



Climatological Data at the Proposed Prototype Sites in the United States for the Evaluation of HUD Operation **BREAKTHROUGH** Housing Systems

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Center for Building Technology
Institute for Applied Technology
National Bureau of Standards
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Final Report

Prepared for
Office of Research and Technology
Department of Housing and Urban Development
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U. S. DEPARTMENT OF COMMERCE, Frederick B. Dent, Secretary
NATIONAL BUREAU OF STANDARDS, Richard W. Roberts, Director

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Introduction

The purpose of this report is to provide preliminary information on site climatology useful for the design and evaluation of HUD Operation Breakthrough prototype building systems. In order to evaluate the design as well as the performance of building systems, the following environmental parameters are considered essential.

Temperature

Humidity

Wind speed and direction

Precipitation (snow and rain)

Solar radiation (direct and diffuse)

Ground temperature (depth of frost)

Background noise level

Air contamination

Earthquake risk

Climatological data for Breakthrough sites that pertain to the above parameters are scattered throughout the scientific literature. The bulk of the information presented, however, comes from the publications of the Environmental Science Services Administration (ESSA). The charge to the task group for this particular undertaking was to rapidly assemble all available climatological data pertaining to the above parameters for the Breakthrough localities, which actually contain the proposed building sites.

1. Sacramento, California (suburban site)
2. Wilmington, Delaware (suburban site)
3. Macon, Georgia (suburban site)
4. Indianapolis, Indiana (city perimeter site)
5. Kalamazoo, Michigan (suburban site)
6. St. Louis, Missouri (inner-city site)
7. Jersey City, New Jersey (inner-city site)
8. Memphis, Tennessee (inner-city site)
9. Houston, Texas (suburban site)
10. Seattle, Washington (suburban and inner-city sites)

Except for a few localities, most of the weather data reported in the literature are recorded at airport weather stations. This fact, however, is not too critical for the evaluation of Breakthrough building systems located in the suburbs. For the inner-city sites, most of the weather data recorded at the weather bureau city office should be appropriate. Only the city office data for St. Louis and Seattle are available, however, for the in-city sites listed above. Data for the Jersey City and Memphis sites are, therefore, to be corrected from those obtained at the airport weather stations^{*/}. City maps shown in the Appendix indicate relative locations of Breakthrough prototype sites with respect to the downtown area and to the airports. These maps should be useful in evaluating the correction factors for the airport weather data as well as the background noise and air contamination of the prototype sites.

^{*/} The corrections were made in accordance with the recommendations made by H. C. S. Thom of the Environmental Science Service Administration.

Climatological data required for the design of safe building systems are usually the extreme values of parameters such as the highest recorded wind velocity, the deepest snow fall, earthquake data and temperature extremes. The building systems are expected to resist these natural forces and to provide protection for the occupants. On the other hand, the data required for the evaluation of the building performance over a period of time are those data associated with the frequency and the sequential nature of occurrences. This latter type of data are used to predict the comfort of the occupants, energy requirements for heating and cooling the building, and weatherability of building materials. Data compiled herein are, therefore, assembled with a view toward fulfilling the need for two requirements: one for the design evaluation and a second for the performance evaluation.

It is most unusual in the planning of buildings and similar engineering structures to have sufficient meteorological data available at the site which can be used directly for design purposes. Regarding wind data, for example, it is usually necessary to make use of detailed records obtained at the nearest Weather Bureau Station. Because of changes in terrain, a conversion may be required. This conversion can take the form of a regression equation which requires that extensive (approximately 4 years) simultaneous records be established for the station and for the site; or the conversion may be based upon an evaluation of the terrain roughness and on assumptions concerning the nature of the atmospheric boundary layer. It is believed that the latter approach is the only reasonable one here because of the limited

According to the 1967 ASHRAE Handbook of Fundamentals the Sol-air temperatures (SAT) are calculated by the following formula:

$$\text{SAT} = \frac{\alpha I}{h} + \text{DB} - 7a \quad (1)$$

where α , I , h and DB represent surface absorptivity of the solar radiation, solar radiation per unit surface, surface heat transfer coefficient and outdoor air dry-bulb temperature, respectively. The negative term, $-7a$, represents the long wavelength radiation of the building surface with respect to the sky. The direction cosine, "a", of the surface is unity for a roof surface and zero for a vertical wall surface. Theoretically, the Sol-air temperature can be considered to be the maximum surface temperature when there is no heat conducted from the exterior surface of the building to the interior surface. Surface temperatures become very high when the surface is a perfect absorber (e.g., black-colored surface with a value of α near unity), when the wind speed is low (very small value of h), when the Zenith angle is small in a cloudless sky (a larger value of I) and when the coincident air temperature (DB) is also high.

The ASHRAE cooling load calculation procedure requires the use of Sol-air temperature profiles. Profiles for a variety of locations are not published in the 1967 ASHRAE Handbook of Fundamentals, nor are they available from other literature sources. Each geographic location must be separately calculated. This may be one of the reasons that some engineers still prefer to use simplified or short-cut cooling load calculation methods, similar to those used for the heating load. Since many of the Breakthrough building systems may be different in design from conventional buildings (for which most of the simplified or short-cut methods have been developed in the past), it is recommended that the ASHRAE cooling load calculation be followed rigorously. Upon this premise, Sol-air temperature profiles for the ten cities have, therefore, been developed for this report. The values for solar radiation for a cloudless sky for July 21 were first calculated using the same procedure described in the 1967 ASHRAE Book of Fundamentals. These are given in Table B (pp. 28-39) for all eleven sites. Since it is also required to have the design day dry-bulb temperature profiles, these were also developed on the assumption that the dry-bulb temperature follows a simple harmonic profile in a manner to achieve a maximum value of 1% ASHRAE at 1600 hours and a minimum value of 500 hours. The minimum value was calculated by subtracting the daily range value listed in the ASHRAE weather data table from the 1% data.

The profile thus synthesized for Houston, Texas, for example, compares well with the ten year mean daily profile representing the hottest days of each year, as shown in Figure 1^{4/}. Similarly good comparisons were obtained for five other cities, Phoenix, (Ariz.), Washington, (D. C.), Lake Charles, (La.), Minneapolis, (Minn.), and Medford, (Oreg.) as shown in a dimensionless scheme of Fig. 2. Although, except for Houston, Texas, these six cities are not the HUD Operation Breakthrough sites, it is believed that the dimensionless relationship verified by these cities should be equally valid for the Breakthrough sites.

The values of 0.15 and 0.3 were used for α/h of eq. (1) to be consistent with the sample Sol-air temperature tables illustrated in the Handbook of Fundamentals^{1/}. Table C (pp. 40-62) shows the Sol-air temperature profiles developed for the ten cities of Breakthrough building sites.

B. Data for Energy Estimates

Accurate estimation of heating and cooling energy requirements is important for evaluating the Breakthrough building systems. This is particularly important because of the many varieties of heating and cooling systems available today which depend upon different energy sources, types of heating and cooling processes, and types of energy distribution systems. Thus, a difference in energy requirements between systems may become a significant factor in the selection of a system. The energy calculation, therefore, should utilize the most precise and reliable up-to-date procedures. The most accurate procedures available are based upon a computer simulation of the hour by hour operation of

the heating and cooling system as it responds to the dynamic thermal behavior of the building. This calculation procedure requires coincident hourly observations of most of the parameters mentioned above for a period of at least one year, when the annual energy usage is of primary concern. Such hourly data are available on magnetic tapes from the National Climatic Center, Ashville, North Carolina. The list of tape reel numbers for ten Breakthrough localities is given in Table D (p. 63).

Although several computer programs are currently available to perform this comprehensive hourly analysis for the energy requirements, the cost for such a calculation may not be warranted in some cases, particularly during early planning stages.

In lieu of the hourly calculation method because of time, cost, availability, and accuracy requirement factors, three simplified methods such as the degree-day method, equivalent full-load hour method, or the "bin" method may be selected. The degree-day concept was designed for residential applications based upon average conditions experienced by several hundred homes in the Northern United States. The seasonal total of the degree days based upon the reference temperature of 65 °F for heating and cooling are given in Table A (p. 27), although the degree-day data for the cooling energy estimate have not been as widely accepted as that for the heating. The second method commonly used for estimating cooling energy requirements has been the equivalent full-load hour method. For this method the energy consumption for each of several buildings of a given type is measured and expressed as the number of

hours of operation at full load which would produce the same energy consumption. These figures are then averaged to arrive at the equivalent full-load hours for a given type of building in a given climatic region. Annual cooling energy requirements are then estimated for a specific building by multiplying the peak cooling load by the equivalent load hours. The equivalent full-load hour data for conventional buildings for the ten Breakthrough localities selected are not available. A third technique which has been gaining acceptance is application of the "bin" method. Each temperature "bin" contains hourly frequency of occurrence of temperature specified for the range of the "bin" (usually in 5 °F increments). Heat gain or heat loss of the building is calculated and expressed as a function of ambient dry-bulb temperature (not necessarily a linear function). The total energy requirements are then calculated from the sum of the product of the heat load and the frequency of the "bin". By making the width of the temperature "bin" smaller, the accuracy of the energy estimate obtained by this method can be increased. For the benefit of engineers who might want to use the "bin" method, "bin" data from Air Force Manual (AFM) 88-8 for the ten Breakthrough localities ... are shown in Table E (pp. 64-84). A detailed account of the use of the "bin" method is given in reference (5).

C. Solar Radiation

Table A (p. 26) shows the maximum daily total solar radiation upon a horizontal surface; it was calculated for the cloudless day of July 21 using the method described in reference (1). The average percent of probable sunshine for the months of July and January may be important for the design of lighting and this data is obtained from reference (11).

More detailed data for the solar radiation levels are given in Table B (pp. 28-39).

D. Coincident Wind Velocity for the Heating and Cooling Load Calculation

Coincident wind velocity designated as VL, L, M and H in Table A (p. 25) as associated with the temperature data refers to the following classification^{2/}:

VL: Very light where 70%^{*/} or more of the cold extreme hours are coincident with wind speeds less than or equal to 7 mph

L: Light, 50 to 69 percent of cold extreme hours are less than or equal to 7 mph wind speed

M: Moderate, where 50 to 74 percent cold extreme hours are coincident with wind speeds of more than 7 mph

H: High, where 75 percent or more of the cold extreme hours are coincident with wind speeds of 7 mph and 50 percent of the cold extreme hours are coincident with wind speeds of more than 12 mph.

^{*/} The percentage figures used in this section refer to the percentage of the number of winter hours.

Figures 3 through 22 show pictorially the annual frequency of the occurrences of coincident wind speeds and dry-bulb temperatures and relative humidities for the ten Breakthrough localities while Figures 23 through 32 indicate the summer and winter coincident wind speed profiles with respect to the wind direction.

E. Ground Temperature

Ground temperature data are needed for calculations to estimate heat gained or lost from the basement floors and walls. These data are also needed for the design of underground heat distribution systems and to evaluate the probabilities for a freeze-up of water mains and sewage disposal lines. It should be noted that underground temperature at depths greater than 30 ft remain relatively unchanged throughout the year at the annual average air temperatures listed in Table A (p. 25). The well-water temperature is also equal to the annual average air temperature. However, most underground installations require heat transfer calculations because they are usually installed at depths less than 10 ft from the surface. Listed in Table A are the integrated average earth temperatures from the surface to the ten foot depth for summer and winter conditions. These values are derived by a method similar to that described in reference (7) assuming the thermal diffusivity of soil to be $0.025 \text{ ft}^2/\text{hr}$. Unless the soil is extremely dry or unless there are strong underground heat sources

nearby, data shown in Table A should be a good approximation of the undisturbed soil temperature for the evaluation of underground installations. The freezing depth indicated in Table A (p. 25) was approximated from the earth temperature data compiled in reference (7).

F. Background Noise Data

The following qualitative estimates of ambient noise levels at the various Breakthrough sites were made by inspection of maps (Appendix) showing locations of nearby highways, airports, or other noise sources. Without field inspection and measurement, sufficient data are not available to enable quantitative estimates of the noise environments at these sites. It should be noted that the increased density of building and people accompanying Operation Breakthrough will result in further increases in ambient noise levels.

<u>Site</u>	<u>Estimated Ambient Noise Level</u>	<u>Comments</u>
Sacramento, Calif.	Medium-to-High	Local traffic, airport
New Castle County, Del.	Medium-to-High	Rural but near highways
Macon, Ga.	Low-to-Medium	Assuming minimal highway noise
Indianapolis, Ind.	High	Highway, adjacent airport, Indianapolis Speedway
Kalamazoo, Mich.	Medium-to-High	Two miles from airport

Jersey City, N. J.	High	High density urban areas
Memphis, Tenn.	Medium-to-High	Urban area but strong enforcement of anti-noise ordinances
St. Louis, Mo.	High	High density urban area
Houston, Tex.	Medium-to-High	Local traffic, highway, airports
Seattle, Wash.	Medium-to-High	Local traffic, highway, airports
Seattle, Wash. (King Co.)	Medium	Highway

Pending availability of more quantitative data, it is recommended that particular attention be given to noise control measures at all sites where the estimated ambient noise level is high or medium-to-high^{*/}.

G. Wind Data for Structural Design

Table F gives tabulated wind data for the stations nearest the ten selected sites. These stations, in every case, are airport locations with open exposures. References or data sources are indicated in the column headings. Extreme mile wind speeds corresponding to a mean recurrence interval of 50 years have been presented by Thom (15) in the form of isotachs and are suggested as basic design speeds, provided the appropriate terrain corrections are made. These corrections can be most conveniently applied by use of the power law and the average parameters suggested by Davenport (16, 17). Under most strong wind (neutral) conditions, the mean velocity profile can

^{*/} Subsequent to this report, the background noise levels of the Jersey City site have been measured (NBS Report 10219 entitled "Noise Survey of Jersey City Operation Breakthrough Prototype Site", November 1970.

be described by the expression

$$\frac{V_Z}{V_G} = \left(\frac{Z}{Z_G}\right)^\alpha \quad (2)$$

where V_Z = wind speed at height Z

V_G = gradient wind speed first attained at height Z_G

α = power law exponent

The gradient speed is assumed to be independent of local terrain and therefore equal at station and site. This then allows the calculation of wind speeds at the site if the parameters α and Z_G are known. The following average values have been suggested by Davenport (17).

<u>Type of Terrain</u>	α	<u>Z_G (ft)</u>
Flat open country	.16	900
Rough wooded country, city suburbs	.28	1300
Heavily built up urban centers	.40	1400

Because of their low probability of occurrence, extreme speeds are not usually a satisfactory basis for evaluating structural performance. For this purpose, mean wind speeds for January and July as the mean annual wind speeds are presented in Table F. These data indicate the relative windiness of the 10 localities and also indicate the relative contribution of extratropical cyclones (for example, winter storms) and thunderstorms being associated with the winter months. Also included in Table F are the average number of storms per year which re-

sulted in wind speeds of 47 mph or greater. It will be noted that this speed corresponds to a loading of approximately one-half the design load and would produce up to 250 loading cycles during the 50-year design life of the structure if wind gusts were neglected. The effect of high intensity gusts would be primarily to increase the number of loading cycles, say to 1000 or more during the 50-year life of the structure. Therefore, the data listed in Table F (p. 85), coupled with known properties of atmospheric boundary layers, can be used to establish the mean wind climate at the 10 localities. Information sufficient for design and evaluation of performance can be developed once the estimates of the terrain roughness become available. It is recommended that an inspection of the surrounding terrain or the sites should be made by qualified personnel for the purpose of estimating the effective roughness parameters.

H. Earthquake Data

In the design of buildings to resist lateral seismic forces, the minimum total lateral shear is usually based on the expression

$$V = ZKCW \quad (3)$$

where V = total lateral shear at the base

Z = numerical coefficient which depends on the seismic zone in which the building is to be situated

K = numerical coefficient which depends upon the structural frame characteristics

C = numerical coefficient for the base shear which depends upon the fundamental period of the structure

W = total dead load.

Of the above factors, only Z has a regional variation. Since no reliable method of predicting the time, place and intensity of earthquakes exists, maps have been constructed indicating the areas which have experienced destructive earthquakes in the past. These maps are the only means available at this time by which the location of future destructive earthquakes may be anticipated. Zones range from 0 to 3 and are characterized by the following expected degrees of damage.

Zone	Degree of Damage	Z Value
0	None	0
1	Minor	0.25
2	Moderate	0.50
3	Major	1.0

A number of different seismic maps are in use, their zone boundaries differing only slightly in most cases. Based on the most recent edition of ANSI-A58-Sec. 6, the following seismic zones are suggested for arriving at design loads:

<u>Selected Site</u>	<u>Seismic Zone</u>
Sacramento, California	2
Wilmington, Delaware	1
Macon, Georgia	1
Indianapolis, Indiana	1
Kalamazoo, Michigan	1
St. Louis, Missouri	1
Jersey City, New Jersey	1
Memphis, Tennessee	2
Houston, Texas	1
Seattle, Washington	3

I. Air Contamination Data

Air pollution data for the ten Operation Breakthrough localities are given in Table G. Included are the locations of the sampling sites and the concentrations of suspended particulates, sulfur dioxide, nitrogen dioxide and ammonia. The geometric mean (which gives a better indication of the central tendency of the values than the arithmetic mean), the 90% frequency distribution value (90% of the readings are equal to or less than this value) and the period of years that these averages represent are given in Table G (p. 86). Blank spaces indicate data is not available. These concentrations represent averages at the sampling sites; the values at the particular Breakthrough site will vary and will depend on pollutant sources, and meteorological and topographical factors (19).

Little information is available in the literature concerning application of these data in the design of housing systems. The following statements, taken from reference (20), are given to illustrate a correlation between exposure to sulfur dioxide and particulates and the effects on health.

- a. At concentrations ranging from 300-500 $\mu\text{g}/\text{m}^3$ (microgram per cubic meter) of sulfur dioxide (24-hour mean), with low particulate levels, increased hospital admissions of older persons for respiratory disease may occur; absenteeism from work, particularly with older persons, may also occur.
- b. A decrease from 140 to 60 $\mu\text{g}/\text{m}^3$ (annual mean) in particulate concentrations may be accompanied by a decrease in mean sputum volume in industrial workers.
- c. Where concentrations range from 100-130 $\mu\text{g}/\text{m}^3$ and above for particulates (annual mean) with sulfur dioxide concentrations (annual mean) greater than 120 $\mu\text{g}/\text{m}^3$, children residing in such areas are likely to experience increased incidence of certain respiratory diseases.

These statements apply to outdoor pollutants, but pollutant levels indoors have not received adequate attention. Considering the fact that people spend most of their lives indoors, the matter of the quality of indoor air becomes very important. Further efforts are recommended to measure indoor and outdoor pollution levels simultaneously to relate them to the various sources of air contaminations, both indoors and

outdoors and to other climatic parameters. With this type of information it should be possible to specify air cleaning devices to maintain indoor air at a healthful level of purity.

J. Precipitation Data

Extreme values in 24 hours and normals (1931-1960) of annual totals for rain - and snowfall were obtained from reference (14) and listed in Table A (p. 26), which also shows the snow load in lbs/sq. ft. on the ground as transcribed from reference (12).

K. Summary and Recommendations

Outdoor environmental data required for the design and the evaluation of Breakthrough building systems have been assembled herein from various sources. The parameters included are temperature, humidity, wind, precipitation, solar radiation, ground temperature, soil conditions, background noise level, air contamination and earthquake risk. It is believed that the data presented in this report can be used to prepare preliminary designs for the Breakthrough building programs. However, more detailed and specific information should be prepared as the Breakthrough program progresses, especially for use in the test and evaluation phase.

The following recommendations are made:

1. After review and approval by HUD this report is to be made available to Breakthrough contractors for use in their design work.
2. Continue efforts to add to and refine the data given with special priority to be given to (a) conduct field inspections and measurements of the background noise levels and terrain roughness at the Breakthrough sites, and (b) measure coincident hourly data for air contamination with reference to temperature, humidity and wind data. These coincident data are essential for predicting the indoor environment of a Breakthrough building especially with respect to the design of the indoor environmental control systems.

L. Acknowledgments

The author wishes to acknowledge the assistance of Mr. John W. Bean for his computer data processing of weather parameters, and the cooperation of Mr. Oscar E. Richard, Chief of the Engineering Meteorology Section of the United States Air Force, for the selection of Air Force bases in the vicinity of the Operation Breakthrough sites and the updating of the Manual 88 data.

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Table A

Data for Heating and Cooling Load Calculations

Table A

Site Localities (Weather Station)	Air Temperatures, °F				Coin- cident wind	Annual Recorded Highest	Annual Recorded Lowest	14/ [*] Average	Ground Temp. °F Upper 10 Ft Average	Frost depth in.			
	Summer	DB	DB Range	Winter DB							99% 97%	99% 97%	Summer Winter
	1% 2 1/2%	5% 10%	10% °F	99% 97%	99% 97%								
Sacramento, Calif. (Airport)	100/72	97/70	94/69 88/67	36	30	32	VL**	115	23	60	76	57	1
Wilmington, Del. (Airport)	93/99	90/77	87/76 84/74	20	12	15	M	102	-4	54	66	44	6
Macon, Ga. (Airport)	98/80	96/79	94/78 92/77	22	23	27	L	104	3	66	75	57	4
Indianapolis, Ind. (Airport)	93/78	91/77	88/76 86/74	22	0	4	M	99	-18	52	66	43	12
Kalamazoo, Mich. (Grand Rapids AP)	92/76	89/75	86/74 83/71	23	1	5	M	100	-16	48	63	41	12
St. Louis, Mo. (City Office)	96/79	94/78	92/77 89/75	18	7	11	M	106	-11	55	65	43	12
Jersey City, N. J. (Corrected from data of Newark AP)	92/77	89/76	86/75 82/73	20	11	15	M	105	1	53	62	44	6
Memphis, Tenn. (Airport)	98/80	96/79	94/78 91/77	21	17	21	L	106	-13	62	69	50	12
Houston, Tex. (Airport)	96/80	94/80	92/79 90/78	18	28	39	M	106	9	69	81	60	1
Seattle, Wash. (Sea/Tac AP)	85/66	81/64	77/63 72/61	22	20	24	L	99	6	51	59	46	5
Seattle, Wash. (City Office)	81/67	79/65	76/64	-	19	28	32	L	100	11	60	47	5

* 14/ and similar nomenclature are numbers for reference citation.

** VL, very light; L, light; M, moderate; H, high. See text, p. 10.

Table A - Continued

Site Localities (Weather Station)	Precipitation Data (1931-1960)					Solar Radiation		
	Rain, In. 14/ Max. hrs.	Mean annual	Max. 24 hrs.	Snow, In. 14/ Mean annual	Snow Load 12/ (psf)	Max. Daily Total Unit	% Sunshine Jan.	July
Sacramento, Calif. Airport	5.6	16.3	-	-	5 ~ 10	3620	45	97
Wilmington, Del. Airport	6.2	44.5	15.6	22.5	20	3615	44	66
Macon, Ga. Airport	5.0	44.1	3.7	0.4	5 ~ 10	2130	56	64
Indianapolis, Ind. Airport	3.9	12.7	12.5	20.3	10 ~ 20	3615	43	66
Kalamazoo, Mich. Grand Rapids AP	2.7	31.2	12.6	78.7	20	3600	-	-
St. Louis, Mo. (City Office)	3.3	35.3	11.2	17.2	20	3620	52	71
Jersey City, N. J. (Corrected from the data of Newark AP)	4.7	43.5	26	29.8	20	3610		
Memphis, Tenn. airport	4.9	49.7	16.1	6.6	5 ~ 10	3624	48	73
Houston, Tex. airport	15.7	46.0	4.4	0.4	less than 5	3612	47	74
Seattle, Wash. Sea/Tac AP	3.4	39.0	21.4	14.7	10	3561	14	68
Seattle, Wash. (City Office)	3.3	34.1	11.5	8.1	10	3561	28	63

Table A - Continued

Site Localities (Weather Station)	Seasonal Degree-Days		No. of annual hrs at or above 67 °F WB ₃ /
	Seasonal Heating	Seasonal Cooling	
Sacramento, Calif. (Airport)	2773	1411	351
Wilmington, Del. (Airport)	4930	1002	1191
Macon, Ga. (Airport)	2130	2367	3069
Indianapolis, Ind. (Airport)	5699	1033	1462
Kalamazoo, Mich. (Grand Rapids AP)	6998	730	833
St. Louis, Mo. (City Office)	4900	1558	1866
Jersey, City, N. J. (Corrected from data of Newark AP)	5067	965	1290
Memphis, Tenn. (Airport)	3233	2078	2631
Houston, Tex. (Airport)	1400	3175	3695
Seattle, Wash. (Sea/Tac AP)	5145	170	17
Seattle, Wash. (City Office)	4424	-	17

Table B

Solar Radiation

ET:	Equation of time, min.
R:	Solar constant modifier
HO:	Daily total radiation upon horizontal surface, Btu/hr ft ²
BETA:	Solar altitude angle, degree
AZIMUTH:	Solar azimuth angle, measured from north, degree
IDN:	Direct normal radiation, Btu/hr ft ²
DIFF:	Diffuse sky radiation, Btu/hr ft ²

Total solar radiation values (for the clearness^{1/} number of unity) expected to fall upon vertical wall surfaces from eight compass directions and upon a horizontal surface are tabulated in these tables.

