

# Phase Equilibria in the System Niobium Pentoxide–Germanium Dioxide

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The phase equilibrium diagram for the system  $\text{Nb}_2\text{O}_5$ – $\text{GeO}_2$  has been determined experimentally, using the quenching technique and examining the samples by optical microscopy and x-ray powder diffractometry. The system contains one compound,  $9\text{Nb}_2\text{O}_5 \cdot \text{GeO}_2$ , which melts incongruently at  $1420^\circ\text{C}$ . A eutectic between this compound and  $\text{GeO}_2$  is located at about 97 mol percent  $\text{GeO}_2$  and  $1090^\circ\text{C}$ . The system does not show liquid immiscibility, and it is concluded that the ionic field strength limit for two-liquid separation in the series of glass formers occurs with the  $\text{Nb}^{+5}$  cation.

Key Words: Germanium dioxide, immiscibility, niobium pentoxide, phase equilibria.

## 1. Introduction

Liquid immiscibility in binary oxide systems appears to be confined to the glass forming systems. In a systematic search for the principles underlying two-liquid formation it is necessary to examine the effect of different glass-forming cations, e.g.,  $\text{B}^{+3}$ ,  $\text{Ge}^{+4}$ ,  $\text{Si}^{+4}$ , and also of different modifier cations, i.e., with varying charges and ionic radii. Many binary phase diagrams of glass formers with modifier oxides from Groups I and II of the Periodic Table have been reported [1].<sup>1</sup> Only a few systems with modifier oxides from Groups III and IV have been reported. Two pertinent systems from Group V have been published:  $\text{Nb}_2\text{O}_5$ – $\text{SiO}_2$  [2] and  $\text{Nb}_2\text{O}_5$ – $\text{V}_2\text{O}_5$  [3]. Finally, in Group VI, phase relationships in the system  $\text{WO}_3$ – $\text{B}_2\text{O}_3$  [4] have been established.

Determination of the phase diagrams of  $\text{Nb}_2\text{O}_5$  with  $\text{B}_2\text{O}_3$ ,  $\text{GeO}_2$ , and  $\text{P}_2\text{O}_5$  has been undertaken in order to complete the study of the effect of a cation of high charge ( $\text{Nb}^{+5}$ ) on immiscibility in a series of glass formers. This paper, therefore, reports the phase equilibrium relations in the  $\text{Nb}_2\text{O}_5$ – $\text{GeO}_2$  system and its bearing on immiscibility.

## 2. Sample Preparation and Test Methods

Starting materials for the preparation of mixtures consisted of high purity niobium pentoxide and electronic grade germanium dioxide, designated by the manufacturers as over 99.7 percent and 99.9+ percent pure, respectively. The  $\text{Nb}_2\text{O}_5$  contained the following impurities when examined by the general qualitative spectrochemical method: Si—less than 0.1 percent; Fe, Sn, Ti—0.001 to 0.01 percent; Ca, Mg—0.0001 to 0.001 percent, Cu—? Spectrographic analysis of the  $\text{GeO}_2$  showed: Si—0.001 to 0.01 percent; Ca, Mg—0.0001 to 0.001 percent; Cu—less than 0.0001 percent, Ag, Al, Fe—?

Calculated amounts of  $\text{Nb}_2\text{O}_5$  and  $\text{GeO}_2$  sufficient to yield 4-g batches, on an ignited basis, were weighed into plastic containers and blended with a high-speed mechanical mixer. The mixtures were formed into discs 16 mm in diameter by pressing in a mold at approximately 20,000 lb/in<sup>2</sup>. The disks were placed in covered platinum crucibles and calcined in air at  $800^\circ\text{C}$  for 15 hr, using an electrically heated furnace. The fired disks were ground in an agate mortar, re-mixed, pressed, and given a second heat treatment at about  $900^\circ\text{C}$  for 12 hr. The complete process of grinding and pressing was repeated a third time, and the specimens were heated in the range of 900 to  $1000^\circ\text{C}$  for 12 hr. Formulated compositions were used in constructing the phase diagram. Analyses of two small samples for  $\text{Nb}_2\text{O}_5$  only, by the Analytical Chemistry Division, were about 0.75 percent low.

The quenching technique was used to obtain sub-solidus and liquidus data on samples sealed in Pt tubes. Constant temperature control of the quenching furnace to within  $\pm 2^\circ\text{C}$  was achieved with a self-adjusting a-c bridge-type controller. Quenched samples were examined with the binocular and polarizing microscopes and by x-ray powder diffractometry (Ni-filtered  $\text{CuK}_\alpha$  radiation) using a high-angle Geiger-counter diffractometer. The technique of sample preparation as well as the apparatus and method have been described in previous publications [5].

The solidus value was deduced from observation of the first temperature at which the sample showed slumping, coupled with x-ray evidence that one of the phases was disappearing. The liquidus temperature was indicated by the formation of a concave meniscus, coupled with microscopic evidence of a quenched glass (for several compositions rich in  $\text{GeO}_2$ ) or x-ray evidence of large amounts of low-temperature niobia-type phases. The polarizing microscope was of limited value in the latter case.

