

A11102 146103



NBS  
PUBLICATIONS

NAT'L INST OF STANDARDS & TECH R.I.C.



A11102146103  
SRDS-NBS  
100 .U573 V3;2;1967 C.2 NBS-PUB-C 1964

NSRDS-NBS 3, Section 2

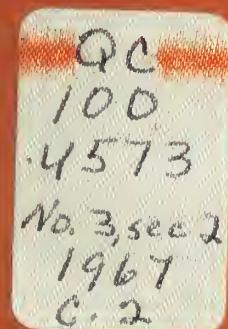
# Selected Tables of Atomic Spectra

## Atomic Energy Levels and Multiplet Tables

Si I

U.S. DEPARTMENT OF COMMERCE

NATIONAL BUREAU OF STANDARDS



**National Standard Reference Data Series**  
**National Bureau of Standards**

National Standard Reference Data System, Plan of Operation, NSRDS-NBS 1—  
15 cents\*

Thermal Properties of Aqueous Uni-univalent Electrolytes NSRDS-NBS 2—45 cents\*

Selected Tables of Atomic Spectra, Atomic Energy Levels and Multiplet Tables—Si II,  
Si III, Si IV, NSRDS-NBS 3, Section 1—35 cents\*

Selected Tables of Atomic Spectra, Atomic Energy Levels and Multiplet Tables—Si I,  
NSRDS-NBS 3, Section 2—20 cents\*

Atomic Transition Probabilities, Volume I, Hydrogen Through Neon, NSRDS-NBS 4—  
\$2.50\*

The Band Spectrum of Carbon Monoxide, NSRDS-NBS 5—70 cents\*

Tables of Molecular Vibrational Frequencies. Part 1, NSRDS-NBS 6—40 cents\*

High Temperature Properties and Decomposition of Inorganic Salts. Part 1. Sulfates,  
NSRDS-NBS 7—35 cents\*

Thermal Conductivity of Selected Materials, NSRDS-NBS 8—\$1.00\*

Tables of Bimolecular Gas Reactions, NSRDS-NBS 9—65 cents\*

Selected Values of Electric Dipole Moments for Molecules in the Gas Phase, NSRDS—  
NBS 10—40 cents\*

Tables of Molecular Vibrational Frequencies, Part 2. NSRDS-NBS 11—30 cents\*

Tables for the Rigid Asymmetric Rotor: Transformation Coefficients for Symmetric to  
Asymmetric Bases and Expectation Values of  $P_z^2$  and  $P_z^4$ , NSRDS-NBS 12—in press.

Hydrogenation of Ethylene on Metallic Catalysts, NSRDS-NBS 13—in press.

\*Send orders with remittance to: Superintendent of Documents, U.S. Government Printing Office,  
Washington, D.C. 20402. Remittances from foreign countries should include an additional one-fourth  
of the purchase price for postage.

UNITED STATES DEPARTMENT OF COMMERCE • Alexander B. Trowbridge, *Secretary*

NATIONAL BUREAU OF STANDARDS • A. V. Astin, *Director*

# Selected Tables of Atomic Spectra

## A Atomic Energy Levels-Second Edition

## B Multiplet Tables

Si I

Data Derived From the Analyses of Optical Spectra

Charlotte E. Moore

Institute for Basic Standards  
National Bureau of Standards  
Washington, D.C. 20234



NSRDS-NBS 3, Section 2  
National Standard Reference Data Series-  
U.S. National Bureau of Standards  
Category 3—Atomic and Molecular Properties

Issued November 30, 1967

JUN 9 1970

OC 100

0575

no. 3, sec. 1

1967

cop 2

## Abstract

The present publication is the second Section of a series being prepared in response to the increasing demand for a current revision of two sets of tables containing data on atomic spectra as derived from analyses of optical spectra.

Both the atomic energy levels and the multiplet table are included in the same publication, as parts A and B, respectively. The Sections are being prepared at irregular intervals for these spectra whose analyses are essentially complete. A flexible paging system permits the arrangement of the various Sections by atomic number regardless of the order in which the spectra are published in this series. Section 1 included three spectra of silicon, Z=14: Si II, Si III, Si IV. The present Section contains similar data for Si I. The form of presentation is described in detail in the text to Section 1, and need not be repeated here.

Key words: Atomic energy levels; atomic spectra Si I; multiplet table; silicon, first spectrum; spectrum, Si I; wavelengths, Si I.

## **Foreword**

The National Standard Reference Data System is a government-wide effort to give to the technical community of the United States optimum access to the quantitative data of physical science, critically evaluated and compiled for convenience. This program was established in 1963 by the President's Office of Science and Technology, acting upon the recommendation of the Federal Council for Science and Technology. The National Bureau of Standards has been assigned responsibility for administering the effort. The general objective of the System is to coordinate and integrate existing data evaluation and compilation activities into a systematic, comprehensive program, supplementing and expanding technical coverage when necessary, establishing and maintaining standards for the output of the participating groups, and providing mechanisms for the dissemination of the output as required.

The NSRDS is conducted as a decentralized operation of nation-wide scope with central coordination by NBS. It comprises a complex of data centers and other activities, carried on in government agencies, academic institutions, and nongovernmental laboratories. The independent operational status of existing critical data projects is maintained and encouraged. Data centers that are components of the NSRDS produce compilations of critically evaluated data, critical reviews of the state of quantitative knowledge in specialized areas, and computations of useful functions derived from standard reference data.

For operational purposes, NSRDS compilation activities are organized into seven categories as listed below. The data publications of the NSRDS, which may consist of monographs, loose-leaf sheets, computer tapes, or any other useful product, will be classified as belonging to one or another of these categories. An additional "General" category of NSRDS publications will include reports on detailed classification schemes, lists of compilations considered to be Standard Reference Data, status reports, and similar material. Thus, NSRDS publications will appear in the following eight categories:

<i>Category</i>	<i>Title</i>
1	General
2	Nuclear Properties
3	Atomic and Molecular Properties
4	Solid State Properties
5	Thermodynamic and Transport Properties
6	Chemical Kinetics
7	Colloid and Surface Properties
8	Mechanical Properties of Materials

The present compilation is in category 3 of the above list. It constitutes the fourteenth publication in a new NBS series known as the National Standard Reference Data Series.

## Preface

The present publication is the second Section of a series that is being prepared in response to the increasing demand for a current revision of two sets of tables containing data on atomic spectra as derived from analyses of optical spectra.

The first set, ATOMIC ENERGY LEVELS, NBS Circular 467, consists of three Volumes published, respectively, in 1949, 1952, and 1958, and a fourth on rare-earth spectra, still in course of preparation.

The second set consists of two Multiplet Tables; one published in 1945 by the Princeton University Observatory, containing spectral lines in the region of wavelengths longer than 3000 Å; the other AN ULTRAVIOLET MULTIPLET TABLE, NBS Circular 488, appearing in five Sections, the first in 1950, the second in 1952, and the others in 1962.

Both the atomic energy levels and the multiplet table are being included in the same publication, as parts A and B, respectively. The Sections are being prepared at irregular intervals for those spectra whose analyses are essentially complete. A flexible paging system permits the arrangement of the various Sections by atomic number regardless of the order in which the spectra are published in this series. Section I included three spectra of silicon,  $Z = 14$ : Si II, Si III, Si IV. The present Section contains similar data for Si I. The form of presentation is described in detail in the text to Section 1, and need not be repeated here.

The manuscript has been prepared by Charlotte E. Moore of the Atomic Physics Division, who also prepared the earlier tables. She acknowledges with gratitude the cordial cooperation of the National Research Council Committee on Line Spectra of the Elements, as well as that of the many atomic spectroscopists who make such a publication possible. It is hoped that as succeeding Sections appear they will provide a stimulus to carry on the analyses of many more atomic spectra.

Washington, D.C., April 14, 1967.

A. V. ASTIN, *Director.*

## **Contents**

	Page
Preface.....	IV

### **Part A—Atomic Energy Levels**

Element: Z Spectrum	
Silicon: 14	
Si I.....	A14 i-l

### **Part B—Multiplet Table**

Element: Z Spectrum	
Silicon: 14	
Si I.....	B14 i-l

NSRDS-NBS 3, SECTION 2

**SILICON, Z=14**

A Si I Atomic Energy Levels

B Si I Multiplet Table

## Atomic Energy Levels

### Part A

### SILICON

#### Si I

14 electrons

$Z = 14$

Ground state  $1s^2 2s^2 2p^6 3s^2 3p^2 3P_0$

$3p^2 3P_0 \mathbf{65747.5 \pm 0.6 \text{ cm}^{-1}}$ ,  $1520.97 \text{ \AA}$  (Vac)

I P 8.151 eV

The analysis is chiefly from the 1965 paper by Radziemski and Andrew, supplemented by observations in the lead sulphide region by Litzén and in the vacuum ultraviolet by these authors and by Kaufman and Wilson. The range of observations is from  $1255 \text{ \AA}$  to  $25854 \text{ \AA}$ . There are approximately 650 classified lines.

The writer has rearranged the  $6f$  pairs and made other adjustments consistent with the observed combinations. Improved level values from the 1967 paper are quoted.

The limit has been derived by a modified Ritz formula from  $nf$  series, with  $n=4$  to 7,  $nd$   $^3F_4^o$  series with  $n=3$  to 8, and  $nd$   $^3D_3^o$  series with  $n=3$  to 10.

Lambert and Warner have extended the present analysis by predicting additional series members and deriving level values from lines in the solar spectrum:  $nf$  to  $n=10$ ;  $nd$  to  $n=11$ . Their values have been added in proof for the levels:

$$\begin{aligned} & 6f' [1\frac{1}{2}]_1, 2 \\ & 7f' [2\frac{1}{2}]_2 \quad \text{corrected} \\ & 7f' [4\frac{1}{2}]_4. \end{aligned}$$

Further confirmation of their data from laboratory observations is desirable.

The present multiplet table might well be extended to include additional predicted lines as the analysis and solar data are carried further.

### REFERENCES

- N. A. El'iashevich, O. N. Nikitina, Soviet Physics "Doklady" **1**, 649 to 651 (1956). T, C L
- C. C. Kiess, unpublished material (July 1957). T, C L
- A. G. Shenstone, J. Opt. Soc. Am. **52**, 479 (1962). T, C L
- U. Litzén, Ark. Fys. **28**, No. 20, 239 to 248 (1964). T, C L
- M. Wilson, Thesis, unpublished (Nov. 1964). T, C L
- H. Niewodniczanski, H. Pietruszka, Acta Physica Polon. **27**, 807 to 813 (1965). Forb. C L
- L. J. Radziemski, Jr., K. L. Andrew, J. Opt. Soc. Am. **55**, 474 to 491 (1965). I P, T, C L
- U. Litzén, Ark. Fys. **31**, No. 30, 453 to 459 (1966). T, C L
- V. Kaufman, L. J. Radziemski, Jr., K. L. Andrew, J. Opt. Soc. Am. **56**, 911 to 915 (1966). T, C L
- L. J. Radziemski, Jr., K. L. Andrew, V. Kaufman, U. Litzén, J. Opt. Soc. Am. **57**, 336 to 340 (1967). T, C L
- D. L. Lambert, B. Warner, Mon. Nat. Roy. Astron. Soc., in press (1967).

