NATIONAL BUREAU OF STANDARDS REPORT 4569

AIR-MAZE AIRCRAFT FILTERS

by

Carl W. Coblentz William F. Goddard, Jr.

Report to Engineering and Development Branch Office of the Chief of Transportation Department of the Army Washington, D. C.



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Carl W. Coblentz William F. Goddard, Jr. Heating and Air Conditioning Section Building Technology Division

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Carl W. Coblentz and William F. Goddard, Jr.

Abstract

The characteristics of a group of twelve Air-Maze aircraft engine filters were determined with different aerosols and air flow rates. Tests were made with the filters oiled. dry and as received. The group consisted of new filters of two different designs and of filters which had been worn to various degrees in service. The filtering efficiency with A.C. Spark Plug Division "coarse" dust reached 98.7%. This type filter is small and light and its pressure loss moderate when the filters are clean; but the pressure loss increases sharply when the filters become loaded with dust. The advantages of the two different designs are described and the effect of the length of service and the value of proper maintenance are explained. The attainment of adequate maintenance appears to be extremely difficult in military use.

1. INTRODUCTION

The performance characteristics and service requirements of the Air-Maze aircraft engine air filters were determined as a part of the research project "Air Filter Systems for Army Aircraft". This type filter is being used in the L-19 Army aircraft. It is an oiled-impingement type filter consisting of pleated flock covered wire screens. This filter is mounted on the air-intake of the carburetor and may be removed for cleaning or replacement.

2. FINDINGS

The filtering efficiency, using A.C. Spark Plug Division "coarse" dust reached 98.7%. Efficiency is about equal with A.C. "fine" dust and with Cottrell precipitate.

The efficiency determined with "coarse" dust was considerably higher than that obtained with "fine" dust; the filtering efficiency of the 50% mixture of fine and coarse dusts was well in between the efficiencies of these dusts alone, as could be expected. The following table shows the gravimetric efficiencies determined for the first two test runs with 15.1g dust each, after the filters had been cleaned and oiled.

TABLE 1

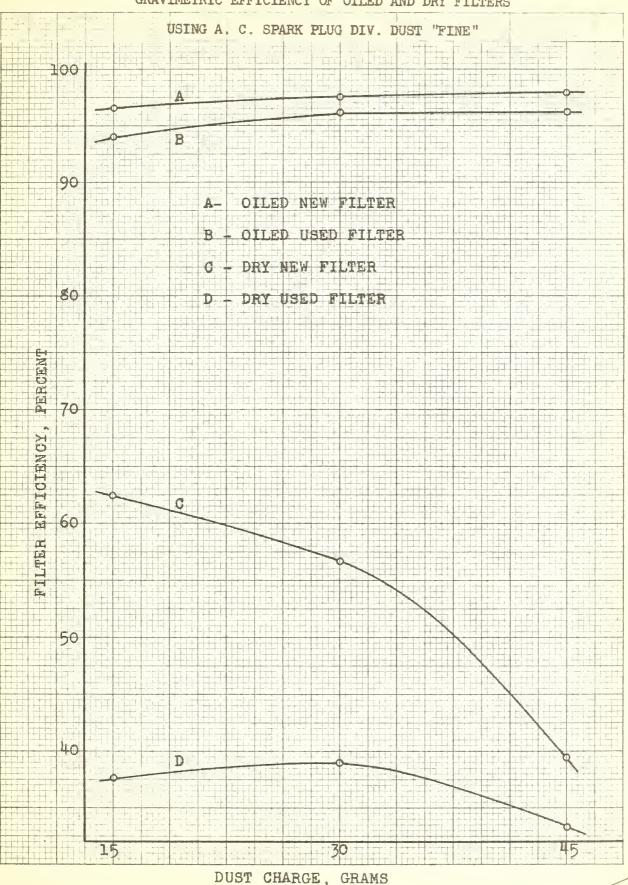
FILTER EFFICIENCY WITH DIFFERENT DUSTS

Tests No.	Filter No.	Dust		iency 2.Run	Average
2181-2 2149-10 4044-5 4051-2 1187-8		A.C. Fine 50% Fine + Coarse A.C. Coarse Cottrell Precipitate	96.5 96.7 97.8 98.6 95.6		97.0 97.0 98.0 98.7 96.9

Tests made with the filters "as received" show values of efficiency lying between those determined for the cleaned filters when tested oiled and those when tested dry. It can be assumed that part of the oil had been lost in storage due to absorption by the wrapping paper, or had been run out of the flocking, indicating the importance of careful oiling for obtaining the highest possible efficiency of this type filter. If the filters are not properly oiled after being cleaned, the filtering efficiency drops to about one-half and the dust holding capacity is reduced.

The importance of the oiling of the filters is expressed in the following table which compares the efficiencies of two filters oiled and not oiled for three consecutive dust charges of 15.1g A.C. "fine" dust.

During the third test run, the oiled new filters passed 2.1% of the dust introduced into the system, whereas, under the same conditions, the filter when dry passed 60.6% or about 30 times as much dust as when it was oiled. Fig. 1 presents the values of the following table as a graph.



