

Tables for the Evaluation of the Faxén Approximation to the Solution of the Lamm Equation

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A table is presented to facilitate the calculation of the Faxén approximation to the concentration and concentration gradient. The table is accurate to within one figure in the last place, and can be used both for no sedimentation dependence on concentration and for the dependence $s = s_0(1 - kc)$.

Key Words: Faxén approximation, Lamm equation, ultracentrifuge, theory of noise, theory of ion exchange columns.

The Faxén approximation to the solution of the Lamm equation has proved to be of considerable utility in the analysis of data from velocity sedimentation experiments with the ultracentrifuge [1].¹ It has recently been shown that the Faxén solution to the nonlinear Lamm equation which arises when the sedimentation coefficient s is related to concentration c by $s = s_0(1 - kc)$ can be written in terms of the Faxén solution for $k = 0$ [2]. Because of this wide range of applicability of the Faxén solution, it is appropriate to present a table to facilitate the calculation of concentration and concentration gradients in that approximation. The best known of earlier, equivalent tables, are those of Opler and Hiester [3]. Their tabulation gives very few values of the relevant function in the range of interest for ultracentrifuge work. A thorough analysis of mathematical properties of the function arising from the Faxén solution has been published by Goldstein [4]. Other applications of the tabulated function are to be found in the theory of noise [5], and in the theory of ion exchange columns [6].

Let us summarize the relevant facts on the Faxén solution. It is assumed that the concentration in the ultracentrifuge is $c(r, t)$, where r is the radius and t the time, with $c(r, 0) = c_0$, a constant. Let r_0 denote radial distance to the meniscus, ω the frequency of revolution, D the diffusion coefficient. The Faxén solution is most conveniently written in terms of the new variables:

$$\begin{aligned} \theta &= c/c_0, & x &= (r/r_0)^2, & \tau &= 2\omega^2 s_0 t, \\ \alpha &= kc_0, & \epsilon &= 2D/(s_0\omega^2 r_0^2), & z &= 2\sqrt{x e^{-\tau}}, & \zeta &= 1 - e^{-\tau}. \end{aligned} \quad (1)$$

When $k = 0$, or equivalently, when $\alpha = 0$, the Faxén expression for $\theta(z, \zeta)$ is

$$\theta_0(z, \zeta) = \frac{1 - \zeta}{2\epsilon\zeta} \int_2^\infty \sigma e^{-\frac{(\sigma^2 + z^2)}{4\epsilon\zeta}} I_0\left(\frac{z\sigma}{2\epsilon\zeta}\right) d\sigma. \quad (2)$$

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¹ Figures in brackets indicate the literature references at the end of this paper.

When $\alpha > 0$ we have

$$\theta_\alpha(z, \zeta) = \frac{1 - \zeta}{1 - (1 + \alpha)\zeta} \left\{ \frac{\theta_0(z^*, \zeta^*) e^{-\frac{\alpha}{\epsilon} \left[1 - \frac{z^2}{4(1 - \alpha\zeta)}\right]}}{1 + \frac{1 - \alpha\zeta}{1 - (1 + \alpha)\zeta} \theta_0(z^*, \zeta^*) e^{-\frac{\alpha}{\epsilon} \left[1 - \frac{z^2}{4(1 - \alpha\zeta)}\right]} - \frac{1}{1 - \zeta} \theta_0(z, \zeta)} \right\} \quad (3)$$

where

$$z^* = z(1 - \alpha\zeta)^{-1}, \quad \zeta^* = \zeta(1 - \alpha\zeta)^{-1}. \quad (4)$$

Hence $\theta_\alpha(z, \zeta)$ can be represented in terms of $\theta_0(z, \zeta)$.

In the following pages we tabulate values of the functions

$$\psi(y, \eta) = \frac{1}{2\eta} \int_2^\infty \sigma e^{-\frac{(\sigma^2 + y^2)}{4\eta}} I_0\left(\frac{\sigma y}{2\eta}\right) d\sigma \quad (5)$$

$$\frac{\partial \psi(y, \eta)}{\partial y} = \frac{1}{4\eta^2} \int_2^\infty \sigma e^{-\frac{(\sigma^2 + y^2)}{4\eta}} \left[\sigma I_1\left(\frac{\sigma y}{2\eta}\right) - y I_0\left(\frac{\sigma y}{2\eta}\right) \right] d\sigma \quad (6)$$

accurate to at least four places with a possible error of 1 in the last place. The intervals of tabulation in η are $\eta = 10^{-6}$ (10^{-6}) 10^{-5} (10^{-5}) 10^{-4} (10^{-4}) 10^{-3} . For each value of η we choose from 28 to 80 steps in y so that $\psi(y, \eta)$ lies in the range (0.005, 0.995).

The solutions for concentration and concentration gradients in terms of the tabulated functions are

$$\theta_0(z, \zeta) = (1 - \zeta)\psi(z, \epsilon\zeta) \quad (7)$$

$$\frac{\partial \theta_0(z, \zeta)}{\partial(r/r_0)} = 2(1 - \zeta)^{3/2} \frac{\partial \psi(z, \epsilon\zeta)}{\partial z} \quad (8)$$

for $\alpha = 0$, and

$$\frac{\partial \theta_\alpha(z, \zeta)}{\partial(r/r_0)} = \frac{1}{(1 - \alpha\zeta)F} \frac{\partial \theta_0(z, \zeta)}{\partial(r/r_0)} + \frac{1 - \zeta - \theta_0(z, \zeta)}{(1 - \alpha\zeta)F^2} \times \left\{ \frac{1}{1 - (1 + \alpha)\zeta} \left[(1 - \alpha\zeta) \frac{\partial \theta_0(z^*, \zeta^*)}{\partial(r/r_0)} + \frac{\alpha\zeta}{\epsilon} (1 - \zeta)^{1/2} \theta_0(z^*, \zeta^*) \right] e^{-\frac{\alpha}{\epsilon} \left[1 - \frac{z^2}{4(1 - \alpha\zeta)}\right]} - \frac{1}{1 - \zeta} \frac{\partial \theta_0(z, \zeta)}{\partial(r/r_0)} \right\} \quad (9)$$

for $\alpha > 0$, where

$$F = 1 + \frac{1 - \alpha\zeta}{1 - (1 + \alpha)\zeta} \theta_0(z^*, \zeta^*) e^{-\frac{\alpha}{\epsilon} \left[1 - \frac{z^2}{4(1 - \alpha\zeta)}\right]} - \frac{1}{1 - \zeta} \theta_0(z, \zeta). \quad (10)$$

The integrals were evaluated using Simpson's rule. The interval of integration h was varied from 2×10^{-5} to 10^{-3} for different values of y and η , so as always to meet the requirements of accuracy. The integration was stopped when the integrand was less than 10^{-25} . As a check on our accuracy, the integration was performed twice; once over the interval (2, ∞) and once over the

interval (0, 2) with the appropriate integrals derived from the formulas

$$\frac{1}{2\eta} \int_2^\infty \sigma e^{-\frac{(\sigma^2+y^2)}{4\eta}} I_0\left(\frac{\sigma y}{2\eta}\right) d\sigma = 1 - \frac{1}{2\eta} \int_0^2 \sigma e^{-\frac{(\sigma^2+y^2)}{4\eta}} I_0\left(\frac{\sigma y}{2\eta}\right) d\sigma \quad (11)$$

and

$$\int_2^\infty \sigma e^{-\frac{(\sigma^2+y^2)}{4\eta}} \left[\sigma I_1\left(\frac{\sigma y}{2\eta}\right) - y I_0\left(\frac{\sigma y}{2\eta}\right) \right] d\sigma = - \int_0^2 \sigma e^{-\frac{(\sigma^2+y^2)}{4\eta}} \left[\sigma I_1\left(\frac{\sigma y}{2\eta}\right) - y I_0\left(\frac{\sigma y}{2\eta}\right) \right] d\sigma \quad (12)$$

Since the argument of the Bessel functions was always greater than 1200, the asymptotic expansions

$$I_0(x) \sim \frac{e^x}{\sqrt{2\pi x}} \left[1 + \frac{1}{1!(8x)} + \frac{3^2}{2!(8x)^2} + \frac{3^2 5^2}{3!(8x)^3} + \dots \right] \quad (13)$$

$$I_1(x) \sim \frac{e^x}{\sqrt{2\pi x}} \left[1 - \frac{3}{1!8x} - \frac{3.5}{2!(8x)^2} - \frac{3^2 5.7}{3!(8x)^3} - \dots \right] \quad (14)$$

were used to evaluate these Bessel functions.

All the calculations are accurate to within one figure in the fifth place. Eight place tables are available from the authors, as well as a tabulation for the range $0.001 < \eta \leq 0.01$.

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000001

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
1.9960	0.23414D-02	0.51718D 01	2.0002	0.55637D 00	0.27927D 03
1.9965	0.66707D-02	0.13205D 02	2.0004	0.61149D 00	0.27101D 03
1.9970	0.16962D-01	0.29755D 02	2.0006	0.66444D 00	0.25778D 03
1.9975	0.38579D-01	0.59167D 02	2.0008	0.71432D 00	0.24034D 03
1.9980	0.78701D-01	0.10383D 03	2.0010	0.76036D 00	0.21964D 03
1.9982	0.10161D-00	0.12555D 03	2.0012	0.80203D 00	0.19675D 03
1.9984	0.12902D-00	0.14881D 03	2.0014	0.83899D 00	0.17276D 03
1.9986	0.16119D-00	0.17288D 03	2.0016	0.87112D 00	0.14869D 03
1.9988	0.19817D-00	0.19687D 03	2.0018	0.89852D 00	0.12544D 03
1.9990	0.23986D-00	0.21975D 03	2.0020	0.92140D 00	0.10373D 03
1.9992	0.28592D-00	0.24043D 03	2.0022	0.94014D 00	0.84076D 02
1.9994	0.33581D-00	0.25785D 03	2.0025	0.96148D 00	0.59093D 02
1.9996	0.38878D-00	0.27106D 03	2.0030	0.98307D 00	0.29710D 02
1.9998	0.44391D-00	0.27930D 03	2.0035	0.99334D 00	0.13182D 02
2.0000	0.50014D 00	0.28209D 03	2.0040	0.99766D 00	0.51616D 01

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000002

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
1.9950	0.621840-02	0.877500 01	2.0002	0.540030 00	0.198470 03
1.9955	0.122400-01	0.158880 02	2.0004	0.579460 00	0.195500 03
1.9960	0.227770-01	0.270220 02	2.0006	0.618100 00	0.190670 03
1.9965	0.401020-01	0.431760 02	2.0008	0.655610 00	0.184100 03
1.9970	0.668730-01	0.648080 02	2.0010	0.691640 00	0.175990 03
1.9972	0.808320-01	0.749170 02	2.0012	0.725910 00	0.166560 03
1.9974	0.968870-01	0.857400 02	2.0014	0.758190 00	0.156070 03
1.9976	0.115170-00	0.971520 02	2.0016	0.788290 00	0.144790 03
1.9978	0.135780-00	0.108990 03	2.0018	0.816070 00	0.132980 03
1.9980	0.158780-00	0.121050 03	2.0020	0.841470 00	0.120920 03
1.9982	0.184190-00	0.133100 03	2.0022	0.864440 00	0.108870 03
1.9984	0.212000-00	0.144900 03	2.0024	0.885030 00	0.970340 02
1.9986	0.242120-00	0.156180 03	2.0026	0.903290 00	0.856280 02
1.9988	0.274420-00	0.166660 03	2.0028	0.919320 00	0.748110 02
1.9990	0.308710-00	0.176080 03	2.0030	0.933260 00	0.647100 02
1.9992	0.344760-00	0.184170 03	2.0032	0.945260 00	0.554160 02
1.9994	0.382280-00	0.190720 03	2.0035	0.959980 00	0.431010 02
1.9996	0.420940-00	0.195540 03	2.0040	0.977280 00	0.269680 02
1.9998	0.460370-00	0.198490 03	2.0045	0.987790 00	0.158520 02
2.0000	0.500200 00	0.199470 03	2.0050	0.993800 00	0.875310 01

