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# Evaluating Office Lighting Environments：Reference Lighting Power Density Data 

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U．S．DEPARTMENT OF COMMERCE National Bureau of Standards Center for Building Technology Building Environment Division Gaithersburg，MD 20899

In Collaboration with：
The Lighting Research Institute
345 East 47th Street
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New York，NY 10017

October 1987
Issued January 1988

Sponsored by：
The National Electrical Manufacturers Association －QC＿ng Equipment Division
100 ．Street，NW

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Washington, DC 20037
U.S. DEPARTMENT OF COMMERCE, C. William Verity, Secretary NATIONAL BUREAU OF STANDARDS, Ernest Ambler, Director


#### Abstract

This document reports on an exercise in archiving in situ lighting power densities for occupied office lighting environments. Using data from a previous study where field surveys of existing lighting installations were recorded, the present study extends these data to include referencable lighting power densities for the installed conditions. In addition, theoretical alternate ANSI lighting power densities were computed assuming one-for-one replacement with either energy saving or standard lamps and ballasts.


Keywords: Lighting power density; unit power density; energy performance; lighting energy standards; occupant satisfaction
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Assistance was received from a number of individuals throughout the scope of the project. Substantial technical support was provided by Belinda Collins and Art Rubin at the National Bureau of Standards, as well as from Harry Lobdell representing the National Electrical Manufacturers Association. Advisory and administrative support was provided by Thomas Schneider and Richard Vincent of the Lighting Research Institute. Will Fisher provided valuable insight during the review process.

The extended study built upon an earlier effort which supplied the raw field data. The original work was supported jointly by the New York State Energy Research and Development Authority, and the Office of Buildings and Community Systems, United States Department of Energy. Robert W. Marans and his colleagues at the Institute for Social Research, University of Michigan, were instrumental in developing the questionnaires and survey procedures in the original study.

With the concern over reducing the energy consumption in buildings, several professional societies, government organizations and others have been exploring strategies to conserve energy in new buildings. As research in this area has progressed, lighting has surfaced as an important area for potential energy savings. As a result, major reductions have been suggested in the unit power density (UPD) ${ }^{1}$ limits used in many building energy standards. These lower numbers, however, differ from those previously recommended by the Illuminating Engineering Society of North America. For example, the base UPD suggested by the draft ASHRAE/IES Standard $90.1 R$ [1] for small enclosed offices shows a reduction of 18 percent for reading and typing tasks to as much as 53 percent for drafting tasks as compared to the original IES Lighting Energy Management document LEM1 [2]. While attractive from an energy standpoint, these lower limits were suggested from modifications in hypothetical lighting systems (computer simulated scenarios) where the impact on the quality of the visual environment was never fully assessed. Also, they do not account for the realities of space use and operational conditions. Unfortunately, measured data have been lacking to date in support of specific lighting power numbers.

Under the auspices of the U.S. Department of Energy and the New York State Energy Research and Development Authority, an earlier research project was initiated to develop a reference set of archival data to help bridge this gap [3]. As part of that project, extensive field measurements were made at several hundred work stations in thirteen office buildings, and collected into a database archived at the National Bureau of Standards [4]. The project scope, however, did not allow for detailed documentation of the lighting system characteristics. Furthermore, some concern was expressed over the lamp/ballast wattages used since they were estimated rather than measured. To supplement the existing data with more referencable lamp/ballast data, and complete the documentation of the lighting power data, an extended documentation program was initiated by the National Electrical Manufacturers Association (NEMA) and the Lighting Research Institute (LRI), in collaboration with the Lighting Group at the National Bureau of Standards.

A full discussion of how the original data were obtained can be found in the methodology report [3]. Of interest in this extended study is the power density data recorded during the field measurements. The connected lighting power load and the floor areas for each work station were determined from drawings, photographs, and field surveys for 912 work stations from thirteen office buildings. Originally, the lamp and ballast wattages were determined by visual inspection, examining the

1 Throughout this study the term lighting power density (LPD) is used in lieu of unit power density to distinguish the measured quantity, LPD, from the prescribed quantity, UPD.
luminaire and assigning wattages based on observed characteristics. The weakness in this approach is that the ballasts are not directly observable: only by disconnecting and disassembling the unit and making individual measurements could the actual input wattages be determined. However, since the lighting systems were well documented, including the type of fixtures, lamps, ballasts, and control media, it was possible in the extended study to augment the database with lamp and ballast wattages conforming to the ANSI $C 82.2$ test method [5]. In this way, more referencable lighting power data associated with the lighting conditions in occupied spaces were developed, including the consideration for ballast and thermal factors in specific luminaires having various lamp/ballast combinations.

## 2. SCOPE OF CURRENT STUDY

There were two general thrusts to the present NEMA/LRI project. First, data review, editing, and additional documentation were done to reconstruct lighting power densities based on a consistent procedure for obtaining lamp/ballast input wattages. These new data were added to the archival database. The second was to extend the database to include alternative ANSI power densities for four different lamp/ ballast combinations.

