NBSIR 73-176 (R) Comparison of Photon Interaction Data Sets. VI. McGuire and Kaman Photoeffect Data.

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**Center for Radiation Research Institute for Basic Standards National Bureau of Standards Washington, D. C. 20234

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Abstract

Photoeffect cross sections calculated by McGuire, covering the energy range 0.0062 to 62.0 keV for elements with Z = 2 to 54, are compared with values interpolated from results calculated by Veigele et al (Kaman) which cover the energy range 0.1 to between 1.0 and 8.0 keV. This comparison is presented in the form of percent differences between these two data sets, with the Kaman values taken as the reference set. The cross sections are listed and the differences are tabulated over the energy range 0.103 to 62.0 keV. At the higher energies (above between 1.0 and 8.0 keV) in this region of overlap, the Kaman values were fitted to experimental data, rather than calculated from theory. Discrepancies ranged from less than 3% up to as much as a factor of ten in the iodine M_{TV} - M_V edge region at 0.620 keV. From this comparison, and from graphical comparison of both sets with experimental data for carbon, aluminum and tin, we estimate that for Z = 2 to 54 the envelope of uncertainty of present calculated values in the region 0.1 to 1.0 keV is of the order of ± 20% except in the presence of resonance absorption features where the uncertainty can be an order of magnitude.



I. Introduction

In a previous report (IV. Kaman and ENDF/B) in this series, we presented a comparison of the photon cross section data set (0.1 to 1000 keV, Z = 1 to 94) $\frac{2.3}{4}$ (Kaman Corp.) with the ENDF/B library data set (1 keV to 100 MeV, 87 elements with Z = 1 to 94).

In that report we also included a comparison of the total attenuation coefficients in the Kaman set with the light-element, low-Z set by Henke and Elgin. The Henke and Elgin set, extending over the range 0.03 to 6.0 keV for Z = 2 to 18, was fitted and interpolated from available experimental data.

The Kaman cross section set in the region 0.1 to 1.0 keV, on the other hand, was calculated from theory for all elements. For elements with Z greater than 21 (Sc) these calculations were extended to energies higher than 1 keV, in one case up to 8.0 keV (Pu, Z = 94), above which, except for hydrogen, the Kaman set consists of values derived from experimental data.

In this low-energy region, particularly below 1 keV, the total attenuation coefficient is comprised almost entirely of the photoeffect cross section as indicated in Table I. The remaining portions of the total cross section, the coherent and incoherent scattering contributions, were calculated by means of the customary scattering-factor, impulse-approximation approach throughout the 0.1 to 1000. keV energy range of the Kaman set. These scattering cross section contributions enter only as small or negligible corrections to the total cross section in the range 0.1 to 1.0 keV. Hence in this low energy region an examination of the total attenuation coefficient reduces essentially to an examination of the photoeffect cross section.

In addition to the Kaman calculation of the photoeffect cross sections below 1 keV, there also exists an independent systematic calculation $\frac{9}{}$ of photoeffect cross sections by McGuire extending over the region 0.0062 keV (2000Å) to 62.0 keV (0.2Å) for elements with Z = 2 to 54. In this report we compare the McGuire and Kaman theoretical photoeffect values in the region 0.103 keV (120Å) to 62.0 keV (0.2Å), Z = 2 to 54.

The theoretical basis and calculational procedure for the Kaman low-energy photoeffect cross section computation were briefly described in report IV of this $\frac{1}{}$ series. We similarly describe briefly as follows the McGuire calculations and indicate some of the similarities and differences with respect to the Kaman calculation.

II. McGuire Photoeffect Calculations

Both the Kaman and McGuire soft x-ray theoretical photoeffect cross sections were calculated using the dipole central-field model discussed in detail by $\frac{10}{10}$ Cooper. In this model, the contribution $\tau_{n\ell}$ of the n^{ℓ} subshell to the total photoionization cross section is

$$\tau_{n\ell} = \frac{4}{3} \pi \alpha a_0^2 N_{n\ell} hv \left[\left(\frac{\ell}{2\ell+1} \right) R_{\ell-1}^2 + \left(\frac{\ell+1}{2\ell+1} \right) R_{\ell+1}^2 \right]$$
(1)

where α is the fine-structure constant, a_{\circ} is the Bohr radius, $N_{n\ell}$ is the subshell occupation number, hv is the photon energy in Rydbergs, and $R_{\ell \pm 1}$ are the radial matrix elements for the transition of the electron from the bound state with orbital quantum number ℓ to continuum states with $\ell' = \ell \pm 1$.

For the evaluations of the radial matrix elements R_{t+1} , both the Kaman and McGuire calculations used the dipole-length expression.

$$R_{\ell \pm 1} = \int_{0}^{\infty} P_{n\ell}(r) r P_{\epsilon, \ell \pm 1}(r) dr$$
(2)

in which r is the electron radial position in Bohr units, ε is the continuum (photo-ejected) electron energy, and $P_{e,\ell \pm 1}(r)$ and $P_{e,\ell \pm 1}(r)$ are the bound and continuum radial wave functions, respectively, of the photoelectron. These wave

functions P(r) were determined by solving the radial Schrödinger equation

$$\int \frac{d^{2}}{dr^{2}} + V(r) + E_{n} - \frac{\ell(\ell+1)}{r^{2}} \int P(r) = 0$$
(3)

in which E_n is the energy ($E_n^{<0}$) in Rydbergs of an electron in the nth subshell. Values of the potential V(r) were taken from the tables of Herman and Skillman for both the Kaman and McGuire calculations.

The principal two points of difference between the Kaman and McGuire calculational procedures are in the treatments of V(r) and E_n in equation (3) for purposes of carrying out the necessary integrations for evaluating $P_{n,\ell}(r)$ and $P_{\varepsilon,\ell,\ell\pm1}(r)$: (1) McGuire approximated the quantity rV(r) by a series of straight lines, by means of which solutions to equation (3) could be expressed analytically in terms of Whittaker functions and evaluated without recourse to numerical integration. In the Kaman calculation the tabulated Herman-Skillman V(r) values were used directly, and numerical integration was used. (2) McGuire used theoretical E_n values in equation (3) corresponding to the initial bound-state configuration, hence the frozen-orbital or unrelaxed-core approximation. In the Kaman calculation, on the other hand, core-relaxation or fast-rearrangement was taken into account to some extent by inserting experimental absorption-edge energies for E_n in equation (3).

Use of experimental E_n values has some advantage in providing absorption edges at the right energies, with no scaling of the calculated results required to relate them to experimental cross sections. There is, however, some risk in this procedure in that corrections may be inconsistently introduced, according 12/ 12/ to Pratt, Ron and Tseng. Pratt et al also suggest, on the basis of results of 13/ Rosen and Lindgren, that the relaxed-core (sudden rearrangement) approximation is more suitable for inner shells, particularly for light and medium Z elements,

where binding energies calculated in this approximation agree best with experimental thresholds. However, for outer electron shells, binding energies calculated using the unrelaxed core (slow rearrangement) approximation tend to agree better with experimental thresholds.

III. Results

The McGuire energy grid is in integral values of angstroms rather than keV, and the upper energy varies from 0.310 keV (40 Å) for helium (Z=2) up to 62.0 keV (0.2Å) for silver (Z=47) through xenon (Z=54). Because of this varying upper energy, and also because McGuire gives no cross section values at the absorption edge energies, we interpolated (log-log linear interpolation) the Kaman photoeffect values to the McGuire energy grid for purposes of this comparison, rather than vice-versa. These interpolated values are listed in barns/atom in the last column in Table II following the McGuire values in the same units as taken from reference (9).

The results of the comparison are given in the second column of Table II. For each element Z = 2 to 54, the percentage deviation of the McGuire photoeffect cross sections from the Kaman values was calculated as

Percent Deviation = 100.0 (
$$^{T}_{McGuire} - ^{T}_{Kaman}$$
)/ $^{T}_{Kaman}$ (4)

The resulting sign indicates that the McGuire cross section is greater (+) or less (-) than the Kaman value. The percent deviations are rounded off to the nearest one-tenth percent.

In Figures 1 and 2 we have indicated the combinations of energy and atomic number for which the absolute deviation of the McGuire photoeffect cross section from the Kaman value exceeds 3% and 20%, respectively. It is evident from Figures 1 and 2 and an inspection of Table II that the majority of the deviations are between 3% and 20%. The only systematic trends appear to be that the McGuire

values are generally greater than the Kaman values below 0.5 keV and tend to be less than the Kaman values in the region 1.0 to 10 keV.

In Figures 3, 4 and 5 we graphically compare the McGuire (dashed line) and Kaman (solid line) calculated results, also the Kaman values above 1.0 keV fitted to experimental data (dotted line) for carbon, aluminum and tin. Also included in these graphs are experimental total cross section data points from the NBS data-file indexed and documented in reference (14). In the regions shown, the total cross section on this scale is indistinguishable from the photoeffect, as was indicated in Table I. In Figure 4 the dip in the McGuire values at 2.07 keV for aluminum we attribute to a typographical error.

In these sample graphical comparisons we see that both the McGuire and Kaman results are for the most part consistent with the experimental data points within the experimental spread of the order of $\pm 20\%$. An exception to the $\pm 20\%$ consistency is seen in Figure 5 for tin below 0.3 keV where a pronounced resonance-type feature is shown by the experimental points. Similar peaks have been observed between 0.1 and 1.0 keV for a number of other medium and high Z elements (see, e.g., Figs. 27-52 of reference (2), Vol. II). Although both the McGuire and Kaman calculated results tend to suggest the presence of such features, these cross section values may disagree with each other and/or with experiment by an order of magnitude at the peak energy.

Some additional isolated large discrepancies between the McGuire and Kaman values (1057% for nitrogen 0.103 keV and 640% for palladium at 6.2 keV) we attribute to misplaced decimal points in the McGuire tables. Other large discrepancies as listed in Table III we attribute to differences between the McGuire theoretical (initial bound-state configuration E_n values as discussed in Section II) $\frac{15}{2}$ absorption-edge energies and the experimental values from Bearden and Burr used in the Kaman calculations. All of these differences are positive, hence the theoretical McGuire threshold energy in each case in less than the Bearden-Burr value also listed in Table III.



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Figure Captions

- Figure 1. Elements and grid-energies (see Table II) for which the McGuire calculated photoeffect cross section is at least 3% greater (+) or less (-) than the corresponding photoeffect cross section interpolated from the Kaman data set. No McGuire values are given for higher energies or Z's beyond the indicated boundary line in Figures 1 and 2.
- Figure 2. Elements and grid-energies for which the McGuire calculated photoeffect cross section is at least 20% greater (+) or less (-) than the corresponding photoeffect cross section interpolated from the Kaman data set.
- Figure 3. Photoeffect cross sections for carbon calculated by McGuire (----) and Kaman (-----), also fitted by Kaman to experimental data (....). The circles are measured total-cross-section data-points (see text).
- Figure 4. Photoeffect cross sections for aluminum, with same notation as Fig. 3.
- Figure 5. Photoeffect cross sections for tin, with same notation as Fig. 3.

Table Captions

- Table I. Ratios of the photoeffect cross section to the total cross section, based on values from the Kaman data set.
- Table II. Percent differences $100 \times ({}^{T}_{McGuire} {}^{T}_{Kaman})/{}^{T}_{Kaman}$ at the McGuire grid energies. The photoeffect cross sections ${}^{T}_{McGuire}$ and ${}^{T}_{Kaman}$ (interpolated to the McGuire energies) are listed in the last two columns in barns/atom.
- Table III. Large percent differences in Table II attributable to discrepancies between the McGuire theoretical edge-energies and the Kaman experimental edge-energies. The experimental edge-energies or ranges of edge-energies, in the last three columns are taken from Bearden and Burr

ATOMIC NUMBER, Z

5 20 4 O 0 O 0 ╅╋╪┾┾╄╄╪╴╋╇╋┲╿╋┲┧┝╋┲╅╴╆╄╋╆╋╪┿╉╄┧┇┽┲╸╎╎╎╽┷╴╎╋┹╋╉╅┿╬╬╬╬╬╬ │╡╕╡╍╸╺┿┿╅╏┪╡╏┪╡╪╪╪┥╞╞┥╡╎╎╎╎╎╎╎┿╎╎┥╇╧╋╵┽┿╧┿ PHOTON ENERG 1+ + ++++ 111++1+++1 1.0 <u>┼┼┼┼┼</u>┽╽╎┽ ││││││┽┿┿╶┽╎ │││┿││││││┼┿╎┨┿┽│┿┽││ │ │╇╋╎╬╬┾║ ****1*1*1*1 11111*** *****11111*** -╻╺╋╗╗╸╹╹╹┥╴╹╹╽╽╽╽╽╽╽╽╽╽╋╋╋╴╹╹╹╽╽╽╏╴╺╬╬╬╏║ ke +++ < ╪╪╉╪╶╶╋╴┊╎╎╎╽╽╽╽<mark>╪╪╪╉╋</mark>╏╏╎╎╿╿╽╽╎╽║ ō ++ |++ +++ +||||| 1+ ╶┾┿╽╽╽╅╇╇╇╇╽║╽╿╇╿╽╽╽╏║╽ \triangle % MC ++++++1ΚD ++GUIRE VS MAN IV RE З ╋╋╋╋╋╋**╋╴╋╴┽╶╬╬╴╶╬** %

Fig.]











