

A11100 988761

NAT'L INST OF STANDARDS & TECH R.I.C.



A11100988761

/NBS monograph  
QC100 .U556 V60:62-69;1963-64 C.1 NBS-PU



DATE DUE

APR 6

1982

**GAYLORD**

PRINTED IN U.S.A.







National Bureau of Standards  
Library, N.W. Bldg

MAY 1 1963

NBS MONOGRAPH 60

National Bureau of Standards

100-100002

1200

QC

100

LL556

# Influence of a Sector Ground Screen On the Field of a Vertical Antenna



U.S. DEPARTMENT OF COMMERCE  
NATIONAL BUREAU OF STANDARDS

## THE NATIONAL BUREAU OF STANDARDS

### Functions and Activities

The functions of the National Bureau of Standards are set forth in the Act of Congress, March 3, 1901, as amended by Congress in Public Law 619, 1950. These include the development and maintenance of the national standards of measurement and the provision of means and methods for making measurements consistent with these standards; the determination of physical constants and properties of materials; the development of methods and instruments for testing materials, devices, and structures; advisory services to government agencies on scientific and technical problems; invention and development of devices to serve special needs of the Government; and the development of standard practices, codes, and specifications. The work includes basic and applied research, development, engineering, instrumentation, testing, evaluation, calibration services, and various consultation and information services. Research projects are also performed for other government agencies when the work relates to and supplements the basic program of the Bureau or when the Bureau's unique competence is required. The scope of activities is suggested by the listing of divisions and sections on the inside of the back cover.

### Publications

The results of the Bureau's research are published either in the Bureau's own series of publications or in the journals of professional and scientific societies. The Bureau itself publishes three periodicals available from the Government Printing Office: The Journal of Research, published in four separate sections, presents complete scientific and technical papers; the Technical News Bulletin presents summary and preliminary reports on work in progress; and Central Radio Propagation Laboratory Ionospheric Predictions provides data for determining the best frequencies to use for radio communications throughout the world. There are also five series of nonperiodical publications: Monographs, Applied Mathematics Series, Handbooks, Miscellaneous Publications, and Technical Notes.

A complete listing of the Bureau's publications can be found in National Bureau of Standards Circular 460, Publications of the National Bureau of Standards, 1901 to June 1947 (\$1.25), and the Supplement to National Bureau of Standards Circular 460, July 1947 to June 1957 (\$1.50), and Miscellaneous Publication 240, July 1957 to June 1960 (includes Titles of Papers Published in Outside Journals 1950 to 1959) (\$2.25); available from the Superintendent of Documents, U.S. Government Printing Office, Washington 25, D.C.

UNITED STATES DEPARTMENT OF COMMERCE • Luther H. Hodges, *Secretary*

NATIONAL BUREAU OF STANDARDS • A. V. Astin, *Director*

# Influence of a Sector Ground Screen on the Field of a Vertical Antenna

James R. Wait and Lillie C. Walters

Central Radio Propagation Laboratory  
National Bureau of Standards  
Boulder, Colorado



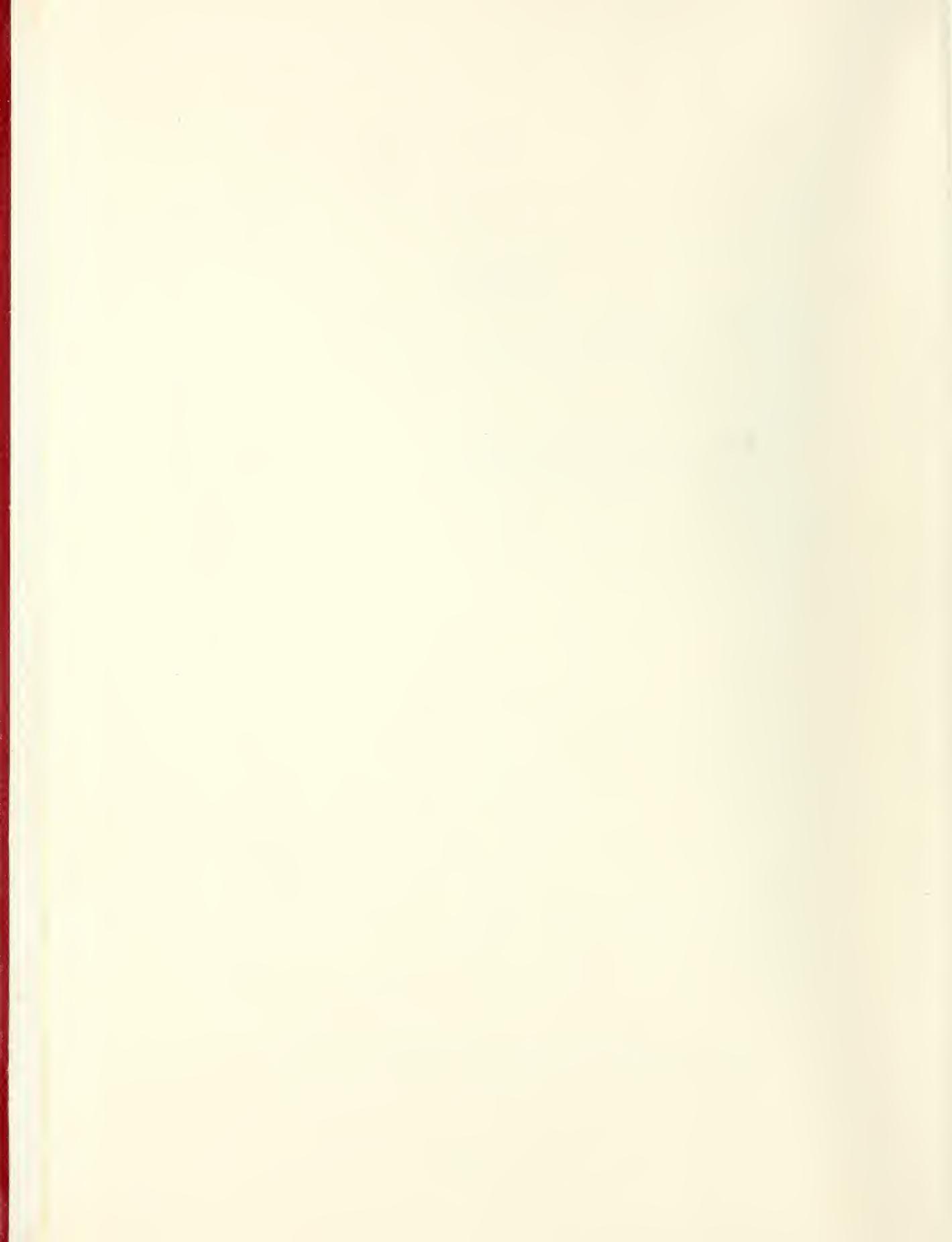
National Bureau of Standards Monograph 60

Issued April 15, 1963

Library of Congress Catalogue Card Number: 63-60051

## Contents

	Page
1. Introduction-----	1
2. Formulation and description of problem-----	1
3. The circular screen-----	2
4. The sector screen-----	3
5. Final remarks-----	5
6.. Appendix-----	6
6.1. Evaluation of the Fresnel integral-----	6
6.2. Evaluation of $G_b$ by Gaussian quadrature-----	6
7. References-----	6
7.1. Additional references-----	7
Figures-----	7
Tables-----	12



# Influence of a Sector Ground Screen on the Field of a Vertical Antenna<sup>1</sup>

James R. Wait and Lillie C. Walters

The field of a short vertical antenna on a homogeneous ground is shown to be modified by the presence of a metallic screen. The screen is taken in the form of a circular disk and a concentric sector. The modification of the field is expressed in the form of surface integrals over the disk and the sector. Extensive numerical results for these basic integrals are given and a number of applications are illustrated.

## 1. Introduction

The influence of the ground on the fields of antennas has been discussed sporadically in the literature for many years. In most propagation calculations it is assumed that the transmitting antenna has a fixed dipole moment and the ground is taken to be a perfect conductor or possibly a homogeneous imperfectly conducting half space. In practice, however, some kind of ground system is used. Usually this takes the form of a metal screen or radial wire system which is on the surface of the ground or may be buried slightly beneath the surface. The design of such systems has been typically empirical. Apparently, the first analytical approach was carried out by Brown et al. [1].<sup>2</sup> Later works [2, 3] have dealt mainly with the influence of the ground system on the impedance. In most cases it has been assumed that the radiated field for a given current on the

antenna was not appreciably affected by the presence of the ground screen. In fact, an approximate analytical method was given previously by Wait and Pope [4] which is suitable for estimating the dependence of the ground wave on the size of a circular ground screen. Calculations [5] based on this work supported the contention that a screen has only a small effect on the radiated field provided the radius of the screen is of the order of a wavelength or less. Very similar conclusions have been arrived at by British workers [6, 7].

In this paper consideration is given to ground screens which may be large in terms of a wavelength. Since the theory has been treated quite generally in a previous paper [8], attention will be focused here on the numerical calculations and the predicted performance.

## 2. Formulation and Description of Problem

The situation is described as follows. A vertical electric dipole is located on a flat homogeneous ground of conductivity  $\sigma$  and dielectric constant  $\epsilon$ . The vertical electric field  $E$  at a distance  $R_0$  and elevation angle  $\psi_0$  is given as follows

$$E_v = \frac{i\mu_0\omega lI}{2\pi R_0} e^{-ikR_0} \cos^2 \psi_0 W(R_0, Z) \quad (1)$$

where

$$\mu_0 = 4\pi \times 10^{-7}$$

$\omega$  = angular frequency

$l$  = effective height of transmitting dipole

$I$  = current at terminals of transmitting dipole

$k = 2\pi/\text{wavelength}$ .

In the above,  $W(R_0, Z)$  is a complex quantity which is a function of the surface impedance  $Z$  of the ground. Over a perfectly conducting ground,  $W$  would approach unity. In the case of finite

ground conductivity [9]

$$W(R_0, Z) \approx 1 - i(\pi p_0)^{1/2} e^{-w_0} \operatorname{erfc}(iw_0^{1/2}) \quad (2)$$

where

$$w_0 = [1 + (\eta_0/Z) \sin \psi_0]^2 p_0, \quad (3a)$$

$$p_0 = -\frac{ikR_0}{2} \left( \frac{Z}{\eta_0} \right)^2, \quad (3b)$$

and

$$\eta_0 = 120\pi.$$

This result is valid for  $kR_0 \gg 1$  and  $|Z/\eta_0|^2 \ll 1$ . If

$$Z = \left( \frac{i\mu_0\omega}{\sigma + i\epsilon\omega} \right)^{1/2} \left[ 1 - \frac{i\epsilon_0\omega}{\sigma + i\epsilon\omega} \cos^2 \psi_0 \right]^{1/2} \quad (4)$$

the expression for  $W$  coincides exactly with the result given by Norton [10] for the same situation. It may be noted that this value of  $Z$  is exactly equal to the ratio of the tangential electric and magnetic fields for a vertically polarized plane wave incident at an angle  $90^\circ - \psi_0$  on the homogeneous flat ground.

<sup>1</sup> This work was sponsored by the Electronics Research Directorate of the Air Force Cambridge Research Laboratories, Office of Aero-Space Research (USAF), Bedford, Mass., under contract PRO-61-568.

<sup>2</sup> Figures in brackets indicate the literature references on page 6.

In applications to practical communication problems it is very convenient to split off the surface wave portion  $W_s$  by writing

$$W = W_r + W_s \quad (5)$$

where, by definition,

$$W_r = [1 + R_v(\psi_0)]/2$$

is the radiation or space wave field, and

$$R_v = \frac{\sin \psi_0 - Z/\eta_0}{\sin \psi_0 + Z/\eta_0} \quad (6)$$

is the Fresnel reflection coefficient. This decomposition of the total field into space and surface wave was first made by Norton [10] and it is a convenient procedure in radio engineering since by definition,  $W_r$  is the radiation pattern of the antenna in the presence of the ground plane. It may be the dominant term in many cases of practical interest although as  $\psi_0$  approaches zero  $W_r$  actually vanishes. Methods for estimating the relative importance of  $W_s$  are given in the papers by Norton [10].

The central task in the present paper is to indicate how a wire mesh or a similar metal screen lying on the ground will modify the field at the receiving antenna. The surface impedance is assumed to be modified to  $Z'$  over the area of the screen, but remains the same outside the screen. The field  $E'_v$  in the presence of the screen is then written

$$E'_v = \frac{i\mu_0\omega I}{2\pi R_0} e^{-ikR_0} \cos^2 \psi_0 W'(R_0, Z, Z'), \quad (7)$$

where  $W'$  is an unknown complex quantity which is now a function of  $Z'$  in addition to  $R_0$  and  $Z$ . The quantity  $W'$  reduces to  $W$  if  $Z' = Z$ :

### 3. The Circular Screen

Over the range  $0 < \rho < a$  it is assumed that the surface impedance is  $Z' = Z'_a$ . Beyond the screen (i.e.,  $\rho > a$ ),  $Z' = Z$ . Furthermore, it is assumed that the receiving antenna is in the far field such that

$$R - R_0 \approx -\rho \cos \phi \cos \psi_0.$$

Thus

$$\begin{aligned} \Omega_a \approx & -\frac{ik}{2\pi \cos \psi_0} \int_{\rho=0}^a \int_{\phi=-\pi}^{\pi} e^{-ik\rho} \\ & \times \left(1 + \frac{1}{ik\rho}\right) e^{ik\rho \cos \phi \cos \psi_0} \cos \phi \left(\frac{Z'_a - Z}{\eta_0}\right) d\phi d\rho. \end{aligned} \quad (10)$$

If  $Z'_a$  does not depend on  $\phi$  the integration with respect to  $\phi$  may be readily carried out to give

In a previous paper [8] an integral equation for  $W'$  was obtained by an application of the Lorentz reciprocity theorem. Although it would be possible to solve this equation directly using a digital computer it was indicated that a first order iteration was satisfactory. In this case it was found that

$$W'(R, Z, Z') \approx W(R, Z) [1 + \Omega] \quad (8)$$

where  $\Omega$  is the fractional change of the field due to the presence of the screen. Within the approximations stated, the factor  $\Omega$  can be regarded as the modification of the effective height of the transmitting antenna, since it influences  $W_r$  and  $W_s$  to the same extent.

Before proceeding further it is convenient to introduce a polar coordinate system  $(\rho, \phi)$  centered at the source dipole as indicated in figure 1. Thus an element of area of the ground plane is  $\rho d\phi d\rho$ .

From the analysis in the previous paper by Wait [8], it was shown that

$$\begin{aligned} \Omega \approx & -\frac{ik}{2\pi \cos \psi_0} \iint_S e^{-ik\rho} e^{-ik(R-R_0)} \left(\frac{Z'-Z}{\eta_0}\right) \\ & \times \left(1 + \frac{1}{ik\rho}\right) (\cos \phi) d\phi d\rho. \end{aligned} \quad (9)$$

where

$$R = [\rho^2 + d^2 + h^2 - 2\rho d \cos \phi]^{1/2}$$

$$R_0 = (d^2 + h^2)^{1/2}, h = R_0 \sin \psi_0$$

and

$$d = R_0 \cos \psi_0.$$

The integral may be evaluated when the shape of the ground screen is specified. In the following, attention will be confined to screens which are in the form of a sector. A special case is a circular screen and this is considered first.

$$\begin{aligned} \Omega_a \approx & \frac{k}{\cos \psi_0} \int_{\rho=0}^a e^{ik\rho} \left(1 + \frac{1}{ik\rho}\right) J_1(k\rho \cos \psi_0) \\ & \times \left(\frac{Z'_a - Z}{\eta_0}\right) d\rho, \end{aligned} \quad (11)$$

where  $J_1$  is the Bessel function of the first type of order one. When dealing with large screens the argument  $k\rho \cos \psi_0$  can be regarded as a large quantity over the major portions of the integrand. Thus,  $J_1$  may be replaced by the first term of its asymptotic expansion. Therefore,

$$\begin{aligned} \Omega_a \approx & -\left(\frac{i}{2\pi \cos^3 \psi_0}\right)^{1/2} \int_0^{ka} \left(\frac{Z'_a - Z}{\eta_0}\right) \\ & \times (1 - ie^{-2ix \cos \psi_0}) \frac{e^{-ix(1-\cos \psi_0)}}{x^{1/2}} dx. \end{aligned} \quad (12)$$

When  $Z'_a$  is essentially constant over the range of integration,  $\Omega_a$  can be expressed in terms of Fresnel integrals. After a change of variable it readily follow that

$$\Omega_a \approx \frac{Z - Z'_a}{\eta_0} e^{-i\pi/4} G$$

where

$$G = \frac{i}{(2 \cos^3 \psi_0)^{1/2}} \left[ \frac{1}{\sin(\psi_0/2)} \int_0^{(4ka/\pi)^{1/2} \sin(\psi_0/2)} \exp[-i(\pi/2)t^2] dt - \frac{i}{\cos(\psi_0/2)} \int_0^{(4ka/\pi)^{1/2} \cos(\psi_0/2)} \exp[-i(\pi/2)t^2] dt \right]. \quad (13a)$$

As  $\psi_0$  approaches zero the above equation reduces to

$$G = i \left( \frac{2ka}{\pi} \right)^{1/2} \left[ 1 - i \left( \frac{\pi}{4ka} \right)^{1/2} \int_0^{(4ka/\pi)^{1/2}} \exp[-i(\pi/2)t^2] dt \right] \quad (13b)$$

and, if  $ka \gg 1$ , this may be approximated by

$$G \approx i \left( \frac{2ka}{\pi} \right)^{1/2} \left[ 1 - \left( \frac{i\pi}{8ka} \right)^{1/2} \right] \approx i \left( \frac{2ka}{\pi} \right)^{1/2}. \quad (14)$$

It is interesting to note that, if the integral in (12) is evaluated by a stationary phase method, the second Fresnel integral in the square bracket term of (13a) is not present. This would correspond to the approximation usually employed in the practical theories of mixed-path ground wave propagation. The value of  $G$  corresponding to this situation is denoted  $G(1)$ .

Numerical values of the integrals  $G$  and  $G(1)$  are given in table 1. The values of  $ka$  (denoted KA) take the values 5, 10, 20, 30, and 100, while  $\psi_0$  (denoted PSI) runs from  $0^\circ$  to  $45^\circ$ . It is immediately evident that, for small values of  $\psi_0$  (i.e., near grazing), the integrals  $G$  and  $G(1)$  are not significantly different. As will be clear from the following section the integral  $G(1)$  would correspond physically to the situation where the screen is semicircular in shape (i.e.,  $\phi$  extends from  $\pi/2$  to  $-\pi/2$  only).

To illustrate the application of the results in table 1, values of the complex quantity  $1 + \Omega_a$  have been computed for several values of the

surface impedances of the ground plane. For this purpose it is convenient to write

$$\frac{Z - Z'_a}{\eta_0} = \frac{1}{N} e^{i\beta} \quad (15)$$

where  $N$  and  $\beta$  are real. If the ground screen is a metal sheet  $Z'_a < Z$  and, consequently,  $Ne^{-i\beta}$  could be regarded as the complex refractive index of the ground itself. However, in general,  $N$  and  $\beta$  have a more general meaning as defined by (15). Taking  $N=3$  and  $\beta=0^\circ$ , the amplitude and phase of  $1 + \Omega_a$  are shown plotted in figures 2a and 2b, respectively, as a function of  $\psi_0$  for various values of  $ka$ . It is emphasized that such curves should not be regarded as radiation patterns but rather as modifications of the effective height of the transmitting antenna due to the ground screen. It is apparent that for the low angles involved in HF communication the ground screen will increase the effective height of the transmitting antenna by a significant amount. The value of  $N$  given in this example corresponds to a dielectric constant of 3<sup>2</sup> or 9 which is typical of very dry ground. The effect of choosing a large value of  $N$  is shown in figures 3a and 3b where  $N=10$  and  $\beta=0^\circ$ . The curves are very similar in shape but the overall effectiveness of the ground screen is reduced somewhat.

The value of  $\beta$ , as defined by (15), determines the phase of the complex refractive index of the ground. For a very dry or nonconducting ground  $\beta$  is zero as indicated in figures 2a to 3b. However, when the conductivity becomes important  $\beta$  may be greater than zero. In fact, for a highly conducting ground where displacement currents are negligible,  $\beta$  may approach  $45^\circ$ . To illustrate the influence of finite  $\beta$ , the amplitude and phase of  $1 + \Omega_a$  are shown in figures 4a and 4b for  $ka=20$ ,  $N=10$ , and various values of  $\beta$  between  $0^\circ$  and  $45^\circ$ . It is evident from these curves that the presence of the conduction currents tends to diminish the amplitude but it does increase the phase.

It is becoming apparent that at the lower frequencies and highly conducting ground the presence of the ground screen has a small effect on the total field (for a given strength  $Il$  of the source dipole). To illustrate this point, the amplitude and phase of  $1 + \Omega_a$  are shown in figures 5a and 5b for  $ka=20$  and  $\beta=45^\circ$  for  $N=10$  and 30. The modification of the effective height of the antenna is less than 2 db and here the radius of the screen is almost 3 wavelengths.

#### 4. The Sector Screen

It is clear from the previous results that a large circular ground screen will, indeed, improve the low angle radiation from a ground-based vertical antenna. However, one might ask if any portions of the circular ground screen could be removed without materially affecting the performance of the system. This is certainly a valid question.

In the first place it is known [5] that the impedance of the antenna is not affected by anything beyond about one-half wavelength from the antenna. Therefore, to throw some light on the question posed above, the ground screen is taken to be in the form of a sector extending from  $\rho=a$  to  $\rho=b$  from the base of the transmitting antenna. From

$\rho=0$  out to  $\rho=a$  the screen is circular in shape. The situation is illustrated in figure 6. The surface impedance over the area of the sector is  $Z_b$ . In terms of the polar coordinate system  $(\rho, \phi)$ , the area of the sector is defined by  $-\Delta_1 < \phi < \Delta_2$  and  $a < \rho < b$ .

It is convenient to express the factor  $\Omega$  as the sum of two parts in the manner

$$\Omega = \Omega_a + \Omega_b \quad (16)$$

where  $\Omega_a$  is the contribution from the circular screen of radius  $a$  and  $\Omega_b$  is the contribution from the sector which extends from  $a$  to  $b$ . The portion  $\Omega_b$  can be written

$$\Omega_b = -\frac{ik}{2\pi \cos \psi_0} \int_{\rho=a}^b \int_{\phi=-\Delta_1}^{\Delta_2} e^{-ik\rho} \,$$

$$\left(1 + \frac{1}{ik\rho}\right) e^{ik\rho \cos \phi \cos \psi_0} \times \cos \phi \left(\frac{Z'_b - Z}{\eta_0}\right) d\phi d\rho \quad (17)$$

where the receiving antenna is assumed to be in the plane  $\phi=0$ . The integral for  $\Omega_b$  given above is sufficiently general to determine the effect of the sector as a function of elevation and azimuth angle. Actually, the integral is analogous to (10) for the circular screen where the limits of  $\phi$  extend from  $-\pi$  to  $\pi$ . As before, only first-order phase terms are retained so that the receiving antenna must be in the far field.<sup>3</sup> The extension to the near-field case has been considered previously by Wait [8]. In actual communication circuits the receiving antenna would always be in the far field.

To evaluate the integral in (17) it is convenient to use the approximation

$$\cos \phi = 1 - \frac{\phi^2}{2}$$

for the exponent in the integrand while, in the integrand,  $\cos \phi$  is replaced by unity. This is valid since the principal contributions correspond to small values of  $\phi$ . An interesting check on this statement is given below.

