

Sheets

NBSIR 78-1418 (NASC)(R)

Stress Corrosion Behavior of X2048 T851 Aluminum Alloy

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Washington, D.C. 20234

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Prepared for
Naval Air Systems Command
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U.S. DEPARTMENT OF COMMERCE, Juanita M. Kreps, *Secretary*

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NATIONAL BUREAU OF STANDARDS, Ernest Ambler, *Acting Director*

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ALUMINUM ALLOY

BY

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Reference: (a) Naval Air Systems Command, Department of the Navy,
request by AIR-52031G.

Introduction

An experimental high strength aluminum alloy designated X2048-T851 has been reported to have good resistance to stress corrosion cracking. Reference (a) requested that NBS conduct tests to determine the stress corrosion behavior of the alloy in a marine atmosphere environment.

Material

An X2048-T851 aluminum alloy plate section with dimensions 3 in. (7.6 cm) thick x 12 in. (30.5 cm) long transverse direction x 6 in. (15.2 cm) rolling direction was obtained from the manufacturer (Reynolds Metals Company).

Metallography

Sections were obtained from the sample for metallographic examination. In general, the microstructure (Figure 1) was typical of that normally associated with aluminum alloys in the -T851 temper, i.e., solution heat-treated, stretched (cold worked) and then artificially aged.

Mechanical Properties

The results of tests conducted by NBS to determine the transverse mechanical properties of the alloy are given in Table 1.

Specimen Preparation

Fourteen 9 in. (22.9 cm) transverse flat test specimens and twelve 2 in. (5.1 cm) transverse round tensile specimens were machined from the plate section.

Stress Corrosion Tests

Stressed and unstressed specimens were exposed at Kure Beach, NC [80 foot (24 m) lot]. A system of weights and levers was used to obtain the desired stress on the 9 in. (22.9 cm) flat stress corrosion specimens, while a constant strain system was utilized to obtain the applied stress on the 2 in. (5.1 cm) round test specimens. The specimens exposed in the marine atmosphere were exposed with an applied stress equivalent to 0%, 50%, and 75% of the yield strength of the alloy as determined by NBS (Table 1).

Results

None of the flat stress corrosion specimens or the round tensile specimens failed after exposures of 770 days and 1130 days respectively. Visual examination of all of the specimens after exposure revealed the presence of heavy adherent gray corrosion products with considerable localized pitting corrosion. Companion unstressed specimens which had been exposed for the same period of time were removed from exposure along with the stressed samples. In order to obtain an indication of the effect of corrosion attack on the alloy, a comparison was made of the properties of unexposed specimens vs. those of specimens exposed in the marine environment. The values obtained were then averaged and calculated as the percent loss in tensile strength due to exposure in the environment. The results are given in Table 2, and indicate a small loss in tensile

strength (5.6% to 6.1%) for the 2 in. (5.1 cm) round specimens and 2.0% to 3.2% loss in tensile strength for the 9 in. (22.9 cm) flat test samples. The loss in tensile strength may be attributed to the reduction in area due to the pitting corrosion observed.

Conclusions

The aluminum alloy 2048 T851 as supplied to NBS appears to be resistant to stress corrosion cracking when exposed in a marine atmosphere environment for periods of up to 1130 days. The alloy's strength, however, was reduced slightly as a result of general corrosion and localized pitting.



Figure 1. Microstructure of 2048-T851
Aluminum alloy. Etched Keller's etch X100.

TABLE 1

Mechanical Properties of 2048-T851 as determined by N.B.S.

Specimens	Tensile Strength Ksi (a)	Yield Strength (0.2% offset) Ksi (a)
2" Round	65.2	58.8
9" Flat	66.2	59.5

(a) 1Ksi = 6.8948 MPa

TABLE 2
Average Loss in Tensile Strength After Exposure

Specimens Type	Exposure Time Marine Atmosphere	Applied Stress during exposure % Yield Strength	Tensile Strength after exposure Ksi (a) (b)	Yield Strength after exposure Ksi (a) (b)	Percent Loss in tensile strength after exposure (b)	% Elongation
2" Round	1130 days	0	61.2	55.4	6.1	-
		50	61.6	56.1	5.6	-
		75	61.2	55.9	6.1	-
9" Flat	770 days	0	64.1	58.5	3.1	4%
		50	64.8	58.2	2.0	4%
		75	64.0	57.9	3.2	4%

(a) 1 Ksi = 6.8948 MPa

(b) average of (3) specimens

U.S. DEPT. OF COMM. BIBLIOGRAPHIC DATA SHEET		1. PUBLICATION OR REPORT NO. NBSIR 78-1418 (NASC)	2. Gov't Accession No.	3. Recipient's Accession No.
4. TITLE AND SUBTITLE Stress Corrosion Behavior of X2048 T851 Aluminum Alloy			5. Publication Date January 1978	6. Performing Organization Code
7. AUTHOR(S) B. T. Sanderson and W. F. Gerhold			8. Performing Organ. Report No.	
9. PERFORMING ORGANIZATION NAME AND ADDRESS NATIONAL BUREAU OF STANDARDS DEPARTMENT OF COMMERCE WASHINGTON, D.C. 20234			10. Project/Task/Work Unit No. 3120410	11. Contract/Grant No.
12. Sponsoring Organization Name and Complete Address (Street, City, State, ZIP) Naval Air Systems Command Department of the Navy Washington, D.C. 20360			13. Type of Report & Period Covered	
			14. Sponsoring Agency Code	
15. SUPPLEMENTARY NOTES				
16. ABSTRACT (A 200-word or less factual summary of most significant information. If document includes a significant bibliography or literature survey, mention it here.) Short transverse tensile specimens of X2048-T851 aluminum alloy were stressed at zero, fifty and seventy-five percent of the alloy's yield strength and exposed in a marine atmosphere environment. After 1130 days exposure, there were no failures. X2048-T851 alloy appears to be resistant to stress corrosion cracking in this environment.				
17. KEY WORDS (six to twelve entries; alphabetical order; capitalize only the first letter of the first key word unless a proper name; separated by semicolons) Alloy; aluminum; atmosphere; marine; mechanical properties; plate; stress corrosion				
18. AVAILABILITY <input type="checkbox"/> Unlimited <input checked="" type="checkbox"/> For Official Distribution. Do Not Release to NTIS <input type="checkbox"/> Order From Sup. of Doc., U.S. Government Printing Office Washington, D.C. 20402, SD Cat. No. C13 <input type="checkbox"/> Order From National Technical Information Service (NTIS) Springfield, Virginia 22151			19. SECURITY CLASS (THIS REPORT) UNCLASSIFIED	21. NO. OF PAGES
			20. SECURITY CLASS (THIS PAGE) UNCLASSIFIED	22. Price