## Atomic Energy Levels

**Si I**
**Si I**

Config.	Desig.	J	Level	Interval	Config.	Desig.	J	Level	Interval	
$3s^2 3p^2$	$3p^2 \ ^3P$	0	0.000		$3s^2 3p(^2P^o)5p$	$5p \ ^3P$	0	57295.881		
		1	77.115	77.115			1	57328.789	32.908	
		2	223.157	146.042			2	57468.239	139.450	
$3s^2 3p^2$	$3p^2 \ ^1D$	2	6298.850		$3s^2 3p(^2P^o)4d$	$4d \ ^3F^o$	2	57372.297		
$3s^2 3p^2$	$3p^2 \ ^1S$	0	15394.370				3	57450.580	78.283	
$3s^2 3p^3$	$3p^3 \ ^5S^o$	2	33326.053		$3s^2 3p(^2P^o)5p$	$5p \ ^3S$	1	57541.918		
$3s^2 3p(^2P^o)4s$	$4s \ ^3P^o$	0	39683.163	77.122	$3s^2 3p(^2P^o)5p$	$5p \ ^1D$	2	57798.072		
		1	39760.285	194.768	$3s^2 3p(^2P^o)5p$	$5p \ ^1S$	0	58311.659		
$3s^2 3p(^2P^o)4s$	$4s \ ^1P^o$	1	40991.884		$3s^2 3p(^2P^o)4f$	$4f[2\frac{1}{2}]$	3	58774.368		
$3s^2 3p^3$	$3p^3 \ ^3D^o$	1	45276.188	17.441	$3s^2 3p(^2P^o)4f$	$4f[3\frac{1}{2}]$	2	58775.451		
		2	45293.629	28.219			3	58786.860		
		3	45321.848		$3s^2 3p(^2P^o)4f$	$4f[3\frac{1}{2}]$	4	58788.880		
$3s^2 3p(^2P^o)4p$	$4p \ ^1P$	1	47284.061		$3s^2 3p(^2P^o)4d$	$4d \ ^1P^o$	1	58801.529		
$3s^2 3p(^2P^o)3d$	$3d \ ^1D^o$	2	47351.554		$3s^2 3p(^2P^o)4d$	$4d \ ^1F^o$	3	58893.40		
$3s^2 3p(^2P^o)4p$	$4p \ ^3D$	1	48020.074	82.249	$3s^2 3p(^2P^o)4d$	$4d \ ^3D^o$	1	59056.508		
		2	48102.323	161.969			2	59032.19	-24.32	
		3	48264.292		$3s^2 3p(^2P^o)4d$	$4d \ ^3D^o$	3	59118.03	85.84	
$3s^2 3p(^2P^o)4p$	$4p \ ^3P$	0	49028.294	32.307	$3s^2 3p(^2P^o)4f$	$4f' [3\frac{1}{2}]$	3	59034.988		
		1	49060.601	128.016			4	59037.043		
		2	49188.617		$3s^2 3p(^2P^o)4f$	$4f' [3\frac{1}{2}]$	3	59109.959		
$3s^2 3p(^2P^o)4p$	$4p \ ^3S$	1	49399.670				2	59110.892		
$3s^2 3p(^2P^o)3d$	$3d \ ^3F^o$	2	49850.830	82.945	"	$4f' [2\frac{1}{2}]$	3			
		3	49933.775	121.02	"		2			
		4	50054.80		"	$4f' [4\frac{1}{2}]$	5	59128.40		
					"		4	59131.912		
$3s^2 3p(^2P^o)4p$	$4p \ ^1D$	2	50189.389		"	$4f' [1\frac{1}{2}]$	1	59190.46		
$3s^2 3p(^2P^o)3d$	$3d \ ^3P^o$	2	50499.838	-66.559			2	59191.072		
		1	50566.397	-36.04	$3s^2 3p(^2P^o)6s$	$6s \ ^3P^o$	0	59221.11		
		0	50602.44				1	59273.575	52.46	
					$3s^2 3p(^2P^o)6s$		2	59506.359	232.784	
$3s^2 3p(^2P^o)4p$	$4p \ ^1S$	0	51612.012		$3s^2 3p(^2P^o)6s$	$6s \ ^1P^o$	1	59636.667		
$3s^2 3p(^2P^o)3d$	$3d \ ^1F^o$	3	53362.24		$3s^2 3p(^2P^o)4d$	$4d \ ^3P^o$	2	59917.336		
$3s^2 3p(^2P^o)3d$	$3d \ ^1P^o$	1	53387.334				1	60010.458	-93.122	
$3s^2 3p(^2P^o)3d$	$3d \ ^3D^o$	1	54185.264	19.826	$3s^2 3p(^2P^o)5d$	$5d \ ^1D^o$	0	60042.50	-32.04	
		2	54205.090	52.492						
		3	54257.582		$3s^2 3p(^2P^o)6p$	$6p \ ^1P$	1	60300.860		
$3s^2 3p(^2P^o)5s$	$5s \ ^3P^o$	0	54245.020	68.798						
		1	54313.818	214.402	$3s^2 3p(^2P^o)6p$	$6p \ ^3D$	1	60487.103		
		2	54528.220				2	60496.358	9.255	
					$3s^2 3p(^2P^o)6p$		3	60704.53	208.17	
$3s^2 3p(^2P^o)5s$	$5s \ ^1P^o$	1	54871.031		$3s^2 3p(^2P^o)6p$	$6p \ ^3P$	0	60621.64		
$3s^2 3p(^2P^o)4d$	$4d \ ^1D^o$	2	56503.346				1	60706.558	84.92	
$3s^2 3p^3$	$3p^3 \ ^3P^o$	2	56690.903	-9.35	$3s^2 3p(^2P^o)6p$		2	60815.925	109.367	
		1	56700.25	-33.13	$3s^2 3p(^2P^o)5d$	$5d \ ^3F^o$	2			
		0	56733.38				3	60645.441		
					$3s^2 3p(^2P^o)5d$		4	60705.464	60.024	
$3s^2 3p(^2P^o)5p$	$5p \ ^1P$	1	56780.427					4	60848.946	143.482
$3s^2 3p(^2P^o)5p$	$5p \ ^3D$	1	56978.256	39.240	$3s^2 3p(^2P^o)6p$	$6p \ ^3S$	1	60856.630		
		2	57017.496	180.531						
		3	57198.027		$3s^2 3p(^2P^o)6p$	$6p \ ^1D$	2	60962.105		

# Atomic Energy Levels

## Si I—Continued

## Si I—Continued

Config.	Desig.	J	Level	Interval	Config.	Desig.	J	Level	Interval	
$3s^2 3p(^2P^{\circ})6p$	$6p\ ^1S$	0	61198.036		$3s^2 3p(^2P^{\circ})6d$	$6d\ ^3D^{\circ}$	1	62925.80		
$3s^2 3p(^2P^{\circ}_{\frac{1}{2}})5f$	$5f[2\frac{1}{2}]$	3	61303.381				2	62874.48	-51.32	
		2	61304.283				3	62936.14	61.66	
$3s^2 3p(^2P^{\circ}_{\frac{1}{2}})5f$	$5f[3\frac{1}{2}]$	3	61305.050		$3s^2 3p(^2P^{\circ})6d$	$6d\ ^3P^{\circ}$	2	62921.08?		
		4	61306.713				1	63097.36	-176.28	
$3s^2 3p(^2P^{\circ})5d$	$5d\ ^1P^{\circ}$	1	61305.67		$3s^2 3p(^2P^{\circ}_{\frac{1}{2}})6f$	$6f'\ [3\frac{1}{2}]$	3	62935.76		
$3s^2 3p(^2P^{\circ})5d$	$5d\ ^1F^{\circ}$	3	61423.23				4	62936.81		
$3s^2 3p(^2P^{\circ})5d$	$5d\ ^3D^{\circ}$	1	61511.77		"	$6f'\ [2\frac{1}{2}]$	3	62954.46		
		2	61447.86	-63.91			2	62955.00		
		3	61574.814	126.95	"	$6f'\ [4\frac{1}{2}]$	5	62966.61		
$3s^2 3p(^2P^{\circ})7s$	$7s\ ^3P^{\circ}$	0	61538.05				4	62968.49?		
		1	61595.43	57.38	"	$6f'\ [1\frac{1}{2}]$	1	62985.96?		
		2	61823.550	228.12			2	62986.32?		
$3s^2 3p(^2P^{\circ}_{\frac{1}{2}})5f$	$5f'\ [3\frac{1}{2}]$	3	61562.477		$3s^2 3p(^2P^{\circ})8s$	$8s\ ^1P^{\circ}$	1	63130.49		
"	$5f'\ [2\frac{1}{2}]$	3	61597.404		$3s^2 3p(^2P^{\circ})7d$	$7d\ ^1D^{\circ}$	2	63204.89		
"		2	61598.145		$3s^2 3p(^2P^{\circ})8p$	$8p\ ^3D?$	3			
"	$5f'\ [4\frac{1}{2}]$	5	61614.37				2	63225.5?		
"		4	61617.17		$3s^2 3p(^2P^{\circ})7d$	$7d\ ^3F^{\circ}$	1			
"	$5f'\ [1\frac{1}{2}]$	1	61647.36				2	63356.24		
		2	61647.875				3	63340.70	-15.54	
$3s^2 3p(^2P^{\circ})5d$	$5d\ ^3P^{\circ}$	2	61841.94	-94.19			4	63514.533	173.83	
		1	61936.13		$3s^2 3p(^2P^{\circ})7d$	$7d\ ^1P^{\circ}$	1	63486.93		
		0	61960.26	-24.13	$3s^2 3p(^2P^{\circ})9s$	$9s\ ^3P^{\circ}$	0	63579.44?		
$3s^2 3p(^2P^{\circ})7s$	$7s\ ^1P^{\circ}$	1	61881.60				1	63584.22	4.78	
$3s^2 3p(^2P^{\circ})7p$	$7p\ ^1P$	1	62141.8?				2	63863.78	279.56	
$3s^2 3p(^2P^{\circ})6d$	$6d\ ^1D^{\circ}$	2	62156.816		$3s^2 3p(^2P^{\circ})8p$	$8p\ ^1S$	0	63618.6?		
$3s^2 3p(^2P^{\circ})7p$	$7p\ ^3D$	1	62226.39		$3s^2 3p(^2P^{\circ})7d$	$7d\ ^1F^{\circ}$	3	63641.77		
		2	62231.99?	5.60		$3s^2 3p(^2P^{\circ})7d$	$7d\ ^3D^{\circ}$	1	63750.39	
		3	62421.03	189.04			2	63714.40	-35.99	
$3s^2 3p(^2P^{\circ})7p$	$7p\ ^3P$	0	62318.7?	131.7			3	63760.24	45.84	
		1	62450.40		$3s^2 3p(^2P^{\circ})7d$	$7d\ ^3P^{\circ}$	2	63721.53?		
		2	62519.66	69.26			1	63770.28	-48.75	
$3s^2 3p(^2P^{\circ})6d$	$6d\ ^3F^{\circ}$	2	62349.93	26.89			0	63844.64	-74.36	
		3	62376.820		$3s^2 3p(^2P^{\circ}_{\frac{1}{2}})7f$	$7f'\ [3\frac{1}{2}]$	3	63762.20?		
		4	62534.08	157.26			4	63762.93?		
$3s^2 3p(^2P^{\circ})7p$	$7p\ ^3S$	1	62545.10		"	$7f'\ [2\frac{1}{2}]$	2	63773.58?		
$3s^2 3p(^2P^{\circ})7p$	$7p\ ^1D$	2	62596.32				3	63773.29?		
$3s^2 3p(^2P^{\circ})6d$	$6d\ ^1P^{\circ}$	1	62666.25		"	$7f'\ [4\frac{1}{2}]$	5	63781.97?		
$3s^2 3p(^2P^{\circ}_{\frac{1}{2}})6f$	$6f[2\frac{1}{2}]$	3	62667.823				4	63783.31?		
		2	62669.727		$3s^2 3p(^2P^{\circ})9s$	$9s\ ^1P^{\circ}$	1	63884.61		
	$6f[3\frac{1}{2}]$	3	62669.164		$3s^2 3p(^2P^{\circ})8d$	$8d\ ^3F^{\circ}$	2	63990.67		
		4	62669.179				3	63945.09	-45.58	
$3s^2 3p(^2P^{\circ})7p$	$7p\ ^1S$	0	62718.99				4	64133.93?	188.84	
$3s^2 3p(^2P^{\circ})6d$	$6d\ ^1F^{\circ}$	3	62802.86		$3s^2 3p(^2P^{\circ})8d$	$8d\ ^1P^{\circ}$	1	64018.31?		
$3s^2 3p(^2P^{\circ})8s$	$8s\ ^3P^{\circ}$	0	62806.65?	6.61		$10s\ ^3P^{\circ}$	0	64086.37?		
		1	62813.26		$3s^2 3p(^2P^{\circ})10s$		1	64086.48?	278.11	
		2	63093.41	280.14			2			

# Atomic Energy Levels

## Si I—Continued

## Si I—Continued

Config.	Desig.	J	Level	Interval	Config.	Desig.	J	Level	Interval
$3s^2 3p(^2P^{\circ})8d$	$8d^{-1}F^{\circ}$	3	64187.80		$3s^2 3p(^2P^{\circ})10d$	$10d^{-3}P^{\circ}$	2 1 0	64882.8?	
$3s^2 3p(^2P^{\circ})8d$	$8d^{-3}P^{\circ}$	2 1 0	64243.38? 64322.69?		$3s^2 3p(^2P^{\circ})10d$	$10d^{-3}D^{\circ}$	1 2 3	64924.4?	
$3s^2 3p(^2P^{\circ})8d$	$8d^{-3}D^{\circ}$	1 2 3	64252.08? 64295.26	43.18	<b>Si II (<math>^2P_{3/2}^{\circ}</math>)</b>	<b>Limit</b>	.....	65747.5 $\pm 0.6$	
$3s^2 3p(^2P^{\circ})10s$	$10s^{-1}P^{\circ}$	1	64351.86		$3s 3p^3$	$3p^3^{-3}S^{\circ}$	1	79664.0	
$3s^2 3p(^2P^{\circ})9d$	$9d^{-3}P^{\circ}$	2 1 0	64616.74?		$3s 3p^2(^4P)4s$	$4s'^{-5}P$	1 2 3	81724.64 81826.16 81976.16	101.52 150.00
$3s^2 3p(^2P^{\circ})9d$	$9d^{-3}D^{\circ}$	1 2 3	64646.78 64661.98	15.20	$3s 3p^2(^4P)3d$	$3d'^{-5}P$	3 2 1	94291.73 94365.59 94413.01	-73.86 -47.42

March 1967.