Following the procedure used in the previous section, a dimensionless function  $G_b$  is introduced by setting

$$\Omega_b = \frac{Z - Z'_b}{\eta_0} e^{-i\pi/4} G_b. \quad (18)$$

The integral for  $G_b$  may now be written in the form

$$G_b = \frac{i}{(2\pi)^{1/2} \cos^{3/2} \psi_0} \int_{ka}^{kb} \frac{e^{-ix(1-\cos \psi_0)}}{x^{1/2}} F(x) dx \quad (19)$$

where

$$F(x) = \frac{1}{1-i} \int_{-\Delta_1[(x/\pi) \cos \psi_0]^{1/2}}^{\Delta_2[(x/\pi) \cos \psi_0]^{1/2}} \exp \left[ -i \frac{\pi}{2} t^2 \right] dt.$$

<sup>3</sup> This far-field condition can be written

$$kR_0 \left[ \left(1 + \frac{\rho^2}{R_0^2} - \frac{2\rho d}{R_0^2} \cos \phi\right)^{1/2} - 1 \right] - \frac{k\rho d}{R_0} \cos \phi < \frac{\pi}{4}.$$

The Fresnel integral  $F(x)$  is normalized so that  $\lim_{x \rightarrow \infty} F(x) = 1$ , provided  $\Delta_1$  and  $\Delta_2$  are both positive. In this limiting case the sector is behaving essentially as a circular screen. For example, one may note that

$$G_b \Big|_{x=\infty} = G_1(kb) - G_1(ka)$$

where  $G_1$  is the integral described by omitting the second term of (13a).

An interesting special case of (19) is when  $\psi_0 \rightarrow 0$  and  $Z'_b$  can be regarded as a constant. Then

$$G_b = i \left( \frac{1}{2\pi} \right)^{1/2} \int_{ka}^{kb} \frac{F(x)}{x^{1/2}} dx. \quad (20)$$

After an integration by parts it readily follows that

$$\begin{aligned} G_b = & i \left( \frac{2kb}{\pi} \right)^{1/2} \left\{ F(kb) \right. \\ & - \left( \frac{2}{\pi kb} \right)^{1/2} e^{i3\pi/4} \left[ \frac{\exp(-ikb\Delta_2^2/2)}{2\Delta_2} + \frac{\exp(-ikb\Delta_1^2/2)}{2\Delta_1} \right] \\ & - \left( \frac{a}{b} \right)^{1/2} \left[ F(ka) - \left( \frac{2}{\pi ka} \right)^{1/2} e^{i3\pi/4} \left( \frac{\exp(-ika\Delta_2^2/2)}{2\Delta_2} \right. \right. \\ & \left. \left. + \frac{\exp(-ika\Delta_1^2/2)}{2\Delta_1} \right) \right] \right\}. \end{aligned} \quad (21)$$

The integral  $G_b$  has been evaluated for a range of values of  $kb$ . To simplify the situation, the lower limit  $ka$  is fixed at 5 and  $\Delta_1 = \Delta_2 = \Delta$ . The numerical results for  $G_b$  [denoted  $G(B)$ ] are given in tables 2 to 8 for  $\Delta$  [DELTA] ranging from  $5^\circ$  to  $60^\circ$ . Within each table  $kb$  [KB] varies from 10 to 100 and  $\psi_0$  [PSI] varies from  $0^\circ$  to  $45^\circ$ .

As a check on the numerical work,  $G_b$  for  $\psi_0 = 0$  was calculated using both (19) and (21). Also, it may be noted that

$$G_b(kb) \Big|_{\Delta \rightarrow \infty} = G_1(kb) - G_1(5)$$

where the values of  $G_1(x)$  are listed in table 1 and where  $x$  is to be identified with KA.

To illustrate the effect of a finite value of  $\Delta$ , some typical cases are shown in figures 7a and 7b where the amplitude and phase of  $G_b$  are plotted as a function of  $\psi_0$  for  $ka=5$ ,  $kb=40$ , and various values of  $\Delta$ . It appears that for these conditions the total sector angle  $2\Delta$  need not be greater than about  $50^\circ$  in order to be fully effective.

In order to demonstrate the effect of the sector on the total field it is convenient to consider both  $Z'_a$  and  $Z'_b$  small compared with  $Z$ . Thus

$$\frac{Z - Z'_b}{\eta_0} \approx \frac{Z - Z'_a}{\eta_0} \approx \frac{Z}{\eta_0} \approx \frac{1}{N} e^{i\beta}$$

where  $N e^{-i\beta}$  is the complex refractive index of the

ground. Consequently, it follows from (16), that

$$1 + \Omega = 1 + \Omega_a + \Omega_b \approx 1 + \frac{e^{i(\beta - \pi/4)}}{N} (G_a + G_b).$$

The amplitude of this quantity (expressed in db) and the phase are shown in figures 8a and 8b for  $ka=5$ ,  $kb=40$ ,  $\beta=0$ , and  $N=3$ . This would correspond to a relatively dry soil. It is certainly evident here that considerable improvement results from the presence of the sector. The corresponding set of curves shown in figures 9a and 9b are for a highly conducting soil characterized by  $N=10$  and  $\beta=45^\circ$ . The sector screen here has a negligible effect on the performance of the system. In fact, there is even a slight degradation for the very low grazing angles.

The marked improvement by using a large sector screen on a dry ground is indicated in figure 10. Here  $ka=5$ ,  $kb=200$ ,  $N=3$ , and  $\beta=0$ . At low angles the gain is greater than 12 db even with a total sector angle,  $2\Delta$ , of  $20^\circ$ .

In the preceding discussion it has been tacitly assumed that the receiving antenna is located in the vertical plane which bisects the sector. Normally, this would be the optimum location and for a fixed communication link it would be considered good practice to orient the sector toward the receiving antenna. However, there may be certain applications where the receiving antenna is located off the center line. The formulas given above are actually valid for this case since  $\Delta_1$  and  $\Delta_2$  may take any positive or negative value. However, rather than computing directly from the general formulas, it is desirable to establish some simple identities which enable the results in tables 2 to 8 to be used.

It may be readily verified that  $G_b(\Delta_1, \Delta_2)$ , as defined by (18), has the following property

$$G_b(\Delta_1, \Delta_2) = \frac{G_b(\Delta_1, \Delta_1) + G_b(\Delta_2, \Delta_2)}{2} = \frac{G_b(\Delta_1) + G_b(\Delta_2)}{2}.$$

Numerical values of  $G_b(\Delta, \Delta)$  or  $G_b(\Delta)$  for various positive values of  $\Delta$  are given in tables 2 to 8 inclusive. If negative values of  $\Delta$  are encountered it is useful to note that

$$G_b(\Delta) = -G_b(-\Delta).$$

With this information it is a simple matter to compute  $(1 + \Omega)$  as a function of the azimuth angle  $\delta$  which is defined by

$$\delta = (\Delta_2 - \Delta_1)/2.$$

Thus

$$1 + \Omega_a + \Omega_b \approx 1 + \frac{Z - Z'_a}{\eta_0} G_a e^{-i\pi/4} + \frac{Z - Z'_b}{\eta_0} e^{-i\pi/4} G(\Delta_1, \Delta_2) \quad (22)$$

which is an obvious generalization of (18).

To illustrate the azimuthal variation of the field when using a sector it is again desirable to write

$$\frac{Z - Z'_a}{\eta_0} \approx \frac{Z - Z'_b}{\eta_0} \approx \frac{Z}{\eta_0} \approx \frac{1}{N} e^{i\alpha}.$$

Then again denoting the total width of the sector by  $2\Delta$ , the amplitudes of  $1 + \Omega_a + \Omega_b$  are shown in figures 11 and 12 for  $N=3$ ,  $\beta=0$ ,  $ka=5$ ,  $\Delta=20^\circ$ , and various values of  $\psi_0$  from  $0^\circ$  to  $25^\circ$ . In figure 11,  $kb=40$  whereas in figure 12,  $kb=200$ . As expected, the maximum response corresponds to small values of  $\delta$ . In fact, as  $\delta$  increases the response decreases quite significantly for the larger sector.

## 5. Final Remarks

In the present study, the electrical properties of the ground are assumed to be characterized by a surface impedance which is a (complex) constant  $Z$  outside a surface  $S$ . Within  $S$ , the impedance  $Z'$  is allowed to be variable. In the case of a radial wire system emanating from  $Q$ , it is appropriate to use formulas which have been developed for the surface of a wire grid in the interface of a conducting half space [11]. In general these are complicated, but recently some numerical results have been obtained which should be useful in this problem.<sup>4</sup> At low radiofrequencies for moderately or well-conducting soils it is a satisfactory approximation to regard the surface  $Z'$  as the parallel combination of the

surface impedance  $Z_s$  of the equivalent grid and the ground beneath. Thus

$$Z' \approx \frac{Z_s Z}{Z + Z_s} \quad (23)$$

where

$$Z_s \approx \frac{i\eta_0 d}{\lambda_0} \log_e \frac{d}{2\pi c}, \quad (24)$$

$$Z \approx (i\mu_0 \omega / \sigma)^{1/2},$$

and  $d$  is the spacing between the radial conductors and  $c$  is the radius of the wires. Such a formula is strictly valid only if  $(\sigma\mu_0\omega)^{1/2}d \ll 1$  everywhere within the ground system. If there are  $N$  radial conductors, it can be seen that  $d$  can be replaced by  $2\pi\rho/N$  where  $N$  is usually of the order of 100.

<sup>4</sup> Available from Mrs. T. Larsen, Laboratory of Electromagnetic Theory, Technical University of Denmark, Copenhagen.

## 6. Appendix

### 6.1. Evaluation of the Fresnel Integral

The integrals occurring in  $G$  (13a), (13b), and  $F(x)$ , (19) are of the type

$$\int_0^u e^{-(i/2)\pi t^2} dt = C(u) - iS(u). \quad (25)$$

These Fresnel integrals were evaluated by the method proposed by Boersma [12]. This method is based on the  $\tau$  method of Lanczos [13]. The Fresnel integral defined by Boersma is

$$f(x) = \int_0^x \frac{e^{-it}}{\sqrt{2\pi t}} dt. \quad (26)$$

The definition in (25) conforms to the one used by Boersma [14] in eq (26) if

$$x = \frac{\pi u^2}{2}.$$

For values of the argument  $0 \leq x \leq 4$  in (26),  $f(x)$  is computed by a finite power series in  $x$ ; for values of the argument  $x \geq 4$ ,  $f(x)$  is approximated by a polynomial in  $1/x$ . For  $n=12$ , the power series in  $x$  valid for  $0 \leq x \leq 4$  is

$$f(x) \cong e^{-ix} \sqrt{\frac{x}{4}} \sum_0^{11} (a_n + ib_n) \left(\frac{x}{4}\right)^n. \quad (27)$$

The power series in  $\frac{1}{x}$ , valid for  $x \geq 4$  is

$$f(x) \cong \frac{1-i}{2} + e^{-ix} \sqrt{\frac{4}{x}} \sum_0^{11} (c_n + id_n) \left(\frac{4}{x}\right)^n. \quad (28)$$

The numerical values of the coefficients  $a_n$ ,  $b_n$ ,  $c_n$ , and  $d_n$  as developed by Boersma [14, 12] are given in table 9. With these coefficients the Fresnel integrals can be computed over the range  $0 \leq x \leq \infty$ , in general, to eight decimal points. The subroutine used in evaluating the Fresnel integral was checked with the tables of Pearcy [15] and those of Wijngaarden and Scheen [16]. The former tables, using definition (26), are accurate to six or seven digits depending on the size of the argument while the latter, using definition (25), are accurate to five digits.

### 7. References

- [1] G. H. Brown, R. F. Lewis, and J. Epstein, Ground systems as a factor in antenna efficiency, Proc. IRE **25**, 753-787 (June 1937).
- [2] F. R. Abbott, Design of optimum buried R. F. ground systems, Proc. IRE **40**, 846-852 (July 1952).
- [3] J. R. Wait and W. A. Pope, Input resistance of LF unipole aerials, Wireless Engineer **32**, 131-138 (May 1955). (In eq (9),  $1/\rho$  should be  $1/\rho^2$ .)
- [4] J. R. Wait and W. A. Pope, The characteristics of a vertical antenna with a radial conductor ground system, Appl. Sci. Research [B] **4**, 177-195 (1954).
- [5] J. R. Wait, Effect of the ground screen on the field radiated from a monopole, IRE Trans. on Antennas and Propagation **AP-4**, 179-181 (April 1956).
- [6] H. Page and G. D. Monteath, The vertical radiation patterns of medium wave broadcasting aerials, Proc. IEE **102**, 279-297 (May 1955).
- [7] G. D. Monteath, The effect of the ground constants, and of the earth system, on the performance of a vertical medium wave aerial, Monograph No. 279R, Inst. Elect. Engrs. (London), pp. 1-15 (Jan. 1958). (This paper contains a valuable and critical survey of previous work.)

### 6.2. Evaluation of $G_b$ by Gaussian Quadrature

With a procedure for evaluating the Fresnel integral, the remaining problem was to compute the integral in (19). The method used, Gaussian quadrature, is described briefly below [17].

In quadrature methods a definite integral is approximated by a weighted sum of particular values of the ordinate with the abscissas properly distributed in the limits of integration. Thus,

$$\int_a^b f(x) dx = \sum_{j=1}^n H_j f(a_j) + E_n. \quad (29)$$

The abscissas  $a_j$  are roots of the Legendre polynomials, the weights  $H_j$  are functions of these roots, and  $E_n$  is the error term which can, in general, be made arbitrarily small with increasing  $n$ . The Gaussian roots and weights are tabulated for various  $n$  for limits between  $-1$  and  $1$  by Davis and Rabinowitz [18], but other limits can be used by a change of variable as follows:

$$\int_a^b f(x) dx = \frac{b-a}{2} \int_{-1}^1 g(y) dy,$$

where

$$x = \frac{b-a}{2} y + \frac{b+a}{2}. \quad (30)$$

Furthermore, in the Gaussian quadrature procedure, the integrand is approximated by a polynomial of  $(2n-1)$  degree which has the same ordinates as the function for  $n$  discrete abscissas.

To obtain accuracy for  $G_b$  eq (19) was written

$$G_b = \frac{i}{\sqrt{2\pi} \cos^{3/2} \psi_0} \left[ \int_5^{10} \frac{e^{-ix(1-\cos \psi_0)} F(x)}{\sqrt{x}} dx + \int_{10}^{15} \frac{e^{-ix(1-\cos \psi_0)} F(x)}{\sqrt{x}} dx \dots + \int_{kb-5}^{kb} \frac{e^{-ix(1-\cos \psi_0)} F(x)}{\sqrt{x}} dx \right] \quad (31)$$

and Gaussian quadrature was used with  $n=16$  in eq (29) for each interval of 5 for  $kb$ . This work was checked against (21) for  $\psi_0=0$  and various values of  $\Delta_1$  and  $\Delta_2$ . The answers agreed to the five digits asked for in the results.

- [8] J. R. Wait, The theory of an antenna over an inhomogeneous ground plane, Proc. Symposium on Electromagnetic Theory and Antennas, Copenhagen, June 1962. (To be published by Pergamon Press.)
- [9] J. R. Wait, Excitation of surface waves on conducting, stratified, dielectric-clad, and corrugated surfaces, J. Research NBS **59**, 365-377 (Dec. 1957) (In eq. (71) ( $p/w$ ) should be  $(p/w)^{\frac{1}{2}}$ ; on page 376,  $r_2$  is defined by  $r_2 = r_1 + 2hC$ .)
- [10] K. A. Norton, The propagation of radio waves over the surface of the earth and in the upper atmosphere, Part I, Proc. IRE **24**, 1367-1387 (Oct. 1936); Part II, Proc. IRE **25**, 1203-1236 (Sept. 1937).
- [11] J. R. Wait, On the theory of reflection from a wire grid parallel to an interface between homogeneous media, Part II, Appl. Sci. Research [B] **7**, 355-360 (1959).
- [12] J. Boersma, Computation of Fresnel integrals, Math. of Computation **14**, Nos. 69-72, 380 (1960).
- [13] C. Lanczos, Applied analysis (Prentice Hall, Englewood Cliffs, N.J., 1956).
- [14] J. Boersma, On a numerical method for computation of Fresnel integrals, Math. Inst., Univ. of Groningen, Report TW2 (1960). (The derivation for  $f(x)$  and constants  $a_n, b_n, c_n$ , and  $d_n$  are given in this reference.)
- [15] T. Pearcey, Table of the Fresnel integral (Cambridge Univ. Press, 1956).
- [16] Adrian van Wijngaarden and W. L. Scheen, Table of Fresnel integrals, Amsterdam, Nord-Hollandsche Uitg. Mij (1949).
- [17] F. Kopal, Numerical analysis (John Wiley & Sons, Inc., New York, N.Y., 1955).
- [18] P. Davis and P. Rabinowitz, Abscissas and weights for Gaussian quadratures of high order, J. Research NBS **56**, 35-37 (Jan. 1956).

## 7.1 Additional References

- T. Larsen, Numerical investigation of the equivalent impedance of a wire grid parallel to the interface between two media, J. Research NBS **66D** (Radio Prop.) No. 1, pp. 7-14 (Jan.-Feb. 1962).
- S. W. Maley and R. J. King, The impedance of a monopole antenna with a circular conducting-disk ground system on the surface of a lossy half space, J. Research NBS **65D** (Radio Prop.) No. 2, pp. 183-188 (Mar.-Apr. 1961).
- A. N. Smith and T. E. Devaney, Fields in electrically short ground systems: An experimental study, J. Research NBS **63D** (Radio Prop.) No. 2, pp. 175-180 (Sept.-Oct. 1959).
- J. R. Wait, Electromagnetic radiation from cylindrical structures (Pergamon Press, London and New York, 1959). (Includes a discussion of slot radiators on wedges and half-planes.)

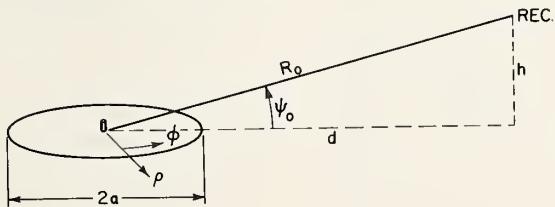


FIGURE 1. Vertical electric dipole located over a circular metal screen which, itself, is lying on a homogeneous ground.

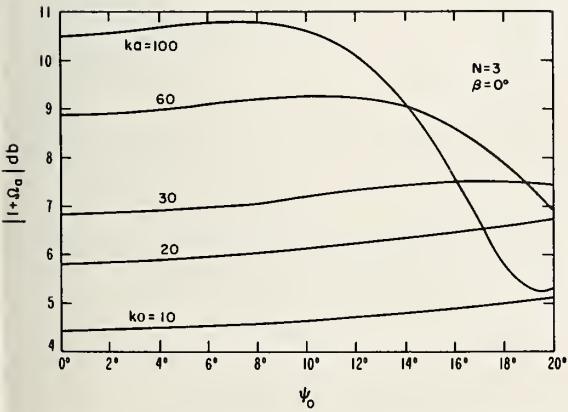


FIGURE 2a. The amplitude of  $1+\Omega_a$  as a function of  $\psi_0$  with parameter  $ka$  for nonconducting ground illustrating the effect of the circular screen of radius  $a$ .

The ordinate can be regarded as the modification of the effective height of the monopole resulting from the presence of the ground screen.]

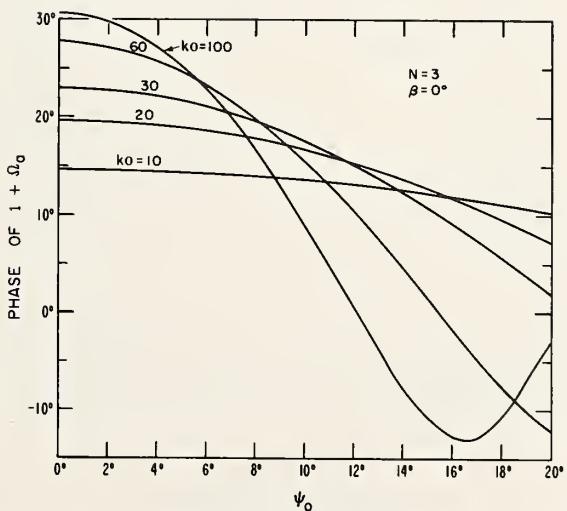


FIGURE 2b. The phase of  $1+\Omega_a$  as a function of  $\psi_0$  with parameter  $ka$  for nonconducting ground.

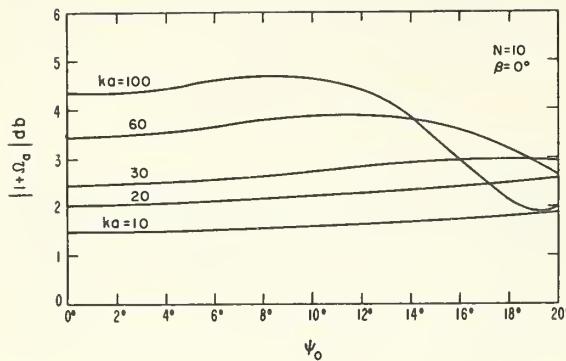


FIGURE 3a. The amplitude of  $1 + \Omega_a$  as a function of  $\psi_0$  with parameter  $ka$  and nonconducting ground illustrating the effect of large  $N$ .

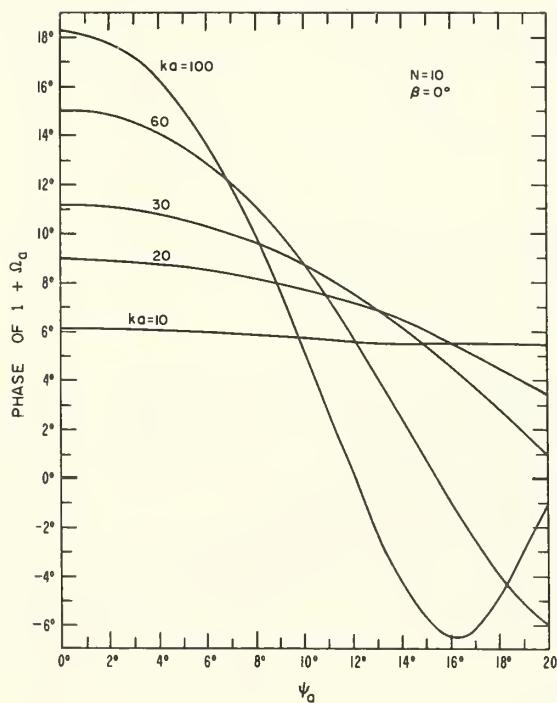


FIGURE 3b. The phase of  $1 + \Omega_a$  as a function of  $\psi_0$  with parameter  $ka$  and nonconducting ground illustrating the effect of large  $N$ .

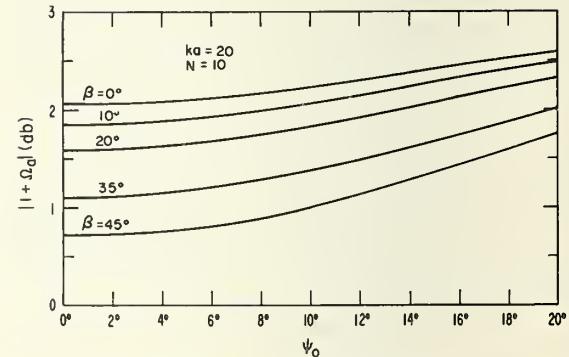


FIGURE 4a. The amplitude of  $1 + \Omega_a$  as a function of  $\psi_0$  illustrating the effect of finite  $\beta$ .

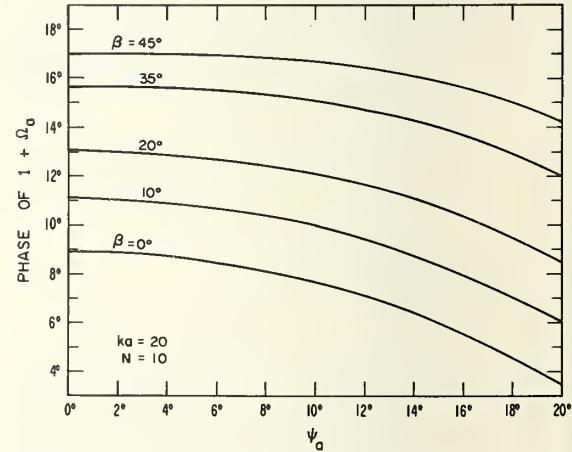


FIGURE 4b. The phase of  $1 + \Omega_a$  as a function of  $\psi_0$  illustrating the effect of finite  $\beta$ .