LOCATION: SACRAMENTO, CALIFORNIA

MONTH= 7 DAY=21 FOR LATITUDE= 38.5 LONGITUDE= 121.5

ET= -6.2000 R= .9690 SUNRZ= 5.0626 HO= 3619.11

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME HR	AIR TEMP	BETA (DEG)	AZI- MUTH	IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	71.	0.	13.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	68.	0.	28.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	65.	0.	42.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	64.	0.	53.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	64.	0.	63.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
6.	65.	10.	72.	107.	15.	13.	13.	13.	13.	45.	106.	113.	60.	33.
7.	68.	22.	81.	196.	27.	30.	30.	30.	30.	59.	178.	210.	136.	99.
8.	71.	33.	90.	236.	32.	44.	44.	44.	44.	46.	185.	242.	183.	161.
9.	75.	45.	100.	257.	35.	88.	57.	57.	57.	57.	162.	236.	205.	216.
10.	80.	56.	113.	268.	36.	126.	67.	67.	67.	67.	123.	204.	206.	259.
11.	84.	66.	134.	274.	37.	152.	74.	74.	74.	74.	75.	154.	185.	288.
12.	89.	72.	171.	277.	38.	163.	128.	77.	77.	77.	77.	91.	148.	300.
13.	93.	69.	213.	276.	37.	158.	172.	129.	76.	76.	76.	76.	96.	295.
14.	96.	60.	240.	271.	37.	138.	200.	186.	104.	70.	70.	70.	70.	273.
15.	99.	50.	255.	262.	36.	104.	208.	226.	147.	61.	61.	61.	61.	235.
16.	100.	38.	267.	246.	33.	61.	195.	243.	178.	50.	50.	50.	50.	185.
17.	100.	26.	276.	216.	29.	36.	158.	228.	186.	56.	36.	36.	36.	125.
18.	99.	15.	284.	153.	21.	20.	95.	163.	147.	57.	20.	20.	20.	60.
19.	96.	4.	293.	14.	2.	1.	6.	14.	14.	7.	1.	1.	1.	3.
20.	93.	0.	303.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	89.	0.	313.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	84.	0.	320.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	80.	0.	341.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	75.	0.	357.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: WILMINGTON, DELAWARE

MONTH= 7 DAY=21 FOR LATITUDE= 39.7 LONGITUDE= 75.6

ET= -6.2000 R= .9690 SUNRZ= 4.9532 HO= 3615.22

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME HR	AIR TEMP	BETA (DEG)	AZI- MUTH	ION	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	77.	0.	14.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	75.	0.	29.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	74.	0.	42.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	73.	0.	54.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	73.	.	64.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
6.	74.	11.	73.	119.	16.	14.	14.	14.	14.	49.	117.	125.	69.	39.
7.	75.	22.	82.	200.	27.	31.	31.	31.	31.	58.	179.	214.	142.	104.
8.	77.	34.	91.	237.	32.	48.	45.	45.	45.	45.	182.	242.	187.	165.
9.	79.	45.	102.	257.	35.	94.	58.	58.	58.	58.	157.	234.	208.	218.
10.	82.	56.	116.	268.	36.	132.	67.	67.	67.	67.	116.	201.	207.	260.
11.	84.	66.	138.	274.	37.	157.	79.	74.	74.	74.	74.	150.	186.	287.
12.	87.	71.	174.	276.	38.	168.	134.	76.	76.	76.	76.	86.	148.	298.
13.	89.	68.	213.	275.	37.	162.	177.	132.	75.	75.	75.	75.	96.	292.
14.	91.	59.	239.	270.	37.	140.	203.	188.	103.	69.	69.	69.	69.	269.
15.	92.	49.	255.	261.	36.	106.	210.	227.	147.	61.	61.	61.	61.	232.
16.	93.	37.	266.	244.	33.	62.	195.	243.	177.	49.	49.	49.	49.	181.
17.	93.	26.	276.	214.	29.	35.	157.	227.	184.	55.	35.	35.	35.	122.
18.	92.	14.	285.	150.	20.	20.	93.	160.	144.	56.	20.	20.	20.	57.
19.	91.	3.	294.	11.	2.	1.	5.	12.	12.	6.	1.	1.	1.	2.
20.	89.	0.	303.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	87.	0.	314.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	84.	0.	327.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	82.	0.	342.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	79.	0.	358.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: MACON, GEORGIA

MONTH= 7 DAY=21 FOR LATITUDE= 32.7 LONGITUDE= 83.6

ET= -6.2000 R= .9690 SUNRZ= 5.7647 HO= 3621.78

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME HR	AIR TEMP	BETA (DEG)	AZI- MUTH	DN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	FAST	SE	HORIZ
1.	80.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	78.	0.	22.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	77.	0.	37.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	76.	0.	49.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	76.	0.	59.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
6.	77.	3.	68.	4.	1.	0.	0.	0.	0.	2.	5.	5.	2.	1.
7.	78.	15.	75.	152.	21.	20.	20.	20.	20.	58.	147.	162.	94.	59.
8.	80.	27.	82.	218.	30.	37.	37.	37.	37.	63.	192.	230.	155.	129.
9.	83.	40.	90.	249.	34.	52.	52.	52.	52.	52.	187.	243.	187.	192.
10.	86.	52.	99.	265.	36.	89.	64.	64.	64.	64.	159.	224.	195.	245.
11.	88.	64.	113.	273.	37.	119.	73.	73.	73.	73.	118.	182.	182.	284.
12.	91.	75.	141.	278.	38.	136.	86.	73.	78.	78.	78.	124.	151.	305.
13.	94.	77.	160.	278.	38.	138.	105.	79.	79.	79.	79.	101.	136.	309.
14.	96.	68.	240.	275.	37.	126.	173.	163.	101.	75.	75.	75.	75.	294.
15.	97.	57.	257.	269.	37.	101.	193.	211.	146.	67.	67.	67.	67.	261.
16.	98.	44.	267.	256.	35.	65.	192.	239.	179.	56.	56.	56.	56.	213.
17.	98.	32.	275.	232.	32.	43.	169.	239.	194.	60.	43.	43.	43.	153.
18.	97.	19.	282.	183.	25.	27.	120.	195.	172.	63.	27.	27.	27.	85.
19.	96.	7.	290.	62.	8.	7.	33.	65.	63.	28.	7.	7.	7.	16.
20.	94.	0.	298.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	91.	0.	307.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	88.	0.	318.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	86.	0.	332.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	83.	0.	348.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: INDIANAPOLIS, INDIANA

MONTH= 7 DAY=21 FOR LATITUDE= 39.7 LONGITUDE= 86.3

ET= -6.2000 R= .9690 SUNRZ= 5.6614 H0= 3614.96

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME HR	AIR TEMP	BETA (DEG)	AZI- MUTH	IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	75.	0.	2.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	73.	0.	18.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	72.	0.	33.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	71.	0.	46.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	71.	0.	57.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
6.	72.	4.	66.	12.	2.	1.	1.	1.	1.	6.	12.	12.	6.	2.
7.	73.	14.	75.	150.	20.	20.	20.	20.	20.	56.	145.	160.	93.	58.
8.	75.	26.	84.	214.	29.	35.	35.	35.	35.	55.	184.	227.	157.	122.
9.	78.	37.	94.	244.	33.	62.	49.	49.	49.	49.	177.	243.	195.	181.
10.	81.	49.	105.	261.	36.	106.	61.	61.	61.	61.	146.	227.	210.	232.
11.	83.	59.	121.	270.	37.	141.	69.	69.	69.	69.	103.	188.	204.	269.
12.	86.	68.	147.	275.	37.	162.	96.	75.	75.	75.	75.	132.	177.	292.
13.	89.	70.	174.	276.	38.	168.	134.	76.	76.	76.	76.	86.	148.	298.
14.	91.	66.	222.	274.	37.	158.	187.	150.	74.	74.	74.	74.	79.	287.
15.	92.	56.	244.	268.	36.	132.	208.	201.	116.	67.	67.	67.	67.	260.
16.	93.	45.	258.	257.	35.	94.	208.	234.	157.	57.	57.	57.	57.	218.
17.	93.	34.	269.	237.	32.	48.	187.	242.	182.	45.	45.	45.	45.	165.
18.	92.	22.	278.	200.	27.	31.	142.	214.	179.	58.	31.	31.	31.	104.
19.	91.	11.	287.	118.	16.	14.	69.	125.	117.	49.	14.	14.	14.	39.
20.	89.	0.	296.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	86.	0.	306.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	83.	0.	318.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	81.	0.	331.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	78.	0.	346.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: KALAMAZOO, MICHIGAN

MONTH= 7 DAY=21 FOR LATITUDE= 42.2 LONGITUDE= 84.5

ET= -6.2000 R= .9690 SUNRZ= 5.4304 HO= 3603.10

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME HR	AIR TEMP	BETA (DEG)	AZI- MUTH	IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	73.	0.	4.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	71.	0.	20.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	70.	0.	34.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	69.	0.	47.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	69.	0.	58.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
6.	70.	6.	68.	43.	6.	5.	5.	5.	5.	21.	44.	44.	21.	10.
7.	71.	16.	77.	165.	22.	22.	22.	22.	22.	58.	156.	177.	107.	69.
8.	73.	27.	87.	219.	30.	37.	37.	37.	37.	49.	183.	232.	167.	130.
9.	76.	38.	97.	247.	34.	74.	50.	50.	50.	50.	169.	242.	202.	187.
10.	79.	49.	110.	262.	36.	118.	61.	61.	61.	61.	135.	222.	215.	234.
11.	82.	59.	127.	270.	37.	153.	69.	69.	69.	69.	89.	180.	207.	268.
12.	85.	66.	154.	274.	37.	173.	109.	74.	74.	74.	74.	123.	179.	288.
13.	88.	68.	170.	275.	37.	177.	135.	75.	75.	75.	75.	93.	160.	292.
14.	90.	63.	222.	273.	37.	164.	196.	155.	72.	72.	72.	72.	78.	280.
15.	91.	54.	243.	266.	36.	136.	214.	205.	114.	65.	65.	65.	65.	252.
16.	92.	44.	258.	255.	35.	95.	211.	236.	155.	56.	56.	56.	56.	210.
17.	92.	33.	269.	234.	32.	48.	186.	241.	180.	44.	44.	44.	44.	158.
18.	91.	21.	278.	195.	27.	30.	138.	210.	176.	56.	30.	30.	30.	98.
19.	90.	11.	288.	112.	15.	13.	64.	118.	111.	47.	13.	13.	13.	36.
20.	88.	0.	298.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	85.	0.	308.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	82.	0.	320.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	79.	0.	333.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	76.	0.	348.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: ST. LOUIS, MISSOURI

MONTH= 7 DAY=21 FOR LATITUDE= 38.6 LONGITUDE= 90.2

LT= -6.2000 R= .9690 SUNRZ= 4.9710 HO= 3618.77

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME HR	AIR TEMP	HETA (DEG)	AZI- MUTH	IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	81.	0.	14.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	80.	0.	29.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	79.	0.	43.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	78.	0.	54.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	78.	.	64.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
6.	79.	11.	73.	118.	16.	14.	14.	14.	14.	49.	117.	125.	69.	39.
7.	80.	23.	81.	201.	27.	31.	31.	31.	31.	59.	180.	215.	142.	104.
8.	81.	34.	90.	238.	32.	47.	46.	46.	46.	46.	184.	242.	186.	167.
9.	84.	46.	101.	258.	35.	92.	58.	58.	58.	58.	159.	234.	206.	220.
10.	86.	57.	115.	269.	37.	129.	68.	68.	68.	68.	118.	200.	205.	262.
11.	88.	67.	137.	275.	37.	154.	78.	74.	74.	74.	74.	149.	183.	289.
12.	90.	72.	175.	277.	38.	164.	133.	77.	77.	77.	77.	85.	144.	300.
13.	93.	68.	216.	275.	37.	158.	175.	134.	75.	75.	75.	75.	92.	293.
14.	94.	60.	241.	271.	37.	136.	201.	190.	108.	70.	70.	70.	70.	270.
15.	95.	49.	256.	261.	36.	101.	208.	228.	150.	61.	61.	61.	61.	231.
16.	96.	37.	267.	244.	33.	58.	193.	243.	180.	49.	49.	49.	49.	180.
17.	96.	25.	276.	212.	29.	35.	154.	225.	185.	56.	35.	35.	35.	119.
18.	95.	14.	285.	145.	20.	19.	89.	154.	140.	55.	19.	19.	19.	54.
19.	94.	3.	294.	5.	1.	0.	2.	5.	5.	2.	.	.	.	1.
20.	93.	0.	304.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	90.	0.	315.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	88.	0.	327.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	86.	0.	342.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	84.	0.	358.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: JERSEY CITY, NEW JERSEY

MONTH= 7 DAY=21 FOR LATITUDE= 40.7 LONGITUDE= 74.2

ET= -6.2000 R= .9690 SUNRZ= 4.8117 HO= 3610.80

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME HR	AIR TEMP	BETA (DEG)	AZI- MUTH	IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	76.	0.	15.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	74.	0.	30.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	73.	0.	45.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	72.	0.	54.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	72.	2.	65.	1.	0.	0.	0.	0.	0.	0.	1.	1.	0.	0.
6.	73.	13.	74.	133.	18.	17.	17.	17.	17.	52.	130.	141.	79.	47.
7.	74.	24.	83.	205.	28.	33.	33.	33.	33.	56.	181.	219.	148.	110.
8.	76.	35.	93.	240.	33.	55.	47.	47.	47.	47.	179.	243.	191.	170.
9.	78.	46.	104.	258.	35.	101.	58.	58.	58.	58.	151.	232.	211.	222.
10.	81.	57.	119.	269.	37.	138.	68.	68.	68.	68.	109.	196.	209.	262.
11.	83.	66.	142.	274.	37.	163.	88.	74.	74.	74.	74.	143.	186.	287.
12.	86.	70.	178.	276.	38.	172.	142.	76.	76.	76.	76.	79.	146.	296.
13.	88.	66.	215.	274.	37.	165.	183.	138.	74.	74.	74.	74.	93.	288.
14.	90.	58.	239.	269.	37.	141.	207.	192.	104.	68.	68.	68.	68.	205.
15.	91.	47.	255.	260.	35.	105.	212.	229.	147.	59.	59.	59.	59.	226.
16.	92.	36.	266.	242.	33.	60.	194.	243.	177.	48.	48.	48.	48.	176.
17.	92.	25.	276.	210.	29.	34.	154.	224.	183.	55.	34.	34.	34.	116.
18.	91.	14.	285.	143.	19.	18.	87.	152.	139.	55.	18.	18.	18.	53.
19.	90.	3.	294.	6.	1.	1.	3.	6.	6.	3.	1.	1.	1.	1.
20.	88.	0.	304.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	86.	0.	316.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	83.	0.	329.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	81.	0.	343.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	78.	0.	359.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: MEMPHIS, TENNESSEE

MONTH= 7 DAY=21 FOR LATITUDE= 35.1 LONGITUDE= 90.0

LT= -6.2000 R= .9690 SUNRZ= 5.1008 HO= 3624.10

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME HR	AIR TEMP	BETA (DEG)	AZI- MUTH	IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	81.	0.	15.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	79.	0.	30.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	78.	0.	44.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	77.	0.	55.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	77.	0.	64.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
6.	78.	10.	72.	108.	15.	13.	13.	13.	13.	45.	107.	114.	61.	34.
7.	79.	22.	80.	190.	27.	31.	31.	31.	31.	62.	181.	212.	137.	102.
8.	81.	34.	88.	238.	32.	46.	46.	46.	46.	52.	189.	242.	180.	167.
9.	83.	47.	97.	259.	35.	81.	59.	59.	59.	59.	167.	235.	109.	223.
10.	86.	59.	110.	270.	37.	117.	69.	69.	69.	69.	129.	202.	196.	267.
11.	89.	69.	131.	276.	37.	140.	76.	76.	76.	76.	82.	150.	174.	295.
12.	92.	75.	174.	278.	38.	150.	124.	78.	78.	78.	78.	86.	134.	306.
13.	94.	71.	222.	276.	38.	143.	166.	137.	77.	77.	77.	77.	81.	299.
14.	96.	61.	247.	271.	37.	123.	193.	192.	120.	71.	71.	71.	71.	274.
15.	97.	49.	260.	262.	36.	90.	200.	230.	160.	61.	61.	61.	61.	234.
16.	98.	37.	270.	244.	33.	49.	186.	243.	187.	49.	49.	49.	49.	180.
17.	98.	25.	278.	210.	29.	34.	148.	223.	187.	61.	34.	34.	34.	116.
18.	97.	13.	286.	135.	18.	17.	81.	143.	132.	53.	17.	17.	17.	48.
19.	96.	1.	294.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
20.	94.	0.	303.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	92.	0.	314.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	89.	0.	327.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	86.	0.	342.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	83.	0.	358.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: HOUSTON, TEXAS

MONTH= 7 DAY=21 FOR LATITUDE= 29.6 LONGITUDE= 95.3

ET= -6.2000 R= .9690 SUNRZ= 5.6457 HO= 3611.36

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME HR	AIR TEMP	BETA (DEG)	AZI- MUTH	IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	81.	0.	10.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	80.	0.	27.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	79.	0.	41.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	78.	0.	52.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	78.	0.	61.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
6.	79.	4.	69.	21.	3.	2.	2.	2.	2.	10.	22.	22.	11.	5.
7.	80.	17.	76.	167.	23.	23.	23.	23.	23.	62.	161.	178.	105.	71.
8.	81.	29.	82.	226.	31.	40.	40.	40.	40.	67.	197.	235.	159.	142.
9.	84.	42.	89.	253.	34.	55.	55.	55.	55.	58.	189.	241.	184.	205.
10.	86.	55.	97.	268.	36.	85.	67.	67.	67.	67.	160.	217.	186.	257.
11.	88.	68.	110.	275.	37.	111.	75.	75.	75.	75.	118.	171.	168.	293.
12.	90.	79.	145.	279.	38.	124.	89.	80.	80.	80.	80.	111.	133.	311.
13.	93.	78.	220.	278.	38.	123.	137.	116.	79.	79.	79.	79.	84.	310.
14.	94.	67.	251.	275.	37.	109.	171.	176.	122.	75.	75.	75.	75.	290.
15.	95.	54.	264.	267.	36.	83.	187.	220.	163.	66.	66.	66.	66.	253.
16.	96.	41.	272.	251.	34.	53.	183.	242.	191.	59.	53.	53.	53.	200.
17.	96.	28.	278.	222.	30.	39.	155.	232.	196.	67.	39.	39.	39.	136.
18.	95.	16.	285.	159.	22.	21.	98.	170.	154.	61.	21.	21.	21.	64.
19.	94.	3.	292.	8.	1.	1.	4.	9.	9.	4.	1.	1.	1.	2.
20.	93.	0.	299.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	90.	0.	309.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	88.	0.	320.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	86.	0.	335.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	84.	0.	352.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: SEATTLE, WASHINGTON (AIRPORT)

MONTH= 7 DAY=21 FOR LATITUDE= 47.4 LONGITUDE= 122.3

ET= -6.2000 R= .9690 SUNRZ= 4.6734 HO= 3562.21

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME HR	AIR TEMP	BETA (DEG)	AZI- MUTH	IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	67.	0.	11.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	65.	0.	26.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	64.	0.	39.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	63.	0.	52.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	63.	3.	63.	6.	1.	1.	1.	1.	1.	3.	6.	6.	2.	1.
6.	64.	12.	73.	130.	18.	16.	16.	16.	16.	53.	128.	138.	76.	45.
7.	65.	22.	84.	199.	27.	31.	31.	31.	31.	51.	174.	214.	146.	102.
8.	67.	32.	95.	234.	32.	60.	43.	43.	43.	43.	171.	240.	194.	157.
9.	70.	42.	107.	253.	34.	110.	54.	54.	54.	54.	141.	233.	220.	205.
10.	73.	51.	123.	264.	36.	153.	63.	63.	63.	63.	97.	201.	224.	242.
11.	75.	59.	144.	270.	37.	182.	91.	69.	69.	69.	69.	151.	207.	268.
12.	78.	63.	172.	272.	37.	196.	147.	72.	72.	72.	72.	89.	172.	279.
13.	81.	61.	202.	272.	37.	191.	191.	120.	71.	71.	71.	71.	121.	275.
14.	83.	56.	227.	268.	36.	170.	218.	177.	72.	67.	67.	67.	67.	257.
15.	84.	47.	245.	259.	35.	133.	225.	219.	120.	59.	59.	59.	59.	225.
16.	85.	37.	259.	245.	33.	86.	210.	240.	158.	49.	49.	49.	49.	182.
17.	85.	27.	271.	219.	30.	37.	173.	232.	177.	40.	37.	37.	37.	131.
18.	84.	17.	281.	172.	23.	24.	115.	185.	160.	56.	24.	24.	24.	75.
19.	83.	8.	292.	72.	10.	8.	36.	75.	74.	35.	8.	8.	8.	19.
20.	81.	0.	303.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	78.	0.	314.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	75.	0.	327.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	73.	0.	341.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	70.	0.	356.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

LOCATION: SEATTLE, WASHINGTON (CITY)

MONTH= 7 DAY=21 FOR LATITUDE= 47.6 LONGITUDE= 122.3

ET= -6.2000 R= .9690 SUNRZ= 4.6668 HO= 3560.77

CALCULATED SOLAR RADIATION DATA, BTU/HR (SQ. FT.)

TIME HR	AIR TEMP	NETA (DEG)	AZI- MUTH	IDN	DIFF	SOUTH	SW	WEST	NW	NORTH	NE	FAST	SE	HORIZ
1.	66.	0.	11.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
2.	64.	0.	26.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
3.	63.	0.	39.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
4.	62.	0.	51.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
5.	62.	3.	63.	6.	1.	1.	1.	1.	1.	3.	6.	6.	2.	1.
6.	63.	12.	73.	130.	18.	16.	16.	16.	16.	53.	128.	138.	77.	46.
7.	64.	22.	84.	199.	27.	31.	31.	31.	31.	51.	174.	214.	146.	102.
8.	66.	32.	95.	234.	32.	60.	43.	43.	43.	43.	171.	240.	104.	157.
9.	68.	42.	107.	253.	34.	110.	54.	54.	54.	54.	141.	233.	220.	204.
10.	70.	51.	123.	264.	36.	153.	63.	63.	63.	63.	97.	201.	224.	242.
11.	73.	59.	144.	270.	37.	183.	92.	69.	69.	69.	69.	151.	207.	267.
12.	75.	63.	172.	272.	37.	196.	148.	72.	72.	72.	72.	89.	172.	279.
13.	77.	61.	202.	272.	37.	192.	191.	120.	71.	71.	71.	71.	122.	275.
14.	79.	55.	227.	268.	36.	170.	218.	177.	71.	67.	67.	67.	67.	257.
15.	80.	47.	245.	259.	35.	134.	225.	219.	119.	59.	59.	59.	59.	225.
16.	81.	37.	259.	245.	33.	87.	210.	240.	158.	49.	49.	49.	49.	182.
17.	81.	27.	271.	220.	30.	38.	174.	232.	177.	40.	38.	38.	38.	131.
18.	80.	17.	261.	172.	23.	24.	115.	185.	161.	56.	24.	24.	24.	75.
19.	79.	8.	292.	73.	10.	8.	37.	76.	75.	35.	8.	8.	8.	20.
20.	77.	0.	303.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
21.	75.	0.	314.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
22.	73.	0.	327.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
23.	70.	0.	341.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
24.	68.	0.	356.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

Table C

Sol-air Temperatures

Sol-air temperature values tabulated in these tables are obtained from the solar radiation values of Table B and estimated outdoor air temperature profiles of a design day using equation (1) of the text.

LOCATION: SACRAMENTO, CALIFORNIA

MONTH= 7 DAY=21 FOR LATITUDE= 38.5 LONGITUDE= 121.5

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	71.	71.	71.	71.	71.	71.	71.	71.	71.	64.
2.	68.	68.	68.	68.	68.	68.	68.	68.	68.	61.
3.	65.	65.	65.	65.	65.	65.	65.	65.	65.	58.
4.	64.	64.	64.	64.	64.	64.	64.	64.	64.	57.
5.	64.	64.	64.	64.	64.	64.	64.	64.	64.	57.
6.	65.	67.	67.	67.	67.	72.	81.	82.	74.	63.
7.	68.	72.	72.	72.	72.	77.	94.	90.	88.	75.
8.	71.	78.	78.	78.	78.	78.	99.	107.	98.	88.
9.	75.	88.	84.	84.	84.	84.	99.	110.	106.	100.
10.	80.	98.	90.	90.	90.	90.	98.	110.	110.	112.
11.	84.	107.	95.	95.	95.	95.	96.	107.	112.	121.
12.	89.	113.	108.	100.	100.	100.	100.	103.	111.	127.
13.	93.	117.	119.	112.	104.	104.	104.	104.	107.	130.
14.	96.	117.	126.	124.	112.	107.	107.	107.	107.	130.
15.	99.	114.	130.	133.	121.	108.	108.	108.	108.	127.
16.	100.	109.	129.	136.	127.	107.	107.	107.	107.	121.
17.	100.	105.	124.	134.	128.	108.	105.	105.	105.	112.
18.	99.	102.	113.	123.	121.	107.	102.	102.	102.	101.
19.	96.	97.	97.	98.	98.	97.	97.	97.	97.	90.
20.	93.	93.	93.	93.	93.	93.	93.	93.	93.	86.
21.	89.	89.	89.	89.	89.	89.	89.	89.	89.	82.
22.	84.	84.	84.	84.	84.	84.	84.	84.	84.	77.
23.	80.	80.	80.	80.	80.	80.	80.	80.	80.	73.
24.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.

LOCATION: SACRAMENTO, CALIFORNIA

MONTH= 7 DAY=21 FOR LATITUDE= 38.5 LONGITUDE= 121.5

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	71.	71.	71.	71.	71.	71.	71.	71.	71.	64.
2.	68.	68.	68.	68.	68.	68.	68.	68.	68.	61.
3.	65.	65.	65.	65.	65.	65.	65.	65.	65.	58.
4.	64.	64.	64.	64.	64.	64.	64.	64.	64.	57.
5.	64.	64.	64.	64.	64.	64.	64.	64.	64.	57.
6.	65.	69.	69.	69.	69.	79.	97.	99.	83.	68.
7.	68.	77.	77.	77.	77.	85.	121.	131.	108.	90.
8.	71.	84.	84.	84.	84.	85.	126.	143.	126.	112.
9.	75.	101.	92.	92.	92.	92.	124.	146.	137.	133.
10.	80.	117.	100.	100.	100.	100.	116.	141.	141.	150.
11.	84.	130.	107.	107.	107.	107.	107.	130.	140.	164.
12.	89.	138.	127.	112.	112.	112.	112.	116.	133.	172.
13.	93.	141.	145.	132.	116.	116.	116.	116.	122.	175.
14.	96.	138.	156.	152.	128.	118.	118.	118.	118.	171.
15.	99.	130.	161.	167.	143.	117.	117.	117.	117.	162.
16.	100.	118.	158.	173.	153.	115.	115.	115.	115.	148.
17.	100.	111.	148.	169.	156.	117.	111.	111.	111.	130.
18.	99.	105.	127.	148.	143.	116.	105.	105.	105.	110.
19.	96.	97.	98.	101.	101.	98.	97.	97.	97.	90.
20.	93.	93.	93.	93.	93.	93.	93.	93.	93.	86.
21.	89.	89.	89.	89.	89.	89.	89.	89.	89.	82.
22.	84.	84.	84.	84.	84.	84.	84.	84.	84.	77.
23.	80.	80.	80.	80.	80.	80.	80.	80.	80.	73.
24.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.

LOCATION: WILMINGTON, DELAWARE

MONTH= 7 DAY=21 FOR LATITUDE= 39.7 LONGITUDE= 75.6

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
2.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.
3.	74.	74.	74.	74.	74.	74.	74.	74.	74.	67.
4.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
5.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
6.	74.	76.	76.	76.	76.	81.	91.	92.	84.	73.
7.	75.	80.	80.	80.	80.	84.	102.	107.	96.	84.
8.	77.	84.	84.	84.	84.	84.	104.	113.	105.	95.
9.	79.	93.	88.	88.	88.	88.	103.	114.	110.	105.
10.	82.	101.	92.	92.	92.	92.	99.	112.	113.	114.
11.	84.	108.	96.	95.	95.	95.	95.	107.	112.	120.
12.	87.	112.	107.	98.	98.	98.	98.	100.	109.	125.
13.	89.	113.	116.	109.	100.	100.	100.	100.	104.	126.
14.	91.	112.	122.	119.	106.	101.	101.	101.	101.	124.
15.	92.	108.	124.	126.	114.	101.	101.	101.	101.	120.
16.	93.	102.	122.	129.	120.	100.	100.	100.	100.	113.
17.	93.	98.	117.	127.	121.	101.	98.	98.	98.	104.
18.	92.	95.	106.	116.	114.	101.	95.	95.	95.	94.
19.	91.	91.	92.	93.	93.	92.	91.	91.	91.	84.
20.	89.	89.	89.	89.	89.	89.	89.	89.	89.	82.
21.	87.	87.	87.	87.	87.	87.	87.	87.	87.	80.
22.	84.	84.	84.	84.	84.	84.	84.	84.	84.	77.
23.	82.	82.	82.	82.	82.	82.	82.	82.	82.	75.
24.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.

LOCATION: WILMINGTON, DELAWARE

MONTH= 7 DAY=21 FOR LATITUDE= 39.7 LONGITUDE= 75.6

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
2.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.
3.	74.	74.	74.	74.	74.	74.	74.	74.	74.	67.
4.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
5.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
6.	74.	78.	78.	78.	78.	88.	109.	111.	94.	78.
7.	75.	84.	84.	84.	84.	92.	129.	139.	117.	99.
8.	77.	91.	90.	90.	90.	90.	132.	150.	133.	119.
9.	79.	107.	96.	96.	96.	96.	126.	149.	142.	138.
10.	82.	121.	102.	102.	102.	102.	117.	142.	144.	153.
11.	84.	132.	108.	106.	106.	106.	106.	129.	140.	163.
12.	87.	137.	127.	110.	110.	110.	110.	113.	131.	169.
13.	89.	138.	142.	129.	112.	112.	112.	112.	118.	170.
14.	91.	133.	152.	147.	122.	112.	112.	112.	112.	165.
15.	92.	124.	155.	160.	136.	110.	110.	110.	110.	155.
16.	93.	111.	152.	166.	146.	108.	108.	108.	108.	140.
17.	93.	104.	140.	161.	148.	109.	104.	104.	104.	123.
18.	92.	98.	120.	140.	136.	109.	98.	98.	98.	103.
19.	91.	91.	93.	94.	95.	93.	91.	91.	91.	85.
20.	89.	89.	89.	89.	89.	89.	89.	89.	89.	82.
21.	87.	87.	87.	87.	87.	87.	87.	87.	87.	80.
22.	84.	84.	84.	84.	84.	84.	84.	84.	84.	77.
23.	82.	82.	82.	82.	82.	82.	82.	82.	82.	75.
24.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.

LOCATION: MACON, GEORGIA

MONTH= 7 DAY=21 FOR LATITUDE= 32.7 LONGITUDE= 83.6

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	80.	80.	80.	80.	80.	80.	80.	80.	80.	73.
2.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
3.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
4.	76.	76.	76.	76.	76.	76.	76.	76.	76.	69.
5.	76.	76.	76.	76.	76.	76.	76.	76.	76.	69.
6.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
7.	78.	81.	81.	81.	81.	87.	100.	103.	92.	80.
8.	80.	86.	86.	86.	86.	90.	109.	115.	103.	93.
9.	83.	90.	90.	90.	90.	91.	111.	119.	111.	105.
10.	86.	99.	95.	95.	95.	95.	109.	119.	115.	115.
11.	88.	106.	99.	99.	99.	99.	106.	116.	116.	124.
12.	91.	112.	104.	103.	103.	103.	103.	110.	114.	130.
13.	94.	114.	110.	106.	106.	106.	106.	109.	114.	133.
14.	96.	115.	122.	120.	111.	107.	107.	107.	107.	133.
15.	97.	112.	126.	129.	119.	107.	107.	107.	107.	129.
16.	98.	108.	127.	134.	125.	106.	106.	106.	106.	123.
17.	98.	104.	123.	134.	127.	107.	104.	104.	104.	114.
18.	97.	101.	115.	127.	123.	107.	101.	101.	101.	103.
19.	96.	97.	101.	106.	105.	100.	97.	97.	97.	91.
20.	94.	94.	94.	94.	94.	94.	94.	94.	94.	87.
21.	91.	91.	91.	91.	91.	91.	91.	91.	91.	84.
22.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
23.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
24.	83.	83.	83.	83.	83.	83.	83.	83.	83.	76.

LOCATION: MACON, GEORGIA

MONTH= 7 DAY=21 FOR LATITUDE= 32.7 LONGITUDE= 83.6

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	Nw	NORTH	NE	EAST	SE	HORIZ
1.	80.	80.	80.	80.	80.	80.	80.	80.	80.	73.
2.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
3.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
4.	76.	76.	76.	76.	76.	76.	76.	76.	76.	69.
5.	76.	76.	76.	76.	76.	76.	76.	76.	76.	69.
6.	77.	77.	77.	77.	77.	77.	78.	78.	77.	70.
7.	78.	84.	84.	84.	84.	96.	122.	127.	106.	89.
8.	80.	91.	91.	91.	91.	99.	138.	149.	127.	112.
9.	83.	96.	98.	98.	98.	98.	139.	156.	139.	133.
10.	86.	112.	105.	105.	105.	105.	133.	153.	144.	152.
11.	88.	124.	110.	110.	110.	110.	124.	143.	143.	167.
12.	91.	132.	117.	115.	115.	115.	115.	129.	137.	176.
13.	94.	135.	125.	117.	117.	117.	117.	124.	135.	179.
14.	96.	134.	148.	145.	126.	118.	118.	118.	118.	177.
15.	97.	128.	155.	161.	141.	117.	117.	117.	117.	169.
16.	98.	118.	156.	170.	152.	115.	115.	115.	115.	155.
17.	98.	111.	149.	170.	156.	116.	111.	111.	111.	137.
18.	97.	105.	133.	156.	149.	116.	105.	105.	105.	116.
19.	96.	98.	106.	115.	115.	104.	98.	98.	98.	94.
20.	94.	94.	94.	94.	94.	94.	94.	94.	94.	87.
21.	91.	91.	91.	91.	91.	91.	91.	91.	91.	84.
22.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
23.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
24.	83.	83.	83.	83.	83.	83.	83.	83.	83.	76.

