NATIONAL BUREAU OF STANDARDS REPORT

2846

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PERFORMANCE TESTS OF CLEANABLE IMPINGEMENT-TYPE AIR FILTERS (Farr Type 44G)

by

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Henry E. Robinson Thomas W. Watson



U. S. DEPARTMENT OF COMMERCE NATIONAL BUREAU OF STANDARDS **U. S. DEPARTMENT OF COMMERCE**

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NBS PROJECT

NBS REPORT

1003-20-4715

October 9, 1953

2846

PERFORMANCE TESTS OF CLEANABLE IMPINGEMENT-TYPE AIR FILTERS (Type 44G)

> manufactured by The Farr Company Los Angeles, California

> > by

Henry E. Robinson Thomas W. Watson Heating and Air Conditioning Section Building Technology Division

to

Bureau of Ships, Code 327 Department of the Navy

Reference: NPO - 15479 Index No. NSM 130-001



U. S. DEPARTMENT OF COMMERCE NATIONAL BUREAU OF STANDARDS

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PERFORMANCE TESTS OF A FARR TYPE 44G AIR FILTER

I. INTRODUCTION

At the request of the Bureau of Ships, Code 327, Navy Department (NPO-15479, Index No. NSM 130-001) qualification tests were made to determine the performance of cleanable viscid-impingement type air filters in accordance with Section 4.5 of Military Specification MIL-F-16552 (Ships) dated 1 October 1951 as modified by Amendment 1 dated 15 April 1952.

The tests were performed on a specimen filter submitted by the manufacturer at the request of the Bureau of Ships, and included determinations of the dust-arresting efficiency, pressure drop, specific dirt load and cleanability of the specimens at three face air velocities, namely 300, 600, and 900 feet per minute.

II. DESCRIPTION OF THE FILTER SPECIMEN

The filter was manufactured by the Farr Company of Los Angeles, California, and was of the cleanable viscid type, 20 x 20 x 2 inches in nominal size. It was identified by nameplate as a Farr Type 44G.

The filtering media was composed of layers of 14-inch mesh screen wire in strips arranged and piled in alternate layers of flat and v-crimped screen. The media was held together at the edges by a steel retaining frame. There were approximately 4 layers of flat screen and 4 layers of v-crimp screen per inch of pile.

The filter had actual outside dimensions of $19 \ 1/2 \ x \ 19 \ 5/8 \ x \ 2$ inches, and had a free opening $18 \ 3/8 \ x \ 18 \ 1/4$ inches in size (2.33 ft² net face area). It weighed 10.2 lb when clean, without oil.

The manufacturer submitted an adhesive designated as "Green Bloom 100" for oiling the filter. This was done in preparation for test by immersing the filter in the liquid and letting the excess oil drain off at a temperature of 75° F or above, with the filter standing on edge for a minimum of 24 hours prior to the test.

III. TEST METHOD AND PROCEDURE

The dust-arresting efficiency of the filter was determined by the NBS "Dust Spot Method" using as a test dust Cottrell precipitate at a concentration of one gram per thousand cubic feet of air. The test method is described in the paper "A Test Method for Air Filters" by R. S. Dill (ASHVE Transactions, Vol. 44, p. 379, 1938).

Dirt-holding capacity was determined by supplying to the filter air in which were dispersed cotton lint and Cottrell precipitate in the approximate proportions of 4% and 96% by weight, respectively. The average rate of feed of the contaminants was not more than 25 grams per hour per square foot of net filter face area at each face velocity. The lint used for this purpose was No. 7 cotton linters ground in a Wiley mill with 4 mm screen.

The efficiency and dirt-loading tests were made at three different air velocities, namely, 300, 600, and 900 fpm.

In the tests at each velocity, the following uniform procedure was employed. The clean filter, after oiling and draining as described above, was installed in the test duct and its initial pressure drop was measured at 300, 600, and 900 fpm air velocity. The initial efficiency of the filter at the test velocity was then determined, following which the process of loading the filter with a mixture of 4% lint and 96% Cottrell precipitate by weight was started. At intervals, the increasing pressure drop of the filter was recorded. At suitable periods as loading progressed, the efficiency of the filter was determined using 100% Cottrell precipitate. In addition, the efficiency of the filter was determined at the end of a day of loading, and at the start of the next day, to ascertain whether the rate of dirt loading was overtaxing the wetting rate of the filter adhesive. The dirt loading was continued, in general, until the rate of pressure drop rise increased to approximately 0.004 inch W.G. per gram of dirt mixture fed per square foot of filter face area.

The filter was then removed from the test duct and cleaned by means of a stream of cold water from a high-pressure hose nozzle, directed at and into the filter media. After drying, the filter was reoiled for subsequent tests or for measurement of its initial pressure drop after the final cleaning.

