NATIONAL BUREAU OF STANDARDS REPORT

DEP-

6908

PERFORMANCE CHARACTERISTICS OF SOME VISCOUS-IMPINGEMENT AND THROW-AWAY TYPES OF AIR FILTERS

by

Carl W. Coblentz and Paul R. Achenbach

Report to

Office of the Chief of Engineers Bureau of Yards and Docks Headquarters, U. S. Air Force Washington 25, D. C.

U. S. DEPARTMENT OF COMMERCE NATIONAL BUREAU OF STANDARDS

FOR OFFICIAL USE ONLY

THE NATIONAL BUREAU OF STANDARDS.

Functions and Activities ...

The functions of the National Bureau of Standards are set forth in the Act of Congress, March 3, 1901, as amended by Congress in Public Law 619, 1950. These include the development and maintenance of the national standards of measurement and the provision of means and methods for making measurements consistent with these standards; the determination of physical constants and properties of materials; the development of methods and instruments for testing materials, devices, and structures; advisory services to Government Agencies on scientific and, technical prohlems; invention and development of devices to serve special needs of the Government; and the development of standard practices, codes, and specifications. The work includes basic and applied research, development, engineering, instrumentation, testing, evaluation, calibration services, and various consultation and information services. A major portion of the Burean's work is performed for other Government Agencies, particularly the Department of Defense and the Atomic Energy Commission. The scope of activities is suggested by the listing of divisions and sections on the inside of the hack cover.

Reports and Publications

The results of the Burean's work take the form of either actual equipment and devices or published papers and reports. Reports are issued to the sponsoring agency of a particular project or program. Published papers appear either in the Bureau's own series of publications or in the journals of professional and scientific societies. The Bureau itself publishes three monthly periodicals, available from the Government Printing Office: The Journal of Research, which presents complete papers reporting technical investigations: the Technical News Bulletin, which presents summary and preliminary reports on work in progress; and Basic Radio Propagation Predictions, which provides data for determining the best frequencies to use for radio communications throughout the world. There are also five series of nonperiodical publications: The Applied Mathematics Series, Circulars, Handbooks, Building Materials and Structures Reports, and Miscellaneous Publications.

Information on the Burean's publications can be found in NBS Circular 460, Publications of the National Bureau of Standards (\$1.25) and its Supplement (\$0.75), available from the Superintendent of Documents, Government Printing Office, Washington 25, D. C.

Inquiries regarding the Bureau's reports should be addressed to the Office of Technical Information, National Bureau of Standards, Washington 25, D. C.

NATIONAL BUREAU OF STANDARDS REPORT

NBS PROJECT

NBS REPORT

1003-12-10431

July 22, 1960

6908

PERFORMANCE CHARACTERISTICS OF SOME VISCOUS-IMPINGEMENT AND THROW-AWAY TYPES OF AIR FILTERS

by

Carl W. Coblentz and Paul R. Achenbach Air Conditioning, Heating, and Refrigeration Section Building Technology Division

to

Office of the Chief of Engineers Bureau of Yards and Docks Headquarters, U. S. Air Force Washington 25, D. C.

IMPORTANT NOTICE

NATIONAL BUREAU OF ST intended for use within the to additional evaluation and listing of this Report, either the Office of the Director, N however, by the Government to reproduce additional copi

Approved for public release by the Director of the National Institute of ision is obtained in writing from Standards and Technology (NIST) on October 9, 2015.

progress accounting documents rmally published it is subjected , reproduction, or open-literature Such permission is not needed, prepared if that agency wishes



U. S. DEPARTMENT OF COMMERCE NATIONAL BUREAU OF STANDARDS FOR OFFICIAL USE ONLY

.

Performance Characteristics of Some Viscous-Impingement and Throw-away Types of Air Filters

by

Carl W. Coblentz and Paul R. Achenbach

1. Introduction

The performance of a group of panel air filters of the cleanable viscous-impingement and throw-away types of 1- and 2-inch nominal thickness was determined to provide information for preparation of new specifications for air filters, to assist in the proper application of these devices, and to permit an economic comparison of cleanable and disposable types of equipment. This investigation was carried out as a part of the Tri-Service research and development program at the National Bureau of Standards.

The performance of the individual filters with respect to arrestance, pressure drop, dust-holding capacity, and cleanability has been described previously in separate reports. This report summarizes and compares the data obtained on 16 viscous-impingement type and 6 throw-away type filters.

