

Second Spectrum of Tungsten (W II)

Donald D. Laun¹

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A preliminary report on the second spectrum of tungsten, published in 1938, presented 27 even energy levels and 50 odd energy levels that were derived from 500 W II lines ranging in wavelength from 1961.43 Å to 4348.13 Å. The present paper submits data on 62 even levels, 132 odd levels, and 2,173 classified lines of W II, ranging in wavelength from 1756.6 Å to 6219.77 Å. The ground state of the W⁺ ion is represented by the ⁶D_{0½} level of a sextet D term arising from the 5d⁴6s¹ electron configuration, but the level intervals and magnetic splitting factors indicate considerable departure from LS-coupling, suggesting that coupling intermediate between LS and Jj may be more appropriate for the spectrum W II.

1. Introduction

The search for regularities among spectral lines emitted by tungsten arcs and sparks was initiated at the National Bureau of Standards in 1925 when O. Laporte and I were both new (temporary) members of the Spectroscopy Section. By exploiting existing data on wavelengths, intensities, and Zeeman patterns, Laporte [1]² identified the first spectral terms and classified lines of W I. Zeeman data confirmed the designation of the six lowest energy levels as ³D from 5d⁴6s² and ⁷S from 5d⁵6s¹. This term analysis and quantum interpretation of W I was later greatly extended by Laporte and Mack [2] until it included 300 energy levels and 2,378 classified lines ranging in wavelength from 2008.64 Å to 11477.97 Å.

Shortly after Laporte found the low-energy terms in W I, I began a search for the theoretical low ⁶D (from 5d⁴6s¹) and ⁶S (from 5d⁵) terms in W II, assuming that ionization removed one s electron. This initial search failed because of insufficient information about the spectrum W II. Then I undertook to reobserve the ultraviolet arc and spark spectra of tungsten, to distinguish W II from W I, to refine the wavelengths, and to observe Zeeman patterns of W II lines. From these observations, 27 even levels (including ⁶D and ⁶S) and 50 odd levels were derived from 500 W II lines ranging in wavelength from 1961.43 Å to 4348.13 Å; these results were published [3] in 1938 as a preliminary report on lines and levels of the spectrum W II. From time to time during the following quarter century, further improvements in observations and extensions of analyses have been made; the purpose of the present paper is to present the final data on 62 even levels, 132 odd levels, and 2,173 classified lines of W II, ranging in wavelength from 1756.6 Å to 6219.77 Å.

2. Experimental Procedure

Small rods of very pure tungsten were used as electrodes in the arcs and sparks that served as light sources. The arcs were operated with applied potential of 220 v and 6 amp dc, the sparks with 30,000 v, about 30 ma, ac, and 0.006 μf capacitance.

The first spectrograms were made in 1925 with a Hilger E 1 (Littrow) quartz spectrograph which could be effectively employed in the ultraviolet down to wavelength 1900 Å. Later, these spectrograms were supplemented by a new series obtained by C. C. Kiess with the first Hilger E 185 (Littrow) quartz spectrograph that was delivered to the Bureau of Standards in 1932. This larger spectrograph has a focal length of 3 m, and reciprocal dispersion, or plate factor, of 0.3 Å/mm at 2100 Å and 1 Å/mm at 3000 Å. These observations of tungsten lines on photographic plates exposed in quartz spectrographs were presented by me as a Master's Thesis at the University of Chicago [4]. Additional spectrograms were made in 1933 by Kiess with a concave grating of 22-ft radius, and 30,000 lines per inch. In a Wadsworth mounting, this grating produced spectra down to 1900 Å with a plate factor of 2.44 Å/mm in the first order, and with a plate factor of 0.88 Å/mm in the second order from 3200 to 4400 Å. This grating spectrograph was employed also to photograph tungsten spectra throughout the visible range.

Since all the above-mentioned spectrographs were stigmatic, movable diaphragms before the slits permitted placing strips of juxtaposed spectra on photographic plates. The usual procedure was to photograph the iron-arc spectrum containing standard wavelengths, then the tungsten arcs and sparks in adjacent strips and another iron spectrum beside the tungsten spark. The positions of tungsten spectral lines relative to iron lines were measured on Gaertner comparators, in 1925–26 at the Bureau of Standards; and in 1933–34 at Marquette University by courtesy of the late Fr. Joseph Carroll, S. J. Linear scale readings allowed the wavelengths of tungsten lines to be interpolated between iron

¹Former member of Spectroscopy Section, NBS; present address: Kiel, Wis.
²Figures in brackets indicate the literature references at the end of this paper.

standards in the case of prismatic spectra with the aid of Hartmann's dispersion formula, and from grating spectrograms by assuming linear dispersion. In both cases, small corrections were made when the interpolated values of iron wavelengths departed from their standard values. For purposes of analysis, the final wavelengths of tungsten lines were converted to vacuum wavenumbers with the aid of the Table of Wavenumbers published by Coleman, Bozman, and Meggers [5].