IV. TEST RESULTS

Table 1

The pressure drop of the clean oiled filter, in inch W.G., at 300, 600, and 900 face air velocity, was measured at the start of each of the tests and after the 900 fpm test, as shown in Table 1.

Face Velocity, fpm	300	600	900
At start of 300 fpm test At start of 600 fpm test At start of 900 fpm test After 900 fpm test	0.037 .041 .043 .043	0.131 .143 .154 .155	0.275 .299 .318 .325
Increase in P.D. after 3 cleanings, percent	16	18	18

A summary of the test data obtained in dirtloading tests conducted at 300, 600, and 900 fpm face velocity is given in Table 2

Table 2

Face Air			
Velocity fpm	<u>Dirt Load*</u> grams/sq ft	Pressure Drop inch WG	Efficiency percent
300	0 3 5 72 75 155 196 199 251 274 289 302 305 323	0.037 .037 .037 .057 .053 .076 .097 .091 .161 .215 .285 .342 .358 .535	54 53 50(P) 52(A) 53(P) 53(A) 58 64 68 69(P) 70(A) 78

*Average mixture: 3.9% lint, 96.1% Cottrell precipitate by weight. Average rate of dirt loading: 16.6 grams per square foot per hour.

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Table 2 - continued

Face Ai <u>Velocit</u> fpm	r y <u>Dirt Load*</u> ġrams/sq ft	Pressure Drop inch WG	Efficiency percent
600	0 6 12 120 126 161 232 252 258 294 338	0.143 .145 .148 .205 .250 .228 .258 .360 .393 .412 .525 .761	60 62 62 63(P) 63(A) 62 64 64(P) 64(A) 71 73
*Averag by Averag foo	ge mixture: 4.0% l: weight. ge rate of dirt log t per hour.	int, 96% Cottre ading: 21.6 gram	ll precipitate ns per square
900	0 9 17 106 160 169 240 286 295 330	0.318 .320 .328 .501 .571 .563 .703 .810 .840 1.016	65 63 69 70(P) 68(A) 76 76(P) 75(A) 77
*Averag by w Averag foot NOTE:	ge mixture: 4.0% liveight. ge rate of dirt los per hour. Efficiencies mark tions made at the at the start of the respectively.	int, 96% Cottrei ading: 22.2 gran ed (P) or (A) we end of a day of he next day of 1	ll precipitate ns per square ere determina- f loading, and loading,

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V. SUMMARY OF RESULTS

A. Performance

The test data are plotted in Figure 1, which shows the variation of the pressure drop and of the efficiency of the filter as it was subjected to increasing specific dirt loading at face velocities of 300, 600, and 900 feet per minute.

Table 3 presents values of the pressure drop (P.D.) in inches of water, and of the approximate efficiency (Eff.) in percent, as taken from the curves of Figure 1, at various specific dirt loadings.

Table 3

Spec. Dirt Ldg.grams/ sq ft	· ′0 (Initial)		100		200		.300	
Face Vel. fpm	P.D.	Eff:	P.D.	Eff.	P.D.	Eff.	P.D.	Eff.
300 600 900	0.04 .14 .32	54 60 65	0.06 .24 .49	52 63 69	0.09 .31 .63	53 63 69	0.33 .55 .85	69 71 75

B. Cleanability

The pressure drops of the clean oiled filter at 300, 600, and 900 fpm face velocity recorded in Table 1 under Test Results indicate that, after the filter had been subjected to three loadings with the dust-lint mixture and three cleanings and re-oilings, its average percentage increase in pressure drop was about 17.3 percent, or about 5.8 percent per loading and cleaning operation. However, although these readings seem to indicate a gradual build-up of filter resistance. thorough visual examination of the filter media after cleaning at the end of the tests revealed no perceptible dirt deposits not removed by the washing operation. The adhesive furnished by the manufacturer and used for oiling the media was unusually viscous - it was estimated to have a viscosity not less than that designated as

SAE 50. It is possible that the changes in filter pressure drop were due to variations in the amount of the oil retained after the oiling and draining operation, which, however, was carried out in a uniform manner. In view of the fact that the filter appeared thoroughly clean at the end of the tests, it is believed it can be considered as satisfactorily cleanable.

C. General

The fact that efficiencies determined at the end of a day of loading of the filter (those marked (P) in Table 2) were approximately the same as those made at the start of the next day of loading (those marked (A)) indicates that the dirt-loading rates to which the filter was subjected did not overtax the wetting-rate of the filter adhesive and cause the filter surfaces to become "dry". FARR 44 G



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THE NATIONAL BUREAU OF STANDARDS

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