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NSRDS-NBS 3, Section 1

# Selected Tables of Atomic Spectra

## Atomic Energy Levels and Multiplet Tables

Si II, Si III, Si IV

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U.S. DEPARTMENT OF COMMERCE

NATIONAL BUREAU OF STANDARDS



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UNITED STATES DEPARTMENT OF COMMERCE • John T. Connor, *Secretary*

NATIONAL BUREAU OF STANDARDS • A. V. Astin, *Director*

# Selected Tables of Atomic Spectra

A Atomic Energy Levels - Second Edition

B Multiplet Tables

Si II, Si III, Si IV

Data Derived From the Analyses of Optical Spectra

Charlotte E. Moore



NSRDS-NBS 3, Section 1

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## Foreword

The present publication has been undertaken in response to the increasing demand for a current revision of two sets of tables containing data on atomic spectra as derived from analyses of optical spectra.

The first set, *Atomic Energy Levels*, NBS Circular 467, consists of three Volumes published, respectively, in 1949, 1952, and 1958, and a fourth on rare-earth spectra, still in course of preparation.

The second set consists of two Multiplet Tables; one published in 1945 by the Princeton University Observatory, containing spectral lines in the region of wavelengths longer than 3000 Å; the other *An Ultraviolet Multiplet Table*, NBS Circular 488, appearing in five Sections, the first in 1950, the second in 1952, and the others in 1962.

In order to make data available sooner for such rapidly developing fields as space technology, plasma physics, and astrophysics, two innovations have been introduced in the present work. First, for each spectrum both the atomic energy levels and the multiplet table are being included in a single publication, as Parts A and B, respectively. Secondly, the Sections will be published at irregular intervals whenever adequate data become available for the individual spectra. In the earlier publications, the data were presented in regular order, i.e., the spectra were arranged in order of increasing atomic number of the various elements. This plan introduced long delays, as is evident from the span of years quoted above. The present plan should reduce such delays. A flexible paging system will permit the arrangement of the various Sections by atomic number regardless of the order in which they are published. Section 1 starts the plan with three spectra of silicon,  $Z=14$ : Si II, Si III, Si IV. The form of presentation is similar to that of the tables mentioned above.

The manuscript has been prepared by Charlotte E. Moore of the Atomic Physics Division, who also prepared the earlier tables. She acknowledges with gratitude the cordial cooperation of the National Research Council Committee on Line Spectra of the Elements, as well as that of the many atomic spectroscopists who make such a publication possible. It is hoped that as the present and succeeding Sections appear, they will inspire further urgently needed research on the analysis of atomic spectra.

A. V. ASTIN, *Director.*

WASHINGTON, D.C., June 1, 1965.



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### Part A—Atomic Energy Levels

Element:	Z	Spectrum			
Silicon:	14				
		Si II .....		A14	II-1
		Si III .....		A14	III-1
		Si IV .....		A14	IV-1

### Part B—Multiplet Tables

Element:	Z	Spectrum			
Silicon:	14				
		Si II .....		B14	II-1
		Si III .....		B14	III-1
		Si IV .....		B14	IV-1

## 1. Introduction

The increasing demand for data derived from the analyses of optical spectra has prompted the planning of a large publication. The present Section is the first of a long series to be published at irregular intervals, as suitable material becomes available. It is felt that the inclusion of both revised "Atomic Energy Levels" and "Selected Multiplets" as Parts A and B, respectively, of the same Volume may meet the present need more satisfactorily than the separate handling of each Part.

Furthermore, a flexible plan of publication permits the

preparation and distribution of the Tables whenever the analysis of a spectrum has reached the stage where no further revision or extension is likely to occur in the foreseeable future.

It is hoped that the complete revision of "Atomic Energy Levels" [1] (Part A) will contain many new results for high-ionization spectra of the light and abundant elements. This can be done only if the revision is carried on gradually, parallel with the development of laboratory programs on the analyses of ultraviolet spectra.

## 2. Arrangement

*Part A.* For the "Atomic Energy Levels" the format is the same as that adopted for the first edition [1]. Recently, however, the conversion factor from  $\text{cm}^{-1}$  to eV has been revised [2]. The new factor has been adopted here. All limits and energy levels (in  $\text{cm}^{-1}$ ) have been multiplied by the factor 0.000123981 to obtain the respective ionization and excitation potentials in eV quoted in the Tables.

The letters following the references are also the same as those used previously to denote the scope of the individual papers. They are as follows:

I P	Ionization potential
T	Terms
C L	Classified lines
G D	Grotrian diagram
E D	Energy diagram
Z E	Zeeman effect
I S	Isotope shift
hfs	Hyperfine structure

Predicted positions of unknown levels are entered in brackets.

*Part B.* A single Multiplet Table covering the observations over the entire spectral range for the various spectra, has long been urgently needed. The writer's Multiplet Table of 1945 [3] includes lines  $>3000 \text{ \AA}$ ; it is seriously out of date and very incomplete as regards infrared data. Her Ultraviolet Multiplet Table [4] is also inadequate for the interpretation of existing ultraviolet solar spectra, and should be greatly expanded in anticipation of future space observations short of  $3000 \text{ \AA}$ . In the present work it is planned to combine these two Multiplet Tables into one that is both revised and extended.

The general style of presentation is that of the "Ultraviolet Multiplet Table" [3]. As explained above, all ionization and excitation potentials have been calculated with the revised conversion factor recently recommended [2].

An arbitrary general grading of the analysis is indicated,

as in the earlier tables. The four grades denote respectively:

Anal A	Analysis essentially complete.
Anal B	Analysis good but not complete.
Anal C	Leading lines classified.
Anal D	Only a few leading lines classified.

A similar grading system has been used to indicate the completeness of the Multiplet Table for a given spectrum. For spectra of the abundant elements, widely used, essentially all classified lines are listed. When multiplet data appear to be needed for only the leading lines of a spectrum, the listing is less complete. In general terms the lists may be described as follows:

List A	All classified lines included in the Multiplet Table.
List B	Most classified lines included, but fainter lines omitted.
List C	Only leading classified lines listed.
List D	Only strongest lines from ground states listed.

The columns of the Multiplet Table are self-explanatory. In column 1, the wavelengths in air are quoted for the region long of  $2000 \text{ \AA}$ . Short of  $2000 \text{ \AA}$ , vacuum wavelengths are quoted. "Vac" and "Air" are inserted in this column to remind the users of the change in the different spectral regions. In column 2 the reference source for the wavelength (and often for other data) is indicated by letters that refer to the separate references used for the tabulation. The references precede the multiplets. The letters following the references have the same meaning as described for Part A. In the Multiplet Table, however, the letter "I" is added to denote the reference source used for the quoted estimated intensity. When the intensity scale changes, either because of a different source, or a different author, parentheses are used in the intensity column.



The low and high excitation potentials (columns 4 and 5), and the  $J$  values (column 6) correspond respectively, to the low and high levels involved in the transition producing the line. The levels in  $\text{cm}^{-1}$  may be found in Part A. The term designations are identical in Parts A and B.

Symbols: An asterisk denotes a blend throughout. In the wavelength column the lines so marked have more than one classification in the same spectrum. In the intensity column the asterisk indicates that the intensity is affected by that of a neighboring line or of an impurity line.

If the blend involves a line in the spectrum of a different stage of ionization of the same element, an asterisk precedes the wavelength and another symbol such as “§” follows it. These symbols are explained on the first page of the Table, following the references.

The *raie ultime* is indicated by the symbol “‡”.

A dagger “†” in the intensity column calls attention to intersystem combinations of astrophysical interest. Throughout the Multiplet Table, intersystem combinations are handled as permitted lines, since they are so commonly observed in the laboratory. I. S. Bowen has pointed out that under special conditions such as pertain in nebulae, for example, certain intersystem combinations from the ground state are stronger than lines from transitions in which the multiplicity does not change. The relative laboratory intensities can, therefore, be misleading under these special circumstances. A dagger denotes such intersystem lines.

An “m” preceding the wavelength indicates that the line is masked, and the spectrum of the masking line is indicated in the intensity column.

Multiplet Numbers: The earlier multiplet numbers from both the 1945 Table and the Ultraviolet Multiplet Table are widely quoted in the literature. For this reason the writer has been urgently requested to keep the old numbers throughout. This involves retaining two systems of numbering; UV numbers for multiplets short of 3000 Å; and regular numbers for those longer than 3000 Å. The old numbers have been dropped entirely in cases where the earlier designations are incorrect. As before, “F” following the multiplet number denotes a forbidden transition.

Newly inserted multiplets are numbered by a decimal system. For example, in Si II nine groups have been inserted between multiplets formerly published as UV 6 and UV 7. The new ones are numbered UV 6.01, UV 6.02 etc. Similarly in the longer wave region a number of multiplets have been inserted between multiplets 7 and 8 in the 1945 table. The new ones are numbered 7.01, 7.02 etc. When the old multiplet numbers are exhausted and new ones follow, the decimal system is no longer used. It is stated on the first page where the new multiplet numbers, not inserted between older ones, start. In Si II, for example, the numbers from UV 21 and 10 for the two respective regions have never been used before.

### 3. Acknowledgments

Many have assisted in planning this large publication. At the Mt. Wilson and Palomar Observatories, the Director, Ira S. Bowen and the late Paul W. Merrill have taken a keen interest in the project and provided much valuable help with the planning. The writer has also benefited greatly from a conference with B. Strömgren, who has carefully appraised this first Section before publication. Many others have also been consulted.

The cordial support of the National Bureau of Standards is making this program possible. Miss Sarah A. Jones and her staff in the library are indispensable for such a task. Nor could it succeed without the able assistance from the Publications Section, where Mr. John Carpenter and Mrs. Betty Arnold have spared no effort in handling

the publication of this difficult material in its present legible style.

In the Spectroscopy group the support of K. G. Kessler, W. F. Meggers, and W. C. Martin, Jr. has been a source of great encouragement. Mrs. Isabel D. Murray is carrying the heavy load of preparing the final manuscript for the press. All users are indebted to her for her extreme skill and competence with these many details.

The writer takes genuine pleasure in thanking everyone who has so willingly encouraged and helped her start this enormous task. It is hoped that within the next decade there will be increased activity in the observation and analyses of atomic spectra, sufficient to fill some of the most striking gaps in our knowledge of atomic spectra.

### REFERENCES

- |   |  |
|---|--|
| <p>[1] C. E. Moore, Atomic Energy Levels, Circ. Nat. Bur. Std. 467:<br/> Volume I. H to V 206 spectra, 309 p. (1949);<br/> Volume II. Cr to Nb 152 spectra, 227 p. (1952);<br/> Volume III. { Mo to La }<br/> { Hf to Ac } 124 spectra, 245 p. (1958).</p> <p>[2] J. A. Bearden and others, New Values for the Physical Constants as Recommended by the NAS-NRC, Physics Today <b>17</b>, 48-49 (1964).</p> <p>[3] C. E. Moore, A Multiplet Table of Astrophysical Interest, Contr. Princeton Univ. Obs. No. 20 (1945). Reprinted as Tech. Note Nat. Bur. Std. No. 36, PB151395 (1959).</p> | <p>[4] C. E. Moore, An Ultraviolet Multiplet Table, Circ. Nat. Bur. Std. 488:<br/> Section 1. H to V 78 p. (1950);<br/> Section 2. Cr to Nb 115 p. (1952);<br/> Section 3. { Mo to La }<br/> { Hf to Ra } 94 p. (1962);<br/> Section 4. }<br/> Section 5. } Finding Lists for Sections 1, 2, and 3 (1962).</p> |
|---|--|



NSRDS-NBS 3, SECTION 1

## SILICON, $Z=14$

A Si II Atomic Energy Levels

B Si II Multiplet Table





## Atomic Energy Levels

## Part A

## SILICON

## Si II

(A1 I sequence; 13 electrons)

 $Z=14$ Ground state  $1s^2 2s^2 2p^6 3s^2 3p^2 P_{0\frac{1}{2}}^\circ$  $3p^2 P_{0\frac{1}{2}}^\circ$  **131838.4**  $\pm 0.1$  cm<sup>-1</sup>, 758.50 Å (Vac)

I P 16.35 eV

Shenstone has reobserved the Si II spectrum from 700 Å to 9500 Å and added 300 new lines to the earlier description. His revised and extended analysis "includes details of the perturbations of the  $3s^2 nx^2X$  series up to  $x=g$ ". The limit is derived from a six-member  $^2G$  series by means of a Ritz formula. Autoionization effects are also discussed.

Intersystem combinations connect the terms of different multiplicity.

All data in the table are taken from Shenstone's 1961 paper.

## REFERENCE

A. G. Shenstone, Proc. Roy. Soc. [A] **261**, 153 to 174 (1961). I P, T, C L

## Si II

## Si II

Config.	Desig.	$J$	Level	Interval	Config.	Desig.	$J$	Level	Interval
$3s^2(^1S)3p$	$3p^2 P^\circ$	$0\frac{1}{2}$ $1\frac{1}{2}$	<i>0.00</i> <i>287.32</i>	287.32	$3s^2(^1S)6p$	$6p^2 P^\circ$	$0\frac{1}{2}$ $1\frac{1}{2}$	<i>113962.34</i> <i>113976.98</i>	14.64
$3s3p^2$	$3p^2^4P$	$0\frac{1}{2}$ $1\frac{1}{2}$ $2\frac{1}{2}$	42824.35 42932.68 43107.97	108.33 175.29	$3s^2(^1S)5g$	$5g^2G$	$3\frac{1}{2}$ $4\frac{1}{2}$	} 114177.4	
$3s3p^2$	$3p^2^2D$	$1\frac{1}{2}$ $2\frac{1}{2}$	55309.61 55325.44	15.83	$3s3p(^3P^\circ)3d$	$3d'^4F^\circ$	$1\frac{1}{2}$ $2\frac{1}{2}$ $3\frac{1}{2}$ $4\frac{1}{2}$	<i>114265.70</i> <i>114327.21</i> <i>114414.64</i> <i>114529.20</i>	61.51 87.43 114.56
$3s^2(^1S)4s$	$4s^2S$	$0\frac{1}{2}$	65500.73		$3s3p(^3P^\circ)4s$	$4s'^4P^\circ$	$0\frac{1}{2}$ $1\frac{1}{2}$ $2\frac{1}{2}$	<i>116862.44</i> <i>116978.44</i> <i>117178.12</i>	116.00 199.68
$3s3p^2$	$3p^2^2S$	$0\frac{1}{2}$	76665.61		$3s^2(^1S)7s$	$7s^2S$	$0\frac{1}{2}$	117915.06	
$3s^2(^1S)3d$	$3d^2D$	$1\frac{1}{2}$ $2\frac{1}{2}$	79338.76 79355.28	16.52	$3s^2(^1S)6d$	$6d^2D$	$1\frac{1}{2}$ $2\frac{1}{2}$	118523.12 118523.19	0.07
$3s^2(^1S)4p$	$4p^2P^\circ$	$0\frac{1}{2}$ $1\frac{1}{2}$	<i>81121.60</i> <i>81251.58</i>	59.98	$3s^2(^1S)7p$	$7p^2P^\circ$	$0\frac{1}{2}$ $1\frac{1}{2}$	<i>119245.48</i> <i>119274.07</i>	28.59
$3s3p^2$	$3p^2^2P$	$0\frac{1}{2}$ $1\frac{1}{2}$	83802.21 84004.52	202.31	$3s^2(^1S)6f$	$6f^2F^\circ$	$3\frac{1}{2}$ $2\frac{1}{2}$	<i>119311.45</i> <i>119311.60</i>	-0.15
$3s^2(^1S)5s$	$5s^2S$	$0\frac{1}{2}$	97972.35		$3s^2(^1S)6g$	$6g^2G$	$3\frac{1}{2}$ $4\frac{1}{2}$	} 119578.49	
$3s^2(^1S)4d$	$4d^2D$	$1\frac{1}{2}$ $2\frac{1}{2}$	101023.31 101024.61	1.30	$3s3p(^3P^\circ)4s$	$4s'^2P^\circ$	$0\frac{1}{2}$ $1\frac{1}{2}$	<i>121444.38</i> <i>121590.45</i>	146.07
$3s^2(^1S)4f$	$4f^2F^\circ$	$3\frac{1}{2}$ $2\frac{1}{2}$	<i>103556.29</i> <i>103556.42</i>	-0.13	$3s^2(^1S)8s$	$8s^2S$	$0\frac{1}{2}$	121814.64	
$3s^2(^1S)5p$	$5p^2P^\circ$	$0\frac{1}{2}$ $1\frac{1}{2}$	<i>103861.00</i> <i>103885.51</i>	24.51	$3s^2(^1S)7d$	$7d^2D$	$1\frac{1}{2}$ $2\frac{1}{2}$	122163.74 122163.80	0.06
$3s3p(^3P^\circ)3d$	$3d'^2D^\circ$	$1\frac{1}{2}$ $2\frac{1}{2}$	<i>108779.0</i> <i>108820.9</i>	41.9	$3s^2(^1S)7f$	$7f^2F^\circ$	$3\frac{1}{2}$ $2\frac{1}{2}$	<i>122655.51</i> <i>122655.63</i>	-0.12
$3s^2(^1S)6s$	$6s^2S$	$0\frac{1}{2}$	111184.72		$3s^2(^1S)7g$	$7g^2G$	$3\frac{1}{2}$ $4\frac{1}{2}$	} 122835.39	
$3s^2(^1S)5d$	$5d^2D$	$1\frac{1}{2}$ $2\frac{1}{2}$	112394.82 112394.98	0.16	$3p^3$	$3p^3^4S^\circ$	$1\frac{1}{2}$	<i>123033.6</i>	
$3s^2(^1S)5f$	$5f^2F^\circ$	$3\frac{1}{2}$ $2\frac{1}{2}$	<i>113760.41</i> <i>113760.58</i>	-0.17					

