0^1 r \exp(-ar) dr d\theta \\
 & + \int_0^{2/\tau} \int_{\tau\theta/2}^1 (\tau\theta r - 2r^2) \exp(-ar) dr d\theta \\
 & - \int_0^1 \int_0^{\pi} r \exp(-ar) d\theta dr \\
 & + \int_0^1 \int_0^{2r/\tau} (\tau\theta r - 2r^2) \exp(-ar) d\theta dr \\
 = & \int_0^1 \left\{ \pi + \int_0^{2r/\tau} (\tau\theta - 2r) d\theta \right\} r \exp(-ar) dr \\
 = & \int_0^1 \left\{ \pi - 2r^2/\tau \right\} r \exp(-ar) dr ,
 \end{aligned}$$

which has a positive integrand. It follows that for $\tau > 2/\pi$, a central location is always preferable.

Thus it suffices to consider (17) and (18), for $x \leq a$. Here (17) has an extraneous root $x=0$ for all a , arising from a multiplication by τ in simplifying to reach (16). The remaining root $x^*(a)$ was determined numerically, and then

$$\tau^*(a) = 2x^*(a)/\pi a$$

was calculated⁽¹¹⁾. It appears as the third column in Table 1. We see that the availability of the short-cut has no great effect on $\tau^*(a)$; it is again a decreasing function which turns negative at approximately $a=2.9$.

So far our illustrations have dealt exclusively with a continuous mass distribution. To help assess the consequences of such an idealization, we conclude by considering a more discrete version of the circular model. Here the roads consist of N radial "spokes" uniformly spread around the disk, lying along the rays

$$\theta = k(2\pi/N) , \quad k = 0, 1, \dots, N-1 ,$$

and also the circumference itself. Along each radius, the mass distribution (as before) decays exponentially as a function of r . For simplicity we treat only the case in which short-cuts through the center are forbidden.

By our general theorem, the optimal location for the facility will lie either at the center of the disk, or at the tip of one of the

(11) The assistance of Miss S. Rose (NBS Technical Analysis Division) in the algebraic and numerical calculations is gratefully acknowledged.

N spokes (which we take to be the one at $\theta=0$.) For a central facility, the total cost of the flow to and from it is

$$f_c = 2NKc_r \int_0^1 r^2 \exp(-ar) dr ,$$

which is $N/2\pi$ times the corresponding expression for the continuous model.

For a peripheral facility, the cost if N is even is

$$\begin{aligned} f_p &= 2NKc_r \int_0^1 (1-r)r \exp(-ar) dr \\ &+ 2Kc_p (2\pi/N) (N/2+2 \sum_{k=0}^{(N-2)/2} k) \int_0^1 r \exp(-ar) dr \\ &= 2NKc_r \int_0^1 (r-r^2) \exp(-ar) dr \\ &+ \pi NKc_p \int_0^1 r \exp(-ar) dr , \end{aligned}$$

which is again $N/2\pi$ times the corresponding expression for the continuous model. This difference from the continuous model is of course simply due to failure to "rescale" by changing K ; the conclusion (for even N) is that $\tau^*(a)$ is exactly the same as for the continuous model.

When N is odd, the cost for a peripheral facility becomes

$$\begin{aligned} f_p &= 2NKc_r \int_0^1 (1-r) r \exp(-ar) dr \\ &+ 2Kc_p (2\pi/N) 2 \sum_{k=0}^{(N-1)/2} k \int_0^1 r \exp(-ar) dr \end{aligned}$$

$$\begin{aligned}
&= 2NKc_r \int_0^1 (r-r^2) \exp(-ar) dr \\
&+ \pi(N-N^{-1})Kc_p \int_0^1 r \exp(-ar) dr .
\end{aligned}$$

Thus

$$\begin{aligned}
(f_p - f_c)/2NKc_r &= \int_0^1 (r-2r^2) \exp(-ar) dr \\
&+ (\pi\tau/2)(1-N^{-2}) \int_0^1 r \exp(-ar) dr .
\end{aligned}$$

For the continuous case, on the other hand, we find from previous formulas that

$$\begin{aligned}
(f_p - f_c)/4\pi Kc_r &= \int_0^1 (r-2r^2) \exp(-ar) dr \\
&+ (\pi\tau/2) \int_0^1 r \exp(-ar) dr .
\end{aligned}$$

It follows that $\tau^*(a)$, for the present model, is $(1-N^{-2})^{-1}$ times its value for the continuous model.

These results give at least some reassurance, that using a continuous idealization in such problems leads neither to qualitative nor to unacceptable quantitative errors.