NBSIR 78-1419 R

Life Test Development for Clothes Dryers

Julius Cohen

Institute for Applied Technology
National Bureau of Standards
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Interim Report

October 1976 - September 1977



U.S. DEPARTMENT OF COMMERCE

NATIONAL BUREAU OF STANDARDS

NBSIR 78-1419

**LIFE TEST DEVELOPMENT FOR
CLOTHES DRYERS**

Julius Cohen

Institute for Applied Technology
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Washington, D.C. 20234

Interim Report

October 1976 - September 1977

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(Normally the door is closed; it is open here for illustration.)
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(Normally the door is closed; it is open here for illustration.)

1. Introduction

The objective of this ongoing work is to demonstrate the feasibility of developing standardized laboratory test methods for estimating useful life* and associated performance-based characteristics--e.g., failure modes** and reliabilities--of major appliances. Other performance testing work generally is made on components for an arbitrary duration of time, and a complete system may be tested for only a fraction of its expected life.

The electric clothes dryer has been chosen for initial work because of its relative electromechanical simplicity. The program is threefold: 1) laboratory test development; 2) energy efficiency testing; 3) controlled field testing. The emphasis of the work is on 1); 2) is an ancillary undertaking in which the time dependence of energy efficiency is being investigated; 3) is quite limited in extent, and is being done to elucidate field testing problems and methodology; it is not expected to yield definitive results. This publication reports on the progress of the program to date.

2. Test Planning: Constraints & Strategy

The test planning, like all other aspects of the testing, is guided closely by a methodology formulated in anticipation of carrying out work such as this: product life testing. The highlights only of the test design are given in this section; for a detailed listing of procedural steps followed, see NBSIR 76-1157 (Chapter 12).

2.1 Restatement of objective

Different make clothes dryers have many superficial similarities, yet they are sufficiently different in design, materials, and construction to render a mixed sampling heterogeneous; (see, for example, Appendix A: Comparison of typical components for various make dryers). Thus, the primary objective of the present work can be restated specifically as the development of a standardized test method for estimating useful life and associated performance-based characteristics of a heterogeneous sampling of electric clothes dryers.

* Useful life is defined as the period of satisfactory reliability measured from the time the product is first put into service (for a discussion of this concept see NBSIR 76-1157). Admittedly it is subjective, but so is the concept of satisfactory performance, which must and is being dealt with.

** Failure modes here means the prevailing, or most frequent failures.

Owing to the heterogeneity, it is not possible to test the different makes identically, and this complicates test development. However, identicalness is not required. Standardized, or uniform, testing requires that different makes receive equivalent, unbiased treatment, with due regard to the prevailing use conditions of each.

2.2 Sample selection

The laboratory facilities available for this work limited testing to a maximum of 16 dryers. Rather than test one or two dryers of many makes -- the results would be of doubtful significance -- 8 dryers each of the two most popular makes, representing over 50% of the home market, were chosen. Although lot sampling was used where feasible, the present sampling cannot strictly be considered random. Nevertheless, it may still be representative of the population at large.

Implementation of the adjunctive controlled field testing required that the dryers be limited to eight in number. All were chosen from a single make from the same lots which were to undergo laboratory testing. Half were placed in very high use situations the other half in average use situations, for control.

2.3 Practical considerations

Clothes dryers are long-lived machines: their life expectancy is greater than 14 yrs. Obviously, laboratory testing must be completed within a small fraction of that (real) time.

The average-size household of four uses a dryer about 400 times (cycles) a year for ~30 minutes per cycle. In the laboratory, the test cycles need to be run continually (a test cycle consists of dryer on period, followed by an off period). Also, labor considerations generally require unattended operation for the major amount of time; i.e., other than the normal work hours. Intensive testing as outlined here can be implemented only if operation is substantially automated.

In summary, testing must be intensive (around-the-clock, if possible); machines must be automated for restarting and must be capable of running unattended for long durations. Notwithstanding, dryers are supposed to be maintained by frequent removal of lint from the filters. Accordingly this latter condition presents a challenge, as will be discussed subsequently.

2.4 Type of testing

Because no historical data regarding failure modes and times to failure were available, it was decided to simulate, as far as

practicable in the laboratory, use in the home. An attempt was made to keep the principal stresses normal so that failure modes and total use times would also be normal, thus providing a benchmark.

2.5 Data sought

Data sought for presentation at the conclusion of this project are:

- o Test method specifications for (electric) clothes dryer life.
- o Identification of factors which under - or overstress components.
- o Years of equivalent life simulated in the laboratory.
- o Description of maintenance actions.
- o Numbers and types of failure; failure modes; times to failure; reliability; estimated useful life; repair actions.
- o Time dependence of energy efficiency.
- o Life of test load.

2.6 Performance criteria

The primary performance criterion is drying ability; i.e., the ability to remove moisture from a specified load within a specified time, satisfactorily.

A secondary criterion is that the load not be abnormally degraded, as determined by visual inspection, by the dryer per se; e.g., burn spots or abrasion.

Failure occurs if either criterion is not met.

2.7 Use conditions

Formulation of use conditions (including load) was aided by availability of extensive private-sector market research data. Three types of load are specified here:

- 1) a normal, or average-weight load;
- 2) a customarily-expected overload;
- 3) an abrasive/impact load. Table 1, below, lists load compositions together with specified drying times and use

frequencies in percent -- loads are expendable* and costing was a factor in selection.

Table 1. Load compositions, drying times, & use frequencies

Type of load	Composition	Drying time	Use frequency (%)
normal-weight	1 doz. towels, 0.5 x 1 m (~20 x 40 in) 2.5 + 0.1 kg (5 1/2 + 1/4 lb.) 86% cotton 14% polyester	make-A ^a : 40-0 min. ⁺² make-B ^a : 45-0 min. ⁺²	90
customarily-expected overload	double the normal weight load, above	70 + 2 min.	5
abrasive/impact	1 doz. metal buttons riveted to 0.33kg/m ² (10 oz./sq.yd) cotton denim, ~ 0.6 x 0.75m (24 x 30 in) 30 + 2 min. (after folding in half and hemming)		5

^a The drying times for the two makes are required to be different. Additionally, the last 10 minutes of the drying cycle of make-A is run without heat, while for make-B, the last 5 minutes of the cycle is run without heat.