At the same time that the positions or wavelengths of tungsten lines were being measured, their relative intensities were estimated in both sources. Although this intensity scale, ranging from 1 for a barely discernible line to 1000 for the strongest, is more or less arbitrary, it is primarily useful in separating W_{II} from W_{I} , and also qualitatively supports the subsequent analysis in which intensities are related to quantum numbers. In some cases W_{II} lines appear to coincide with W_{I} , and if a W_{II} line sometimes appears stronger in the arc than in the spark, it may be an example of pole effect. Unfortunately, no deliberate attempt to exclude or exploit pole effect in the tungsten arc was made.

Finally, some information about tungsten spectra in the vacuum ultraviolet was obtained by measuring two spectrograms made by J. C. Boyce at the Massachusetts Institute of Technology in 1940 and kindly presented to the Bureau of Standards. These spectrograms were obtained with an evacuated grating spectrograph having a plate factor of 4.26 Å/mm. The spectra were measured down to 1200 Å. Although the excitation conditions were altered, the differences between spectra were so slight that only above 1756 Å was it possible positively to identify W_{II} lines. The wavelengths from this point to 1950 Å were finally corrected to the scale of values calculated from atomic energy levels.

My preliminary paper [3] of 1938 reported Zeeman-effect measurements of spectrograms made with a Weiss magnet and quartz spectrographs at the Bureau of Standards. These data have been superseded by those obtained with the more powerful Bitter magnet and grating spectrographs at the Massachusetts Institute of Technology. These results will be mentioned in the next section.

3. Results

The main result of the experiments mentioned above is that the wavelengths of about 13,000 spectral lines characteristic of arcs and sparks between tungsten electrodes have been measured. Among these, about 4,000 have been attributed to W_{II} and 2,173 of these lines, including 90 percent of the total intensity, have been shown to arise from transitions between 194 derived energy levels, 62 even and 132 odd. The even levels are displayed in table 1 and the odd levels in table 2. In these tables, the electron configuration is given in col-

umn 1, the spectral term designation in column 2, total angular momentum, J , in column 3, relative values of energy levels in column 4, intervals between levels of complex terms in column 5, and observed magnetic splitting factor, g , in column 6. Most of these data were supplied in 1956 for the third volume of Atomic Energy Levels [6] which contains J and level values for 45 even and 90 odd levels. In that volume, g -factors were reported for 38 even levels and for 58 odd. These were derived from MIT Zeeman spectrograms measured by J. E. Mack and Mrs. Taschek at the University of Wisconsin. Since 1956, the number of even levels has increased from 45 to 62 and odd levels from 90 to 132. Likewise, g -factors are now available for 46 even and 71 odd levels as compared with 38 and 58 respectively, in 1956.

In Atomic Energy Levels [6], it is stated that because of departure from LS -coupling it is difficult to assign term designations except for the lowest terms. Consequently, only six even terms, comprising 21 levels between 0 and 17437 K, were completely grouped and designated, and 24 higher even levels, between 18000 and 26929 K, were tentatively designated, guided by analogy with Mo_{II} , g -factors, and theoretical calculations of the late R. E. Trees. Likewise, two odd terms, comprising six levels, were tentatively designated 6F and 2S , but the remaining 84 levels were given as miscellaneous. In the present paper, additional levels and g -factors are reported but no revision or extension of designations has been made.

The spectral lines of tungsten from which all the information in tables 1 and 2 was derived, are listed in table 3 in order of increasing wavelength. Each line is described by its measured wavelength in angstroms, by its estimated intensity in a tungsten arc and/or spark, by its appropriate vacuum wavenumber in kaysers ($1\text{ K}=1\text{ cm}^{-1}$), by the difference ($O-C$) between the observed wavenumber and that calculated from the combination of energy levels shown in the next-to-last column. Abbreviated notes about the observed Zeeman patterns for 307 lines appear in the final column.

Table 3 contains 2,173 classified lines of W_{II} , including 42 doubly classified. The only other table of classified W_{II} lines was published [3] in 1938; it contained 500 lines, including 6 doubly classified. In addition to 2,173 classified lines, table 3 also contains wavelengths, intensities, and wavenumbers of 25 of the strongest W_{II} lines still unclassified; these are included with the hope that the blank spaces under "combinations" may eventually be filled in.

The "Intensity" column of table 3 shows that the great majority of these W_{II} lines were observed in arc as well as spark sources but with generally higher intensity in the latter when spectrogram exposures were chosen to make W_{I} lines appear in both sources with nearly equal intensities. In a few cases, W_{II} lines appear only, or stronger, in arc spectra; most if not all such deviations may be explained by coincident W_{I} lines, pole effects, or air lines that occa-

sionally mask metal lines in sparks operated at atmospheric pressure. Where the letter *A* follows an arc intensity, a line with nearly identical wavelength has actually been classified as a combination of W_I energy levels. The letter *d* in table 3 indicates a double line.