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GRAVIMETRIC EFFICIENCY OF OILED AND DRY FILTERS

TABLE 2

GRAVIMETRIC EFFICIENCY OF OILED AND DRY FILTERS

Tests No.	Condition of Filter	1. Charge	Efficiency 2. Charge	3. Charge
2181-3	New; oiled	96.5	97•5	97.9
1288, 1311-2	New, dry	62.4	56.6	39.4
2151-3	Used; oiled	94.0	96.1	96.2
1181-3	Used, dry	37.6	39•0	33.2

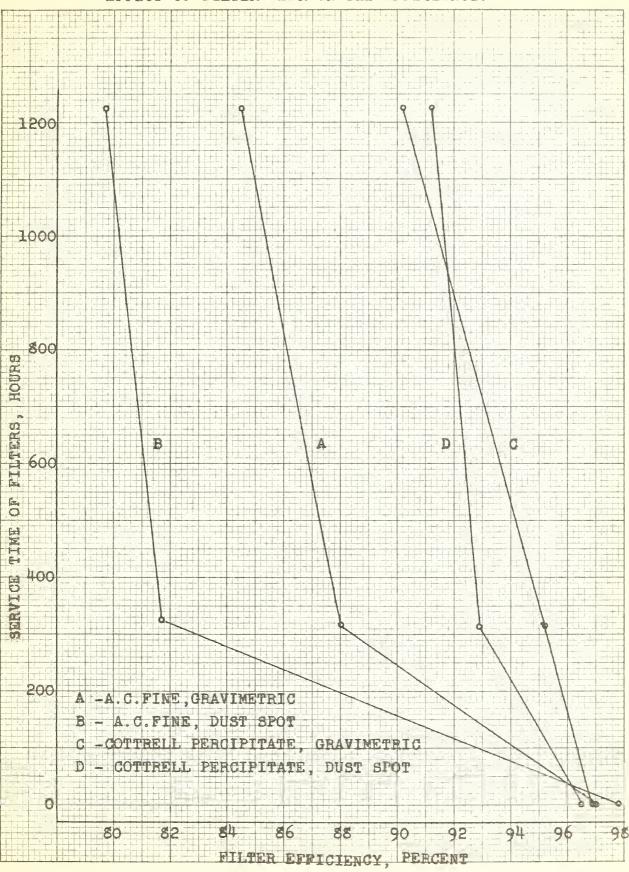
The effect of filter wear was determined by comparing three filters of the same design with different lengths of service. Table 3, below, shows the number of the filters and their length of previous service and the values calculated for the efficiency with A.C. "fine" dust and Cottrell precipitate using the gravimetric as well as the dust spot methods. The effectiveness of the filter decreases sharply when the flock wears off as a result of repeated cleanings and due to the air stream in operation.

TABLE 3

EFFECT OF FILTER WEAR ON EFFICIENCY

Filter	Hrs. of			Cottrell Precipitate		
No.	Service	<u>Gravimetric</u>	Dust Spot	<u>Gravimetric</u>	Dust Spot	
6 3 5	New. 331 1226	97.0 88.0 84.5	97.8 81.7 79.7	96.9 95.2 90.2	96.5 92.9 91.2	

These values, which are plotted on a graph in Fig. 2, indicate the loss of efficiency not only to be a function of the wear, but also, to be different when different aerosols are used. When Cottrell precipitate was used, the efficiency decreased almost linearly with the hours of service, whereas, with A.C. "fine" dust, the decrease of the efficiency was more than twice as much during the first 300 hours of service as it was during the succeeding 900 hours.



EFFECT OF FILTER WEAR ON THE EFFICIENCY.

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Table 4 presents a summary of the efficiency and pressure loss for both the old and the new design filters at air flow rates of 200 CFM, 305 CFM, and 360 CFM, using A.C. "fine" dust as an aerosol. As it had been noticed that the specimen filters of each type did not produce identical test results, all tests of this series were conducted with at least two specimens of each type. The average values from the duplicated tests are more representative than the individual tests would be, as they alleviate the deviation of test observations resulting from certain construction differences in the filters, as well as from slightly varying conditions that may affect these observations.

These average values are shown as a graph in Fig. 3, indicating that the pressure loss and the efficiency are higher on the old design filters for any comparable air flow rate and dust charge.

The filtering efficiency of the older design with two flocked screens was found to be better than that of the new design which has only one flocked screen. The efficiency of the old design at 305 CFM exceeded 98% and decreased for both higher and lower flow rates.

The pressure loss of the Air-Maze filters stays rather low as long as the filters are not overloaded, but increases fast once a certain load has been reached.

It was noted that neither the weight nor the pressure loss presented a positive criterion of the condition of the used filters. It was noted, however, that a pressure loss of less than 1 inch W.G. at the design air flow rate occurred only when the flock had worn off to such a degree that the filtering efficiency had dropped considerably and the filter should have been replaced.