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000003

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
1.9935	0.398900-02	0.482460 01	2.0002	0.532780 00	0.162320 03
1.9940	0.716510-02	0.812080 01	2.0004	0.565100 00	0.160690 03
1.9945	0.123920-01	0.131110 02	2.0006	0.596990 00	0.158030 03
1.9950	0.206440-01	0.203050 02	2.0008	0.628250 00	0.154380 03
1.9955	0.331410-01	0.301610 02	2.0010	0.658680 00	0.149810 03
1.9960	0.512990-01	0.429740 02	2.0012	0.688110 00	0.144410 03
1.9965	0.766090-01	0.587320 02	2.0014	0.716390 00	0.138280 03
1.9968	0.958140-01	0.694360 02	2.0016	0.743380 00	0.131530 03
1.9970	0.110450-00	0.769910 02	2.0018	0.768970 00	0.124270 03
1.9972	0.126630-00	0.848010 02	2.0020	0.793070 00	0.116640 03
1.9974	0.144380-00	0.927820 02	2.0022	0.815610 00	0.108750 03
1.9976	0.163750-00	0.100840 03	2.0024	0.836560 00	0.100720 03
1.9978	0.184720-00	0.108870 03	2.0026	0.855900 00	0.926610 02
1.9980	0.207280-00	0.116760 03	2.0028	0.873630 00	0.846820 02
1.9982	0.231400-00	0.124390 03	2.0030	0.889780 00	0.768750 02
1.9984	0.257010-00	0.131630 03	2.0032	0.904400 00	0.693250 02
1.9986	0.284020-00	0.138370 03	2.0034	0.917530 00	0.621010 02
1.9988	0.312320-00	0.144490 03	2.0037	0.934620 00	0.519970 02
1.9990	0.341770-00	0.149880 03	2.0040	0.948830 00	0.428890 02
1.9992	0.372220-00	0.154440 03	2.0045	0.966950 00	0.300940 02
1.9994	0.403490-00	0.158080 03	2.0050	0.979420 00	0.202540 02
1.9996	0.435380-00	0.160730 03	2.0055	0.987650 00	0.130760 02
1.9998	0.467710-00	0.162330 03	2.0060	0.992860 00	0.809670 01
2.0000	0.500250 00	0.162870 03	2.0065	0.996030 00	0.480910 01

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000004

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
			2.0002	0.52847D 00	0.14069D 03
			2.0004	0.55651D 00	0.13963D 03
			2.0006	0.58427D 00	0.13789D 03
1.9930	0.66773D-02	0.66084D 01	2.0008	0.61162D 00	0.13549D 03
1.9935	0.10798D-01	0.10075D 02	2.0010	0.63843D 00	0.13247D 03
1.9940	0.16977D-01	0.14888D 02	2.0012	0.66457D 00	0.12887D 03
1.9945	0.25957D-01	0.21324D 02	2.0014	0.68994D 00	0.12474D 03
1.9950	0.38609D-01	0.29602D 02	2.0016	0.71444D 00	0.12014D 03
1.9955	0.55885D-01	0.39829D 02	2.0018	0.73797D 00	0.11514D 03
1.9960	0.78754D-01	0.51940D 02	2.0020	0.76047D 00	0.10979D 03
1.9962	0.89669D-01	0.57257D 02	2.0022	0.78187D 00	0.10417D 03
1.9964	0.10167D-00	0.62803D 02	2.0024	0.80213D 00	0.98346D 02
1.9966	0.11480D-00	0.68542D 02	2.0026	0.82120D 00	0.92383D 02
1.9968	0.12910D-00	0.74433D 02	2.0028	0.83907D 00	0.86349D 02
1.9970	0.14458D-00	0.80427D 02	2.0030	0.85574D 00	0.80306D 02
1.9972	0.16127D-00	0.86470D 02	2.0032	0.87120D 00	0.74314D 02
1.9974	0.17917D-00	0.92504D 02	2.0034	0.88547D 00	0.68425D 02
1.9976	0.19827D-00	0.98465D 02	2.0036	0.89858D 00	0.62689D 02
1.9978	0.21855D-00	0.10429D 03	2.0038	0.91056D 00	0.57148D 02
1.9980	0.23997D-00	0.10990D 03	2.0040	0.92145D 00	0.51836D 02
1.9982	0.26249D-00	0.11524D 03	2.0042	0.93131D 00	0.46784D 02
1.9984	0.28604D-00	0.12024D 03	2.0045	0.94427D 00	0.39740D 02
1.9986	0.31056D-00	0.12483D 03	2.0050	0.96151D 00	0.29528D 02
1.9988	0.33595D-00	0.12895D 03	2.0055	0.97413D 00	0.21266D 02
1.9990	0.36210D-00	0.13253D 03	2.0060	0.98308D 00	0.14844D 02
1.9992	0.38892D-00	0.13554D 03	2.0065	0.98924D 00	0.10043D 02
1.9994	0.41628D-00	0.13793D 03	2.0070	0.99335D 00	0.65854D 01
1.9996	0.44405D-00	0.13966D 03			
1.9998	0.47210D-00	0.14070D 03			
2.0000	0.50028D 00	0.14105D 03			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000005

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
1.9920	0.57189D-02	0.51527D 01	2.0002	0.52553D 00	0.12590D 03
1.9925	0.88720D-02	0.75905D 01	2.0004	0.55064D 00	0.12514D 03
1.9930	0.13456D-01	0.10906D 02	2.0006	0.57555D 00	0.12389D 03
1.9935	0.19955D-01	0.15282D 02	2.0008	0.60016D 00	0.12216D 03
1.9940	0.28942D-01	0.20885D 02	2.0010	0.62438D 00	0.11997D 03
1.9945	0.41065D-01	0.27838D 02	2.0012	0.64812D 00	0.11736D 03
1.9950	0.57014D-01	0.36190D 02	2.0014	0.67130D 00	0.11434D 03
1.9955	0.77479D-01	0.45886D 02	2.0016	0.69384D 00	0.11096D 03
1.9958	0.92193D-01	0.52278D 02	2.0018	0.71566D 00	0.10724D 03
1.9960	0.10309D-00	0.56742D 02	2.0020	0.73671D 00	0.10324D 03
1.9962	0.11490D-00	0.61342D 02	2.0022	0.75694D 00	0.98986D 02
1.9964	0.12764D-00	0.66051D 02	2.0024	0.77629D 00	0.94531D 02
1.9966	0.14132D-00	0.70836D 02	2.0026	0.79474D 00	0.89916D 02
1.9968	0.15597D-00	0.75665D 02	2.0028	0.81225D 00	0.85185D 02
1.9970	0.17159D-00	0.80501D 02	2.0030	0.82881D 00	0.80381D 02
1.9972	0.18817D-00	0.85304D 02	2.0032	0.84440D 00	0.75545D 02
1.9974	0.20571D-00	0.90033D 02	2.0034	0.85903D 00	0.70716D 02
1.9976	0.22418D-00	0.94644D 02	2.0036	0.87269D 00	0.65932D 02
1.9978	0.24355D-00	0.99094D 02	2.0038	0.88541D 00	0.61226D 02
1.9980	0.26380D-00	0.10334D 03	2.0040	0.89719D 00	0.56629D 02
1.9982	0.28487D-00	0.10734D 03	2.0042	0.90807D 00	0.52168D 02
1.9984	0.30672D-00	0.11104D 03	2.0044	0.91807D 00	0.47867D 02
1.9986	0.32927D-00	0.11442D 03	2.0047	0.93150D 00	0.441756D 02
1.9988	0.35246D-00	0.11743D 03	2.0050	0.94317D 00	0.36099D 02
1.9990	0.37621D-00	0.12003D 03	2.0055	0.95907D 00	0.27762D 02
1.9992	0.40045D-00	0.12221D 03	2.0060	0.97116D 00	0.20822D 02
1.9994	0.42507D-00	0.12392D 03	2.0065	0.98012D 00	0.15232D 02
1.9996	0.44998D-00	0.12516D 03	2.0070	0.98660D 00	0.10868D 02
1.9998	0.47510D-00	0.12591D 03	2.0075	0.99117D 00	0.75621D 01
2.0000	0.50031D 00	0.12616D 03	2.0080	0.99431D 00	0.51322D 01

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000006

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
			2.0002	0.52336D 00	0.11497D 03
			2.0004	0.54631D 00	0.11439D 03
1.9910	0.46992D-02	0.39496D 01	2.0006	0.56910D 00	0.11343D 03
1.9915	0.70860D-02	0.56864D 01	2.0008	0.59166D 00	0.11211D 03
1.9920	0.10485D-01	0.80181D 01	2.0010	0.61392D 00	0.11044D 03
1.9925	0.15225D-01	0.11073D 02	2.0012	0.63581D 00	0.10843D 03
1.9930	0.21699D-01	0.14976D 02	2.0014	0.65727D 00	0.10610D 03
1.9935	0.30360D-01	0.19837D 02	2.0016	0.67823D 00	0.10347D 03
1.9940	0.41709D-01	0.25735D 02	2.0018	0.69864D 00	0.10058D 03
1.9945	0.56274D-01	0.32698D 02	2.0020	0.71844D 00	0.97436D 02
1.9950	0.74579D-01	0.40689D 02	2.0022	0.73760D 00	0.94080D 02
1.9953	0.87564D-01	0.45930D 02	2.0024	0.75606D 00	0.90537D 02
1.9956	0.10217D-00	0.51460D 02	2.0026	0.77380D 00	0.86838D 02
1.9958	0.11284D-00	0.55280D 02	2.0028	0.79079D 00	0.83013D 02
1.9960	0.12428D-00	0.59187D 02	2.0030	0.80700D 00	0.79092D 02
1.9962	0.13652D-00	0.63158D 02	2.0032	0.82242D 00	0.75106D 02
1.9964	0.14955D-00	0.67172D 02	2.0034	0.83704D 00	0.71083D 02
1.9966	0.16339D-00	0.71204D 02	2.0036	0.85085D 00	0.67052D 02
1.9968	0.17803D-00	0.75226D 02	2.0038	0.86386D 00	0.63039D 02
1.9970	0.19348D-00	0.79211D 02	2.0040	0.87607D 00	0.59068D 02
1.9972	0.20971D-00	0.83129D 02	2.0042	0.88749D 00	0.55164D 02
1.9974	0.22672D-00	0.86951D 02	2.0044	0.89814D 00	0.51347D 02
1.9976	0.24448D-00	0.90646D 02	2.0046	0.90804D 00	0.47634D 02
1.9978	0.26297D-00	0.94184D 02	2.0048	0.91720D 00	0.44043D 02
1.9980	0.28214D-00	0.97533D 02	2.0050	0.92566D 00	0.40587D 02
1.9982	0.30197D-00	0.10067D 03	2.0055	0.94392D 00	0.32608D 02
1.9984	0.32239D-00	0.10355D 03	2.0060	0.95844D 00	0.25658D 02
1.9986	0.34337D-00	0.10617D 03	2.0065	0.96976D 00	0.19773D 02
1.9988	0.36484D-00	0.10849D 03	2.0070	0.97839D 00	0.14924D 02
1.9990	0.38675D-00	0.11049D 03	2.0075	0.98484D 00	0.11031D 02
1.9992	0.40902D-00	0.11216D 03	2.0080	0.98956D 00	0.79860D 01
1.9994	0.43159D-00	0.11347D 03	2.0085	0.99295D 00	0.56622D 01
1.9996	0.45438D-00	0.11441D 03	2.0090	0.99532D 00	0.39318D 01
1.9998	0.47732D-00	0.11498D 03			
2.0000	0.50035D 00	0.11516D 03			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000007

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
1.9905	0.55736D-02	0.42565D 01	2.0002	0.52169D 00	0.10646D 03
1.9910	0.80991D-02	0.59220D 01	2.0004	0.54294D 00	0.10600D 03
1.9915	0.11580D-01	0.80934D 01	2.0006	0.56407D 00	0.10524D 03
1.9920	0.16293D-01	0.10865D 02	2.0008	0.58502D 00	0.10419D 03
1.9925	0.22560D-01	0.14328D 02	2.0010	0.60573D 00	0.10286D 03
1.9930	0.30749D-01	0.18560D 02	2.0012	0.62614D 00	0.10125D 03
1.9935	0.41259D-01	0.23617D 02	2.0014	0.64621D 00	0.99379D 02
1.9940	0.54508D-01	0.29520D 02	2.0016	0.66588D 00	0.97267D 02
1.9945	0.70916D-01	0.36245D 02	2.0018	0.68510D 00	0.94928D 02
1.9950	0.90877D-01	0.43714D 02	2.0020	0.70383D 00	0.92382D 02
1.9952	0.99936D-01	0.46882D 02	2.0022	0.72204D 00	0.89647D 02
1.9954	0.10964D-00	0.50135D 02	2.0024	0.73968D 00	0.86745D 02
1.9956	0.11999D-00	0.53461D 02	2.0026	0.75673D 00	0.83698D 02
1.9958	0.13102D-00	0.56845D 02	2.0028	0.77315D 00	0.80527D 02
1.9960	0.14274D-00	0.60271D 02	2.0030	0.78893D 00	0.77255D 02
1.9962	0.15513D-00	0.63721D 02	2.0032	0.80405D 00	0.73905D 02
1.9964	0.16822D-00	0.67177D 02	2.0034	0.81849D 00	0.70498D 02
1.9966	0.18200D-00	0.70618D 02	2.0036	0.83224D 00	0.67056D 02
1.9968	0.19647D-00	0.74023D 02	2.0038	0.84531D 00	0.63601D 02
1.9970	0.21161D-00	0.77371D 02	2.0040	0.85769D 00	0.60151D 02
1.9972	0.22741D-00	0.80639D 02	2.0042	0.86937D 00	0.56726D 02
1.9974	0.24386D-00	0.83806D 02	2.0044	0.88038D 00	0.53344D 02
1.9976	0.26093D-00	0.86849D 02	2.0046	0.89071D 00	0.50020D 02
1.9978	0.27859D-00	0.89746D 02	2.0048	0.90039D 00	0.46770D 02
1.9980	0.29681D-00	0.92474D 02	2.0050	0.90943D 00	0.43605D 02
1.9982	0.31557D-00	0.95014D 02	2.0052	0.91784D 00	0.40539D 02
1.9984	0.33480D-00	0.97345D 02	2.0055	0.92934D 00	0.36146D 02
1.9986	0.35449D-00	0.99448D 02	2.0060	0.94570D 00	0.29432D 02
1.9988	0.37457D-00	0.10131D 03	2.0065	0.95891D 00	0.23541D 02
1.9990	0.39499D-00	0.10291D 03	2.0070	0.96938D 00	0.18496D 02
1.9992	0.41571D-00	0.10423D 03	2.0075	0.97754D 00	0.14275D 02
1.9994	0.43667D-00	0.10528D 03	2.0080	0.98378D 00	0.10822D 02
1.9996	0.45780D-00	0.10602D 03	2.0085	0.98848D 00	0.80591D 01
1.9998	0.47906D-00	0.10647D 03	2.0090	0.99194D 00	0.58954D 01
2.0000	0.50037D 00	0.10662D 03	2.0095	0.99446D 00	0.42363D 01