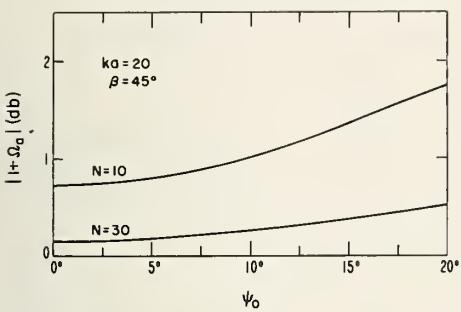


FIGURE 5a. The amplitude of  $1 + \Omega_a$  as a function of  $\psi_0$  for highly conducting ground illustrating the effect of large  $N$ .

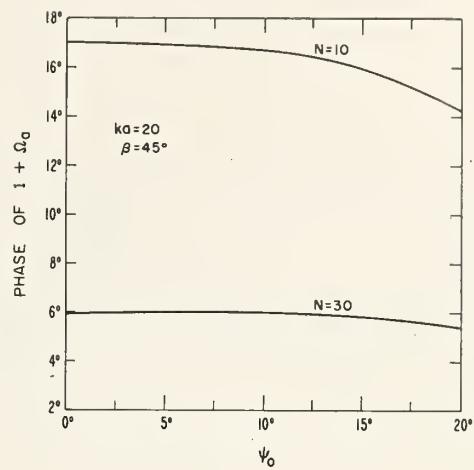


FIGURE 5b. The phase of  $1 + \Omega_a$  as a function of  $\psi_0$  for highly conducting ground illustrating the effect of large  $N$ .

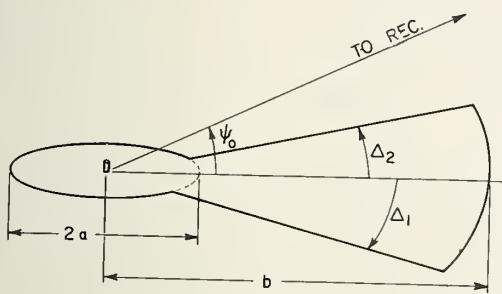


FIGURE 6. Vertical electric dipole located over a combination circular-sector screen which, itself, is lying on a homogeneous ground.

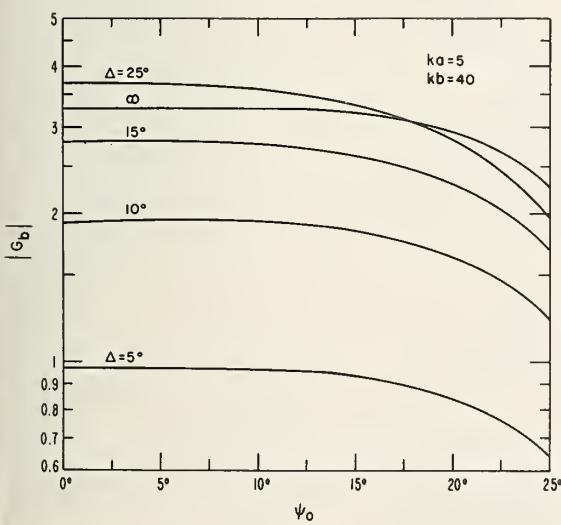


FIGURE 7a. The amplitude of  $G_b$  as a function of  $\psi_0$  illustrating the effect of finite  $\Delta$ . (These curves are for a circular screen of radius  $a$  and a sector which extends from  $a$  to  $b$ ).

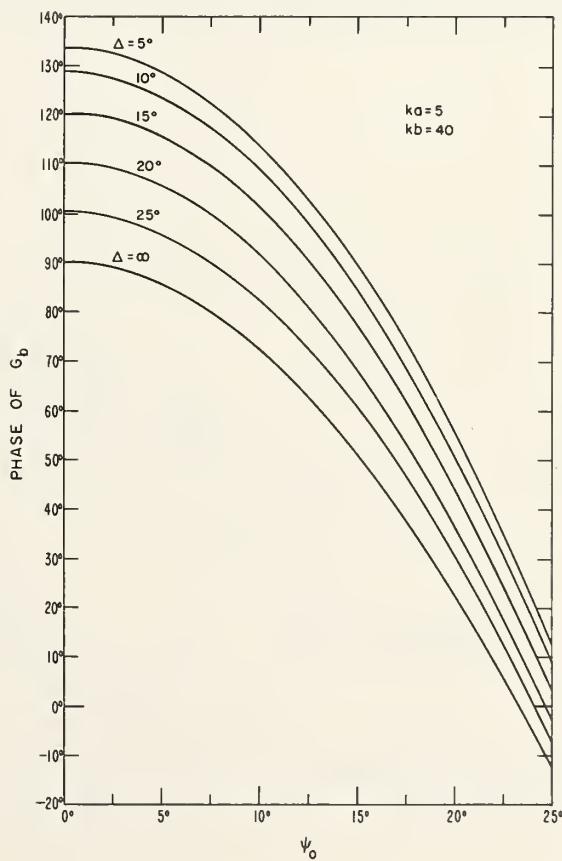


FIGURE 7b. The phase of  $G_b$  as a function of  $\psi_0$  illustrating the effect of finite  $\Delta$ .

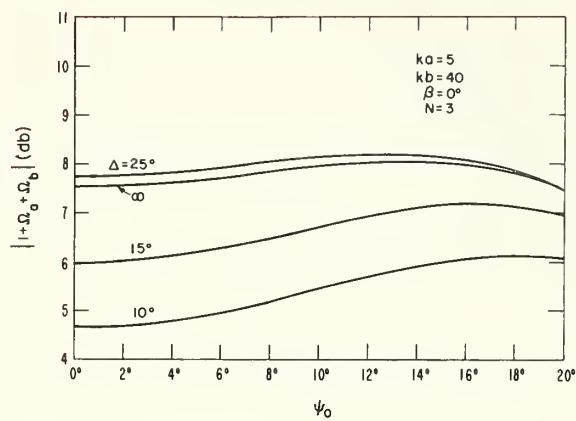


FIGURE 8a. The amplitude of  $1 + \Omega_a + \Omega_b$  as a function of  $\psi_0$  illustrating the effect of finite  $\Delta$  for nonconducting ground.

[The ordinate can be regarded as the modification of the effective height of the monopole resulting from the presence of the ground screen which is in the combined form of a circular disk and a sector.]

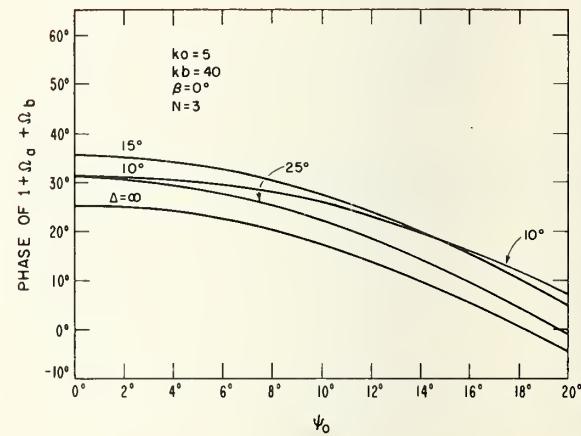


FIGURE 8b. The phase of  $1 + \Omega_a + \Omega_b$  as a function of  $\psi_0$  illustrating the effect of finite  $\Delta$  for nonconducting ground.

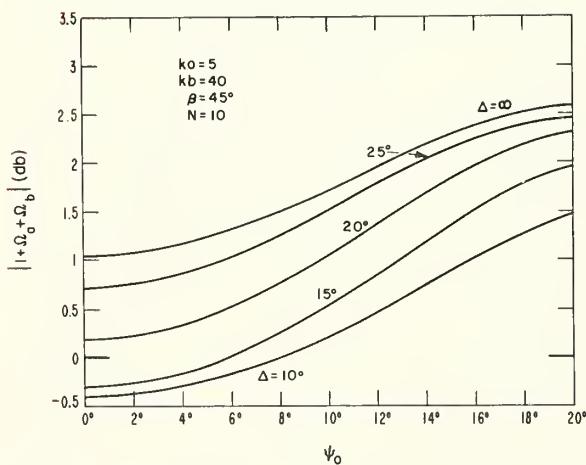


FIGURE 9a. The amplitude of  $1 + \Omega_a + \Omega_b$  as a function of  $\psi_0$  for highly conducting ground and large  $N$  illustrating the effect of finite  $\Delta$ .

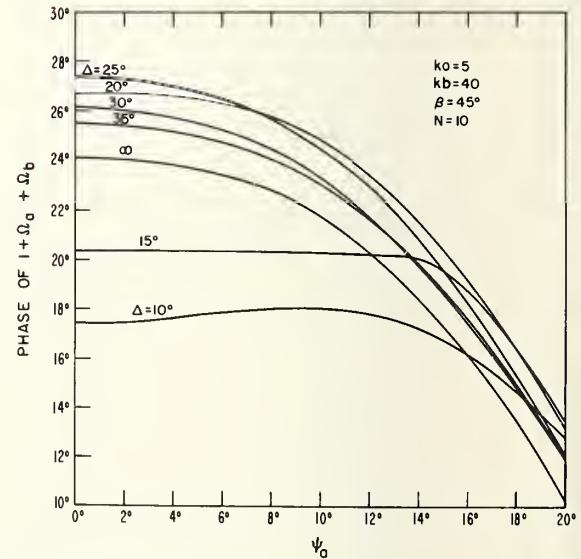


FIGURE 9b. The phase of  $1 + \Omega_a + \Omega_b$  as a function of  $\psi_0$  for highly conducting ground and large  $N$  illustrating the effect of finite  $\Delta$ .

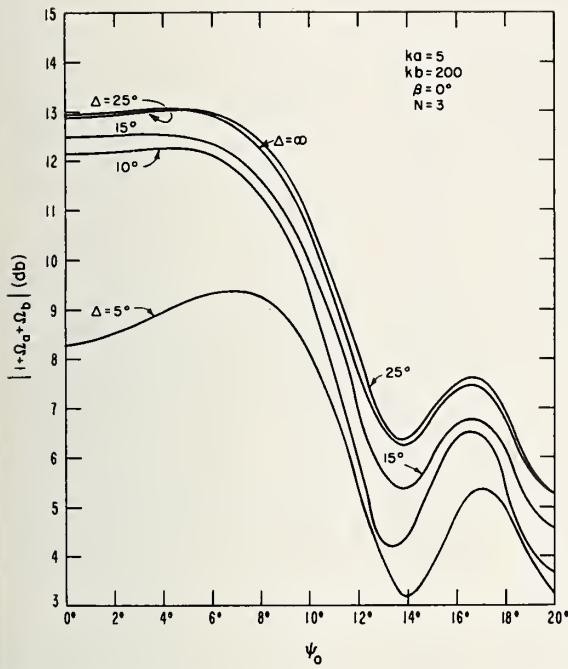


FIGURE 10. The amplitude of  $1 + \Omega_a + \Omega_b$  as a function of  $\psi_0$  illustrating the effect of finite  $\Delta$  for nonconducting ground.

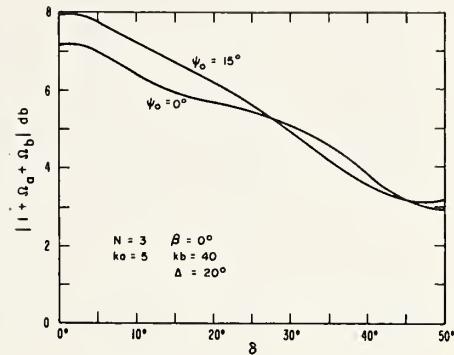


FIGURE 11. The amplitude of  $1 + \Omega_a + \Omega_b$  as a function of the azimuthal angle  $\delta$  for nonconducting ground illustrating the effect of finite  $\psi_0$  for  $k_b = 40$ .

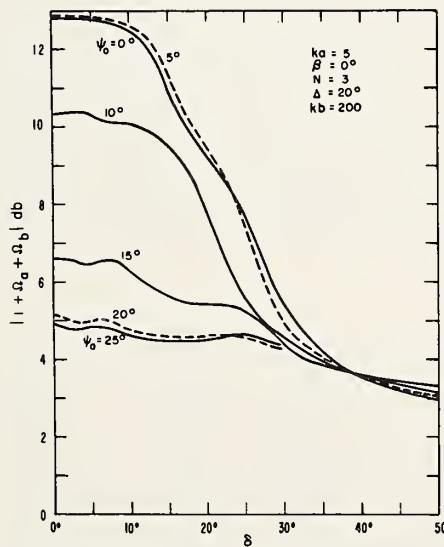


FIGURE 12. The amplitude of  $1 + \Omega_a + \Omega_b$  as a function of the azimuthal angle  $\delta$  for nonconducting ground illustrating the effect of finite  $\psi_0$  for  $k_b = 200$ .

Table 1

KA= 5					KA= 20				
PS1(OEGREES)	G	PHASE(OEGREES)	G(1)	PHASE(1)(OEGREES)	PS1(OEGREES)	G	PHASE(OEGREES)	G(1)	PHASE(1)(DEGREES)
0	1.3887 +00	7.7144 +01	1.7841 +00	9.0000 +01	0	3.2088 +00	8.3070 +01	3.5682 +00	9.0000 +01
1	1.3891 +00	7.7123 +01	1.7845 +00	8.9985 +01	1	3.2101 +00	8.3004 +01	3.5691 +00	8.9942 +01
2	1.3902 +00	7.7058 +01	1.7858 +00	8.9942 +01	2	3.2139 +00	8.2807 +01	3.5715 +00	8.9767 +01
3	1.3921 +00	7.6951 +01	1.7878 +00	8.9869 +01	3	3.2202 +00	8.2478 +01	3.5755 +00	8.9477 +01
4	1.3948 +00	7.6801 +01	1.7907 +00	8.9767 +01	4	3.2289 +00	8.2018 +01	3.5809 +00	8.9070 +01
5	1.3983 +00	7.6608 +01	1.7943 +00	8.9637 +01	5	3.2400 +00	8.1428 +01	3.5878 +00	8.8547 +01
7	1.4076 +00	7.6092 +01	1.8041 +00	8.9288 +01	7	3.2690 +00	7.9862 +01	3.6050 +00	8.7153 +01
10	1.4277 +00	7.4998 +01	1.8251 +00	8.8549 +01	10	3.3269 +00	7.6572 +01	3.6362 +00	8.4202 +01
15	1.4790 +00	7.2324 +01	1.8769 +00	8.6747 +01	15	3.4450 +00	6.8737 +01	3.6817 +00	7.7036 +01
20	1.5561 +00	6.8612 +01	1.9507 +00	8.4246 +01	20	3.5403 +00	5.8358 +01	3.6697 +00	6.7258 +01
25	1.6649 +00	6.3934 +01	2.0477 +00	8.1070 +01	25	3.5192 +00	4.5993 +01	3.5258 +00	5.5374 +01
30	1.8143 +00	5.8423 +01	2.1699 +00	7.7256 +01	30	3.2728 +00	3.2262 +01	3.1724 +00	4.2577 +01
35	2.0161 +00	5.2294 +01	2.3201 +00	7.2852 +01	35	2.7678 +00	1.8491 +01	2.5782 +00	3.1891 +01
40	2.2849 +00	4.5830 +01	2.5027 +00	6.7927 +01	40	2.1566 +00	9.9872 +00	1.8936 +00	3.1532 +01
45	2.6379 +00	3.9340 +01	2.7242 +00	6.2566 +01	45	1.8859 +00	1.8111 +01	1.7183 +00	4.9660 +01
KA= 10					KA= 30				
PS1(OEGREES)	G	PHASE(OEGREES)	G(1)	PHASE(1)(DEGREES)	PS1(OEGREES)	G	PHASE(OEGREES)	G(1)	PHASE(1)(DEGREES)
0	2.2347 +00	7.9418 +01	2.5231 +00	9.0000 +01	0	3.9966 +00	8.5080 +01	4.3702 +00	9.0000 +01
1	2.2355 +00	7.9386 +01	2.5237 +00	8.9971 +01	1	3.9980 +00	8.4983 +01	4.3712 +00	8.9913 +01
2	2.2380 +00	7.9292 +01	2.5254 +00	8.9884 +01	2	4.0023 +00	8.4690 +01	4.3741 +00	8.9651 +01
3	2.2420 +00	7.9136 +01	2.5283 +00	8.9738 +01	3	4.0093 +00	8.4202 +01	4.3789 +00	8.9215 +01
4	2.2477 +00	7.8917 +01	2.5323 +00	8.9535 +01	4	4.0188 +00	8.3519 +01	4.3852 +00	8.8604 +01
5	2.2550 +00	7.8637 +01	2.5374 +00	8.9273 +01	5	4.0308 +00	8.2642 +01	4.3927 +00	8.7820 +01
7	2.2743 +00	7.7892 +01	2.5510 +00	8.8576 +01	7	4.0604 +00	8.0308 +01	4.4097 +00	8.5731 +01
10	2.3148 +00	7.6322 +01	2.5791 +00	8.7099 +01	10	4.1127 +00	7.5377 +01	4.4306 +00	8.1311 +01
15	2.4102 +00	7.2551 +01	2.6441 +00	8.3499 +01	15	4.1757 +00	6.3599 +01	4.3932 +00	7.0654 +01
20	2.5325 +00	6.7426 +01	2.7254 +00	7.8518 +01	20	4.0867 +00	4.8299 +01	4.1355 +00	5.6486 +01
25	2.6670 +00	6.1034 +01	2.8118 +00	7.2242 +01	25	3.6387 +00	3.1535 +01	3.5046 +00	4.0737 +01
30	2.7920 +00	5.3391 +01	2.8880 +00	6.4819 +01	30	2.7230 +00	1.7663 +01	2.4964 +00	2.9776 +01
35	2.8846 +00	4.4417 +01	2.9340 +00	5.6499 +01	35	1.8352 +00	2.0147 +01	1.7175 +00	4.2202 +01
40	2.9320 +00	3.4006 +01	2.9260 +00	4.7700 +01	40	2.1422 +00	3.4366 +01	2.1749 +00	5.7104 +01
45	2.9472 +00	2.2358 +01	2.8406 +00	3.9159 +01	45	2.8481 +00	2.5315 +01	2.6110 +00	4.4159 +01
KA=100									
PS1(OEGREES)	G	PHASE(OEGREES)	G(1)	PHASE(1)(DEGREES)					
0	7.6424 +00	8.7479 +01	7.9788 +00	9.0000 +01					
1	7.6455 +00	8.7177 +01	7.9806 +00	8.9709 +01					
2	7.6541 +00	8.6269 +01	7.9848 +00	8.8837 +01					
3	7.6652 +00	8.4757 +01	7.9886 +00	8.7383 +01					
4	7.6741 +00	8.2639 +01	7.9870 +00	8.5350 +01					
5	7.6743 +00	7.9919 +01	7.9731 +00	8.2741 +01					
7	7.6137 +00	7.2692 +01	7.8714 +00	7.5832 +01					
10	7.2068 +00	5.7679 +01	7.3572 +00	6.1585 +01					
15	4.9918 +00	2.7524 +01	4.8443 +00	3.3696 +01					
20	2.5271 +00	4.0004 +01	2.5377 +00	5.2124 +01					
25	3.2011 +00	2.8208 +01	3.0747 +00	3.9259 +01					
30	2.3910 +00	3.8703 +01	2.4284 +00	5.3722 +01					
35	2.0752 +00	2.5785 +01	1.9458 +00	4.4941 +01					
40	2.2996 +00	1.9230 +01	2.0482 +00	3.9115 +01					
45	2.4683 +00	1.7372 +01	2.1607 +00	3.9056 +01					

Table 2  
KA=5  
DELTA(DEGREES)= 5

K8	PSI(DEGREES) = 0	PSI(DEGREES) = 0.5	PSI(DEGREES) = 1	PSI(DEGREES) = 2
	G(8)	PHASE(DEGREES)	G(8)	PHASE(DEGREES)
10	1.3888 -01	1.3445 +02	1.3889 -01	1.3444 +02
15	2.7776 -01	1.3427 +02	2.7777 -01	1.3425 +02
20	4.1661 -01	1.3409 +02	4.1663 -01	1.3406 +02
25	5.5545 -01	1.3391 +02	5.5547 -01	1.3388 +02
30	6.9425 -01	1.3373 +02	6.9428 -01	1.3365 +02
35	8.3303 -01	1.3355 +02	8.3306 -01	1.3350 +02
40	9.7176 -01	1.3336 +02	9.7179 -01	1.3332 +02
45	1.1104 +00	1.3318 +02	1.1105 +00	1.3313 +02
50	1.2491 +00	1.3300 +02	1.2491 +00	1.3294 +02
55	1.3877 +00	1.3282 +02	1.3877 +00	1.3275 +02
60	1.5262 +00	1.3264 +02	1.5262 +00	1.3257 +02
65	1.6646 +00	1.3246 +02	1.6647 +00	1.3238 +02
70	1.8030 +00	1.3227 +02	1.8030 +00	1.3219 +02
75	1.9413 +00	1.3209 +02	1.9413 +00	1.3201 +02
80	2.0795 +00	1.3191 +02	2.0795 +00	1.3182 +02
85	2.2176 +00	1.3173 +02	2.2176 +00	1.3163 +02
90	2.3556 +00	1.3155 +02	2.3556 +00	1.3145 +02
95	2.4935 +00	1.3137 +02	2.4936 +00	1.3126 +02
100	2.6313 +00	1.3119 +02	2.6313 +00	1.3107 +02

K8	PSI(DEGREES) = 3	PSI(DEGREES) = 4	PSI(DEGREES) = 5	PSI(DEGREES) = 7
	G(8)	PHASE(DEGREES)	G(8)	PHASE(DEGREES)
10	1.3907 -01	1.3387 +02	1.3922 -01	1.3341 +02
15	2.7813 -01	1.3349 +02	2.7842 -01	1.3288 +02
20	4.1716 -01	1.3311 +02	4.1758 -01	1.3235 +02
25	5.5616 -01	1.3273 +02	5.5669 -01	1.3182 +02
30	6.9511 -01	1.3236 +02	6.9573 -01	1.3129 +02
35	8.3400 -01	1.3198 +02	8.3468 -01	1.3076 +02
40	9.7283 -01	1.3160 +02	9.7353 -01	1.3023 +02
45	1.1116 +00	1.3122 +02	1.1123 +00	1.2970 +02
50	1.2502 +00	1.3084 +02	1.2509 +00	1.2917 +02
55	1.3888 +00	1.3047 +02	1.3893 +00	1.2864 +02
60	1.5272 +00	1.3009 +02	1.5276 +00	1.2811 +02
65	1.6656 +00	1.2971 +02	1.6657 +00	1.2758 +02
70	1.8038 +00	1.2934 +02	1.8036 +00	1.2705 +02
75	1.9418 +00	1.2895 +02	1.9412 +00	1.2652 +02
80	2.0798 +00	1.2858 +02	2.0787 +00	1.2599 +02
85	2.2175 +00	1.2820 +02	2.2159 +00	1.2546 +02
90	2.3551 +00	1.2783 +02	2.3528 +00	1.2493 +02
95	2.4925 +00	1.2745 +02	2.4895 +00	1.2441 +02
100	2.6297 +00	1.2707 +02	2.6258 +00	1.2388 +02

K8	PSI(DEGREES) = 10	PSI(DEGREES) = 12	PSI(DEGREES) = 14	PSI(DEGREES) = 15
	G(8)	PHASE(DEGREES)	G(8)	PHASE(DEGREES)
10	1.4099 -01	1.2793 +02	1.4191 -01	1.2508 +02
15	2.8173 -01	1.2558 +02	2.8333 -01	1.2177 +02
20	4.2198 -01	1.2322 +02	4.2380 -01	1.1846 +02
25	5.6150 -01	1.2087 +02	5.6284 -01	1.1515 +02
30	7.0005 -01	1.1851 +02	6.9999 -01	1.1185 +02
35	8.4379 -01	1.1616 +02	8.3477 -01	1.0854 +02
40	9.7329 -01	1.1381 +02	9.6674 -01	1.0523 +02
45	1.1075 +00	1.1145 +02	1.0955 +00	1.0193 +02
50	1.2398 +00	1.0910 +02	1.2205 +00	9.8620 +01
55	1.3700 +00	1.0675 +02	1.3414 +00	9.5315 +01
60	1.4978 +00	1.0439 +02	1.4579 +00	9.2011 +01
65	1.6230 +00	1.0204 +02	1.5694 +00	8.8707 +01
70	1.7455 +00	9.9689 +01	1.6756 +00	8.5404 +01
75	1.8649 +00	9.7338 +01	1.7762 +00	8.2101 +01
80	1.9812 +00	9.4987 +01	1.8709 +00	7.8800 +01
85	2.0940 +00	9.2637 +01	1.9593 +00	7.5500 +01
90	2.2033 +00	9.0288 +01	2.0411 +00	7.2200 +01
95	2.3087 +00	8.7940 +01	2.1161 +00	6.8902 +01
100	2.4102 +00	8.5592 +01	2.1839 +00	6.5605 +01