## Atomic Energy Levels

## Si II—Continued

## Si II—Continued

Config.	Desig.	<i>J</i>	Level	Interval	Config.	Desig.	<i>J</i>	Level	Interval
3s <sup>2</sup> ( <sup>1</sup> S)8p	8p <sup>2</sup> P°	0½ 1½	123097. 89 123138. 93	41. 06	3s 3p( <sup>3</sup> P°)4d	4d' <sup>2</sup> D°	1½ 2½	149871. 5 149928. 3	56. 8
3s <sup>2</sup> ( <sup>1</sup> S)9s	9s <sup>2</sup> S	0½	124277. 0		3s 3p( <sup>3</sup> P°)5s	5s' <sup>4</sup> P°	0½ 1½ 2½	150321. 9 150442. 6 150657. 6	120. 7 215. 0
3s 3p( <sup>3</sup> P°)3d	3d' <sup>4</sup> D°	0½ 1½ 2½ 3½	124337. 4 124325. 4 124317. 0 124449. 6	-12. 0 -8. 4 132. 6	3s 3p( <sup>3</sup> P°)4d	4d' <sup>4</sup> F°	1½ 2½ 3½ 4½	151077. 6 151142. 2 151240. 0 151377. 9	64. 6 97. 8 137. 9
3s <sup>2</sup> ( <sup>1</sup> S)8d	8d <sup>2</sup> D	1½ 2½	124496. 0		3s 3p( <sup>3</sup> P°)5s	5s' <sup>2</sup> P°	0½ 1½	151949. 7	
3s 3p( <sup>3</sup> P°)3d	3d' <sup>4</sup> P°	2½ 1½ 0½	124567. 5 124615. 7 124639. 0	-48. 2 -23. 3	3s 3p( <sup>3</sup> P°)4d	4d' <sup>4</sup> D°	0½ 1½ 2½ 3½	152418. 2 152431. 7 152460. 9 152535. 6	13. 5 29. 2 74. 7
3s <sup>2</sup> ( <sup>1</sup> S)8f	8f <sup>2</sup> F°	3½ 2½	124822. 34 124822. 40	-0. 06	3s 3p( <sup>3</sup> P°)4p	4p' <sup>2</sup> S	0½	152977. 0?	
3s <sup>2</sup> ( <sup>1</sup> S)8g	8g <sup>2</sup> G	3½ 4½	124948. 66		3s 3p( <sup>3</sup> P°)4d	4d' <sup>4</sup> P°	2½ 1½ 0½	153093. 7 153184. 4 153233. 4	-90. 7 -49. 0
3s <sup>2</sup> ( <sup>1</sup> S)9p	9p <sup>2</sup> P°	0½ 1½	125025. 2 125034. 0	8. 8	3s 3p( <sup>3</sup> P°)4d	4d' <sup>2</sup> P°	0½ 1½	153494. 4 153537. 5	43. 1
3s 3p( <sup>3</sup> P°)3d	3d' <sup>2</sup> P°	1½ 0½	126236. 7 126279. 3	-42. 6	3s 3p( <sup>3</sup> P°)4f	4f' <sup>2</sup> F	2½ 3½	155571. 9 155610. 1	38. 2
3s <sup>2</sup> ( <sup>1</sup> S)9f	9f <sup>2</sup> F°	2½ 3½	126305. 08		3s 3p( <sup>3</sup> P°)4f	4f' <sup>4</sup> F	1½ 2½ 3½ 4½	155623. 3 155633. 7 155666. 1 155695. 2	10. 4 32. 4 29. 1
3s <sup>2</sup> ( <sup>1</sup> S)9g	9g <sup>2</sup> G	3½ 4½	126396. 73		3s 3p( <sup>3</sup> P°)4f	4f' <sup>4</sup> G	2½ 3½ 4½ 5½	156676. 3 156811. 2 156811. 2 156955. 7	134. 9 0. 0 144. 5
3s <sup>2</sup> ( <sup>1</sup> S)10p	10p <sup>2</sup> P°	1½ 0½	126526. 1 126545. 7	-19. 6	3s 3p( <sup>3</sup> P°)4f	4f' <sup>2</sup> G	3½ 4½	156683. 2 156963. 4	280. 2
3s <sup>2</sup> ( <sup>1</sup> S)10f	10f <sup>2</sup> F°	2½ 3½	127363. 76		3s 3p( <sup>3</sup> P°)4f	4f' <sup>2</sup> D	1½ 2½	157186. 9? 157191. 7?	4. 8
3s <sup>2</sup> ( <sup>1</sup> S)10g	10g <sup>2</sup> G	3½ 4½	127432. 28		3s 3p( <sup>3</sup> P°)4f	4f' <sup>4</sup> D	3½ 2½ 1½ 0½	157310. 9 157411. 4 157461. 3 157484. 0	-100. 5 -49. 9 -22. 7
3s <sup>2</sup> ( <sup>1</sup> S)11f	11f <sup>2</sup> F°	2½ 3½	128145. 61		3s 3p( <sup>3</sup> P°)5d	5d' <sup>4</sup> F°	1½ 2½ 3½ 4½	163907. 6?	
3s <sup>2</sup> ( <sup>1</sup> S)11g	11g <sup>2</sup> G	3½ 4½	128198. 2		3s 3p( <sup>3</sup> P°)6s	6s' <sup>4</sup> P°	0½ 1½ 2½	164111. 0?	
3s 3p( <sup>3</sup> P°)3d	3d' <sup>2</sup> F°	2½ 3½	131677. 4 131919. 1	241. 7	3s 3p( <sup>3</sup> P°)5d	5d' <sup>4</sup> D°	0½ 1½ 2½ 3½	164844. 0?	
3s 3p( <sup>3</sup> P°)4p	4p' <sup>4</sup> D	0½ 1½ 2½ 3½	131785. 0 131861. 99 131988. 11 132162. 35	76. 99 126. 12 174. 24	3s 3p( <sup>3</sup> P°)5d	5d' <sup>4</sup> P°	0½ 1½ 2½	164966. 0?	
Si III (3s <sup>2</sup> <sup>1</sup> S <sub>0</sub> )	<i>Limit</i>	-----	131838. 4		Si III 3s 3p <sup>3</sup> P <sub>2</sub>	<i>Limit</i>	-----	184953. 0	
3s 3p( <sup>3</sup> P°)4p	4p' <sup>2</sup> P	0½ 1½	132592. 4 132676. 5	84. 1					
3s 3p( <sup>3</sup> P°)4p	4p' <sup>4</sup> P	0½ 1½ 2½	134016. 96 134079. 06 134213. 69	62. 10 134. 63					
3s 3p( <sup>3</sup> P°)4p	4p' <sup>4</sup> S	1½	134905. 34						
3p <sup>3</sup>	3p <sup>3</sup> <sup>2</sup> D°	2½ 1½	135298. 1 135304. 2	-6. 1					
3s 3p( <sup>3</sup> P°)4p	4p' <sup>2</sup> D	1½ 2½	140580 140773	193					
3p <sup>3</sup>	3p <sup>3</sup> <sup>2</sup> P°	1½ 0½	143982. 9 144004. 3	-21. 4					

March 1964.

# Atomic Energy Levels

## Si II OBSERVED TERMS

Configuration $1s^2 2s^2 2p^6 +$	Observed Terms				
	$ns(n \geq 4)$	$np(n \geq 4)$	$nd(n \geq 3)$	$nf(n \geq 4)$	$ng(n \geq 5)$
$3s^2(1S)3p$					
$3s 3p^2$	$3p \ ^2P^\circ$				
$3p^3$	$\begin{Bmatrix} 3p^2 \ ^2S \\ 3p^3 \ ^4S^\circ \end{Bmatrix}$	$\begin{Bmatrix} 3p^2 \ ^4P \\ 3p^2 \ ^2P \end{Bmatrix}$	$3p^2 \ ^2D$		
	$3p^3 \ ^2P^\circ$		$3p^3 \ ^2D^\circ$		
$3s^2(1S)nl$	$ns(n \geq 4)$	$np(n \geq 4)$	$nd(n \geq 3)$	$nf(n \geq 4)$	$ng(n \geq 5)$
$3s 3p(3P^\circ)nl'$	$4-9s \ ^2S$	$4-10p \ ^2P^\circ$	$3-8d \ ^2D$	$4-11f \ ^2F^\circ$	$5-11g \ ^2G$
	$\begin{Bmatrix} 4-6s' \ ^4P^\circ \\ 4,5s' \ ^2P^\circ \end{Bmatrix}$	$\begin{Bmatrix} 4p' \ ^4S \\ 4p' \ ^2S \end{Bmatrix}$ $4p' \ ^4P$ $4p' \ ^2P$ $4p' \ ^4D$ $4p' \ ^2D$	$3-5d' \ ^4P^\circ$ $3,4d' \ ^2P^\circ$ $3-5d' \ ^4D^\circ$ $3,4d' \ ^2D^\circ$ $3-5d' \ ^4F^\circ$ $3d' \ ^2F^\circ$	$4f' \ ^4D$ $4f' \ ^2D$ $4f' \ ^4F$ $4f' \ ^2F$ $4f' \ ^4G$ $4f' \ ^2G$	





# Multiplet Table

Part B

SILICON

Si II (Z=14)

I P 16.35 eV Limit  $131838.4 \pm 0.1 \text{ cm}^{-1}$  758.50 Å (Vac)

Anal A List A February 1964

## REFERENCES

- A A. G. Shenstone, Proc. Roy. Soc. [A] **261**, 153 to 174 (1961). I P, T, C L, I; W L 711 Å to 9412 Å  
P Predicted wavelength.  
New Multiplet Numbers, not inserted between older ones, start with UV 21 and 10.

Si II

Si II

I A.	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Air							Vac						
2334.606	A	30	0.04	5.34	$1\frac{1}{2}-2\frac{1}{2}$	$3p^2 P^\circ - 3p^2 ^4P$	711.83	A	1h	0.04	17.45	$1\frac{1}{2}-2\frac{1}{2}$	$3p^2 P^\circ - 4p^2 ^2D$
2344.203	A	10	0.04	5.32	$1\frac{1}{2}-1\frac{1}{2}$	UV 0.01	711.34	A	0h	0.00	17.43	$0\frac{1}{2}-1\frac{1}{2}$	UV 6.09
2334.404	A	30	0.00	5.31	$0\frac{1}{2}-0\frac{1}{2}$								
2350.174	A	20	0.04	5.31	$1\frac{1}{2}-0\frac{1}{2}$								
Vac													
1816.921	A	200	0.04	6.86	$1\frac{1}{2}-2\frac{1}{2}$	$3p^2 P^\circ - 3p^2 ^2D$	1350.057	A	150	5.34	14.53	$2\frac{1}{2}-2\frac{1}{2}$	$3p^2 ^4P - 4s' ^4P^\circ$
1808.003	A	150	0.00	6.86	$0\frac{1}{2}-1\frac{1}{2}$	UV 1	1350.520	A	20	5.32	14.50	$1\frac{1}{2}-1\frac{1}{2}$	UV 7
1817.445	A	10	0.04	6.86	$1\frac{1}{2}-1\frac{1}{2}$		1350.658	A	20	5.31	14.49	$0\frac{1}{2}-0\frac{1}{2}$	
							1353.718	A	100	5.34	14.50	$2\frac{1}{2}-1\frac{1}{2}$	
							1352.635	A	100	5.32	14.49	$1\frac{1}{2}-0\frac{1}{2}$	
1533.445†	A	1000	0.04	8.12	$1\frac{1}{2}-0\frac{1}{2}$	$3p^2 P^\circ - 4s ^2S$	1346.873	A	100	5.32	14.53	$1\frac{1}{2}-2\frac{1}{2}$	
1526.719	A	500	0.00	8.12	$0\frac{1}{2}-0\frac{1}{2}$	UV 2	1348.543	A	100	5.31	14.50	$0\frac{1}{2}-1\frac{1}{2}$	
1309.274	A	200	0.04	9.51	$1\frac{1}{2}-0\frac{1}{2}$	$3p^2 P^\circ - 3p^2 ^2S$	1251.164	A	200	5.34	15.25	$2\frac{1}{2}-1\frac{1}{2}$	$3p^2 ^4P - 3p^3 ^4S^\circ$
1304.369	A	100	0.00	9.51	$0\frac{1}{2}-0\frac{1}{2}$	UV 3	1248.426	A	150	5.32	15.25	$1\frac{1}{2}-1\frac{1}{2}$	UV 8
							1246.738	A	100	5.31	15.25	$0\frac{1}{2}-1\frac{1}{2}$	
1264.730	A	2000	0.04	9.84	$1\frac{1}{2}-2\frac{1}{2}$	$3p^2 P^\circ - 3d ^2D$	1229.388	A	200	5.34	15.43	$2\frac{1}{2}-3\frac{1}{2}$	$3p^2 ^4P - 3d' ^4D^\circ$
1260.418	A	1000	0.00	9.84	$0\frac{1}{2}-1\frac{1}{2}$	UV 4	1228.746	A	150	5.32	15.41	$1\frac{1}{2}-2\frac{1}{2}$	UV 8.01
1265.023	A	200	0.04	9.84	$1\frac{1}{2}-1\frac{1}{2}$		1226.986	A	40	5.31	15.41	$0\frac{1}{2}-1\frac{1}{2}$	
							1231.406	A	5	5.34	15.41	$2\frac{1}{2}-2\frac{1}{2}$	
1194.496	A	250	0.04	10.41	$1\frac{1}{2}-1\frac{1}{2}$	$3p^2 P^\circ - 3p^2 ^2P$	1228.617	A	25	5.32	15.41	$1\frac{1}{2}-1\frac{1}{2}$	
1193.284	A	200	0.00	10.39	$0\frac{1}{2}-0\frac{1}{2}$	UV 5	1226.814	A	50	5.31	15.42	$0\frac{1}{2}-0\frac{1}{2}$	
1197.389	A	100	0.04	10.39	$1\frac{1}{2}-0\frac{1}{2}$		1228.437	A	10	5.32	15.42	$1\frac{1}{2}-0\frac{1}{2}$	
1190.418	A	100	0.00	10.41	$0\frac{1}{2}-1\frac{1}{2}$								
1023.693	A	50	0.04	12.15	$1\frac{1}{2}-0\frac{1}{2}$	$3p^2 P^\circ - 5s ^2S$	1227.604	A	100	5.34	15.44	$2\frac{1}{2}-2\frac{1}{2}$	$3p^2 ^4P - 3d' ^4P^\circ$
1020.699	A	25	0.00	12.15	$0\frac{1}{2}-0\frac{1}{2}$	UV 5.01	1224.252	A	20	5.32	15.45	$1\frac{1}{2}-1\frac{1}{2}$	UV 8.02
							1222.288	A	0	5.31	15.45	$0\frac{1}{2}-0\frac{1}{2}$	
992.675	A	200	0.04	12.53	$1\frac{1}{2}-2\frac{1}{2}$	$3p^2 P^\circ - 4d ^2D$	1226.887	A	20	5.34	15.45	$2\frac{1}{2}-1\frac{1}{2}$	
989.867	A	100	0.00	12.52	$0\frac{1}{2}-1\frac{1}{2}$	UV 6	1223.907	A	20	5.32	15.45	$1\frac{1}{2}-0\frac{1}{2}$	
							1224.972	A	10	5.32	15.44	$1\frac{1}{2}-2\frac{1}{2}$	
901.735	A	20	0.04	13.78	$1\frac{1}{2}-0\frac{1}{2}$	$3p^2 P^\circ - 6s ^2S$	1222.635	A	5	5.31	15.45	$0\frac{1}{2}-1\frac{1}{2}$	
899.405	A	10	0.00	13.78	$0\frac{1}{2}-0\frac{1}{2}$	UV 6.01							
							929.810	A	20	5.34	18.68	$2\frac{1}{2}-2\frac{1}{2}$	$3p^2 ^4P - 5s' ^4P^\circ$
891.999	A	200	0.04	13.93	$1\frac{1}{2}-2\frac{1}{2}$	$3p^2 P^\circ - 5d ^2D$	930.242	A	0	5.31	18.64	$0\frac{1}{2}-0\frac{1}{2}$	UV 8.03
889.722	A	100	0.00	13.93	$0\frac{1}{2}-1\frac{1}{2}$	UV 6.02	931.667	A	5	5.34	18.65	$2\frac{1}{2}-1\frac{1}{2}$	
							931.200	A	5	5.32	18.64	$1\frac{1}{2}-0\frac{1}{2}$	
850.142	A	10	0.04	14.62	$1\frac{1}{2}-0\frac{1}{2}$	$3p^2 P^\circ - 7s ^2S$	928.297	A	5	5.32	18.68	$1\frac{1}{2}-2\frac{1}{2}$	
848.074	A	5	0.00	14.62	$0\frac{1}{2}-0\frac{1}{2}$	UV 6.03	929.206	A	1	5.31	18.65	$0\frac{1}{2}-1\frac{1}{2}$	
845.774	A	40h	0.04	14.69	$1\frac{1}{2}-2\frac{1}{2}$	$3p^2 P^\circ - 6d ^2D$	913.853	A	20	5.34	18.91	$2\frac{1}{2}-3\frac{1}{2}$	$3p^2 ^4P - 4d' ^4D^\circ$
843.718	A	20h	0.00	14.69	$0\frac{1}{2}-1\frac{1}{2}$	UV 6.04	913.012	A	10	5.32	18.90	$1\frac{1}{2}-2\frac{1}{2}$	UV 8.04
							912.375	A	5	5.31	18.90	$0\frac{1}{2}-1\frac{1}{2}$	
822.844	A	5h	0.04	15.10	$1\frac{1}{2}-0\frac{1}{2}$	$3p^2 P^\circ - 8s ^2S$	914.476	A	2	5.34	18.90	$2\frac{1}{2}-2\frac{1}{2}$	
820.918	A	3h	0.00	15.10	$0\frac{1}{2}-0\frac{1}{2}$	UV 6.05	913.264	A	3	5.32	18.90	$1\frac{1}{2}-1\frac{1}{2}$	
							912.459	A	5	5.31	18.90	$0\frac{1}{2}-0\frac{1}{2}$	
820.516	A	20h	0.04	15.15	$1\frac{1}{2}-2\frac{1}{2}$	$3p^2 P^\circ - 7d ^2D$	909.209	A	3	5.34	18.98	$2\frac{1}{2}-2\frac{1}{2}$	$3p^2 ^4P - 4d' ^4P^\circ$
818.590	A	2h	0.00	15.15	$0\frac{1}{2}-1\frac{1}{2}$	UV 6.06	907.033	A	0	5.32	18.99	$1\frac{1}{2}-1\frac{1}{2}$	UV 8.05
							905.71	A	0	5.31	19.00	$0\frac{1}{2}-0\frac{1}{2}$	
805.101	A	10h	0.04	15.44	$1\frac{1}{2}-$	$3p^2 P^\circ - 8d ^2D$	908.461	A	1	5.34	18.99	$2\frac{1}{2}-1\frac{1}{2}$	
803.234	A	3h	0.00	15.44	$0\frac{1}{2}-1\frac{1}{2}$	UV 6.07	906.586	A	1	5.32	19.00	$1\frac{1}{2}-0\frac{1}{2}$	
							907.762	A	0	5.32	18.98	$1\frac{1}{2}-2\frac{1}{2}$	
755.362	A	2	0.04	16.45	$1\frac{1}{2}-1\frac{1}{2}$	$3p^2 P^\circ - 4p ^2P$	906.126	A	0	5.31	18.99	$0\frac{1}{2}-1\frac{1}{2}$	
						UV 6.08							