			(ph	otoeffect c	ross section)/(total cro	ss section)			
3(keV)	1 ^Н	2 ^{He}	3 ^{Li}	°c	13 ^{A1}	29 ^{Cu}	50 ^{Sn}	74 ^W	82 ^{Pb}	94 ^{Pu}
0.1	1.0000	1 .0000	1 .0000	1 °0000	1.0000	6666°0	0,9988	0666°0	0,9985	0°9993
0.2	7999.	1,0000	1.0000	1 0000	1.0000	.9998	.9988	。 9994	0266.	,99 24
0.5	.9942	.9993	7999.	6666°	9666°	.9992	.9987	0666*	0666°	,997 2
1 .0	.9423	.9936	°9981	°9995	°9980	°9995	0666°	.9971	°9978	.9980
2.0	.6260	°9464	°9867	0266.	.9992	.9979	°99 59	°9976	。9916	.9943
5.0	.0699	°5197	°8350	°9748	.9939	°9846	6496°	°9871	° 9895	.9916
10 。	°0071	。1150	, 3892	。8704	°9744	°9958	。 9818	, 9535	,9 632	. 9720
20.	°000 °	•0139	。0688	,4881	,9 020	°9776	。9409	, 9704	°9740	°9646
50 °	1000' >	° 0007	.0039	。0567	°4655	。8926	.9624	。8889	。9114	9272
°00	<pre>1000* ></pre>	°0001	°0007	。0071	。109 <i>2</i>	.6234	.8738	。 9343	。9427	。 8337

Table I

HELIUM

		a contra da la contra	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KAMAN
.103	3.1	3.402+05	3.308+05
.124	-12.4	1.808+05	2.06E+05
.155	-12.8	1.00E+05	1.15F+05
.207	-11.7	4.60E+04	5.216+04
.310	-7.6	1.50E+04	1.62F+04

LITHIUM

		A CAR A CARACTER CONTRACTOR	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	ACGUIRE	KAMAN
.103	18.8	1.52E+06	1.28F+05
.124	18.4	9.80E+05	H. 27F+05
.155	20.1	5.806+05	4.83E+05
.207	22.8	2.85E+05	2.32F+05
.310	13.0	8.90E+04	7.88F+04
.413	7.8	3.80€+04	3.52F+04
.620	-9.0	1.00E+04	1.10F+04

		BERYLLIUM	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KAMAN
.103	16.3	1.30E+05	1.128+05
.124	14.2	2.16E+06	1.898+06
.155	12.7	1.33E+06	1.18F+06
.202	R.3	6.70E+05	5.14+05
.310	-2.1	2.20E+05	2.25F+115
•413	11.4	1.]8E+05	1.04F+05
.620	15.3	4. 106+14	3.478+04
.827	18.6	1.80E+04	1.526+04
1.033	23.6	1.00E+04	5.09F+03

RORON

ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KAMAN
.103	16.2	2.90E+05	2.50F+05
.124	10.3	1.856+05	1.68F+05
.155	2.4	1.058+05	1.03F+115
.202	17.7	1.32E+06	1.12F+06
.310	• 6	4.80E+05	4.77F+05
•413	-6.2	2.206+05	2.358+45
.620	- , 9	8.00E+()4	8.075+114
.827	3.6	3. ×0E+04	3.67F+04
1.033	27.1	2.50E+1)4	1.97F + 64

		CARAON	
ENERGY	PERCENT		
(KFV)	DIFFERENCE	MCGUTRE	KDALI
.103	19.0	5.405+05	4.42++(15
.124	21.9	4.00E+35	3.288+05
.155	20.3	5.40E+05	1. 448+115
.207	4 . 5	1.086+05	1.03F+05
.310	3.7	H.10E+05	7.31++05
•413	6.3	4.50E+05	4.24E+65
620	17.7	1.825+05	1.448+05
.827	17.9	3.5AE+04	1.21F+114
1.033	19.4	4.70E+04	3.44F+1)4
1.240	20.8	2.90E+04	2.475+04
1.550	19.5	1.50E+04	1.256+134
		NITROGEN	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIZE	К∆⊴д№
.103	1056.5	1.11E+07	9.678+05
.124	2.7	6.50E+05	6. 23F+05
.155	2.7	3.90F+05	3.40++05
.207	7.2	2.081+05	1.44+415
.310	-4.5	7.00E+04	7. 34F+04
.413	3.8	6. HOE+05	5.555+05
.620	-2.8	2.556+05	2.621+115
.827	7	1.258+05	1.2FF+05
1.033	7.0	7.508+04	7.015+04
1.240	6.9	4.70E+04	4.415+04
1.550	11.7	2.601+04	2. XXF+04
2.066	18.8	1.201+04	1 - 61 + 04
		OXYGEN	

CNERDI	PFRCFNI		
(KEV)	DIFFFPFNCF	MCGUIRE	KAMLN
.103	14.9	1.776+06	1.544+06
.124	R.4	1.12E+06	1.031+05
.155	10.8	7.00E+05	5.325+05
.207	18.3	3.×5 <u>E</u> +05	3.255+05
.310	30.3	1.60E+05	1.238+05
•413	6.7	5.50E+04	6.095+04
.620	• ^Q	3.95E+05	3.42F+05
.827	• 4	1.958+05	1.44++05
1.033	8.6	1.208+05	1.115+05
1.240	2.1	7.20E+04	7.045+04
1.550	7.6	4.10E+04	3.81F+04
2.066	18.4	2.00E+04	1.60F+04

		FLUORIME	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KAMAN
.103	2.3	2-60E+06	2-548+06
.124	4.9	1.80E+06	1.725+65
.155	23.0	1-30E+06	1.06E+06
.207	8.3	5 40F+05	5.458+45
.310	19.4	2.45++05	2 051+05
.413	23 7	1 24E+05	1 00F+05
620	30 9	5 005+04	1.606100
.827	7 7	3 055105	3.03E.04
1.033	3 2	1 706 105	
1.240	5.6	1 166.06	1.002.00
1.550	14 J		1.085+05
2 066	14.7		5.055+94
2.000	14 e 3	3 • 0 0 <u>C</u> + 9 4	C . M C + 114
		NEON	
ENEDOX	DEDOLME	50N	
	DIFFERENCE		< A. 1
103	DIFFERENCE		A DISTAN
• 1 () 5	3.5	4 . 111F + 11F	3. HAR + 11 P
• 174	3.0	→ 80±+05	2.12++15
• 1 ~ ~ ~	1.1	1.75+465	1.54F+6h
• 201	2.1	9.10E+05	H. HEr + 15
• 510	1.6	3.601+05	3-3-+-35
•413	4.4	1.70E+95	1.63++05
• 520	9.7	$6 \cdot 30 + 04$	5.74++44
.827	11.6	3.00++04	2.647+04
1.033	-13.6	2.05k+05	2.37F+(15
1.740	-11.2	1.356+05	1.528-45
1.550	- 9 . 3	7.708+04	M. 404+04
2.066	1.7	3.90E+04	3。43月+04
C.U.C.D.O.M		SODIUM	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	WCCUTPH	KAHAN
.103	11.2	4.954+06	4.45+415
.124	24.0	4.00E+06	3.238+06
• [5 5	11.3	2.40E+06	5.] HE + UD
.207	-7.4	1.10E+06	1.14+40
• 310	-21.4	3.708+05	4.715+115
•413	-21.7	1.868+05	2.34E+05
.620	-12.6	7.50E+04	8,548+64
.827	-13.9	3.501+04	4.07F+04
1.033	-21.2	1.80E+04	2.245+()4
1.240	R.J	2.32E+05	2.158+05
1.550	15.9	1.38E+05	1.148+05
2.066	11.7	6.10F+04	5.46F+04

MAGNESTUM

ENERGY	PFRCENT		
(KEV)	DIFFERENCE	MCGUIPE	KAMAN
.103	17.1	6.65F+06	5 64F+115
.124	12.2	4.80E+06	4.24+44
.155	3.8	3.10E+06	2.994 +06
.207	-2.]	1.65E+06	1.698+06
.310	6	6.H0E+05	6.84F+05
.413	3.7	3.60E+05	3.478+05
.620	-].4	1.25E+05	1.27F+05
.827	-1.0	6.00E+04	6.05F+04
1.033	4.3	3.50E+04	3.365+114
1.240	15.4	2.40E+04	2.02F+04
1.550	-7.8	1.528+05	1.59++115
2.066	7.0	7.90E+04	7.345+04
3.100	12.4	2.758+04	2.44F+14
4.133	23.9	$1.34 \pm +04$	1.048+04
		ALUM INHM	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUTRE	KAHAN
103	22.6	6.48E+06	5.295+06
.124	6.9	5.50E+06	5.158+06
.155	11.0	4.13E+06	3.728+05
.207	16.3	2.55E+06	2.14F+U5
.310] 7.5	1.05E+06	4.25F+115
.413	7.2	5.10E+05	4.76F+115
.620	4.7	1.85E+05	1.77F+05
.827	6.0	9.00E+04	8.448+()4
1.033	1.0	4.801+04	4.75F+64
1.240	-10.2	2.658+04	2.955+114
1.550	962.0	1.70E+05	1.0115+14
2.066	-40.4	5.808+04	4.748+04
3.100	1.5	3.35E+04	3.348+44
4.133	17.6	1.75E + 04	1.49F+04
		SILICON	
ENERGY	PERCENT		

CIVENOI	PFR(FM)		
(KEV)	DIFFERENCE	10GUTRE	■ Δ 33 位 11
.103	-87.8	3.605+05	2.455+06
.124	10.7	5.242+06	4.731+ut
.155	3.4	4.62E+06	4.475+06
.207	10.1	3.10E+06	2.425+06
.310	11.2	1.368+06	1.20++05
.413	6.7	5.20E+05	6.375+115
.620	2.1	2.45E+05	2.478+65
.R27	9	1.155+05	1.16++05
1.033	-3.P	6.30E+04	6.55F+114
1.240	-9.4	3.758+04	4.14+04
1.550	-6.4	2.122+04	1.215+04
2.066	-15.4	1.08t+05	1.288+05
3.100	3.3	4.458+04	4 . 5 1 + 84
4.133	5.7	2.05E+04	1. 44 + 14

PHOSPHOPUS

		ALCONDAL CONTRACTOR	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KANAN
.103	15.4	5.708+05	4.545+05
.124	25.3	4.708+05	3.755+05
.155	21.0	5.40E+06	4.46F+0b
.207	- 3.4	3.46E+06	3.58F+00
.310	3.6	L.70E+06	1.64F+0F
.413	-1.2	H.50E+05	A.605+05
	-7.8	3.00E+05	3.265+05
.827	-4.9	1.50E+05	1.54E+115
1.033	-10.0	8.00E+04	8,298+114
1.240	-8.7	5.10E+04	5.585+04
1.550	- • A	3.05E+04	3.075+04
2.066	-12.2	1.25E+04	1.428+04
3.100	• 0	5.50E+04	5.501+04
4.133	7.9	2.70F+04	2-50F+04

SULFUR

ENERGY	PEPCENT		
(KEV)	DIFFERENCE	MCGUTRE	KAMAN
.103	18.8	8.50E+05	7.164+05
.124	25.1	7.00E+05	5.548+05
.155	26.5	5.00E+05	3.95F+05
.207	-1.5	3.60E+06	3.65F+06
.310	6	2.05E+05	2.04F+U5
.413	1.6	1.12E+06	1.10F+06
.620	-7.7	3.90E+05	4.23F+05
.827	-12.8	1.80E+05	2.07F+U5
1.033	-14.4	1.00ビ+05	1.17F+05
1.240	-5.0	7.00E+04	1.37F+04
1.550	-6.3	3.80E+04	4.116F+04
2.066	-12.8	1.64E+04	1. + 4 + 14
3.100	-2.9	6.70E+04	E.94F+04
4.133	7.6	3.40E+04	3.1n++04

CHLOFINE

ENERGY	PERCENT		
(KEV)	DIFFEPENCE	MCGUIRE	K-AMAN
.103	1.9	1.005+06	9.816+15
.124	3.9	4.20E+05	7.20E+05
.155	4.5	6.00E+05	5.74F+15
.207	129.0	6.40E+06	2. knF+65
.310	-1.6	2.45E+06	2.49++06
.413	1.6	1.40E+06	1.345+05
•650	-16.1	4.50E+05	5.37F+05
.827	-16.7	2.20E+05	2.648+45
1.033	-18.2	1.23E+05	1.50F+05
1.240	-17.2	7.90E+04	9.54F+114
1.550	-10.9	4.70E+04	5.27t+04
2.066	-20.6	1.95E+04	2.44F+04
3.100	-11.9	7.50E+04	8.5]E+04
4.133	- <u>,</u> A	3.90E+04	3.478+114