## Si I Observed Terms

Config. $1s^2 2s^2 2p^6 +$	Observed Terms					
$3s^2 3p^2$	$3p^2^{-1}S$ $3p^2^{-3}P$ $3p^2^{-1}D$ ..					
$3s - 3p^3$	$3p^3^{-5}S^{\circ}$ $3p^3^{-3}S^{\circ}$ $3p^3^{-3}P^{\circ}$ $3p^3^{-3}D^{\circ}$					
	$ns(n \geq 4)$		$np(n \geq 3)$			
$3s^2 3p(^2P^{\circ})nl$	$4-10s^{-3}P^{\circ}$ $4-10s^{-1}P^{\circ}$		$4-7p^{-3}S$ $4-7p^{-3}P$ $4-8p^{-3}D$ $4-8p^{-1}S$ $5-7p^{-1}P$ $4-7p^{-1}D$			
$3s - 3p^2(^4P)nl'$	$4s'^{-5}P$					
	$nd(n \geq 3)$					
$3s^2 3p(^2P^{\circ})nl$	$3-10d^{-3}P^{\circ}$ $3-10d^{-3}D^{\circ}$ $3-8d^{-3}F^{\circ}$ $3-8d^{-1}P^{\circ}$ $3-7d^{-1}D^{\circ}$ $3-8d^{-1}F^{\circ}$					
$3s - 3p^2(^4P)nl'$	$3d'^{-5}P$					

## *jl*—Coupling Notation

	Observed Pairs
	$nf(n \geq 4)$
$3s^2 3p(^2P_{3/2}^{\circ})nl$	$4-6f [2\frac{1}{2}]$ $4-6f [3\frac{1}{2}]$
$3s^2 3p(^2P_{1/2}^{\circ})nl'$	$4-7f' [3\frac{1}{2}]$ $4-7f' [2\frac{1}{2}]$ $4-7f' [4\frac{1}{2}]$ $4-6f' [1\frac{1}{2}]$

## Part B

Multiplet Table  
SILICON  
**Si I (Z = 14)**

I P 8.151 eV Limit  $65747.5 \pm 0.6 \text{ cm}^{-1}$  1520.97 Å (Vac)

Anal A List A March 1967

REFERENCES

- L. J. Radziemski, Jr., K. L. Andrew, V. Kaufman, U. Litzén, J. Opt. Soc. Am. **57**, 336 to 340 (1967). T, C L; W L 1560 Å to 1991 Å
- A L. J. Radziemski, Jr., K. L. Andrew, J. Opt. Soc. Am. **55**, 474 to 491 (1965). I P, T, C L, I; W L 1255 Å to 12270 Å
- B V. Kaufman, L. J. Radziemski, Jr., K. L. Andrew, J. Opt. Soc. Am. **56**, 911 to 915 (1966). T, C L, I; W L 1548 Å to 2103 Å
- C A. G. Shenstone, see Ref. A. C L, (I)
- D M. Wilson, Thesis, unpublished (Nov. 1964). T, C L; W L 1255 Å to 1787 Å
- E U. Litzén, Ark. Fys. **28**, No. 20, 239 to 248 (1964). T, C L, (I); W L 10288 Å to 24854 Å
- F U. Litzén, Ark. Fys. **31**, No. 30, 453 to 459 (1966). T, C L; W L 11984 Å to 15888 Å
- P Predicted wavelength.

New Multiplet Numbers, not inserted between older ones, start with 93 and UV 97.

‡ riae ultime

\* Blend

**Si I**

**Si I**

IA	Ref	Int	E P		J	Multiplet No.	IA	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Air													
16454.53	P		0.03	0.78	2-2	$3p^2 \ ^3P - 3p^2 \ ^1D$	1988.994	B	1000	0.03	6.26	2-2	$3p^2 \ ^3P - 3d \ ^3P^\circ$
16068.30	P		0.01	0.78	1-2	0.01 F	1980.618	B	300	0.01	6.27	1-1	UV 7
15871.58	P		0.00	0.78	0-2		1986.364	A	500	0.03	6.27	2-1	
							1979.206	B	400	0.01	6.27	1-0	
6589.611	P		0.03	1.91	2-0	$3p^2 \ ^3P - 3p^2 \ ^1S$	1983.232	B	300	0.01	6.26	1-2	
6526.782	P		0.01	1.91	1-0	1 F	1977.597	B	400	0.00	6.27	0-1	
3020.004	A	75	0.03	4.13	2-2	$3p^2 \ ^3P - 3p^3 \ ^5S^\circ$	1881.854	B	30	0.03	6.62	2-3	$3p^2 \ ^3P - 3d \ ^1F^\circ$
3006.739	A	50	0.01	4.13	1-2	0.01							UV 8
2516.112‡	A	500	0.03	4.95	2-2	$3p^2 \ ^3P - 4s \ ^3P^\circ$							
2519.202	A	350	0.01	4.93	1-1	UV 1	1880.966	B	5	0.03	6.62	2-1	$3p^2 \ ^3P - 3d \ ^1P^\circ$
2528.509	A	450	0.03	4.93	2-1		1875.813	B	30	0.01	6.62	1-1	UV 9
2524.108	A	425	0.01	4.92	1-0		1873.104	B	25	0.00	6.62	0-1	
2506.897	A	425	0.01	4.95	1-2								
2514.316	A	375	0.00	4.93	0-1		1850.672	B	400	0.03	6.73	2-3	$3p^2 \ ^3P - 3d \ ^3D^\circ$
							1847.473	B	300	0.01	6.72	1-2	UV 10
2452.118	A	70	0.03	5.08	2-1	$3p^2 \ ^3P - 4s \ ^1P^\circ$	1845.520	B	200	0.00	6.72	0-1	
2443.364	A	65	0.01	5.08	1-1	UV 2	1852.472	B	250	0.03	6.72	2-2	
2438.767	A	65	0.00	5.08	0-1		1848.150	B	200	0.01	6.72	1-1	
							1853.152	B	35	0.03	6.72	2-1	
2216.669	A	120	0.03	5.62	2-3	$3p^2 \ ^3P - 3p^3 \ ^3D^\circ$							
2210.894	A	115	0.01	5.62	1-2	UV 3							
2207.978	A	110	0.00	5.61	0-1		1841.449	B	400	0.03	6.76	2-2	$3p^2 \ ^3P - 5s \ ^3P^\circ$
2218.057	A	120	0.03	5.62	2-2		1843.770	B	200	0.01	6.73	1-1	UV 11
2211.744	A	110	0.01	5.61	1-1		1848.748	B	250	0.03	6.73	2-1	
2218.915	A	50	0.03	5.61	2-1		1846.112	B	200	0.01	6.73	1-0	
							1836.509	B	200	0.01	6.76	1-2	
2121.194	A	10	0.03	5.87	2-2	$3p^2 \ ^3P - 3d \ ^1D^\circ$	1841.152	B	125	0.00	6.73	0-1	
2114.631	C	(30)	0.01	5.87	1-2	UV 4							
2010.993	B	45	0.03	6.19	2-3	$3p^2 \ ^3P - 3d \ ^3F^\circ$	1829.897	B	10	0.03	6.80	2-1	$3p^2 \ ^3P - 5s \ ^1P^\circ$
2008.443	B	45	0.01	6.18	1-2	UV 6	1825.021	B	1	0.01	6.80	1-1	UV 12
2014.356	B	3	0.03	6.18	2-2		1822.455	B	30	0.00	6.80	0-1	