## Si II—Continued

## Multiplet Table

## Si II—Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac 826.42	A	1h	5.34	20.35	2½—2½	3p <sup>2</sup> 4P —6s' 4P°?	Vac 1127.907 1127.442	A	40h 20h	6.86 6.86	17.85 17.85	2½—1½ 1½—0½	3p <sup>2</sup> 2D —3p <sup>3</sup> 2P° UV 13.06
821.450	A	2h	5.34	20.44	2½—3½	3p <sup>2</sup> 4P —5d' 4D°?	1057.050 1057.503 1057.690 1056.899	A A A A	30 15 2 2	6.86 6.86 6.86 6.86	18.59 18.58 18.58 18.59	2½—2½ 1½—1½ 2½—1½ 1½—2½	3p <sup>2</sup> 2D —4d' 2D° UV 13.07
820.63 819.49	A A	3h 0h	5.34 5.32	20.45 20.45	2½—2½ 1½—2½?	3p <sup>2</sup> 4P —5d' 4P°? UV 8.08	1034.967	A	0?	6.86	18.84	2½—1½	3p <sup>2</sup> 2D —5s' 2P°? UV 13.08
Air 3856.017 3862.595 3853.664	A A A	500h 200h 100h	6.86 6.86 6.86	10.07 10.07 10.07	2½—1½ 1½—0½ 1½—1½	3p <sup>2</sup> 2D —4p 2P° 1	Air 6347.103 6371.359	A A	1000 1000	8.12 8.12	10.07 10.07	0½—1½ 0½—0½	4s 2S —4p 2P° 2
2072.701 2072.016	A A	200 200	6.86 6.86	12.84 12.84	2½—3½ 1½—2½	3p <sup>2</sup> 2D —4f 2F° UV 9	2604.422 2606.084	A A	(2) (1)	8.12 8.12	12.88 12.88	0½—1½ 0½—0½	4s 2S —5p 2P° UV 15
2058.646 2059.014 2057.965	A A A	50 50 (2)	6.86 6.86 6.86	12.88 12.88 12.88	2½—1½ 1½—0½ 1½—1½	3p <sup>2</sup> 2D —5p 2P° UV 9.01	2346.234	A	0H	9.51	14.79	0½—1½	3p <sup>2</sup> 2S —7p 2P° UV 15.01
Vac 1869.317 1870.227 1870.782 1868.765	A A A A	20 15 3 1	6.86 6.86 6.86 6.86	13.49 13.49 13.49 13.49	2½—2½ 1½—1½ 2½—1½ 1½—2½	3p <sup>2</sup> 2D —3d 2D° UV 9.02	2225.267	A	(1)	9.51	15.07	0½—1½	3p <sup>2</sup> 2S —4s' 2P° UV 15.02
1711.296 1710.826	A A	20h 10h	6.86 6.86	14.10 14.10	2½—3½ 1½—2½	3p <sup>2</sup> 2D —5f 2F° UV 10	2016.654 2014.92	A A	3h 0h	9.51 9.51	15.65 15.66	0½—1½ 0½—0½	3p <sup>2</sup> 2S —3d' 2P° UV 15.03
1704.967	A	2h	6.86	14.13	1½—0½	3p <sup>2</sup> 2D —6p 2P° UV 10.01	Vac 1485.513 1485.024	A A	100hp 90hp	9.51 9.51	17.85 17.85	0½—1½ 0½—0½	3p <sup>2</sup> 2S —3p <sup>3</sup> 2P° UV 15.04
1563.765 1564.066	A A	10 5	6.86 6.86	14.79 14.78	2½—1½ 1½—0½	3p <sup>2</sup> 2D —7p 2P° UV 10.02	Air 4130.893 4128.067	A A	500H 300H	9.84 9.84	12.84 12.84	2½—3½ 1½—2½	3d 2D —4f 2F° 3
1562.845 1562.451	A A	15 10	6.86 6.86	14.79 14.79	2½—3½ 1½—2½	3p <sup>2</sup> 2D —6f 2F° UV 11	4075.451 4076.781 4072.711	A A A	20H 15H 3h	9.84 9.84 9.84	12.88 12.88 12.88	2½—1½ 1½—0½ 1½—1½	3d 2D —5p 2P° 3.01
1509.101 1512.072 1508.741	A A A	100h 50h 3h	6.86 6.86 6.86	15.07 15.06 15.07	2½—1½ 1½—0½ 1½—1½	3p <sup>2</sup> 2D —4s 2P° UV 11.01	2905.692 2904.283	A A	500 300	9.84 9.84	14.10 14.10	2½—3½ 1½—2½	3d 2D —5f 2F° UV 17
1485.224 1484.873	A A	30 15	6.86 6.86	15.21 15.21	2½—3½ 1½—2½	3p <sup>2</sup> 2D —7f 2F° UV 12	2887.511 2887.358 2886.133	A A A	10h 5h (1)	9.84 9.84 9.84	14.13 14.13 14.13	2½—1½ 1½—0½ 1½—1½	3d 2D —6p 2P° UV 17.01
1476.928	A	1	6.86	15.25	2½—1½	3p <sup>2</sup> 2D —3p <sup>3</sup> 4S° UV 12.01	2851.456 2857.231 2858.514	A A A	(2) (1) (1)	9.84 9.84 9.84	14.19 14.17 14.17	2½—3½ 1½—2½ 2½—2½	3d 2D —3d' 4F° UV 17.02
1474.649 1475.188 1474.304	A A A	15h 5h 1h	6.86 6.86 6.86	15.27 15.26 15.27	2½—1½ 1½—0½ 1½—1½	3p <sup>2</sup> 2D —8p 2P° UV 12.02	2504.331 2505.091	A A	2h 2h	9.84 9.84	14.79 14.78	2½—1½ 1½—0½	3d 2D —7p 2P° UV 17.03
1438.931 1438.576	A A	4h 2h	6.86 6.86	15.48 15.48	2½—3½ 1½—2½	3p <sup>2</sup> 2D —8f 2F° UV 13	2501.970 2500.928	A A	5h 3h	9.84 9.84	14.79 14.79	2½—3½ 1½—2½	3d 2D —6f 2F° UV 18
1434.542 1434.400	A A	2h 1h	6.86 6.86	15.50 15.50	2½—1½ 1½—0½	3p <sup>2</sup> 2D —9p 2P° UV 13.01	2366.972 2374.255 2366.053	A A A	5h 5h (5)	9.84 9.84 9.84	15.07 15.06 15.07	2½—1½ 1½—0½ 1½—1½	3d 2D —4s' 2P° UV 18.01
1410.219 1409.073 1409.90	A A A	20h 10h 2h	6.86 6.86 6.86	15.65 15.66 15.65	2½—1½ 1½—0½ 1½—1½	3p <sup>2</sup> 2D —3d' 2P° UV 13.02	2307.863	A	(2)	9.84	15.21	1½—2½	3d 2D —7f 2F° UV 18.02
1404.478 1403.783 1404.170	A A A	6h 5h 1h	6.86 6.86 6.86	15.69 15.69 15.69	2½—1½ 1½—0½ 1½—1½	3p <sup>2</sup> 2D —10p 2P° UV 13.03	2283.266 2284.542	A A	(3) (1)	9.84 9.84	15.27 15.26	2½—1½ 1½—0½	3d 2D —8p 2P° UV 18.03
1305.590 1309.458 1309.77	A A A	50h 20h 2h	6.86 6.86 6.86	16.36 16.33 16.33	2½—3½ 1½—2½ 2½—2½	3p <sup>2</sup> 2D —3d' 2F° UV 13.04	Vac 1902.459 1910.621 1911.265	A A A	100h 50h 0h	9.84 9.84 9.84	16.36 16.33 16.33	2½—3½ 1½—2½ 2½—2½	3d 2D —3d' 2F° UV 18.04
1250.433 1250.089	A A	150 100	6.86 6.86	16.77 16.78	2½—2½ 1½—1½	3p <sup>2</sup> 2D —3p <sup>3</sup> 2D° UV 13.05							



Multiplet Table

Si II—Continued

Si II—Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac							Air						
1787.538	A	8	9.84	16.77	$2\frac{1}{2}-2\frac{1}{2}$	$3d^2D - 3p^3^2D^\circ$	4232.864	A	(10)	12.15	15.07	$0\frac{1}{2}-1\frac{1}{2}$	$5s^2S - 4s'^2P^\circ$
1786.817	A	4	9.84	16.78	$1\frac{1}{2}-1\frac{1}{2}$	UV 18.05	4259.202	A	(5)	12.15	15.06	$0\frac{1}{2}-0\frac{1}{2}$	7.01
1416.972	A	10h	9.84	18.59	$2\frac{1}{2}-2\frac{1}{2}$	$3d^2D - 4d'^2D^\circ$							
1417.781	A	5	9.84	18.58	$1\frac{1}{2}-1\frac{1}{2}$	UV 18.06							
1418.110	A	0	9.84	18.58	$2\frac{1}{2}-1\frac{1}{2}$		7849.72	A	(500)	12.53	14.10	$2\frac{1}{2}-3\frac{1}{2}$	$4d^2D - 5f^2F^\circ$
							7848.80	A	(400)	12.52	14.10	$1\frac{1}{2}-2\frac{1}{2}$	7.02
Air							5466.868	A	500H	12.53	14.79	$2\frac{1}{2}-3\frac{1}{2}$	$4d^2D - 6f^2F^\circ$
5978.929	A	500	10.07	12.15	$1\frac{1}{2}-0\frac{1}{2}$	$4p^2P^\circ - 5s^2S$	5466.432	A	500H	12.52	14.79	$1\frac{1}{2}-2\frac{1}{2}$	7.03
5957.561	A	500	10.07	12.15	$0\frac{1}{2}-0\frac{1}{2}$	4	4861.095	A	(10)	12.53	15.07	$2\frac{1}{2}-1\frac{1}{2}$	$4d^2D - 4s'^2P^\circ$
							4895.558	A	0h	12.52	15.06	$1\frac{1}{2}-0\frac{1}{2}$	7.04
5055.981	A	1000	10.07	12.53	$1\frac{1}{2}-2\frac{1}{2}$	$4p^2P^\circ - 4d^2D$	4621.721	A	(150)	12.53	15.21	$2\frac{1}{2}-3\frac{1}{2}$	$4d^2D - 7f^2F^\circ$
5041.026	A	1000	10.07	12.52	$0\frac{1}{2}-1\frac{1}{2}$	5	4621.418	A	(100)	12.52	15.21	$1\frac{1}{2}-2\frac{1}{2}$	7.05
5056.314	A	(30)	10.07	12.52	$1\frac{1}{2}-1\frac{1}{2}$								
3339.819	A	500	10.07	13.78	$1\frac{1}{2}-0\frac{1}{2}$	$4p^2P^\circ - 6s^2S$	4200.898	A	(40)	12.53	15.48	$2\frac{1}{2}-3\frac{1}{2}$	$4d^2D - 8f^2F^\circ$
3333.139	A	300	10.07	13.78	$0\frac{1}{2}-0\frac{1}{2}$	6	4200.657	A	(30)	12.52	15.48	$1\frac{1}{2}-2\frac{1}{2}$	7.06
3210.025	A	200HH	10.07	13.93	$1\frac{1}{2}-2\frac{1}{2}$	$4p^2P^\circ - 5d^2D$	3954.507	A	(10)	12.53	15.66	$2\frac{1}{2}-3\frac{1}{2}$	$4d^2D - 9f^2F^\circ$
3203.872	A	100HH	10.07	13.93	$0\frac{1}{2}-1\frac{1}{2}$	7	3954.296	A	(5)	12.52	15.66	$1\frac{1}{2}-2\frac{1}{2}$	7.07
2726.702	A	5h	10.07	14.62	$1\frac{1}{2}-0\frac{1}{2}$	$4p^2P^\circ - 7s^2S$	3795.553	A	(1)	12.53	15.79	$2\frac{1}{2}-3\frac{1}{2}$	$4d^2D - 10f^2F^\circ$
2722.250	A	2h	10.07	14.62	$0\frac{1}{2}-0\frac{1}{2}$	UV 19	3795.362	A	(3)	12.52	15.79	$1\frac{1}{2}-2\frac{1}{2}$	7.08
2682.210	A	10h	10.07	14.69	$1\frac{1}{2}-2\frac{1}{2}$	$4p^2P^\circ - 6d^2D$	3686.133	A	(2)	12.53	15.89	$2\frac{1}{2}-3\frac{1}{2}$	$4d^2D - 11f^2F^\circ$
2677.906	A	3h	10.07	14.69	$0\frac{1}{2}-1\frac{1}{2}$	UV 20	3685.950	A	(1)	12.52	15.89	$1\frac{1}{2}-2\frac{1}{2}$	7.09
2439.953	A	0H	10.07	15.15	$0\frac{1}{2}-1\frac{1}{2}$	$4p^2P^\circ - 7d^2D$	3235.92	A	(2H)	12.53	16.36	$2\frac{1}{2}-3\frac{1}{2}$	$4d^2D - 3d'^2F^\circ$
						UV 21							7.10
2311.719	A	(1)	10.07	15.44	$1\frac{1}{2}-$	$4p^2P^\circ - 8d^2D$	Vac						
						UV 22	1904.326	A	5h	12.53	19.04	$2\frac{1}{2}-1\frac{1}{2}$	$4d^2D - 4d'^2P^\circ$
Vac							1905.878	A	3h	12.52	19.03	$1\frac{1}{2}-0\frac{1}{2}$	UV 31
1944.586	A	15	10.07	16.45	$1\frac{1}{2}-1\frac{1}{2}$	$4p^2P^\circ - 4p'^2P$							
1945.504	A	3	10.07	16.44	$0\frac{1}{2}-0\frac{1}{2}$	UV 23							
1947.769	A	1	10.07	16.44	$1\frac{1}{2}-0\frac{1}{2}$		Air						
							9412.72	A	100	12.84	14.16		$4f^2F^\circ - 5g^2G$
Air													7.11
2834.472	A	3h	10.41	14.79	$1\frac{1}{2}-1\frac{1}{2}$	$3p^2^2P - 7p^2P^\circ$	6679.65	A	(2)	12.84	14.69		$4f^2F^\circ - 6d^2D$
2820.580	A	2h	10.39	14.78	$0\frac{1}{2}-0\frac{1}{2}$	UV 24							7.12
2836.765	A	(1)	10.41	14.78	$1\frac{1}{2}-0\frac{1}{2}$		6239.630	A	(100)	12.84	14.83		$4f^2F^\circ - 6g^2G$
2818.302	A	(2)	10.39	14.79	$0\frac{1}{2}-1\frac{1}{2}$								7.13
2659.781	A	5h	10.41	15.07	$1\frac{1}{2}-1\frac{1}{2}$	$3p^2^2P - 4s'^2P^\circ$	5185.535	A	(100)	12.84	15.23		$4f^2F^\circ - 7g^2G$
2655.803	A	3h	10.39	15.06	$0\frac{1}{2}-0\frac{1}{2}$	UV 25							7.14
2670.153	A	0h	10.41	15.06	$1\frac{1}{2}-0\frac{1}{2}$		4673.273	A	(20)	12.84	15.49		$4f^2F^\circ - 8g^2G$
2645.539	A	0h	10.39	15.07	$0\frac{1}{2}-1\frac{1}{2}$								7.15
2554.530	A	(10)	10.41	15.27	$1\frac{1}{2}-1\frac{1}{2}$	$3p^2^2P - 8p^2P^\circ$	4376.957	A	(5h)	12.84	15.67		$4f^2F^\circ - 9g^2G$
2544.046	A	(3)	10.39	15.26	$0\frac{1}{2}-0\frac{1}{2}$	UV 26							7.16
2557.206	A	(1)	10.41	15.26	$1\frac{1}{2}-0\frac{1}{2}$		4187.137	A	(5h)	12.84	15.80		$4f^2F^\circ - 10g^2G$
2541.393	A	(2)	10.39	15.27	$0\frac{1}{2}-1\frac{1}{2}$								7.17
Vac							4056.993	A	(2h)	12.84	15.89		$4f^2F^\circ - 11g^2G$
1949.564	A	100	10.41	16.77	$1\frac{1}{2}-2\frac{1}{2}$	$3p^2^2P - 3p^3^2D^\circ$							7.18
1941.667	A	50	10.39	16.78	$0\frac{1}{2}-1\frac{1}{2}$	UV 27							
1949.331	A	10	10.41	16.78	$1\frac{1}{2}-1\frac{1}{2}$								
1667.267	A	0	10.41	17.85	$1\frac{1}{2}-1\frac{1}{2}$	$3p^2^2P - 3p^3^2P^\circ$							
1661.059	A	3h	10.39	17.85	$0\frac{1}{2}-0\frac{1}{2}$	UV 28							
1661.633	A	1h	10.39	17.85	$0\frac{1}{2}-1\frac{1}{2}$		7125.84	A	(4)	12.88	14.62	$1\frac{1}{2}-0\frac{1}{2}$	$5p^2P^\circ - 7s^2S$
							7113.45	A	(2)	12.88	14.62	$0\frac{1}{2}-0\frac{1}{2}$	7.19
1516.910	A	60p	10.41	18.59	$1\frac{1}{2}-2\frac{1}{2}$	$3p^2^2P - 4d'^2D^\circ$							
1513.570	A	30p	10.39	18.58	$0\frac{1}{2}-1\frac{1}{2}$	UV 29							
1518.221	A	5p	10.41	18.58	$1\frac{1}{2}-1\frac{1}{2}$		6829.82	A	(40)	12.88	14.69	$1\frac{1}{2}-2\frac{1}{2}$	$5p^2P^\circ - 6d^2D$
							6818.45	A	(20)	12.88	14.69	$0\frac{1}{2}-1\frac{1}{2}$	7.20
1471.775	A	2	10.41	18.84	$1\frac{1}{2}-1\frac{1}{2}$	$3p^2^2P - 5s'^2P^\circ$							
						UV 30	5575.973	A	(5)	12.88	15.10	$1\frac{1}{2}-0\frac{1}{2}$	$5p^2P^\circ - 8s^2S$
							5568.355	A	(2)	12.88	15.10	$0\frac{1}{2}-0\frac{1}{2}$	7.21

