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# Analysis of Results of Mini Round Robin Reflectance Test 

U.S. DEPARTIVENT OF COMMEPCE<br>National Bureau of Stardards<br>Thermal Processes Division<br>National Engineering Laboratory<br>Center for Chemical Engineering<br>- Washington, DC 20234

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## Introduction

A round-robin test of directional-hemispherical reflectance measurements was conducted by the National Bureau of Standards at the request of the Solar Energy Research Institute. Four national laboratories participated. Measurements were made of the directional-hemispherical reflectance of two samples, having high and low reflectance, respectively, in the wavelength range of 250 to 2500 nm .

Measured directional-hemispherical reflectance is used to compute solar reflectance of materials, and solar absorptance of opaque materials. The overall objective of the round-robin test was to obtain data on the performance of the several laboratories in making such measurements. Since all participants were national laboratories, it is to be expected that the accuracy of such measurements will approach the state of the art for measurements made with commercially available instruments.

## Participating Laboratories

The participating laboratories, in alphabetical order are:

1. Battelle Pacific Northwest Laboratories, Richland, Washington
2. National Bureau of Standards, Center for Building Technology, National Engineering Laboratory, Gaithersburg, Maryland (Mail address: Washington, D.C.)
3. Sandia National Laboratory, Albuquerque, New Mexico
4. Solar Energy Research Institute, Golden, Colorado

In addition to the above, the reference measurements on the samples to which the reported values were compared, were made in the Radiometric Physics Division of the Center for Radiation Research, National Measurement Laboratory of NBS. The high-accuracy reflectometer designed and built at NBS was used for these measurements.

## Preliminary Discussion

An integrating sphere reflectometer, the instrument used in evaluating directional-hemispherical reflectance, actually measures directional-near-hemispherical reflectance factor. Reflectance is defined as the ratio of reflected flux to incident flux. Reflectance factor is defined as the ratio of the flux reflected by a sample under specified conditions of irradiation and viewing, to that reflected by the ideal completely reflecting, isotropically diffusing surface. Such an ideal surface does not exist, but it is closely approximated by several materials which are near-perfect isotropic diffusers, and have high reflectance. If the reflectance of such a material is known, a correction can be made for its reflectance.

It is physically impossible to design an instrument that has true directional irradiance and hemispherical collection, because the solid angles of irradiance and collection are mutually exclusive. Some of the reflected flux is lost out the entrance aperture of the sphere, and some is lost out the detector aperture. The fraction of the flux lost in this manner is approximately equal to the ratio of the total area of all apertures to the total area of the sphere wall, apertures included. If the diameter of the apertures is small compared to the diameter of the sphere, the fractional losses will be small.

In a reflectance factor measurement in which a comparison standard of known reflectance is used, the flux losses through the ports will be exactly compensated for if the relative geometric (directional) distribution of the reflected flux is the same for sample and standard. If both sample and standard reflect diffusely, the losses will be nearly compensated.

For true geometrical conditions of hemispherical collection, reflectance factor is identically equal to reflectance. For diffusely reflecting samples, the measured directional-hemispherical reflectance factor will be identically equal to the directional-hemispherical reflectance if the ideal comparison standard is used, and the error will be smali if a real diffusely reflecting standard is used and a correction is made for the absolute reflectance of the standard.

Measurement of the absolute reflectance of a diffusely reflecting sample is difficult and time-consuming. It is normally done only by a primary standards laboratory, and then only at rather long intervals.

An integrating sphere reflectometer measures only the ratio of the reflectance factor of a sample to that of the comparison standard used in the measurement. The measured value will include uncertainties due to (1) the error, if any, in the reflectance value assigned to the comparison standard, (2) differences in the fractional flux losses out the ports, due to differences in the geometrical distributions of flux by the sample and reference, (3) nonlinearity of the detector-amplifier system, and (4) scattering in double-beam instruments, so that some of the flux in the reference beam is scattered into the sample beam, or vice versa. To this must be added an uncertainty due to the statistical fluctuation in the output of the instrument, usually referred to as noise.

With double-beam instruments, it is customary to run a $100 \%$ curve and a zero curve. The $100 \%$ curve is obtained with identical samples in the two beams. The zero curve is usually obtained when the sample beam is blocked before entering the sphere. A correction for deviation of the two curves from $100 \%$ and $0 \%$ respectively is made by use of the following equation.

$$
\begin{equation*}
R_{\lambda}=\frac{S_{\lambda^{-0}}{ }^{-0}}{H_{\lambda}{ }^{-0} \lambda} \tag{1}
\end{equation*}
$$

where $R_{\lambda}$ is the corrected directional-hemispherical reflectance factor, $S_{\lambda}$ is the sample reading, ${ }_{\lambda}$ is the zero curve reading, and $H_{\lambda}$ is the 100\% curve reading, all at wavelength $\lambda$.

The results of a round-robin test can be analyzed to give an estimate of the fractions of the total error that may be due to bias and random error, respectively, and may give some indication of the source of some of the bias.

## Samples for Measurement

The samples sent to the participants were black and white samples, either $50.8 \times 50.8 \mathrm{~mm}$ ( $2 \times 2$ inch) or $25.4 \times 25.4 \mathrm{~mm}$ ( 1 xl inch) for the black, and $50.8 \times 50.8 \mathrm{~mm}(2 \times 2$ inch) or $25.4 \times 76.2 \mathrm{~mm}$ ( $1-1 / 2 \times 3$ inch) for the white. The smaller samples were intended for measurement in instruments utilizing an Edwards-type integrating sphere in which the sample is held at the center of the sphere by a rod inserted through an aperture in the top of the sphere. The aperture in these spheres is too small to admit a $50.8 \times 50.8 \mathrm{~mm}$ ( $2 \times 2$ inch) sample. The black samples were of black porcelain enamel, with spectral directional-hemispherical reflectance in the range of about 0.06 to 0.11 in the wavelength range of 250 to 2500 nm . The white samples were white ceramic tile, with reflectance generally above 0.8 at wavelengths from about 500 to 2500 nm , dropping from about 0.8 at 500 nm to about 0.15 at 250 nm .

These samples were among those calibrated for directional-hemispherical reflectance in the Radiometric Physics Division of NBS.

## Data Requested

The data requested from all participants was the measured directionalhemispherical reflectance for near-normal incidence, including the specular component, and if possible, the same data for angles of incidence of $15,30,45$ and 60 degrees from normal. Data were requested at 10 nm intervals over as much of the wavelength range of 250 to 2500 nm as the measurement instrument was capable of providing. The instructions for the test are given in Appendix 1.

## Results of Measurements

The results reported by the different laboratories are shown in Table 1 for the white samples and Table 2 for the black samples, together with the calibration values for the sample measured in each case.

The values reported for the solar reflectance of the white sample and the solar absorptance of the black sample are given in Table 3. The procedures used to compute the solar properties are given in Table 4.

Because different samples were measured by each laboratory, direct comparison of the reported values is not justified. The calibration values for each sample at each wavelength are included in Table 1 in the column headed "Cal", and the algebraic difference between the calibration value and the reported value is included in the column headed "Diff".

The difference values obtained by subtracting the calibration value from the reported value were plotted as a function of wavelength as shown in figures 1 to 3 . The average differences for the white samples were about 0.029 for Lab 1, 0.012 for Lab 2, 0.019 for Lab 3 and 0.010 for Lab 4. The standard deviations associated with these values were about 0.02 for Lab 1, 0.01 for Lab 2, 0.012 for Lab 3 and 0.003 for Lab 4.

A review of figures 1 to 4 , where the data for the white samples are plotted, gives some clues to the errors that may be present in the reported values. Figure 1 shows that the data are slightly wavelength dependent. The average value of the difference is about 0.003 , and the standard deviation about 0.006 . The wavelength dependence and average difference suggests that the values assigned to the halon reference are in error, particularly at wavelengths below 600 nm .

Figure 2, showing the differences for Lab 2, indicates that the values assigned to the Halon reference are high at wavelengths below about 360 nm , and uniformly low by about . 0013 at wavelengths beyond about 400 nm .

Figure 3, showing the differences for Lab 3, indicates that the errors are unacceptably high at wavelengths of 800 to 850 nm and at 1380 nm , and at the very short wavelengths in the ultraviolet and at wavelengths beyond 1900 nm in the infrared. The peaks at about 820 nm and 1380 nm may be at the points where detectors were changed, and the signal-tpnoise ratio is small. The signal-to-noise ratio may also be small at the two ends of the spectral range. The comparison standard used for the measurements was not identified.

