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NATIONAL BUREAU OF STANDARDS REPORT

10201

CLIMATOLOGICAL DATA AT THE ELEVEN PROTOTYPE SITES IN THE UNITED STATES FOR THE EVALUATION OF HUD OPERATION BREAKTHROUGH EXPERIMENTAL HOUSING SYSTEMS

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CLIMATOLOGICAL DATA AT THE ELEVEN PROTOTYPE SITES IN THE UNITED STATES FOR THE EVALUATION OF HUD OPERATION BREAKTHROUGH EXPERIMENTAL HOUSING SYSTEMS

by

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Prepared for
**DEPARTMENT OF HOUSING
AND URBAN DEVELOPMENT**

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Introduction

The purpose of this report is to provide preliminary information on site climatology useful for the design and evaluation of HUD Operation Breakthrough experimental building systems. In order to evaluate the design as well as the performance of building systems, the following environmental parameters are considered essential.

Temperature

Humidity

Wind speed and direction

Precipitation (snow and rain)

Solar radiation (direct and diffuse)

Ground temperature (depth of frost)

Background noise level

Air contamination

Earthquake risk

Climatological data for Breakthrough sites that pertain to the above parameters are scattered throughout the scientific literature. The bulk of the information presented, however, comes from the publications of the Environmental Science Services Administration (ESSA). The charge to the task group for this particular undertaking was to rapidly assemble all available climatological data pertaining to the above parameters for the Breakthrough localities, which actually contain a total of eleven building sites. This report was prepared in one month. The localities are:

1. Sacramento, California (suburban site)
2. Wilmington, Delaware (suburban site)
3. Macon, Georgia (suburban site)
4. Indianapolis, Indiana (city perimeter site)
5. Kalamazoo, Michigan (suburban site)
6. St. Louis, Missouri (inner-city site)
7. Jersey City, New Jersey (inner-city site)
8. Memphis, Tennessee (inner-city site)
9. Houston, Texas (suburban site)
10. Seattle, Washington (suburban and inner-city sites)

Except for a few localities, most of the weather data reported in the literature are recorded at airport weather stations. This fact, however, is not too critical for the evaluation of Breakthrough building systems located in the suburbs. For the inner-city sites, most of the weather data recorded at the weather bureau city office should be appropriate. Only the city office data for St. Louis and Seattle are available, however, for the in-city sites listed above. Data for the Jersey City and Memphis sites are, therefore, to be corrected from those obtained at the airport weather stations. City maps shown in the Appendix indicate relative locations of Breakthrough prototype sites with respect to the downtown area and to the airports. These maps should be useful in evaluating the correction factors for the airport weather data as well as the background noise and air contamination of the prototype sites.

Climatological data required for the design of safe building systems are usually the extreme values of parameters such as the highest recorded wind velocity, the deepest snow fall, earthquake data and temperature extremes. The building systems are expected to resist these natural forces and to provide protection for the occupants. On the other hand, the data required for the evaluation of the building performance over a period of time are those data associated with the frequency and the sequential nature of occurrences. This latter type of data are used to predict the comfort of the occupants, energy requirements for heating and cooling the building, and weatherability of building materials. Data compiled herein are, therefore, assembled with a view toward fulfilling the need for two requirements: one for the design evaluation and a second for the performance evaluation.

It is most unusual in the planning of buildings and similar engineering structures to have sufficient meteorological data available at the site which can be used directly for design purposes. Regarding wind data, for example, it is usually necessary to make use of detailed records obtained at the nearest Weather Bureau Station. Because of changes in terrain, a conversion may be required. This conversion can take the form of a regression equation which requires that extensive (approximately 4 years) simultaneous records be established for the station and for the site; or the conversion may be based upon an evaluation of the terrain roughness and on assumptions concerning the nature of the atmospheric boundary layer. It is believed that the latter approach is the only reasonable one here because of the limited

time available. However, for evaluating performance, sufficient time would be available to allow the use of regression equations.

A. Data for the Design of Heating and Cooling Systems

There are several calculation procedures available today for determining the heating and cooling loads for buildings. The method as described in the 1967 American Society of Heating, Refrigerating and Air-Conditioning Engineers Book of Fundamentals^{1/} is considered to be the state-of-the-art and is used by a majority of practicing engineers as the most accurate and comprehensive available to the profession. The ASHRAE procedure requires selection of the following design values: outdoor air temperature and wind velocity for use in calculating the heating load; an hourly profile of the Sol-air temperature and solar heat gain factors for calculation of the cooling load; and a set of dry- and wet-bulb temperature data for sizing of the mechanical equipment. The sets of outdoor temperatures for summer and winter are given by ASHRAE in the form of a percentile of the number of hours in the season; such as 1%, 2½%, and 5% for summer dry- and wet-bulb temperatures and 99% and 97½% for winter dry-bulb temperatures^{2/}. The value for the 1% summer percentile temperature is that temperature which is exceeded by only 29 hourly observations during an average summer out of a total number of 2928 hourly observations for four summer months. Similarly, winter design temperature data are represented by 99 and 97½ percentile values which mean that the 99 and 97½% of the winter hourly observations exceed these

designated temperatures during the 2160 winter hours occurring in December, January, and February. In addition to the ASHRAE summer percentile values for 1, $2\frac{1}{2}$ and 5, the U. S. Air Force Publication AFM-88-8^{3/} lists 10% data. Temperature data for design purposes at all of these percentiles are given in Table A for each of the eleven Operation Breakthrough prototype sites. Table A also includes the annual average air temperature as well as the recorded extreme values, which may be useful for some critical design problems.

Also transcribed from AFM-88-8 and listed in Table A are the number of total annual hours at or above 67 °F wet-bulb temperature. This data is sometimes used as an approximate criteria for determining whether air conditioning is necessary.

It should be noted that there is a basic difference in determining the heating load and air-conditioning cooling load. The former is usually calculated for extremely cold days where the outdoor temperature remains low and at a relatively constant level, whereas the latter is evaluated for a condition of strong solar radiation effect. Consequently, for the cooling load calculation, the outdoor temperature alone is not a good indicator. Thus, while the calculation method based upon steady temperature conditions may be a good approximation for a winter heating load determination, it usually results in a large error, if applied directly to the summer design problem. The Sol-air temperature concept should be used for summer to improve the accuracy of the cooling load calculations.

According to the 1967 ASHRAE Handbook of Fundamentals the Sol-air temperatures (SAT) are calculated by the following formula:

$$SAT = \frac{\alpha I}{h} + DB - 7a \quad (1)$$

where α , I, h and DB represent surface absorptivity of the solar radiation, solar radiation per unit surface, surface heat transfer coefficient and outdoor air dry-bulb temperature, respectively. The negative term, $-7a$, represents the long wavelength radiation of the building surface with respect to the sky. The direction cosine, "a", of the surface is unity for a roof surface and zero for a vertical wall surface. Theoretically, the Sol-air temperature can be considered to be the maximum surface temperature when there is no heat conducted from the exterior surface of the building to the interior surface. Surface temperatures become very high when the surface is solar absorptive (e.g., black-colored surface with a value of α near unity), when the wind speed is low (very small value of h), when the sun is high in a cloudless sky (a larger value of I) and when the coincident air temperature (DB) is also high.

The ASHRAE cooling load calculation procedure requires the use of Sol-air temperature profiles. Profiles for a variety of locations are not published in the 1967 ASHRAE Handbook of Fundamentals, nor are they available from other literature sources. Each geographic location must be separately calculated. This may be one of the reasons that some engineers still prefer to use simplified or short-cut cooling load calculation methods, similar to those used for the heating load. Since many of the Breakthrough building systems may be different in design from conventional buildings (for which most of the simplified or short-cut methods have been developed in the past), it is recommended that the ASHRAE cooling load calculation be followed rigorously. Upon this premise, Sol-air temperature profiles for the ten cities have, therefore, been developed here and are given in Table C. The values for solar radiation for a cloudless sky for July 21 were first calculated using the same procedure described in the 1967 ASHRAE Book of Fundamentals. These are given in Table B for all eleven sites. Since it is also required to have the design day dry-bulb temperature profiles, these were also developed on the assumption that the dry-bulb temperature follows a simple harmonic profile in a manner to achieve a maximum value of 99% at 1600 hours and a minimum value at 0500 hours. The minimum value was calculated by subtracting the daily range value listed in the ASHRAE weather data table from the 1% data.

The profile thus synthesized for Houston, Texas, for example, compares well with the ten year mean daily profile representing the hottest days of each year, as shown in Figure 1^{4/}. Similarly good comparisons were obtained for five other cities, Phoenix, (Ariz.), Washington, (D. C.), Lake Charles, (La.), Minneapolis, (Minn.), and Medford, (Oreg.), as shown in a dimensionless scheme of Fig. 2. On this basis it is believed that the dry-bulb temperature profile data given for ten Breakthrough localities as listed in Table C are accurate.

The values of 0.15 and 0.3 were used for α/h of eq. (1) to be consistent with the sample Sol-air temperature tables illustrated in the Handbook of Fundamentals^{1/}. Table C shows the Sol-air temperature profiles developed for the ten cities of Breakthrough building sites.

B. Data for Energy Estimates

Accurate estimation of heating and cooling energy requirements is important for evaluating the Breakthrough building systems. This is particularly important because of the many varieties of heating and cooling systems available today which depend upon different energy sources, types of heating and cooling processes, and types of energy distribution systems. Thus, a difference in energy requirements between systems may become a significant factor in the selection of a system. The energy calculation, therefore, should utilize the most precise and reliable up-to-date procedures. The most accurate procedures available are based upon a computer simulation of the hour by hour operation of the heating and cooling system as it responds to the dynamic

thermal behavior of the building. This calculation procedure requires coincident hourly observations of most of the parameters mentioned above for a period of at least one year, when the annual energy usage is of primary concern. Such hourly data are available on magnetic tapes from the U. S. Weather Record Center, Ashville, North Carolina. The list of tape reel numbers for ten Breakthrough localities is given in Table D.

Although several computer programs are currently available to perform this comprehensive hourly analysis for the energy requirements, the cost for such a calculation may not be warranted in some cases, particularly during early planning stages.

In lieu of the hourly calculation method because of time, cost, availability, and accuracy requirement factors, three simplified methods such as the degree-day method, equivalent full-load hour method, or the "bin" method may be selected. The degree-day concept was designed for residential applications based upon average conditions experienced by several hundred homes in the Northern United States. The seasonal total of the degree days based upon the reference temperature of 65 °F for heating and cooling are given in Table A, although the degree-day data for the cooling energy estimate have not been as widely accepted as that for the heating. The second method commonly used for estimating cooling energy requirements has been the equivalent full-load hour method. For this method the energy consumption for each of several buildings of a given type is measured and expressed as the number of

hours of operation at full load which would produce the same energy consumption. These figures are then averaged to arrive at the equivalent full-load hours for a given type of building in a given climatic region. Annual cooling energy requirements are then estimated for a specific building by multiplying the peak cooling load by the equivalent load hours. The equivalent full-load hour data for conventional buildings for the ten Breakthrough localities selected are not available. A third technique which has been gaining acceptance is application of the "bin" method. Each temperature "bin" contains hourly frequency of occurrence of temperature specified for the range of the "bin" (usually in 5 °F increments). Heat gain or heat loss of the building is calculated and expressed as a function of ambient dry-bulb temperature (not necessarily a linear function). The total energy requirements are then calculated from the sum of the product of the heat load and the frequency of the "bin". By making the width of the temperature "bin" smaller, the accuracy of the energy estimate obtained by this method can be increased. For the benefit of engineers who might want to use the "bin" method, "bin" data from Air Force Manual (AFM) 88-8 for the ten Breakthrough localities ... are shown in Table E. A detailed account of the use of the "bin" method is given in Reference (5).

C. Solar Radiation

Table A shows the maximum daily total solar radiation upon a horizontal surface; it was calculated for the cloudless day of July 21 using the method described in Reference (1). The average percent of probable sunshine for the months of July and January may be important for the design of lighting and this data is obtained from Reference (11).

More detailed data for the solar radiation levels are given in Table B.

D. Coincident Wind Velocity for the Heating and Cooling Load Calculation

Coincident wind velocity designated as VL, L, M and H in Table A as associated with the temperature data refers to the following classification^{2/}:

VL: Very light where 70% or more of the cold extreme hours are coincident with wind speeds less than or equal to 7 mph

L: Light, 50 to 69 percent of cold extreme hours are less than or equal to 7 mph wind speed

M: Moderate, where 50 to 74 percent cold extreme hours are coincident with wind speeds of more than 7 mph

H: High, where 75 percent or more of the cold extreme hours are coincident with wind speeds of 7 mph and 50 percent of the cold extreme hours are coincident with wind speeds of more than 12 mph.

Figures 3 through 22 show pictorially the annual frequency of the occurrences of coincident wind speeds and dry-bulb temperatures for the ten Breakthrough localities while Figures 23 through 32 indicate the annual coincident wind speed profiles with respect to the wind direction. Indicated in the latter figures are the direction of the prevailing winds during summer and winter.

E. Ground Temperature

Ground temperature data are needed for calculations to the estimate heat gained or lost from the basement floors and walls. These data are also needed for the design of underground heat distribution systems and to evaluate the probabilities for a freeze-up of water mains and sewage disposal lines. It should be noted that underground temperature at depths greater than 30 ft remain relatively unchanged throughout the year at the annual average air temperatures listed in Table A. The well-water temperature is also equal to the annual average air temperature. However, most underground installations require heat transfer calculations because they are usually installed at depths less than 10 ft from the surface. Listed in Table A are the integrated average earth temperatures from the surface to the ten foot depth for summer and winter conditions. These values are derived by a method similar to that described in Reference (7) assuming the thermal diffusivity of soil to be $0.025 \text{ ft}^2/\text{hr}$. Unless the soil is extremely dry or unless there are strong underground heat sources

nearby, data shown in Table A should be a good approximation of the undisturbed soil temperature for the evaluation of underground installations. The freezing depth indicated in Table A was approximated from the earth temperature data compiled in Reference (7).

F. Background Noise

The following qualitative estimates of ambient noise levels at the various Breakthrough sites were made by inspection of maps (Appendix) showing locations of nearby highways, airports, or other noise sources. Without field inspection and measurement, sufficient data are not available to enable quantitative estimates of the noise environments at these sites. It should be noted that the increased density of building and people accompanying Operation Breakthrough will result in further increases in ambient noise levels.

<u>Site</u>	<u>Estimated Ambient Noise Level</u>	<u>Comments</u>
Sacramento, Calif.	Medium-to-High	Local traffic, airport
New Castle County, Del.	Medium-to-High	Rural but near highways
Macon, Ga.	Low-to-Medium	Assuming minimal highway noise
Indianapolis, Ind.	High	Highway, adjacent airport, Indianapolis Speedway
Kalamazoo, Mich.	Medium-to-High	Two miles from airport

Jersey City, N. J.	High	High density urban areas
Memphis, Tenn.	Medium-to-High	Urban area but strong enforcement of anti-noise ordinances
St. Louis, Mo.	High	High density urban area
Houston, Tex.	Medium-to-High	Local traffic, highway, airports
Seattle, Wash.	Medium-to-High	Local traffic, highway, airports
Seattle, Wash. (King Co.)	Medium	Highway

Pending availability of more quantitative data, it is recommended that particular attention be given to noise control measures at all sites where the estimated ambient noise level is high or medium-to-high.

G. Wind Data for Structural Design

Table F gives tabulated wind data for the stations nearest the ten selected sites. These stations, in every case, are airport locations with open exposures. References or data sources are indicated in the column headings. Extreme mile wind speeds corresponding to a mean recurrence interval of 50 years have been presented by Thom (15) in the form of isotachs and are suggested as basic design speeds, provided the appropriate terrain corrections are made. These corrections can be most conveniently applied by use of the power law and the average parameters suggested by Davenport (16, 17). Under most strong wind (neutral) conditions, the mean velocity profile can

be described by the expression

$$\frac{V_Z}{V_G} = \left(\frac{Z}{Z_G}\right)^\alpha \quad (2)$$

where V_Z = wind speed at height Z

V_G = gradient wind speed first attained at height Z_G

α = power law exponent

The gradient speed is assumed to be independent of local terrain and therefore equal at station and site. This then allows the calculation of wind speeds at the site if the parameters α and Z_G are known.

The following average values have been suggested by Davenport (17).

Type of Terrain	α	Z_G (ft)
Flat open country	.16	900
Rough wooded country, city suburbs	.28	1300
Heavily built up urban centers	.40	1400

Because of their low probability of occurrence, extreme speeds are not usually a satisfactory basis for evaluating structural performance. For this purpose, mean wind speeds for January and July as the mean annual wind speeds are presented in Table F. These data indicate the relative windiness of the 10 localities and also indicate the relative contribution of extratropical cyclones and thunderstorms being associated with the winter months. Also included in Table F are the average number of storms per year which resulted in wind speeds

of 47 mph or greater. It will be noted that this speed corresponds to a loading of approximately one-half the design load and would produce up to 250 loading cycles during the 50-year design life of the structure if wind gusts were neglected. The effect of high intensity gusts would be primarily to increase the number of loading cycles, say to 1000 or more during the 50-year life of the structure. Therefore, the data listed in Table F, coupled with known properties of atmospheric boundary layers, can be used to establish the mean wind climate at the 10 localities. Information sufficient for design and evaluation of performance can be developed once the estimates of the terrain roughness become available. It is recommended that an inspection of the surrounding terrain or the sites be made by qualified personnel for the purpose of estimating the effective roughness parameters.

H. Earthquake Data

In the design of buildings to resist lateral seismic forces, the minimum total lateral shear is usually based on the expression

$$V = ZKCW \quad (3)$$

where V = total lateral shear at the base

Z = numerical coefficient which depends on the seismic zone in which the building is to be situated

K = numerical coefficient which depends upon the structural frame characteristics

C = numerical coefficient for the base shear which
depends upon the fundamental period of the
structure

W = total dead load.

Of the above factors, only Z has a regional variation. Since no reliable method of predicting the time, place and intensity of earthquakes exists, maps have been constructed indicating the areas which have experienced destructive earthquakes in the past. These maps are the only means available at this time by which the location of future destructive earthquakes may be anticipated. Zones range from 0 to 3 and are characterized by the following expected degrees of damage.

Zone	Degree of Damage	Z Value
0	None	0
1	Minor	0.25
2	Moderate	0.50
3	Major	1.0

A number of different seismic maps are in use, their zone boundaries differing only slightly in most cases. Based on the most recent edition of ANSI-A58-Sec. 6, the following seismic zones are suggested for arriving at design loads:

<u>Selected Site</u>	<u>Seismic Zone</u>
Sacramento, California	2
Wilmington, Delaware	1
Macon, Georgia	1
Indianapolis, Indiana	1
Kalamazoo, Michigan	1
St. Louis, Missouri	1
Jersey City, New Jersey	1
Memphis, Tennessee	2
Houston, Texas	1
Seattle, Washington	3

I. Air Contamination Data

Air pollution data for the ten Operation Breakthrough localities are given in Table G. Included are the locations of the sampling sites and the concentrations of suspended particulates, sulfur dioxide, nitrogen dioxide and ammonia. The geometric mean (which gives a better indication of the central tendency of the values than the arithmetic mean), the 90% frequency distribution value (90% of the readings are equal to or less than this value) and the period of years that these averages represent are given in Table G. Blank spaces indicate data is not available. These concentrations represent averages at the sampling sites; the values at the particular Breakthrough site will vary and will depend on pollutant sources, and meteorological and topographical factors (19).

Little information is available in the literature concerning application of these data in the design of housing systems. The following statements, taken from reference (20), are given to illustrate a correlation between exposure to sulfur dioxide and particulates and the effects on health.

- a. At concentrations ranging from 300-500 of sulfur dioxide (24-hour mean), with low particulate levels, increased hospital admissions of older persons for respiratory disease may occur; absenteeism from work, particularly with older persons, may also occur.
- b. A decrease from 140 to 60 (annual mean) in particulate concentrations may be accompanied by decrease in mean spectrum volume in industrial workers.
- c. Where concentrations range from 100-130 and above for particulates (annual mean) with sulfur dioxide concentrations (annual mean) greater than 120, children residing in such areas are likely to experience increased incidence of certain respiratory diseases.

These statements apply to outdoor pollutants, but pollutant levels indoors have not received adequate attention. Considering the fact that people spend most of their lives indoors, the matter of the quality of indoor air becomes very important. Further efforts are recommended to measure indoor and outdoor pollution levels simultaneously to relate them to the various sources of air contaminations, both indoors and

outdoors and to other climatic parameters. With this type of information it should be possible to specify air cleaning devices to maintain indoor air at a healthful level of purity.

J. Precipitation Data

Extreme values in 24 hours and normals (1931-1960) of annual totals for rain - and snowfall were obtained from reference (14) and listed in Table A, which also shows the snow load in lbs/sq. ft. on the ground as transcribed from reference (12).

K. Summary and Recommendations

Outdoor environmental data required for the design and the evaluation of Breakthrough building systems have been assembled herein from various sources. The parameters included are temperature, humidity, wind, precipitation, solar radiation, ground temperature, soil conditions, background noise level, air contamination and earthquake risk. It is believed that the data presented in this report can be used to prepare preliminary designs for the Breakthrough building programs. However, more detailed and specific information should be prepared as the Breakthrough program progresses, especially for use in the test and evaluation phase.

The following recommendations are made:

1. After review and approval by HUD this report should be made available to Breakthrough contractors for use in their design work.
2. Continue efforts to add to and refine the data given with special priority to be given to (a) conduct field inspections and measurements of the background noise levels and terrain roughness at the Breakthrough sites, and (b) measure coincident hourly data for air contamination with reference to temperature, humidity and wind data. These coincident data are essential for predicting the indoor environment of a Breakthrough building especially with respect to the design of the indoor environmental control systems.

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20. "Guidelines for the Development of Air Quality Standards and Implementation Plans", National Air Pollution Control Administration, HEW, (May, 1969).

Table A

Data for Heating and Cooling Load Calculations

Table A

Site Localities (Weather Station)	Air Temperatures, °F						Annual Temperature, °F	$\frac{14}{*}$	Ground Temp., °F	
	Summer 1%	DB/WB $2\frac{1}{2}\%$	5%	Winter DB Range 10% °F	99% DB	Coin- cident wind 97% VL			Upper 10 Ft Average Summer	
Sacramento, Calif. (Airport)	100/72	97/70	94/69	88/67	36	30	32	VL*	115	23
Wilmington, Del. (Airport)	93/99	90/77	87/76	84/74	20	12	15	M	102	-4
Macon, Ga. (Airport)	98/80	96/79	94/78	92/77	22	23	27	L	104	3
Indianapolis, Ind. (Airport)	93/78	91/77	88/76	86/74	22	0	4	M	99	-18
Kalamazoo, Mich. (Grand Rapids AP)	92/76	89/75	86/74	83/71	23	1	5	M	100	-16
St. Louis, Mo. (City Office)	96/79	94/78	92/77	89/75	18	7	11	M	106	-11
Jersey City, N. J. (Corrected from data of Newark AP)	92/77	89/76	86/75	82/73	20	11	15	M	105	1
Memphis, Tenn. (Airport)	98/80	96/79	94/78	91/77	21	17	21	L	106	-13
Houston, Tex. (Airport)	96/80	94/80	92/79	90/78	18	28	39	M	106	9
Seattle, Wash. (SeaTac AP)	85/66	81/64	77/63	72/61	22	20	24	L	99	6
Seattle, Wash. (City Office)	81/67	79/65	76/64	-	19	28	32	L	100	11

* $\frac{14}{*}$ and similar nomenclature are numbers for reference citation.

* VL, very light; L, light; M, moderate; H, high. See text, p. 10.

Table A - Continued

Site Localities (Weather Station)	Precipitation Data (1931-1960)						Solar Radiation		
	Rain, In. $\frac{14}{24}$ / Max. 24 hrs.	Mean annual	Snow, In. $\frac{14}{24}$ / Max. 24 hrs.	Mean annual	Snow Load $\frac{12}{psf}$	Max. Daily Total	% Sunshine Jan.	% Sunshine July	
Sacramento, Calif. Airport	5.6	16.3	-	-	5 ~ 10	3620	45	97	
Wilmington, Del. Airport	6.2	44.5	15.6	22.5	20	3615	44	66	
Macon, Ga. Airport	5.0	44.1	3.7	0.4	5 ~ 10	2130	56	64	
Indianapolis, Ind. Airport	3.9	12.7	12.5	20.3	10 ~ 20	3615	43	66	
Kalamazoo, Mich. Grand Rapids AP	2.7	31.2	12.6	78.7	20	3600	-	-	
St. Louis, Mo. (City Office)	3.3	35.3	11.2	17.2	20	3620	52	71	
Jersey City, N. J. (Corrected from the data of Newark AP)	4.7	43.5	26	29.8	20	3610			
Memphis, Tenn. airport	4.9	49.7	16.1	6.6	5 ~ 10	3624	48	73	
Houston, Tex. airport	15.7	46.0	4.4	0.4	less than 5	3612	47	74	
Seattle, Wash. Sea/Fac AP	3.4	39.0	21.4	14.7	10	3561	14	68	
Seattle, Wash. (City Office)	3.3	34.1	11.5	8.1	10	3561	28	63	

Table A - Continued

Site Localities (Weather Station)	Seasonal Degree-Days		No. of annual hrs/ WB ₃ at or above 67 °F
	Seasonal Heating	Seasonal Cooling	
Sacramento, Calif. (Airport)	2 773	1411	351
Wilmington, Del. (Airport)	4 930	1 002	1191
Macon, Ga. (Airport)	2 130	2 367	3069
Indianapolis, Ind. (Airport)	5 699	1 033	1462
Kalamazoo, Mich. (Grand Rapids AP)	6 998	730	833
St. Louis, Mo. (City Office)	4 900	1 558	1866
Jersey, City, N. J. (Corrected from data of Newark AP)	5 067	965	1290
Memphis, Tenn. (Airport)	3 233	2 078	2 631
Houston, Tex. (Airport)	14 00	3 175	3 695
Seattle, Wash. (Sea/Tac AP)	5 145	170	17
Seattle, Wash. (City Office)	4 424	-	17

Table B

Solar Radiation

ET: Equation of time, min.

R: Solar constant modifier

HO: Daily total radiation upon horizontal surface, Btu/hr ft²

BETA: Solar altitude angle, degree

AZIMUTH: Solar azimuth angle, measured from north, degree

IDN: Direct normal radiation, Btu/hr ft²

DIFF: Diffuse sky radiation, Btu/hr ft²

Total solar radiation values (for the clearness number of unity) expected to fall upon vertical wall surfaces from eight compass directions and upon a horizontal surface are tabulated in these tables.

LOCATION: SACRAMENTO, CALIFORNIA

MONTH= 7 DAY=21 FOR LATITUDE= 38.5 LONGITUDE= 121.5

ET= -6.2000 R= .9690 SUNRZ= 5.0626 HO= 3619.11

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME AIR BETA AZI- IDN DIFF SOUTH SW WEST NW NORTH NE FAST SE HORIZ
HR TEMP (DEG) MUTH

1.	71.	0.	13.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	68.	0.	28.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	65.	0.	42.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	64.	0.	53.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	64.	0.	63.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
6.	65.	10.	72.	107.	15.	13.	13.	13.	45.	106.	113.	60.	33.		
7.	68.	22.	81.	196.	27.	30.	30.	30.	59.	178.	210.	136.	99.		
8.	71.	33.	90.	236.	32.	44.	44.	44.	46.	185.	242.	183.	161.		
9.	75.	45.	100.	257.	35.	88.	57.	57.	57.	162.	236.	205.	216.		
10.	80.	56.	113.	268.	36.	126.	67.	67.	67.	123.	204.	206.	259.		
11.	84.	66.	134.	274.	37.	152.	74.	74.	74.	75.	154.	185.	288.		
12.	89.	72.	171.	277.	38.	163.	128.	77.	77.	77.	91.	148.	300.		
13.	93.	69.	213.	276.	37.	158.	172.	129.	76.	76.	76.	96.	295.		
14.	96.	60.	240.	271.	37.	138.	200.	186.	104.	70.	70.	70.	273.		
15.	99.	50.	255.	262.	36.	104.	208.	226.	147.	61.	61.	61.	235.		
16.	100.	38.	267.	246.	33.	61.	195.	243.	178.	50.	50.	50.	185.		
17.	100.	26.	276.	216.	29.	36.	158.	228.	186.	56.	36.	36.	125.		
18.	99.	15.	284.	153.	21.	20.	95.	163.	147.	57.	20.	20.	60.		
19.	96.	4.	293.	14.	2.	1.	6.	14.	14.	7.	1.	1.	3.		
20.	93.	0.	303.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.		
21.	89.	0.	313.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.		
22.	84.	0.	326.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.		
23.	80.	0.	341.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.		
24.	75.	0.	357.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.		

LOCATION: WILMINGTON, DELAWARE

MONTH= 7 DAY=21 FOR LATITUDE= 39.7 LONGITUDE= 75.6

ET= -6.2000 R= .9690 SUNRZ= 4.9532 HO= 3615.22

CALCULATED SOLAR RADIATION DATA: BTU/HR (SQ. FT.)