3. SPECIMEN AND TEST APPARATUS

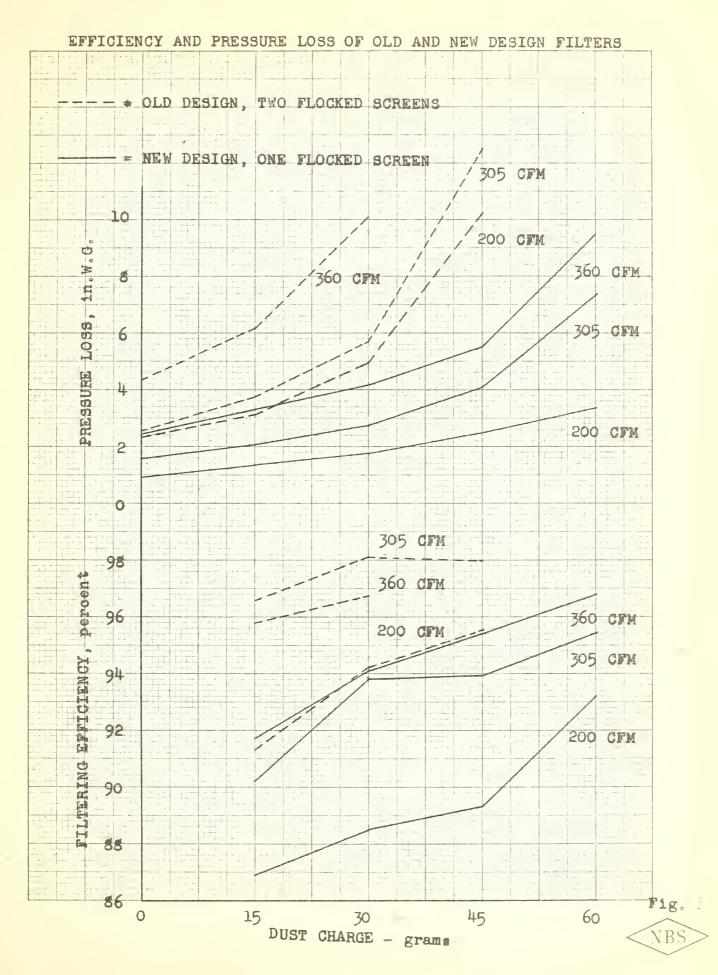
The test specimens were products of the Air-Maze Corporation of Cleveland, Ohio. The Office of the Chief of Transportation furnished 12 filters for testing, all having the same outside dimensions of $7\frac{1}{2} \ge 7 \ge 1$ inch with a free filtering area of $6-3/4 \ge 6-1/4$ inches or 0.293 square feet. According to the manufacturer's catalog, these filters are designed for a face velocity of 1050 ft/min. corresponding to about 305 CFM air flow rate.

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GRAVIMETRIC EFFICIENCY AND PRESSURE LOSS OF NEW AND OLD DESIGN FILTERS AT DIFFERENT AIR FLOW RATES WITH A.C. SPARK PLUG DIV., DUST "FINE"

60g Dust Charge Eff. Press. Loss % in. WG		93.2 3.38 93.2 3.38		94.1 6.93 96.6 7.76 95.4 7.35		96.3 9.14 97.3 9.94 96.8 9.54
45g Dust Charge (iff. Press. Loss E: % in. WG ?	9.89 10.146 10.18	6 111 2 115 2 10 2 10 2 10 2 10 2 10 2 10	9.68 15.29 12.49	ц. 22 ц. 06 11, 11		5.82 5.27 5.55 9.9
H5g D Bff.]	94.8 96.2 95.5	91.2 87.4 89.3	9.79 0.86 0.86	92.4 95.4 93.9		93.6 97.2 95.4
30g Dust Charge ff. Press. Loss % in. WG	4.17 5.70 4.94	1.81 1.73 1.77	н. 88 6.38 5.63	2.87 2.68 2.76	10.17 10.00 10.09	4.55 4.13 4.13 19
Eff.	94.2 94.3	85.1 91.9 88.5	97.5 98.6 98.1	93.4 94.3 93.8	97.2 96.2 96.7	94.5 94.5
Dust Charge Press. Loss in. WG	2.40 3.81 3.11	1.34 1.38 1.36	3.42 4.10 3.76	2.09 2.01 2.05	6.14 6.18 6.16	3.34 3.26 3.30
15 <u>8</u> Bff.	89 <mark>.</mark> 1 93.1	89.1 84.6 86.9	96.5 96.7 96.6	91.0 89.3 90.2	94.4 97.2 95.8	90.1 93.3 91.7
Clean Press, Loss In, WG	1.57 3.11 2.34	0.87 0.91 0.89	2.56 2.56 2.56	1.58 1.58	4.33 4.40 4.37	2.36 2.44
Filter No.	2 2 2 2 49	11 12 11+11	2+9 2	11 12 11+11	2+9 2	11 12 11+12
	Average	Average	Average	Average	Average	11 12 Average 11+12
Air Flow Rate, CFM	200 200	200 200	305 305	305 305	360	360



Some of the test specimens were new and others had different lengths of service. The used filters had two pleated flock covered wire screens as the filter media. There were two new filters of this same construction and two new filters of a new design - one flocked screen, the other screen being bare. The cotton flock had worn off considerably on some of the used filters leaving a practically bare wire mesh.

Table 5 shows a listing of the test specimens giving the consecutive numbers, time of service as reported by the Transportation Corps, their weight as received after removing the holding clips and gaskets, and their pressure loss at 305 CFM air flow.

Fig. 4 is a photograph of the test apparatus, showing the 20 ft. long duct made of 5 inch brass pipe in the middle of which is an adapter to hold the rectangular test specimen. The two halves of the adapter are equipped with foam rubber strips so that any outside air leakage is prevented when the two halves are pulled against the specimen with 4 steel bolts. Vertical and horizontal stops are provided to assure proper alignment of the test specimen in the adapter. The air is drawn into the duct by a blower installed in a room behind the test panel and the air flow rates are measured with orifice flow meters designed in accordance with the A.S.M.E. Research Publication "Fluid Meters, Their Theory and Application."