K8	PSI(DEGREES) = 16	PSI(DEGREES) = 17	PSI(DEGREES) = 18	PSI(DEGREES) = 18.5
	G(8)	PHASE(DEGREES)	G(8)	PHASE(DEGREES)
10	1.4424 -01	1.1783 +02	1.4493 -01	1.1570 +02
15	2.8703 -01	1.1211 +02	2.8802 -01	1.0927 +02
20	4.2695 -01	1.0638 +02	4.2747 -01	1.0284 +02
25	5.6260 -01	1.0066 +02	5.6152 -01	9.6405 +01
30	6.9262 -01	9.4937 +01	6.8849 -01	8.9974 +01
35	8.1571 -01	8.9215 +01	8.0676 -01	8.3543 +01
40	9.3064 -01	8.3494 +01	9.1485 -01	7.7113 +01
45	1.0363 +00	7.7774 +01	1.0114 +00	7.0683 +01
50	1.1315 +00	7.2054 +01	1.0952 +00	6.4255 +01
55	1.2155 +00	6.6335 +01	1.1652 +00	5.7828 +01
60	1.2873 +00	6.0618 +01	1.2205 +00	5.1403 +01
65	1.3463 +00	5.4902 +01	1.2604 +00	4.4979 +01
70	1.3918 +00	4.9187 +01	1.2844 +00	3.8557 +01
75	1.4234 +00	4.3475 +01	1.2922 +00	3.2137 +01
80	1.4408 +00	3.7764 +01	1.2838 +00	2.5720 +01
85	1.4439 +00	3.2056 +01	1.2592 +00	1.9307 +01
90	1.4425 +00	2.6351 +01	1.2188 +00	1.2898 +01
95	1.4069 +00	2.0650 +01	1.1631 +00	6.4948 +00
100	1.3673 +00	1.4953 +01	1.0927 +00	9.8482 -02

Table 2 - Continued

	PSI(0EGREES) = 19		PSI(0EGREES) = 19.5		PSI(0EGREES) = 20		PSI(0EGREES) = 20.5	
KB	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)
10	1.4641 -01	1.1107 +02	1.4681 -01	1.0984 +02	1.4722 -01	1.0857 +02	1.4763 -01	1.0728 +02
15	2.8998 -01	1.0310 +02	2.9047 -01	1.0145 +02	2.9095 -01	9.9763 +01	2.9142 -01	9.8035 +01
20	4.2793 -01	9.5122 +01	4.2791 -01	9.3064 +01	4.2783 -01	9.0955 +01	4.2764 -01	8.8794 +01
25	5.5759 -01	8.7147 +01	5.5617 -01	8.4678 +01	5.5456 -01	8.2147 +01	5.5274 -01	7.9554 +01
30	6.7644 -01	7.9173 +01	6.7253 -01	7.6292 +01	6.6821 -01	7.4339 +01	6.6347 -01	7.0315 +01
35	7.8218 -01	7.1200 +01	7.7447 -01	6.7907 +01	7.6608 -01	6.4533 +01	7.5697 -01	6.1076 +01
40	8.7278 -01	6.3227 +01	8.5984 -01	5.9523 +01	8.4585 -01	5.5727 +01	8.3080 -01	5.1839 +01
45	9.4647 -01	5.5256 +01	9.2679 -01	5.1141 +01	9.0566 -01	4.6923 +01	8.8304 -01	4.2603 +01
50	1.0018 +00	4.7286 +01	9.7390 -01	4.2759 +01	9.4408 -01	3.8120 +01	9.1236 -01	3.3368 +01
55	1.0378 +00	3.9317 +01	1.0002 +00	3.4380 +01	9.6023 -01	2.9430 +01	9.1799 -01	2.4136 +01
60	1.0537 +00	3.1351 +01	1.0050 +00	2.6003 +01	9.5372 -01	2.0522 +01	8.9979 -01	1.4908 +01
65	1.0492 +00	2.3388 +01	9.8842 -01	1.7629 +01	9.2472 -01	1.1727 +01	8.5825 -01	5.6828 +00
70	1.0244 +00	1.5428 +01	9.5067 -01	9.2594 +00	8.7392 -01	2.9379 +00	7.9444 -01	3.5361 +00
75	9.7979 -01	7.4721 +00	8.9260 -01	8.9493 -01	8.0252 -01	-5.8449 +00	7.1005 -01	-1.2746 +01
80	9.1626 -01	-4.7760 -01	8.1547 -01	-7.4619 +00	7.1223 -01	-1.4618 +01	6.0726 -01	-2.1943 +01
85	8.3504 -01	-8.4188 +00	7.2093 -01	-1.5807 +01	6.0518 -01	-2.3374 +01	4.8877 -01	-3.1113 +01
90	7.3772 -01	-1.6367 +01	6.1103 -01	-2.4134 +01	4.8391 -01	-3.2100 +01	3.5764 -01	-4.0229 +01
95	6.2617 -01	-2.4255 +01	4.8811 -01	-3.2426 +01	3.5129 -01	-4.0760 +01	2.1731 -01	-4.9182 +01
100	5.0258 -01	-3.2127 +01	3.5483 -01	-4.0645 +01	2.1047 -01	-4.9220 +01	7.1444 -02	-5.6964 +01

	PSI(0EGREES) = 20.75		PSI(0EGREES) = 21		PSI(0EGREES) = 21.75		PSI(0EGREES) = 22	
KB	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)
10	1.4784 -01	1.0662 +02	1.4806 -01	1.0595 +02	1.4872 -01	1.0390 +02	1.4894 -01	1.0320 +02
15	2.9166 -01	9.7156 +01	2.9189 -01	9.6266 +01	2.9257 -01	9.3536 +01	2.9279 -01	9.2606 +01
20	4.2752 -01	8.7695 +01	4.2739 -01	8.6583 +01	4.2686 -01	8.3170 +01	4.2663 -01	8.2008 +01
25	5.5175 -01	7.8235 +01	5.5070 -01	7.6900 +01	5.4720 -01	7.2806 +01	5.4591 -01	7.1410 +01
30	6.6094 -01	6.8776 +01	6.5830 -01	6.7219 +01	6.4966 -01	6.2442 +01	6.4654 -01	6.0814 +01
35	7.5214 -01	5.9317 +01	7.4712 -01	5.7538 +01	7.3090 -01	5.2078 +01	7.2510 -01	5.0218 +01
40	8.2285 -01	4.9860 +01	8.1463 -01	4.7858 +01	7.8827 -01	4.1717 +01	7.7891 -01	3.9624 +01
45	8.7117 -01	4.0404 +01	8.5893 -01	3.8180 +01	8.1990 -01	3.1357 +01	8.0613 -01	2.9032 +01
50	8.9578 -01	3.0950 +01	8.7873 -01	2.8504 +01	8.2476 -01	2.0999 +01	8.0584 -01	1.8442 +01
55	8.9602 -01	2.1499 +01	8.7350 -01	1.8831 +01	8.0269 -01	1.0645 +01	7.7806 -01	7.8551 +00
60	8.7188 -01	1.2051 +01	8.4337 -01	9.1611 +00	7.5444 -01	2.9440 -01	7.2374 -01	-2.7267 +00
65	8.2404 -01	2.6672 +00	7.8923 -01	-5.0395 -01	6.8158 -01	-1.0049 +01	6.4476 -01	-1.3301 +01
70	7.5380 -01	-6.8300 +00	7.1263 -01	-1.0162 +01	5.8650 -01	-2.0382 +01	5.4380 -01	-2.3863 +01
75	6.6309 -01	-1.6257 +01	6.1575 -01	-1.9808 +01	4.7232 -01	-3.0695 +01	4.2434 -01	-3.4401 +01
80	5.5438 -01	-2.5668 +01	5.0137 -01	-2.9434 +01	3.4277 -01	-4.0965 +01	2.9045 -01	-4.4880 +01
85	4.3064 -01	-3.5045 +01	3.7276 -01	-3.9016 +01	2.0210 -01	-5.1099 +01	1.4672 -01	-5.5122 +01
90	2.9526 -01	-4.4344 +01	2.3360 -01	-4.8475 +01	5.4915 -02	-6.0002 +01	2.6595 -03	7.1299 +01
95	1.5191 -01	-5.3335 +01	8.7867 -02	-5.7195 +01	9.4061 -02	1.0649 +02	1.5051 -01	1.0232 +02
100	9.1376 -03	-3.4545 +01	6.0386 -02	1.0939 +02	2.3983 -01	9.6842 +01	2.9383 -01	9.2073 +01

	PSI(0EGREES) = 23		PSI(0EGREES) = 24		PSI(0EGREES) = 25	
KB	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)
10	1.4986 -01	1.0034 +02	1.5082 -01	9.7351 +01	1.5181 -01	9.4245 +01
15	2.9363 -01	8.8784 +01	2.9442 -01	8.4801 +01	2.9512 -01	8.0660 +01
20	4.2550 -01	7.7230 +01	4.2394 -01	7.2252 +01	4.2190 -01	6.7075 +01
25	5.4011 -01	6.5678 +01	5.3319 -01	5.9704 +01	5.2506 -01	5.3492 +01
30	6.3281 -01	5.4126 +01	6.1695 -01	4.7157 +01	5.9884 -01	3.9910 +01
35	6.9985 -01	4.2575 +01	6.7122 -01	3.4611 +01	6.3909 -01	2.6329 +01
40	7.3852 -01	3.1026 +01	6.9340 -01	2.2067 +01	6.4358 -01	1.2750 +01
45	7.4726 -01	1.9479 +01	6.8246 -01	9.5255 +00	6.1206 -01	-8.2556 -01
50	7.2571 -01	7.9350 +00	6.3890 -01	-3.0120 +00	5.4630 -01	-1.4396 +01
55	6.7476 -01	-3.6044 +00	5.6484 -01	-1.5543 +01	4.5000 -01	-2.7956 +01
60	5.9648 -01	-1.5137 +01	4.6381 -01	-2.8063 +01	3.2855 -01	-4.1495 +01
65	4.9406 -01	-2.6657 +01	3.4066 -01	-4.0558 +01	1.8875 -01	-5.4963 +01
70	3.7165 -01	-3.8151 +01	2.0127 -01	-5.2974 +01	3.8456 -02	-6.7522 +01
75	2.3424 -01	-4.9572 +01	5.2330 -02	-6.4636 +01	1.1396 -01	9.7193 +01
80	8.7397 -02	-6.0547 +01	9.9076 -02	1.0101 +02	2.5992 -01	8.3862 +01
85	6.2957 -02	1.0574 +02	2.4566 -01	8.8847 +01	3.9128 -01	7.0355 +01
90	2.1065 -01	9.5083 +01	3.8045 -01	7.6402 +01	5.0070 -01	5.6815 +01
95	3.4975 -01	8.3694 +01	4.9700 -01	6.3908 +01	5.8205 -01	4.3266 +01
100	4.7461 -01	7.2218 +01	5.8975 -01	5.1401 +01	6.3081 -01	2.9716 +01

Table 3

	KA=5 DELTA(0EGREES)=10		PSI(0EGREES) = 0		PSI(0EGREES) = 1	
KB	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)
10	2.7760 -01	1.3282 +02	2.7765 -01	1.3275 +02	2.7777 -01	1.3256 +02
15	5.5488 -01	1.3209 +02	5.5496 -01	1.3201 +02	5.5520 -01	1.3175 +02
20	8.3163 -01	1.3137 +02	8.3175 -01	1.3126 +02	8.3209 -01	1.3093 +02
25	1.1077 +00	1.3064 +02	1.1078 +00	1.3051 +02	1.1082 +00	1.3012 +02
30	1.3828 +00	1.2920 +02	1.3830 +00	1.2977 +02	1.3835 +00	1.2931 +02
35	1.6569 +00	1.2920 +02	1.6571 +00	1.2903 +02	1.6575 +00	1.2850 +02
40	1.9298 +00	1.2848 +02	1.9299 +00	1.2828 +02	1.9303 +00	1.2770 +02
45	2.2012 +00	1.2776 +02	2.2013 +00	1.2755 +02	2.2016 +00	1.2690 +02
50	2.4710 +00	1.2705 +02	2.4710 +00	1.2681 +02	2.4712 +00	1.2610 +02
55	2.7390 +00	1.2634 +02	2.7390 +00	1.2608 +02	2.7388 +00	1.2530 +02
60	3.0050 +00	1.2563 +02	3.0049 +00	1.2535 +02	3.0045 +00	1.2451 +02
65	3.2690 +00	1.2492 +02	3.2687 +00	1.2462 +02	3.2679 +00	1.2372 +02
70	3.5306 +00	1.2422 +02	3.5302 +00	1.2390 +02	3.5289 +00	1.2293 +02
75	3.7899 +00	1.2353 +02	3.7893 +00	1.2318 +02	3.7873 +00	1.2215 +02
80	4.0465 +00	1.2284 +02	4.0457 +00	1.2247 +02	4.0430 +00	1.2137 +02
85	4.3004 +00	1.2215 +02	4.2993 +00	1.2176 +02	4.2957 +00	1.2060 +02
90	4.5513 +00	1.2147 +02	4.5500 +00	1.2106 +02	4.5455 +00	1.1984 +02
95	4.7993 +00	1.2079 +02	4.7976 +00	1.2036 +02	4.7920 +00	1.1908 +02
100	5.0441 +00	1.2012 +02	5.0420 +00	1.1967 +02	5.0353 +00	1.1832 +02

Table 3 - Continued

PSI(DEGREES) = 4		PSI(DEGREES) = 5		PSI(DEGREES) = 7		PSI(DEGREES) = 10		
K8	G(8)	PHASE(DEGREES)	G(8)	PHASE(DEGREES)	G(8)	PHASE(DEGREES)	G(8)	PHASE(DEGREES)
10	2.7827 -01	1.3178 +02	2.7865 -01	1.3119 +02	2.7965 -01	1.2963 +02	2.8178 -01	1.2632 +02
15	5.5616 -01	1.3070 +02	5.5688 -01	1.2992 +02	5.5875 -01	1.2784 +02	5.6256 -01	1.2343 +02
20	8.3343 -01	1.2963 +02	8.3441 -01	1.2866 +02	8.3688 -01	1.2606 +02	8.4149 -01	1.2055 +02
25	1.1098 +00	1.2856 +02	1.1110 +00	1.2739 +02	1.1136 +00	1.2427 +02	1.1177 +00	1.1766 +02
30	1.3851 +00	1.2749 +02	1.3863 +00	1.2613 +02	1.3886 +00	1.2249 +02	1.3904 +00	1.1478 +02
35	1.6591 +00	1.2643 +02	1.6600 +00	1.2487 +02	1.6614 +00	1.2071 +02	1.6588 +00	1.1190 +02
40	1.9315 +00	1.2536 +02	1.9320 +00	1.2361 +02	1.9316 +00	1.1894 +02	1.9220 +00	1.0903 +02
45	2.2022 +00	1.2430 +02	2.2020 +00	1.2235 +02	2.1988 +00	1.1717 +02	2.1793 +00	1.0617 +02
50	2.4708 +00	1.2324 +02	2.4696 +00	1.2110 +02	2.4627 +00	1.1540 +02	2.4299 +00	1.0331 +02
55	2.7372 +00	1.2219 +02	2.7347 +00	1.1986 +02	2.7229 +00	1.1364 +02	2.6731 +00	1.0046 +02
60	3.0011 +00	1.2114 +02	2.9969 +00	1.1862 +02	2.9790 +00	1.1189 +02	2.9083 +00	9.7626 +01
65	3.2624 +00	1.2009 +02	3.2561 +00	1.1738 +02	3.2307 +00	1.1014 +02	3.1347 +00	9.4797 +01
70	3.5208 +00	1.1905 +02	3.5120 +00	1.1615 +02	3.4477 +00	1.0840 +02	3.3518 +00	9.1980 +01
75	3.7761 +00	1.1802 +02	3.7644 +00	1.1492 +02	3.7195 +00	1.0667 +02	3.5590 +00	8.9175 +01
80	4.0282 +00	1.1699 +02	4.0131 +00	1.1370 +02	3.9559 +00	1.0495 +02	3.7557 +00	8.6384 +01
85	4.2769 +00	1.1597 +02	4.2579 +00	1.1249 +02	4.1868 +00	1.0324 +02	3.9415 +00	8.3607 +01
90	4.5220 +00	1.1495 +02	4.4985 +00	1.1129 +02	4.4116 +00	1.0153 +02	4.1159 +00	8.0846 +01
95	4.7632 +00	1.1394 +02	4.7347 +00	1.1009 +02	4.6303 +00	9.9838 +01	4.2786 +00	7.8101 +01
100	5.0006 +00	1.1294 +02	4.9665 +00	1.0890 +02	4.8425 +00	9.8156 +01	4.4291 +00	7.5375 +01

PSI(DEGREES) = 12		PSI(DEGREES) = 15		PSI(DEGREES) = 16		PSI(DEGREES) = 17		
K8	G(8)	PHASE(DEGREES)	G(8)	PHASE(DEGREES)	G(8)	PHASE(DEGREES)	G(8)	PHASE(DEGREES)
10	2.8361 -01	1.2348 +02	2.8896 -01	1.1825 +02	2.8824 -01	1.1626 +02	2.8960 -01	1.1414 +02
15	5.6566 -01	1.1964 +02	5.7092 -01	1.1267 +02	5.7278 -01	1.1001 +02	5.7466 -01	1.0719 +02
20	8.4476 -01	1.1580 +02	8.4907 -01	1.0710 +02	8.5012 -01	1.0377 +02	8.5088 -01	1.0024 +02
25	1.1195 +00	1.1197 +02	1.1186 +00	1.0152 +02	1.1169 +00	9.7539 +01	1.1141 +00	9.3303 +01
30	1.3886 +00	1.0814 +02	1.3770 +00	9.5961 +01	1.3697 +00	9.1313 +01	1.3603 +00	8.6373 +01
35	1.6506 +00	1.0432 +02	1.6215 +00	9.0407 +01	1.6056 +00	8.5097 +01	1.5858 +00	7.9453 +01
40	1.9044 +00	1.0051 +02	1.8499 +00	8.4862 +01	1.8217 +00	7.8892 +01	1.7874 +00	7.2547 +01
45	2.1486 +00	9.6702 +01	2.0599 +00	7.9330 +01	2.0154 +00	7.2701 +01	1.9620 +00	6.5656 +01
50	2.3822 +00	9.2907 +01	2.2496 +00	7.3813 +01	2.1845 +00	6.6527 +01	2.1071 +00	5.8784 +01
55	2.6040 +00	8.9122 +01	2.4172 +00	6.8311 +01	2.3269 +00	6.0371 +01	2.2206 +00	5.1935 +01
60	2.8130 +00	8.5350 +01	2.5611 +00	6.2829 +01	2.4412 +00	5.4239 +01	2.3012 +00	4.5112 +01
65	3.0082 +00	8.1592 +01	2.6800 +00	5.7369 +01	2.5260 +00	4.8132 +01	2.3476 +00	3.8320 +01
70	3.1889 +00	7.7848 +01	2.7731 +00	5.1934 +01	2.5806 +00	4.2056 +01	2.3595 +00	3.1567 +01
75	3.3541 +00	7.4122 +01	2.8395 +00	4.6528 +01	2.6044 +00	3.6015 +01	2.3369 +00	2.4860 +01
80	3.5033 +00	7.0414 +01	2.8788 +00	4.1155 +01	2.5975 +00	3.0018 +01	2.2806 +00	1.8210 +01
85	3.6359 +00	6.6727 +01	2.8908 +00	3.5821 +01	2.5602 +00	2.4071 +01	2.1915 +00	1.1631 +01
90	3.7514 +00	6.3062 +01	2.8758 +00	3.0531 +01	2.4933 +00	1.8185 +01	2.0714 +00	5.1428 +00
95	3.8493 +00	5.9421 +01	2.8342 +00	2.5294 +01	2.3979 +00	1.2375 +01	1.9224 +00	-1.2244 +00
100	3.9295 +00	5.5807 +01	2.7667 +00	2.0118 +01	2.2755 +00	6.6593 +00	1.7472 +00	-7.4261 +00

PSI(DEGREES) = 18		PSI(DEGREES) = 19		PSI(DEGREES) = 19.5		PSI(DEGREES) = 20		
K8	G(8)	PHASE(DEGREES)	G(8)	PHASE(DEGREES)	G(8)	PHASE(DEGREES)	G(8)	PHASE(DEGREES)
10	2.9104 -01	1.1189 +02	2.9255 -01	1.0953 +02	2.9334 -01	1.0830 +02	2.9415 -01	1.0704 +02
15	5.7655 -01	1.0420 +02	5.7842 -01	1.0104 +02	5.7935 -01	9.9400 +01	5.8026 -01	9.7719 +01
20	8.5128 -01	9.6504 +01	8.5123 -01	9.2559 +01	8.5102 -01	9.0509 +01	8.5067 -01	8.8409 +01
25	1.1101 +00	8.8818 +01	1.1049 +00	8.4085 +01	1.1017 +00	8.1627 +01	1.0982 +00	7.9107 +01
30	1.3484 +00	8.1142 +01	1.3338 +00	7.5623 +01	1.3254 +00	7.2755 +01	1.3161 +00	6.9816 +01
35	1.5618 +00	7.3478 +01	1.5329 +00	6.7173 +01	1.5165 +00	6.3898 +01	1.4988 +00	6.0541 +01
40	1.7463 +00	6.5829 +01	1.6978 +00	5.8740 +01	1.6706 +00	5.5058 +01	1.6414 +00	5.1284 +01
45	1.8987 +00	5.8197 +01	1.8251 +00	5.0328 +01	1.7841 +00	4.6240 +01	1.7403 +00	4.2050 +01
50	2.0164 +00	5.0588 +01	1.9119 +00	4.1941 +01	1.8543 +00	3.7450 +01	1.7930 +00	3.2847 +01
55	2.0974 +00	4.3005 +01	1.9566 +00	3.3585 +01	1.8796 +00	2.8694 +01	1.7983 +00	2.3682 +01
60	2.1403 +00	3.5453 +01	1.9585 +00	2.5269 +01	1.8599 +00	1.9982 +01	1.7563 +00	1.4566 +01
65	2.1446 +00	2.7941 +01	1.9176 +00	1.7003 +01	1.7957 +00	1.1328 +01	1.6685 +00	5.5187 +00
70	2.1105 +00	2.0478 +01	1.8393 +00	8.8034 +00	1.6889 +00	2.7530 +00	1.5375 +00	-3.4340 +00
75	2.0388 +00	1.3077 +01	1.7137 +00	6.9294 -01	1.5424 +00	-5.7116 +00	1.3670 +00	-1.2245 +01
80	1.9314 +00	5.7575 +00	1.5557 +00	-7.2910 +00	1.3605 +00	-1.4010 +01	1.1621 +00	-2.0828 +01
85	1.7903 +00	-1.4536 +00	1.3653 +00	-1.5084 +01	1.1475 +00	-2.2037 +01	9.2853 -01	-2.8995 +01
90	1.6186 +00	-8.5117 +00	1.1471 +00	-2.2567 +01	9.0926 -01	-2.9565 +01	6.7317 -01	-3.6258 +01
95	1.4197 +00	-1.5342 +01	9.0636 -01	-2.9476 +01	6.5223 -01	-3.5991 +01	4.0431 -01	-4.0800 +01
100	1.1978 +00	-2.1808 +01	6.4937 -01	-3.5120 +01	3.8479 -01	-3.9000 +01	1.4106 -01	-2.6796 +01