No data were available regarding environmental conditions of dryers in the field. In the laboratory, dryers were tested at whatever temperatures and relative humidities prevailed.

2.8 Energy efficiency

The time dependence of energy efficiency is to be investigated by making measurements on dryers as new, and periodically thereafter as they age. The Department of Energy Test** is being used because it is state-of-the-art.

* The survival time of towels against degradation by drying has been found to be ~600 hours.

** "Clothes Dryer Test Procedure", Federal Register, dated September 14, 1977, Vol. 42, No. 178, pg. 46145.

2.9 Field testing

Controlled-field testing will be used to monitor both performance and energy efficiency. In case of failure, repairs will be made by qualified (NBS) personnel. Energy efficiency will be measured shortly after installation and periodically thereafter at six month intervals.

2.10 Recording data

Forms were devised, preparatory to the experimental work, for the systematic and comprehensive recording of data. These are: 1) failure report, 2) failure analysis, 3) field installation, 4) energy test; and examples are given in Appendix B. 1) in particular is operational in the sense that it initiates a systematic course of action from the initial allegation of failure, to inspection, and finally to disposition or corrective action, if required; 2) is used for dryer failures other than early, where the cause is not readily discernable; 3) is used to identify the recipient, and to record safety test data; 4) is used for energy efficiency tests in the laboratory and in the field.

3. Instrumentation

Each dryer is instrumented with a cycle counter and an elapsed time meter to register total operating time. Dryers for the field have an additional elapsed time meter installed across the heater element for estimation of energy consumption.

In the laboratory, each dryer is equipped with a control box -- of which a circuit diagram is shown in figure 1 -- used in automatizing the following: 1) recycling of dryers; 2) rewetting of loads at the start of each drying cycle; and 3) discontinuation of recycling in the event of water leaks (associated with dryer failure).

1) Figure 2 is a photograph of the control panel of dryer make-A, as equipped for automatic recycling. A motor mounted above the timer knob (left) advances the timer to the desired setting and a solenoid above the start button pushes down. Figure 3 is a more detailed view of the mechanism used to advance the timer. When activated by the control box, a one rpm electric motor turns the dryer timer knob through a mechanical coupling. The angular displacement, or time setting, is determined by means of an adjustable cam which actuates a microswitch to stop the motor. For the starting operation, a solenoid is used to depress a plunger which rests on the start push button.

Figure 4 is a photograph of the control panel of dryer make-B, as equipped for automatic recycling; the timer is at the right, and the start switch at the left. The automation instrumentation is similar to

that used for make-A, except for starting, the solenoid is mechanically coupled to pull the start switch instead of pushing down.

2) Immediately after a dryer is started, a metered amount of water is squirted into the drum of the closed dryer, and onto the tumbling load of towels; thus, the load is fairly uniformly wetted. The water-squirting system consists in sequence of 1) an on-off rotary valve at the source; 2) filter; 3) main line solenoid valve (normally energized to remain open); 4) pressure regulator; 5) pressure gauge; and 6) water pipe to the dryers. Coming off the water pipe at each dryer station is a solenoid valve coupled to a flexible length of plastic tubing, connected in turn at the dryer, to a small copper tubing (nominal 1/8" o.d., 0.030" wall thickness). The amount of water dispensed is a function of the water pressure, pipe dimensions, and time. The pressure is held constant by means of the regulator so that the quantity of water is adjusted by regulating the time.

Figures 5 and 6 show respectively, makes A and B equipped for squirting. (Normally doors are closed; they are opened here for illustration.) For make-A, the tubing enters at the bottom (for ease of installation); approaches, but does not extend to the rim of the drum; and is directed to squirt upwards and to the right into the tumbling load. The copper tubing is terminated with neoprene tubing to prevent possible load damage. For make-B, on the other hand, the tubing enters at the top and is directed to squirt downward and to the right into the drum. (A prior arrangement similar to that used for make-A was found to be unsatisfactory because water from the squirt tube would be deflected by the tumbling load into the lint filter and blower assembly, as well as out the door.)

3) Under each dryer, at a strategic location for early warning, is fastened a small pan containing a water sensor. In case of leaks due to dryer failure, the sensor will signal the control box not to restart the affected dryer (the dryer cycle in progress, however, will run to completion).

In the event of leaks due to solenoid valve failures at the dryers, additional sensors positioned near the front of each dryer will activate an independent control box, thus closing the main solenoid valve to the water supply. The dryers will continue to recycle, but with unwetted loads.

4. Experimental Procedure

4.1 Performance

Compositions of the various type loads, together with their drying-time settings and use frequencies have been given in Sect. 2.7. An abridged procedure for running these loads is given

below; all tests are made with dryer temperature set at HIGH, or NORMAL.

4.1.1 Normal-weight load

For attended operation normal-weight loads are placed in each of 16 dryers; clean lint filters are installed, and the on-off switches of the individual dryer control boxes and the master timer are turned ON. Groups of four dryers each will be activated sequentially and automatically at 15 minute intervals, and will be recycled every 60 minutes thereafter. At activation, first the dryer timer is rotated to the prescribed setting, then the machine is started and simultaneously a metered amount of water, 75-80% by weight relative to the nominal weight of the dry load, is ejected for approximately two minutes onto the tumbling load for uniform wetting. At the completion of the drying cycle the machine turns off for 15 or 20 minutes, depending on make, until being automatically restarted. The attendant frequently cleans the lint filters.

Owing to design differences it is found necessary to use different methods for running the different makes unattended for long times. For make-A, (clean) filters may be left in the machine overnight; for weekend runs, the filters are removed and the lint collected in a filter external to the machine. For make-B, a special auxiliary filter, developed for this work, is installed in the normal air stream to extend the filtering capacity sufficiently to run the dryers overnight -- it is essential, however, that the towels not be new or old, as these are very prolific generators of lint. At present it is not feasible to run make-B dryers weekends -- attempts to run with the filter removed were unsuccessful -- and development work to meet such an objective is continuing.