Temperatures were measured with a Pt versus 90 Pt:10 Rh thermocouple which was taken from lengths of thermocouple wire which originally had been calibrated by the temperature physics section.

<sup>1</sup> Figures in brackets indicate the literature references at the end of this paper.

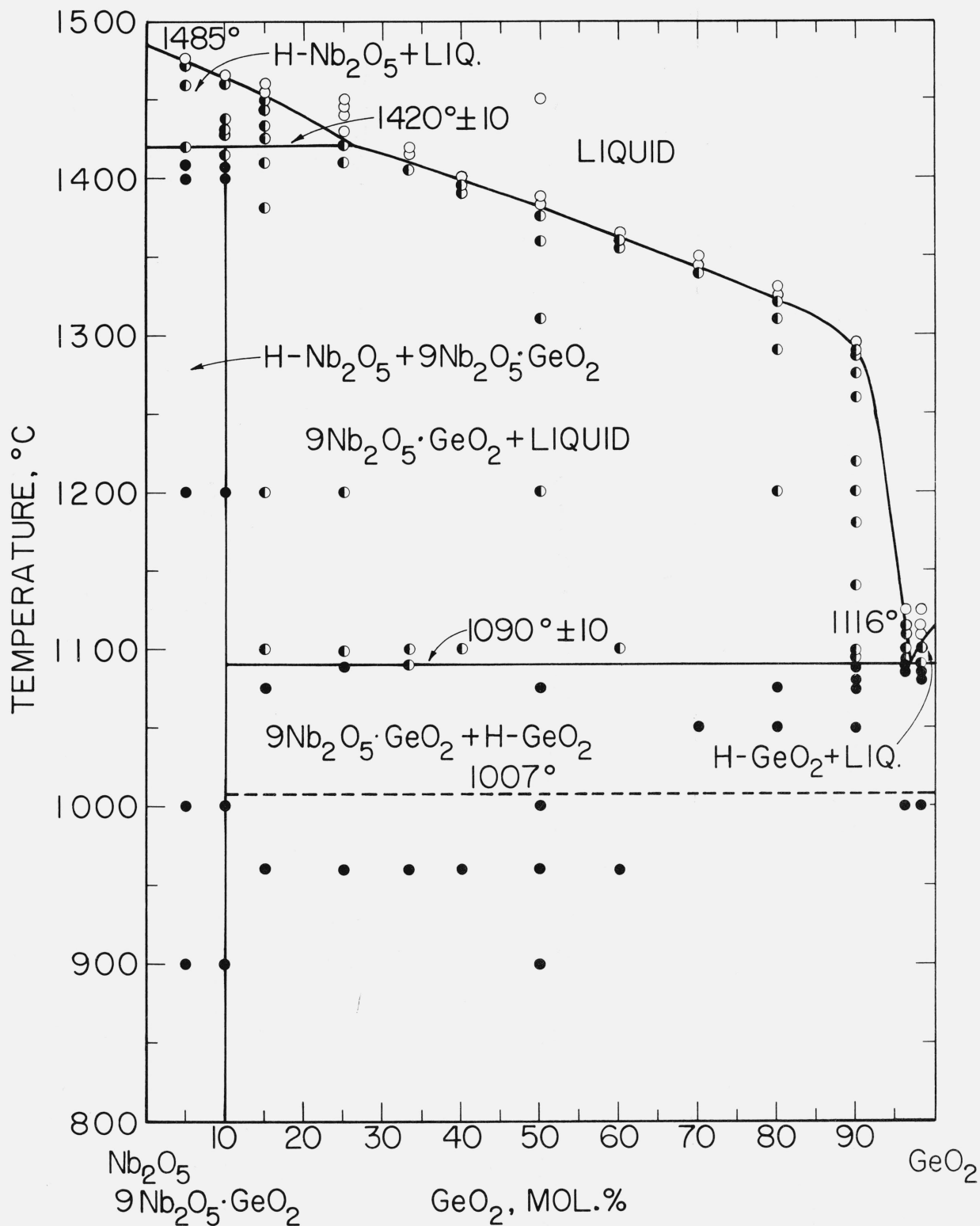


FIGURE 1. Phase equilibrium diagram for the system  $\text{Nb}_2\text{O}_5$ – $\text{GeO}_2$ .

● – No melting; ◐ – partial melting; ○ – complete melting.  
H– $\text{Nb}_2\text{O}_5$  – High-temperature form of  $\text{Nb}_2\text{O}_5$ .  
H– $\text{GeO}_2$  – Quartz form of  $\text{GeO}_2$ .

Temperatures are given on the International Practical Temperature Scale of 1961. During the course of the experiments the thermocouple was checked against the melting points of gold (1063 °C) and of barium disilicate (1420 °C). The overall maximum uncertainty of the temperature values reported herein is estimated to be within  $\pm 10$  °C.