The observed minus calculated wavenumbers ($O-C$) have an average value of 0.1 K for wavelengths measured in air, that is, above 2000 Å. This means that the average error in these wavelength measurements is of the order of 0.01 Å, and there is high confidence that the great majority of the combinations are real, rather than accidental. However, in the vacuum ultraviolet, below 2000 Å, the average $O-C$ is considerably greater, in a few cases as large as 5 K, which entails an error in wavelength of the order of 0.2 Å. In such cases, confidence that the combinations are genuine is greatly reduced but they have been tentatively retained for the following reasons. Since the scale of wavenumbers is greatly compressed in the vacuum region, and the tungsten spectra below 2000 Å were photographed with relatively small dispersion and measured without adequate standard wavelengths, it was inevitable that these measured wavelengths of W_{II} lines would be more or less uncertain. Furthermore, it appears that most of these W_{II} short waves involve the lowest and adjacent metastable energy levels, which is precisely what should be expected of strong lines with high energy. Therefore, these combinations with relatively large $O-C$ may be regarded as real pending wavelength measurements of higher accuracy.

In the introduction, I mentioned that the first spectral terms, both in W_I and in W_{II} , were found from Zeeman-effect observations. In both spectra, such observations have greatly facilitated their analyses, and constitute the supreme test of validity. In the last column of table 3, are found some notes about the observed Zeeman patterns of 307 W_{II} lines extending from 2216 Å to 4358 Å. The Zeeman

patterns of W_I and W_{II} on MIT spectrograms were measured at the University of Wisconsin by J. E. Mack and Mrs. Taschek who supplied most of the magnetic splitting factors (*g*-factors) for tungsten levels that appear in Atomic Energy Levels [6]. Recently, those spectrograms were kindly loaned to me for examination. Without giving any details, I have merely written "res" to indicate resolved Zeeman patterns that agree with the combinations of W_{II} lines in table 3. Unresolved Zeeman patterns are numbered 4, 5, 6, and 7, according to the notation of Back and Landé [7]. Incidentally, Zeeman types 4, 5, and 6 uniquely characterize, and fix *J*-values of, energy levels belonging to even multiplicities such as those responsible for W_{II} lines. All the Zeeman-effect spectrograms are thickly covered by patterns of W_I lines, and the W_{II} patterns are often obscured, or vice versa, but despite these difficulties, the combinations are generally verified.

Finally, reference is made to the Tables of Spectral-Line Intensities by Meggers, Corliss, and Scribner [8] which list 1,300 tungsten lines, 1168 W_I and 132 W_{II} , observed in an arc between copper electrodes containing 0.1 atomic percent of tungsten. It is noteworthy that no W_{II} lines appear among the first 28 lines of highest intensity; they are all W_I . Tungsten is similar to rhenium in this respect, but unlike thorium or uranium in which spark lines predominate in this type of arc source. Ionization potentials may be responsible for this difference, since the I.P. of copper is less than that of tungsten or rhenium but greater than that of thorium or uranium. In the list of all observed lines of tungsten [8], all of the W_{II} lines are now classified, and will be given in this paper.

In conclusion, let me say that since my association with the Bureau of Standards in 1925-26, when this investigation began, and again in 1943-44, when I collaborated on the uranium project [9], this work on W_{II} has been pursued as a part-time occasional avocation with the goal of finding order in a complex spectrum.

TABLE 1. Even levels of W_{II}

Configuration	Designation	<i>J</i>	Level	Interval	Obs. <i>g</i>
$5d^4(^3D)6s$	<i>a</i> 6D	0½	0.00		3.186
		1½	1518.78	1518.78	1.839
		2½	3172.52	1653.74	1.639
		3½	4716.32	1543.80	1.563
		4½	6147.16	1430.84	1.522
$5d^5$	<i>a</i> 6S	2½	7420.43		1.913
$5d^4(^3F)6s$	<i>a</i> 4F	1½	8711.26	2589.82	0.624
		2½	11301.08	2110.88	1.084
		3½	13411.96	1445.26	1.186
		4½	14857.22		1.234