TIME	AIR	BETA	AZI-	IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
HR	TEMP	(DEG)	MUTH											

1.	77.	0.	14.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	75.	0.	29.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	74.	0.	42.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	73.	0.	54.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	73.	.	64.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
6.	74.	11.	73.	119.	16.	14.	14.	14.	49.	117.	125.	69.	39.	
7.	75.	22.	82.	200.	27.	31.	31.	31.	58.	179.	214.	142.	104.	
8.	77.	34.	91.	237.	32.	48.	45.	45.	45.	182.	242.	187.	165.	
9.	79.	45.	102.	257.	35.	94.	58.	58.	58.	157.	234.	208.	218.	
10.	82.	56.	116.	268.	36.	132.	67.	67.	67.	116.	201.	207.	260.	
11.	84.	66.	138.	274.	37.	157.	79.	74.	74.	74.	150.	186.	287.	
12.	87.	71.	174.	276.	38.	168.	134.	76.	76.	76.	76.	86.	148.	298.
13.	89.	68.	213.	275.	37.	162.	177.	132.	75.	75.	75.	75.	96.	292.
14.	91.	59.	239.	270.	37.	140.	203.	188.	103.	69.	69.	69.	69.	269.
15.	92.	49.	255.	261.	36.	106.	210.	227.	147.	61.	61.	61.	61.	232.
16.	93.	37.	266.	244.	33.	62.	195.	243.	177.	49.	49.	49.	49.	181.
17.	93.	26.	276.	214.	29.	35.	157.	227.	184.	55.	35.	35.	35.	122.
18.	92.	14.	285.	150.	20.	20.	93.	160.	144.	56.	20.	20.	20.	57.
19.	91.	3.	294.	11.	2.	1.	5.	12.	12.	6.	1.	1.	1.	2.
20.	89.	0.	303.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	87.	0.	314.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	84.	0.	327.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	82.	0.	342.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	79.	0.	358.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: MACON, GEORGIA

MONTH= 7 DAY=21 FOR LATITUDE= 32.7 LONGITUDE= 83.6

E_T= -6.2000 R= .9690 SUNRZ= 5.7647 H0= 3621.78

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME	AIR	BETA	AZI-	IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NF	FAST	SE	HORIZ
HR	TEMP	(DEG)	MUTH											

1.	80.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	78.	0.	22.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	77.	0.	37.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	76.	0.	49.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	76.	0.	59.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
6.	77.	3.	68.	4.	1.	0.	0.	0.	0.	2.	5.	5.	2.	1.
7.	78.	15.	75.	152.	21.	20.	20.	20.	58.	147.	162.	144.	59.	
8.	80.	27.	82.	218.	30.	37.	37.	37.	63.	192.	230.	155.	129.	
9.	83.	40.	90.	249.	34.	52.	52.	52.	52.	187.	243.	187.	192.	
10.	86.	52.	99.	265.	36.	89.	64.	64.	64.	159.	224.	105.	245.	
11.	88.	64.	113.	273.	37.	119.	73.	73.	73.	118.	182.	182.	284.	
12.	91.	75.	141.	278.	38.	136.	86.	78.	78.	78.	124.	151.	305.	
13.	94.	77.	160.	278.	38.	138.	105.	79.	79.	79.	101.	136.	309.	
14.	96.	68.	240.	275.	37.	126.	173.	163.	101.	75.	75.	75.	294.	
15.	97.	57.	257.	269.	37.	101.	193.	211.	146.	67.	67.	67.	67.	261.
16.	98.	44.	267.	256.	35.	65.	192.	239.	179.	56.	56.	56.	56.	213.
17.	98.	32.	275.	232.	32.	43.	169.	239.	194.	60.	43.	43.	43.	153.
18.	97.	19.	282.	183.	25.	27.	120.	195.	172.	63.	27.	27.	27.	65.
19.	96.	7.	290.	62.	8.	7.	33.	65.	63.	28.	7.	7.	7.	10.
20.	94.	0.	298.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	91.	0.	307.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	88.	0.	318.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	86.	0.	332.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	83.	0.	348.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: INDIANAPOLIS, INDIANA

MONTH= 7 DAY=21 FOR LATITUDE= 39.7 LONGITUDE= 86.3

ET= -6.2000 R= .9690 SUNRZ= 5.6614 HO= 3614.96

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME	AIR	BETA	AZI-	IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
HR	TEMP	(DEG)	MUTH											

1.	75.	0.	2.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	73.	0.	18.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	72.	0.	33.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	71.	0.	46.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	71.	0.	57.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
6.	72.	4.	66.	12.	2.	1.	1.	1.	1.	6.	12.	12.	6.	2.
7.	73.	14.	75.	150.	20.	20.	20.	20.	20.	56.	145.	160.	93.	58.
8.	75.	26.	84.	214.	29.	35.	35.	35.	35.	55.	184.	227.	157.	122.
9.	78.	37.	94.	244.	33.	62.	49.	49.	49.	49.	177.	243.	195.	181.
10.	81.	49.	105.	261.	36.	106.	61.	61.	61.	61.	146.	227.	210.	232.
11.	83.	59.	121.	270.	37.	141.	69.	69.	69.	69.	103.	188.	204.	269.
12.	86.	68.	147.	275.	37.	162.	96.	75.	75.	75.	132.	177.	292.	
13.	89.	70.	174.	276.	38.	168.	134.	76.	76.	76.	86.	148.	298.	
14.	91.	66.	222.	274.	37.	158.	187.	150.	74.	74.	74.	74.	79.	287.
15.	92.	56.	244.	268.	36.	132.	208.	201.	116.	67.	67.	67.	67.	260.
16.	93.	45.	258.	257.	35.	94.	208.	234.	157.	57.	57.	57.	57.	218.
17.	93.	34.	269.	237.	32.	48.	187.	242.	182.	45.	45.	45.	45.	165.
18.	92.	22.	278.	200.	27.	31.	142.	214.	179.	58.	31.	31.	31.	104.
19.	91.	11.	287.	118.	16.	14.	69.	125.	117.	49.	14.	14.	14.	39.
20.	89.	.	296.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	86.	0.	306.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	83.	0.	318.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	81.	0.	331.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	78.	0.	346.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: KALAMAZOO, MICHIGAN

MONTH= 7 DAY=21 FOR LATITUDE= 42.2 LONGITUDE= 84.5

ET= -6.2000 RF= .9690 SUNRZ= 5.4304 HO= 3603.10

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME	AIR	BETA	AZI-	IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	FAST	SE	HORIZ
HR	TEMP	(DEG)	MUTH											

1.	73.	0.	4.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	71.	0.	20.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	70.	0.	34.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	69.	0.	47.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	69.	0.	58.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
6.	70.	6.	68.	43.	6.	5.	5.	5.	5.	21.	44.	44.	21.	10.
7.	71.	16.	77.	165.	22.	22.	22.	22.	22.	58.	156.	177.	107.	69.
8.	73.	27.	87.	219.	30.	37.	37.	37.	37.	49.	183.	232.	167.	130.
9.	76.	38.	97.	247.	34.	74.	50.	50.	50.	50.	169.	242.	202.	187.
10.	79.	49.	110.	262.	36.	118.	61.	61.	61.	61.	135.	222.	215.	234.
11.	82.	59.	127.	270.	37.	153.	69.	69.	69.	69.	89.	180.	207.	268.
12.	85.	66.	154.	274.	37.	173.	109.	74.	74.	74.	74.	123.	179.	288.
13.	88.	68.	170.	275.	37.	177.	135.	75.	75.	75.	75.	93.	160.	292.
14.	90.	63.	222.	273.	37.	164.	196.	155.	72.	72.	72.	72.	78.	280.
15.	91.	54.	243.	266.	36.	136.	214.	205.	114.	65.	65.	65.	65.	252.
16.	92.	44.	258.	255.	35.	95.	211.	236.	155.	56.	56.	56.	56.	210.
17.	92.	33.	269.	234.	32.	48.	186.	241.	180.	44.	44.	44.	44.	158.
18.	91.	21.	278.	195.	27.	30.	138.	210.	176.	56.	30.	30.	30.	98.
19.	90.	11.	288.	112.	15.	13.	64.	118.	111.	47.	13.	13.	13.	30.
20.	88.	.	298.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	85.	0.	308.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	82.	0.	320.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	79.	0.	333.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	76.	0.	348.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: ST. LOUIS, MISSOURI

MONTH= 7 DAY=21 FOR LATITUDE= 38.6 LONGITUDE= 90.2

ET= -6.2000 R= .9690 SUNRZ= 4.9710 H0= 3618.77

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME AIR BETA AZI- IDN DIFF SOUTH SW WEST NW NORTH NE FAST SE HORIZ
HR TEMP (DEG) MUTH

1.	81.	0.	14.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	80.	0.	29.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	79.	0.	43.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	78.	0.	54.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	78.	.	64.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
6.	79.	11.	73.	118.	16.	14.	14.	14.	49.	117.	125.	69.	39.		
7.	80.	23.	81.	201.	27.	31.	31.	31.	59.	180.	215.	142.	104.		
8.	81.	34.	90.	238.	32.	47.	46.	46.	46.	184.	242.	186.	167.		
9.	84.	46.	101.	258.	35.	92.	58.	58.	58.	159.	234.	206.	220.		
10.	86.	57.	115.	269.	37.	129.	68.	68.	68.	118.	200.	205.	262.		
11.	88.	67.	137.	275.	37.	154.	78.	74.	74.	74.	149.	183.	289.		
12.	90.	72.	175.	277.	38.	164.	133.	77.	77.	77.	85.	144.	300.		
13.	93.	68.	216.	275.	37.	158.	175.	134.	75.	75.	75.	92.	293.		
14.	94.	60.	241.	271.	37.	136.	201.	190.	108.	70.	70.	70.	270.		
15.	95.	49.	256.	261.	36.	101.	208.	228.	150.	61.	61.	61.	231.		
16.	96.	37.	267.	244.	33.	58.	193.	243.	180.	49.	49.	49.	180.		
17.	96.	25.	276.	212.	29.	35.	154.	225.	185.	56.	35.	35.	119.		
18.	95.	14.	285.	145.	20.	19.	89.	154.	140.	55.	19.	19.	54.		
19.	94.	3.	294.	5.	1.	0.	2.	5.	5.	2.	.	.	.	1.	
20.	93.	0.	304.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	
21.	90.	0.	315.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	
22.	88.	0.	327.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	
23.	86.	0.	342.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	
24.	84.	0.	358.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	

LOCATION: JERSEY CITY, NEW JERSEY

MONTH= 7 DAY=21 FOR LATITUDE= 40.7 LONGITUDE= 74.2

ET= -6.2000 R= .9690 SUNRZ= 4.8117 HO= 3610.80

CALCULATED SOLAR RADIATION DATA, RTU/HR (SQ. FT.)

TIME HR	AIR TEMP (DEG)	BETA MUTH	AZI- IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	FAST	SE	HORIZ
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1.	76.	0.	15.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	74.	0.	30.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	73.	0.	43.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	72.	0.	54.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	72.	2.	65.	1.	0.	0.	0.	0.	0.	1.	1.	0.	0.
6.	73.	13.	74.	133.	18.	17.	17.	17.	52.	130.	141.	79.	47.
7.	74.	24.	83.	205.	28.	33.	33.	33.	56.	181.	219.	148.	110.
8.	76.	35.	93.	240.	33.	55.	47.	47.	47.	179.	243.	191.	170.
9.	78.	46.	104.	258.	35.	101.	58.	58.	58.	151.	232.	211.	222.
10.	81.	57.	119.	269.	37.	138.	68.	68.	68.	109.	196.	209.	262.
11.	83.	66.	142.	274.	37.	163.	88.	74.	74.	74.	143.	186.	287.
12.	86.	70.	178.	276.	38.	172.	142.	76.	76.	76.	79.	146.	296.
13.	88.	66.	215.	274.	37.	165.	183.	138.	74.	74.	74.	74.	288.
14.	90.	58.	239.	269.	37.	141.	207.	192.	104.	68.	68.	68.	205.
15.	91.	47.	255.	260.	35.	105.	212.	229.	147.	59.	59.	59.	226.
16.	92.	36.	260.	242.	33.	60.	194.	243.	177.	48.	48.	48.	176.
17.	92.	25.	276.	210.	29.	34.	154.	224.	183.	55.	34.	34.	116.
18.	91.	14.	285.	143.	19.	18.	87.	152.	139.	55.	18.	18.	53.
19.	90.	3.	294.	6.	1.	1.	3.	6.	6.	3.	1.	1.	1.
20.	88.	0.	304.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	86.	0.	316.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	83.	0.	329.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	81.	0.	343.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	78.	0.	359.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: MEMPHIS, TENNESSEE

MUNTH= 7 DAY=21 FOR LATITUDE= 35.1 LONGITUDE= 90.0

ET= -6.2000 R= .9690 SUNRZ= 5.1008 H0= 3624.1°

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME	AIR	BETA	AZI-	IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
HR	TEMP	(DEG)	MUTH											

1.	81.	0.	15.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	79.	0.	30.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	78.	0.	44.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	77.	0.	55.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	77.	0.	64.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
6.	78.	10.	72.	108.	15.	13.	13.	13.	45.	107.	114.	61.	34.	
7.	79.	22.	80.	199.	27.	31.	31.	31.	62.	181.	212.	137.	102.	
8.	81.	34.	88.	238.	32.	46.	46.	46.	52.	189.	242.	180.	167.	
9.	83.	47.	97.	259.	35.	81.	59.	59.	59.	167.	235.	199.	223.	
10.	86.	59.	110.	270.	37.	117.	69.	69.	69.	129.	202.	196.	267.	
11.	89.	69.	131.	276.	37.	140.	76.	76.	76.	82.	150.	174.	295.	
12.	92.	75.	174.	278.	38.	150.	124.	78.	78.	78.	86.	134.	306.	
13.	94.	71.	222.	276.	38.	143.	166.	137.	77.	77.	77.	81.	299.	
14.	96.	61.	247.	271.	37.	123.	193.	192.	120.	71.	71.	71.	71.	274.
15.	97.	49.	260.	262.	36.	90.	200.	230.	160.	61.	61.	61.	61.	234.
16.	98.	37.	270.	244.	33.	49.	186.	243.	187.	49.	49.	49.	49.	180.
17.	98.	25.	278.	210.	29.	34.	148.	223.	187.	61.	34.	34.	34.	116.
18.	97.	13.	286.	135.	18.	17.	81.	143.	132.	53.	17.	17.	17.	48.
19.	96.	1.	294.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
20.	94.	0.	303.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	92.	0.	314.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	89.	0.	327.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	86.	0.	342.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	83.	0.	358.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: HOUSTON, TEXAS

MONTH= 7 DAY=21 FOR LATITUDE= 29.6 LONGITUDE= 95.3

ET= -6.2000 RE= .9690 SUNRZ= 5.6457 H0= 3611.36

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME	AIR	BETA	AZI-	ION	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
HR	TEMP	(DEG)	MUTH											

1.	81.	0.	10.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	80.	0.	27.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	79.	0.	41.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	78.	0.	52.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	78.	0.	61.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
6.	79.	4.	69.	21.	3.	2.	2.	2.	10.	22.	22.	11.	5.	
7.	80.	17.	76.	167.	23.	23.	23.	23.	62.	161.	178.	105.	71.	
8.	81.	29.	82.	226.	31.	40.	40.	40.	67.	197.	235.	159.	142.	
9.	84.	42.	89.	253.	34.	55.	55.	55.	58.	189.	241.	184.	205.	
10.	86.	55.	97.	268.	36.	85.	67.	67.	67.	160.	217.	186.	257.	
11.	88.	68.	110.	275.	37.	111.	75.	75.	75.	118.	171.	168.	293.	
12.	90.	79.	145.	279.	38.	124.	89.	80.	80.	80.	111.	133.	311.	
13.	93.	78.	220.	278.	38.	123.	137.	116.	79.	79.	79.	79.	84.	310.
14.	94.	67.	251.	275.	37.	109.	171.	176.	122.	75.	75.	75.	75.	290.
15.	95.	54.	264.	267.	36.	83.	187.	220.	163.	66.	66.	66.	66.	253.
16.	96.	41.	272.	251.	34.	53.	183.	242.	191.	59.	53.	53.	53.	200.
17.	96.	28.	278.	222.	30.	39.	155.	232.	196.	67.	39.	39.	39.	156.
18.	95.	16.	285.	159.	22.	21.	98.	170.	154.	61.	21.	21.	21.	64.
19.	94.	3.	292.	8.	1.	1.	4.	9.	9.	4.	1.	1.	1.	2.
20.	93.	0.	299.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	90.	0.	309.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	88.	0.	320.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	86.	0.	335.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	84.	0.	352.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: SEATTLE, WASHINGTON (AIRPORT)

MONTH= 7 DAY=21 FOR LATITUDE= 47.4 LONGITUDE= 122.3

ET= -6.2000 R= .9690 SUNRZ= 4.6734 H0= 3562.21

CALCULATED SOLAR RADIATION DATA, RTU/HR (SQ. FT.)

TIME	AIR	BETA	AZI-	IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	FAST	SE	HORIZ
HR	TEMP	(DEG)	MUTH											

1.	67.	0.	11.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	65.	0.	26.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	64.	0.	39.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	63.	0.	52.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	63.	3.	63.	6.	1.	1.	1.	1.	1.	3.	6.	6.	2.	1.
6.	64.	12.	73.	130.	18.	16.	16.	16.	16.	53.	128.	138.	76.	45.
7.	65.	22.	84.	199.	27.	31.	31.	31.	31.	51.	174.	214.	146.	102.
8.	67.	32.	95.	234.	32.	60.	43.	43.	43.	43.	171.	240.	194.	157.
9.	70.	42.	107.	253.	34.	110.	54.	54.	54.	54.	141.	233.	220.	205.
10.	73.	51.	123.	264.	36.	153.	63.	63.	63.	63.	97.	201.	224.	242.
11.	75.	59.	144.	270.	37.	182.	91.	69.	69.	69.	69.	151.	207.	268.
12.	78.	63.	172.	272.	37.	196.	147.	72.	72.	72.	72.	89.	172.	279.
13.	81.	61.	202.	272.	37.	191.	191.	120.	71.	71.	71.	71.	121.	275.
14.	83.	56.	227.	268.	36.	170.	218.	177.	72.	67.	67.	67.	67.	257.
15.	84.	47.	245.	259.	35.	133.	225.	219.	120.	59.	59.	59.	59.	225.
16.	85.	37.	259.	245.	33.	86.	210.	240.	158.	49.	49.	49.	49.	182.
17.	85.	27.	271.	219.	30.	37.	173.	232.	177.	40.	37.	37.	37.	131.
18.	84.	17.	281.	172.	23.	24.	115.	185.	160.	56.	24.	24.	24.	75.
19.	83.	8.	292.	72.	10.	8.	36.	75.	74.	35.	8.	8.	8.	19.
20.	81.	0.	303.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	78.	0.	314.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	75.	0.	327.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	73.	0.	341.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	70.	0.	356.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: SEATTLE, WASHINGTON (CITY)

MONTH= 7 DAY=21 FOR LATITUDE= 47.6 LONGITUDE= 122.3

ET= -6.2000 RF= .9690 SUNRZ= 4.6668 H0= 3560.77

CALCULATED SOLAR RADIATION DATA, RTU/HR (SQ. FT.)

TIME	AIR TEMP	META	AZI- IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	FAST	SE	HORIZ
HR	(DEG)	MUTH											

1.	66.	0.	11.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	64.	0.	26.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	63.	0.	39.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	62.	0.	51.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	62.	3.	63.	6.	1.	1.	1.	1.	3.	6.	6.	2.	1.
6.	63.	12.	73.	130.	18.	16.	16.	16.	53.	128.	138.	77.	46.
7.	64.	22.	84.	199.	27.	31.	31.	31.	51.	174.	214.	146.	102.
8.	66.	32.	95.	234.	32.	60.	43.	43.	43.	171.	240.	194.	157.
9.	68.	42.	107.	253.	34.	110.	54.	54.	54.	141.	233.	220.	204.
10.	70.	51.	123.	264.	36.	153.	63.	63.	63.	97.	201.	224.	242.
11.	73.	59.	144.	270.	37.	183.	92.	69.	69.	69.	151.	207.	267.
12.	75.	63.	172.	272.	37.	196.	148.	72.	72.	72.	89.	172.	279.
13.	77.	61.	202.	272.	37.	192.	191.	120.	71.	71.	71.	122.	275.
14.	79.	55.	227.	268.	36.	170.	218.	177.	71.	67.	67.	67.	257.
15.	80.	47.	245.	259.	35.	134.	225.	219.	119.	59.	59.	59.	225.
16.	81.	37.	259.	245.	33.	87.	210.	240.	158.	49.	49.	49.	182.
17.	81.	27.	271.	220.	30.	38.	174.	232.	177.	40.	38.	38.	131.
18.	80.	17.	281.	172.	23.	24.	115.	185.	161.	56.	24.	24.	75.
19.	79.	8.	292.	73.	10.	8.	37.	76.	75.	35.	8.	8.	20.
20.	77.	0.	303.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	75.	0.	314.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	73.	0.	327.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	70.	0.	341.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	68.	0.	356.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

Table C

Sol-air Temperatures

Sol-air temperature values tabulated in these tables are obtained from the solar radiation values of Table B and estimated outdoor air temperature profiles of a design day using equation (1) of the text.

LOCATION: SACRAMENTO, CALIFORNIA
MONTH= 7 DAY=21 FOR LATITUDE= 38.5 LONGITUDE= 121.5

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SF	HORIZ
1.	71.	71.	71.	71.	71.	71.	71.	71.	71.	64.
2.	68.	68.	68.	68.	68.	68.	68.	68.	68.	61.
3.	65.	65.	65.	65.	65.	65.	65.	65.	65.	58.
4.	64.	64.	64.	64.	64.	64.	64.	64.	64.	57.
5.	64.	64.	64.	64.	64.	64.	64.	64.	64.	57.
6.	65.	67.	67.	67.	67.	72.	81.	82.	74.	63.
7.	68.	72.	72.	72.	72.	77.	94.	99.	88.	75.
8.	71.	78.	78.	78.	78.	78.	99.	107.	98.	88.
9.	75.	88.	84.	84.	84.	84.	99.	110.	106.	100.
10.	80.	98.	90.	90.	90.	90.	98.	110.	110.	112.
11.	84.	107.	95.	95.	95.	95.	96.	107.	112.	121.
12.	89.	113.	108.	100.	100.	100.	100.	103.	111.	127.
13.	93.	117.	119.	112.	104.	104.	104.	104.	107.	130.
14.	90.	117.	126.	124.	112.	107.	107.	107.	107.	130.
15.	99.	114.	130.	133.	121.	108.	108.	108.	108.	127.
16.	100.	109.	129.	136.	127.	107.	107.	107.	107.	121.
17.	100.	105.	124.	134.	128.	108.	105.	105.	105.	112.
18.	93.	102.	113.	123.	121.	107.	102.	102.	102.	101.
19.	90.	97.	97.	98.	98.	97.	97.	97.	97.	90.
20.	93.	93.	93.	93.	93.	93.	93.	93.	93.	86.
21.	89.	89.	89.	89.	89.	89.	89.	89.	89.	82.
22.	84.	84.	84.	84.	84.	84.	84.	84.	84.	77.
23.	80.	80.	80.	80.	80.	80.	80.	80.	80.	73.
24.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.

LOCATION: SACRAMENTO, CALIFORNIA

MONTH= 7 DAY=21 FOR LATITUDE= 38.5 LONGITUDE= 121.5

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	71.	71.	71.	71.	71.	71.	71.	71.	71.	64.
2.	68.	68.	68.	68.	68.	68.	68.	68.	68.	61.
3.	65.	65.	65.	65.	65.	65.	65.	65.	65.	58.
4.	64.	64.	64.	64.	64.	64.	64.	64.	64.	57.
5.	64.	64.	64.	64.	64.	64.	64.	64.	64.	57.
6.	65.	69.	69.	69.	69.	79.	97.	99.	83.	68.
7.	68.	77.	77.	77.	85.	121.	131.	108.	90.	
8.	71.	84.	84.	84.	85.	126.	143.	126.	112.	
9.	75.	101.	92.	92.	92.	124.	146.	137.	133.	
10.	80.	117.	100.	100.	100.	116.	141.	141.	150.	
11.	84.	130.	107.	107.	107.	107.	130.	140.	164.	
12.	89.	138.	127.	112.	112.	112.	116.	133.	172.	
13.	93.	141.	145.	132.	116.	116.	116.	122.	175.	
14.	96.	138.	156.	152.	128.	118.	118.	118.	171.	
15.	99.	130.	161.	167.	143.	117.	117.	117.	162.	
16.	100.	118.	158.	173.	153.	115.	115.	115.	148.	
17.	100.	111.	148.	169.	156.	117.	111.	111.	111.	130.
18.	99.	105.	127.	148.	143.	116.	105.	105.	105.	110.
19.	96.	97.	98.	101.	101.	98.	97.	97.	97.	90.
20.	93.	93.	93.	93.	93.	93.	93.	93.	93.	86.
21.	89.	89.	89.	89.	89.	89.	89.	89.	89.	82.
22.	84.	84.	84.	84.	84.	84.	84.	84.	84.	77.
23.	80.	80.	80.	80.	80.	80.	80.	80.	80.	73.
24.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.

LOCATION: WILMINGTON, DELAWARE

MONTH= 7 DAY=21 FOR LATITUDE= 39.7 LONGITUDE= 75.6

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
2.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.
3.	74.	74.	74.	74.	74.	74.	74.	74.	74.	67.
4.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
5.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
6.	74.	76.	76.	76.	76.	81.	91.	92.	84.	73.
7.	75.	80.	80.	80.	80.	84.	102.	107.	96.	84.
8.	77.	84.	84.	84.	84.	84.	104.	113.	105.	95.
9.	79.	93.	88.	88.	88.	88.	103.	114.	110.	105.
10.	82.	101.	92.	92.	92.	92.	99.	112.	113.	114.
11.	84.	108.	96.	95.	95.	95.	95.	107.	112.	120.
12.	87.	112.	107.	98.	98.	98.	98.	100.	109.	125.
13.	89.	113.	116.	109.	100.	100.	100.	100.	104.	126.
14.	91.	112.	122.	119.	106.	101.	101.	101.	101.	124.
15.	92.	108.	124.	126.	114.	101.	101.	101.	101.	120.
16.	93.	102.	122.	129.	120.	100.	100.	100.	100.	113.
17.	93.	98.	117.	127.	121.	101.	98.	98.	98.	104.
18.	92.	95.	106.	116.	114.	101.	95.	95.	95.	94.
19.	91.	91.	92.	93.	93.	92.	91.	91.	91.	84.
20.	89.	89.	89.	89.	89.	89.	89.	89.	89.	82.
21.	87.	87.	87.	87.	87.	87.	87.	87.	87.	80.
22.	84.	84.	84.	84.	84.	84.	84.	84.	84.	77.
23.	82.	82.	82.	82.	82.	82.	82.	82.	82.	75.
24.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.

LOCATION: WILMINGTON, DELAWARE

MONTH= 7 DAY=21 FOR LATITUDE= 39.7 LONGITUDE= 75.6

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
2.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.
3.	74.	74.	74.	74.	74.	74.	74.	74.	74.	67.
4.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
5.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
6.	74.	78.	78.	78.	78.	88.	109.	111.	94.	78.
7.	75.	84.	84.	84.	84.	92.	129.	139.	117.	99.
8.	77.	91.	90.	90.	90.	90.	132.	150.	133.	119.
9.	79.	107.	96.	96.	96.	96.	126.	149.	142.	138.
10.	82.	121.	102.	102.	102.	102.	117.	142.	144.	153.
11.	84.	132.	108.	106.	106.	106.	106.	129.	140.	163.
12.	87.	137.	127.	110.	110.	110.	110.	113.	131.	169.
13.	89.	138.	142.	129.	112.	112.	112.	112.	118.	170.
14.	91.	133.	152.	147.	122.	112.	112.	112.	112.	165.
15.	92.	124.	155.	160.	136.	110.	110.	110.	110.	155.
16.	93.	111.	152.	166.	146.	108.	108.	108.	108.	140.
17.	93.	104.	140.	161.	148.	109.	104.	104.	104.	123.
18.	92.	98.	120.	140.	136.	109.	98.	98.	98.	103.
19.	91.	91.	93.	94.	95.	93.	91.	91.	91.	85.
20.	89.	89.	89.	89.	89.	89.	89.	89.	89.	82.
21.	87.	87.	87.	87.	87.	87.	87.	87.	87.	80.
22.	84.	84.	84.	84.	84.	84.	84.	84.	84.	77.
23.	82.	82.	82.	82.	82.	82.	82.	82.	82.	75.
24.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.

LOCATION: MACON, GEORGIA

MONTH= 7 DAY=21 FOR LATITUDE= 32.7 LONGITUDE= 83.6

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	80.	80.	80.	80.	80.	80.	80.	80.	80.	73.
2.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
3.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
4.	76.	76.	76.	76.	76.	76.	76.	76.	76.	69.
5.	76.	76.	76.	76.	76.	76.	76.	76.	76.	69.
6.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
7.	78.	81.	81.	81.	81.	87.	100.	103.	92.	80.
8.	80.	86.	86.	86.	86.	90.	109.	115.	103.	93.
9.	83.	90.	90.	90.	90.	91.	111.	119.	111.	105.
10.	86.	99.	95.	95.	95.	95.	109.	119.	115.	115.
11.	88.	106.	99.	99.	99.	99.	106.	116.	116.	124.
12.	91.	112.	104.	103.	103.	103.	103.	110.	114.	130.
13.	94.	114.	110.	106.	106.	106.	106.	109.	114.	133.
14.	96.	115.	122.	120.	111.	107.	107.	107.	107.	133.
15.	97.	112.	126.	129.	119.	107.	107.	107.	107.	129.
16.	98.	108.	127.	134.	125.	106.	106.	106.	106.	123.
17.	98.	104.	123.	134.	127.	107.	104.	104.	104.	114.
18.	97.	101.	115.	127.	123.	107.	101.	101.	101.	103.
19.	96.	97.	101.	106.	105.	100.	97.	97.	97.	91.
20.	94.	94.	94.	94.	94.	94.	94.	94.	94.	87.
21.	91.	91.	91.	91.	91.	91.	91.	91.	91.	84.
22.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
23.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
24.	83.	83.	83.	83.	83.	83.	83.	83.	83.	76.

LOCATION: MACON, GEORGIA

MONTH= 7 DAY=21 FOR LATITUDE= 32.7 LONGITUDE= 83.6

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	80.	80.	80.	80.	80.	80.	80.	80.	80.	73.
2.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
3.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
4.	76.	76.	76.	76.	76.	76.	76.	76.	76.	69.
5.	76.	76.	76.	76.	76.	76.	76.	76.	76.	69.
6.	77.	77.	77.	77.	77.	77.	78.	78.	77.	70.
7.	78.	84.	84.	84.	84.	96.	122.	127.	106.	89.
8.	80.	91.	91.	91.	91.	99.	138.	149.	127.	112.
9.	83.	98.	98.	98.	98.	98.	139.	156.	139.	133.
10.	85.	112.	105.	105.	105.	133.	153.	144.	152.	
11.	88.	124.	110.	110.	110.	124.	143.	143.	167.	
12.	91.	132.	117.	115.	115.	115.	129.	137.	176.	
13.	94.	135.	125.	117.	117.	117.	124.	135.	179.	
14.	95.	134.	148.	145.	126.	118.	118.	118.	118.	177.
15.	97.	128.	155.	161.	141.	117.	117.	117.	117.	169.
16.	98.	118.	156.	170.	152.	115.	115.	115.	115.	155.
17.	98.	111.	149.	170.	156.	116.	111.	111.	111.	137.
18.	97.	105.	133.	156.	149.	116.	105.	105.	105.	116.
19.	96.	98.	106.	115.	115.	104.	98.	98.	98.	94.
20.	94.	94.	94.	94.	94.	94.	94.	94.	94.	87.
21.	91.	91.	91.	91.	91.	91.	91.	91.	91.	84.
22.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
23.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
24.	83.	83.	83.	83.	83.	83.	83.	83.	83.	76.