### 3. Results and Discussions

#### 3.1. Nb<sub>2</sub>O<sub>5</sub> and GeO<sub>2</sub> Components

No quenching experiments were made with the components, as they were the same materials that had been used previously in phase equilibrium studies originating in this laboratory [3, 6, 7].

The Nb<sub>2</sub>O<sub>5</sub> used as starting material gave an x-ray pattern of poorly crystalline low-Nb<sub>2</sub>O<sub>5</sub> [8]. The so-called high temperature, monoclinic form [9] was the only stable modification encountered in the present work. This finding agrees with that reported in studies of other binary phase diagrams [9, 10].

The GeO<sub>2</sub> used as starting material was the high-temperature (quartz form) polymorph, and it was the only form detected throughout the experiments. In pure GeO<sub>2</sub> the transition from the low to the high form is given at 1007 °C [11], and the phase diagram is constructed on the assumption of no solid solubility of niobia in germania.

#### 3.2. Phase Diagram

Figure 1 shows the phase diagram for the system. Table 1 lists the compositions studied, the important heat treatments, and the phases identified, as well as the indices for several quenched phases. The system is characterized by one eutectic point at about 97.0 mole percent, GeO<sub>2</sub> (3.0% Nb<sub>2</sub>O<sub>5</sub>) and 1090 °C and by one peritectic point at about 25 percent GeO<sub>2</sub> (75% Nb<sub>2</sub>O<sub>5</sub>) and 1420 °C. The latter temperature corresponds to the incongruent melting point of 9Nb<sub>2</sub>O<sub>5</sub> · GeO<sub>2</sub>, the only binary compound found in the system.

TABLE 1. Experimental data<sup>1</sup> for compositions in the binary system Nb<sub>2</sub>O<sub>5</sub>–GeO<sub>2</sub>

| Composition                    |                  | Heat treatment <sup>2</sup> |       | Results               |  | Notes                          |
|--------------------------------|------------------|-----------------------------|-------|-----------------------|--|--------------------------------|
| Nb <sub>2</sub> O <sub>5</sub> | GeO <sub>2</sub> | Temp.                       | Time  | Physical observation  | X-ray diffraction analyses <sup>3</sup>  |                                |
| Mole %                         | Mole %           | °C                          | Hours |                       |  |                                |
| 2.0                            | 98.0             | 1000                        | 12    | No melting.           | GeO <sub>2</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                      | Solidus.                       |
|                                |                  | 1080                        | 1     | No melting.           | GeO <sub>2</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                      |                                |
|                                |                  | 1084                        | 1.25  | No melting.           | GeO <sub>2</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                      |                                |
|                                |                  | 1090                        | 1.25  | Start of melting.     | GeO <sub>2</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                      |                                |
|                                |                  | 1100                        | 1     | Considerable melting. | GeO <sub>2</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                      |                                |
|                                |                  | 1109                        | 16    | Complete melting.     | Glass + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                                 |                                |
|                                |                  | 1114                        | 2     | Complete melting.     | Glass + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                                 |                                |
| 4.0                            | 96.0             | 1000                        | 12    | No melting.           | GeO <sub>2</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                      | N <sub>91</sub> = 1.613 (25°). |
|                                |                  | 1086                        | 1.25  | No melting.           | GeO <sub>2</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                      |                                |
|                                |                  | 1089                        | 1.5   | No melting.           | GeO <sub>2</sub> + Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                       |                                |
|                                |                  | 1093                        | 1     | Partial melting.      | [GeO <sub>2</sub> ] + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                   |                                |
|                                |                  | 1099                        | 1.5   | Considerable melting. | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + [GeO <sub>2</sub> ]                   |                                |
|                                |                  | 1109                        | 1.5   | Complete melting.     | Glass + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                                 |                                |
|                                |                  |                             |       |                       |  |                                |
| 10.0                           | 90.0             | 1050                        | 15    | No melting.           | GeO <sub>2</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                      | 1098°/18 hr starting material. |
|                                |                  | 1075                        | 67.5  | No melting.           | GeO <sub>2</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                      |                                |
|                                |                  | 1088                        | 18    | No melting.           | GeO <sub>2</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                      |                                |
|                                |                  | 1095                        | 2     | Start of melting.     | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + GeO <sub>2</sub>                      |                                |
|                                |                  | 1098                        | 18    | Partial melting.      | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + glass                                 |                                |
|                                |                  | 1200                        | 2     | Partial melting.      | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + glass                                 |                                |
|                                |                  | 1275                        | 1.5   | Considerable melting. | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + glass                                 |                                |
|                                |                  | 1287                        | 2     | Almost melted.        | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + glass                                 |                                |
|                                |                  | 1291                        | 2     | Almost melted.        |  |                                |
|                                |                  | 1295                        | 1.75  | Complete melting.     | [L – Nb <sub>2</sub> O <sub>5</sub> ] + glass  |                                |
|                                |                  |                             |       |                       |  |                                |
| 20.0                           | 80.0             | 1050                        | 15    | No melting.           | GeO <sub>2</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                      | N <sub>91</sub> = 1.771 (25°). |
|                                |                  | 1075                        | 67.5  | No melting.           | GeO <sub>2</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                      |                                |
|                                |                  | 1200                        | 5     | Partial melting.      | GeO <sub>2</sub> + glass   |                                |
|                                |                  | 1310                        | 1.5   | Considerable melting. | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + [L – Nb <sub>2</sub> O <sub>5</sub> ] |                                |
|                                |                  | 1320                        | 1     | Almost melted.        | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + [L – Nb <sub>2</sub> O <sub>5</sub> ] |                                |
|                                |                  | 1325                        | 1     | Complete melting.     |  |                                |
|                                |                  | 1330                        | 2     | Complete melting.     | [L – Nb <sub>2</sub> O <sub>5</sub> ]  |                                |
|                                |                  |                             |       |                       |  |                                |
| 30.0                           | 70.0             | 1050                        | 15    | No melting.           | GeO <sub>2</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                      | N <sub>91</sub> = 1.84.        |
|                                |                  | 1339                        | 1.5   | Considerable melting. | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + [L – Nb <sub>2</sub> O <sub>5</sub> ] |                                |
|                                |                  | 1344                        | 2     | Complete melting.     | [L – Nb <sub>2</sub> O <sub>5</sub> ]  |                                |
|                                |                  |                             |       |                       |  |                                |
| 40.0                           | 60.0             | 960                         | 2.5   | No melting.           | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + GeO <sub>2</sub>                      |                                |
|                                |                  | 1100                        | 15    | Partial melting.      | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + glass                                 |                                |
|                                |                  | 1355                        | 1.5   | Considerable melting. | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + [L – Nb <sub>2</sub> O <sub>5</sub> ] |                                |
|                                |                  | 1360                        | 2     | Almost melted.        | [L – Nb <sub>2</sub> O <sub>5</sub> ] + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> |                                |
|                                |                  | 1365                        | 1.25  | Complete melting.     | [L – Nb <sub>2</sub> O <sub>5</sub> ]  |                                |
|                                |                  |                             |       |                       |  |                                |