LOCATION: INDIANAPOLIS, INDIANA

MONTH= 7 DAY=21 FOR LATITUDE= 39.7 LONGITUDE= 86.3

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.
2.	75.	73.	73.	73.	73.	73.	73.	73.	73.	66.
3.	72.	72.	72.	72.	72.	72.	72.	72.	72.	65.
4.	71.	71.	71.	71.	71.	71.	71.	71.	71.	64.
5.	71.	71.	71.	71.	71.	71.	71.	71.	71.	64.
6.	72.	72.	72.	72.	72.	73.	74.	74.	73.	65.
7.	73.	76.	76.	76.	76.	82.	95.	97.	87.	75.
8.	75.	81.	81.	81.	81.	83.	103.	109.	99.	87.
9.	78.	87.	85.	85.	85.	85.	104.	114.	107.	98.
10.	81.	96.	90.	90.	90.	90.	103.	115.	112.	108.
11.	83.	105.	94.	94.	94.	94.	99.	112.	114.	117.
12.	86.	111.	101.	97.	97.	97.	97.	106.	113.	123.
13.	89.	114.	109.	100.	100.	100.	100.	102.	111.	126.
14.	91.	114.	119.	113.	102.	102.	102.	102.	103.	127.
15.	92.	112.	123.	122.	110.	102.	102.	102.	102.	124.
16.	93.	107.	124.	128.	117.	102.	102.	102.	102.	119.
17.	93.	100.	121.	129.	120.	100.	100.	100.	100.	111.
18.	92.	97.	113.	124.	119.	101.	97.	97.	97.	101.
19.	91.	93.	101.	110.	108.	98.	93.	93.	93.	90.
20.	89.	89.	89.	89.	89.	89.	89.	89.	89.	82.
21.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
22.	83.	83.	83.	83.	83.	83.	83.	83.	83.	76.
23.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
24.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.

LOCATION: INDIANAPOLIS, INDIANA

MONTH= 7 DAY=21 FOR LATITUDE= 39.7 LONGITUDE= 86.3

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.
2.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
3.	72.	72.	72.	72.	72.	72.	72.	72.	72.	65.
4.	71.	71.	71.	71.	71.	71.	71.	71.	71.	64.
5.	71.	71.	71.	71.	71.	71.	71.	71.	71.	64.
6.	72.	72.	72.	72.	72.	74.	75.	75.	73.	65.
7.	73.	79.	79.	79.	79.	90.	117.	121.	101.	84.
8.	75.	86.	86.	86.	86.	92.	131.	143.	122.	105.
9.	78.	96.	92.	92.	92.	92.	131.	151.	136.	125.
10.	81.	112.	99.	99.	99.	99.	124.	149.	144.	143.
11.	83.	126.	104.	104.	104.	104.	114.	140.	145.	157.
12.	80.	135.	115.	109.	109.	109.	109.	126.	139.	167.
13.	89.	139.	129.	112.	112.	112.	112.	115.	133.	171.
14.	91.	138.	147.	136.	113.	113.	113.	113.	115.	170.
15.	92.	132.	155.	153.	127.	112.	112.	112.	112.	163.
16.	93.	121.	155.	163.	140.	110.	110.	110.	110.	151.
17.	93.	108.	149.	166.	148.	107.	107.	107.	107.	135.
18.	92.	102.	135.	156.	146.	110.	102.	102.	102.	116.
19.	91.	95.	111.	128.	126.	105.	95.	95.	95.	96.
20.	89.	89.	89.	89.	89.	89.	89.	89.	89.	82.
21.	80.	86.	86.	86.	86.	86.	86.	86.	86.	79.
22.	83.	83.	83.	83.	83.	83.	83.	83.	83.	76.
23.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
24.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.

LOCATION: KALAMAZOO, MICHIGAN

MONTH= 7 DAY=21 FOR LATITUDE= 42.2 LONGITUDE= 84.5

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
2.	71.	71.	71.	71.	71.	71.	71.	71.	71.	64.
3.	70.	70.	70.	70.	70.	70.	70.	70.	70.	63.
4.	69.	69.	69.	69.	69.	69.	69.	69.	69.	62.
5.	69.	69.	69.	69.	69.	69.	69.	69.	69.	62.
6.	70.	70.	70.	70.	70.	73.	76.	76.	73.	64.
7.	71.	75.	75.	75.	75.	80.	95.	98.	87.	75.
8.	73.	79.	79.	79.	79.	81.	101.	108.	98.	86.
9.	76.	87.	84.	84.	84.	84.	101.	112.	106.	97.
10.	79.	97.	88.	88.	88.	88.	99.	112.	111.	107.
11.	82.	105.	92.	92.	92.	92.	95.	109.	113.	115.
12.	85.	111.	101.	96.	96.	96.	96.	103.	112.	121.
13.	86.	114.	108.	99.	99.	99.	99.	101.	112.	124.
14.	90.	114.	119.	113.	101.	101.	101.	101.	101.	125.
15.	91.	112.	123.	122.	108.	101.	101.	101.	101.	122.
16.	92.	106.	124.	127.	115.	100.	100.	100.	100.	117.
17.	92.	99.	120.	128.	119.	99.	99.	99.	99.	109.
18.	91.	96.	112.	123.	118.	100.	96.	96.	96.	99.
19.	90.	92.	99.	107.	106.	97.	92.	92.	92.	88.
20.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
21.	85.	85.	85.	85.	85.	85.	85.	85.	85.	78.
22.	82.	82.	82.	82.	82.	82.	82.	82.	82.	75.
23.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.
24.	76.	76.	76.	76.	76.	76.	76.	76.	76.	69.

LOCATION: KALAMAZOO, MICHIGAN

MONTH= 7 DAY=21 FOR LATITUDE= 42.2 LONGITUDE= 84.5

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
2.	71.	71.	71.	71.	71.	71.	71.	71.	71.	64.
3.	70.	70.	70.	70.	70.	70.	70.	70.	70.	63.
4.	69.	69.	69.	69.	69.	69.	69.	69.	69.	62.
5.	69.	69.	69.	69.	69.	69.	69.	69.	69.	62.
6.	70.	71.	71.	71.	71.	76.	83.	83.	76.	66.
7.	71.	78.	78.	78.	78.	89.	118.	124.	103.	85.
8.	73.	85.	85.	85.	85.	88.	128.	143.	123.	106.
9.	76.	98.	91.	91.	91.	91.	127.	149.	137.	125.
10.	79.	114.	97.	97.	97.	97.	119.	146.	144.	142.
11.	82.	128.	103.	103.	103.	103.	109.	136.	144.	156.
12.	85.	137.	118.	107.	107.	107.	107.	122.	139.	164.
13.	88.	141.	128.	110.	110.	110.	110.	115.	136.	168.
14.	90.	139.	149.	136.	111.	111.	111.	111.	113.	167.
15.	91.	132.	155.	153.	125.	111.	111.	111.	111.	160.
16.	92.	121.	155.	163.	138.	109.	109.	109.	109.	148.
17.	92.	106.	148.	164.	146.	105.	105.	105.	105.	132.
18.	91.	100.	133.	154.	144.	108.	100.	100.	100.	114.
19.	90.	94.	109.	125.	123.	104.	94.	94.	94.	93.
20.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
21.	85.	85.	85.	85.	85.	85.	85.	85.	85.	78.
22.	82.	82.	82.	82.	82.	82.	82.	82.	82.	75.
23.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.
24.	76.	76.	76.	76.	76.	76.	76.	76.	76.	69.

LOCATION: ST. LOUIS, MISSOURI

MONTH= 7 DAY=21 FOR LATITUDE= 38.6 LONGITUDE= 90.2

ALPHA/HZ .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
2.	80.	80.	80.	80.	80.	80.	80.	80.	80.	73.
3.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.
4.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
5.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
6.	79.	81.	81.	81.	81.	86.	96.	97.	89.	77.
7.	80.	84.	84.	84.	84.	89.	107.	112.	101.	88.
8.	81.	89.	88.	88.	88.	88.	109.	118.	109.	99.
9.	84.	97.	92.	92.	92.	92.	107.	119.	114.	110.
10.	86.	105.	96.	96.	96.	96.	104.	116.	117.	118.
11.	88.	111.	100.	99.	99.	99.	99.	110.	116.	125.
12.	90.	115.	110.	102.	102.	102.	102.	103.	112.	128.
13.	93.	116.	119.	113.	104.	104.	104.	104.	106.	130.
14.	94.	115.	124.	123.	110.	105.	105.	105.	105.	128.
15.	95.	111.	127.	130.	118.	104.	104.	104.	104.	123.
16.	96.	105.	125.	132.	123.	103.	103.	103.	103.	116.
17.	96.	101.	119.	130.	124.	104.	101.	101.	101.	107.
18.	95.	98.	109.	119.	116.	104.	98.	98.	98.	97.
19.	94.	94.	95.	95.	95.	95.	94.	94.	94.	87.
20.	93.	93.	93.	93.	93.	93.	93.	93.	93.	86.
21.	90.	90.	90.	90.	90.	90.	90.	90.	90.	83.
22.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
23.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
24.	84.	84.	84.	84.	84.	84.	84.	84.	84.	77.

LOCATION: ST. LOUIS, MISSOURI

MONTH= 7 DAY=21 FOR LATITUDE= 38.6 LONGITUDE= 90.2

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
2.	80.	80.	80.	80.	80.	80.	80.	80.	80.	73.
3.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.
4.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
5.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
6.	79.	83.	83.	83.	83.	93.	114.	116.	99.	83.
7.	80.	89.	89.	89.	89.	97.	134.	144.	122.	104.
8.	81.	96.	95.	95.	95.	95.	137.	154.	137.	124.
9.	84.	111.	101.	101.	101.	101.	131.	154.	145.	143.
10.	86.	124.	106.	106.	106.	106.	121.	146.	147.	157.
11.	88.	134.	112.	110.	110.	110.	110.	133.	143.	168.
12.	90.	140.	130.	114.	114.	114.	114.	116.	134.	173.
13.	93.	140.	145.	133.	115.	115.	115.	115.	120.	174.
14.	94.	135.	155.	151.	127.	115.	115.	115.	115.	168.
15.	95.	126.	158.	164.	141.	114.	114.	114.	114.	158.
16.	96.	113.	154.	169.	150.	111.	111.	111.	111.	143.
17.	96.	106.	142.	164.	151.	113.	106.	106.	106.	125.
18.	95.	101.	122.	142.	137.	112.	101.	101.	101.	105.
19.	94.	94.	95.	96.	96.	95.	94.	94.	94.	87.
20.	93.	93.	93.	93.	93.	93.	93.	93.	93.	86.
21.	90.	90.	90.	90.	90.	90.	90.	90.	90.	83.
22.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
23.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
24.	84.	84.	84.	84.	84.	84.	84.	84.	84.	77.

LOCATION: JERSLY CITY, NEW JERSEY

MONTH= 7 DAY=21 FOR LATITUDE= 40.7 LONGITUDE= 74.2

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	70.	76.	76.	76.	76.	76.	76.	76.	76.	69.
2.	74.	74.	74.	74.	74.	74.	74.	74.	74.	67.
3.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
4.	72.	72.	72.	72.	72.	72.	72.	72.	72.	65.
5.	72.	72.	72.	72.	72.	72.	72.	72.	72.	65.
6.	73.	75.	75.	75.	75.	81.	92.	94.	85.	73.
7.	74.	79.	79.	79.	79.	82.	101.	107.	96.	84.
8.	76.	84.	83.	83.	83.	83.	103.	112.	105.	94.
9.	78.	93.	87.	87.	87.	87.	101.	113.	110.	104.
10.	81.	101.	91.	91.	91.	91.	97.	110.	112.	113.
11.	83.	108.	96.	94.	94.	94.	94.	105.	111.	119.
12.	86.	112.	107.	97.	97.	97.	97.	98.	108.	123.
13.	88.	113.	116.	109.	99.	99.	99.	99.	102.	124.
14.	90.	111.	121.	119.	106.	100.	100.	100.	100.	123.
15.	91.	107.	123.	126.	113.	100.	100.	100.	100.	118.
16.	92.	101.	121.	128.	119.	99.	99.	99.	99.	111.
17.	92.	97.	115.	126.	119.	100.	97.	97.	97.	102.
18.	91.	94.	104.	114.	112.	100.	94.	94.	94.	92.
19.	90.	90.	90.	91.	91.	90.	90.	90.	90.	83.
20.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
21.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
22.	83.	83.	83.	83.	83.	83.	83.	83.	83.	76.
23.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
24.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.

LOCATION: JERSEY CITY, NEW JERSEY

MONTH= 7 DAY=21 FOR LATITUDE= 40.7 LONGITUDE= 74.2

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	76.	76.	76.	76.	76.	76.	76.	76.	76.	69.
2.	74.	74.	74.	74.	74.	74.	74.	74.	74.	67.
3.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
4.	72.	72.	72.	72.	72.	72.	72.	72.	72.	65.
5.	72.	72.	72.	72.	72.	72.	72.	72.	72.	65.
6.	73.	78.	78.	78.	78.	88.	112.	115.	96.	80.
7.	74.	84.	84.	84.	84.	91.	128.	140.	119.	100.
8.	76.	92.	90.	90.	90.	90.	130.	149.	133.	120.
9.	78.	108.	96.	96.	96.	96.	123.	148.	141.	138.
10.	81.	122.	101.	101.	101.	101.	113.	140.	143.	152.
11.	83.	132.	110.	105.	105.	105.	105.	126.	139.	162.
12.	80.	137.	128.	109.	109.	109.	109.	110.	130.	168.
13.	88.	138.	143.	129.	110.	110.	110.	110.	116.	168.
14.	90.	132.	152.	148.	121.	111.	111.	111.	111.	162.
15.	91.	123.	155.	160.	136.	109.	109.	109.	109.	152.
16.	92.	110.	150.	165.	145.	106.	106.	106.	106.	138.
17.	92.	102.	138.	159.	147.	108.	102.	102.	102.	120.
18.	91.	97.	117.	137.	133.	108.	97.	97.	97.	100.
19.	90.	90.	91.	92.	92.	91.	90.	90.	90.	83.
20.	80.	88.	88.	88.	88.	88.	88.	88.	88.	81.
21.	80.	86.	86.	86.	86.	86.	86.	86.	86.	79.
22.	83.	83.	83.	83.	83.	83.	83.	83.	83.	76.
23.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
24.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.

LOCATION: MEMPHIS, TENNESSEE

MONTH= 7 DAY=21 FOR LATITUDE= 35.1 LONGITUDE= 90.0

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
2.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.
3.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
4.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
5.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
6.	78.	80.	80.	80.	80.	84.	94.	95.	87.	76.
7.	79.	84.	84.	84.	84.	88.	106.	111.	100.	87.
8.	81.	88.	88.	88.	88.	89.	109.	117.	108.	99.
9.	83.	96.	92.	92.	92.	92.	109.	119.	113.	110.
10.	86.	104.	96.	96.	96.	96.	105.	116.	116.	119.
11.	89.	110.	100.	100.	100.	100.	101.	111.	115.	126.
12.	92.	114.	110.	103.	103.	103.	103.	104.	112.	130.
13.	94.	115.	119.	114.	105.	105.	105.	105.	106.	132.
14.	96.	114.	125.	125.	114.	107.	107.	107.	107.	130.
15.	97.	111.	127.	132.	121.	106.	106.	106.	106.	125.
16.	98.	105.	126.	135.	126.	105.	105.	105.	105.	118.
17.	98.	103.	120.	131.	126.	107.	103.	103.	103.	108.
18.	97.	100.	109.	119.	117.	105.	100.	100.	100.	98.
19.	96.	96.	96.	96.	96.	96.	96.	96.	96.	89.
20.	94.	94.	94.	94.	94.	94.	94.	94.	94.	87.
21.	92.	92.	92.	92.	92.	92.	92.	92.	92.	85.
22.	89.	89.	89.	89.	89.	89.	89.	89.	89.	82.
23.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
24.	83.	83.	83.	83.	83.	83.	83.	83.	83.	76.

LOCATION: MEMPHIS, TENNESSEE

MONTH= 7 DAY=21 FOR LATITUDE= 35.1 LONGITUDE= 90.0

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
2.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.
3.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
4.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
5.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
6.	78.	82.	82.	82.	82.	91.	110.	112.	96.	81.
7.	79.	88.	88.	88.	88.	98.	133.	143.	120.	103.
8.	81.	95.	95.	95.	95.	97.	138.	154.	135.	124.
9.	83.	108.	101.	101.	101.	101.	134.	154.	143.	143.
10.	86.	121.	107.	107.	107.	107.	125.	147.	145.	159.
11.	89.	131.	112.	112.	112.	112.	114.	134.	141.	170.
12.	92.	136.	129.	115.	115.	115.	115.	117.	132.	176.
13.	94.	137.	144.	135.	117.	117.	117.	117.	118.	177.
14.	96.	133.	154.	153.	132.	117.	117.	117.	117.	171.
15.	97.	124.	157.	166.	145.	116.	116.	116.	116.	160.
16.	98.	113.	154.	171.	154.	113.	113.	113.	113.	145.
17.	98.	108.	142.	165.	154.	116.	108.	108.	108.	126.
18.	97.	102.	122.	140.	137.	113.	102.	102.	102.	105.
19.	96.	96.	96.	96.	96.	96.	96.	96.	96.	89.
20.	94.	94.	94.	94.	94.	94.	94.	94.	94.	87.
21.	92.	92.	92.	92.	92.	92.	92.	92.	92.	85.
22.	89.	89.	89.	89.	89.	89.	89.	89.	89.	82.
23.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
24.	83.	83.	83.	83.	83.	83.	83.	83.	83.	76.

LOCATION: HOUSTON, TEXAS

MONTH= 7 DAY=21 FOR LATITUDE= 29.6 LONGITUDE= 95.3

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
2.	80.	80.	80.	80.	80.	80.	80.	80.	80.	73.
3.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.
4.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
5.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
6.	79.	79.	79.	79.	79.	82.	85.	85.	82.	73.
7.	80.	87.	87.	87.	87.	99.	128.	133.	111.	94.
8.	81.	93.	93.	93.	93.	102.	140.	152.	129.	117.
9.	84.	100.	100.	100.	100.	101.	140.	156.	139.	138.
10.	86.	111.	106.	106.	106.	106.	134.	151.	142.	156.
11.	88.	121.	111.	111.	111.	111.	124.	140.	139.	169.
12.	90.	128.	117.	114.	114.	114.	114.	124.	130.	177.
13.	93.	130.	134.	127.	116.	116.	116.	116.	118.	179.
14.	94.	127.	145.	147.	131.	117.	117.	117.	117.	174.
15.	95.	120.	151.	161.	144.	115.	115.	115.	115.	164.
16.	96.	112.	151.	169.	153.	114.	112.	112.	112.	149.
17.	96.	108.	143.	166.	155.	116.	108.	108.	108.	130.
18.	95.	102.	125.	146.	142.	114.	102.	102.	102.	108.
19.	94.	94.	95.	97.	97.	95.	94.	94.	94.	88.
20.	93.	93.	93.	93.	93.	93.	93.	93.	93.	86.
21.	90.	90.	90.	90.	90.	90.	90.	90.	90.	83.
22.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
23.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
24.	84.	84.	84.	84.	84.	84.	84.	84.	84.	77.

LOCATION: HOUSTON, TEXAS

MONTH= 7 DAY=21 FOR LATITUDE= 29.6 LONGITUDE= 95.3

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SF	HORIZ
1.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
2.	80.	80.	80.	80.	80.	80.	80.	80.	80.	73.
3.	79.	79.	79.	79.	79.	79.	79.	79.	79.	72.
4.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
5.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
6.	79.	79.	79.	79.	79.	80.	82.	82.	80.	72.
7.	80.	83.	83.	83.	83.	89.	104.	107.	96.	83.
8.	81.	87.	87.	87.	87.	92.	111.	117.	105.	96.
9.	84.	92.	92.	92.	92.	92.	112.	120.	111.	107.
10.	86.	99.	96.	96.	96.	96.	110.	118.	114.	117.
11.	88.	105.	99.	99.	99.	99.	106.	114.	113.	125.
12.	90.	109.	104.	102.	102.	102.	102.	107.	110.	130.
13.	93.	111.	113.	110.	104.	104.	104.	104.	105.	132.
14.	94.	111.	120.	121.	112.	105.	105.	105.	105.	131.
15.	95.	108.	123.	128.	120.	105.	105.	105.	105.	126.
16.	96.	104.	123.	132.	125.	105.	104.	104.	104.	119.
17.	96.	102.	119.	131.	125.	106.	102.	102.	102.	109.
18.	95.	99.	110.	121.	118.	104.	99.	99.	99.	98.
19.	94.	94.	95.	95.	95.	95.	94.	94.	94.	87.
20.	93.	93.	93.	93.	93.	93.	93.	93.	93.	86.
21.	90.	90.	90.	90.	90.	90.	90.	90.	90.	83.
22.	88.	88.	88.	88.	88.	88.	88.	88.	88.	81.
23.	86.	86.	86.	86.	86.	86.	86.	86.	86.	79.
24.	84.	84.	84.	84.	84.	84.	84.	84.	84.	77.

LOCATION: SEATTLE, WASHINGTON (CITY)

MONTH= 7 DAY=21 FOR LATITUDE= 47.6 LONGITUDE= 122.3

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	66.	66.	66.	66.	66.	66.	66.	66.	66.	59.
2.	64.	64.	64.	64.	64.	64.	64.	64.	64.	57.
3.	63.	63.	63.	63.	63.	63.	63.	63.	63.	56.
4.	62.	62.	62.	62.	62.	62.	62.	62.	62.	55.
5.	62.	62.	62.	62.	62.	63.	63.	63.	62.	55.
6.	63.	65.	65.	65.	65.	71.	82.	83.	74.	62.
7.	64.	69.	69.	69.	69.	72.	90.	96.	86.	72.
8.	66.	75.	72.	72.	72.	72.	91.	102.	95.	82.
9.	68.	84.	76.	76.	76.	76.	89.	103.	101.	91.
10.	70.	93.	80.	80.	80.	80.	85.	100.	104.	100.
11.	73.	100.	86.	83.	83.	83.	83.	95.	104.	106.
12.	75.	105.	97.	86.	86.	86.	86.	89.	101.	110.
13.	77.	106.	106.	95.	88.	88.	88.	88.	96.	112.
14.	79.	105.	112.	106.	90.	89.	89.	89.	89.	111.
15.	80.	100.	114.	113.	98.	89.	89.	89.	89.	107.
16.	81.	94.	113.	117.	105.	88.	88.	88.	88.	101.
17.	81.	87.	107.	116.	108.	87.	87.	87.	87.	94.
18.	80.	84.	98.	108.	104.	89.	84.	84.	84.	85.
19.	79.	80.	85.	90.	90.	84.	80.	80.	80.	75.
20.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
21.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.
22.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
23.	70.	70.	70.	70.	70.	70.	70.	70.	70.	63.
24.	68.	68.	68.	68.	68.	68.	68.	68.	68.	61.

LOCATION: SEATTLE, WASHINGTON (AIRPORT)

MONTH= 7 DAY=21 FOR LATITUDE= 47.4 LONGITUDE= 122.3

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	67.	67.	67.	67.	67.	67.	67.	67.	67.	60.
2.	65.	65.	65.	65.	65.	65.	65.	65.	65.	58.
3.	64.	64.	64.	64.	64.	64.	64.	64.	64.	57.
4.	63.	63.	63.	63.	63.	63.	63.	63.	63.	56.
5.	63.	63.	63.	63.	63.	64.	65.	65.	64.	56.
6.	64.	69.	69.	69.	69.	80.	102.	105.	87.	70.
7.	65.	74.	74.	74.	74.	80.	118.	129.	109.	89.
8.	67.	85.	80.	80.	80.	80.	119.	139.	125.	107.
9.	70.	103.	86.	86.	86.	86.	112.	140.	136.	124.
10.	73.	118.	91.	91.	91.	91.	102.	133.	140.	138.
11.	75.	130.	103.	96.	96.	96.	96.	121.	138.	149.
12.	78.	137.	122.	100.	100.	100.	100.	105.	130.	155.
13.	81.	138.	138.	117.	102.	102.	102.	102.	117.	156.
14.	83.	134.	148.	136.	104.	103.	103.	103.	103.	153.
15.	84.	124.	152.	150.	120.	102.	102.	102.	102.	145.
16.	85.	111.	148.	157.	132.	100.	100.	100.	100.	133.
17.	85.	96.	137.	155.	138.	97.	96.	96.	96.	117.
18.	84.	91.	119.	140.	132.	101.	91.	91.	91.	100.
19.	83.	85.	94.	105.	105.	93.	85.	85.	85.	82.
20.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
21.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
22.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.
23.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
24.	70.	70.	70.	70.	70.	70.	70.	70.	70.	63.

LOCATION: SEATTLE, WASHINGTON (AIRPORT)

MONTH= 7 DAY=21 FOR LATITUDE= 47.4 LONGITUDE= 122.3

ALPHA/H= .150

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	67.	67.	67.	67.	67.	67.	67.	67.	67.	60.
2.	65.	65.	65.	65.	65.	65.	65.	65.	65.	58.
3.	64.	64.	64.	64.	64.	64.	64.	64.	64.	57.
4.	63.	63.	63.	63.	63.	63.	63.	63.	63.	56.
5.	63.	63.	63.	63.	63.	63.	64.	64.	63.	56.
6.	64.	66.	66.	66.	66.	72.	83.	84.	75.	64.
7.	65.	70.	70.	70.	70.	73.	91.	97.	87.	74.
8.	67.	76.	74.	74.	74.	74.	93.	103.	96.	84.
9.	70.	86.	78.	78.	78.	78.	91.	105.	103.	93.
10.	73.	95.	82.	82.	82.	82.	87.	103.	106.	102.
11.	75.	103.	89.	86.	86.	86.	86.	98.	107.	109.
12.	78.	108.	100.	89.	89.	89.	89.	92.	104.	113.
13.	81.	109.	109.	99.	91.	91.	91.	91.	99.	115.
14.	83.	108.	115.	109.	94.	93.	93.	93.	93.	114.
15.	84.	104.	118.	117.	102.	93.	93.	93.	93.	111.
16.	85.	98.	117.	121.	109.	92.	92.	92.	92.	105.
17.	85.	91.	111.	120.	112.	91.	91.	91.	91.	98.
18.	84.	88.	101.	112.	108.	93.	88.	88.	88.	88.
19.	83.	84.	88.	94.	94.	88.	84.	84.	84.	79.
20.	81.	81.	81.	81.	81.	81.	81.	81.	81.	74.
21.	78.	78.	78.	78.	78.	78.	78.	78.	78.	71.
22.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.
23.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
24.	70.	70.	70.	70.	70.	70.	70.	70.	70.	63.

LOCATION: SEATTLE, WASHINGTON (CITY)

MONTH= 7 DAY=21 FOR LATITUDE= 47.6 LONGITUDE= 122.3

ALPHA/H= .300

SOL-AIR TEMPERATURES (DEG. F)

TIME (HR)	AIR TEMP	SOUTH	SW	WEST	NW	NORTH	NE	EAST	SE	HORIZ
1.	60.	66.	66.	66.	66.	66.	66.	66.	66.	59.
2.	64.	64.	64.	64.	64.	64.	64.	64.	64.	57.
3.	63.	63.	63.	63.	63.	63.	63.	63.	63.	56.
4.	62.	62.	62.	62.	62.	62.	62.	62.	62.	55.
5.	62.	62.	62.	62.	62.	63.	64.	64.	63.	55.
6.	63.	68.	68.	68.	68.	78.	101.	104.	86.	69.
7.	64.	73.	73.	73.	73.	79.	116.	128.	108.	88.
8.	66.	84.	79.	79.	79.	79.	117.	138.	124.	106.
9.	68.	101.	84.	84.	84.	84.	110.	138.	134.	122.
10.	70.	116.	89.	89.	89.	89.	99.	131.	138.	136.
11.	73.	128.	100.	93.	93.	93.	93.	118.	135.	146.
12.	75.	134.	119.	97.	97.	97.	97.	102.	127.	152.
13.	77.	135.	135.	113.	99.	99.	99.	99.	114.	153.
14.	79.	130.	145.	132.	100.	99.	99.	99.	99.	149.
15.	80.	120.	148.	146.	116.	98.	98.	98.	98.	141.
16.	81.	107.	144.	153.	128.	96.	96.	96.	96.	129.
17.	81.	92.	133.	151.	134.	93.	92.	92.	92.	113.
18.	80.	88.	115.	136.	129.	97.	88.	88.	88.	96.
19.	79.	82.	90.	102.	102.	90.	82.	82.	82.	78.
20.	77.	77.	77.	77.	77.	77.	77.	77.	77.	70.
21.	75.	75.	75.	75.	75.	75.	75.	75.	75.	68.
22.	73.	73.	73.	73.	73.	73.	73.	73.	73.	66.
23.	70.	70.	70.	70.	70.	70.	70.	70.	70.	63.
24.	68.	68.	68.	68.	68.	68.	68.	68.	68.	61.