4.1.2 Overload

Running the customarily-expected overloads requires operator action. Two dozen towels, or double the normal-weight load, are placed in the dryers, and the amount of water to be dispensed may be doubled also by resetting the timer on the individual control boxes to twice that used for the normal-weight load. As before, control boxes and master timer are switched ON; when machines start automatically, the operator advances the timers to 70 minutes (this obviates cool-down). Recycling will occur every 60 minutes.

4.1.3 Abrasive/impact load

The special test cloths are thoroughly wetted in a clothes washer (new cloths are first washed twice with detergent and thoroughly rinsed, to remove sizing), and spin dried to completion of the spin cycle. One test cloth is placed in each dryer, and the control box switches are turned OFF to disengage the automatic restart system. The operator sets the dryer timer and pushes the start button.

4.1.4 Monitoring

Several times each day, dryness of the loads is monitored tactually*, soon after the drying cycles are completed. In case of failure, repairs are carried out, repair data are recorded, and the unit is restored to test.

Drum linings are visually inspected after running impact/abrasive loads, for signs of degradation.

4.2 Energy efficiency

For measurements of energy efficiency the test procedure previously cited, is being used. Thirty-three pieces of special test cloth of 50% cotton - 50% polyester composition are spin dried in a washer, then tumble dried in a dryer, both to prescribed tolerances of moisture content. For procedural details see the test procedure cited; for details of the quantities measured, as well as the method for calculating energy efficiency, see Form LCP-4, Energy Test, in the Appendix to this report. The tests are being carried out periodically in the laboratory with different small samplings each time, and in the field.

4.3 Field testing

Dryers are checked for safety 1) in the laboratory, after being instrumentated and, 2) in the field, after being installed; for details see Form LCP-3, Field Installation Report, in the Appendix. Subsequently, qualified laboratory personnel carry out periodic energy efficiency tests, and make repairs when necessary.

* For better reproducibility, it is planned to replace this subjective determination by one based on weighing.

5. Results

5.1 Performance

Laboratory testing began, for all practical purposes, some six months ago, and since then, make-A dryers have logged six years of equivalent life* and make-B, four years of equivalent life. There have been three bona-fide dryer failures: one early, and two random, all with make-A. Failed components were a timer, a timer knob, and a heater element.

5.2 Energy efficiency

Thus far, energy efficiencies measured in the laboratory show little or no change with simulated age of dryers. The value is roughly $1 \text{ kg(H}_2\text{O)}/\text{kWh}$, with make-B appearing slightly more efficient.

5.3 Field testing

Dryers were placed in the field about five months ago, and there have been no reports of failure. Energy efficiencies measured shortly after installation were similar to those measured in the laboratory before installation.

6. Discussion

The reliability of the dryers so far has been high, as was expected for an established and slowly evolving product. The dryers are now in their random failure period of life where reliability is maximum, and appreciable failures are not expected until well into life, when parts wear out.

On the other hand, the automation system, new and untried, required considerable debugging. Most problems appear to have been corrected with the exception of the water injection system: leaks or flooding occurs frequently owing to malfunctioning solenoid valves. The primary cause of failures, however, appears to be the water supply itself, or specifically, the mineral salts dissolved therein. These precipitate in the pipe, then migrate as particles to the solenoid valves and prevent complete closure. Corrective action will be attempted: it is planned to install a water softener, and to use another kind of valve which may be less sensitive to debris.

An important finding has been made already in field testing. At one site the initial energy efficiency measured was about 20% lower than expected. Investigation showed the existent ductwork to have been improperly installed; this led eventually to substantial accumulation of trapped lint, and as a consequence, appreciable decrease in air flow. Cleaning the lint from inside the ductwork restored energy

*Based on 416 cycles per year. In the laboratory work the average duration of a cycle is 40 min., in the field it is a 30 min., and the difference is due to the types of load.

efficiency to a normal value. Improperly installed ductwork can lead to decreased energy efficiency and higher operating costs, as well as failure to dry.

A reminder: This is a test development project being made from scratch and modifications in procedure and instrumentation may be expected before its completion.

Appendix A

Comparison of typical components for various make dryers

Make	1	2	3	4	5	6
Heater (240V)	expanded Nichrome foil	Nichrome coils	Nichrome coils	Nichrome coils	Nichrome coils	Nichrome coils
Drum materials	polymer on steel	polymer on steel	porcelain	stainless steel	polymer on steel	porcelain
Drum suspension	rear: rollers front: plastic to felt; circular	rear: rollers front: plastic to felt; circular	axial rear bearing front: nylon glides	axial rear bearing front: glides	rear: rollers front: felt; circular	axial rear bearing front: glides (top)
Motor (115V)	1/3 H.P. 1725 RPM	1/3 H.P. 1725 RPM	1/4 H.P. 1725 RPM	1/6 H.P. 1725 RPM	1/4 H.P. 1725 RPM	1/4 H.P. 1725 RPM
Belt, Motor to-Blower	None	None	None	1	None	None
Timer	rotary switch + solid state	electro-mechanical	electro-mechanical	electro-mechanical	electro-mechanical	electro-mechanical

Appendix B
Forms for reporting data

- LCP-1 Failure report
- LCP-2 Failure analysis report
- LCP-3 Field installation report
- LCP-4 Energy test for clothes dryer