LOCATION: INDIANAPOLIS, INDIANA

MONTH= 7 DAY=21 FOR LATITUDE= 39.7 LONGITUDE= 86.3

ALPHA/HF .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NF	EAST	SE	HORIZ
1.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.
2.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
3.	72.	72.	72.	72.	72.	72.	72.	72.	72.	65.
4.	71.	71.	71.	71.	71.	71.	71.	71.	71.	64.
5.	71.	71.	71.	71.	71.	71.	71.	71.	71.	64.
6.	72.	72.	72.	72.	72.	73.	74.	74.	73.	65.
7.	73.	76.	76.	76.	76.	82.	95.	97.	87.	75.
8.	75.	81.	81.	81.	81.	83.	103.	109.	99.	87.
9.	78.	87.	85.	85.	85.	85.	104.	114.	107.	98.
10.	81.	96.	90.	90.	90.	90.	103.	115.	112.	108.
11.	83.	105.	94.	94.	94.	94.	99.	112.	114.	117.
12.	86.	111.	101.	97.	97.	97.	97.	106.	113.	123.
13.	89.	114.	109.	100.	100.	100.	100.	102.	111.	126.
14.	91.	114.	119.	113.	102.	102.	102.	102.	103.	127.
15.	92.	112.	123.	122.	110.	102.	102.	102.	102.	124.
16.	93.	107.	124.	128.	117.	102.	102.	102.	102.	119.
17.	93.	100.	121.	129.	120.	100.	100.	100.	100.	111.
18.	92.	97.	113.	124.	119.	101.	97.	97.	97.	101.
19.	91.	93.	101.	110.	108.	98.	93.	93.	93.	90.
20.	89.	89.	89.	89.	89.	89.	89.	89.	89.	82.
21.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
22.	83.	83.	83.	83.	83.	83.	83.	83.	83.	76.
23.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
24.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.

LOCATION: INDIANAPOLIS, INDIANA

MONTH= 7 DAY=21 FOR LATITUDE= 39.7 LONGITUDE= 86.3

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NF	EAST	SE	HORIZ
1.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.
2.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
3.	72.	72.	72.	72.	72.	72.	72.	72.	72.	65.
4.	71.	71.	71.	71.	71.	71.	71.	71.	71.	64.
5.	71.	71.	71.	71.	71.	71.	71.	71.	71.	64.
6.	72.	72.	72.	72.	72.	74.	75.	75.	73.	65.
7.	73.	79.	79.	79.	79.	90.	117.	121.	101.	84.
8.	75.	86.	86.	86.	86.	92.	131.	143.	122.	105.
9.	78.	96.	92.	92.	92.	92.	131.	151.	136.	125.
10.	81.	112.	99.	99.	99.	99.	124.	149.	144.	143.
11.	83.	126.	104.	104.	104.	104.	114.	140.	145.	157.
12.	86.	135.	115.	109.	109.	109.	109.	126.	139.	167.
13.	89.	139.	129.	112.	112.	112.	112.	115.	133.	171.
14.	91.	138.	147.	136.	113.	113.	113.	113.	115.	170.
15.	92.	132.	155.	153.	127.	112.	112.	112.	112.	163.
16.	93.	121.	155.	163.	140.	110.	110.	110.	110.	151.
17.	93.	108.	149.	166.	148.	107.	107.	107.	107.	135.
18.	92.	102.	135.	156.	146.	110.	102.	102.	102.	116.
19.	91.	95.	111.	128.	126.	105.	95.	95.	95.	96.
20.	89.	89.	89.	89.	89.	89.	89.	89.	89.	82.
21.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
22.	83.	83.	83.	83.	83.	83.	83.	83.	83.	76.
23.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
24.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.

LOCATION: KALAMAZOO, MICHIGAN

MONTH= 7 DAY=21 FOR LATITUDE= 42.2 LONGITUDE= 84.5

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
2.	71.	71.	71.	71.	71.	71.	71.	71.	71.	64.
3.	70.	70.	70.	70.	70.	70.	70.	70.	70.	63.
4.	69.	69.	69.	69.	69.	69.	69.	69.	69.	62.
5.	69.	69.	69.	69.	69.	69.	69.	69.	69.	62.
6.	70.	70.	70.	70.	70.	73.	76.	76.	73.	64.
7.	71.	75.	75.	75.	75.	80.	95.	98.	87.	75.
8.	73.	79.	79.	79.	79.	81.	101.	108.	98.	86.
9.	76.	87.	84.	84.	84.	84.	101.	112.	106.	97.
10.	79.	97.	88.	88.	88.	88.	99.	112.	111.	107.
11.	82.	105.	92.	92.	92.	92.	95.	109.	113.	115.
12.	85.	111.	101.	96.	96.	96.	96.	103.	112.	121.
13.	88.	114.	108.	99.	99.	99.	99.	101.	112.	124.
14.	90.	114.	119.	113.	101.	101.	101.	101.	101.	125.
15.	91.	112.	123.	122.	108.	101.	101.	101.	101.	122.
16.	92.	106.	124.	127.	115.	100.	100.	100.	100.	117.
17.	92.	99.	120.	128.	119.	99.	99.	99.	99.	109.
18.	91.	96.	112.	123.	118.	100.	96.	96.	96.	99.
19.	90.	92.	99.	107.	106.	97.	92.	92.	92.	88.
20.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
21.	85.	85.	85.	85.	85.	85.	85.	85.	85.	78.
22.	82.	82.	82.	82.	82.	82.	82.	82.	82.	75.
23.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.
24.	76.	76.	76.	76.	76.	76.	76.	76.	76.	69.

LOCATION: KALAMAZOO, MICHIGAN

MONTH= 7 DAY=21 FOR LATITUDE= 42.2 LONGITUDE= 84.5

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
2.	71.	71.	71.	71.	71.	71.	71.	71.	71.	64.
3.	70.	70.	70.	70.	70.	70.	70.	70.	70.	63.
4.	69.	69.	69.	69.	69.	69.	69.	69.	69.	62.
5.	69.	69.	69.	69.	69.	69.	69.	69.	69.	62.
6.	70.	71.	71.	71.	71.	76.	83.	83.	76.	66.
7.	71.	78.	78.	78.	78.	89.	118.	124.	103.	85.
8.	73.	85.	85.	85.	85.	88.	128.	143.	123.	106.
9.	76.	98.	91.	91.	91.	91.	127.	149.	137.	125.
10.	79.	114.	97.	97.	97.	97.	119.	146.	144.	142.
11.	82.	128.	103.	103.	103.	103.	109.	136.	144.	156.
12.	85.	137.	118.	107.	107.	107.	107.	122.	139.	164.
13.	88.	141.	128.	110.	110.	110.	110.	115.	136.	168.
14.	90.	139.	149.	136.	111.	111.	111.	111.	113.	167.
15.	91.	132.	155.	153.	125.	111.	111.	111.	111.	160.
16.	92.	121.	155.	163.	138.	109.	109.	109.	109.	148.
17.	92.	106.	148.	164.	146.	105.	105.	105.	105.	132.
18.	91.	100.	133.	154.	144.	108.	100.	100.	100.	114.
19.	90.	94.	109.	125.	123.	104.	94.	94.	94.	93.
20.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
21.	85.	85.	85.	85.	85.	85.	85.	85.	85.	78.
22.	82.	82.	82.	82.	82.	82.	82.	82.	82.	75.
23.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.
24.	76.	76.	76.	76.	76.	76.	76.	76.	76.	69.

LOCATION: ST. LOUIS, MISSOURI

MONTH= 7 DAY=21 FOR LATITUDE= 38.6 LONGITUDE= 90.2

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
2.	80.	80.	80.	80.	80.	80.	80.	80.	80.	73.
3.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.
4.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
5.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
6.	79.	81.	81.	81.	81.	86.	96.	97.	89.	77.
7.	80.	84.	84.	84.	84.	89.	107.	112.	101.	88.
8.	81.	89.	88.	88.	88.	88.	109.	118.	109.	99.
9.	84.	97.	92.	92.	92.	92.	107.	119.	114.	110.
10.	86.	105.	96.	96.	96.	96.	104.	116.	117.	118.
11.	88.	111.	100.	99.	99.	99.	99.	110.	116.	125.
12.	90.	115.	110.	102.	102.	102.	102.	103.	112.	128.
13.	93.	116.	119.	113.	104.	104.	104.	104.	106.	130.
14.	94.	115.	124.	123.	110.	105.	105.	105.	105.	128.
15.	95.	111.	127.	130.	118.	104.	104.	104.	104.	123.
16.	96.	105.	125.	132.	123.	103.	103.	103.	103.	116.
17.	96.	101.	119.	130.	124.	104.	101.	101.	101.	107.
18.	95.	98.	109.	119.	116.	104.	98.	98.	98.	97.
19.	94.	94.	95.	95.	95.	95.	94.	94.	94.	87.
20.	93.	93.	93.	93.	93.	93.	93.	93.	93.	86.
21.	90.	90.	90.	90.	90.	90.	90.	90.	90.	83.
22.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
23.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
24.	84.	84.	84.	84.	84.	84.	84.	84.	84.	77.

LOCATION: ST. LOUIS, MISSOURI

MONTH= 7 DAY=21 FOR LATITUDE= 38.6 LONGITUDE= 90.2

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
2.	80.	80.	80.	80.	80.	80.	80.	80.	80.	73.
3.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.
4.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
5.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
6.	79.	83.	83.	83.	83.	93.	114.	116.	99.	83.
7.	80.	89.	89.	89.	89.	97.	134.	144.	122.	104.
8.	81.	96.	95.	95.	95.	95.	137.	154.	137.	124.
9.	84.	111.	101.	101.	101.	101.	131.	154.	145.	143.
10.	86.	124.	106.	106.	106.	106.	121.	146.	147.	157.
11.	88.	134.	112.	110.	110.	110.	110.	133.	143.	168.
12.	90.	140.	130.	114.	114.	114.	114.	116.	134.	173.
13.	93.	140.	145.	133.	115.	115.	115.	115.	120.	174.
14.	94.	135.	155.	151.	127.	115.	115.	115.	115.	168.
15.	95.	126.	158.	164.	141.	114.	114.	114.	114.	158.
16.	96.	113.	154.	169.	150.	111.	111.	111.	111.	143.
17.	96.	106.	142.	164.	151.	113.	106.	106.	106.	125.
18.	95.	101.	122.	142.	137.	112.	101.	101.	101.	105.
19.	94.	94.	95.	96.	96.	95.	94.	94.	94.	87.
20.	93.	93.	93.	93.	93.	93.	93.	93.	93.	86.
21.	90.	90.	90.	90.	90.	90.	90.	90.	90.	83.
22.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
23.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
24.	84.	84.	84.	84.	84.	84.	84.	84.	84.	77.

LOCATION: JERSEY CITY, NEW JERSEY

MONTH= 7 DAY=21 FOR LATITUDE= 40.7 LONGITUDE= 74.2

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	76.	76.	76.	76.	76.	76.	76.	76.	76.	69.
2.	74.	74.	74.	74.	74.	74.	74.	74.	74.	67.
3.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
4.	72.	72.	72.	72.	72.	72.	72.	72.	72.	65.
5.	72.	72.	72.	72.	72.	72.	72.	72.	72.	65.
6.	73.	75.	75.	75.	75.	81.	92.	94.	85.	73.
7.	74.	79.	79.	79.	79.	82.	101.	107.	96.	84.
8.	76.	84.	83.	83.	83.	83.	103.	112.	105.	94.
9.	78.	93.	87.	87.	87.	87.	101.	113.	110.	104.
10.	81.	101.	91.	91.	91.	91.	97.	110.	112.	113.
11.	83.	108.	96.	94.	94.	94.	94.	105.	111.	119.
12.	86.	112.	107.	97.	97.	97.	97.	98.	108.	123.
13.	88.	113.	116.	109.	99.	99.	99.	99.	102.	124.
14.	90.	111.	121.	119.	106.	100.	100.	100.	100.	123.
15.	91.	107.	123.	126.	113.	100.	100.	100.	100.	118.
16.	92.	101.	121.	128.	119.	99.	99.	99.	99.	111.
17.	92.	97.	115.	126.	119.	100.	97.	97.	97.	102.
18.	91.	94.	104.	114.	112.	100.	94.	94.	94.	92.
19.	90.	90.	91.	91.	91.	90.	90.	90.	90.	83.
20.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
21.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
22.	83.	83.	83.	83.	83.	83.	83.	83.	83.	76.
23.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
24.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.

LOCATION: JERSEY CITY, NEW JERSEY

MONTH= 7 DAY=21 FOR LATITUDE= 40.7 LONGITUDE= 74.2

ALPHA/HF .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	76.	76.	76.	76.	76.	76.	76.	76.	76.	69.
2.	74.	74.	74.	74.	74.	74.	74.	74.	74.	67.
3.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
4.	72.	72.	72.	72.	72.	72.	72.	72.	72.	65.
5.	72.	72.	72.	72.	72.	72.	72.	72.	72.	65.
6.	73.	78.	78.	78.	78.	88.	112.	115.	96.	80.
7.	74.	84.	84.	84.	84.	91.	128.	140.	119.	100.
8.	76.	92.	90.	90.	90.	90.	130.	149.	133.	120.
9.	78.	108.	96.	96.	96.	96.	123.	148.	141.	138.
10.	81.	122.	101.	101.	101.	101.	113.	140.	143.	152.
11.	83.	132.	110.	105.	105.	105.	105.	126.	139.	162.
12.	86.	137.	128.	109.	109.	109.	109.	110.	130.	168.
13.	88.	138.	143.	129.	110.	110.	110.	110.	116.	168.
14.	90.	132.	152.	148.	121.	111.	111.	111.	111.	162.
15.	91.	123.	155.	160.	136.	109.	109.	109.	109.	152.
16.	92.	110.	150.	165.	145.	106.	106.	106.	106.	138.
17.	92.	102.	138.	159.	147.	108.	102.	102.	102.	120.
18.	91.	97.	117.	137.	133.	108.	97.	97.	97.	100.
19.	90.	90.	91.	92.	92.	91.	90.	90.	90.	83.
20.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
21.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
22.	83.	83.	83.	83.	83.	83.	83.	83.	83.	76.
23.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
24.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.

LOCATION: MEMPHIS, TENNESSEE

MONTH= 7 DAY=21 FOR LATITUDE= 35.1 LONGITUDE= 90.0

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
2.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.
3.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
4.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
5.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
6.	78.	80.	80.	80.	80.	84.	94.	95.	87.	76.
7.	79.	84.	84.	84.	84.	88.	106.	111.	100.	87.
8.	81.	88.	88.	88.	88.	89.	109.	117.	108.	99.
9.	83.	96.	92.	92.	92.	92.	109.	119.	113.	110.
10.	80.	104.	96.	96.	96.	100.	105.	116.	116.	119.
11.	89.	110.	100.	100.	100.	100.	101.	111.	115.	126.
12.	92.	114.	110.	103.	103.	103.	103.	104.	112.	130.
13.	94.	115.	119.	114.	105.	105.	105.	105.	106.	132.
14.	96.	114.	125.	125.	114.	107.	107.	107.	107.	130.
15.	97.	111.	127.	132.	121.	106.	106.	106.	106.	125.
16.	98.	105.	126.	135.	126.	105.	105.	105.	105.	118.
17.	98.	103.	120.	131.	126.	107.	103.	103.	103.	108.
18.	97.	100.	109.	119.	117.	105.	100.	100.	100.	98.
19.	96.	96.	96.	96.	96.	96.	96.	96.	96.	89.
20.	94.	94.	94.	94.	94.	94.	94.	94.	94.	87.
21.	92.	92.	92.	92.	92.	92.	92.	92.	92.	85.
22.	89.	89.	89.	89.	89.	89.	89.	89.	89.	82.
23.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
24.	83.	83.	83.	83.	83.	83.	83.	83.	83.	76.

LOCATION: MEMPHIS, TENNESSEE

MONTH= 7 DAY=21 FOR LATITUDE= 35.1 LONGITUDE= 90.0

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
2.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.
3.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
4.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
5.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
6.	78.	82.	82.	82.	82.	91.	110.	112.	96.	81.
7.	79.	88.	88.	88.	88.	98.	133.	143.	120.	103.
8.	81.	95.	95.	95.	95.	97.	138.	154.	135.	124.
9.	83.	108.	101.	101.	101.	101.	134.	154.	143.	143.
10.	86.	121.	107.	107.	107.	107.	125.	147.	145.	159.
11.	89.	131.	112.	112.	112.	112.	114.	134.	141.	170.
12.	92.	136.	129.	115.	115.	115.	115.	117.	132.	176.
13.	94.	137.	144.	135.	117.	117.	117.	117.	118.	177.
14.	96.	133.	154.	153.	132.	117.	117.	117.	117.	171.
15.	97.	124.	157.	166.	145.	116.	116.	116.	116.	160.
16.	98.	113.	154.	171.	154.	113.	113.	113.	113.	145.
17.	98.	108.	142.	165.	154.	116.	108.	108.	108.	126.
18.	97.	102.	122.	140.	137.	113.	102.	102.	102.	105.
19.	96.	96.	96.	96.	96.	96.	96.	96.	96.	89.
20.	94.	94.	94.	94.	94.	94.	94.	94.	94.	87.
21.	92.	92.	92.	92.	92.	92.	92.	92.	92.	85.
22.	89.	89.	89.	89.	89.	89.	89.	89.	89.	82.
23.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
24.	83.	83.	83.	83.	83.	83.	83.	83.	83.	76.

LOCATION: HOUSTON, TEXAS

MONTH= 7 DAY=21 FOR LATITUDE= 29.6 LONGITUDE= 95.3

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
2.	80.	80.	80.	80.	80.	80.	80.	80.	80.	73.
3.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.
4.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
5.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
6.	79.	79.	79.	79.	79.	82.	85.	85.	82.	73.
7.	80.	87.	87.	87.	99.	128.	133.	111.	94.	
8.	81.	93.	93.	93.	102.	140.	152.	129.	117.	
9.	84.	100.	100.	100.	101.	140.	156.	139.	138.	
10.	80.	111.	106.	106.	106.	134.	151.	142.	156.	
11.	88.	121.	111.	111.	111.	124.	140.	139.	169.	
12.	90.	128.	117.	114.	114.	114.	124.	130.	177.	
13.	93.	130.	134.	127.	116.	116.	116.	118.	179.	
14.	94.	127.	145.	147.	131.	117.	117.	117.	174.	
15.	95.	120.	151.	161.	144.	115.	115.	115.	164.	
16.	96.	112.	151.	169.	153.	114.	112.	112.	149.	
17.	96.	108.	143.	166.	155.	116.	108.	108.	130.	
18.	95.	102.	125.	146.	142.	114.	102.	102.	102.	108.
19.	94.	94.	95.	97.	97.	95.	94.	94.	94.	88.
20.	93.	93.	93.	93.	93.	93.	93.	93.	93.	86.
21.	90.	90.	90.	90.	90.	90.	90.	90.	90.	83.
22.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
23.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
24.	84.	84.	84.	84.	84.	84.	84.	84.	84.	77.

LOCATION: HOUSTON, TEXAS

MONTH= 7 DAY=21 FOR LATITUDE= 29.6 LONGITUDE= 95.3

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SF	HORIZ
1.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
2.	80.	80.	80.	80.	80.	80.	80.	80.	80.	73.
3.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.
4.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
5.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
6.	79.	79.	79.	79.	79.	80.	82.	82.	80.	72.
7.	80.	83.	83.	83.	83.	89.	104.	107.	96.	83.
8.	81.	87.	87.	87.	87.	92.	111.	117.	105.	96.
9.	84.	92.	92.	92.	92.	92.	112.	120.	111.	107.
10.	80.	99.	96.	96.	96.	96.	110.	118.	114.	117.
11.	88.	105.	99.	99.	99.	99.	106.	114.	113.	125.
12.	90.	109.	104.	102.	102.	102.	102.	107.	110.	130.
13.	93.	111.	113.	110.	104.	104.	104.	104.	105.	132.
14.	94.	111.	120.	121.	112.	105.	105.	105.	105.	131.
15.	95.	108.	123.	128.	120.	105.	105.	105.	105.	126.
16.	96.	104.	123.	132.	125.	105.	104.	104.	104.	119.
17.	90.	102.	119.	131.	125.	106.	102.	102.	102.	100.
18.	95.	99.	110.	121.	118.	104.	99.	99.	99.	98.
19.	94.	94.	95.	95.	95.	95.	94.	94.	94.	87.
20.	93.	93.	93.	93.	93.	93.	93.	93.	93.	86.
21.	90.	90.	90.	90.	90.	90.	90.	90.	90.	83.
22.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
23.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
24.	84.	84.	84.	84.	84.	84.	84.	84.	84.	77.

LOCATION: SEATTLE, WASHINGTON (CITY)

MONTH= 7 DAY=21 FOR LATITUDE= 47.6 LONGITUDE= 122.3

ALPHA/HF .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	66.	66.	66.	66.	66.	66.	66.	66.	66.	59.
2.	64.	64.	64.	64.	64.	64.	64.	64.	64.	57.
3.	63.	63.	63.	63.	63.	63.	63.	63.	63.	56.
4.	62.	62.	62.	62.	62.	62.	62.	62.	62.	55.
5.	62.	62.	62.	62.	62.	63.	63.	63.	62.	55.
6.	63.	65.	65.	65.	65.	71.	82.	83.	74.	62.
7.	64.	69.	69.	69.	69.	72.	90.	96.	86.	72.
8.	66.	75.	72.	72.	72.	72.	91.	102.	95.	82.
9.	68.	84.	76.	76.	76.	76.	89.	103.	101.	91.
10.	70.	93.	80.	80.	80.	80.	85.	100.	104.	100.
11.	73.	100.	86.	83.	83.	83.	83.	95.	104.	106.
12.	75.	105.	97.	86.	86.	86.	86.	89.	101.	110.
13.	77.	106.	106.	95.	88.	88.	88.	88.	96.	112.
14.	79.	105.	112.	106.	90.	89.	89.	89.	89.	111.
15.	80.	100.	114.	113.	98.	89.	89.	89.	89.	107.
16.	81.	94.	113.	117.	105.	88.	88.	88.	88.	101.
17.	81.	87.	107.	116.	108.	87.	87.	87.	87.	94.
18.	80.	84.	98.	108.	104.	89.	84.	84.	84.	85.
19.	79.	80.	85.	90.	90.	84.	80.	80.	80.	75.
20.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
21.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.
22.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
23.	70.	70.	70.	70.	70.	70.	70.	70.	70.	63.
24.	68.	68.	68.	68.	68.	68.	68.	68.	68.	61.

LOCATION: SEATTLE, WASHINGTON (AIRPORT)

MONTH= 7 DAY=21 FOR LATITUDE= 47.4 LONGITUDE= 122.3

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	67.	67.	67.	67.	67.	67.	67.	67.	67.	60.
2.	65.	65.	65.	65.	65.	65.	65.	65.	65.	58.
3.	64.	64.	64.	64.	64.	64.	64.	64.	64.	57.
4.	63.	63.	63.	63.	63.	63.	63.	63.	63.	56.
5.	63.	63.	63.	63.	63.	64.	65.	65.	64.	56.
6.	64.	69.	69.	69.	80.	102.	105.	87.	70.	
7.	65.	74.	74.	74.	80.	118.	129.	109.	89.	
8.	67.	85.	80.	80.	80.	119.	139.	125.	107.	
9.	70.	103.	86.	86.	86.	112.	140.	136.	124.	
10.	73.	118.	91.	91.	91.	102.	133.	140.	138.	
11.	75.	130.	103.	96.	96.	96.	121.	138.	149.	
12.	78.	137.	122.	100.	100.	100.	105.	130.	155.	
13.	81.	138.	138.	117.	102.	102.	102.	117.	156.	
14.	83.	134.	148.	136.	104.	103.	103.	103.	153.	
15.	84.	124.	152.	150.	120.	102.	102.	102.	145.	
16.	85.	111.	148.	157.	132.	100.	100.	100.	100.	133.
17.	85.	96.	137.	155.	138.	97.	96.	96.	96.	117.
18.	84.	91.	119.	140.	132.	101.	91.	91.	91.	100.
19.	83.	85.	94.	105.	105.	93.	85.	85.	85.	82.
20.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
21.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
22.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.
23.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
24.	70.	70.	70.	70.	70.	70.	70.	70.	70.	63.

LOCATION: SEATTLE, WASHINGTON (AIRPORT)
 MONTH= 7 DAY=21 FOR LATITUDE= 47.4 LONGITUDE= 122.3
ALPHA/HF .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	67.	67.	67.	67.	67.	67.	67.	67.	67.	60.
2.	65.	65.	65.	65.	65.	65.	65.	65.	65.	58.
3.	64.	64.	64.	64.	64.	64.	64.	64.	64.	57.
4.	63.	63.	63.	63.	63.	63.	63.	63.	63.	56.
5.	63.	63.	63.	63.	63.	63.	64.	64.	63.	56.
6.	64.	66.	66.	66.	66.	72.	83.	84.	75.	64.
7.	65.	70.	70.	70.	70.	73.	91.	97.	87.	74.
8.	67.	76.	74.	74.	74.	74.	93.	103.	96.	84.
9.	70.	86.	78.	78.	78.	78.	91.	105.	103.	93.
10.	73.	95.	82.	82.	82.	82.	87.	103.	106.	102.
11.	75.	103.	89.	86.	86.	86.	86.	98.	107.	109.
12.	78.	108.	100.	89.	89.	89.	89.	92.	104.	113.
13.	81.	109.	109.	99.	91.	91.	91.	91.	99.	115.
14.	83.	108.	115.	109.	94.	93.	93.	93.	93.	114.
15.	84.	104.	118.	117.	102.	93.	93.	93.	93.	111.
16.	85.	98.	117.	121.	109.	92.	92.	92.	92.	105.
17.	85.	91.	111.	120.	112.	91.	91.	91.	91.	98.
18.	84.	88.	101.	112.	108.	93.	88.	88.	88.	88.
19.	83.	84.	88.	94.	94.	88.	84.	84.	84.	79.
20.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
21.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
22.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.
23.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
24.	70.	70.	70.	70.	70.	70.	70.	70.	70.	63.

LOCATION: SEATTLE, WASHINGTON (CITY)

MONTH= 7 DAY=21 FOR LATITUDE= 47.6 LONGITUDE= 122.3

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	66.	66.	66.	66.	66.	66.	66.	66.	66.	59.
2.	64.	64.	64.	64.	64.	64.	64.	64.	64.	57.
3.	63.	63.	63.	63.	63.	63.	63.	63.	63.	56.
4.	62.	62.	62.	62.	62.	62.	62.	62.	62.	55.
5.	62.	62.	62.	62.	62.	63.	64.	64.	63.	55.
6.	63.	68.	68.	68.	68.	78.	101.	104.	86.	69.
7.	64.	73.	73.	73.	73.	79.	116.	128.	108.	88.
8.	66.	84.	79.	79.	79.	79.	117.	138.	124.	106.
9.	68.	101.	84.	84.	84.	84.	110.	138.	134.	122.
10.	70.	116.	89.	89.	89.	89.	99.	131.	138.	136.
11.	73.	128.	100.	93.	93.	93.	93.	118.	135.	146.
12.	75.	134.	119.	97.	97.	97.	97.	102.	127.	152.
13.	77.	135.	135.	113.	99.	99.	99.	99.	114.	153.
14.	79.	130.	145.	132.	100.	99.	99.	99.	99.	149.
15.	80.	120.	148.	146.	116.	98.	98.	98.	98.	141.
16.	81.	107.	144.	153.	128.	96.	96.	96.	96.	129.
17.	81.	92.	133.	151.	134.	93.	92.	92.	92.	113.
18.	80.	88.	115.	136.	129.	97.	88.	88.	88.	96.
19.	79.	82.	90.	102.	102.	90.	82.	82.	82.	78.
20.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
21.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.
22.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
23.	70.	70.	70.	70.	70.	70.	70.	70.	70.	63.
24.	68.	68.	68.	68.	68.	68.	68.	68.	68.	61.

Table D

Magnetic Tape TDF 14 for Breakthrough Localities

<u>Localities</u>	<u>Station No.</u>	<u>Record Period</u>	<u>Reel No.</u>
Sacramento, Calif.	23232	Jan. '49 - Dec. '58	069
Wilmington, Del. (Phila., Pa.)	13739	Jan. '49 - Dec. '58	268
Macon, Ga.	03813	Jan. '55 - Dec. '64	527
Indianapolis, Ind.	93819	Jan. '49 - Dec. '58	550
Kalamazoo, Mich. (Battle Creek)	14815	Jan. '49 - Dec. '54	073
St. Louis, Mo.	13984	Jan. '49 - Dec. '58	261
Jersey City, N. J. (Newark, N. J.)	14734	Jan. '49 - Dec. '58	205
Memphis Tennessee	93839	Jan. '49 - Dec. '58	173
Houston, Tex.	12918	Jan. '49 - Dec. '58	259
Seattle, Wash. Sea/Tac airport	24233	Jan. '49 - Dec. '58	088
Downtown Seattle	24244		302, 86, 326

Table E

AFM 88-8 Data for Coincident
Dry- and Wet-Bulb Temperature Frequencies

These tables show the frequency of the hourly dry-bulb temperature observations for a temperature range of 5 degrees F for three daily time periods; from 02 to 09 hours, from 10 to 17 hours and from 18 to 01 hours. Also listed are total frequencies of hourly observations for each month at 5 ° temperature "bin" and average wet-bulb temperature that occurs coincident with the same temperature level specified in the "bin".