Table D

Magnetic Tape TDF 14 for Breakthrough Localities

<u>Localities</u>	<u>Station No.</u>	<u>Record Period</u>	<u>Reel No.</u>
Sacramento, Calif.	23232	Jan. '49 - Dec. '58	069
Wilmington, Del. (Phila., Pa.)	13739	Jan. '49 - Dec. '58	268
Macon, Ga.	03813	Jan. '55 - Dec. '64	527
Indianapolis, Ind.	93819	Jan. '49 - Dec. '58	550
Kalamazoo, Mich. (Battle Creek)	14815	Jan. '49 - Dec. '54	073
St. Louis, Mo.	13984	Jan. '49 - Dec. '58	261
Jersey City, N. J. (Newark, N. J.)	14734	Jan. '49 - Dec. '58	205
Memphis Tennessee	93839	Jan. '49 - Dec. '58	173
Houston, Tex.	12918	Jan. '49 - Dec. '58	259
Seattle, Wash. Sea/Tac airport	24233	Jan. '49 - Dec. '58	088
Downtown Seattle	24244		302, 86, 326

Table E

AFM 88-8* Data for Coincident

Dry- and Wet-Bulb Temperature Frequencies

These tables show the frequency of the hourly dry-bulb temperature observations for a temperature range of 5 degrees F for three daily time periods; from 02 to 09 hours, from 10 to 17 hours and from 18 to 01 hours. Also listed are total frequencies of hourly observations for each month at 5 ° temperature "bin" and average wet-bulb temperature that occurs coincident with the same temperature level specified in the "bin".

* Amended by O. E. Richard in 1971

SACRAMENTO, CALIFORNIA

COOLING SEASON

Mean Frequency of Occurrence of Dry Bulb Temperature (°F) With Mean Coincident Wet Bulb Temperature (°F) For Each Dry Bulb Temperature Range

Tem- per- ature Range (°F)	May					June					July					August					September					October					Mean Co- inci- dent Wet Bulb (°F)
	Obsn/ Hour Gp			Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp			Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp			Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp			Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp			Total Obsn	Mean Co- inci- dent Wet Bulb (°F)						
	02 to 09	10 to 17	18 to 01			02 to 09	10 to 17	18 to 01			02 to 09	10 to 17	18 to 01			02 to 09	10 to 17	18 to 01			02 to 09	10 to 17	18 to 01			02 to 09	10 to 17	18 to 01	02 to 09	10 to 17	
115/119	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0					
110/114	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0					
105/109	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0					
100/104	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0					
95/99	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0					
90/94	0	1	0	1	65	0	15	3	18	70	0	29	3	32	69	0	28	3	31	69	0	10	1	11	68	0					
85/89	0	6	1	7	66	0	25	5	30	68	0	47	8	55	68	0	52	7	59	68	0	35	3	38	67	0					
80/84	0	16	2	18	64	2	36	7	45	66	1	50	11	62	67	0	55	12	67	67	0	42	7	49	64	0					
75/79	0	35	5	40	63	4	49	14	67	64	4	44	20	68	65	3	48	20	71	65	1	49	14	64	63	0					
70/74	2	40	10	52	61	7	42	21	70	62	8	28	26	62	63	10	33	29	72	63	5	48	24	77	62	0					
65/69	5	53	14	72	59	23	28	32	83	60	26	14	38	78	61	24	17	46	87	61	14	33	37	84	60	3					
60/64	14	43	25	82	57	35	9	38	82	58	42	2	51	95	59	50	3	55	108	59	35	15	54	104	58	12					
55/59	34	25	46	105	55	49	2	52	103	56	67	0	47	114	56	71	1	54	126	57	68	3	58	129	56	37					
50/54	57	8	66	131	52	60	1	34	95	53	64	0	20	84	54	76	0	22	98	54	76	0	36	112	54	82					
45/49	75	2	47	124	49	38	1	12	51	50	14	0	1	15	51	14	0	0	14	51	38	0	6	44	50	85					
40/44	32	0	9	41	45	1	0	0	1	46	0	0	0	0	0	0	0	0	0	0	3	0	0	3	47	44	22				
35/39	6	0	1	7	41	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	6					
30/34	1	0	0	1	37	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1					
25/29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0					
20/24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0					

HEATING SEASON

Time- base Rate (°F)	November			December			January			February			March			April			Annual (Total - All Months)			
	Obsn/ hour Cp			Obsn/ hour Cp			Obsn/ hour Cp			Obsn/ hour Cp			Obsn/ hour Cp			Obsn/ hour Cp			Obsn/ hour Cp			
	02 to 09	10 to 17	18 to 01	02 to 09	10 to 17	18 to 01	02 to 09	10 to 17	18 to 01	02 to 09	10 to 17	18 to 01	02 to 09	10 to 17	18 to 01	02 to 09	10 to 17	18 to 01	02 to 09	10 to 17	18 to 01	
115/119	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
105/110	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
100/104	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
95/99	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
90/94	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
85/89	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
80/84	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
75/79	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
70/74	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
65/69	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
60/64	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
55/59	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
50/54	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
45/49	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
40/44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
35/39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
30/34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
25/29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20/24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

*** WILMINGTON DELAWARE**

Mean Frequency of Occurrence of Dry Bulb Temperature (°F) With Mean Coincident Wet Bulb Temperature (°F) For Each Dry Bulb Temperature Range

COOLING SEASON

Temperature Range (°F)	MAY				JUNE				JULY				AUGUST				SEPTEMBER				OCTOBER					
	Oben/ Hour Gp		Total Oben	Mean Co-incident Wet Bulb (°F)	Oben/ Hour Gp		Total Oben	Mean Co-incident Wet Bulb (°F)	Oben/ Hour Gp		Total Oben	Mean Co-incident Wet Bulb (°F)	Oben/ Hour Gp		Total Oben	Mean Co-incident Wet Bulb (°F)	Oben/ Hour Gp		Total Oben	Mean Co-incident Wet Bulb (°F)	Oben/ Hour Gp		Total Oben	Mean Co-incident Wet Bulb (°F)		
	08 to 09	10 to 17			08 to 09	10 to 17			08 to 09	10 to 17			08 to 09	10 to 17			08 to 09	10 to 17			08 to 09	10 to 17			08 to 09	10 to 17
	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01	18 to 01		
100/104																										
95/99																										
90/94																										
85/89																										
80/84																										
75/79																										
70/74																										
65/69																										
60/64																										
55/59																										
50/54																										
45/49																										
40/44																										
35/39																										
30/34																										

HEATING SEASON

Temperature Range (°F)	NOVEMBER				DECEMBER				JANUARY				FEBRUARY				MARCH				APRIL				ANNUAL (TOTAL - ALL MONTHS)											
	Obem/ Hour Gp		Mean Co-incident W/kt Bulb (°F)		Obem/ Hour Gp		Mean Co-incident W/kt Bulb (°F)		Obem/ Hour Gp		Mean Co-incident W/kt Bulb (°F)		Obem/ Hour Gp		Mean Co-incident W/kt Bulb (°F)		Obem/ Hour Gp		Mean Co-incident W/kt Bulb (°F)		Obem/ Hour Gp		Mean Co-incident W/kt Bulb (°F)		Obem/ Hour Gp		Mean Co-incident W/kt Bulb (°F)									
	02	10	18	Total	02	10	18	Total	02	10	18	Total	02	10	18	Total	02	10	18	Total	02	10	18	Total	02	10	18	Total	02	10	18	Total				
	09	17	01		09	17	01		09	17	01		09	17	01		09	17	01		09	17	01		09	17	01		09	17	01					
100/104																																				
95/99																																				
90/94																																				
85/89																																				
80/84	0			0																																
75/79	0			0																																
70/74	5			5																																
65/69	2	12	1	15																																
60/64	6	25	8	39	0	3	1	4																												
55/59	19	36	22	77	2	10	3	15	1	4	0	5	2	8	1	11	5	23	10	38	4	15	3	22	1	5	2	8	1	5	2	8	1	5	2	8
50/54	21	45	26	92	6	21	7	34	2	8	2	12	5	20	6	31	9	36	17	62	4	15	3	22	3	12	4	19	3	12	4	19	3	12	4	19
45/49	29	52	45	126	16	39	18	67	4	21	8	33	10	30	17	57	23	45	35	103	42	53	29	124	53	29	53	135	48	22	21	91	43	22	21	91
40/44	47	39	43	134	38	26	47	110	39	15	36	20	71	38	19	46	31	96	88	215	43	43	49	135	38	45	13	34	92	39	243	285	727	39	243	285
35/39	49	18	53	120	34	40	47	110	34	38	73	52	168	34	44	52	51	147	84	231	64	64	41	105	34	32	4	18	54	34	268	330				
30/34	47	6	23	81	30	55	41	126	30	63	50	69	182	29	63	32	64	159	30	52	17	40	109	29	11	0	4	15	30	49						
25/29	15	2	7	24	25	35	26	86	25	48	29	45	122	25	89	18	23	80	25	29	9	19	57	24	2	0	2	25	168	203						
20/24	3	0	2	5	20	88	15	29	77	32	17	24	73	20	19	9	10	38	20	15	3	8	26	20			104	44	74	222						
15/19	2			2	25	3	13	41	15	24	9	16	49	15	11	5	9	25	15	5	1	6	15				87	17	40	124						
10/14					9	1	3	13	11	12	1	8	21	11	8	2	4	14	11	2		2	11				31	4	15	50						
5/9					1	0	0	1	6	2	0	3	9	6	3	1	2	6	6						10	1	6	17								
0/4					0			0	2	2	2	1	3	2	1	1	1	1	1						4	4	1	5								
-5/-1																																				

* INDIANAPOLIS INDIANA

Mean Frequency of Occurrence of Dry Bulb Temperature (°F) With Mean Coincident Wet Bulb Temperature (°F) For Each Dry Bulb Temperature Range

COOLING SEASON

Temperature Range (°F)	MAY			JUNE			JULY			AUGUST			SEPTEMBER			OCTOBER		
	Obm./Hour Gp			Obm./Hour Gp			Obm./Hour Gp			Obm./Hour Gp			Obm./Hour Gp			Obm./Hour Gp		
	08 to 09	10 to 17	18 to 01	08 to 09	10 to 17	18 to 01	08 to 09	10 to 17	18 to 01	08 to 09	10 to 17	18 to 01	08 to 09	10 to 17	18 to 01	08 to 09	10 to 17	18 to 01
	Total Obm.	Co-incident Wet Bulb (°F)	Mean Co-incident Wet Bulb (°F)	Total Obm.	Co-incident Wet Bulb (°F)	Mean Co-incident Wet Bulb (°F)	Total Obm.	Co-incident Wet Bulb (°F)	Mean Co-incident Wet Bulb (°F)	Total Obm.	Co-incident Wet Bulb (°F)	Mean Co-incident Wet Bulb (°F)	Total Obm.	Co-incident Wet Bulb (°F)	Mean Co-incident Wet Bulb (°F)	Total Obm.	Co-incident Wet Bulb (°F)	Mean Co-incident Wet Bulb (°F)
100/104																		
95/99																		
90/94	1			3	0	3	76	0	3	76	0	3	76	0	3	76	0	3
85/89	0	7	0	4	37	6	47	72	4	58	9	71	73	2	52	4	58	73
80/84	1	22	2	11	51	22	84	70	14	80	31	125	71	10	80	21	111	71
75/79	4	42	12	28	54	42	124	68	39	57	63	169	69	27	60	55	142	69
70/74	15	48	26	47	37	61	145	66	77	22	81	180	68	70	27	80	177	68
65/69	35	47	45	127	60	56	23	62	68	5	46	119	64	69	8	55	132	64
60/64	48	39	54	141	57	48	8	58	34	0	15	49	59	49	0	26	75	59
55/59	43	16	42	101	52	29	5	54	9	2	11	55	55	17	7	24	55	55
50/54	42	14	30	86	48	14	1	50	2				52	4	0	6	4	51
45/49	30	8	21	59	44	3	1	46	2				46	20	1	8	29	45
40/44	19	3	12	34	39	0	0	41	7				41	7		1	8	41
35/39	9	1	4	14	36	0	0	38	0				38	0		0	0	37
30/34	2		0	2	31													
25/29																		
20/24																		

GRAND RAPIDS, MICHIGAN (Substitute Station for Kalamazoo)

Mean Frequency of Occurrence of Dry Bulb Temperature (°F) With Mean Coincident Wet Bulb Temperature (°F) For Each Dry Bulb Temperature Range

COOLING SEASON

Tem- pera- ture Range (°F)	May				June				July				August				September				October				Mean Co- inci- dent Wet Bulb (°F)
	Obsn/ Hour Gp		Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp		Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp		Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp		Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp		Total Obsn	Mean Co- inci- dent Wet Bulb (°F)					
	02 to 09	10 to 17			18 to 01	02 to 09			10 to 17	18 to 01			02 to 09	10 to 17			18 to 01	02 to 09			10 to 17	18 to 01	02 to 09	10 to 17	
100/104	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
95/99	0	0	0	0	0	0	76	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
90/94	0	0	0	0	0	0	77	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
85/89	0	0	0	75	0	0	73	0	0	0	0	78	0	0	0	0	0	0	0	0	0	0			
80/84	0	3	0	69	0	0	71	0	0	0	0	73	0	0	0	0	0	0	0	0	0	0			
75/79	0	14	2	66	4	4	68	5	63	27	95	68	3	62	20	85	69	1	22	7	30	69			
70/74	1	26	10	63	12	51	67	16	64	48	128	67	13	64	42	119	67	10	32	19	61	66			
65/69	5	38	19	60	29	49	65	50	48	65	163	65	47	46	64	157	66	17	44	25	86	63			
60/64	20	41	32	57	49	35	60	69	12	54	135	63	64	24	58	146	63	29	51	42	122	60			
55/59	32	41	41	54	49	17	57	59	5	32	96	59	56	5	37	98	59	42	40	45	127	56			
50/54	39	34	43	50	43	8	53	32	1	11	44	54	40	1	14	55	55	43	21	40	104	55			
45/49	40	24	41	47	33	3	49	15	0	1	16	50	18	0	3	21	50	42	8	33	83	53			
40/44	45	18	32	43	15	0	45	1	0	0	1	47	6	0	0	7	46	32	1	16	49	49			
35/39	34	7	19	39	6	0	41	0	0	0	0	0	0	0	0	0	43	15	0	7	22	41			
30/34	26	2	7	35	1	0	37	0	0	0	0	0	0	0	0	0	0	8	0	2	10	36			
25/29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	1	33			
20/24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
15/19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
10/14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
5/9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
0/4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
-5/-1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
-10/-6	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			

NEWARK, NEW JERSEY (Substitute Station for Jersey City)

Mean Frequency of Occurrence of Dry Bulb Temperature (°F) With Mean Coincident Wet Bulb Temperature (°F) For Each Dry Bulb Temperature Range

COOLING SEASON

Tem- pera- ture Range (°F)	May				June				July				August				September				October				Mean Co- inci- dent Wet Bulb (°F)
	Obsn/ Hour Gp		Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp		Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp		Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp		Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp		Total Obsn	Mean Co- inci- dent Wet Bulb (°F)					
	02 to 09	10 to 17			18 to 01	02 to 09			10 to 17	18 to 01			02 to 09	10 to 17			18 to 01	02 to 09			10 to 17	18 to 01	02 to 09	10 to 17	
100/104	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
95/99	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
-90/94	0	4	0	4	0	13	3	16	4	0	74	74	0	4	0	2	21	4	0	0	0	0			
85/89	0	12	1	13	69	2	31	8	41	70	72	72	1	41	10	52	72	0	18	3	21	10			
80/84	1	19	7	27	66	7	47	22	76	68	69	69	14	67	39	103	70	2	34	12	48	1			
75/79	4	29	13	46	63	20	52	34	106	66	66	66	37	66	66	169	69	15	49	28	92	68			
70/74	16	40	24	80	60	49	44	56	149	64	67	67	80	43	79	202	66	38	43	47	128	65			
65/69	26	54	38	118	58	62	31	53	146	61	62	62	75	9	48	132	63	46	46	53	145	60			
60/64	45	47	50	142	54	58	14	43	115	57	57	58	36	1	12	49	58	56	29	50	135	60			
55/59	57	22	55	134	51	35	4	19	58	53	54	54	10	1	1	12	54	41	10	29	80	57			
50/54	53	13	37	103	47	6	0	1	7	49	0	0	0	0	0	0	0	27	1	13	41	52			
45/49	34	8	19	61	43	0	0	0	0	47	0	0	0	0	0	0	0	11	0	4	15	48			
40/44	10	0	3	13	39	0	0	0	0	0	0	0	0	0	0	0	0	3	0	0	3	43			
35/39	1	0	1	2	36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	39			
30/34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	38			
25/29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
20/24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
15/19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
10/14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
5/9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
0/4	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			

MEMPHIS HAS TENNESSEE

Mean Frequency of Occurrence of Dry Bulb Temperature ($^{\circ}F$) With Mean Coincident Wet Bulb Temperature ($^{\circ}F$) For Each Dry Bulb Temperature Range

COOLING SEASON

Temperature Range ($^{\circ}F$)	MAY					JUNE					JULY					AUGUST					SEPTEMBER					OCTOBER					
	Obs./Hour Gp			Mean Co-incident Wet Bulb ($^{\circ}F$)	Total Obsm	Obs./Hour Gp			Mean Co-incident Wet Bulb ($^{\circ}F$)	Total Obsm	Obs./Hour Gp			Mean Co-incident Wet Bulb ($^{\circ}F$)	Total Obsm	Obs./Hour Gp			Mean Co-incident Wet Bulb ($^{\circ}F$)	Total Obsm	Obs./Hour Gp			Mean Co-incident Wet Bulb ($^{\circ}F$)	Total Obsm	Obs./Hour Gp			Mean Co-incident Wet Bulb ($^{\circ}F$)	Total Obsm	
	08 to 09	10 to 17	18 to 01			08 to 09	10 to 17	18 to 01			08 to 09	10 to 17	18 to 01			08 to 09	10 to 17	18 to 01			08 to 09	10 to 17	18 to 01			08 to 09	10 to 17	18 to 01			08 to 09
105/109				0	0	0	76	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0			
100/104				2	0	2	76	2	0	2	76	2	0	2	76	2	0	2	76	2	0	2	76	2	0	2	76	2	0		
95/99				0	7	1	8	75	1	8	75	1	19	78	1	19	78	1	19	78	1	19	78	1	19	78	1	19	78		
90/94				0	44	6	50	75	44	6	50	75	1	77	12	90	77	1	76	10	87	77	1	26	74	6	0	6	74		
85/89				0	48	5	54	72	48	5	54	72	6	66	30	92	73	6	66	30	92	73	6	66	30	92	73	6	66		
80/84				7	62	24	93	70	25	60	43	128	72	41	47	67	135	74	33	43	64	140	74	9	59	22	90	71	1	68	
75/79				28	47	47	117	68	51	37	73	161	70	88	19	87	194	72	81	18	82	181	72	32	45	58	135	70	7	66	
70/74				51	33	63	147	66	88	19	63	170	68	85	5	43	133	70	85	5	46	136	69	69	30	69	168	67	18	64	
65/69				72	25	50	147	62	44	3	25	72	63	18	0	4	22	64	30	1	9	40	64	85	12	46	113	62	35	61	
60/64				45	13	30	88	57	20	2	7	29	59	4	4	0	4	58	7	2	9	59	58	43	4	26	73	58	41	57	
55/59				25	7	15	47	52	5	2	7	55	0	5	0	0	0	57	1	1	1	56	22	1	8	31	53	43	52	41	
50/54				13	2	10	25	47	1	1	1	51	1	1	1	1	1	51	7	2	9	49	7	2	9	49	41	9	48	41	
45/49				11	0	2	13	43										44	1	1	1	44	1	1	1	1	1	1	1	44	
40/44				1	0	0	1	40										40				40								40	
35/39																															
30/34																															

HOUSTON, TEXAS

Mean Frequency of Occurrence of Dry Bulb Temperature (°F) With Mean Coincident Wet Bulb Temperature (°F) For Each Dry Bulb Temperature Range

COOLING SEASON

October

September

August

July

June

May

Tem- pera- ture Range (°F)	Obsn/ Hour Gp			Mean Co- inci- dent Wet Bulb (°F)	Total Obsn	Obsn/ Hour Gp			Mean Co- inci- dent Wet Bulb (°F)	Total Obsn	Obsn/ Hour Gp			Mean Co- inci- dent Wet Bulb (°F)	Total Obsn	Obsn/ Hour Gp			Mean Co- inci- dent Wet Bulb (°F)	Total Obsn	Obsn/ Hour Gp			Mean Co- inci- dent Wet Bulb (°F)	Total Obsn			
	to					to					to					to					to					to		
	02 to 09	10 to 17	18 to 01			02 to 09	10 to 17	18 to 01			02 to 09	10 to 17	18 to 01			02 to 09	10 to 17	18 to 01			02 to 09	10 to 17	18 to 01			02 to 09	10 to 17	18 to 01
105/109	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0		
100/104	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	
95/99	0	0	0	78	5	0	5	0	77	0	19	1	20	0	18	1	19	0	79	0	0	0	0	0	0	0	0	
90/94	0	9	0	74	9	0	52	3	76	0	108	8	116	0	93	6	99	0	77	0	41	1	42	77	0	7	76	
85/89	0	77	3	74	80	0	118	21	76	22	87	36	145	18	85	29	132	77	77	6	96	10	112	76	1	37	74	
80/84	19	106	27	72	152	42	41	61	75	50	20	87	157	43	32	88	163	77	77	28	57	47	132	75	5	74	71	
75/79	60	36	82	72	178	72	95	16	74	145	11	108	264	153	13	112	278	75	75	98	29	115	242	74	22	62	70	
70/74	80	15	90	69	185	76	76	7	71	30	2	7	39	30	2	10	42	71	71	68	11	46	125	69	51	36	67	
65/69	57	4	34	65	95	12	1	4	65	0	0	0	0	2	0	0	2	66	66	26	2	17	45	64	61	16	63	
60/64	23	1	11	59	35	3	0	1	59	0	0	0	0	0	0	0	0	0	0	11	0	2	13	60	48	7	63	
55/59	8	0	1	54	9	0	0	0	57	0	0	0	0	0	0	0	0	0	0	1	0	0	1	54	31	4	58	
50/54	1	0	0	50	1	0	0	0	50	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	20	2	53	
45/49	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	5	1	49	
40/44	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	1	43	
35/39	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	39	
30/34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	36	
25/29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
20/24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15/19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

SEATTLE, WASHINGTON

Mean Frequency of Occurrence of Dry Bulb Temperature (°F) With Mean Coincident Wet Bulb Temperature (°F) For Each Dry Bulb Temperature Range

COOLING SEASON

Tem- pera- ture Range (°F)	May				June				July				August				September				October					
	Obsn/ Hour Gp		Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp		Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp		Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp		Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp		Total Obsn	Mean Co- inci- dent Wet Bulb (°F)	Obsn/ Hour Gp		Total Obsn	Mean Co- inci- dent Wet Bulb (°F)		
	02 to 09	10 to 17			18 to 01	02 to 09			10 to 17	18 to 01			02 to 09	10 to 17			18 to 01	02 to 09			10 to 17	18 to 01			02 to 09	10 to 17
95/99	0	0	0	0	0	1	67	0	1	0	1	70	0	1	0	1	68	0	0	0	0	0	0	0	0	
90/94	0	1	0	64	0	1	67	0	4	1	5	68	0	0	1	6	68	0	0	0	0	0	0	0	0	
85/89	0	3	0	64	0	4	65	0	12	4	16	66	0	5	1	6	67	0	2	0	2	0	0	0	0	
80/84	0	7	2	62	0	10	64	1	22	9	32	65	0	20	5	25	65	0	8	1	9	0	0	0	0	
75/79	0	11	4	60	0	17	62	1	34	16	51	63	0	39	11	50	63	0	20	3	23	0	1	1	62	
70/74	1	20	7	58	2	35	59	7	50	32	89	61	3	66	31	100	61	0	41	11	53	0	6	6	60	
65/69	3	38	17	55	8	58	57	19	61	50	130	58	16	70	61	147	59	6	62	30	98	58	0	26	2	28
60/64	12	51	35	53	34	60	55	70	36	72	178	56	85	37	95	217	57	37	69	79	185	56	12	54	25	91
55/59	43	60	56	51	100	30	53	104	9	40	153	54	108	7	36	151	54	90	34	76	200	53	39	78	64	181
50/54	83	34	68	48	67	6	49	22	0	2	24	50	31	0	5	36	51	74	4	34	200	50	79	62	85	226
45/49	59	4	31	44	8	0	46	2	0	0	2	46	3	0	0	3	47	25	0	6	112	50	71	17	53	141
40/44	23	0	6	40	0	0	42	0	0	0	0	40	0	0	0	0	0	7	0	0	31	46	36	4	17	57
35/39	2	0	0	36	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	7	42	9	0	1	41
30/34	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	37
25/29	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	1	0	0	33
20/24	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
15/19	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
10/14	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
5/9	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Table F Mean Wind Climate Airport Exposure for the Structural Design

Site localities and U. S. W. B. Station Location	Ref. (14)	Ref. (14)	Ref. (11)	Ref. (14, 9)		Ref. (9)	
	Station Elevation Above MSL (ft)	Observed Fastest Mile Wind Speed (mph)	Annual Extreme Mile Speed 50-year Mean Recurrence Interval (mph)	Mean Wind Speed and Direction (mph)		Average Annual Number of Storms with Winds of 47 mph or over	
				January	July	Annual	
Sacramento, Calif. Municipal AP	17	70	65	8.3 SE	9.4 SSW	9.3 SSE	5
Wilmington, Del. New Castle County AP	78	58	75	9.7 WNW	7.6 S	8.8 NW	2
Macon, Georgia Cochran Field	354	70	80	8.5 NW	7.2 WSW	8.9 WNW	1
Indianapolis, Ind. Weir Cook AP	792	90	90	11.3 NW	7.4 SW	10.8 SW	5
Kalamazoo, Mich. Grand Rapids, Mich. Kent County AP	784	58	75	11.5 W	8.3 W	9.8 W	4
St. Louis, Mo. Lambert Field	535	60	70	10.1 NW	7.6 S	9.3 S	2
Jersey City, N. J. Newark, N. J. Newark AP	7	82	75	11.3 WNW	8.9 SW	9.8 SW	1
Memphis, Tenn. Municipal AP	258	56	70	10.7 S	7.7 S	9.4 S	1
Houston, Texas International AP	50	54	80	11.9 SSE	8.8 SSE	11.8 SSE	5
Seattle, Wash. Seattle-Tacoma AP	400	55	80	10.4 SSW	8.7 SW	10.7 SW	1

Table G Air Contamination Data

Air Pollution Sampling Sites	Suspended Particulates (Micrograms per cubic meter)				Sulfur Dioxide (Micrograms per cubic meter)				Nitrogen Dioxide (Micrograms per cubic meter)				Ammonia (Micrograms per cubic meter)			
	Geo- metric Mean	Maxi- mum	90% Freq. Dist.	Years Covered	Geo- metric Mean	Maxi- mum	90% Freq. Dist.	Years Covered	Geo- metric Mean	Maxi- mum	90% Freq. Dist.	Years Covered	Geo- metric Mean	Maxi- mum	90% Freq. Dist.	Years Covered
Sacramento, California Health Center 2221 Stockton Boulevard Sacramento County Health Dept.	68	403	132	1958- 1966	58	492	168	1964- 1968	133	384	276	1964- 1968	46	79	71	1968
Wilmington, Delaware Public Building 1000 King Street City Dept. of Health	144	743	262	1957- 1968	34	249	115	1964- 1968	105	405	190	1964- 1968	48	113	65	1968
Macon, Georgia W. T. Grant Co. 418 3rd Street Georgia Dept. of Public Health	96	861	235	1958- 1968	79	258	151	1957- 1962	142	658	236	1957- 1967	126	336	201	1959- 1968
Indianapolis, Indiana Fire Station No. 301 East New York Street City Bureau of Air Pollution	147	367	237	1958- 1968	142	658	236	1957- 1967	126	336	201	1959- 1968	94	281	149	1958- 1968
Kalamazoo, Michigan 241 West South Street City County Health Dept.	79	258	151	1957- 1962	94	281	149	1958- 1968	70	294	169	1964- 1968	136	405	263	1964- 1968
St. Louis, Missouri P. O. Bldg. - 18th & Market St. Div. Air Pollution Cont. City Dept. Public Safety	142	658	236	1957- 1967	70	294	169	1964- 1968	136	405	263	1964- 1968	50	82	70	1968
Jersey City, New Jersey Medical Center Garage Bldg. Cornellison Ave. City Board of Health	126	336	201	1959- 1968	34	323	221	1967- 1968	217	473	429	1967	157	404	238	1968
Memphis, Tennessee Health Dept. Bldg. 814 Jefferson Street Memphis-Shelby Co. Health Dept.	94	281	149	1958- 1968	9	23	18	1968	157	404	238	1968	57	96	87	1968
Houston, Texas Sam Houston Coliseum 810 Bagby Street City Health Dept.	97	385	168	1957- 1968	22	122	58	1964- 1968	89	315	199	1964- 1968	48	74	61	1968
Seattle, Washington Public Safety Bldg. 604 Third Ave. Puget Sound Air Pollution Control Agency	70	446	127	1957- 1968	22	122	58	1964- 1968	89	315	199	1964- 1968	48	74	61	1968