FAILURE REPORT

1. No. _____

NOTIFICATION

2. System _____ 3. Ident. _____ 4. Environmental _____

5. Unit _____ 6. Unit oper. time _____ A. _____ Lab

A. _____ Inoperative A. _____ Hr. elapsed B. _____ Field

B. _____ Intermittent B. _____ Cycle no.

C. _____ Other

7. Symptoms _____

8. Originator _____ Ext. _____ 9. Date _____

INSPECTION

10. Tests performed, results, comments _____

11. Confirmation _____ 12. Causes _____

A. _____ Yes A. _____ Defective part D. _____ Secondary

B. _____ No B. _____ Testing error E. _____ Other

C. _____ Primary

13. Analysis required _____ 14. Part operating time to failure _____

A. _____ Yes _____ Hr

B. _____ No _____ Cycle

15. Cognizant engineer _____; Ext. _____ 16. Date _____

ACTION

16. Describe corrective action taken (list parts replaced, part nos.) _____

17. Active repair time _____ hr 18. Repairman _____ 19. Date _____

20. Date returned to test _____ 21. Associated failure reports _____

FAILURE ANALYSIS REPORT

LCP-2

REFERENCE INFO.	System	Ident.	Assoc. Failure Report No.
Part description		Part Mfr. & Part No.	
What was reported wrong? (FAILURE INDICATOR)			
LABORATORY INSTRUCTIONS	Perform following tests, in order:		
TESTS RESULTS			
			By
			Date
ANALYSIS FINDINGS	MODE	MECHANISM	
Probable Failure Cause			
RESPONSIBILITY: _____ Mfr. _____ User. Explain			
FAILURE CLASSIFICATION	_____ Early _____ Random _____ Wear Out _____ Aging		
MTBF _____	Hr. _____	Cycles	
EFFECT OF FAILURE ON SYSTEM			
_____ Complete loss	_____ Reduced Function	_____ Reduced Performance	
_____ None	_____ Other		
NOTES			By
		Date	

ENERGY TEST FOR CLOTHES DRYER

BACKGROUND

1. Site: A. _____ Lab. Bldg. _____ Identification _____
 B. _____ Field Code No. _____
2. Environmental (for field use only)
- A. Location (kitchen, laundry room, basement, other) _____
- B. Conditioning (heated, air conditioned, neither) _____
- C. Type of dwelling (private res., apt. bldg., other) _____
3. History
- A. Elapsed time: Heater _____ hr; Motor _____ hr. B. Cycles _____

TEST

4. A. Load _____ B. Rinse water temp. _____
5. Weights 6. Energy 7. Ambient
- A. Bone dry _____ kg A. Initial _____ kWh A. Dry bulb _____ °F
- B. Spin dry _____ kg B. After _____ min. _____ kWh B. Wet bulb _____ °F
- C. Heat dry _____ kg C. After _____ min. _____ kWh C. _____ %RH
 (_____ min.)
- D. Heat dry _____ kg
 (additional _____ min.)
8. Observer _____; Ext. _____ 9. Date _____

COMPUTATION

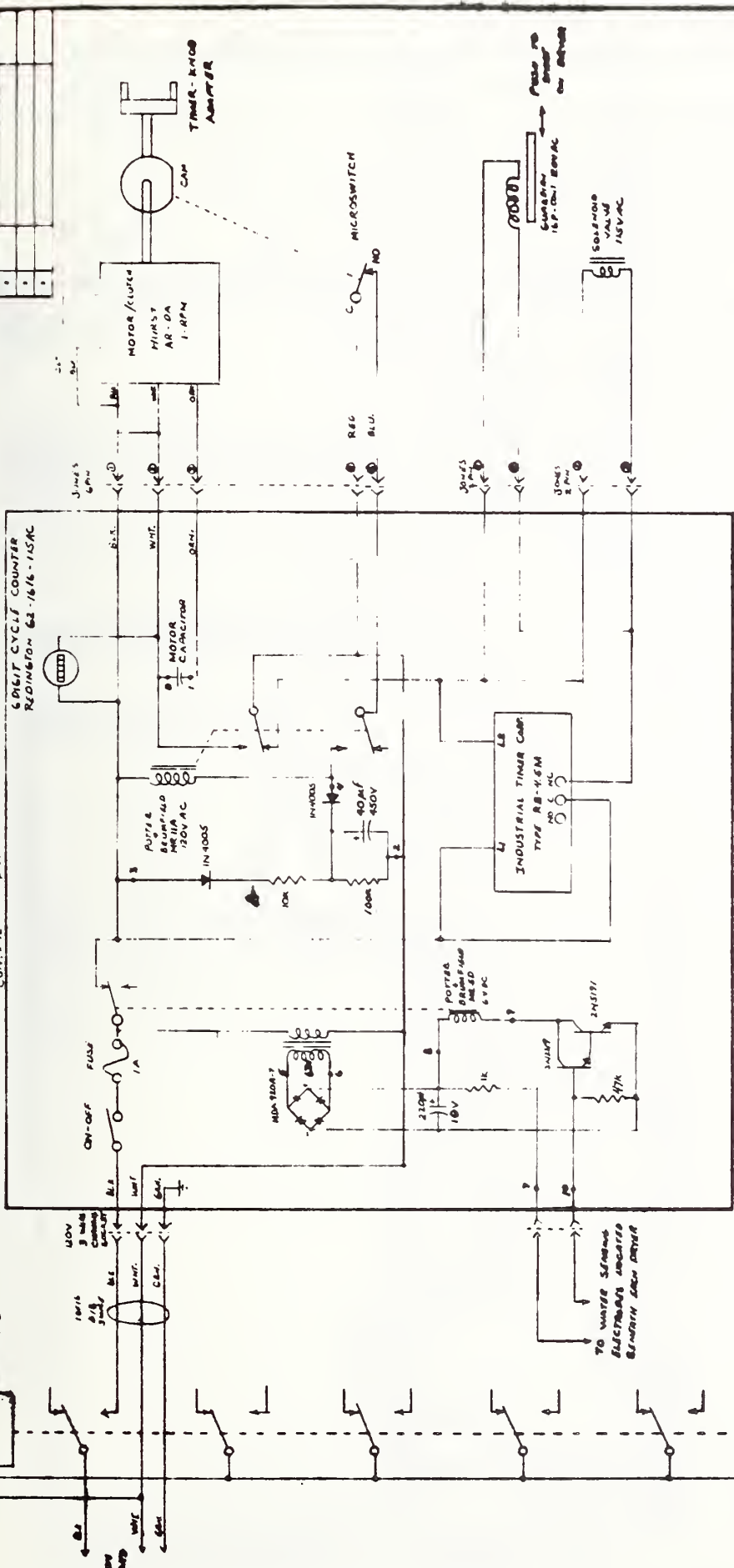
10. Computation
- A. DoE
- 1) Moisture removed = $5B - 5C =$ _____ kg
- 2) Energy used = $6B - 6A =$ _____ kWh
- 3) Efficiency = $\frac{\text{Moisture removed}}{\text{Energy used}} =$ _____ $\frac{\text{kg}}{\text{kWh}}$
- B. Modified
- 1) Moisture removed = $5B - 5D =$ _____ kg
- 2) Energy used = $6C - 6A =$ _____ kWh
- 3) Efficiency = $\frac{\text{Moisture removed}}{\text{Energy used}} =$ _____ $\frac{\text{kg}}{\text{kWh}}$

Acknowledgment

Thanks are due Owen Laug for designing the automating instrumentation.