BEALE AFB CALIFORNIA (Substitute Station for Sacramento)

Mean Frequency of Occurrence of Dry Bulb Temperature (°F) With Mean Coincident Wet Bulb Temperature (°F) For Each Dry Bulb Temperature Range

COOLING SEASON

Temper- ature Range (°F)	MAY			JUNE			JULY			AUGUST			SEPTEMBER			OCTOBER			
	Obsn/ Hour Gp		Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp															
	08 to 09	10 to 11		08 to 09	10 to 11	18 to 01													
110/114 105/109				1	1	73	6	71	7	2	9	70				0	0	0	70
100/104 95/99	1	0	1	14	4	18	69	25	7	82	68	11	1	12	3	0	3	69	
90/94 85/89	3	1	4	19	6	25	59	49	14	63	58	87	7	44	12	1	13	67	
80/84 75/79	18	4	22	32	10	44	66	1	63	24	88	66	65	20	85	66	37	4	41
65/69 60/64	37	9	46	61	7	48	28	61	64	8	47	33	88	64	1	63	25	79	65
55/59 50/54	80	9	55	144	51	62	14	34	42	90	52	10	42	89	91	65	0	46	10
45/49 40/44	73	4	28	105	48	23	1	6	30	49	2	50	3	50	17	1	18	49	61
35/39 1	19	0	7	26	44	1	1	46					0		0	47	18	6	24
	9	2	11	89	1	37	0	1					1		1	6	1	6	39
	1	1	0	1												1	1	1	36

HEATING SEASON

ANNUAL (TOTAL— ALL MONTHS)											
APRIL											
MARCH											
FEBRUARY											
JANUARY											
DECEMBER											
NOVEMBER											
110/114 165/169	0	0	58								
100/104 95/99	0	10	18	Total Obars Bulb (°F) 69 17 01	02	10	18	Total Obars Bulb (°F) 69 17 01	02	10	18
90/94 85/89	0	0	58								
75/79 70/74	4	4	55								
65/69 60/64	0	22	2	Total Obars Bulb (°F) 69 17 01	1	4	1	1	55	1	53
55/59 50/54	2	51	9	Total Obars Bulb (°F) 69 17 01	53	22	7	34	55	0	1
45/49 40/44	27	68	48	Total Obars Bulb (°F) 69 17 01	1	4	1	6	53	1	53
30/34 25/29	57	49	76	Total Obars Bulb (°F) 69 17 01	1	4	1	1	55	1	55
20/24 25/29	59	14	62	Total Obars Bulb (°F) 69 17 01	22	51	32	105	48	17	60
10/14 20/24	63	4	24	Total Obars Bulb (°F) 69 17 01	33	71	60	44	44	51	20
0/4 5/9	66	9	25	Total Obars Bulb (°F) 69 17 01	48	69	182	49	52	49	73
0/4 5/9	6	0	6	Total Obars Bulb (°F) 69 17 01	11	16	47	31	51	9	31
0/4 5/9	0	0	24	Total Obars Bulb (°F) 69 17 01	1	1	9	27	24	1	4
0/4 5/9	0	0	24	Total Obars Bulb (°F) 69 17 01	2	2	2	26	0	0	25

* WILMINGTON DELAWARE

Mean Frequency of Occurrence of Dry Bulb Temperature ($^{\circ}\text{F}$) With Mean Coincident Wet Bulb Temperature ($^{\circ}\text{F}$) For Each Dry Bulb Temperature Range

COOLING SEASON

Temperature Range ($^{\circ}\text{F}$)	MAY						JUNE						JULY						AUGUST						SEPTEMBER						OCTOBER					
	Obsn./Hour Gp			Obsn./Hour Gp			Obsn./Hour Gp			Obsn./Hour Gp			Obsn./Hour Gp			Obsn./Hour Gp			Obsn./Hour Gp			Obsn./Hour Gp			Obsn./Hour Gp			Obsn./Hour Gp								
	08 to 09	10 to 11	18 to 01																																	
100/104																																				
96/99																																				
90/94	3	3	71	0	12	1	13	74	0	22	2	24	74	0	13	0	13	75	0	5	5	76	0	5	5	76	0	5	5	76	0	5	5			
85/89	10	1	11	70	1	89	3	43	72	3	58	9	70	73	1	47	4	52	73	0	21	1	22	74	0	9	9	71	0	9	9					
80/84	1	20	8	24	68	6	54	17	77	69	12	81	80	123	70	7	68	20	96	71	2	39	6	47	72	0	9	9	71	0	9	9				
75/79	4	36	10	49	65	19	52	37	108	67	44	53	69	166	69	32	72	60	164	69	13	49	28	90	69	1	19	3	23	66	1	19	3			
70/74	12	49	23	84	62	49	43	56	148	65	87	23	82	192	68	34	35	90	299	68	40	50	49	139	66	6	33	10	49	64	6	33	10			
65/69	31	54	42	127	60	64	25	62	151	61	3	43	107	64	74	8	54	136	64	67	47	59	163	62	14	53	20	87	60	14	53	20				
60/64	50	39	60	149	56	54	9	48	106	58	33	0	12	45	59	38	1	17	51	60	43	22	43	108	58	30	48	43	121	57	30	48	43			
55/59	57	23	50	180	52	34	3	16	58	54	8	1	9	55	16	3	19	55	38	6	31	75	58	43	43	52	138	63	43	43	52					
50/54	49	13	37	99	48	12	2	5	19	50	0	0	50	1	1	1	51	28	0	17	45	49	51	28	55	134	48	51	28	55	134	48				
45/49	30	2	18	50	44	1	1	45										13	0	6	18	45	49	10	36	95	44	13	0	6	18	45	49	10		
40/44	11	1	4	15	39	0	3	35										5	1	6	40	32	3	20	65	39	12	32	3	20	65	39	12	32		
35/39	3																	1	1	1	36	18	0	7	25	35	12	32	3	20	65	39	12	32		
30/34																																				

HEATING SEASON

ROBINS AFB GEORGIA (Substitute Station for Macon)

Mean Frequency of Occurrence of Dry Bulb Temperature ($^{\circ}\text{F}$) With Mean Coincident Wet Bulb Temperature ($^{\circ}\text{F}$) For Each Dry Duo I Temperature Range

COOLING SEASON

HEATING SEASON

Temperature Range (°F)	NOVEMBER			DECEMBER			JANUARY			FEBRUARY			MARCH			APRIL			ANNUAL (TOTAL—ALL MONTHS)		
	Obsn/Hour Gp	Mean Co-incident Wet Bulb (°F)	Total Obsn (°F)	Obsn/Hour Gp	Mean Co-incident Wet Bulb (°F)	Total Obsn (°F)	Obsn/Hour Gp	Mean Co-incident Wet Bulb (°F)	Total Obsn (°F)	Obsn/Hour Gp	Mean Co-incident Wet Bulb (°F)	Total Obsn (°F)	Obsn/Hour Gp	Mean Co-incident Wet Bulb (°F)	Total Obsn (°F)	Obsn/Hour Gp	Mean Co-incident Wet Bulb (°F)	Total Obsn (°F)			
100/104																					
95/99																					
90/94																					
85/89	1	1	69	0	0	69				0	0	59	1	0	1	67	15	2	71	3	76
80/84	8	0	8	68	0	68				3	0	66	6	1	7	65	38	12	50	54	59
75/79	25	3	29	64	5	65	3	0	3	55	10	2	12	55	20	5	26	63	0	25	74
70/74	1	37	15	53	2	17	2	21	62	0	10	3	13	62	1	16	8	25	51	12	50
65/69	17	48	31	95	50	4	25	13	42	50	4	20	10	34	60	6	25	19	50	44	106
60/64	30	45	40	115	56	15	34	25	74	56	10	31	17	58	55	17	30	27	74	56	144
65/69	32	30	43	105	62	15	39	30	85	61	18	35	27	80	51	24	37	35	95	51	131
50/54	33	25	39	97	47	23	41	44	108	46	21	39	35	95	45	26	34	35	61	29	125
45/49	31	13	34	78	43	32	35	36	103	42	28	35	44	107	42	35	30	34	99	42	47
40/44	42	5	20	57	39	28	43	110	38	33	36	42	110	38	43	12	21	75	38	15	44
35/39	35	2	10	48	34	46	15	31	92	34	50	21	32	103	34	32	12	18	52	34	40
30/34	18	0	4	17	30	37	7	17	51	29	42	13	25	80	29	23	4	10	37	29	11
35/29	4	1	5	25	25	1	6	32	25	28	5	10	43	25	16	2	3	21	3	0	3
20/24	1	1	21	7	1	9	20	11	1	3	15	20	3	0	1	4	19	1	20	23	2
15/19				1	0	0	1	15	3	0	0	3	15	1	0	1	2	14	6	1	1
10/14				1	0	0	1	11	0	0	0	0	9	1	0	0	5	0	2	10	1
5/9				0				8					0					1	1	7	

SCOTT AFB ILLINOIS (Substitute Station for St. Louis)

Mean Frequency of Occurrence of Dry Bulb Temperature ($^{\circ}\text{F}$) With Mean Coincident Wet Bulb Temperature Range

COOLING SEASON

HEATING SEASON

* INDIANAPOLIS INDIANA

Mean Frequency of Occurrence of Dry Bulb Temperature (°F) With Mean Coincident Wet Bulb Temperature (°F) For Each Dry Bulb Temperature Range

COOLING SEASON

Temperature Range (°F)	MAY			JUNE			JULY			AUGUST			SEPTEMBER			OCTOBER				
	Obsn/Hr Gp			Obsn/Hr Gp			Obsn/Hr Gp			Obsn/Hr Gp			Obsn/Hr Gp			Obsn/Hr Gp				
	08 to 09	10 to 11	18 to 01	Total Obsn	08 to 09	10 to 11	18 to 01	Total Obsn	08 to 09	10 to 11	18 to 01	Total Obsn	08 to 09	10 to 11	18 to 01	Total Obsn	08 to 09	10 to 11	18 to 01	Total Obsn
100/104					0	0	0	76	0	0	78	2	2	72	0	0	71	0	0	71
95/99					3	0	3	76	4	0	76	19	0	19	74	0	11	0	8	69
90/94	1	1	1	69	0	24	1	25	74	-1	22	1	24	75	1	31	2	34	71	
85/89	0	7	0	7	69	4	37	6	47	72	4	58	9	71	73	2	52	4	58	73
80/84	1	22	2	25	67	11	51	22	84	70	14	80	31	125	71	10	80	21	111	71
75/79	4	42	12	58	65	28	54	42	124	68	39	57	63	159	69	27	60	55	142	69
70/74	15	48	26	89	63	47	37	61	145	66	77	22	61	180	68	70	27	80	177	68
65/69	86	47	45	127	60	56	20	52	128	62	68	5	46	119	64	69	8	55	132	64
60/64	48	39	54	141	57	48	8	32	98	84	0	15	49	59	49	0	26	75	59	47
55/59	43	16	42	101	52	29	5	16	60	64	9	2	11	65	17	0	24	55	39	4
50/54	42	14	30	86	48	14	1	7	22	50	2	2	62	4	0	4	51	30	1	22
45/49	30	8	21	59	44	8	1	4	46	46	0	0	41	0	7	1	8	20	1	8
40/44	19	3	12	34	39	0	0	0	41	0	0	0	0	0	0	1	8	41	1	8
35/39	9	1	4	14	36	0	0	0	38	0	0	0	0	0	0	0	0	0	0	0
30/34	2	0	2	31														0	0	0
25/29																		3	1	4
20/24																		0	0	22

HEATING SEASON

* BATTLE CREEK MICHIGAN (Substitute Station for Kalamazoo)

Mean Frequency of Occurrence of Dry Bulb Temperature ($^{\circ}\text{F}$) With Mean Coincident Wet Bulb Temperature ($^{\circ}\text{F}$) For Each Dry Bulb Temperature Range

COOLING SEASON

Temperature Range ($^{\circ}\text{F}$)	MAY						JUNE						JULY						AUGUST						SEPTEMBER						OCTOBER					
	Open/ Hour Gp			Mean Coincident Wet Bulb ($^{\circ}\text{F}$)			Open/ Hour Gp			Mean Coincident Wet Bulb ($^{\circ}\text{F}$)			Open/ Hour Gp			Mean Coincident Wet Bulb ($^{\circ}\text{F}$)			Open/ Hour Gp			Mean Coincident Wet Bulb ($^{\circ}\text{F}$)			Open/ Hour Gp			Mean Coincident Wet Bulb ($^{\circ}\text{F}$)								
	02 to 03	10 to 09	18 to 08	Total Open	02 to 09	10 to 09	18 to 09	Total Open	02 to 09	10 to 09	18 to 09	Total Open	02 to 09	10 to 09	18 to 09	Total Open	02 to 09	10 to 09	18 to 09	Total Open	02 to 09	10 to 09	18 to 09	Total Open	02 to 09	10 to 09	18 to 09	Total Open	02 to 09	10 to 09	18 to 09	Total Open				
95/99	0	0	0	73	2	0	2	76	2	0	2	75	4	0	4	71	1	1	1	71	0	5	0	6	70	0	6	1	70	1	1	1	70			
90/94	0	5	0	70	9	1	10	76	16	1	17	73	1	25	4	30	70	0	6	1	7	69	1	7	1	70	9	9	9	64						
85/89	5	0	5	70	1	86	6	43	1	45	9	55	70	4	64	16	74	68	0	17	3	20	66	0	17	3	20	66	0	17	3	20				
80/84	0	22	3	25	66	4	61	13	73	70	7	73	27	107	69	4	64	16	74	68	3	20	66	0	17	3	20	66	0	17	3	20				
75/79	2	29	9	40	64	21	43	33	107	68	21	63	47	126	67	12	61	31	104	66	3	31	10	44	64	0	14	2	16	64	0	14	2	16		
70/74	7	84	19	60	60	43	39	50	132	65	60	85	63	168	65	40	54	63	157	65	13	44	21	73	62	2	23	7	32	61	2	23	7	32		
65/69	21	42	84	97	58	60	27	51	138	62	62	13	60	125	62	61	25	54	140	62	21	50	36	107	60	9	34	16	59	59	9	34	16	59		
60/64	80	40	36	106	56	45	17	87	99	57	55	6	31	92	58	61	9	52	122	59	44	45	46	186	57	19	32	22	73	56	19	32	22	73		
55/59	43	31	44	113	52	86	3	22	66	54	29	0	13	42	55	44	1	19	64	55	51	28	50	129	53	20	33	34	92	51	20	33	34	92		
50/54	49	24	47	120	48	20	3	13	86	49	10	2	12	50	17	6	23	50	45	10	37	92	49	83	35	36	104	47	83	35	36	104	47			
45/49	46	13	82	90	44	7	0	3	10	46	3	0	3	46	7	1	8	46	39	3	25	67	46	50	36	49	135	43	50	36	49	135	43			
40/44	31	6	15	52	89	3	1	4	41	1	1	4	1	41	1	1	42	17	0	9	26	41	41	13	40	106	40	41	13	40	106	40				
35/39	15	2	7	24	35	0	0	0	88	0	0	0	0	88	0	0	1	42	6	2	7	37	7	23	72	35	23	72	35	23	72	35				
30/34	5	6	0	2	7	31	0	0	27	0	0	0	0	27	0	0	0	2	0	2	32	25	1	10	36	31	4	8	7	26	26					
25/29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	2	22	1	1	1	2	22	1	1	1	2	22			
20/24																																				

HEATING SEASON

Temperature Range (°F)	NOVEMBER			DECEMBER			JANUARY			FEBRUARY			MARCH			APRIL			ANNUAL (TOTAL—ALL MONTHS)									
	Obsn/ Hour Gp 08 09	Obsn/ Hour Gp 10 09	Mean Co-incident Wet Bulb (°F)	Obsn/ Hour Gp 02 09	Obsn/ Hour Gp 10 09	Total Obsn Wet Bulb (°F)	Obsn/ Hour Gp 02 09	Obsn/ Hour Gp 10 09	Total Obsn Wet Bulb (°F)	Obsn/ Hour Gp 02 09	Obsn/ Hour Gp 10 09	Total Obsn Wet Bulb (°F)	Obsn/ Hour Gp 02 09	Obsn/ Hour Gp 10 09	Total Obsn Wet Bulb (°F)	Obsn/ Hour Gp 02 09	Obsn/ Hour Gp 10 09	Total Obsn Wet Bulb (°F)	Mean Co-incident Wet Bulb (°F)									
95/99																				10	0	10	73					
90/94																				0	45	5	51					
85/89																				3	118	21	142					
80/84																				16	227	55	309					
75/79	1	1	64																	0	1	1	61					
70/74	1	0	1	60																10	0	7	1	51	59			
65/69	0	6	1	7	65															3	1	4	58	0	13			
60/64	2	11	3	15	54															1	7	2	10	58	15			
55/59	6	15	10	31	51	1	3	2	6	52	1	2	1	4	55	1	2	7	4	13	54	7	24	14	45			
50/54	13	17	15	45	47	2	5	3	11	49	2	4	5	12	50	0	4	2	6	47	8	16	12	35	22	35		
45/49	15	29	18	62	43	4	8	5	17	44	7	6	3	15	45	3	11	4	18	42	10	22	14	46	42	26		
40/44	28	38	39	105	38	9	16	9	34	39	8	12	9	29	39	8	14	11	33	38	18	27	23	68	38	35		
35/39	43	48	45	137	35	26	37	30	93	35	19	31	22	72	35	19	41	25	85	34	30	50	33	113	34	48		
30/34	54	41	50	155	31	45	51	52	159	30	36	57	46	139	30	43	58	57	168	30	49	44	147	30	46	17	30	
25/29	38	22	34	94	25	50	51	54	155	25	48	54	51	163	26	51	43	52	145	26	41	32	42	115	26	20	5	13
20/24	19	9	16	43	22	43	34	37	114	21	48	38	43	129	21	36	24	28	87	21	41	15	30	87	21	9	1	7
15/19	5	1	6	12	17	31	20	24	75	16	35	23	34	93	16	28	16	23	55	15	27	9	14	50	16	3	0	8
10/14	3	0	2	6	12	20	9	17	45	12	25	16	20	50	11	18	8	11	37	12	10	2	7	19	11	0	0	12
5/9	1	1	0	2	7	10	2	10	22	7	11	4	8	23	7	8	2	7	17	5	4	1	3	8	7	3	0	7
0/4	1	0	0	1	2	5	1	3	9	2	4	1	4	9	2	5	1	3	10	2	0	0	2	1	1	0	2	
-5/-1	2	1	3	1	0	1	2	4	2	1	1	-7	1	0	0	-7	1	1	-8	3	-2	1	0	0	-7	0	2	
-10/-5																			0	-12	0	0	-11	0	0	0	-7	
-15/-11																			0	-12	0	0	-11	0	0	0	-7	

MITCHELL AFB NEW YORK (Substitute Station for Jersey City)

Mean Frequency of Occurrence of Dry Bulb Temperature (°F) With Mean Coincident Wet Bulb Temperature (°F) For Each Dry Bulb Temperature Range

COOLING SEASON

Temperature Range (°F)	COOLING SEASON												OCTOBER													
	MAY				JUNE				JULY				AUGUST				SEPTEMBER				OCTOBER					
	Obsn/ Hour Gp		Mean Co- incident Wet Bulb (°F)		Obsn/ Hour Gp		Mean Co- incident Wet Bulb (°F)		Obsn/ Hour Gp		Mean Co- incident Wet Bulb (°F)		Obsn/ Hour Gp		Mean Co- incident Wet Bulb (°F)		Obsn/ Hour Gp		Mean Co- incident Wet Bulb (°F)		Obsn/ Hour Gp		Mean Co- incident Wet Bulb (°F)			
100/104	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
95/99	0	0	0	0	74	0	7	1	8	75	1	16	1	18	74	0	8	0	8	74	0	2	2	74	0	
90/94	4	4	70	2	22	3	27	72	3	46	5	53	72	2	35	2	39	73	0	7	0	7	73	5	0	5
85/89	0	11	1	12	67	6	41	8	55	69	14	74	22	110	70	9	66	15	90	71	1	29	2	32	71	
80/84	2	24	3	29	64	17	68	26	101	67	43	73	66	182	68	39	73	61	173	69	12	58	17	87	68	
75/79	8	41	13	62	61	40	50	141	64	92	28	101	221	67	75	44	85	204	67	41	58	52	161	66	7	26
70/74	22	59	28	109	59	36	68	63	62	63	5	42	110	63	69	16	59	144	63	50	49	57	156	61	16	21
65/69	43	51	62	146	56	66	17	54	137	58	27	1	10	38	59	39	3	22	64	79	62	28	60	140	58	
60/64	62	36	69	167	62	36	6	23	65	54	5	1	1	7	55	15	4	19	55	48	8	32	88	53	46	47
55/59	61	15	56	132	48	13	0	7	20	50	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
50/54	45/49	36	7	22	64	44	1	1	46	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
40/44	15	0	4	19	40	0	0	0	33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
35/39	0	0	0	0	33	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
30/34																										

HEATING SEASON

Temperature Range (°F)	ANNUAL (TOTAL—ALL MONTHS)																		
	NOVEMBER			DECEMBER			JANUARY			FEBRUARY			MARCH			APRIL			
	Open/Hour Gp	Mean Co-incident Wet Bulb (°F)	Open/Hour Gp	Open/Hour Gp	Mean Co-incident Wet Bulb (°F)	Open/Hour Gp	Open/Hour Gp	Mean Co-incident Wet Bulb (°F)	Open/Hour Gp	Open/Hour Gp	Mean Co-incident Wet Bulb (°F)	Open/Hour Gp	Open/Hour Gp	Mean Co-incident Wet Bulb (°F)	Open/Hour Gp	Open/Hour Gp	Mean Co-incident Wet Bulb (°F)		
100/104																			
95/99																			
90/94																			
86/89																			
80/84																			
75/79																			
70/74	1	56	0	10	58	0	0	58											
65/69	1	9	0	10	58	0	2	1	8	18	10	18	10	18	10	18	10	18	
60/64	8	23	9	40	57	0	2	1	8	19	15	19	15	19	15	19	15	19	
55/59	21	48	28	97	53	5	13	6	24	53	1	1	52	1	53	0	7	0	7
50/54	34	45	44	124	47	11	23	10	44	48	4	5	2	12	49	3	16	51	15
45/49	42	48	47	137	42	15	32	22	59	43	8	23	8	39	44	12	32	15	59
40/44	47	35	46	128	38	33	51	43	127	38	19	35	26	80	38	43	36	112	55
35/39	46	19	39	104	34	53	50	54	157	34	40	55	55	160	34	53	59	151	33
30/34	27	9	20	55	29	48	34	45	127	29	52	69	173	29	55	142	29	57	44
25/29	9	1	6	16	24	34	23	32	89	24	50	32	48	130	24	38	16	26	31
20/24	4	1	1	5	19	25	13	19	57	19	33	21	25	79	19	22	8	13	43
15/19	1	16	5	16	16	5	13	13	35	15	25	10	17	52	15	5	0	1	5
10/14	7	1	7	1	2	10	10	11	2	8	21	11	6	2	6	13	10	0	11
5/9	1	1	2	5	5	0	1	5	5	0	1	5	5	3	1	2	5	5	6
0/4	0	0	0	1	1	1	1	1	1	1	2	1	0	0	1	1	0	0	2
-5/-1																			-4

MEMPHIS NAS TENNESSEE

Mean Frequency of Occurrence of Dry Bulb Temperature (°F) With Mean Coincident Wet Bulb Temperature (°F) For Each Dry Bulb Temperature Range

COOLING SEASON

Temper- ature Range (°F)	MAY						JUNE						JULY						AUGUST						SEPTEMBER						OCTOBER					
	Open/ Hour Gp			Mean Co- in- ci- dent Wet Bulb (°F)			Open/ Hour Gp			Mean Co- in- ci- dent Wet Bulb (°F)			Open/ Hour Gp			Mean Co- in- ci- dent Wet Bulb (°F)			Open/ Hour Gp			Mean Co- in- ci- dent Wet Bulb (°F)			Open/ Hour Gp			Mean Co- in- ci- dent Wet Bulb (°F)								
	08 to 09	10 to 11	18 to 01	Total Open	08 to 09	10 to 11	18 to 01	Total Open	08 to 09	10 to 11	18 to 01	Total Open	08 to 09	10 to 11	18 to 01	Total Open	08 to 09	10 to 11	18 to 01	Total Open	08 to 09	10 to 11	18 to 01	Total Open	08 to 09	10 to 11	18 to 01	Total Open	08 to 09	10 to 11	18 to 01	Total Open				
106/106					0	0	76																													
100/104					0	2	0	2	76	4	0	4	77	4	0	4	78	2	2	2	74															
96/99	11	1	12	73	0	44	6	50	75	1	77	12	90	18	1	19	78	24	2	26	74															
90/94	0	48	6	54	72	6	66	20	92	73	11	78	34	123	76	10	77	87	10	76	1	25	1	26	74											
86/89	7	62	24	93	70	25	60	43	128	72	41	47	67	155	74	33	43	64	140	74	9	59	22	90	71	1	37	3	41	68						
80/84	28	47	117	68	51	37	73	161	70	88	19	87	194	72	81	18	82	181	72	32	45	58	136	70	7	50	14	71	66							
76/79	51	33	63	147	66	88	19	63	170	68	85	6	43	188	70	86	6	46	136	69	30	69	168	67	18	47	31	96	64							
70/74	72	25	60	147	62	44	3	25	72	63	18	0	4	22	64	30	1	9	40	64	55	12	46	113	62	85	87	44	116	61						
66/69	45	13	30	88	57	20	2	7	29	59	4	0	4	58	7	2	2	57	43	4	26	73	58	41	31	50	122	57								
60/64	25	7	15	47	62	5	2	7	56	0	0	0	57	1	1	1	56	22	1	8	31	58	42	17	41	100	52									
50/54	13	2	10	25	47	1	1	61																												
45/49	11	0	2	13	43																															
40/44	1		0	1	40																															
36/39																																				
30/34																																				

HEATING SEASON

Temperature Range (°F)	NOVEMBER			DECEMBER			JANUARY			FEBRUARY			MARCH			APRIL			ANNUAL (TOTAL—ALL MONTHS)					
	Obsn./Hour Gp 02 to 09	Obsn./Hour Gp 10 to 09	Obsn./Hour Gp 18 to 01	Total Obsn./Hour Gp 02 to 09	Mean Co-incident Wet Bulb (°F)	Total Obsn./Hour Gp 10 to 01	Total Obsn./Hour Gp 18 to 01	Mean Co-incident Wet Bulb (°F)	Total Obsn./Hour Gp 02 to 09	Mean Co-incident Wet Bulb (°F)	Total Obsn./Hour Gp 10 to 01	Total Obsn./Hour Gp 18 to 01	Mean Co-incident Wet Bulb (°F)	Total Obsn./Hour Gp 02 to 09	Mean Co-incident Wet Bulb (°F)	Total Obsn./Hour Gp 10 to 01	Total Obsn./Hour Gp 18 to 01	Mean Co-incident Wet Bulb (°F)	Total Obsn./Hour Gp 02 to 09	Mean Co-incident Wet Bulb (°F)	Total Obsn./Hour Gp 10 to 01	Total Obsn./Hour Gp 18 to 01	Mean Co-incident Wet Bulb (°F)	
106/109																								
100/104																								
95/99																								
90/94																								
85/89																								
80/84																								
75/79																								
70/74																								
65/69																								
60/64																								
55/59																								
50/54																								
45/49																								
40/44																								
35/39																								
30/34																								
25/29																								
20/24																								
15/19																								
10/14																								
5/9																								
0/4																								

ELLINGTON AFB TEXAS (Substitute Station for Houston)

Mean Frequency of Occurrence of Dry Bulb Temperature ($^{\circ}$ F) With Mean Coincident Wet Bulb Temperature ($^{\circ}$ F) For Each Dry Bulb Temperature Range

COOLING SEASON

HEATING SEASON

Temperature Range (°F)	NOVEMBER			DECEMBER			JANUARY			FEBRUARY			MARCH			APRIL			ANNUAL (TOTAL—ALL MONTHS)																		
	Open/ Hour Gp 02 to 09	10 to 17	18 to 01	Total Open 02 to 09	Open/ Hour Gp 02 to 09	10 to 17	18 to 01	Total Open 02 to 09	Open/ Hour Gp 02 to 09	10 to 17	18 to 01	Total Open 02 to 09	Open/ Hour Gp 02 to 09	10 to 17	18 to 01	Total Open 02 to 09	Open/ Hour Gp 02 to 09	10 to 17	18 to 01	Total Open 02 to 09	Open/ Hour Gp 02 to 09	10 to 17	18 to 01	Total Open 02 to 09													
100/104																																					
95/99																																					
90/94																																					
85/89	3			8	72			2	71		6		6	69		10	0	10	63	1	57	1	59	71	186	427	320	933	72								
30/34	0	26	26	72	4			2	71		6		6	69		10	0	10	63	1	57	1	59	71	186	427	320	933	72								
75/79	10	42	11	63	70	0	17	17	63	12	67	0	18	0	13	63	1	42	2	45	66	16	33	25	124	69	535	385	603	1573	70						
70/74	24	42	32	98	67	5	30	7	42	65	8	29	7	39	65	7	34	14	55	65	16	59	24	98	65	70	49	79	198	67	457	312	427	1196	68		
65/69	31	40	83	104	62	16	41	22	79	62	17	30	20	67	62	26	35	26	87	62	33	52	51	141	62	50	23	61	139	63	340	249	327	916	64		
60/64	31	33	40	104	57	30	45	37	112	58	24	35	25	84	57	20	28	28	76	58	39	14	40	93	58	267	196	273	741	53							
55/59	31	25	40	96	52	33	42	41	116	58	25	41	37	103	53	26	34	39	98	53	46	24	46	116	52	33	3	24	60	53	237	171	250	653	53		
50/54	36	16	33	90	47	40	30	44	114	43	33	36	50	119	43	39	30	41	110	43	37	11	36	84	43	19	0	3	27	49	221	128	229	573	48		
45/49	36	8	25	69	43	39	21	48	108	44	37	27	39	103	43	41	18	37	96	44	31	8	21	60	43	10	2	12	44	199	33	174	456	44			
40/44	24	4	15	43	39	39	21	48	76	39	40	16	31	87	39	32	12	23	67	40	23	4	10	37	39	161	47	107	315	39							
35/39	12	1	5	18	34	23	6	15	49	34	32	11	22	65	34	21	7	12	40	35	10	1	3	14	36	0	0	0	37	104	26	57	187	35			
30/34	5	1	6	30	15	2	4	21	30	22	5	10	37	29	9	2	4	15	31	3	0	3	30	65	9	20	34	30	34	30	34	30	34	30			
25/29	0		0	26	3	0	2	5	24	9	8	3	15	24	4	0	4	26																			
20/24				1	21	1	3	1	3	7	20		1	21	3	1	3	7	20																		
15/19																																					

GRAY AAF, FORT LEWIS WASHINGTON (Substitute Station for Seattle)

Mean Frequency of Occurrence of Dry Bulb Temperature ($^{\circ}\text{F}$) With Mean Coincident Wet Bulb Temperature ($^{\circ}\text{F}$) For Each Dry Bulb Temperature Range