## 3. PROCEDURE FOR OBTAINING POWER DENSITY DATA

The compilation of lighting powex density data involved obtaining the in situ lamp and ballast characteristics for all luminaires in and around each work station, and assigning fixture wattages and floor areas associated wich these wattages. The luminaire characteristics for portable and stationary units were obtained by a combination of field observations and reviewing drawings and photographs of the space. Once the lamp, ballast, and fixture characteristics were recorded, tables for each luminaire with a unique lamp/ballast combination (Appendix A) were prepared. Fixture category assignments, Table 1, were employed to arrange the various fixture mountings into four representative categories for obtaining luminaire thermal factors. Working in conjunction with the NEMA Lighting Divisional Technical Advisory Committee, ANSI input wattages were established for the individual lamp/ballast combinations based on laboratory measurements following the ANSI C82.2 test method ${ }^{2}$. Also in consultation with the NEMA Committee, luminaire thermal correction factors were assigned for the various lamp/ballast, and louver/lens combinations (Tables 2, 3, and 4). Thus, the installed input wattages conformed to the ANSI wattages, with the correction factors applied.

The lighting power density for the space was computed as follows:

2 ANSI C82.2 test results were provided by the NEMA Lighting Divisional Technical Advisory Committee.

LPD = Wattage for zone lighting + Wattage for task lighting Zone area
where,
LPD = total lighting power density associated with the specified work station
Zone $=$ space enclosed by walls, such as a fully enclosed office or the bay where cubicles reside.
Work station
area $=$ personal space area (defined on pages 79-81 in reference [3]).

## 4. PROCEDURE FOR OBTAINING ALTERNATE ANSI POWER DENSITY DATA

In addition to the installed lighting power density, LPD, four alternative lighting power densities were computed using only the ANSI C82.2 reference wattages. Here, theoretical scenarios were generated analytically assuming a one-for-one substitution of lamps and/or ballasts, replacing the existing equipment in the occupied space with either standard or energy saving alternatives. No changes were made in the work station or fixture data, other than the ballast and lamp wattage. It should be noted that although the operating conditions with the substituted equipment would be similar, they would not be identical since luminaire light output varies depending on the particular lamp and ballast combination. No attempt was made to evaluate the potential differences in measured illuminance or luminance attributable to the four different lamps and ballasts described. The first scenario assumed that all the luminaires in the database had energy saving lamps and energy saving ballasts, where available. The second scenario assumed that the luminaires had energy saving lamps and standard ballasts, and the third scenario used only energy saving ballasts with standard lamps. The last scenario assumed that standard lamps and standard ballasts were used throughout. Unlike the input wattage for the installed power densities, the ANSI alternative power densities did not employ the luminaire thermal factors.

## 5. SUMMARY OF RESULTS

The lighting power densities for each work station are given in Appendix B and summarized in tables 5 and 6. A frequency distribution of all lighting power densities is given in figure 1. Inspection of the figure reveals that the most frequently occurring LPD band is 20 $\mathrm{w} / \mathrm{m}^{2}\left(1.9 \mathrm{w} / \mathrm{ft}^{2}\right)$ with 15 percent of the sample. Fourteen percent of the sample is below $20 \mathrm{w} / \mathrm{m}^{2}$, 52 percent between 20 and $29 \mathrm{w} / \mathrm{m}^{2}(2.7$ $\left.\mathrm{w} / \mathrm{ft} \mathrm{t}^{2}\right), 26$ percent between $30 \mathrm{w} / \mathrm{m}^{2}\left(2.8 \mathrm{w} / \mathrm{ft}^{2}\right)$ and $39 \mathrm{w} / \mathrm{m}^{2}\left(3.6 \mathrm{w} / \mathrm{ft} \mathrm{t}^{2}\right)$, and 8 percent above $40 \mathrm{w} / \mathrm{m}^{2}\left(3.7 \mathrm{w} / \mathrm{ft}^{2}\right)$. Since both the unit power density limits presently in use and currently under consideration in LEM-1 and Standard 90.1 R are between $19.4 \mathrm{w} / \mathrm{m}^{2}\left(1.8 \mathrm{w} / \mathrm{ft} \mathrm{t}^{2}\right)$ and 50.6
$\mathrm{w} / \mathrm{m}^{2}\left(4.7 \mathrm{w} / \mathrm{ft}^{2}\right)$, depending on the task type and the room geometry, the present data can be considered comparable to the range of lighting power densities specified by various existing standards in place and under revision.

Figure 2 presents the distribution of lighting power densities for each type of ambient lighting system. The maximum and the minimum (the range) are shown along with the standard deviation about the mean for the seven lighting systems. By inspection, no one type of lighting system appears to be substantially different in terms of mean power densities. It is important to note that the mean for each system type is between 23 and 31 watts per square meter ( 2.1 and $2.9 \mathrm{w} / \mathrm{ft}^{2}$, respectively) (table 5). The three direct fluorescent systems (DRFLV, DRFLN, DF-SM) have a broad range of power densities, with the recessed lensed system (DRFLN) providing one of the lowest means while the surface mounted system (DF-SM) has the highest mean scor?. On the other hand, the fluorescent indirect systems (IF-FM, INDF-P, both show higher power densities. The other two pendant mounted systems, the direct/indirect fluorescent (DIF-P) and the metal halide indirect (HIDP), show lower mean power densities as well as a more constricted range.

