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# NATIONAL BUREAU OF STANDARDS REPORT

2560

A TESTING PLAN FOR CEMENT

By

.

W. H. Clatworthy, W. S. Connor, and D. N. Evans

**U. S. DEPARTMENT OF COMMERCE NATIONAL BUREAU OF STANDARDS** 

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#### FOREWORD

This report illustrates a statistical approach of wide applicability, and was prepared in the Statistical Engineering Laboratory of the National Bureau of Standards, for the information and use of the Bureau's Mineral Products Division.

> Churchill Eisenhart Chief, Statistical Engineering Laboratory

A. V. Astin Director National Bureau of Standards . .

#### A TESTING PLAN FOR CEMENT

Ву

W. H. Clatworthy, W. S. Connor, and D. M. Evans

1. Introduction. This report studies the amount of testing which is being done by the National Bureau of Standards of cement produced by the Hermitage plant at Nashville, Tennessee. The object of the report is to determine whether the present testing program provides enough testing or too much testing of Hermitage production, and if too much, to suggest an alternative program. Such an alternative testing program should be simple to apply and applicable to the production of any plant.

The data studied were taken from the files of the Concreting Materials section of the Mineral Products division (9.6) of the National Bureau of Standards. The data are the results of tests made on grab samples taken from Hermitage production of Type II cement during the period January, 1952 through May, 1953. The properties studied are sulphur trioxide  $(SO_3)$ , silicon dioxide  $(SiO_2)$ , aluminum oxide  $(Al_2O_3)$ , magnesium oxide (MgO), autoclave expansion, 7-day strength, and air permeability fineness (A.P.F.).

Most bins sampled contained 4500 barrels, from which 9 samples were taken. Except for fineness, composite samples were formed from the first and second sets of four samples each, leaving a single sample to be tested as an individual. Fineness determinations were made of each of the 9 individual samples. From these we have chosen the first and fifth. For the purposes of this study the data have been split into test results for composite samples, which are given in Table 1, and those for individual samples, which are given in Table 5.

A proposed testing plan is described in section 3, applied to tests of composite samples in section 4, and applied to tests of individual samples in section 6. The reasoning underlying the plan is developed in section 5. The conclusions are presented in the following section.

2. <u>Conclusions</u>. The testing plan which is described in section 3 is simple to apply, and can be used either for composite samples or for individual samples. If it had been applied to the Hermitage plant from the middle of October, 1952 to the middle of May, 1953, then for SO<sub>3</sub>, SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, MgO, autoclave expansion, and 7-day strength it would have reduced the number of tests from 762 to 333. For SO<sub>3</sub> the proposed testing plan would not have materially reduced the number of tests. However, for the other properties considered the number of tests would have been reduced to approximately one-third as many tests as were actually made. This reduction would have been achieved at no appreciable increase in the risk of failing to detect violations of the specifications.

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The plan is general. Barring some factors or conditions not found in the cement studied, it can be applied to grab samples from any plant and to properties other than those studied. It also can be modified to apply/and other samples.

3. <u>The testing plan</u>. We can best describe the testing plan by applying it to a particular property. So let us trace the application to SO<sub>3</sub> composites. For the sake of realism we shall suppose that it was decided to put the plan into effect in October, 1952, when results for bins 1 through 32 were available, but before bin 33 had been tested.

The steps in the application of the plan are as follows:

(1) From the files take the first test result for each of the last 32 bins, dividing them into groups of 8 each. These results (from Table 1) are as follows:

		Grou	up	
	<u>1</u>	2	<u>3</u>	4
Distance in the second s	1.4 1.6 1.7 1.1 1.6 1.6 1.4 1.2	1.5 1.7 1.4 1.6 1.5 1.6 1.5 1.5	1.4 1.6 2.1 1.6 1.7 1.8 1.6 1.6	1.8 1.7 2.0 1.8 2.0 2.0 1.9 2.0

We emphasize that only the first result from each bin is used.

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(2) Determine the range, r, of each group. The range is the difference between the largest and the smallest number in the group, so that the ranges are as follows:

		Group		
Largest Smallest Range (r <sub>i</sub> )	1.7 1.1 0.6	$\frac{2}{1.7}$ $\frac{1.4}{0.3}$	3 2.1 1.4 0.7	$\frac{4}{2.0}$ $\frac{1.7}{0.3}$

(3) Compute the average range,  $\overline{r}_1$ , thus:

 $\overline{\mathbf{r}}_{1} = (\mathbf{r}_{1} + \mathbf{r}_{2} + \mathbf{r}_{3} + \mathbf{r}_{4})/4$ = (.6 + .3 + .7 + .3)/4 = 0.475

(4) Subtract 0.7025  $\mathbf{F}_1$  from 2.0. (If the property has a minimum specification, add 0.7025  $\overline{\mathbf{r}}_1$  to the specification instead of subtracting.) Round off to the same number of decimal places as are recorded for the test results. Obtain

$$2.000 - (0.7025)(0.475) = 1.666$$

and round off to 1.7. We shall call this value F(Frequent) to denote the limit for frequent testing.

(5) Subtract 0.7025  $\overline{r}_1$  from 1.666. (If the property has a minimum specification, add.) Obtain 1.334 and round to 1.3. We shall call this value I (Infrequent) to denote the limit for infrequent testing.

.7025 = <u>m(28d.f.)</u> = 2.0 de = 2.0 7.11, on p.54 F) office. (3] Note: per practice and take gives only 2 digits (6) (Optional but recommended.) Make up a chart, such as Figure 1, showing the specification, the 32 test results, and the numbers F and I. The specification line should start with bin 1 and extend as far into the future as is feasible. The F and I lines should extend from bin 33 through 64.

The preliminary calculations are complete, so the plan may now be put into operation. The first new test result, which in our case occurs for bin 33 will determine the testing rate. If it is greater than or equal to F, we shall test frequently (two tests per bin) but if it is less than F we shall test infrequently (one test per bin). As it turns out (see Table 1 or Figure 1), the first new test result is 2.1 which exceeds F = 1.7, so that we start out testing frequently. Frequent tests continue until a test result is less than I, which is the signal for infrequent testing. The first such result occurs for bin 38, when the test result drops to 1.1, less than I = 1.3, so that we switch to infrequent testing. This continues until test result 1.7 is reached for bin 40, which again orders frequent testing. Since no further test result is as small as I, frequent tests are run for the remaining bins. Although for SO F and I are unchanged throughout our illustration, we shall see below that there is, in general, the possibility that they will change after each 32 additional bins.