2. Description of Test Specimens

The test specimens were designated as types A through L and marked with the suffix 1 or 2 to indicate their nominal thickness in inches. The actual thickness of the nominal 1-inch filters ranged from 7/8 inch to 1 inch, whereas that for the nominal 2-inch filters ranged from 1 13/16 inches to 2 inches. The cleanable viscous-impingement filters were manufactured and furnished by 6 different manufacturers and the throw-away filters were manufactured and furnished by 4 different manufacturers.

The eight types of cleanable viscous-impingement filters were made of corrosion-resisting material, either aluminum or galvanized steel, with the frames and filter media always composed of the same metal. The steel filters had media made of wire whereas the aluminum filters used layers of perforated sheets. The four types of throw-away filters had glass fiber media and cardboard frames.

The adhesives used on the cleanable filters were furnished by the respective manufacturers and were soluble in water. The throw-away type filters were furnished with an adhesive, believed to be Tricresyl phosphate.

· · ·

3. Test Method and Procedure

All of the cleanable filters and a part of the throw-away filters were tested at both 360 ft/min and 540 ft/min face velocity. The air flow rates were determined as the product of the net face area and the face velocity. Since all filters tested had a nominal size of 20×20 inches, the actual air flow rates corresponding to the two values of face velocity were all close to 800 cfm and 1200 cfm, respectively.

The cleanable type filters were immersed in the adhesive furnished by the manufacturer and left to dry in the laboratory at least 16 hours before being weighed and installed in the test apparatus. The initial pressure drop of each filter was determined for both face velocities after which the arrestance of the clean filter at the air velocity desired for that test was determined with the NBS "Dust Spot Method" as described in the paper, "A Test Method for Air Filters" by R. S. Dill (ASHVE Transactions, Vol. 44, p. 379, 1938).

The arrestance determinations were made with laboratory air into which Cottrell precipitate had been injected and diffused at a ratio of 1 gram per 1000 cu ft of air. The sampling air was drawn from the center points of the test duct one foot upstream and eight feet downstream of the filter at equal flow rates and passed through known areas of Whatman No. 41 filter paper. The change of opacity of these areas was determined with a photometer which measured the light transmission of a part of the area on each sampling paper before and after the sampling period. The two sampling papers used for each arrestance measurement were selected to have the same light transmission readings when clean. In order to obtain similar increases of opacity on both samplers, different size areas were used upstream and downstream of the filter. The arrestance, A (in percent), was calculated by the following formula:

$$A = \left(1 - \frac{S_{D}}{S_{U}} \times \frac{\Delta D}{\Delta U}\right) \times 100$$

where S_D and S_U are the downstream and upstream areas, and ΔD and ΔU the observed changes in the opacity of the downstream and upstream sampling areas, respectively.

Whereas the arrestance determinations were made with Cottrell precipitate only, cotton lint was added during the loading process in a ratio of 4 parts by weight to every 96 parts of Cottrell precipitate, including that amount used for arrestance measurements. Arrestance determinations were made at the beginning and at the end of the loading period of each filter and at several intermediate load conditions.



The pressure drop across the filter under test was recorded after each increment of 20 grams of dust had been introduced into the test duct, and the test was terminated when the pressure drop reached 0.5 in. W.G. at the lower air flow rate and 0.8 in. W.G. at the higher air flow rate.

The cleanable viscous-impingement type filters were washed with hot water using a hose until the effluent water appeared clean and then were allowed to dry. After drying, the filter was re-oiled, weighed and installed in the test apparatus for determining any change in pressure drop and for a second loading, after which the cleaning procedure and the determination of the pressure drop were repeated.

4. Test Results

The data obtained on arrestance, dust holding capacity, pressure drop, and cleanability for the two types of air filters are summarized in Tables 1 to 4 and a part of the data is shown graphically in Fig. 1 to 4.

The "Dust Load" shown in these tables and graphs is the dust holding capacity of the filters, or the dust received by the filter, at the selected final pressure drops of 0.5 and 0.8 in. W.G. for face velocities of 360 and 540 ft/min, respectively. It is the weight of Cottrell precipitate and lint introduced into the test apparatus divided by the net face area of the filter and diminished by the percentage of dust fallout upstream of the filter. This fallout was determined by weight at the conclusion of the test by sweeping out the test duct.