For each test run, a measured amount of dust is placed in a small hopper which feeds into the groove of a turntable to a constant level. The turntable is mounted on a variable speed Graham transmission and the dust is picked up from the groove by a high pressure aspirator which breaks up any agglomerations and supplies the dust to the open inlet of the test duct, at the desired feed rate. By changing the speed of the turntable, infinite variations of dust concentrations can be obtained for any air flow rate and can be maintained constant during each test run.

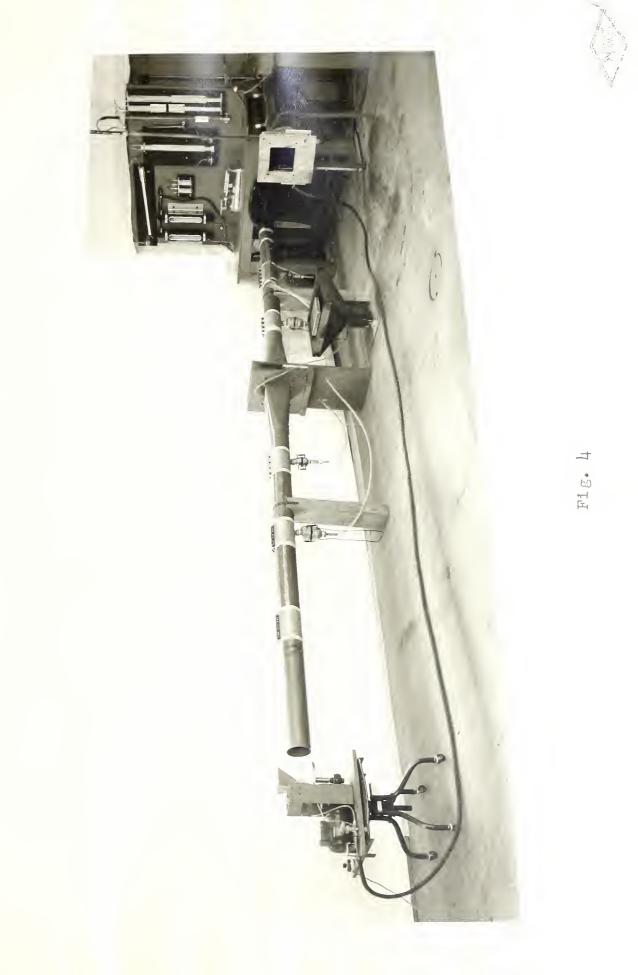
The test dust used is classified air cleaner test dust produced by the A.C. Spark Plug Division of General Motors Corporation. Most tests were made with "fine" dust; for comparative purposes, a few tests were made with "coarse" dust and also with a mixture of 50% each fine and coarse dust and also with Cottrell precipitate.



TABLE 5

No.	Length of Service Hrs.	Weight g	Pressure Loss at 305 CFM, in. WG
1	Used	234.9	1.38
2	986	239.7	1.14
3	330	248.4	1.12
4	Used	222.9	0.75
5	1225	237.6	0.83
6	New	218.4	1.97
7	New	220.6	1.93
8	200-300	288.2	2.36
9	434	221.7	1.22
10	200-300	227.6	1.07
11	New	249.0	1.26
12	New	236.4	1.26

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The efficiency of the test specimen is determined by sampling the air upstream and downstream of the air cleaner with identical sampling nozzles installed in the center of the duct. A representative sampling is assured by maintaining isokinetic flow between nozzle inlet and duct. The dust drawn through the sampling nozzle is collected on glass fiber paper whose smallest fibers are about 0.3 micron in diameter. Tests of the air cleaning efficiency of similar paper by the Atomic Energy Commission indicate that such paper retains more than 99.99 per cent of all particles 0.3 micron and larger and it can, therefore, be considered an absolute filter for these tests.

Fig. 5 is a photograph of this sampling device. It shows one nozzle installed in a 3 inch duct, chosen for ease of photography, and three others with different openings to compensate for a wide range of air velocities in the test duct. One sampling paper holder is shown with the nozzles and another one is installed between the two bell caps. These holders consist of aluminum rings between which the glass fiber paper is clamped tight.

The air flow rate through the upstream and downstream samples is measured with two identical orifice flow meters which were calibrated with a gas meter. The manometers connected to these flow meters are mounted on either side of a graduated rule to facilitate the adjustments for maintaining equal flow through the two samplers during each test. The filter efficiency was calculated from the formula

$$E_{G} = (1 - \frac{D}{U}) \times 100\%$$

where E_G = gravimetric efficiency, per cent, D^G = weight gain of downstream sampler, U = weight gain of upstream sampler.

In order to ascertain that the observed sampler gains are representative for the prevailing dust concentrations in the duct, the test apparatus is operated without filter, at frequent intervals, in which case the upstream and downstream filter gains must be equal.

The efficiency of the filter was also determined by another method based on the discoloration caused by the dust. This method is known as the "National Bureau of







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Standards Dust Spot Method" and is described in the paper "A Test Method for Air Filters" by R. S. Dill, ASHVE Transactions, Vol. 44, p 339, 1938. In this method, equal air samples from upstream and downstream of the filter are passed through known areas of Whatman #41 filter paper. The areas of the upstream and downstream filter papers are selected by repeated trials to obtain an approximately equal change of light transmission through these papers for a given test condition.