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(7) This step is designed to keep a check on the stability of the range. When the test results for bins 33 through 64 become available, divide the first test results of the bins into 4 groups of 8 each, and compute the range of each group, and the average range,  $\overline{r}_2$ . Then form the ratio of the larger of  $\overline{r}_1$  and  $\overline{r}_2$  to the smaller. If the ratio is less than 1.5, continue to use F and I as previously computed through bin 96. If step (6) is in use, we now extend our original F and I lines through bin 96. If the ratio is as great as 1.5, use  $\overline{r}_2$  to recompute F and I according to steps (1) through (5), and draw new F and I lines. After each additional 32 bins, we compare the new  $\overline{r}$  with the  $\overline{r}$  in use to decide whether we need to recalculate F and I.

For SO<sub>3</sub> the calculations are as follows:

#### Group

	1.9 1.9 2.0 1.4 1.1 1.6 1.7	1.8 1.7 1.7 1.7 1.9 1.6 1.8 2.0	3 1.6 1.7 1.8 1.8 1.7 1.8 1.6 1.4	4 1.7 1.6 1.7 1.4 1.7 1.8 2.0
Largest	2.1	2.0	1.8	2.0
Smallest	1.1	<u>1.6</u>	<u>1.4</u>	1.4
Range(r <sub>i</sub> )	1.0	0.4	0.4	0.6

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$$\overline{\mathbf{r}}_2 = (\mathbf{r}_5 + \mathbf{r}_6 + \mathbf{r}_7 + \mathbf{r}_8)/4$$
$$= (1.0 + 0.4 + .04 + .06)/4 = 0.600$$
$$\overline{\mathbf{r}}_2/\overline{\mathbf{r}}_1 = .600/.475 = 1.26$$

Since 1.26 is less than 1.50, we continue to use F = 1.7 and I = 1.3. Thus, the F and I lines have been extended through bin 74 in Figures 1 and 4, and in practice would be extended through bin 96. This complete the description of the plan.

It is apparent that with rare exceptions SO<sub>3</sub> needs frequent testing. The testing plan would have reduced the number of tests by only four tests. We determine this by remembering that two composite samples and one individual sample actually were tested on all bins except bin 51, for which three composites and one individual were tested. Hence, if when our plan requires frequent tests we include the individual sample for each bin, we find that one composite and one individual test would have been saved for each of bins 38 and 39. This is a reduction of 4 tests out of 127 tests.

4. <u>Application of the plan to composite samples for</u> <u>several properties</u>. We have seen that SO<sub>3</sub> is running so close to the specification that frequent testing is almost always necessary. We now shall consider composite sample test results for several other properties, SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, MgO, 7-day strength, and autoclave expansion. These results are given in Table 1.

We shall see that the testing plan of section 3 would have required many fewer tests than actually were made during the period considered.

Table 2 supplies the necessary calculations for determining F and I. Perhaps the most striking property for which infrequent tests would have sufficed throughout the period is autoclave expansion. Autoclave never came close to specification, nor for that matter to I. The testing plan for autoclave is vividly depicted in Figure 2. The first test result for bin 33, .15, is much smaller than I = .38, so from m the beginning the plan calls for infrequent testing. Since the largest test result during the period was .33 (bin 67), much less than F = .44, the plan never requires frequent testing.

Let us count the saving in the number of tests which the testing plan would have provided. As the testing was really done, one individual and two composite tests were run on every bin but one, and that bin (bin 51) had three composites and one individual, giving a total of 127 tests. The testing plan, on the other hand, would have required only one test per bin, or 42 tests altogether. Thus, the plan would have cut the number of tests to one-third.

The same saving would have been realized for  $\text{SiO}_2$ ,  $\text{Al}_2\text{O}_3$ , MgO:, and 7-day strength. Using only the first sample for each bin the smallest test result for SiO<sub>2</sub> was 21.9 (bin 73), greater

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than F = 21.6; the largest for  $Al_2O_3$  was 5.3 (bins 62 and 72), less than F = 5.6; the largest for MgO was 4.4 (bin 72), less than F = 4.5; and the smallest for 7-day strength was 1960 (bin 60) greater than F = 1,870. Hence, for each of these properties infrequent testing would have sufficed.

To summarize, the testing plan would have reduced the number of tests for each of autoclave,  $SiO_2$ ,  $Al_2O_3$ , MgO, and 7-day strength from 127 tests to 42 tests, or altogether from 635 tests to 210 tests.

5. <u>Rationale of the testing plan</u>. We consider a testing plan to be a good one if it prescribes frequent tests when it is likely that a sample will violate the specification, but infrequent tests otherwise. The plan which we have described has these characteristics.

To judge whether or not it is likely that a current sample will violate the specification for some particular property, it is necessary to look at the history of that property. If past sample test results were close to the specification, then there is a good chance that the next sample will violate the specification, and frequent tests should be made. On the other hand, if history reveals that the test results were far from the specification, then there is little danger of a violation, and infrequent testing is sufficient.

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The problem is to decide what is meant by a test result being close to or far from the specification. It is apparent that knowledge of the average value of past results, though important, is not enough by itself to decide this. To know, for example, that the last ten test results for autoclave expansion averaged 0.34 percent does not enable us to judge whether or not a new sample will exceed 0.50. Further scrutiny of the data is necessary. If we find that the largest of the ten was 0.48, it will seem quite possible for the new sample to violate the specification, but if the largest was only 0.37, we shall doubt that the new-sample will exceed 0.50. The average, then, has to be accompanied by a measure of the variation, and these two measures together form the basis for a sound sampling plan.

In the following remarks we shall assume that the test results are approximately normally distributed. Although we have not investigated their distribution, there is no reason to expect any serious departure from normality.

We chose the range as the measure of variation because (i) it is easy to calculate and (ii) there are long-run shifts in the average levels of the properties, which suggests that the data should be divided into groups of consecutive observations and the variation estimated within each group, a situation

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in which the range is nearly as efficient an estimator of the variation as is the theoretically preferred standard deviation [1]\*.

Under certain circumstances, theoretical considerations show that the average of the ranges of groups of 8 tests each is a better estimator of the variation than the corresponding average for groups of any other size [2]. For this reason we have used groups of 8 tests each.

For each bin several samples are available for testing, whether we test them or not. The problem of how many samples to test for a bin can be answered by testing the first sample and judging how close the result is to the specification. This judgment should be made by consideration of the variation among samples from the same bin. The ranges which we use, based as they are on one sample per bin, do not measure this variation, but rather measure the variation among samples from different bins. We prefer to use them, however, because they are convenient, requiring only one test per bin, and they are conservative, since they tend to overestimate the variation within bins.