The "Average Arrestance" in the tables and graphs is the average of the arrestance values obtained during the period in which the capacity dust load was accumulated. It was determined graphically from a curve drawn through the plotted values of arrestance versus dust load for each filter test.

The values shown in Tables 1 to 4 for weight increase and pressure drop increase after the second cleaning are cumulative; that is, they are changes from the initial values for the clean filter.

Tables 1 and 2 show that the average arrestance of the oneinch cleanable filters ranged from 47 to 69 percent at a face velocity of 360 ft/min with an average of 56 percent for all specimens, and ranged from 47 to 73 percent at a face velocity of 540 ft/min with an average of 59 percent for all specimens.

The arrestance did not increase for all of the filters at the higher air velocity; it remained constant for two filters and decreased for one other. The average arrestance of one of the one-inch throw-away filters decreased significantly, from 58 to 46 percent, and that of a nother remained about constant as the face velocity was increased from 360 to 540 ft/min.

The dust load of the one-inch cleanable filters ranged from 85 to 362 g/sq ft at the lower face velocity and from 78 to 690 g/sq ft at the higher face velocity, indicating a wide disparity among the eight different models. The variation in dust load for the specimens of the throw-away type was much less than for the cleanable filters. The average dust load of the two types of filters was comparable for the 1-inch thick media, but in the 2-inch filters the cleanable type had a higher dust-holding capacity.

A graph of average arrestance versus dust load for the eight models of cleanable filters shows a general inverse relationship between these two variables. However, the correlation is not good enough to warrant developing a mathematical expression for it.

Tables 1 and 2 show that the initial pressure drop increased less than 0.01 in. W.G. after two cleanings for most of the viscous-impingement filters and several of the filters showed no measurable increase in pressure drop after two cleanings at the lower face velocity. The weight change after two cleanings ranged from a loss of 12 grams to a gain of 123 grams, with an average gain in weight of 34 grams for all specimens. This average weight gain was about 6 percent of the average total dust load on the filters. In the worst case, that of specimen E-1, the weight increase after two cleanings was about 27 percent of the dust load for the lower face velocity and 31 percent of the dust load for the higher face velocity.

Tables 3 and 4 show that the average arrestance of the twoinch cleanable filters ranged from 58 to 66 percent with an average of 60 percent for all specimens at a face velocity of 360 ft/min, and ranged from 57 to 74 percent with an average of 65 percent at a face velocity of 540 ft/min. All except one of the cleanable filters increased in average arrestance as the face velocity was increased. The average arrestance of the one 2-inch throw-away filter tested at both face velocities decreased from 74 to 71 percent as the face velocity was increased from 360 to 540 ft/min.

The dust load of the two-inch cleanable filters ranged from 110 to 468 g/sq ft at the lower face velocity and from 92 to 775 g/sq ft at the higher face velocity. The ratio of the maximum to the minimum values of dust load for the eight specimens was about the same for the two-inch filters as for the one-inch specimens.

The arrestance values obtained for the two-inch throw-away filters was appreciably higher than for the cleanable filters.

Tables 3 and 4 show that the initial pressure drop increased 0.021 in. W.G. at the lower face velocity and 0.035 in. W.G. at the higher face velocity, on the average, after two cleanings. One filter showed a decrease in pressure drop after two cleanings and two filters, specimens B-2 and E-2, showed an increase much higher than the average. The weight increase after two cleanings ranged from 0 to 385 grams, with an average of 145 grams for all specimens. This average weight gain was about 12 percent of the average total dust load on the filters. In the two worst cases, specimens B-2 and E-2, the weight increases after two cleanings were 64 and 49 percent of the total dust loads for the two filters, respectively.

Small variations in weight, in either direction, would be expected after cleaning and re-oiling as a result of variations in oil drainage, but this does not account for the large changes in weight shown in Tables 1 to 4. Variations in oil drainage probably accounts for the decreases in weight shown in the tables as compared to the initial weight of the specimens.

The average values of the dust load and arrestance for the two types and two thicknesses of filters are summarized in Table 5 for face velocities of 360 and 540 ft/min. This summary shows that the average arrestance of the 2-inch cleanable filters was 4 to 6 percent higher than that of the 1-inch filters of the same type, whereas the average arrestance of the 2-inch throw-away filters was 11 to 13 percent higher than that of the 1-inch filters. Table 5 also shows that the arrestance of the cleanable filters increased, on the average, with increased face velocity, whereas it decreased for the throw-away types with increased face veloc,ity. It should be noted that the number of throw-away filters tested was considerably less than the number of cleanable filters, so the average values obtained on the former type are perhaps less representative of all available models than for the latter type.