Table II. Continued

		AR(-1)1.	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KAMAN
.103	4.7	1.33E+06	1.27-+06
.124	4.9	1.10E+06	1.055+06
.155	7.9	8.50E+05	7. HAF+05
.207	9.5	5.50E+05	5.02F+05
.310	-9.4	2.52E+05	2.78F+05
.413	-5.9	1.66E+06	1.76F+06
.620	-10.4	6.20E+05	6.425+05
.827	-14.9	2.90E+05	3.41F+05
1.033	-17.4	1.60E+05	1.94++05
1.240	-18.3	1.000+05	1.22++05
1.550	-10.8	6.00E+04	4.72F+114
2.066	-16.3	2.60E+04	3.118+94
3.100	-18.8	8.50E+03	1.055+64
4.133	-7.1	4.60E+04	4.951+14
		POTASSTEM	
ENERGY	PFRCENT		
ENERGY (KEV)	PFRCENT DIFFERENCE	MCGUIRE	KAMAN
ENERGY (KEV) .103	PFRCENT DTFFERENCF 9.8	MCGUIRE 1.50E+06	КАМАN 1.37F+95
ENERGY (KEV) .103 .124	PFRCENT DIFFERENCE 9.8 13.8	MCGUIRE 1.50E+06 1.30E+06	КАМАЮ 1.37F+95 1.14F+06
ENERGY (KEV) .103 .124 .155	PFPCENT DIFFERENCE 9.8 13.8 13.7	MCGUIRE 1.50E+06 1.30E+06 1.03E+06	КАМАЛ 1.37F+95 1.14F+06 9.06F+05
ENERGY (KEV) .103 .124 .155 .207	PFRCENT DIFFERENCF 9.8 13.8 13.7 13.4	MCGUIRE 1.50E+06 1.30E+06 1.03E+06 6.80E+05	КДМДN 1.37F+UD 1.14F+06 9.06F+U5 5.99F+05
ENERGY (KEV) .103 .124 .155 .207 .310	PFRCENT DIFFERENCE 9.8 13.8 13.7 13.4 -7.7	MCGUIRE 1.50E+06 1.30E+06 1.03E+06 6.80E+05 3.30E+06	КАМАN 1.37F+05 1.14F+06 9.06F+05 5.99F+05 3.54F+05
ENERGY (KEV) •103 •124 •155 •207 •310 •413	PFRCENT DIFFERENCE 9.8 13.8 13.7 13.4 -7.7 -7.1	MCGUIRE 1.50E+06 1.30E+06 1.03E+06 6.80E+05 3.30E+06 1.92E+06	KAMAN 1.37F+05 1.14F+06 9.06F+05 5.99F+05 3.54F+05 2.07F+06
ENERGY (KEV) •103 •124 •155 •207 •310 •413 •620	PFRCENT DIFFERENCF 9.8 13.8 13.7 13.4 -7.7 -7.1 -12.9	MCGUIRE 1.50E+06 1.30E+06 1.03E+06 6.80E+05 3.30E+06 1.92E+06 7.30E+05	KAMAN 1.37F+05 1.14F+06 9.06F+05 5.99F+05 3.58F+05 2.07F+06 8.38F+05
ENERGY (KEV) 103 124 155 207 310 413 620 .827	PFRCENT DTFFERENCF 9.8 13.8 13.7 13.4 -7.7 -7.1 -12.9 -4.4	MCGUIRE 1.50E+06 1.30E+06 1.03E+06 6.80E+05 3.30E+06 1.92E+06 7.30E+05 4.00E+05	KAMAN 1.37F+05 1.14F+06 9.06F+05 5.99F+05 3.58F+05 2.07F+06 K.38F+05 4.18F+05
ENERGY (KEV) .103 .124 .155 .207 .310 .413 .620 .827 1.033	PFRCENT DIFFERENCE 9.8 13.8 13.7 13.4 -7.7 -7.1 -12.9 -4.4 -8.2	MCGUIRE 1.50E+06 1.30E+06 1.03E+06 6.80E+05 3.30E+06 1.92E+06 7.30E+05 4.00E+05 2.20E+05	KAMAN 1.37F+05 1.14F+06 9.06F+05 5.99F+05 3.58F+05 2.07F+06 8.38F+05 4.18F+05 2.40F+05
ENERGY (KEV) •103 •124 •155 •207 •310 •413 •620 •827 1.033 1.240	PFRCENT DTFFERENCF 9.8 13.8 13.7 13.4 -7.7 -7.1 -12.9 -4.4 -8.2 -14.8	MCGUIRE 1.50E+06 1.30E+06 1.03E+06 6.80E+05 3.30E+06 1.92E+06 7.30E+05 4.00E+05 2.20E+05 1.30E+05	KAMAN 1.37F+05 1.14F+06 9.06F+05 5.99F+05 3.54F+05 2.07F+06 K.28F+05 4.14F+05 2.40F+05 1.53F+05
ENERGY (KEV) •103 •124 •155 •207 •310 •413 •620 •827 1.033 1.240 1.550	PFRCENT DIFFERENCE 9.8 13.8 13.7 13.4 -7.7 -7.1 -12.9 -4.4 -8.2 -14.8 -7.4	MCGUIRE 1.50E+06 1.30E+06 1.03E+06 6.80E+05 3.30E+06 1.92E+06 7.30E+05 4.00E+05 2.20E+05 1.30E+05 7.80E+04	KAMAN 1.37F+05 1.14F+06 9.06F+05 3.54F+05 2.07F+06 8.38F+05 4.14F+05 2.40F+05 1.53F+05 3.42F+04
ENERGY (KEV) •103 •124 •155 •207 •310 •413 •620 •827 1.033 1.240 1.550 2.066	PFRCENT DTFFERENCF 9.8 13.8 13.7 13.4 -7.7 -7.1 -12.9 -4.4 -8.2 -14.8 -7.4 -13.2	MCGUIRE 1.50E+06 1.30E+06 1.03E+06 6.80E+05 3.30E+06 1.92E+06 7.30E+05 4.00E+05 2.20E+05 1.30E+05 7.80E+04 3.40E+04	KAMAN 1.37F+05 1.14F+06 9.06F+05 3.64F+05 3.64F+05 2.07F+06 4.34F+05 2.40F+05 1.53F+05 3.42F+04 3.42F+04
ENERGY (KEV) 103 124 155 207 310 413 620 .827 1.033 1.240 1.550 2.066 3.100	PFRCENT DIFFERENCE 9.8 13.8 13.7 13.4 -7.7 -7.1 -12.9 -4.4 -8.2 -14.8 -7.4 -13.2 -9.9	MCGUIRE 1.50E+06 1.30E+06 1.03E+06 6.80E+05 3.30E+06 1.92E+06 7.30E+05 2.20E+05 1.30E+05 7.80E+04 3.40E+04 1.20E+04	$KAMAN 1 \cdot 37F + 05 1 \cdot 14F + 06 9 \cdot 06F + 05 5 \cdot 99F + 05 3 \cdot 53F + 05 4 \cdot 13F + 05 4 \cdot 13F + 05 1 \cdot 53F + 05 3 \cdot 42F + 04 3 \cdot 33F + 04 1 \cdot 33F + 04 \\ 1 \cdot 35F + 05F \\ 1 \cdot 45F + $
ENERGY (KEV) 103 124 155 207 310 413 620 827 1.033 1.240 1.550 2.066 3.100 4.133	PFRCENT DTFFERENCF 9.8 13.8 13.7 13.4 -7.7 -7.1 -12.9 -4.4 -8.2 -14.8 -7.4 -13.2 -9.9 -7.3	MCGUIRE 1.50E+06 1.30E+06 1.03E+06 6.80E+05 3.30E+06 1.92E+06 7.30E+05 2.20E+05 1.30E+05 1.30E+05 7.80E+04 3.40E+04 1.20E+04	$KAMAN 1 \cdot 37F + 05 1 \cdot 14F + 06 9 \cdot 06F + 05 3 \cdot 68F + 05 3 \cdot 68F + 05 2 \cdot 07F + 05 4 \cdot 18F + 05 4 \cdot 18F + 05 1 \cdot 53F + 04 3 \cdot 32F + 04 1 \cdot 33F + 04 5 \cdot 83F + 04 \\ 5 \cdot 83F + 0$
ENERGY (KEV) 103 124 155 207 310 413 620 827 1.033 1.240 1.550 2.066 3.100 4.133 6.199	PFRCENT DTFFERENCE 9.8 13.8 13.7 13.4 -7.7 -7.1 -12.9 -4.4 -8.2 -14.8 -7.4 -13.2 -9.9 -7.3 3.7	MCGUIRE 1.50E+06 1.30E+06 1.03E+06 6.80E+05 3.30E+06 1.92E+06 7.30E+05 2.20E+05 1.30E+05 1.30E+05 7.80E+04 3.40E+04 1.20E+04 2.00E+04	$KAMAN 1 \cdot 37F + 05 1 \cdot 14F + 06 9 \cdot 06F + 05 5 \cdot 99F + 05 5 \cdot 57F + 05 5 \cdot 57F + 05 5 \cdot 57F + 05 5 \cdot 40F + 04 5 \cdot 40F + 05 \cdot 40F +$
ENERGY (KEV) •103 •124 •155 •207 •310 •413 •620 •827 1.033 1.240 1.550 2.066 3.100 4.133 6.199 8.265	PFRCENT DTFFERENCF 9.8 13.8 13.7 13.4 -7.7 -7.1 -12.9 -4.4 -8.2 -14.8 -7.4 -13.2 -9.9 -7.3 3.7 5.7	MCGUIRE 1.50E+06 1.30E+06 1.03E+06 6.80E+05 3.30E+06 7.30E+05 4.00E+05 2.20E+05 1.30E+05 7.80E+04 3.40E+04 1.20E+04 2.00E+04 4.00E+04 4.10E+03	$KAMAN 1 \cdot 37F + 05 1 \cdot 14F + 06 9 \cdot 06F + 05 5 \cdot 99F + 05 3 \cdot 54F + 05 2 \cdot 07F + 05 4 \cdot 14F + 05 1 \cdot 53F + 05 1 \cdot 53F + 04 3 \cdot 42F + 04 1 \cdot 33F + 04 1 \cdot 93F + 04 3 \cdot 61F + 03 5 + 04 5 \cdot 61F + 05 5 + 0$

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ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUTRE	KAMAN
.103	18.8	1.80E+06	1.51++00
.124	18.2	1.53E+06	1.24F+06
.155	10.1	1.16E+06	1.05F+0b
.207	8.7	7.80E+05	7.17F+05
.310	16.5	4.30E+05	3.69E+05
.413	5.2	5.50E+06	2.09F+06
.620	-7.7	9.20E+05	9.97F+05
.827	6	5.00E+05	5.03E+05
1.033	3.4	3.00E+05	2.90E+15
1.240	-1.4	1.80E+05	1.825+05
1.550	-4.3	4. HOE+04	1.02E+05
2.066	-3.9	4.60E+04	4.78F+04
3.100	-8.5	1.50E+04	1.64F + 04
4.133	-12.0	6.10E+04	6.93E+14
6.199	3.3	2.40E+04	2.32F+04
8.265	5.3	1.10E+04	1.1)4F+1)4
10.332	9.9	5.10E+03	5.55++03
ENERGY	00000	SCANDIUM	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KAMAN
•105	1.5	1.95E+0.6	1.425+06
•174	3.4	1.671.+06	1.621+06
• 1 ¬¬¬	-3.3	1.252+06	1.295+06
• 210	-11.0	(• 80E + 05	4.76++05
• 510	-4.8	4.302+05	4.52E+115
•413 600	13.0	2.506+05	2.215+08
+020 807	• 1	1.20E+06	1.20++06
1 700	11.4	5.80E+05	6.11r+05
1 240	10.4	4.10E+05	3.72++05
1 560	12.44		2.235+05
2 066	7 5		1.255+05
3.100	1.5	9. JUE + 04	5.46F+04
4.133	7 4		-01++04
6,199	-2 5	2 705+04	7.345+U3
8.265	7.6	1 355404	1 245 - 0.0
10 222	10 5		

CHROMIUM

ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUTRE	# A - A wing
.103	14.4	4.158+06	3. + 7++115
.124	12.9	3.30E+06	2.42F+UN
.155	7.8	2.40E+06	2.225+135
.207	7	1.45E+06	1.44++06
.310	-2.6	7.208+05	7.34F + 15
.413	4.6	4.50E+05	4.308+45
•650	-88.2	2.00£+05	1.70++06
.827	11.5	1.10E+06	5.44F+UD
1.033	15.4	6.70E+05	5.315+(15
1.240	8.1	4.00E+05	3.70++05
1.550	9.4	2.30E+05	2.1115+115
2.066	3.4	1.03E+05	9.97E+04
3.100	-3.0	3.30E+04	3.49F+114
4.133	-4.5	1.50E+04	1.578+04
6.199	-11.0	4.00E+04	4.448+04
8.265	1.4	2.10E+04	2.179+04
10.332	5.5	1.18E+04	1.12F+04
12.398	7.4	7.20E+03	6.71F+43
		MANGANESE	
ENERGY	PERCENT		