Appendix

City Maps for the
Breakthrough Sites



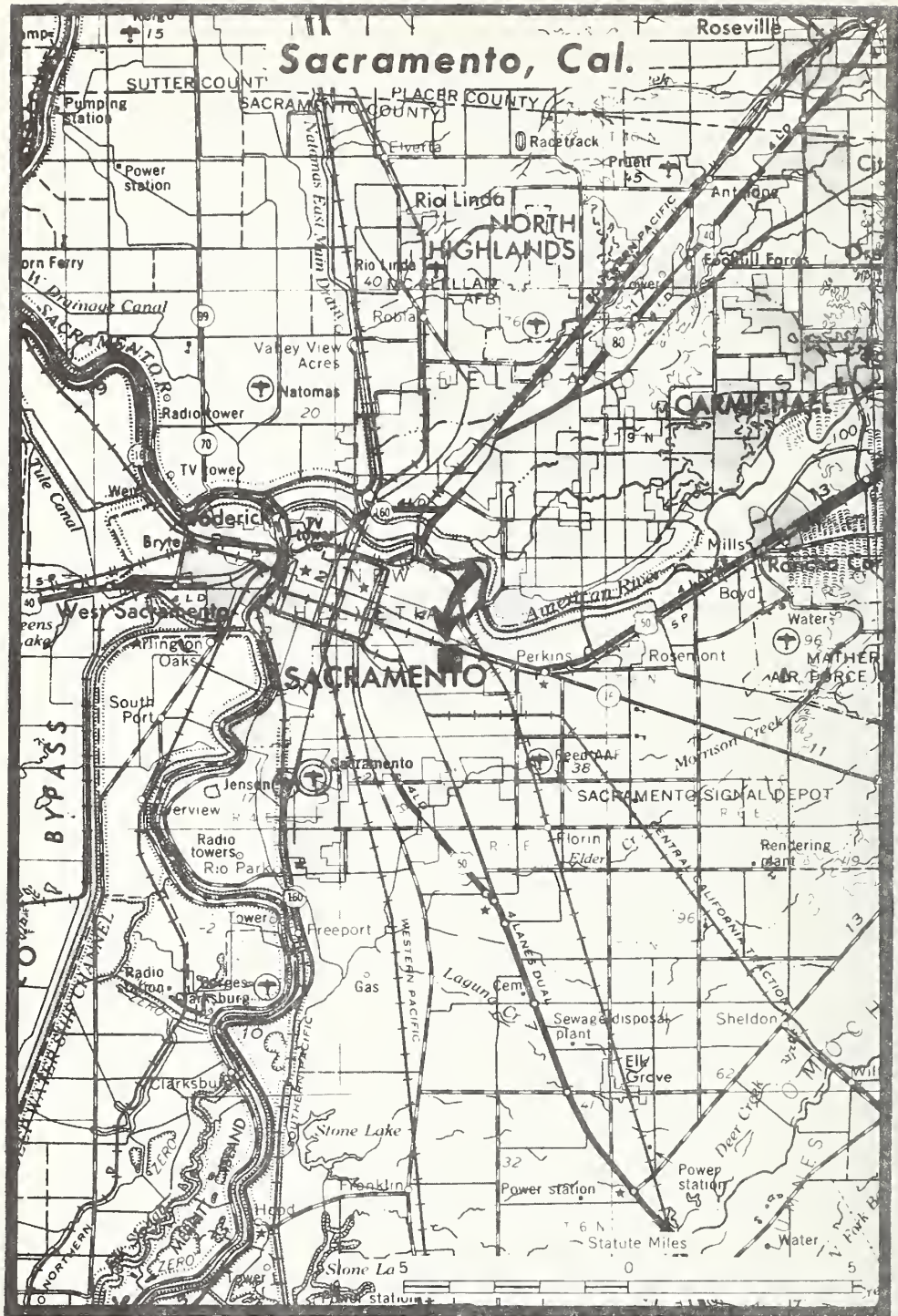
■ Breakthrough Site



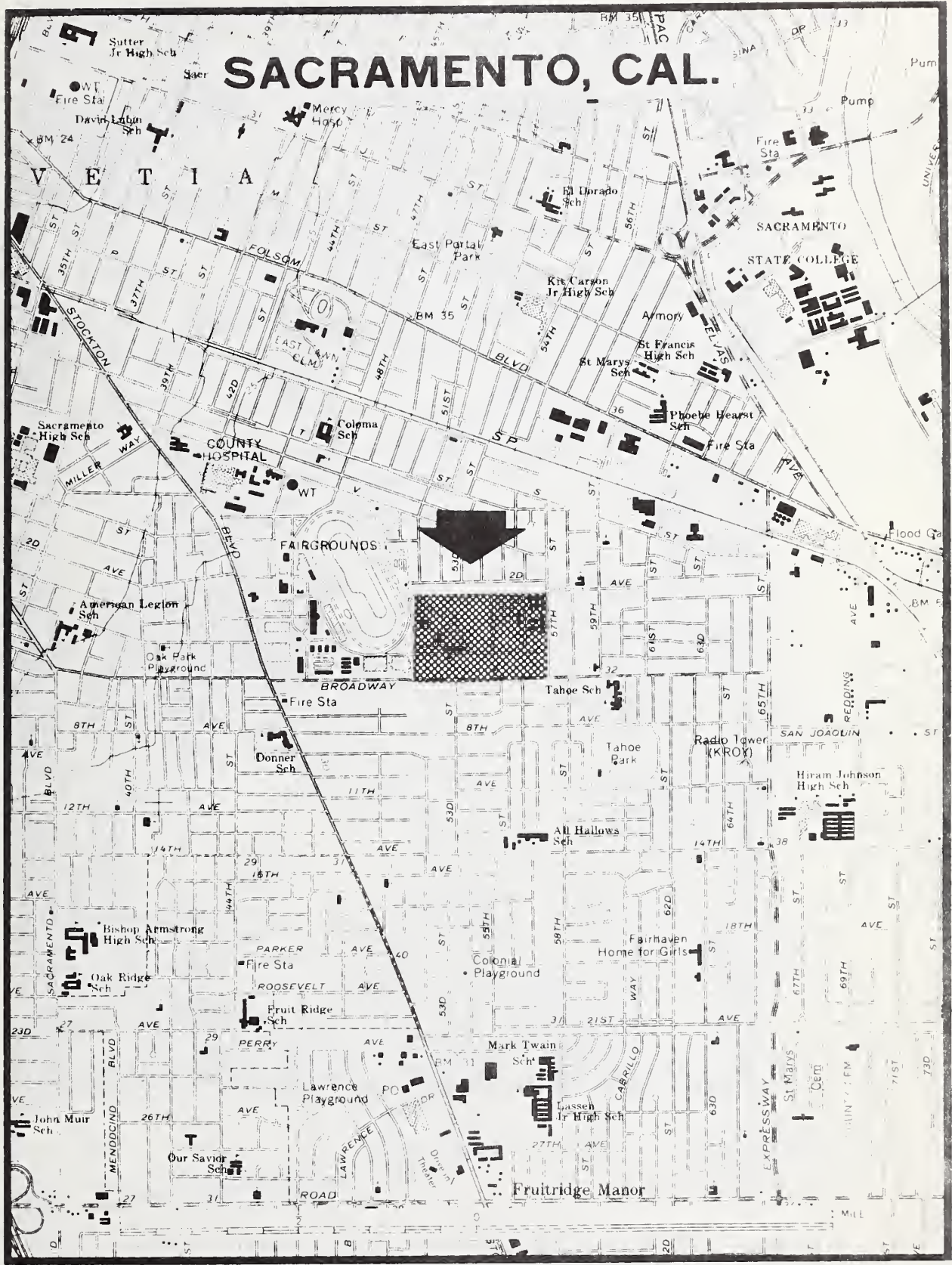
⊕ Airport



○ Weather Data Station

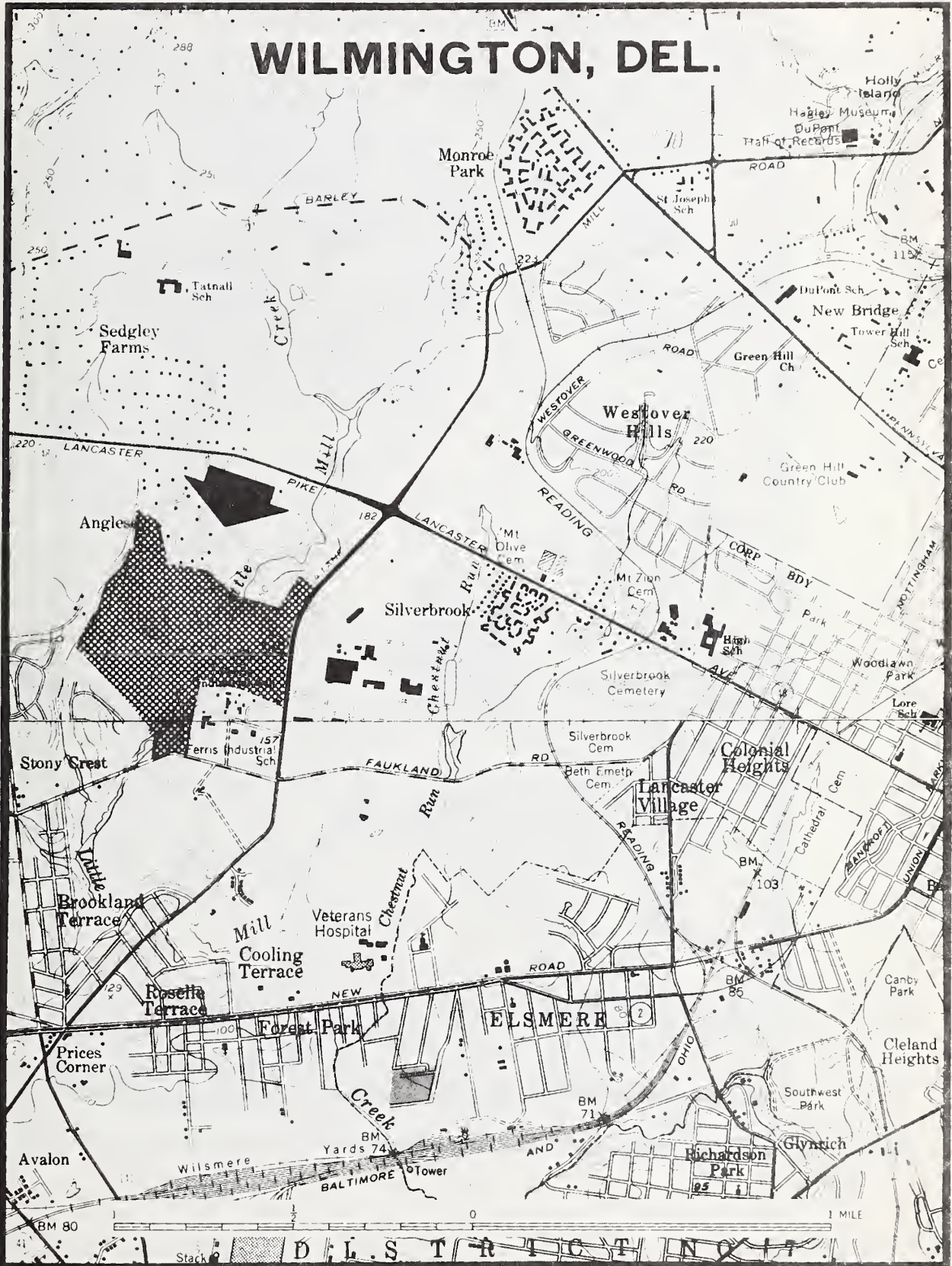


SACRAMENTO, CAL.

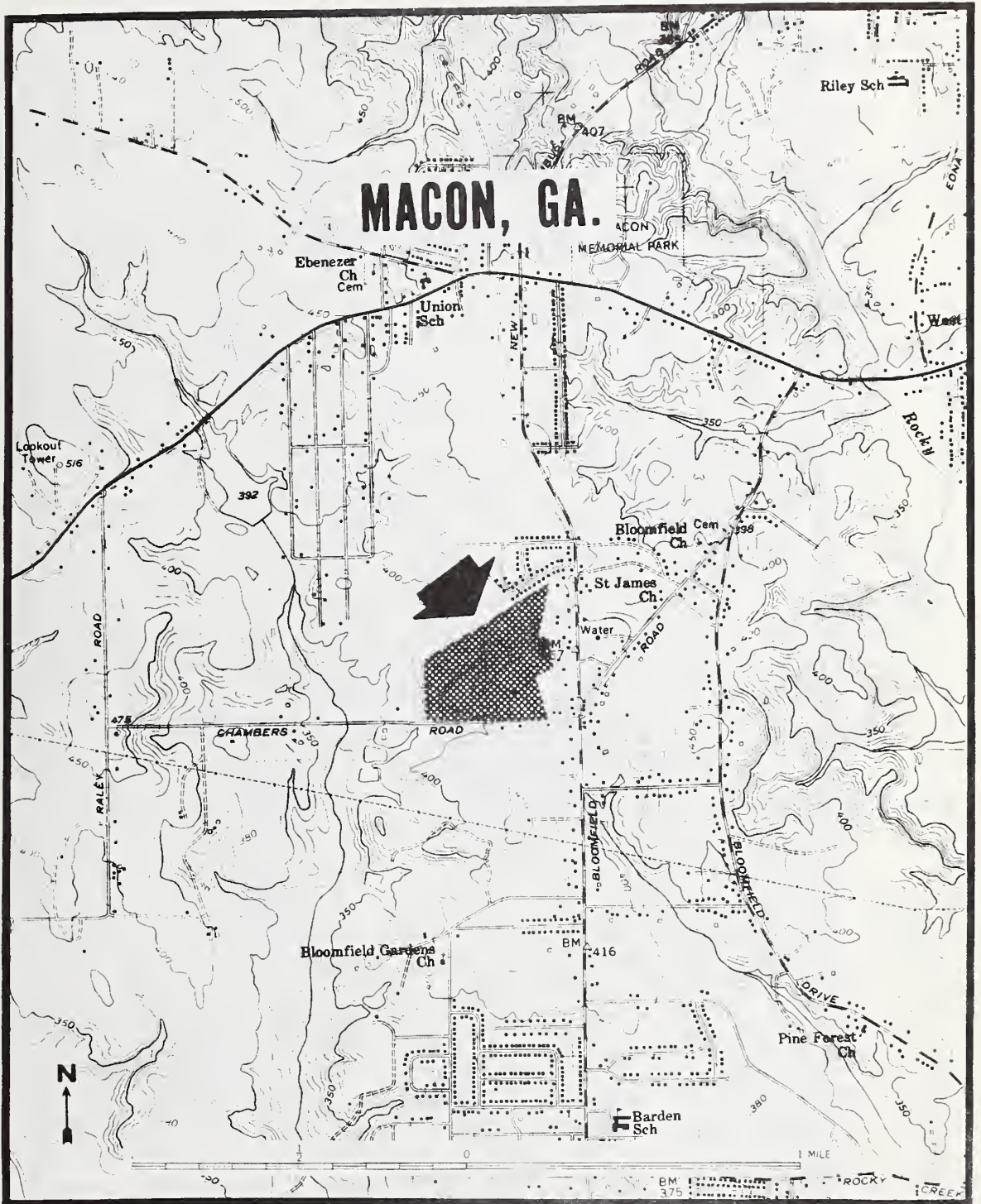


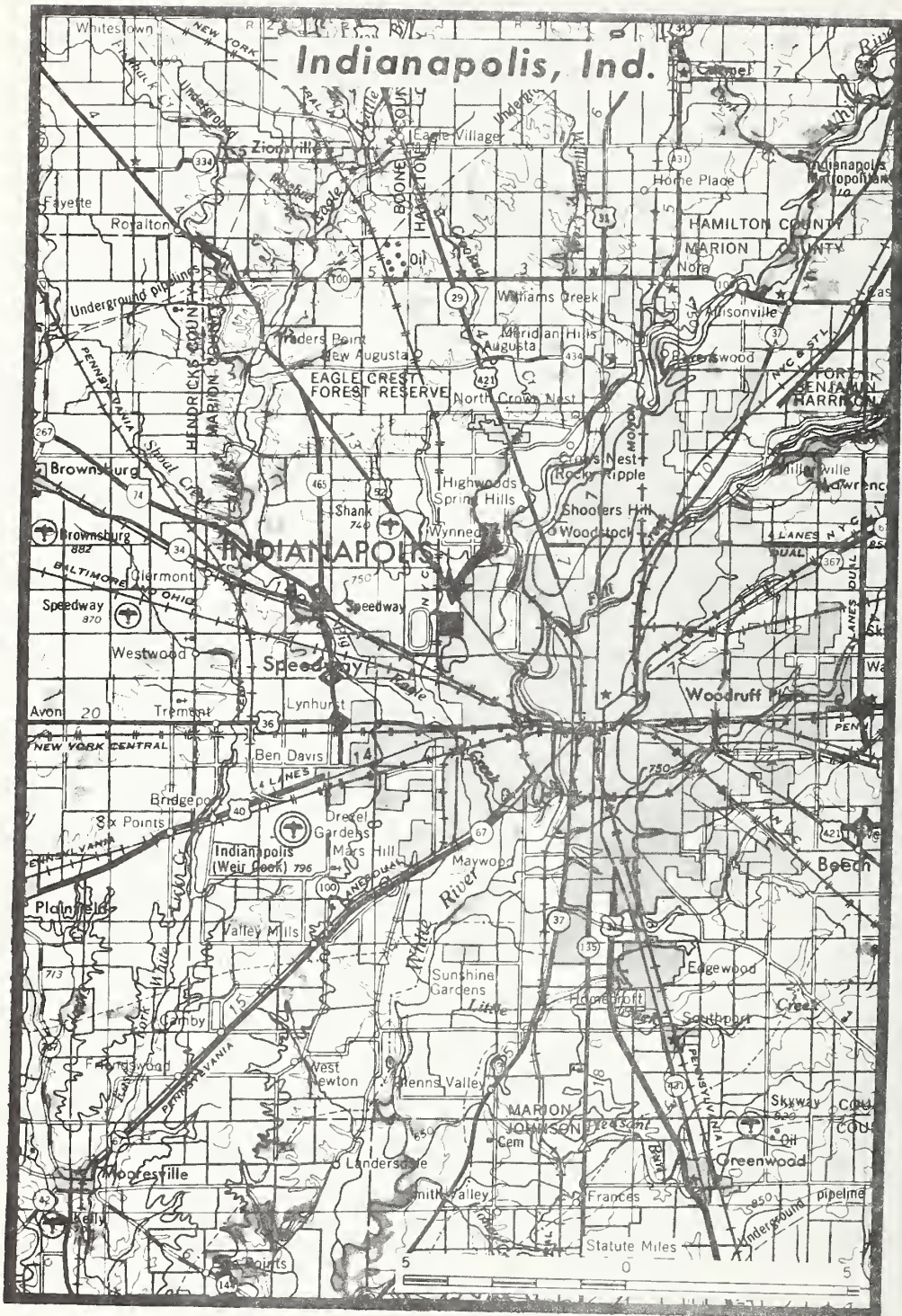


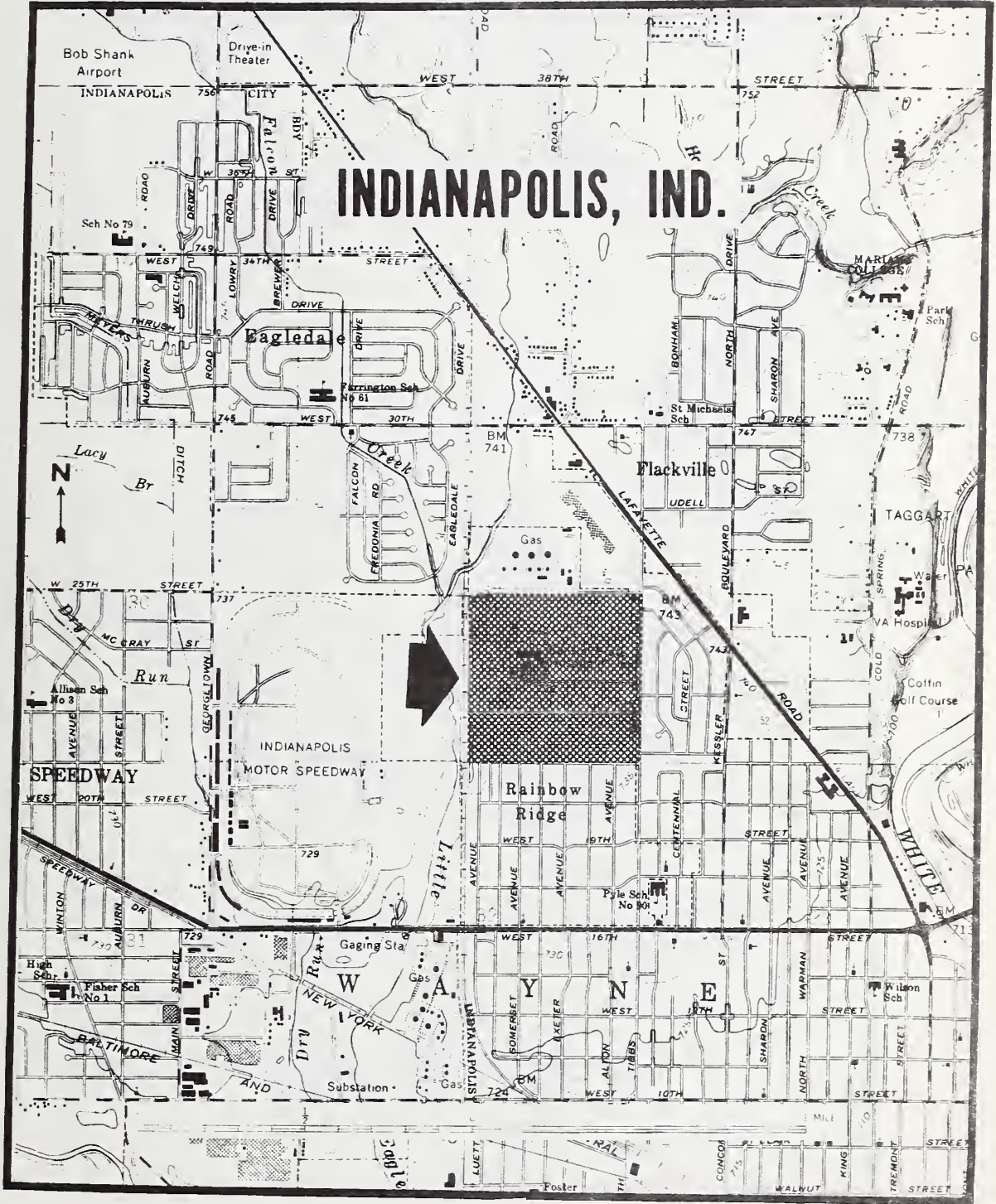
WILMINGTON, DEL.