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000008

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
			2.0002	0.520340 00	0.996060 02
			2.0004	0.540220 00	0.992280 02
			2.0006	0.560010 00	0.986050 02
1.9895	0.434520-02	0.318940 01	2.0008	0.579650 00	0.977410 02
1.9900	0.622720-02	0.439300 01	2.0010	0.599090 00	0.966430 02
			2.0012	0.618290 00	0.953180 02
1.9905	0.879820-02	0.595710 01	2.0014	0.637210 00	0.937770 02
1.9910	0.122560-01	0.795280 01	2.0016	0.655790 00	0.920310 02
1.9915	0.168350-01	0.104520 02	2.0018	0.674000 00	0.900910 02
1.9920	0.228040-01	0.135250 02	2.0020	0.691810 00	0.879720 02
1.9925	0.304650-01	0.172290 02			
			2.0022	0.709180 00	0.856890 02
1.9930	0.401450-01	0.216070 02	2.0024	0.726080 00	0.832560 02
1.9935	0.521880-01	0.266780 02	2.0026	0.742480 00	0.806910 02
1.9940	0.669370-01	0.324280 02	2.0028	0.758350 00	0.780090 02
1.9945	0.847210-01	0.388060 02	2.0030	0.773670 00	0.752280 02
1.9950	0.105830-00	0.457190 02			
			2.0032	0.788430 00	0.723650 02
1.9952	0.115260-00	0.486050 02	2.0034	0.802610 00	0.694370 02
1.9954	0.125280-00	0.515430 02	2.0036	0.816210 00	0.664610 02
1.9956	0.135880-00	0.545230 02	2.0038	0.829200 00	0.634540 02
1.9958	0.147090-00	0.575310 02	2.0040	0.841590 00	0.604320 02
1.9960	0.158900-00	0.605530 02			
			2.0042	0.853370 00	0.574100 02
1.9962	0.171310-00	0.635750 02	2.0044	0.864550 00	0.544030 02
1.9964	0.184330-00	0.665810 02	2.0046	0.875130 00	0.514250 02
1.9966	0.197940-00	0.695550 02	2.0048	0.885120 00	0.484880 02
1.9968	0.212150-00	0.724810 02	2.0050	0.894530 00	0.456050 02
1.9970	0.226930-00	0.753410 02			
			2.0052	0.903370 00	0.427860 02
1.9972	0.242280-00	0.781180 02	2.0055	0.915590 00	0.387000 02
1.9974	0.258170-00	0.807950 02	2.0060	0.933320 00	0.323310 02
1.9976	0.274590-00	0.833560 02	2.0065	0.948030 00	0.265910 02
1.9978	0.291500-00	0.857830 02	2.0070	0.960030 00	0.215320 02
1.9980	0.308890-00	0.880600 02			
			2.0075	0.969670 00	0.171640 02
1.9982	0.326720-00	0.901720 02	2.0080	0.977300 00	0.134710 02
1.9984	0.344950-00	0.921040 02	2.0085	0.983250 00	0.104080 02
1.9986	0.363540-00	0.938430 02	2.0090	0.987810 00	0.791700 01
1.9988	0.382470-00	0.953750 02	2.0095	0.991250 00	0.592890 01
1.9990	0.401680-00	0.966910 02			
			2.0100	0.993810 00	0.437110 01
1.9992	0.421130-00	0.977800 02	2.0105	0.995680 00	0.317270 01
1.9994	0.440780-00	0.986340 02			
1.9996	0.460570-00	0.992480 02			
1.9998	0.480460-00	0.996160 02			
2.0000	0.500400 00	0.997350 02			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000009

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
1.9890	0.47757D-02	0.32716D 01	2.0002	0.51922D 00	0.93922D 02
1.9895	0.66840D-02	0.44095D 01	2.0004	0.53798D 00	0.93605D 02
1.9900	0.92374D-02	0.58612D 01	2.0006	0.55665D 00	0.93082D 02
1.9905	0.12607D-01	0.76834D 01	2.0008	0.57520D 00	0.92356D 02
			2.0010	0.59358D 00	0.91433D 02
1.9910	0.16992D-01	0.99332D 01	2.0012	0.61176D 00	0.90317D 02
1.9915	0.22620D-01	0.12665D 02	2.0014	0.62969D 00	0.89018D 02
1.9920	0.29745D-01	0.15924D 02	2.0016	0.64735D 00	0.87542D 02
1.9925	0.38639D-01	0.19747D 02	2.0018	0.66470D 00	0.85900D 02
1.9930	0.49589D-01	0.24150D 02	2.0020	0.68170D 00	0.84101D 02
1.9935	0.62884D-01	0.29126D 02	2.0022	0.69833D 00	0.82157D 02
1.9940	0.78805D-01	0.34644D 02	2.0024	0.71456D 00	0.80080D 02
1.9945	0.97609D-01	0.40639D 02	2.0026	0.73035D 00	0.77883D 02
1.9948	0.11036D-00	0.44426D 02	2.0028	0.74570D 00	0.75577D 02
1.9950	0.11951D-00	0.47014D 02	2.0030	0.76058D 00	0.73177D 02
1.9952	0.12917D-00	0.49642D 02	2.0032	0.77497D 00	0.70696D 02
1.9954	0.13937D-00	0.52300D 02	2.0034	0.78885D 00	0.68147D 02
1.9956	0.15009D-00	0.54979D 02	2.0036	0.80222D 00	0.65545D 02
1.9958	0.16136D-00	0.57667D 02	2.0038	0.81507D 00	0.62901D 02
1.9960	0.17316D-00	0.60352D 02	2.0040	0.82738D 00	0.60231D 02
1.9962	0.18550D-00	0.63021D 02	2.0042	0.83916D 00	0.57546D 02
1.9964	0.19837D-00	0.65663D 02	2.0044	0.85040D 00	0.54858D 02
1.9966	0.21176D-00	0.68263D 02	2.0046	0.86110D 00	0.52180D 02
1.9968	0.22567D-00	0.70809D 02	2.0048	0.87127D 00	0.49523D 02
1.9970	0.24008D-00	0.73287D 02	2.0050	0.88091D 00	0.46896D 02
1.9972	0.25498D-00	0.75683D 02	2.0052	0.89003D 00	0.44310D 02
1.9974	0.27035D-00	0.77984D 02	2.0054	0.89864D 00	0.41774D 02
1.9976	0.28616D-00	0.80176D 02	2.0057	0.91062D 00	0.38081D 02
1.9978	0.30241D-00	0.82248D 02	2.0060	0.92151D 00	0.34541D 02
1.9980	0.31905D-00	0.84185D 02	2.0065	0.93738D 00	0.29032D 02
1.9982	0.33607D-00	0.85977D 02	2.0070	0.95063D 00	0.24065D 02
1.9984	0.35344D-00	0.87612D 02	2.0075	0.96154D 00	0.19673D 02
1.9986	0.37111D-00	0.89080D 02	2.0080	0.97040D 00	0.15861D 02
1.9988	0.38906D-00	0.90372D 02	2.0085	0.97749D 00	0.12611D 02
1.9990	0.40724D-00	0.91478D 02	2.0090	0.98310D 00	0.98887D 01
1.9992	0.42563D-00	0.92393D 02	2.0095	0.98746D 00	0.76471D 01
1.9994	0.44419D-00	0.93110D 02	2.0100	0.99082D 00	0.58320D 01
1.9996	0.46286D-00	0.93624D 02	2.0105	0.99336D 00	0.43865D 01
1.9998	0.48162D-00	0.93932D 02	2.0110	0.99525D 00	0.32537D 01
2.0000	0.50042D 00	0.94031D 02			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000010

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
1.9885	0.50797D-02	0.32791D 01	2.0002	0.51828D 00	0.89112D 02
1.9890	0.69749D-02	0.43436D 01	2.0004	0.53608D 00	0.88841D 02
1.9895	0.94690D-02	0.56822D 01	2.0006	0.55381D 00	0.88394D 02
1.9900	0.12710D-01	0.73408D 01	2.0008	0.57142D 00	0.87773D 02
1.9905	0.16871D-01	0.93659D 01	2.0010	0.58890D 00	0.86982D 02
1.9910	0.22145D-01	0.11801D 02	2.0012	0.60621D 00	0.86026D 02
1.9915	0.28747D-01	0.14685D 02	2.0014	0.62330D 00	0.84911D 02
1.9920	0.36909D-01	0.18047D 02	2.0016	0.64016D 00	0.83642D 02
1.9925	0.46876D-01	0.21902D 02	2.0018	0.65675D 00	0.82228D 02
1.9930	0.58894D-01	0.26251D 02	2.0020	0.67304D 00	0.80677D 02
1.9935	0.73206D-01	0.31073D 02	2.0022	0.68901D 00	0.78996D 02
1.9940	0.90038D-01	0.36323D 02	2.0024	0.70463D 00	0.77196D 02
1.9945	0.10959D-00	0.41933D 02	2.0026	0.71988D 00	0.75286D 02
1.9948	0.12269D-00	0.45433D 02	2.0028	0.73474D 00	0.73277D 02
1.9950	0.13202D-00	0.47808D 02	2.0030	0.74919D 00	0.71179D 02
1.9952	0.14182D-00	0.50207D 02	2.0032	0.76321D 00	0.69003D 02
1.9954	0.15210D-00	0.52620D 02	2.0034	0.77678D 00	0.66760D 02
1.9956	0.16286D-00	0.55039D 02	2.0036	0.78991D 00	0.64460D 02
1.9958	0.17411D-00	0.57455D 02	2.0038	0.80257D 00	0.62116D 02
1.9960	0.18585D-00	0.59856D 02	2.0040	0.81475D 00	0.59737D 02
1.9962	0.19806D-00	0.62234D 02	2.0042	0.82646D 00	0.57334D 02
1.9964	0.21074D-00	0.64576D 02	2.0044	0.83768D 00	0.54919D 02
1.9966	0.22388D-00	0.66873D 02	2.0046	0.84843D 00	0.52499D 02
1.9968	0.23748D-00	0.69113D 02	2.0048	0.85868D 00	0.50086D 02
1.9970	0.25152D-00	0.71286D 02	2.0050	0.86846D 00	0.47689D 02
1.9972	0.26599D-00	0.73380D 02	2.0052	0.87776D 00	0.45316D 02
1.9974	0.28087D-00	0.75384D 02	2.0054	0.88659D 00	0.42974D 02
1.9976	0.29614D-00	0.77289D 02	2.0057	0.89896D 00	0.39539D 02
1.9978	0.31178D-00	0.79083D 02	2.0060	0.91032D 00	0.36214D 02
1.9980	0.32776D-00	0.80757D 02	2.0065	0.92710D 00	0.30972D 02
1.9982	0.34407D-00	0.82302D 02	2.0070	0.94137D 00	0.26159D 02
1.9984	0.36068D-00	0.83709D 02	2.0075	0.95334D 00	0.21820D 02
1.9986	0.37755D-00	0.84970D 02	2.0080	0.96327D 00	0.17975D 02
1.9988	0.39465D-00	0.86078D 02	2.0085	0.97140D 00	0.14623D 02
1.9990	0.41197D-00	0.87025D 02	2.0090	0.97797D 00	0.11748D 02
1.9992	0.42945D-00	0.87808D 02	2.0095	0.98322D 00	0.93216D 01
1.9994	0.44708D-00	0.88420D 02	2.0100	0.98736D 00	0.73043D 01
1.9996	0.46481D-00	0.88859D 02	2.0105	0.99059D 00	0.56524D 01
1.9998	0.48261D-00	0.89121D 02	2.0110	0.99307D 00	0.43198D 01
2.0000	0.50045D 00	0.89206D 02	2.0115	0.99495D 00	0.32604D 01