An another data plot is shown in figure 3. Here all work stations are grouped by presence and type of task lighting. The combined data for all work stations are shown to the left, and to the right, the same data are grouped into one of three categories: 1) work stations with no local task units, 2) work stations with furniture integrated task units, and 3) work stations with desk mounted movable task units. Figure 3 clearly shows an increase in the power density for work stations with task units, particularly if they are movable. The mean LPD for work stations without task lighting is $21.7 \mathrm{w} / \mathrm{m}^{2}\left(2.02 \mathrm{w} / \mathrm{ft}^{2}\right)$ as compared to that for work stations with furniture integrated task lighting of $28.9 \mathrm{w} / \mathrm{m}^{2}\left(2.69 \mathrm{w} / \mathrm{ft}^{2}\right)$, and that for work stations with movable task lighting of $34.4 \mathrm{w} / \mathrm{m}^{2}\left(3.20 \mathrm{w} / \mathrm{ft}^{2}\right)$.

The mean lighting power density for all work stations is $26.7 \mathrm{w} / \mathrm{m}^{2}$ ( $2.48 \mathrm{w} / \mathrm{ft}^{2}$ ). Table 5 suggests that if energy saving lamps and energy saving ballasts ${ }^{3}$ were used where possible, the mean would be $23.8 \mathrm{w} / \mathrm{m}^{2}$ (2.21 w/ft ${ }^{2}$ ), and if no energy saving lamps or ballasts were used the mean would be $29.7 \mathrm{w} / \mathrm{m}^{2}\left(2.76 \mathrm{w} / \mathrm{ft}^{2}\right)$. Thus, a 20 percent reduction in lighting power density can be attributed to the use of efficient components in the installed lighting systems covered in the database. In addition, table 1 implies that the bulk of this improvement (12 percent) can be attributed to the use of energy saving lamps.

As defined by the NEMA Lighting Divisional Technical Advisory Committee.

## 6. CONCLUSIONS AND RECOMMENDATIONS FOR FURTHER WORK

In conclusion, the lighting power data examined have revealed a wide range of power densities contained in the database. The review and editing of the LPD data have successfully sreated a unique database of reference lighting power data from a range of lighting system types. The 912 work stations are from 13 office buildings representing a variety of construction types, includir!g government (state and federal), university, speculative, and corporate offices. To the best of the author's knowledge, the database described here is the most sizable and unique collection of information about LPD's in existing buildings. Obviously, 13 buildings cannot represent the entire national building stock, but they do represent a beginning and do provide information about what is actually being done in lighting practice over the last two decades.

The data show a substantial range in lighting power densities for each lighting system with no one system (in terms of mounting type) clearly superior to the others. However, the data have revealed that task lighting plays a key role in increasing the lighting power density of a work station. In addition, the alternative energy scenarios have underscored the value of energy saving lamps and ballasts. The analysis in the present paper indicates that while several of these buildings are already using energy efficient lamps and energy efficient ballasts, the potential still exist for additional energy reduction by simply a more extensive application of energy efficient equipment in existing buildings.

Several areas of further work are suggested:

* The shape of the distribution curves in figure 1 is non-gaussian. It was assumed that this can be explained solely by the presence of multiple lighting systems displayed together. This should be tested.
* Task lighting appears to be associated with higher lighting power densities. The cause for this needs to be explored.
* The database contains occupant satisfaction measures that need to be explored in relation to the revised power data.
* Several factors, such as room geometry ani room size, type of lighting system, type of work station, and type of work activity, appear to be related to lighting power dersity. These factors and their impact should be evaluated.
* A variety of work station types, visual task types, lighting system types (beyond the seven groups in figure 2), and other group types are present in the database. The data need to be analyzed into work stations of comparable characteristics and evaluated.
* The relationship between LPD's and the task illuminances need to be explored.
* The impact of daylighting on the illuminance at the work stations needs to be explored, including an assessment of the effect on user satisfaction. If a sufficient number of work stations without daylighting can be identified, these should be evaluated separately.


Figure 1
Lighting power density histogram for all work stations


DRFLV = Direct recessed fluorescent units with louvers DRFLN $=$ Direct recessed fluorescent units with prismatic lens $D F-S M=$ Direct fluorescent surface mounted units with egg crates IF-FM = Indirect fluorescent furniture mounted units INDF-P= Indirect fluorescent pendant mounted units DIF-P = Direct/indirect fluorescent pendant mounted units HID-P = High intensity discharge (metal halide) indirect pendant mounted units

Figure 2
Lighting power distribution by lighting system


Combined = all work stations
None $=$ work stations without local task units
Furn int $=$ work stations with furniture integrated task units Movable $=$ work stations with desk mounted movable task units