COOLING SEASON

Tempera-ture Range ($^{\circ}\text{F}$)	MAY				JUNE				JULY				AUGUST				SEPTEMBER				OCTOBER										
	Obsn/ Hour Gp		Mean Co-incident Wet Bulb ($^{\circ}\text{F}$)		Obsn/ Hour Gp		Mean Co-incident Wet Bulb ($^{\circ}\text{F}$)		Obsn/ Hour Gp		Mean Co-incident Wet Bulb ($^{\circ}\text{F}$)		Obsn/ Hour Gp		Mean Co-incident Wet Bulb ($^{\circ}\text{F}$)		Obsn/ Hour Gp		Mean Co-incident Wet Bulb ($^{\circ}\text{F}$)		Obsn/ Hour Gp		Mean Co-incident Wet Bulb ($^{\circ}\text{F}$)								
	08 to 09	10 to 11	12 to 13	14 to 15	08 to 09	10 to 11	12 to 13	14 to 15	08 to 09	10 to 11	12 to 13	14 to 15	08 to 09	10 to 11	12 to 13	14 to 15	08 to 09	10 to 11	12 to 13	14 to 15	08 to 09	10 to 11	12 to 13	14 to 15							
95/99	1	1	65	0	0	68	4	1	5	69	0	10	1	11	65	0	1	4	67	1	1	1	66	0	0	0					
90/94	8	0	64	4	1	65	13	3	16	67	0	19	5	24	64	7	7	1	8	63	0	0	0	0	0	0	0				
85/89	4	1	62	11	3	14	62	0	23	7	30	66	0	19	6	24	64	14	2	16	61	0	0	0	0	0	0	0			
80/84	0	10	2	12	60	0	23	9	32	61	2	42	14	68	62	1	36	11	48	63	35	7	42	69	6	0	0	63			
75/79	1	15	5	21	58	8	40	14	57	59	6	53	28	87	60	4	53	22	79	61	2	66	19	87	58	22	1	23	58		
70/74	3	36	10	48	66	7	52	22	81	67	17	58	39	114	58	13	68	41	122	59	21	74	61	146	56	5	50	14	69	55	
65/69	7	54	23	84	53	22	58	42	122	54	44	43	64	151	56	49	46	72	167	69	39	83	191	53	80	71	46	147	53		
60/64	26	62	46	134	50	57	43	66	166	52	94	11	64	169	54	104	12	70	186	64	4	38	8	0	8	33	0	0	28		
55/59	60	48	71	179	48	96	9	64	168	49	67	0	25	92	50	58	0	22	80	50	73	4	49	126	50	66	68	70	204	50	
50/54	78	18	56	147	44	47	0	18	66	45	15	3	18	46	16	3	19	46	47	0	22	69	46	65	26	72	163	45	0	0	
45/49	48	8	25	76	40	8	1	9	42	3	0	3	42	3	0	3	42	4	24	6	80	41	46	5	32	83	41	0	0	0	
40/44	35/39	18	8	26	85	1	1	1	38	7	1	8	32	0	1	1	38	4	28	0	13	41	36	8	0	8	33	0	0	28	
30/34	25/29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

HEATING SEASON

Temperature Range (°F)	NOVEMBER			DECEMBER			JANUARY			FEBRUARY			MARCH			APRIL			ANNUAL (TOTAL—ALL MONTHS)		
	Open/Hour Gp 02 10 18 to to to 09 17 01	Mean/Coincident Wet Bulb 02 10 18 to to to 09 17 01	Total Open 02 10 18 to to to 09 17 01	Open/Hour Gp 02 10 18 to to to 09 17 01	Mean/Coincident Wet Bulb 02 10 18 to to to 09 17 01	Total Open 02 10 18 to to to 09 17 01	Open/Hour Gp 02 10 18 to to to 09 17 01	Mean/Coincident Wet Bulb 02 10 18 to to to 09 17 01	Total Open 02 10 18 to to to 09 17 01	Open/Hour Gp 02 10 18 to to to 09 17 01	Mean/Coincident Wet Bulb 02 10 18 to to to 09 17 01	Total Open 02 10 18 to to to 09 17 01	Open/Hour Gp 02 10 18 to to to 09 17 01	Mean/Coincident Wet Bulb 02 10 18 to to to 09 17 01	Total Open 02 10 18 to to to 09 17 01	Open/Hour Gp 02 10 18 to to to 09 17 01	Mean/Coincident Wet Bulb 02 10 18 to to to 09 17 01	Total Open 02 10 18 to to to 09 17 01			
95/99																					
90/94																					
86/89																					
80/84																					
76/79																					
70/74																					
66/69																					
60/64	3	3	53	4	7	4	0	1	64	2	8	2	12	51	2	14	3	19	61		
66/69	8	21	5	29	61	4	7	4	15	60	2	8	2	12	51	2	14	3	19	61	
50/64	21	71	27	119	49	16	32	14	61	49	12	23	14	49	48	10	48	20	78	47	
46/49	61	69	63	183	45	88	64	54	166	46	28	65	36	119	44	41	78	63	172	44	
40/44	61	46	63	169	41	66	68	180	41	43	71	69	173	40	72	66	78	206	40	76	
35/39	62	24	61	127	36	61	46	67	164	36	67	60	66	193	36	47	18	44	109	36	
30/34	88	7	26	70	82	42	25	40	107	81	67	19	47	123	31	82	6	20	67	31	
25/29	14	6	20	27	22	4	16	42	27	22	8	16	46	26	15	0	6	20	27	12	
20/24	0	0	24	8	2	3	13	21	9	2	4	15	21	3	1	4	21	2	20	1	
16/19				0	1	1	2	16	4	1	8	8	15	2	0	2	16	0	17	0	
10/14				1	0	1	2	10	3	1	4	11	1	6	1	1	6	1	9	1	
6/9																					

Table F Mean Wind Climate Airport Exposure for the Structural Design

	Ref. (14)	Ref. (14)	Ref. (11)	Ref. (14, 9)	Ref. (9)
Site localities and U. S. W. B. Station location	Station Elevation Above MSL (ft)	Observed Fastest Mile Wind Speed (mph)	Annual Extreme Mile Speed 50-year Mean Recurrence Interval (mph)	Mean Wind Speed (mph)	Direction January July Annual
Sacramento, Calif. Municipal AP	17	70	65	8.3 SE	9.4 SSE 9.3 SSE
Wilmington, Del. New Castle County AP	78	58	75	9.7 WNW	7.6 S 8.8 NW
Macon, Georgia Cochran Field	354	70	80	8.5 NW	7.2 WSW 8.9 NW
Indianapolis, Ind. Weir Cook AP	792	90	90	11.3 NW	7.4 SW 10.8 SW
Kalamazoo, Mich. Grand Rapids, Mich. Kent County AP	784	58	75	11.5 W	8.3 W 9.8 W
St. Louis, Mo. Lambert Field	535	60	70	10.1 NW	7.6 S 9.3 S
Jersey City, N. J. Newark, N. J. Newark AP	7	82	75	11.3 WNW	8.9 SW 9.8 SW
Memphis, Tenn. Municipal AP	258	56	70	10.7 S	7.7 S 9.4 S
Houston, Texas International AP	50	54	80	11.9 SSE	8.8 SSE 11.8 SSE
Seattle, Wash. Seattle-Tacoma AP	400	55	80	10.4 SSW	8.7 SW 10.7 SW

Table G Air Contamination Data

Suspended Particulates (Micrograms per cubic meter)		Sulfur Dioxide (Micrograms per cubic meter)				Nitrogen Dioxide (Micrograms per cubic meter)				Ammonia (Micrograms per cubic meter)			
Geo- metric Mean	90% Maxi- mum	Geo- metric Mean	90% Maxi- mum	Geo- metric Mean	90% Maxi- mum	Geo- metric Mean	90% Maxi- mum	Geo- metric Mean	90% Maxi- mum	Geo- metric Mean	90% Maxi- mum	Geo- metric Mean	90% Maxi- mum
Air Pollution Sampling Sites													
Sacramento, California	6.8	4.03	1.32	1.958- 1966									
Health Center 2221 Stockton Boulevard Sacramento County Health Dept.													
Wilmington, Delaware	144	74.3	262	1.957- 1968	58	4.92	1.68	1.964- 1968	133	3.84	2.76	1.964- 1968	4.6
Public Building 10000 King Street City Dept. of Health													
Macon, Georgia	96	86.1	235	1.958- 1968									
W. T. Grant Co. 418 3rd Street Georgia Dept. of Public Health													
Indianapolis, Indiana	147	367	237	1.958- 1968	34	24.9	1.15	1.964- 1968	105	4.05	1.90	1.964- 1968	4.8
Fire Station No. 301 East New York Street City Bureau of Air Pollution													
Kalamazoo, Michigan	79	258	151	1.957- 1962									
241 West South Street City County Health Dept.													
St. Louis, Missouri	142	658	236	1.957- 1967	70	2.94	1.69	1.964- 1968	136	4.05	2.63	1.964- 1968	5.0
P. O. Bldg. - 18th & Market St. Div. Air Pollution Cont. City Dept. Public Safety													
Jersey City, New Jersey	126	336	201	1.959- 1968	34	32.3	2.21	1.967- 1968	217	4.73	4.29	1.967	
Medical Center Garage Bldg. Cornellison Ave. City Board of Health													
Memphis, Tennessee	94	281	149	1.958- 1968	9	23	1.8	1.968	157	4.04	2.38	1.968	5.7
Health Dept. Bldg. 814 Jefferson Street Memphis-Shelby Co. Health Dept.													
Houston, Texas	97	385	168	1.957- 1968									
Sam Houston Coliseum 810 Bagley Street City Health Dept.													
Seattle, Washington	70	446	127	1.957- 1968	22	122	58	1.964- 1968	89	3.15	1.99	1.964- 1968	4.8
Public Safety Bldg. 604 Third Ave. Puget Sound Air Pollution Control Agency													

Appendix

City Maps for the Breakthrough Sites



Breakthrough Site



Airport

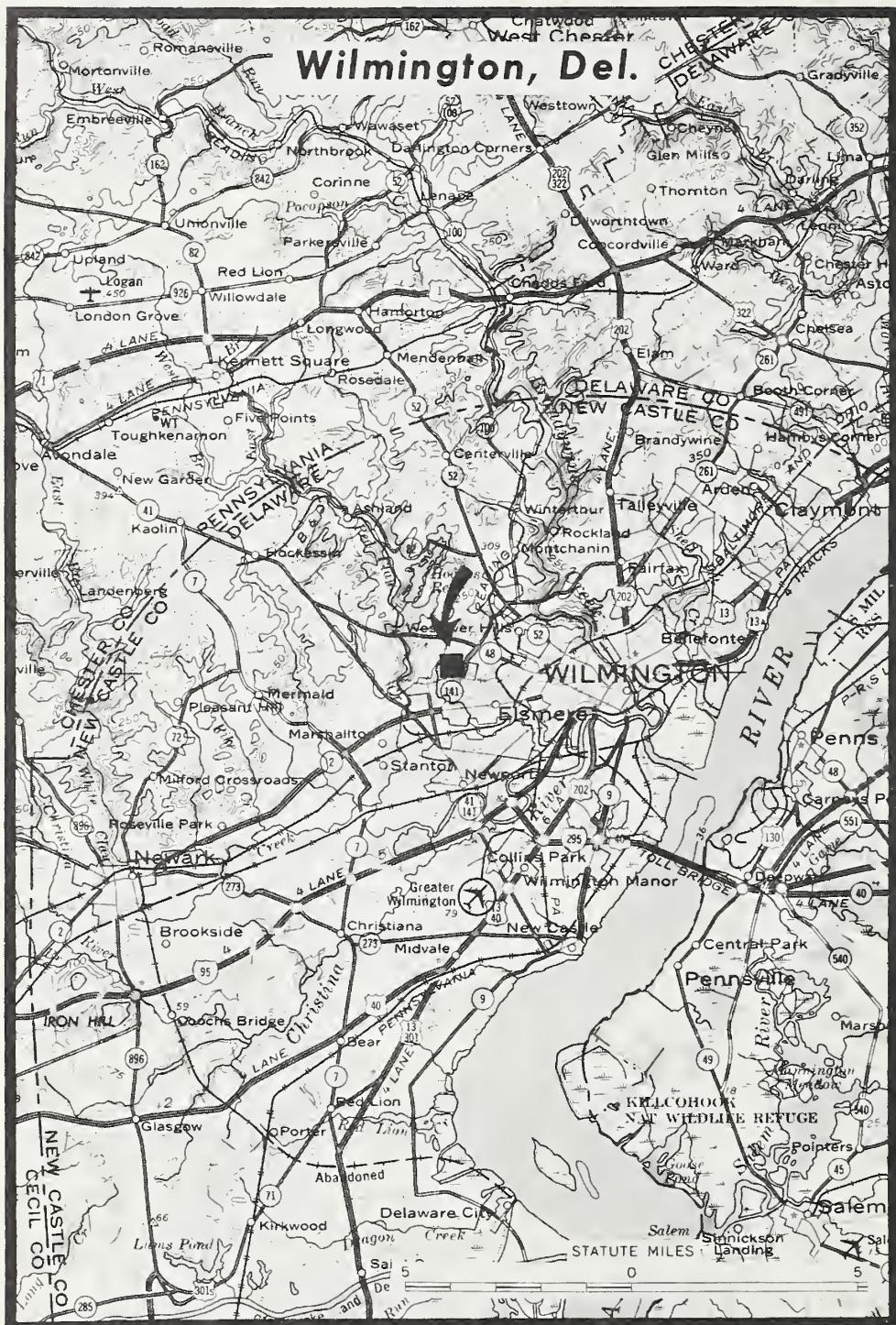


Weather Data Station

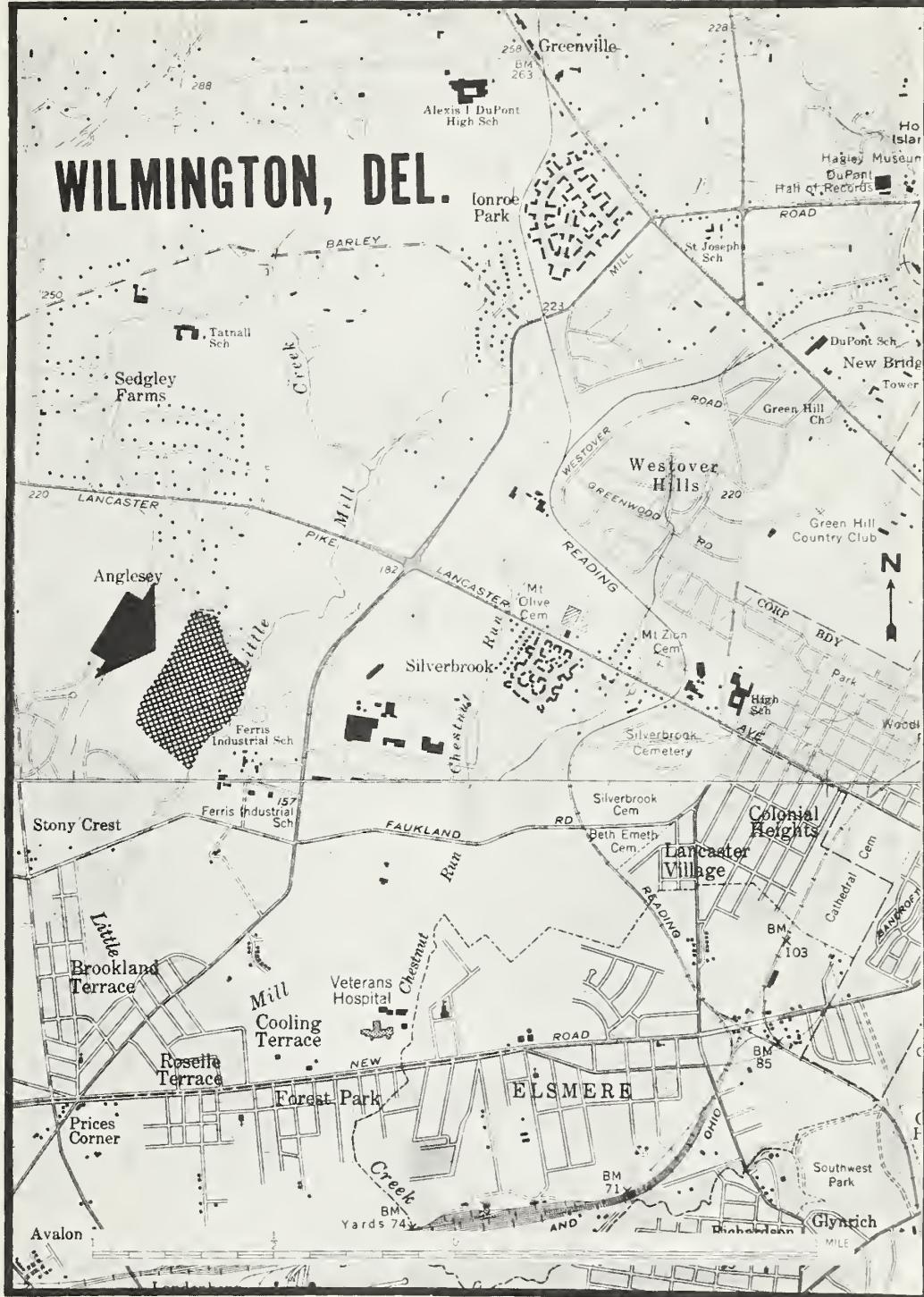


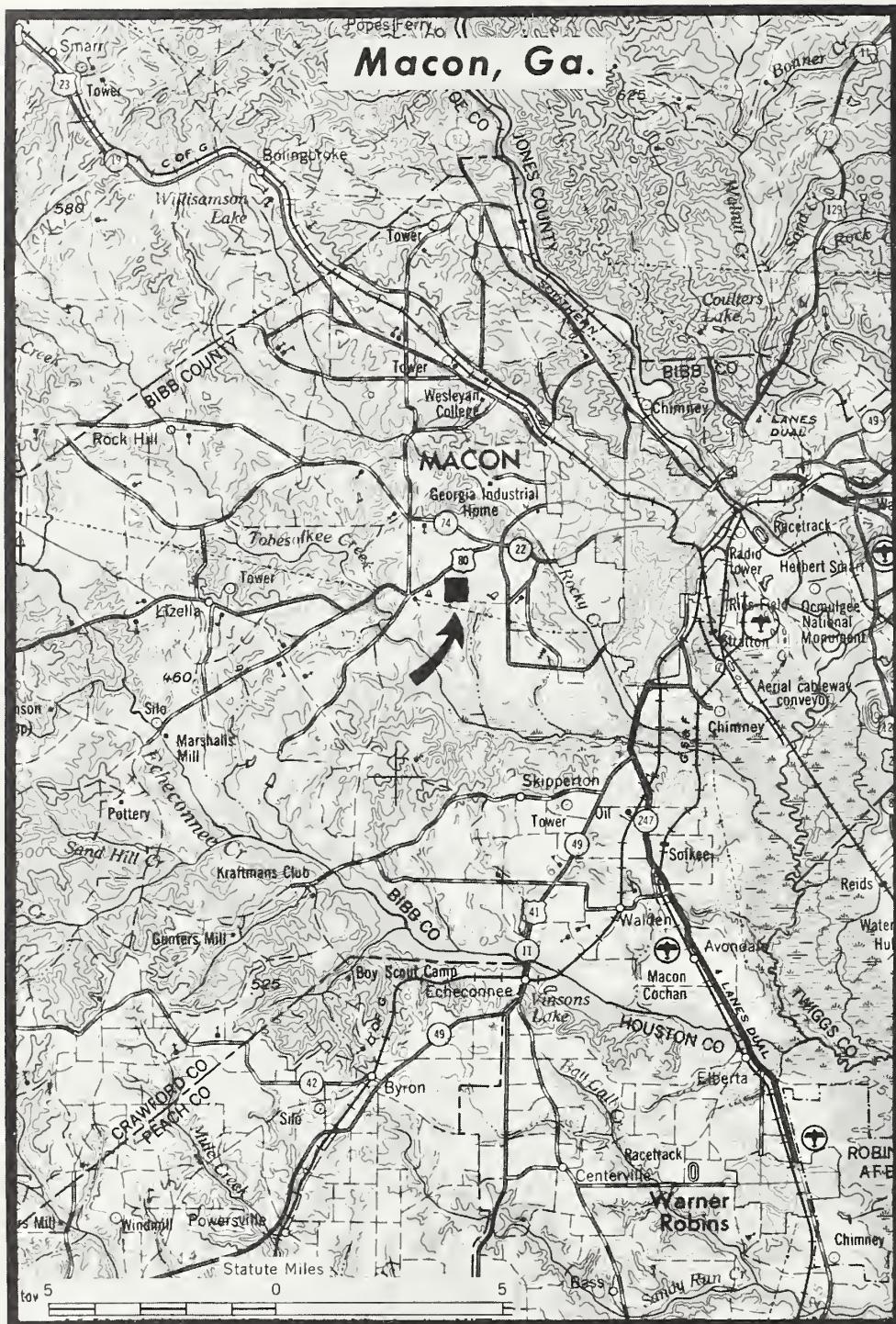
SACRAMENTO, CAL.

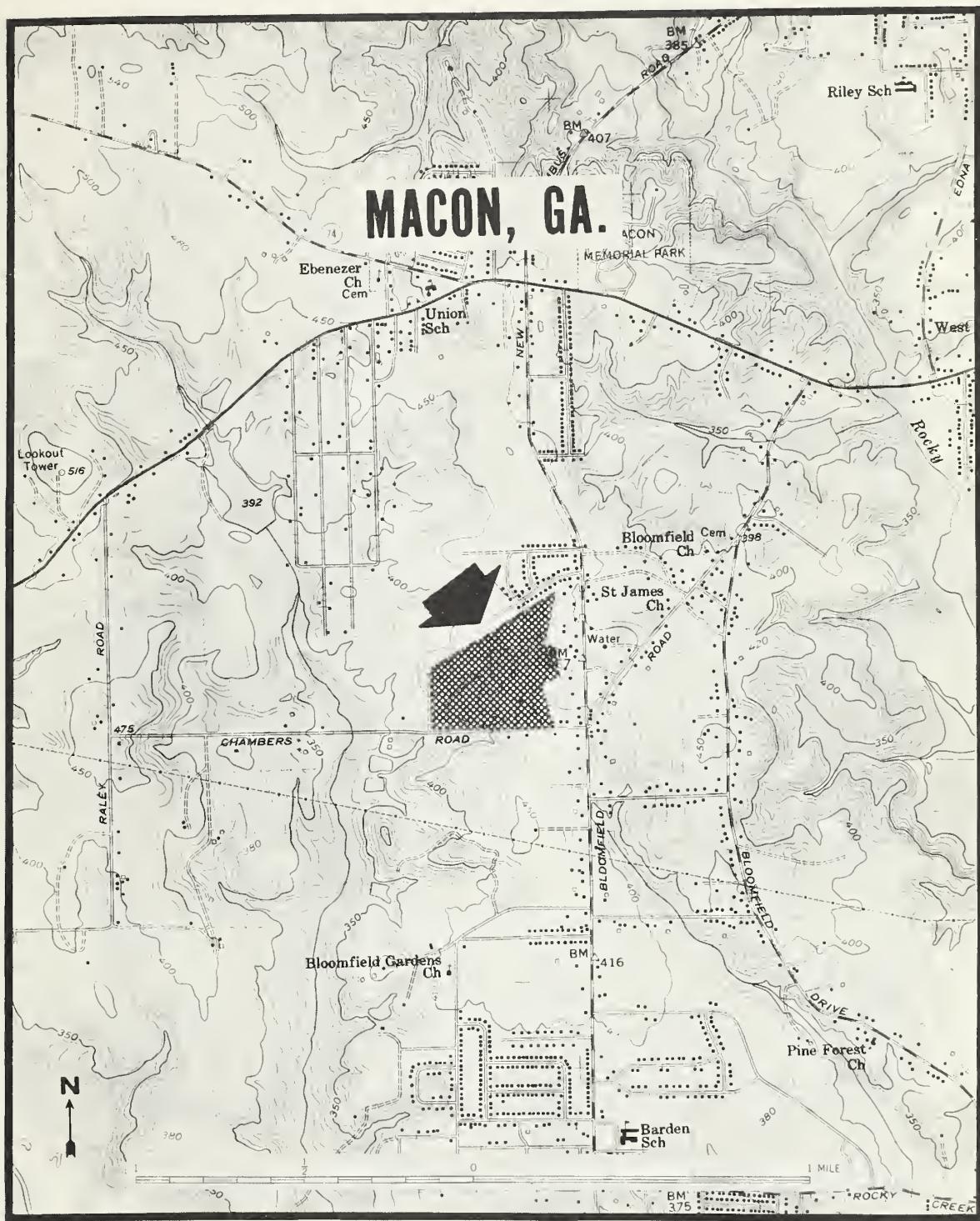




WILMINGTON, DEL.