TABLE 1. *Even levels of W II—Continued*

Configuration	Designation	J	Level	Interval	Obs. g
$5d^4(^3P)6s$	$a\ ^4P$	$0\frac{1}{2}$	8832. 66		2. 383
		$1\frac{1}{2}$	10592. 52	1759. 86	1. 471
		$2\frac{1}{2}$	13434. 10	2841. 58	1. 526
$5d^4(^5D)6s$	$a\ ^4D$	$0\frac{1}{2}$	13173. 38		0. 455
		$1\frac{1}{2}$	14634. 36	1460. 98	1. 183
		$2\frac{1}{2}$	14967. 82	333. 46	1. 013
		$3\frac{1}{2}$	15147. 02	179. 20	0. 872
$5d^4(^3G)6s$	$a\ ^4G$	$2\frac{1}{2}$	16234. 84		0. 995
		$3\frac{1}{2}$	16589. 67	354. 83	1. 153
		$4\frac{1}{2}$	16553. 14	-36. 53	1. 137
		$5\frac{1}{2}$	17437. 02	883. 88	1. 181
$5d^4(^3H)6s$	4H	$3\frac{1}{2}$	18000. 70		1. 098
$5d^5$	2D	$1\frac{1}{2}$	18990. 96		0. 90
$5d^5$	4G	$4\frac{1}{2}$	19070. 68		1. 102
$5d^5$	4G	$2\frac{1}{2}$	19276. 52		0. 997
$5d^4(^3P)6s$	2P	$0\frac{1}{2}$	19404. 08		0. 64
$5d^4(^3H)6s$	4H	$6\frac{1}{2}$	19442. 54		
$5d^5$	2D	$2\frac{1}{2}$	19637. 38		1. 102
$5d^5$	4G	$3\frac{1}{2}$	20039. 74		1. 107
$5d^5$	4D	$1\frac{1}{2}$	20455. 93		0. 51
$5d^5$	4G	$5\frac{1}{2}$	20534. 35		1. 197
$5d^4(^3H)6s$	4H	$4\frac{1}{2}$	20780. 38		1. 065
$5d^5$	4F	$2\frac{1}{2}$	22139. 97		1. 06
$5d^5$	4F	$3\frac{1}{2}$	22194. 08		1. 119
$5d^4(^3P)6s$	2P	$1\frac{1}{2}$	22503. 06		1. 22
		$0\frac{1}{2}$	22535. 80		2. 2
$5d^4(^3D)6s$	4D	$3\frac{1}{2}$	23046. 80		0. 86
$5d^5$	4F	$4\frac{1}{2}$	23234. 87		1. 249
$5d^5$	4D	$2\frac{1}{2}$	23450. 50		1. 297
$5d^5$	4D	$3\frac{1}{2}$	23803. 84		
$5d^5$	2I	$5\frac{1}{2}$	23955. 40		1. 10
		$3\frac{1}{2}$	24804. 67		1. 10
$5d^5$	4F	$1\frac{1}{2}$	24918. 10		
		$1\frac{1}{2}$	24991. 56		0. 9
		$0\frac{1}{2}$	25045. 20		0. 32
$5d^5$	4P	$1\frac{1}{2}$	25169. 87		1. 64
		$4\frac{1}{2}$	25209. 28		
		$2\frac{1}{2}$	25672. 16		0. 9
		$4\frac{1}{2}$	26158. 74		
$5d^4(^3H)6s$	2H	$4\frac{1}{2}$	26227. 00		1. 04
$5d^5$	4P	$2\frac{1}{2}$	26929. 34		
$5d^5(^3H)6s$	2H	$5\frac{1}{2}$	27273. 86		
		$3\frac{1}{2}$	27273. 86		
		$2\frac{1}{2}$	28118. 90		
		$6\frac{1}{2}$	28187. 60		
		$5\frac{1}{2}$	28377. 80		
		$1\frac{1}{2}$	28491. 00		
		$3\frac{1}{2}$	28631. 86		
		$4\frac{1}{2}$	29341. 56		
		$4\frac{1}{2}$	30633. 02		
		$5\frac{1}{2}$	31100. 46		
		$5\frac{1}{2}$	33910. 56		1. 34
	$4\frac{1}{2}$	34091. 02			