PSI(DEGREES) = 20.5		PSI(DEGREES) = 21		PSI(DEGREES) = 21.5		PSI(DEGREES) = 22		
K8	G(8)	PHASE(DEGREES)	G(8)	PHASE(DEGREES)	G(8)	PHASE(DEGREES)	G(8)	PHASE(DEGREES)
10	2.9497 -01	1.0574 +02	2.9582 -01	1.0442 +02	2.9668 -01	1.0307 +02	2.9757 -01	1.0169 +02
15	5.8116 -01	9.5998 +01	5.8204 -01	9.4235 +01	5.8290 -01	9.2433 +01	5.8374 -01	9.0590 +01
20	8.5018 -01	8.6257 +01	8.4952 -01	8.4045 +01	8.4869 -01	8.1802 +01	8.4768 -01	7.9498 +01
25	1.0942 +00	7.6525 +01	1.0897 +00	7.3883 +01	1.0848 +00	7.1180 +01	1.0795 +00	6.8417 +01
30	1.3060 +00	6.6806 +01	1.2951 +00	6.3725 +01	1.2832 +00	6.0572 +01	1.2704 +00	5.7349 +01
35	1.4797 +00	5.7102 +01	1.4591 +00	5.3582 +01	1.4370 +00	4.9982 +01	1.4133 +00	4.6300 +01
40	1.6101 +00	4.7418 +01	1.5766 +00	4.3461 +01	1.5409 +00	3.9414 +01	1.5030 +00	3.5276 +01
45	1.6937 +00	3.7759 +01	1.6441 +00	3.3368 +01	1.5916 +00	2.8875 +01	1.5362 +00	2.4283 +01
50	1.7281 +00	2.8133 +01	1.6596 +00	2.3310 +01	1.5876 +00	1.8376 +01	1.5121 +00	1.3334 +01
55	1.7127 +00	1.8550 +01	1.6229 +00	1.3300 +01	1.5291 +00	7.9316 +00	1.4316 +00	2.4473 +00
60	1.6481 +00	9.0237 +00	1.5354 +00	3.3556 +00	1.4186 +00	-2.4357 +00	1.2982 +00	-8.3473 +00
65	1.5365 +00	-4.2268 -01	1.4002 +00	-6.4922 +00	1.2602 +00	-1.2684 +01	1.1171 +00	-1.8992 +01
70	1.3815 +00	-9.7513 +00	1.2220 +00	-1.6190 +01	1.0597 +00	-2.2734 +01	8.9568 -01	-2.9361 +01
75	1.1880 +00	-1.8892 +01	1.0067 +00	-2.5627 +01	8.2436 -01	-3.2400 +01	6.4255 -01	-3.9111 +01
80	9.6188 -01	-2.7700 +01	7.6156 -01	-3.4537 +01	5.6294 -01	-4.1128 +01	3.6810 -01	-4.6842 +01
85	7.1032 -01	-3.5804 +01	4.9519 -01	-4.2051 +01	2.8599 -01	-4.6175 +01	9.1228 -02	-3.3449 +01
90	4.4166 -01	-4.1902 +01	2.1911 -01	-4.2856 +01	5.4766 -02	2.8970 +01	2.1606 -01	9.0972 +01
95	1.7009 -01	-3.6236 +01	9.7219 -02	7.1437 +01	2.9581 -01	9.1407 +01	4.9105 -01	8.7359 +01
100	1.4608 -01	8.1227 +01	3.6108 -01	9.1045 +01	5.6559 -01	8.6113 +01	7.4785 -01	7.8480 +01

Table 3 - Continued

KB	PSI(0DEGREES) = 23		PSI(0DEGREES) = 24		PSI(0DEGREES) = 25	
	G(8)	PHASE(0DEGREES)	G(B)	PHASE(0DEGREES)	G(B)	PHASE(0DEGREES)
10	2.9939 -01	9.8833 +01	3.0129 -01	9.5857 +01	3.0327 -01	9.2763 +01
15	5.8532 -01	8.6783 +01	5.8678 -01	8.2816 +01	5.8807 -01	7.8691 +01
20	8.4508 -01	7.4740 +01	8.4162 -01	6.9783 +01	8.3721 -01	6.4627 +01
25	1.0671 +00	6.2709 +01	1.0526 +00	5.6761 +01	1.0357 +00	5.0576 +01
30	1.2417 +00	5.0693 +01	1.2089 +00	4.3757 +01	1.1716 +00	3.6544 +01
35	1.3612 +00	3.8697 +01	1.3024 +00	3.0776 +01	1.2369 +00	2.2538 +01
40	1.4203 +00	2.6730 +01	1.3286 +00	1.7827 +01	1.2278 +00	8.5704 +00
45	1.4158 +00	1.4801 +01	1.2862 +00	4.9250 +00	1.1452 +00	-5.3385 +00
50	1.3510 +00	2.9267 +00	1.1779 +00	-7.9049 +00	9.9437 -01	-1.9148 +01
55	1.2252 +00	-8.8635 +00	1.0094 +00	-2.0613 +01	7.8463 -01	-3.2765 +01
60	1.0481 +00	-2.0514 +01	7.8980 -01	-3.3084 +01	5.2901 -01	-4.5891 +01
65	8.2499 -01	-3.1897 +01	5.3094 -01	-4.4952 +01	2.4353 -01	-5.6784 +01
70	5.6720 -01	-4.2628 +01	2.44699 -01	-5.4119 +01	6.1614 -02	8.0614 +01
75	2.8700 -01	-5.0784 +01	5.8918 -01	7.5317 +01	3.5154 -01	8.5780 +01
80	3.8617 -02	3.1086 +01	3.4331 -01	8.8119 +01	6.2217 -01	7.3627 +01
85	2.9971 -01	9.0640 +01	6.1451 -01	7.7521 +01	8.5420 -01	6.0417 +01
90	5.7313 -01	8.2295 +01	8.5266 -01	6.5536 +01	1.0337 +00	4.6951 +01
95	8.2016 -01	7.1668 +01	1.0454 +00	5.3203 +01	1.1503 +00	3.3427 +01
100	1.0296 +00	6.0496 +01	1.1832 +00	4.0770 +01	1.1975 +00	1.9938 +01

Table 4

KB	KA=5				PSI(0DEGREES) = 3	
	PSI(0DEGREES) = 0		PSI(0DEGREES) = 1		PSI(0DEGREES) = 2	PSI(0DEGREES)
10	4.1534 -01	1.3010 +02	4.1541 -01	1.3003 +02	4.1559 -01	1.2984 +02
15	8.2819 -01	1.2847 +02	8.2830 -01	1.2838 +02	8.2865 -01	1.2812 +02
20	1.2371 +00	1.2685 +02	1.2373 +00	1.2674 +02	1.2377 +00	1.2642 +02
25	1.6408 +00	1.2525 +02	1.6410 +00	1.2512 +02	1.6415 +00	1.2473 +02
30	2.0380 +00	1.2366 +02	2.0381 +00	1.2351 +02	2.0385 +00	1.2306 +02
35	2.4273 +00	1.2209 +02	2.4274 +00	1.2192 +02	2.4276 +00	1.2141 +02
40	2.8077 +00	1.2055 +02	2.8076 +00	1.2036 +02	2.8075 +00	1.1978 +02
45	3.1779 +00	1.1904 +02	3.1777 +00	1.1882 +02	3.1771 +00	1.1818 +02
50	3.5371 +00	1.1755 +02	3.5367 +00	1.1732 +02	3.5354 +00	1.1662 +02
55	3.8843 +00	1.1610 +02	3.8837 +00	1.1584 +02	3.8815 +00	1.1508 +02
60	4.2188 +00	1.1468 +02	4.2178 +00	1.1441 +02	4.2145 +00	1.1359 +02
65	4.5399 +00	1.1331 +02	4.5384 +00	1.1302 +02	4.5339 +00	1.1214 +02
70	4.8470 +00	1.1198 +02	4.8451 +00	1.1167 +02	4.8391 +00	1.1073 +02
75	5.1397 +00	1.1070 +02	5.1373 +00	1.1037 +02	5.1297 +00	1.0938 +02
80	5.4179 +00	1.0947 +02	5.4149 +00	1.0912 +02	5.4055 +00	1.0808 +02
85	5.6814 +00	1.0830 +02	5.6777 +00	1.0793 +02	5.6663 +00	1.0683 +02
90	5.9302 +00	1.0718 +02	5.9258 +00	1.0680 +02	5.9123 +00	1.0564 +02
95	6.1645 +00	1.0612 +02	6.1594 +00	1.0572 +02	6.1436 +00	1.0452 +02
100	6.3847 +00	1.0513 +02	6.3789 +00	1.0471 +02	6.3607 +00	1.0346 +02

KB	PSI(0DEGREES)= 4		PSI(0DEGREES)= 5		PSI(0DEGREES)= 7		PSI(0DEGREES)= 12	
	G(8)	PHASE(0DEGREES)	G(B)	PHASE(0DEGREES)	G(8)	PHASE(0DEGREES)	G(B)	PHASE(0DEGREES)
10	4.1634 -01	1.2906 +02	4.1690 -01	1.2848 +02	4.1838 -01	1.2693 +02	4.2425 -01	1.2081 +02
15	8.3002 -01	1.2709 +02	8.3104 -01	1.2632 +02	8.3370 -01	1.2425 +02	8.4352 -01	1.1610 +02
20	1.2395 +00	1.2513 +02	1.2408 +00	1.2416 +02	1.2440 +00	1.2158 +02	1.2539 +00	1.1141 +02
25	1.6433 +00	1.2319 +02	1.6445 +00	1.2203 +02	1.6474 +00	1.1894 +02	1.6518 +00	1.0674 +02
30	2.0399 +00	1.2126 +02	2.0408 +00	1.1991 +02	2.0421 +00	1.1631 +02	2.0337 +00	1.0211 +02
35	2.4281 +00	1.1936 +02	2.4280 +00	1.1782 +02	2.4263 +00	1.1371 +02	2.3964 +00	9.7520 +01
40	2.8064 +00	1.1748 +02	2.8049 +00	1.1575 +02	2.7985 +00	1.1165 +02	2.7369 +00	9.2981 +01
45	3.1737 +00	1.1563 +02	3.1702 +00	1.1372 +02	3.1572 +00	1.0862 +02	3.0526 +00	8.8500 +01
50	3.5289 +00	1.1382 +02	3.5228 +00	1.1172 +02	3.5011 +00	1.0614 +02	3.3416 +00	8.4084 +01
55	3.8711 +00	1.1205 +02	3.8616 +00	1.0977 +02	3.8291 +00	1.0370 +02	3.6019 +00	7.9749 +01
60	4.1994 +00	1.1031 +02	4.1858 +00	1.0786 +02	4.1403 +00	1.0131 +02	3.8324 +00	7.5497 +01
65	4.5132 +00	1.0863 +02	4.4948 +00	1.0600 +02	4.4339 +00	9.8984 +01	4.0323 +00	7.1340 +01
70	4.8119 +00	1.0699 +02	4.7880 +00	1.0419 +02	4.7094 +00	9.6719 +01	4.2013 +00	6.7289 +01
75	5.0952 +00	1.0541 +02	5.0650 +00	1.0244 +02	4.9664 +00	9.4522 +01	4.3395 +00	6.3355 +01
80	5.3629 +00	1.0389 +02	5.3257 +00	1.0075 +02	5.2050 +00	9.2397 +01	4.4476 +00	5.9547 +01
85	5.6148 +00	1.0243 +02	5.5700 +00	9.9131 +01	5.4252 +00	9.0350 +01	4.5268 +00	5.5877 +01
90	5.8513 +00	1.0103 +02	5.7982 +00	9.7579 +01	5.6273 +00	8.8384 +01	4.5785 +00	5.2355 +01
95	6.0724 +00	9.9707 +01	6.0107 +00	9.6101 +01	5.8121 +00	8.6505 +01	4.6048 +00	4.8991 +01
100	6.2789 +00	9.8452 +01	6.2080 +00	9.4699 +01	5.9802 +00	8.4715 +01	4.6079 +00	4.5796 +01

KB	PSI(0DEGREES)= 14		PSI(0DEGREES)= 15		PSI(0DEGREES)= 16		PSI(0DEGREES)= 17	
	G(8)	PHASE(0DEGREES)	G(B)	PHASE(0DEGREES)	G(B)	PHASE(0DEGREES)	G(B)	PHASE(0DEGREES)
10	4.2745 -01	1.1748 +02	4.2923 -01	1.1562 +02	4.3113 -01	1.1364 +02	4.3315 -01	1.1154 +02
15	8.4839 -01	1.1166 +02	8.5095 -01	1.0918 +02	8.5356 -01	1.0654 +02	8.5619 -01	1.0374 +02
20	1.2575 +00	1.0586 +02	1.2589 +00	1.0277 +02	1.2599 +00	9.9472 +01	1.2604 +00	9.5968 +01
25	1.6496 +00	1.0009 +02	1.6470 +00	9.6389 +01	1.6430 +00	9.2438 +01	1.6375 +00	8.8238 +01
30	2.0201 +00	9.4364 +01	2.0097 +00	9.0053 +01	9.9965 +00	8.5452 +01	1.9800 +00	8.0562 +01
35	2.3646 +00	8.8688 +01	2.3422 +00	8.3773 +01	2.3147 +00	7.8527 +01	2.2814 +00	7.2951 +01
40	2.6792 +00	8.3073 +01	2.6400 +00	7.7559 +01	2.5926 +00	7.1675 +01	2.5362 +00	6.5422 +01
45	2.9608 +00	7.7529 +01	2.8995 +00	7.1424 +01	2.8264 +00	6.4910 +01	2.7404 +00	5.7990 +01
50	3.2068 +00	7.2067 +01	3.1181 +00	6.5382 +01	3.0132 +00	5.8250 +01	2.8909 +00	5.0675 +01
55	3.4152 +00	6.701 +01	3.2937 +00	5.9446 +01	3.1512 +00	5.1711 +01	2.9865 +00	4.3501 +01
60	3.5848 +00	6.1443 +01	3.4253 +00	5.3635 +01	3.2397 +00	4.5316 +01	3.0270 +00	3.6495 +01
65	3.7151 +00	5.6308 +01	3.5129 +00	4.7966 +01	3.2793 +00	3.9088 +01	3.0138 +00	2.9691 +01
70	3.8065 +00	5.1313 +01	3.5571 +00	4.2460 +01	3.2715 +00	3.0356 +01	2.9497 +00	2.3131 +01
75	3.8598 +00	4.6473 +01	3.5598 +00	3.7142 +01	3.2189 +00	2.7256 +01	2.8387 +00	1.6870 +01
80	3.8767 +00	4.1809 +01	3.5232 +00	3.2038 +01	3.1251 +00	2.1730 +01	2.6858 +00	1.0977 +01
85	3.8595 +00	3.7340 +01	3.4507 +00	2.7179 +01	2.9946 +00	1.6528 +01	2.4972 +00	5.5504 +00
90	3.8110 +00	3.3088 +01	3.3460 +00	2.6201 +01	2.8325 +00	1.1717 +01	2.2800 +00	7.2241 -01
95	3.7345 +00	2.9077 +01	3.2135 +00	1.8345 +01	2.6447 +00	7.3762 +00	2.0421 +00	-3.3154 +00
100	3.6337 +00	2.5331 +01	3.0581 +00	1.4458 +01	2.4377 +00	3.6124 +00	1.7925 +00	-6.2803 +00

Table 4 - Continued

	PSI(0DEGREES) = 18		PSI(0DEGREES) = 19		PSI(0DEGREES) = 20		PSI(0DEGREES) = 21	
KB	G(B)	PHASE(0DEGREES)	G(B)	PHASE(0DEGREES)	G(B)	PHASE(0DEGREES)	G(B)	PHASE(0DEGREES)
10	4.3528 -01	1.0931 +02	4.3753 -01	1.0696 +02	4.3990 -01	1.0448 +02	4.4238 -01	1.0188 +02
15	8.5883 -01	1.0077 +02	8.6144 -01	9.7632 +01	8.6398 -01	9.4334 +01	8.6643 -01	9.0875 +01
20	1.2603 +00	9.2258 +01	1.2596 +00	8.8343 +01	1.2581 +00	8.4224 +01	1.2557 +00	7.9903 +01
25	1.6302 +00	8.3792 +01	1.6209 +00	7.9101 +01	1.6094 +00	7.4165 +01	1.5953 +00	6.8986 +01
30	1.9598 +00	7.5384 +01	1.9354 +00	6.9921 +01	1.9065 +00	6.4173 +01	1.8726 +00	5.8143 +01
35	2.2417 +00	6.7048 +01	2.1949 +00	6.0820 +01	2.1404 +00	5.4268 +01	2.0778 +00	4.7396 +01
40	2.4699 +00	5.8802 +01	2.3930 +00	5.1819 +01	2.3045 +00	4.4475 +01	2.2041 +00	3.6775 +01
45	2.6403 +00	5.0666 +01	2.5254 +00	4.2942 +01	2.3949 +00	3.4824 +01	2.2485 +00	2.6317 +01
50	2.7501 +00	4.2664 +01	2.5900 +00	3.4221 +01	2.4103 +00	2.5355 +01	2.2111 +00	1.6078 +01
55	2.7985 +00	3.4825 +01	2.45871 +00	2.5694 +01	2.3525 +00	1.6124 +01	2.0958 +00	6.1376 +00
60	2.7866 +00	2.7189 +01	2.5190 +00	1.7416 +01	2.2258 +00	7.2106 +00	1.9097 +00	-3.3747 +00
65	2.7169 +00	1.9802 +01	2.3902 +00	9.4621 +00	2.0372 +00	-1.2599 +00	1.6628 +00	-1.2232 +01
70	2.5937 +00	1.2732 +01	2.2072 +00	1.9429 +00	1.7958 +00	-9.0798 +00	1.3681 +00	-1.9987 +01
75	2.4230 +00	6.0710 +00	1.9781 +00	-4.9675 +00	1.5134 +00	-1.5870 +01	1.0421 +00	-2.5619 +01
80	2.2118 +00	-4.8177 -02	1.7130 +00	-1.0979 +01	1.2040 +00	-2.0857 +01	7.0816 -01	-2.6230 +01
85	1.9686 +00	-5.4208 +00	1.4239 +00	-1.5563 +01	8.8692 -01	-2.2206 +01	4.1930 -01	-1.1417 +01
90	1.7033 +00	-9.7184 +00	1.1259 +00	-1.7675 +01	5.9663 -01	-1.4900 +01	3.5317 -01	3.4597 +01
95	1.4276 +00	-1.2383 +01	8.4130 -01	-1.5043 +01	4.2309 -01	1.2012 +01	5.6921 -01	6.0387 +01
100	1.1563 +00	-1.2419 +01	6.1250 -01	-2.9460 +00	4.9478 -01	4.6075 +01	8.4685 -01	6.3836 +01

	PSI(0DEGREES) = 21.5		PSI(0DEGREES) = 22		PSI(0DEGREES) = 23		PSI(0DEGREES) = 24	
KB	G(B)	PHASE(0DEGREES)	G(B)	PHASE(0DEGREES)	G(B)	PHASE(0DEGREES)	G(B)	PHASE(0DEGREES)
10	4.4366 -01	1.0054 +02	4.4497 -01	9.9167 +01	4.4768 -01	9.6330 +01	4.5051 -01	9.3374 +01
15	8.6760 -01	8.9084 +01	8.6874 -01	8.7254 +01	8.7089 -01	8.3473 +01	8.7283 -01	7.9533 +01
20	1.2541 +00	7.7667 +01	1.2522 +00	7.5381 +01	1.2476 +00	7.0659 +01	1.2417 +00	6.5738 +01
25	1.5872 +00	6.6306 +01	1.5784 +00	6.3567 +01	1.5585 +00	5.7908 +01	1.5353 +00	5.2011 +01
30	1.8536 +00	5.5023 +01	1.8333 +00	5.1833 +01	1.7882 +00	4.5244 +01	1.7370 +00	3.8380 +01
35	2.0432 +00	4.3840 +01	2.0064 +00	4.0206 +01	1.9258 +00	3.2700 +01	1.8358 +00	2.4882 +01
40	2.1493 +00	3.2792 +01	2.0913 +00	2.8721 +01	1.9658 +00	2.0319 +01	1.8277 +00	1.1574 +01
45	2.1693 +00	2.1920 +01	2.0861 +00	1.7429 +01	1.9081 +00	8.1676 +00	1.7151 +00	-1.4520 +00
50	2.1044 +00	1.1290 +01	1.9932 +00	6.4043 +00	1.7579 +00	-3.6624 +00	1.5073 +00	-1.4024 +01
55	1.9598 +00	9.9917 -01	1.8192 +00	-4.2276 +00	1.5257 +00	-1.4907 +01	1.2196 +00	-2.5772 +01
60	1.7443 +00	-8.7820 +00	1.5748 +00	-1.4241 +01	1.2267 +00	-2.5184 +01	8.7274 -01	-3.5681 +01
65	1.4697 +00	-1.7733 +01	1.2741 +00	-2.3167 +01	8.8049 -01	-3.3295 +01	4.9593 -01	-3.9597 +01
70	1.1515 +00	-2.5153 +01	9.3545 -01	-2.9823 +01	5.1599 -01	-3.4714 +01	1.8663 -01	-1.2075 +00
75	8.0999 -01	-2.9144 +01	5.8577 -01	-3.0234 +01	2.2982 -01	2.4748 -01	3.8496 -01	6.5933 +01
80	4.8145 -01	-2.2816 +01	3.0180 -01	-5.2151 +00	3.8397 -01	6.1795 +01	7.2934 -01	6.6692 +01
85	3.0025 -01	1.8334 +01	3.6189 -01	5.2492 +01	7.0868 -01	6.6964 +01	1.0373 +00	5.8551 +01
90	4.7090 -01	5.8529 +01	6.5242 -01	6.5742 +01	1.0118 +00	6.1154 +01	1.2821 +00	4.8399 +01
95	7.5941 -01	6.4956 +01	9.4859 -01	6.3381 +01	1.2630 +00	5.2688 +01	1.4512 +00	3.7702 +01
100	1.0377 +00	6.1804 +01	1.2070 +00	5.7030 +01	1.4498 +00	4.3399 +01	1.5388 +00	2.7014 +01

	PSI(0DEGREES) = 25	
KB	G(B)	PHASE(0DEGREES)
10	4.5344 -01	9.0300 +01
15	8.7453 -01	7.5436 +01
20	1.2343 +00	6.0621 +01
25	1.5086 +00	4.5879 +01
30	1.6793 +00	3.1242 +01
35	1.7362 +00	1.6756 +01
40	1.6772 +00	2.4938 +00
45	1.5086 +00	-1.1410 +01
50	1.2445 +00	-2.4672 +01
55	9.0632 -01	-3.6529 +01
60	5.2297 -01	-4.3896 +01
65	1.6973 -01	-1.5124 +01
70	3.5366 -01	6.7451 +01
75	7.1385 -01	6.6208 +01
80	1.0292 +00	5.6319 +01
85	1.2719 +00	4.4689 +01
90	1.4279 +00	3.2660 +01
95	1.4913 +00	2.0749 +01
100	1.4632 +00	9.3076 +00