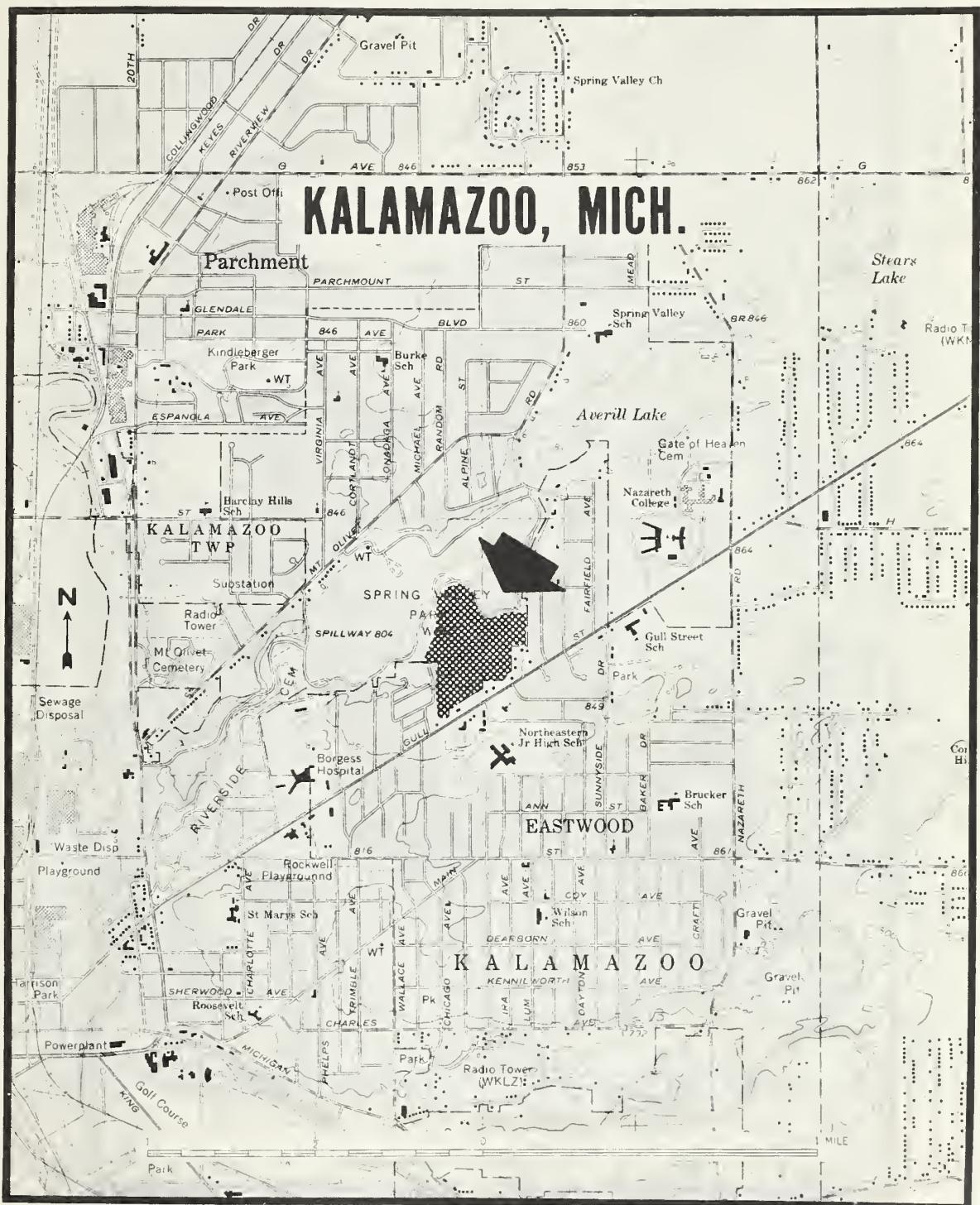


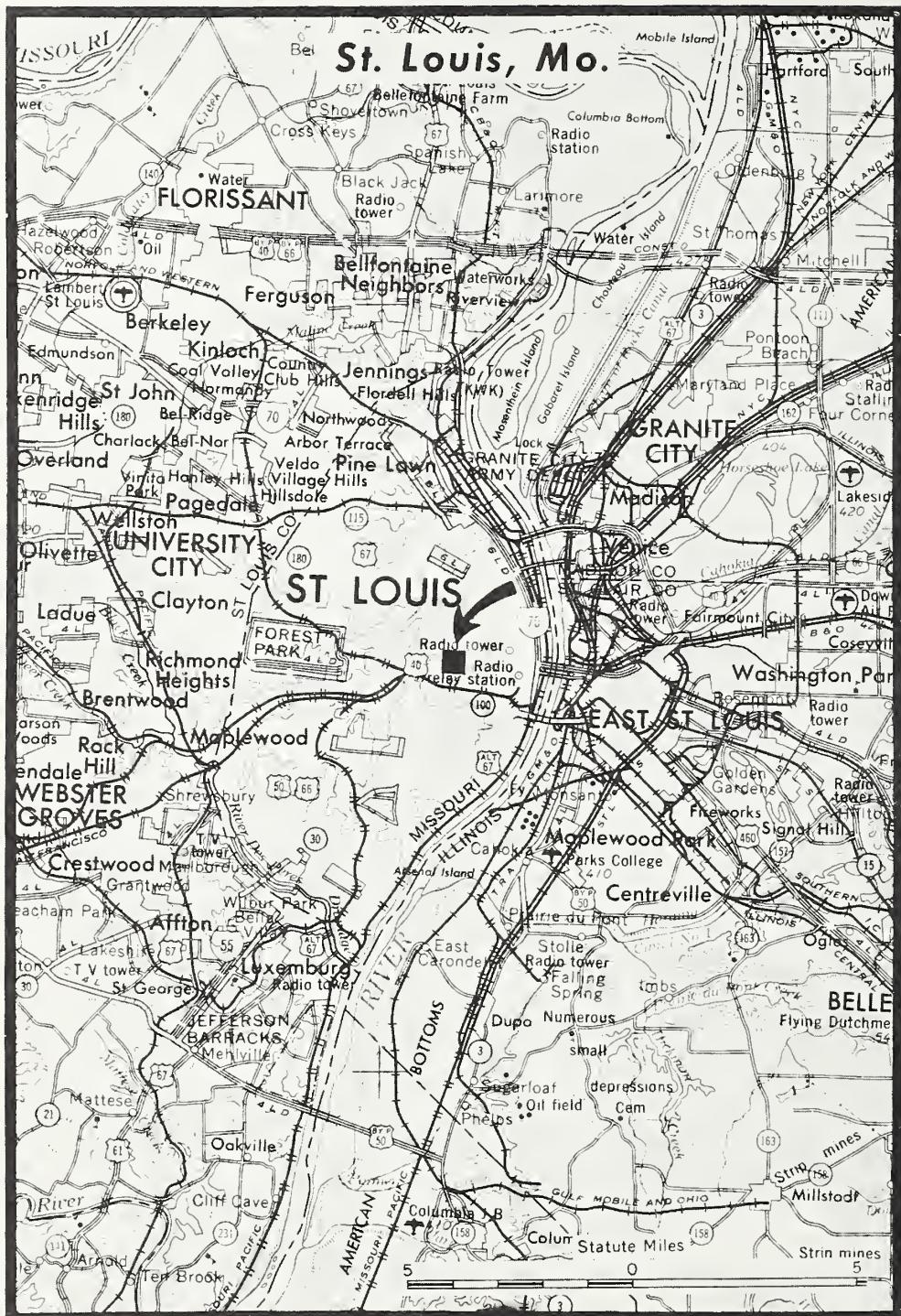


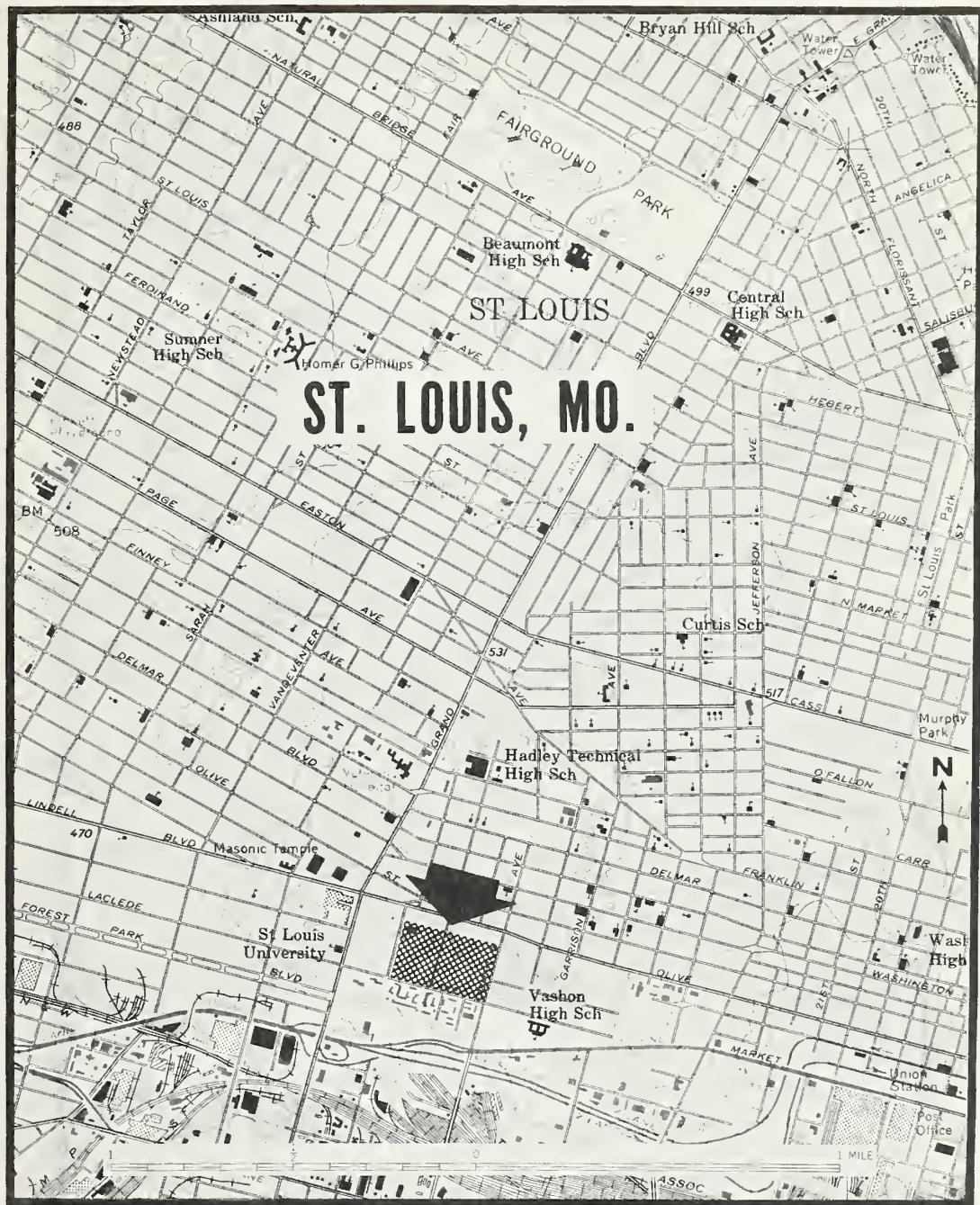






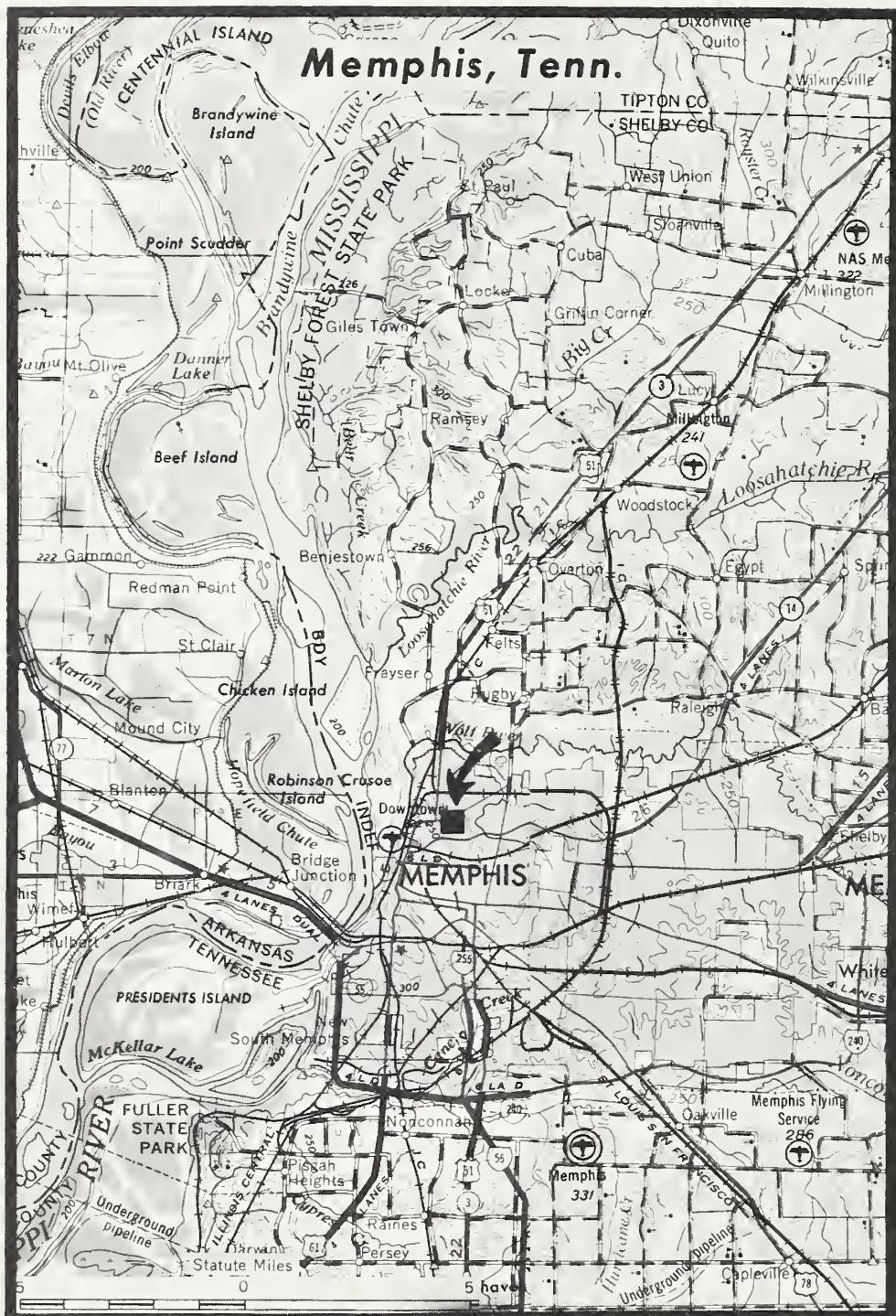




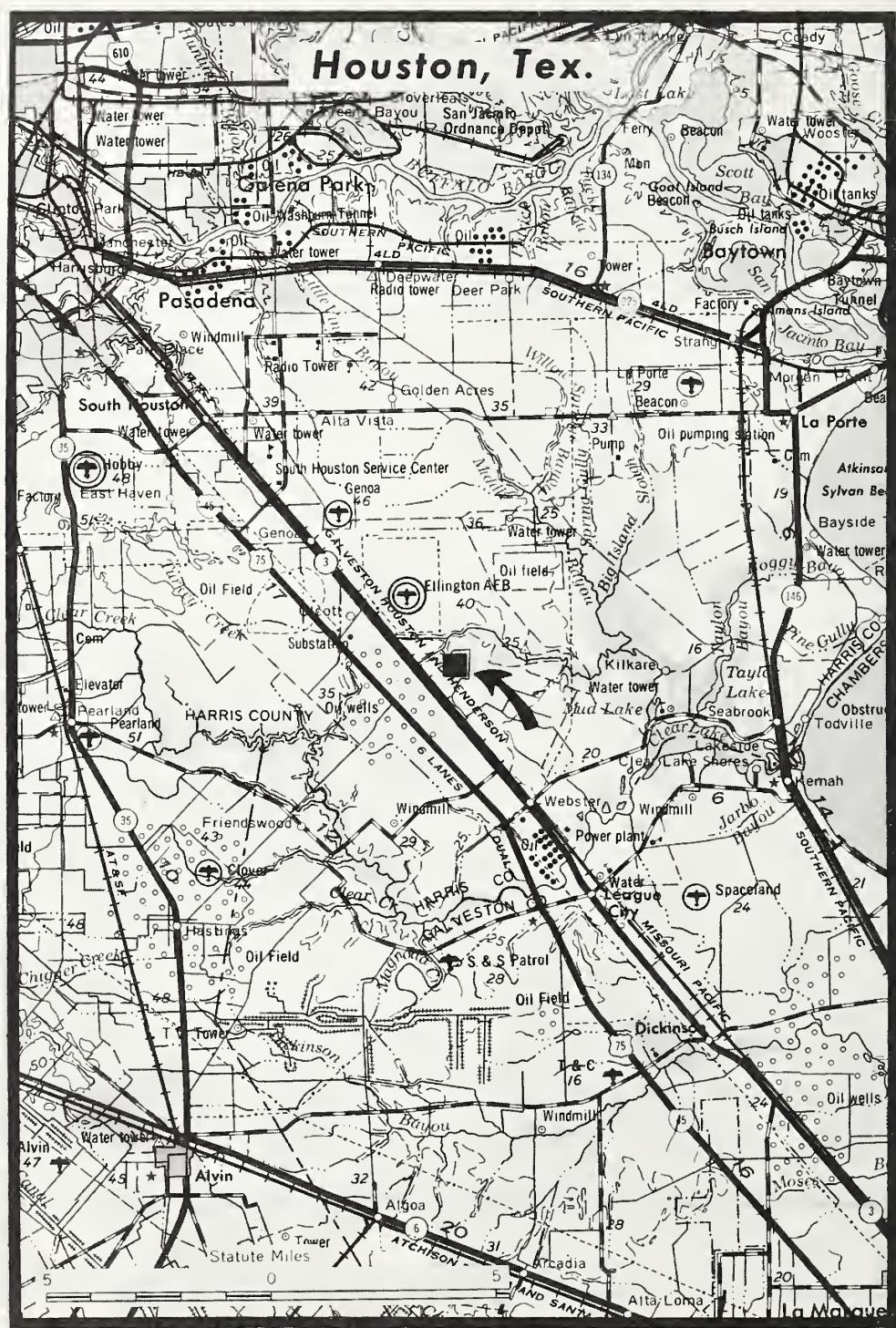




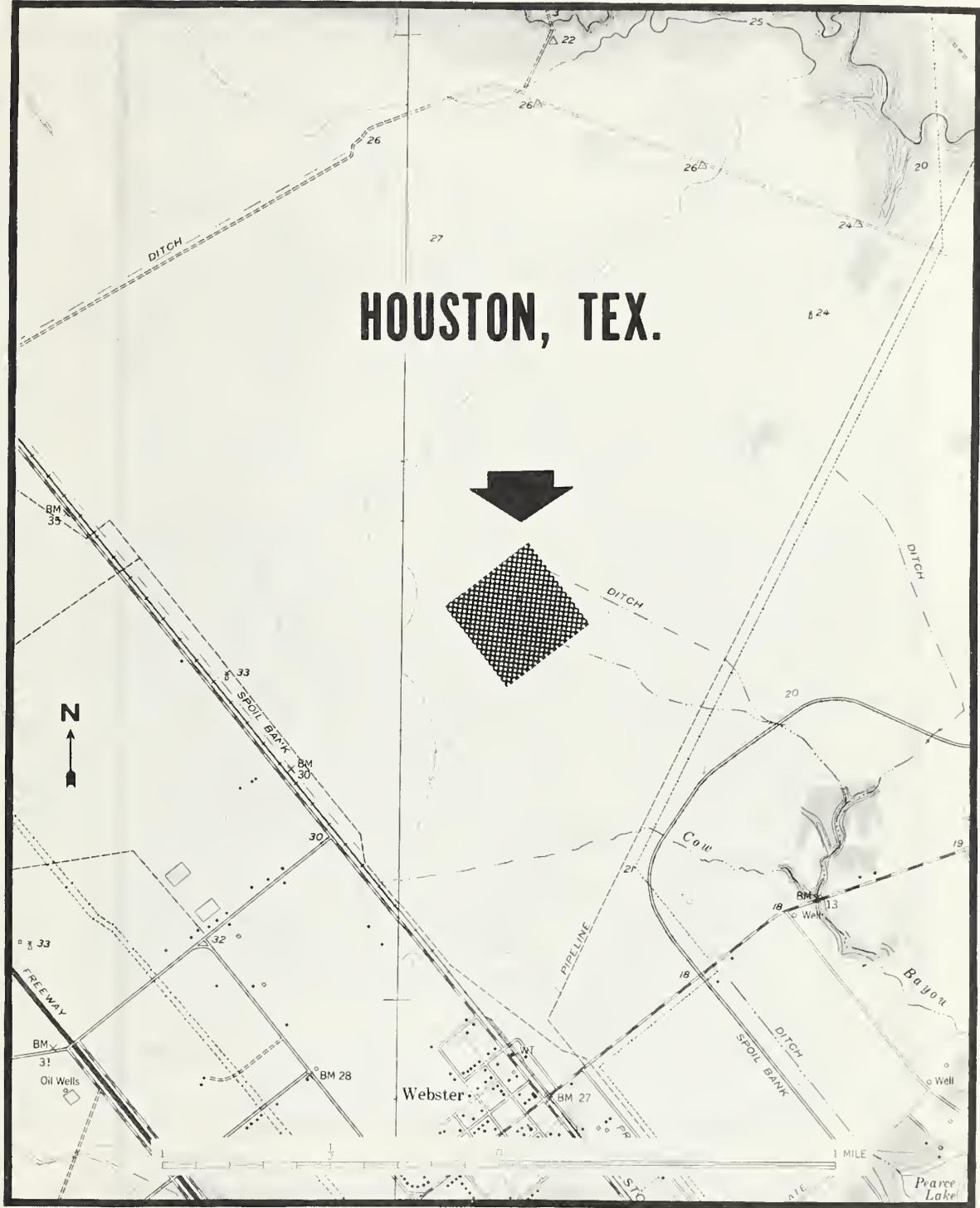






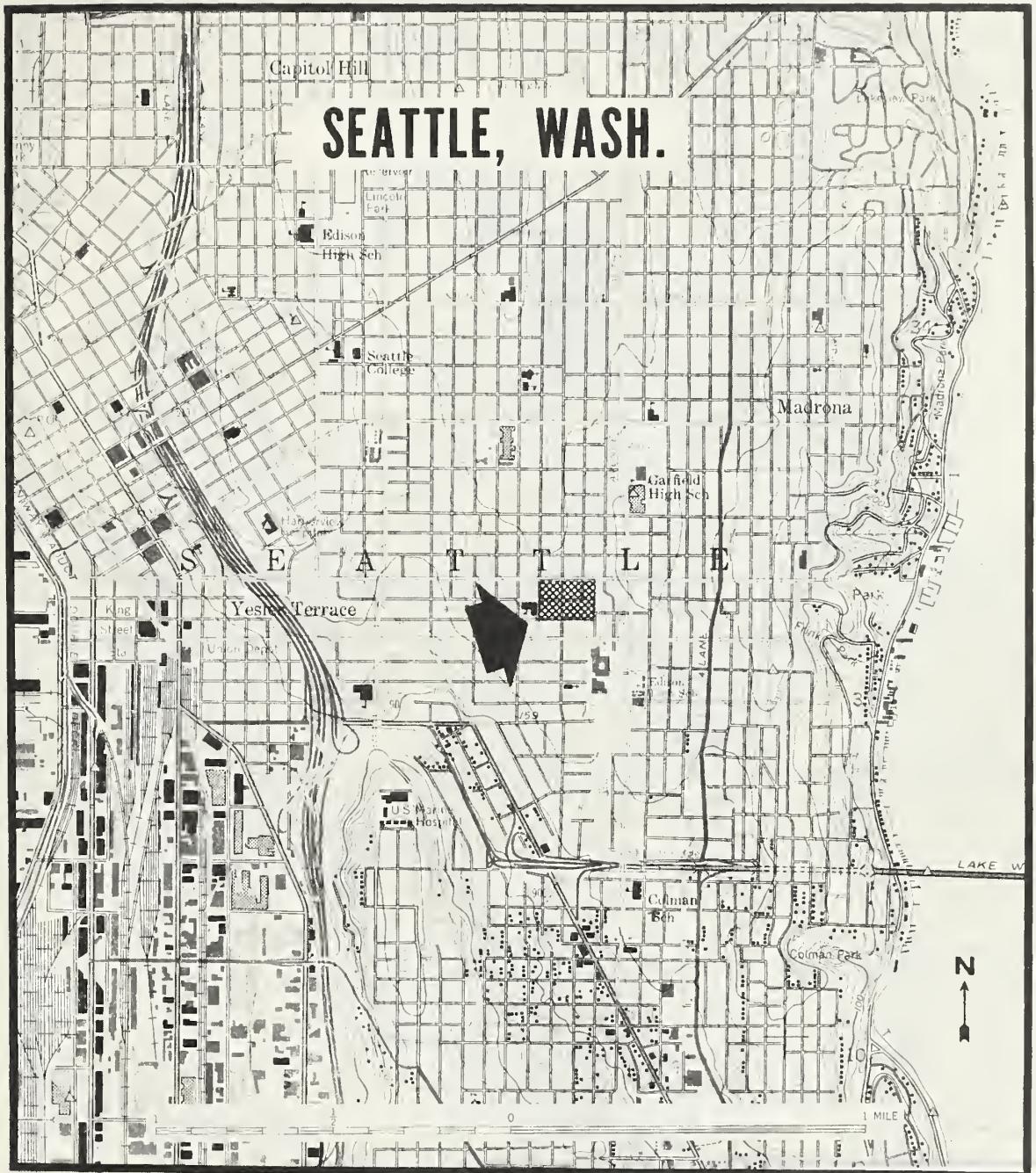


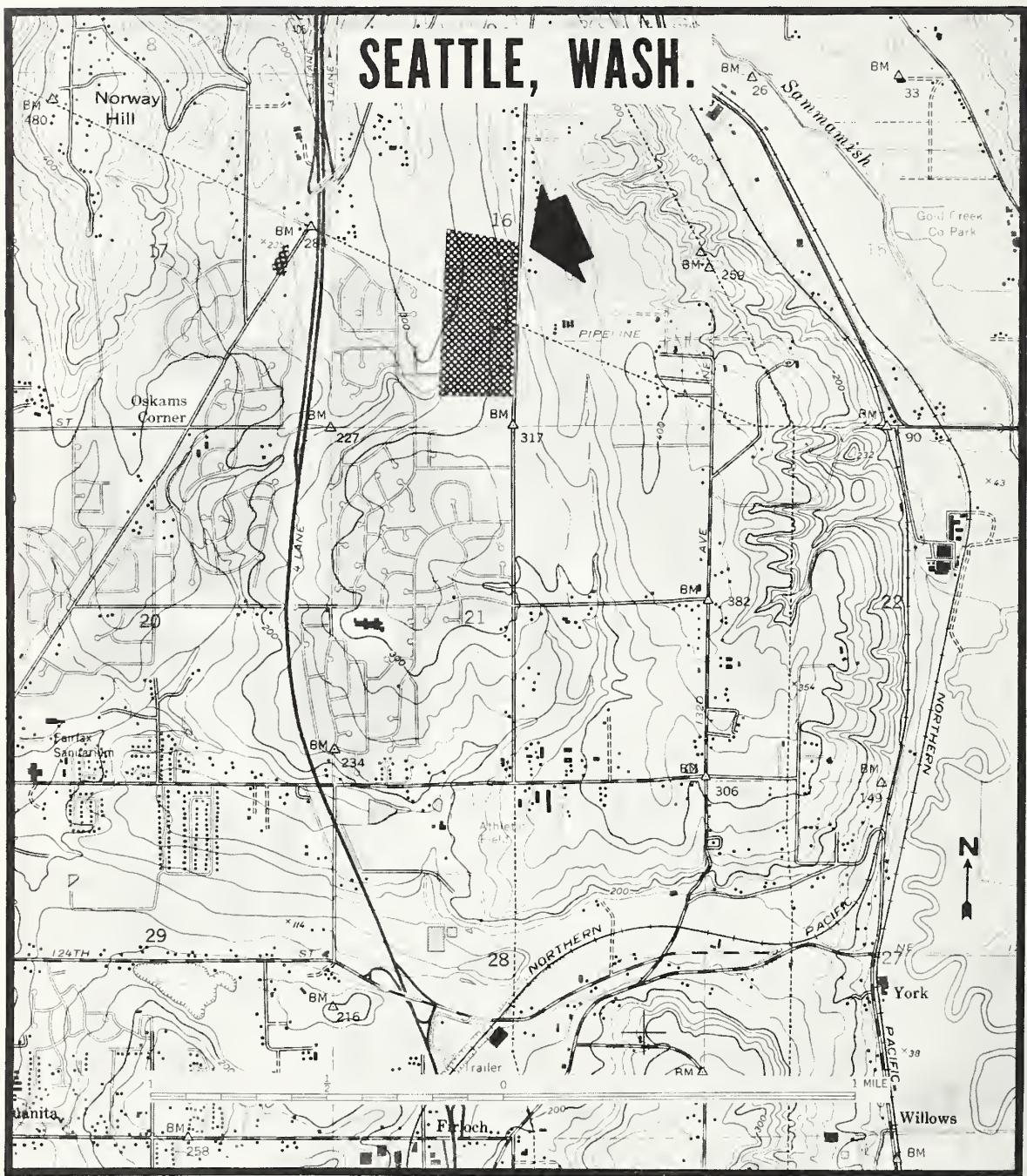
HOUSTON, TEX.

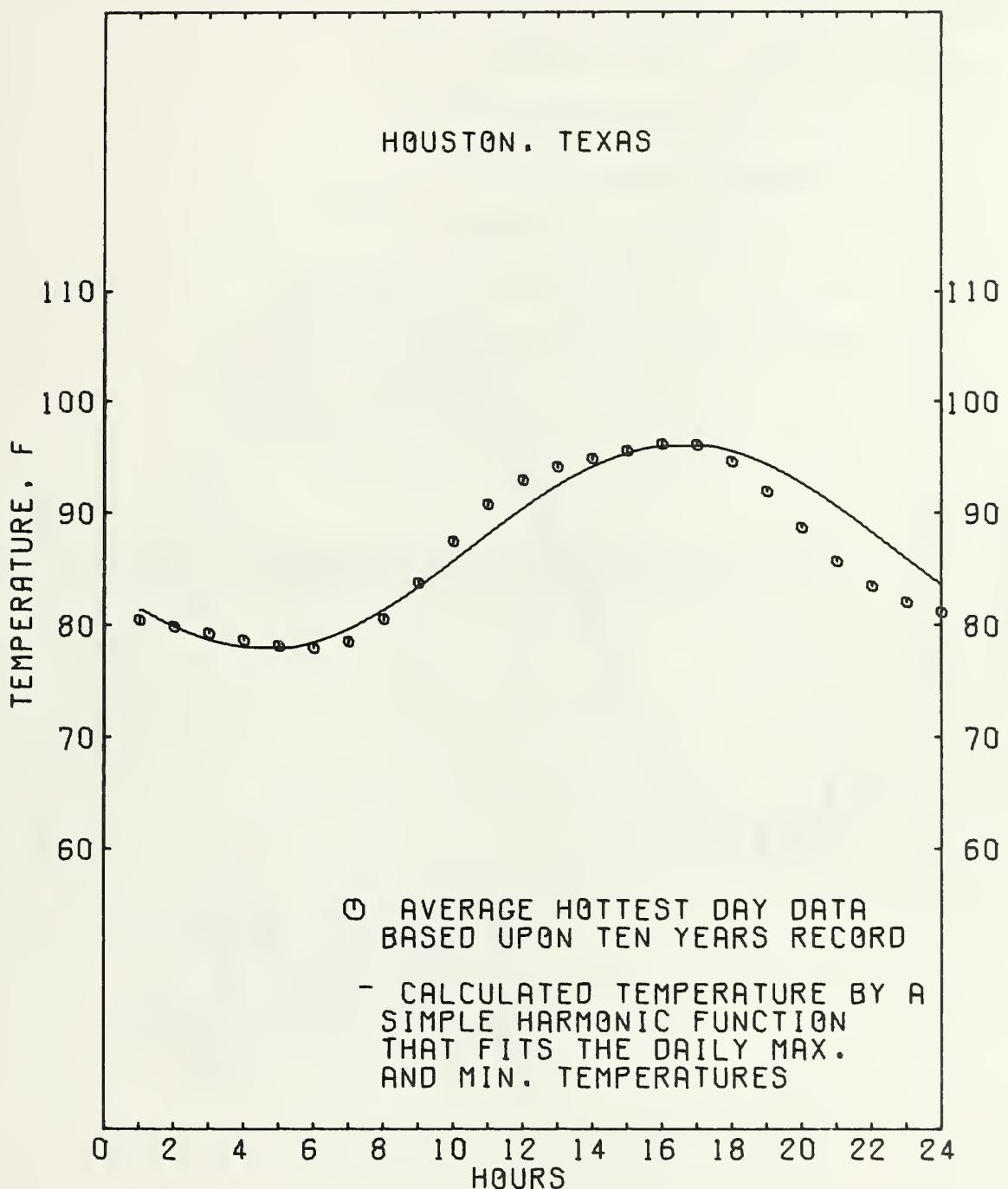


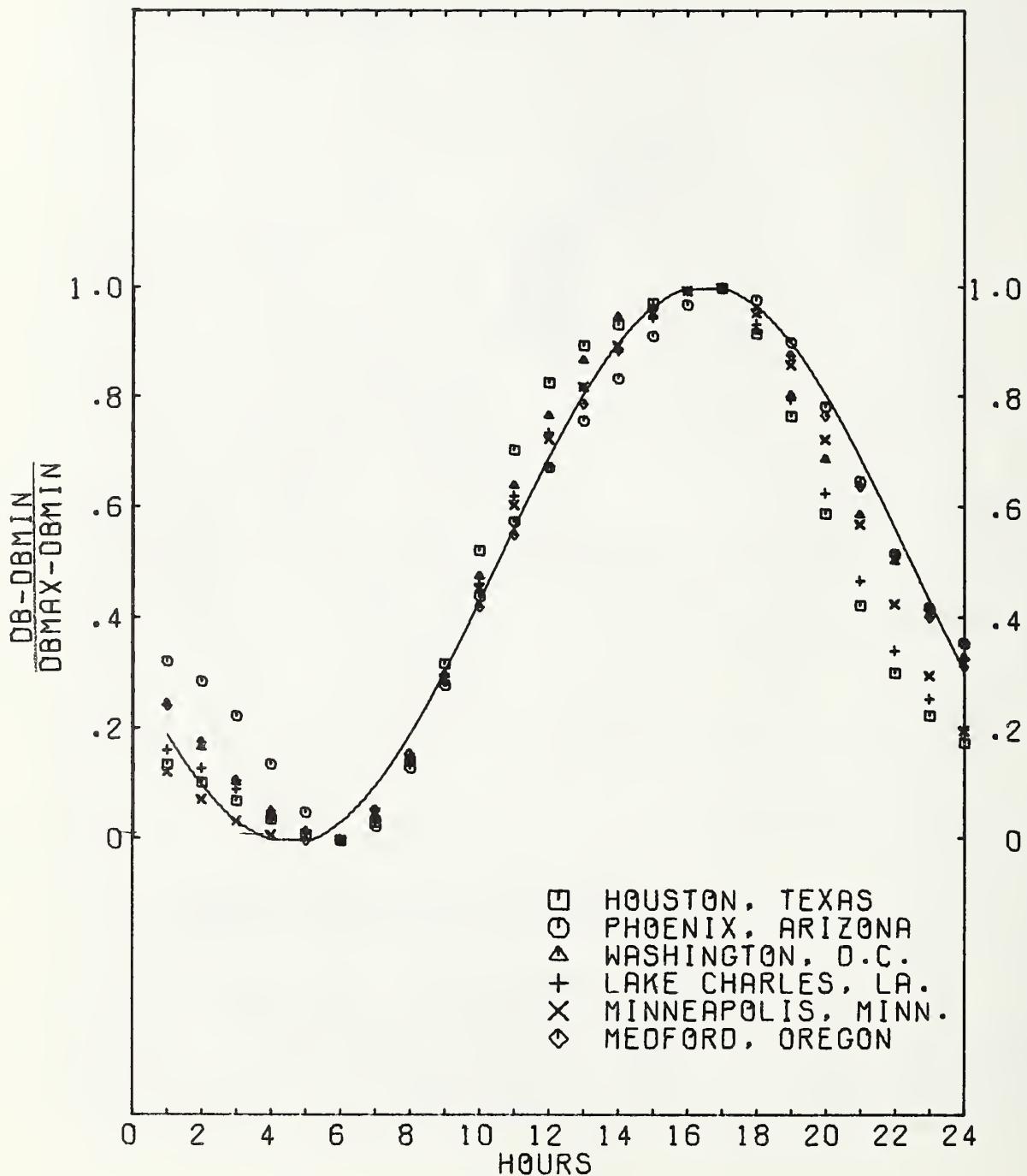
Seattle, Wash.