Si II—Continued

Multiplet Table

Si II—Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Air							Air						
5469.450	A	(30)	12.88	15.15	$1\frac{1}{2}-2\frac{1}{2}$	$5p\ ^2P^\circ -7d\ ^2D$	2349.54	A	10H	14.19	19.46	$3\frac{1}{2}-4\frac{1}{2}$	$3d'\ ^4F^\circ -4f'\ ^2G$
5462.146	A	(10)	12.88	15.15	$0\frac{1}{2}-1\frac{1}{2}$	7.22	2360.20	A	10H	14.17	19.43	$2\frac{1}{2}-3\frac{1}{2}$	UV 36
4902.65	A	(3h)	12.88	15.41	$1\frac{1}{2}-0\frac{1}{2}$	$5p\ ^2P^\circ -9s\ ^2S$	2365.06	A	2h	14.19	19.43	$3\frac{1}{2}-3\frac{1}{2}$	
						7.23	2336.730	A	2h	14.20	19.50	$4\frac{1}{2}-3\frac{1}{2}$	$3d'\ ^4F^\circ -4f'\ ^4D$
4850.550	A	(5h)	12.88	15.44	$1\frac{1}{2}-2\frac{1}{2}$	$5p\ ^2P^\circ -8d\ ^2D$	2325.04	P		14.19	19.52	$3\frac{1}{2}-2\frac{1}{2}$	UV 37
4844.82	A	(2h)	12.88	15.44	$0\frac{1}{2}-1\frac{1}{2}$	7.24	2317.64	P		14.17	19.52	$2\frac{1}{2}-1\frac{1}{2}$	
3472.43	A	2h	12.88	16.45	$1\frac{1}{2}-1\frac{1}{2}$	$5p\ ^2P^\circ -4p'\ ^2P$	2313.100	A	(0?)	14.17	19.53	$1\frac{1}{2}-0\frac{1}{2}$	
3479.538	A	2	12.88	16.44	$0\frac{1}{2}-0\frac{1}{2}$	7.25							
							6671.88	A	100	14.53	16.39	$2\frac{1}{2}-3\frac{1}{2}$	$4s'\ ^4P^\circ -4p'\ ^4D$
							6660.52	A	50h	14.50	16.36	$1\frac{1}{2}-2\frac{1}{2}$	7.34
							6665.00	A	15	14.49	16.35	$0\frac{1}{2}-1\frac{1}{2}$	
4190.724	A	100h	13.49	16.45	$2\frac{1}{2}-1\frac{1}{2}$	$3d'\ ^2D^\circ -4p'\ ^2P$	6750.28	A	20h	14.53	16.36	$2\frac{1}{2}-2\frac{1}{2}$	
4198.133	A	50	13.49	16.44	$1\frac{1}{2}-0\frac{1}{2}$	7.26	6717.04	A	50h	14.50	16.35	$1\frac{1}{2}-1\frac{1}{2}$	
4183.345	A	10h	13.49	16.45	$1\frac{1}{2}-1\frac{1}{2}$		6699.38	A	20	14.49	16.34	$0\frac{1}{2}-0\frac{1}{2}$	
3128.77	A	1	13.49	17.45	$2\frac{1}{2}-2\frac{1}{2}$	$3d'\ ^2D^\circ -4p'\ ^2D$	6808.19	A	2h	14.53	16.35	$2\frac{1}{2}-1\frac{1}{2}$	
						7.27	6751.88	A	5	14.50	16.34	$1\frac{1}{2}-0\frac{1}{2}$	
2136.560	A	50h	13.49	19.29	$2\frac{1}{2}-3\frac{1}{2}$	$3d'\ ^2D^\circ -4f'\ ^2F$	5868.404	A	300h	14.53	16.64	$2\frac{1}{2}-2\frac{1}{2}$	$4s'\ ^4P^\circ -4p'\ ^4P$
2136.402	A	30h	13.49	19.29	$1\frac{1}{2}-2\frac{1}{2}$	UV 32	5846.134	A	50	14.50	16.62	$1\frac{1}{2}-1\frac{1}{2}$	8
2133.99	A	10h	13.49	19.30	$2\frac{1}{2}-3\frac{1}{2}$	$3d'\ ^2D^\circ -4f'\ ^4F$	5827.801	A	30	14.49	16.62	$0\frac{1}{2}-0\frac{1}{2}$	
						UV 33	5915.220	A	150	14.53	16.62	$2\frac{1}{2}-1\frac{1}{2}$	
							5867.483	A	10	14.50	16.62	$1\frac{1}{2}-0\frac{1}{2}$	
							5800.468	A	150h	14.50	16.64	$1\frac{1}{2}-2\frac{1}{2}$	
							5806.738	A	200	14.49	16.62	$0\frac{1}{2}-1\frac{1}{2}$	
8044.50	A	(15)	13.93	15.48		$5d\ ^2D -8f\ ^2F^\circ$	5639.478	A	200h	14.53	16.73	$2\frac{1}{2}-1\frac{1}{2}$	$4s'\ ^4P^\circ -4p'\ ^4S$
						7.28	5576.661	A	150h	14.50	16.73	$1\frac{1}{2}-1\frac{1}{2}$	9
							5540.74	A	100h	14.49	16.73	$0\frac{1}{2}-1\frac{1}{2}$	
7187.04	A	(2)	13.93	15.66		$5d\ ^2D -9f\ ^2F^\circ$							
						7.29							
7911.47	A	(10h)	14.10	15.67		$5f\ ^2F^\circ -9g\ ^2G$	7490.33	A	(1)	14.78	16.44	$0\frac{1}{2}-0\frac{1}{2}$	$7p\ ^2P^\circ -4p'\ ^2P?$
						7.30							10
7312.29	A	(3h)	14.10	15.80		$5f\ ^2F^\circ -10g\ ^2G$	3185.99	A	(10h)	15.07	18.97	$1\frac{1}{2}-0\frac{1}{2}$	$4s'\ ^2P^\circ -4p'\ ^2S$
						7.31	3170.40	A	1h	15.06	18.97	$0\frac{1}{2}-0\frac{1}{2}$	11
6924.53	A	(0H)	14.10	15.89		$5f\ ^2F^\circ -11g\ ^2G$							
						7.32	3208.25	A	(2)	15.43	19.29	$3\frac{1}{2}-3\frac{1}{2}$	$3d'\ ^4D^\circ -4f'\ ^2F$
							3194.69	A	50	15.41	19.29	$2\frac{1}{2}-3\frac{1}{2}$	12
5669.562	A	1000h	14.20	16.39	$4\frac{1}{2}-3\frac{1}{2}$	$3d'\ ^4F^\circ -4p'\ ^4D$	3199.514	A	200	15.43	19.30	$3\frac{1}{2}-4\frac{1}{2}$	$3d'\ ^4D^\circ -4f'\ ^4F$
5688.811	A	300h	14.19	16.36	$3\frac{1}{2}-2\frac{1}{2}$	7.33	3188.97	A	150	15.41	19.30	$2\frac{1}{2}-3\frac{1}{2}$	13
5701.374	A	200h	14.17	16.35	$2\frac{1}{2}-1\frac{1}{2}$		3193.09	A	150	15.41	19.30	$1\frac{1}{2}-2\frac{1}{2}$	
5706.370	A	100h	14.17	16.34	$1\frac{1}{2}-0\frac{1}{2}$		3195.41	A	100	15.42	19.29	$0\frac{1}{2}-1\frac{1}{2}$	
5632.973	A	100h	14.19	16.39	$3\frac{1}{2}-3\frac{1}{2}$		3202.49	A	20	15.43	19.30	$3\frac{1}{2}-3\frac{1}{2}$	
5660.656	A	150h	14.17	16.36	$2\frac{1}{2}-2\frac{1}{2}$		3192.25	A	50	15.41	19.30	$2\frac{1}{2}-2\frac{1}{2}$	
5681.44	A	30h	14.17	16.35	$1\frac{1}{2}-1\frac{1}{2}$		3194.21	A	50	15.41	19.29	$1\frac{1}{2}-1\frac{1}{2}$	
5605.351	A	3h	14.17	16.39	$2\frac{1}{2}-3\frac{1}{2}$		3205.77	A	(1)	15.43	19.30	$3\frac{1}{2}-2\frac{1}{2}$	
5641.01	A	2h	14.17	16.36	$1\frac{1}{2}-2\frac{1}{2}$								
2428.45	A	10h	14.20	19.30	$4\frac{1}{2}-4\frac{1}{2}$	$3d'\ ^4F^\circ -4f'\ ^4F$	3042.191	A	30h	15.43	19.50	$3\frac{1}{2}-3\frac{1}{2}$	$3d'\ ^4D^\circ -4f'\ ^4D$
2423.42	A	3h	14.19	19.30	$3\frac{1}{2}-3\frac{1}{2}$	UV 34	3020.78	P		15.41	19.52	$2\frac{1}{2}-2\frac{1}{2}$	14
2420.19	A	3h	14.17	19.30	$2\frac{1}{2}-2\frac{1}{2}$		3017.00	P		15.41	19.52	$1\frac{1}{2}-1\frac{1}{2}$	
2417.20	A	2h	14.17	19.29	$1\frac{1}{2}-1\frac{1}{2}$		3015.980	A	(3)	15.42	19.53	$0\frac{1}{2}-0\frac{1}{2}$	
2421.72	A	3h	14.19	19.30	$3\frac{1}{2}-4\frac{1}{2}$		3032.85	A	2H	15.43	19.52	$3\frac{1}{2}-2\frac{1}{2}$	
2418.29	A	2h	14.17	19.30	$2\frac{1}{2}-3\frac{1}{2}$		3014.920	A	(3)	15.41	19.53	$1\frac{1}{2}-0\frac{1}{2}$	
2416.60	A	1h	14.17	19.30	$1\frac{1}{2}-2\frac{1}{2}$		3030.000	A	100h	15.41	19.50	$2\frac{1}{2}-3\frac{1}{2}$	
							3021.55	A	20H	15.41	19.52	$1\frac{1}{2}-2\frac{1}{2}$	
							3018.04	A	2H	15.42	19.52	$0\frac{1}{2}-1\frac{1}{2}$	
2356.295	A	100H	14.20	19.46	$4\frac{1}{2}-5\frac{1}{2}$	$3d'\ ^4F^\circ -4f'\ ^4G$							
2357.97	A	50H	14.19	19.44	$3\frac{1}{2}-4\frac{1}{2}$	UV 35	3220.44	A	10	15.44	19.29	$2\frac{1}{2}-3\frac{1}{2}$	$3d'\ ^4P^\circ -4f'\ ^2F$
2353.09	A	20H	14.17	19.44	$2\frac{1}{2}-3\frac{1}{2}$								15
2357.18	A	30H	14.17	19.42	$1\frac{1}{2}-2\frac{1}{2}$								
2364.33	A	3h	14.20	19.44	$4\frac{1}{2}-4\frac{1}{2}$								
2357.96	P	Si II	14.19	19.44	$3\frac{1}{2}-3\frac{1}{2}$								
2360.59	A	5h	14.17	19.42	$2\frac{1}{2}-2\frac{1}{2}$								



Multiplet Table

Si II—Continued

Si II—Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Air							Air						
3214.66	A	75	15.44	19.30	2½—3½	3d' 4P°—4f' 4F	5794.90	A	30H	16.45	18.59	1½—2½	4p' 2P—4d' 2D°
3223.01	A	20	15.45	19.30	1½—2½	16	5785.73	A	30h	16.44	18.58	0½—1½	27
3217.99	A	15h	15.44	19.30	2½—2½		5813.99	A	1H	16.45	18.58	1½—1½	
3224.13	A	1	15.45	19.29	1½—1½								
3053.184	A	150h	15.44	19.50	2½—3½	3d' 4P°—4f' 4D	4792.29	A	5h	16.45	19.04	1½—1½	4p' 2P—4d' 2P°
3048.30	A	50H	15.45	19.52	1½—2½	17	4782.89	A	3h	16.44	19.03	0½—0½	28
3045.77	A	10H	15.45	19.52	0½—1½								
3043.85	A	10H	15.44	19.52	2½—2½								
*3043.692	A	100hh	15.45	19.52	1½—1½		6080.06	A	20H	16.64	18.68	2½—2½	4p' 4P—5s' 4P°
*3043.692	A	100hh	15.45	19.53	0½—0½		6019.76	A	4H	16.62	18.65	1½—1½	29
3039.21	A	3H	15.44	19.52	2½—1½		6131.76	A	4H	16.62	18.64	0½—0½	
3041.573	A	20H	15.45	19.53	1½—0½		6160.16	A	5H	16.64	18.65	2½—1½	
							6155.17	A	5H	16.62	18.64	1½—0½	
							6030.27	A	5H	16.62	18.68	1½—2½	
							6086.67	A	10H	16.62	18.65	0½—1½	
3125.26	A	1	15.48	19.44	—3½	8f 2F°—4f' 4G	5456.45	A	100H	16.64	18.91	2½—3½	4p' 4P—4d' 4D°
3138.21	A	(3)	15.48	19.42	—2½?	18	5438.62	A	100h	16.62	18.90	1½—2½	30
							5428.92	A	15H	16.62	18.90	0½—1½	
4016.22	A	5HH	16.36	19.44	3½—4½	3d' 2F°—4f' 4G	5478.73	A	5H	16.64	18.90	2½—2½	
3977.46	A	10HH	16.33	19.44	2½—3½	19	5447.26	A	20H	16.62	18.90	1½—1½	
							5432.89	A	15H	16.62	18.90	0½—0½	
3991.77	A	15HH	16.36	19.46	3½—4½	3d' 2F°—4f' 2G	5451.18	A	0h	16.62	18.90	1½—0½	
3998.01	A	10HH	16.33	19.43	2½—3½	20							
3955.74	A	10h	16.36	19.49	3½—2½	3d' 2F°—4f' 2D?	5295.19	A	30h	16.64	18.98	2½—2½	4p' 4P—4d' 4P°
3919.00	A	5h	16.33	19.49	2½—1½	21	5232.76	A	0h	16.62	18.99	1½—1½	31
							5269.74	A	3h	16.64	18.99	2½—1½	
							*5219.37	A	10h	16.62	19.00	1½—0½	
							5257.64	A	3h	16.62	18.98	1½—2½	
							5215.67	A	1h	16.62	18.99	0½—1½	
5405.34	A	100h	16.39	18.68	3½—2½	4p' 4D—5s' 4P°							
5417.24	A	15H	16.36	18.65	2½—1½	22							
5415.64	A	5H	16.35	18.64	1½—0½		5496.45	A	200h	16.73	18.98	1½—2½	4p' 4S—4d' 4P°
5354.89	A	5H	16.36	18.68	2½—2½		5469.21	A	100h	16.73	18.99	1½—1½	32
5380.48	A	5H	16.35	18.65	1½—1½		5454.49	A	15H	16.73	19.00	1½—0½	
5393.18	A	3H	16.34	18.64	0½—0½								
*5202.413	A	500h	16.39	18.77	3½—4½	4p' 4D—4d' 4F°							
5192.86	A	200h	16.36	18.75	2½—3½	23	4932.80	A	20h	16.78	19.29	1½—2½	3p3 2D°—4f' 2F?
5185.25	A	100h	16.35	18.74	1½—2½								33
5181.90	A	100	16.34	18.73	0½—1½								
5240.31	A	5h	16.39	18.75	3½—3½		4908.18	A	5h	16.77	19.30	2½—3½	3p3 2D°—4f' 4F
*5219.37	A	10h	16.36	18.74	2½—2½								34
*5202.413	A	500h	16.35	18.73	1½—1½								
4906.99	A	20h	16.39	18.91	3½—3½	4p' 4D—4d' 4D°	Unclassified Lines of Si II						
4883.20	A	15h	16.36	18.90	2½—2½	24	Air						
4860.16	P		16.35	18.90	1½—1½		6067.45	A	10HH				
4845.26	A	3h	16.34	18.90	0½—0½		3461.642	A	(2)				
4890.25	A	0h	16.36	18.90	2½—1½		3414.758	A	(3)				
4853.35	A	2h	16.35	18.90	1½—2½		Vac						
4842.32	A	2h	16.34	18.90	0½—1½		1311.265	A	2				
							1275.662	A	5h				
4776.20	A	3h	16.39	18.98	3½—2½	4p' 4D—4d' 4P°	1274.300	A	3h				
						25							
3149.92	A	(20)	16.39	20.32	3½—4½	4p' 4D—5d' 4F°?							
						26							



NSRDS-NBS 3, SECTION 1

**SILICON,  $Z=14$**

A Si III Atomic Energy Levels

B Si III Multiplet Table





## Si III

(Mg I sequence; 12 electrons)

 $Z=14$ Ground state  $1s^2 2s^2 2p^6 3s^2 {}^1S_0$  $3s^2 {}^1S_0$   $270139.3 \pm 0.4 \text{ cm}^{-1}$ ,  $370.179 \text{ \AA}$  (Vac)

I P 33.49 eV

The analysis is by Toresson, who has reobserved the spectrum from  $400 \text{ \AA}$  to  $10000 \text{ \AA}$ . He has measured some 360 lines and added 107 energy levels to the earlier analysis.

Observed intersystem combinations connect the terms of different multiplicity. Three levels not connected with the rest by observed transitions, are indicated by "+x". Predicted positions of the  $8d {}^3D_{1,2}$  levels and of the  ${}^3K^\circ$  and  ${}^3L$  terms are entered in brackets in the table.

The ionization limit has been well determined from the  $nh$ -series, by means of a Ritz formula.