Figure 4, showing the differences for Lab 4, indicates that the value assigned to the pressed Halon comparison standard may be low by about 0.01 . The random error is the lowest of any of the laboratories.

The average differences for the black samples are about 0.005 for Lab 1, 0.002 for Lab 2, 0.004 for Lab 3 and -.005 for Lab 4, and the standard deviations are about 0.0013 for Lab 1, 0.0028 for Lab 2, 0.0043 for Lab 3 and 0.0037 for Lab 4.

Figure 5 is a plot of the differences for Lab 1 and shows an average difference of 0.0056 , and the standard deviation is about 0.0013 . The standard deviation is the lowest reported for the black samples, and indicates a very low random error. There is a slight tendency for the error to be greater at the short and long wavelengths. The bias in the data, of about $0.5 \%$, is much too large to be accounted for by an incorrect value for comparison standard, since the value assigned to the comparison standard would have to be about $8 \%$ high to account for such a large bias, and the data on the white sample indicates that such a large error is highly unlikely. The bias must be due to a zero line error. The equation used for reducing the data as reported by the investigator, does not show that a zero line correction was made.

Figure 6 shows that the bias in the results reported by Lab 2 is very low, which is also indicated by the average difference of 0.00178 , the lowest reported by any of the laboratories for the black samples. The standard deviation is about double that reported by Lab 1 . There is no marked variation of the differences with wavelength.

Figure 7 shows that there is an overall trend of increasing difference with wavelength. The peak at about 800 to 850 nm , which is very prominent in figure 3, is still present, but the peak at about 1380 nm , if present, is masked by the random error, which is the largest reported for a black sample, as indicated by the standard deviation of about 0.004 .

Figure 8 shows a slight trend toward increasing difference with wavelength. There is a very pronounced peak at about 900 nm and valley at about 1000 nm . This is near the wavelength where detectors are likely to be changed, and may be due to nonlinearity of the detectors in spectral regions where the response is low. The random error appears to be low, and the high standard deviation, 0.00433 , appears to be due largely to fluctuations of the difference with wavelength. Again, it appears likely that the observed differences are due to zero line errors.

The coefficient of variation, the ratio of the standard deviation to the mean, may be a more useful measure of the significance of the errors in the measured reflectances. These are shown in Table 5, in which the mean reflectance is taken-as the solar reflectance redorted by each laboratory. The values for the white samples range from $0.0038 \pm$ 0.0069 for Lab 1 to $0.0225 \pm 0.0140$ for Lab 3 , and for the black samples from $0.0250 \pm 0.0399$ for $\operatorname{Lab} 2$ to $-.0811 \pm .0524$ for Lab 1 . The average of the absolute values is $0.0128 \pm .00915$ for the white samples, and $0.0456 \pm 0.0432$. In each case the $\pm$ uncertainty is taken as one standard deviation. This is probably much too large for the uncertainty of the average values, for which the individual values vary from 47 to 220 , but may be more reasonable for the uncertainty in a single value at one wavelength. The reported data provided essentially no information on which a valid evaluation of the true random error could be based, which would involve multiple measurements at each wavelength with each reflectometer.

Within the limitations of the available data, the figures in Table 5 give an estimate of the state of the art in reflectance measurements in the participating laboratories.

Some general conclusions can be drawn from the results of this round-robin test. The bias in the reported values can be largely eliminated by proper use of the reflectance standards recently made available by
the National Bureau of Standards as SRM's 2019, 2020, 2021, and 2022 under the sponsorship of SERI. The errors are due partly to the use of incorrect reflectance values for the reference standards, and partly to $100 \%$ line and zero-line errors. The white standards can be used to check the values assigned to the reference standards, and also to evaluate the $100 \%$ errors. The black standards can be used to detect, and to help correct the zero line errors. The errors in the values reported by the participating laboratories are larger than were expected, and especially the errors in the measurement of solar absorptance. Such errors introduce rather large errors into the computations of the thermal efficiencies of solar collectors from the measured absorptance of the absorber.

## Appendix I

## Instructions for Round Robin Test

## 1. Preparation of Samples

The reflectance of the samples may be significantly affected by dirt or surface films that are not easily seen. They should be cleaned before measurement, using the following procedure.

The white samples are glazed ceramic tiles that have been cut to size. The ceramic body is porous, and would absorb water if not sealed. The back and edges have been sealed with an epoxy base masonry sealant. If this seal is breached, the sample may absorb water, particularly if immersed. Absorbed water will change the reflectance, primarily in the infrared. The samples should be handled gently to avoid chipping or a breach of the seal, and should never be immersed in water. Momentary exposure to water as described in the cleaning procedure will not affect them if the seal is not broken.

The cleaning procedure is as follows for both black and white samples.

1. Rinse with tepid tap water.
2. Wash with a dilute solution of a mild liquid soap, such as Ivory Liquid, ${ }^{1}$ using gentle rubbing with a soft cloth or rubber sponge. Never use on abrasive cleaner.
3. Rinse with tepid tap water, to remove soap.
4. Rinse with distilled water.
5. Blot dry with a fresh facial tissue. Do not rub.
6. Allow to air dry for at least 30 minutes before measuring.
${ }^{1}$ Any other noncorrosive liquid soap is also suitable for this use.

## Measurement Procedure

The data desired are the spectral directional-hemispherical reflectance for near-normal incidence, including the specular component. In addition, if you have the facilities, also the spectral directional-hemishperical reflectance for angles of incidence of $15,30,45$ and 60 degrees from normal, including the specular component.

1. Calibrate your reflectometer, using your normal procedure.
2. Measure the samples, using your normal procedure, making corrections as required.
3. Report data at 10 nm intervals over as much of the wavelength range of 250 to 2500 nm as your reflectometer can cover.
4. Compute solar reflectance of the white sample and solar absorptance of the black sample, using your normal procedures, and report the results.
5. Send the data to
J. C. Richmond

Room B126 Metrology
National Bureau of Standards
Washington, DC 20234
6. Include with the data a detailed description of all procedures used, including the manufacturer and model number of all instruments used, the method of reducing data, and the solar spectral distribution and method of computation used for computing solar properties.
table 1 - results of round robin test on white samples