Table 5

Summary of Average Performance

Thickness of Filters, inches	Face <u>Velocity</u> , ft/min	Dust Loa Cleanable	d <u>, g/sq ft</u> Throw-away	Mean Arre	estance, % Throw-away
1	360	200	200	56	65
1	540	254	249	59	60
2	360	279	187	60	78
2	540	325	264	65	71

Table 6 was prepared to show the general nature of the arrestance curve plotted against dust load for each filter tested. Filters A, D, E, F, G, and J showed a continuous rise in arrestance from the beginning to the end of the loading period for both face velocities and both filter thicknesses, whereas filter B showed this same characteristic in the 1-inch thickness, filters K and L showed this rising characteristic in the 2-inch thickness, and filter C had this characteristic at a face velocity of 360 ft/min for both thicknesses. Filter C revealed minimum arrestance values at: 20 and 30 percent of full dust load for the 1- and 2-inch thicknesses, respectively. Filter H had a rather flat arrestance curve at the higher face velocity, but the curve drooped a little near full dust load. The arrestance curve for filter I, in the 1-inch thickness, sloped downward continuously throughout the loading of the filter.

The current Federal Specification for cleanable viscousimpingement type air filters, F-F-300, dated October 1957, specifies a 2-inch thick filter with the following performance characteristics at a face velocity of 350 ft/min;

- (a) Initial arrestance, 45% minimum
- (b) Dust load at 0.4 in. W.G. pressure drop, 250 g/sq ft minimum
- (c) Pressure drop increase after 1 cleaning, 0.01 in. W.G. maximum.

Table 6 indicates that all of the filters, A to H inclusive, had a minimum arrestance in excess of 45% at 360 ft/min face velocity. Figure 3 shows that the dust load of filters C, E, G, and H was in excess of 250 g/sq ft at a pressure drop of 0.5 in. W.G. An examination of the curves for these filters showed that the dust load requirement was also met at a pressure drop of 0.4 in. W.G.

The other filters of this type did not meet the dust load requirement. Table 3 shows that filters A, D, and E exceeded the specified maximum increase in pressure drop of 0.01 in. W.G. after one cleaning. Thus, of the eight specimens tested, only specimens C, G, and H met all three requirements of Federal Specification F-F-300.

The current Federal Specification for throw-away type filters, F-F-310, dated October 1957, specifies one-inch filters or two-inch filters with the following characteristics at a face velocity of 370 ft/min.

Nominal Filter Thickness1-inch2-inchArrestance, Minimum60%70%Dust Load at 0.5 in. W.G., Minimum115 g/sq ft115 g/sq ft

Figure 1 shows that only filter J met both requirements in a 1inch thick filter, and all four specimens, I through L, met both requirements in a 2-inch thick filter.

5. Discussion and Conclusions

It seems more logical to specify the arrestance of air filters on the basis of the average value during the loading of the filter rather than the initial value for a clean filter, since most filters improve in arrestance as the load increases and the change of arrestance with load is gradual. Furthermore, where a considerable number of suppliers is available and the performance of the different models covers a wide range, it should not be necessary to set the requirements so low that all can comply.

The results of this series of tests indicate that, on the average, a 2-inch thick filter of the cleanable viscous-impingement type had about 5 percent higher arrestance and from 25 to 30% greater dust-holding capacity than a 1-inch thick filter of the same type in the range of face velocity from 360 to 540 ft/min. These average values do not apply to every model tested, because some 2-inch thick filters had lower arrestance than the corresponding 1-inch filter.

The two models of 1-inch throw-away type filters used in these tests revealed arrestances and dust-holding capacities generally comparable with those obtained for the cleanable filters of the same thickness. The 2-inch throw-away type filters had higher arrestances than any of the cleanable filters and a lower dust-holding capacity, on the average, than the cleanable filters at a face velocity of 360 ft/min, but the same comparison was not true at the higher face velocity. The principal

difference between the two types of filters was the relation of arrestance to face velocity. An increase in face velocity was accompanied by an increase in arrestance, on the average, for the cleanable filters, but the reverse was true for the throwaway filters in two out of three cases.