TABLE 1. Experimental data<sup>1</sup> for compositions in the binary system Nb<sub>2</sub>O<sub>5</sub>—GeO<sub>2</sub>—Continued

| Composition                    |                  | Heat treatment <sup>2</sup> |       | Results               |  | Notes   |
|--------------------------------|------------------|-----------------------------|-------|-----------------------|--|---|
| Nb <sub>2</sub> O <sub>5</sub> | GeO <sub>2</sub> | Temp.                       | Time  | Physical observation  | X-ray diffraction analyses <sup>3</sup>  |   |
| Mole %                         | Mole %           | °C                          | Hours |                       |  |   |
| 50.0                           | 50.0             | 900                         | 1.75  | No melting.           | GeO <sub>2</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + [Nb <sub>2</sub> O <sub>5</sub> ]                      | L—GeO <sub>2</sub> not formed.                                  |
|                                |                  | 960                         | 456   | No melting.           | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + GeO <sub>2</sub>  |   |
|                                |                  | 1000                        | 1.75  | No melting.           | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + GeO <sub>2</sub>  |   |
|                                |                  | 1075                        | 144   | No melting.           | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + GeO <sub>2</sub>  |   |
|                                |                  | 1200                        | 5     | Partial melting.      | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>   |   |
|                                |                  | 1375                        | 1.5   | Considerable melting. | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + [L—Nb <sub>2</sub> O <sub>5</sub> ]                                       |   |
|                                |                  | 1379                        | 1.5   | Almost melted.        | [L—Nb <sub>2</sub> O <sub>5</sub> ] + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                                       |   |
|                                |                  | 1383                        | 1.5   | Complete melting.     | [L—Nb <sub>2</sub> O <sub>5</sub> ]  |   |
|                                |                  | 1450                        | 2     | Complete melting.     | [L—Nb <sub>2</sub> O <sub>5</sub> ]  |   |
|                                |                  | 960                         | 2.5   | No melting.           | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + GeO <sub>2</sub>  | At solidus.   |
|                                |                  | 1100                        | 15    | Just melting.         | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>   |   |
|                                |                  | 1390                        | 1.5   | Considerable melting. | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + [L—Nb <sub>2</sub> O <sub>5</sub> ]                                       |   |
|                                |                  | 1395                        | 2     | Almost melted.        | [L—Nb <sub>2</sub> O <sub>5</sub> ] + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                                       |   |
|                                |                  | 1400                        | 1.5   | Complete melting.     | [L—Nb <sub>2</sub> O <sub>5</sub> ]  |   |
| 60.0                           | 40.0             | 960                         | 2.5   | No melting.           | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + GeO <sub>2</sub>  |   |
|                                |                  | 1100                        | 15    | Just melting.         | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>   |   |
|                                |                  | 1390                        | 1.5   | Considerable melting. | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + [L—Nb <sub>2</sub> O <sub>5</sub> ]                                       |   |
|                                |                  | 1395                        | 2     | Almost melted.        | [L—Nb <sub>2</sub> O <sub>5</sub> ] + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                                       |   |
|                                |                  | 1400                        | 1.5   | Complete melting.     | [L—Nb <sub>2</sub> O <sub>5</sub> ]  |   |
| 66.7                           | 33.3             | 960                         | 2.5   | No melting.           | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + GeO <sub>2</sub>  | At solidus.   |
|                                |                  | 1090                        | 18    | Start of melting.     | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>   |   |
|                                |                  | 1100                        | 15    | Slight melting.       | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + glass   |   |
|                                |                  | 1405                        | 1     | Considerable melting. | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + [L—Nb <sub>2</sub> O <sub>5</sub> ]                                       |   |
|                                |                  | 1414                        | 1     | Complete melting.     | [L—Nb <sub>2</sub> O <sub>5</sub> ] + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>                                       |   |
| 75.0                           | 25.0             | 960                         | 2.5   | No melting.           | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + GeO <sub>2</sub>  | Decomp. 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> .    |
|                                |                  | 1090                        | 15    | No melting.           | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + GeO <sub>2</sub>  |   |
|                                |                  | 1098                        | 18    | Slight melting.       | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>   |   |
|                                |                  | 1200                        | 5     | Some melting.         | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>   |   |
|                                |                  | 1410                        | 1.1   | Partial melting.      | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>   |   |