| $\lambda$ | Lab 1 |  |  | Lab 2 |  |  | Lab 3 |  |  | Lab 4 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 m | 0 | Cal | Dife | $\bigcirc$ | Cal | Diff | - | Cal | Diff | $\bigcirc$ | Cal | Dife |
| 300 | . 134 | . 147 | -. 013 | . 1470 | . 147 | . 0000 | . 2126 | . 140 | . 0726 | . 1446 | . 147 | -. 0024 |
| 310 |  |  |  | . 1940 | . 190 | . 0040 | . 2212 | . 190 | . 0312 | . 1829 | . 190 | -. 0071 |
| 320 |  |  |  | . 2025 | . 238 | -. 0355 | . 2630 | . 238 | . 0250 | . 2365 | . 238 | -.0015 |
| 330 |  |  |  | . 3251 | . 303 | -. 0221 | . 3241 | . 303 | . 0211 | . 3063 | . 303 | . 0033 |
| 340 |  |  |  | . 3304 | . 377 | -. 0466 | . 3995 | . 377 | . 0225 | . 3082 | . 377 | . 0032 |
| 350 | . 437 | . 451 | -. 014 | . 4556 | . 460 | -. 0044 | . 4783 | . 460 | . 0183 | . 4620 | . 451 | . 0110 |
| 360 |  |  |  | . 5377 | . 541 | -. 0033 | . 5614 | . 541 | . 0204 | . 5438 | . 533 | . 0108 |
| 370 |  |  |  | . 6118 | . 608 | . 0038 | . 6266 | . 608 | . 0186 | . 6119 | . 601 | . 0109 |
| 380 |  |  |  | . 6616 | . 654 | . 0076 | . 6739 | . 654 | . 0199 | . 6593 | . 648 | . 0113 |
| 390 |  |  |  | . 7025 | . 690 | . 0125 | . 7096 | . 690 | . 0196 | . 6937 | . 684 | . 0097 |
| 400 | . 703 | . 714 | -. 011 | . 734 T | . 720 | . 0147 | . 7382 | . 720 | . 0182 | . 7245 | . 714 | . 0105 |
| 410 |  |  |  | . 7536 | . 737 | . 0166 | . 7537 | . 737 | . 0167 | . 7427 | . 731 | . 0117 |
| 420 |  |  |  | . 7663 | . 749 | . 0173 | . 7743 | . 749 | . 0253 | . 7520 | . 742 | . 0100 |
| 430 |  |  |  | . 7755 | . 757 | . 0185 | . 7736 | . 767 | . 0166 | . 7631 | . 751 | . 0121 |
| 440 |  |  |  | . 7807 | . 762 | . 0187 | .7782 | . 762 | . 0162 | . 7665 | . 756 | . 0105 |
| 450 | . 755 | . 761 | -. 006 | . 7824 | . 767 | . 0154 | . 7815 | . 767 | :. 0145 | . 7716 | . 761 | . 0106 |
| 460 |  |  |  | . 7890 | . 772 | . 0170 | . 7858 | . 772 | . 0138 | . 7770 | . 765 | . 0120 |
| 470 |  |  |  | . 7934 | . 776 | . 0174 | . 7891 | . 776 | . 0131 | . 7819 | . 770 | . 0119 |
| 480 |  |  |  | . 7994 | . 780 | . 0194 | . 7938 | . 780 | . 0138 | . 7867 | . 774 | . 0127 |
| 490 |  |  |  | . 8046 | . 787 | . 0176 | . 8010 | . 787 | . 0140 | . 7930 | . 781 | . 0120 |
| 500 | . 783 | . 787 | -. 004 | . 8114 | . 793 | . 0184 | . 8074 | . 793 | . 0144 | . 7993 | . 787 | . 0123 |
| 510 |  |  |  | . 8177 | . 799 | . 0187 | . 8125 | . 799 | . 0135 | . 8056 | . 793 | . 0126 |
| 520 |  |  |  | . 8229 | . 805 | . 0179 | . 8163 | . 805 | . 0113 | . 3111 | . 799 | . 0121 |
| 530 |  |  |  | . 8288 | . 811 | . 0178 | . 8217 | . 811 | . 0107 | . 8166 | . 805 | . 0116 |
| 540 |  |  |  | . 8339 | . 816 | . 0179 | . 8271 | . 816 | . 0111 | . 8231 | . 811 | . 0121 |
| 550 | . 813 | . 815 | -. 002 | . 8379 | . 820 | . 0179 | . 8295 | . 820 | . 0095 | . 8279 | . 815 | . 0129 |
| 560 |  |  |  | . 8816 | . 825 | . 0166 | . 8346 | . 825 | . 0096 | . 8322 | . 819 | . 0132 |
| 570 |  |  |  | . 8451 | . 829 | . 0161 | . 8383 | . 829 | . 0093 | . 8351 | . 824 | . 0111 |
| 580 |  |  |  | . 8464 | . 831 | . 0154 | . 8367 | . 831 | . 0057 | . 8359 | . 826 | . 0099 |
| 590 |  |  |  | . 8484 | . 834 | . 0144 | . 8427 | . 834 | . 0087 | . 3402 | . 829 | . 0112 |
| 600 | . 832 | . 833 | -. 001 | . 8546 | . 837 | . 0176 | . 8468 | . 837 | . 0098 | . 8451 | . 833 | . 0121 |
| 610 | - |  |  | . 8568 | . 839 | . 0178 | . 8484 | . 839 | . 0094 | . 8478 | . 835 | . 0128 |
| 6こ0 |  |  |  | . 8591 | . 842 | . 0171 | . 8523 | . 842 | . 0103 | . 8497 | . 836 | . 0137 |
| 530 |  |  |  | . 8610 | . 843 | . 0180 | . 8546 | . 843 | . 0116 | . 8503 | . 838 | . 0123 |
| 640 |  |  |  | . 8638 | . 846 | . 0178 | .. 8561 | . 846 | . 0101 | . 8513 | . 340 | . 0113 |
| 650 | . 0 ¢ 1 | . 838 | . 003 | . 8629 | . 344 | . 0189 | . 8567 | . 344 | . 0127 | . 8519 | . 838 | . 0139 |
| 660 |  |  |  | . 8628 | . 848 | . 0148 | . 8614 | . 848 | . 0134 | . 8561 | . 842 | . 0141 |
| 670 |  |  |  | . 8698 | . 851 | . 0188 | . 8646 | . 851 | . 0136 | . 3589 | . 844 | . 0149 |
| 580 |  |  |  | . 8722 | . 851 | . 0212 | . 8662 | . 851 | . 0152 | . 8609 | . 345 | . 0159 |
| 690 |  |  |  | . 8724 | . 853 | . 0194 | . 8660 | . 853 | . 0130 | . 8618 | . 847 | . 0148 |
| 300 | . 853 | . 851 | . 002 |  |  |  |  |  |  |  |  |  |
| 700 | . 854 | . 851 | . 003 | . 8745 | . 857 | . 0175 | . 8717 | . 857 | . 0147 | . 8642 | . 351 | . 0132 |
| 710 |  |  |  |  |  |  | . 8768 | . 858 | . 0188 | . 8667 | . 853 | . 0137 |
| 720 |  |  |  |  |  |  | . 8801 | . 859 | . 0211 | . 8690 | . 354 | . 0150 |
| 730 |  |  |  |  |  |  | . 8842 | . 860 | . 0242 | . 8699 | . 854 | . 0159 |
| 740 |  |  |  | . 8718 | . 861 | . 0108 | . 8877 | . 861 | . 0267 | . 8686 | . 855 | . 0136 |
| 750 | . 857 | . 856 | . 001 |  |  |  |  |  |  |  |  |  |
| 750 | . 858 | . 356 | . 002 |  |  |  | . 8903 | . 362 | . 0283 | . 8652 | . 856 | . 0092 |
| 760 |  |  |  |  |  |  | . 8986 | . 862 | . 0366 | . 8648 | . 856 |  |
| 770 |  |  |  |  |  |  | . 9008 | . 863 | . 0378 | . 3642 | . 857 | . 0072 |
| 780 |  |  |  | . 8768 | . 863 | . 0138 | . 9051 | . 363 | . 0421 | . 8628 | . 856 | . 0068 |
| 790 |  |  |  |  |  |  | . 9100 | . 861 | . 0490 | . 8636 | . 855 | . 0086 |
| 800 | . 856 | . 854 | . 002 |  |  |  |  |  |  |  |  |  |
| 800 | . 858 | . 854 | . 004 |  |  |  | . 9129 | . 860 | . 0529 | . 3637 | . 854 | . 0097 |
| 810 |  |  |  |  |  |  | . 9128 | . 862 | . 0508 | . 3604 | . 856 | . 0044 |
| 820 |  |  |  | . 8718 | . 860 | . 0118 | . 9136 | . 860 | . 0536 | . 8610 | . 354 | . 0070 |
| 830 |  |  |  |  |  |  | . 9129 | . 859 | . 0539 | . 8606 | . 853 | . 0076 |
| 840 |  |  |  |  |  |  | . 9100 | . 857 | . 0530 | . 8591 | . 852 | . 0071 |
| 850 | . 851 | . 850 | . 001 |  |  |  | . 9043 | . 856 | . 0483 | . 3588 | . 850 | . 0088 |
| 860 |  |  |  | . 8640 | . 855 | . 0090 | . 8977 | . 855 | . 0427 | . 8597 | . 349 | . 0107 |
| 870 |  |  |  |  |  |  | . 8860 | . 853 | . 0330 | . 8581 | . 847 | . 0111 |
| 880 |  |  |  |  |  |  | . 8780 | . 852 | . 0260 | . 8567 | . 846 | . 0107 |
| 890 |  |  |  |  |  |  | . 8692 | . 852 | . 0172 | 8549 | . 845 | . 0099 |