The data obtained on cleanable viscous-impingement filters during this series of tests are considered to be sufficiently comprehensive to serve as a basis for revising the Federal Specification requirements and providing requirements for both l-inch and 2-inch filters. Estimates could probably be made from these data on the relative merits of l-inch and 2-inch cleanable filters for various applications. Data on additional models of throw-away filters are needed before any revision of the Federal Specification on this type of filter could be suggested.

At the same time, it should be remembered that either type of filter can readily be modified by the manufacturer with respect to media density, pressure drop, thickness, and type of adhesive, accompanied by a change in performance. Thus, it cannot be assumed that the performance data observed during a given series of tests will be applicable over a long period of time unless the design of the filter is known to be unchanged. For example, a cleanable filter made for similar duty by the same manufacturer as one of the present test specimens, but with a different model number, was tested at the National Bureau of Standards about a year prior to this series of tests. In the present series, this filter had a very low dust-holding capacity, but in the earlier test the dust-holding capacity was comparable to other models. A careful examination of the construction of the filters revealed that a small change in the arrangement of the filter media had increased the arrestance somewhat, but had very considerably reduced the dust-holding capacity. Conversely, an earlier design of one of the throw-away type filters reported herein, was tested less than a year ago and found to have a very low arrestance. The filter was redesigned and retested with the resulting performance being incorporated in this summary.

The determination of acceptable cleanability should probably be based on more than one loading and cleaning of a filter, and probably should be based on weight gain rather than increase in pressure drop. Changes in pressure drop of a few thousandths of an inch of water cannot always be determined with certainty in such laboratory procedures. It will be noted in Table 1 that filter E-1 gained 65 grams in weight, which was approximately 14% of the total dust load, after the first cleaning, accompanied by a pressure drop increase of only

0.005 in. W.G.; and in Table 3, filter C-2 gained 212 grams in weight, which was about 26% of the total dust load, after the first cleaning, accompanied by a pressure drop increase of only 0.003 in. W.G. Experience with the specimens tested indicates that a more reliable indication of cleanability would be established after two or three cleanings than after one cleaning.

ocity	op Increase After Second Cleaning in. W.G.		0.000 0.005 0.000 0.000 0.000 0.000 0.000		
min Face Vel	Pressure Dr After First Cleaning in. W.G.	lters	0.002 0.007 0.001 0.001 0.001 0.001 0.001		
at 360 ft/1	Increase After Second Cleaning g	ngement Fi	123 123 34 34 123 123 123 123 123 123 123 123 123 123	lters	
? Filters	Weight After First Cleaning g	scous-Impi	1 50 50 50 50 50 50 50 50 50 50 50 50 50	ow-Away Fi	
f l-inch Air	Average Arrestance	leanable Vis	00 400 400 10 400 100 10 400 100 100 100 100 100 100 100 100 100	Thr	58 72 65
ormance o	Dust Load <u>g/sq ft</u>	G	85 316 3162 3162 3162 362 200 200		208 191 200
Perf	Initial Pressure Drop in. W.G.		0.075 0.075 0.040 0.055 0.055 0.055 0.055 0.055		0.100 0.086 0.093
	Filter Designation		A-1 B-1 C-1 G-1 H-1 Average		I−1 J−1 Average

Table 1

ocity	op Increase After Second Cleaning in. W.G.		0.000 0.009 0.003 0.003 0.003 0.003 0.012		
nin Face Vel	Pressure Dr After First Cleaning in. W.G.	lters	-0.005 0.0002 0.0002 0.015 0.005 -0.008 0.002		
at 540 ft/1	Increase After Second g Cleaning	ngement Fi	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	LITERS	
r Filters	Weight After First Cleaning g	scous-Impi	- 5 5 1 1 2 3 8 2 1 3 8 1 3 8 1 1 3 8 2 1 3 8 1 3 8 1 1 3 8 1 1 3 8 1 1 3 8 1 1 3 8 1 1 3 8 1 1 1 1	ow-Away F	
f l-inch Ai	Average Arrestance	leanable Vi:	1 20 20 20 20 20 20 20 20 20 20 20 20 20	JUL	46 73 60
ormance o	Dust Load <u>g/sq ft</u>	C	78 1158 690 254 254 254		325 173 249
Perf	Initial Pressure Drop in. W.G.		0.155 0.125 0.087 0.125 0.125 0.125 0.125 0.121 0.131		0.145 0.156 0.151
	Filter Designation		А-1 В-1 С-1 К-1 К-1 Аverage		I-1 J-1 Average