|                                |                  | 1421                        | 2     | Considerable melting. | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + [L—Nb <sub>2</sub> O <sub>5</sub> ]                                       |   |
|                                |                  | 1430                        | 1.25  | Complete melting.     | [L—Nb <sub>2</sub> O <sub>5</sub> ] + [9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> ]                                    |   |
|                                |                  | 1438                        | 3.5   | Complete melting.     | [L—Nb <sub>2</sub> O <sub>5</sub> ]  |   |
|                                |                  | 960                         | 2.5   | No melting.           | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + GeO <sub>2</sub>  | Nonequilibrium.<br>Nonequilibrium.<br>Single phase.             |
|                                |                  | 1075                        | 144   | No melting.           | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + GeO <sub>2</sub>  |   |
| 85.0                           | 15.0             | 1100                        | 16    | Slight melting.       | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + glass   |   |
|                                |                  | 1200                        | 5     | Slight melting.       | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>   |   |
|                                |                  | 1409                        | 65    | Partial melting.      | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>   |   |
|                                |                  | 1427                        | 1.5   | Partial melting.      | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>   |   |
|                                |                  | 1433                        | 9     | Partial melting.      | [9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> ] + H—Nb <sub>2</sub> O <sub>5</sub>                                       |   |
|                                |                  | 1442                        | 3     | Considerable melting. | [9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> ] + H—Nb <sub>2</sub> O <sub>5</sub> + [L—Nb <sub>2</sub> O <sub>5</sub> ] |   |
|                                |                  | 1450                        | 1.5   | Considerable melting. | [9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> ] + H—Nb <sub>2</sub> O <sub>5</sub> + [L—Nb <sub>2</sub> O <sub>5</sub> ] |   |
|                                |                  | 1455                        | 2     | Complete melting.     | [L—Nb <sub>2</sub> O <sub>5</sub> ]  |   |
|                                |                  | 900                         | 12    | No melting.           | Nb <sub>2</sub> O <sub>5</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>  | At decomp. 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> . |
|                                |                  | 1000                        | 12    | No melting.           | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + H—Nb <sub>2</sub> O <sub>5</sub>  |   |
| 90.0                           | 10.0             | 1200                        | 5     | No melting.           | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>   |   |
|                                |                  | 1401                        | 2     | No melting.           | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>   |   |
|                                |                  | 1409                        | 1.75  | No melting.           | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>   |   |
|                                |                  | 1415                        | 2     | Slight slumping.      | 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + H—Nb <sub>2</sub> O <sub>5</sub>  |   |
|                                |                  | 1427                        | 2     | Partial melting.      | [9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> ] + [9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> ]                  |   |
|                                |                  | 1460                        | 1.5   | Considerable melting. | [9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> ] + H—Nb <sub>2</sub> O <sub>5</sub> + [L—Nb <sub>2</sub> O <sub>5</sub> ] |   |
|                                |                  | 1465                        | 1.5   | Complete melting.     | [L—Nb <sub>2</sub> O <sub>5</sub> ]  |   |
|                                |                  | 900                         | 12    | No melting.           | Nb <sub>2</sub> O <sub>5</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + [GeO <sub>2</sub> ]                      | Nonequilibrium.<br>Nonequilibrium.                              |
|                                |                  | 1000                        | 12    | No melting.           | Nb <sub>2</sub> O <sub>5</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> + [GeO <sub>2</sub> ]                      |   |
|                                |                  | 1200                        | 5     | No melting.           | H—Nb <sub>2</sub> O <sub>5</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>  |   |
| 95.0                           | 5.0              | 1400                        | 1.5   | No melting.           | H—Nb <sub>2</sub> O <sub>5</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>  |   |
|                                |                  | 1409                        | 2.75  | No melting.           | H—Nb <sub>2</sub> O <sub>5</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>  |   |
|                                |                  | 1421                        | 2     | Slight melting.       | H—Nb <sub>2</sub> O <sub>5</sub> + 9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub>  |   |
|                                |                  | 1459                        | 1.5   | Slight melting.       | H—Nb <sub>2</sub> O <sub>5</sub> + [9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> ]                                       |   |
|                                |                  | 1472                        | 1.5   | Considerable melting. | H—Nb <sub>2</sub> O <sub>5</sub> + [9Nb <sub>2</sub> O <sub>5</sub> · GeO <sub>2</sub> ] + [L—Nb <sub>2</sub> O <sub>5</sub> ] |   |
|                                |                  | 1476                        | 1.5   | Complete melting.     | [L—Nb <sub>2</sub> O <sub>5</sub> ] + [H—Nb <sub>2</sub> O <sub>5</sub> ]  |   |