| $\lambda$ | Lab 1 |  |  | Lab 2 |  |  | Lab 3 |  |  | Lab 4 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 8 mm | $\rho$ | Cal | Diff | $\rho$ | Cal | Diff | $\bigcirc$ | Csl | Diff | $\bigcirc$ | Cal | Dife |
| 900 | . 847 | . 845 | . 002 | . 8576 | . 852 | . 0056 | . 8645 | . 852 | . 0125 | . 8560 | . 845 | . 0110 |
| 910 |  |  |  |  |  |  | . 8590 | . 853 | . 0060 | . 8566 | . 845 | . 0116 |
| 920 |  |  |  |  |  |  | . 8584 | . 853 | . 0054 | . 8575 | . 846 | . 0115 |
| 930 |  |  |  |  |  |  | . 8566 | . 853 | . 0036 | . 8574 | . 846 | . 0114 |
| 940 |  |  |  | . 8644 | . 853 | . 0114 | . 8564 | . 853 | . 0034 | . 8585 | . 846 | . 0125 |
| 950 | . 849 | . 846 | . 003 |  |  |  | . 8551 | :853 | . 0021 | . 8586 | . 846 | . 0126 |
| 960 |  |  |  |  |  |  | . 8576 | . 853 | . 0046 | . 8585 | . 846 | . 0125 |
| 970 |  |  |  |  |  |  | . 8578 | . 853 | . 0048 | . 8589 | . 847 | . 0119 |
| 980 |  |  |  | . 8685 | . 856 | . 0125 | . 8585 | . 856 | . 0025 | . 8595 | . 849 | . 0105 |
| 990 |  |  |  |  |  |  | . 8598 | . 856 | . 0038 | . 8624 | . 849 | . 0134 |
| 1000 | . 851 | . 851 | . 000 | - |  |  | . 8604 | . 858 | . 0024 | . 8631 | . 851 | . 0121 |
| 1010 |  |  |  |  |  |  | . 8618 | . 859 | . 0028 | . 8630 | . 852 | . 0110 |
| 1020 |  |  |  | . 8733 | . 860 | . 0133 | . 8652 | . 860 | . 0052 | . 8636 | . 853 | . 0106 |
| 1030 |  |  |  |  |  |  | . 8661 | . 860 | . 0061 | . 8631 | .854 | . 0091 |
| 1040 |  |  |  |  |  |  | . 8692 | . 861 | . 0082 | . 8626 | . 855 | . 0076 |
| 1050 | . 856 | . 856 | . 000 |  |  |  | . 8703 | . 861 | . 0093 | . 8625 | . 856 | . 0065 |
| 1060 |  |  |  | . 8708 | . 861 | . 0098 | . 8692 | . 861 | . 0082 | . 8626 | . 857 | . 0056 |
| 1070 |  |  |  |  |  |  | . 8709 | . 861 | . 0099 | . 8627 | . 857 | . 0057 |
| 1080 |  |  |  |  |  |  | . 8708 | . 862 | . 0088 | . 3627 | . 857 | . 0057 |
| 1090 |  |  |  |  |  |  | . 8698 | . 862 | . 0078 | . 8641 | . 857 | . 0071 |
| 1100 | . 860 | . 857 | . 003 | . 8698 | . 861 | . 0088 | . 8686 | . 361 | . 0076 | . 8650 | . 857 | . 0080 |
| 1110 |  |  |  |  |  |  | . 8670 | . 862 | . 0050 | . 8655 | . 857 | . 0085 |
| 1120 |  |  |  |  |  |  | . 8707 | . 865 | . 0057 | . 8665 | . 860 | . 0065 |
| 1130 |  |  |  |  |  |  | . 8742 | . 868 | . 0062 | . 8686 | . 862 | . 0066 |
| 1140 |  |  |  | . 8778 | . 869 | . 0088 | . 8748 | . 869 | . 0058 | . 8696 | . 864 | . 0056 |
| 1150 | . 867 | . 865 | . 002 |  |  |  | . 8783 | . 870 | . 0083 | . 8710 | . 865 | . 00650 |
| 1160 |  |  |  |  |  |  | . 8777 | . 871 | . 0067 | . 8716 | . 867 | .00~6 |
| 1170 |  |  |  |  |  |  | . 8795 | . 871 | . 0085 | . 8726 | . 867 | . 0056 |
| 1180 |  |  |  | . 8798 | . 871 | . 0088 | . 8812 | . 871 | . 0102 | . 8730 | . 866 | . 0070 |
| 1190 |  |  |  |  |  |  | . 8826 | . 371 | . 0116 | . 8740 | . 867 | . 0070 |
| 1200 | . 870 | . 867 | . 003 |  |  |  | . 8833 | . 872 | . 0113 | . 8740 | . 867 | . 0070 |
| 1210 |  |  |  |  |  |  | . 8823 | . 872 | . 0103 | . 8732 | . 867 | . 0062 |
| 1220 |  |  |  | . 8809 | . 872 | . 0089 | . 8828 | . 872 | . 0108 | . 8732 | . 867 | . 0052 |
| 1230 |  |  |  |  |  |  | . 8818 | . 872 | . 0098 | . 8737 | . 867 | . 0067 |
| 1240 |  |  |  |  |  |  | . 8827 | . 871 | . 0117 | . 8737 | . 867 | . 0067 |
| 1250 | . 872 | . 868 | . 004 |  |  |  | . 8826 | . 872 | . 0106 | . 8741 | . 868 | . 0061 |
| 1260 |  |  |  | . 8806 | . 873 | . 0076 | . 8852 | . 373 | . 0122 | . 8737 | . 968 | . 0057 |
| 1270 |  |  |  |  |  |  | . 8834 | . 871 | . 0124 | . 8736 | . 367 | . 00 万6́ |
| 1280 |  |  |  |  |  |  | . 8817 | . 871 | . 0107 | . 8723 | . 367 | . 0053 |
| 1290 |  |  |  |  |  |  | . 8798 | . 871 | . 0088 | . 8722 | . 867 | . 0052 |
| 1300 | . 870 | . 866 | . 004 | . 8791 | . 870 | . 0091 | . 3806 | . 870 | . 0106 | . 8732 | . 866 | . 0072 |
| 1310 |  |  |  |  |  |  | . 8809 | . 870 | . 0109 | . 3726 | . 866 | . 0066 |
| 1320 |  |  |  |  |  |  | . 8807 | . 870 | . 0107 | . 8731 | . 866 | . 0071 |
| 1330 |  |  |  |  |  |  | . 8800 | . 870 | . 0100 | . 8726 | . 866 | . 0055 |
| 1340 |  |  |  | . 8838 | . 869 | . 0148 | . 8806 | . 869 | . 0116 | . 8726 | . 866 | . 0066 |
| 1350 | . 870 | . 865 | . 005 |  |  |  | . 8837 | . 869 | . 0147 | . 8727 | . 865 | . 0077 |
| 1360 |  |  |  |  |  |  | . 8875 | . 869 | . 0185 | . 8710 | . 865 | . 0060 |
| 1370 |  |  |  |  |  |  | . 8916 | . 869 | . 0226 | . 8710 | . 865 | . 0060 |
| 1380 |  |  |  | . 8831 | . 867 | . 0161 | . 9116 | . 367 | . 0446 | . 8699 | . 364 | . 0059 |
| 1390 |  |  |  |  |  |  | . 9074 | . 866 | . 0414 | . 8711 | . 862 | . 0091 |
| 1400 | . 866 | . 862 | . 004 |  |  |  | $\text { . } 8939$ | $.366$ | . 0279 | $.8691$ | $.362$ |  |
| 1410 |  |  |  |  |  |  | . 8859 | . 867 | . 0189 | . 3702 | . 863 | . 0072 |
| 1420 |  |  |  | . 8832 | . 867 | . 0162 | . 8848 | . 867 | . 0178 | . 8697 | . 863 | . 0067 |
| 1430 |  |  |  |  |  |  | . 8830 | . 868 | . 0150 | . 8707 | . 863 | . 0077 |
| 1440 |  |  |  |  |  |  | . 8846 | . 867 | . 0176 | . 8712 | . 863 | . 0082 |
| 1450 | . 869 | . 863 | . 006 |  |  |  | . 8836 | . 867 | . 01606 | . 8708 | . 363 | . 0078 |
| 1460 |  |  |  | . 8833 | . 867 | . 0163 | . 8826 | . 867 | . 0156 | . 8707 | . 863 | . 0077 |
| 1470 |  |  |  |  |  |  | . 8831 | . 866 | . 0171 | . 8707 | . 862 | . 0087 |
| 1480 |  |  |  |  |  |  | . 8825 | . 865 | . 0175 | . 8702 | . 861 | . 0092 |
| 1490 |  |  |  |  |  |  | . 8806 | . 863 | . 0176 | . 8701 | . 359 | . 0111 |
| 1500 | . 864 | . 859 | . 005 | . 8741 | . 863 | . 0111 |  | $.863$ | $.0140$ |  | $.859$ |  |
| 1510 |  |  |  |  |  |  | . 8818 | . 867 | . 0148 | . 8722 | . 864 | $.0082$ |
| 1520 |  |  |  |  |  |  | . 8848 | . 869 | . 0158 | . 8747 | . 866 | . 0087 |
| 1530 |  |  |  |  |  |  | . 8851 | . 871 | . 0141 | . 8747 | . 866 | . 0087 |
| 1540 |  |  |  | . 8830 | . 871 | . 0120 | . 8858 | . 871 | . 0148 | . 3748 | . 866 | . 0088 |