TABLE 2. *Odd levels of W II*

Configuration	Designation	<i>J</i>	Level	Interval	Obs. g
$5d^4(^5D)6p$	$z\ ^6F^\circ$	$0\frac{1}{2}$	36165. 35		0. 678
		$1\frac{1}{2}$	39129. 41	2964. 06	1. 147
		$2\frac{1}{2}$	42049. 45	2920. 04	1. 292
		$3\frac{1}{2}$	44877. 18	2827. 73	1. 277
		$4\frac{1}{2}$	46493. 43	1616. 25	1. 311
		$5\frac{1}{2}$	51495. 00	5001. 57	1. 054
$5d^4(^3P)6p$	$z\ ^2S^\circ$	$0\frac{1}{2}$	38576. 32		1. 614
		$2\frac{1}{2}$	39936. 81		0. 889
		$1\frac{1}{2}$	42298. 20		1. 498
		$3\frac{1}{2}$	42390. 27		1. 161
		$2\frac{1}{2}$	44354. 82		1. 390
		$0\frac{1}{2}$	44455. 18		-0. 217
		$4\frac{1}{2}$	44758. 10		1. 270
		$1\frac{1}{2}$	44911. 63		1. 221
		$0\frac{1}{2}$	45457. 02		0. 519
		$1\frac{1}{2}$	45553. 70		1. 033
		$3\frac{1}{2}$	46175. 42		1. 452
		$2\frac{1}{2}$	46355. 40		1. 236
		$0\frac{1}{2}$	46625. 27		1. 70
		$1\frac{1}{2}$	47179. 94		1. 007
		$2\frac{1}{2}$	47413. 33		1. 111
		$1\frac{1}{2}$	47588. 64		2. 00
		$2\frac{1}{2}$	48284. 48		1. 366
		$5\frac{1}{2}$	48332. 73		
		$3\frac{1}{2}$	48830. 70		1. 008
		$1\frac{1}{2}$	48982. 86		1. 72
		$3\frac{1}{2}$	49124. 52		1. 499
		$0\frac{1}{2}$	49154. 50		2. 78
		$4\frac{1}{2}$	49181. 04		1. 409
		$2\frac{1}{2}$	49242. 10		1. 510
		$2\frac{1}{2}$	50292. 33		1. 334
		$1\frac{1}{2}$	50430. 95		0. 93
		$4\frac{1}{2}$	50863. 05		1. 194
		$3\frac{1}{2}$	51045. 25		
		$1\frac{1}{2}$	51254. 40		1. 58
		$2\frac{1}{2}$	51438. 03		1. 301
		$3\frac{1}{2}$	51863. 03		0. 937
		$2\frac{1}{2}$	52087. 02		
		$3\frac{1}{2}$	52275. 28		1. 297
		$0\frac{1}{2}$	52355. 11		0. 981
		$4\frac{1}{2}$	52567. 15		
		$0\frac{1}{2}$	52593. 72		1. 56 ?
		$1\frac{1}{2}$	52803. 00		
		$3\frac{1}{2}$	52901. 74		1. 374
		$2\frac{1}{2}$	53113. 52		1. 262
		$1\frac{1}{2}$	53329. 71		1. 357
		$3\frac{1}{2}$	53338. 07		0. 968
		$4\frac{1}{2}$	53369. 97		1. 086
$1\frac{1}{2}$	53422. 98		0. 976		
$0\frac{1}{2}$	53440. 17		2. 038		
$2\frac{1}{2}$	54026. 24				
$4\frac{1}{2}$	54056. 54		1. 123		
$1\frac{1}{2}$	54137. 20		1. 608		
$5\frac{1}{2}$	54229. 06				
$2\frac{1}{2}$	54375. 82		1. 51		
$0\frac{1}{2}$	54485. 60		1. 46		
$3\frac{1}{2}$	54498. 57				
$2\frac{1}{2}$	54704. 61		0. 623		
$0\frac{1}{2}$	54760. 06				
$5\frac{1}{2}$	54958. 58		1. 141		
$3\frac{1}{2}$	55022. 86				
$2\frac{1}{2}$	55162. 30		1. 00		
$4\frac{1}{2}$	55392. 37		1. 061		
$1\frac{1}{2}$	55488. 01				
$1\frac{1}{2}$	56084. 30		1. 021		
$5\frac{1}{2}$	56376. 45				
$4\frac{1}{2}$	56413. 64				
$6\frac{1}{2}$	56439. 60				
$2\frac{1}{2}$	56544. 40				

TABLE 2. *Odd levels of W II—Continued*

Configuration	Designation	<i>J</i>	Level	Interval	Obs. g
<i>5d⁴(³P)6p</i>	<i>z²S⁰</i>	3½	56612. 74		1. 22
		3½	56768. 61		1. 147
		2½	56874. 99		0. 815
		1½	56932. 27		1. 06
		4½	57089. 46		
		2½	57252. 00		
		3½	57729. 92		1. 184
		2½	57856. 70		1. 36
		4½	57986. 92		
		1½	58007. 60		1. 20
		2½	58336. 98		
		4½	58687. 88		
		3½	58709. 56		
		1½	58747. 94		0. 78
		5½	58891. 74		1. 144
		3½	59276. 81		1. 102
		4½	59399. 34		1. 179
		1½	59816. 30		
		3½	59869. 14		1. 125
		3½	59933. 66		
		2½	59992. 20		
		5½	60218. 84		1. 130
		3½	60256. 45		
		4½	60278. 71		
		3½	60424. 14		
		2½	60474. 67		
		2½	60656. 51		
		2½	60900. 97		0. 92
		4½	61055. 80		
		5½	61240. 81		1. 120
		3½	61326. 29		
		4½	61360. 54		
		3½	61550. 60		
		2½	61566. 70		1. 07
		5½	61589. 46		1. 149
		6½	61602. 18		
		2½	62333. 20		
		4½	62437. 04		
		6½	62714. 56		
		4½	62715. 98		
		5½	62966. 56		
		2½	62989. 60		
		6½	63087. 90		
		3½	63266. 30		
		3½	63788. 20		
		2½	63880. 10		
		2½	64030. 34		
		4½	64207. 50		
		2½	64310. 00		
		3½	64356. 70		
		4½	64516. 37		
		3½	64896. 22		
		5½	64969. 10		
		2½	64990. 32		
		4½	65003. 20		
		2½	65141. 56		
5½	65326. 40				
3½	65644. 00				
5½	65684. 80				
4½	66270. 95				
5½	66703. 50				
5½	68012. 50				
6½	68078. 98				