## REFERENCE

Y. G. Toresson, Ark. Fys. (Stockholm) **18**, No. 28, 389 to 416 (1960). I P, T, C L, G D

## Si III

## Si III

Config.	Desig.	$J$	Level	Interval	Config.	Desig.	$J$	Level	Interval
$3s^2$	$3s^2 {}^1S$	0	0. 00		$3p({}^2P^\circ)3d$	$3d' {}^1D^\circ$	2	205029. 09	
$3s({}^2S)3p$	$3p {}^3P^\circ$	0	52724. 69	128. 59	$3s({}^2S)5s$	$5s {}^3S$	1	206176. 08	
		1	52853. 28	261. 73	$3s({}^2S)5s$	$5s {}^1S$	0	207874. 09	
		2	53115. 01		$3s({}^2S)4f$	$4f {}^3F^\circ$	2	209531. 40	27. 93
$3s({}^2S)3p$	$3p {}^1P^\circ$	1	82884. 41				3	209559. 33	40. 37
$3p^2$	$3p^2 {}^1D$	2	122214. 52				4	209599. 70	
$3p^2$	$3p^2 {}^3P$	0	129708. 45	133. 52	$3s({}^2S)5p$	$5p {}^1P^\circ$	1	214532. 17	
		1	129841. 97	258. 55	$3s({}^2S)5p$	$5p {}^3P^\circ$	2	214989. 27	-5. 38
		2	130100. 52				1	214994. 65	-0. 81
$3s({}^2S)3d$	$3d {}^3D$	3	142943. 74	-2. 10			0	214995. 46	
		2	142945. 84	-2. 41	$3p({}^2P^\circ)3d$	$3d' {}^3P^\circ$	2	216190. 24	-98. 45
		1	142948. 25				1	216288. 69	-61. 57
$3s({}^2S)4s$	$4s {}^3S$	1	153377. 05				0	216350. 26	
$3p^2$	$3p^2 {}^1S$	0	153444. 23		$3p({}^2P^\circ)3d$	$3d' {}^3D^\circ$	1	217385. 77	54. 15
$3s({}^2S)4s$	$4s {}^1S$	0	159069. 61				2	217439. 92	49. 57
$3s({}^2S)3d$	$3d {}^1D$	2	165765. 00				3	217489. 49	
$3s({}^2S)4p$	$4p {}^3P^\circ$	0	175230. 01	33. 09	$3s({}^2S)5f$	$5f {}^1F^\circ$	3	225526. 33	
		1	175263. 10	73. 16	$3p({}^2P^\circ)4s$	$4s' {}^3P^\circ$	0	226400. 00	127. 42
		2	175336. 26				1	226527. 42	292. 86
$3s({}^2S)4p$	$4p {}^1P^\circ$	1	176487. 19				2	226820. 28	
$3p({}^2P^\circ)3d$	$3d' {}^3F^\circ$	2	198923. 15	103. 34	$3s({}^2S)5d$	$5d {}^3D$	1	227081. 19	3. 02
		3	199026. 49	137. 61			2	227084. 21	4. 51
		4	199164. 10				3	227088. 72	
$3s({}^2S)4d$	$4d {}^3D$	1	201597. 73	0. 55	$3s({}^2S)5d$	$5d {}^1D$	2	227665. 09	
		2	201598. 28	1. 20	$3p({}^2P^\circ)3d$	$3d' {}^1P^\circ$	1	228699. 75	
		3	201599. 48		$3s({}^2S)6s$	$6s {}^3S$	1	229623. 19	
$3s({}^2S)4d$	$4d {}^1D$	2	204330. 79		$3s({}^2S)5f$	$5f {}^3F^\circ$	2	230267. 7	0. 9
$3s({}^2S)4f$	$4f {}^1F^\circ$	3	204828. 06				3	230268. 62	2. 04
							4	230270. 66	

## Atomic Energy Levels

## Si III—Continued

## Si III—Continued

Config.	Desig.	<i>J</i>	Level	Interval	Config.	Desig.	<i>J</i>	Level	Interval
3s(2S)5g	5g 3G	3 4 5	230301. 22 230301. 66 230302. 35	0. 44 0. 69	3s(2S)7h	7h 3.1H°	4, 5, 6	249937. 29	
					3s(2S)7i	7i 3.1I	5, 6, 7	249966. 49	
3s(2S)5g	5g 1G	4	230302. 01		3s(2S)7f	7f 1F°	3	250366. 22	
3s(2S)6s	6s 1S	0	230364. 46		3s(2S)7d	7d 3D	2	250636. 55	
3s(2S)6p	6p 1P°	1	234387. 64		3s(2S)8d	8d 3D	1 2 3	[254002] [254004] 254007. 48	2 3
3s(2S)6p	6p 3P°	0 1 2	234415. 07 234428. 40 234442. 18	13. 33 13. 78	3s(2S)8f	8f 3F°	2 3 4	254557. 03 254557. 26 254557. 64	0. 23 0. 38
3p(2P°)3d	3d' 1F°	3	235413. 93		3s(2S)8g	8g 1G	4	254584. 6	
3p(2P°)4s	4s' 1P°	1	235951. 09		3s(2S)8g	8g 3G	3, 4 5	254584. 8 254585. 75	1. 0
3s(2S)6d	6d 3D	1 2 3	240262. 28 240284. 28 240314. 63	22. 00 30. 35	3s(2S)8h	8h 3.1H°	4, 5, 6	254674. 4	
3s(2S)6d	6d 1D	2	240549. 77		3s(2S)8i	8i 3.1I	5, 6, 7	254694. 99	
3s(2S)7s	7s 3S	1	242145. 10		3s(2S)8k	8k 3.1K°	6, 7, 8	[254702. 29]	
3s(2S)6f	6f 3F°	2 3 4	242410. 88 242411. 27 242411. 70	0. 39 0. 43	3s(2S)8d	8d 1D	2	254766. 75	
					3s(2S)8f	8f 1F°	3	254855. 42	
3s(2S)6g	6g 3G	3 4 5	242473. 66 242473. 86 242474. 81	0. 20 0. 95	3s(2S)9d	9d 3D	1, 2, 3	257415. 6	
					3s(2S)9f	9f 3F°	2, 3, 4	257831. 4	
3s(2S)6g	6g 1G	4	242474. 27		3s(2S)9d	9d 1D	2	257848. 5	
3s(2S)7s	7s 1S	0	242537. 95		3s(2S)9g	9g 3G	3, 4, 5	257853. 6	
3s(2S)6h	6h 3.1H°		242639. 38		3s(2S)9h	9h 3.1H°	4, 5, 6	257922. 0	
3p(2P°)4p	4p' 1P	1	242885. 30		3s(2S)9i	9i 3.1I	5, 6, 7	257936. 99	
3s(2S)6f	6f 1F°	3	243868. 50		3s(2S)9k	9k 3.1K°	6, 7, 8	[257942. 30]	
3p(2P°)4p	4p' 3D	1 2 3	244736. 93 244866. 05 245086. 58	129. 12 220. 53	3s(2S)9l	9l 3.1L	7, 8, 9	[257944. 45]	
					3s(2S)9f	9f 1F°	3	258013. 37	
3s(2S)7p	7p 1P°	1	244871. 47		3p(2P°)4p	4p' 1S	0	258978. 66	
3s(2S)7p	7p 3P°	0 1 2	244928. 72 244933. 36 244943. 31	4. 64 9. 95	3p(2P°)4d	4d' 1D°?	2	267483. 87	
					3p(2P°)4d	4d' 3F°?	4 3, 2	267686. 48	
3p(2P°)4p	4p' 3P	0 1 2	247871. 66 247953. 69 248168. 04	82. 03 214. 35	Si IV (2S <sub>0 1/2</sub> )	Limit	-----	270139. 3	
3p(2P°)4p	4p' 1D	2	247935. 39		3p(2P°)4f	4f' [2½]?	3	278920. 68	
3p(2P°)4p	4p' 3S	1	248772. 86		3p(2P°)4f	4f' [3½]?	3 4	278938. 08 278938. 08+x	
3s(2S)7d	7d 3D	1 2 3	249093. 5 249103. 90 249121. 14	10. 4 17. 24	3p(2P°)5p	5p' 1P?	1	282291. 19?	
					3p(2P°)5f	5f' [3½]?	3	301484. 51	
3s(2S)8s	8s 3S	1	249766. 19		3p(2P°)5g	5g' [4½]°	5 4	301884. 14+x 301890. 97+x	-6. 83
3s(2S)7f	7f 3F°	2 3 4	249774. 48 249774. 70 249774. 98	0. 22 0. 28	3p(2P°)5g	5g' [3½]°	3 4	301887. 94 301892. 26	4. 32
3s(2S)7g	7g 3G	3 4 5	249817. 32 249817. 85 249818. 93	0. 53 1. 08	-----	-----	-----	-----	
3s(2S)7g	7g 1G	4	249817. 94		Si IV (2P <sub>0 1/2</sub> )	Limit	-----	341426. 8	
3s(2S)8s	8s 1S	0	249857. 26		Si IV (2P <sub>1 1/2</sub> )	Limit	-----	341887. 9	

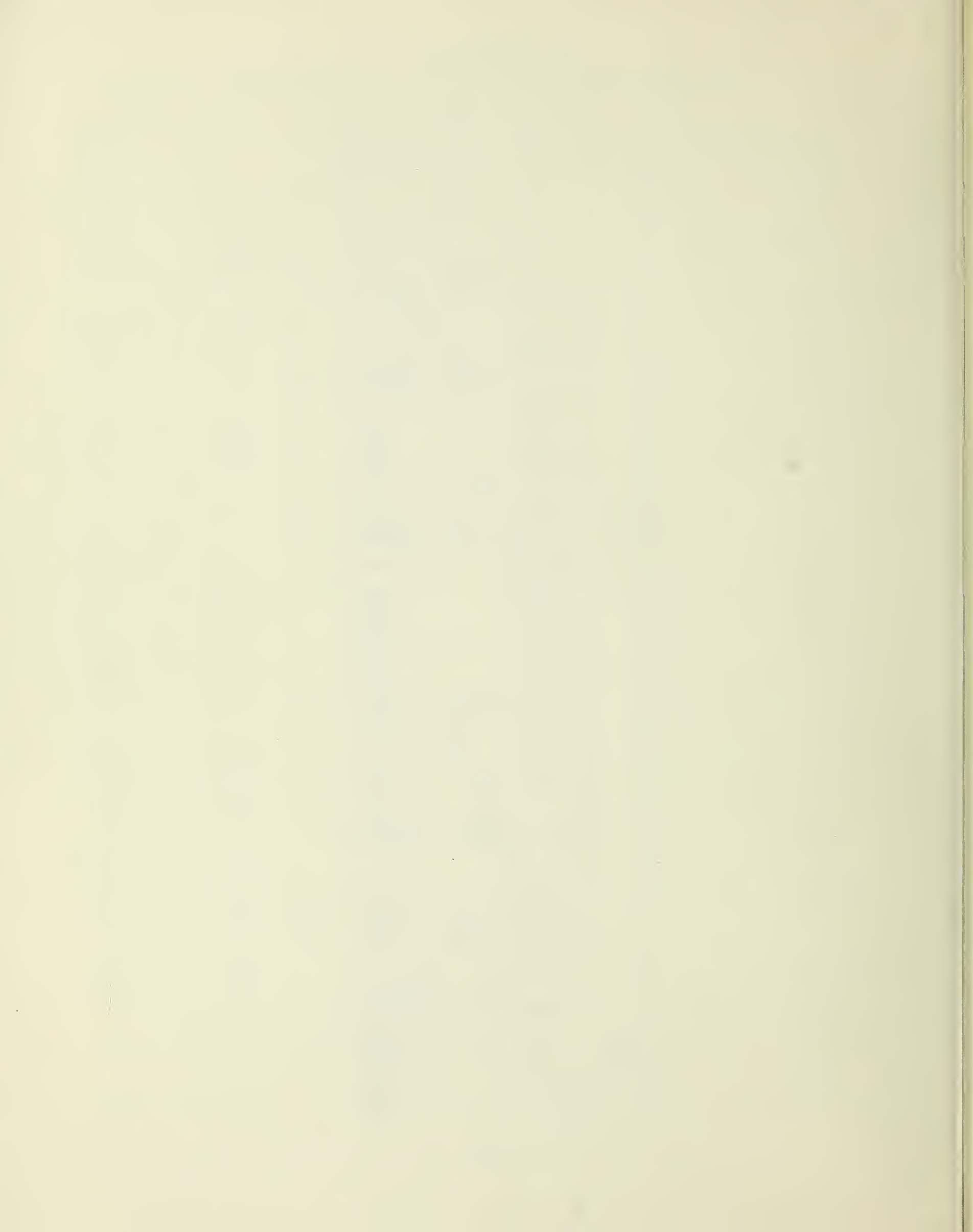
May 1964.

# Atomic Energy Levels

## Si III OBSERVED TERMS

Config. $1s^2 2s^2 2p^6 +$	Observed Terms									
$3s^2$	$3s^2 \ ^1S$									
$3s(^2S)3p$	$\left\{ \begin{array}{l} 3p \ ^3P^\circ \\ 3p \ ^1P^\circ \end{array} \right.$									
$3p^2$	$\left\{ \begin{array}{l} 3p^2 \ ^3P \\ 3p^2 \ ^1S \end{array} \right.$	$3p^2 \ ^1D$								
	$ns(n \geq 4)$		$np(n \geq 4)$		$nd(n \geq 3)$		$nf(n \geq 4)$	$ng(n \geq 5)$	$nh(n \geq 6)$	$ni(n \geq 7)$
$3s(^2S)nl$	$\left\{ \begin{array}{l} 4-8s \ ^3S \\ 4-8s \ ^1S \end{array} \right.$		$\begin{array}{l} 4-7p \ ^3P^\circ \\ 4-7p \ ^1P^\circ \end{array}$		$\begin{array}{l} 3-9d \ ^3D \\ 3-9d \ ^1D \end{array}$		$\begin{array}{l} 4-9f \ ^3F^\circ \\ 4-9f \ ^1F^\circ \end{array}$	$\begin{array}{l} 5-9g \ ^3G \\ 5-8g \ ^1G \end{array}$	$\begin{array}{l} 6-9h \ ^3H^\circ \\ 7-9i \ ^3I \end{array}$	$\begin{array}{l} 7-9i \ ^3I \\ 7-9i \ ^3I \end{array}$
$3p(^2P^\circ)nl'$	$\left\{ \begin{array}{l} 4s' \ ^3P^\circ \\ 4s' \ ^1P^\circ \end{array} \right.$		$\begin{array}{l} 4p' \ ^3S \\ 4p' \ ^1S \end{array}$		$\begin{array}{l} 3d' \ ^3P^\circ \\ 3d' \ ^1P^\circ \end{array}$	$\begin{array}{l} 3, 4?d' \ ^3F^\circ \\ 3d' \ ^1F^\circ \end{array}$	$\begin{array}{l} 4, 5f' \ ^3F? \\ 4, 5f' \ ^3I \end{array}$	$\begin{array}{l} 5g' \ ^3G \\ 5g' \ ^3I \end{array}$	$\begin{array}{l} 6-9h \ ^3H^\circ \\ 7-9i \ ^3I \end{array}$	$\begin{array}{l} 7-9i \ ^3I \\ 7-9i \ ^3I \end{array}$





# Multiplet Table

Part B

SILICON

Si III ( $Z=14$ )

I P 33.49 eV Limit  $270139.3 \pm 0.4 \text{ cm}^{-1}$  370.179 Å (Vac)

Anal A List A April 1964

## REFERENCES

- A Y. G. Toresson, Ark. Fys. (Stockholm) **18**, No. 28, 389 to 416 (1960).  
 I P, T, C L, I, G D; W L 423 Å to 9799 Å  
 P Predicted wavelength  
 New Multiplet Numbers, not inserted between older ones, start with UV 11 and 14.  
 \*Blend  
 \*and § Blend of Si III and Si IV

Si III

Si III

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac 1892.030	A	3†	0.00	6.55	0—1	$3s^2 \ ^1S - 3p \ ^3P^\circ$ UV 1	Vac 1447.196 1441.732	A A	6 5	6.58 6.55	15.15 15.15	2—2 1—2	$3p \ ^3P^\circ - 3p^2 \ ^1D$ UV 3.05
1206.510†	A	30*	0.00	10.28	0—1	$3s^2 \ ^1S - 3p \ ^1P^\circ$ UV 2	1298.960 1298.891 1303.320	A A A	18 15 16	6.58 6.55 6.58	16.13 16.10 16.10	2—2 1—1 2—1	$3p \ ^3P^\circ - 3p^2 \ ^3P$ UV 4
566.613	A	8	0.00	21.88	0—1	$3s^2 \ ^1S - 4p \ ^1P^\circ$ UV 3	1301.146 1294.543 1296.726	A A A	14 17 14	6.55 6.55 6.54	16.08 16.13 16.10	1—0 1—2 0—1	
466.129	A	4	0.00	26.60	0—1	$3s^2 \ ^1S - 5p \ ^1P^\circ$ UV 3.01	1113.228 1109.970 1108.368	A A A	18 16 14	6.58 6.55 6.54	17.72 17.72 17.72	2—3 1—2 0—1	$3p \ ^3P^\circ - 3d \ ^3D$ UV 5
437.255	P		0.00	28.35	0—1	$3s^2 \ ^1S - 3d' \ ^1P^\circ$ UV 3.02	1113.204 1109.940 1113.174	P P P	16	6.58 6.55 6.58	17.72 17.72 17.72	2—2 1—1 2—1	
426.644	P		0.00	29.06	0—1	$3s^2 \ ^1S - 6p \ ^1P^\circ$ UV 3.03							
423.817	P		0.00	29.25	0—1	$3s^2 \ ^1S - 4s' \ ^1P^\circ$ UV 3.04							

Multiplet Table

Si III—Continued

Si III—Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac							Vac						
997.389	A	16	6.58	19.02	2—1	$3p^3P^\circ - 4s^3S$	690.689	A	2	10.28	28.23	1—2	$3p^1P^\circ - 5d^1D$
994.787	A	13	6.55	19.02	1—1	UV 6							UV 14
993.519	A	10	6.54	19.02	0—1		678.055	A	2	10.28	28.56	1—0	$3p^1P^\circ - 6s^1S$
*673.477	A	5	6.58	24.99	2—3	$3p^3P^\circ - 4d^3D$							UV 15
*672.293	A	4	6.55	24.99	1—2	UV 6.01	634.255	P		10.28	29.82	1—2	$3p^1P^\circ - 6d^1D$
671.718	A	2	6.54	24.99	0—1								UV 16
*673.477	A	5	6.58	24.99	2—2		624.997	P		10.28	30.11	1—1	$3p^1P^\circ - 4p'^1P$
*672.293	A	4	6.55	24.99	1—1								UV 17
*673.477	A	5	6.58	24.99	2—1		605.873	P		10.28	30.74	1—2	$3p^1P^\circ - 4p'^1D$
653.332	A	8	6.58	25.56	2—1	$3p^3P^\circ - 5s^3S$							UV 18
652.223	A	6	6.55	25.56	1—1	UV 6.02	567.878	P		10.28	32.11	1—0	$3p^1P^\circ - 4p'^1S$
651.668	A	4	6.54	25.56	0—1								UV 19
574.799	P		6.58	28.15	2—3	$3p^3P^\circ - 5d^3D$							
573.951	P		6.55	28.15	1—2	UV 6.03							
573.538	P		6.54	28.15	0—1								
574.814	P		6.58	28.15	2—2								
573.961	P		6.55	28.15	1—1								
574.824	P		6.58	28.15	2—1		1842.547	A	9	15.15	21.88	2—1	$3p^2^1D - 4p^1P^\circ$
566.546	P		6.58	28.47	2—1	$3p^3P^\circ - 6s^3S$							UV 20
565.698	A	2	6.55	28.47	1—1	UV 6.04	1210.456	A	10	15.15	25.39	2—3	$3p^2^1D - 4f^1F^\circ$
565.289	A	1	6.54	28.47	0—1								UV 21
534.189	P		6.58	29.79	2—3	$3p^3P^\circ - 6d^3D$	1207.517	A	9	15.15	25.42	2—2	$3p^2^1D - 3d'^1D^\circ$
533.530	P		6.55	29.79	1—2	UV 6.05							UV 22
533.226	P		6.54	29.79	0—1		1083.210	A	6	15.15	26.60	2—1	$3p^2^1D - 5p^1P^\circ$
534.276	P		6.58	29.79	2—2								UV 23
533.592	P		6.55	29.79	1—1		967.946	A	9	15.15	27.96	2—3	$3p^2^1D - 5f^1F^\circ$
534.339	P		6.58	29.79	2—1								UV 24
520.92	A	0	6.58	30.39	2—3	$3p^3P^\circ - 4p'^3D$	939.093	A	7	15.15	28.35	2—1	$3p^2^1D - 3d'^1P^\circ$
*520.79	A	00	6.55	30.36	1—2	UV 6.06							UV 25
*520.79	A	00	6.54	30.34	0—1		891.479	P		15.15	29.06	2—1	$3p^2^1D - 6p^1P^\circ$
521.510	P		6.58	30.36	2—2								UV 26
521.149	P		6.55	30.34	1—1		883.398	A	5	15.15	29.19	2—3	$3p^2^1D - 3d'^1F^\circ$
521.861	P		6.58	30.34	2—1								UV 27
512.681	P		6.58	30.77	2—2	$3p^3P^\circ - 4p'^3P$	879.233	A	0	15.15	29.25	2—1	$3p^2^1D - 4s'^1P^\circ$
512.557	P		6.55	30.74	1—1	UV 6.07							UV 28
513.245	P		6.58	30.74	2—1		822.004	P		15.15	30.24	2—3	$3p^2^1D - 6f^1F^\circ$
512.772	P		6.55	30.73	1—0								UV 29
511.994	P		6.55	30.77	1—2								
512.219	P		6.54	30.74	0—1								
511.096	P		6.58	30.84	2—1	$3p^3P^\circ - 4p'^3S$							
510.414	P		6.55	30.84	1—1	UV 6.08							
510.079	P		6.54	30.84	0—1								
Air							*1178.004	A	8	16.13	26.65	2—2	$3p^2^3P - 5p^3P^\circ$
2541.818	A	25	10.28	15.15	1—2	$3p^1P^\circ - 3p^2^1D$	*1174.369	A	5	16.10	26.66	1—1	UV 30
						UV 6.09	*1178.004	A	8	16.13	26.66	2—1	
							*1174.369	A	5	16.10	26.66	1—0	
							1174.432	A	6	16.10	26.65	1—2	
							1172.529	A	4	16.08	26.66	0—1	
Vac							1161.579	A	8	16.13	26.80	2—2	$3p^2^3P - 3d'^3P^\circ$
1417.237	A	13	10.28	19.02	1—0	$3p^1P^\circ - 3p^2^1S$	1156.782	A	4	16.10	26.82	1—1	UV 31
						UV 9	1160.255	A	6	16.13	26.82	2—1	
1312.590	A	13	10.28	19.72	1—0	$3p^1P^\circ - 4s^1S$	1155.957	A	6	16.10	26.82	1—0	
						UV 10	1158.102	A	7	16.10	26.80	1—2	
1206.533	A	30*	10.28	20.55	1—2	$3p^1P^\circ - 3d^1D$	1154.998	A	6	16.08	26.82	0—1	
						UV 11							
823.408	A	9	10.28	25.33	1—2	$3p^1P^\circ - 4d^1D$	1144.306	A	8	16.13	26.96	2—3	$3p^2^3P - 3d'^3D^\circ$
						UV 12	1141.580	A	7	16.10	26.96	1—2	UV 32
800.066	A	5	10.28	25.77	1—0	$3p^1P^\circ - 5s^1S$	1140.545	A	6	16.08	26.95	0—1	
						UV 13	1144.959	A	6	16.13	26.96	2—2	
							1142.282	A	6	16.10	26.95	1—1	
							1145.669	P		16.13	26.95	2—1	