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000020

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
1.9825	0.28426D-02	0.13780D 01	2.0010	0.56344D 00	0.62279D 02
1.9850	0.88911D-02	0.38024D 01	2.0020	0.62469D 00	0.59972D 02
1.9875	0.24143D-01	0.89744D 01	2.0030	0.68294D 00	0.56324D 02
1.9900	0.57105D-01	0.18118D 02	2.0040	0.73697D 00	0.51592D 02
			2.0050	0.78586D 00	0.46091D 02
1.9910	0.77595D-01	0.22969D 02	2.0060	0.82901D 00	0.40160D 02
1.9920	0.10324D-00	0.28400D 02	2.0070	0.86615D 00	0.34128D 02
1.9930	0.13453D-00	0.34248D 02	2.0080	0.89733D 00	0.28286D 02
1.9940	0.17179D-00	0.40281D 02	2.0090	0.92286D 00	0.22865D 02
1.9950	0.21506D-00	0.46207D 02	2.0100	0.94326D 00	0.18027D 02
1.9960	0.26406D-00	0.51696D 02	2.0110	0.95914D 00	0.13862D 02
1.9970	0.31819D-00	0.56409D 02	2.0125	0.97604D 00	0.89185D 01
1.9980	0.37652D-00	0.60032D 02	2.0150	0.99118D 00	0.37740D 01
1.9990	0.43781D-00	0.62310D 02	2.0175	0.99718D 00	0.13660D 01
2.0000	0.50063D 00	0.63078D 02			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000030

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
1.9800	0.49394D-02	0.18466D 01	2.0010	0.55213D 00	0.51063D 02
1.9825	0.11995D-01	0.40307D 01	2.0020	0.60262D 00	0.49790D 02
1.9850	0.26523D-01	0.79280D 01	2.0030	0.65145D 00	0.47746D 02
1.9875	0.53503D-01	0.14051D 02	2.0040	0.69789D 00	0.45029D 02
1.9900	0.98690D-01	0.22439D 02	2.0050	0.74132D 00	0.41765D 02
1.9910	0.12303D-00	0.26282D 02	2.0060	0.78128D 00	0.38097D 02
1.9920	0.15130D-00	0.30275D 02	2.0070	0.81743D 00	0.34177D 02
1.9930	0.18359D-00	0.34297D 02	2.0080	0.84960D 00	0.30154D 02
1.9940	0.21986D-00	0.38212D 02	2.0090	0.87775D 00	0.26164D 02
1.9950	0.25993D-00	0.41869D 02	2.0100	0.90198D 00	0.22327D 02
1.9960	0.30347D-00	0.45119D 02	2.0110	0.92249D 00	0.18738D 02
1.9970	0.34999D-00	0.47817D 02	2.0125	0.94692D 00	0.13963D 02
1.9980	0.39887D-00	0.49839D 02	2.0150	0.97371D 00	0.78687D 01
1.9990	0.44941D-00	0.51088D 02	2.0175	0.98813D 00	0.39956D 01
2.0000	0.50077D 00	0.51503D 02	2.0200	0.99512D 00	0.18282D 01

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000040

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
			2.0010	0.54540D 00	0.44314D 02
			2.0020	0.58934D 00	0.43480D 02
			2.0030	0.63218D 00	0.42132D 02
			2.0040	0.67345D 00	0.40318D 02
1.9775	0.59799D-02	0.18953D 01	2.0050	0.71269D 00	0.38103D 02
1.9800	0.12747D-01	0.36797D 01	2.0060	0.74954D 00	0.35563D 02
1.9825	0.25332D-01	0.66070D 01	2.0070	0.78373D 00	0.32779D 02
1.9875	0.81463D-01	0.16850D 02	2.0080	0.81505D 00	0.29838D 02
1.9890	0.10980D-00	0.20995D 02	2.0090	0.84338D 00	0.26824D 02
1.9900	0.13226D-00	0.23934D 02	2.0100	0.86870D 00	0.23815D 02
1.9910	0.15769D-00	0.26945D 02	2.0110	0.89104D 00	0.20880D 02
1.9920	0.18615D-00	0.29958D 02	2.0125	0.91921D 00	0.16745D 02
1.9930	0.21758D-00	0.32894D 02	2.0150	0.95345D 00	0.10890D 02
1.9940	0.25188D-00	0.35670D 02	2.0175	0.97493D 00	0.65494D 01
1.9950	0.28884D-00	0.38199D 02	2.0200	0.98740D 00	0.36431D 01
1.9960	0.32817D-00	0.40399D 02	2.0225	0.99410D 00	0.18741D 01
1.9970	0.36950D-00	0.42195D 02			
1.9980	0.41240D-00	0.43523D 02			
1.9990	0.45638D-00	0.44336D 02			
2.0000	0.50089D 00	0.44603D 02			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000050

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
1.9750	0.62539D-02	0.17639D 01	2.0010	0.54082D 00	0.39685D 02
1.9775	0.12304D-01	0.31919D 01	2.0020	0.58024D 00	0.39084D 02
1.9800	0.22886D-01	0.54262D 01	2.0030	0.61886D 00	0.38110D 02
1.9825	0.40276D-01	0.86656D 01	2.0040	0.65634D 00	0.36790D 02
			2.0050	0.69234D 00	0.35162D 02
1.9850	0.67133D-01	0.13001D 02	2.0060	0.72658D 00	0.33272D 02
1.9865	0.88911D-01	0.16093D 02	2.0070	0.75881D 00	0.31171D 02
1.9880	0.11556D-00	0.19477D 02	2.0080	0.78887D 00	0.28911D 02
1.9890	0.13621D-00	0.21845D 02	2.0090	0.81660D 00	0.26549D 02
1.9900	0.15926D-00	0.24258D 02	2.0100	0.84195D 00	0.24137D 02
1.9910	0.18473D-00	0.26668D 02	2.0110	0.86488D 00	0.21725D 02
1.9920	0.21258D-00	0.29027D 02	2.0120	0.88541D 00	0.19360D 02
1.9930	0.24275D-00	0.31280D 02	2.0130	0.90363D 00	0.17081D 02
1.9940	0.27509D-00	0.33372D 02	2.0140	0.91962D 00	0.14920D 02
1.9950	0.30942D-00	0.35250D 02	2.0150	0.93351D 00	0.12903D 02
1.9960	0.34550D-00	0.36864D 02	2.0175	0.96016D 00	0.85901D 01
1.9970	0.38304D-00	0.38167D 02	2.0200	0.97738D 00	0.53722D 01
1.9980	0.42172D-00	0.39123D 02	2.0225	0.98785D 00	0.31562D 01
1.9990	0.46116D-00	0.39705D 02	2.0250	0.99383D 00	0.17420D 01
2.0000	0.50100D 00	0.39894D 02			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000060

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
			2.0010	0.53746D 00	0.36257D 02
			2.0020	0.57351D 00	0.35798D 02
			2.0030	0.60896D 00	0.35051D 02
			2.0040	0.64352D 00	0.34035D 02
1.9725	0.60771D-02	0.15698D 01	2.0050	0.67694D 00	0.32774D 02
1.9750	0.11321D-01	0.27106D 01	2.0060	0.70900D 00	0.31298D 02
1.9775	0.20123D-01	0.44430D 01	2.0070	0.73948D 00	0.29641D 02
1.9800	0.34152D-01	0.69131D 01	2.0080	0.76823D 00	0.27838D 02
1.9825	0.55381D-01	0.10210D 02	2.0090	0.79512D 00	0.25928D 02
1.9850	0.85882D-01	0.14315D 02	2.0100	0.82006D 00	0.23948D 02
1.9860	0.10111D-00	0.16150D 02	2.0110	0.84301D 00	0.21936D 02
1.9870	0.11821D-00	0.18068D 02	2.0120	0.86394D 00	0.19927D 02
1.9880	0.13726D-00	0.20047D 02	2.0130	0.88287D 00	0.17951D 02
1.9890	0.15831D-00	0.22057D 02	2.0140	0.89986D 00	0.16037D 02
1.9900	0.18138D-00	0.24068D 02	2.0150	0.91497D 00	0.14208D 02
1.9910	0.20644D-00	0.26045D 02	2.0160	0.92831D 00	0.12484D 02
1.9920	0.23344D-00	0.27949D 02	2.0175	0.94523D 00	0.10122D 02
1.9930	0.26230D-00	0.29745D 02	2.0200	0.96626D 00	0.68443D 01
1.9940	0.29288D-00	0.31392D 02	2.0225	0.98014D 00	0.43933D 01
1.9950	0.32503D-00	0.32856D 02	2.0250	0.98884D 00	0.26770D 01
1.9960	0.35852D-00	0.34103D 02	2.0275	0.99402D 00	0.15484D 01
1.9970	0.39315D-00	0.35104D 02			
1.9980	0.42864D-00	0.35834D 02			
1.9990	0.46472D-00	0.36276D 02			
2.0000	0.50109D 00	0.36418D 02			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000070

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
			2.0010	0.53485D 00	0.33588D 02
			2.0020	0.56828D 00	0.33221D 02
			2.0030	0.60122D 00	0.32625D 02
			2.0040	0.63345D 00	0.31812D 02
1.9700	0.56629D-02	0.13651D 01	2.0050	0.66478D 00	0.30798D 02
1.9725	0.10138D-01	0.22796D 01	2.0060	0.69499D 00	0.29604D 02
1.9750	0.17433D-01	0.36405D 01	2.0070	0.72393D 00	0.28254D 02
1.9775	0.28807D-01	0.55600D 01	2.0080	0.75146D 00	0.26774D 02
1.9800	0.45769D-01	0.81209D 01	2.0090	0.77744D 00	0.25190D 02
1.9825	0.69965D-01	0.11343D 02	2.0100	0.80181D 00	0.23532D 02
1.9850	0.10298D-00	0.15153D 02	2.0110	0.82449D 00	0.21826D 02
1.9860	0.11895D-00	0.16802D 02	2.0120	0.84546D 00	0.20100D 02
1.9870	0.13660D-00	0.18498D 02	2.0130	0.86469D 00	0.18378D 02
1.9880	0.15596D-00	0.20221D 02	2.0140	0.88222D 00	0.16685D 02
1.9890	0.17704D-00	0.21946D 02	2.0150	0.89808D 00	0.15039D 02
1.9900	0.19984D-00	0.23650D 02	2.0160	0.91232D 00	0.13460D 02
1.9910	0.22432D-00	0.25304D 02	2.0175	0.93083D 00	0.11244D 02
1.9920	0.25042D-00	0.26881D 02	2.0200	0.95480D 00	0.80401D 01
1.9930	0.27805D-00	0.28353D 02	2.0225	0.97158D 00	0.54978D 01
1.9940	0.30709D-00	0.29693D 02	2.0250	0.98282D 00	0.35953D 01
1.9950	0.33738D-00	0.30875D 02	2.0275	0.99002D 00	0.22485D 01
1.9960	0.36877D-00	0.31876D 02	2.0300	0.99443D 00	0.13448D 01
1.9970	0.40107D-00	0.32674D 02			
1.9980	0.43405D-00	0.33255D 02			
1.9990	0.46750D-00	0.33605D 02			
2.0000	0.50118D 00	0.33716D 02			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000080

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
1.9675	0.514150-02	0.117190 01	2.0010	0.532760 00	0.314320 02
1.9700	0.892960-02	0.190840 01	2.0020	0.564060 00	0.311310 02
1.9725	0.149700-01	0.298870 01	2.0030	0.594960 00	0.306410 02
1.9750	0.242340-01	0.450130 01	2.0040	0.625280 00	0.299710 02
			2.0050	0.654850 00	0.291320 02
1.9775	0.378990-01	0.651980 01	2.0060	0.683500 00	0.281410 02
1.9800	0.572870-01	0.908150 01	2.0070	0.711080 00	0.270140 02
1.9825	0.837440-01	0.121650 02	2.0080	0.737490 00	0.257700 02
1.9840	0.103520-00	0.142280 02	2.0090	0.762590 00	0.244310 02
1.9850	0.118470-00	0.156720 02	2.0100	0.786320 00	0.230170 02
1.9860	0.134880-00	0.171540 02	2.0110	0.808610 00	0.215490 02
1.9870	0.152780-00	0.186590 02	2.0120	0.829410 00	0.200500 02
1.9880	0.172200-00	0.201710 02	2.0130	0.848700 00	0.185390 02
1.9890	0.193120-00	0.216680 02	2.0140	0.866490 00	0.170340 02
1.9900	0.215520-00	0.231320 02	2.0150	0.882780 00	0.155550 02
1.9910	0.239370-00	0.245410 02	2.0160	0.897610 00	0.141150 02
1.9920	0.264580-00	0.258730 02	2.0170	0.911030 00	0.127290 02
1.9930	0.291080-00	0.271080 02	2.0185	0.928640 00	0.107730 02
1.9940	0.318760-00	0.282250 02	2.0200	0.943440 00	0.899120 01
1.9950	0.347490-00	0.292050 02	2.0225	0.962620 00	0.644690 01
1.9960	0.377120-00	0.300310 02	2.0250	0.976120 00	0.444550 01
1.9970	0.407490-00	0.306870 02	2.0275	0.985270 00	0.294790 01
1.9980	0.438430-00	0.311620 02	2.0300	0.991220 00	0.188000 01
1.9990	0.469750-00	0.314480 02	2.0325	0.994950 00	0.115300 01
2.0000	0.501260 00	0.315390 02			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000090