<sup>1</sup> Only definitive data are given; figure 1 shows all of the heat treatments.<sup>2</sup> Specimens quenched in sealed Pt tubes.<sup>3</sup> Phases identified are listed in order of amount present at room temperature. Brackets enclose phases not necessarily present at the elevated temperature or not believed to be in final equilibrium. Only the high-temperature, hexagonal (quartz form) of GeO<sub>2</sub>(H-GeO<sub>2</sub>) was observed in these experiments. H—Nb<sub>2</sub>O<sub>5</sub> and L—Nb<sub>2</sub>O<sub>5</sub> refer to high and low temperature forms, respectively. Glass identified as a broad diffuse band in 18° to 28°—2θ range.<sup>4</sup> This phase quenched from the liquid indexes on a hexagonal unit cell basis (table 2).<sup>5</sup> This phase quenched from the liquid indexes on a pseudo-orthorhombic basis (table 2).

### 3.3. Compound 9Nb<sub>2</sub>O<sub>5</sub> · GeO<sub>2</sub>

This compound was reported by Waring and Roth [12] to be a tetragonal phase conforming to the general type 10M<sub>2</sub>O<sub>5</sub> · 90M<sub>2</sub>O<sub>5</sub> apparently isostructural with Ta<sub>2</sub>O<sub>5</sub> · 2Nb<sub>2</sub>O<sub>5</sub>. The existence of this phase and the unit cell dimensions<sup>2</sup> were verified in the present

$$^2 a = 15.70 \text{ \AA}, c = 3.817 \text{ \AA}.$$

study. The phase formed readily throughout the system at temperatures above 1000 °C. Decomposition of the phase above the incongruent melting point (1420 °C) was sluggish. For example, a sample of composition 85 percent Nb<sub>2</sub>O<sub>5</sub> heated at 1433 °C for 9 hr (table 1) still showed a considerable proportion of the compound.

In the eight reported isostructural compounds [12] of the general type 10M<sub>2</sub>O<sub>5</sub> · 90M<sub>2</sub>O<sub>5</sub>, Ge<sup>4+</sup> is the only

cation not pentavalent. It would be instructive for crystal chemical reasons to know if the compound composition were indeed exactly  $9\text{Nb}_2\text{O}_5 \cdot \text{GeO}_2$ . Results of the present study are consistent with the 9:1 ratio and indicate no solid solution region. However, limitations in the sensitivity of microscopic and x-ray detection of homogeneity preclude an unequivocal statement of the compound composition. For example, the ratio  $10\text{Nb}_2\text{O}_5 \cdot \text{GeO}_2$  contains 90.9 mole percent  $\text{Nb}_2\text{O}_5$ , and would not be distinguishable from the 9:1 composition.

### 3.4. Metastable Phases Quenched From Liquid

Two metastable low niobia-like phases were obtained from quenched liquids (see table 1, footnotes d and e, and table 2). Samples of composition  $50\text{Nb}_2\text{O}_5 : 50\text{GeO}_2$  and richer in niobia when quenched from the liquid gave a phase that could be partially indexed on the basis of low- $\text{Ta}_2\text{O}_5$  [13]. The several unindexed peaks (table 2), however, indicate that this cell is at best a subcell of low- $\text{Nb}_2\text{O}_5$ . The pseudo-orthorhombic cell has unit cell dimensions:  $a = 6.17 \text{ \AA}$ ,  $b = 3.64 \text{ \AA}$ , and  $c = 3.92 \text{ \AA}$ .