Multiplet Table

Si III—Continued

Si III—Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac							Vac						
1033.920	A	8	16.13	28.12	2—2	$3p^2\ ^3P - 4s'\ ^3P^\circ$ UV 33	1092.915	P		17.72	29.07	3—2	$3d\ ^3D - 6p\ ^3P^\circ$ UV 42
1034.287	A	4	16.10	28.09	1—1		1093.105	P		17.72	29.06	2—1	
1037.053	A	7	16.13	28.09	2—1		1093.293	P		17.72	29.06	1—0	
1035.657	A	3	16.10	28.07	1—0		1092.940	P		17.72	29.07	2—2	
1031.169	A	7	16.10	28.12	1—2		1093.133	P		17.72	29.06	1—1	
1032.851	A	3	16.08	28.09	0—1		1092.969	P		17.72	29.07	1—2	
Air							1005.349	P	7*	17.72	30.05	3—4	$3d\ ^3D - 6f\ ^3F^\circ$ UV 43
3086.236	A	25	17.72	21.74	3—2	$3d\ ^3D - 4p\ ^3P^\circ$ 1	1005.374	P		17.72	30.05	2—3	
3093.424	A	20	17.72	21.73	2—1		1005.403	P		17.72	30.05	1—2	
3096.826	A	16	17.72	21.73	1—0		1005.353	P		17.72	30.05	3—3	
3086.46	A	6	17.72	21.74	2—2		1005.378	P		17.72	30.05	2—2	
3093.65	A	5	17.72	21.73	1—1		1005.357	P		17.72	30.05	3—2	
3086.666	P		17.72	21.74	1—2								
2980.519	A	5	17.72	21.88	2—1	$3d\ ^3D - 4p\ ^1P^\circ$ UV 34	936.056	P	3*	17.72	30.97	3—4	$3d\ ^3D - 7f\ ^3F^\circ$ UV 44
							936.077	P		17.72	30.97	2—3	
							936.100	P		17.72	30.97	1—2	
							936.058	P		17.72	30.97	3—3	
							936.079	P		17.72	30.97	2—2	
							936.060	P		17.72	30.97	3—2	
Vac							Air						
1778.715	P		17.72	24.69	3—4	$3d\ ^3D - 3d'\ ^3F^\circ$ UV 35	4552.616	A	30	19.02	21.74	1—2	$4s\ ^3S - 4p\ ^3P^\circ$ 2
1783.146	P		17.72	24.68	2—3		4567.823	A	25	19.02	21.73	1—1	
1786.515	P		17.72	24.66	1—2		4574.759	A	20	19.02	21.73	1—0	
1783.079	P		17.72	24.68	3—3								
1786.438	P		17.72	24.66	2—2								
1786.371	P		17.72	24.66	3—2								
1500.241	A	12	17.72	25.99	3—4	$3d\ ^3D - 4f\ ^3F^\circ$ UV 36	Vac			19.02	26.65	1—2	$4s\ ^3S - 5p\ ^3P^\circ$ UV 45
1501.191	A	10	17.72	25.98	2—3		1623.055	P		19.02	26.66	1—1	
1501.870	A	9	17.72	25.98	1—2		1622.913	P		19.02	26.66	1—0	
1501.150	P		17.72	25.98	3—3		1622.892	P					
1501.827	P		17.72	25.98	2—2		1361.597	A	8	19.02	28.12	1—2	$4s\ ^3S - 4s'\ ^3P^\circ$ UV 46
1501.780	P		17.72	25.98	3—2		1367.049	A	7	19.02	28.09	1—1	
							1369.437	A	5	19.02	28.07	1—0	
1388.011	P	5	17.72	26.65	3—2	$3d\ ^3D - 5p\ ^3P^\circ$ UV 37	Air						
1387.948	P		17.72	26.66	2—1		4338.501	A	9	19.02	21.88	0—1	$3p^2\ ^1S - 4p\ ^1P^\circ$ 3
1387.979	P		17.72	26.66	1—0								
1388.052	P		17.72	26.65	2—2								
1387.994	P		17.72	26.66	1—1								
1388.098	P		17.72	26.65	1—2								
1365.253	P	8	17.72	26.80	3—2	$3d\ ^3D - 3d'\ ^3P^\circ$ UV 38	Vac			19.02	26.60	0—1	$3p^2\ ^1S - 5p\ ^1P^\circ$ UV 47
1363.459	P	7	17.72	26.82	2—1		1636.990	A	1				
1362.366	A	5	17.72	26.82	1—0					19.02	28.35	0—1	$3p^2\ ^1S - 3d'\ ^1P^\circ$ UV 48
1365.292	P		17.72	26.80	2—2		1328.806	P					
1363.504	P		17.72	26.82	1—1					19.02	29.06	0—1	$3p^2\ ^1S - 6p\ ^1P^\circ$ UV 49
1365.337	P		17.72	26.80	1—2		1235.431	A	7				
1341.465	A	8	17.72	26.96	3—3	$3d\ ^3D - 3d'\ ^3D^\circ$ UV 39	1212.011	A	2	19.02	29.25	0—1	$3p^2\ ^1S - 4s'\ ^1P^\circ$ UV 50
1342.392	A	7	17.72	26.96	2—2								
*1343.388	A	6	17.72	26.95	1—1								
1342.351	P		17.72	26.96	3—2								
*1343.388	A	6	17.72	26.95	2—1		Air						
1341.496	P		17.72	26.96	2—3		6173.712	A	3	19.72	21.73	0—1	$4s\ ^1S - 4p\ ^3P^\circ$ 3.01
1342.432	P		17.72	26.96	1—2								
1192.228	P		17.72	28.12	3—2	$3d\ ^3D - 4s'\ ^3P^\circ$ UV 40	5739.733	A	20	19.72	21.88	0—1	$4s\ ^1S - 4p\ ^1P^\circ$ 4
1196.436	P		17.72	28.09	2—1								
1198.297	P		17.72	28.07	1—0								
1192.258	P		17.72	28.12	2—2								
1196.470	P		17.72	28.09	1—1		Vac			19.72	26.60	0—1	$4s\ ^1S - 5p\ ^1P^\circ$ UV 51
1192.293	P		17.72	28.12	1—2		1803.023	A	3				
1145.122	P	8*	17.72	28.55	3—4	$3d\ ^3D - 5f\ ^3F^\circ$ UV 41	1436.166	A	7	19.72	28.35	0—1	$4s\ ^1S - 3d'\ ^1P^\circ$ UV 52
1145.177	P	7*	17.72	28.55	2—3								
1145.22	P		17.72	28.55	1—2		1327.703	P		19.72	29.06	0—1	$4s\ ^1S - 6p\ ^1P^\circ$ UV 53
1145.149	P	8*	17.72	28.55	3—3								
1145.19	P	7*	17.72	28.55	2—2								
1145.16	P		17.72	28.55	3—2								

Multiplet Table

Si III—Continued

Si III—Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac 1300.703	P		19.72	29.25	0—1	4s <sup>1</sup> S —4s' <sup>1</sup> P° UV 54	Vac 1361.719 1360.360 1359.751	P A P	1	21.74 21.73 21.73	30.84 30.84 30.84	2—1 1—1 0—1	4p <sup>3</sup> P° —4p' <sup>3</sup> S UV 68
Air 9323.899	A	3h	20.55	21.88	2—1	3d <sup>1</sup> D —4p <sup>1</sup> P° 4.01	Air 3981.238	A	5	21.88	24.99	1—1	4p <sup>1</sup> P° —4d <sup>3</sup> D 6.01
2559.210	A	14	20.55	25.39	2—3	3d <sup>1</sup> D —4f <sup>1</sup> F° UV 55	3590.465	A	20	21.88	25.33	1—2	4p <sup>1</sup> P° —4d <sup>1</sup> D 7
2546.093	A	10	20.55	25.42	2—2	3d <sup>1</sup> D —3d' <sup>1</sup> D° UV 56	3185.125	A	16	21.88	25.77	1—0	4p <sup>1</sup> P° —5s <sup>1</sup> S 8
2049.913	A	2	20.55	26.60	2—1	3d <sup>1</sup> D —5p <sup>1</sup> P° UV 57	Vac 1953.968	P		21.88	28.23	1—2	4p <sup>1</sup> P° —5d <sup>1</sup> D UV 69
Vac 1673.315	A	7	20.55	27.96	2—3	3d <sup>1</sup> D —5f <sup>1</sup> F° UV 58	1856.062	A	1	21.88	28.56	1—0	4p <sup>1</sup> P° —6s <sup>1</sup> S UV 70
1588.950	A	2	20.55	28.35	2—1	3d <sup>1</sup> D —3d' <sup>1</sup> P° UV 59	1560.974	P		21.88	29.82	1—2	4p <sup>1</sup> P° —6d <sup>1</sup> D UV 71
1457.253	A	5	20.55	29.06	2—1	3d <sup>1</sup> D —6p <sup>1</sup> P° UV 60	1506.060	A	6	21.88	30.11	1—1	4p <sup>1</sup> P° —4p' <sup>1</sup> P UV 72
1435.776	A	8	20.55	29.19	2—3	3d <sup>1</sup> D —3d' <sup>1</sup> F° UV 61	1399.615	P		21.88	30.74	1—2	4p <sup>1</sup> P° —4p' <sup>1</sup> D UV 73
1424.775	A	2	20.55	29.25	2—1	3d <sup>1</sup> D —4s' <sup>1</sup> P° UV 62	1212.247	P		21.88	32.11	1—0	4p <sup>1</sup> P° —4p' <sup>1</sup> S UV 74
1280.354	A	6	20.55	30.24	2—3	3d <sup>1</sup> D —6f <sup>1</sup> F° UV 63							
1182.018	A	3	20.55	31.04	2—3	3d <sup>1</sup> D —7f <sup>1</sup> F° UV 64	Air 3580.050 3563.11 3550.38	A A A	3h 2h* 1h*	24.69 24.68 24.66	28.15 28.15 28.15	4—3 3—2 2—1	3d' <sup>3</sup> F° —5d <sup>3</sup> D 8.01
							3210.554 3196.504 3186.022	A A A	15 14 13	24.69 24.68 24.66	28.55 28.55 28.55	4—5 3—4 2—3	3d' <sup>3</sup> F° —5g <sup>3</sup> G 8.02
Air 3806.544 3796.114 3791.41	A A A	30 25 20*	21.74 21.73 21.73	24.99 24.99 24.99	2—3 1—2 0—1	4p <sup>3</sup> P° —4d <sup>3</sup> D 5	2429.35 2423.049 2418.281	A P P	7*	24.69 24.68 24.66	29.79 29.79 29.79	4—3 3—2 2—1	3d' <sup>3</sup> F° —6d <sup>3</sup> D UV 75
3447.938 3439.242	P A		21.74 21.73	25.33 25.33	2—2 1—2	4p <sup>3</sup> P° —4d <sup>1</sup> D 5.01	2308.191 2300.930 2295.476	A A A	10 8 6	24.69 24.68 24.66	30.06 30.06 30.06	4—5 3—4 2—3	3d' <sup>3</sup> F° —6g <sup>3</sup> G UV 76
3241.622 3233.954 3230.499	A A A	15 14 12	21.74 21.73 21.73	25.56 25.56 25.56	2—1 1—1 0—1	4p <sup>3</sup> P° —5s <sup>3</sup> S 6	2176.894 2180.836 2182.049 2170.42	A A A A	5 4 3 0	24.69 24.68 24.66 24.68	30.39 30.36 30.34 30.39	4—3 3—2 2—1 3—3	3d' <sup>3</sup> F° —4p' <sup>3</sup> D UV 77
Vac 1842.064 1839.585 1838.466	P P P		21.74 21.73 21.73	28.47 28.47 28.47	2—1 1—1 0—1	4p <sup>3</sup> P° —6s <sup>3</sup> S UV 65							
1433.690 1436.724 1438.702 1438.228 1439.391 1440.908	A A A A A P	6 4 2 2 2 2	21.74 21.73 21.73 21.74 21.73 21.74	30.39 30.36 30.34 30.36 30.34 30.34	2—3 1—2 0—1 2—2 1—1 2—1	4p <sup>3</sup> P° —4p' <sup>3</sup> D UV 66	7466.322 *7462.624 7461.890 7465.669 7462.347	A A A A P	9h 8h 5h 4h 4h	24.99 24.99 24.99 24.99 24.99	26.65 26.66 26.66 26.65 26.66	3—2 2—1 1—0 2—2 1—1	4d <sup>3</sup> D —5p <sup>3</sup> P° 8.03
							6851.65 6805.244 6776.623 6851.18 6805.029	A A A A P	7h 4h 2h 3h 3h	24.99 24.99 24.99 24.99 24.99	26.80 26.82 26.82 26.80 26.82	3—2 2—1 1—0 2—2 1—1	4d <sup>3</sup> D —3d' <sup>3</sup> P° 8.04
1373.030 1375.688 1377.082 1377.238 1371.652 1375.083	A A A A A A	5 2 3 2 3 2	21.74 21.73 21.74 21.73 21.73 21.73	30.77 30.74 30.74 30.73 30.77 30.74	2—2 1—1 2—1 1—0 1—2 0—1	4p <sup>3</sup> P° —4p' <sup>3</sup> P UV 67							