Multiplet Table

## Si I—Continued

## Si I—Continued

IA	Ref	Int	EP		J	Multiplet No.	IA	Ref	Int	EP		J	Multiplet No.
			Low	High						Low	High		
Vac													
1776.824	B	150	0.03	7.01	2-2	$3p^2 \ ^3P - 4d \ ^1D^\circ$	1622.881	B	90	0.03	7.67	2-2	$3p^2 \ ^3P - 5d \ ^3P^\circ$
1772.226	B	12	0.01	7.01	1-2	UV 13	1616.579	B	70	0.01	7.68	1-1	UV 30
1770.922	B	300	0.03	7.03	2-2	$3p^2 \ ^3P - 3p^3 \ ^3P^\circ$	1615.949	B	50	0.01	7.68	2-1	
1766.063	B	100	0.01	7.03	1-1	UV 14	1619.046	B	8	0.01	7.67	1-2	
1770.630	B	125	0.03	7.03	2-1		1614.567	B	30	0.00	7.68	0-1	
1765.030	B	90	0.01	7.03	1-0		1621.838	B	2	0.03	7.67	2-1	$3p^2 \ ^3P - 7s \ ^1P^\circ$
1766.354	B	50	0.01	7.03	1-2		1618.006	B	8	0.01	7.67	1-1	UV 31
1763.661	B	80	0.00	7.03	0-1		1615.99	D	(-)	0.00	7.67	0-1	
1747.414	B	40	0.03	7.12	2-3	$3p^2 \ ^3P - 4d \ ^3F^\circ$	1614.630	B	25	0.03	7.71	2-2	$3p^2 \ ^3P - 6d \ ^1D^\circ$
1745.348	B	25	0.01	7.11	1-2	UV 15	1610.82	D	(-)	0.01	7.71	1-2	UV 32
1749.808	B	3	0.03	7.11	2-2		1608.916	B	25	0.03	7.73	2-3	$3p^2 \ ^3P - 6d \ ^3F^\circ$
1707.115	B	8	0.03	7.29	2-1	$3p^2 \ ^3P - 4d \ ^1P^\circ$	1605.837	B	20	0.01	7.73	1-2	UV 33
1702.868	B	70	0.01	7.29	1-1	UV 16	1601.46	P		0.03	7.77	2-1	$3p^2 \ ^3P - 6d \ ^1P^\circ$
1700.635	B	80	0.00	7.29	0-1		*1597.721	B	25	0.01	7.77	1-1	UV 33.01
1704.442	B	100	0.03	7.30	2-3	$3p^2 \ ^3P - 4d \ ^1F^\circ$	1595.755	B	30	0.00	7.77	0-1	
1697.941	B	250	0.03	7.33	2-3	$3p^2 \ ^3P - 4d \ ^3D^\circ$	1597.963	B	60	0.03	7.79	2-3	$3p^2 \ ^3P - 6d \ ^1F^\circ$
1696.206	B	200	0.01	7.32	1-2	UV 18	1590.576	B	15	0.03	7.82	2-2	$3p^2 \ ^3P - 8s \ ^3P^\circ$
1693.293	B	125	0.00	7.32	0-1		*1597.721	B	25	0.03	7.79	2-1	UV 35.01
1700.419	B	90	0.03	7.32	2-2		1594.146	B	3	0.01	7.79	1-0?	
1695.507	B	90	0.01	7.32	1-1		1586.892	B	3	0.01	7.82	1-2	
1699.717	B	10	0.03	7.32	2-1		1592.020	B	20	0.00	7.79	0-1	
1686.818	B	100	0.03	7.38	2-2	$3p^2 \ ^3P - 6s \ ^3P^\circ$	1594.566	B	70	0.03	7.80	2-3	$3p^2 \ ^3P - 6d \ ^3D^\circ$
1689.290	B	60	0.01	7.35	1-1	UV 21	1592.423	B	60	0.01	7.80	1-2	UV 35.02
1693.468	B	60	0.03	7.35	2-1		1589.173	B	15	0.00	7.80	0-1	
1690.788	B	60	0.01	7.34	1-0		1591.123	B	20	0.01	7.80	1-1	
1682.672	B	70	0.01	7.38	1-2		1594.79	D	—	0.03	7.80	2-1	
1687.092	B	20	0.00	7.35	0-1		1594.949	B	70	0.03	7.80	2-2?	$3p^2 \ ^3P - 6d \ ^3P^\circ$
1683.119	B	3	0.03	7.39	2-1	$3p^2 \ ^3P - 6s \ ^1P^\circ$	1586.791	B	20	0.01	7.82	1-1	UV 35.03
1678.992	P	0.01	7.39	1-1			1590.477	B	20	0.03	7.82	2-1	
1676.821	B	15	0.00	7.39	0-1		1586.137	B	15	0.01	7.83	1-0?	
1675.205	B	200	0.03	7.43	2-2	$3p^2 \ ^3P - 4d \ ^3P^\circ$	1591.24	P		0.01	7.80	1-2?	
1668.520	B	70	0.01	7.44	1-1	UV 23	1584.854	B	2	0.00	7.82	0-1	
1672.596	B	80	0.03	7.44	2-1		1589.639	B	7	0.03	7.83	2-1	$3p^2 \ ^3P - 8s \ ^1P^\circ$
1667.629	B	70	0.01	7.44	1-0		1585.958	B	3	0.01	7.83	1-1	UV 37
1671.117	B	40	0.01	7.43	1-2		1584.022	B	8	0.00	7.83	0-1	
1666.376	B	60	0.00	7.44	0-1		1587.761	B	15	0.03	7.84	2-2	$3p^2 \ ^3P - 7d \ ^1D^\circ$
1664.511	B	35	0.03	7.48	2-2	$3p^2 \ ^3P - 5d \ ^1D^\circ$	1584.346	B	12	0.03	7.85	2-3	$3p^2 \ ^3P - 7d \ ^3F^\circ$
1660.476	B	15	0.01	7.48	1-2	UV 24	1580.300	B	12	0.01	7.85	1-2	UV 37.02
1653.376	B	40	0.03	7.53	2-3	$3p^2 \ ^3P - 5d \ ^3F^\circ$	1583.95	D	(-)	0.03	7.85	2-2	
1651.028	B	25	0.01	7.52	1-2	UV 25	1577.044	B	2	0.01	7.87	1-1	
1655.012	C	(1h)	0.03	7.52	2-2		1575.127	B	10	0.00	7.87	0-1	
1633.223	B	45	0.01	7.60	1-1	$3p^2 \ ^3P - 5d \ ^1P^\circ$	1580.68	D	(-)	0.03	7.87	2-1	$3p^2 \ ^3P - 7d \ ^1P^\circ$
1631.168	B	70	0.00	7.60	0-1	UV 26	1577.044	B	2	0.01	7.87	1-1	UV 37.03
1629.946	B	100	0.03	7.63	2-3	$3p^2 \ ^3P - 5d \ ^3D^\circ$	1571.323	B	1	0.03	7.92	2-2	$3p^2 \ ^3P - 9s \ ^3P^\circ$
1629.438	B	100	0.01	7.62	1-2	UV 27	1574.63	P		0.01	7.88	1-1	UV 37.04
1625.704	B	70	0.00	7.63	0-1		1578.25	D	(-)	0.03	7.88	2-1	
1633.326	B	40	0.03	7.62	2-2		1574.746	B	1	0.01	7.88	1-0?	
1627.745	B	30	0.01	7.63	1-1		1567.726	B	8	0.01	7.92	1-2	
1631.62	P		0.03	7.63	2-1		1572.717	B	2	0.00	7.88	0-1	
1633.983	B	90	0.03	7.62	2-3	$3p^2 \ ^3P - 5d \ ^1F^\circ$	1576.829	B	12	0.03	7.89	2-3	$3p^2 \ ^3P - 7d \ ^1F^\circ$
1623.368	B	8	0.03	7.66	2-2	UV 29	1573.884	B	25	0.03	7.91	2-3	$3p^2 \ ^3P - 7d \ ^3D^\circ$
1625.531	B	35	0.01	7.64	1-1		1571.406	B	10	0.01	7.90	1-2	UV 40
1629.403	B	20	0.03	7.64	2-1		1568.618	B	3	0.00	7.90	0-1	
1627.050	B	20	0.01	7.63	1-0		1570.518	B	3	0.01	7.90	1-1	
1619.526	B	15	0.01	7.66	1-2		1574.128	B	1	0.03	7.90	2-1	

Multiplet Table

## Si I—Continued

## Si I—Continued

IA	Ref	Int	E P		J	Multiplet No.	IA	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac													
1574.844	B	30	0.03	7.90	2-2	$3p^2 \ ^3P - 7d \ ^3P^\circ$	2291.034	A	35	0.78	6.19	2-3	$3p^2 \ ^1D - 3d \ ^3F^\circ$
1570.028	B	2	0.01	7.91	1-1	UV 40.01	2295.401	A	10	0.78	6.18	2-2	UV 46
1573.635	B	10	0.03	7.91	2-1		2261.693	A	5	0.78	6.26	2-2	$3p^2 \ ^1D - 3d \ ^3P^\circ$
1568.196	B	10	0.01	7.92	1-0		2258.292	P		0.78	6.27	2-1	UV 47
1570.810	B	1	0.03	7.92	2-1	$3p^2 \ ^3P - 9s \ ^1P^\circ$	2124.122	A	100	0.78	6.62	2-3	$3p^2 \ ^1D - 3d \ ^1F^\circ$
1567.21	D	(-)	0.01	7.92	1-1	UV 41							UV 48
1565.32	D	(-)	0.00	7.92	0-1								
1569.318	B	8	0.03	7.93	2-3	$3p^2 \ ^3P - 8d \ ^3F^\circ$	2122.994	A	15	0.78	6.62	2-1	$3p^2 \ ^1D - 3d \ ^3P^\circ$
1564.614	B	8	0.01	7.93	1-2	UV 41.01							UV 49
1562.053	B	1	0.00	7.94	0-1	$3p^2 \ ^3P - 8d \ ^1P^\circ?$	2084.463	B	50	0.78	6.73	2-3	$3p^2 \ ^1D - 3d \ ^3D^\circ$
						UV 41.02	2086.745	C	(1)	0.78	6.72	2-2	
							2087.612	B	1	0.78	6.72	2-1	
1559.00	D	(-)	0.03	7.98	2-2	$3p^2 \ ^3P - 10s \ ^3P^\circ?$	2072.764	P		0.78	6.76	2-2	$3p^2 \ ^1D - 5s \ ^3P^\circ$
1562.28	D	(-)	0.01	7.95	1-1	UV 41.03	2082.021	B	60	0.78	6.73	2-1	UV 51
1565.84	D	(-Al?)	0.03	7.95	2-1								
1555.516	B	1	0.01	7.98	1-2		2058.132	B	600	0.78	6.80	2-1	$3p^2 \ ^1D - 5s \ ^1P^\circ$
1560.39	D	(-)	0.00	7.95	0-1								UV 52
1563.364	B	1	0.03	7.96	2-3	$3p^2 \ ^3P - 8d \ ^1F^\circ$	Vac						
						UV 41.04	1991.852	B	50	0.78	7.01	2-2	$3p^2 \ ^1D - 4d \ ^1D^\circ$
1562.006	B	4	0.03	7.96	2-2	$3p^2 \ ^3P - 8d \ ^3P^\circ?$							
1556.527	B	1	0.01	7.97	1-0	UV 41.05	1984.439	B	20	0.78	7.03	2-2	$3p^2 \ ^1D - 3p^3 \ ^3P^\circ$
							1984.069	B	3	0.78	7.03	2-1	UV 53.01
1560.742	B	8	0.03	7.97	2-3	$3p^2 \ ^3P - 8d \ ^3D^\circ$							
1558.240	B	2	0.01	7.97	1-2?	UV 41.06	1954.968	B	50	0.78	7.12	2-3	$3p^2 \ ^1D - 4d \ ^3F^\circ$
1561.81	D	(10r)	0.03	7.97	2-2?		1957.965	B	1	0.78	7.11	2-2	UV 55
1559.364	B	2	0.03	7.98	2-1	$3p^2 \ ^3P - 10s \ ^1P^\circ$	1904.666	B	40	0.78	7.29	2-1	$3p^2 \ ^1D - 4d \ ^1P^\circ$
						UV 41.07							UV 56
1552.950	B	2	0.03	8.01	2-2	$3p^2 \ ^3P - 9d \ ^3P^\circ?$	1901.337	B	400	0.78	7.30	2-3	$3p^2 \ ^1D - 4d \ ^1F^\circ$
						UV 41.08							UV 57
1551.860	B	2	0.03	8.02	2-3	$3p^2 \ ^3P - 9d \ ^3D^\circ?$	1893.252	B	175	0.78	7.33	2-3	$3p^2 \ ^1D - 4d \ ^3D^\circ$
1548.715	B	2	0.01	8.01	1-2	UV 41.09	1896.339	B	1	0.78	7.32	2-2	
1552.209	B	1	0.03	8.01	2-2		1895.461	B	1	0.78	7.32	2-1	
1546.56	C	(1r)	0.03	8.04	2-2	$3p^2 \ ^3P - 10d \ ^3P^\circ?$	1879.434	P		0.78	7.38	2-2	$3p^2 \ ^1D - 6s \ ^3P^\circ$
						UV 41.10	1887.693	B	45	0.78	7.35	2-1	UV 61
1545.56	C	(1r)	0.03	8.05	2-3	$3p^2 \ ^3P - 10d \ ^3D^\circ?$	1874.842	B	175	0.78	7.39	2-1	$3p^2 \ ^1D - 6s \ ^1P^\circ$
						UV 41.11							UV 62
1258.80	C	(50)	0.03	9.88	2-1	$3p^2 \ ^3P - 3p^3 \ ^3S^\circ$	1865.028	B	2	0.78	7.43	2-2	$3p^2 \ ^1D - 4d \ ^3P^\circ$
1256.49	C	(40)	0.01	9.88	1-1	UV 41.12	1861.795	B	2	0.78	7.44	2-1	UV 63
1255.28	C	(10)	0.00	9.88	0-1		1851.782	B	70	0.78	7.48	2-2	$3p^2 \ ^1D - 5d \ ^1D^\circ$
													UV 64
Air													
10991.414	P		0.78	1.91	2-0	$3p^2 \ ^1D - 3p^2 \ ^1S$	1838.011	B	40	0.78	7.53	2-3	$3p^2 \ ^1D - 5d \ ^3F^\circ$
						2F	1840.042	B	8	0.78	7.52	2-2	UV 65
2970.355	A	55	0.78	4.95	2-2	$3p^2 \ ^1D - 4s \ ^3P^\circ$	1817.956	B	10	0.78	7.60	2-1	$3p^2 \ ^1D - 5d \ ^1P^\circ$
2987.645	A	150	0.78	4.93	2-1	1	1814.079	B	250	0.78	7.62	2-3	$3p^2 \ ^1D - 5d \ ^1F^\circ$
2881.579	A	1000	0.78	5.08	2-1	$3p^2 \ ^1D - 4s \ ^1P^\circ$	1809.104	B	100	0.78	7.63	2-3	$3p^2 \ ^1D - 5d \ ^3D^\circ$
						UV 43	1813.27	P	(1h)	0.78	7.62	2-2	UV 68.01
2561.823	P		0.78	5.62	2-3	$3p^2 \ ^1D - 3p^3 \ ^3D^\circ$	1801.000	P					
2563.679	A	30	0.78	5.62	2-2	UV 44	1808.429	B	20	0.78	7.66	2-2	$3p^2 \ ^1D - 7s \ ^3P^\circ$
2564.824	A	20	0.78	5.61	2-1					0.78	7.64	2-1	UV 69
2435.154	A	300	0.78	5.87	2-2	$3p^2 \ ^1D - 3d \ ^1D^\circ$	1800.404	B	1	0.78	7.67	2-2	$3p^2 \ ^1D - 5d \ ^3P^\circ$
						UV 45	1797.356	B	6	0.78	7.68	2-1	UV 70