MCGUINE * Annant (KEV) DIFFERENCE .103 5.45E+06 3.96F+06 37.5 .124 37.5 4.45E+06 3.24++05 3.30E+06 2.50-+05 .155 32.0 .207. 23.8 2.05E+06 1.66F+55 .310 15.7 4.80E+05 B.47E+05 .413 20.5 6.00E+05 4.92F+05 .620 13.9 2.50E+05 2.20F+05 .827 - <u> </u> 1.10E+06 1.118+05 1.033 -9.2 6.00E+05 5.611+05 1.240 -5.9 4.00E+05 4.25F+05 1.550 -13.7 2.10E+05 2.47F+(15 2.066 -15.8 9.90E+04 1.16F+05 3.100 -22.8 3.10E+04 4.021+04 4.133 -24.2 1.40E+04 1.25F+04 6.199 -25.6 4.60E+03 6.145+113 8.265 7.9 2.555+04 2.368+04 1.28F+14 10.332 9.4 1.40E+04 12.398 5.3 H.10E+03 7. +4+43 15.498 -2.2 4.00E+03 4.04F+03

TITANIHM

		Carl Contractor	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KAMAN
.103	12.6	2.55E+06	1.26F+00
.124	23.3	2.32E+0h	1.446 +00
.155	14.5	-1.70E+06	1.428+115
.207	1.4	1.02E + 0.6	1.01F+05
.310	-8.4	4 • R0E+05	5.248+05
.413	3.8	3.201+05	3.045+05
.620	1.3	1.40E+06	1.388+06
.827	3.1	7.40E+05	7.17F+05
1.033	5.5	4.40E+05	4.17F+05
1.240] 3.4	3.008+05	2.658+05
1.550	6.8	1.60E+05	1.50F+05
2.066	3.5	7.30E+04	7.055+04
3.100	2.8	2.50E+04	2.43F+04
4.133	2.7	1.15E+04	1.12E+04
6.199	-1.2	3.20E+04	3.24F+114
8.265	3. P	1.556+()4	1.49F+04
10.332	6	8.005+03	8.05E+03
12.398	-4.5	4.60E+03	4.825+03

		MANAD TIM	
		VANALITIM	
ENERGY	DERCENT		
(KEV)	DIFFERENCE	MCGUTPE	KAMAN
.103	18.6	3.20E+06	2.70E+06
.124	21.7	2.70E+06	2.22E+06
.155	18.3	2.05E+06	1.73F+Uh
.502	4.5	1.22E+05	1.17F + 06
.310	-9.6	5.50E+05	5.09F+115
•413	-2.7	3.506+05	3.405+05
.620	12.0	1.55E+06	1. 385+115
.827	-4.]	8.00E+05	0.34F+115
1.033	2.1	5.00E+05	4.90F+05
1.240	-3.R	3.00E+05	3.12F+05
1.550	-4.1	1.70E+05	1.775+05
2.066	-2.1	H.20E+04	8.3×F+U4
3.100	-3.4	2.75E+04	2.355+04
4.133	-5.9	1.23E+04	1.315+114
6.199	-9.4	3.451+04	3.218+04
8.265	-2.8	1.70E+04	1.75F+04
10.335	-3.4	9.10E+03	9.42F+13
15.368	-2.5	5.50E+03	5.548+03

Table II. Continued

T	υ	\cap	2.1
	1.4	1.1	1.4

ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KAMAN
.103	28.9	6.00E+06	4.665+60
.124	32.3	5.05E+06	3.82F+06
.155	31.7	3.90E+06	2.96F+06
.202	27.2	2.50E+06	1.97F+06
.310	9.8	1.10E+06	1.00F+06
.413	7.6	6.30E+05	5.868+05
.620	1.2	2.60c+05	2.578+05
.827	- • 9	1.10E+06	1.]]F+05
1.033	1.3	7.70E+05	7.60F+115
1.240	12.0	5.50E+05	4.91F+05
1.550	-4.3	2.70E+05	5.426+02
2.066	-7.8	1.25E+05	1.36F+05
3.100	-6.7	4.40E+04	4.725+04
4.133	-3.0	2.10E+04	2.168+94
6.199	6.6	7.70E+03	7.221+113
8.265	1.7	2.752+04	2.70E+04
10.332	1.5	1.501+04	1.48E+04
12.398	3.0	4.211E+13	H. 47F+13
15.498	2.6	4.90E+03	4.72F+113

COHALT

ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRF	KAMAN
.103	29.3	6.80E+06	5.26F+UB
.124	27.7	5.55E+06	4.151+00
.155	20.3	4.10E+06	3.418+06
.207	11.6	2.55E+06	2.29F+00
•310	7.}	1.25E+06	1.17F+06
•413	-4 • A	6.50E+05	6.83E+05
•620	20.6	3.60F+05	2.49E+UD
.827	-3.8	1.50F+0E	1.75E+06
1.033	-10.7	7.70E+05	8.02F+05
1.240	-5.3	5.30E+05	5.608+115
1.550	-4.1	3.108+05	3.23F+05
2.066	-4.1	1.501-+05	1.568+05
3.100	-14.1	4.70E+04	5.47+444
4.133	-16.6	2.108+04	2.52++(14
6.199	-15.7	7.10E+03	6.425+03
8.262	-2.7	3.108+04	3.14F+04
10.335	4.0	1.806+04	1.73F + ()4
12.398	3.7	1.048+04	1.04F + 04
15.498	4.5	5. ROE+03	5 45F+03

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ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIPE	KATIAN
.103	38.1	7.70E+116	5.5×5+15
.124	35.2	6.755+06	4.444+110
.155	34.8	5.35E+06	3.97E+Ub
.207	27.8	3.40E+06	2.66F+66
.310	9.6	1.50E+06	1.37E + 0.6
.413	6.5	8.502+05	7.94E+05
.620	10.4	3.90E+05	1.53F+05
.827	1.5	1.90E+05	1.×7F+05
1.033	-9.6	9.00E+05	9.95E+05
1.240	-6.2	5.000+05	5.408+05
1.550	-8.1	3.40E+05	3.708+05
2.066	-11.0	1.60E+05	1.405+05
3.100	-17.4	5.20E+04	5.29F+U4
4.133	-13.3	2.50E+04	2.44F+U4
6.199	-]4.7	8.20E+03	4.61F+03
8.265	-20.5	3.50E+03	4.41F+03
10.332	9,8	2.07E+04	1.89F+04
12.398	8.4	1.25E+04	1.15F+04
15.498	4.1	6.50E+03	5-24F+113

		COPPER	
LNERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KAMAN
.103	24.6	8.15E+06	5.545+16
.124	26.1	7.15E+06	5.67F+06
.155	21.5	5.80E+06	4.77F+06
.207	28.8	4.00E+06	3.10F+06
.310	6.0	1.70E+06	1.60F+06
.413	. P	9.50E+05	4.42F+05
.620	2.9	4.30£+05	4.188+05
.827	-7.1	2.10E+05	5.54F+05
1.033	- . 8	1.00E+06	1.01F+06
1.240	-9.6	6.70E+05	7.4]++05
1.550	- A . R	3.40E+05	4.258+05
2.066	-8.4	1.90E+05	5.04E+05
3.100	-8.8	6.50E+04	7.13F+04
4.133	-10.5	3.00E+04	3.35F+04
6.199	-10.7	1.00E+04	1.12E + 04
8.265	-12.5	4.50E+13	5.14F+U3
10.335	9.2	2.351+114	2.158+04
12.398	10.1	1.45E+04	1.32F+04
15.498	- 8	7.201+03	7-148+03

ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUTPE	KA Apr.
.103	18.3	H.45E+06	7.14++05
.124	15.8	7.05E+06	5.09F+06
.155	10.3	5.75E+06	5.21F+00
.207	4.0	3.80E+16	3.65F+06
.310	-3.7	1.45E+06	1.428+06
.413	-5.1	1.07E+06	1.13E+4E
.620	-8.9	4.40E+05	4.836+00
.827	-18.2	2.10E+05	2.578+05
1.033	109.3	1.06E+06	5.07F+05
1.240	-20.7	6.60F+05	8.32F+05
1.550	-13.0	4.20E+05	4.43++05
2.066	-17.0	1.951+115	2.35F+05
3.100	- ^A .]	7.50E+04	8.16E+U4
4.133	-25.2	2.85E+114	3.818+04
6.199	-26.9	9.40E+03	1.29E+04
8.265	-29.4	4.20E+03	5.95F+03
10.335	• 9	2.50E+04	2.4×E+04
12.398	2.3	1.55E+04	1.528+04
15.498	1.1	8.30E+13	8.21F+03
20.663	-1.5	3.606+03	3.65F+0.3

GALLIUM

ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIPE	K A 4 4 4
.103	23.8	8.65E+06	6.446+40
.124	16.2	7.556+06	6.561+06
.155	17.3	6.35E+06	5.41F+10
.207	19.2	4.901+05	4.11F+06
.310	15.0	2.556+46	2.725+06
.413	7.4	1.40E+06	1.34F+UH
.620	-7.4	5.20E+05	5.62F+05
.827	-6.4	2.80E+05	2.448+05
1.033	-9.5	1.602+05	1.77F+05
1.240	-4.6	7.80E+05	4.19F+05
1.550	-6.0	5.10E+05	5.42F+05
2.066	-13.3	2.301+115	2.65F+115
3.100	-18.9	7.501+()4	4.24F+04
4.133	-16.0	3.60E+04	4.24F+04
6.199	-18.0	1.201+04	1.451+14
8.265	-21.1	5.30E+03	6.728+03
10.335	634.4	2.70E+04	3.6KF+(13
12.398	1.8	1.70E+04	1.67F+U4
15.498	2.4	4.30F+03	4.04F+U3
20.663	3.4	4.20E+03	4.965+03

GERMANTUM

		Sector of the sector	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRF	KAMAN
.103	17.5	B.20F+06	6.98E+06
.124	13.8	7.85E+06	6.90F+U6
.155	15.5	-6.80E+06	5.89F+06
.202	19.8	5.50E+06	4.595+10
.310	30.0	3.30E+06	2.54F+05
.413	39.7	2.10E+06	1.50F+05
.620	-2.1	6.40E+05	6.54F+05
·827	-2.1	3.40£+05	3.475+05
1.033	-3.0	2.00E+05	2.068+05
1.240	90.2	9.10E+05	4.74F+05
1.550	-5.0	5.80E+05	6.11F+05
2.066	-9.7	2.70E+05	2.448+05
3.100	-19.1	5.50E+04	1.05F+05
4.133	-17.8	4.00E+04	4.47F+04
6.199	-17.7	1.35E+04	1.64F + ()4
8.265	-18.8	6.10E+03	7.51F+U3
10.332	-]9.4	3.30E+03	4.09F+03
12.398	4.3	1.90 <u></u> +04	1. H2F+U4
15.498	6.4	1.06E+04	9.47E+03
20.663	4.6	4.70E+03	4.49F+03

ARSENIC

		- No. 62 - 137 - 152 - 17 - 6	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUTPE	KANAN
.103	18.1	7.62E+05	6.451+06
.124	17.5	7.405+06	5.30F+06
.155	13.9	7.10E+06	6.231+06
.207	12.0	5.705+06	5:041+00
.310	11.7	3.226+06	2.547+06
.413	9.1	1.89E+06	1.72F+0t
.620	-10.0	5.80E+05	7.56F+05
.827	-7.7	3.70E+05	4.075+05
1.033	-7.9	2.20E+05	2.34F+05
1.240	-6.7	1,450+05	1.558+05
1.550	-5, A	6.40E+05	5,74F+05
2.066	-4.6	3.20E+05	3. 355+65
3.100	-7.1	1.101+05	1.12F+115
4.133	-11.1	4.40E+04	5.5] F+04
6.199	-9.5	1.70E+04	1. 438 + 1)4
8.265	-]0.6	7.70E+03	8.61F+03
10.332	-17.2	3.90E+03	4.718+113
12.398	10.1	2.30E+04	2.095+04
15.498	3.4	1.1×±+04	1.14 - + 04
20.663	-2.8	5.008+03	5-148+13