4. TEST PROCEDURE AND OBSERVATIONS

All filters were tested at the design air flow rate of 305 CFM and Table 6 shows a summary of the more indicative test results. In order to determine the characteristics of this type filter, tests were made under nine different conditions:

A/ Filters oiled; tested with A.C. "fine" dust.
B/ Filters as received; tested with A.C. "fine" dust.
C/ Filters dry (cleaned and not oiled); tested with A.C. "fine" dust.
D/ Filters as received; tested with A.C. "coarse" dust.
E/ Filters oiled; tested with A.C. "coarse" dust.
F/ Filters oiled; tested with 50% each A.C. "fine" and "coarse" dust.
G/ Filters oiled; tested with Cottrell precipitate.
H/ Filters oiled; tested with A.C. "fine" dust and 200 CFM air flow.
I/ Filters oiled; tested with A.C. "fine" dust and 360 CFM air flow.

Between two and four individual test runs were made with each filter for every condition tested to observe the change of its characteristics with the increase of the dust load. 15g to 20g of dust were used for each run and the filter weight was determined before and after each test run so that an approximation of the filtering efficiency was obtained as the ratio of the weight increase of the filter to the weight of the dust introduced into the duct. This efficiency, E_F , was mostly lower than the efficiency E_G computed from the weight increase of the samplers because dust dropped off the filter when it was removed from the test duct to be weighed.

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The pressure drop across the filter was observed and the duration of the tests was noted. From the latter, the dust concentration upstream of the filter was calculated. This concentration was maintained at about 10 mg/cu ft, equivalent to a heavy dust cloud.

A comparison of the efficiency of the filter resulting from the use of dust of different mean particle size was made. Sufficient tests with the four different dusts used were conducted on the two new filters, numbers 6 and 7, to obtain average value for each dust.

The new design filters were loaded with 60g of dust for all three air flow rates showing a minimum efficiency of 86.9% and a maximum pressure loss of 9.54 in. W.G. The old design filters were charged with 45g of dust for the 200 CFM and 305 CFM tests at which dust loads, the desired maximum pressure loss of 10 in. W.G. was exceeded.

At the design air flow rate and using A.C. "fine" dust, the efficiency of the new type filter was 90.2% for the first 15g of dust introduced after cleaning and oiling the filter, and 96.6% under the same condition of the old type filter. This means that almost three times as much dust passes through the new filter than the old one.

Under conditions as indicated above, the pressure loss of the new design filters was 1.58 in. W.G. against 2.56 in. W.G. for the old design. This margin in favor of the new design increased significantly as the dust load increased. Whereas, the pressure loss of the old design at a load of 45g increased to 12.45 in. W.G., the pressure loss of the new design reached only 7.35 in. W.G. with a dust load of 60g.

The weight of these filters appeared to vary less with the condition of the screen flock than the amount of residual dust which had not been removed from the filter in recent cleaning operations. The pressure loss of any one filter at a constant air flow rate depends on the condition of the screen flock and its oiling, and the amount of dust load accumulated on the filter.

The light weight and small space requirements, however, make the use of this kind of filter attractive as an induction air cleaner for small aircraft.

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SUMMARY OF TEST RESULTS A/ FILTERS OILED, A.C. "FINE", 305 CFM

911ter Number			Ч			N		ß			9			7	
Test Number		2151	2152	2153	1121	1122	1123	1127	1128	2181	2182	2183	2149	ειμε οιμιε _θ μιε	11413
											OBSE	OBSERVED VALUES	UES		
Filter Weight Start	40	299.6	31 ⁴ .1	328.2	272.2	.			8 7 8	267.7	291.4	306.2	296.3		325.5
Filter Gain Duct Introduced	ნე წ	14.5 14.1 15.1 15.1	14°1	14.0 15.1	Tot הקו	al 40.	5 15 1	Total 15 1	26.1 15 1		14.8 15.1	14.8 15 1	14.8 15.1	14°4	14.8
Duration of Test	Min.	4.22	4.89 4.89	1 1 1 1 1 1 1 1	5.57	5.57 4.89 4.98	4.98		4.86	t.30	t.07	4.80	4.55		1.37 14.37
Pressure Loss Start	In. WG	1.54	2.05	2.87	0.96	1.97	2.87	0.95	1.14	2 . لہل	3.39	h.88	2.68		6.38
Pressure Loss Finish	In. WG	1.97	2.91	4.85	1.97	2.83	5.75	1.14	1.30	3.42	h.88	9.68	4,10	6.38	15.29
Sampler Gain Upstream	а В	to.ù	67.2	52.8	68.9	67.8	73.4	73 . 4	71.0	57.2	59.0	62.9	55.2	58.0	58.6
Sampler Gain Downstream	କ୍ଷ ଅ	₽ * 1	2.6	2.0	9,2	6.1	0°†	11.1	11.6	5.0	1.5	1.3	1.8	1.5	1.0
											COMP	COMPUTED VALUES	SEU		
Dust Concentration	mg/ Cu. ft.	11.7	10.1	11.1	8.9	10.1	6.9	9.8	10.2	11.5	12.2	10.3	10.9	11.0	11.3
Jificiency - EG Gravimetric	BC.	0,46	96.1	96.2	86.7	86.7 91.0	94.6	84.9	83.7	96.5	97.5	6.76	96.7	4 . 76	98.2
Efficiency - EF Filter Gain	DC.	96.1	93.5	92.9	Aver	Average 89.	.6	Average	86.4	97.5	98.1	98.1	98.1	95.5	98.1
LIIICIONCY - LD Discoloration	BC		1		 	79.6	83.3	6.77	76.6	1		8	91.6	93.9	96.5