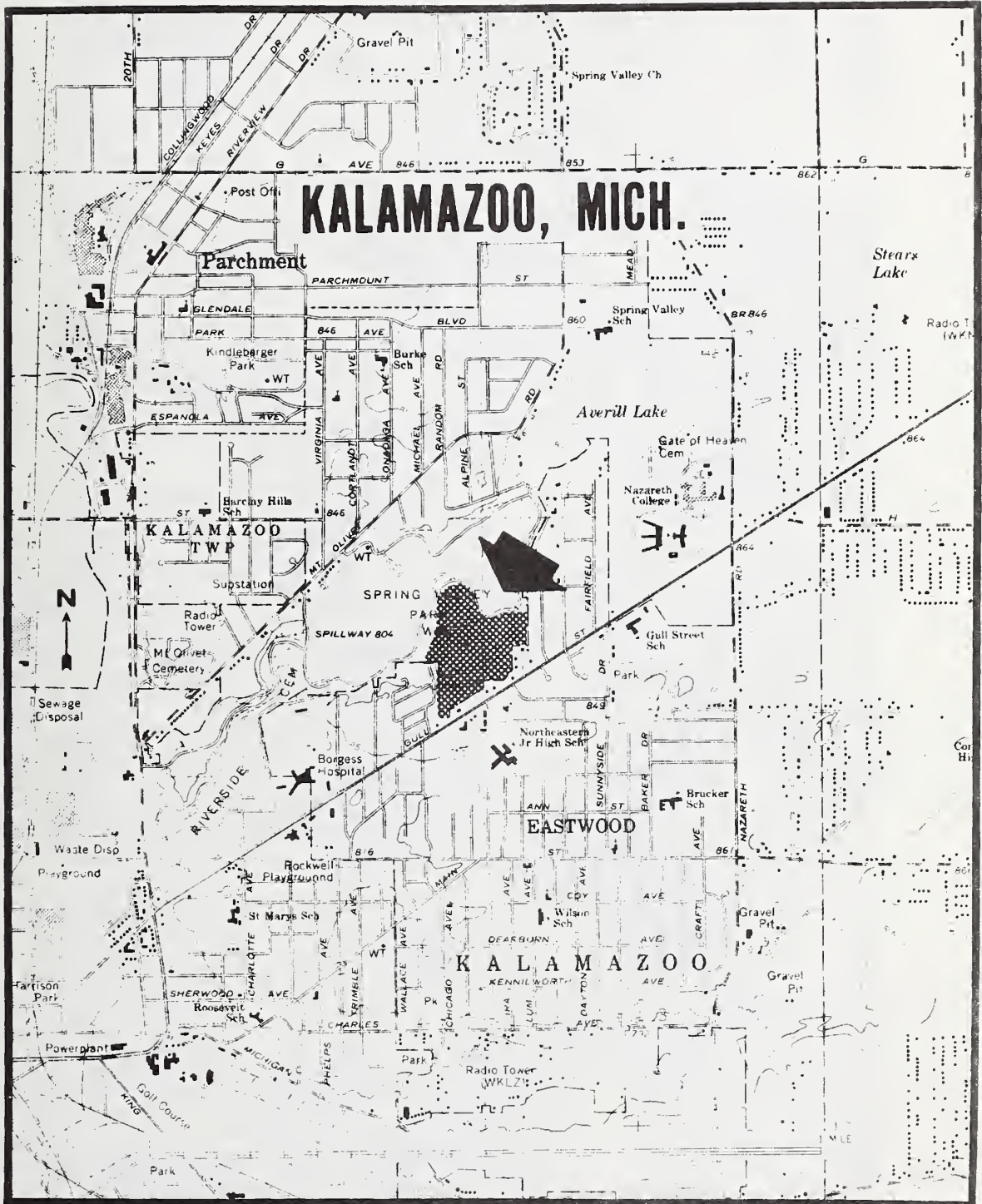


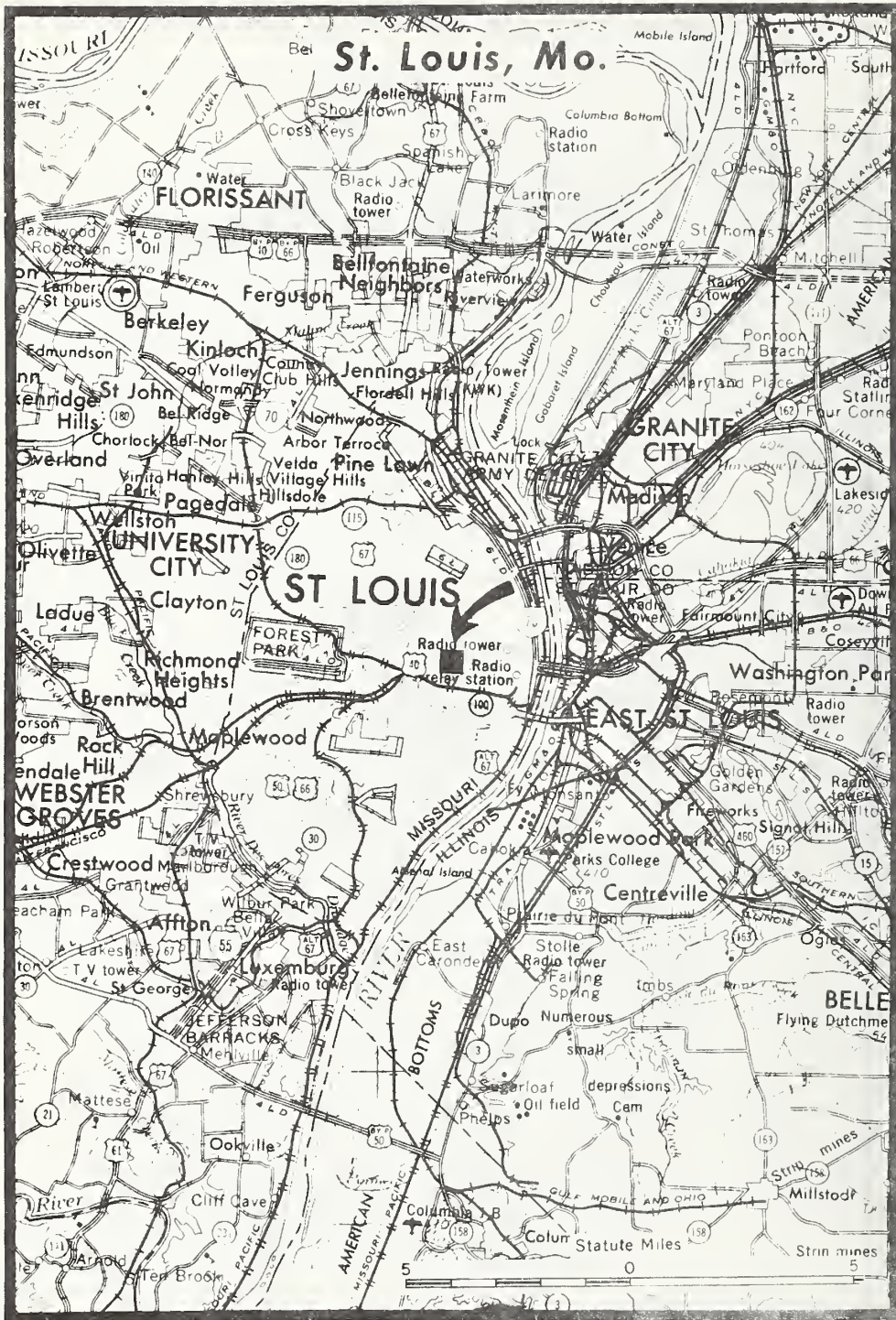












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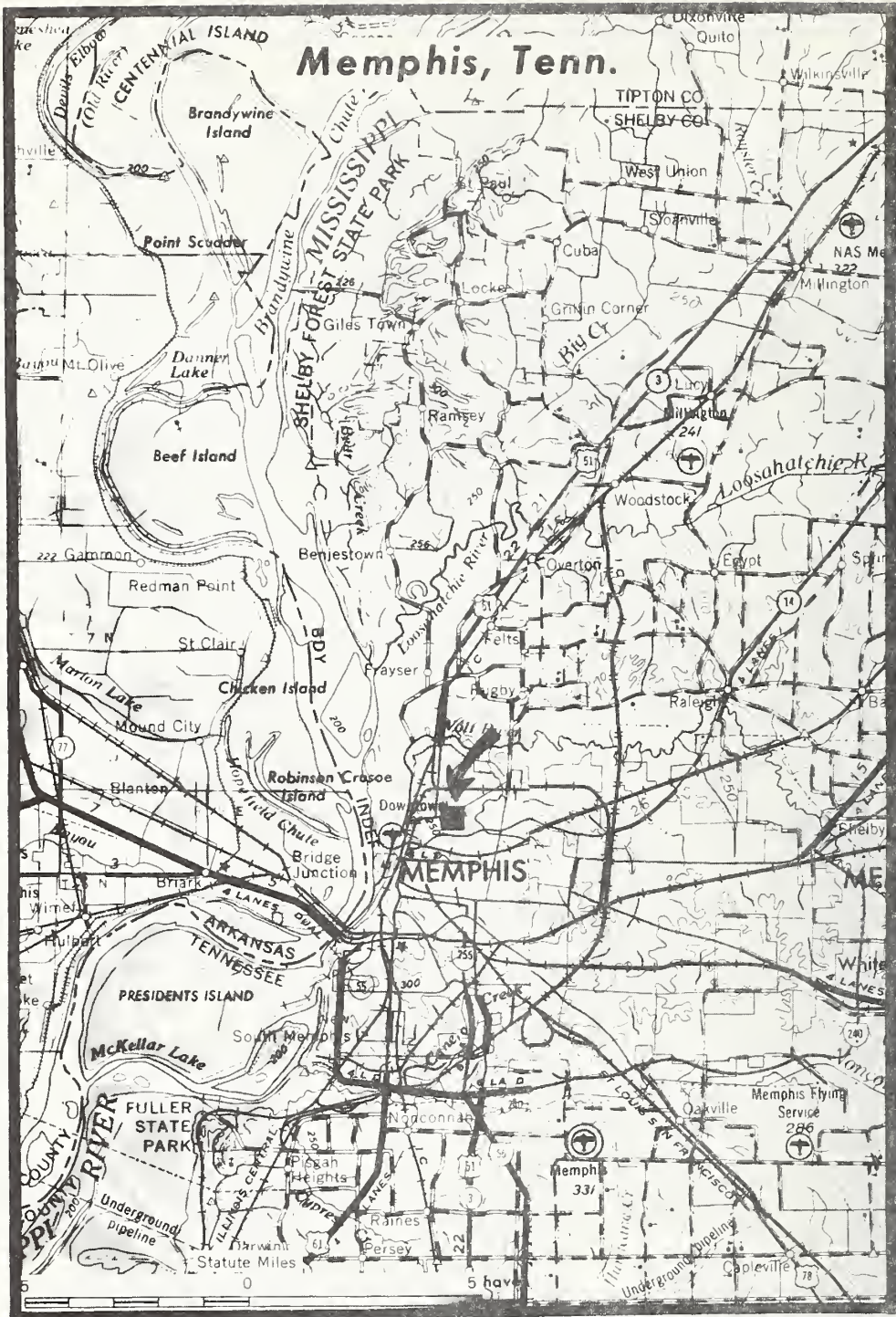
ST. LOUIS, MO.





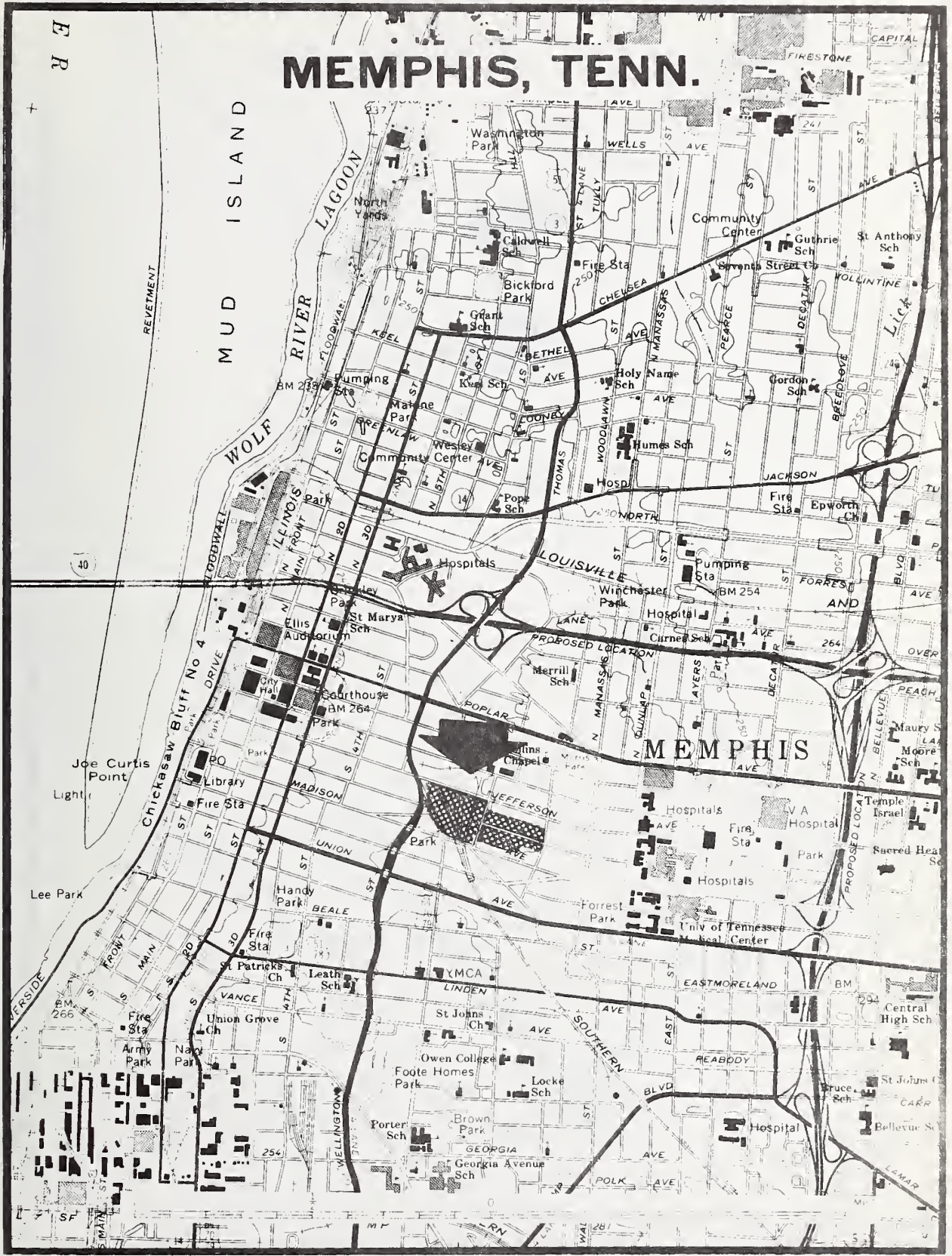
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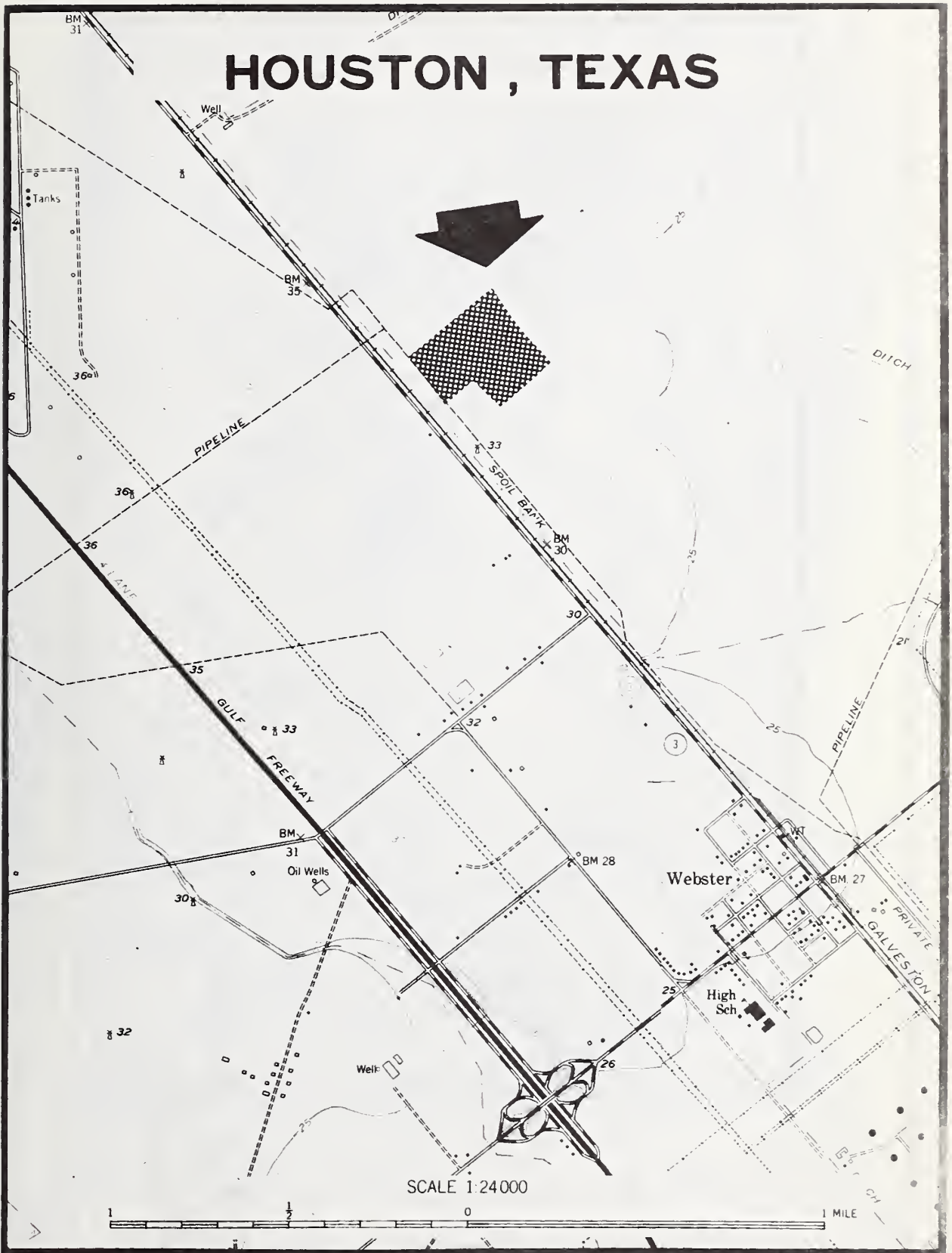


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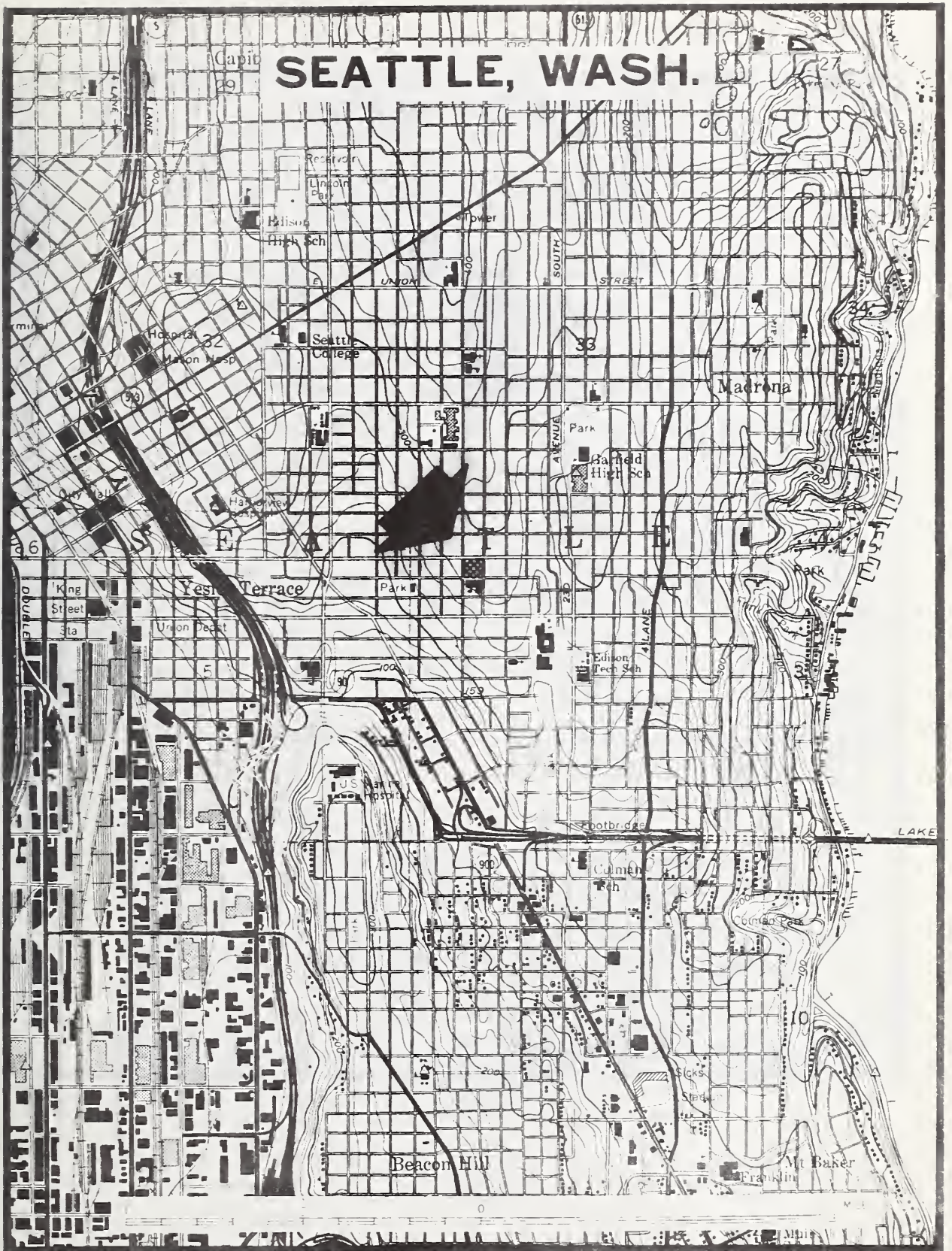
MEMPHIS, TENN.

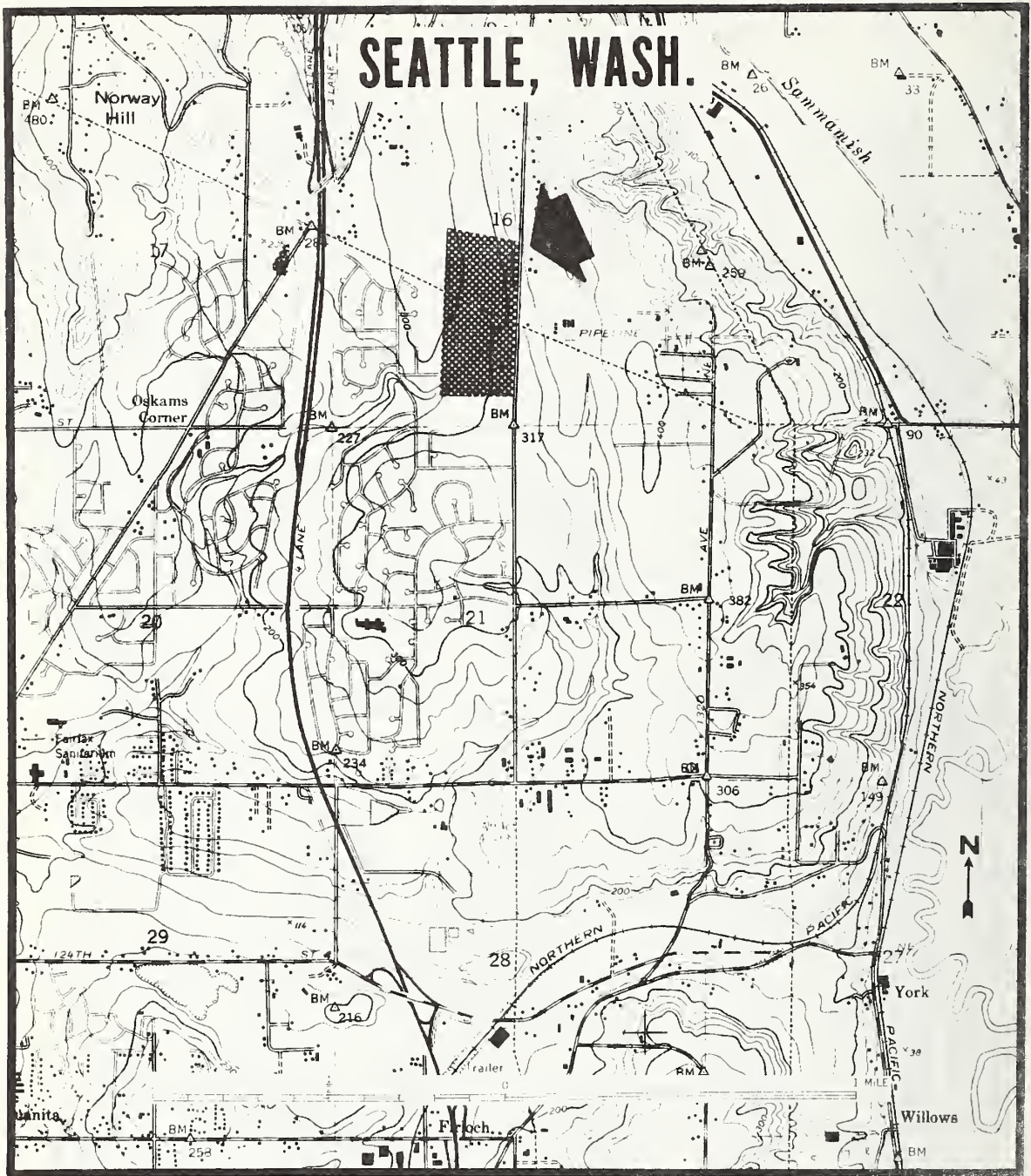


HOUSTON, TEXAS









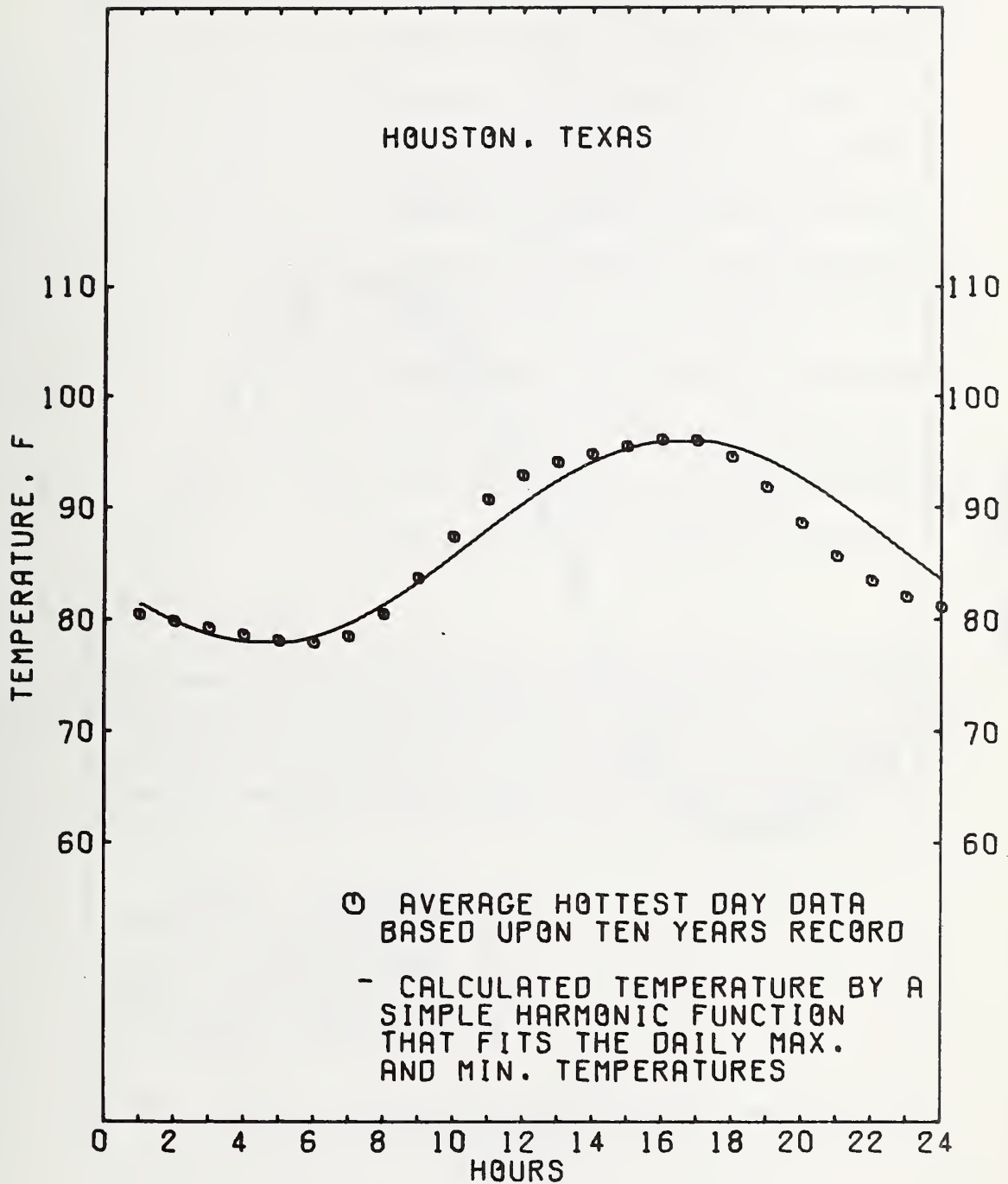


Figure 1

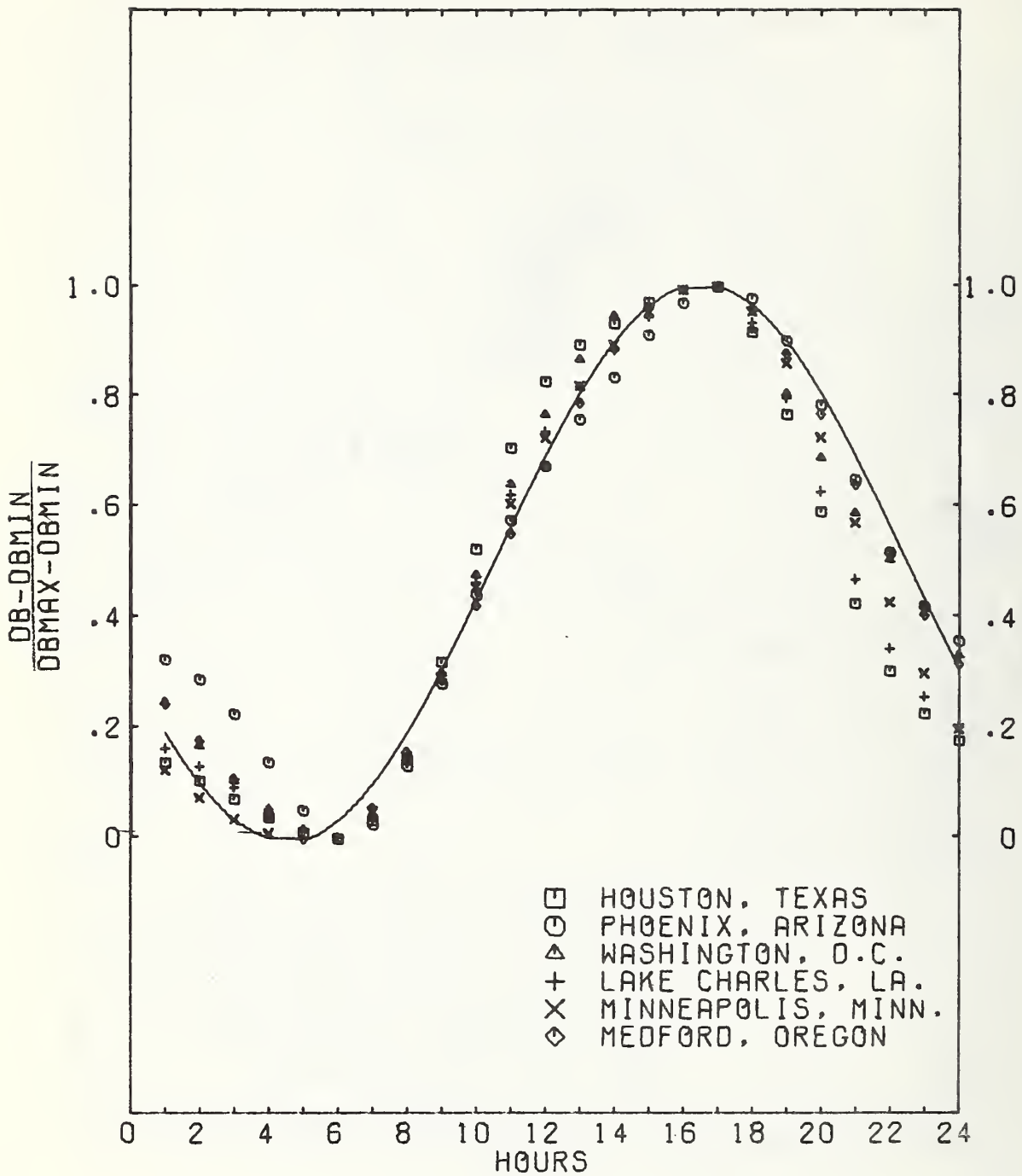


Figure 2

Figures 3 through 22 - Coincident annual frequency profiles for the hourly dry-bulb temperature and wind speed, and those for this relative humidity and wind speed. The height of the profile represents relative frequency of the coincident occurrences^{*/} based upon ten year average. All ten localities show the highest frequency profile at the wind speed in the vicinity of 5 mph. But the coincident dry-bulb temperature and relative humidity widely vary from locality to locality.

^{*/}The approximate value of frequency for these three dimensional profiles may be determined by noting in Figure 3 that it's peak represents 750 hourly observations while in Figure 4 that it is 2200 hourly observations. The scales for all the other profiles for temperature/wind speed and relative humidity/wind speed are consistent with Figures 3 and 4, respectively.