SELENIHM

ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIPE	KAMAN
.103	11.5	6.00F+05	5.38++00
.124	29.5	7.50E+06	5.748+00
.155	15.8	7.10E+06	6.1 ×F+06
.207	17.0	6.25E+11A	5.44+45
.310	8.0	3.551+06	3.248+06
•413	a.	2.00E+06	1.488406
•650	-14.3	7.506+05	3.15F+15
.827	-13.8	4.00±+05	4.64F+05
1.033	-11.6	2.455+05	2.77++05
1.240	-16.3	1.50E+05	1.798+05
1.550	-8.7	6.00E+05	6.67F+05
2.066	1.0	3.80E+05	3.76F+U5
3.100	-13.8	1.15E+05	1.33F+05
4.133	-16.5	5.20£+04	5.238+04
6.199	-15.1	1.ROE+ 04	2.128+04
8.265	-13.8	8.40E+03	9.745+03
10.332	-13.6	4.60E+03	5.336+03
12.398	-17.0	2.70E+03	3.25F+63
15.498	6.9	1.37E+04	1.288+04
20.663	• 1	5.800+03	5.K0F+03
30.995	3.4	1.40E+03	1.848+03
		COMINE	
		is iteration Table	
ENERGY	PERCENT		
ENERGY (KEV)	PERCENT DIFFERENCE	MCGUINE	KAMAN
ENERGY (KEV) .103	PERCENT DIFFEPENCE -19.6	MCGUINE 3.001+06	КАНАЛ 3.738+05
ENERGY (KEV) .103 .124	PERCENT DIFFERENCE -19.6 36.0	MCGUIRE 3.00E+06 6.40E+06	KAMAN 3.738+05 4.718+05
ENERGY (KEV) .103 .124 .155	PERCENT DIFFERENCE -19.6 36.0 30.7	MCGUINE 3.00E+06 6.40E+06 7.75E+06	KAMAN 3.738+05 4.718+05 5.938+05
ENERGY (KEV) .103 .124 .155 .207	PERCENT DIFFERENCE -19.6 36.0 30.7 31.6	MCGUINF 3.00E+06 6.40E+06 7.75E+06 7.35E+06	KAMAN 3.738+00 4.718+00 5.938+00 5.548+00
ENERGY (KEV) .103 .124 .155 .207 .310	PERCENT DIFFEPENCE -19.6 36.0 30.7 31.6 13.7	MCGUIRE 3.00E+06 6.40E+06 7.75E+06 7.35E+06 4.10E+06	KAMAN 3.738+45 4.718+05 5.938+08 5.548+08 3.608+06
ENERGY (KEV) .103 .124 .155 .207 .310 .413	PERCENT DIFFEPENCE -19.6 36.0 30.7 31.6 13.7 3.8	MCGUTHF 3.00E+06 5.40E+06 7.75E+06 7.35E+06 4.10E+06 2.30E+06	KAMAN 3.73F+U5 4.71F+05 5.93F+05 5.54F+06 3.60F+05 2.22F+06
ENERGY (KEV) .103 .124 .155 .207 .310 .413 .620	PERCENT DIFFERENCE -19.6 36.0 30.7 31.6 13.7 3.8 -21.2	MCGUIRF 3.00E+06 5.40E+06 7.75E+06 7.35E+06 4.10E+06 2.30E+06 7.80E+05	KAMAN 3.73F+45 4.71F+05 5.93F+06 5.59F+06 3.60F+05 2.22F+06 9.44F+05
ENERGY (KEV) .103 .124 .155 .207 .310 .413 .620 .827	PERCENT DIFFERENCE -19.6 36.0 30.7 31.6 13.7 3.8 -21.2 -12.8	MCGUINF 3.00E+06 5.40E+06 7.75E+06 7.35E+06 4.10E+06 2.30E+06 7.80E+05 4.60E+05	KAMAN 3.73F+U5 4.71F+05 5.93F+05 5.59F+06 3.60F+05 2.22F+05 9.84F+05 5.28F+05
ENERGY (KEV) .103 .124 .155 .207 .310 .413 .620 .827 1.033	PERCENT DIFFERENCE -19.6 36.0 30.7 31.6 13.7 3.8 -21.2 -12.8 -9.9	MCGUIRF 3.00E+06 5.40E+06 7.75E+06 7.35E+06 4.10E+06 2.30E+06 7.80E+05 4.60E+05 2.55E+05	KAMAN 3.73F+U5 4.71F+05 5.93F+05 5.54F+06 3.60F+05 7.22F+05 5.28F+05 5.28F+05 3.16F+05
ENERGY (KEV) .103 .124 .155 .207 .310 .413 .620 .827 1.033 1.240	PERCENT DIFFEPENCE -19.6 36.0 30.7 31.6 13.7 3.8 -21.2 -12.8 -9.9 -10.0	MCGUIRF 3.00E+06 6.40E+06 7.75E+06 7.35E+06 4.10E+06 2.30E+06 7.80E+05 4.60E+05 2.85E+05 1.85E+05	KAMAQ 3.73F+U5 4.71F+05 5.93F+06 5.59F+06 3.60F+05 7.22F+05 5.28F+05 5.28F+05 3.16F+05 2.05F+05
ENERGY (KEV) .103 .124 .155 .207 .310 .413 .620 .827 1.033 1.240 1.550	PERCENT DIFFEPENCE -19.6 36.0 30.7 31.6 13.7 3.8 -21.2 -12.8 -9.9 -10.0 416.3	MCGUIRF 3.00E+06 5.40E+06 7.75E+06 7.35E+06 4.10E+06 2.30E+06 7.80E+05 4.60E+05 1.85E+05 1.85E+05 6.20E+05	KAMAN 3.73F+U5 4.71F+05 5.93F+05 5.54F+05 3.60F+05 3.60F+05 5.22F+05 5.24F+05 3.16F+05 2.05F+05 1.20F+05
ENERGY (KEV) .103 .124 .155 .207 .310 .413 .620 .827 1.033 1.240 1.550 2.066	PERCENT DIFFEPENCE -19.6 36.0 30.7 31.6 13.7 3.8 -21.2 -12.8 -9.9 -10.0 416.3 -10.4	MCGUTHF 3.00E+06 5.40E+06 7.75E+06 7.35E+06 4.10E+06 2.30E+06 7.80E+05 4.60E+05 2.85E+05 1.85E+05 1.85E+05 3.75E+05	KAMAN 3.73F+U5 4.71F+05 5.93F+05 5.54F+05 3.60F+05 7.22F+05 9.44F+05 5.24F+05 3.16F+05 2.05F+05 1.20F+05 4.1×F+05
ENERGY (KEV) .103 .124 .155 .207 .310 .413 .620 .827 1.033 1.240 1.550 2.066 3.100	PERCENT DIFFEPENCE -19.6 36.0 30.7 31.6 13.7 3.8 -21.2 -12.8 -9.9 -10.0 416.3 -10.4 -19.6	MCGUTHF 3.00E+06 5.40E+06 7.75E+06 7.35E+06 4.10E+06 2.30E+06 7.80E+05 4.60E+05 2.85E+05 1.85E+05 3.75E+05 1.20E+05	KAMAN 3.73 F +00 4.71 F +00 5.93 F +00 5.93 F +00 3.60 F +00 3.60 F +00 3.60 F +00 3.16 F +05 3.16 F +05 3.16 F +05 1.20 F +0
ENERGY (KEV) .103 .124 .155 .207 .310 .413 .620 .827 1.033 1.240 1.550 2.066 3.100 4.133	PERCENT DIFFEPENCE -19.6 36.0 30.7 31.6 13.7 3.8 -21.2 -12.8 -9.9 -10.0 416.3 -10.4 -19.6 -22.7	MCGUTHE 3.00E1HE 3.00E1HE 3.00E1HE 5.40E1HE 7.75E1HE 7.35E1HE 4.10E1HE 2.30E1HE 7.80E1HE 2.55E1HE 2.55E1HE 3.75E1HE 3.75E1HE 3.75E1HE 5.40E1HE	KAMAN 3.73 F +00 4.71 F +00 5.93 F +00 5.93 F +00 3.60 F +00 3.60 F +00 3.60 F +05 3.16 F +05 3.16 F +05 3.16 F +05 1.20 F +05 4.1 E F+05 4.1 E F+05 4.5 F +05 4.5 F +05 4.5 F +05 4.5 F +05 5.5 F +05
ENERGY (KEV) .103 .124 .155 .207 .310 .413 .620 .827 1.033 1.240 1.550 2.066 3.100 4.133 6.199	PERCENT DIFFEPENCE -19.6 36.0 30.7 31.6 13.7 3.8 -21.2 -12.8 -9.9 -10.0 416.3 -10.4 -19.6 -22.7 -22.1	MCGUIRF 3.00E+06 5.40E+06 7.75E+06 7.35E+06 4.10E+06 2.30E+06 7.80E+05 4.60E+05 1.85E+05 1.85E+05 5.20E+05 1.20E+05 1.20E+06 5.40E+04	KAMAA 3.73F+05 4.71F+05 5.93F+05 5.54F+05 3.60F+05 3.60F+05 3.22F+05 3.28F+05 3.16F+05 3.16F+05 4.1×F+05 4.1×F+05 4.3×F+04 4.3×F+04
ENERGY (KEV) 103 124 155 207 310 413 620 827 1033 1.240 1.550 2.066 3.100 4.133 6.199 8.265	PERCENT DIFFEPENCE -19.6 36.0 30.7 31.6 13.7 3.8 -21.2 -12.8 -9.9 -10.0 416.3 -10.4 -19.6 -22.7 -22.1 -21.9	MCGUIPF 3.00E+06 5.40E+06 7.75E+06 7.35E+06 4.10E+06 2.30E+06 7.80E+05 4.60E+05 1.85E+05 1.85E+05 5.20E+05 1.20E+05 1.20E+05 1.85E+04 1.85E+04 4.50E+03	KAMAA3.73F+054.71F+055.93F+055.54F+053.60F+055.22F+055.24F+055.24F+055.24F+051.20F+051.20F+051.44F+051.44F+051.44F+042.34F+042.34F+04
ENERGY (KEV) .103 .124 .155 .207 .310 .413 .620 .827 1.033 1.240 1.550 2.066 3.100 4.133 6.199 8.265 10.332	PERCENT DIFFEPENCE -19.6 36.0 30.7 31.6 13.7 3.8 -21.2 -12.8 -9.9 -10.0 416.3 -10.4 -19.6 -22.7 -22.1 -21.9 -24.2	MCGUTHF 3.00E+06 5.40E+06 7.75E+06 7.75E+06 4.10E+06 2.30E+06 7.80E+05 4.60E+05 1.85E+05 1.85E+05 3.75E+05 1.20E+05 3.75E+05 1.20E+04 1.85E+04 1.85E+03 4.50E+03	KAMAN 3.73 F +05 4.71 F +05 5.93 F +05 5.54 F +05 3.60 F +05 3.60 F +05 3.22 F +05 3.16 F +05 3.16 F +05 3.16 F +05 1.20 F +04 1.04 F +04 5.94 F +03
ENERGY (KEV) .103 .124 .155 .207 .310 .413 .620 .827 1.033 1.240 1.550 2.066 3.100 4.133 6.199 8.265 10.332 12.398	PERCENT DIFFEPENCE -19.6 36.0 30.7 31.6 13.7 3.8 -21.2 -12.8 -9.9 -10.0 416.3 -10.4 -19.6 -22.7 -22.1 -21.9 -24.2 -25.4	MCGUTHF 3.00E+06 5.40E+06 7.75E+06 7.75E+06 4.10E+06 2.30E+06 7.80E+05 4.60E+05 1.85E+05 1.85E+05 1.85E+05 3.75E+05 1.20E+05 1.20E+04 1.85E+04 1.85E+04 4.50E+03 4.50E+03	KAMAA3.73F+054.71F+055.93F+055.54F+053.60F+053.60F+055.24F+053.16F+053.16F+051.20F+051.20F+054.1xF+054.1xF+054.1xF+054.34F+042.34F+042.34F+043.52F+043.52F+04
ENERGY (KEV) .103 .124 .155 .207 .310 .413 .620 .827 1.033 1.240 1.550 2.066 3.100 4.133 6.199 8.265 10.332 12.398 15.498	PERCENT DIFFEPENCE -19.6 36.0 30.7 31.6 13.7 3.8 -21.2 -12.8 -9.9 -10.0 416.3 -10.4 -19.6 -22.7 -22.1 -21.9 -24.2 -25.4 16.8	MCGUTHF 3.00E+06 5.40E+06 7.75E+06 7.75E+06 7.35E+06 4.10E+06 2.30E+06 7.80E+05 4.60E+05 1.85E+05 1.85E+05 1.85E+05 1.20E+05 1.20E+05 1.85E+04 1.85E+04 1.85E+04	KAMAA3.73F+004.71F+005.93F+005.93F+003.60F+003.60F+005.24F+005.24F+001.20F+001.20F+001.20F+001.44F+042.30F+041.04F+041.04F+031.41F+04
ENERGY (KEV) .103 .124 .155 .207 .310 .413 .620 .827 1.033 1.240 1.550 2.066 3.100 4.133 6.199 8.265 10.332 12.398 15.498 20.663	PERCENT DIFFEPENCE -19.6 36.0 30.7 31.6 13.7 3.8 -21.2 -12.8 -9.9 -10.0 416.3 -10.4 -19.6 -22.7 -22.1 -21.9 -24.2 -25.4 16.8 7.6	MCGUTHF 3.00E10F 3.00E106 5.40E+06 7.75E+06 7.75E+06 7.35E+06 4.10E+06 2.30E+06 7.80E+05 4.60E+05 1.85E+05 1.85E+05 1.85E+05 1.85E+05 1.85E+05 1.85E+05 1.85E+05 1.85E+05 1.85E+04 1.85E+04 1.85E+04 1.65E+04 2.70E+03 1.65E+04 5.90E+03	$\begin{array}{c} KAMAN\\ 3.73F + 0.6\\ 4.71F + 0.6\\ 5.93F + 0.6\\ 5.93F + 0.6\\ 5.60F + 0.6\\ 3.60F + 0.6\\ 9.84F + 0.5\\ 3.62F + 0.5\\ 3.16F + 0.5\\ 3.16F + 0.5\\ 3.16F + 0.5\\ 1.20F + 0.5\\ 1.49F + 0.4\\ 1.04F + 0.4\\ 1.04F + 0.3\\ 3.62F + 0.3\\ 1.41F + 0.4\\ 5.94F + 0.3\\ 1.41F + 0.4\\ 5.94F + 0.3\\ 1.41F + 0.4\\ 1.41F + 0.4\\ 1.41F + 0.3\\ 1.41$