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
			2.0010	0.531040 00	0.296450 02
			2.0020	0.560570 00	0.293920 02
			2.0030	0.589770 00	0.289790 02
1.9650	0.458880-02	0.998370 00	2.0040	0.618480 00	0.284140 02
1.9675	0.778110-02	0.159440 01	2.0050	0.646550 00	0.277050 02
1.9700	0.127850-01	0.245930 01	2.0060	0.673850 00	0.268650 02
1.9725	0.203610-01	0.366400 01	2.0070	0.700240 00	0.259060 02
1.9750	0.314420-01	0.527250 01	2.0080	0.725620 00	0.248420 02
1.9775	0.470970-01	0.732820 01	2.0090	0.749900 00	0.236910 02
1.9800	0.684620-01	0.983780 01	2.0100	0.772980 00	0.224670 02
1.9810	0.788560-01	0.109610 02	2.0110	0.794810 00	0.211890 02
1.9820	0.904040-01	0.121440 02	2.0120	0.815350 00	0.198720 02
1.9830	0.103160-00	0.133810 02	2.0130	0.834550 00	0.185350 02
1.9840	0.117180-00	0.146620 02	2.0140	0.852410 00	0.171910 02
1.9850	0.132500-00	0.159760 02	2.0150	0.868940 00	0.158570 02
1.9860	0.149140-00	0.173120 02	2.0160	0.884130 00	0.145450 02
1.9870	0.167120-00	0.186550 02	2.0170	0.898040 00	0.132670 02
1.9880	0.186450-00	0.199920 02	2.0180	0.910680 00	0.120350 02
1.9890	0.207100-00	0.213060 02	2.0190	0.922130 00	0.108570 02
1.9900	0.229050-00	0.225800 02	2.0200	0.932420 00	0.974000 01
1.9910	0.252240-00	0.237970 02	2.0210	0.941630 00	0.868930 01
1.9920	0.276620-00	0.249420 02	2.0225	0.953560 00	0.724620 01
1.9930	0.302090-00	0.259970 02	2.0250	0.969030 00	0.520700 01
1.9940	0.328570-00	0.269460 02	2.0275	0.979970 00	0.361390 01
1.9950	0.355940-00	0.277750 02	2.0300	0.987430 00	0.242270 01
1.9960	0.384080-00	0.284710 02	2.0325	0.992360 00	0.156870 01
1.9970	0.412840-00	0.290230 02	2.0350	0.995500 00	0.981050 00
1.9980	0.442070-00	0.294210 02			
1.9990	0.471630-00	0.296600 02			
2.0000	0.501340 00	0.297350 02			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000100

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
			2.0010	0.529590 00	0.281310 02
			2.0020	0.557630 00	0.279140 02
1.9625	0.404750-02	0.846600 00	2.0030	0.585380 00	0.275610 02
1.9650	0.673100-02	0.133100 01	2.0040	0.612300 00	0.270760 02
1.9675	0.108800-01	0.202830 01	2.0050	0.639490 00	0.264670 02
			2.0060	0.665600 00	0.257420 02
1.9700	0.170980-01	0.299570 01	2.0070	0.690940 00	0.249130 02
1.9725	0.261300-01	0.428850 01	2.0080	0.715390 00	0.239900 02
1.9750	0.388480-01	0.595020 01	2.0090	0.738890 00	0.229860 02
1.9775	0.562070-01	0.800180 01	2.0100	0.761340 00	0.219140 02
1.9800	0.791720-01	0.104300 02			
			2.0110	0.782700 00	0.207880 02
1.9810	0.901310-01	0.114950 02	2.0120	0.802910 00	0.196220 02
1.9820	0.102180-00	0.126060 02	2.0130	0.821930 00	0.184290 02
1.9830	0.115360-00	0.137550 02	2.0140	0.839760 00	0.172210 02
1.9840	0.129700-00	0.149340 02	2.0150	0.856380 00	0.160130 02
1.9850	0.145230-00	0.161340 02			
			2.0160	0.871790 00	0.148150 02
1.9860	0.161970-00	0.173420 02	2.0170	0.886010 00	0.136390 02
1.9870	0.179910-00	0.185490 02	2.0180	0.899080 00	0.124930 02
1.9880	0.199060-00	0.197400 02	2.0190	0.911010 00	0.113860 02
1.9890	0.219380-00	0.209030 02	2.0200	0.921870 00	0.103260 02
1.9900	0.240850-00	0.220240 02			
			2.0210	0.931680 00	0.931770 01
1.9910	0.263410-00	0.230900 02	2.0225	0.944590 00	0.791230 01
1.9920	0.287010-00	0.240860 02	2.0250	0.961740 00	0.587630 01
1.9930	0.311560-00	0.250000 02	2.0275	0.974300 00	0.422990 01
1.9940	0.336980-00	0.258200 02	2.0300	0.983200 00	0.295120 01
1.9950	0.363160-00	0.265330 02			
			2.0325	0.989320 00	0.199560 01
1.9960	0.390010-00	0.271300 02	2.0350	0.993400 00	0.130800 01
1.9970	0.417380-00	0.276020 02	2.0375	0.996040 00	0.830880 00
1.9980	0.445170-00	0.279420 02			
1.9990	0.473220-00	0.281460 02			
2.0000	0.501410 00	0.282090 02			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000200

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
			2.0020	0.541810 00	0.198370 02
			2.0040	0.581210 00	0.195320 02
1.9500	0.629900-02	0.887540 00	2.0060	0.619810 00	0.190400 02
1.9550	0.123860-01	0.160510 01	2.0080	0.657260 00	0.183760 02
1.9600	0.230240-01	0.272680 01	2.0100	0.693220 00	0.175590 02
1.9650	0.404960-01	0.435190 01			
			2.0120	0.727410 00	0.166110 02
1.9700	0.674620-01	0.652480 01	2.0140	0.759590 00	0.155580 02
1.9730	0.893180-01	0.807350 01	2.0160	0.789580 00	0.144260 02
1.9760	0.116050-00	0.976770 01	2.0180	0.817260 00	0.132440 02
1.9780	0.136760-00	0.109530 02	2.0200	0.842550 00	0.120380 02
1.9800	0.159870-00	0.121590 02			
			2.0220	0.865410 00	0.108330 02
1.9820	0.185400-00	0.133640 02	2.0240	0.885890 00	0.965120 01
1.9840	0.213310-00	0.145420 02	2.0260	0.904050 00	0.851300 01
1.9860	0.243530-00	0.156670 02	2.0280	0.919980 00	0.743420 01
1.9880	0.275930-00	0.167110 02	2.0300	0.933830 00	0.642760 01
1.9900	0.310300-00	0.176470 02			
			2.0350	0.960370 00	0.427650 01
1.9920	0.346430-00	0.184500 02	2.0400	0.977520 00	0.267290 01
1.9940	0.384000-00	0.190970 02	2.0450	0.987930 00	0.156940 01
1.9960	0.422700-00	0.195710 02	2.0500	0.993880 00	0.865630 00
1.9980	0.462160-00	0.198570 02			
2.0000	0.501990 00	0.199460 02			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000300

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
			2.0020	0.534970 00	0.162240 02
			2.0040	0.567270 00	0.160540 02
1.9350	0.405580-02	0.489670-00	2.0060	0.599120 00	0.157810 02
1.9400	0.727740-02	0.823260 00	2.0080	0.630320 00	0.154090 02
1.9450	0.125730-01	0.132760 01	2.0100	0.660690 00	0.149460 02
			2.0120	0.690050 00	0.144010 02
1.9500	0.209230-01	0.205360 01	2.0140	0.718250 00	0.137840 02
1.9550	0.335560-01	0.304700 01	2.0160	0.745150 00	0.131050 02
1.9600	0.518890-01	0.433650 01	2.0180	0.770640 00	0.123770 02
1.9650	0.774130-01	0.591970 01	2.0200	0.794630 00	0.116110 02
1.9700	0.111500-00	0.775120 01			
			2.0220	0.817070 00	0.108210 02
1.9720	0.127780-00	0.853360 01	2.0240	0.837900 00	0.100170 02
1.9740	0.145650-00	0.933250 01	2.0260	0.857130 00	0.921200 01
1.9760	0.165120-00	0.101380 02	2.0280	0.874760 00	0.841500 01
1.9780	0.186200-00	0.109410 02	2.0300	0.890810 00	0.763580 01
1.9800	0.208870-00	0.117280 02			
			2.0320	0.905320 00	0.688280 01
1.9820	0.233090-00	0.124890 02	2.0350	0.924350 00	0.581700 01
1.9840	0.258800-00	0.132100 02	2.0400	0.949400 00	0.425060 01
1.9860	0.285900-00	0.138800 02	2.0450	0.967350 00	0.297920 01
1.9880	0.314280-00	0.144880 02	2.0500	0.979690 00	0.200290 01
1.9900	0.343800-00	0.150210 02			
			2.0550	0.987820 00	0.129160 01
1.9920	0.374310-00	0.154710 02	2.0600	0.992970 00	0.798930 00
1.9940	0.405620-00	0.158280 02	2.0650	0.996090 00	0.474010-00
1.9960	0.437560-00	0.160860 02			
1.9980	0.469900-00	0.162400 02			
2.0000	0.502440 00	0.162860 02			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000400

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
			2.0020	0.531000 00	0.140610 02
			2.0040	0.559020 00	0.139490 02
1.9250	0.409130-02	0.427380-00	2.0060	0.586750 00	0.137690 02
1.9300	0.679970-02	0.671490 00	2.0080	0.614050 00	0.135240 02
			2.0100	0.640800 00	0.132160 02
			2.0120	0.666880 00	0.128510 02
1.9350	0.109840-01	0.102260 01	2.0140	0.692170 00	0.124340 02
1.9400	0.172520-01	0.150930 01	2.0160	0.716590 00	0.119710 02
1.9450	0.263500-01	0.215920 01	2.0180	0.740030 00	0.114670 02
1.9500	0.391530-01	0.299390 01	2.0200	0.762430 00	0.109290 02
1.9550	0.566150-01	0.402360 01			
			2.0220	0.783730 00	0.103650 02
1.9600	0.797030-01	0.524110 01	2.0240	0.803880 00	0.978130 01
1.9630	0.966280-01	0.605050 01	2.0260	0.822850 00	0.918410 01
1.9660	0.116050-00	0.690680 01	2.0280	0.840610 00	0.858040 01
1.9680	0.130460-00	0.749700 01	2.0300	0.857170 00	0.797640 01
1.9700	0.146050-00	0.809700 01			
			2.0320	0.872520 00	0.737800 01
1.9720	0.162850-00	0.870140 01	2.0340	0.886690 00	0.679040 01
1.9740	0.180850-00	0.930430 01	2.0360	0.899690 00	0.621840 01
1.9760	0.200060-00	0.989940 01	2.0380	0.911570 00	0.566620 01
1.9780	0.220440-00	0.104800 02	2.0400	0.922370 00	0.513730 01
1.9800	0.241960-00	0.110390 02			
			2.0450	0.944980 00	0.393410 01
1.9820	0.264580-00	0.115700 02	2.0500	0.962030 00	0.292000 01
1.9840	0.288220-00	0.120670 02	2.0550	0.974500 00	0.210070 01
1.9860	0.312820-00	0.125220 02	2.0600	0.983340 00	0.146470 01
1.9880	0.338280-00	0.129290 02	2.0650	0.989420 00	0.989870 00
1.9900	0.364500-00	0.132820 02			
			2.0700	0.993460 00	0.648390 00
1.9920	0.391370-00	0.135780 02	2.0750	0.996080 00	0.411640-00
1.9940	0.418770-00	0.138110 02			
1.9960	0.446570-00	0.139770 02			
1.9980	0.474630-00	0.140760 02			
2.0000	0.502820 00	0.141040 02			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000500