Samples in the composition range  $30\text{Nb}_2\text{O}_5 : 70\text{GeO}_2$  to  $10\text{Nb}_2\text{O}_5 : 90\text{GeO}_2$  quenched from the liquid to give a phase that could be indexed on a hexagonal unit cell basis:  $a = 3.60 \text{ \AA}$ ,  $c = 3.90 \text{ \AA}$ ,  $c/a = 1.088$ . In table 2 the coincidence of orthorhombic indices as related to the hexagonal indices is indicated. Thus, the orthorhombic (110) and (200) become the hexagonal (100), etc.

Quenches from the liquid of samples of composition  $40\text{Nb}_2\text{O}_5 : 60\text{GeO}_2$ , intermediate between the compo-

sition ranges for the two metastable phases, showed both phases (table 1). It should be noted, however, that no detectable change in unit cell dimensions with changing composition was noted for either metastable phase. Furthermore, as some  $\text{GeO}_2$ -rich glass was present in the quenched specimens, the exact composition limits of the metastable phases cannot be specified.

### 3.5. Application to Liquid Immiscibility Theory

From the standpoint of liquid immiscibility considerations, this system is noteworthy because of the absence of expected immiscibility. It is instructive to consider the following binary systems of  $\text{Nb}_2\text{O}_5$  with the glass formers:  $\text{B}_2\text{O}_3$ ,  $\text{SiO}_2$ , and  $\text{GeO}_2$ .

The  $\text{Nb}_2\text{O}_5 - \text{B}_2\text{O}_3$  [14] and  $\text{Nb}_2\text{O}_5 - \text{SiO}_2$  [2] systems have large regions of immiscibility, whereas the  $\text{Nb}_2\text{O}_5 - \text{GeO}_2$  system shows complete miscibility. In the hexavalent group of modifier cations, only the  $\text{WO}_3 - \text{B}_2\text{O}_3$  system has been reported [4]; and this system does not exhibit liquid immiscibility. The ionic field strength<sup>3</sup> (i.f.s.) of  $\text{Nb}^{+5}$  is greater than that of  $\text{Ge}^{+4}$ , slightly greater than that of  $\text{B}^{+3}$ , and less than that of  $\text{Si}^{+4}$ ; the i.f.s. of  $\text{W}^{+6}$  is considerably greater than that of  $\text{B}^{+3}$ ,  $\text{Ge}^{+4}$ , and  $\text{Si}^{+4}$ .

From the above information on immiscibility in oxide systems and i.f.s. of the modifier cations it may be concluded that the existence of immiscibility, per se, is not directly related to the extent of immiscibility. Whereas structural considerations determine the

<sup>3</sup> e.g., calculated as  $\frac{Z}{(R_+ + 1.40)^2}$ , where  $Z$  is the cationic charge and  $R_+$  and 1.40 are the ionic radii of the cation and oxygen, respectively.

TABLE 2. X-ray diffraction powder data for metastable low niobia-type phases quenched from liquid ( $\text{CuK}\alpha$  radiation)

| 50Nb <sub>2</sub> O <sub>5</sub> :50GeO <sub>2</sub><br>(quenched from 1450 °C/2hr) |                     |                  |                                 |                                  | 20Nb <sub>2</sub> O <sub>5</sub> :80GeO <sub>2</sub><br>(quenched from 1330 °C/2hr) |        |                  |                                 |                                  |
|---|---------------------|------------------|---------------------------------|----------------------------------|---|--------|------------------|---------------------------------|----------------------------------|
| hkl <sup>1</sup>  | d                   | I/I <sub>0</sub> | 1/d <sub>obs</sub> <sup>2</sup> | 1/d <sub>calc</sub> <sup>2</sup> | hkl <sup>2</sup>  | d      | I/I <sub>0</sub> | 1/d <sub>obs</sub> <sup>2</sup> | 1/d <sub>calc</sub> <sup>2</sup> |
| 001   | 5.18<br>3.922       | 8<br>100         | 0.0373<br>.0650                 | 0.0650                           | 001   | 3.912  | 93               | 0.0653                          | 0.0653                           |
| 110   | 3.136               | 94               | .1017                           | .1017                            | 100   | 3.114  | 100              | .1031                           | .1031                            |
| 200   | 3.084               | 63               | .1052                           | .1051                            |   |        |                  |                                 |                                  |
|   | 2.731               | 4                | .1341                           |                                  |   |        |                  |                                 |                                  |
| 111   | 2.449               | 45               | .1667                           | .1667                            | 101   | 2.437  | 43               | .1684                           | .1684                            |
| 201   | 2.425               | 25               | .1701                           |                                  |   |        |                  |                                 |                                  |
|   | 2.116               | 7                | .2234                           |                                  |   |        |                  |                                 |                                  |
|   | 2.010               | 8                | .2475                           |                                  |   |        |                  |                                 |                                  |
| 002   | 1.9604              | 25               | .2602                           | .2602                            | 002   | 1.9568 | 18               | .2612                           | .2612                            |
| 020   | 1.8212              | 11               | .3015                           | .3016                            | 110   | 1.7987 | 18               | .3091                           | .3093                            |
| 310   | 1.7908              | 20               | .3118                           | .3118                            |   |        |                  |                                 |                                  |
| 112   | 1.6625              | 15               | .3618                           | .3618                            | 102   | 1.6562 | 18               | .3645                           | .3644                            |
| 021   | 1.6570              | 14               | .3642                           | .3666                            |   |        |                  |                                 |                                  |
| 202   | 1.6537              | 14               | .3657                           | .3653                            |   |        |                  |                                 |                                  |
| 311   | 1.6297              | 10               | .3765                           | .3769                            | 111   | 1.6339 | 15               | .3746                           | .3746                            |
| 220   | 1.5690              | 7                | .4062                           | .4067                            | 200   | 1.5570 | 7                | .4125                           | .4123                            |
| 400   | 1.5436              | 4                | .4197                           | .4203                            |   |        |                  |                                 |                                  |
| 221   | 1.4576              | 7                | .4708                           | .4717                            |   |        |                  |                                 |                                  |
| 022   | <sup>3</sup> 1.3358 | 4                | .5605                           | .5618                            |   |        |                  |                                 |                                  |
| 312   | <sup>3</sup> 1.3214 | 5                | .5727                           | .5720                            |   |        |                  |                                 |                                  |