TABLE 3. *Classified lines of W II*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Vac.						
1756.604		8	56928.0	-4.3	$a^6D_{0\frac{1}{2}}-56932\frac{1}{2}$	
1757.789		3	56889.6	0.0	$a^6S_{2\frac{1}{2}}-64310\frac{3}{2}$	
1759.408		4	56837.3	+3.0	$a^6D_{3\frac{1}{2}}-61550\frac{3}{2}$	
1760.00		5	56818.2	0.0	$a^6D_{1\frac{1}{2}}-58336\frac{3}{2}$	
1765.514		20	56640.7	-3.1	$a^6D_{2\frac{1}{2}}-59816\frac{1}{2}$	
				-3.5	$a^6D_{3\frac{1}{2}}-61360\frac{1}{2}$	
1766.319		8	56614.9	+4.9	$a^6D_{3\frac{1}{2}}-61326\frac{3}{2}$	
				+5.0	$a^6S_{2\frac{1}{2}}-64030\frac{3}{2}$	
1775.023		3	56337.3	-0.6	$a^6D_{1\frac{1}{2}}-57856\frac{3}{2}$	
1776.834		4	56279.9	+0.8	$a^4F_{1\frac{1}{2}}-64990\frac{3}{2}$	
1783.050		10	56083.7	-0.6	$a^6D_{0\frac{1}{2}}-56084\frac{1}{2}$	
1794.166		4	55736.2	+3.0	$a^6D_{1\frac{1}{2}}-57252\frac{3}{2}$	
1795.131		20	55706.2	-1.6	$a^6D_{3\frac{1}{2}}-60424\frac{3}{2}$	
1798.60		3	55598.8	+0.1	$a^4F_{1\frac{1}{2}}-64310\frac{3}{2}$	
1799.558		4	55569.2	0.0	$a^6S_{2\frac{1}{2}}-62989\frac{3}{2}$	
1800.570		20	55538.0	+1.0	$a^6D_{2\frac{1}{2}}-58709\frac{3}{2}$	
				-2.1	$a^6D_{3\frac{1}{2}}-60256\frac{3}{2}$	
1802.211		8	55487.4	-0.6	$a^6D_{0\frac{1}{2}}-55488\frac{1}{2}$	
1803.840		8	55437.3	-5.0	$a^6D_{4\frac{1}{2}}-61589\frac{3}{2}$	
1804.51		6	55416.7	+3.2	$a^6D_{1\frac{1}{2}}-56932\frac{1}{2}$	
1806.437		3	55357.6	+1.4	$a^6D_{1\frac{1}{2}}-56874\frac{3}{2}$	
1807.645		2	55320.5	+1.4	$a^4F_{1\frac{1}{2}}-64030\frac{3}{2}$	
1809.082		2	55276.6	+0.7	$a^6D_{3\frac{1}{2}}-59992\frac{3}{2}$	
1811.021		5	55217.5	+0.2	$a^6D_{3\frac{1}{2}}-59933\frac{3}{2}$	
1812.161		40	55182.7	+3.6	$a^6D_{4\frac{1}{2}}-61326\frac{3}{2}$	
1812.765		6	55164.4	-0.1	$a^6D_{2\frac{1}{2}}-58336\frac{3}{2}$	
1812.977		5	55157.9	+5.1	$a^6D_{3\frac{1}{2}}-59869\frac{3}{2}$	
1815.073		2	55094.2	+0.6	$a^6D_{4\frac{1}{2}}-61240\frac{3}{2}$	
1817.347		10	55025.2	-0.4	$a^6D_{1\frac{1}{2}}-56544\frac{3}{2}$	
1821.062		30	54913.0	+4.4	$a^6D_{4\frac{1}{2}}-61055\frac{3}{2}$	
				+0.2	$a^6S_{2\frac{1}{2}}-62333\frac{3}{2}$	
1823.64		3	54835.4	+0.3	$a^6D_{2\frac{1}{2}}-58007\frac{1}{2}$	
1826.126		20	54760.7	+0.6	$a^6D_{0\frac{1}{2}}-54760\frac{0}{2}$	
1828.69		6	54684.0	+1.0	$a^6D_{3\frac{1}{2}}-59399\frac{3}{2}$	
				-0.2	$a^6D_{2\frac{1}{2}}-57856\frac{3}{2}$	
1838.338		25	54397.0	-0.8	$a^4P_{1\frac{1}{2}}-64990\frac{3}{2}$	