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
1.9200	0.583860-02	0.524790 00	2.0020	0.528360 00	0.125830 02
1.9250	0.904790-02	0.772170 00	2.0040	0.553450 00	0.125010 02
1.9300	0.137080-01	0.110810 01	2.0060	0.578330 00	0.123710 02
1.9350	0.203070-01	0.155090 01	2.0080	0.602900 00	0.121930 02
1.9400	0.294230-01	0.211720 01	2.0100	0.627070 00	0.119690 02
1.9450	0.417050-01	0.281870 01	2.0120	0.650750 00	0.117030 02
1.9500	0.578440-01	0.366010 01	2.0140	0.673860 00	0.113970 02
1.9550	0.785300-01	0.463540 01	2.0160	0.696320 00	0.110550 02
1.9580	0.933900-01	0.527750 01	2.0180	0.718060 00	0.106800 02
1.9600	0.104390-00	0.572560 01	2.0200	0.739020 00	0.102770 02
1.9620	0.116300-00	0.618690 01	2.0220	0.759150 00	0.984910 01
1.9640	0.129150-00	0.665870 01	2.0240	0.778400 00	0.940160 01
1.9660	0.142940-00	0.713790 01	2.0260	0.796740 00	0.893870 01
1.9680	0.157700-00	0.762100 01	2.0280	0.814150 00	0.846460 01
1.9700	0.173420-00	0.810430 01	2.0300	0.830600 00	0.798370 01
1.9720	0.190110-00	0.858390 01	2.0320	0.846080 00	0.750010 01
1.9740	0.207760-00	0.905560 01	2.0340	0.860600 00	0.701760 01
1.9760	0.226330-00	0.951510 01	2.0360	0.874160 00	0.653990 01
1.9780	0.245800-00	0.995800 01	2.0380	0.886760 00	0.607050 01
1.9800	0.266150-00	0.103800 02	2.0400	0.898440 00	0.561220 01
1.9820	0.287310-00	0.107760 02	2.0420	0.909220 00	0.516780 01
1.9840	0.309230-00	0.111440 02	2.0440	0.919130 00	0.473970 01
1.9860	0.331860-00	0.114770 02	2.0470	0.932420 00	0.413190 01
1.9880	0.355120-00	0.117740 02	2.0500	0.943960 00	0.356980 01
1.9900	0.378930-00	0.120290 02	2.0550	0.959690 00	0.274230 01
1.9920	0.403200-00	0.122420 02	2.0600	0.971620 00	0.205460 01
1.9940	0.427860-00	0.124080 02	2.0650	0.980460 00	0.150130 01
1.9960	0.452810-00	0.125260 02	2.0700	0.986840 00	0.107000 01
1.9980	0.477940-00	0.125960 02	2.0750	0.991330 00	0.743750 00
2.0000	0.503150 00	0.126140 02	2.0800	0.994420 00	0.504210 00

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000600

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
			2.0020	0.52647D 00	0.11490D 02
			2.0040	0.54939D 00	0.11427D 02
1.9100	0.48098D-02	0.40320D-00	2.0060	0.57215D 00	0.11327D 02
1.9150	0.72448D-02	0.57982D 00	2.0080	0.59467D 00	0.11190D 02
1.9200	0.10708D-01	0.81661D 00	2.0100	0.61689D 00	0.11018D 02
1.9250	0.15533D-01	0.11264D 01	2.0120	0.63872D 00	0.10812D 02
1.9300	0.22115D-01	0.15217D 01	2.0140	0.66011D 00	0.10575D 02
1.9350	0.30910D-01	0.20133D 01	2.0160	0.68100D 00	0.10309D 02
1.9400	0.42421D-01	0.26088D 01	2.0180	0.70133D 00	0.10016D 02
1.9450	0.57117D-01	0.33108D 01	2.0200	0.72105D 00	0.96990D 01
1.9500	0.75700D-01	0.41151D 01	2.0220	0.74011D 00	0.93608D 01
1.9530	0.88828D-01	0.46420D 01	2.0240	0.75848D 00	0.90043D 01
1.9560	0.10338D-00	0.51972D 01	2.0260	0.77612D 00	0.86326D 01
1.9580	0.11436D-00	0.55805D 01	2.0280	0.79300D 00	0.82486D 01
1.9600	0.12591D-00	0.59721D 01	2.0300	0.80911D 00	0.78556D 01
1.9620	0.13825D-00	0.63699D 01	2.0320	0.82442D 00	0.74563D 01
1.9640	0.15139D-00	0.67717D 01	2.0340	0.83893D 00	0.70538D 01
1.9660	0.16534D-00	0.71748D 01	2.0360	0.85264D 00	0.66509D 01
1.9680	0.18009D-00	0.75766D 01	2.0380	0.86554D 00	0.62501D 01
1.9700	0.19564D-00	0.79743D 01	2.0400	0.87764D 00	0.58539D 01
1.9720	0.21198D-00	0.83649D 01	2.0420	0.88896D 00	0.54645D 01
1.9740	0.22909D-00	0.87455D 01	2.0440	0.89951D 00	0.50841D 01
1.9760	0.24695D-00	0.91130D 01	2.0460	0.90930D 00	0.47145D 01
1.9780	0.26553D-00	0.94643D 01	2.0480	0.91837D 00	0.43571D 01
1.9800	0.28480D-00	0.97965D 01	2.0500	0.92674D 00	0.40135D 01
1.9820	0.30471D-00	0.10107D 02	2.0550	0.94478D 00	0.32210D 01
1.9840	0.32521D-00	0.10392D 02	2.0600	0.95912D 00	0.25317D 01
1.9860	0.34625D-00	0.10649D 02	2.0650	0.97028D 00	0.19489D 01
1.9880	0.36779D-00	0.10877D 02	2.0700	0.97878D 00	0.14693D 01
1.9900	0.38974D-00	0.11073D 02	2.0750	0.98513D 00	0.10849D 01
1.9920	0.41205D-00	0.11235D 02	2.0800	0.98977D 00	0.78458D 00
1.9940	0.43466D-00	0.11361D 02	2.0850	0.99310D 00	0.55568D 00
1.9960	0.45747D-00	0.11450D 02	2.0900	0.99543D 00	0.38545D-00
1.9980	0.48043D-00	0.11502D 02			
2.0000	0.50345D 00	0.11515D 02			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000700

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
1.9050	0.57129D-02	0.43504D-00	2.0020	0.52504D 00	0.10640D 02
1.9100	0.82925D-02	0.60455D 00	2.0040	0.54627D 00	0.10589D 02
1.9150	0.11844D-01	0.82524D 00	2.0060	0.56738D 00	0.10509D 02
1.9200	0.16646D-01	0.11066D 01	2.0080	0.58829D 00	0.10399D 02
1.9250	0.23026D-01	0.14575D 01	2.0100	0.60895D 00	0.10261D 02
1.9300	0.31350D-01	0.18859D 01	2.0120	0.62932D 00	0.10096D 02
1.9350	0.42022D-01	0.23969D 01	2.0140	0.64932D 00	0.99054D 01
1.9400	0.55460D-01	0.29924D 01	2.0160	0.66892D 00	0.96906D 01
1.9450	0.72083D-01	0.36699D 01	2.0180	0.68807D 00	0.94534D 01
1.9500	0.92282D-01	0.44210D 01	2.0200	0.70672D 00	0.91957D 01
1.9520	0.10144D-00	0.47391D 01	2.0220	0.72484D 00	0.89196D 01
1.9540	0.11124D-00	0.50657D 01	2.0240	0.74239D 00	0.86270D 01
1.9560	0.12171D-00	0.53993D 01	2.0260	0.75934D 00	0.83202D 01
1.9580	0.13284D-00	0.57384D 01	2.0280	0.77566D 00	0.80014D 01
1.9600	0.14466D-00	0.60814D 01	2.0300	0.79134D 00	0.76729D 01
1.9620	0.15717D-00	0.64266D 01	2.0320	0.80635D 00	0.73369D 01
1.9640	0.17037D-00	0.67720D 01	2.0340	0.82068D 00	0.69956D 01
1.9660	0.18426D-00	0.71156D 01	2.0360	0.83433D 00	0.66512D 01
1.9680	0.19883D-00	0.74553D 01	2.0380	0.84729D 00	0.63057D 01
1.9700	0.21408D-00	0.77889D 01	2.0400	0.85955D 00	0.59610D 01
1.9720	0.22998D-00	0.81142D 01	2.0420	0.87113D 00	0.56192D 01
1.9740	0.24653D-00	0.84290D 01	2.0440	0.88203D 00	0.52818D 01
1.9760	0.26369D-00	0.87311D 01	2.0460	0.89226D 00	0.49505D 01
1.9780	0.28144D-00	0.90182D 01	2.0480	0.90184D 00	0.46268D 01
1.9800	0.29975D-00	0.92881D 01	2.0500	0.91078D 00	0.43119D 01
1.9820	0.31858D-00	0.95389D 01	2.0520	0.91909D 00	0.40069D 01
1.9840	0.33789D-00	0.97685D 01	2.0550	0.93045D 00	0.35703D 01
1.9860	0.35764D-00	0.99750D 01	2.0600	0.94660D 00	0.29040D 01
1.9880	0.37777D-00	0.10157D 02	2.0650	0.95963D 00	0.23202D 01
1.9900	0.39825D-00	0.10313D 02	2.0700	0.96995D 00	0.18210D 01
1.9920	0.41901D-00	0.10441D 02	2.0750	0.97798D 00	0.14039D 01
1.9940	0.43999D-00	0.10540D 02	2.0800	0.98411D 00	0.10632D 01
1.9960	0.46115D-00	0.10611D 02	2.0850	0.98872D 00	0.79089D 00
1.9980	0.48242D-00	0.10651D 02	2.0900	0.99212D 00	0.57794D 00
2.0000	0.50373D 00	0.10661D 02	2.0950	0.99458D 00	0.41485D-00

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000800

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
			2.0020	0.523920 00	0.995460 01
			2.0040	0.543790 00	0.991240 01
			2.0060	0.563550 00	0.984580 01
1.9000	0.639180-02	0.449520-00	2.0080	0.583160 00	0.975510 01
1.9050	0.902100-02	0.608840 00	2.0100	0.602560 00	0.964120 01
1.9100	0.125530-01	0.811840 00	2.0120	0.621710 00	0.950480 01
1.9150	0.172240-01	0.106580 01	2.0140	0.640560 00	0.934700 01
1.9200	0.233070-01	0.137740 01	2.0160	0.659080 00	0.916880 01
1.9250	0.311040-01	0.175260 01	2.0180	0.677230 00	0.897160 01
1.9300	0.409450-01	0.219540 01	2.0200	0.694960 00	0.875670 01
1.9350	0.531730-01	0.270740 01	2.0220	0.712240 00	0.852560 01
1.9400	0.681320-01	0.328710 01	2.0240	0.729050 00	0.827980 01
1.9450	0.861490-01	0.392910 01	2.0260	0.745350 00	0.802110 01
1.9480	0.985480-01	0.434040 01	2.0280	0.761130 00	0.775110 01
1.9500	0.107510-00	0.462370 01	2.0300	0.776350 00	0.747150 01
1.9520	0.117050-00	0.491320 01	2.0320	0.791010 00	0.718400 01
1.9540	0.127170-00	0.520790 01	2.0340	0.805080 00	0.689030 01
1.9560	0.137880-00	0.550640 01	2.0360	0.818570 00	0.659210 01
1.9580	0.149190-00	0.580750 01	2.0380	0.831450 00	0.629110 01
1.9600	0.161110-00	0.610970 01	2.0400	0.843730 00	0.598880 01
1.9620	0.173630-00	0.641170 01	2.0420	0.855400 00	0.568680 01
1.9640	0.186760-00	0.671180 01	2.0440	0.866480 00	0.538660 01
1.9660	0.200480-00	0.700840 01	2.0460	0.876950 00	0.508950 01
1.9680	0.214790-00	0.729980 01	2.0480	0.886840 00	0.479670 01
1.9700	0.229670-00	0.758440 01	2.0500	0.896140 00	0.450950 01
1.9720	0.245120-00	0.786040 01	2.0520	0.904880 00	0.422900 01
1.9740	0.261110-00	0.812610 01	2.0540	0.913060 00	0.395590 01
1.9760	0.277620-00	0.837980 01	2.0570	0.924340 00	0.356240 01
1.9780	0.294620-00	0.861980 01	2.0600	0.934460 00	0.319000 01
1.9800	0.312090-00	0.884460 01	2.0650	0.948960 00	0.262080 01
1.9820	0.329990-00	0.905260 01	2.0700	0.960780 00	0.211980 01
1.9840	0.348280-00	0.924240 01	2.0750	0.970270 00	0.168810 01
1.9860	0.366940-00	0.941260 01	2.0800	0.977770 00	0.132340 01
1.9880	0.385920-00	0.956200 01	2.0850	0.983610 00	0.102140 01
1.9900	0.405180-00	0.968950 01	2.0900	0.988080 00	0.776110 00
1.9920	0.424660-00	0.979420 01	2.0950	0.991460 00	0.580580 00
1.9940	0.444340-00	0.987530 01	2.1000	0.993960 00	0.427590-00
1.9960	0.464150-00	0.993230 01			
1.9980	0.484050-00	0.996460 01			
2.0000	0.503990 00	0.997210 01			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.000900