		KRYPTON	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KAMAN
.103	-6.7	1.20E+06	1.29E+06
.124	31.7	3.40E+06	2.58E+06
.155	13.7	- 6.10E+06	5.37E+06
.502	25.9	6.80E+06	5.408+06
.310	6.7	4.40E+06	4.12F+06
.413	3.2	2.65E+06	2.57E+06
• 650	-17.6	9.50E+05	1.15E+06
.827	-12.2	5.408+05	6.15E+05
1.033	-7.9	3.40E+05	3.64E+05
1.240	-8.3	2.20E+05	2.40E+05
1.550	401.4	7.00E+05	1.40F+05
2.066	-21.1	4.10E+05	5.20F+05
3.100	-19.4	1.40E+05	1.74F+05
4.133	-23.5	6.10E+04	7.98E+04
6.199	-25.0	2.00E+04	2.67F+14
8.265	-21.6	9.60E+03	1.22F+04
10.332	-20.8	5.30E+03	6.70F+03
12.398	-21.8	3.20E+03	4.04F+113
15.498	32.2	2.058+04	1.55F+U4
20.663	11.6	7.906+173	7.08E+03
30.995	-3.2	2.20E+03	2.275+03

RUHIDIUM

		A O A LEATAN	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KAMAN
.103	-45.6	2.50E+05	4.60E+05
.124	-31.5	1.00E+06	1.46F+05
.155	-8.3	3.90E+06	4.25F+06
.207	-10.0	4.80E+06	5.334+05
.310	2.9	4.30E+06	4.18F+06
•413	-5.1	2.656+06	2.795+06
• 620	-1.7	1.25E+06	1.27E+06
.827	15.1	7.70E+05	6.87E+05
1.033	21.3	5.00E+05	4.125+05
1.240	11.1	3.00E+05	2.705+05
1.550	1.7	1.602+05	1.576+05
2.066	-19.5	4.80E+115	5.46F+05
3.100	-18.7	1.605+05	1.478+05
4.133	-10.8	A.00E+04	B.445+14
6.199	-5.0	2.90E+04	2.96F+14
8.265	3.9	1.40E+04	1.358+44
15.398	10.2	4.40E+03	4.444+113
15.498	-5.9	1.60E+04	1.70 + 04
20.663	12.8	8.×0E+03	7.80++03
30.995	7.3	2.70E+03	2.525+03
41.327	4.0	1.15E+03	1.11F+0.5

Table II. Continued

STRONTIUM

ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KANAN
.103	-6.7	5.106+05	5.478+05
.124	-3.7	4.70E+05	4 427+45
.155	-83.3	3.90E+05	2.37F+06
.207	-14.8	4.30E+06	5.05++06
.310	13.3	5.00E+06	4.418+06
.413	12.0	3.40E+06	3.04F+06
.620	13.4	1.60E+06	1.418+06
.827	17.3	9.00E+05	7.67F+05
1.033	23.0	5.70E+05	4.63E+65
1.240	31.7	4.00E+05	3.04F+05
1.550	49.1	2.65E+05	1.74F+05
2.066	-15.1	4.70E+05	5.54E+05
3.100	-4.2	S.10E+05	2.19F+05
4.133	5.1	1.058+05	4.99F+04
6.199	33.6	4.40E+04	3.29E+04
8.265	53.4	2.30E+04	1.50F+04
12.398	100.0	9.90E+03	4.95++03
15.498	108.3	5.60E+03	2.69F+113
20.663	36.0	1.17E+04	×.60++03
30.995	25.6	3.50E+03	2.79F+03
41.327	25.2	1.505+03	1.23F+03
		YTTRIUM	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	WCENINF	$K \Delta M \Delta M$

(KEV)	DIFFERENCE	MCGUIHF	KAMAN
.103	18.3	7.60E+05	h.42F+05
.124	16.7	6.80E+05	5.83F+05
.155	444.8	2.80E+06	5.14F+05
.207	50.9	6.90E+06	4.571+06
.310	-6.0	4.4NE+06	4.648+10
.417	-3.0	3.25E+06	3.355+110
.620	-5.0	1.50E+06	1.525+00
.827	-3.6	8.30E+05	8.615+05
1.033	-4.1	5.00E+05	5.22F+UD
1.240	17.0	4.000+05	3.421+05
1.550	17.3	2.35E+()5	2.005+05
2.066	42.7	1.40E+05	4. R1F+14
3.100	-9.7	S. 20E+05	2.448+05
4.133	3.7	1.155+05	1.118+05
6.199	23.0	4.50F+14	3.66F+04
8.265	44.]	2.40F+04	1. 77+ + 04
12.398	P5.0	1.00E+04	5.441+93
15.498	104.5	6.10E+03	2.748+03
20.663	26. ⁸	1.20E+04	7.46E+113
30.995	33.2	4.10E+03	3.688 + 43
41.327	58.3	2.15E+03	1.365+03

		2 T	
ENEDOX	DEDOENT	ZIRCUNTU™	
CNERGI	DIFFERENCE	MCCUTO	
103	DIFFERENCE	7 20E 0F	T D C C C C C
+103	• M	7.201 +05	1.145+10
•174	ر • ر <u>-</u>	5.30t+05	6.671+119
- درج I ه	-14.2	, , , , , , , , , , , , , , , , , , ,	6.166×10
• 207	- 14.5	1.00E+05	2.155+115
• 310	19.2	5.101+06	4.295+05
•413	14.8	3.951+06	3.445+110
•620	14.7	2.00E+06	1.74++05
.827	10.9	1.06E+06	4.664405
1.033	16.9	6.80E+05	ちょみびちょいつ
1.240	25.7	4.80±+0%	す。わびを一日ち
1.550	38.]	3.10E+05	2.248+115
2.066	6].7	1.80E+05	1.115+05
3.100	- • O	2.70E+05	2.13F+15
4.133	9.7	1.35E+05	1.24F+115
6.199	23.4	5.00E+04	4.055+04
8.265	36.2	2.50E+04	1.84F+14
12.398	66.1	1.00E+04	6.02F+0.4
15.498	81.1	5.908+03	3.268+03
20.663	29.5	1.305+04	1.00F+114
30.995	25.1	4.20E+03	3.365+113
41.327	33.3	2.00E+03	1.505+03
i.		N108194	
ENERGY	PERCENT	NIGBIUM	
ENERGY (KEV)	PEPCENT DIFFERENCE	NIGRIUM	ለ በተ ፋላ
ENERGY (KEV) •103	PERCENT DIFFERENCE -8.6	NIGB190 MCGUIPE 7.10E+05	к лиан 7.77F+05
ENERGY (KEV) •103 •124	PERCENT DIFFERENCE -8.6 -14.3	NIGRIUM MCGUTPE 7.16E+05 5.50E+05	к Амал 7.,778+115 7.,546+115
ENERGY (KEV) .103 .124 .155	PEPCENT DIFFERENCE -8.6 -14.3 -24.2	NIGB190 MCGUTPE 7.10E+05 6.50E+05 5.50E+05	к ЛМАЦ 7.775+05 7.546+05 1.256+05
ENERGY (KEV) .103 .124 .155 .207	PEPCENT DIFFERENCE -8.6 -14.3 -24.2 -54.6	NIGBIUM MCGUTHE 7.10E+05 6.50E+05 5.50E+05 5.50E+05 3.90E+05	к Алам 7.775+05 7.595+05 7.255+05 4.555+05
ENERGY (KEV) •103 •124 •155 •207 •310	PEPCENT DIFFERENCE -8.6 -14.3 -24.2 -54.6 -10.0	NIGB194 MCGUTPE 7.10E+05 5.50E+05 5.50E+05 3.90E+05 4.10E+06	к Аман 7.775+105 7.545+105 7.255+105 4.555+105 4.565+100
ENERGY (KEV) 103 124 155 .207 .310 .413	PERCENT DIFFERENCE -8.6 -14.3 -24.2 -54.6 -10.0 13.0	NIGB194 MCGUTPE 7.10E+05 5.50E+05 5.50E+05 3.90E+05 4.10E+06 4.32E+06	KAMAN 7.77F+05 7.54F+05 7.25F+05 4.54F+05 4.54F+05 3.22F+05
ENERGY (KEV) 103 124 155 207 310 413 620	PEPCENT DIFFERENCE -8.6 -14.3 -24.2 -54.6 -10.0 13.0 22.2	NIGB194 MCGUTPE 7.10E+05 5.50E+05 5.50E+05 3.90E+05 4.10E+06 4.32E+06 2.40E+06	KAMAN 7.77F+05 7.59F+05 7.25F+05 4.55F+05 4.55F+00 3.22F+05 1.96F+06
ENERGY (KEV) .103 .124 .155 .207 .310 .413 .620 .827	PEPCENT DIFFERENCE -8.6 -14.3 -24.2 -54.6 -10.0 13.0 22.2 22.3	NIGB194 MCGJTPE 7.16E+05 5.50E+05 5.50E+05 5.90E+05 4.10E+06 4.32E+06 2.40E+06 1.32E+06	KAMAA 7.77F+05 7.59F+05 7.25F+05 4.56F+05 4.56F+06 3.22F+05 1.96F+06 1.08F+06
ENERGY (KEV) 103 124 155 207 310 413 620 827 1.033	PEPCENT DIFFERENCE -8.6 -14.3 -24.2 -54.6 -10.0 13.0 22.2 22.3 21.9	NIGB194 MCGUTPE 7.10E+05 5.50E+05 5.50E+05 3.90E+05 4.10E+06 4.32E+06 2.40E+06 1.32E+06 5.00E+05	<pre>KAMAQ 7.77F+05 7.54F+05 7.54F+05 4.56F+05 4.56F+05 1.96F+06 1.04F+06 1.04F+06 6.56F+05</pre>
ENERGY (KEV) 103 124 155 207 310 413 620 827 1.033 1.240	PEPCENT DIFFERENCE -8.6 -14.3 -24.2 -54.6 -10.0 13.0 22.2 22.3 21.9 23.1	NIGB194 MCGUTPE 7.10E+05 5.50E+05 5.50E+05 3.90E+05 4.10E+06 4.32E+06 2.40E+06 1.32E+06 5.00E+05 5.30E+05	KAMAQ 7.77F+05 7.54F+05 7.54F+05 4.54F+05 4.54F+05 3.42F+05 1.94F+05 1.94F+05 4.31F+05 4.31F+05
ENERGY (KEV) 103 124 155 207 310 413 620 827 1.033 1.240 1.550	PEPCENT DIFFERENCE -8.6 -14.3 -24.2 -54.6 -10.0 13.0 22.2 22.3 21.9 23.1 30.5	NIGB194 MCGUTPE 7.10E+05 5.50E+05 5.50E+05 5.50E+05 4.10E+06 4.32E+06 2.40E+06 1.32E+06 5.00E+05 5.30E+05 3.30E+05	KAMAQ 7.77F+05 7.59F+05 7.59F+05 7.59F+05 4.56F+00 3.42F+05 1.96F+06 1.96F+06 6.56F+05 4.31F+05 2.53F+05
ENERGY (KEV) 103 124 155 207 310 413 620 827 1.033 1.240 1.550 2.066	PEPCENT DIFFERENCE -8.6 -14.3 -24.2 -54.6 -10.0 13.0 22.2 22.3 21.9 23.1 30.5 40.4	NIGB1900 MCGUTPE 7.10E+05 5.50E+05 5.50E+05 5.50E+05 4.10E+06 4.32E+06 2.40E+06 1.32E+06 5.30E+05 3.30E+05 1.75E+05	KAMAA 7.77F+05 7.54F+05 7.54F+05 7.25F+05 4.56F+06 3.42F+05 1.96F+06 1.96F+06 6.56F+05 4.31F+05 4.31F+05 2.53F+05 1.25F+05
ENERGY (KEV) 103 124 155 207 310 413 620 827 1.033 1.240 1.550 2.066 3.100	PEPCENT DIFFERENCE -8.6 -14.3 -24.2 -54.6 -10.0 13.0 22.2 22.3 21.0 23.1 30.5 40.4 -1.2	NIGB194 MCGUTPE 7.10E+05 5.50E+05 5.50E+05 4.00E+05 4.10E+06 4.32E+06 2.40E+06 1.32E+06 5.30E+05 3.30E+05 1.75E+05 3.00E+05	KAMAA 7.77F+05 7.59F+05 7.59F+05 4.56F+05 4.56F+06 1.96F+06 1.96F+06 1.96F+06 4.31F+05 4.31F+05 4.35F+05 1.25F+05 1.25F+05
ENERGY (KEV) 103 124 155 207 310 413 620 827 1.033 1.240 1.550 2.066 3.100 4.133	PEPCENT DIFFERENCE -8.6 -14.3 -24.2 -54.6 -10.0 13.0 22.2 22.3 21.9 23.1 30.5 40.4 -1.2 -1.9	NIGB194 MCGUTPE 7.10E+05 5.50E+05 5.50E+05 4.00E+05 4.10E+06 4.32E+06 2.40E+06 1.32E+06 5.30E+05 3.30E+05 1.75E+05 3.00E+05 1.35E+05	KAMAN 7.77F+05 7.59F+05 7.59F+05 4.55F+05 4.56F+05 1.96F+05 1.96F+05 1.96F+05 4.31F+05 4.31F+05 2.53F+05 1.25F+05 1.25F+05 1.32F+05
ENERGY (KEV) 103 124 155 207 310 413 620 827 1.033 1.240 1.550 2.066 3.100 4.133 6.199	PEPCENT DIFFERENCE -8.6 -14.3 -24.2 -54.6 -10.0 13.0 22.2 22.3 21.9 23.1 30.5 40.4 -1.2 -1.9 10.8	NIGB194 MCGUTPE 7.10E+05 5.50E+05 5.50E+05 4.10E+06 4.32E+06 2.40E+06 1.32E+06 5.30E+05 3.30E+05 1.75E+05 3.00E+05 1.35E+05 5.60E+04	KAMAN 7.77F+05 7.54F+05 7.54F+05 7.54F+05 4.56F+06 3.42F+06 1.96F+06 1.96F+06 1.96F+05 4.31F+05 4.31F+05 1.25F+05 1.25F+05 1.32F+05 1.32F+05
ENERGY (KEV) 103 124 155 207 310 413 620 827 1.033 1.240 1.550 2.066 3.100 4.133 6.199 8.265	PEPCENT DIFFERENCE -8.6 -14.3 -24.2 -54.6 -10.0 13.0 22.2 22.3 21.9 23.1 30.5 40.4 -1.2 -1.9 10.8 17.4	NIGB194 MCGUTPE 7.10E+05 5.50E+05 5.50E+05 4.10E+06 4.32E+06 2.40E+06 1.32E+06 5.30E+05 3.30E+05 3.30E+05 1.75E+05 5.00E+04 2.40E+04	KAMAN 7.77F+05 7.54F+05 7.54F+05 7.54F+05 4.56F+00 3.42F+05 1.96F+06 1.96F+06 1.96F+05 4.31F+05 4.31F+05 1.25F+05 1.32F+05 1.32F+05 1.32F+05 1.32F+05 2.04F+04
ENERGY (KEV) 103 124 155 207 310 413 620 827 1.033 1.240 1.550 2.066 3.100 4.133 6.199 8.265 12.398	PFPCENT DIFFERENCE -8.6 -14.3 -24.2 -54.6 -10.0 13.0 22.2 22.3 21.0 23.1 30.5 40.4 -1.2 -1.9 10.8 17.4 32.8	NIGB194 MCGUTPE 7.16E+05 5.50E+05 5.50E+05 5.50E+05 4.10E+06 4.32E+06 2.40E+06 1.32E+06 5.30E+05 3.30E+05 1.35E+05 5.60E+04 2.40E+04 2.40E+04 2.40E+04	KAMAN 7.77F+05 7.54F+05 7.54F+05 7.54F+05 4.54F+05 4.54F+05 1.94F+05 1.94F+05 4.31F+05 4.31F+05 1.75F+05 1.32F+05 1.32F+05 1.32F+05 1.32F+05 1.32F+05 1.32F+05 1.32F+05 1.32F+05 1.32F+05 1.51F+04 2.04F+04 5.70F+03
ENERGY (KEV) 103 124 155 207 310 413 620 827 1.033 1.240 1.550 2.066 3.100 4.133 6.199 8.265 12.398 15.498	PFPCENT DIFFERENCE -8.6 -14.3 -24.2 -54.6 -10.0 13.0 22.2 22.3 21.9 23.1 30.5 40.4 -1.2 -1.9 10.8 17.4 32.8 40.6	NIGB194 MCGUTPE 7.10E+05 5.50E+05 5.50E+05 5.50E+05 4.10E+06 4.32E+06 2.40E+06 1.32E+06 5.30E+05 3.30E+05 1.75E+05 1.35E+05 1.35E+05 5.00E+04 2.40E+04 2.40E+04 3.10E+03 5.10E+03	K A F A A A A A A A A A A A A A A A A A
ENERGY (KEV) 103 124 155 207 310 413 620 827 1.033 1.240 1.550 2.066 3.100 4.133 6.199 8.265 12.398 15.498 20.663	PFPCENT DIFFERENCE -8.6 -14.3 -24.2 -54.6 -10.0 13.0 22.2 22.3 21.9 23.1 30.5 40.4 -1.2 -1.9 10.8 17.4 32.8 40.6 12.7	NIGBIUM MCGUTPE 7.10E+05 5.50E+05 5.50E+05 5.50E+05 4.10E+06 4.32E+06 2.40E+06 1.32E+06 5.30E+05 3.30E+05 1.35E+05 1.35E+05 5.00E+04 2.40E+04 2.40E+04 2.40E+04 3.10E+03 5.10E+03 1.22E+04	$K \Delta F \Delta H \Delta H A H A H A H A H A H A H A H A H$
ENERGY (KEV) 103 124 155 207 310 413 620 827 1.033 1.240 1.550 2.066 3.100 4.133 6.199 8.265 12.398 15.498 20.663 30.995	PFPCFNT DTFFFPFNCF -8.6 -14.3 -24.2 -54.6 -10.0 13.0 22.2 22.3 21.0 23.1 30.5 40.4 -1.2 -1.9 10.P 17.4 32.8 40.6 12.7 14.3	NIGB194 MCGUTPE 7.16E+05 5.50E+05 5.50E+05 4.90E+05 4.10E+06 4.32E+06 2.40E+06 1.32E+06 2.40E+06 1.32E+05 3.30E+05 3.30E+05 1.35E+05 1.35E+05 1.35E+05 1.35E+05 3.00E+04 2.40E+04 2.40E+03 5.10E+03 1.22E+04 4.20E+03	K A H A A A A A A A A A A A A A A A A A