\* See reference at end of text.

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That the variation among samples from different bins exceeds the variation among samples from the same bin is brought out by Table 4. The numbers in the table were computed from the results for bins 49 through 74. The last column, "Estimated variance (or variation)", is of main interest because the first number there (between bins) estimates the variation among samples from different bins and the second number (within bins) estimates the variation among samples from the same bin. For every property the former exceeds the latter, and for some properties is several times larger.

The number F has been chosen such that if the true average for the property is equal to F, then the chance that a test result will violate the specification is only about 25 in 1,000 [3]. This is a conservative choice of F, as we shall see. Suppose that the history of the property is such that infrequent tests have been made in the recent past, but the current test result is equal to F or lies between F and the specification. We at once switch to frequent testing, taking the dim view that the true average for the property may be at least as close to the specification as F, even though the current result could be due only to sampling fluctuations or testing error when in reality the true average is not as close to the specification

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as F. Thus unless there is a marked trend in the data, the chance of the next test result violating the specification is not greater than about 25 in 1,000.

The number I has been chosen similarly. If the true average for the property is equal to F, then the probability of obtaining a test result which is as far from F as I is only .025. Thus, we do not resume infrequent sampling until it becomes virtually certain that the true average is not as close to the specification as F.

These remarks assume that the true variability does not change. If there is an increase or decrease in the true variability, then the probability, .025, will increase or decrease, respectively. Small changes in the variability will not affect this probability much, and so may be ignored. However, a sizeable change must be taken into account, and it is for this reason that step (7) of the plan (section 3) is included.

If  $\overline{r}_1$  is the average of the ranges from 4 groups each of size 8 and  $\overline{r}_2$  is a similar measure from 4 other groups, then there is good reason to believe that the probability that the larger of  $\overline{r}_1$  and  $\overline{r}_2$  will exceed the smaller by as much as 1.5 (when in reality they estimate the same variation) is small. Hence, we do not recompute F and I unless there is a good chance that the variation between bins really has changed.

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1.5×2.8472 = 0,2708 PS R. 5 4,2708 53 2 .95

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To obtain a graphic picture of the stability of the range for SO<sub>3</sub>, autoclave expansion, and 7-day strength, we have plotted ranges of groups of 4 test results each in Figures 4 and 6. Also given are the average range,  $\overline{R}_1$ , for the first 8 groups and a control limit which is determined from  $\overline{R}_1$ . Summary calculations for Figure 4 are given in Table 3. The control limit (L in Table 3) is determined such that the chance of an individual range exceeding it if  $\overline{R}_1$  were equal to its expected value is only about 15 in 10,000. The fact that no individual ranges exceed the limit for any of the groups 1 through 18 attests to the stability of the process variation. This is further confirmed by calculation of  $\overline{R}_2$  from the ranges of groups through 16. In no case is  $\overline{R}_2$  very different from  $\overline{R}_1$ .

6. <u>Application of the testing plan to individual samples</u>. The testing plan of section 3 applies to individual samples equally as well as to composite samples. In Table 6 we have determined F and I for individuals for all of the properties already treated for composites, and in addition, A.P. fineness.

Since only one individual sample is available from each bin, it is impossible to show on a chart all of the test results which would be required by frequent sampling. However, Figure 5 gives a plot of the available test results for 7-day

L ans 1able 3 = 2 = 8 R. Z(R,) = 2.8472 5 P[ B < GOOD 1 75 . 999 85 1 103,867 2 7.26

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strength, together with the minimum specification and the F and I lines. In practice, when a sample result is as small as F, several samples would be tested for each bin.

As one would expect, the variation among individuals tends to exceed that among composites. This can be seen by comparison of the ranges of Table 6 with those of Table 2. For 7-day strength the difference in ranges is reflected in an increase in F from 1,870 for composites to 2,080 for individuals, and an increase in I from 2,250 for composites to 2,650 for individuals.

In the application of the testing plan to 7-day strength, composite samples never required frequent testing, but individual samples oten did. In fact, the available test results for individuals ordered frequent tests beginning with bins 33, 50, and 61. For other properties studied, the plan when applied to individuals requires about the same number of tests as when applied to composites.

For autoclave, since  $\overline{r}_1/\overline{r}_2 = 1.5$  (see Table 6), F and I should be recomputed and the new values used for bins 65 through 96. F and I would then be .43 and .37, closer to the specification.

7. <u>Acknowledgment</u>. The authors wish to thank Dr. E. P. King (11.3) for advice about technical aspects of the use of the range.

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# Table 1

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# TEST RESULTS FOR COMPOSITES

Bin N	o. Sample Date	Bin	<sup>S0</sup> 3	Si0 <sub>2</sub>	A12 <sup>0</sup> 3	Mg0	7-Day Str.	
l	1/4-5/52	S-1-2	1.4	23.0	4.9	3.1	2000	.15
<u></u> 2	1/21-22/52	s-4-2	1.4	23.0	4.8 4.8	3.2	2000 1850	•15 •12
3	2/7-8/52	S-1-3	1.4	22.8 22.5	4.9	3.2	1680 1790	•17 •20
4	1/25-26/52	S-5-7	1.6	22.6	5.3 5.3 5.1	3.6	1660 1480	.22 .15
5	3/3-4/52	<b>S-4-</b> 3	1.1	23.0 22.5	5.1	3.4	1520 1910	.16 .18
. 6	3/12-13/52	s-5-8	1.4	23.0 22.4	5.2 4.7	3.4	1500 2060	.16 .11
7	3/25 <b>-</b> 26/52	s-1-4	1.4	22.4	4.8	3.0	2220 2020	.11 .12
8	4/2-3/52	s-4-4	1.4	22.4 22.4	4.6	2.9	2010 2250	.13 .13
9	4/11 <b>-</b> 12/52	s-5-9	2.0	22.1 22.2	4.9 4.8	3.4 3.5 3.7	2210 2260	•11 •11
10	4/28-29/52	S-1-5	1.2	22.4	5.1	3.1	1890 2220	.17
11	5/14-15/52	<b>S-2-</b> 2	1.4	22.5	4.8 4.6	3.2	2210 2090	•13 •16
12	5/26 <b>-28/</b> 52	0-1-3	1.6 1.6	22.6 22.7	4.5	3.3 3.1	2100 2510	.17 .12
13	6/4-5/52	<mark>8-4-</mark> 5	1.5	22.9	4.3	3.1	2300 2480 2140	•13 •13
14	6 <b>/9-</b> 10/52	S-1-6	1.4	22.9	4.4	2.9	2460 2350	•14 •13
15	6/12 <b>-</b> 13/52	S-5-10	1.5	22.7	4.9	2.9	2050 2350	.14 .12
16	6/23 <b>-</b> 25/52	S-2-3	1.5 1.5 1.4	22.7 22.9	4.6	3.1 3.2	2440 2340 2140	.13 .12 .11
17	6 <b>/</b> 30/7 <b>-</b> 1/52	S-3-7	1.4 1.6	23.0 23.1 23.1	4.4	3.2 3.2 3.2	2460 2000 2250	•14 •13
18	7/14-15/52	<b>S-</b> 4-6	1.6	22.4	4.3	4.1	1860 1800	•17 •21
19	7 <b>/17-1</b> 8/52	S-1-7	2.1	21.7	4.8	4.1	2040 1680	•15 •16
20	7/30-31/52	S-5-11	1.6	22.2 22.3	4.6 4.6 4.6	3.3 3.8 3.7	2410 2550	•18 •16