1847.041		5	54140.6	+3.4	$a^6D_{0\frac{1}{2}}-54137\frac{1}{2}$	
1848.104		30	54109.7	+0.4	$a^6D_{4\frac{1}{2}}-60256\frac{3}{2}$	
1852.110		15	53992.5	-0.7	$a^6D_{3\frac{1}{2}}-58709\frac{3}{2}$	
1852.917		20	53969.0	-0.2	$a^6D_{1\frac{1}{2}}-55488\frac{1}{2}$	
1860.069		4	53761.4	+1.6	$a^6D_{2\frac{1}{2}}-56932\frac{1}{2}$	
1861.26		6	53727.0	+5.0	$a^6D_{4\frac{1}{2}}-59869\frac{3}{2}$	
1864.976		15	53620.0	-0.7	$a^6D_{3\frac{1}{2}}-58336\frac{3}{2}$	
1865.818		8	53595.8	-0.3	$a^6D_{2\frac{1}{2}}-56768\frac{3}{2}$	
				-0.3	$a^6D_{0\frac{1}{2}}-53440\frac{0}{2}$	
1871.261		6	53439.9	-0.3	$a^6D_{2\frac{1}{2}}-56612\frac{3}{2}$	
				-0.3		
1871.90		6	53421.6	-1.4	$a^6D_{0\frac{1}{2}}-53422\frac{1}{2}$	
1873.646		20	53371.9	0.0	$a^6D_{2\frac{1}{2}}-56544\frac{3}{2}$	
1875.156		12	53328.9	-0.8	$a^6D_{0\frac{1}{2}}-53329\frac{1}{2}$	
1877.33		2	53267.2	-3.4	$a^6D_{3\frac{1}{2}}-57986\frac{3}{2}$	
1877.869		20	53251.8	-0.4	$a^6D_{4\frac{1}{2}}-59399\frac{3}{2}$	
1878.54		4	53233.0	-3.1	$a^6S_{2\frac{1}{2}}-60656\frac{3}{2}$	
1880.216		8	53185.4	-0.4	$a^6D_{1\frac{1}{2}}-54704\frac{3}{2}$	
1881.798		15	53140.6	+0.2	$a^6D_{3\frac{1}{2}}-57856\frac{3}{2}$	
1882.185		8	53129.7	+0.1	$a^6D_{4\frac{1}{2}}-59276\frac{3}{2}$	
1886.304		6	53013.7	+0.1	$a^6D_{3\frac{1}{2}}-57729\frac{3}{2}$	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	<i>O-C</i>		
Vac.						
1891. 908		6	52856. 7	{ -0. 3	<i>a</i> ⁶ D _{1½} —54375 _{3½}	
1892. 442		15	52841. 8	+1. 3	<i>a</i> ⁴ F _{1½} —61566 _{3½}	
1893. 80		4	52803. 9	+5. 8	<i>a</i> ⁶ S _{2½} —60256 _{3½}	
1895. 943		30	52744. 2	+0. 9	<i>a</i> ⁶ D _{0½} —52803 _{1½}	
1900. 563		12	52617. 6	-0. 4	<i>a</i> ⁶ D _{4½} —58891 _{3½}	
				-0. 8	<i>a</i> ⁶ D _{1½} —54137 _{1½}	
1901. 245		30	52597. 1	+3. 4	<i>a</i> ⁶ D _{0½} —52593 _{0½}	
1902. 51		20	52562. 1	-0. 3	<i>a</i> ⁶ D _{4½} —58709 _{3½}	
1906. 677		12	52447. 3	-1. 4	<i>a</i> ⁶ S _{2½} —59869 _{3½}	
1908. 750		10	52390. 3	-5. 6	<i>a</i> ⁶ S _{2½} —59816 _{1½}	
1909. 16		6	52379. 0	+5. 9	<i>a</i> ⁶ D _{3½} —57089 _{4½}	
1909. 80		4	52361. 4	+6. 3	<i>a</i> ⁶ D _{0½} —52355 _{0½}	
1911. 50		25	52314. 9	-0. 6	<i>a</i> ⁶ D _{2½} —55488 _{1½}	
1915. 38		8	52209. 0	-0. 9	<i>a</i> ⁴ P _{2½} —65644 _{3½}	
1925. 99		12	51921. 3	-0. 1	<i>a</i> ⁶ D _{1½} —53440 _{0½}	
1928. 61		20	51850. 8	+0. 5	<i>a</i> ⁶ D _{2½} —55022 _{3½}	