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A/	FILTERS	OILEI

Filter Number						1	2	
Test Number		2151	3	214 4	2145	2146	214 7	2148
Filter Weight Start Filter Gain Dust Introduced Duration of Test Pressure Loss Start Pressure Loss Finish Sampler Gain Upstream Sampler Gain Downstream	g g Min. In, WG In. WG mg mg	299.6 14.5 15.1 4.22 1.54 1.97 70.4 4.2	1 1 3 2 2	13.7 15.1 4.62 4.17 6.93 47.9	13.9 15.1 4.35 1.57 2.01 52.4	1.93 2.68	14.1 15.1 4.12 2.64 4.06 68.4	14.2 15.1 4.63 4.06 7.76 59.8
Dust Concentration Efficiency - E_G Gravimetric Efficiency - E_F Filter Gain Efficiency - E_D Discoloration	mg/ Cu. ft. % %	.11.7 94.0 96.1)4	10.7 94.1 90.9 91.7			95.4	96.6 94.2

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TABLE 6

SUMMARY OF TEST RESULTS A/ FILTERS OILED, A.C. "FINE", 305 CFM

Filter Number			1			2		5	5		6			7	1		1	1			12	2	
Test Number		2151	2152	2153	1121	1122	1123	1127	1128	2181	2182	2183	2149	21410	21411	2141	2142	2143	2144	2145	2146	2147	2148
											OBSE	RVED VA	LUES										
Filter Weight Start Filter Gain	g		314.1 14.1	328.2 14.0	272.2 Tot	al 40.		269.1 Total	-		291.4 14.8	306.2 14.8	296.3 14.8	311.1 14.4		289.0	303.1 14.0			274.4	288.3] 14.4		
Dust Introduced Duration of Test	g Min.	15.1	15.1	15.1 4.45	15.1	15.1 4.89	15.1	15.1	15.1 4.86	15.1	15.1 4.07	15.1	15.1	15.1		15.1	15.1	15.1	15.1	15.1	15.1 4.42	15.1	15.1
Pressure Loss Start	In, WG	1.54	2.05	2.87	0.96	1.97	2.87	0.95	1.14	2,44	3.39	4.88	2,68	3.98	6.38	1.57	2.09	2.83	4.17	1.57	1.93	2.64	4.06
Pressure Loss Finish Sampler Gain	In. WG	1.97	2.91	4.85	1.97	2.83	5.75	1.14	1.30	3.42	4.88	9.68	4.10	6.38	15.29	2.09	2.87	4.22	6.93	2.01	2.68	4.06	7.76
Upstream	mg	70.4	67.2	52.8	68.9	67.8	73.4	73.4	71.0	57.2	59.0	62.9	55 .2	58.0	58.6	60.0	51.7	38.2	47.9	52.4	55.8	68.4	59.8
Sampler Gain Downstream	ng	4.2	2.6	2.0	9.2	6.1	4.0	11.1	11.6	2.0	1.5	1.3	1.8	1.5	1.0	5.4	3.4	2.9	2.8	5.6	3.2	2.8	2.0
											COM	PUTED VA	LUES										
Dust Concentration	mg/ Cu. ft.	.11.7	10.1	11.1	8.9	10.1	9.9	9.8	10.2	11.5	12,2	10.3	10.9	11.0	11.3	10.8	10.6	10.0	10.7	11.4	11.3	12.2	10.7
Efficiency - E _G Gravimetric	%	94.0	96.1	96.2	86.7	91.0	94.6	84.9	83.7	96.5	97.5	97.9	96.7	97.4	98.2	91.0	93.4	92.4	94.1	89.3	94.3	95.4	96.6
Efficiency - E _F Filter Gain	ø	96.1	93.5	92.9	Avei	age 89	.6	Average	e 86.4	97.5	98.1	98.1	98.1	95.5	98.1	93.6	92.8	93.5	90.9		95.5		
Efficiency - E _D Discoloration	%					79.6	83.3	7 7.9	76.6				91.6	93.9	96.5	87.7	86.8	89.1	91.7	88.9	90.0	91.8	94.0



Filter Nn Test Num Filter Wn Start Filter Gn Dust Int: Duration Pressure Start Pressure Finish Sampler (Upstrea Sampler (Downst)

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B/ FILTERS AS RECEIVED, A.C. "FINE", 305 CFM (Continuation of TABLE 6)