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Table 1 (Continued)

Bin 1	No. Sample Date	Bin	<sup>S0</sup> 3	Si0 <sub>2</sub>	Al2 <sup>0</sup> 3	Mg0	7-Day Str.	Auto- clave
21	8/4-5/52	s-2-4	1.7 1.5	22.4	4.2	3.0 3.1	2250 2080	.11 .12
22	8/6-7/52	S-3-8	1.8 1.6	22.1 22.3	4.0	3.1 3.3	1860 2010	•12 •11 •09
23	8/13-14/52	S-1-8	1.6	22.7	4.0	2.8	1980 2160	•09 •06 •06
24	8/18-19/52	S-4-7	1.6	23.0	4.2	2.8 2.8	2170 2280	.06
25	9/2-3/52	S <b>-5-1</b> 2	1.7 1.8 2.0	23.0 22.9 22.4	4.5	3.2	1980	•06 •10
26	9/4-5/52	s <b>-2-</b> 5	1.7	22.6 22.8	4.5	3.1	2470 2120 2160	.10 .10
27	9 <b>/11-12/</b> 52	S-3-9	1.6 2.0 1.8	22.8	4.7 4.9	3.1 3.0	1880	.11 .12
28	9 <b>/15-16/</b> 52	S-1-9	1.8	22.9	4.8	3.2	2140 1990	.12 .17
29	9/18 <b>-</b> 19/52	s-4-8	1.8	22.8 22.6	5.0 4.8	2.9	2000 1980	•18 •14
30	9/29 <b>-</b> 30/52		2.0	22.5	4.8	2.7	2070 2190	.16 .18
31	10/1/52	S-2-6	2.0	22.5 22.8	4.8 5.0	2.9	2210 2100	•15 •18
32	10/3 <b>-</b> 4/52	S <b>-</b> 3 <b>-</b> 10		22.5 22.5	5.0	2.9	2480 2270	.20 .11
33	10/7-8/52	S-1-10		22.3	4.9 4.8	3.0	2330 1990	.13 .15
34	10/7-8/52	s-4-9	1.8	22.6 22.5	4.9 4.8	2.9 3.1	2070 2120	.18 .13
35	10/22-23/52	<b>S-5-1</b> 4		22.5 22.5	4.7	3.1	2200 2310	.16 .10
36	10/23 <b>-</b> 25/52	S-2-7	1.8 2.0 2.0	22.7 22.8	4.7	2.9	2170 2090	.13 .14
37	11/1 <b>-</b> 2/52	S-3-11	1.4	22.6	4.8 4.7	2.9	2120 2560	.12
38	11/3 <b>-</b> 4/52	S-1-11		23.1 22.7	4.6	2.6	2500 2630	.11
39	11/5 <b>-</b> 6/52	S-4-10		22.5 22.3	4.5	3.0	2620 2260	•09 •09
40	11/11 <b>-</b> 12/52	S-5-15		22.4 22.5	4.3	.3.0		.08 .11
41	11/13 <b>-1</b> 4/52	S-2-8	1.7 1.8 1.7	22.5 22.6 22.7	4•7 4•6 4•7	3.4 3.3 3.3	2090 2 <b>1</b> 30 2170	.12 .13 .11

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Table 1 (Continued)

Bin N	o. Sample Date	Bin	<sup>S0</sup> 3	Si0 2	Al 23	MgO	7-Day Str.	Auto- clave
42	11/25-26/52	S-3-12	1.7	22.7	4.5	3.0	2360	•10
43	11/28-29/52	S-1-12	1.6 1.7	22.7	4.6	3.0 3.0 3.0	2370 2080 2050	.20 .09 .10
- 44	12/2-4/52	s-4-11	1.5 1.7 1.7	22.7 23.0 22.9	4•9 4•8 4•8	2.7	2210 2260	.07 .08
45	12/15-16/52	s-5 <b>-1</b> 6	1.9	22.9	4.4	2.9	2640 2400	•07 •08
46	12/18-19/52	S-2-9	1.6 1.6	22.6	4.7	2.9	2700 2690	.10
47	12/26-27/52	S-3-13	1.8	22.4 22.5	4.7	3.3	2550 2530	.11 .11
- 48	12/29-30/52	S-1-13	2.0	22.6 22.7	4.8	3.3	2430 2360	.12 .13
49	1/5-6/53	S-4-12	1.6	22.6 22.7	4.5	3.2	25 <b>10</b> 2350	.10 .10
50	1/21-22/53	S-2-10	1.7	22.7	4.9	3.3	2160 2160	.12 .13
51	1/26-28/53	0-5-4	1.8 1.8	22.3	4.9 5.2 5.2	3.9	2080 2490	.20 .19
52	1/19-20/53	S-5-17	1.8	22.8	4.8 4.8	3.0 3.1	2120 2080	.09 .10
53	1/30-31/53	S-3-14	1.7	22.4 22.3	4.9	3.5	2550 2550	.08 .17
54	2/4 <b>-</b> 5/53	<b>S-1-1</b> 4	1.8	22.9	5.0	3.2	2100 2090	•13 •15
55	2/26-27/53	<b>S-2-11</b>	1.6 1.5	22.6	4.9	3.4	2210 2390	.11
56	2/28-3/1/53	S <b>-3-</b> 15	1.4	22.7	4•7 4•9 5•0	3.4 3.6 3.9	2230 2180	•14 •15
5 <b>7</b>	3/2 <b>-</b> 3/53	<b>S-4-1</b> 3	1.7	22.5	4.9	4.0	2100 2100 1940	•19 •17 •19
58	3/6-7/53	S <b>-1-1</b> 5	1.7	22.5	4.9	4.1	2380	.12 .12
59	3/4-5/53	<b>S-5-1</b> 8	1.5	22.3	4.9	3.2	2540 2230	.16
60	3/18-19/53	S-2-12	1.6 1.8 1.7	22.2	4.9	3.4643999 3.3.3.9.99	2190 1960	.17 .12
61	3/23 <b>-</b> 24/53	S-3-16	1.9	23.0	4.0 5.1	3.9	2000 2060	.12 .18
62 `	3/25- 26/53	s-4-14	1.6	22.7 22.3	5.3	4.0	2000 2340	.18 .22
63	3/27-28/53	S-5-19	1.4 1.8 1.7	22.5 22.5 22.6	4.8 5.2 5.0 5.0 10	4.2 3.9 3.9	2100 2060 1820	.23 .18 .20