Table 2

	`
	1
	Ň
\sim	
le	
ab	
-	

Performance of 2-inch Air Filters at 360 ft/min Face Velocity

ΦI		
op Increas After Second Cleaning in. W.G.		0.030 0.080 0.020 0.025 0.001 0.001 0.001
Pressure Dr After First Cleaning in. W.G.	ters	0.035 0.010 0.011 0.0014 0.005 0.005 0.005 0.000
Increase After Second Cleaning g	ngement Fil	1 40 1 1 1 1 1 1 1 1 1 1 1 2 0 3 3 3 3 3 3 3 2 3 3 2 3 3 3 3 3 3 3
Weight] After First Cleaning g	cous-Impir	85 175 175 175 175 85 85
Average Arrestance	leanable Vis	000000000000000000000000000000000000000
Dust Load <u>g/sq ft</u>	G	110 540 540 540 540 540 540 540 540 540 54
Initial Pressure Drop in. W.G.		0.080 0.070 0.060 0.046 0.107 0.107 0.107 0.107
Filter)esignation		е ка А С С С С С С С С С С С С С С С С С С С

Throw-Away Filters

279

0.068

Average

77 77 78 78

124 172 169

0.121 0.107 0.147 0.147 0.101

0.119

Average

,³⁼

ocity	op Increase After Second Cleaning in. W.G.		0.155 0.022 0.036 0.036 0.010 0.010 0.035	
iin Face Vel	Pressure Dr After First Cleaning in. W.G.	lters	0.020 0.020 0.023 0.010 0.012 0.012	
at 540 ft/m	Increase After Second Cleaning g	ngement Fil	197 197 197 197 197 145 145	
Filters	Weight After First Cleaning g	cous-Impi	85 175 85 85 85	гл Хрмау-мо
f 2-inch Air	Average Arrestance	leanable Vis	02 20 08 12 08 12 0 2 0 2 10 0 10 0 10 0	11.
ormance of	Dust Load <u>g/sq ft</u>	G	92 250 250 250 255 255 255 255 255 255 25	264
Perf	Initial Pressure Drop in. W.G.		0.225 0.170 0.146 0.128 0.128 0.128 0.128 0.128 0.128	0.196
	Filter Designation		е ка челололо А е – – – – – – – Ка А е – – – – – – – Ка В С С В С В С С С В С В С С В С В С В С В С С В В С В С В С В В В В С В С В В С В С В С В С В С В С В С В	* * * 0000 1111 1527

* Not tested at 540 ft/min face velocity.

-13-

Table 4

17 C F

E110 ft /min

Table 6

	Maxim the Perc	um ar ent c	nd Mini of Dust	Lmum A ; Load	arrestar 1 at Whi	ice Val Ich The	ues an y Occu	airred	
Thickness	of Filter		l ir	nch			2 inc	hes	
Face Veloc:	ity, ft/min	36	50	5 ¹	40	36	0	5 ¹	10
Filter Specimen	Arrestance	А	L	А	L	А	L	А	L
А	max.	70	100	78	100	76	100	72	100
	min.	52	0	64	0	55	0	64	0
В	max.	63	100	66	100	68	100	79	60
	min.	50	0	56	0	52	0	64	0
С	max.	50	100	61	100	65	90	70	100
	min.	47	0	41	20	53	0	57	30
D	max.	62	100	63	100	65	100	65	100
	min.	51	0	51	0	53	0	56	0
E	max.	71	100	81	100	71	100	81	100
	min.	50	0	51	0	52	0	57	0
F	max.	77	100	56	100	75	100	65	100
	min.	42	0	43	0	49	0	50	0
G	max.	79	100	80	100	79	100	81	100
	min.	60	0	62	0	59	0	60	0
H	max.	53	70	48	50	62	100	59	90
	min.	38	0	45	100	48	0	56	100
I	max. min.	60 54	0 100	55 38	0 100	86 73	100 0	-	
J	max.	78	100	79	100	78	100	77	100
	min.	58	0	63	0	61	0	59	0
К	max. min.	-	-	-	-	85 74	100 0	-	-
L	max. min.	-	-			82 69	100 0	-	-

A is the arrestance of Cottrell precipitate. L is the percent of full dust load at which the maximum or minimum arrestance occurred.