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Filter Number		2	3	5	9	11	12
Test Number		1251 1252 1253	12154 12155	1 21 61 12162	1281 1282 1283	1264 1265 1266	1267 1268 1269
				OBSE	RVED VALUES		
Filter Weight Start	g	239.7	248.4	237.6 254.5	221.7 232.8 246.6	249.0 259.8 271.8	236.4 245.9 255.4
Filter Gain	g	Total 53.0	Total 34.4	16.9 16.5	11.1 13.8 11.3	10.8 12.0 11.0	9.5 9.5 7.7
Dust Introduced	g	20.1 20.1 20.1	20.1 20.2	20.1 20.1	15.1 15.1 15.1	15.1 15.1 15.1	15.1 15.1 15.1
Duration of Test	Min.	7.54 10.25 6.22	5.45 6.36	5.84 6.80	4.73 4.55 4.68	4.92 5.08 5.18	4.85 5.08 5.18
Pressure Loss Start	In. WG	1.14 1.69 2.52	1.18 1.57	0.79 1.02	1.22 1.57 2.05	1.26 1.89 3.50	1.26 1.73 3.19
Pressure Loss							
Finish	In. WG	1.77 2.71 6.42	1.69 2.36	1.02 1.30	1.57 2.16 2.91	2.09 3.86 10.70	1.81 3.31 5.99
Sampler Gain		0 F0 0 00 P	97.4 93.2	54.4 48.2	82.4 67.4 60.6	69.6 69.8 71.7	72.2 71.4 74.0
Upstream Sampler Gain	mg	88.8 90.0 93.0	91.4 93.2	<u>94.4</u> 40.2	82.4 01.4 00.0	09.0 09.6 (1.)	<i>[2.2 1.4 4.0</i>
Downstream	ng	19.8 14.4 12.8	25.0 19.2	11.8 14.6	16.0 16.4 18.0	21.0 15.2 16.0	27.3 26.6 32.6
				COMPI	UTED VALUES		
Dest Generation	mg/	9.1 6.7 10.6	12.1 10.4	11.3 9.7	10.5 10.9 10.6	10.0 9.7 9.6	10.2 9.7 9.5
Dust Concentration Efficiency - E _G	Cu. ft.	9.1 0.1 10.0	12.1 10.4	···)) · (10,) 10,) 10, 0	10.0).1).0	
Gravimetric	%	77.6 83.8 86.2	74.3 79.4	78.3 69.3	81.6 75.6 70.3	69.8 78.2 77.7	62.2 61.3 56.0
Efficiency - E _F Filter Gain	%	Average 87.8	Average 85.0	83.9 82.1	73.5 75.0	71.6 79.6 72.9	63.0 63.0 51.0
Efficiency - E _D Discoloration	%	69.8 76.8 83.5	76.1 77.5	64.3 68.1		84.5 84.4 88.3	83.6 83.1 80.8



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C/ FILTEF	S DRY (NO)T OILED)), A.C	. "FINE				of TABL	A			ECEIVED, 305 OFM		ES OILED, SE", 305 CFM
Filter Number			1			6					10		e	
Test Number		1181	1182	1183	1288	1311	1312	1313	L	³⁴ 1284	1285	1276	4051	4052
Tidl ton Madah t							С	BSERVED	VALU	es				
Filter Weight Start Filter Gain Dust Introduced	80 80 80	243.6 Tota 15.0	al 17.	2			 15.1	 15 2			238.4 8.8 15.1	8.3		281,1 15,1 15,2
Duration of Test Pressure Loss	Min.		5.21			4.65					2.95			2.53
Start Pressure Loss	In. WG	1.50	1.61	1.73	2.08	2.25	2.28			1.14	1.26	1,42		3.27
Finish Sampler Gain	In. WG	1.61	1.77	1.81	2.75	2,91	2.83				1.50			4.10
Upstream Sampler Gain	mg		73.4			78.8					77.2			63.0
Downstream	ng	43.4	44.8	47.8	27.4	34.2					28.4	27.2	1.0	0.8
							C	OMPUTEI	VALU	ES				
Dust Concentration	mg/ Cu. ft.	9.6	9.5	9.7	8.5	10.6	11,1	11.5		14.6	15.6	15 .5	20.7	19.6
Efficiency - E _G Gravimetric	Þ	37.6	39.0	33.2	62.4	56.6	39.4	27.6		73.2	63.2	67.8	98.6	98.7
Efficiency - E _F Filter Gain Efficiency - E _D	%	Aver	age 38	.1	61.0					65.2	58.4	55.	100	99.3
Discoloration	×	50.6	55.0	53.2									000 EFF (10)	