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Table 1 (Continued)

Bin	No.	Sample Date	Bin	S0 3	Si0 <sub>2</sub>	Al203	Mg0	7-Day Str.	Auto- clave
64	. 3/	/30-31/53	S-1-16	2.0 1.5	22.1 22.5	5 <b>.1</b> 5 <b>.</b> 2	4.1 4.1	2060 1840	•26 •22
65	° 4/	/8-9/53	S-3-17	1.7 1.8	22.4 22.5	5.2	4.2	2100 1980	•20
66	4/	/2-3/53	S-2-13	1.7	22.5	5.2	4.1 3.9	2340	•19 •19
67	4/	/13-14/53	` <b>s-4-1</b> 5	1.7 2.0	22.5	5•3 4•9	4.1	2220 2540	•21 •33
68	4/	/15-16/53	S-5-20	1.7	22.1	4.8 4.9	4.6 4.1	2350 2260	•31 •32
69	4/	<b>/17-1</b> 8/53	S-1-17	2.2	21.8 22.0	5.0 5.0	4.2 4.1	2380 2480	•27 •21
70	4/	/27-28/53	s-2-14	1.7	22.4	5.1 5.1	4.1	2170 2470	.25
71	5/	<b>/1-</b> 2/53	s-4-16	1.7 2.0	22.3	5.1 4.8	4.0	2360 2530	•26 •22
72	5/	/5-6/53	S-5-21	1.8	21.9	5.0 5.3	4.1	2640 2460	.20 .29
73	4/	/29-30/53	S-3-18	1.7 2.1	22.1	5.2 4.9	4.3	2480 2610	•27 •20
		/8-9/53	<b>S-1-1</b> 8	2.0 1.6 1.5	21.9 22.2 22.2	5.2 4.9 5.1	4.0 4.3 4.2	2430 2600 2740	•21 •28 •30

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### Table 2

.

CALCULATION OF F AND I FOR COMPOSITES

	<sup>S0</sup> 3	si) <sub>2</sub>	Al203	MgO	Auto- clave	7-Day Strength
$r_{1}$ $r_{2}$ $r_{3}$ $r_{4}$	0.6 0.3 0.7 0.3	0.6 0.7 1.4 0.6	0.7 0.4 0.6 0.5	0.6 0.6 1.3 0.4	.09 .05 .12 .08	7 <b>7</b> 0 420 550 390
$\Sigma r_{i}$ i=1	1.9	3.3	2.2	2.9	•34	2130
r-1 Fl	0.475	0.825	0.550	0.725	0.085	532.5
0.7025r	0.334	0.580	0.386	0.509	0.0597	374.1
Max. Spec.	2.0		6.0	5.0	0.5	
Min. Spec.		21.0				1500
Ŧ	1.7	21.6	5.6	4.5	0.44	1870
I	1:3	22,2	5.2	4.0	0.38	2250
r r 6 r 7 8	1.0 0.4 0.4 0.6	0.9 0.6 0.6 0.8	0.4 0.4 0.7 0.6	0.5 0.6 0.9 0.8	.06 .06 .12 .14	640 6 <b>20</b> 470 420
Σr i=5_i	2,4	2.9	2.1	2.8	•38	2150
1=5_r r2	0.600	0.725	0.525	0,700	•095	537•5
Ratio of T's	1.26	1.14	1.05	1.04	1.12	1.01

### Table 3

CALCULATION	OF	R <sub>l</sub> ,	L,	AND	R <sub>2</sub>	FOR	RANGE	CONTROL	CHARTS
			FOF	R COI	MPOS	SI TES	5		

	so <sub>3</sub>	Si0 <sub>2</sub>	A1203	MgO	Auto- clave	7-Day Strength
RI2 RR3 RR3 RF2 R7 R7 R7 8	0:6 0:4 0:3 0:1 0:7 0:2 0:3 0.1	0:5 0:15 0:5 1:4 0:3 0:3	0:5 0:3 0:4 0:4 0:4 0:4 0:4	0:5 0:4 0:3 1:0 0:2 0:2	-08 -07 -05 -01 -04 -05 -07 -07	520 340 420 140 550 390 240 290
8 <sup>8</sup> ∑ R <sub>i</sub> i=1	2.7	4.9	2.9	3.4	0:44	2890
$\overline{R}_1$	0.3375	0.6125	0.3625	0.4250	0,0550	361.25
L=2.292R1	0.77	1.40	0.83	0.97	0,126	824
R9 R10 R11 R12 R13 R14 R15 R16	0:2 0:6 0:1 0:4 0:2 0.1 0.1 0.6	000000000000000000000000000000000000000	0:3 0:3 0:4 0:7 0:1 0:2 0.2	0:3 0:5 0:6 0:4 1.0 0.4 0.7 0.2	.05 .03 .06 .05 .05 .05 .08	320 550 280 270 4 <b>30</b> 450 420 280
Σ <sub>R</sub> i=9_1	2.6	4.0	2.5	4.1	0.49	3000
R <sub>2</sub>	0.3250	0.5000	0.3125	0.5125	0.06125	375.00

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### Table 4

COMPARISON OF BETWEEN AND WITHIN BIN VARIATION FOR INDIVIDUALS

Property	Source of Variation	Degrees of Freedom	Sum of E Squares	stimated Variance (or variation)
so3	Between Bins Within Bins Total	25 26 51	1.15 0.56 1.71	0.0460 0.0215
Si02	Between Bins Within Bins Total	25 26 51	4•423 0•365 4•788	0.17692 0.01404
Al 2 <sup>0</sup> 3	Between Bins Within Bins Total	25 26 51	1.71 0.21 1.92	0.684 0.00807
MgO	Between Bins Within Bins Total	25 26 51	8.07 0.35 8.42	0.3228 0.01346
Auto- cl <b>a</b> ve	Between Bins Within Bins Total	25 26 51	0.20155 0,00955 0.21110	0.008062 0.000367
7-Day Strength	Between Bins Within Bins Total	25 26 51	2,221,13 351,95 2,573,08	0 13,536.53

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T.L.