SACRAMENTO, CALIFORNIA

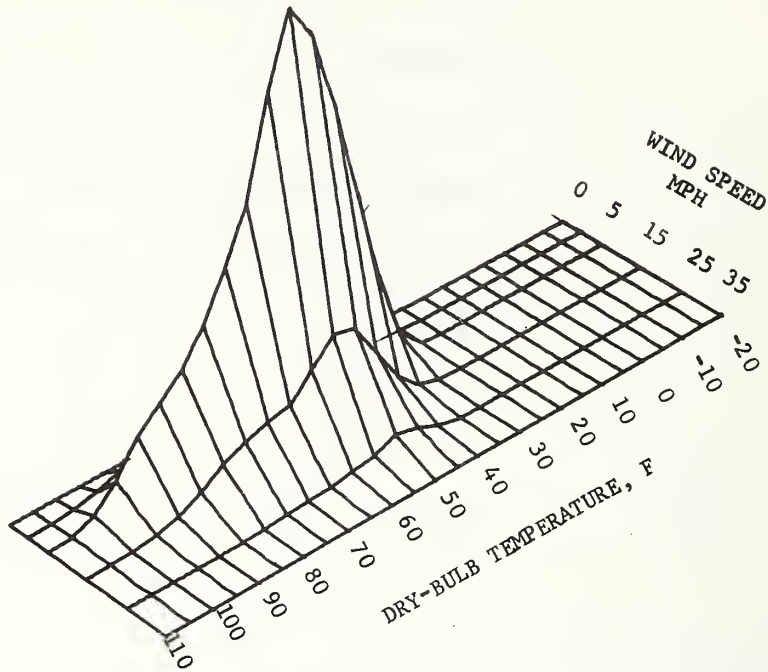


Fig. 3 COINCIDENT PROFILE FOR WIND SPEED AND DRY BULB TEMPERATURE

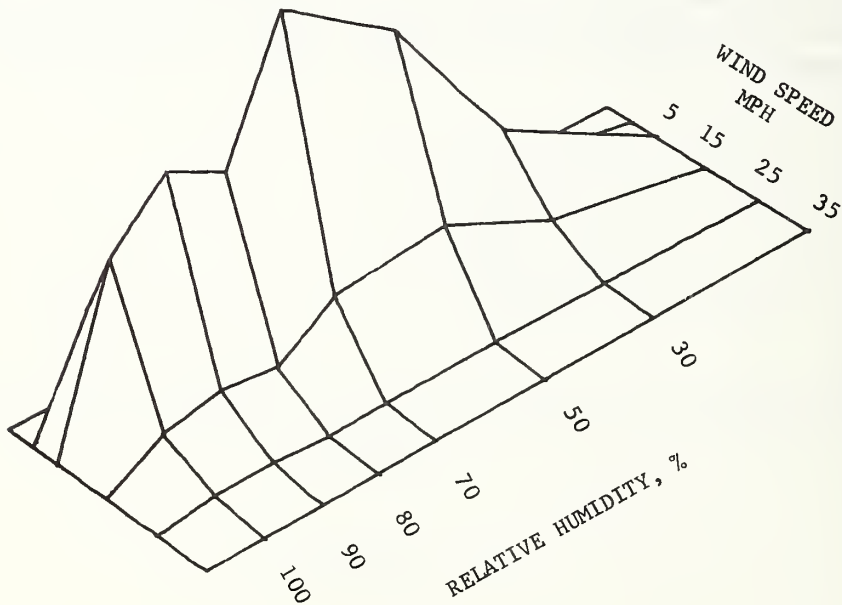


Fig. 4 COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY

WILMINGTON, DELAWARE

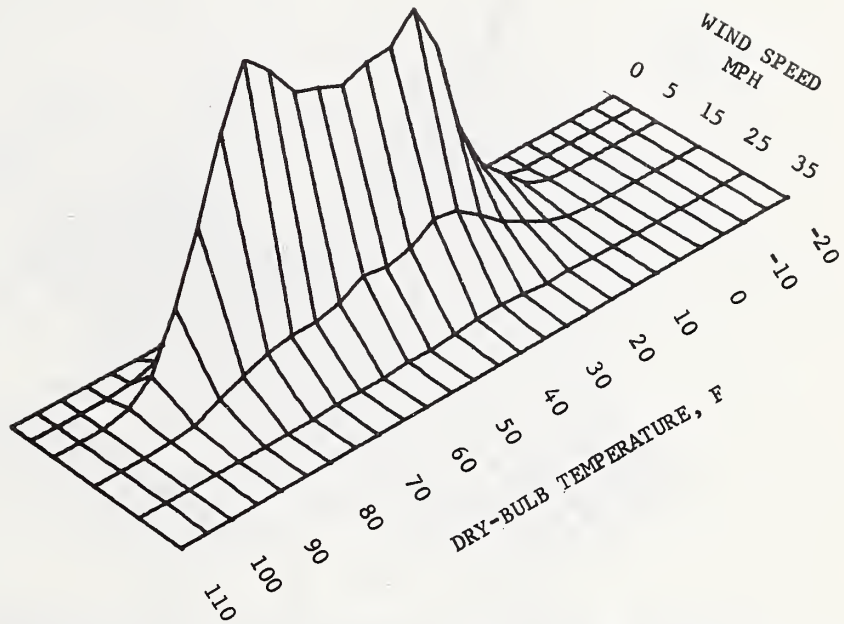


Fig. 5. COINCIDENT PROFILE FOR WIND SPEED AND DRY BULB TEMPERATURE

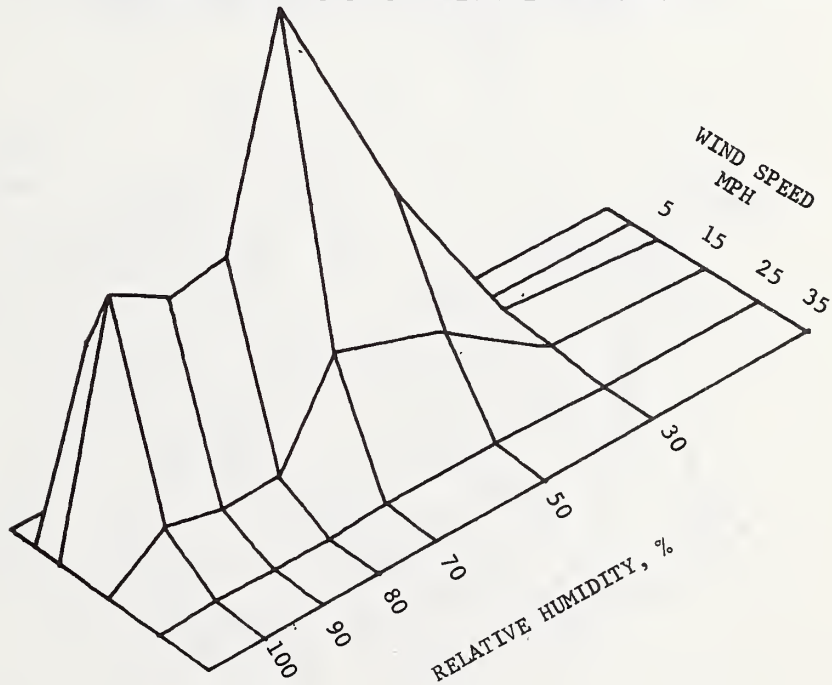


Fig. 6 COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY

MACON, GEORGIA

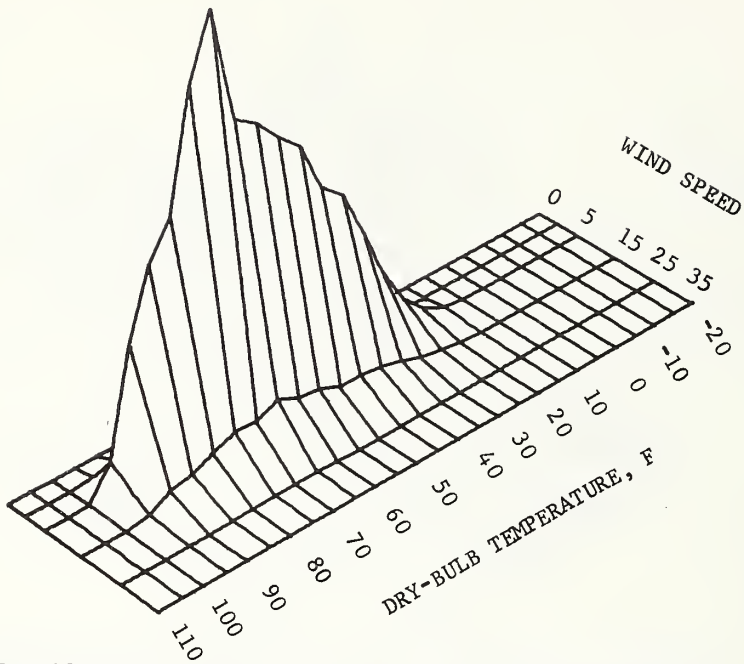


Fig. 7 COINCIDENT PROFILE FOR WIND SPEED AND DRY BULB TEMPERATURE

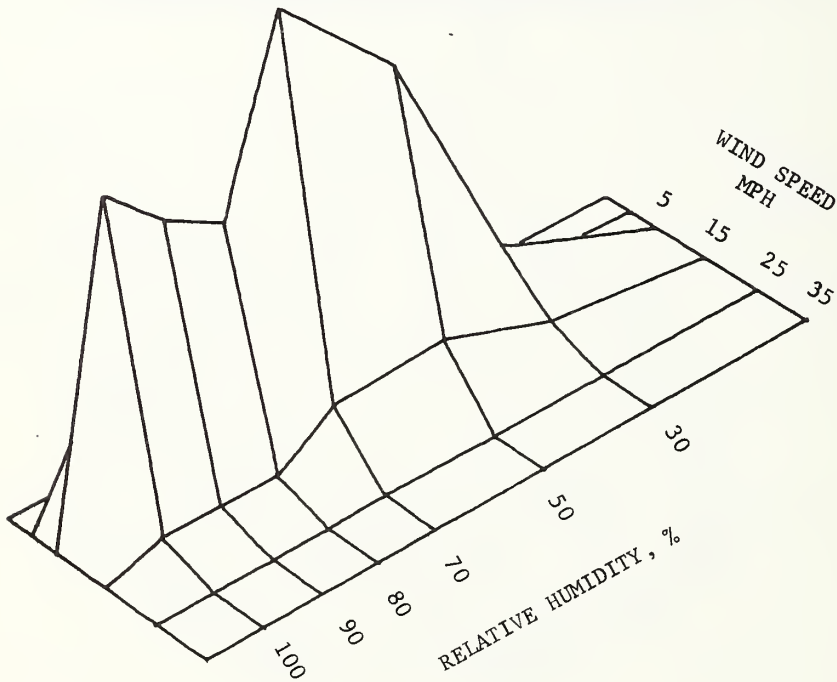


Fig. 8 COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY

INDIANAPOLIS, INDIANA

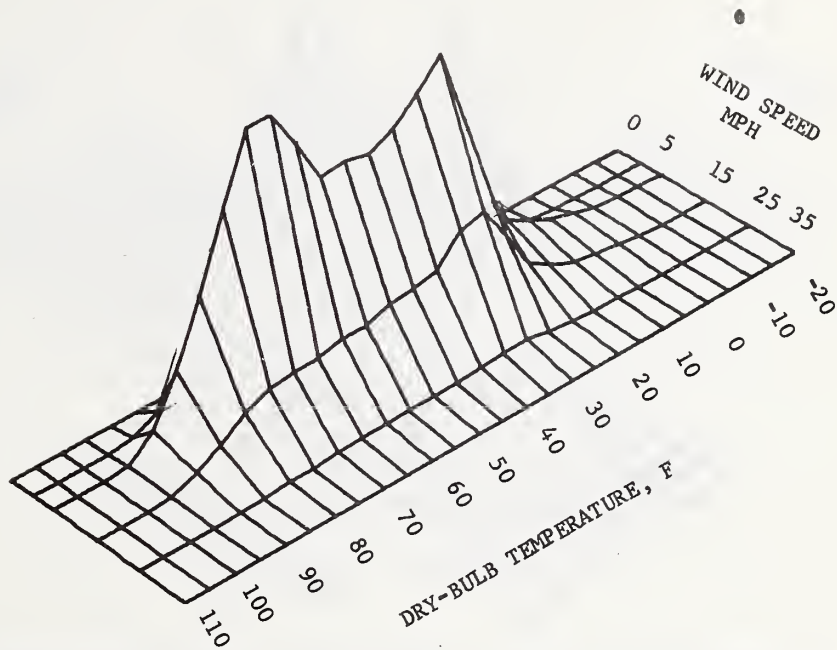


Fig. 9 COINCIDENT PROFILE FOR WIND SPEED AND DRY BULB TEMPERATURE

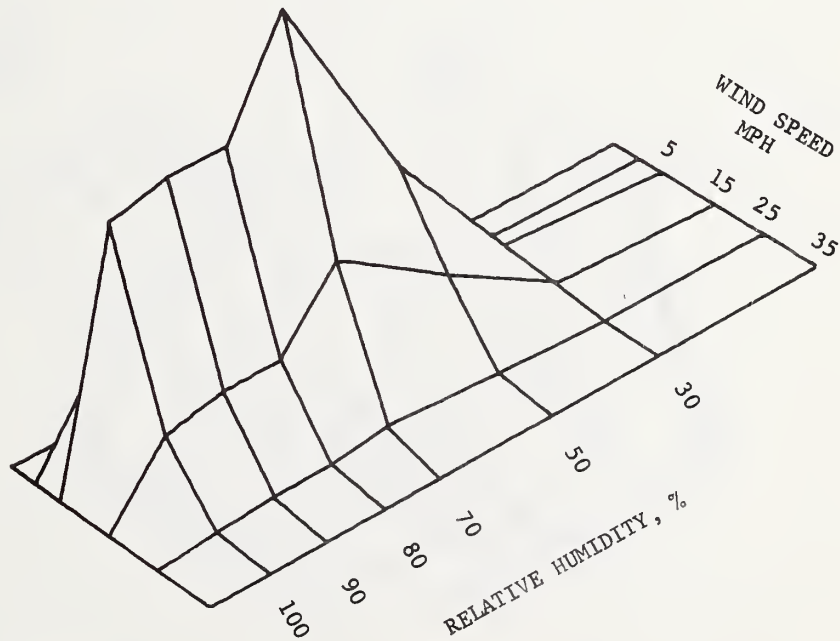


Fig. 10 COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY

GRAND RAPIDS, MICHIGAN

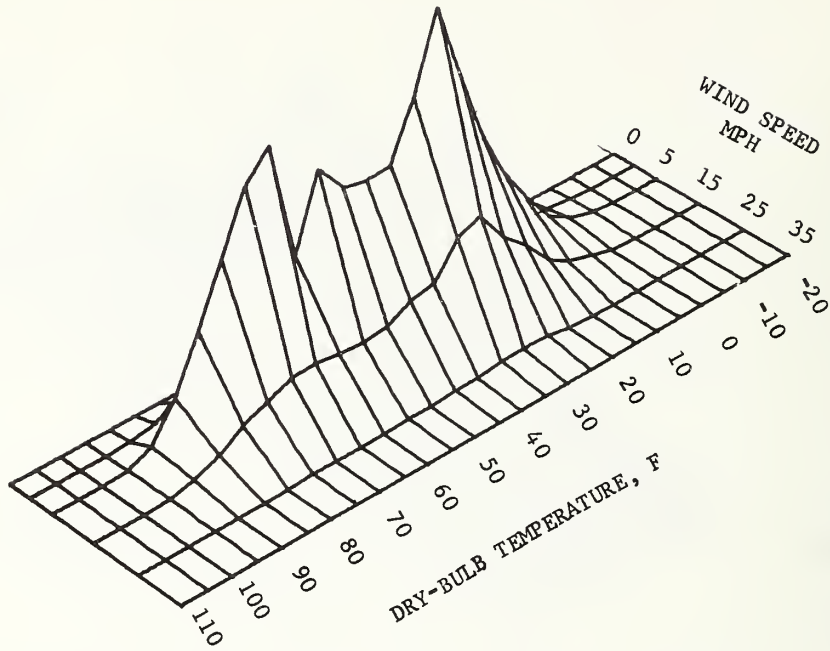


Fig. 11 COINCIDENT PROFILE FOR WIND SPEED AND DRY BULB TEMPERATURE

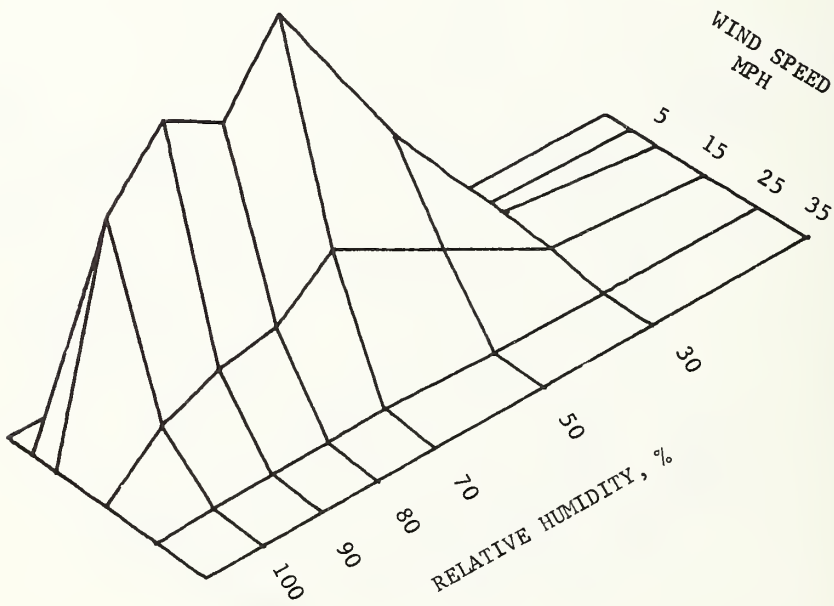


Fig. 12 COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY

NEWARK, NEW JERSEY

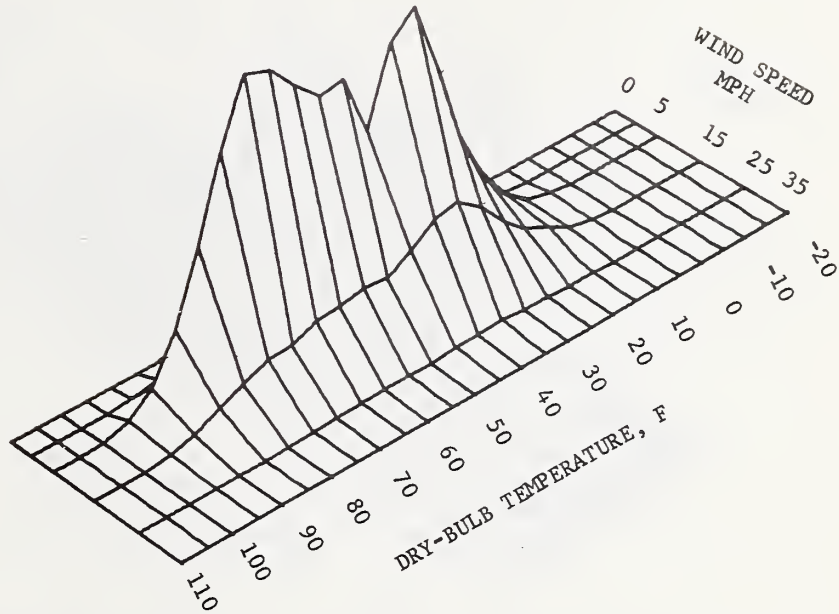


Fig. 13 COINCIDENT PROFILE FOR WIND SPEED AND DRY BULB TEMPERATURE

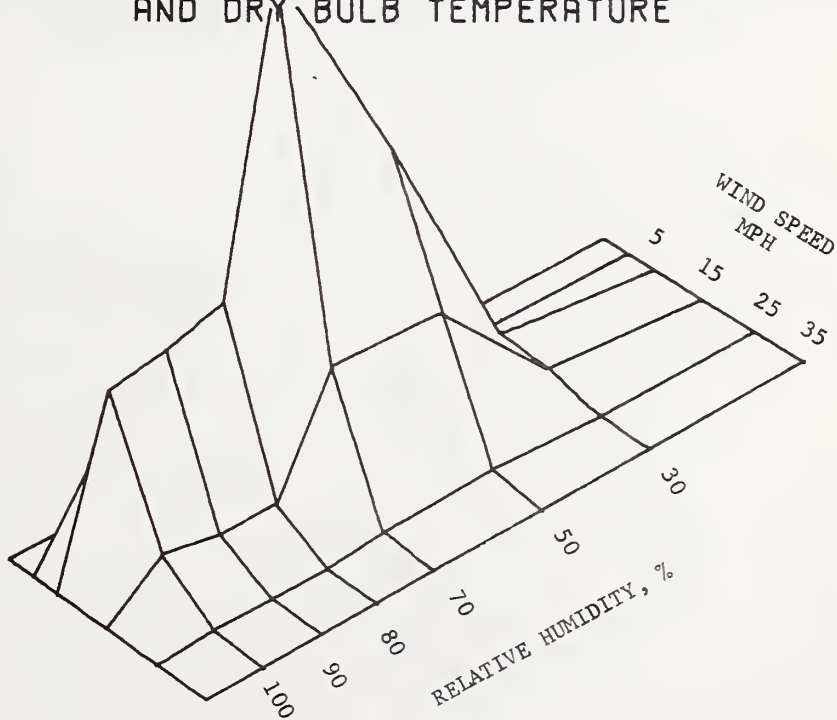


Fig. 14 COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY

ST. LOUIS, MISSOURI

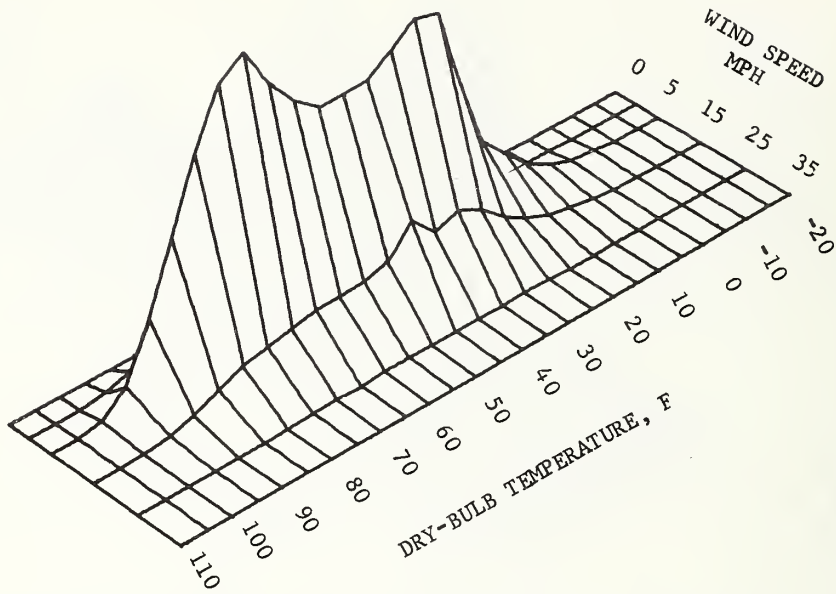


Fig. 15

COINCIDENT PROFILE FOR WIND SPEED AND DRY-BULB TEMPERATURE

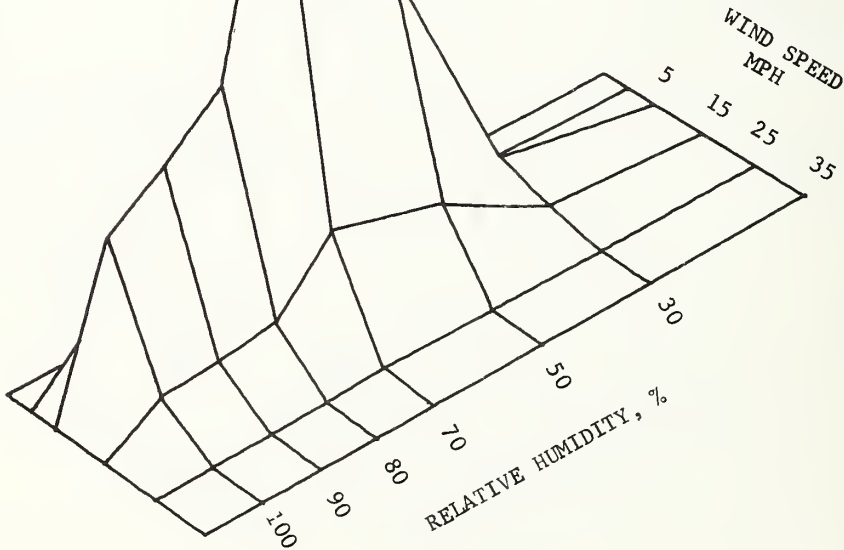


Fig. 16

COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY

MEMPHIS, TENNESSEE

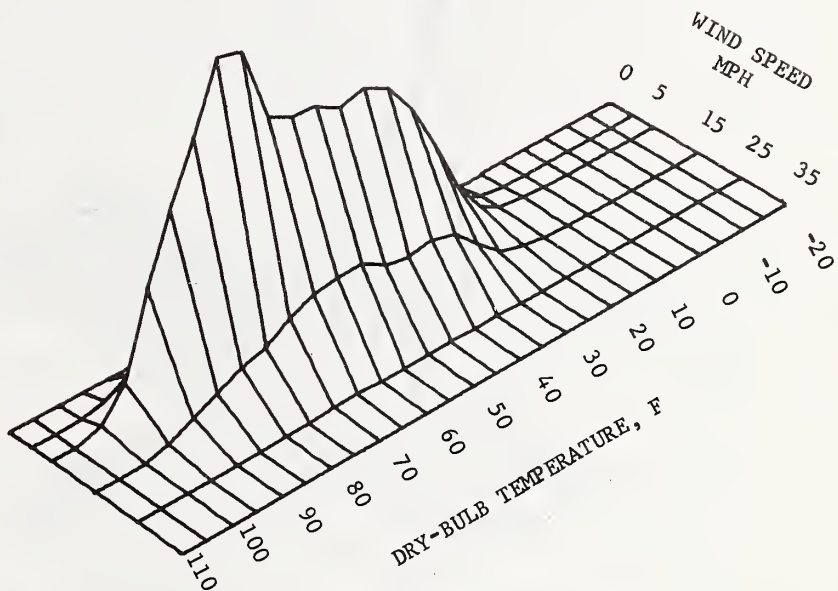


Fig. 17 COINCIDENT PROFILE FOR WIND SPEED AND DRY BULB TEMPERATURE

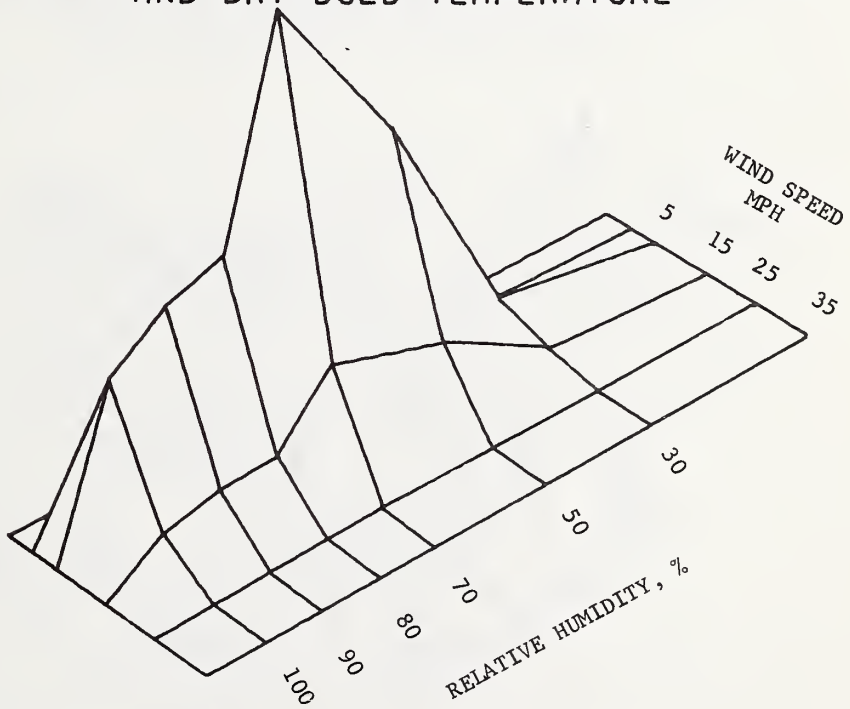


Fig. 18 COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY

HOUSTON, TEXAS

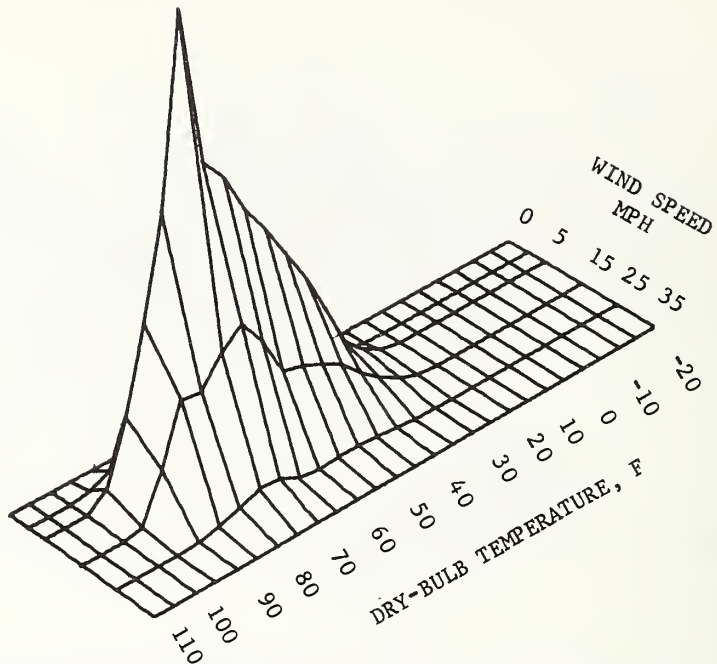


Fig. 19 COINCIDENT PROFILE FOR WIND SPEED AND DRY BULB TEMPERATURE

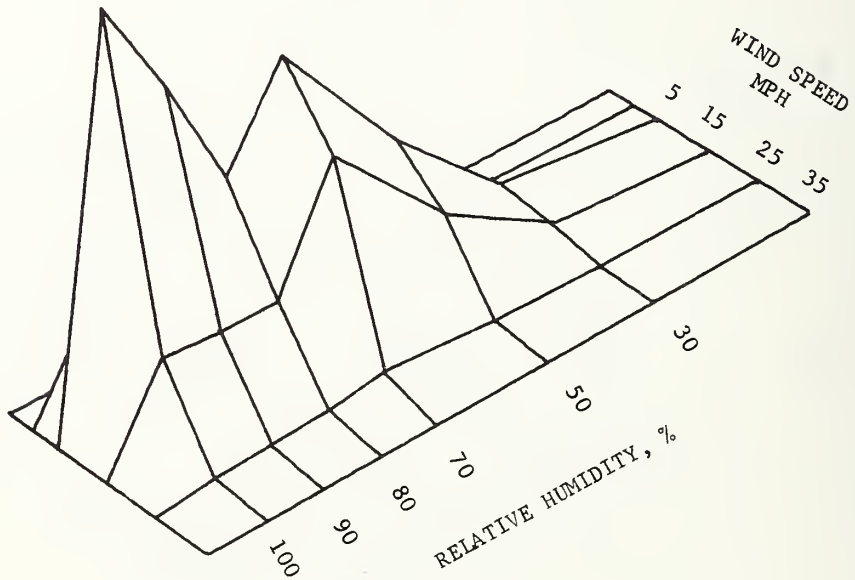


Fig. 20 COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY

SEATTLE, WASHINGTON

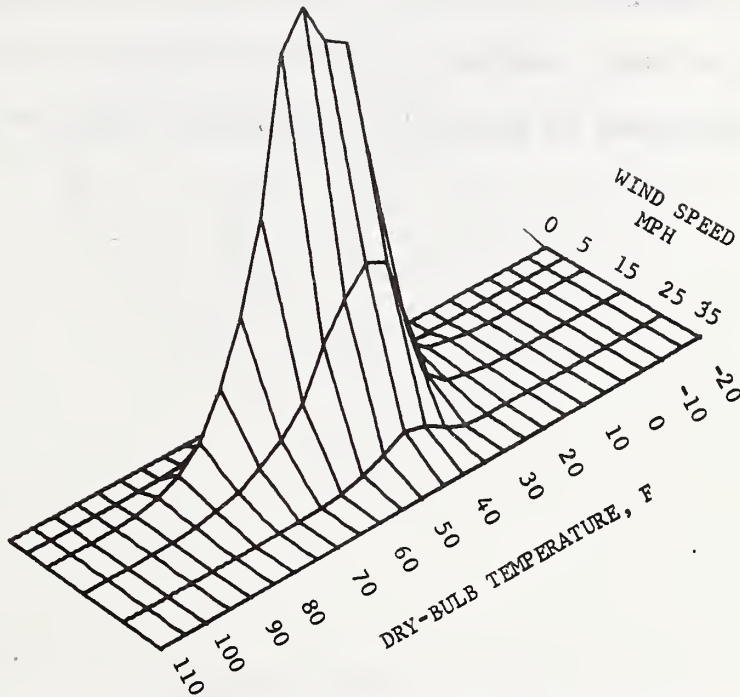


Fig. 21 COINCIDENT PROFILE FOR WIND SPEED AND DRY BULB TEMPERATURE

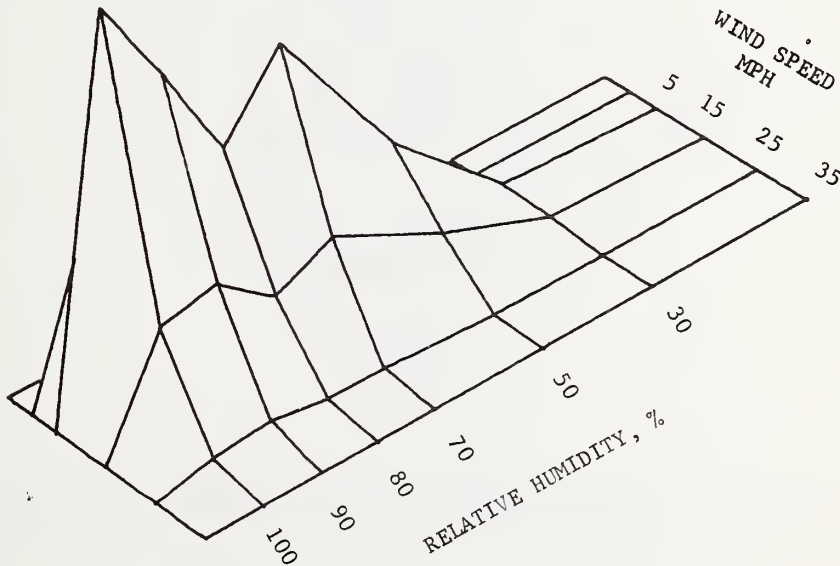
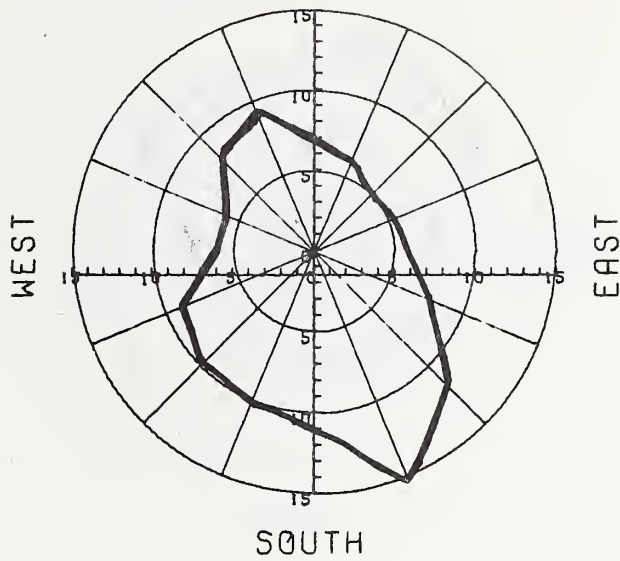


Fig. 22 COINCIDENT PROFILE FOR WIND SPEED AND RELATIVE HUMIDITY

Figures 23 through 32 present wind flow patterns by plotting the annual average wind speed in a polar form with respect to the direction of wind. Indicated on the polar diagram of the wind speed are the directions of prevailing wind during summer and winter seasons.