WASH-CAM RECYCLING TIMER
60 MIN. TIME CYCLE
INDUSTRIAL TIMER CORP.
MODEL MC6-A-12



NATIONAL BUREAU OF STANDARDS WASHINGTON, D.C. 20540	
CONTROL CIRCUIT	
TEST NO.	TEST DATE
TEST NAME	TEST RESULT
TESTER	TESTED BY
DATE	APPROVED BY
THIS CIRCUIT IS THE PROPERTY OF NATIONAL BUREAU OF STANDARDS IT IS LOANED TO YOU BY THE NATIONAL BUREAU OF STANDARDS IT IS NOT TO BE REPRODUCED OR TRANSMITTED IN ANY FORM OR BY ANY MEANS, ELECTRONIC OR MECHANICAL, INCLUDING PHOTOCOPYING, RECORDING, OR BY ANY INFORMATION STORAGE AND RETRIEVAL SYSTEM.	
REPORT NUMBER 1-72-77	

Figure 1. Circuit diagram of control box for automatically recycling dryers.

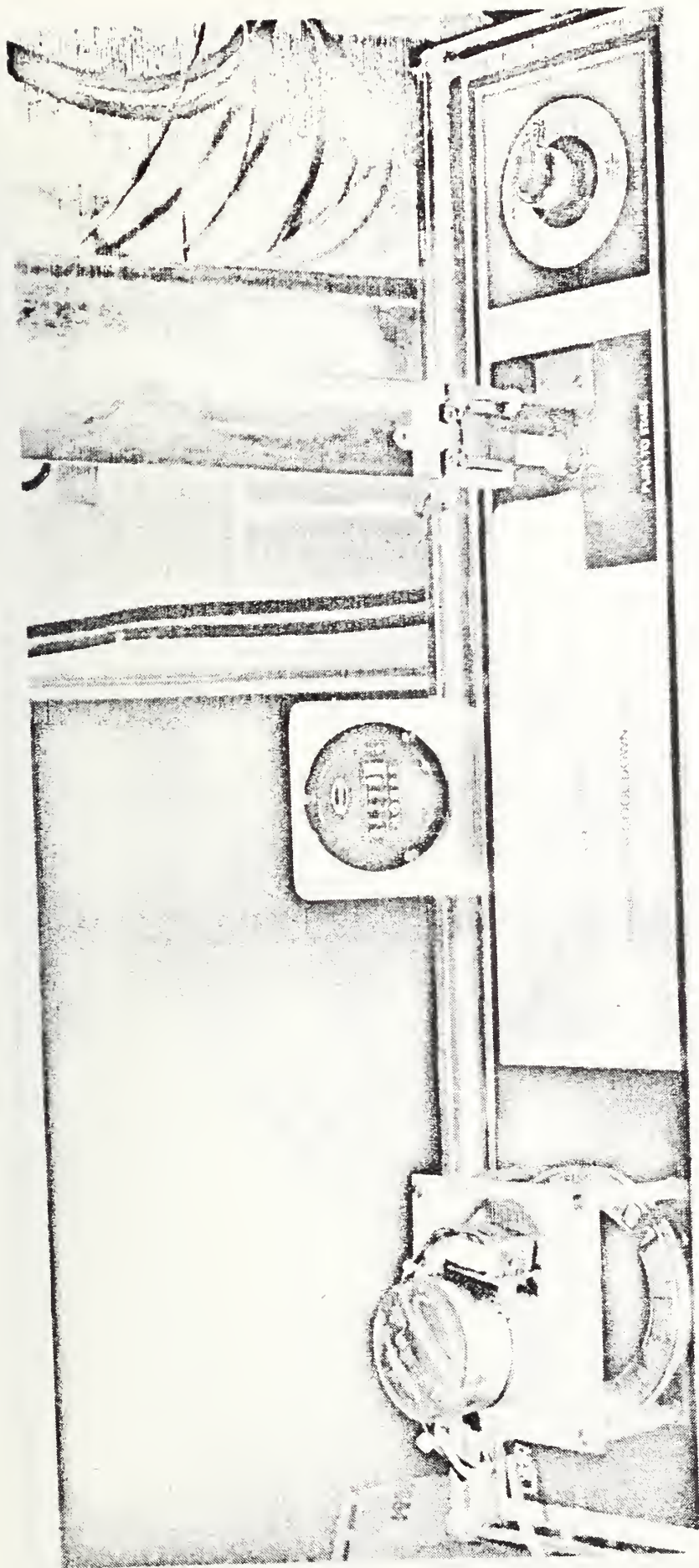


FIGURE 2 Driver control panel equipped for automatic recycling -- make-A.