Multiplet Table

Si III—Continued

Si III—Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Air							Air						
3963.838	A	6	24.99	28.12	3—2	4d <sup>3</sup> D —4s' <sup>3</sup> P°	4800.428	A	8	25.77	28.35	0—1	5s <sup>1</sup> S —3d' <sup>1</sup> P°
*4010.192	A	4	24.99	28.09	2—1	8.05							8.16
4030.752	A	2	24.99	28.07	1—0								
3963.671	P		24.99	28.12	2—2								
*4010.192	A	4	24.99	28.09	1—1		5716.289	A	8	25.99	28.15	4—3	4f <sup>3</sup> F° —5d <sup>3</sup> D
							5704.598	A	7	25.98	28.15	3—2	8.17
3486.911	A	15	24.99	28.55		4d <sup>3</sup> D —5f <sup>3</sup> F°	5696.50	A	7*	25.98	28.15	2—1	
						8.06	5703.121	A	4	25.98	28.15	3—3	
							5695.522	A	3	25.98	28.15	2—2	
3043.932	A	7	24.99	29.07	3—2	4d <sup>3</sup> D —6p <sup>3</sup> P°	4828.968	A	18	25.99	28.55	4—5	4f <sup>3</sup> F° —5g <sup>3</sup> G
3045.076	A	5	24.99	29.06	2—1	8.07	4819.718	A	16	25.98	28.55	3—4	9
3046.284	A	3	24.99	29.06	1—0		4813.330	A	15	25.98	28.55	2—3	
2449.484	A	11	24.99	30.05		4d <sup>3</sup> D —6f <sup>3</sup> F°							
						UV 78	3254.800	A	7	25.99	29.79	4—3	4f <sup>3</sup> F° —6d <sup>3</sup> D
2306.42	A	2h*	24.99	30.37	3—2	4d <sup>3</sup> D —7p <sup>3</sup> P°	3253.741	A	5	25.98	29.79	3—2	9.01
2306.889	P	1h*	24.99	30.37	2—1	UV 79	3253.117	A	4	25.98	29.79	2—1	
2307.107	P		24.99	30.37	1—0		3250.56	A	1	25.98	29.79	3—3	
							3250.79	A	1	25.98	29.79	2—2	
2075.04	A	2h	24.99	30.97		4d <sup>3</sup> D —7f <sup>3</sup> F°	3040.933	A	9	25.99	30.06	4—5	4f <sup>3</sup> F° —6g <sup>3</sup> G
						UV 80	3037.287	A	8	25.98	30.06	3—4	10
							3034.732	A	6	25.98	30.06	2—3	
9799.906	A	2h	25.33	26.60	2—1	4d <sup>1</sup> D —5p <sup>1</sup> P°	2817.110	A	9	25.99	30.39	4—3	4f <sup>3</sup> F° —4p' <sup>3</sup> D
						8.08	2831.490	A	7	25.98	30.36	3—2	UV 88
4716.651	A	16	25.33	27.96	2—3	4d <sup>1</sup> D —5f <sup>1</sup> F°	2839.622	A	5	25.98	30.34	2—1	
						8.09	2813.912	P		25.98	30.39	3—3	
4102.422	A	8	25.33	28.35	2—1	4d <sup>1</sup> D —3d' <sup>1</sup> P°	2829.23	A	1*	25.98	30.36	2—2	
						8.10	m2485.623	P	Cu II	25.99	30.97	4—5	4f <sup>3</sup> F° —7g <sup>3</sup> G
3216.249	A	7	25.33	29.19	2—3	4d <sup>1</sup> D —3d' <sup>1</sup> F°	2483.196	A	6	25.98	30.97	3—4	UV 89
						8.11	2481.508	A	3	25.98	30.97	2—3	
3161.610	A	8	25.33	29.25	2—1	4d <sup>1</sup> D —4s' <sup>1</sup> P°							
						8.12	7612.356	A	12h	26.60	28.23	1—2	5p <sup>1</sup> P° —5d <sup>1</sup> D
m2528.471	P	Si I	25.33	30.24	2—3	4d <sup>1</sup> D —6f <sup>1</sup> F°	6314.459	A	7	26.60	28.56	1—0	5p <sup>1</sup> P° —6s <sup>1</sup> S
						UV 81							10.02
2171.559	A	1	25.33	31.04	2—3	4d <sup>1</sup> D —7f <sup>1</sup> F°	3842.458	A	7	26.60	29.82	1—2	5p <sup>1</sup> P° —6d <sup>1</sup> D
						UV 82							10.03
Vac							3569.673	A	8	26.60	30.07	1—0	5p <sup>1</sup> P° —7s <sup>1</sup> S
m1979.233	P	Si I	25.33	31.60	2—3	4d <sup>1</sup> D —8f <sup>1</sup> F°							10.04
						UV 83							
Air							3525.939	A	9	26.60	30.11	1—1	5p <sup>1</sup> P° —4p' <sup>1</sup> P
4377.626	A	8h	25.39	28.23	3—2	4f <sup>1</sup> F° —5d <sup>1</sup> D							10.05
						8.13	2830.02	A	1*	26.60	30.98	1—0	5p <sup>1</sup> P° —8s <sup>1</sup> S
3924.468	A	20	25.39	28.55	3—4	4f <sup>1</sup> F° —5g <sup>1</sup> G							UV 90
						8.14							
2655.512	A	14	25.39	30.06	3—4	4f <sup>1</sup> F° —6g <sup>1</sup> G	8262.568	A	9h	26.65	28.15	2—3	5p <sup>3</sup> P° —5d <sup>3</sup> D
						UV 84	8269.324	A	8h	26.66	28.15	1—2	10.06
2222.01	A	2h	25.39	30.97	3—4	4f <sup>1</sup> F° —7g <sup>1</sup> G	8271.944	A	6h	26.66	28.15	0—1	
						UV 85	8265.640	A	5h	26.65	28.15	2—2	
							8271.377	A	5h	26.66	28.15	1—1	
2640.788	A	11	25.42	30.11	2—1	3d' <sup>1</sup> D° —4p' <sup>1</sup> P	8267.75	A	0h	26.65	28.15	2—1	
						UV 86	6831.560	A	6h	26.65	28.47	2—1	5p <sup>3</sup> P° —6s <sup>3</sup> S
2329.931	A	2h	25.42	30.74	2—2	3d' <sup>1</sup> D° —4p' <sup>1</sup> D	6834.08	A	4h	26.66	28.47	1—1	10.07
						UV 87	6834.38	A	2h	26.66	28.47	0—1	
							3947.488	A	6h	26.65	29.79	2—3	5p <sup>3</sup> P° —6d <sup>3</sup> D
							3953.080	A	4h	26.66	29.79	1—2	10.08
							3956.66	A	2h	26.66	29.79	0—1	
4842.57	A	5*	25.56	28.12	1—2	5s <sup>3</sup> S —4s' <sup>3</sup> P°	3952.239	A	1h	26.65	29.79	2—2	
4912.332	A	4	25.56	28.09	1—1	8.15	3956.55	A	1h	26.66	29.79	1—1	
m4943.260	P	O II	25.56	28.07	1—0								
							3681.402	A	7h	26.65	30.02	2—1	5p <sup>3</sup> P° —7s <sup>3</sup> S
							3682.15	A	5h	26.66	30.02	1—1	10.09
							3682.25	A	2h	26.66	30.02	0—1	

Multiplet Table

Si III—Continued

Si III—Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Air							Air						
3321.578	A	4	26.65	30.39	2—3	5p <sup>3</sup> P° —4p' <sup>3</sup> D	6111.571	A	1	28.09	30.11	1—1	4s' <sup>3</sup> P° —4p' <sup>1</sup> P
3346.717	A	2	26.66	30.36	1—2	10.10							12.07
3361.343	P		26.66	30.34	0—1		5473.045	A	7	28.12	30.39	2—3	4s' <sup>3</sup> P° —4p' <sup>3</sup> D
							5451.462	A	6	28.09	30.36	1—2	12.08
3013.091	A	5	26.65	30.77	2—2	5p <sup>3</sup> P° —4p' <sup>3</sup> P	5451.961	A	4	28.07	30.34	0—1	
3032.66	A	4*	26.65	30.74	2—1	10.11	5539.926	A	3	28.12	30.36	2—2	
							5490.114	A	3	28.09	30.34	1—1	
2959.150	A	5	26.65	30.84	2—1	5p <sup>3</sup> P° —4p' <sup>3</sup> S	5579.94	A	0	28.12	30.34	2—1	
*2959.67	A	3*	26.66	30.84	1—1	UV 91							
*2959.67	A	3*	26.66	30.84	0—1		4683.022	A	9	28.12	30.77	2—2	4s' <sup>3</sup> P° —4p' <sup>3</sup> P
							4665.869	A	8	28.09	30.74	1—1	13
2874.626	A	4	26.65	30.97	2—1	5p <sup>3</sup> P° —8s <sup>3</sup> S	4730.519	A	7	28.12	30.74	2—1	
*2875.09	A	2*	26.66	30.97	1—1	UV 92	4683.797	A	7	28.09	30.73	1—0	
*2875.09	A	2*	26.66	30.97	0—1		4619.657	A	7	28.09	30.77	1—2	
							4638.277	A	7	28.07	30.74	0—1	
7442.327	A	4h	26.80	28.47	2—1	3d' <sup>3</sup> P° —6s <sup>3</sup> S	4734.627	A	2	28.12	30.74	2—2	4s' <sup>3</sup> P° —4p' <sup>1</sup> D
7497.286	A	3h	26.82	28.47	1—1	10.12	4669.89	A	1	28.09	30.74	1—2	14
7532.055	A	1h	26.82	28.47	0—1								
							4553.996	A	8	28.12	30.84	2—1	4s' <sup>3</sup> P° —4p' <sup>3</sup> S
3126.267	A	6	26.80	30.77	2—2	3d' <sup>3</sup> P° —4p' <sup>3</sup> P	4494.048	A	6	28.09	30.84	1—1	15
3157.159	A	1	26.82	30.74	1—1	11	4468.452	A	2	28.07	30.84	0—1	
3147.371	A	7	26.80	30.74	2—1								
*3165.38§	A	2	26.82	30.73	1—0		4482.884	A	3h	28.12	30.89	2—3	4s' <sup>3</sup> P° —7d <sup>3</sup> D
3135.906	A	3	26.82	30.77	1—2		4428.146	A	1h	28.09	30.88	1—2	16
3163.281	A	2	26.82	30.74	0—1		4486.28	A	0h	28.12	30.88	2—2	
3068.238	A	7	26.80	30.84	2—1	3d' <sup>3</sup> P° —4p' <sup>3</sup> S							
3077.523	A	4	26.82	30.84	1—1	11.01	6524.357	A	6h	28.15	30.05	3—4	5d <sup>3</sup> D —6f <sup>3</sup> F°
3083.363	A	2	26.82	30.84	0—1		6522.626	A	4h	28.15	30.05	2—3	17
							6521.485	A	3h	28.15	30.05	1—2	
4379.876	A	1h	26.96	29.79	3—3	3d' <sup>3</sup> D° —6d <sup>3</sup> D	5599.246	A	4	28.15	30.37	3—2	5d <sup>3</sup> D —7p <sup>3</sup> P°
						11.02	5600.952	A	3	28.15	30.37	2—1	18
3622.538	A	8h	26.96	30.39	3—3	3d' <sup>3</sup> D° —4p' <sup>3</sup> D	5601.461	A	2	28.15	30.37	1—0	
3645.123	A	6h	26.96	30.36	2—2	11.03	5597.90	A	0.5	28.15	30.37	2—2	
3655.112	A	4h	26.95	30.34	1—1		5600.00	A	0	28.15	30.37	1—1	
3651.721	A	2h	26.96	30.36	3—2								
3662.366	A	2h	26.96	30.34	2—1		4406.721	A	8h	28.15	30.97	3—4	5d <sup>3</sup> D —7f <sup>3</sup> F°
3616.040	A	1h	26.96	30.39	2—3		4405.901	A	6h	28.15	30.97	2—3	19
3637.943	A	2h	26.95	30.36	1—2		4405.351	A	4h	28.15	30.97	1—2	
3258.664	A	12	26.96	30.77	3—2	3d' <sup>3</sup> D° —4p' <sup>3</sup> P	3639.445	A	5h	28.15	31.56	3—4	5d <sup>3</sup> D —8f <sup>3</sup> F°
3276.264	A	10	26.96	30.74	2—1	12	3638.898	A	3h	28.15	31.56	2—3	20
3279.258	A	7	26.95	30.73	1—0		3638.524	A	2h	28.15	31.56	1—2	
3253.401	A	7	26.96	30.77	2—2								
3270.456	A	6	26.95	30.74	1—1		3251.871	A	1h	28.15	31.97	3—	5d <sup>3</sup> D —9f <sup>3</sup> F°
							3251.383	A	0.5	28.15	31.97	2—	21
3283.570	A	1	26.96	30.74	3—2	3d' <sup>3</sup> D° —4p' <sup>1</sup> D	3251.07	P	0h	28.15	31.97	1—	
						12.01							
5898.788	A	10h	27.96	30.06	3—4	5f <sup>1</sup> F° —6g <sup>1</sup> G	6169.835	A	3h	28.23	30.24	2—3	5d <sup>1</sup> D —6f <sup>1</sup> F°
						12.02							22
4461.27	A	0	27.96	30.74	3—2	5f <sup>1</sup> F° —4p' <sup>1</sup> D	5810.187	A	3h	28.23	30.36	2—1	5d <sup>1</sup> D —7p <sup>1</sup> P°
						12.03							23
4115.504	A	5h	27.96	30.97	3—4	5f <sup>1</sup> F° —7g <sup>1</sup> G	m4403.830	P	Si iv	28.23	31.04	2—3	5d <sup>1</sup> D —7f <sup>1</sup> F°
						12.04							24
3440.37	A	5*	27.96	31.56	3—4	5f <sup>1</sup> F° —8g <sup>1</sup> G	3676.731	A	3h	28.23	31.60	2—3	5d <sup>1</sup> D —8f <sup>1</sup> F°
						12.05							25
7408.467	A	3h	28.12	29.79	2—3	4s' <sup>3</sup> P° —6d <sup>3</sup> D	8436.487	A	1h	28.35	29.82	1—2	3d' <sup>1</sup> P° —6d <sup>1</sup> D
7267.090	A	2h	28.09	29.79	1—2	12.06							26
7211.836	A	1h	28.07	29.79	0—1								
7425.10	A	1h	28.12	29.79	2—2		*7047.58§	A	5h	28.35	30.11	1—1	3d' <sup>1</sup> P° —4p' <sup>1</sup> P
7278.79	A	0h	28.09	29.79	1—1								27



Multiplet Table

Si III—Continued

Si III—Continued

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Air 5135.110	A	3	28.35	30.77	1—2	$3d' ^1P^\circ - 4p' ^3P_{28}$	8341.931	A	2h	29.25	30.74	1—2	$4s' ^1P^\circ - 4p' ^1D_{44}$
5197.264	A	5	28.35	30.74	1—2	$3d' ^1P^\circ - 4p' ^1D_{29}$	7189.072	A	1h	29.25	30.98	1—0	$4s' ^1P^\circ - 8s ^1S_{45}$
8191.679	A	8h	28.55	30.06	4—5	$5f ^3F^\circ - 6g ^3G_{30}$	4341.400	A	8	29.25	32.11	1—0	$4s' ^1P^\circ - 4p' ^1S_{46}$
8191.16	A	6h	28.55	30.06	3—4		2157.280	A	2	29.25	35.00	1—1	$4s' ^1P^\circ - 5p' ^1P?_{UV\ 95}$
*8190.431	A	7h	28.55	30.06	2—3								
*8190.431	A	7h	28.55	30.06	3—4	$5f ^3F^\circ - 6g ^1G_{31}$	5724.609	A	1h	29.82	31.99	2—3	$6d ^1D - 9f ^1F^\circ_{47}$
5303.415	A	2	28.55	30.89	4—3	$5f ^3F^\circ - 7d ^3D_{32}$							
5307.709	A	1	28.55	30.88	3—2		8212.05	A	2H	30.05	31.56		$6f ^3F^\circ - 8g ^3G_{48}$
5310.390	A	1	28.55	30.88	2—1		6662.95	A	0H	30.05	31.91		$6f ^3F^\circ - 9d ^3D_{49}$
5114.116	A	8h	28.55	30.97	4—5	$5f ^3F^\circ - 7g ^3G_{33}$	6473.96	A	1H	30.05	31.97		$6f ^3F^\circ - 9g ^3G_{50}$
*5113.76	A	7h	28.55	30.97	3—4								
*5113.76	A	7h	28.55	30.97	2—3		8194.71	A	3H*	30.06	31.57	5—	$6g ^3,1G - 8h ^3,1H^\circ_{51}$
4211.679	A	2h	28.55	31.49	4—3	$5f ^3F^\circ - 8d ^3D_{34}$	8194.18	A	3H	30.06	31.57	4,3—	
4111.512	A	3h	28.55	31.56	4—5	$5f ^3F^\circ - 8g ^3G_{35}$	6471.86	A	2H	30.06	31.98	5—	$6g ^3G - 9h ^3,1H^\circ_{52}$
4111.255	A	2h	28.55	31.56	3—4								
8255.81	A	1H	28.55	30.05		$5g ^3G - 6f ^3F^\circ_{36}$	8292.615	A	3h	30.08	31.58		$6h ^3,1H^\circ - 8i ^3,1I_{53}$
8103.448	A	11h	28.55	30.08	5—	$5g ^3,1G - 6h ^3,1H^\circ_{37}$	6535.163	A	2h	30.08	31.98		$6h ^3,1H^\circ - 9i ^3,1I_{54}$
8102.862	A	9h	28.55	30.08	4,3—		4064.113	A	2h	30.11	33.16	1—2	$4p' ^1P - 4d' ^1D^\circ?_{55}$
5091.419	A	10h	28.55	30.99		$5g ^3,1G - 7h ^3,1H^\circ_{38}$	9173.267	A	2h	30.24	31.59	3—2	$6f ^1F^\circ - 8d ^1D_{56}$
4101.86	A	5H	28.55	31.57		$5g ^3,1G - 8h ^3,1H^\circ_{39}$	7151.08	A	2H	30.24	31.97	3—2	$6f ^1F^\circ - 9d ^1D_{57}$
3619.581	A	3h	28.55	31.98	5—	$5g ^3G - 9h ^3,1H^\circ_{40}$	4423.556	A	4h	30.39	33.19	3—4	$4p' ^3D - 4d' ^3F^\circ?_{58}$
6152.556	A	2	29.06	31.07	1—2	$6p ^1P^\circ - 7d ^1D_{41}$	8728.019	A	3h	33.16	34.58	2—3	$4d' ^1D^\circ - 4f' [3\frac{1}{2}]?_{59}$
6810.594	A	1h	29.07	30.89	2—3	$6p ^3P^\circ - 7d ^3D_{42}$	4351.974	A	2h	34.58	37.43	3—4	$4f' [2\frac{1}{2}] - 5g' [3\frac{1}{2}]^\circ?_{60}$
6812.200	A	0.5	29.06	30.88	1—2		4352.810	A	2h	34.58	37.43	3—3	
6810.79	A	0h	29.06	30.88	0—1								
7984.20	A	0h	29.19	30.74	3—2	$3d' ^1F^\circ - 4p' ^1D_{43}$	4356.821	A	4h	(34.58	37.43)	4—5	$4f' [3\frac{1}{2}] - 5g' [4\frac{1}{2}]^\circ?_{61}$
2296.873	A	10	29.19	34.58	3—3	$3d' ^1F^\circ - 4f' [3\frac{1}{2}]?_{UV\ 93}$	4355.525	A	3h	(34.58	37.43)	4—4	
Vac 1513.533	A	2	29.19	37.38	3—3	$3d' ^1F^\circ - 5f' [3\frac{1}{2}]?_{UV\ 94}$	4355.281	A	3h	34.58	37.43	3—4	
							4356.100	A	2h	34.58	37.43	3—3	$[3\frac{1}{2}]^\circ?$



NSRDS-NBS 3, SECTION 1

**SILICON,  $Z=14$**

A Si iv Atomic Energy Levels

B Si iv Multiplet Table





## Part A

## SILICON

## Si IV

(Na I sequence; 11 electrons)

 $Z=14$ Ground state  $1s^2 2s^2 2p^6 3s^2 S_{0\frac{1}{2}}$  $3s^2 S_{0\frac{1}{2}}$  **364093.1**  $\pm 0.6$   $\text{cm}^{-1}$ , 274.655 Å (Vac)

I P 45.14 eV

Toresson has reobserved the spectrum from 400 Å to 10000 Å. He has revised and extended the entire term system and thus made it possible to calculate reliable wavelengths for extended series members.

The limit is well determined by application of the polarization formula to the hydrogen-like terms  $4,5f^2 F^\circ$  and  $5g^2 G$ . The undisturbed  $nf$ ,  $ng$ ,  $nh$  and  $ni$  series are excellently represented.