WINTER, NORTH



SUMMER NORTH

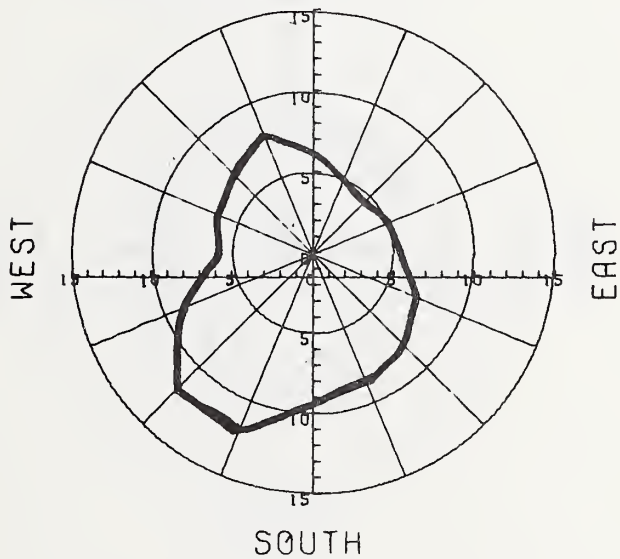
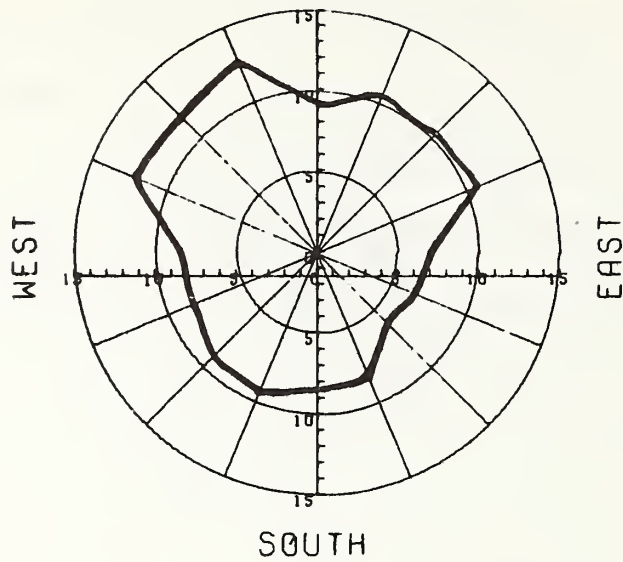


Fig. 23 SACRAMENTO, CALIFORNIA

WINTER NORTH



SUMMER NORTH

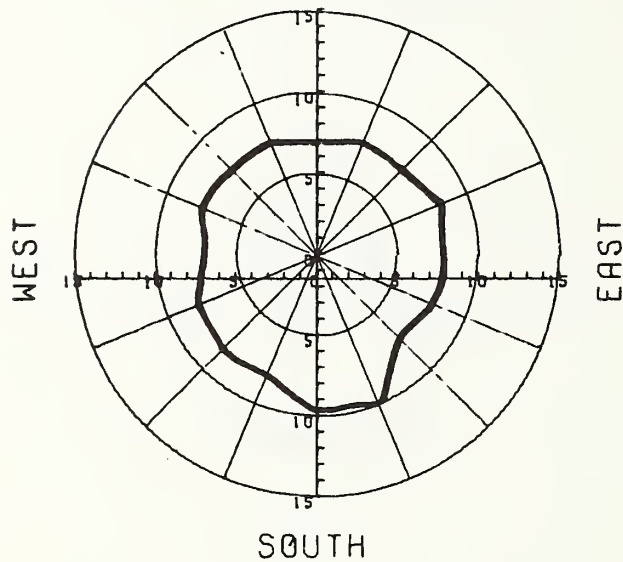
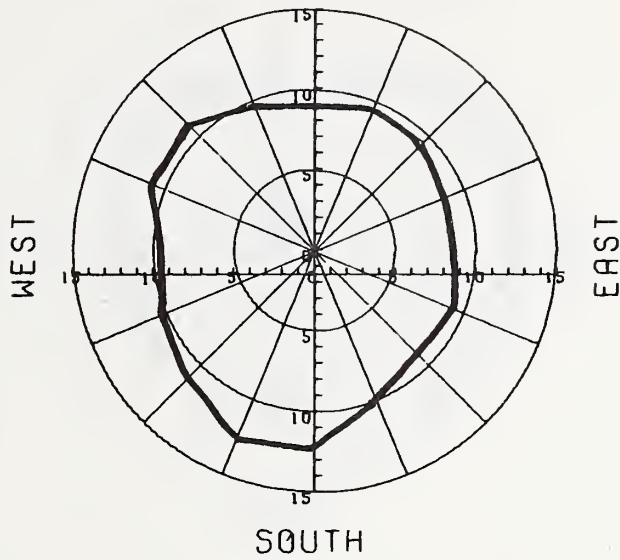


Fig. 24

WILMINGTON, DELAWARE

WINTER NORTH



SUMMER NORTH

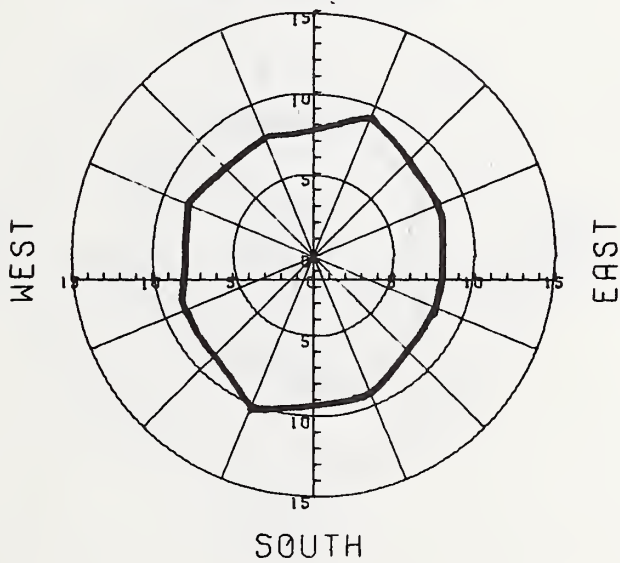
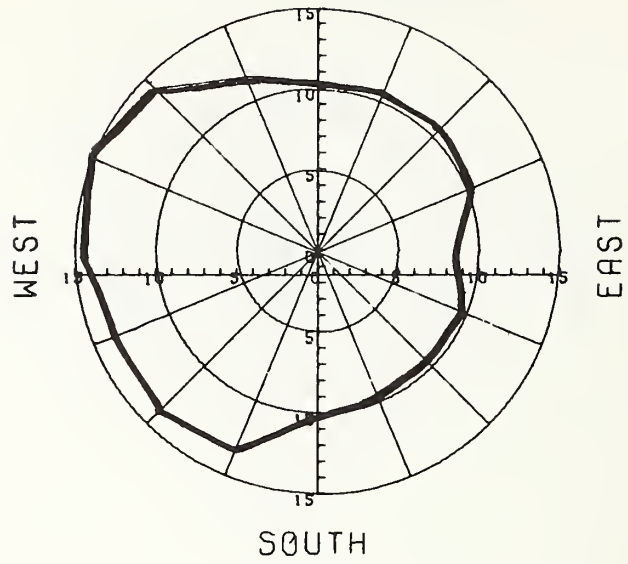


Fig. 25

MACON, GEORGIA

WINTER NORTH



SUMMER NORTH

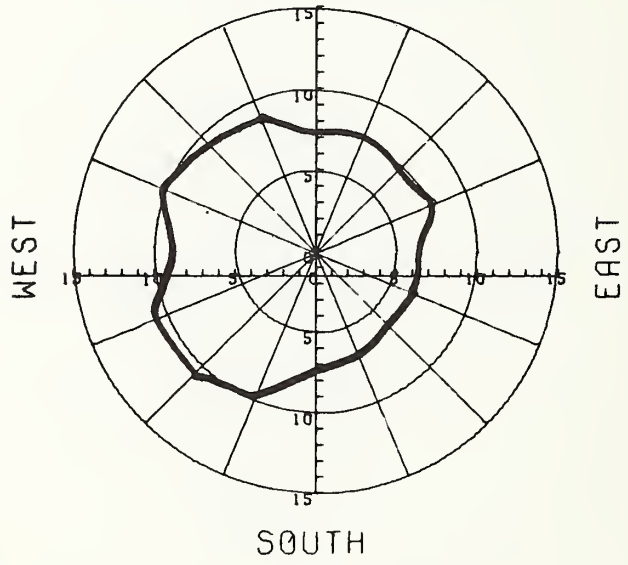
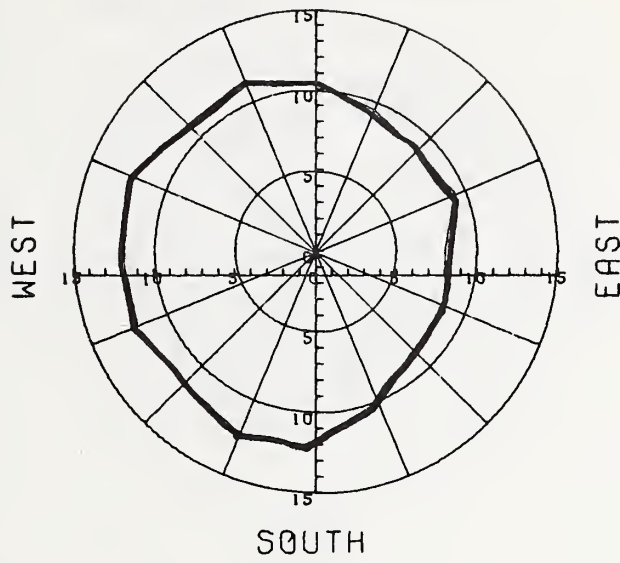


Fig. 26 INDIANAPOLIS, INDIANA

WINTER NORTH



SUMMER NORTH

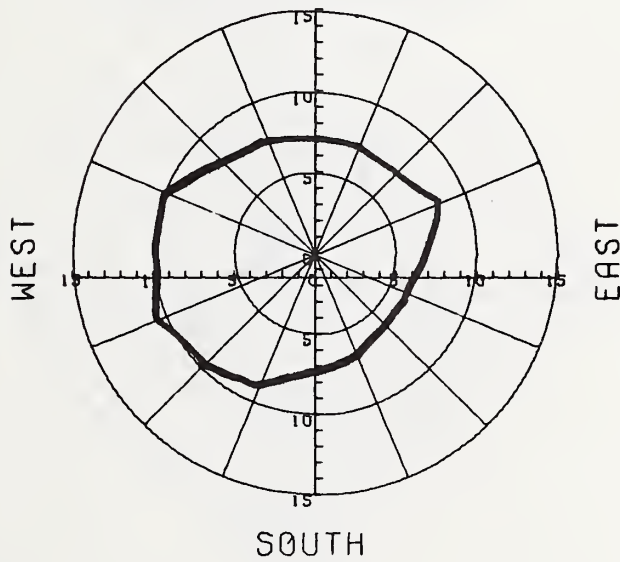
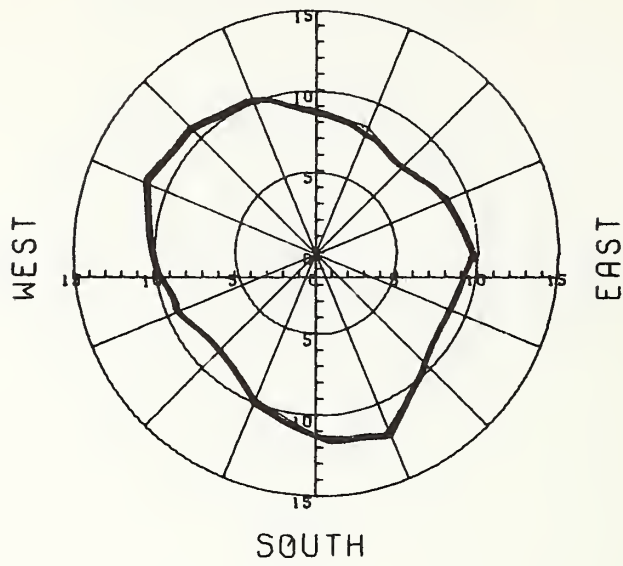


Fig. 27 GRAND RAPIDS, MICHIGAN

WINTER NORTH



SUMMER NORTH

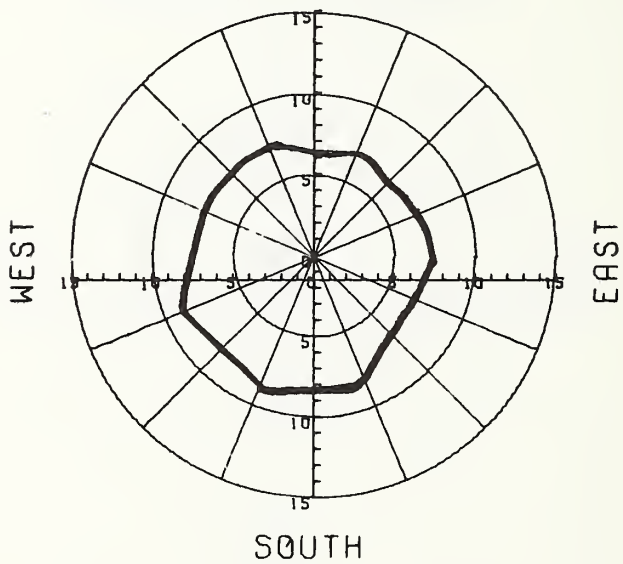
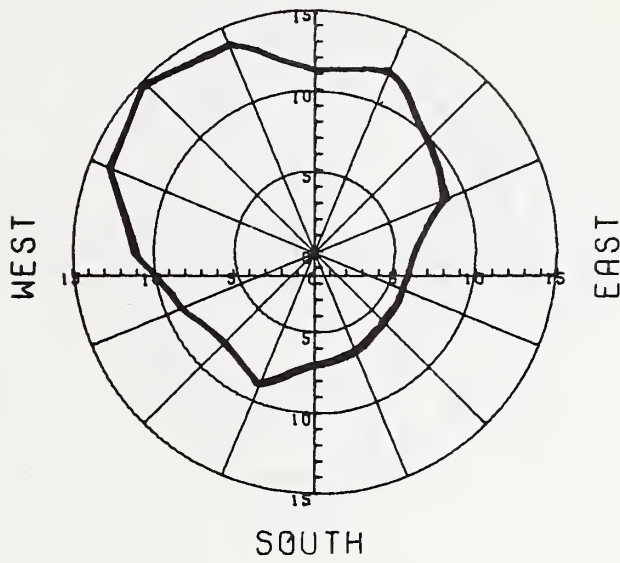


Fig. 28

ST. LOUIS, MISSOURI

WINTER NORTH



SUMMER NORTH

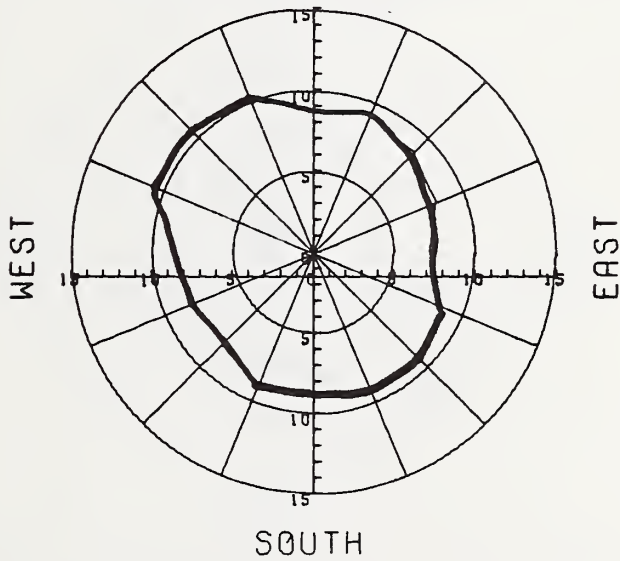
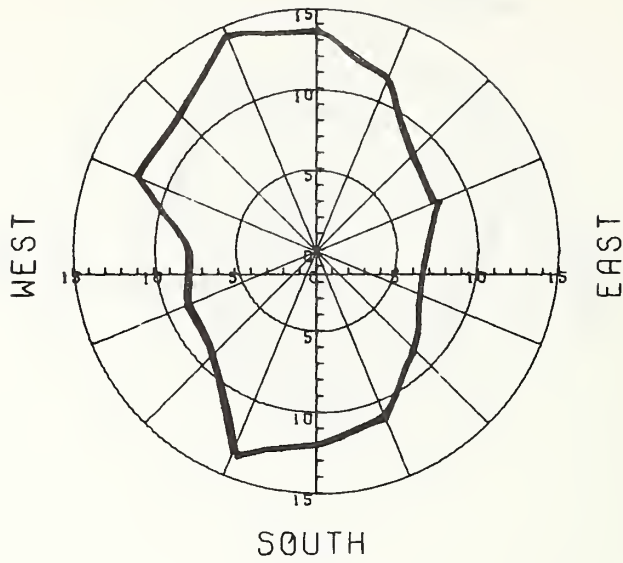


Fig. 29

NEWARK, NEW JERSEY

WINTER NORTH



SUMMER NORTH

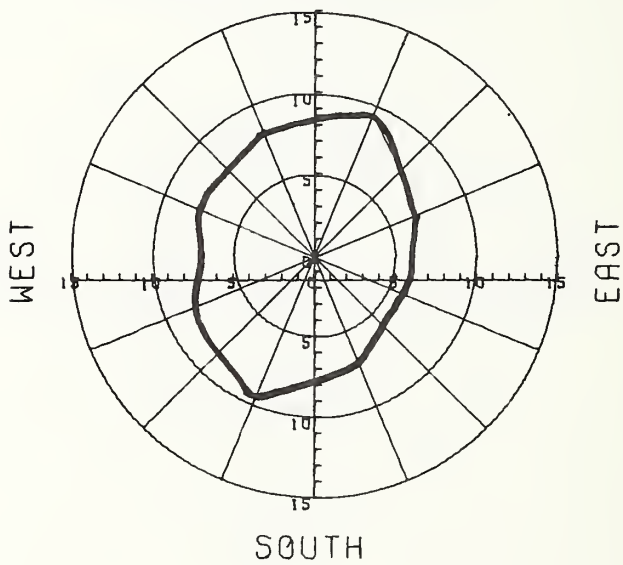
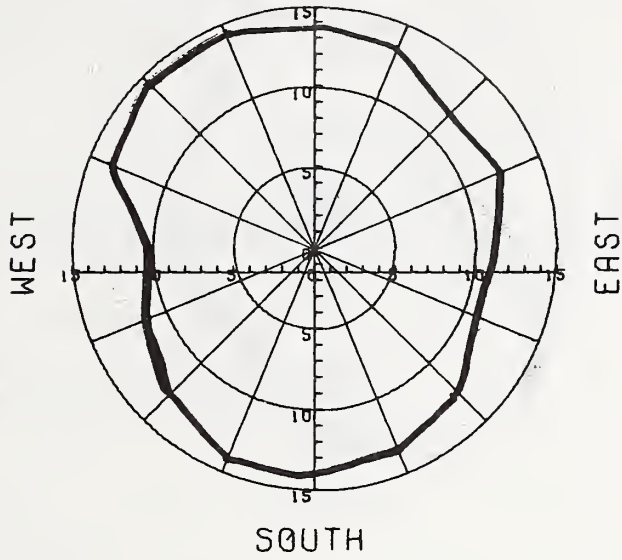


Fig. 30

MEMPHIS, TENNESSEE

WINTER NORTH



SUMMER NORTH

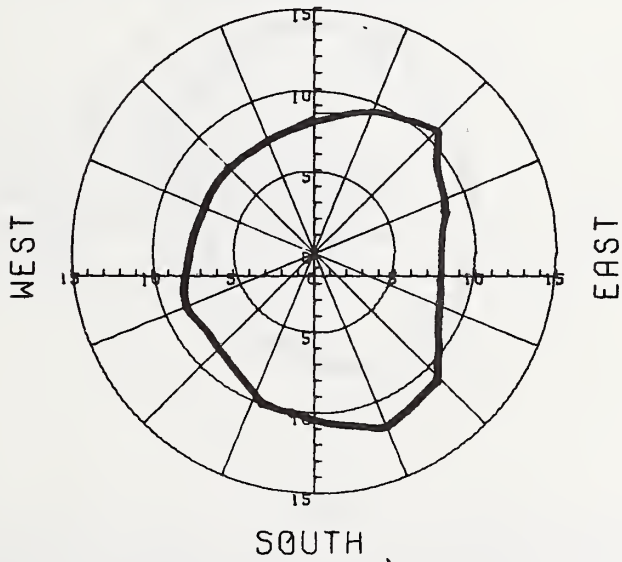
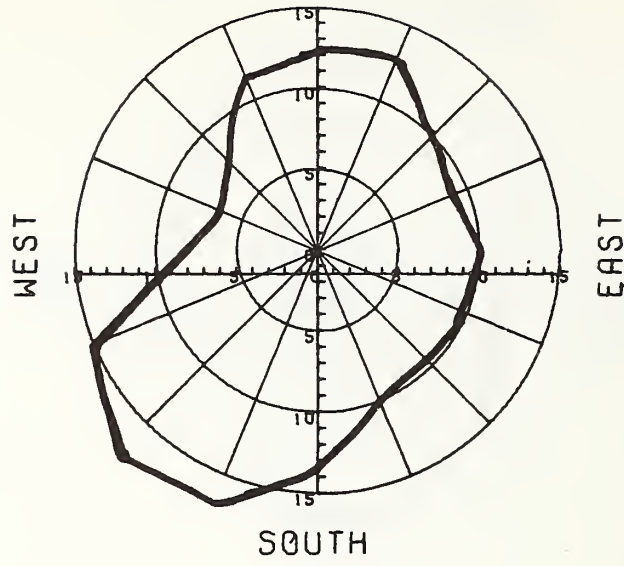


Fig. 31

HOUSTON, TEXAS

WINTER NORTH



SUMMER NORTH

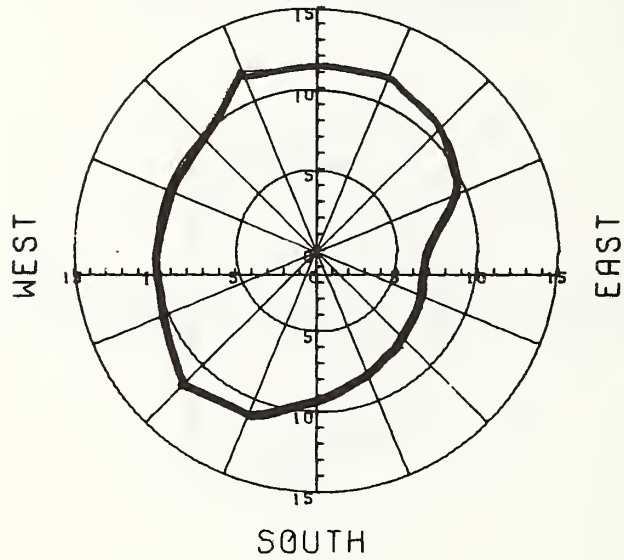


Fig. 32

SEATTLE, WASHINGTON

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7. AUTHOR(S) Tamami Kusuda		8. Performing Organization NBSIR 73-144	
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16. ABSTRACT (A 200-word or less factual summary of most significant information. If document includes a significant bibliography or literature survey, mention it here.) The purpose of this report is to provide preliminary information on site climatology useful for the design and evaluation of HUD Operation BREAKTHROUGH experimental building systems. In order to evaluate the design as well as the performance of building systems, the following environmental parameters are considered essential and are included in this report for each of the selected sites. Temperature Humidity Wind speed and direction Precipitation (snow and rain) Solar radiation (direct and diffuse) Ground temperature (depth and frost) Background noise level Air contamination Earthquake risk			
17. KEY WORDS (Alphabetical order, separated by semicolons) Air contamination; design conditions; earthquake risk; evaluation; ground temperature; humidity; noise level; Operation BREAKTHROUGH; precipitation; solar radiation; temperature; wind direction; wind speed			
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