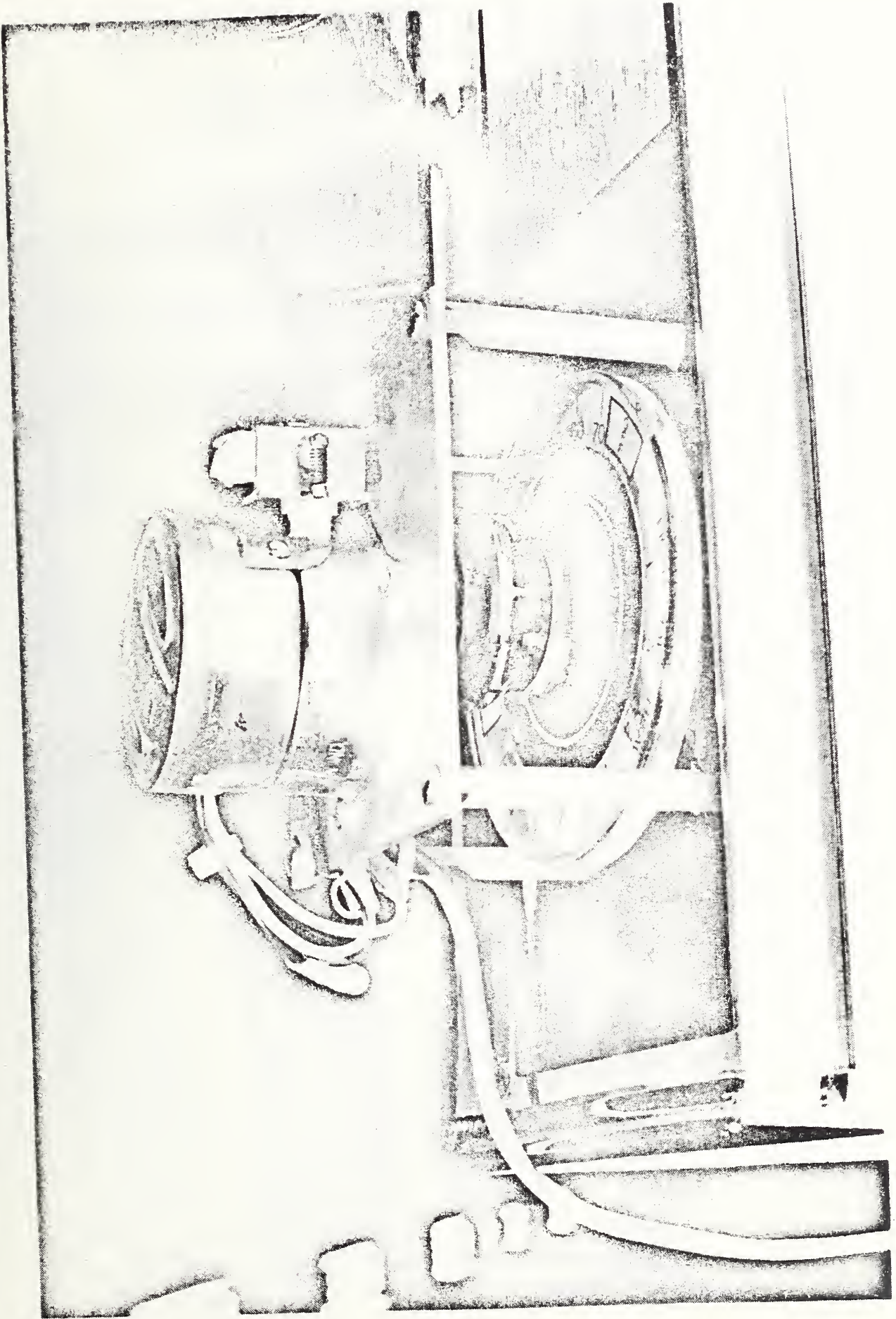


Figure 3. Close-up view of timer-advancer.

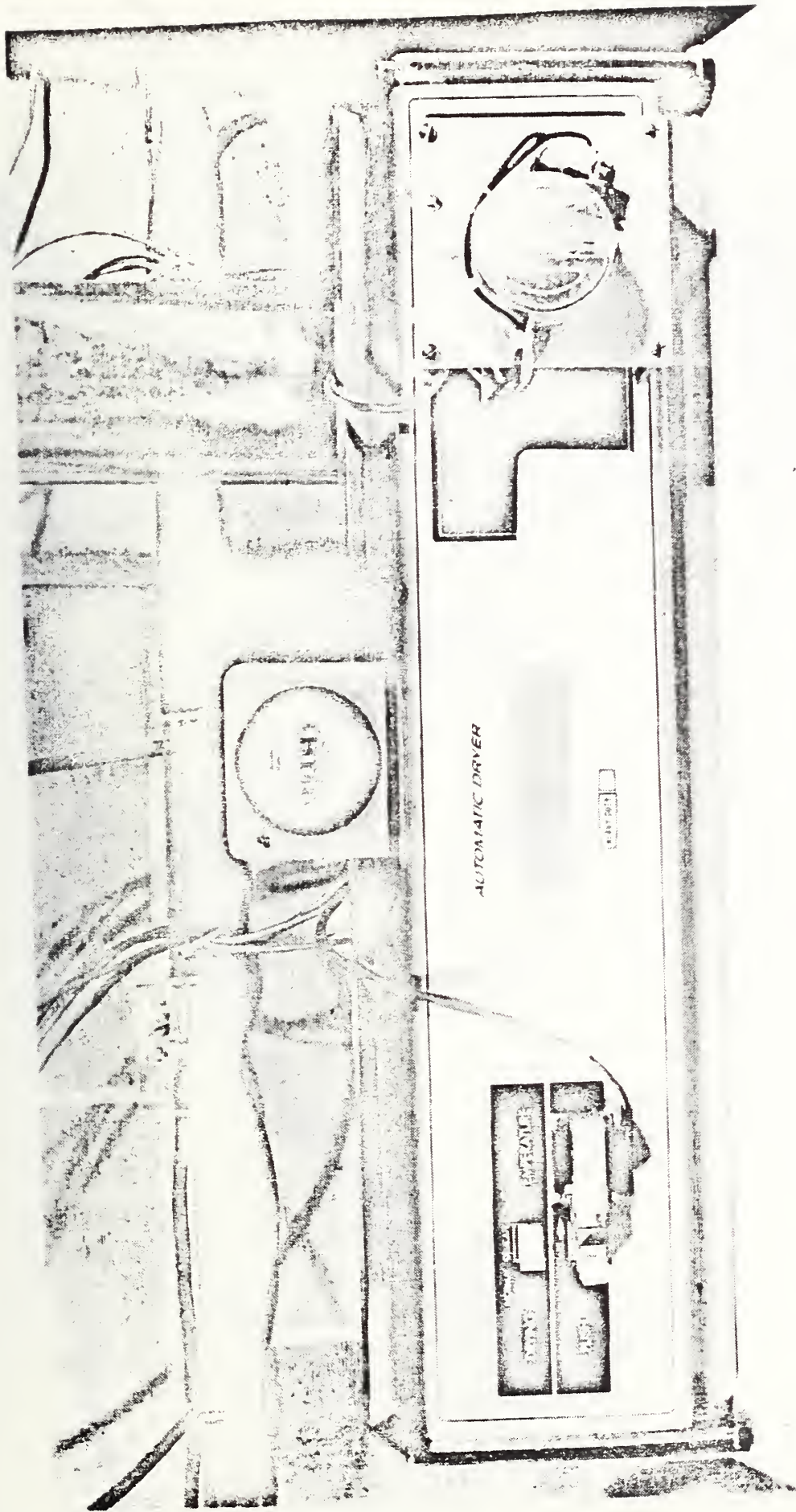


Figure 4. Dryer control panel equipped for automatic recycling -- make-B.