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		F/ FII 50%."FINE_C	TERS OILED, CARSE", 305 CFM	COT: Continuation of TABLE 6)	G/ FILTERS OID IRELL PRECIPITATI	LED, E, 305 CFM	
Filter Number		6	7	5	6	3	1
Test Number		4053 4043	4044 4045 4046	1184 1185 11 86	118 7 11 88	1 1 89 11810	1 174 1175
				OBSERVED VALUES			
Filter Weight Start Filter Gain	e e	296.2 292.8 14.8 15.1	267.9 282.7 297.0 14.8 14.3 15.1	284.5 Total 40.2	330.6 Total 27.6	318.7 Total 28.4	237.0 Total 9.7
Dust Introduced Duration of Test Pressure Loss	g Min.	15.1 15.1 3.42 3.07	15.1 15.1 15.1 2.28 3.42 3.50	15.1 15.1 15.1 6.78 5. ⁴⁴ 5.62	15.1 15.1 5.20 5. 3 8	15.1 15.1 5.62 5.32	15.1 15.1 5.34 5.62
Start Pressure Loss	In, WG	4.10 4.84	3.30 3.46 5.00	0.98 1.10 1.34	3. 90 5 .31	1.57 2.04	1.38 1.54
Finish Sampler Gain	In. WG	6.34 8.78	3.30 5.00 9.60	1.14 1.38 1.96	5.42 7.98	2.08 5.79	1.61 1.65
Upstream Sampler Gain	mg	59.8 78.4	86.2 86.2 81.8	79.5 77.4 70.8	76.7 66.6	65.1 57.8	68.2 69.2
Downstream	mg	1.2 1.0	1.9 1.6 1.0	8.0 7.4 9.4	3.4 1.2	3.2 2.8	49.6 50.6
				COMPUTED VALUES			
Dust Concentration	mg/ Cu. ft.	14.5 16.2	14.5 14.5 14.2	7.3 9.1 8.8	9.5 9.2	8.8 9.3	9.3 8.8
Efficiency - E _G Gravimetric	%	98.0 98.7	97.8 98.1 98.8	90.0 90.4 86.7	95.6 98.2	95 . 1 95 . 2	27.3 26.9
Efficiency - E _F Filter Gain	%	97.7 100	97.7 94.4 100	Average 88.8	Average 91.4	Average 94.0	Average 31.2
Efficiency - E _D Discoloration	%			90.0 92.4 91.5	95.9 97.1	92.1 93.6	54.1 61.6



5314 15.1 15.0 7.53 7.75 0.91 1.30 1.65 1.78 2.44 60.5 50.9 6.4 10.1 10.0 9.7 87.4 Average 80.1 Total 36.2 5313 91.9 4.9 12 287.6 ---1.42 **8**4.6 15.1 7.50 51.2 5312 7.9 5278 15.1 6.90 4°5 91.5 3.34 9.9 10.6 10.9 5.11 1,9,1 6 6 0 53.3 15.1 7.10 1.38 1.85 2.52 3.38 3.7 2.28 5274 5275 5276 5277 85.1 91.2 93.2 Total 40.3 15.0 15.1 15.1 15.1 15.0 15.1 7.13 7.60 7.63 7.10 Average 89.2 0 1.77 56.8 5.0 Ц 0.87 1.30 56**.0** 49.6 6.1 7.⁴ 10.5 9.9 OBSERVED VALUES COMPUTED VALUES 1 295.0 ----89.1 52.6 5263 2.0 15.1 7.42 5.52 5.87 10.46 10.8 10.0 93.4 94.3 96.2 Average 73.0 Total 21.5 15.0 6.92 3.62 57.9 **5261** 526**2** 3.3 352.6 ---3.11 15.1 6.92 4°05 48.2 10.8 3.2 15.1 15.1 6.87 7.22 5273 2.7 4.17 9.88 52.2 11.1 10.4 94.1 94.8 8 303.7 --- -- ---Total 40.7 Average 92.5 5272 2.36 4.17 57.4 ₫. М 8 9 15.0 7.13 89.1 2.40 10.5 1.57 50.5 5271 5.5 ft. In. WG In. WG g Min. Cu. မာ E မ် ရ R 60 60 R *be* Dust Concentration Duration of Test Efficiency - EG Efficiency - ED Discoloration Dust Introduced Efficiency - EF Filter Gain Pressure Loss Filter Weight Pressure Loss Filter Number Gravime ter Sampler Gain Sampler Gain Downs tream Filter Gain Test Number Ups tream Fintsh Start Start

H/ FILTERS OILED, A.C. "FINE", 200 CFM (Continuation of TABLE 6)



I/ FILTERS OILED, A.C. "FINE", 360 CFM (Continuation of TABLE 6)

Filter Number		9		7			11	~			Ч	12	
		6023	6024	6021	6022	6013	6 01 3 6014 6015	6015	6016	6025	6026	6026 6031	6032
						OBSER	OBSERVED VALUES	LUES					
	٥	303,8		314.3	1	299.5		1 9 1	1	312.8	8		1
) 6 0	Total		To tal			Total	53.0			Total		
	<u>س</u>	15.1	15.1	15.1	15.1	15.0	15.1	15.1	15.1	15.1	15.0		15.1
	Min.	3.50	3.67	3.85	3.52	3.58	3.58	4°03	3.52	3.73	3.72	3.33	3.86
	In. WG	4.32	6.05	<mark>0ग</mark> ग	6.08	2.36	3.26	h.17	5.73	2.44	3.18	3.69	5.34
	In. WG	6.16 10.14	10,1 ⁴	6.2 ⁴	10.00	3.42	4.32	5.89	9.12	3.30	h_2, H	5.19	9.90
	8 8	32.0	35.8	35.2	28.8	30.4	31.7	28.0	33.0	33.0	ۍ4 . 8	35.6	29.7
	ଅ ଅ	1.8	1.0	1.0	1,1	3.0	2.0	1.8	1,2	2.2	1.9	1.0	0.8
						C OMP	COMPUTED VALUES	ALUES					
	mg/ Cu. ft.	11.9	11.2	10.9	11.9	11.7	11.7 11.7	10.4	11.7	11.2	11.2	12.6	10.8
	BC	14° 116	0.76	97.2	96.2	90.1	93.7	93.6	96.3	93.3	94.5	97.2	97.3
	BE	Average	e 86.0	Average	e 82.0		Average	87.9			Averag	Average 82.9	
	82	8	1	1 1 1			8	1 1 1	1	î Ş	8	 	



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