Figures 3 through 22 - Coincident frequency profiles for the dry-bulb temperature and wind speed, and those for this relative humidity and wind speed. The height of the profile represents relative frequency of the coincident occurrences. All ten localities show the highest frequency profile at the wind speed in the vicinity of 5 mph. But the coincident dry-bulb temperature and relative humidity widely vary from locality to locality.

SACRAMENTO, CALIFORNIA

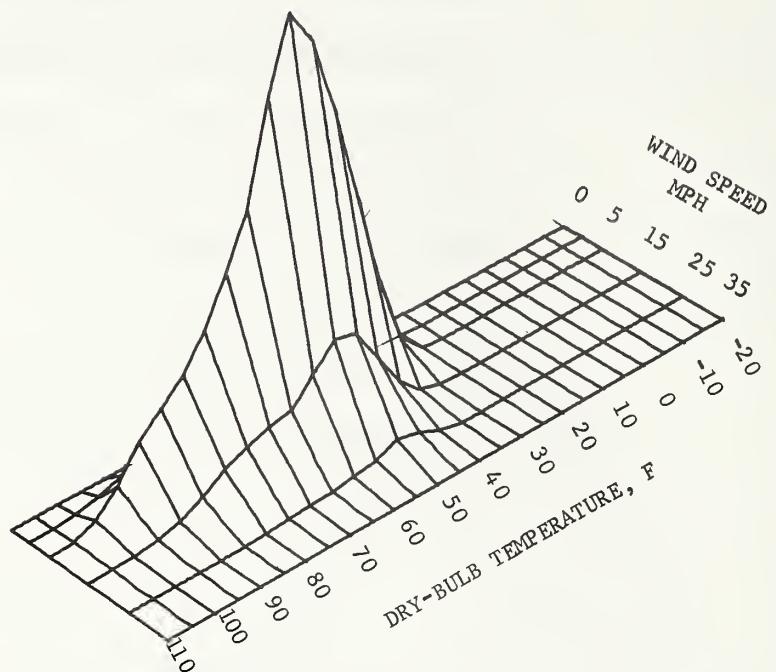


Fig. 3 COINCIDENT PROFILE FOR WIND SPEED
AND DRY BULB TEMPERATURE

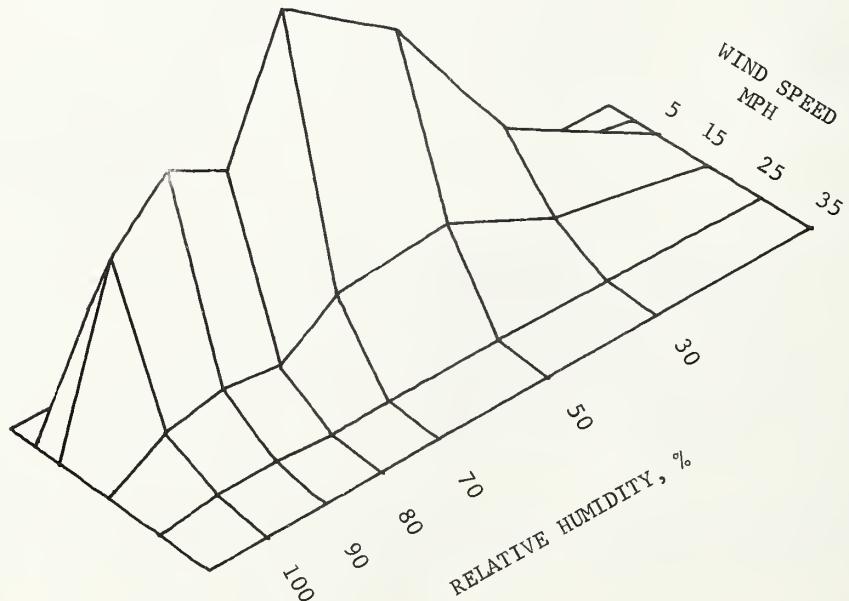


Fig. 4 COINCIDENT PROFILE FOR WIND SPEED
AND RELATIVE HUMIDITY

WILMINGTON, DELAWARE

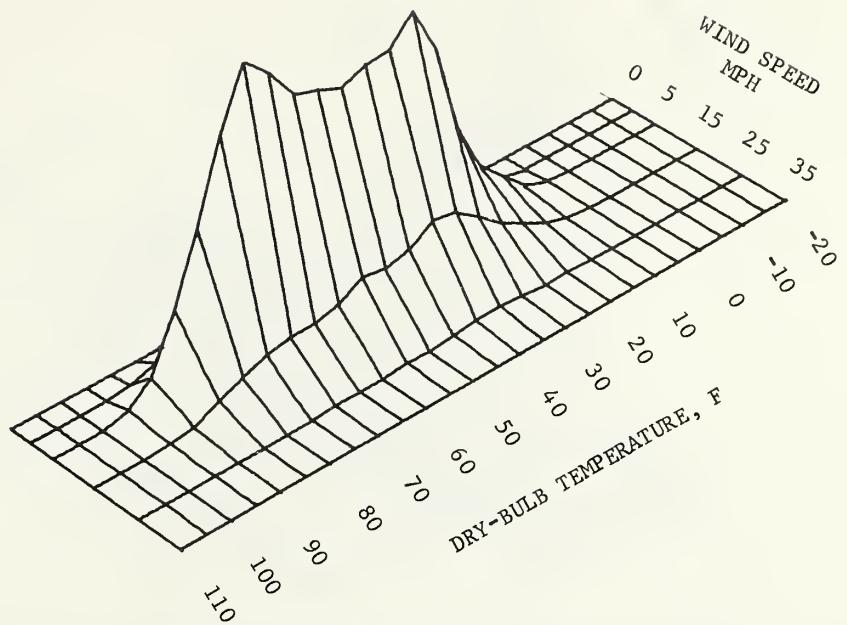


Fig. 5. COINCIDENT PROFILE FOR WIND SPEED AND DRY BULB TEMPERATURE

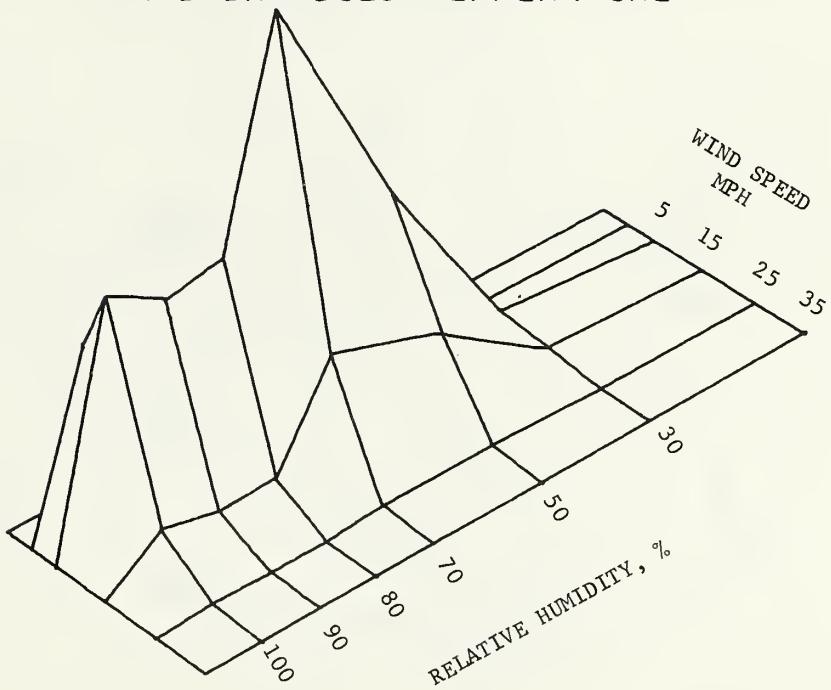


Fig. 6 COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY

MACON, GEORGIA

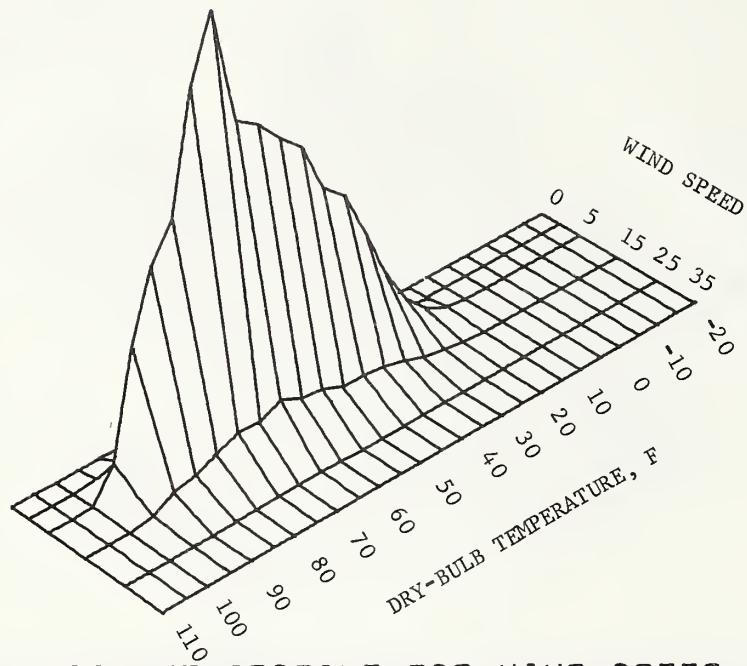


Fig. 7 COINCIDENT PROFILE FOR WIND SPEED AND DRY BULB TEMPERATURE

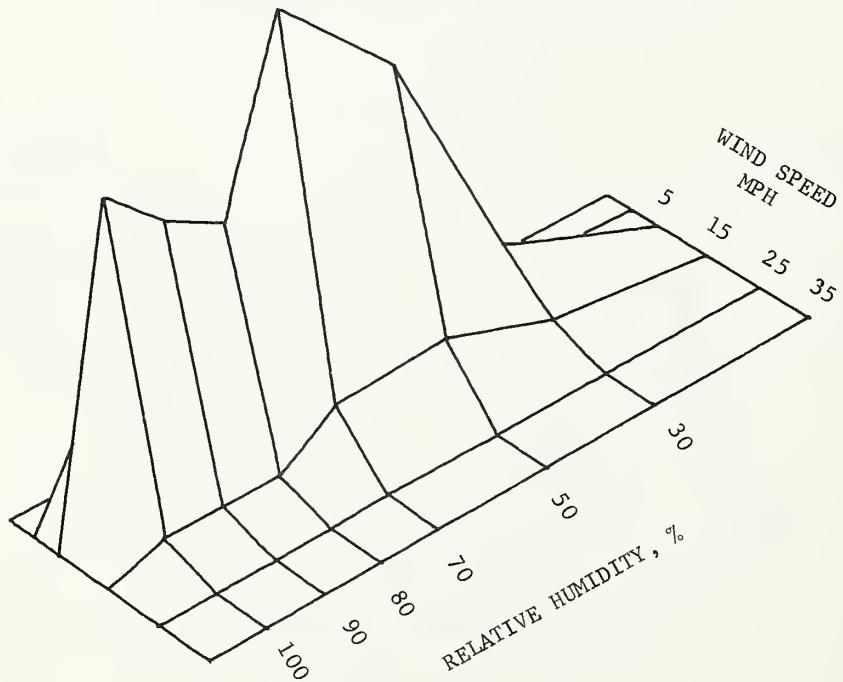


Fig. 8 COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY

INDIANAPOLIS, INDIANA

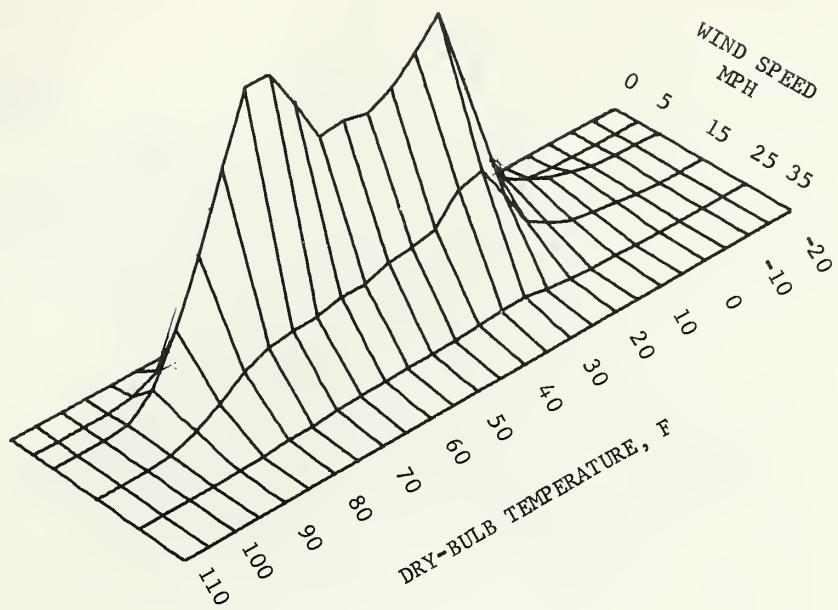


Fig. 9 COINCIDENT PROFILE FOR WIND SPEED AND DRY BULB TEMPERATURE

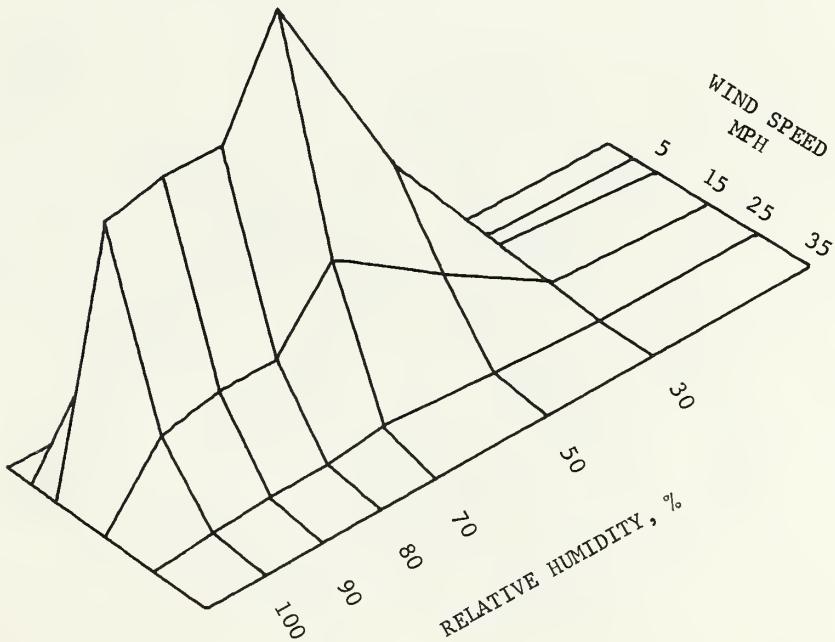


Fig. 10 COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY

GRAND RAPIDS, MICHIGAN

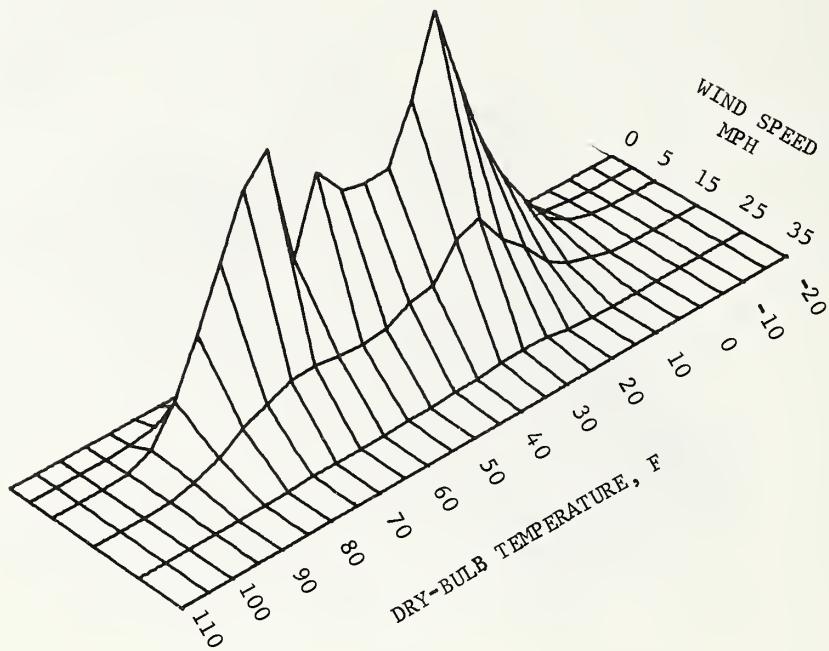


Fig. 11 COINCIDENT PROFILE FOR WIND SPEED
AND DRY BULB TEMPERATURE

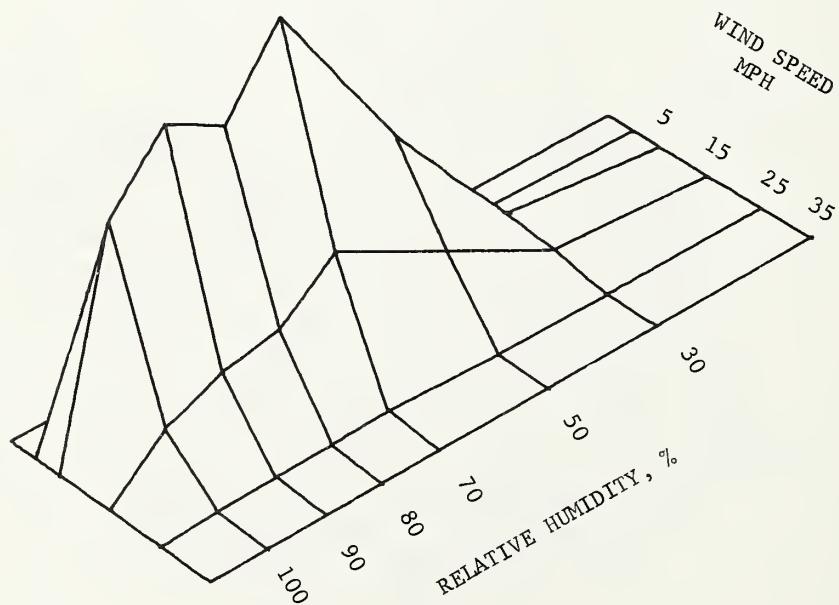


Fig. 12 COINCIDENT PROFILE FOR WIND SPEED
AND RELATIVE HUMIDITY

NEWARK, NEW JERSEY

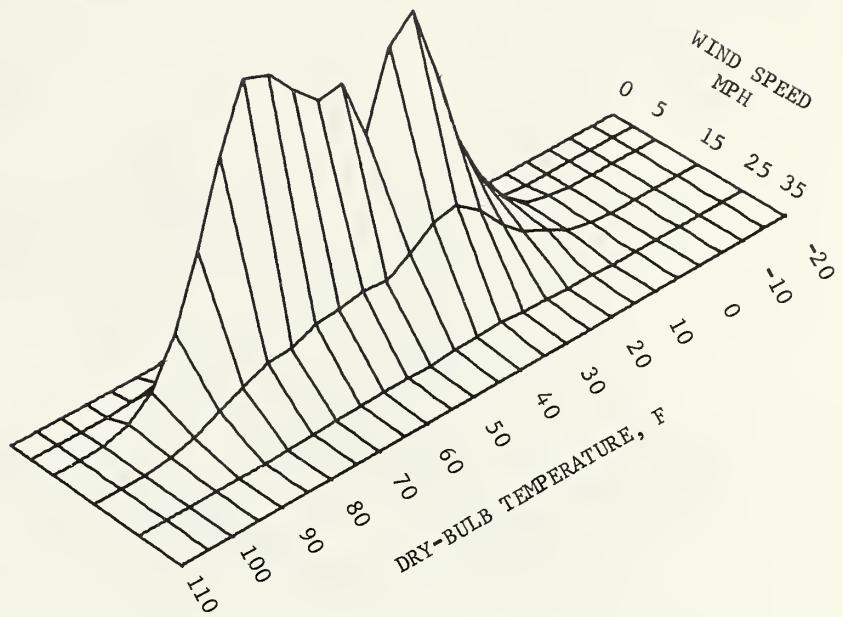


Fig. 13 COINCIDENT PROFILE FOR WIND SPEED AND DRY BULB TEMPERATURE

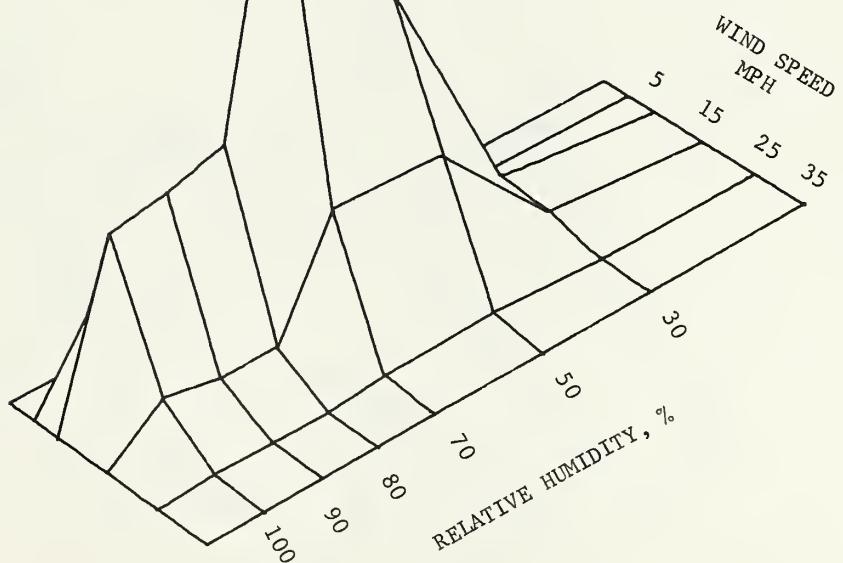


Fig. 14 COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY

ST. LOUIS, MISSOURI

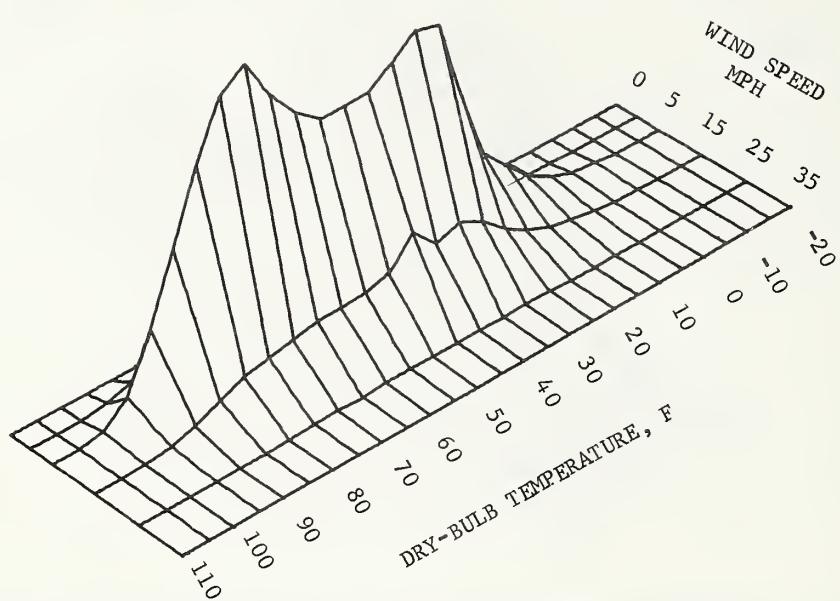


Fig. 15 COINCIDENT PROFILE FOR WIND SPEED AND DRY BULB TEMPERATURE

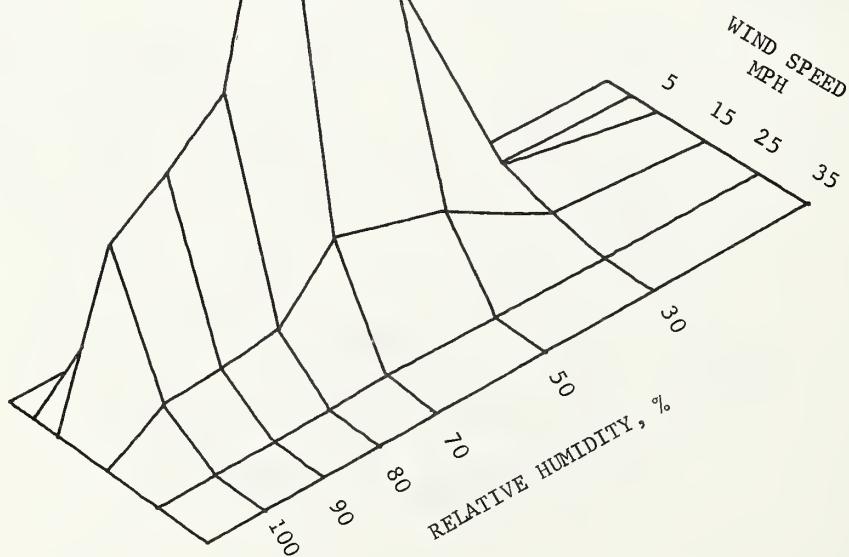


Fig. 16 COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY

MEMPHIS, TENNESSEE

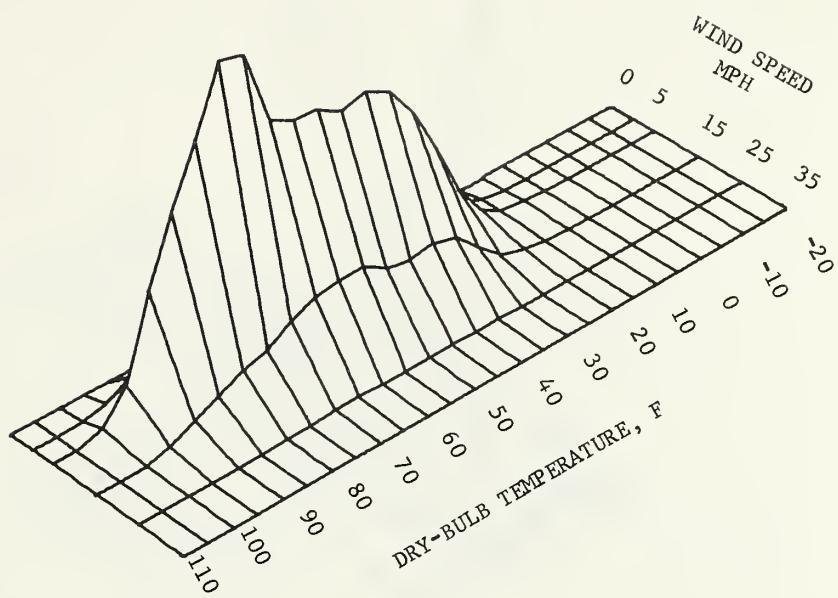


Fig. 17 COINCIDENT PROFILE FOR WIND SPEED
AND DRY BULB TEMPERATURE