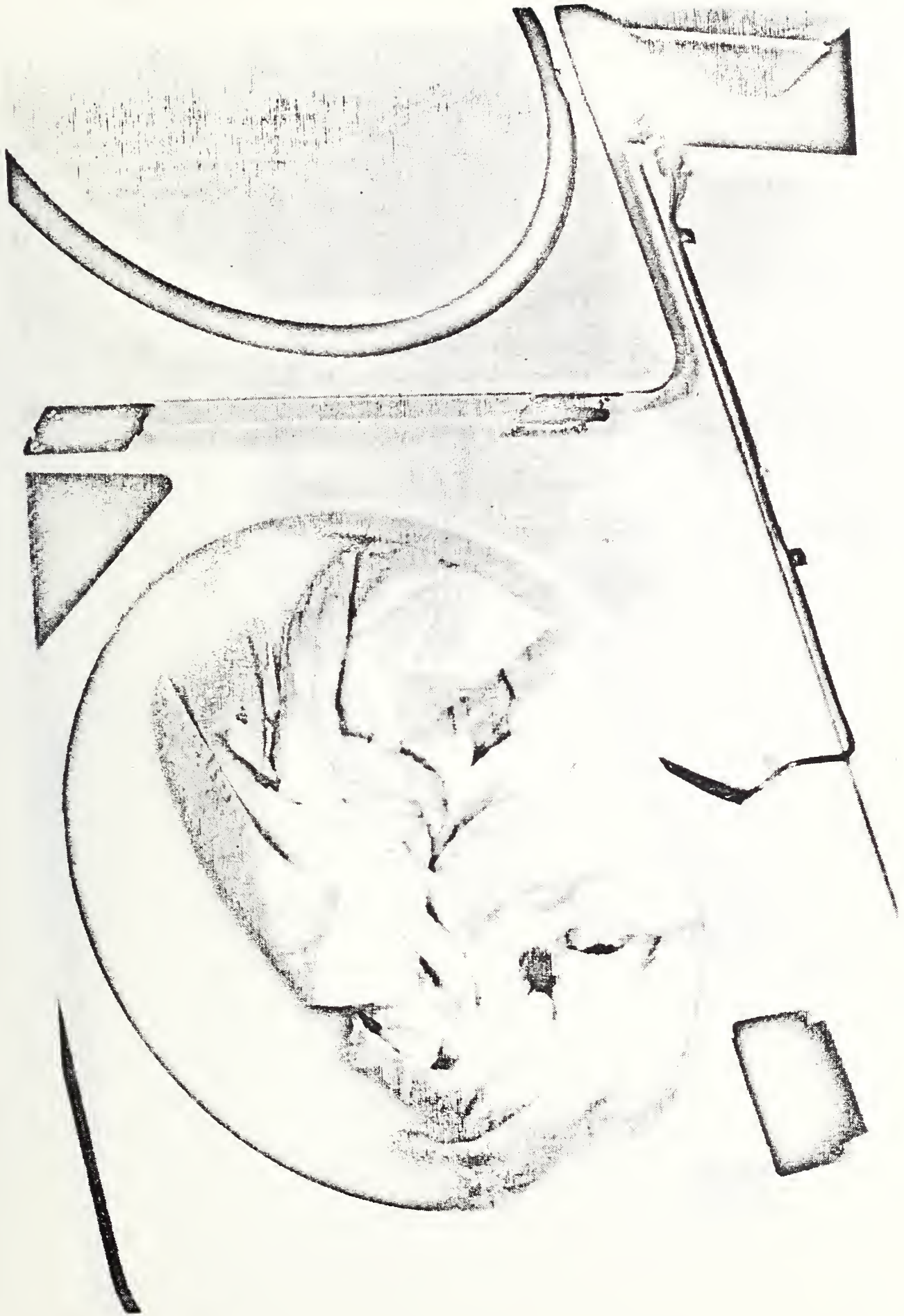


Figure 5. Make-A dryer equipped for squirting water onto loads.
(Normally the door is closed; it is open here for illustration).



Figure 6. Make-B dryer equipped for squirting water onto loads.
(Normally the door is closed; it is open here for illustration.)

U.S. DEPT. OF COMM. BIBLIOGRAPHIC DATA SHEET	1. PUBLICATION OR REPORT NO. NBSIR 78-1419	2. Gov't Accession No.	3. Recipient's Accession No.
4. TITLE AND SUBTITLE Life Test Development For Clothes Dryers		5. Publication Date January 1978	
		6. Performing Organization Code	
7. AUTHOR(S) Julius Cohen		8. Performing Organ. Report No.	
9. PERFORMING ORGANIZATION NAME AND ADDRESS NATIONAL BUREAU OF STANDARDS DEPARTMENT OF COMMERCE WASHINGTON, D.C. 20234		10. Project/Task/Work Unit No.	
		11. Contract/Grant No.	
12. Sponsoring Organization Name and Complete Address (Street, City, State, ZIP) Same as No. 9		13. Type of Report & Period Covered Interim Oct. 1976-Sept. 1977	
		14. Sponsoring Agency Code	
15. SUPPLEMENTARY NOTES			
<p>16. ABSTRACT (A 200-word or less factual summary of most significant information. If document includes a significant bibliography or literature survey, mention it here.)</p> <p>This interim report deals mainly with development of a life test for electric clothes dryers. The testing is being guided by a previously formulated methodology, and highlights of the test planning process are given. Testing is intensive, and up to seven years of life have been simulated in the laboratory. As expected for a long-lived product, there have been only a few dryer failures so far. Additionally, the temporal dependence of energy efficiency is being investigated.</p>			
<p>17. KEY WORDS (six to twelve entries; alphabetical order; capitalize only the first letter of the first key word unless a proper name; separated by semicolons)</p> <p>Clothes dryer; energy efficiency; life test; performance; reliability engineering</p>			
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<p>Order From Sup. of Doc., U.S. Government Printing Office Washington, D.C. 20402, SD Cat. No. C13</p> <p>Order From National Technical Information Service (NTIS) Springfield, Virginia 22151</p>		<p>20. SECURITY CLASS (THIS PAGE)</p> <p>UNCLASSIFIED</p>	<p>22. Price</p>