Figure 3
Lighting power density by type of task lighting

Table 1
Fixture category assignment

Fixture Mounting
Recessed Ceiling
Cove
Furniture Mounted Indirect Fluorescent Wall Wash
Wall Panel
Ceiling Wall Wash
Ceiling Wash Indirect Fluorescent Furniture Indirect Fluorescent

Pendant
Drafting Unit Desk Unit

Surface Ceiling
Ceiling Surface
Under Shelf
Above Shelf
Surface Wall Wash
Shelf Box Unit

Free Standing
Recessed Can
Track Ceiling

Category to Use
Recessed Category

Pendant Category

Surface Category

Use standard wattage input

Table 2
Recessed category input wattage
1x4 Single Lamp F40T12-

## Lamp

1 standard
1 standard
1 energy saving
1 energy saving

Ballast
standard
energy saving
standard
energy saving

|  | Louver | Lens |
| :--- | :--- | :--- |
| 57 | $-3=54$ | $-4=53$ |
| 50 | $-2=48$ | $-3=47$ |
| 50 | $-1=49$ | $-2=48$ |
| 43 | $-1=42$ | $-1=42$ |

1x4 Single Lamp F40T12 (Tandem Ballast)

## Lamp

1 standard
1 standard
1 energy saving
1 energy saving

## Ballast

1/2 standard
1/2 energy saving
1/2 standard
$1 / 2$ energy saving

ANSI Louver Lens
$48-2=46-3=45$
$43-1=42-2=41$
$41-1=40-1=40$
$360=36 \quad 0=36$
$1 \times 42$ Lamp F40T12-

## Lamp

2 standard
2 standard
2 energy saving
2 energy saving

Ballast
standard
energy saving
standard
energy saving

| ANSI | Louver | Lens |
| :--- | :--- | :--- |
| 96 | $-7=89$ | $-8=88$ |
| 86 | $-5=81$ | $-6=80$ |
| 82 | $-4=78$ | $-5=77$ |
| 72 | $-3=69$ | $-3=69$ |

## Ballast

standard
energy saving standard energy saving

| ANSI | Louver | Lens. |
| :--- | :--- | :--- |
| 96 | $-6=90$ | $-7=89$ |
| 86 | $-4=82$ | $-5=81$ |
| 82 | $-3=79$ | $-4=78$ |
| 72 | $-2=70$ | $-2=70$ |

Ballast
1+1 Standard
$1+1$ Energy saving
1+1 Standard
$1+1$ Energy saving

ANSI Louver Lens
$153-10=143-11=142$
$136-6=130-7=129$
$132-5=127-5=127$
$115-3=112-4=111$
$2 \times 43$ Lamp F40T12 (Tandem Ballast)-

Lamp
3 standard
3 standard
3 energy saving
3 energy saving
Ballast
1 1/2 Standard
$11 / 2$ Energy saving $129 \quad-5=124 \quad-6=123$
$11 / 2$ Standard $\quad 123 \quad-4=119 \quad-4=119$
$11 / 2$ Energy saving $108 \quad-2=106 \quad-3=105$
2x4 4 Lamp F40T12-

## Lamp

4 standard
4 standard
4 energy saving
4 energy saving

## Ballast

2 standard
2 energy saving
2 standard
2 energy saving

ANSI Louver Lens
$196-12=180-16=176$
$172-8=164-12=160$
$164-5=159-9=155$
$144-4=140-6=138$

Table 3
Surface category input wattage
Single Lamp F40T12-

| $\frac{\text { Lamp }}{}$ | $\frac{\text { Ballast }}{\text { standard }}$ |
| :--- | :--- |
| 1 standard | energy saving |
| 1 standard | standard |
| 1 energy saving | energy saving |
| 1 | energy saving |


| ANSI | Louver | Lens |
| :--- | :--- | :--- |
| 57 | $-5=52$ | $-6=51$ |
| 50 | $-4=46$ | $-5=45$ |
| 50 | $-3=47$ | $-4=46$ |
| 43 | $-3=40$ | $-3=40$ |

2 Lamp F40T12-

Lamp
2 standard
2 standard
2 energy saving
2 energy saving
3 Lamp F40T12-
Lamp
3 standard
3 standard
3 Energy saving
3 Energy saving
4 Lamp F40T12-
Lamp
4 standard
4 standard
4 energy saving
4 energy saving
Single Lamp F30T12-
Lamp

1 standard
1 energy saving
2 Lamp F30T12-
Lamp
2 standard
2 standard
2 energy saving
2 energy saving
Single Lamp F20T12-
Lamp
1 standard

Ballast standard
energy saving standard
energy saving

Ballast
$1+1$ Standard
$1+1$ Energy saving
1+1 Standard
$1+1$ Energy saving

Ballast
standard
energy saving standard
energy saving

## Ballast

standard
standard

Ballast
standard
energy saving standard
energy saving

Ballast
standard
Single and Double Lamp F48T12/HO-

## Lamp

1 standard
2 standard

Ballast
standard
standard
ANSI Louver Lens
$96-9=87-10=86$
$86-7=79-8=78$
$82-6=76-7=75$
$72-5=67-5=67$

| ANSI | Louver | Lens |
| :--- | :---: | ---: |
| 153 | $-18=135$ | N/A |
| 136 | N/A | N/A |
| 132 | N/A | N/A |
| 115 | N/A | N/A |