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# Table 5

TEST	RESULTS	FOR	INDIVIDUALS
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Bin No.	Sample Date	Bin	<sup>S0</sup> 3	Si0 <sub>2</sub>	A12 <sup>0</sup> 3	Mg0	7-Day Str.	Auto- clave	A.P.F.*
l	1/4-5/52	S-1-2	1.4	22.9	4.9	3•4	1980	.15	3730
2	1/21-22/52	s-4-2	1.1	23.0	5.0	3.3	1540	•20	3900 3640
3	2/7-8/52	S-1-3	1.6	22.6	5.2	3.6	1560	.25	3940 4330 3790
4	1/25-26/52	S-5-7	1.2	23.0	5.1	3•4	1500	.18	3410 3630
5	3/3-4/52	S-4-3	1.2	23.0	5.2	3.5	1540	•19	3340 3380
6	3/12-13/52	s-5-8	1.8	22.3	4.7	3.0	2140	.10	3640 3510
7	3/25-26/52	<b>S-1-</b> 4	1.4	22.3	4.6	3.0	1960	•13	3480 3520
8	4/2-3/52	s-4-4	1.6	22.2	5.0	3.4	2050	.12	3860 3610
9	4 <b>/11-12/</b> 52	<b>S-</b> 5-9	1.2	22.2	5.0	3.8	1950	•17	3970
10	4/28-29/52	<b>S-1-</b> 5	1.5	22.5	5.0	3.2	2260	.10	3760 3570
11	5 <b>/1</b> 4 <b>-1</b> 5/52	S-2-2	<b>1.</b> 4	22.7	4.5	3.3	2000	.16	3850 3380
12	5/26 <b>-</b> 28/52	0-1-3	1.7	22.8	4.2	3.1	2430	.11	3590 3740
13	6/4-5/52	<b>S-</b> 4-5	1.3	22.9	4.6	2.9	2700	<b>.1</b> 4	3730 3630
14	6/9-10/52	S-1-6	1.5	22.8	4.8	2.9	2150	.13	3860 3570
15	6/12 <b>-</b> 13/52	S-5-10	1.4	22.7	4.6	3.0	2270	•13	3610 3500
16	6/23-24/52	S-2-3	1.6	23.1	4.3	3.2	2630	•11	3740 3590
17	6/30/7-1/52	S <b>-</b> 3-7	1.6	23.1	4.3	3.2	2150,	.15	3610 3470
18	7/14-15/52	S-4-6	1.9	22.3	4.8	3.9	1850	.14	3800 3480
19	7/17 <b>-</b> 18/52	S-1-7	l.7	22.6	4.8	4.2	1320	.26	4250 3940

A.P.F. means A. P. Fineness

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Table 5 (Continued)

Bin No.	Sample Date	Bin	<sup>S0</sup> 3	Si0 2	A1203	MgO	7-Day Str.	Auto- clave	A.P.F.
20	7/30-31/52	S-5-11	1.3	22.5	4.7	3.6	2270	.15	3780
21	8/4-5/52	S-2-4	2.0	22.1	4.4	3.1	2110	.11	3410 3870 3850
22	8/6 <b>-</b> 7/52	S-3-8	2.0	22.2	3.6	3.2	2290	•09	4180 3840
23	8/13 <b>-1</b> 4/52	S-1-8	1.8	22.7	4.2	2.7	2530	.06	3800 3980
24	8/18-19/52	S-4-7	1.7	23.0	4.3	2.9	2240	•09	3540 3670
25	9/2-3/52	S-5-12	1.6	22.4	4.6	3•3	2470,	.11	3730 3570
26	9/4-5/52	S-2-5	2.0	22.3	4.5	3.0	2260	•08	3680
27	9 <b>/11-12/</b> 52	<b>S-</b> 3-9	1.9	22.9	4.8	3.2	2010	.12	3210 3840
28	9/15-16/52	S-1-9	1.9	22.9	5.1	2.9	2010	.17	3250 3490
29	9 <b>/</b> 18 <b>-</b> 19/52	<b>S-</b> 4-8	1.9	22.4	4.8	2.7	2290	.17	3830 3790
30	9/29-30/52	<b>S-5-</b> 13	2.0	22.5	4.8	2.9	2330	•05	3660 4010
31	10/1/52	<b>S-2-</b> 6	1.8	22.2	4.8	2.9	2690	.20	3630 3890
32	10/3-4/52	S-3-10	1.4	22.7	4.9	3.0	2010	-14	3640 3640
33	10/7-8/52	S-1-10	1.7	22.6	4.9	3.0	2060	•17	3710 3830
34	10/7-8/52	<b>S-4-</b> 9	1.7	22.5	4.8	3.1	2230	.14	3520 3530
35	10/22-23/52	<b>S-5-1</b> 4	2.0	22.7	4.8	2.5	1830	.12	4070 3960
36	10/23 <b>-</b> 25/52	S-2-7	1.8	22.7	4.6	2.6	2020	.11	3670 3990
37	11/1 <b>-</b> 2/52	S-3-11	l.7	22.9	4.5	2.8	2500	.10	3550 3 <b>50</b> 0
38	11/3-4/52	S <b>-1-11</b>	1.6	22.4	4.5	3.0	2530	•09	4090 4300
39	11/5 <b>-</b> 6/52	S-4-10	1.8	22.2	4.3	3.1	2550	• 07	4220 3820
40	11/11-12/52	S-5-15	1.6	22.3	4.7	3.5	1930	.12	3790 3730

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Table 5 (Continued)