<sup>1</sup> Indices determined by analogy to low  $\text{Ta}_2\text{O}_5$  [13], but refer only to a pseudocell as several peaks cannot be indexed. Unit cell dimensions of the pseudocell are:  $a = 6.17 \text{ \AA}$ ,  $b = 3.64 \text{ \AA}$ ,  $c = 3.92 \text{ \AA}$ .

<sup>2</sup> Hexagonal unit cell dimensions:  $a = 3.59 \text{ \AA}$ ,  $c = 3.91 \text{ \AA}$ ,  $c/a = 1.088$ .

<sup>3</sup> Broad peak.

extent of the immiscible region [15], i.f.s. relationships between the glass-forming cation and the modifier cation largely govern the presence or absence of immiscibility. Just as the differences in i.f.s. between the modifier cation with oxygen and the glass-forming cation with oxygen can be too large to produce immiscibility, they may also be too small. The maximum i.f.s. difference occurs in the series of glass formers with  $\text{Ba}^{+2}$ , and the minimum occurs with  $\text{Nb}^{+5}$ . It may also be concluded that none of the hexavalent ions, e.g.,  $\text{Mo}^{+6}$ ,  $\text{Te}^{+6}$ ,  $\text{Cr}^{+6}$ , will show immiscibility phenomenon. These principles will be elaborated in future publications [16].

#### 4. Summary

The phase equilibrium diagram for the system  $\text{Nb}_2\text{O}_5\text{--GeO}_2$  has been constructed from "quenching" data on 13 selected compositions. Solidus and liquidus values were determined by examination of the samples with the binocular and polarizing microscopes and x-ray powder diffractometry.

The system was found to contain: one compound,  $9\text{Nb}_2\text{O}_5 \cdot \text{GeO}_2$ , melting incongruently at  $1420^\circ\text{C}$ ; one eutectic point between  $\text{GeO}_2$  and the compound, located at about 97 mole percent  $\text{GeO}_2$  and  $1090^\circ\text{C}$ ; and one peritectic point at about 25 mole percent  $\text{GeO}_2$  and  $1420^\circ\text{C}$ .

Although the 9:1 ratio of oxides in the  $9\text{Nb}_2\text{O}_5 \cdot \text{GeO}_2$  compound is consistent with the results, various limitations in the experimental method preclude an unequivocal statement as to the exactness of this ratio.

Two metastable low niobia-type phases were obtained from quenched liquids. A quenched liquid of composition  $50\text{Nb}_2\text{O}_5:50\text{GeO}_2$  gave an x-ray powder pattern that could be partially indexed on a subcell of low  $\text{Nb}_2\text{O}_5$ . It had pseudo-orthorhombic unit cell dimensions of  $a = 6.17 \text{ \AA}$ ,  $b = 3.64 \text{ \AA}$ ,  $c = 3.92 \text{ \AA}$ . The pattern of quenched liquid of composition  $20\text{Nb}_2\text{O}_5:80\text{GeO}_2$  was indexed on a hexagonal unit cell basis:  $a = 3.59_6 \text{ \AA}$ ,  $c = 3.91_3 \text{ \AA}$ .

Application of the results to liquid immiscibility theory leads one to the conclusion that a cation may

have too strong an ionic field strength, as well as one that is too weak, to produce two-liquid separation. Furthermore, the limiting maximum occurs in the series of  $\text{Nb}_2\text{O}_5$  with the glass formers, as  $\text{B}_2\text{O}_3$  and  $\text{SiO}_2$  both show large regions of immiscibility.

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