	KA=5 DELTA(0DEGREES)=20		PSI(0DEGREES) = 2		PSI(0DEGREES) = 3	
KB	G(B)	PHASE(0DEGREES)	G(B)	PHASE(0DEGREES)	G(B)	PHASE(0DEGREES)
10	5.5000 -01	1.2630 +02	5.5008 -01	1.2623 +02	5.5032 -01	1.2604 +02
15	1.0896 +00	1.2344 +02	1.0897 +00	1.2336 +02	1.0902 +00	1.2310 +02
20	1.6132 +00	1.2064 +02	1.6134 +00	1.2054 +02	1.6139 +00	1.2022 +02
25	2.1158 +00	1.1792 +02	2.1159 +00	1.1779 +00	2.1163 +00	1.1741 +02
30	2.5928 +00	1.1529 +02	2.5929 +00	1.1514 +02	2.5930 +00	1.1470 +02
35	3.0406 +00	1.1278 +02	3.0405 +00	1.1261 +02	3.0401 +00	1.1211 +02
40	3.4563 +00	1.1040 +02	3.4559 +00	1.1021 +02	3.4548 +00	1.0965 +02
45	3.8381 +00	1.0817 +02	3.8374 +00	1.0797 +02	3.8352 +00	1.0736 +02
50	4.1851 +00	1.0612 +02	4.1840 +00	1.0590 +02	4.1806 +00	1.0523 +02
55	4.4977 +00	1.0427 +02	4.4961 +00	1.0403 +02	4.4914 +00	1.0331 +02
60	4.7772 +00	1.0261 +02	4.7752 +00	1.0236 +02	4.7690 +00	1.0159 +02
65	5.0262 +00	1.0118 +02	5.0237 +00	1.0091 +02	5.0159 +00	1.0010 +02
70	5.2481 +00	9.9979 +01	5.2451 +00	9.9693 +01	5.2357 +00	9.8836 +01
75	5.4472 +00	9.9007 +01	5.4437 +00	9.8707 +01	5.4329 +00	9.7809 +01
80	5.6282 +00	9.8262 +01	5.6243 +00	9.7949 +01	5.6123 +00	9.7012 +01
85	5.7965 +00	9.7732 +01	5.7923 +00	9.7407 +01	5.7793 +00	9.6431 +01
90	5.9573 +00	9.7398 +01	5.9529 +00	9.7060 +01	5.9391 +00	9.6046 +01
95	6.1155 +00	9.7230 +01	6.1110 +00	9.6879 +01	6.0968 +00	9.5828 +01
100	6.2754 +00	9.7194 +01	6.2708 +00	9.6831 +01	6.2565 +00	9.5739 +01

Table 5 - Continued

		PSI(DEGREES) = 4		PSI(DEGREES) = 5		PSI(DEGREES) = 7		PSI(DEGREES) = 10	
KB	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	
10	5.5131 -01	1.2527 +02	5.5204 -01	1.2470 +02	5.5401 -01	1.2316 +02	5.5816 -01	1.1990 +02	
15	1.0919 +00	1.2208 +02	1.0931 +00	1.2131 +02	1.0965 +00	1.1927 +02	1.1032 +00	1.1493 +02	
20	1.6158 +00	1.1894 +02	1.6173 +00	1.1799 +02	1.6208 +00	1.1544 +02	1.6270 +00	1.1004 +02	
25	2.1178 +00	1.1589 +02	2.1188 +00	1.1475 +02	2.1208 +00	1.1171 +02	2.1222 +00	1.0525 +02	
30	2.5932 +00	1.1294 +02	2.5930 +00	1.1161 +02	2.5915 +00	1.0808 +02	2.5825 +00	1.0660 +02	
35	3.0380 +00	1.1011 +02	3.0360 +00	1.0860 +02	3.0285 +00	1.0460 +02	3.0031 +00	9.6108 +01	
40	3.4494 +00	1.0742 +02	3.4446 +00	1.0574 +02	3.4288 +00	1.0128 +02	3.3804 +00	9.1809 +01	
45	3.8255 +00	1.0490 +02	3.8172 +00	1.0306 +02	3.7907 +00	9.8146 +01	3.7128 +00	8.7732 +01	
50	4.1658 +00	1.0256 +02	4.1531 +00	1.0056 +02	4.1134 +00	9.5222 +01	4.0002 +00	8.3906 +01	
55	4.4705 +00	1.0043 +02	4.4530 +00	9.8274 +01	4.3982 +00	9.2530 +01	4.2443 +00	8.0355 +01	
60	4.7146 +00	9.8520 +01	4.7186 +00	9.6218 +01	4.6473 +00	9.0088 +01	4.4486 +00	7.7102 +01	
65	4.9817 +00	9.6843 +01	4.9531 +00	9.4404 +01	4.8644 +00	8.7909 +01	4.6180 +00	7.4161 +01	
70	5.1949 +00	9.5408 +01	5.1606 +00	9.2840 +01	5.0541 +00	8.6000 +01	4.7585 +00	7.1536 +01	
75	5.3856 +00	9.4217 +01	5.3458 +00	9.1525 +01	5.2219 +00	8.4359 +01	4.8771 +00	6.9220 +01	
80	5.5593 +00	9.3262 +01	5.5144 +00	9.0453 +01	5.3740 +00	8.2974 +01	4.9809 +00	6.7190 +01	
85	5.7214 +00	9.2529 +01	5.6721 +00	8.9605 +01	5.6165 +00	8.1821 +01	5.0765 +00	6.5409 +01	
90	5.8774 +00	9.1993 +01	5.8244 +00	8.8954 +01	5.6550 +00	8.0866 +01	5.1698 +00	6.3825 +01	
95	6.0324 +00	9.1620 +01	5.9763 +00	8.8466 +01	5.7946 +00	8.0067 +01	5.2649 +00	6.2377 +01	
100	6.1904 +00	9.1373 +00	6.1318 +00	8.8098 +01	5.9388 +00	7.9375 +01	5.3642 +00	6.1002 +01	

PSI(0EGREES) = 12		PSI(0EGREES) = 13		PSI(0EGREES) = 14		PSI(0EGREES) = 15		
KB	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)
10	5.6174 -01	1.1710 +02	5.6377 -01	1.1551 +02	5.6456 -01	1.1380 +02	5.6831 -01	1.1196 +02
15	1.1087 +00	1.1120 +02	1.1116 +00	1.0909 +02	1.1147 +00	1.0681 +02	1.1178 +00	1.0436 +02
20	1.6310 +00	1.0539 +02	1.6328 +00	1.0276 +02	1.6342 +00	9.9912 +01	1.6352 +00	9.6861 +01
25	2.1201 +00	9.9699 +01	2.1176 +00	9.6548 +01	2.1138 +00	9.3149 +01	2.1085 +00	8.9504 +01
30	2.5686 +00	9.4156 +01	2.5581 +00	9.0501 +01	2.5447 +00	8.6558 +01	2.5280 +00	8.2329 +01
35	2.9708 +00	8.8797 +01	2.9481 +00	8.4650 +01	2.9203 +00	8.0177 +01	2.8865 +00	7.5380 +01
40	3.3228 +00	8.3657 +01	3.2837 +00	7.9034 +01	3.2364 +00	7.4049 +01	3.1798 +00	6.8703 +01
45	3.6232 +00	7.8772 +01	3.5633 +00	7.3692 +01	3.4915 +00	6.8216 +01	3.4066 +00	6.2347 +01
50	3.8722 +00	7.4174 +01	3.7876 +00	6.8660 +01	3.6870 +00	6.2721 +01	3.5688 +00	5.6361 +01
55	4.0725 +00	6.9895 +01	3.9598 +00	6.3975 +01	3.8266 +00	5.7603 +01	3.6711 +00	5.0790 +01
60	4.2287 +00	6.5960 +01	4.0853 +00	5.9663 +01	5.9166 +00	5.2897 +01	3.7209 +00	4.5677 +01
65	4.3468 +00	6.2386 +01	4.1709 +00	5.5745 +01	3.9650 +00	4.8623 +01	3.7272 +00	4.1047 +01
70	4.4344 +00	5.9176 +01	4.2250 +00	5.2222 +01	3.9809 +00	4.4788 +01	3.7005 +00	3.6911 +01
75	4.4994 +00	5.6316 +01	4.2562 +00	4.9081 +01	3.9737 +00	4.1372 +01	3.6510 +00	3.3249 +01
80	4.5498 +00	5.3775 +01	4.2728 +00	4.6281 +01	3.9522 +00	3.8331 +01	3.5879 +00	3.0012 +01
85	4.5924 +00	5.1500 +01	4.2818 +00	4.3761 +01	3.9243 +00	3.5593 +01	3.5182 +00	2.7118 +01
90	4.6326 +00	4.9423 +01	4.2882 +00	4.1444 +01	3.8919 +00	3.3069 +01	3.4460 +00	2.4463 +01
95	4.6737 +00	4.7466 +01	4.2946 +00	3.9241 +01	3.8593 +00	3.0659 +01	3.3720 +00	2.1939 +01
100	4.7166 +00	4.5552 +01	4.3008 +00	3.7068 +01	3.8244 +00	2.8273 +01	3.2938 +00	1.9451 +01

PSI(0EGREES) = 16		PSI(0EGREES) = 17		PSI(0EGREES) = 18		PSI(0EGREES) = 19		
KB	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)
10	5.7081 -01	1.1000 +02	5.7347 -01	1.0791 +02	5.7628 -01	1.0570 +02	5.7925 -01	1.0337 +02
15	1.1211 +00	1.0175 +02	1.1243 +00	9.8969 +01	1.1275 +00	9.6029 +01	1.1307 +00	9.2927 +01
20	1.6356 +00	9.3600 +01	1.6354 +00	9.0143 +01	1.6344 +00	8.6478 +01	1.6325 +00	8.2610 +01
25	2.1013 +00	8.5612 +01	2.0921 +00	8.1475 +01	2.0805 +00	7.7095 +01	2.0663 +00	7.2473 +01
30	2.5074 +00	7.7814 +01	2.4825 +00	7.3016 +01	2.4527 +00	6.7936 +01	2.4176 +00	6.2576 +01
35	2.8461 +00	7.0260 +01	2.7982 +00	6.4819 +01	2.7421 +00	5.9060 +01	2.6771 +00	5.2985 +01
40	3.1130 +00	6.3000 +01	3.0348 +00	5.6942 +01	2.9445 +00	5.0534 +01	2.8410 +00	4.3379 +01
45	3.3072 +00	5.6090 +01	3.1922 +00	4.9450 +01	3.0604 +00	4.2433 +01	2.9110 +00	3.5049 +01
50	3.4315 +00	4.9588 +01	3.2739 +00	3.4241 +01	3.0950 +00	3.4843 +01	2.8941 +00	2.6902 +01
55	3.4917 +00	4.3549 +01	3.2874 +00	3.5895 +01	3.0575 +00	2.7855 +01	2.8021 +00	1.9464 +01
60	3.4966 +00	3.8024 +01	3.2431 +00	2.9972 +01	2.9605 +00	2.1565 +01	2.6501 +00	1.2876 +01
65	3.4567 +00	3.3053 +01	3.1534 +00	2.4697 +01	2.8187 +00	1.6063 +01	2.4558 +00	7.2944 +00
70	3.3837 +00	2.8653 +01	3.0316 +00	2.0105 +01	2.6476 +00	1.4243 +01	2.2373 +00	2.4309 +00
75	3.2889 +00	2.4807 +01	2.8904 +00	1.6197 +01	2.4614 +00	7.6822 +00	2.0115 +00	-2.4309 +01
80	3.1822 +00	2.1465 +01	2.7404 +00	1.2927 +01	2.2719 +00	4.8329 +00	1.7922 +00	-1.9519 +00
85	3.0705 +00	1.8537 +01	2.5886 +00	1.0209 +01	2.0867 +00	2.8022 +00	1.5890 +00	-2.1821 +00
90	2.9573 +00	1.5908 +01	2.4380 +00	7.9283 +00	1.9089 +00	1.5732 +00	1.4067 +00	-8.6112 -01
95	2.8423 +00	1.3466 +01	2.2877 +00	5.9864 +00	1.7377 +00	1.0686 +00	1.2477 +00	2.1743 +00
100	2.7225 +00	1.1123 +01	2.1341 +00	4.3411 +00	1.5709 +00	1.4187 +00	1.1157 +00	7.2494 +00

PSI(0EGREES) = 20		PSI(0EGREES) = 20.5		PSI(0EGREES) = 21		PSI(0EGREES) = 22		
KB	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)
10	5.8237 -01	1.0092 +02	5.8734 -01	9.7016 +01	5.8565 -01	9.8347 +01	5.8907 -01	9.5655 +01
15	1.1337 +00	8.9663 +01	1.1381 +00	8.4466 +01	1.1367 +00	8.6238 +01	1.1394 +00	8.2654 +01
20	1.6295 +00	7.8541 +01	1.6227 +00	7.2062 +01	1.6253 +00	7.4271 +01	1.6197 +00	6.9803 +01
25	2.0490 +00	6.7611 +01	2.0168 +00	5.9869 +01	2.0285 +00	6.2509 +01	2.0043 +00	5.7169 +01
30	2.3766 +00	5.6938 +01	2.3029 +00	4.7963 +01	2.3292 +00	5.1023 +01	2.2749 +00	4.4834 +01
35	2.6025 +00	4.6598 +01	2.4712 +00	3.6438 +01	2.5176 +00	3.9901 +01	2.4220 +00	3.2899 +01
40	2.7237 +00	3.6683 +01	2.5204 +00	2.5417 +01	2.5919 +00	2.9254 +01	2.4453 +00	2.1499 +01
45	2.7435 +00	2.7308 +01	2.4577 +00	1.5063 +01	2.5575 +00	1.9225 +01	2.3534 +00	1.0823 +01
50	2.6714 +00	1.8612 +01	2.2976 +00	5.6057 +00	2.4273 +00	1.0009 +01	2.1521 +00	1.1473 +00
55	2.5222 +00	1.0775 +01	2.0610 +00	-2.6150 +00	2.2197 +00	1.8734 +00	1.8979 +00	-7.0944 +00
60	2.3146 +00	4.0221 +00	1.7739 +00	-9.0766 +00	1.9581 +00	-4.7934 +00	1.5870 +00	-1.43178 +01
65	2.0699 +00	-1.3610 +00	1.4661 +00	-1.2937 +01	1.6687 +00	-9.4197 +00	1.2648 +00	-1.5825 +01
70	1.8100 +00	-5.0232 +00	1.1717 +00	-1.2838 +01	1.3802 +00	-1.1160 +01	9.7384 -01	-1.2811 +01
75	1.5564 +00	-6.5523 +00	9.3078 -01	-6.9048 +00	1.2133 +00	-8.8547 +00	7.7032 -01	-1.4311 +00
80	1.3277 +00	-5.5115 +00	7.8879 -01	5.7418 +00	9.3029 -01	-1.4188 +00	7.1125 -01	1.6515 +01
85	1.1394 +00	-1.5407 +00	7.7278 -01	2.1306 +00	8.3017 -01	1.0502 +01	7.9111 -01	3.1720 +01
90	1.0034 +00	5.4352 +00	8.5901 -01	3.3448 +01	8.3093 -01	2.3869 +01	9.4297 -01	3.9770 +01
95	9.2831 -01	1.4881 +01	9.9961 -01	4.0319 +01	9.1131 -01	3.4339 +01	1.1159 +00	4.2651 +01
100	9.1945 -01	2.5400 +01	1.1626 +00	4.3220 +01	1.0412 +00	4.0892 +01	1.2885 +00	4.2555 +01

Table 5 - Continued

PSI(DEGREES) = 23		PSI(0EGREES) = 24		PSI(DEGREFS) = 25	
KB	G(B)	PHASE(DEGREES)	G(B)	PHASE(DEGREES)	G(B)
10	5.9265 -01	9.2845 +01	5.9637 -01	8.9916 +01	6.0024 -01
15	1.1419 +00	7.8911 +01	1.1442 +00	7.5012 +01	1.1461 +00
20	1.6126 +00	6.5137 +01	1.6037 +00	6.0275 +01	1.5930 +00
25	1.9761 +00	5.1594 +01	1.9437 +00	4.5785 +01	1.9067 +00
30	2.2133 +00	3.8374 +01	2.1439 +00	3.1645 +01	2.0664 +00
35	2.3151 +00	2.5597 +01	2.1967 +00	1.8000 +01	2.0666 +00
40	2.2837 +00	1.3431 +01	2.1075 +00	5.0639 +00	1.9170 +00
45	2.1317 +00	2.1315 +00	1.8938 +00	-6.8017 +00	1.6415 +00
50	1.8810 +00	-7.8830 +00	1.5842 +00	-1.6925 +01	1.2770 +00
55	1.5614 +00	-1.5858 +01	1.2170 +00	-2.3854 +01	8.4745 -01
60	1.2109 +00	-2.0280 +01	8.4556 -01	-2.3905 +01	5.2800 -01
65	8.7998 -01	-1.7876 +01	5.6658 -01	-7.9265 +00	4.6265 -01
70	6.5030 -01	-3.0203 +00	5.4550 -01	2.4033 +01	7.0159 -01
75	6.2369 -01	2.1432 +01	7.4820 -01	4.0900 +01	9.8267 -01
80	7.7255 -01	3.7315 +01	9.9282 -01	4.3413 +01	1.2162 +00
85	9.7660 -01	4.2374 +01	1.2081 +00	4.0514 +01	1.3839 +00
90	1.1743 +00	4.2076 +01	1.3775 +00	3.5674 +01	1.4868 +00
95	1.3476 +00	3.9387 +01	1.5008 +00	3.0124 +01	1.5323 +00
100	1.4931 +00	3.5499 +01	1.5614 +00	2.4280 +01	1.5275 +00

Table 6

KA=5 DELTA(DEGREES)=25					
PSI(DEGREES) = 0		PSI(DEGREES) = 1		PSI(DEGREES) = 2	
KB	G(B)	PHASE(DEGREES)	G(B)	PHASE(DEGREES)	G(B)
10	6.7759 -01	1.2145 +02	6.7770 -01	1.2139 +02	6.7800 -01
15	1.3242 +00	1.1712 +02	1.3244 +00	1.1704 +02	1.3249 +00
20	1.9249 +00	1.1300 +02	1.9251 +00	1.1290 +02	1.9256 +00
25	2.4680 +00	1.0918 +02	2.4681 +00	1.0905 +02	2.4684 +00
30	2.9461 +00	1.0572 +02	2.9460 +00	1.0558 +02	2.9457 +00
35	3.3565 +00	1.0271 +02	3.3562 +00	1.0255 +02	3.3552 +00
40	3.7021 +00	1.0020 +02	3.7015 +00	1.0003 +02	3.6996 +00
45	3.9907 +00	9.8257 +01	3.9898 +00	9.8066 +01	3.9869 +00
50	4.2344 +00	9.6884 +01	4.2331 +00	9.6679 +01	4.2294 +00
55	4.4482 +00	9.6061 +01	4.4468 +00	9.5843 +01	4.4425 +00
60	4.6481 +00	9.5714 +01	4.6466 +00	9.5482 +01	4.6420 +00
65	4.8484 +00	9.5722 +01	4.8470 +00	9.5477 +01	4.8423 +00
70	5.0594 +00	9.5935 +01	5.0580 +00	9.5675 +01	5.0537 +00
75	5.2859 +00	9.6202 +01	5.2847 +00	9.5926 +01	5.2807 +00
80	5.5270 +00	9.6397 +01	5.4529 +00	9.6105 +01	5.5223 +00
85	5.7774 +00	9.6444 +01	5.7764 +00	9.6134 +01	5.7728 +00
90	6.0290 +00	9.6316 +01	6.0278 +00	9.5987 +01	6.0240 +00
95	6.2730 +00	9.6030 +01	6.2718 +00	9.5683 +01	6.2673 +00
100	6.5024 +00	9.5636 +01	6.5008 +00	9.5271 +01	6.4953 +00

PSI(DEGREES) = 4		PSI(DEGREES) = 5		PSI(DEGREES) = 7		PSI(DEGREES) = 10	
KB	G(B)	PHASE(DEGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(DEGREES)	G(B)
10	6.7922 -01	1.2044 +02	6.8013 -01	1.1987 +02	6.8256 -01	1.1836 +02	6.8772 -01
15	1.3269 +00	1.1578 +02	1.3284 +00	1.1502 +02	1.3323 +00	1.1301 +02	1.3401 +00
20	1.9276 +00	1.1133 +02	1.9290 +00	1.1040 +02	1.9325 +00	1.0790 +02	1.9384 +00
25	2.4693 +00	1.0720 +02	2.4698 +00	1.0608 +02	2.4704 +00	1.0312 +02	2.4684 +00
30	2.9444 +00	1.0344 +02	2.9431 +00	1.0216 +02	2.9384 +00	9.8747 +01	2.9218 +00
35	3.3507 +00	1.0105 +02	3.3468 +00	9.8710 +01	3.3343 +00	9.4877 +01	3.2971 +00
40	3.6912 +00	9.7385 +01	3.6842 +00	9.5800 +01	3.6621 +00	9.1576 +01	3.5997 +00
45	3.9744 +00	9.5198 +01	3.9640 +00	9.3477 +01	3.9316 +00	8.8893 +01	3.8414 +00
50	4.2132 +00	9.3602 +01	4.1996 +00	9.1756 +01	4.1573 +00	8.6837 +01	4.0390 +00
55	4.4233 +00	9.2567 +01	4.4071 +00	9.0603 +01	4.3562 +00	8.5366 +01	4.2117 +00
60	4.6212 +00	9.2011 +01	4.6032 +00	8.9928 +01	4.5456 +00	8.4375 +01	4.3775 +00
65	4.8211 +00	9.1802 +01	4.8022 +00	8.9596 +01	4.7397 +00	8.3712 +01	4.5497 +00
70	5.0329 +00	9.1780 +01	5.0136 +00	8.9441 +01	4.9471 +00	8.3200 +01	4.7347 +00
75	5.2606 +00	9.1791 +01	5.2410 +00	8.9306 +01	5.1700 +00	8.2674 +01	4.9313 +00
80	5.5024 +00	9.1710 +01	5.4820 +00	8.9069 +01	5.4045 +00	8.2017 +01	5.1322 +00
85	5.7521 +00	9.1466 +01	5.7299 +00	8.8661 +01	5.6425 +00	8.1172 +01	5.3268 +00
90	6.0009 +00	9.1043 +01	5.9755 +00	8.8071 +01	5.8744 +00	8.0141 +01	5.5048 +00
95	6.2401 +00	9.0466 +01	6.2102 +00	8.7331 +01	6.0912 +00	7.8968 +01	5.6580 +00
100	6.4627 +00	8.9791 +01	6.4272 +00	8.6500 +01	6.2871 +00	7.7725 +01	5.7824 +00

PSI(DEGREES) = 12		PSI(0EGREES) = 14		PSI(DEGREES) = 15		PSI(DEGREES) = 16	
KB	G(B)	PHASE(DEGREES)	G(B)	PHASE(DEGREES)	G(B)	PHASE(DEGREES)	G(B)
10	6.9216 -01	1.1237 +02	6.9739 -01	1.0911 +02	7.0030 -01	1.0729 +02	7.0340 -01
15	1.3464 +00	1.0506 +02	1.3534 +00	1.0072 +02	1.3571 +00	9.8311 +01	1.3608 +00
20	1.9419 +00	9.8033 +01	1.9442 +00	9.2651 +01	1.9445 +00	8.9655 +01	1.9442 +00
25	2.4629 +00	9.1399 +01	2.4520 +00	8.5004 +01	2.4438 +00	8.1444 +01	2.4333 +00
30	2.9006 +00	8.5266 +01	2.8672 +00	7.7910 +01	2.8448 +00	7.3815 +01	2.8178 +00
35	3.2538 +00	7.9737 +01	3.1893 +00	7.1480 +01	3.1473 +00	6.6885 +01	3.0977 +00
40	3.5292 +00	7.4900 +01	3.4267 +00	6.5815 +01	3.3608 +00	6.0764 +01	3.2838 +00
45	3.7407 +00	7.0806 +01	3.5957 +00	6.0970 +01	3.5033 +00	5.5511 +01	3.3958 +00
50	3.9071 +00	6.7448 +01	3.7177 +00	5.6929 +01	3.5973 +00	5.1106 +01	3.4580 +00
55	4.0491 +00	6.4739 +01	3.8149 +00	5.3581 +01	3.6663 +00	4.7424 +01	3.4946 +00
60	4.1849 +00	6.2513 +01	3.9057 +00	5.0719 +01	3.7282 +00	4.4233 +01	3.5234 +00
65	4.3269 +00	6.0546 +01	4.0002 +00	4.8081 +01	3.7920 +00	4.1248 +01	3.5518 +00
70	4.4786 +00	5.8615 +01	4.0988 +00	4.5417 +01	3.8559 +00	3.8208 +01	3.5758 +00
75	4.6358 +00	5.6546 +01	4.1933 +00	4.2559 +01	3.9098 +00	3.4949 +01	3.5837 +00
80	4.7884 +00	5.4252 +01	4.2712 +00	3.9444 +01	3.9403 +00	3.1432 +01	3.5611 +00
85	4.9245 +00	5.1729 +01	4.3197 +00	3.6115 +01	3.9348 +00	2.7727 +01	3.4967 +00
90	5.0336 +00	4.9044 +01	4.3299 +00	3.2682 +01	3.8860 +00	2.3980 +01	3.3855 +00
95	5.1093 +00	4.6299 +01	4.2986 +00	2.9289 +01	3.7933 +00	2.0374 +01	3.2303 +00
100	5.1503 +00	4.3604 +01	4.2286 +00	2.6085 +01	3.6625 +00	1.7088 +01	3.0412 +00