Multiplet Table

## Si I—Continued

## Si I—Continued

IA	Ref	Int	EP		J	Multiplet No.	IA	Ref	Int	EP		J	Multiplet No.
			Low	High						Low	High		
Vac 1799.118	B	30	0.78	7.67	2-1	$3p^2 \ ^1D - 7s \ ^1P^o$ UV 71	2842.334	A	15	1.91	6.27	0-1	$3p^2 \ ^1S - 3d \ ^3P^o$ UV 82
1790.254	B	25	0.78	7.71	2-2	$3p^2 \ ^1D - 6d \ ^1D^o$ UV 72	2631.282	A	190	1.91	6.62	0-1	$3p^2 \ ^1S - 3d \ ^1P^o$ UV 83
1783.232	B	25	0.78	7.73	2-3	$3p^2 \ ^1D - 6d \ ^3F^o$ UV 73	2577.151	A	45	1.91	6.72	0-1	$3p^2 \ ^1S - 3d \ ^3D^o$ UV 84
1784.088	B	8	0.78	7.73	2-2								
1774.08	P		0.78	7.77	2-1	$3p^2 \ ^1D - 6d \ ^1P^o$ UV 73.01	2568.641	A	85	1.91	6.73	0-1	$3p^2 \ ^1S - 5s \ ^3P^o$ UV 85
1769.785	B	70	0.78	7.79	2-3	$3p^2 \ ^1D - 6d \ ^1F^o$ UV 75	2532.381	A	110	1.91	6.80	0-1	$3p^2 \ ^1S - 5s \ ^1P^o$ UV 86
1769.461	B	2	0.78	7.79	2-1	$3p^2 \ ^1D - 8s \ ^3P^o$ UV 75.01	2420.24	A	5	1.91	7.03	0-1	$3p^2 \ ^1S - 3p^3 \ ^3P^o$ UV 86.01
1765.622	B	50	0.78	7.80	2-3	$3p^2 \ ^1D - 6d \ ^3D^o$ UV 76	2303.058	A	55	1.91	7.29	0-1	$3p^2 \ ^1S - 4d \ ^1P^o$ UV 87
1767.54	P		0.78	7.80	2-2								
1765.945	B	8	0.78	7.80	2-1		2289.607	A	20	1.91	7.32	0-1	$3p^2 \ ^1S - 4d \ ^3D^o$ UV 88
1759.583	B	10	0.78	7.83	2-1	$3p^2 \ ^1D - 8s \ ^1P^o$ UV 77	2278.281	A	10	1.91	7.35	0-1	$3p^2 \ ^1S - 6s \ ^3P^o$ UV 89
1757.283	B	3	0.78	7.84	2-2	$3p^2 \ ^1D - 7d \ ^1D^o$ UV 77.01	2259.587	A	10	1.91	7.39	0-1	$3p^2 \ ^1S - 6s \ ^1P^o$ UV 90
1753.101	B	15	0.78	7.85	2-3	$3p^2 \ ^1D - 7d \ ^3F^o$ UV 77.02	2240.649	P		1.91	7.44	0-1	$3p^2 \ ^1S - 4d \ ^3P^o$ UV 90.01
1752.634	B	3	0.78	7.85	2-2								
1745.647	B	1	0.78	7.88	2-1	$3p^2 \ ^1D - 9s \ ^3P^o$ UV 77.03	2177.432	A	10	1.91	7.60	0-1	$3p^2 \ ^1S - 5d \ ^1P^o$ UV 91
1743.894	B	20	0.78	7.89	2-3	$3p^2 \ ^1D - 7d \ ^1F^o$ UV 79	2167.700	A	5	1.91	7.63	0-1	$3p^2 \ ^1S - 5d \ ^2D^o$ UV 92
1740.299	B	20	0.78	7.91	2-3	$3p^2 \ ^1D - 7d \ ^3D^o$ UV 80	2163.773	A	7	1.91	7.64	0-1	$3p^2 \ ^1S - 7s \ ^3P^o$ UV 93
1736.538	B	3	0.78	7.92	2-1	$3p^2 \ ^1D - 9s \ ^1P^o$ UV 81	2147.911	C	(50h)	1.91	7.68	0-1	$3p^2 \ ^1S - 5d \ ^3P^o$ UV 94
1734.718	B	8	0.78	7.93	2-3	$3p^2 \ ^1D - 8d \ ^3F^o$ UV 81.01	2150.46	A	2	1.91	7.67	0-1	$3p^2 \ ^1S - 7s \ ^1P^o$ UV 95
1733.346	B	1	0.78	7.93	2-2								
1727.444	B	2	0.78	7.96	2-3	$3p^2 \ ^1D - 8d \ ^1F^o$ UV 81.02	2114.75	P		1.91	7.77	0-1	$3p^2 \ ^1S - 6d \ ^1P^o$ UV 95.01
1724.242	B	6	0.78	7.97	2-3	$3p^2 \ ^1D - 8d \ ^3D^o$ UV 81.03	2108.20	P		1.91	7.79	0-1	$3p^2 \ ^1S - 8s \ ^3P^o$ UV 95.02
1722.562	B	4	0.78	7.98	2-1	$3p^2 \ ^1D - 10s \ ^1P^o$ UV 81.04	2103.205	A	1	1.91	7.80	0-1	$3p^2 \ ^1S - 6d \ ^3D^o$ UV 95.03
1713.412	D	(-)	0.78	8.02	2-3	$3p^2 \ ^1D - 9d \ ^3D^o$ UV 81.05	2095.64	P		1.91	7.82	0-1	$3p^2 \ ^1S - 6d \ ^3P^o$ UV 95.04
1713.85	D	(-)	0.78	8.01	2-2								
Air 4102.936	A	70	1.91	4.93	0-1	$3p^2 \ ^1S - 4s \ ^3P^o$ 2	2094.21	C	(10h)	1.91	7.83	0-1	$3p^2 \ ^1S - 8s \ ^1P^o$ UV 96
3905.523	A	300	1.91	5.08	0-1	$3p^2 \ ^1S - 4s \ ^1P^o$ 3	2078.66	P		1.91	7.87	0-1	$3p^2 \ ^1S - 7d \ ^1P^o$ UV 97
3345.555	P		1.91	5.61	0-1	$3p^2 \ ^1S - 3p^3 \ ^3D^o$ 3.01	2074.46	P		1.91	7.88	0-1	$3p^2 \ ^1S - 9s \ ^3P^o$ UV 98
							2067.39	C	(3H)	1.91	7.90	0-1	$3p^2 \ ^1S - 7d \ ^3D^o?$ UV 99

Multiplet Table

## Si I—Continued

## Si I—Continued

IA	Ref	Int	EP		J	Multiplet No.	IA	Ref	Int	EP		J	Multiplet No.
			Low	High						Low	High		
Air 2066.41	C	(0h)	1.91	7.91	0-1	$3p^2 \ ^1S - 7d \ ^3P^\circ$ UV 100	Air 5602.875 5542.378	A P	20	4.95 4.93	7.17 7.17	2-2 1-2	$4s \ ^3P^\circ - 5p \ ^1D$ 11.01
2061.64	C	(1H)	1.91	7.92	0-1	$3p^2 \ ^1S - 9s \ ^1P^\circ$ UV 101	5388.938	P		4.93	7.23	1-0	$4s \ ^3P^\circ - 5p \ ^1S$ 11.02
2041.93	P		1.91	7.98	0-1	$3p^2 \ ^1S - 10s \ ^1P^\circ$ UV 102	5145.02 5124.86	A P	2	4.93 4.92	7.34 7.34	1-2 0-1	$4s \ ^3P^\circ - 4f' [1\frac{1}{2}]$ 11.03
2054.836	B	(50)	4.13	10.16	2-3	$3p^3 \ ^5S^\circ - 4s' \ ^5P$ UV 103	4818.06	A	7	4.95	7.53	2-3	$4s \ ^3P^\circ - 6p \ ^3D$ 11.04
2061.19	C	(40)	4.13	10.14	2-2		4821.167	A	15	4.93	7.50	1-2	
2065.52	C	(30)	4.13	10.13	2-1		4805.440	A	20	4.92	7.50	0-1	
Vac 1640.267	B	(20)	4.13	11.69	2-3	$3p^3 \ ^5S^\circ - 3d' \ ^5P$ UV 104	4866.881	A	7	4.95	7.50	2-2	
1638.282	B	(10)	4.13	11.70	2-2		4823.31	A	10	4.93	7.50	1-1	
1637.011	B	(5)	4.13	11.71	2-1		4869.074	P		4.95	7.50	2-1	
Air 13640.68	P		4.95	5.86	2-1	$4s \ ^3P^\circ - 4p \ ^1P$ 3.02	4755.276	A	25	4.93	7.54	1-2	
13287.58	E	9	4.93	5.86	1-1		4782.990	A	50	4.95	7.55	2-1	$4s \ ^3P^\circ - 6p \ ^3S$ 11.06
13152.74	P		4.92	5.86	0-1		4738.832	P		4.93	7.55	1-1	
12031.507	F	(440)	4.95	5.98	2-3	$4s \ ^3P^\circ - 4p \ ^3D$ 4	4721.571	P	13	4.92	7.55	0-1	
11984.187	F	(370)	4.93	5.96	1-2		4758.972	A					
11991.565	F	(220)	4.92	5.95	0-1		4715.257	P					
12270.699	F	(120)	4.95	5.96	2-2		4449.93	A	5	4.95	7.74	2-3	$4s \ ^3P^\circ - 7p \ ^3D$ 11.08
12103.544	F	(150)	4.93	5.95	1-1		4448.79	P		4.93	7.72	1-2?	
12395.82	E	(6)	4.95	5.95	2-1		4434.69	A	10	4.92	7.71	0-1	
10827.091	A	140	4.95	6.10	2-2	$4s \ ^3P^\circ - 4p \ ^3P$ 5	4430.470	A	10	4.95	7.75	2-2	$4s \ ^3P^\circ - 7p \ ^3P$ 11.09
10749.384	A	60	4.93	6.08	1-1		4405.96	A	5H	4.93	7.74	1-1	
10979.308	A	80	4.95	6.08	2-1		4444.12	P		4.95	7.74	2-1	
10786.856	A	80	4.93	6.08	1-0		4431.68	A	5	4.93	7.73	1-0	
10603.431	A	120	4.93	6.10	1-2		4392.59	A	10	4.93	7.75	1-2	
10660.975	A	120	4.92	6.08	0-1		4391.05	A	5H	4.92	7.74	0-1	
10585.141	A	120	4.95	6.12	2-1	$4s \ ^3P^\circ - 4p \ ^3S$ 6	4425.49	A	10	4.95	7.75	2-1	$4s \ ^3P^\circ - 7p \ ^3S$ 11.10
10371.269	A	30	4.93	6.12	1-1		4387.65	P		4.93	7.75	1-1	
10288.942	A	10	4.92	6.12	0-1		4372.85	P		4.92	7.75	0-1	
9768.35	A	6	4.95	6.22	2-2	$4s \ ^3P^\circ - 4p \ ^1D$ 7	4415.50	A	5H	4.95	7.76	2-2	$4s \ ^3P^\circ - 7p \ ^1D$ 11.11
9585.92	A	10	4.93	6.22	1-2								
8435.24	A	8	4.93	6.40	1-0	$4s \ ^3P^\circ - 4p \ ^1S$ 8							
5941.758	P		4.95	7.04	2-1	$4s \ ^3P^\circ - 5p \ ^1P$ 8.01	15888.39	E	(190)	5.08	5.86	1-1	$4s \ ^1P^\circ - 4p \ ^1P$ 11.12
5873.764	A	40	4.93	7.04	1-1								
5847.268	P		4.92	7.04	0-1								
5797.859	A	100	4.95	7.09	2-3	$4s \ ^3P^\circ - 5p \ ^3D$ 9	14059.99	P		5.08	5.96	1-2	$4s \ ^1P^\circ - 4p \ ^3D$ 11.13
5793.071	A	90	4.93	7.07	1-2		14224.54	E	(6)	5.08	5.95	1-1	
5780.384	A	70	4.92	7.06	0-1		12196.64	P		5.08	6.10	1-2	$4s \ ^1P^\circ - 4p \ ^3P$ 11.14
5859.201	P		4.95	7.07	2-2		12390.16	E	(4)	5.08	6.08	1-1	
5806.276	P		4.93	7.06	1-1		12439.96	P		5.08	6.08	1-0	
5872.708	P		4.95	7.06	2-1								
5708.397	A	160	4.95	7.12	2-2	$4s \ ^3P^\circ - 5p \ ^3P$ 10	11890.48	P		5.08	6.12	1-1	$4s \ ^1P^\circ - 4p \ ^3S$ 12
5690.425	A	100	4.93	7.11	1-1								
5754.220	A	45	4.95	7.11	2-1		10869.541	A	130	5.08	6.22	1-2	$4s \ ^1P^\circ - 4p \ ^1D$ 13
5701.105	A	90	4.93	7.10	1-0								
5645.611	A	90	4.93	7.12	1-2		9413.506	A	100	5.08	6.40	1-0	$4s \ ^1P^\circ - 4p \ ^1S$ 14
5665.554	A	80	4.92	7.11	0-1								
5684.484	A	120	4.95	7.13	2-1	$4s \ ^3P^\circ - 5p \ ^3S$ 11	6331.954	A	45	5.08	7.04	1-1	$4s \ ^1P^\circ - 5p \ ^1P$ 14.01
5622.221	A	30	4.93	7.13	1-1								
5597.941	P		4.92	7.13	0-1								