| $\lambda$ |  | Lab 1 |  | Lab 2 |  |  | Lab 3 |  |  | Lab 4 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| na | $\rho$ | Cal | Diff | $\bigcirc$ | Cal | Diff | $\bigcirc$ | Cal | Diff | - | Cal | D1f\% |
| 1550 | . 874 | . 867 | . 007 |  |  |  | . 8876 | . 871 | . 0166 | . 8748 | . 367 | . 0078 |
| 1560 |  |  |  |  |  |  | . 8874 | . 871 | . 0164 | . 8752 | . 867 | . 0082 |
| 1570 |  |  |  |  |  |  | . 8873 | . 871 | . 0163 | . 8752 | . 867 | . 0082 |
| 1580 |  |  |  | . 8.888 | . 872 | . 0167 | . 8884 | : 872 | . 0164 | . 8766 | . 867 | . 0096 |
| 1580 |  |  |  |  |  |  | . 8876 | . 872 | . 0156 | . 8761 | . 868 | . 0081 |
| 1600 | . 873 | . 868 | . 005 |  |  |  | . 8877 | . 872 | . 0157 | . 8766 | . 868 | . 0086 |
| 1610 |  |  |  |  |  |  | . 8875 | . 872 | . 0155 | . 8766 | . 868 | . 0086 |
| 1620 |  |  |  | . 8841 | . 872 | . 0121 | . 8877 | . 872 | . 0157 | . 8761 | . 868 | . 0081 |
| 1630 |  |  |  | - |  |  | . 8873 | . 871 | . 0163 | . 8753 | . 367 | . 0083 |
| 1640 |  |  |  | - |  |  | . 8884 | . 872 | . 0164 | . 8753 | . 867 | . 0083 |
| 1650 | . 873 | . 867 | . 006 |  |  |  | . 8878 | . 872 | . 0158 | . 8753 | . 867 | . 0083 |
| 1660 |  |  |  | . 8836 | . 872 | . 0116 | . 8883 | . 872 | . 0163 | . 8757 | . 867 | .002\% |
| 1670 |  |  |  |  |  |  | . 8887 | . 872 | . 0167 | . 8758 | . 867 | . $00 \% 8$ |
| 1680 |  |  |  |  |  |  | . 8899 | . 872 | . 0179 | . 8757 | . 367 | . 008 \% |
| 1690 |  |  |  |  |  |  | . 8883 | . 871 | .0173 | . 8749 | . 867 | . 0079 |
| 1700 | . 872 | . 867 | . 005 | . 8840 | . 871 | . 0130 | . 8900 | . 871 | . 0190 | . 8753 | . 867 | . 0023 |
| 1710 |  |  |  |  |  |  | . 8892 | . 871 | . 0182 | . 8749 | . 867 | . 0079 |
| 1720 |  |  |  |  |  |  | . 8894 | . 871 | . 0184 | . 8753 | . 866 | . 0093 |
| 1730 |  |  |  |  |  |  | . 8885 | . 870 | . 0185 | . 8743 | . 866 | . 0083 |
| 1740 |  |  |  | . 8821 | . 870 | . 0121 | . 8871 | . 870 | . 0171 | . 8744 | . 865 | . 0092 |
| 1750 | . 871 | . 865 | . 006 |  |  |  | . 8869 | . 870 | . 0169 | . 8733 | . 865 | . 20 ¢? |
| 1760 |  |  |  |  |  |  | . 8856 | . 870 | . 0156 | . 8743 | . 365 | . 0n9? |
| 1770 |  |  |  |  |  |  | . 8862 | . 870 | . 0162 | . 8742 | . 855 | . 004 - |
| 1780 |  |  |  | . 8826 | . 870 | . 0126 | . 8866 | . 870 | . 0166 | . 8738 | . 865 | . nos. |
| 1790 |  |  |  |  |  |  | . 8861 | . 870 | . 0161 | . 8738 | . 864 | . 0098 |
| 1800 | . 870 | . 865 | . 005 |  |  |  | . 8871 | . 870 | . 0171 | . 8739 | . 865 | .0n*9 |
| 1810 |  |  |  |  |  |  | . 8811 | . 869 | . 0121 | . 3738 | .8ヶ4 | . onc. |
| 1820 |  |  |  | . 8807 | . 868 | . 0127 | . 8868 | . 868 | . 0188 | . 8738 | . 8 ¢́3 | .010\% |
| 1830 |  |  |  |  |  |  | . 8846 | . 868 | . 0166 | . 8732 | . 863 | - 011$)$ |
| 1840 |  |  |  |  |  |  | . 8858 | . 867 | . 0188 | . 8724 | . 862 | .010* |
| 1850 | . 869 | . 861 | . 008 |  |  |  | . 8886 | . 866 | . 0226 | . 3709 | . 851 | .8090 |
| 1860 |  |  |  | . 8772 | . 865 | . 0122 | . 8887 | . 865 | . 0207 | . 8723 | . 861 | .0:13 |
| 1870 |  |  |  |  |  |  | . 8897 | . 865 | . 0247 | . 9672 | . 851 | .onk: |
| 1880 |  |  |  |  |  |  | . 8844 | . 861 | . 0234 | . 8671 | . 350 | .0:1: |
| 1890 |  |  |  |  |  |  | . 8784 | . 856 | . 0224 | . 8659 | . 352 | .0.130 |
| 1900 | . 857 | . 852 | . 005 | . 8682 | . 854 | . 0142 | . 8778 | . 854 | . 0233 | . 8606 | .85? | nosm |
| 1910 |  |  |  |  |  |  | . 8793 | . 856 | . 0233 | . 3601 | .85: | ma! |
| 1920 |  |  |  |  |  |  | . 8830 | . 860 | . 0230 | . 3631 | . 856 | .nn-1 |
| 1930 |  |  |  |  |  |  | . 8837 | . 862 | . 0217 | . 8650 | . 955 | . \% |
| 1940 |  |  |  | . 8807 | . 863 | . 0177 | . 8843 | . 863 | . 0213 | . 8686 | . 359 | . 00065 |
| 1950 | . 865 | . 859 | . 006 |  |  |  | . 8836 | . 863 | . 0206 | . 8705 |  |  |
| 1960 |  |  |  |  |  |  | . 8862 | . 865 | . 0212 | . 3701 | . 361 | .009! |
| 1970 |  |  |  |  |  |  | . 8892 | . 867 | . 0222 | . 3729 | . 862 | . 0117 |
| 1980 |  |  |  | . 8757 | . 867 | . 0087 | . 8903 | . 867 | . 0233 | . 8733 | . 563 | . 0103 |
| 1990 |  |  |  |  |  |  | . 8999 | . 868 | . 0319 | . 3744 | . 364 | .010' |
| 2000 | . 866 | . 863 | . 003 |  |  |  | . 8921 | . 869 | . 0231 |  |  |  |
| 2010 |  |  |  |  |  |  | . 8954 | . 869 | . 0264 | . 3776 | .364 | . 0136 |
| 2020 |  |  |  | . 8799 | . 870 | . 0099 | . 8980 | . 870 | . 0280 | . 8777 | . 865 | . 0127 |
| 2030 |  |  |  |  |  |  | . 9041 | . 870 | . 0341 | . 8784 | . 866 | .0124 |
| 2040 |  |  |  |  |  |  | . 9038 | . 870 | . 0338 | . 8776 | . 360 | . 0116 |
| 2050 | . 870 | . 865 | . 005 |  |  |  | . 9043 | . 870 | . 0343 | . 8791 | . 865 |  |
| 2060 |  |  |  | . 8787 | . 869 | . 0097 | . 9049 | . 869 | . 0359 | . 8781 | . 865 | . 0131 |
| 2070 |  |  |  |  |  |  | . 9079 | . 870 | . 0379 | . 8792 | . 365 | . $01-2$ |
| 2080 |  |  |  |  |  |  | . 9131 | . 870 | . 0431 | . 8798 | . 866 | . 0138 |
| 2090 |  |  |  |  |  |  | . 9088 | . 871 | . 0378 | . 3808 | . 867 | . 0138 |
| 2100 | . 874 | . 867 | . 007 | . 8872 | . 871 | . 0162 | . 9148 | . 871 | . 0438 | . 3804 |  |  |
| 2110 |  |  |  |  |  |  | . 9122 | . 873 | . 0392 | . 8811 | . 868 | . 0131 |
| 2120 |  |  |  |  |  |  | . 9156 | . 872 | . 0436 | . 8827 | . 868 | . 0147 |
| 2130 |  |  |  |  |  |  | . 9146 | . 870 | . 0446 | . 3798 | . 866 | . 0138 |
| 2140 |  |  |  | . 8828 | . 869 | . 0138 | . 9145 | . 869 | . 0455 | . 8775 | . 864 | . 0135 |
| 2150 | . 874 | . 863 | . 011 |  |  |  | . 9128 | . 867 | . 0458 |  |  |  |
| 2160 |  |  |  |  |  |  |  |  | . 0458 | . 8751 | . 861 | . 0141 |
| 2170 |  |  |  |  |  |  |  |  |  |  |  |  |
| 2180 |  |  |  | . 8769 | . 860 | . 0169 |  |  |  | . 87682 | . 8585 | . 013132 |
| 2190 |  |  |  |  |  |  |  |  |  | . 8641 | . 852 | . 0121 |