2.8329 +00 6.2379 +00

Table 6 - Continued

KB	PSI(0EGREES) = 17.		PSI(0EGREES) = 18.		PSI(0EGREES) = 18.5		PSI(0EGREES) = 19	
	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)
10	7.0670 -01	1.0329 +02	7.1019 -01	1.0111 +02	7.1201 -01	9.9973 +01	7.1388 -01	9.8807 +01
15	1.3645 +00	9.2998 +01	1.3682 +00	9.0099 +01	1.3700 +00	8.8589 +01	1.3718 +00	8.7040 +01
20	1.9430 +00	8.3057 +01	1.9408 +00	7.9457 +01	1.9393 +00	7.7582 +01	1.9375 +00	7.5657 +01
25	2.4204 +00	7.3608 +01	2.4046 +00	6.9331 +01	2.3955 +00	6.7104 +01	2.3855 +00	6.4817 +01
30	2.7857 +00	6.4799 +01	2.7479 +00	5.9881 +01	2.7268 +00	5.7321 +01	2.7040 +00	5.4693 +01
35	3.0397 +00	5.6777 +01	2.9725 +00	5.1269 +01	2.9352 +00	4.8404 +01	2.8954 +00	4.5465 +01
40	3.1947 +00	4.9671 +01	3.0924 +00	4.3640 +01	3.0360 +00	4.0507 +01	2.9760 +00	3.7298 +01
45	3.2721 +00	4.3555 +01	3.1313 +00	3.7081 +01	3.0542 +00	3.3728 +01	2.9725 +00	3.0300 +01
50	3.2984 +00	3.8406 +01	3.1178 +00	3.1573 +01	3.0195 +00	2.8050 +01	2.9157 +00	2.4463 +01
55	3.2987 +00	3.4067 +01	3.0782 +00	2.6944 +01	2.5988 +00	2.3296 +01	2.8333 +00	1.9604 +01
60	3.2904 +00	3.0254 +01	3.0295 +00	2.2881 +01	2.8890 +00	1.9139 +01	2.7421 +00	1.5384 +01
65	3.2793 +00	2.6628 +01	2.9757 +00	1.9019 +01	2.8130 +00	1.5201 +01	2.6438 +00	1.1413 +01
70	3.2591 +00	2.2908 +01	2.9083 +00	1.5073 +01	2.7216 +00	1.1202 +01	2.5285 +00	7.4205 +00
75	3.2165 +00	1.8960 +01	2.8129 +00	1.0946 +01	2.5999 +00	7.0752 +00	2.3814 +00	3.3881 +00
80	3.1372 +00	1.4820 +01	2.6762 +00	6.7559 +00	2.4357 +00	3.0048 +00	2.1916 +00	-4.0456 -01
85	3.0117 +00	1.0673 +01	2.4921 +00	2.8174 +00	2.2254 +00	-5.8290 -01	1.9590 +00	-3.3611 +00
90	2.8388 +00	6.8118 +00	2.2649 +00	-3.8226 -01	1.9775 +00	-3.0196 +00	1.6976 +00	-4.5251 +00
95	2.6261 +00	3.6006 +00	2.0102 +00	-2.1955 +00	1.7133 +00	-3.4380 +00	1.4380 +00	-2.5444 +00
100	2.3894 +00	1.4365 +00	1.7532 +00	-1.8500 +00	1.4670 +00	-5.6168 -01	1.2269 +00	3.9796 +00

KB	PSI(0EGREES) = 20		PSI(0EGREES) = 21		PSI(0EGREES) = 21.5		PSI(0EGREES) = 22	
	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)
10	7.1775 -01	9.6384 +01	7.2182 -01	9.3843 +01	7.4239 -01	9.2528 +01	7.2607 -01	9.1184 +01
15	1.3753 +00	8.3821 +01	1.3786 +00	8.0444 +01	1.3801 +00	7.8696 +01	1.3816 +00	7.6910 +01
20	1.9328 +00	7.1659 +01	1.9267 +00	6.7464 +01	1.9229 +00	6.5293 +01	1.9188 +00	6.3073 +01
25	2.3629 +00	6.0068 +01	2.3363 +00	5.5084 +01	2.3215 +00	5.2507 +01	2.3055 +00	4.9871 +01
30	2.6532 +00	4.9237 +01	2.5951 +00	4.3516 +01	2.5631 +00	4.0557 +01	2.5291 +00	3.7533 +01
35	2.8076 +00	3.9368 +01	2.7085 +00	3.2985 +01	2.6546 +00	2.9689 +01	2.5976 +00	2.6324 +01
40	2.8450 +00	3.0655 +01	2.6988 +00	2.3727 +01	2.6199 +00	2.0161 +01	2.5371 +00	1.6533 +01
45	2.7953 +00	2.3237 +01	2.5996 +00	1.5927 +01	2.4950 +00	1.2194 +01	2.3860 +00	8.4198 +00
50	2.6923 +00	1.7127 +01	2.4485 +00	9.6424 +00	2.3195 +00	5.8783 +00	2.1862 +00	2.1253 +00
55	2.5654 +00	1.2145 +01	2.2768 +00	4.7170 +00	2.1261 +00	1.0861 +00	1.9718 +00	-2.4333 +00
60	2.4309 +00	7.9300 +00	2.1010 +00	7.9395 -01	1.9314 +00	-2.5180 +00	1.7603 +00	-5.5472 +00
65	2.2892 +00	4.0841 +00	1.9203 +00	-2.4904 +00	1.7345 +00	-5.2463 +00	1.5509 +00	-7.4358 +00
70	2.1287 +00	3.9437 -01	1.7231 +00	-5.1862 +00	1.5250 +00	-6.9835 +00	1.3355 +00	-7.7265 +00
75	1.9361 +00	-2.9816 +00	1.5005 +00	-6.7078 +00	1.2985 +00	-6.7468 +00	1.1172 +00	-4.8753 +00
80	1.7060 +00	-5.3945 +00	1.2599 +00	-5.5236 +00	1.0744 +00	-2.2876 +00	9.3348 -01	3.9800 +00
85	1.4498 +00	-5.5603 +00	1.0394 +00	1.0362 +00	9.1373 -01	9.2931 +00	8.6653 -01	1.9805 +01
90	1.2027 +00	-1.4241 +00	9.1761 -01	1.4918 +01	9.0574 -01	2.6100 +01	9.7588 -01	3.4984 +01
95	1.0288 +00	9.0156 +00	9.6757 -01	3.1010 +01	1.0671 +00	3.8687 +01	1.2093 +00	4.2149 +01
100	9.9877 -01	2.3768 +01	1.1605 +00	4.0304 +01	1.3155 +00	4.3252 +01	1.4761 +00	4.2503 +01

KB	PSI(0EGREES) = 23		PSI(0EGREES) = 24		PSI(0EGREES) = 25	
	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)
10	7.3051 -01	8.8407 +01	7.3514 -01	8.5513 +01	7.3995 -01	8.2503 +01
15	1.3844 +00	7.3218 +01	1.3869 +00	6.9372 +01	1.3889 +00	6.5371 +01
20	1.9091 +00	5.8488 +01	1.8972 +00	5.3709 +01	1.8832 +00	4.8739 +01
25	2.2699 +00	4.4427 +01	2.2293 +00	3.8754 +01	2.1834 +00	3.2856 +01
30	2.4548 +00	3.1292 +01	2.3716 +00	2.4797 +01	2.2794 +00	1.8054 +01
35	2.4745 +00	1.9395 +01	2.3388 +00	1.2210 +01	2.1906 +00	4.7870 +00
40	2.3599 +00	9.1017 +00	2.1677 +00	1.4718 +00	1.9612 +00	-6.2993 +00
45	2.1553 +00	7.9103 -01	1.9095 +00	-0.8432 +00	1.6512 +00	-1.4291 +01
50	1.9081 +00	-5.2361 +00	1.6190 +00	-1.2121 +01	1.3255 +00	-1.7943 +01
55	1.6567 +00	-8.8791 +00	1.3414 +00	-1.3833 +01	1.0422 +00	-1.5764 +01
60	1.4211 +00	-1.0216 +01	1.1038 +00	-1.1541 +01	8.4547 -01	-6.6279 +00
65	1.2040 +00	-9.0796 +00	9.2027 -01	-4.5169 +00	7.6686 -01	8.3409 +00
70	1.0083 +00	-4.2702 +00	8.1570 -01	8.1140 +00	8.2149 +01	2.3665 +01
75	8.6552 -01	6.5326 +00	8.3667 -01	2.3806 +00	9.9112 -01	3.3214 +01
80	8.4642 -01	2.4722 +01	9.9727 -01	3.5139 +01	1.2276 +00	3.5666 +01
85	9.9074 -01	3.6036 +01	1.2441 +00	3.8728 +01	1.4748 +00	3.2770 +01
90	1.2391 +00	4.1117 +01	1.5062 +00	3.6449 +01	1.6813 +00	2.6540 +01
95	1.5090 +00	3.9849 +01	1.7276 +00	3.0771 +01	1.8076 +00	1.8527 +01
100	1.7422 +00	3.5085 +01	1.8718 +00	2.3425 +01	1.8317 +00	9.9188 +00
			1.9218 +00	1.5585 +01		

KB	PSI(0EGREES) = 0		PSI(0EGREES) = 1		PSI(0EGREES) = 2		PSI(0EGREES) = 3	
	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)
10	7.6723 -01	7.9230 +01	7.6750 -01	7.9168 +01	7.6829 -01	7.8982 +01	7.6961 -01	7.8672 +01
15	1.2894 +00	8.7186 +01	1.2898 +00	8.7103 +01	1.2910 +00	8.6853 +01	1.2929 +00	8.6437 +01
20	1.8110 +00	8.6549 +01	1.8116 +00	8.6448 +01	1.8132 +00	8.6145 +01	1.8159 +00	8.5640 +01
25	2.1874 +00	8.7702 +01	2.1881 +00	8.7583 +01	2.1900 +00	8.7224 +01	2.1933 +00	8.6626 +01
30	2.6073 +00	8.8007 +01	2.6081 +00	8.7870 +01	2.6105 +00	8.7459 +01	2.6143 +00	8.6775 +01
35	2.9259 +00	8.8023 +01	2.9268 +00	8.7869 +01	2.9294 +00	8.7405 +01	2.9337 +00	8.6632 +01
40	3.2732 +00	8.8561 +01	3.2742 +00	8.8389 +01	3.2771 +00	8.7874 +01	3.2818 +00	8.7016 +01
45	3.5681 +00	8.8315 +01	3.5692 +00	8.8126 +01	3.5724 +00	8.7560 +01	3.5775 +00	8.6616 +01
50	3.8588 +00	8.8780 +01	3.8600 +00	8.8574 +01	3.8634 +00	8.7957 +01	3.8688 +00	8.6929 +01
55	4.1410 +00	8.8591 +01	4.1422 +00	8.8369 +01	4.1459 +00	8.7701 +01	4.1516 +00	8.6589 +01
60	4.3914 +00	8.8858 +01	4.3927 +00	8.8619 +01	4.3966 +00	8.7901 +01	4.4026 +00	8.6706 +01
65	4.6594 +00	8.8829 +01	4.6608 +00	8.8573 +01	4.6649 +00	8.7805 +01	4.6711 +00	8.6527 +01
70	4.8861 +00	8.8895 +01	4.8876 +00	8.8623 +01	4.8919 +00	8.7806 +01	4.8982 +00	8.6445 +01
75	5.1344 +00	8.9003 +01	5.1360 +00	8.8714 +01	5.1405 +00	8.7848 +01	5.1469 +00	8.6405 +01
80	5.3507 +00	8.8943 +01	5.3524 +00	8.8638 +01	5.3570 +00	8.7723 +01	5.3635 +00	8.6198 +01
85	5.5758 +00	8.9108 +01	5.5775 +00	8.8787 +01	5.5823 +00	8.7822 +01	5.5888 +00	8.6216 +01
90	5.7887 +00	8.9018 +01	5.7905 +00	8.8681 +01	5.7954 +00	8.7667 +01	5.8019 +00	8.5979 +01
95	5.9918 +00	8.9157 +01	5.9937 +00	8.8803 +01	5.9987 +00	8.7741 +01	6.0051 +00	8.5972 +01
100	6.2016 +00	8.9110 +01	6.2035 +00	8.8740 +01	6.2086 +00	8.7630 +01	6.2149 +00	8.5779 +01

Table 7 - Continued

	PSI(0EGREES) = 4	PSI(0EGREES) = 5	PSI(0EGREES) = 7	PSI(0EGREES) = 10
KB	G(B) PHASE(0EGREES)	G(B) PHASE(0EGREES)	G(B) PHASE(0EGREES)	G(B) PHASE(0EGREES)
10	7.7145 -01 7.8239 +01	7.7383 -01 7.7683 +01	7.8019 -01 7.6201 +01	7.9377 -01 7.3065 +01
15	1.2956 +00 8.5854 +01	1.2990 +00 8.5105 +01	1.3082 +00 8.3112 +01	1.3273 +00 7.8893 +01
20	1.8197 +00 8.4934 +01	1.8246 +00 8.4026 +01	1.8372 +00 8.1609 +01	1.8629 +00 7.6691 +01
25	2.1978 +00 8.5789 +01	2.2034 +00 8.4715 +01	2.2179 +00 8.1853 +01	2.2457 +00 7.5795 +01
30	2.6195 +00 8.5817 +01	2.6260 +00 8.4586 +01	2.6422 +00 8.1310 +01	2.6707 +00 7.4375 +01
35	2.9395 +00 8.5551 +01	2.9466 +00 8.4162 +01	2.9635 +00 8.0465 +01	2.9897 +00 7.2640 +01
40	3.2881 +00 8.5815 +01	3.2956 +00 8.4272 +01	3.3126 +00 8.0166 +01	3.3337 +00 7.1479 +01
45	3.5842 +00 8.5296 +01	3.5920 +00 8.3600 +01	3.6084 +00 7.9086 +01	3.6217 +00 6.9537 +01
50	3.8758 +00 8.5491 +01	3.8836 +00 8.3643 +01	3.8985 +00 7.8725 +01	3.9004 +00 6.8330 +01
55	4.1588 +00 8.5034 +01	4.1666 +00 8.3035 +01	4.1792 +00 7.7717 +01	4.1669 +00 6.6479 +01
60	4.4098 +00 8.5033 +01	4.4172 +00 8.2885 +01	4.4267 +00 7.7169 +01	4.3961 +00 6.5101 +01
65	4.6784 +00 8.4739 +01	4.6853 +00 8.2441 +01	4.6908 +00 7.6329 +01	4.6388 +00 6.3434 +01
70	4.9053 +00 8.4941 +01	4.9116 +00 8.2095 +01	4.9119 +00 7.5591 +01	4.8344 +00 6.1878 +01
75	5.1539 +00 8.4386 +01	5.1592 +00 8.1793 +01	5.1537 +00 7.4897 +01	5.0470 +00 6.0374 +01
80	5.3701 +00 8.4064 +01	5.3743 +00 8.1324 +01	5.3618 +00 7.4039 +01	5.2216 +00 5.8711 +01
85	5.5950 +00 8.3968 +01	5.5979 +00 8.1082 +01	5.5774 +00 7.3410 +01	5.4000 +00 5.7290 +01
90	5.8075 +00 8.3618 +01	5.8087 +00 8.0586 +01	5.7792 +00 7.2527 +01	5.5599 +00 5.5614 +01
95	6.0101 +00 8.3497 +01	6.0096 +00 8.0320 +01	5.9699 +00 7.1879 +01	5.7049 +00 5.4192 +01
100	6.2191 +00 8.3192 +01	6.2165 +00 7.9869 +01	6.1655 +00 7.1045 +01	5.8501 +00 5.2578 +01

	PSI(0EGREES) = 15	PSI(0EGREES) = 16	PSI(0EGREES) = 17	PSI(0EGREES) = 20
KB	G(B) PHASE(0EGREES)	G(B) PHASE(0EGREES)	G(B) PHASE(0EGREES)	G(B) PHASE(0EGREES)
10	8.2746 -01 6.5447 +01	8.3590 -01 6.3572 +01	8.4492 -01 6.1583 +01	8.7552 -01 5.4937 +01
15	1.3725 +00 6.8643 +01	1.3834 +00 6.6121 +01	1.3947 +00 6.3444 +01	1.4312 +00 5.4505 +01
20	1.9181 +00 6.4054 +01	1.9301 +00 6.0993 +01	1.9420 +00 5.7746 +01	1.9758 +00 4.6901 +01
25	2.2953 +00 6.1085 +01	2.3035 +00 5.7468 +01	2.3102 +00 5.3633 +01	2.3184 +00 4.0844 +01
30	2.7059 +00 5.7564 +01	2.7067 +00 5.3414 +01	2.7041 +00 4.9034 +01	2.6686 +00 3.4464 +01
35	2.9962 +00 5.3672 +01	2.9848 +00 4.9022 +01	2.9671 +00 4.4099 +01	2.8651 +00 2.7767 +01
40	3.2978 +00 5.0464 +01	3.2695 +00 4.5327 +01	3.2311 +00 3.9897 +01	3.0411 +00 2.1980 +01
45	3.5290 +00 4.6475 +01	3.4789 +00 4.0852 +01	3.4140 +00 3.4919 +01	3.1147 +00 1.5462 +01
50	3.7351 +00 4.3305 +01	3.6579 +00 3.7234 +01	3.5608 +00 3.0847 +01	3.1327 +00 1.0118 +01
55	3.9137 +00 3.9495 +01	3.8044 +00 3.2978 +01	3.6697 +00 2.6415 +01	3.0954 +00 4.2435 +00
60	4.0384 +00 3.6248 +01	3.8922 +00 2.9330 +01	3.7145 +00 2.2114 +01	2.9816 +00 -5.4068 -01
65	4.1608 +00 3.2733 +01	3.9731 +00 2.5430 +01	3.7478 +00 1.7856 +01	2.8475 +00 -5.2847 +00
70	4.2195 +00 2.9412 +01	3.9858 +00 2.1771 +01	3.7089 +00 1.3914 +01	2.6391 +00 -9.0631 +00
75	4.2802 +00 2.6209 +01	3.9970 +00 1.8272 +01	3.6658 +00 1.0201 +01	2.4334 +00 -1.1918 +01
80	4.2861 +00 2.2903 +01	3.9499 +00 1.4717 +01	3.5617 +00 5.5147 +00	2.1801 +00 -1.3670 +01
85	4.2828 +00 1.9977 +01	3.8919 +00 1.1626 +01	3.4470 +00 3.4375 +00	1.9511 +00 -1.3234 +01
90	4.2451 +00 1.6827 +01	3.7971 +00 8.3617 +00	3.2949 +00 2.9423 -01	1.7240 +00 -1.1066 +01
95	4.1819 +00 1.4138 +01	3.6773 +00 5.7013 +00	3.1221 +00 1.9876 +00	1.5590 +00 -5.4315 +00
100	4.1053 +00 1.1300 +01	3.5437 +00 2.9668 +00	2.9387 +00 4.1658 +00	1.4619 +00 1.7286 +00

	PSI(0EGREES) = 21	PSI(0EGREES) = 22	PSI(0EGREES) = 25
KB	G(B) PHASE(0EGREES)	G(B) PHASE(0EGREES)	G(B) PHASE(0EGREES)
10	8.8692 -01 5.2499 +01	8.9894 -01 4.9953 +01	9.3872 -01 4.1675 +01
15	1.4441 +00 5.1227 +01	1.4572 +00 4.4780 +01	1.4972 +00 3.6680 +01
20	1.9858 +00 4.2928 +01	1.9947 +00 3.8779 +01	2.0128 +00 2.5312 +01
25	2.3156 +00 3.6166 +01	2.3094 +00 3.1288 +01	2.2642 +00 1.5509 +01
30	2.6451 +00 2.9150 +01	2.6146 +00 2.4362 +01	2.4728 +00 5.8502 +00
35	2.8114 +00 2.1837 +01	2.7460 +00 1.5687 +01	2.4722 +00 -3.8727 +00
40	2.9486 +00 1.5524 +01	2.8396 +00 8.8698 +00	2.4084 +00 -1.1856 +01
45	2.9753 +00 8.5210 +00	2.8148 +00 1.4269 +00	2.2090 +00 -1.9916 +01
50	2.9406 +00 2.8558 +00	2.7237 +00 -4.4456 +00	1.9481 +00 -2.4776 +01
55	2.8460 +00 -3.2473 +00	2.5702 +00 -1.0590 +01	1.6452 +00 -2.8088 +01
60	2.6744 +00 -7.9532 +00	2.3432 +00 -1.4845 +01	1.3429 +00 -2.4869 +01
65	2.4845 +00 -1.2358 +01	2.1055 +00 -1.8311 +01	1.1445 +00 -1.6294 +01
70	2.2285 +00 -1.5195 +01	1.8205 +00 -1.9098 +01	1.1058 +00 -1.2668 +00
75	1.9903 +00 -1.6406 +01	1.5841 +00 -1.7010 +01	1.2584 +00 8.9076 +00
80	1.7284 +00 -1.5318 +01	1.3731 +00 -1.0801 +01	1.4924 +00 1.3715 +01
85	1.5333 +00 -1.0722 +01	1.2967 +00 -9.7764 -01	1.7514 +00 1.2355 +01
90	1.3897 +00 -3.3798 +00	1.3208 +00 9.2129 +00	1.9530 +00 8.8490 +00
95	1.3736 +00 6.4074 +00	1.4788 +00 1.6708 +01	2.1096 +00 3.3214 +00
100	1.4467 +00 1.4491 +01	1.6714 +00 1.9994 +01	2.1623 +00 -2.5758 +00

Table 8  
KA=5  
DELTA(0EGREES)=∞

	PSI(0EGREES) = 0	PSI(0EGREES) = 1	PSI(0EGREES) = 2	PSI(0EGREES) = 3
KB	G(B) PHASE(0EGREES)	G(B) PHASE(0EGREES)	G(B) PHASE(0EGREES)	G(B) PHASE(0EGREES)
10	7.3901 -01 9.0000 +01	7.3918 -01 8.9936 +01	7.3968 -01 8.9743 +01	7.4053 -01 8.9422 +01
15	1.3061 +00 9.0000 +01	1.3064 +00 8.9917 +01	1.3073 +00 8.9667 +01	1.3087 +00 8.9250 +01
20	1.7841 +00 9.0000 +01	2.2058 +00 8.9808 +01	1.7857 +00 8.9593 +01	1.7878 +00 8.9084 +01
25	2.2053 +00 9.0000 +01	2.5867 +00 8.9863 +01	2.2073 +00 8.9521 +01	2.2098 +00 8.8922 +01
30	2.5861 +00 9.0000 +01	1.7845 +00 8.9898 +01	2.5884 +00 8.9450 +01	2.5913 +00 8.8763 +01
35	2.9362 +00 9.0000 +01	2.9369 +00 8.9845 +01	2.9389 +00 8.9381 +01	2.9421 +00 8.8607 +01
40	3.2621 +00 9.0000 +01	3.2629 +00 8.9828 +01	3.2651 +00 8.9312 +01	3.2685 +00 8.8452 +01
45	3.5682 +00 9.0000 +01	3.5691 +00 8.9811 +01	3.5714 +00 8.9244 +01	3.5751 +00 8.8299 +01
50	3.8578 +00 9.0000 +01	3.8586 +00 8.9794 +01	3.8612 +00 8.9176 +01	3.8651 +00 8.8147 +01
55	4.1331 +00 9.0000 +01	4.1341 +00 8.9777 +01	4.1368 +00 8.9109 +01	4.1408 +00 8.7996 +01
60	4.3963 +00 9.0000 +01	4.3973 +00 8.9761 +01	4.4001 +00 8.9042 +01	4.4043 +00 8.7845 +01
65	4.6486 +00 9.0000 +01	4.6497 +00 8.9744 +01	4.6526 +00 8.8976 +01	4.6569 +00 8.7696 +01
70	4.8915 +00 9.0000 +01	4.8926 +00 8.9727 +01	4.8956 +00 8.8910 +01	4.8999 +00 8.7547 +01
75	5.1258 +00 9.0000 +01	5.1269 +00 8.9711 +01	5.1300 +00 8.8844 +01	5.1343 +00 8.7399 +01
80	5.3524 +00 9.0000 +01	5.3536 +00 8.9695 +01	5.3568 +00 8.8778 +01	5.3610 +00 8.7252 +01
85	5.5720 +00 9.0000 +01	5.5732 +00 8.9678 +01	5.5765 +00 8.8713 +01	5.5806 +00 8.7105 +01
90	5.7853 +00 9.0000 +01	5.7866 +00 8.9662 +01	5.7899 +00 8.8648 +01	5.7938 +00 8.6958 +01
95	5.9927 +00 9.0000 +01	5.9940 +00 8.9646 +01	5.9974 +00 8.8583 +01	6.0011 +00 8.6812 +01
100	6.1947 +00 9.0000 +01	6.1961 +00 8.9630 +01	6.1995 +00 8.8518 +01	6.2030 +00 8.6667 +01