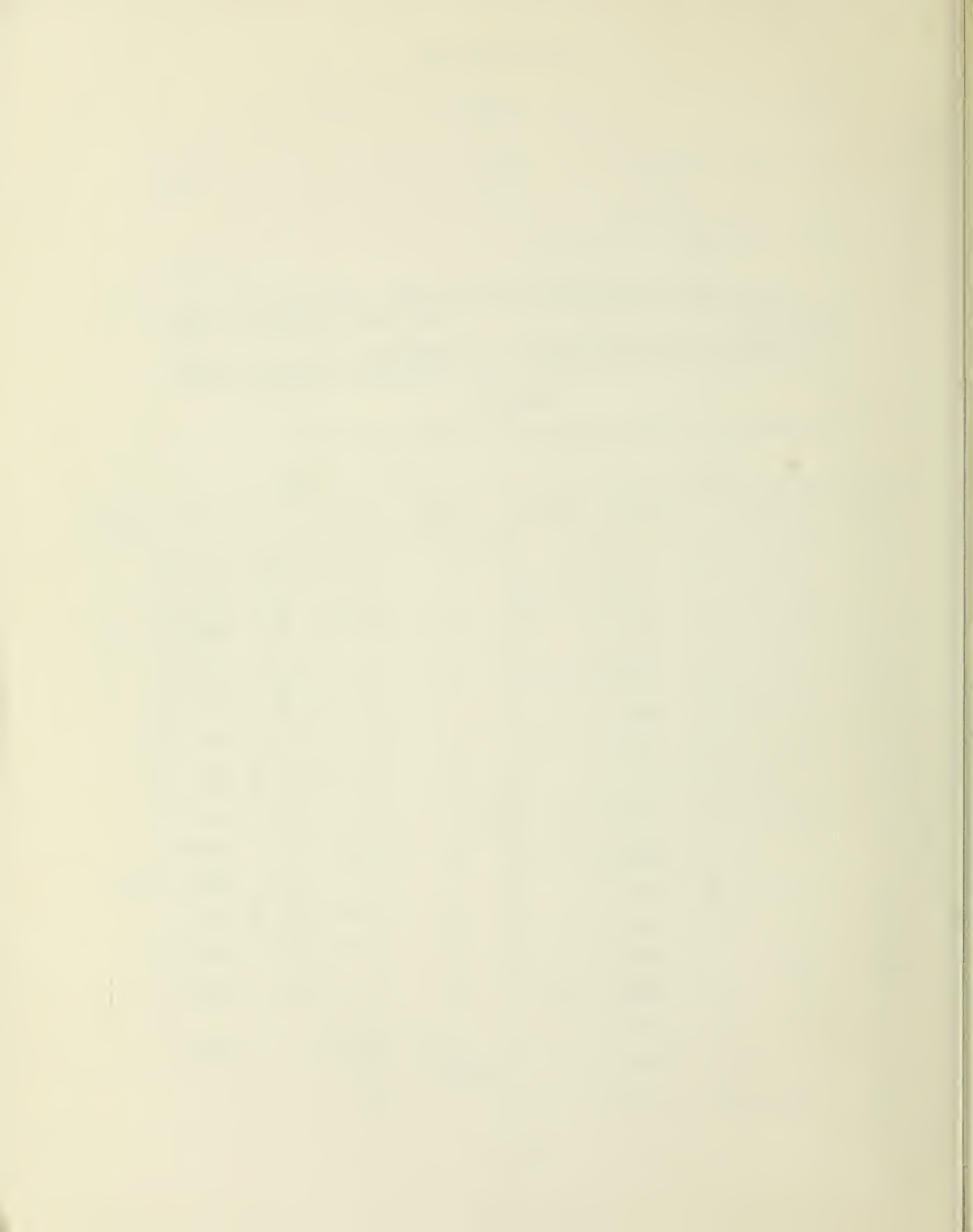
## REFERENCE

Y. G. Toresson, Ark. Fys. (Stockholm) 17, No. 12, 179 to 192 (1960). I P, T, C L, G D

## Si IV

## Si IV

Config.	Desig.	$J$	Level	Interval	Config.	Desig.	$J$	Level	Interval
3s	3s $^2S$	$0\frac{1}{2}$	0. 00		6h	6h $^2H^\circ$ { $4\frac{1}{2}$ $5\frac{1}{2}$ }		315317. 36	
3p	3p $^2P^\circ$	$0\frac{1}{2}$ $1\frac{1}{2}$	71287. 54 71748. 64	461. 10	7s	7s $^2S$	$0\frac{1}{2}$	318742. 79	
3d	3d $^2D$	$2\frac{1}{2}$ $1\frac{1}{2}$	160374. 41 160375. 60	-1. 19	7p	7p $^2P^\circ$	$0\frac{1}{2}$ $1\frac{1}{2}$	322312. 93 322337. 83	24. 90
4s	4s $^2S$	$0\frac{1}{2}$	193978. 89		7d	7d $^2D$ { $1\frac{1}{2}$ $2\frac{1}{2}$ }		327361. 97	
4p	4p $^2P^\circ$	$0\frac{1}{2}$ $1\frac{1}{2}$	218266. 86 218428. 67	161. 81	7f	7f $^2F^\circ$ { $2\frac{1}{2}$ $3\frac{1}{2}$ }		328200. 04	
4d	4d $^2D$	$2\frac{1}{2}$ $1\frac{1}{2}$	250008. 02 250008. 14	-0. 12	7g	7g $^2G$ { $3\frac{1}{2}$ $4\frac{1}{2}$ }		328249. 64	
4f	4f $^2F^\circ$	$2\frac{1}{2}$ $3\frac{1}{2}$	254127. 08 254129. 03	1. 95	7h	7h $^2H^\circ$ { $4\frac{1}{2}$ $5\frac{1}{2}$ }		328257. 12	
5s	5s $^2S$	$0\frac{1}{2}$	265417. 95		7i	7i $^2I$ { $5\frac{1}{2}$ $6\frac{1}{2}$ }		328260. 76	
5p	5p $^2P^\circ$	$0\frac{1}{2}$ $1\frac{1}{2}$	276503. 67 276579. 03	75. 36	8s	8s $^2S$	$0\frac{1}{2}$	330439. 66	
5d	5d $^2D$	$1\frac{1}{2}$ $2\frac{1}{2}$	291497. 50 291497. 60	0. 10	8p	8p $^2P^\circ$	$0\frac{1}{2}$ $1\frac{1}{2}$	332743. 87 332759. 92	16. 05
5f	5f $^2F^\circ$	{ $2\frac{1}{2}$ $3\frac{1}{2}$ }	293718. 99		8d	8d $^2D$ { $1\frac{1}{2}$ $2\frac{1}{2}$ }		336051. 55	
5g	5g $^2G$	{ $3\frac{1}{2}$ $4\frac{1}{2}$ }	293837. 92		8f	8f $^2F^\circ$ { $2\frac{1}{2}$ $3\frac{1}{2}$ }		336616. 55	
6s	6s $^2S$	$0\frac{1}{2}$	299676. 95		8g	8g $^2G$ { $3\frac{1}{2}$ $4\frac{1}{2}$ }		336650. 69	
6p	6p $^2P^\circ$	$0\frac{1}{2}$ $1\frac{1}{2}$	305641. 10 305682. 27	41. 17	-----				
6d	6d $^2D$	{ $1\frac{1}{2}$ $2\frac{1}{2}$ }	313914. 92		Si v ( $^1S_0$ )	Limit	-----	364093. 1	
6f	6f $^2F^\circ$	{ $2\frac{1}{2}$ $3\frac{1}{2}$ }	315230. 27		May 1964.				
6g	6g $^2G$	{ $3\frac{1}{2}$ $4\frac{1}{2}$ }	315305. 28						



# Multiplet Table

Part B

SILICON

Si IV (Z=14)

I P 45.14 eV Limit 364093.1  $\pm 0.6$  cm<sup>-1</sup> 274.655 Å (Vac)

Anal A List A April 1964

## REFERENCES

- A Y. G. Toresson, Ark. Fys. (Stockholm) 17, No. 12, 179 to 192 (1960).  
I P, T, C L, I, G D; W L 400 Å to 10000 Å  
P Predicted Wavelength  
New Multiplet Numbers, not inserted between older ones, start with UV 5 and 8.

Si IV

Si IV

I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Vac							Vac						
1393.755	A	15	0.00	8.90	0½—1½	3s 2S —3p 2P°	860.551	P		19.88	34.29	2½—1½	3d 2D —5p 2P°
1402.769	A	12	0.00	8.84	0½—0½	UV 1	861.118	P		19.88	34.28	1½—0½	UV 12
							860.560	P		19.88	34.29	1½—1½	
457.818	A	4	0.00	27.08	0½—1½	3s 2S —4p 2P°	749.941	A	5	19.88	36.42		3d 2D —5f 2F°
458.155	A	3	0.00	27.06	0½—0½	UV 2							UV 13
361.560	P		0.00	34.29	0½—1½	3s 2S —5p 2P°	688.194	P		19.88	37.90	2½—1½	3d 2D —6p 2P°
361.659	P		0.00	34.28	0½—0½	UV 2.01	688.395	P		19.88	37.89	1½—0½	UV 14
327.137	P		0.00	37.90	0½—1½	3s 2S —6p 2P°	688.200	P		19.88	37.90	1½—1½	
327.181	P		0.00	37.89	0½—0½	UV 2.02	645.759	A	2	19.88	39.08		3d 2D —6f 2F°
													UV 15
1128.340	A	10	8.90	19.88	1½—2½	3p 2P°—3d 2D							
1122.486	A	8	8.84	19.88	0½—1½	UV 3	Air						
1128.325	P		8.90	19.88	1½—1½		4088.854	A	10	24.05	27.08	0½—1½	4s 2S —4p 2P°
							4116.097	A	9	24.05	27.06	0½—0½	1
818.129	A	8	8.90	24.05	1½—0½	3p 2P°—4s 2S							
815.049	A	7	8.84	24.05	0½—0½	UV 4	Vac						
							1210.652	P		24.05	34.29	0½—1½	4s 2S —5p 2P°
560.980	P		8.90	31.00	1½—	3p 2P° —4d 2D	1211.757	P		24.05	34.28	0½—0½	UV 16
559.533	P		8.84	31.00	0½—1½	UV 5							
516.348	A	3	8.90	32.91	1½—0½	3p 2P° —5s 2S	895.228	P		24.05	37.90	0½—1½	4s 2S —6p 2P°
515.118	A	2	8.84	32.91	0½—0½	UV 6	895.558	P		24.05	37.89	0½—0½	UV 17
455.065	P		8.90	36.14	1½—	3p 2P° —5d 2D							
454.112	P		8.84	36.14	0½—1½	UV 7	Air						
							*3165.710	A	9	27.08	31.00	1½—2½	4p 2P°—4d 2D
438.734	P		8.90	37.15	1½—0½	3p 2P° —6s 2S	3149.561	A	7	27.06	31.00	0½—1½	2
437.849	P		8.84	37.15	0½—0½	UV 8	*3165.710	A	9	27.08	31.00	1½—1½	
412.939	P		8.90	38.91	1½—	3p 2P° —6d 2D	2127.467	A	4	27.08	32.91	1½—0½	4p 2P°—5s 2S
412.155	P		8.84	38.92	0½—1½	UV 9	2120.179	A	3	27.06	32.91	0½—0½	UV 18
*1722.534	A	6	19.88	27.08	2½—1½	3d 2D —4p 2P°	Vac						
1727.377	A	5	19.88	27.06	1½—0½	UV 10	1368.571	P		27.08	36.14	1½—2½	4p 2P°—5d 2D
*1722.534	A	6	19.88	27.08	1½—1½		1365.549	P		27.06	36.14	0½—1½	UV 19
							1368.573	P		27.08	36.14	1½—1½	
1066.629	A	8	19.88	31.51		3d 2D —4f 2F°	1230.795	P		27.08	37.15	1½—0½	4p 2P°—6s 2S
						UV 11	1228.349	P		27.06	37.15	0½—0½	UV 20
							1047.271	P		27.08	38.92	1½—	4p 2P°—6d 2D
							1045.500	P		27.06	38.92	0½—1½	UV 21



Multiplet Table

Si IV—Continued

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I A	Ref	Int	E P		J	Multiplet No.	I A	Ref	Int	E P		J	Multiplet No.
			Low	High						Low	High		
Air							Air						
*3762.435	A	8	31.00	34.29	$2\frac{1}{2}-1\frac{1}{2}$	$4d\ ^2D - 5p\ ^2P^\circ$	4628.62	A	3H	36.42	39.09		$5f\ ^2F^\circ - 6h\ ^2H^\circ$
3773.151	A	6	31.00	34.28	$1\frac{1}{2}-0\frac{1}{2}$	3							6.01F
*3762.435	A	8	31.00	34.29	$1\frac{1}{2}-1\frac{1}{2}$		2971.522	A	1h	36.42	40.59		$5f\ ^2F^\circ - 7d\ ^2D$
2287.041	A	5h	31.00	36.42		$4d\ ^2D - 5f\ ^2F^\circ$							UV 33
						UV 22	2895.131	A	3hl	36.42	40.70		$5f\ ^2F^\circ - 7g\ ^2G$
Vac													UV 34
1796.162	P		31.00	37.90	$2\frac{1}{2}-1\frac{1}{2}$	$4d\ ^2D - 6p\ ^2P^\circ$	2328.56	A	2H	36.42	41.74		$5f\ ^2F^\circ - 8g\ ^2G$
1797.496	P		31.00	37.89	$1\frac{1}{2}-0\frac{1}{2}$	UV 23							UV 35
1796.166	P		31.00	37.90	$1\frac{1}{2}-1\frac{1}{2}$								
1533.220	P		31.00	39.08		$4d\ ^2D - 6f\ ^2F^\circ$							
						UV 24	4673.297	A	2h	36.43	39.08		$5g\ ^2G - 6f\ ^2F^\circ$
Air													6.02
2675.249	A	4	31.51	36.14	$3\frac{1}{2}-2\frac{1}{2}$	$4f\ ^2F^\circ - 5d\ ^2D$	4656.92	A	3H	36.43	39.09		$5g\ ^2G - 6g\ ^2G$
*2675.120	A	4	31.51	36.14	$2\frac{1}{2}-$	UV 25							6.03F
2517.506	A	7	31.51	36.43		$4f\ ^2F^\circ - 5g\ ^2G$	4654.323	A	10hs	36.43	39.09		$5g\ ^2G - 6h\ ^2H^\circ$
						UV 26							7
Vac							2904.470	A	2h	36.43	40.70		$5g\ ^2G - 7h\ ^2H^\circ$
1672.612	P		31.51	38.92		$4f\ ^2F^\circ - 6d\ ^2D$							UV 36
						UV 27							
1634.607	A	1	31.51	39.09		$4f\ ^2F^\circ - 6g\ ^2G$							
						UV 28	4411.652	A	0h	37.15	39.96	$0\frac{1}{2}-1\frac{1}{2}$	$6s\ ^2S - 7p\ ^2P^\circ$
Air							m4416.506	P	O II	37.15	39.96	$0\frac{1}{2}-0\frac{1}{2}$	8
8957.245	A	2h	32.91	34.29	$0\frac{1}{2}-1\frac{1}{2}$	$5s\ ^2S - 5p\ ^2P^\circ$							
9018.162	A	1h	32.91	34.28	$0\frac{1}{2}-0\frac{1}{2}$	3.01	7654.555	A	4h	37.90	39.52	$1\frac{1}{2}-0\frac{1}{2}$	$6p\ ^2P^\circ - 7s\ ^2S$
							7630.497	A	2h	37.89	39.52	$0\frac{1}{2}-0\frac{1}{2}$	9
2482.816	A	2	32.91	37.90	$0\frac{1}{2}-1\frac{1}{2}$	$5s\ ^2S - 6p\ ^2P^\circ$	4611.27	A	0h	37.90	40.59	$1\frac{1}{2}-$	$6p\ ^2P^\circ - 7d\ ^2D$
2485.378	A	1	32.91	37.89	$0\frac{1}{2}-0\frac{1}{2}$	UV 29	m4602.578	P	O II	37.89	40.59	$0\frac{1}{2}-1\frac{1}{2}$	10
*6701.207	A	7	34.29	36.14	$1\frac{1}{2}-2\frac{1}{2}$	$5p\ ^2P^\circ - 5d\ ^2D$	4038.057	A	2h	37.90	40.97	$1\frac{1}{2}-0\frac{1}{2}$	$6p\ ^2P^\circ - 8s\ ^2S$
6667.556	A	5	34.28	36.14	$0\frac{1}{2}-1\frac{1}{2}$	3.02	4031.39	A	1h*	37.89	40.97	$0\frac{1}{2}-0\frac{1}{2}$	11
*6701.207	A	7	34.29	36.14	$1\frac{1}{2}-1\frac{1}{2}$								
4328.175	A	5	34.29	37.15	$1\frac{1}{2}-0\frac{1}{2}$	$5p\ ^2P^\circ - 6s\ ^2S$	6998.358	A	3h	38.92	40.69		$6d\ ^2D - 7f\ ^2F^\circ$
4314.104	A	3	34.28	37.15	$0\frac{1}{2}-0\frac{1}{2}$	4							12
2677.57	A	1*	34.29	38.92	$1\frac{1}{2}-$	$5p\ ^2P^\circ - 6d\ ^2D$	5304.971	A	2h	38.92	41.26	$-1\frac{1}{2}$	$6d\ ^2D - 8p\ ^2P^\circ$
2672.193	A	1	34.28	38.92	$0\frac{1}{2}-1\frac{1}{2}$	UV 30	5309.493	A	1h	38.92	41.25	$1\frac{1}{2}-0\frac{1}{2}$	13
2370.985	A	3	34.29	39.52	$1\frac{1}{2}-0\frac{1}{2}$	$5p\ ^2P^\circ - 7s\ ^2S$	4403.734	A	2hl	38.92	41.73		$6d\ ^2D - 8f\ ^2F^\circ$
2366.755	A	2	34.28	39.52	$0\frac{1}{2}-0\frac{1}{2}$	UV 31							14
*7047.939	A	6h	36.14	37.90	$2\frac{1}{2}-1\frac{1}{2}$	$5d\ ^2D - 6p\ ^2P^\circ$	8240.606	A	1h	39.08	40.59		$6f\ ^2F^\circ - 7d\ ^2D$
7068.410	A	4h	36.14	37.89	$1\frac{1}{2}-0\frac{1}{2}$	4.01							15
*7047.939	A	6h	36.14	37.90	$1\frac{1}{2}-1\frac{1}{2}$		7678.748	A	4hl	39.08	40.70		$6f\ ^2F^\circ - 7g\ ^2G$
													16
4212.407	A	7hl	36.14	39.08		$5d\ ^2D - 6f\ ^2F^\circ$	4667.14	A	1H	39.08	41.74		$6f\ ^2F^\circ - 8g\ ^2G$
						5							17
m3241.583	P	Si III	36.14	39.96	$2\frac{1}{2}-1\frac{1}{2}$	$5d\ ^2D - 7p\ ^2P^\circ$	7752.905	A	1h	39.09	40.69		$6g\ ^2G - 7f\ ^2F^\circ$
3244.192	A	1h	36.14	39.96	$1\frac{1}{2}-0\frac{1}{2}$	5.01							18
m3241.572	P	Si III	36.14	39.96	$1\frac{1}{2}-1\frac{1}{2}$		7718.785	A	5hl	39.09	40.70		$6g\ ^2G - 7h\ ^2H^\circ$
													19
2723.812	A	3h	36.14	40.69		$5d\ ^2D - 7f\ ^2F^\circ$							
						UV 32	7730.469	A	1h	39.09	40.70		$6h\ ^2H^\circ - 7g\ ^2G$
													20
4950.105	A	3	36.42	38.92		$5f\ ^2F^\circ - 6d\ ^2D$	7725.64	A	2H	39.09	40.70		$6h\ ^2H^\circ - 7h\ ^2H^\circ$
						5.02							21F
4647.45	A	1hl	36.42	39.08		$5f\ ^2F^\circ - 6f\ ^2F^\circ$	7723.818	A	6hs	39.09	40.70		$6h\ ^2H^\circ - 7i\ ^2I$
						5.03F							22
4631.241	A	9hl	36.42	39.09		$5f\ ^2F^\circ - 6g\ ^2G$							
						6							