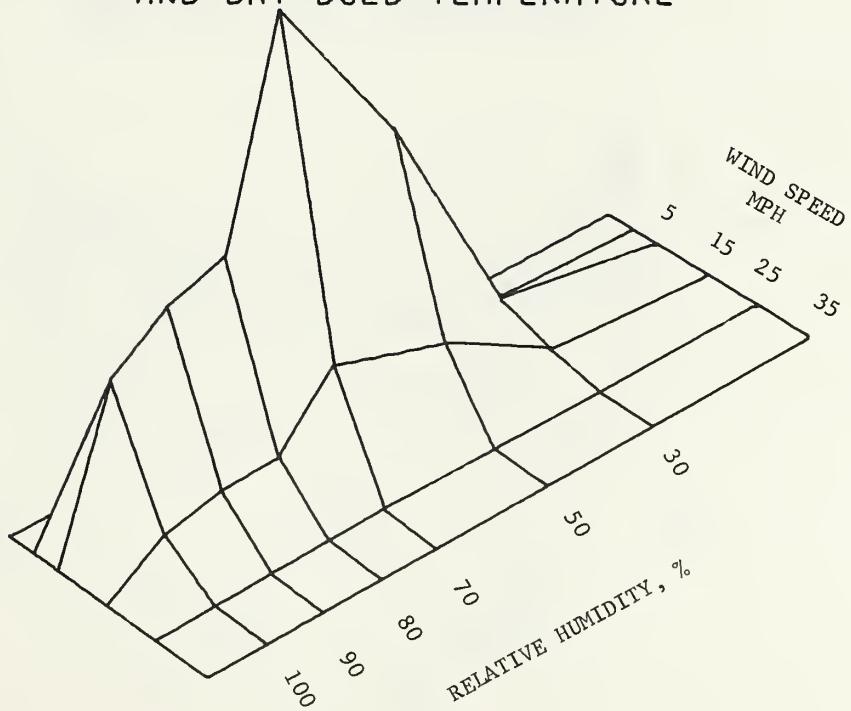


Fig. 18 COINCIDENT PROFILE FOR WIND SPEED
AND RELATIVE HUMIDITY

HOUSTON, TEXAS

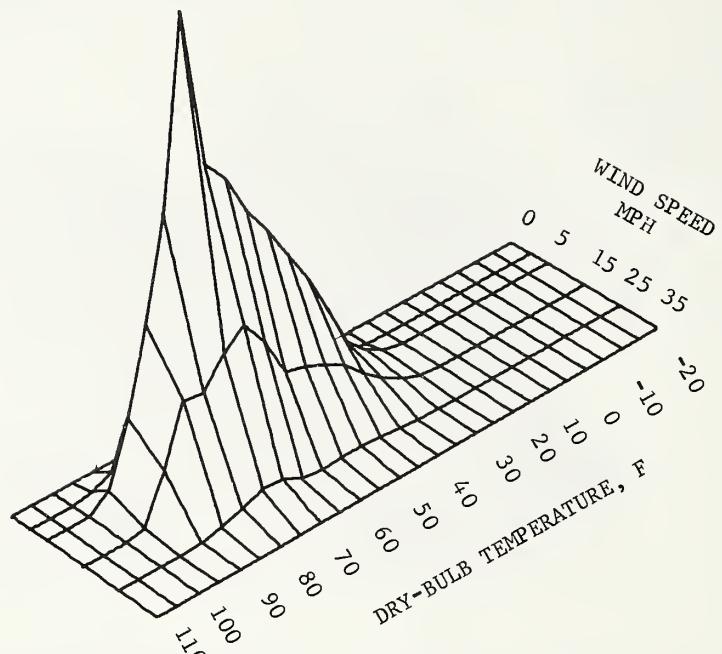


Fig. 19 COINCIDENT PROFILE FOR WIND SPEED AND DRY BULB TEMPERATURE

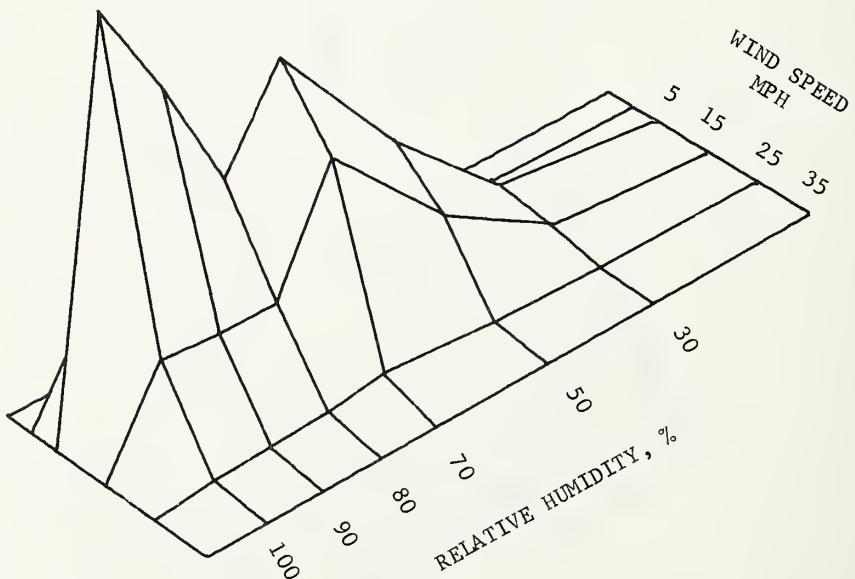


Fig. 20 COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY

SEATTLE, WASHINGTON

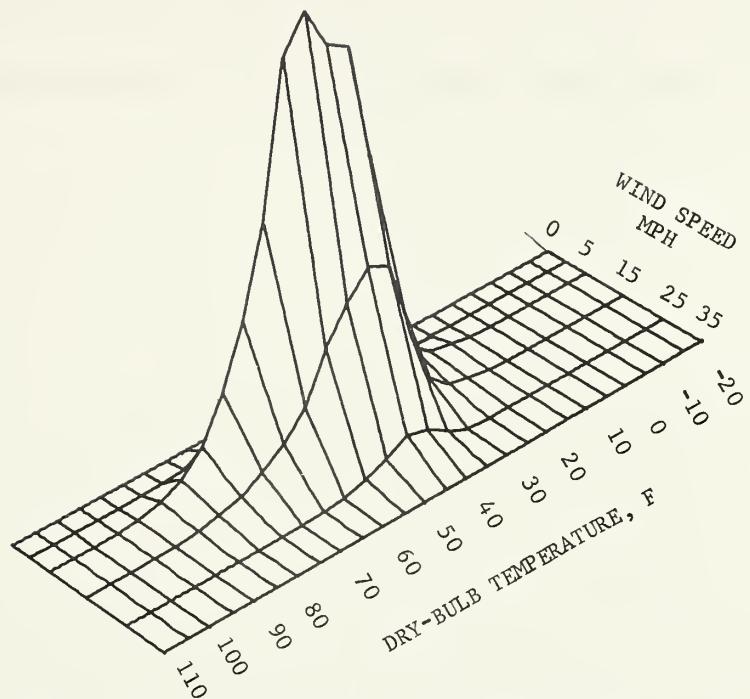


Fig. 21 COINCIDENT PROFILE FOR WIND SPEED AND DRY BULB TEMPERATURE

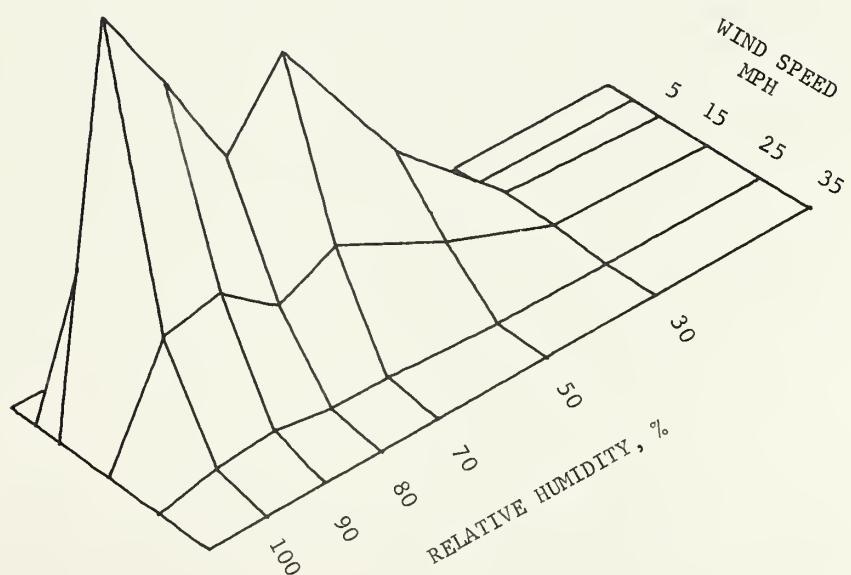


Fig. 22 COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY



Figures 23 through 32 present wind flow patterns by plotting the annual average wind speed in a polar form with respect to the direction of wind. Indicated on the polar diagram of the wind speed are the directions of prevailing wind during summer and winter seasons.

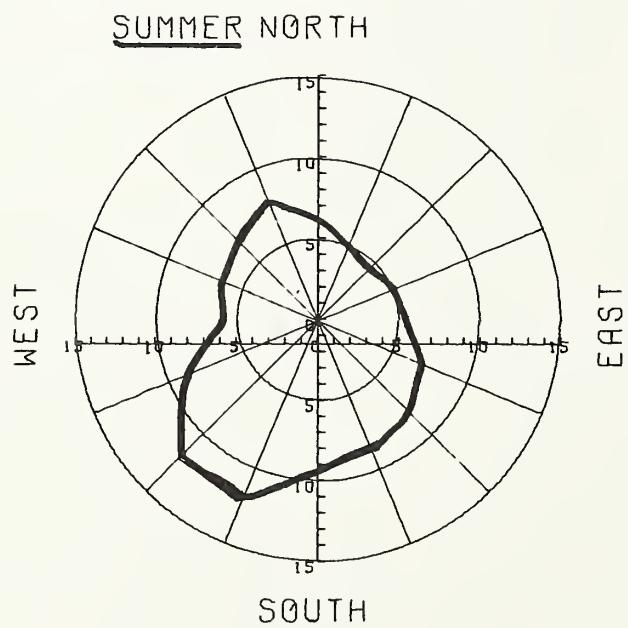
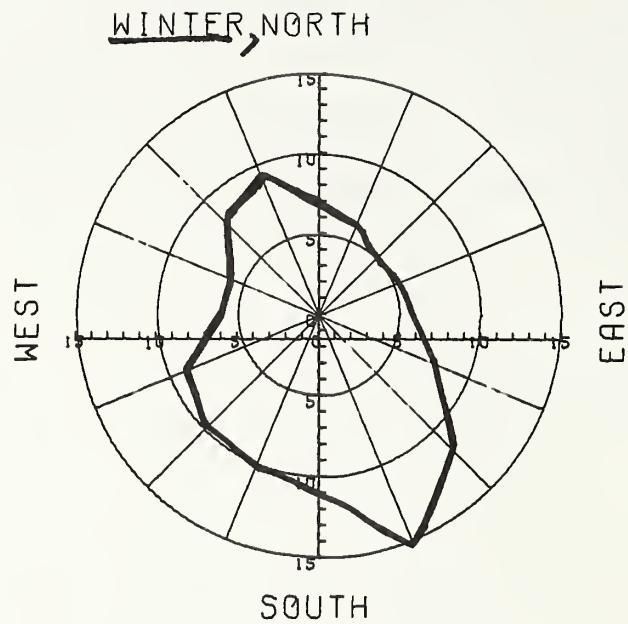
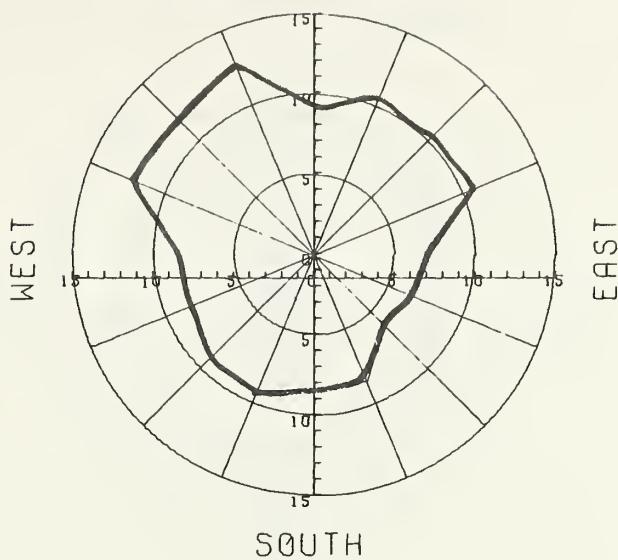


Fig. 23 SACRAMENTO, CALIFORNIA

WINTER NORTH



SUMMER NORTH

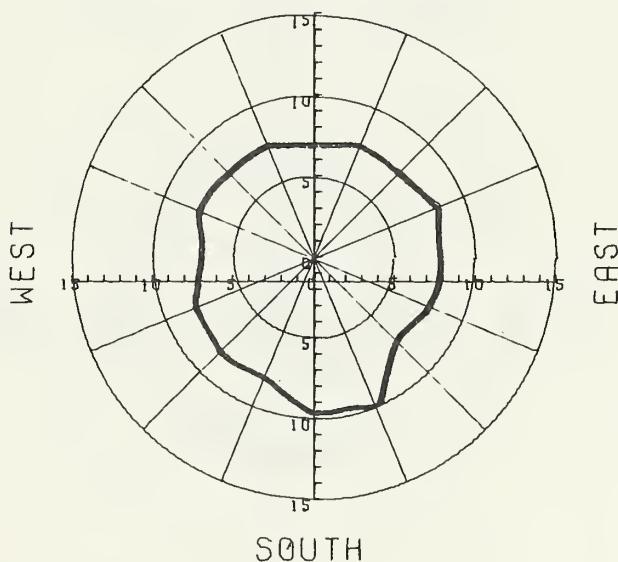
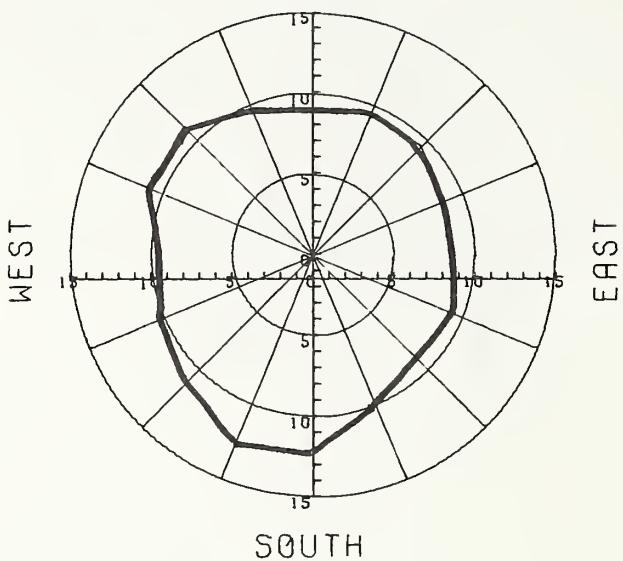


Fig. 24

WILMINGTON, DELAWARE

WINTER NORTH



SUMMER NORTH

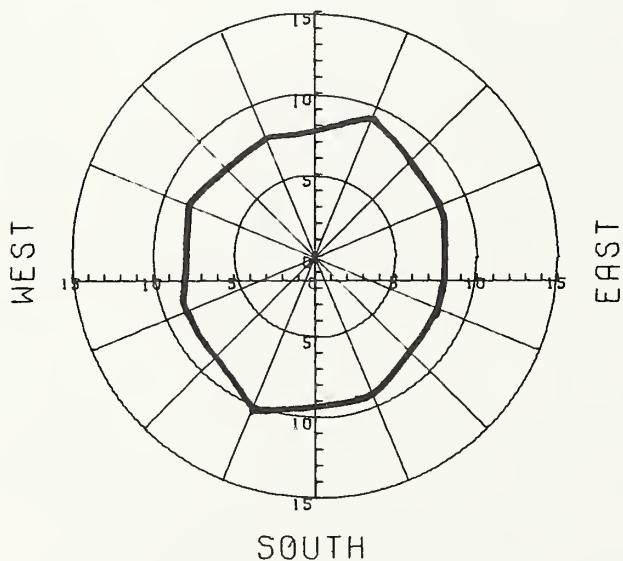
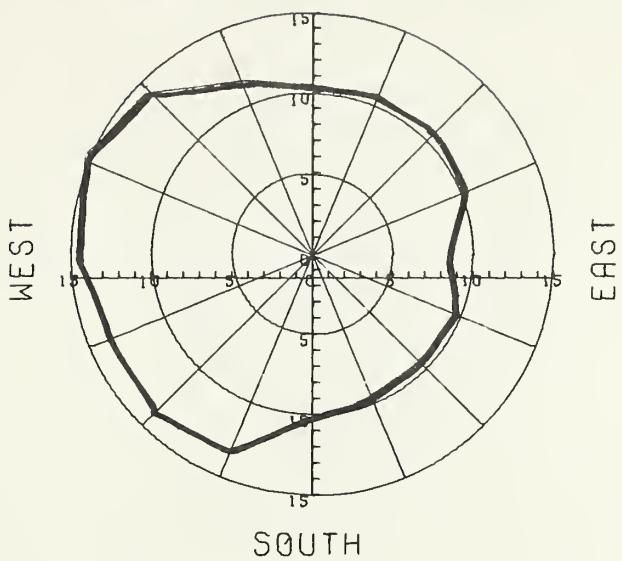


Fig. 25

MACON, GEORGIA

WINTER NORTH



SUMMER NORTH

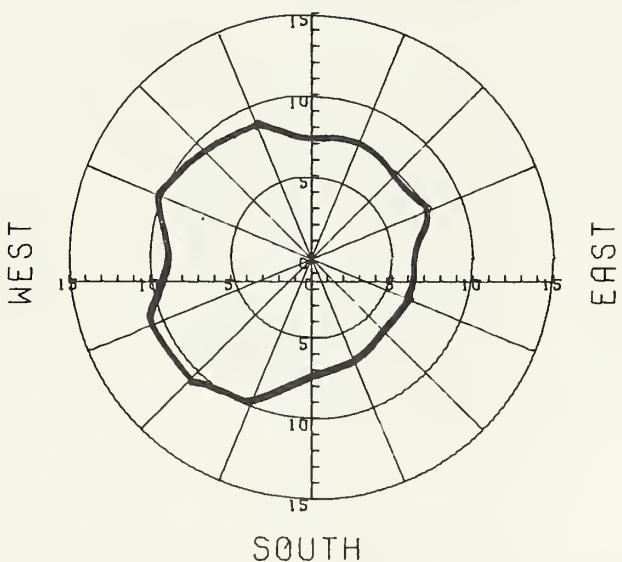
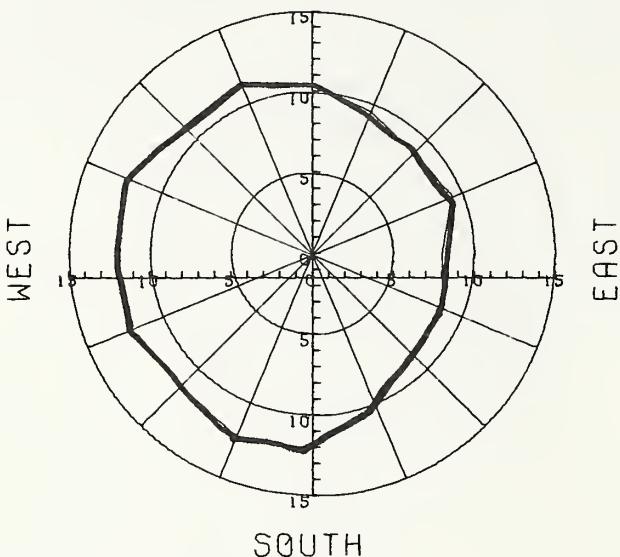


Fig. 26 INDIANAPOLIS, INDIANA

WINTER NORTH



SUMMER NORTH

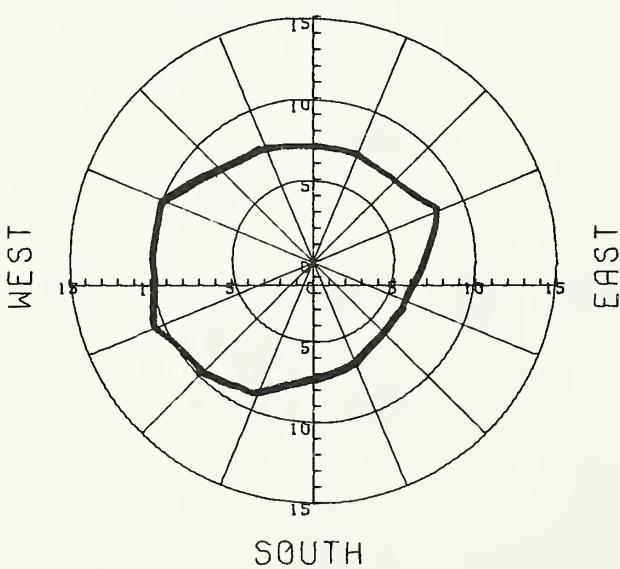
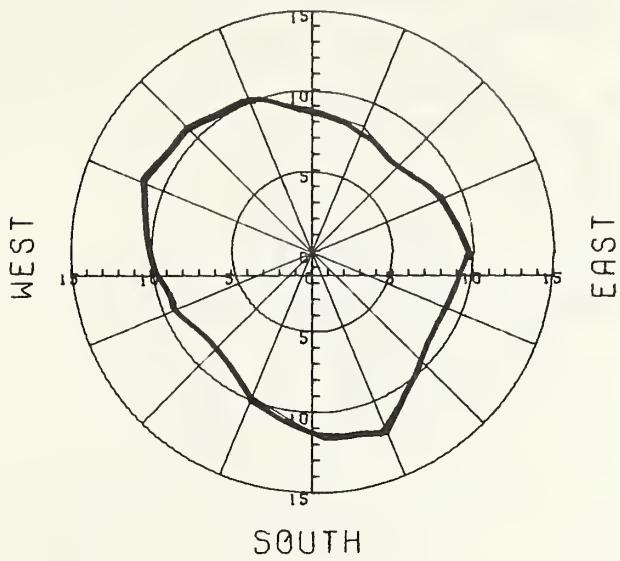


Fig. 27 GRAND RAPIDS, MICHIGAN

WINTER NORTH



SUMMER NORTH

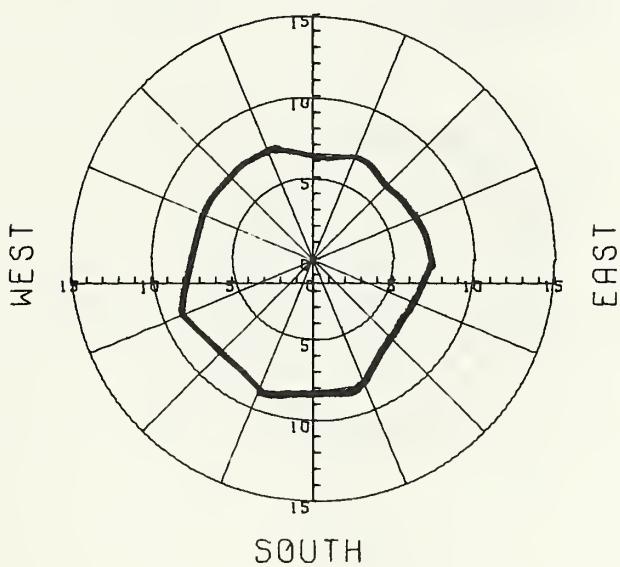
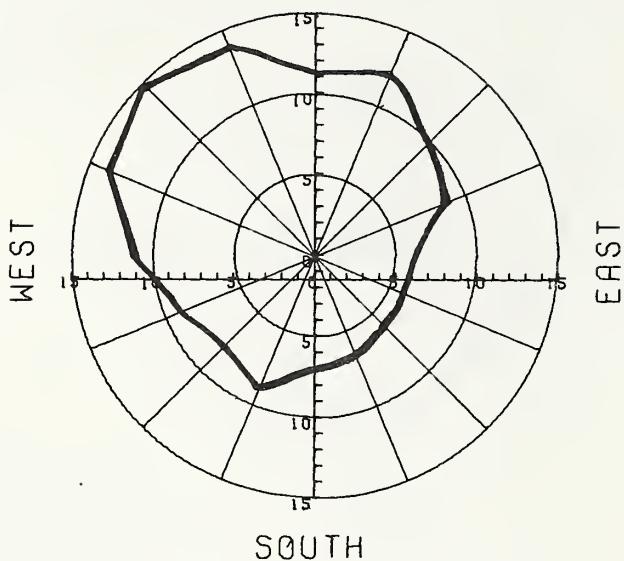


Fig. 28

ST. LOUIS, MISSOURI

WINTER NORTH



SUMMER NORTH

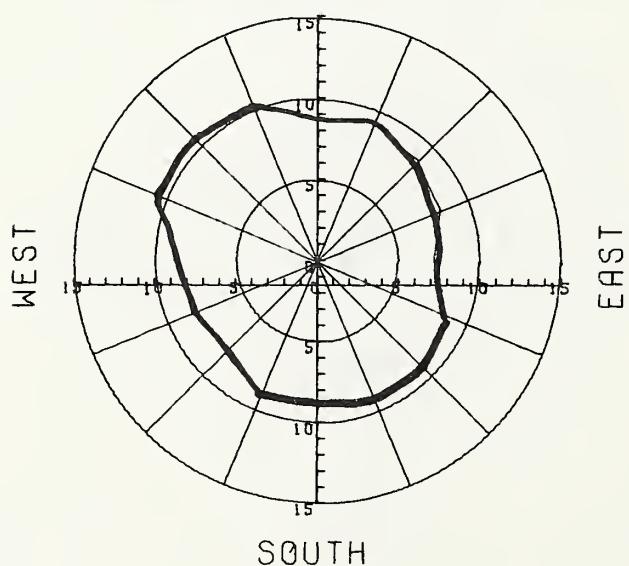
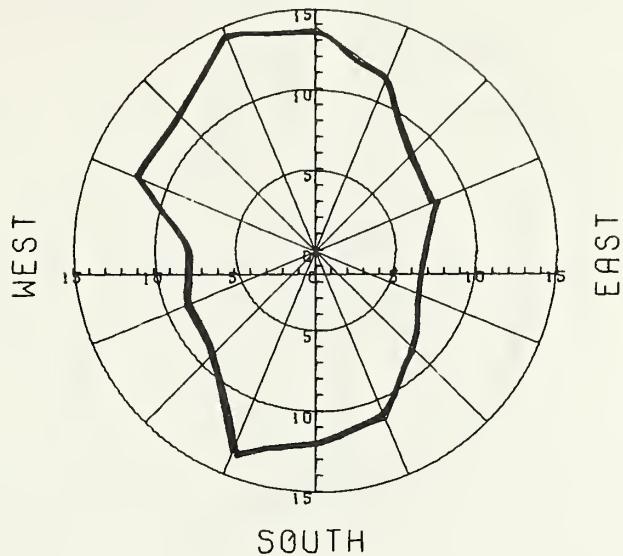


Fig. 29

NEWARK, NEW JERSEY

WINTER NORTH



SUMMER NORTH

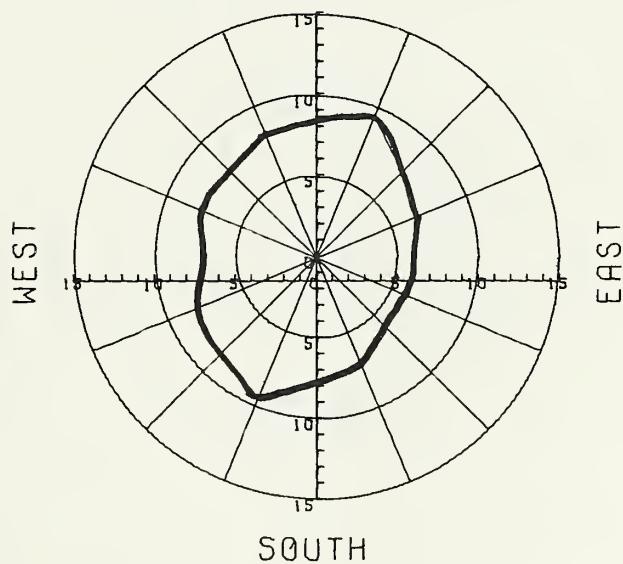
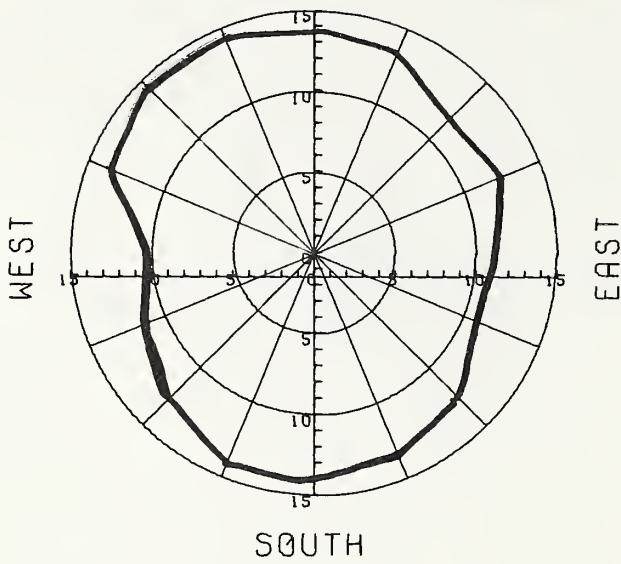


Fig. 30

MEMPHIS, TENNESSEE

WINTER NORTH



SUMMER NORTH

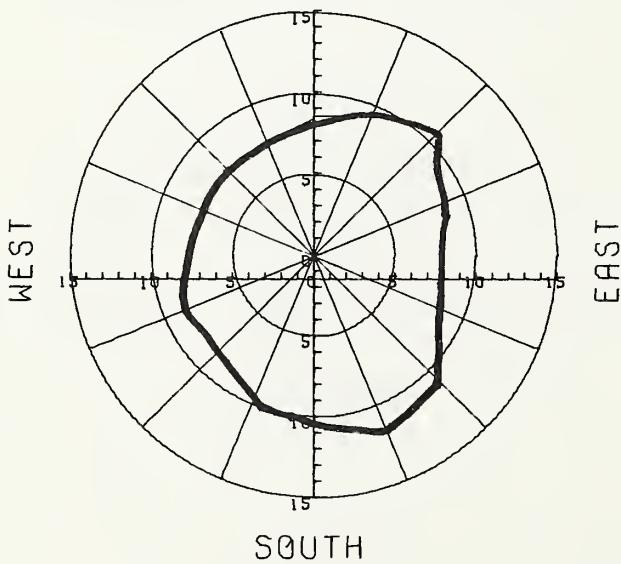
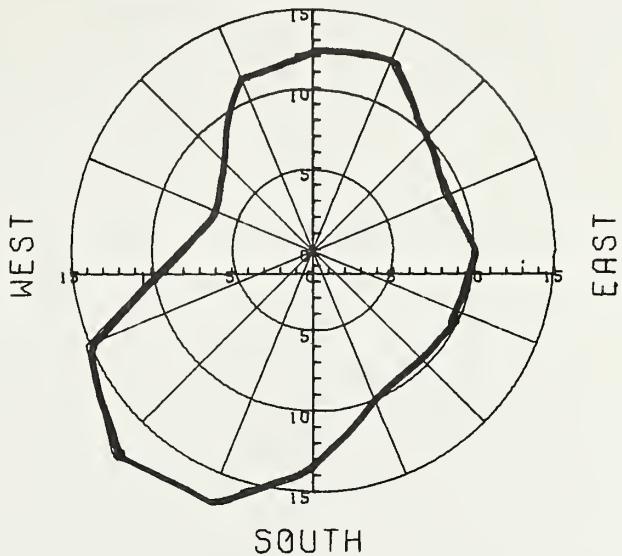


Fig. 31

HOUSTON, TEXAS

WINTER NORTH



SUMMER NORTH

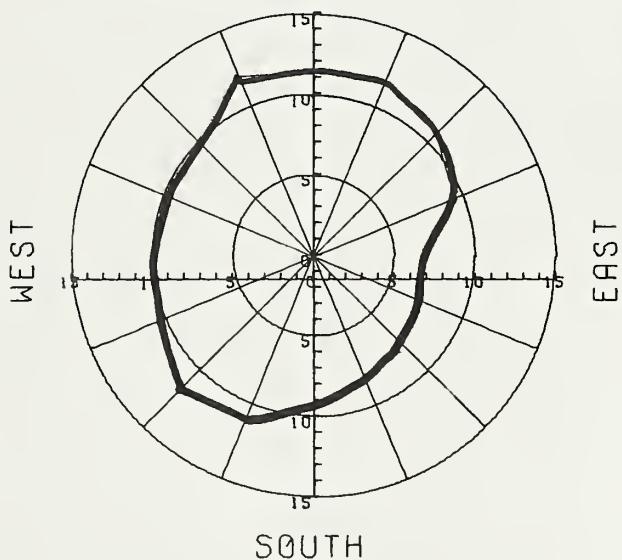


Fig. 32

SEATTLE, WASHINGTON