TABLE 1 - continued

tAble 2 - RESULTS OF ROUND ROBIN TEST ON BLACK SAMPLES

## 300 310

## 330

 340350


400
410
420
430
430
440
450
450
460
470
480
490





| 750 | $\begin{aligned} & .059 \\ & .059 \end{aligned}$ | $\begin{aligned} & .065 \\ & .065 \end{aligned}$ | $\begin{aligned} & -.006 \\ & -.006 \end{aligned}$ | . 0574 | . 065 | -. 0076 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 750 |  |  |  |  |  |  |
| 760 |  |  |  |  |  |  |
| 770 |  |  |  |  |  |  |
| 780 |  |  |  |  |  |  |
| 790 |  |  |  |  |  |  |
| 800 | . 060 | . 065 | -. 005 |  |  |  |


| 800 | .060 | .065 | -.005 |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 800 | .061 | .065 | -.004 |  |  |  | .078 |
| 810 |  |  |  | .0698 | .066 | .0038 | .07 |
| 820 |  |  |  | .068 |  |  |  |
| 830 |  |  |  |  |  |  | .07 |
| 840 |  |  |  |  |  |  | .07 |
| 850 | .065 | .068 | -.003 |  |  |  |  |
| 860 |  |  |  | .0676 | .069 | -.0014 | .07 |
| 870 |  |  |  |  |  |  | .07 |
| 880 |  |  |  |  |  |  | .07 |
| 890 |  |  |  |  |  |  | .07 |

Lab 1

Lab 2

- Cal Diff o Cal Diff

| .049 | .057 | -.008 | .0559 | .057 | -.0011 |
| :--- | :--- | :--- | :--- | :--- | :--- |

$\begin{array}{llllll}.049 & .057 & -.008 & .0559 & .057 & -.0011\end{array}$
.
.056
.057
.0
.0
.06
.06
.068
$64 \quad .070-$

Lab 4
Lab 3

| $\bigcirc$ | Cal | Diff | - | Cal | Diff |
| :---: | :---: | :---: | :---: | :---: | :---: |
| . 0701 | . 057 | . 0131 | . 0534 | . 057 | -. 0036 |
| . 0670 | . 057 | . 0100 | . 0534 | . 057 | -. 0036 |
| . 0658 | . 059 | . 0068 | . 0544 | . 059 | -. 0046 |
| . 0660 | . 059 | . 0070 | . 0574 | . 059 | -. 0016 |
| . 0668 | . 060 | . 0068 | . 0573 | . 060 | -. 0027 |
| . 0681 | . 060 | . 0021 | . 0563 | . 060 | -. 0037 |
| . 0694 | . 062 | . 0074 | . 0575 | . 062 | -. 0045 |
| . 0712 | . 063 | . 0082 | . 0605 | . 063 | -. 0025 |
| . 0741 | . 065 | . 0091 | . 0634 | . 065 | -. 0016 |
| . 0769 | . 068 | . 0089 | . 0643 | . 068 | -. 0037 |
| . 0770 | . 070 | . 0070 | . 0643 | . 070 | -. 0057 |
| . 0767 | . 071 | . 0057 | . 0652 | . 071 | -. 0058 |
| . 0759 | . 070 | . 0059 | . 0662 | . 070 | -. 0038 |
| . 0754 | . 070 | . 0054 | . 0663 | . 070 | -. 0037 |
| . 0749 | . 069 | . 0059 | . 0644 | . 069 | -. 0046 |
| . 0745 | . 069 | . 0055 | . 0645 | . 069 | -. 0045 |
| . 0744 | . 069 | . 0054 | . 0645 | . 069 | -. 0045 |
| . 0742 | . 069 | . 0052 | . 0635 | . 069 | -. 0055 |
| . 0736 | . 069 | . 0046 | . 0645 | . 069 | -. 0045 |
| . 0733 | . 068 | . 0053 | . 0634 | . 068 | -. 0046 |
| . 0727 | . 068 | . 0047 | . 0634 | . 068 | -. 0046 |
| . 0721 | . 068 | . 0041 | . 0644 | . 068 | -. 0036 |
| . 0718 | . 067 | . 0048 | . 0612 | . 067 | -. 0058 |
| . 0714 | . 067 | . 0054 | . 0613 | . 067 | -. 0057 |
| . 0711 | . 066 | . 0051 | . 0622 | . 066 | -. 0038 |
| . 0708 | . 066 | . 0048 | . 0613 | . 066 | -. 0047 |
| . 0704 | . 066 | . 0044 | . 0616 | . 066 | -. 0044 |
| . 0692 | . 065 | . 0042 | . 0614 | . 065 | -. 0036 |
| . 0685 | . 065 | . 0035 | . 0593 | . 065 | -. 0057 |
| . 0683 | . 064 | . 0043 | . 0603 | . 064 | -. 0037 |
| . 0678 | . 064 | . 0038 | . 0614 | . 054 | -. 0026 |
| . 0677 | . 064 | . 0037 | . 0625 | . 064 | -. 0015 |
| . 0675 | . 064 | . 0035 | . 0615 | . 064 | -. 0025 |
| . 0675 | . 064 | . 0035 | . 0605 | . 064 | -. 0035 |
| . 0674 | . 063 | . 0044 | . 0605 | . 063 | -. 0025 |
| . 0677 | . 063 | . 0047 | . 0624 | . 063 | -. 0006 |
| . 0678 | . 063 | . 0048 | . 0614 | . 063 | -. 0016 |
| . 0681 | . 063 | . 0051 | . 0624 | . 063 | -. 0005 |
| . 0685 | . 066 | . 0045 | . 0633 | . 064 | -. 0007 |
| . 0687 | . 064 | . 0047 | . 0634 | . 064 | -. 0006 |
| . 0666 | . 065 | . 0016 | .0614 | . 065 | -. 0035 |
| . 0683 | . 065 | . 0033 | . 0671 | . 065 | . 0021 |
| . 0673 | . 065 | . 0023 | . 0662 | . 065 | . 0012 |
| . 0677 | . 065 | . 0027 | . 0642 | . 065 | -. 0003 |
| . 0673 | . 065 | . 0023 | . 0643 | . 065 | -. 0007 |
| . 0701 | . 065 | . 0051 | . 0623 | . 065 | -. 0027 |
| . 0652 | . 065 | . 0002 | . 0624 | . 065 | -. 0026 |
| . 0677 | . 065 | . 0027 | . 0624 | . 065 | -. 0026 |
| . 0722 | . 065 | . 0072 | . 0624 | . 065 | -. 0025 |
| . 0716 | . 065 | . 0066 | . 0624 | . 065 | -. 0026 |
| . 0740 | . 065 | . 0090 | . 0624 | . 065 | -. 0026 |
| . 0762 | . 065 | . 0112 | . 0622 | . 065 | -. 0028 |
| . 0741 | . 066 | . 0081 | . 0643 | . 066 | -. 0017 |
| . 0763 | . 067 | . 0093 | . 0654 | . 067 | -. 0016 |
| . 0759 | . 067 | . 0089 | . 0665 | . 067 | -. 0005 |
| . 0756 | . 068 | . 0076 | . 0675 | . 068 | -. 0005 |
| . 0745 | . 069 | . 0055 | . 0694 | . 069 | . 0004 |
| . 0729 | . 070 | . 0029 | . 0714 | . 070 | . 0014 |
| . 0729 | . 072 | . 0009 | . 0733 | . 072 | . 0013 |
| . 0776 | . 073 | . 0046 | . 0753 | 073 | 0023 |