Bin No.	Sample Date	Bin	<sup>S0</sup> 3	<sup>Si0</sup> 2	Al 2 <sup>0</sup> 3	Mg0	7-Day Str.	Auto- clave	A.P.F.
4 <b>.1</b>	11/13 <b>-</b> 14/52	S-2-8	2.1	22.5	4.7	3.2	2270	.10	3500
42	11/25-26/52	S-3-12	1.6	22.7	4.6	2.9	2560	•09	3570 3940
43	11/28-29/52	S-1-12	1.6	22.8	4.8	3.0	2220	.10	3640 2600 3530
44	12/2-4/52	s-4-11	1.6	22.9	4.8	2.5	2310	• 08	3590 3660
45	12/15 <b>-</b> 16/52	S-5-16	1.8	22.6	4.5	2.9	2820	•08	3800 3730
46	12/18 <b>-</b> 19/52	S-2-9	1.7	22.5	4.8	2.9	2430	•08	3790 3650
47	12/26-27/52	S-3-13	1.8	22.5	4.8	3•3	2280	•13	3980 3730
48	12/29 <b>-</b> 30/52	S <b>-1-</b> 13	1.4	22.6	4.7	3•2	2620	•14	3640 3760
49	1/5-6/53	s-4-12	1.5	23.1	4.5	3.2	2420	•11	3610 3550
50	1/21 <b>-</b> 22/53	S-2-10	1.5	22.9	5.2	3.5	1990	.18	3600 3710
51	1/26-28/53	0-5-4			~ ~ ~				3450 3750
52	1/19 <b>-</b> 20/53	S-5-17	1.8	22.9	4.6	3.0	2140	•09	3480 3350
53	1/30 <b>-</b> 31/53	<b>S-3-1</b> 4	1.9	22.3	4.8	3.4	2650	•19	3450 3720
54	2/4 <b>-</b> 5/53	s-1-14	2.3	22.5	4.9	3.3	2550	.11	3370 3730
55	2/26-27/53	S-2-11	1.5	22.6	4.8	3•3	2360	.12	3300 3670
56	2/28-3/1/53	<b>S-3-1</b> 5	1.6	22.6	4.8	3.8	2480	•13	3200 3640
5 <b>7</b>	3/2 <b>-</b> 3/53	S-4-13	1.4	22.6	4.9	4.1	2210	.18	3440 3300
58	3/6-7/53	<b>S-1-</b> 15	1.7	22.3	4.5	3.4	2660	.12	3550 3790
59	3/4 <b>-</b> 5/53	S-5-18	1.6	22.2	4.5	3.4	2640	.13	3440 3440
60	3/18-19/53	S-2-12	2.0	22.8	4.8	3•4	1960	•13	3390 3350
61	3/23-24/53	S-3-16	1.8	22.2	5.2	3.8	2080	.18	3460 3310

Table 5 (Continued)

Bin No.	Sample Date	Bin	so 3	Si0 <sub>2</sub>	A12 <sup>0</sup> 3	MgO	7-Day Str.	Auto- clave	A.P.F.
62	3/25 <b>-</b> 26/53	<b>s-4-1</b> 4	-1-3	22.8	5.4	4.2	1850	.24	3530
63	3/27 <b>-</b> 28/53	s <b>-</b> 5-19	1.4	22.7	5.1	3•9	2020	.21	3560 3440
64	3/30 <b>-</b> 31/53	S <b>-1-</b> 16	1.7	22.4	5.2	4.1	1960	•20	3360 3330 21110
65	4/8-9/53	S-3-17	1.7	22.5	5.2	4.0	1970	.20	3440 3640 3270
66	4/2-3/53	S-2-13	1.7	22.4	5.2	3.9	2090	.21	3460 3420
67	4/13 <b>-</b> 14/53	s <b>-</b> 4 <b>-</b> 15	1.4	22.3	5.0	4.3	2160	• 34	3570 3590
68	4 <b>/</b> 15 <b>-</b> 16/53	S-5-20	2.3	21.9	5.1	4.1	2370	•25	3670 3380
69	4 <b>/17-18/</b> 53	S-1-17	2.0	22.2	5.2	4.1	2310	•27	4030 3410
70	4/27 <b>-</b> 28/53	<b>S</b> -2-14	1.9	22.2	5.0	4.0	2390	.21	3280 3510
71	5/1 <b>-</b> 2/53	S-4-16	1.7	22.1	5.0	3+9	2630	.20	3520 3530
72	5/5-6/53	S-5=21	1.6	22.3	5.2	4.3	2480	.29	3690 3 <b>7</b> 20
73	4/29 <b>-</b> 30/53	S-3-18	1.3	21.9	5.0	4.1	2240	•23	3650
74	5/8 <b>-</b> 9/53	<b>S-1-</b> 18	1.5	22.2	5.0	4.2	2770	•28	3480 3820

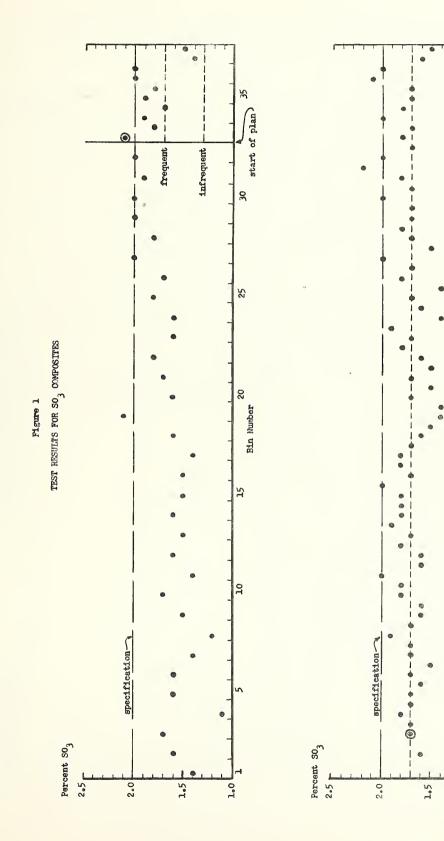
### Table 6

CALCULATION OF F AND I FOR INDIVIDUALS

	<sup>S0</sup> 3	Si02	A1203	MgO	Auto- clave	7-Day Strength	A.P.F.
$\begin{array}{c} \mathbf{r}_{1}\\ \mathbf{r}_{2}\\ \mathbf{r}_{3}\\ \mathbf{r}_{4}\\ \mathbf{r}_{4}\end{array}$	0.7 0.5 0.7 0.6	0.8 0.9 1.0 0.7	0.6 0.7 1.2 0.6	0.6 0.9 1.5 0.6	0.15 0.07 0.20 0.15	640 750 1210 680	990 380 710 620
i=l <sup>w</sup> iy	2.5	3.4	3.1	3.6	0.57	3280	2700
<b>r</b> l.	0,625	0.850	0.775	0.900	0.1425	820	675
0.7025 <b>r</b> 1	0.439	0.597	0.544	0.632	0.100	576.0	474.2
Max. Spec.	2.0		6.0	5.0	0.5		
Min. Spec.		21.0				1500	3000
F.	1.6	21.6	5.5	4.4	0.40	2080	3470
I.	1.1	22.2	4.9	3.7	0.30	2650	3950
r5 r6 r7 r8	0.4 0.7 0.9 0.7	0.7 0.4 0.8 0.6	0.6 0.3 0.7 0.9	1.0 0.8 1.1 0.8	0.10 0.06 0.10 0.12	720 600 660 810	700 1380 410 <u>3</u> 20
Σr.	2.7	2.5	2.5	3.7	0,38	2790	2710
i=5_i r2	0.675	0.625	0.625	0.925	0.095	697.5	677.5
Ratio of r's	1.08	1.36	1.24	1.03	1.50	1.18	1.00
F					0.43		
					0 27		