ANSI Louver Lens
$192-14=178-18=174$
$172-10=162-14=158$
$164-7=157-11=153$
$144-6=138-8=136$

| ANSI | Louver | Lens |
| :--- | :--- | :--- |
| 46 | $-2=44$ | $-3=43$ |
| 42 | $-1=41$ | $-2=40$ |

ANSI Louver Lens
$79-9=70-10=69$
$74-7=67-8=66$
$71-6=65-7=64$
$66-5=31-5=61$

| ANSI | Louver | Lens |
| :--- | :--- | :--- |
| 32 | $-2=30$ | $-3=29$ |


| ANSI | Louver | Lens |
| :--- | :---: | ---: |
| 80 | $-7=75$ | $-9=79$ |
| 145 | N/A | $-14=131$ |

Table 4
Pendant category input wattage

Single Lamp F40T12-

Lamp
1 standard
1 standard
1 energy saving
1 energy saving

Ballast
standard
energy saving standard
energy saving

| ANSI | Louver | Lens |
| :--- | :--- | :--- |
| 57 | $-2=55$ | $-3=53$ |
| 50 | $-1=49$ | $-2=48$ |
| 50 | $-1=49$ | $-1=49$ |
| 43 | $-0=43$ | $-0=43$ |

Ballast standard ANSI Louver Lens
energy saving standard
$86-4=82-5=81$
$82-3=79-4=78$
energy saving
Single and Double Lamp F48T12/HO (60w) =

Lamp
1 standard
2 standard

Ballast
standard
standard

| ANSI | Louver | Lens |
| :--- | :---: | :---: |
| 80 | $-5=75$ | $-7=73$ |
| 145 | $-14=131$ | $\mathrm{~N} / \mathrm{A}$ |

Single and Double Lamp F72T12/HO (85w)-

Lamp
1 standard
2 standard
2 standard

Ballast
standard
standard
energy saving
ANSI Louver Lens
$135-29=106$ N/A
$220-10=210-14=206$
$200-7=193-11=189$

Single and Double Lamp F96T12/HO (110/95w)-

Lamp
1 standard
1 energy saving
2 standard
2 standard
2 energy saving
2 energy saving

Ballast standard standard standard energy saving standard energy saving

| ANSI | Louver | Lens |
| :--- | :---: | :---: |
| 135 | N/A | N/A |
| 125 | N/A | N/A |

$257-10=247-14=243$
$237-7=230-11=226$
$227-10=217-14=213$
$207-7=200-11=196$

Single and double Lamp F15T8-

Lamp
1 standard
2 standard
2 standard

Ballast
low power factor standard
low power factor

ANSI Louver Lens
$27-9=18 \quad \mathrm{~N} / \mathrm{A}$
$50-8=42-9=41$
$40-7=35-8=32$
Single Lamp F8T5, FC6T9, And FC8T9-
Lamp
1 standard F8T5
1 standard FC6T9
1 standard FC8T9

Ballast
standard
standard
standard

ANSI Louver Lens

| $15-6$ | $=9$ | $\mathrm{~N} / \mathrm{A}$ |
| ---: | :--- | ---: |
| $33-11$ | $=22$ | $\mathrm{~N} / \mathrm{A}$ |
| 29 | -5 | $=24$ |
| $\mathrm{~N} / \mathrm{A}$ |  |  |





$z \mid$ 우
g
g

Minimum
 Building \#13:
All energy saving lamps and ballasts Energy saving lamps only No energy saving lamps or ballasts numbers (with only a few exceptions, the lighting system installed had energy saving lamps and ballasts throughout)
Table 7
Building Descriptions

$$
\text { Mean LPD, } w / m^{2}\left(w / f t^{2}\right)
$$

$$
(3.18)
$$

$$
\left(26^{\circ} 乙\right)
$$

$$
\left(26^{\circ} Z\right)
$$

$$
\left(\tau Z^{\circ} \tau\right)
$$

$$
(Z L \cdot Z)
$$

$$
\tau^{\left(\angle \varepsilon^{\circ} \tau\right)} \varsigma^{\circ} \varsigma \tau
$$

Building Descriptions
ұuəosəxontf pəssəวəx ұวəxtp yx General building description
Mid-rise corporate offices