Multiplet Table

## Si I—Continued

## Si I—Continued

IA	Ref	Int	E P		J	Multiplet No.	IA	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Air 6238.287 6253.60	A A	40 15	5.08 5.08	7.07 7.06	1-2 1-1	4s $^1\text{P}^\circ - 5p$ ${}^3\text{D}$ 14.02	Air 4551.80	A	7	5.08 5.08	7.81 7.84	1-2 1-2	4s $^1\text{P}^\circ - 6f'$ $[2\frac{1}{2}]$ 17.19
6067.624 6119.417 6131.769	A P P	20	5.08 5.08 5.08	7.12 7.11 7.10	1-2 1-1 1-0	4s $^1\text{P}^\circ - 5p$ ${}^3\text{P}$ 15	4496.43	A	5H	5.08 5.08	7.84 7.89	1-2 1-0	4s $^1\text{P}^\circ - 8p$ ${}^3\text{D}?$ 17.20
6040.611	P		5.08	7.13	1-1	4s $^1\text{P}^\circ - 5p$ ${}^3\text{S}$ 15.01	4418.31	A	5H	5.08	7.89	1-0	4s $^1\text{P}^\circ - 8p$ ${}^1\text{S}?$ 17.21
5948.545	A	200	5.08	7.17	1-2	4s $^1\text{P}^\circ - 5p$ ${}^1\text{D}$ 16	25854.38 26539.28 26644.44	E P P	(6)	5.62 5.62 5.61	6.10 6.08 6.08	3-2 2-1 1-0	$3p^3$ ${}^3\text{D}^\circ - 4p$ ${}^3\text{P}$ 17.22
5772.145	A	70	5.08	7.23	1-0	4s $^1\text{P}^\circ - 5p$ ${}^1\text{S}$ 17	8703.256 8690.062	P P		5.62 5.61	7.04 7.04	2-1 1-1	$3p^3$ ${}^3\text{D}^\circ - 5p$ ${}^1\text{P}$ 17.23
5621.607	A	15	5.08	7.29	1-2	4s $^1\text{P}^\circ - 4f$ $[2\frac{1}{2}]$ 17.01	8417.88 8527.26	A A	7 1	5.62 5.62	7.09 7.07	3-3 2-2	$3p^3$ ${}^3\text{D}^\circ - 5p$ ${}^3\text{D}$ 18
5517.535	A	35	5.08	7.33	1-2	4s $^1\text{P}^\circ - 4f'$ $[2\frac{1}{2}]$ 17.02	8543.151 8547.84 8555.90	P A A	3 1	5.61 5.62 5.62	7.06 7.07 7.06	1-1 3-2 2-1	
5493.23 5493.41	A P	40	5.08 5.08	7.34 7.34	1-2 1-1	4s $^1\text{P}^\circ - 4f'$ $[1\frac{1}{2}]$ 17.03	8397.949 8514.599	P P		5.62 5.61	7.09 7.07	2-3 1-2	
5156.023	A	8	5.08	7.49	1-1	4s $^1\text{P}^\circ - 6p$ ${}^1\text{P}?$ 17.04	8230.642 8306.710 8317.39	A A A	35 25 15	5.62 5.62 5.61	7.12 7.11 7.10	3-2 2-1 1-0	$3p^3$ ${}^3\text{D}^\circ - 5p$ ${}^3\text{P}$ 19
5125.598 5128.031	A A	10 10	5.08 5.08	7.50 7.50	1-2 1-1	4s $^1\text{P}^\circ - 6p$ ${}^3\text{D}$ 17.05	8211.63 8294.675 8199.811	A A P	7 13	5.62 5.61 5.61	7.12 7.11 7.12	2-2 1-1 1-2	
5042.97 5070.951 5092.89	A P P	3	5.08 5.08 5.08	7.54 7.53 7.52	1-2 1-1 1-0	4s $^1\text{P}^\circ - 6p$ ${}^3\text{P}$ 17.06	8162.170 8150.54	A A	15 7	5.62 5.61	7.13 7.13	2-1 1-1	$3p^3$ ${}^3\text{D}^\circ - 5p$ ${}^3\text{S}$ 20
5032.640	P		5.08	7.55	1-1	4s $^1\text{P}^\circ - 6p$ ${}^3\text{S}$ 17.07	8013.042 7994.959 7983.823	P P P		5.62 5.62 5.61	7.17 7.17 7.17	3-2 2-2 1-2	$3p^3$ ${}^3\text{D}^\circ - 5p$ ${}^1\text{D}$ 21
5006.061	A	40	5.08	7.56	1-2	4s $^1\text{P}^\circ - 6p$ ${}^1\text{D}$ 17.08	7669.265	P		5.61	7.23	1-0	$3p^3$ ${}^3\text{D}^\circ - 5p$ ${}^1\text{S}$ 21.01
4947.607	A	30	5.08	7.59	1-0	4s $^1\text{P}^\circ - 6p$ ${}^1\text{S}$ 17.09	7431.505 7430.906	P P		5.62 5.62	7.29 7.29	3-3 3-2	$3p^3$ ${}^3\text{D}^\circ - 4f$ $[2\frac{1}{2}]$ 21.02
4921.72	A	1	5.08	7.60	1-2	4s $^1\text{P}^\circ - 5f$ $[2\frac{1}{2}]$ 17.10	7415.946 7415.35 7405.774	A A A	275 40 375	5.62 5.62 5.61	7.29 7.29 7.29	2-3 2-2 1-2	
4851.540	A	13	5.08	7.64	1-2	4s $^1\text{P}^\circ - 5f'$ $[2\frac{1}{2}]$ 17.11	7423.497 7424.60 7409.082	A A A	425 85 200	5.62 5.62 5.62	7.29 7.29 7.29	3-4 3-3 2-3	$3p^3$ ${}^3\text{D}^\circ - 4f$ $[3\frac{1}{2}]$ 21.03
4839.861 4839.98	A P	11	5.08 5.08	7.64 7.64	1-2 1-1	4s $^1\text{P}^\circ - 5f'$ $[1\frac{1}{2}]$ 17.12	7289.173 7290.26	A A	400 55	5.62 5.62	7.32 7.32	3-4 3-3	$3p^3$ ${}^3\text{D}^\circ - 4f'$ $[3\frac{1}{2}]$ 21.04
4726.84	A	5	5.08	7.70	1-1	4s $^1\text{P}^\circ - 7p$ ${}^1\text{P}?$ 17.13	7275.294	A	160	5.62	7.32	2-3	
4706.76 4707.98	A A	8 4	5.08 5.08	7.72 7.71	1-2? 1-1	4s $^1\text{P}^\circ - 7p$ ${}^3\text{D}$ 17.14	7250.625 7250.14 7235.82	A A A	180 25 60	5.62 5.62 5.62	7.33 7.33 7.33	3-3 3-2 2-3	$3p^3$ ${}^3\text{D}^\circ - 4f'$ $[2\frac{1}{2}]$ 21.05
4658.82 4643.86	A P	5	5.08	7.74	1-1	4s $^1\text{P}^\circ - 7p$ ${}^3\text{P}$ 17.15	7226.206	A	100	5.61	7.33	1-2	
4638.38	P		5.08	7.75	1-1	4s $^1\text{P}^\circ - 7p$ ${}^3\text{S}$ 17.16	7208.21 7193.58 7193.90	A A A	25 65 30	5.62 5.62 5.62	7.34 7.34 7.34	3-2 2-2 2-1	$3p^3$ ${}^3\text{D}^\circ - 4f'$ $[1\frac{1}{2}]$ 21.06
4627.383	A	18	5.08	7.76	1-2	4s $^1\text{P}^\circ - 7p$ ${}^1\text{D}$ 17.17	7184.57 7184.89	A	70	5.61	7.34	1-1	
4601.26	A	5	5.08	7.78	1-0	4s $^1\text{P}^\circ - 7p$ ${}^1\text{S}$ 17.18	6499.02 6575.950 6572.411	P P P		5.62 5.62 5.61	7.53 7.50 7.50	3-3 2-2 1-1	$3p^3$ ${}^3\text{D}^\circ - 6p$ ${}^3\text{D}$ 21.07

Multiplet Table

## Si I—Continued

## Si I—Continued

IA	Ref	Int	EP			Multiplet No.	IA	Ref	Int	EP		J	Multiplet No.
			Low	High						Low	High		
Air													
6452.29	A	20	5.62	7.54	3-2	$3p^3 \ ^3D^o - 6p \ ^3P$ 21.08	10843.854	A	60	5.86	7.01	1-2	$4p \ ^1P - 4d \ ^1D^o$ 31
6486.34	A	2	5.62	7.53	2-1								
6514.85	A	2	5.61	7.52	1-0								
6478.87	A	1H	5.61	7.53	1-1								
6423.80	A	2	5.62	7.55	2-1	$3p^3 \ ^3D^o - 6p \ ^3S$ 21.09	10627.647	A	20	5.86	7.03	1-2	$4p \ ^1P - 3p^3 \ ^3P^o$ 32
6255.47	A	13	5.62	7.60	3-3	$3p^3 \ ^3D^o - 5f [2\frac{1}{2}]$ 21.10	10617.10	P		5.86	7.03	1-1	
6255.139	P		5.62	7.60	3-2		10579.87	P		5.86	7.03	1-0	
6244.468	A	125	5.62	7.60	2-3								
6244.114	P		5.62	7.60	2-2								
6237.320	A	160	5.61	7.60	1-2								
6254.188	A	180	5.62	7.60	3-4	$3p^3 \ ^3D^o - 5f [3\frac{1}{2}]$ 21.11	9909.819	P		5.86	7.11	1-2	$4p \ ^1P - 4d \ ^3D^o$ 32.01
6254.85	A	20	5.62	7.60	3-3		8680.079	A	11	5.86	7.29	1-1	$4p \ ^1P - 4d \ ^1P^o$ 32.02
6243.813	A	125	5.62	7.60	2-3								
6155.134	A	160	5.62	7.63	3-4	$3p^3 \ ^3D^o - 5f' [3\frac{1}{2}]$ 21.12	8509.65	P		5.86	7.32	1-2	$4p \ ^1P - 6s \ ^3P^o$ 33
6155.70	A	20	5.62	7.63	3-3		8492.078	A	15	5.86	7.32	1-1	
6145.015	A	100	5.62	7.63	2-3								
6142.487	A	100	5.62	7.64	3-3	$3p^3 \ ^3D^o - 5f' [2\frac{1}{2}]$ 21.13	8179.518	P		5.86	7.38	1-2	$4p \ ^1P - 6s \ ^3P^o$ 33
6142.204	P		5.62	7.64	3-2		8338.328	A	20	5.86	7.35	1-1	
6131.850	A	90	5.62	7.64	2-3								
6131.574	A	85	5.62	7.64	2-2		8374.98	P		5.86	7.34	1-0	
6125.021	A	90	5.61	7.64	1-2								
6123.494	P		5.62	7.64	3-2	$3p^3 \ ^3D^o - 5f' [1\frac{1}{2}]$ 21.14	8093.241	A	70	5.86	7.39	1-1	$4p \ ^1P - 5d \ ^1D^o$ 34
6112.926	A	10	5.62	7.64	2-2		7680.267	A	100	5.86	7.48	1-2	$4p \ ^1P - 5d \ ^1D^o$ 36
6113.15	A	4	5.62	7.64	2-1								
6106.605	A	15	5.61	7.64	1-1		7482.19	A	25	5.86	7.52	1-2	$4p \ ^1P - 5d \ ^3F^o$ 36.01
5813.20	A	3	5.62	7.75	3-2	$3p^3 \ ^3D^o - 7p \ ^3P$ 21.15	7129.88	P		5.86	7.60	1-1	$4p \ ^1P - 5d \ ^1P^o$ 36.02
5747.667	A	45	5.61	7.77	1-2	$3p^3 \ ^3D^o - 6f [2\frac{1}{2}]$ 21.16	7058.31	P		5.86	7.62	1-2	$4p \ ^1P - 5d \ ^3D^o$ 36.03
5762.977	A	45	5.62	7.77	3-4	$3p^3 \ ^3D^o - 6f [3\frac{1}{2}]$ 21.17	7026.62	A	25	5.86	7.63	1-1	
5753.625	A	45	5.62	7.77	2-3								
5675.418	A	20	5.62	7.80	3-4	$3p^3 \ ^3D^o - 6f' [3\frac{1}{2}]$ 21.18	6875.924	P		5.86	7.66	1-2	$4p \ ^1P - 7s \ ^3P^o$ 36.04
5675.73	A	5	5.62	7.80	3-3		6985.52	P		5.86	7.64	1-1	
5666.677	A	10	5.62	7.80	2-3		7013.65	P		5.86	7.63	1-0	
5669.743	A	10	5.62	7.81	3-3	$3p^3 \ ^3D^o - 6f' [2\frac{1}{2}]$ 21.19	6867.22	A	20	5.86	7.67	1-2	$4p \ ^1P - 5d \ ^3P^o$ 36.05
5660.683	A	13	5.62	7.81	2-3								
5660.502	A	10	5.62	7.81	2-2		6848.568	A	30	5.86	7.67	1-1	$4p \ ^1P - 7s \ ^1P^o$ 37
5654.924	A	15	5.61	7.81	1-2								
5421.168	A	10	5.62	7.91	3-4	$3p^3 \ ^3D^o - 7f' [3\frac{1}{2}]?$ 21.20	6721.853	A	100	5.86	7.71	1-2	$4p \ ^1P - 6d \ ^1D^o$ 38
5409.766	P		5.62	7.91	2-2		6635.65	A	25	5.86	7.73	1-2	$4p \ ^1P - 6d \ ^3F^o$ 38.01
5404.665	P		5.61	7.91	1-2	$3p^3 \ ^3D^o - 7f' [2\frac{1}{2}]?$ 21.21	6437.79	A	8	5.86	7.79	1-1	$4p \ ^1P - 8s \ ^3P^o$ 38.02
16380.12	E	(8)	5.86	6.62	1-1	$4p \ ^1P - 3d \ ^1P^o$ 21.22	6279.35	A	15	5.86	7.84	1-2	$4p \ ^1P - 7d \ ^1D^o$ 38.03
14444.77	P		5.86	6.72	1-2	$4p \ ^1P - 3d \ ^3D^o$ 21.23	6220.21	P		5.86	7.85	1-2	$4p \ ^1P - 7d \ ^3F^o$ 38.04
14486.27	P		5.86	6.72	1-1								
14221.36	E	(2)	5.86	6.73	1-1	$4p \ ^1P - 5s \ ^3P^o$ 21.24	10602.817	P		5.87	7.04	2-1	$3d \ ^1D^o - 5p \ ^1P$ 38.05
14361.91	P		5.86	6.73	1-0								
13176.90	E	(11)	5.86	6.80	1-1	$4p \ ^1P - 5s \ ^1P^o$ 21.25	9569.93	A	6	5.87	7.17	2-2	$3d \ ^1D^o - 5p \ ^1D$ 42