Ι

0.37





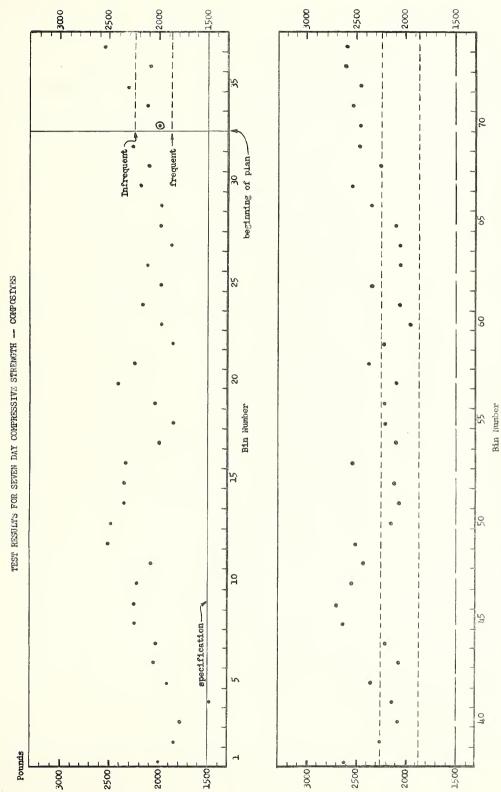
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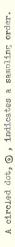


Figure 3

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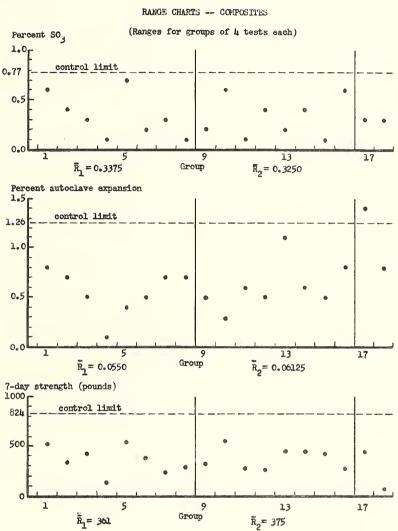


Figure 4

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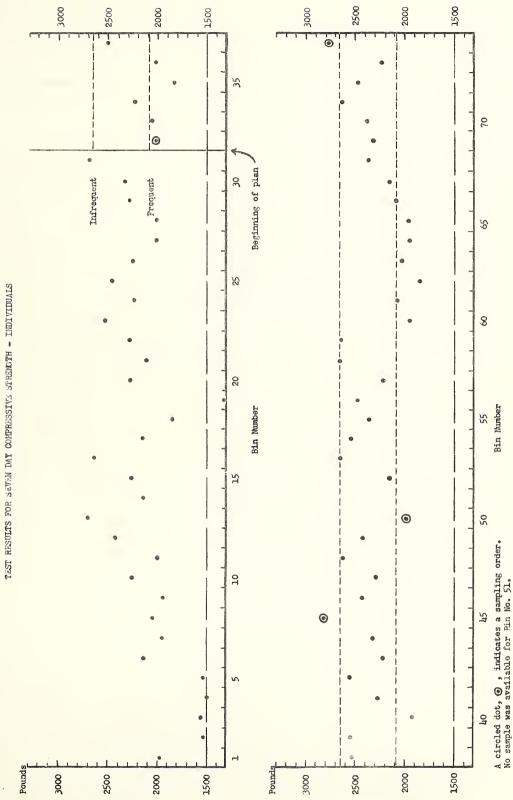
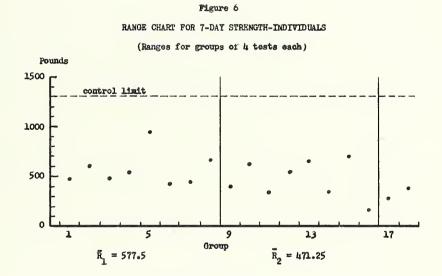


Figure 5

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## THE NATIONAL BUREAU OF STANDARDS

## **Functions and Activities**

The functions of the National Bureau of Standards are set forth in the Act of Congress, March 3, 1901, as amended by Congress in Public Law 619, 1950. These include the development and maintenance of the national standards of measurement and the provision of means and methods for making measurements consistent with these standards; the determination of physical constants and properties of materials; the development of methods and instruments for testing materials, devices, and structures; advisory services to Government Agencies on scientific and technical problems; invention and development of devices to serve special needs of the Government; and the development of standard practices, codes, and specifications. The work includes basic and applied research, development, engineering, instrumentation, testing, evaluation, calibration services, and various consultation and information services. A major portion of the Bureau's work is performed for other Government Agencies, particularly the Department of Defense and the Atomic Energy Commission. The scope of activities is suggested by the listing of divisions and sections on the inside of the front cover.

## **Reports and Publications**

The results of the Bureau's work take the form of either actual equipment and devices or published papers and reports. Reports are issued to the sponsoring agency of a particular project or program. Published papers appear either in the Bureau's own series of publications or in the journals of professional and scientific societies. The Bureau itself publishes three monthly periodicals, available from the Government Printing Office: The Journal of Research, which presents complete papers reporting technical investigations; the Technical News Bulletin, which presents summary and preliminary reports on work in progress; and Basic Radio Propagation Predictions, which provides data for determining the best frequencies to use for radio communications throughout the world. There are also five series of nonperiodical publications: The Applied Mathematics Series, Circulars, Handbooks, Building Materials and Structures Reports, and Miscellaneous Publications.

Information on the Bureau's publications can be found in NBS Circular 460, Publications of the National Bureau of Standards (\$1.00). Information on calibration services and fees can be found in NBS Circular 483, Testing by the National Bureau of Standards (25 cents). Both are available from the Government Printing Office. Inquiries regarding the Bureau's reports and publications should be addressed to the Office of Scientific Publications, National Bureau of Standards, Washington 25, D. C.

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