High-xise corporate offices Small regional center
 Low-rise corporate offices High-rise federal offices High-rise federal offices See Appendix A for detailed description of luminaire characteristics (first digit in luminaire code in Appendix $A$ is building number). High-rise corporate offices
Low-rise manufacturing offices ———_ 1
Building \#

$$
\text { Principal lighting system }{ }^{1}
$$

$$
1 \times 4 \text { direct recessed fluorescent }
$$

Indirect fluorescent furniture mounted
Indixect pendant mounted metai halide

$$
2 \times 4 \text { direct recessed fluorescent }
$$

$$
2 \times 4 \text { direct recessed ceiling }
$$

Indirect furniture mounted

$$
24.2(2.25)
$$

$$
24.5(2.28)
$$

$$
(2.07)
$$

$$
(3.18)
$$

$$
21.2(1.97)
$$

$$
24.4(2.27)
$$

$$
25.4(2.36)
$$



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$$
\underline{1}
$$

| age Notes |  |
| :---: | :---: |
|  |  |
| 46 Baliast shared by two units |  |
| 45 Ballast shared by two units |  |
| 45 |  |
| 46 Ballast shared by two units |  |
| 150 |  |
| 29 |  |
| 43 |  |
| 43 |  |
| 51 |  |
| 60 |  |
| 100 |  |
| 150 |  |
| 60 |  |
| 35 |  |
| 18 |  |
| 247 |  |
| 89 |  |
| 58 |  |
| 54 |  |
| 49 |  |
| 46.5 ballast shared by two units |  |
| 44 |  |
| 54 |  |
| 54 |  |
| 29 |  |
| 51 |  |
| 82 |  |
| 35 |  |
| 150 |  |
| 60 |  |
| - 46 |  |
| 43 |  |
| 29 |  |
| 77 |  |
| 155 |  |
| 295 |  |
| 88 |  |
| 55 |  |
| 89 |  |
| 90 |  |
| 210 |  |
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| 9010 *A*type | DRF-LM | 2x4 | Recessed Celling | Prisatic lens | CHF | F40112/RS/CW | 40 | 2 | STD Ballast | 29 |
| 9008 ${ }^{\text {a }}$ A type | DRF-IN | 2x4 | Recessed Ceiling | Prisadic lens | CWF | F40\%12/RS/MW | 40 | 2 | SID Ballast | 89 |
| $90200^{\circ}{ }^{\circ} \mathrm{t}$ type | FH-tast |  | Orafting Unit | Reflector | IN | A19/IF | 75 | 1 | None | 75 |
| $9021{ }^{\text {a a }}$ - 9 ype | Fh-task |  | Brafting Unit | Reflector | 819 | A $19 / 1 \mathrm{~F}$ | 95 | 1 | None | 95 |
| 90:2 "a'type | Fh-lask |  | Orafting Unit | Reflector | 811 | A21/IF | 100 | 1 | None | 100 |
| 91530 "6 trype | FM-task |  | Dest Unit | Fieflector | CWF | F1518/CM | 15 | 8 | Oallast (low PF) | 35 |
| $90400^{\circ} c^{\circ}$ 'rype | Fh-task |  | Desk Unit | Reflector | IN | Sll hi intensity | $y \quad 40$ |  | Wone | 40 High intensity unit |
| 9050 -d trype | FM-task |  | Dest Unat | Reflector | 1110 | Al9/IF | 110 | i | Mone | 75 |
| $90511^{\text {ce }}$ 'type | FM-tast |  | Dest Unit | Lapp Shade | IN | A21/IF | 206 | 1 | Mone | 200 |
| $90592^{\text {a }}$ 905 $0^{\circ}$ type | FM-task |  | Desk Unit | Lapp Shade | If | A21/1F | 100 | 1 | Mone | 100 |
| 9055] "e 'trpe | FM-task |  | Desk Unit | Lasp Shade | III | A21/1F | $75: 100$ | 2 | None | 175 |
| 10010 "Actype | IF-FM |  | Above Shell | Prisatic lens | UWF | F40TI2/RS/MIM | 40 | 4 | STD 8allast | 174 |
| $100200^{\circ} 8{ }^{\text {ctitype }}$ | If-FS |  | Floor lorchere | None | (1) | A21150/100/1501 | 150 | 1 | None | 150 |
| $10030{ }^{\circ} \mathrm{C}$ 'type | 18-MMT | Linear | Celling Mash | Cove | WUF | F40FI2/RS/MIW | 40 | 1 | STO 8allast | 54 |
| $10031{ }^{\circ} C^{\circ}$ 'type | IF-unt | Linear | Ceiling Mash | Cove | WMF | F40TI2/RS/MM | 40 | 2 | STO dalliast | 89 |
| $10040{ }^{\circ} \mathrm{C}$ 'type | IF- $\mathrm{HRT}^{\text {IF }}$ | Linear | Ceiling Mash | Cove | WMF | F30112/RS/MW | 30 | 1 | 5Id 8allast | 44 |
| 10041 ${ }^{\circ} 0^{\prime \prime}$ 'type | IF-Wht | Linear | Ceiling Mash | Cove | UWF | F20112/m | 20 | 1 | Irigger start | 29 low pomer factor assused |
| $10042{ }^{\circ} \mathrm{C}$ 'type | IF-Whit | Linear | Ceiling Mash | Cove | WHF | F20112/my | 20 | 2 | Irigger start | 42 low power factor assuaed |
| $10050{ }^{\circ} 0{ }^{\circ}$ type | REC-IM |  | Recessed Cans | Cove | IN | 840 Spot | 150 | , | Mone | 150 |
| $10060{ }^{\circ} \mathrm{d}^{\circ} \mathrm{type}$ | Fl-tast |  | Under Shell Unit | Prisatic lens | CWF | F40712/RS/CW | 40 | 1 | STO Pallast | 51 |
| $10061{ }^{\text {a }}$ ' ${ }^{\text {chape }}$ | Fi-task |  | Under Shelf Unit | Priseatic lens | WMF | FGOTI2/RS/M以 | 40 | 1 | STD dallast | 51 |
| $100622^{\circ} \mathrm{a}^{\text {ctype }}$ | OF-Mnt |  | Mall Panel | Prisatic lens | WMF | F40TI2/RS/MM | 40 | 1 | STO Oailast | 51 |
| $10070{ }^{\circ} \mathrm{B}$ 'type | FM-task |  | Desk Unit | Lamp Shade | IM | A21 150/100/1501 | 150 | 1 | None | 150 |