Table II. Continued

		WOL VEDEDIN	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KAMAN
.103	10.2	8.80E+05	7.94F+05
.124	11.8	9.00E+05	8.05F+05
.155	15.1	9.20E+05	7.94F+04
.207	16.7	8.00E+05	F. HEF+US
.310	-2.8	4.47E+06	4.56F+08
•413	2.9	4.04E+06	3.47F+UF
.620]	2.13E+06	2.13F+0#
.827	-2.6	1.158+06	1.]RF+()
1.033	-3.0	7.00E+05	7.22F+05
1.240	-3.2	4.602+05	4.75F+05
1.550	-10.6	2.50E+05	2.40F+05
2.066	-10.2	1.25E+05	1.346+05
3.100	-16.6	2.406+05	3.36F+U:
4.133	-17.5	1.25E+05	1.528+05
6.199	-17.1	4.10E+04	4.94F+()4
8.265	-14.9	1.90E+04	2.238+04
12.398	-9.4	5.60E+03	7.28E+03
15.498	-5.9	3.70E+03	3.43F+U:
20.663	. 3	1.20E+04	1.20F+(14
30.995	4.0	4.20E+03	4,04F+0;
41.327	1.6	1.958+03	1.228+0.

TECHNETILM

ENERGY	DFR(FN)		
(KEV)	DIFFERENCE	MCGUIRE	KARAB
.103	18.0	1.04t+06	8.82F+05
.124	7.7	4.60E+15	8.41F+05
.155	2.6	9.10E+05	8.57F+05
.207	9.7	8.30F+05	7.568+05
.310	-15.0	3.701+06	4.35F+(A
.413	27.2	4 . 50E+06	3.548+06
.620	5.1	2.408+06	2.29F+05
.827	-2.3	1.25++06	1.28F+116
1.033	-4.5	7.50E+05	7.855405
1.240	-5.1	4 . GOE+35	5.16E+05
1.550	-5.7	2.908+15	3.146+15
2.066	-2.4	1.508+05	1.54F+05
3.100	-18.9	2.458+05	3.64F+05
4.133	-20.1	1.326+05	1.55++05
6.199	-17.0	4.508+04	5.428+04
8.265	-12.7	2.15月+04	2.444+114
15.398	-4 . R	7.70E+03	n, 1998 + 11.1
15.499	ء م	4.40E+03	4.398+()3
20.663	703.5	1.60E+04	1.448+03
30.995	5.2	4.70E+03	4.445+03
41.327	11.1	2.20E+03	1.0RF+113

and a second

6.199

8.265

12.398

15.498

20.663

30.995

41.327

6.7

RUTI	HE N	ΠI	JM
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ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KAMAN
.103	26.0	1.08E+06	5.57F+(15
.124	16.8	1.06E+06	4.1748+05
.155	6.7	1.02F+06	9.56F+05
.207	R.4	9.SAE+AS	H. 765+U5
.310	-60.3	7.50E+05	1.89F+06
.413	-3.A	3.73E+06	3.49F+115
.620	15.1	2.858+06	2.54F+66
.827	7	1.428+06	1.43F+06
1.033	-1.0	4.70E+05	H. 79F+05
1.240	3.9	6.00E+05	5.74F+114
1.550	-7.0	3.208+05	3.44F+05
2.066	-9.1	1.55405	1.701+05
3.100	-6.7	3.10±+05	3.726+115
4.133	-22.7	1.40E+05	1.416+05
6.199	-19.4	4. ROE+04	5.95++1)4
8.265	-13.1	2.35E+04	2.70F+04
12.398	-10.0	8.00E+03	R. HOF+93
15.498	-6.6	4.50E+03	4.42E+03
20.663	• 5	2.206+03	2.19F+03
30.995	5.3	5.10E+03	4.44++03
41.327].7	2.20E+03	2.16F+03
		RHUUIUM	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	WEGUIPE	* AMD N
•] 0 3	16.0	1.03E+0E	H. H. H. + 45
.124	15.A	1.105+06	9.50++U5
• 155	15.2	1.17E+06	1.026+400
.207	18.7	1.152+06	9.64E+05
• 3] ()	26.4	$1 \cdot 10E + 06$	A.711+05
.4]1	9.9	4.52E+06	4.11F+ub
• 6 7 () 0 0 7	-2.3	2.55t + 0.5	2.61++06
. 477	-/.5	1.45+16	1
1.031	-4. 4	9.206+05	7.07-+90
1.740		6.00E+05	6.365+65
1.55()	-18.3	3.101+05	3.20-405
2.100	-17.4	1.555	1. 2. 142 + 0.2
3.100	LL • 5	2.25F+16	くいちち キリシー

4.133 -12.1 1.72E+05 1.065+05 -10.3 5.80E+04 0.478+94 -8.4 2.708+04 2,95F+04 -5.6 4.20E+12 4.745+113 -3.8 5.108+03 5.308+03 -2.7 2.356+03 1.425+03 3.9 5.40E+03 5.201+04

2.50E+03

2.34F+03

ENERGY	PERCENT		
(KEV)	DIFFERENCE	ACGUIPE	KAMAN
.103	4.4	1.105+06	1.05E+06
.124	-3.6	1.00E+45	1.04++00
.155	-2.9	1.001+06	1.031+00
.207	9	1.07E+06	1.041+11n
.310	10.2	4.20E+05	4.75F+05
.413	-4.1	4.10F+06	4.246+06
.620	-9.R	2.601+06	2.248+110
.827	- F . P	1.628+116	1.74F+0n
1.033	2.5	1.106+06	3.1)7F+06
1.240	- . A	7.00E+05	7.06++05
1.550	-9.7	3.808+05	4.218+05
2.066	-16.5	1.75E+05	2.04++05
3.100	283.7	3.00E+05	7. 32F+114
4.133	-22.5	1.70E+05	2.148+05
6.199	640.1	5.30E+05	7.145+14
8.265	-25.9	≥.40±+04	3.24F+04
12.398	401.2	5.301+04	1.06++04
15.498	-19.5	4.601+113	5.718+03
20.663	-14.8	5.20E+03	2.52F+03
30.995	5.5	5.408+03	5.59F+03
41.327	2.4	2.601+03	2-548+113

SILVER

ENERGY	PERCENT		
(KEV)	DIFFEHENCE	MCGUTHE	* A \$5 16 S
.103	34.1	1.376+06	1.028+08
.124	25.5	1.32E+96	1.05F+06
.155	37.3	1.508+06	1.044+00
.502	36.0	1.542+116	1.14++06
.310	23.1	1.10E+06	H.94F+05
.413	118.4	5.45E+06	2.508+(16)
•620	-14.5	5.40E+04	3.04F+06
.827	-24.1	1.42E+06	1.87E+06
1.033	-19.2	9.40E+05	1.165+06
1.240	-12.7	6.70E+05	7.688+05
1.550	-30.4	3.20E+15	4.676+115
2.066	-32.4	1.556+05	2.248+45
3.100	105.8	1.772+05	3. KUF+44
4.133	-19.8	1.90E+05	2.37F+05
6.199	-16.4	5.50E+14	7.77F+1;4
8.265	-14.9	3.006+04	3.538+04
15.308	-10.9	1.03F+04	1.164+14
15.498	-10.6	5.608+03	6.26F+U3
20.663	-8.5	2.60E+03	2.945+03
30.995	5.3	5.30E+03	5.421+113
41.327	5.7	S. 00E+03	2.741+43
61.990	13.1	1.00±+03	H. HAF+11C