USCOMM-NBS-DC





			T HOLD CH THI FT/MI T LOA P Icm RAGE	ING CAI CK FILT N. FACI D AT O = 50g / ARRES	PACITY ERS E VELO 5 IN. W. 1 SQ. FT TANCE	AND A CITY G. FIN	RRESTA AL PRE							
800.80														
700 70														
600 60														
00														
500 50 z			un na la											
ERCE														
400 40 ⁰								WIII						
AD, GRAMS 000 000 ARRESTAN														
200 20													-	-
500												- 2		
100 10														· · · ·
0-0-														
	A+C	8-2	Ç - 2	FILTER	E=2	F=2	6-2	H-2	EIC 3	J+2	K.+ 2		2	



.*

U.S. DEPARTMENT OF COMMERCE Frederick H. Mueller, Secretary

NATIONAL BUREAU OF STANDARDS

A. V. Aslin, Director



• Office of Weights and Measures.

THE NATIONAL BUREAU OF STANDARDS

The scope of activities of the National Bureau of Standards at its major laboratories in Washington, D.C., and Boulder, Colorado, is suggested in the following listing of the divisions and sections engaged in technical work. In general, each section carries out specialized research, development, and engineering in the field indicated by its title. A brief description of the activities, and of the resultant publications, appears on the inside of the front cover.

WASHINGTON, D.C.

Electricity and Electronics. Resistance and Reactance. Electron Devices. Electrical Instruments. Magnetic Measurements. Dielectrics. Engineering Electronics. Electronic Instrumentation. Electrochemistry.

Optics and Metrology. Photometry and Colorimetry. Photographic Technology. Length. Engineering Metrology.

Heat. Temperature Physics. Thermodynamics. Cryogenic Physics. Rheology. Molecular Kinetics. Free Radicals Research.

Atomic and Radiation Physics. Spectroscopy. Radiometry. Mass Spectronictry. Solid State Physics. Electron Physics. Atomic Physics. Neutron Physics. Radiation Theory. Radioactivity. X-rays. High Energy Radiation. Nucleonic Instrumentation. Radiological Equipment.

Chemistry. Organic Coatings. Surface Chemistry. Organic Chemistry. Analytical Chemistry. Inorganic Chemistry, Electrodeposition. Molecular Structure and Properties of Gases. Physical Chemistry. Thermochemistry. Spectrochemistry. Pure Substances.

Mechanics, Sound. Mechanical Instruments. Fluid Mechanics. Engineering Mechanics. Mass and Scale. Capacity, Density, and Fluid Meters. Combustion Controls.

Organic and Fibrous Materials. Rubber. Textiles. Paper. Leather. Testing and Specifications. Polymer Structure. Plastics. Dental Research.

Metallurgy, Thermal Metallurgy, Chemical Metallurgy, Mechanical Metallurgy, Corrosion, Metal Physics,

Mineral Products, Engineering Ceramics, Glass, Refractories, Enameled Metals, Constitution and Microstructure,

Building Technology. Structural Engineering. Fire Protection. Air Conditioning, Heating, and Refrigeration. Floor, Roof, and Wall Coverings. Codes and Safety Standards. Heat Transfer. Concreting Materials.

Applied Mathematics. Numerical Analysis. Computation, Statistical Engineering. Mathematical Physics.

Data Processing Systems. SEAC Engineering Group. Components and Techniques. Digital Circuitry. Digital Systems. Analog Systems. Application Engineering.

• Office of Basic Instrumentation.

BOULDER, COLORADO

Cryogenic Engineering. Cryogenic Equipment. Cryogenic Processes. Properties of Materials. Gas Liquefaction.

Radio Propagation Physics. Upper Atmosphere Research. Ionospheric Research. Regular Propagation Services. Sun-Earth Relationships. VHF Research. Radio Warning Services. Airglow and Aurora. Radio Astronomy and Arctic Propagation.

Radio Propagation Engineering. Data Reduction Instrumentation. Modulation Research. Radio Noise. Tropospheric Measurements. Tropospheric Analysis. Propagation Obstacles Engineering. Radio-Meteorology. Lower Atmosphere Physics.

Radio Standards. High Frequency Electrical Standards. Radio Broadcast Service. High Frequency Impedance Standards. Electronic Calibration Center. Microwave Physics. Microwave Circuit Standards.

Radio Communication and Systems. Low Frequency and Very Low Frequency Research. High Frequency and Very High Frequency Research. Ultra High Frequency and Super High Frequency Research. Modulation Research. Antenna Research. Navigation Systems. Systems Analysis. Field Operations.



)