| $10071{ }^{\circ} \mathrm{b}$ 'trpe | FH-task |  | Dest Unit | Laep Shade | In | A 21 150/200/2501 | 250 | 1 | Wone | 250 |
| $10080{ }^{\circ} \mathrm{c}$ 'type | FH-task |  | Orafting Unit | Reflector | CWF/IM | FC819/RS/CH \&AL | - 22.60 | 2 | Oailastilom PFi | 84 lom power factor |
| $10081{ }^{\circ} \mathrm{C}$ 'type | FM-task |  | Orafting Unit | Reflector | CWF/IM | FC8I9/RS/CH BAL9 | 9 22:67 | 8 | Ballastiliom PFI | 91 low power factor |
| $10090{ }^{\text {- }} \mathrm{d}$ "type | FM-task |  | Orafting Unit | Reflector | IM | A19/IF | 67 | 1 | Mone | $67$ |
| $10091{ }^{\text {d d }}$ - type | FM-task |  | Dratting Unit | Reflector | IN | Al9/IF | 52 | 1 | Wone | 52 |
| 10092 "d cippe | FM-task |  | Orafting Unit | Reflector | IH | Al9/IF | 60 | - | Mone | 60 |
| $11010{ }^{\circ} A^{\circ}$ type | DRF-LM | tinear | Recessed Ceiling | Prisadic lens | CWF | F40ti2/RS/CM | 40 | 2 | STD Ballast | 日8 |
| $11011{ }^{\circ} A^{\circ}$ type | DRF-LIM | linear | Recessed Ceiling | Prisatic Lens | CMF | F40TI2/RS/CN | 40 | 1 | STO Ballast | 53 |
| $11020{ }^{\circ} \mathrm{A}^{\circ}$ type | DRF-(M) | Linear | Recessed Ceiling | Prisatic Lens | CHF | F201t3/RS/CM | 20 | 1 | Irigger gtart | 29 |
| $11030{ }^{\circ} \mathrm{a}^{\circ}$ trpe | FH-task |  | Orafting Unit | Reflector | In | A19/IF | 40 | 1 | None | 40 |
| $110400^{\circ}{ }^{\circ}$ type | Fh-task |  | Desk Unit | Lanp Shade | III | Al9130/70/100) | 100 | 1 | None | 100 |
| $11050{ }^{\circ} \mathrm{c}^{\circ} \mathrm{type}$ | FM-task |  | Desk Unit | Mone | SWF | F15122/Sw | 15 | 1 | galiastliom Pri | 88 L Low power factor |
| $11058{ }^{\circ} c^{\circ}$ type | FM-task |  | Desk Unit | Mone | SUF | F151/2/Sw | 15 | 2 | gallastilow PFi | 35 Low power factor |
| $12019{ }^{\circ} \mathrm{A}^{\circ}$ lype | DRF-LV | $9 \cdot 14$ | Recessed Ceiling | Paratollc louver | MuF | F40Ti2/RS/W | 40 | 1 | SID Tandea mallast | 44.5 8allast shared by two units |
| $12018{ }^{\circ} A^{\circ}$ type | DRF-14 | $9 \cdot 14$ | Recessed Celling | Paratolic Louver | WUF | F40712/RS/MIW | 40 | 1 | STD daliast | 54. |
| $12020{ }^{\text {a }}{ }^{\circ} \mathrm{P}$ iype | DRF-IV | $9 \cdot 8$ | Recessed Ceiling | Parabolic Louver | WMF | F20112/RS/MW | 20 | 1 | Irigger start | 29 Low power factor |
| 12030 ${ }^{\circ}{ }^{\circ} \mathrm{typ}$ type | Fi-task |  | Under Shelf Unit | Prisatic Lens | CMF | F40512/RS/CU | 40 |  | STD Ballast | 51 |
| $120311^{\circ} \mathrm{a}^{\circ}$ trye | FI-8ask |  | Under Shelf Unit | Prisatic lens | mar | F40FI2/RS/WM | 40 | 1 | STD Ballast | $5!$ |
| $180400^{\prime \prime} \mathrm{H}^{\text {ctrpe }}$ | FM-task |  | Drafting Unit | Reflector | IVI | R-20 | 50 | 1 | Mone | 50 |
| $820811^{\circ} 6$ "8ype | FM-task |  | Oratting Unit | Reflector | 81 | A19/IF | 60 | 1 | Mone | 60 |
| $12050{ }^{\circ}{ }^{\text {c }}$ 'type | FM-tast |  | Drafting Unit | Reflector | CWF/IM | FCer9/CH E Al9 | 22 86 | 2 | Galiastion Pr: | 84 |
| \$2051 ${ }^{\circ} \mathrm{c}$ "type | FM-t ask |  | Orafting Unit | Reflector | CWF/IM | FC8T9/CH \& A19 | 22 \% 75 | 2 | dallast (lom PF) | 99 |
| $12052{ }^{\circ} \mathrm{c}$ 'type | FM-task |  | Orafting Unit | Reflector | CWF/IM | Fcerg/cu : Al9 | 22-100 | 2 | Oallastllow PFI | 124 |
| 12060 | FM-task |  | Dest Unit | Lasp Shade | IM | A19130/70/1008 | 100 | 8 | Mone | 100 |
| $13010{ }^{\text {a }}$ A ${ }^{\text {a }}$ 19pe | ORF-L 4 | $2 \times 4$ | Recessed Ceiling | Low Brightness Lve | duF | F90T12/RS/mu/wn | 34 | 3 | 2-ES Ballast | 112 |
| $13011{ }^{\circ}{ }^{\text {a }}$ - $13012{ }^{\circ}{ }^{\circ}$-type | DRF-LV | 2 x 4 | Recessed Ceiling | Low Brightness lyr | UMF | F80TI2/RS/Wy/W | 34 | 2 | ES Ballest | 70 |
| $13012{ }^{\circ} \mathrm{A}^{\circ} \mathrm{type}$ | ORF-LV | 2×4 | Recessed Celling | Low irightness Lvr | WHF | F40TI2/RS/WM/WM | 38 | 1 | ES Dellast | 42 |
| 13n30 ${ }^{\text {a }}$ 'type | ORF-LM Fl-tast | $2 \times 4$ | Recessed Ceiling | Prisatic Lens | WMF | FSOII2/RS/WU/WK | 34 | 3 | 2-ES Baliast | 111 |
| $130400^{\circ} \mathrm{b}$ 'type | FM-tast |  | Under Shell Unit Orafting Unit | None Rellector | WMF | F.901I2/RS/Wแ/Wh A2IIIF | 34 100 | 8 | ES Dallast | 40 |
| $13041{ }^{\text {ce }}$ 'type | FH-tast |  | Drafting tinit | Retlector | in | A19/IF | 100 75 | 1 | Mone | 100 75 |
| $13050{ }^{\circ} \mathrm{c}^{\text {ctype }}$ | Fh-task |  | Desk Unit | Reflector | CWF | F1518/CM | 15 | $\downarrow$ | yallastijom PFI | 22 2-t.os ballastis lane out |