## Multiplet Table

## Si I—Continued

## Si I—Continued

IA	Ref	Int	E P		J	Multiplet No.	IA	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Air							Air						
8752.009	A	100	5.87	7.29	2-3	$3d^1D^o - 4f [2\frac{1}{2}]$ 42.01	10727.408	A	30	5.98	7.14	3-4	$4p^3D - 4d^3F^o$ 53
8751.174	A	10	5.87	7.29	2-2		10694.251	A	30	5.96	7.12	2-3	
8742.451	A	75	5.87	7.29	2-3	$3d^1D^o - 4f [3\frac{1}{2}]$ 42.02	10689.719	A	25	5.95	7.11	1-2	
							10882.802	A	30	5.98	7.12	3-3	
							10784.560	A	30	5.96	7.11	2-2	
							10976.346	P		5.98	7.11	3-2	
8556.780	A	120	5.87	7.32	2-3	$3d^1D^o - 4f' [3\frac{1}{2}]$ 42.03	8892.728	A	20	5.98	7.38	3-2	$4p^3D - 6s^3P^o$ 54
8502.221	A	60	5.87	7.33	2-3	$3d^1D^o - 4f' [2\frac{1}{2}]$ 42.04	8949.10	A	10	5.96	7.35	2-1	
8501.547	A	40	5.87	7.33	2-2		8925.30	A	10	5.95	7.34	1-0	
8443.982	A	40	5.87	7.34	2-2	$3d^1D^o - 4f' [1\frac{1}{2}]$ 42.05	8766.422	A	14	5.96	7.38	2-2	
8444.40	P		5.87	7.34	2-1		8883.68	A	4	5.95	7.35	1-1	
							8703.644	P		5.95	7.38	1-2	
7672.648	P		5.87	7.49	2-1	$3d^1D^o - 6p^1P?$ 42.06	8667.373	A	7	5.96	7.39	2-1	$4p^3D - 6s^1P^o$ 55
							8606.014	A	8	5.95	7.39	1-1	
7345.218	P		5.87	7.56	2-2	$3d^1D^o - 6p^1D$ 42.07	8579.09	A	6	5.98	7.43	3-2	$4p^3D - 4d^3P^o$ 56
							8395.24	A	5	5.96	7.44	2-1	
							8461.48	A	6	5.96	7.43	2-2	
7165.545	A	200	5.87	7.60	2-3	$3d^1D^o - 5f [2\frac{1}{2}]$ 42.08	8195.44	A	2	5.96	7.48	2-2	$4p^3D - 5d^1D^o$ 56.01
7165.082	P		5.87	7.60	2-2		8140.55	A	15	5.95	7.48	1-2	
7164.69	A	70	5.87	7.60	2-3	$3d^1D^o - 5f [3\frac{1}{2}]$ 42.09	7944.001	A	140	5.98	7.54	3-4	$4p^3D - 5d^3F^o$ 57
							7932.349	A	120	5.96	7.53	2-3	
							7918.386	A	90	5.95	7.52	1-2	
7034.903	A	250	5.87	7.63	2-3	$3d^1D^o - 5f' [3\frac{1}{2}]$ 42.10	8035.619	A	35	5.98	7.53	3-3	
							7970.306	A	35	5.96	7.52	2-2	
							8074.574	P		5.98	7.52	3-2	
7017.646	A	90	5.87	7.64	2-3	$3d^1D^o - 5f' [2\frac{1}{2}]$ 42.11	7597.30	A	5	5.98	7.62	3-3	$4p^3D - 5d^1F^o$ 57.01
7017.28	A	30	5.87	7.64	2-2		7504.93	P		5.96	7.62	2-3	
6992.88	A	15	5.87	7.64	2-2	$3d^1D^o - 5f' [1\frac{1}{2}]$ 42.12	7510.785	P		5.98	7.63	3-3	$4p^3D - 5d^3D^o$ 57.02
							7491.08	P		5.96	7.62	2-2	
6527.199	A	45	5.87	7.77	2-3	$3d^1D^o - 6f [2\frac{1}{2}]$ 42.13	7409.92	P		5.95	7.63	1-1	
6526.391	P		5.87	7.77	2-2		7583.11	P		5.98	7.62	3-2	
6526.609	A	45	5.87	7.77	2-3	$3d^1D^o - 6f [3\frac{1}{2}]$ 42.14	7420.489	A	25	5.96	7.63	2-3	
							7445.19	P		5.95	7.62	1-2	
6414.97	A	25	5.87	7.80	2-3	$3d^1D^o - 6f' [3\frac{1}{2}]$ 42.15	7373.00	A	35	5.98	7.66	3-2	$4p^3D - 7s^3P^o$ 58
							7409.15	P	15	5.96	7.64	2-1	
							7395.52	A		5.95	7.63	1-0	
6407.27	A	15	5.87	7.81	2-3	$3d^1D^o - 6f' [2\frac{1}{2}]$ 42.16	7362.88	A	1	5.98	7.67	3-2	$4p^3D - 5d^3P^o$ 58.01
6407.07	P		5.87	7.81	2-2								
6394.233	P	15	5.87	7.81	2-2?	$3d^1D^o - 6f' [1\frac{1}{2}]$ 42.17	7255.27	P		5.96	7.67	2-1	$4p^3D - 7s^1P^o$ 59
6394.380	P		5.87	7.81	2-1?								
6091.92	A	15	5.87	7.91	2-3	$3d^1D^o - 7f' [3\frac{1}{2}]?$ 42.18	7005.883	A	180	5.98	7.75	3-4	$4p^3D - 6d^3F^o$ 60
							7003.566	A	180	5.96	7.73	2-3	
6087.80	A	10	5.87	7.91	2-3	$3d^1D^o - 7f' [2\frac{1}{2}]?$ 42.19	6976.523	A	80	5.95	7.73	1-2	
							7083.95	A	5	5.98	7.73	3-3	
							7016.74	A	10	5.96	7.73	2-2	
							7097.47	P		5.98	7.73	3-2	
16680.77	E	(29)	5.98	6.73	3-3	$4p^3D - 3d^3D^o$ 42.20	6876.40	A	5H	5.98	7.79	3-3	$4p^3D - 6d^1F^o$ 60.01
16381.55	E	(16)	5.96	6.72	2-2		6800.63	A	1	5.96	7.79	2-3	
16215.68	E	(11)	5.95	6.72	1-1								
16828.18	E	(3)	5.98	6.72	3-2		6741.64	A	30	5.98	7.82	3-2	$4p^3D - 8s^3P^o$ 60.02
16434.98	E	(1)	5.96	6.72	2-1		6668.79	P		5.96	7.82	2-2	
16241.84	E	(7)	5.96	6.73	2-3								
16163.71	E	(6)	5.95	6.72	1-2		6813.89	P		5.98	7.80	3-3	$4p^3D - 6d^3D^o$ 60.03
							6767.62	P		5.96	7.80	2-2	
15960.04	E	(40)	5.98	6.76	3-2	$4p^3D - 5s^3P^o$ 42.21	6706.98	P		5.95	7.80	1-1	
16094.80	E	(20)	5.96	6.73	2-1		6842.65	P		5.98	7.80	3-2	
16060.03	E	(10)	5.95	6.73	1-0		6739.49	P		5.96	7.80	2-3	
15557.81	E	(7)	5.96	6.76	2-2		6652.33	P		5.96	7.83	2-1	$4p^3D - 8s^1P^o$ 60.04
15884.41	E	(5)	5.95	6.73	1-1		6616.12	P		5.95	7.83	1-1	
15361.16	P		5.96	6.73	1-2								