## nm 900 910 920 930 940



1000









1250
1260
1270
1280
1290

1300
1310
1320
1330
1340
～ぃぃぃぃぃ
1350
$\omega \underset{\omega}{\omega} \omega$
$0 \sim \sim$
0
0

1400
1410
1420
1430
1440

| いけんちゃ | トトトトゥ |
| :---: | :---: |
|  | －¢ \％ |
| OOOO | －0000 |

410

## 430


.069
.069
－． 00
.069
074
－．
.005

Lab 1
ค Cal Diff o
0
.071

| Cal | Diff |
| :---: | :---: |
| .074 | -.003 |

$.086 \quad .089 \quad-.003$
$.095 \quad .100 \quad-.005$
$.091 \quad .097 \quad-.006$
080


.071
.076
$-.076-.0$
0781

Cal Diff 0934 .0934
.07
.085
.085
.0084
01
$.080 \quad .085-.005 \quad .085$
（1）
.0763
067
072
$-.00$
$+0$
.0777

Lab
Lab 3


| 0 |
| :---: |
| ． 0781 |
| ． 0811 |
| ． 0805 |
| ． 0873 |
| ． 0920 |
| ． 0902 |
| ． 0933 |
| ． 0968 |
| ． 0968 |
| ． 1001 |


| Cal | Di |
| :--- | :--- |
| .074 | . |
| .077 | . |
| .079 | . |
| .082 | . |
| .085 | . |
| .089 | . |
| .092 | . |
| .095 | . |
| .099 | .- |

Diff

| ． 074 | ． 0041 |
| :---: | :---: |
| ． 077 | ． 0041 |
| ． 079 | ． 0015 |
| ． 082 | ． 0053 |
| ． 085 | ． 0070 |
| ． 089 | ． 0012 |
| ． 092 | ． 0013 |
| ． 095 | ． 0018 |
| ． 097 | －． 0002 |
| ． 099 | ． 0011 |
| ． 100 | －． 0016 | .1010 ：

.0961
2
.0960
.0953
.0901
.0904
.0903
$\lambda$

| nom | - | Cal | D1ff | - | Cal | Diff | - | Cal | Diff | - | Cal | D1fe |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1550 | . 102 | . 107 | -. 005 |  |  |  | . 1071 | . 107 | . 0001 | . 1037 | . 107 | -. 0033 |
| 1560 |  |  |  |  |  |  | . 1077 | . 108 | -. 0003 | . 1057 | . 108 | -. 0023 |
| 1570 |  |  |  |  |  |  | . 1107 | . 108 | . 0027 | . 1057 | . 108 | -. 0023 |
| 1580 |  |  |  | . 1136 | . 109 | . 0046 | . 1152 | . 109 | . 0062 | . 1058 | . 109 | -. 0032 |
| 1590 |  |  |  |  |  | . | . 1103 | . 109 | . 0013 | . 1058 | . 109 | -. 0032 |
| 1600 | . 105 | . 110 | -. 005 |  |  |  | . 1124 | 110 | . 0024 | . 1058 | . 110 | -. 0042 |
| 1610 |  |  |  |  |  |  | . 1126 | . 110 | . 0026 | . 1059 | . 110 | -. 0041 |
| 1620 |  |  |  | . 1183 | . 110 | . 0083 | . 1144 | . 110 | . 0044 | . 1058 | . 110 | -. 0042 |
| 1630 |  |  |  |  |  |  | . 1158 | . 111 | . 0048 | . 1057 | . 111 | -. 0052 |
| 1640 |  |  |  |  |  |  | . 1149 | . 111 | . 0039 | . 1057 | . 111 | -. 0053 |
| 1650 | . 106 | . 111 | -. 005 | - |  |  | . 1161 | . 111 | . 0051 | . 1057 | . 111 | -. 0053 |
| 1660 |  |  |  | . 1186 | . 111 | . 0076 | . 1188 | . 111 | . 0078 | . 1057 | . 111 | -. 0053 |
| 1670 |  |  |  |  |  |  | . 1194 | . 111 | . 0084 | . 1067 | . 111 | -. 0043 |
| 1680 |  |  |  |  |  |  | . 1156 | . 111 | . 0046 | . 1067 | . 111 | -. 0043 |
| 1690 |  |  |  |  |  |  | .1171 | .111 | . 0061 | . 1066 | . 111 | -. 0044 |
| 1700 | . 107 | . 111 | -. 004 | . 1136 | . 111 | . 0026 | . 1183 | . 111 | . 0073 | . 1056 | . 111 | -. 0054 |
| 1710 |  |  |  |  |  |  | . 1198 | . 111 | . 0088 | . 1056 | . 111 | -. 0054 |
| 1720 |  |  |  |  |  |  | . 1174 | . 111 | . 0064 | . 1057 | . 111 | -. 0053 |
| 1730 |  |  |  |  |  |  | . 1154 | . 111 | . 0044 | . 1046 | . 111 | -. 0064 |
| 1740 |  |  |  | . 1155 | . 111 | . 0045 | . 1132 | . 111 | . 0022 | . 1036 | . 111 | -. 0074 |
| 1750 | . 105 | . 110 | -. 005 |  |  |  | . 1143 | . 110 | . 0043 | . 1026 | . 110 | -. 0074 |
| 1760 |  |  |  |  |  |  | . 1133 | . 110 | . 0023 | . 1017 | . 110 | -. 0083 |
| 1770 |  |  |  |  |  |  | . 1118 | . 110 | . 0018 | . 1007 | . 110 | -. 0093 |
| 1780 |  |  |  | . 1124 | . 109 | . 0034 | . 1067 | . 109 | -. 0023 | . 1007 | .109 | -. 0083 |
| 1790 |  |  |  |  |  |  | . 1123 | . 109 | . 0033 | . 0997 | . 109 | -. 0093 |
| 1800 | . 104 | . 109 | -. 005 |  |  |  | . 1103 | . 109 | . 0013 | . 0996 | . 109 | -. 0094 |
| 1810 |  |  |  |  |  |  | . 1093 | . 108 | . 0013 | . 0987 | . 108 | -. 0093 |
| 1820 |  |  |  | . 1083 | . 108 | . 0003 | . 1050 | . 108 | -. 0030 | . 0978 | . 108 | -.0092 |
| 1830 |  |  |  |  |  |  | . 1159 | . 107 | . 0089 | . 0978 | . 107 | -.0092 |
| 1840 |  |  |  |  |  |  | . 1113 | . 107 | . 0043 | . 0978 | . 107 | -. 0092 |
| 1850 | . 101 | . 106 | -. 005 |  |  |  | . 1052 | . 106 | -. 0008 | . 0969 | . 106 | -. 0091 |
| 1860 |  |  |  | . 1096 | . 106 | . 0036 | . 1083 | . 106 | . 0023 | . 0960 | . 106 | -. 0100 |
| 1870 |  |  |  |  |  |  | . 1032 | . 105 | -. 0018 | . 0956 | . 105 | -.0094 |
| 1880 |  |  |  |  |  |  | . 1074 | . 105 | . 0024 | . 0966 | . 105 | -.nos: |
| 1890 |  |  |  |  |  |  | . 1015 | . 104 | -. 0025 | . 0965 | . 104 | -.0075 |
| 1900 | . 098 | . 104 | -. 006 | . 1065 | . 104 | . 0025 | . 1085 | . 104 | . 0045 | . 0963 | . 104 | -.00-- |
| 1910 |  |  |  |  |  |  | . 1083 | . 104 | . 0043 | . 0961 | . 104 | -.00:9 |
| 1920 |  |  |  |  |  |  | . 0984 | . 103 | -. 0046 | . 0953 | . 03 | -.097: |
| 1930 |  |  |  |  |  |  | . 1109 | . 103 | . 0079 | . 0943 | . 103 | -.008 |
| 1940 |  |  |  | .1043 | . 102 | . 0023 | . 1085 | . 102 | . 0065 | . 0933 | . 102 | -. 0178 - |
| 1950 | . 095 | . 102 | -. 007 |  |  |  | . 1041 | . 102 | . 0021 | . 0943 | . 102 | -.007 |
| 1960 |  |  |  |  |  |  | . 1076 | . 102 | . 0056 | . 0943 | . 102 | -.007 |
| 1970 |  |  |  |  |  |  | . 1083 | . 102 | . 0063 | . 0952 | . 102 | -. 0068 |
| 1980 |  |  |  | . 1020 | . 101 | . 0010 | . 1077 | . 101 | . 0067 | . 0951 | . 101 | -. 00057 |
| 1990 |  |  |  |  |  |  | . 1017 | . 101 | . 0007 | . 0951 | . 101 | -. 0059 |
| 2000 | . 094 | . 101 | -. 007 |  |  |  | . 1045 | . 101 | . 0035 | . 0930 | . 101 | -. 0030 |
| 2010 |  |  |  |  |  |  | . 1032 | .101 | . 0022 | . 0929 | . 101 | -. 0081 |
| 2020 |  |  |  | . 1045 | . 100 | . 0045 | . 1087 | . 100 | . 0087 | . 0918 | . 100 | -. 0082 |
| 2030 |  |  |  |  |  |  | . 1058 | . 100 | . 0058 | . 0926 | . 100 | -.0074 |
| 2040 |  |  |  |  |  |  | . 0966 | . 099 | -. 0024 | . 0935 | . 099 | -. 0055 |
| 2050 | . 093 | . 099 | -. 006 |  |  |  | . 1112 | . 099 | . 0122 | . 0934 | . 099 | -. 0056 |
| 2060 |  |  |  | . 1060 | . 099 | . 0070 | . 0857 | . 099 | -. 0133 | . 0933 | . 099 | -. 0057 |
| 2070 |  |  |  |  |  |  | . 1024 | . 099 | . 0034 | . 0932 | . 099 | -. 0058 |
| 2080 |  |  |  |  |  |  | . 0977 | . 099 | -. 0013 | . 0932 | . 099 | -. 0058 |
| 2090 |  |  | - |  |  |  | . 1076 | . 098 | . 0096 | . 0932 | . 098 | -. 0048 |
| 2100 | . 092 | . 098 | -. 006 | . 1011 | . 098 | . 0031 | . 1012 | . 098 | . 0032 | . 0922 | . 098 | -. 0053 |
| 2110 |  |  |  |  |  |  | . 0960 | . 098 | -. 0020 | . 0920 | . 098 | -. 0060 |
| 2120 |  |  |  |  |  |  | . 0988 | . 098 | . 0008 | . 0920 | . 098 | -. 0060 |
| 2130 |  |  |  |  |  |  | . 2051 | . 097 | . 0081 | . 0908 | . 097 | -. 0062 |
| 2140 |  |  |  | . 0966 | . 097 | -. 0004 | . 1000 | . 097 | . 0030 | . 0907 | . 097 | -. 0063 |
| 2150 | . 091 | . 097 | -. 006 |  |  |  | . 1350 | . 097 | . 0380 | . 0890 | . 097 | -. 0080 |
| 2160 |  |  |  |  |  |  |  |  |  | . 0894 | . 096 | -. 0066 |
| 2170 |  |  |  |  |  |  |  |  |  | . 0895 | . 096 | -. 0065 |
| 2180 |  |  |  | . 0991 | . 095 | . 0041 |  |  |  | . 0897 | . 095 | -. 0053 |
| 2190 |  |  |  |  |  |  |  |  |  | . 0898 | . 095 | -. 0052 |