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## APPENDIX B: LIGHTING POWER DENSITIES BY WORK STATION

Notes:

WS - Work station identifier [3]
BLDG - Building identifer [3]
LTGSYS - Lighting system code
1 = direct recessed fluorescent w/ louvers 2 = direct recessed fluorescent w/ lenses 3 = direct surface mounted fluorescent w/ egg crates 4 = indirect fluorescent furniture mounted 5 = indirect fluorescent pendant mounted $6=$ direct/indirect fluorescent pendant mounted 7 = metal halide indirect pendant mounted $0=$ other or hybrid

LPD - Installed lighting power density, in $w / m^{2}\left(w / f t^{2}\right)$
LPDES - Alternate LPD with all energy saving lamps and ballasts in $w / m^{2}\left(w / f t^{2}\right)$

LPDSTD - Alternate LPD with all standard lamps and ballasts in $w / m^{2}\left(w / f t^{2}\right)$

LPDELSB - Alternate LPD with energy saving lamps and standard ballasts in $w / m^{2}\left(w / f t^{2}\right)$

LPDEBSL - Alternate LPD with energy saving ballasts and standard lamps in $w / \mathrm{m}^{2}\left(\mathrm{w} / f \mathrm{t}^{2}\right)$

The following listing of individual lighting power densities is presented in ascending order of estimated installed LPD, with the associated alternate (theoretical) power densities also listed. The alternate columns LPDES, LPDSTD, LPDELSB, and LPDEBSL are based on ANSI C82.2 input wattages alone, without the thermal factors applied; consequently, they are not directly compared to the installed LPD numbers. Also, there was no attempt made to evaluate the potential differences in measured light output attributable to the four alternate scenarios.


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12. KEY WORDS (Six to twelve entries: alphabetical order: capitalize only proper names; and separate key words by semicolons)

Lighting power density; unit power density; energy performance; lighting energy standards; occupant satisfaction
13. AVAILABILITYUnlimitedFor Official Distribution. Do Not Release to NTIS
Order
20402Order From National Technical Information Service (NTIS), Springfield, VA. 22161
14. NO. OF

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15. Price
\$1.3.95


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