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
1.8900	0.491410-02	0.335560-00	2.0020	0.523020 00	0.938640 01
1.8950	0.687020-02	0.451730-00	2.0040	0.541760 00	0.935050 01
1.9000	0.948450-02	0.599740 00	2.0060	0.560410 00	0.929410 01
1.9050	0.129300-01	0.785260 00	2.0080	0.578930 00	0.921750 01
			2.0100	0.597270 00	0.912120 01
1.9100	0.174090-01	0.101400 01	2.0120	0.615400 00	0.900600 01
1.9150	0.231510-01	0.129130 01	2.0140	0.633280 00	0.887240 01
1.9200	0.304110-01	0.162170 01	2.0160	0.650880 00	0.872140 01
1.9250	0.394630-01	0.200870 01	2.0180	0.668150 00	0.855400 01
1.9300	0.505940-01	0.245360 01	2.0200	0.685080 00	0.837120 01
1.9350	0.640950-01	0.295580 01	2.0220	0.701630 00	0.817400 01
1.9400	0.802420-01	0.351170 01	2.0240	0.717770 00	0.796390 01
1.9450	0.992900-01	0.411460 01	2.0260	0.733480 00	0.774190 01
1.9480	0.112200-00	0.449490 01	2.0280	0.748730 00	0.750940 01
1.9500	0.121450-00	0.475450 01	2.0300	0.763510 00	0.726770 01
1.9520	0.131220-00	0.501790 01	2.0320	0.777800 00	0.701810 01
1.9540	0.141520-00	0.528420 01	2.0340	0.791580 00	0.676210 01
1.9560	0.152360-00	0.555230 01	2.0360	0.804840 00	0.650100 01
1.9580	0.163730-00	0.582110 01	2.0380	0.817580 00	0.623610 01
1.9600	0.175640-00	0.608930 01	2.0400	0.829780 00	0.596870 01
1.9620	0.188090-00	0.635570 01	2.0420	0.841450 00	0.570010 01
1.9640	0.201060-00	0.661910 01	2.0440	0.852580 00	0.543150 01
1.9660	0.214560-00	0.687810 01	2.0460	0.863180 00	0.516410 01
1.9680	0.228570-00	0.713130 01	2.0480	0.873240 00	0.489900 01
1.9700	0.243080-00	0.737750 01	2.0500	0.882780 00	0.463710 01
1.9720	0.258080-00	0.761520 01	2.0520	0.891790 00	0.437950 01
1.9740	0.273540-00	0.784310 01	2.0540	0.900300 00	0.412700 01
1.9760	0.289440-00	0.806000 01	2.0570	0.912130 00	0.375970 01
1.9780	0.305770-00	0.826440 01	2.0600	0.922870 00	0.340790 01
1.9800	0.322490-00	0.845530 01	2.0650	0.938520 00	0.286130 01
1.9820	0.339580-00	0.863130 01	2.0700	0.951580 00	0.236920 01
1.9840	0.357010-00	0.879150 01	2.0750	0.962310 00	0.193470 01
1.9860	0.374730-00	0.893470 01	2.0800	0.971020 00	0.155810 01
1.9880	0.392730-00	0.906010 01	2.0850	0.977990 00	0.123750 01
1.9900	0.410960-00	0.916700 01	2.0900	0.983480 00	0.969360 00
1.9920	0.429390-00	0.925440 01	2.0950	0.987760 00	0.748820 00
1.9940	0.447970-00	0.932200 01	2.1000	0.991040 00	0.570470 00
1.9960	0.466660-00	0.936930 01	2.1050	0.993530 00	0.428610-00
1.9980	0.485430-00	0.939580 01	2.1100	0.995380 00	0.317590-00
2.0000	0.504230 00	0.940160 01			

TABLE FOR THE EVALUATION OF THE FAXEN APPROXIMATION TO THE SOLUTION OF THE LAMM EQUATION

ETA = 0.001000

Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY	Y	PSI(Y,ETA)	DPSI(Y,ETA)/DY
1.8850	0.52342D-02	0.33673D-00	2.0020	0.52229D 00	0.89056D 01
1.8900	0.71791D-02	0.44550D-00	2.0040	0.54007D 00	0.88745D 01
1.8950	0.97356D-02	0.58210D 00	2.0060	0.55777D 00	0.88258D 01
1.9000	0.13054D-01	0.75112D 00	2.0080	0.57536D 00	0.87599D 01
1.9050	0.17309D-01	0.95719D 00	2.0100	0.59280D 00	0.86771D 01
1.9100	0.22695D-01	0.12047D 01	2.0120	0.61006D 00	0.85779D 01
1.9150	0.29430D-01	0.14973D 01	2.0140	0.62710D 00	0.84629D 01
1.9200	0.37748D-01	0.18378D 01	2.0160	0.64390D 00	0.83328D 01
1.9250	0.47891D-01	0.22278D 01	2.0180	0.66043D 00	0.81882D 01
1.9300	0.60108D-01	0.26671D 01	2.0200	0.67665D 00	0.80302D 01
1.9350	0.74640D-01	0.31533D 01	2.0220	0.69254D 00	0.78594D 01
1.9400	0.91712D-01	0.36818D 01	2.0240	0.70808D 00	0.76769D 01
1.9450	0.11152D-00	0.42455D 01	2.0260	0.72324D 00	0.74837D 01
1.9480	0.12478D-00	0.45967D 01	2.0280	0.73800D 00	0.72807D 01
1.9500	0.13421D-00	0.48348D 01	2.0300	0.75235D 00	0.70691D 01
1.9520	0.14412D-00	0.50750D 01	2.0320	0.76628D 00	0.68500D 01
1.9540	0.15451D-00	0.53165D 01	2.0340	0.77975D 00	0.66244D 01
1.9560	0.16539D-00	0.55583D 01	2.0360	0.79277D 00	0.63934D 01
1.9580	0.17674D-00	0.57996D 01	2.0380	0.80532D 00	0.61581D 01
1.9600	0.18858D-00	0.60392D 01	2.0400	0.81740D 00	0.59197D 01
1.9620	0.20090D-00	0.62762D 01	2.0420	0.82900D 00	0.56791D 01
1.9640	0.21368D-00	0.65095D 01	2.0440	0.84011D 00	0.54374D 01
1.9660	0.22693D-00	0.67379D 01	2.0460	0.85075D 00	0.51956D 01
1.9680	0.24063D-00	0.69604D 01	2.0480	0.86090D 00	0.49546D 01
1.9700	0.25477D-00	0.71759D 01	2.0500	0.87057D 00	0.47154D 01
1.9720	0.26933D-00	0.73833D 01	2.0520	0.87976D 00	0.44788D 01
1.9740	0.28430D-00	0.75816D 01	2.0540	0.88848D 00	0.42455D 01
1.9760	0.29965D-00	0.77695D 01	2.0570	0.90071D 00	0.39035D 01
1.9780	0.31537D-00	0.79463D 01	2.0600	0.91192D 00	0.35730D 01
1.9800	0.33143D-00	0.81108D 01	2.0650	0.92846D 00	0.30524D 01
1.9820	0.34780D-00	0.82622D 01	2.0700	0.94251D 00	0.25753D 01
1.9840	0.36447D-00	0.83997D 01	2.0750	0.95430D 00	0.21458D 01
1.9860	0.38139D-00	0.85223D 01	2.0800	0.96406D 00	0.17657D 01
1.9880	0.39855D-00	0.86295D 01	2.0850	0.97204D 00	0.14349D 01
1.9900	0.41590D-00	0.87206D 01	2.0900	0.97848D 00	0.11516D 01
1.9920	0.43342D-00	0.87950D 01	2.0950	0.98363D 00	0.91277D 00
1.9940	0.45107D-00	0.88523D 01	2.1000	0.98768D 00	0.71447D 00
1.9960	0.46881D-00	0.88922D 01	2.1050	0.99083D 00	0.55231D 00
1.9980	0.48662D-00	0.89145D 01	2.1100	0.99325D 00	0.42165D-00
2.0000	0.50446D 00	0.89189D 01	2.1150	0.99509D 00	0.31790D-00

Thanks are due to Dr. Robert Jastrow, Director, Goddard Institute for Space Studies, for use of the Institute's computing facilities.

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(Paper 70B1-171)

Publications of the National Bureau of Standards*

Selected Abstracts

A new differential operator of the pure wave type, J. E. Lagnese, *J. Different. Eq.* **1**, No. 2, 171–187 (Apr. 1965).

Consider the differential operator $\mathcal{L}u = u + c(t)u$ ($= \partial_t^2 - \sum_{i=1}^n \partial_{x_i}^2$) with $c(t)$ analytic on some open, connected interval of the real t -axis. Under this requirement, we seek to determine explicitly the form of $c(t)$ for which \mathcal{L} satisfies Huygen's principle in the sense of "Hadamard's premise." (Mathisson called such operators "pure wave".) *Theorem.* \mathcal{L} is of pure waves if, and only if, it is equivalent to one of the following operators: u , $u - \frac{2}{t^2}u$, $u - \frac{6}{t^2}u$, $u - \frac{6t(2+t^3)}{(1-t^3)^2}u$.

This theorem extends earlier results along this line and presents a new, and substantially more complicated, counterexample to "Hadamard's conjecture," namely the operator $u - 6t(2+t^3)/(1-t^3)^2 u$.

Aggregation in matrix models of resource flows, D. Rosenblatt, *Am. Stat.* **19**, No. 3, 36–39 (June 1965).

The aggregation of finite substochastic systems of the form $x(I-A)=w$, A a square and substochastic matrix and w a nonnegative vector, is considered from normative and descriptive standpoints in connection with models of resource flows. Certain of the fundamental functional equations of the theory of aggregation are derived and are given a graph theoretic interpretation.

An application of the inverse Z-transform theory to the synthesis of linear antenna arrays, M. T. Ma, *IEEE Trans. Ant. Prop.* **AP-12**, No. 6, 798–799 (Nov. 1964).

It has been known that the Z-transform theory can be applied as a new technique for analyzing linear array problems. The reverse problem, synthesizing linear arrays by applying the inverse Z-transform theory, has not yet been reported in the literature. This communication demonstrates that the job of synthesizing an antenna array, when certain conditions are satisfied by the given radiation pattern, can be accomplished particularly as a result of applying the inverse Z-transform theory originally developed for sampled-data systems, and that the error occurring between the synthesized and specified patterns can be estimated.

Spacetime coordinate systems, G. E. Hudson, *Proc. Intern. Conf. Chronometry*, pp. 197–221 (Lausanne, Switzerland, June 1964).

The principle of covariance is sometimes said to preclude the necessity for specifying a set of coordinates operationally. A simple example illustrates that this is not the case. This leads to the basic problem of specifying coordinate systems of physical use and interest over the vast reaches of spacetime. Examples of two operational definitions for spacetime networks associated with the surface of a spinning sphere serve to make definite some of the requirements, and show the importance and use of the general Doppler effect. For space navigational purposes, the gravitational fields, medium refraction and dispersion, and instrument uncertainty are discussed.

The point of view we have adopted here stems from, but is not limited to, a consideration of general relativistic effects and uses much of the formalism of relativity theory. It suggests moreover, a new general approach to time synchronization, space communication, and tracking problems, which is reminiscent of the concept of "homologue" space introduced by various authors to eliminate major refraction effects in a medium, or of Fock's concept of harmonic coordinates. Of more importance is the demonstration that a generalized range and range-rate coordinate system introduced here can be identified with a class of "null" coordinate systems previously mentioned by Synge.

Correlated walk and diffusion equations in a driving force, J. R. Manning, *Phys. Rev.* **139**, No. 1A, A126–A135 (July 5, 1965).

The correlation factor for diffusion by a vacancy mechanism arises because an atom can exchange with a given vacancy more than once. This results in a series of correlated exchanges between the atom and vacancy. In order to include correlation effects in the diffusion equations, one must allow the atom sufficient time to complete any correlated series of jumps. With this in mind, the basic diffusion equations are derived in terms of the number N of correlated series. A complete description of planar diffusion then can be presented in terms of effective jump frequencies, where each jump is independent of previous jumps. The resulting equations are correct to first order in small quantities. This is shown to be true even where there are driving forces and a diffusion coefficient gradient. Final expressions for the diffusion coefficient, correlation factor, drift velocity, and diffusion flux are valid for diffusion in any direction in cubic crystals and along particular directions in non-cubic crystals. As an example, effects from a chemical concentration gradient are discussed.

Generalized master equation for quantum mechanical systems to all orders in the density, J. Weinstock, *Phys. Rev.* **136**, 2d series, No. 4A, A879–A888 (Nov. 1964).

An exact generalized master equation is derived for a large quantum mechanical system in the form of a power series in the density. This derivation is a quantum mechanical generalization of a previous work by the author for classical systems. The quantum equation can be viewed as a time-dependent analog of the virial expansion of the quantum mechanical partition function for both degenerate systems (B.E. or F.D. statistics) and non-degenerate systems. The coefficients of the series, in the quantum equation, are explicitly given in terms of operators (Green functions) which are determined by the dynamics of isolated groups of particles and are convergent functions of the interaction potential. Equations are obtained for the off-diagonal elements of the density matrix as well as for the diagonal elements. The equation for the diagonal elements is shown to reduce to a Markoffian master equation for asymptotically long times, and an explicit expression is obtained for the "scattering" operator of this asymptotic equation.

Master equations and Markov processes, I. Oppenheim and K. E. Shuler, *Phys. Rev.* **138**, No. 4B, B117–B1011 (May 24, 1965).

The processes described by generalized master equations (GME), derived from the Liouville equation on the basis of various physical and dynamic arguments, have been termed Markovian or non-Markovian depending upon whether the GME did not or did involve an explicit time integration. We have shown here that these designations are not in accord with the (very specific) mathematical definition of a Markov and a non-Markovian process. We suggest that the much more appropriate terms Pauli process (or equation) and non-Paulian process (or equation) be used instead to designate processes described by the GME.

Analogies between theories of antenna arrays and passive networks, M. T. Ma., *IEEE Intern. Conv. Record* **13**, Pt. 5, 150–154 (Mar. 1965).