TAOLLE 2 - continued


## TABLE 3 - REPORTED VALUES FOR SOLAR PROPERTIES

| Property | Lab $1^{1}$ | Lab $2^{2}$ | Lab $3^{3}$ | Lab 4 | NBS |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | \% | \% | \% | \% |  |
| Reflectance of White Sample | 82.5 | 87.1 | 84.3 | $\begin{aligned} & 81.06^{4} \\ & 83.66^{5} \\ & 83.77 \\ & 80.40 \end{aligned}$ | $\begin{aligned} & 81.94^{8} \\ & 83.33^{9} \end{aligned}$ |
| Absorptance of Black Sample | 93.1 | 92.9 | 92.5 | $\begin{aligned} & 93.04^{4} \\ & 92.98{ }^{4} \\ & 92.07 \end{aligned}$ | 92.44 |

1. Beckman 5270 Spectroreflectometer - Halon powder
2. Beckman 5270 double-beam grating-filter instrument with high intensity source
3. Varian Cary 17D integrating sphere reflectometer
4. Perkin-Elmer 340 - Halon standards
5. Beckman 5420 - Halon standards
6. Beckman $5420-\mathrm{BaSO}_{4}$ standard
7. Cary 17 - Halon standard
8. For Comparison to Laboratories 1 and 4
9. For Comparison to Laboratories 2 and 3

## TABLE 4 - PROCEDURES USED FOR CCMPUTING SOLAR PROPERTIES

```
Laboratory 1 - 100 Selected Ordinate Method, based on Thekaekara AM 1.5 solar spectral irradiance.
Laboratory 2 - Weighted Ordinate Method, based on NASA AM 1.5 TDSSID.
Laboratory 3 - ASTM E-424, Method A, Weighted Ordinate Method based on Parry Moon data.
Laboratory 4 - Weighted Ordinate Method, based on proposed revision of ASTM E-424.
NBS - 100 Selected Ordinate Method, based on ASTM E-44 direct solar irradiance.
```

TABLE 5 - DIFFERENCES AS FRACTION OF REPORTED SOLAR VALUES

| Diff | 0.0038 | 0.0133 | 0.0225 | 0.0118 |
| :--- | :--- | :---: | :---: | :---: |
| $\sigma$ | 0.0069 | 0.0119 | 0.0140 | 0.0038 |
|  |  | BLACK SAMPLES - SOLAR ABSORPTANCE |  |  |
| Diff | -0.0033 | 0.0019 | 0.0039 | 0.0057 |
| $\sigma$ | 0.0060 | 0.0030 | 0.0047 | 0.0039 |



Figure 1 - Difference between the data reported by Laboratory 1 and the calibration data for the white sample, plotted as a function of wavelength.


Figure 2 - Difference between data reported by Laboratory 2 and calibration data for the white sample, plotted as a function of wavelength.


Figure 3 - Difference betwaen data reported by Laboratory 3 and calibration data for the white sample, plotted as a function of wavelength.


Figure 4 - Difference between data reported by Laboratory 4 and calibration data for the black sample, plotted as a function of wavelength.


Figure 5 - Difference between the data reported by Laboratory 1 and the calibration data for the black sample, plotted as a function of wavelength.


Figure 6 - Difference between the data reported by Laboratory 2 and calibration data for the black sample, plotted as a function of wavelength.


Figure 7 - Difference between the data reported by Laboratory 3 and the calibration data for the black sample, plotted as a function of wavelength.


Figure 8 - Difference between data reported by Laboratory 4 and the calibration data for the balck sample, plotted as a function of wavelength.
4. TITLE AND SUBTITLE

Analysis of Results of Mini Round Robin Reflectance Test
5. AUTHOR(S)

Joseph C. Richmond
6. PERFORMING ORGANIZATION (If joint or other than NBS, see in structions)
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Solar Energy Research Institute, Golden, CO 80401
10. SUPPLEMENTARY NOTES
$\qquad$ Document describes a computer program; SF-185, FIPS Software Summary, is attached.
11. ABSTRACT (A 200-word or less factual summary of most significant information. If document includes a significant bibliography or literature survey. mention it here)
A mini round robin test was conducted in which four national laboratories participated. The spectral directional-hemispherical reflectance for near-normal incidence of two samples, one black and one white, was measured in the wavelength range of 250 to 2500 nm . The solar reflectance of the white sample and the solar absorptance of the black sample was then computed. Each laboratory used a different procedure for making the computations. The measured samples had previously been calibrated in the Radiometric Physics Division of the National Bureau of Standards for certification as reflectance standards. The average difference between the reported values and the calibration values varied from $+0.0116 \pm 0.0634$ to $0.0386 \pm 0.0205$ for the white samples and from $-0.00475 \pm 0.00366$ to $+0.003 \overline{5} 7 \pm 0.00433$ for the black samples. The differences for the white samples were ascribed primarily to errors in the reflectance value assigned to the reference standard used in the measurements The differences for the black samples were ascribed primarily to zero line errors.
12. KEY WORDS (Six to twelve entries; alphabetical order: capitalize only proper names; and separate key words by semicolons) diffuse reflectance; directional-hemispherical reflectance; integrating spheres; laboratory intercomparisons; reflcctance measurements; reflectance standards; solar properties of materials; spectral reflectance measurements.

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