Multiplet Table

## Si I—Continued

## Si I—Continued

IA	Ref	Int	EP		J	Multiplet No.	IA	Ref	Int	EP			Multiplet No.
			Low	High						Low	High		
Air 6691.32 6619.56 6583.71	P P A		5.98 5.96 5.95	7.84 7.84 7.84	3-2 2-2 1-2	$4p\ ^3D - 7d\ ^1D^\circ$ 60.05	Air 7821.82	A	4	6.08	7.67	1-2	$4p\ ^3P - 5d\ ^3P^\circ$ 68.01
6555.462 6560.556 6518.73 6631.05	A A A P	15 25 20 5	5.98 5.96 5.95 5.98	7.87 7.85 7.85 7.85	3-4 2-3 1-2 3-3	$4p\ ^3D - 7d\ ^3F^\circ$ 60.06	7777.96	P		6.08	7.67	0-1	$4p\ ^3P - 7s\ ^1P^\circ$ 68.02
6299.60	A		5.98	7.95	3-4	$4p\ ^3D - 8d\ ^3F^\circ?$ 60.07	7343.27	A	1	6.10	7.79	2-3	$4p\ ^3P - 6d\ ^1F^\circ?$ 68.03
							6917.13	A	1	6.10	7.89	2-3	$4p\ ^3P - 7d\ ^1F^\circ$ 68.04
19722.50 19432.97 19385.94 19928.88 19508.13 20007.97	E E E E E E	(110) (48) (15) (31) (14) (3)	6.10 6.08 6.08 6.10 6.08 6.10	6.73 6.72 6.72 6.72 6.72 6.72	2-3 1-2 0-1 2-2 1-1 2-1	$4p\ ^3P - 3d\ ^3D^\circ$ 60.08	20804.13	E	(4)	6.12	6.72	1-2	$4p\ ^3S - 3d\ ^3D^\circ$ 68.05
18722.90 19030.79 19506.12 19283.29 18284.51 18914.48	E E E E E E	(26) (5) (5) (8) (3) (8)	6.10 6.08 6.10 6.08 6.08 6.08	6.76 6.73 6.73 6.73 6.76 6.73	2-2 1-1 2-1 1-0 1-2 0-1	$4p\ ^3P - 5s\ ^3P^\circ$ 60.09	19493.38 20343.87	E E	(13) (4)	6.12 6.12	6.76 6.73	1-2 1-1	$4p\ ^3S - 5s\ ^3P^\circ$ 68.06
13667.35 13432.23	E P	(3)	6.10 6.08	7.01 7.01	2-2 1-2	$4p\ ^3P - 4d\ ^1D^\circ$ 60.10	14073.39	E	(3)	6.12	7.01	1-2	$4p\ ^3S - 4d\ ^1D^\circ$ 68.07
13325.67 13086.03 13309.04 13029.52 13102.05 13030.92	E P E P E P	(3) (3) (5) (3) (3) (3)	6.10 6.08 6.10 6.08 6.08 6.08	7.03 7.03 7.03 7.03 7.03 7.03	2-2 1-1 2-1 1-0 1-2 0-1	$4p\ ^3P - 3p\ ^3P^\circ$ 60.11	13711.36 13693.85 13631.94	E E E	(5) (8) (4)	6.12 6.12 6.12	7.03 7.03 7.03	1-2 1-1 1-0	$4p\ ^3S - 3p\ ^3P^\circ$ 68.08
10068.22 10025.81 9969.05 10155.83	A A A A	2 2 2 5	6.10 6.08 6.08 6.10	7.33 7.32 7.32 7.32	2-3 1-2 0-1 2-2	$4p\ ^3P - 4d\ ^3D^\circ$ 60.12	9891.72 10124.930	A P	10	6.12 6.12	7.38 7.35	1-2 1-1	$4p\ ^3S - 6s\ ^3P^\circ$ 71
9689.39 9788.80 9912.96 9839.36 9570.65 9757.95	A A A A A A	10 6 2 6 8 2	6.10 6.08 6.10 6.08 6.08 6.08	7.38 7.35 7.35 7.34 7.38 7.35	2-2 1-1 2-1 1-0 1-2 0-1	$4p\ ^3P - 6s\ ^3P^\circ$ 65	9505.19 9421.78 8297.71 8046.803	A A A P	20 15 2 6.12	6.12 6.12	7.43 7.44 7.62 7.66	1-2 1-1 1-2 1-2	$4p\ ^3S - 4d\ ^3P^\circ$ 72
9318.22 9130.03 9238.04 9208.35 9103.18	A P A A A	10 6.08 6 15 7	6.10 7.44 6.10 6.08 6.08	7.43 7.44 7.44 7.43 7.44	2-2 1-1 2-1 1-2 0-1	$4p\ ^3P - 4d\ ^3P^\circ$ 66	11446.27 11448.92 11289.83 11292.40 11187.588	P P A P A		6.21 6.21 6.19 6.19 6.18	7.29 7.29 7.29 7.29 7.29	4-4 4-3 3-4 3-3 2-2	$3d\ ^3F^\circ - 4f\ [2\frac{1}{2}]$ 74.01
8171.288	A	25	6.10	7.62	2-3	$4p\ ^3P - 5d\ ^1F^\circ$ 66.01	11130.03 11132.57 10982.061 10984.527 10885.336	A P A A A	12 30 30 20 30	6.21 6.21 6.19 6.19 6.18	7.32 7.32 7.32 7.32 7.32	4-4 4-3 3-4 3-3 2-3	$3d\ ^3F^\circ - 4f'\ [3\frac{1}{2}]$ 74.03
8071.285 8070.598 8008.37 8154.872 8029.17 8112.58	A A A A P P	25 25 2 15 6.08 6.08	6.10 6.08 6.08 6.10 6.08 6.10	7.63 7.62 7.63 7.62 7.63 7.63	2-3 1-2 0-1 2-2 1-1 2-1	$4p\ ^3P - 5d\ ^3D^\circ$ 66.02	10976.06	A	7	6.18	7.33	2-2	$3d\ ^3F^\circ - 4f'\ [2\frac{1}{2}]$ 74.04
7912.383 7975.579 8057.87 8012.25 7833.025 7955.07	A A P P P P	20 13 6.10 6.08 6.08 6.08	6.10 6.08 6.10 6.08 6.08 6.08	7.66 7.64 7.64 7.63 7.66 7.64	2-2 1-1 2-1 1-0 1-2 0-1	$4p\ ^3P - 7s\ ^3P^\circ$ 68	11017.965 11013.69 9387.33 9464.78 9399.211	A A A A P	80 5 10 4 30	6.21 6.21 6.21 6.19 6.19	7.33 7.33 7.53 7.50 7.50	4-5 4-4 4-3 3-2 2-1	$3d\ ^3F^\circ - 4f'\ [4\frac{1}{2}]$ 74.05

Multiplet Table

## Si I—Continued

## Si I—Continued

IA	Ref	Int	E P		J	Multiplet No.	IA	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Air													
8887.57	P		6.21	7.60	4-3	$3d^3F^o - 5f [2\frac{1}{2}]$							
8792.957	A	5	6.19	7.60	3-3	74.07							
8729.282	P		6.18	7.60	2-3								
8728.595	P		6.18	7.60	2-2								
8884.94	P		6.21	7.60	4-4	$3d^3F^o - 5f [3\frac{1}{2}]$							
8790.389	A	35	6.19	7.60	3-4	74.08							
8791.675	P		6.19	7.60	3-3								
8728.011	A	40	6.18	7.60	2-3								
8686.35	P		6.21	7.63	4-4	$3d^3F^o - 5f' [3\frac{1}{2}]$							
8687.46	P		6.21	7.63	4-3	74.09							
8595.962	A	25	6.19	7.63	3-4								
8597.047	A	20	6.19	7.63	3-3								
8536.164	A	40	6.18	7.63	2-3								
8571.307	P		6.19	7.64	3-3	$3d^3F^o - 5f' [2\frac{1}{2}]$							
8510.24	A	8	6.18	7.64	2-2	74.10							
8648.462	A	50	6.21	7.64	4-5	$3d^3F^o - 5f' [4\frac{1}{2}]$							
8646.36	A	6	6.21	7.64	4-4?	74.11							
7850.802	P		6.19	7.77	3-3	$3d^3F^o - 6f [2\frac{1}{2}]$							
7800.008	A	30	6.18	7.77	2-3	74.12							
7925.28	P		6.21	7.77	4-4	$3d^3F^o - 6f [3\frac{1}{2}]$							
7849.967	A	30	6.19	7.77	3-4	74.13							
7760.63	P		6.21	7.80	4-4	$3d^3F^o - 6f' [3\frac{1}{2}]$							
7688.40	P		6.19	7.80	3-4	74.14							
7689.02	P		6.19	7.80	3-3								
7640.31	A	20	6.18	7.80	2-3								
7742.71	A	40	6.21	7.81	4-5	$3d^3F^o - 6f' [4\frac{1}{2}]$							
7669.71	A	5	6.19	7.81	3-4?	74.15							
7282.81	A	40	6.21	7.91	4-5	$3d^3F^o - 7f' [4\frac{1}{2}]$							
						74.16							
21354.24	E	(21)	6.22	6.80	2-1	$4p^1D - 5s^1P^o$							
						74.17							
15833.58	E	(7)	6.22	7.01	2-2	$4p^1D - 4d^1D^o$							
						74.18							
15376.88	E	(4)	6.22	7.03	2-2	$4p^1D - 3p^33P^o$							
						74.19							
11485.83	E	(5)	6.22	7.30	2-3	$4p^1D - 4d^1F^o$							
						83							
11196.80	A	2	6.22	7.33	2-3	$4p^1D - 4d^3D^o$							
						83.01							
10582.14	A	2	6.22	7.39	2-1	$4p^1D - 6s^1P^o$							
						84							
9887.06	A	10	6.22	7.48	2-2	$4p^1D - 5d^1D^o$							
						85							
8899.23	A	2	6.22	7.62	2-3	$4p^1D - 5d^1F^o$							
						86							
8780.747	A	11	6.22	7.63	2-3	$4p^1D - 5d^3D^o$							
						86.01							
8593.02	P		6.22	7.66	2-2	$4p^1D - 7s^3P^o$							
8764.88	P		6.22	7.64	2-1	86.02							
8550.35	P		6.22	7.67	2-1	$4p^1D - 7s^1P^o$							
						88							

Multiplet Table  
Strongest Unclassified Lines of Si I

**Si I—Continued**

**Si I—Continued**

IA	Ref	Int	IA	Ref	Int
Air					
10414.70	A	10	4587.23	A	12
9576.45	A	4	4585.73	A	5
7490.87	A	5	4574.01	A	7
6394.67	A	15	4573.66	A	7
5421.61	A	10 <i>H</i>	4556.44	A	7
4922.77	A	7	4528.07	A	5
4806.03	A	5	4516.08	A	4
4764.92	A	5	2166.599	A	3
4671.22	A	4	2158.526	A	5 <i>h</i>
4669.83	A	4	Vac		
4658.82	A	5	1752.634	B	3
4639.335	A	6	1597.736	B	20
4638.17	A	15	1571.796	B	6
4621.50	A	4	1545.095	C	(1 <i>r</i> )
4603.31	A	3			



**Announcement of New Publications in  
National Standard Reference Data Series**

Superintendent of Documents,  
Government Printing Office,  
Washington, D.C. 20402

(cut here)

Dear Sir:

Please add my name to the announcement list of new publications to be issued in the series: National Standard Reference Data Series—National Bureau of Standards.

Name.....

Company.....

Address.....

City..... State..... Zip Code.....

(Notification key N-337)



## THE NATIONAL BUREAU OF STANDARDS

The National Bureau of Standards<sup>1</sup> provides measurement and technical information services essential to the efficiency and effectiveness of the work of the Nation's scientists and engineers. The Bureau serves also as a focal point in the Federal Government for assuring maximum application of the physical and engineering sciences to the advancement of technology in industry and commerce. To accomplish this mission, the Bureau is organized into three institutes covering broad program areas of research and services:

**THE INSTITUTE FOR BASIC STANDARDS** . . . provides the central basis within the United States for a complete and consistent system of physical measurements, coordinates that system with the measurement systems of other nations, and furnishes essential services leading to accurate and uniform physical measurements throughout the Nation's scientific community, industry, and commerce. This Institute comprises a series of divisions, each serving a classical subject matter area:

—Applied Mathematics—Electricity—Metrology—Mechanics—Heat—Atomic Physics—Physical Chemistry—Radiation Physics—Laboratory Astrophysics<sup>2</sup>—Radio Standards Laboratory,<sup>2</sup> which includes Radio Standards Physics and Radio Standards Engineering—Office of Standard Reference Data.

**THE INSTITUTE FOR MATERIALS RESEARCH** . . . conducts materials research and provides associated materials services including mainly reference materials and data on the properties of materials. Beyond its direct interest to the Nation's scientists and engineers, this Institute yields services which are essential to the advancement of technology in industry and commerce. This Institute is organized primarily by technical fields:

—Analytical Chemistry—Metallurgy—Reactor Radiations—Polymers—Inorganic Materials—Cryogenics<sup>2</sup>—Office of Standard Reference Materials.

**THE INSTITUTE FOR APPLIED TECHNOLOGY** . . . provides technical services to promote the use of available technology and to facilitate technological innovation in industry and government. The principal elements of this Institute are:

—Building Research—Electronic Instrumentation—Technical Analysis—Center for Computer Sciences and Technology—Textile and Apparel Technology Center—Office of Weights and Measures  
—Office of Engineering Standards Services—Office of Invention and Innovation—Office of Vehicle Systems Research—Clearinghouse for Federal Scientific and Technical Information<sup>3</sup>—Materials Evaluation Laboratory—NBS/GSA Testing Laboratory.

---

<sup>1</sup> Headquarters and Laboratories at Gaithersburg, Maryland, unless otherwise noted; mailing address Washington, D. C., 20234.

<sup>2</sup> Located at Boulder, Colorado, 80302.

<sup>3</sup> Located at 5285 Port Royal Road, Springfield, Virginia 22151.

U.S. DEPARTMENT OF COMMERCE  
WASHINGTON, D.C. 20230

POSTAGE AND FEES PAID  
U.S. DEPARTMENT OF COMMERCE

OFFICIAL BUSINESS

---