This paper demonstrates the analogy between two different fields, antenna arrays and passive networks, which are generally not known to each other. Successful application, either directly or with modification, of various known techniques for synthesizing a passive network, when an impulse response is specified, to the synthesis of linear antenna arrays with amplitude excitations, phase distributions and element spacings as the controlling parameters, when a desired radiation pattern is given, is presented with many interesting examples.

Approximations to the distribution of quadratic forms, M. M. Siddiqui, *Ann. Math. Stat.* **36**, No. 2, 677-682 (Apr. 1965). Let $Q = 1/2 \sum_{j=1}^{2k} a_j X_j^2$, where $0 < a_1 \leq a_2 \leq \dots \leq a_{2k}$ are constants and X_1, \dots, X_{2k} are independent $N(0, 1)$ variates. If a_j 's are equal within groups of even sizes the distribution of Q can be evaluated exactly; otherwise some approximations to this distribution are needed. In the present paper an approximation to $F(x) = Pr(Q > x)$ is obtained by bounding Q by Q_1 and Q_2 , where Q_1 and Q_2 are quadratic forms whose exact distributions can be evaluated. Let $F_i(x) = Pr(Q_i > x)$, $i = 1, 2$, and let $\hat{F}(x) = (1 - \theta) F_1(x) + \theta F_2(x)$. The approximation to $F(x)$ is obtained by minimizing $d(F, \hat{F})$ for variations of θ where $d(\cdot, \cdot)$ is the distance function of the metric space $L^2(0, \infty)$.

Estimation for a one-parameter exponential model, J. A. Speckman and R. G. Cornell, *J. Amer. Stat. Assoc.* **60**, 560-572 (1965).

The partial totals estimation procedure is presented, illustrated and evaluated for the model $y = \exp(-\rho t) + e$ when the values of t are equally spaced. Tables of estimates using this estimation procedure are given for the case where the smallest value of t is zero. The evaluation consists of an analytical investigation of the large sample properties of the partial totals estimator and a comparative study of its small sample properties relative to three other estimators based on Monte Carlo results where it is assumed either that y is a binomial proportion or that y is a proportion with variance proportional to a binomial variance.

Inequalities for permanents and permanent minors, R. A. Brualdi and M. Newman, *Proc. Cambridge Phil. Soc.* **61**, pt. 3, 741-746 (Jan. 26, 1965).

The principal result of this paper is that for all non-negative doubly-stochastic matrices A and all α such that $0 \leq \alpha \leq 1$, $\text{per}(\alpha A + (1 - \alpha)A) \leq \alpha + (1 - \alpha)\text{per}(A)$, where $\text{per}(A)$ denotes the permanent of A .

On the binary collision expansion of the classical N -body Green's function, J. Weinstock, *Phys. Rev.* **126**, No. 1, 341-344 (Apr. 1, 1962).

The explicit time integrations in the formal Binary Collision Expansion of the classical N -body Green's function are performed to obtain a product of binary collision operators which bears a strong resemblance to the Mayer product of f_{ij} 's. These integrations are exact for hard sphere interactions and are expected to be a good approximation for finite but short range pair interactions. The resulting expansion can be averaged over configuration space to obtain a transport equation for a dense gas in analogy with the cluster expansion of the classical partition function.

On matching problems, J. Edmonds, A. J. Goldman, C. Witzgall, C. T. Zahn, Jr., *Proc. ARO Working Group on Computer, ARO-D Report 65-1*, pp. 46-50 (Office Chief Res. and Develop., Feb. 1964).

Combinatorial optimization problems, although finite, remain intractable in practice so long as all known solution methods involve an amount of labor which increases exponentially with problem size. The present paper reports the recent development, by members of the Combinatorial Mathematics Project at the National Bureau of Standards, of efficient solution and checking algorithms for one class of problems. The prototype of this class is the problem of finding in a linear graph a set of pairwise disjoint edges (a "matching") with as many edges as possible; several generalizations are also discussed.

Paths, trees, and flowers, J. Edmonds, *Can. J. Math.* **17**, 449-467 (1965).

A matching in a graph is a subset of its edges such that no two meet the same vertex. The theory of matchings is treated. In particular, an efficient algorithm is described for finding in a given graph a matching of maximum cardinality. The Konig theorem is generalized to arbitrary (non-bipartite) graphs.

Realization of semi-multipliers as multipliers, H. Fell and A. J. Goldman, *Am. Math. Mo.* **72**, No. 6, 641 (June-July 1965).

The semi-multipliers of a linear associative algebra A are linear transformations obeying a generalization of the formula imposed

on the multipliers of A by the associative law. Buck showed that A could be imbedded as an ideal in a very large algebra B so that each semi-multiplier of A was realized as a multiplier in B , and asked how to construct a smaller algebra B with the same property. This note presents such a construction.

Some remarks on certain generalized Dedekind sums, H. Rademacher, *Acta Arithmetica* **9**, Sec. 1, 97-105 (1964).

Some years ago the German mathematician C. Meyer introduced a certain generalization of the Dedekind sums. This paper has as its aim to formulate the "true" generalization, which lies behind all the previous attempts. In this new formulation the theorems become not only general but also really transparent. A reciprocity theorem is to be expected in this theory and is indeed fully established. The paper closes with a hint at a useful Euclidean algorithm.

The paper is dedicated to L. J. Mordell (who himself has made contributions to the theory of Dedekind sums). It is an invited paper for an anniversary volume.

Stochastic theory of diffusion in a plasma across a magnetic field, C. M. Tchen, *Proc. Intern. Symp. Diffusion, Feldafing, Germany, June 29-July 3, 1964*, pp. 118-123 (1964).

A stochastic theory is proposed to investigate the diffusion across a constant magnetic field for the cases of collision and collective oscillations. A general formula is obtained, which shows the two cases separately, and the underlying assumptions permitting such a separation are clarified. It is found that the diffusion by collective oscillations is determined by the wave energy, while the collisional diffusion is determined by the thermal energy.

Electromagnetic properties of a quantized relativistic electron-positron gas, L. A. Steinert, *Il Nuovo Cimento, Serie X* **36**, 935-953 (Apr. 1965).

A relativistic quantum statistical description is given of electromagnetic wave propagation in a uniformly magnetized electron-positron gas, with specific attention devoted to long wavelength propagation as determined by the "collective" approximation. Collisionless absorption effects derived from relativity theory are compared with those obtained from the corresponding nonrelativistic treatment, showing that the two theories predict substantially different effects even for "nonrelativistic" temperatures. Contrasts appear in the predicted characteristics of the cyclotron resonance absorption effect, including the fact that Landau damping is completely nonexistent in the relativistic gas for waves propagating at phase velocities exceeding the velocity of light.

Wave functions for anharmonic oscillators by perturbation methods, A. M. Shorb, R. Schroeder, and E. R. Lippincott, *J. Chem. Phys.* **37**, 1043 (Sept. 1, 1962).

Approximate wave functions and the corresponding energies are given in tabular form for anharmonic potentials which can be expanded in polynomial series up to the sixth power in the displacement, x .

Localized-induction concept on a curved vortex and motion of an elliptic vortex ring, R. J. Arms and F. R. Hama, *Phys. Fluids* **8**, No. 4, 553-559 (Apr. 1965).

The localized-induction concept for the induction effect of a smooth curved vortex on itself is derived. This concept is applicable to the limiting case of a vortex filament of infinitesimal core size and of negligible long-distance effect, and was already successfully utilized in the investigations of the motion and deformation of a curved vortex filament given various initial configurations. Two theorems obtained under this concept are that the arc length of a vortex filament and the projected area of a closed vortex filament are both invariant with respect to time. These theoretical predictions are examined by a numerical analysis of the motion of an initially plane elliptic vortex ring of various eccentricities.

Random-walk model of chain-polymer adsorption at a surface, R. J. Rubin, *J. Chem. Phys.* **43**, No. 7, 2392-2407 (Oct. 1, 1965). A random walk lattice model of adsorption of an isolated polymer chain at a solution surface is investigated. On neglecting the self-excluded volume, a number of one-dimensional characteristics of the monomer unit distribution are determined analytically in the limit of long polymer chains. On assuming that one end of the poly-

mer chain lies in the surface layer, the mean number of monomer units adsorbed in the surface layer $\nu(\theta, N)$ and the mean distance of the other end of the chain from the surface layer $z(\theta, N)$ are determined, where N is the number of monomer units in the chain and θ is the adsorption energy of each monomer unit in the surface layer measured in units of kT . The lattice models considered include the simple cubic, hexagonal, close-packed, face-centered cubic, and body-centered cubic lattices. In the limit in which $N \rightarrow \infty$, both $\nu(\theta, N)$ and $z(\theta, N)$ exhibit a very interesting discontinuity at a lattice-dependent adsorption energy θ_c . For example for $\theta > \theta_c$, $\nu(\theta, N)$ (which is also proportional to the average adsorption energy of a polymer chain) is proportional to N . For $\theta < \theta_c$, $\nu(\theta, N)$ is proportional to a constant of order unity; and for $\theta = \theta_c$, $\nu(\theta, N)$ is proportional to $N^{1/2}$. It is shown that the probability distribution of the end of the chain decreases exponentially with increasing distance from the surface layer for $\theta > \theta_c$. In addition, the mean number of monomer units in the k th layer from the surface is determined for $N \gg 1$ and $\theta > \theta_c$ and is found to decrease exponentially with increasing k . In effect, for $\theta > \theta_c$ the polymer chain exists in an adsorbed state. An improvement in the model, which includes short range correlation between successive steps in the random walk description, is also considered.

Interaction between configurations with several open shells, U. Fano, *Phys. Rev.* **140**, No. 1A, A67-A75 (Oct. 4, 1965). Antisymmetrized product wave functions are written for atomic configurations with an arbitrary number of partially or entirely filled shells. Interaction matrix elements between such configurations are calculated and a numerical evaluation is given for the autoionization of an inner excitation level of neon. A suitable notation keeps the analytical complexities within reasonable bounds.

Other NBS Publications

J. Res. NBS 69A (Phys. and Chem.), No. 6 (Nov.-Dec. 1965), 75 cents.

- Arc measurement of some argon transition probabilities. C. H. Popenoe and J. B. Shumaker, Jr.
- Theoretical interpretation of the third spectrum of gold (Au III). Y. Shadmi.
- Photopolarographic behavior of inorganic depolarizers. R. A. Durst and J. K. Taylor.
- Spectral structure of critical opalescence: binary mixture. R. D. Mountain.
- Irregularities in the NBS (1955) provisional temperature scale. H. M. Roder.
- Isotherms determined by the National Bureau of Standards acoustical thermometer in the liquid helium temperature range. G. Cataland and H. Plumb.
- Synthesis of D-glucose-3-¹⁴C and related compounds. H. L. Frush, L. T. Sniegowski, N. B. Holt, and H. S. Isbell.
- Correlation of large longitudinal deformations with different histories. L. J. Zapas and T. Craft.
- Crystallography of tetracalcium phosphate. W. E. Brown and E. F. Epstein.
- Electrode potentials in fused systems XII. Measurement of cation concentration in molten salts using glass membrane electrodes. K. H. Stern and S. E. Meador.

Radio Sci. J. Res. NBS/USNC-URSI 69D, No. 12 (December 1965), \$1.00

- Symposium on Planetary Atmospheres and Surfaces, May 1965:
 - I Session: Jupiter, as observed at long radio waves.
 - II Session: Jupiter, as observed at short radio waves.
 - III Session: Passive radio observations of Venus, Saturn, Mercury, Mars, and Uranus.
 - IV Session: Passive radio observations of the Moon.
 - V Session: Radar observations of the planets.
 - VI Session: Radar observations of the Moon.

Oxidation of polycyclic, aromatic hydrocarbons. A review of the literature, R. S. Tipson, NBS Mono. 87 (Sept. 17, 1965), 40 cents.

Spot diagrams for the prediction of lens performance from design

data, O. N. Stavroudis and L. E. Sutton, NBS Mono. 93 (Sept. 7, 1965), 75 cents.

- Thermodynamic and related properties of parahydrogen from the triple point to 100 °K at pressures to 340 atmospheres, H. M. Roder, L. A. Weber, and R. D. Goodwin, NBS Mono. 94 (Aug. 10, 1965), 75 cents.
- Specifications, tolerances, and other technical requirements for commercial weighing and measuring devices, NBS Handb. 44-3d edition (Oct. 12, 1965), \$2.00. Supersedes NBS Handb. 44-2d edition.
- Standard Reference Materials: Catalog and price list of standard materials issued by the National Bureau of Standards, NBS Misc. Publ. 260, (Oct. 1, 1965), 45 cents. Supersedes NBS Misc. Publ. 241.
- Standard Reference Materials: Methods for the chemical analysis of white cast iron standards, J. I. Shultz, NBS Misc. Publ. 260-6 (July 16, 1965), 45 cents.
- Hydraulic research in the United States 1965, ed. H. K. Middleton, NBS Misc. Publ. 270 (July 22, 1965), \$1.25.
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