PALLODIUM

1

		CADMIUM	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KAMAN
.103	96.5	1.70E+06	8.65F+05
.124	13.8	1.246+06	1.04F+06
.155	10.8	1.268+06	1.14F+00
.202	6.4	1.308+06	1.226+06
.310	10.9	1.09E+06	4 . ~ 3+ + (15)
.413	-3.5	9.208+05	9.54F+115
.620	27.1	1.45E+05	2.71++10
.827	۹.4	2.20E+06	6.17F+05
1.033	R.9	1.388+05	1.218+05
1.240	6.1	B. PAE+AS	4. 3115+114
1.550	G. 3	5.40E+05	4.445+15
2.066	3.3	2.608+05	2.525+05
3.100	-16.7	7.7NE+04	1.256+414
4.133	-23.0	2.00E+05	1.60++05
6.199	-23.3	6.50E+94	1.4RF+04
8.265	-21.7	3.008+04	3. ARF+04
12.398	-25.7	9.30F+03	1.258+04
15.498	-27.5	4.90E+03	5.76F+113
20.663	-31.3	2.10E+03	3.0KF+03
30.995	3.1	6.70E+03	6.505+03
+1.327	-2.5	2.90E+03	2.978+13
51.990	4.6	1.00E+03	4. EAF+UC

INDIUM

ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRE	KAWAN
.103	50.7	1.60E+06	1.06F+05
.124	18.3	1.25E+06	1.06F+06
.155	23.9	1.45E+06	1.17F+05
.207	23.8	1.606+06	1.29F+06
•310	4 . R	1.126+06	1.07F+06
•413	27.4	1.008+06	7. 85F+115
.620	24.6	3.651.+06	2.43F+06
.827	9 <u>e</u>	2.42E+06	2.20F+05
1.033	9.4	1.506+06	1.37F+05
1.240	1	9.00E+05	9.01F+05
1.550	2.2	5.501+15	5.38F+05
2.046	-5.6	2.60E+05	2.76F+115
3.100	-14.2	H.70E+04	1.018+05
4.133	-1.5	2.306+05	2.34F+05
6.199	-21.8	1.206+04	9.21F+94
8.265	-21.0	3.30E+04	4.146+04
15.398	-19.P	1.10E+04	1. 178+114
15.498	-17.9	6.10E+03	1.43+403
20.663	-17.0	2.80E+113	3.375+03
30.995	6.3	7.80E+03	7.34F+03
41.327	3.4	3.40E+03	3.24F+0.1
61.990	5.8	1.10F+0.3	1.048+03

	TIM		
PERCENT			
DIFFERENCE		MCEUIRE	KAMAN
214.2		4.20E+06	1.34E+06
88.0		1.85E+06	4.84F+05
91.2		2.30E+06	1.20E+06
55.2		2.10E+06	1.35F+06
16.8		1.35E+06	1.16F+U5
6.7		9.20E+05	8.628+115
-6.]		3.00E+06	3.14F+110
-3.4		2.15E+06	5.53E+0P
-7.2		1.38E+06	1.49F+()6
-8.0		9.00E+05	9.72F+05
-7.8		5.40E+05	5.465+05
-8.6		2.75E+05	3.01++05
-17.3		9.20E+04	1.11E+05
41.2		2.60E+05	1.848+05
-20.8		8.00E+04	1.018+05
-16.8		3.80E+04	4.56F+04
-16.1		1.25E+04	1.498+04
-14.3		6.90E+03	5.05F+03
-12.0		3.20E+03	3.54F+113
10.7		8.20E+03	7.41E+03
4.4		3.60E+03	3.45F+03
7.1		1.20E+03	1.128+03
	PERCENT DIFFEPENCF 214.2 88.0 91.2 55.2 16.8 6.7 -6.1 -3.4 -7.2 -8.0 -7.8 -8.6 -17.3 41.2 -20.8 -16.8 -16.1 -14.3 -12.0 10.7 4.4 7.1	PERCENT DIFFEPENCE 214.2 88.0 91.2 55.2 16.8 6.7 -6.1 -3.4 -7.2 -8.0 -7.8 -8.6 -17.3 41.2 -20.8 -16.8 -16.1 -14.3 -12.0 10.7 4.4 7.1	PERCENT DIFFEPENCE MCGUIRE 214.2 4.20E+06 88.0 1.85E+06 91.2 2.30E+06 55.2 2.10E+06 16.8 1.35E+06 6.7 9.20E+05 -6.1 3.00E+06 -3.4 2.15E+06 -7.2 1.38E+06 -8.0 9.00E+05 -7.8 5.40E+05 -8.6 2.75E+05 -17.3 9.20E+04 41.2 2.60E+05 -20.8 8.00E+04 -16.1 1.25E+04 -16.3 0.20E+03 -12.0 3.20E+03 10.7 3.20E+03 4.4 3.60E+03 7.1 1.20E+03

ANTIMONY

ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIRF	KAMAN
.103	62.R	2.60E+06	1.608+05
.124	81.0	2.25E+06	1.24F+06
.155	58.7	1.95E+06	1.238+06
.207	48.2	2.10E+06	1.425+06
.310	73.6	2.15E+06	1.24F+06
.413	33.9	1.25E+06	4.34F+05
•650	94.5	7.00E+06	3.60F+06
.827	14.8	2.72E+06	2.37E+U6
1.033	14.3	1.83E+06	1.60F+06
1.240	13.5	1.20E+06	1.065+06
1.550	18.0	7.50E+05	6.167+05
2.066	18.9	3.90E+05	3.28F+05
3.100	7.4	1.30E+05	1.21F+05
4.133	25. ⁸	2.40E+05	1.915+05
6.199	-26.0	7.90E + 04	1.07F+05
8.265	-24.4	3.70E+04	4 . ROF+()4
12.398	-23.3	1.25E+04	1.63F+()4
15.498	-23.5	6.80E+03	H.HJE+US
20.663	-23.9	3.106+03	4.035+03
30.995	-1.7	8.30E+03	8.455+03
41.327	8	3.80E+03	3.838+113
61.990	6.2	1.30E+03	1.22F+13

TELLURIUM

		the second s	
ENERGY	PFRCENT		
(KEV)	DIFFERENCE	MCGUIRE	KAMAIN
.103	89.9	2.35E+06	1.24F+06
.124	75.3	2.03E+06	1.168+06
.155	63.0	1.668+06	1.02F+05
.207	47.5	2.18E+06	1.48F+06
.310	47.3	1.45E+06	1.32F+06
.413	20.7	1.22E+06	1.015+06
.620	18.0	6.30E+06	5.34E+06
.827	47.4	3.05E+06	2.07F+06
1.033	22.6	2.10E+06	1.71E+U6
1.240	5.6	1.20E+06	1.14F+06
1.550	7.7	7.40E+05	6.87F+05
2.066	6.4	3.800+05	3.57E+115
3.100	6.0	1.40E+05	1.32E+05
4.133	331.7	2.906+05	6.72F+04
6.199	-21.9	> 9.10E+04	1.164+05
8.265	-19.4	4.30E+04	5.33F+114
12.398	-21.2	1.40E+04	1.748+04
15.498	-20.5	7.70E+03	9.69F+03
20.663	-21.1	3.50E+03	4.44F+03
30.995	543.3	9.50E+03	1.44++03
41.327	-1.2	4.]0E+03	4.157+03
61.990	-2.7	1.30E+03	1.345+03

IODINE

ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUTHE	KAMAN
.103	264.9	6.60E+06	1.81F+06
.124	174.4	3.00E+06	1.09F+06
.155	61.5	1.70E+06	1.056+06
.207	18.1	1.80E+06	1.528+00
.310	38.1	1.45E+16	1.41F+06
.413	30.9	1.43F+06	1.09F+06
.620	1039.6	7.208+16	6.32F+05
.827	6.9	2.40E+06	2.24F+116
1.033	5.4	1.855+06	1.756+00
1.240	3	1.238+06	1.235+110
1.550	-7.6	5.90E+05	1.465+05
2.066	-7.1	3.60E+05	3.448+00
3.100	-18.5	1.178+05	1.44F+115
4.133	-33.9	4.405+14	7.26++04
6.199	-26.0	7.30E+04	1.24F+05
8.265	-28.5	4.10t+04	5.74E+04
12.398	-30.6	1.328+04	1.901+04
15.498	-31.4	7.10++03	1.0 ++++++++++++++++++++++++++++++++++++
20.663	-28.1	3.402+03	4.73++03
30.995	-29.8	1.108+93	1.57++0.5
41.327	4.5	4.60E+03	4.4NF+U3
61,990	6.8	1.506+03	1.41+45

Table II. Continued

		XENON	
ENERGY	PERCENT		
(KEV)	DIFFERENCE	MCGUIAE	KAMAN
.103	312.3	1.40 + 07	3.408+06
.124	85.3	2.50E+06	1.3=F+05
.155	-2.9	1.10++06	1.136+06
.207	-27.3	1.000 + 06	1. 34E+00
.310	-25.3	1.156+06	1.54++05
.413	-17.2	1.001+06	1.216+06
.620	-10.5	5.301+05	7.04++05
.827	-6.6	2.30E+06	2.41-8+116
1.033	-5.6	1.80E+0F	1.41F+05
1.240	1.3	1.37E+06	1.35F+06
1.550	5.3	B. FOE+OF	4.171+05
2.066	- . A	4.20E+05	4.23++05
3.100	-3.7	1.50E+05	1.568+115
4.133	-8.1	7.10E+04	7.73F+04
6.199	-17.0	1.10E+05	1.231+115
8.265	-16.0	5.]0E+04	5.07F+04
12.398	-15.8	1.70E+04	2.02F+04
15.498	-18.3	9.00E+03	1.10F+04
20.663	-20.7	4.00E+03	5.04F+U.3
30.995	-22.5	1.30E+03	1.646+113
41.327	5	4.60E+03	4.631+03
61.990	• 4	1.508+03	1.49F+03

Ele	ement	Energy (keV)	Percent Difference	M-edges (keV)	L-edges (keV)	K-edge (keV)
Zn	(30)	1.03	109%		1.02-1.19	
Ga	(31)	10.3	634%			10.37
Kr	(36)	1.55	401%		1.67-1.92	
Y	(39)	0,155	445%	0.157-0.394		
Tc	(43)	20.7	704%			21.04
Pd	(46)	3.10	284%		3.17-3.60	
Те	(52)	4.13 31.0	332% 543%		4.34-4.94	31.81
I	(53)	0.620	1040%	0.619-1.072		

Table III

Constraint A 1-710									
U.S. DEPT. OF COMM. BIBLIOGRAPHIC DATA SHEET	1. PUBLICATION OR REPORT NO. NBSIR 73-176	2. Gov't Accession No.	3. Recipient'	s Accession No.					
4. TITLE AND SUBTITLE	5. Publication Date								
Comparison of Photo VI. McGuire	6. Performing Organization Code								
7	D. D. famia	Ormaization							
G. L. Simm	NBSIR 73-176								
9. PERFORMING ORGANIZAT	2400 2400	2400432 2400105							
DEPARTMEN	11. Contract/	Grant No.							
WASHINGTON	DNA-EO-7	DNA-E0-72-804							
	Subtask No. PC-100-05								
12. Sponsoring Organization Na	13. Type of Report & Period Covered								
Derense N	uclear Agency		Interim Report for						
Washingto	n, D. C. 20305		14. Sponsoring Agency Code						
Support was also rece	o of Standard Reference Dat.	a							
15. SUPPLEMENTARY NOTES	Cor Standard Acreschice Data	_	1						
16. ABSTRACT (A 200-word or less factual summary of most significant information. If document includes a significant bibliography or literature survey, mention it here.) Photoeffect cross sections calculated by McGuire, covering the energy range 0.0062 to 62.0 keV for elements with $Z = 2$ to 54, are compared with values interpolated from results calculated by Veigele et al (Kaman) which cover the energy range 0.1 to between 1.0 and 8.0 keV. This comparison is presented in the form of percent differences between these two data sets, with the Kaman values taken as the reference set. The cross sections are listed and the differences are tabulated over the energy range 0.103 to 62.0 keV, thus at the higher energies the comparison is with Kaman values which were fitted to experimental data. Discrepancies ranged from less than 3% up to as much as a factor of ten in the iodine $M_{IV} - M_V$ edge region at 0.620 keV. From this comparison, and from graphical comparison of both sets with experimental data for carbon, aluminum and tin, we estimate that for $Z = 2$ to 54 the envelop of uncertainty of the Kaman calculated values in the region 0.1 to 1.0 keV is of the order of $\pm 20\%$ except in the presence of resonance absorption features where the uncertainty can be an order of magnitude.									
17. KEY WORDS (Alphabetical order, separated by semicolons) Attenuation coefficients; comparison; cross sections; photoeffect; photons; x-rays									
18. AVAILABILITY STATEME	NT	19. SECURIT (THIS RE	Y CLASS PORT)	21. NO. OF PAGES					
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