Table 8 - Continued

	PSI(0EGREES) = 4		PSI(0EGREES) = 5		PSI(0EGREES) = 7		PSI(0EGREES) = 10	
KB	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)
10	7.4171 -01	8.8973 +01	7.4324 -01	8.8396 +01	7.4731 -01	8.6858 +01	7.5599 -01	8.3596 +01
15	1.3108 +00	8.8667 +01	1.3135 +00	8.7917 +01	1.3205 +00	8.5920 +01	1.3351 +00	8.1684 +01
20	1.7906 +00	8.8372 +01	1.7941 +00	8.7456 +01	1.8033 +00	8.5018 +01	1.8216 +00	7.9845 +01
25	2.0232 +00	8.8084 +01	2.0217 +00	8.7007 +01	2.0281 +00	8.4138 +01	2.0478 +00	7.8053 +01
30	2.5951 +00	8.7802 +01	2.5999 +00	8.6566 +01	2.6114 +00	8.3274 +01	2.6301 +00	7.6295 +01
35	2.9463 +00	8.7524 +01	2.9514 +00	8.6132 +01	2.9631 +00	8.2423 +01	2.9781 +00	7.4563 +01
40	3.2731 +00	8.7249 +01	3.2784 +00	8.5702 +01	3.2895 +00	8.1582 +01	3.2981 +00	7.2851 +01
45	3.5799 +00	8.6976 +01	3.5852 +00	8.5276 +01	3.5949 +00	8.0749 +01	3.5943 +00	7.1158 +01
50	3.8699 +00	8.6706 +01	3.8751 +00	8.4854 +01	3.8827 +00	7.9923 +01	3.8696 +00	6.9481 +01
55	4.1457 +00	8.6437 +01	4.1505 +00	8.4435 +01	4.1552 +00	7.9102 +01	4.1263 +00	6.7818 +01
60	4.4090 +00	8.6170 +01	4.4132 +00	8.4018 +01	4.4142 +00	7.8287 +01	4.3661 +00	6.6167 +01
65	4.6614 +00	8.5905 +01	4.6649 +00	8.3604 +01	4.6612 +00	7.7477 +01	4.5903 +00	6.4529 +01
70	4.9041 +00	8.5641 +01	4.9067 +00	8.3191 +01	4.8974 +00	7.6670 +01	4.7999 +00	6.2902 +01
75	5.1382 +00	8.5378 +01	5.1396 +00	8.2780 +01	5.1237 +00	7.5868 +01	4.9958 +00	6.1286 +01
80	5.3643 +00	8.5116 +01	5.3644 +00	8.2371 +01	5.3409 +00	7.5069 +01	5.1787 +00	5.9681 +01
85	5.5834 +00	8.4855 +01	5.5818 +00	8.1964 +01	5.5498 +00	7.4274 +01	5.3491 +00	5.8086 +01
90	5.7958 +00	8.4594 +01	5.7925 +00	8.1557 +01	5.7508 +00	7.3482 +01	5.5075 +00	5.6503 +01
95	6.0023 +00	8.4335 +01	5.9969 +00	8.1153 +01	5.9444 +00	7.2692 +01	5.6543 +00	5.4930 +01
100	6.2032 +00	8.4076 +01	6.1955 +00	8.0749 +01	6.1312 +00	7.1906 +01	5.7899 +00	5.3368 +01

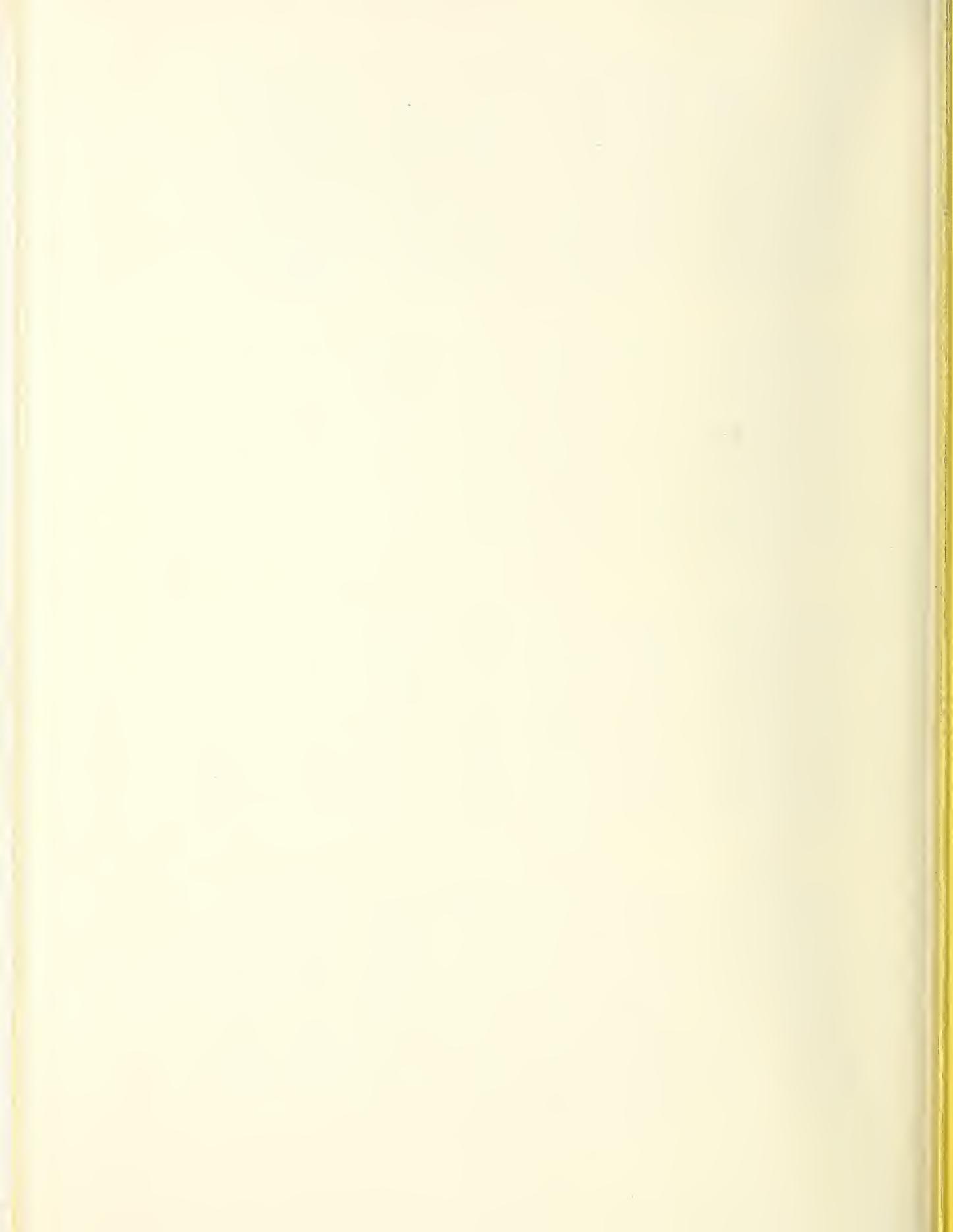
	PSI(0EGREES) = 12		PSI(0EGREES) = 15		PSI(0EGREES) = 16		PSI(0EGREES) = 17	
KB	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)
10	7.6353 -01	8.0789 +01	7.7751 -01	7.5637 +01	7.8290 -01	7.3671 +01	7.8866 -01	7.1582 +01
15	1.3474 +00	7.8039 +01	1.3691 +00	7.1350 +01	1.3771 +00	6.8798 +01	1.3855 +00	6.6086 +01
20	1.8359 +00	7.5395 +01	1.8588 +00	6.7230 +01	1.8663 +00	6.4116 +01	1.8736 +00	6.0807 +01
25	2.0213 +00	7.2818 +01	2.0277 +00	6.3221 +01	2.0283 +00	5.9562 +01	2.0281 +00	5.5676 +01
30	2.6397 +00	7.0292 +01	2.6416 +00	5.9295 +01	2.6368 +00	5.5106 +01	2.6284 +00	5.0661 +01
35	2.9804 +00	6.7805 +01	2.9583 +00	5.5439 +01	2.9409 +00	5.0736 +01	2.9170 +00	4.5749 +01
40	3.2893 +00	6.5352 +01	3.2334 +00	5.1646 +01	3.1987 +00	4.6443 +01	3.1538 +00	4.0934 +01
45	3.5703 +00	6.2927 +01	3.4702 +00	4.7912 +01	3.4132 +00	4.2225 +01	3.3417 +00	3.6217 +01
50	3.8263 +00	6.0528 +01	3.6711 +00	4.4235 +01	3.5869 +00	3.8085 +01	3.4832 +00	3.1602 +01
55	4.0593 +00	5.8153 +01	3.8378 +00	4.0618 +01	3.7215 +00	3.4025 +01	3.5802 +00	2.7100 +01
60	4.2708 +00	5.5802 +01	3.9718 +00	3.7063 +01	3.8187 +00	3.0053 +01	3.6347 +00	2.7274 +01
65	4.4619 +00	5.3474 +01	4.0743 +00	3.3574 +01	3.8797 +00	2.6178 +01	3.6486 +00	1.8491 +01
70	4.6336 +00	5.1169 +01	4.1464 +00	3.0157 +01	3.9063 +00	2.2421 +01	3.6241 +00	1.4426 +01
75	4.7867 +00	4.8888 +01	4.1892 +00	2.6819 +01	3.8999 +00	1.8768 +01	3.5638 +00	1.0556 +01
80	4.9218 +00	4.6630 +01	4.2039 +00	2.3569 +01	3.8623 +00	1.5267 +01	3.4703 +00	6.9219 +00
85	5.0394 +00	4.4397 +01	4.1917 +00	2.0419 +01	3.7955 +00	1.1932 +01	3.3469 +00	3.5713 +00
90	5.1400 +00	4.2190 +01	4.1539 +00	1.7382 +01	3.7016 +00	8.7900 +00	3.1972 +00	5.6779 -01
95	5.2241 +00	4.0011 +01	4.0191 +00	1.4474 +01	3.5831 +00	5.8782 +00	3.0255 +00	-2.0070 +00
100	5.2921 +00	3.7860 +01	4.0074 +00	1.1714 +01	3.4428 +00	3.2411 +00	2.8368 +00	-4.0476 +00

	PSI(0EGREES) = 18		PSI(0EGREES) = 19		PSI(0EGREES) = 20		PSI(0EGREES) = 21	
KB	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)
10	7.9479 -01	6.9369 +01	8.0131 -01	6.7035 +01	8.0820 -01	6.4580 +01	8.1549 -01	6.2003 +01
15	1.3941 +00	6.3215 +01	1.4030 +00	6.0185 +01	1.4121 +00	5.6999 +01	1.4213 +00	5.3657 +01
20	1.8804 +00	5.7305 +01	1.8866 +00	5.3611 +01	1.8920 +00	4.9728 +01	1.8965 +00	4.5656 +01
25	2.0830 +00	5.1565 +01	2.2806 +00	4.7232 +01	2.2756 +00	4.2680 +01	2.2674 +00	3.7911 +01
30	2.6157 +00	4.5963 +01	2.5981 +00	4.1015 +01	2.5749 +00	3.5824 +01	2.5455 +00	3.0394 +01
35	2.8856 +00	4.0485 +01	2.8459 +00	3.4951 +01	2.7967 +00	2.9155 +01	2.7373 +00	2.3108 +01
40	3.0974 +00	3.5129 +01	3.0283 +00	2.9041 +01	2.9453 +00	2.2684 +01	2.8475 +00	1.6078 +01
45	3.2540 +00	2.9901 +01	3.1487 +00	2.3299 +01	3.0246 +00	1.6437 +01	2.8808 +00	9.3494 +00
50	3.3580 +00	2.4813 +01	3.2101 +00	1.7749 +01	3.0384 +00	1.0456 +01	2.8426 +00	2.9951 +00
55	3.4120 +00	1.9882 +01	3.2158 +00	1.2423 +01	2.9914 +00	4.8000 +00	2.7396 +00	-2.8776 +00
60	3.4418 +00	1.5134 +01	3.1695 +00	7.3694 +00	2.8891 +00	-4.4378 -01	2.5802 +00	-8.1093 +00
65	3.3802 +00	1.0604 +01	3.0756 +00	2.6516 +00	2.7383 +00	-5.1530 +00	2.3748 +00	-1.2461 +01
70	3.3007 +00	6.3358 +00	2.9393 +00	-1.6419 +00	2.5470 +00	-9.1513 +00	2.1364 +00	-1.5573 +01
75	3.1837 +00	2.3897 +00	2.7667 +00	-5.3890 +00	2.3255 +00	-1.2183 +01	1.8820 +00	-1.6903 +01
80	3.0339 +00	-1.1548 +00	2.5654 +00	-8.4202 +00	2.0864 +00	-1.3881 +01	1.6348 +00	-1.5687 +01
85	2.8565 +00	-4.1915 +00	2.3445 +00	-1.0500 +01	1.8463 +00	-1.3732 +01	1.4258 +00	-1.1076 +01
90	2.6580 +00	-6.5781 +00	2.1154 +00	-1.1307 +01	1.6269 +00	-1.1115 +01	1.2938 +00	-2.8499 +00
95	2.4458 +00	-8.1250 +00	1.8926 +00	-1.0429 +01	1.4561 +00	-5.5539 +00	1.2706 +00	7.3393 +00
100	2.2293 +00	-8.5865 +00	1.6946 +00	-7.4288 +00	1.3639 +00	2.6160 +00	1.3574 +00	1.6308 +01

	PSI(0EGREES) = 22		PSI(0EGREES) = 23		PSI(0EGREES) = 24		PSI(0EGREES) = 25	
KB	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)	G(B)	PHASE(0EGREES)
10	8.2318 -01	5.9307 +01	8.3127 -01	5.6492 +01	8.3977 -01	5.3559 +01	8.4869 -01	5.0509 +01
15	1.4307 +00	5.0159 +01	1.4400 +00	4.6508 +01	1.4494 +00	4.2705 +01	1.4587 +00	3.8752 +01
20	1.8998 +00	4.1397 +01	1.9018 +00	3.6955 +01	1.9021 +00	3.2330 +01	1.9007 +00	2.7526 +01
25	2.0257 +00	3.2929 +01	2.2401 +00	2.7739 +01	2.2201 +00	2.2344 +01	2.1953 +00	1.6750 +01
30	2.5092 +00	2.4733 +01	2.4654 +00	1.8848 +01	2.4133 +00	1.2749 +01	2.3525 +00	6.4482 +00
35	2.6668 +00	1.6824 +01	2.5844 +00	1.0318 +01	2.4894 +00	3.6101 +00	2.3815 +00	-3.2723 +00
40	2.7339 +00	9.2475 +00	2.6039 +00	2.2253 +00	2.4574 +00	-4.9451 +00	2.2944 +00	-1.2204 +01
45	2.7168 +00	2.0833 +00	2.5326 +00	-5.2958 +00	2.3292 +00	-1.2695 +01	2.1081 +00	-1.9976 +01
50	2.6231 +00	-4.5440 +00	2.3815 +00	-1.2031 +01	2.1209 +00	-1.9264 +01	1.8460 +00	-2.5922 +01
55	2.4628 +00	-1.0442 +01	2.1653 +00	-1.7629 +01	1.8543 +00	-2.4002 +01	1.5413 +00	-2.8807 +01
60	2.2485 +00	-1.5311 +01	1.9033 +00	-2.1512 +01	1.5600 +00	-2.5770 +01	1.2446 +00	-2.6447 +01
65	1.9964 +00	-1.8675 +01	1.6218 +00	-2.2720 +01	1.2832 +00	-2.2728 +01	1.0354 +00	-1.6307 +01
70	1.7283 +00	-1.9787 +01	1.3593 +00	-1.9806 +01	1.0922 +00	-1.3079 +01	1.0049 +00	-6.8880 -01
75	1.4747 +00	-1.7570 +01	1.1709 +00	-1.1427 +01	1.0596 +00	1.0308 +00	1.1574 +00	1.1109 +01
80	1.2783 +00	-1.0951 +01	1.1166 +00	1.0771 +00	1.1910 +00	1.2345 +01	1.4008 +00	1.5260 +01
85	1.1882 +00	-3.6135 -01	1.2112 +00	1.2338 +01	1.6144 +00	1.7261 +01	1.6509 +00	1.4031 +01
90	1.2304 +00	1.0734 +01	1.4054 +00	1.8529 +01	1.6567 +00	1.7169 +01	1.8597 +00	9.8428 +00
95	1.2807 +00	1.8454 +01	1.6355 +00	1.9978 +01	1.8725 +00	1.4084 +01	2.0016 +00	4.1581 +00
100	1.5878 +00	2.1865 +01	1.8568 +00	1.8279 +01	2.0360 +00	9.3540 +00	2.0643 +00	-2.1418 +00

Table 9

$a_0 = + 1.595769140$	$b_0 = - 0.000000033$	$c_0 = 0$	$d_0 = + 0.199471140$
$a_1 = - 0.000001702$	$b_1 = + 4.255387524$	$c_1 = - 0.024933975$	$d_1 = + 0.000000023$
$a_2 = - 6.808568856$	$b_2 = - 0.000092809$	$c_2 = + 0.000003936$	$d_2 = - 0.009351341$
$a_3 = - 0.000576361$	$b_3 = - 7.780020406$	$c_3 = + 0.005770956$	$d_3 = + 0.000023006$
$a_4 = + 6.920691905$	$b_4 = - 0.009520896$	$c_4 = + 0.000689892$	$d_4 = + 0.004851466$
$a_5 = - 0.016898657$	$b_5 = + 5.075161301$	$c_5 = - 0.009497136$	$d_5 = + 0.001903218$
$a_6 = - 3.050485662$	$b_6 = - 0.138341946$	$c_6 = + 0.011948809$	$d_6 = - 0.017122914$
$a_7 = - 0.075752420$	$b_7 = - 1.363729125$	$c_7 = - 0.006748873$	$d_7 = + 0.029064067$
$a_8 = + 0.850663781$	$b_8 = - 0.403349276$	$c_8 = + 0.000246420$	$d_8 = - 0.027928955$
$a_9 = - 0.025639041$	$b_9 = + 0.702222017$	$c_9 = + 0.002102967$	$d_9 = + 0.016497308$
$a_{10} = - 0.150230960$	$b_{10} = - 0.216195929$	$c_{10} = - 0.001217930$	$d_{10} = - 0.005598515$
$a_{11} = + 0.034404779$	$b_{11} = + 0.019547031$	$c_{11} = + 0.000233939$	$d_{11} = + 0.000838386$



**U.S. DEPARTMENT OF COMMERCE**Luther H. Hodges, *Secretary***NATIONAL BUREAU OF STANDARDS**A. V. Astin, *Director***THE NATIONAL BUREAU OF STANDARDS**

The scope of activities of the National Bureau of Standards at its major laboratories in Washington, D.C., and Boulder, Colorado, is suggested in the following listing of the divisions and sections engaged in technical work. In general, each section carries out specialized research, development, and engineering in the field indicated by its title. A brief description of the activities, and of the resultant publications, appears on the inside of the front cover.

**WASHINGTON, D.C.**

**Electricity.** Resistance and Reactance. Electrochemistry. Electrical Instruments. Magnetic Measurements. Dielectrics. High Voltage.

**Metrology.** Photometry and Colorimetry. Refractometry. Photographic Research. Length. Engineering Metrology. Mass and Scale. Volumetry and Densimetry.

**Heat.** Temperature Physics. Heat Measurements. Cryogenic Physics. Equation of State. Statistical Physics.

**Radiation Physics.** X-ray. Radioactivity. Radiation Theory. High Energy Radiation. Radiological Equipment. Nucleonic Instrumentation. Neutron Physics.

**Analytical and Inorganic Chemistry.** Pure Substances. Spectrochemistry. Solution Chemistry. Standard Reference Materials. Applied Analytical Research. Crystal Chemistry.

**Mechanics.** Sound. Pressure and Vacuum. Fluid Mechanics. Engineering Mechanics. Rheology. Combustion Controls.

**Polymers.** Macromolecules: Synthesis and Structure. Polymer Chemistry. Polymer Physics. Polymer Characterization. Polymer Evaluation and Testing. Applied Polymer Standards and Research. Dental Research.

**Metallurgy.** Engineering Metallurgy. Microscopy and Diffraction. Metal Reactions. Metal Physics. Electrocatalysis and Metal Deposition.

**Inorganic Solids.** Engineering Ceramics. Glass. Solid State Chemistry. Crystal Growth. Physical Properties. Crystallography.

**Building Research.** Structural Engineering. Fire Research. Mechanical Systems. Organic Building Materials. Codes and Safety Standards. Heat Transfer. Inorganic Building Materials. Metallic Building Materials.

**Applied Mathematics.** Numerical Analysis. Computation. Statistical Engineering. Mathematical Physics. Operations Research.

**Data Processing Systems.** Components and Techniques. Computer Technology. Measurements Automation. Engineering Applications. Systems Analysis.

**Atomic Physics.** Spectroscopy. Infrared Spectroscopy. Solid State Physics. Electron Physics. Atomic Physics.

**Instrumentation.** Engineering Electronics. Electron Devices. Electronic Instrumentation. Mechanical Instruments. Basic Instrumentation.

**Physical Chemistry.** Thermochemistry. Surface Chemistry. Organic Chemistry. Molecular Spectroscopy. Elementary Processes. Mass Spectrometry. Photochemistry and Radiation Chemistry.

**Office of Weights and Measures.**

**BOULDER, COLO.**

**Cryogenic Engineering Laboratory.** Cryogenic Equipment. Cryogenic Processes. Properties of Materials. Cryogenic Technical Services.

**CENTRAL RADIO PROPAGATION LABORATORY**

**Ionosphere Research and Propagation.** Low Frequency and Very Low Frequency Research. Ionosphere Research. Prediction Services. Sun-Earth Relationships. Field Engineering. Radio Warning Services. Vertical Soundings Research.

**Radio Propagation Engineering.** Data Reduction Instrumentation. Radio Noise. Tropospheric Measurements. Tropospheric Analysis. Propagation-Terrain Effects. Radio-Meteorology. Lower Atmosphere Physics.

**Radio Systems.** Applied Electromagnetic Theory. High Frequency and Very High Frequency Research. Modulation Research. Antenna Research. Navigation Systems.

**Upper Atmosphere and Space Physics.** Upper Atmosphere and Plasma Physics. Ionosphere and Exosphere Scatter. Airglow and Aurora. Ionospheric Radio Astronomy.

**RADIO STANDARDS LABORATORY**

**Radio Physics.** Radio Broadcast Service. Radio and Microwave Materials. Atomic Frequency and Time-Interval Standards. Millimeter-Wave Research.

**Circuit Standards.** High Frequency Electrical Standards. Microwave Circuit Standards. Electronic Calibration Center.