1929. 47		10	51827. 7	-0. 4	<i>a</i> ⁶ D _{3½} —56544 _{2½}	
1930. 10		6	51810. 8	-0. 1	<i>a</i> ⁶ D _{1½} —53329 _{1½}	
1931. 87		10	51763. 3	-0. 1	<i>a</i> ⁴ F _{1½} —60474 _{2½}	
1934. 345		10	51697. 1	-0. 2	<i>a</i> ⁶ D _{3½} —56413 _{4½}	
1934. 62		3	51689. 7	+1. 2	<i>a</i> ⁴ F _{2½} —62989 _{3½}	
1938. 21		25	51594. 0	-0. 7	<i>a</i> ⁶ D _{1½} —53113 _{2½}	
1938. 74		3	51579. 9	{ -2. 9	<i>a</i> ⁶ D _{4½} —57729 _{3½}	
1940. 54		8	51532. 0	+1. 5	<i>a</i> ⁴ F _{3½} —64990 _{2½}	
1943. 27		4	51459. 6	-0. 1	<i>a</i> ⁶ D _{2½} —54704 _{2½}	
1945. 02		10	51413. 5	+0. 2	<i>a</i> ⁴ G _{4½} —68012 _{3½}	
1948. 35		30	51325. 5	-0. 2	<i>a</i> ⁴ F _{4½} —66270 _{4½}	
				-0. 5	<i>a</i> ⁶ D _{2½} —54498 _{3½}	
1949. 55		40	51293. 9	+4. 8	<i>a</i> ⁶ S _{2½} —58709 _{3½}	
1949. 93		4	51283. 9	-0. 3	<i>a</i> ⁶ D _{1½} —52803 _{1½}	
1951. 06		40	51254. 2	-0. 2	<i>a</i> ⁶ D _{0½} —51254 _{1½}	
1953. 00		3	51203. 3	0. 0	<i>a</i> ⁶ D _{2½} —54375 _{3½}	
1957. 90		2	51075. 1	+0. 2	<i>a</i> ⁶ D _{1½} —52593 _{0½}	
1959. 54		5	51032. 3	+0. 2	<i>a</i> ⁴ F _{2½} —62333 _{3½}	
1961. 42		6	50983. 5	-0. 1	<i>a</i> ⁴ P _{0½} —59816 _{1½}	
1962. 14		40	50964. 7	0. 0	<i>a</i> ⁶ D _{2½} —54137 _{1½}	
1962. 92		20	50944. 4	-0. 3	<i>a</i> ⁴ F _{3½} —64356 _{3½}	
1963. 02		2	50941. 9	-0. 4	<i>a</i> ⁶ D _{4½} —57089 _{4½}	
1967. 09		2	50836. 5	+0. 2	<i>a</i> ⁶ D _{1½} —52355 _{0½}	
1967. 41		10	50828. 2	+0. 6	<i>a</i> ⁴ F _{4½} —65684 _{3½}	
1968. 67		8	50795. 6	+0. 1	<i>a</i> ⁴ F _{3½} —64207 _{4½}	
1973. 32		20	50676. 0	0. 0	<i>a</i> ⁶ D _{3½} —55392 _{4½}	
1974. 66		4	50641. 6	-0. 3	<i>a</i> ⁴ G _{5½} —68078 _{8½}	
1975. 48		15	50620. 7	-0. 7	<i>a</i> ⁶ D _{4½} —56768 _{3½}	
1976. 70		25	50589. 4	+2. 2	<i>a</i> ⁶ S _{2½} —58007 _{1½}	
1977. 24		12	50575. 6	+0. 1	<i>a</i> ⁴ G _{5½} —68012 _{3½}	
1977. 53		15	50568. 1	-0. 1	<i>a</i> ⁶ D _{1½} —52087 _{2½}	
1981. 42		20	50468. 8	+3. 2	<i>a</i> ⁶ D _{4½} —56612 _{3½}	
1982. 35		15	50445. 1	-0. 9	<i>a</i> ⁶ D _{3½} —55162 _{2½}	
1982. 73		1	50435. 5	-0. 8	<i>a</i> ⁶ S _{2½} —57856 _{3½}	
1982. 92		20	50430. 7	-0. 3	<i>a</i> ⁶ D _{0½} —50430 _{1½}	
1987. 80		25	50301. 9	-4. 6	<i>a</i> ⁶ D _{3½} —55022 _{3½}	
1989. 41		30	50266. 1	-0. 4	<i>a</i> ⁶ D _{4½} —56413 _{4½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	<i>O-C</i>		
Vac.						
1990. 07		15	50249. 4	{ -0. 1 -1. 1 +0. 3 -1. 9 -3. 3 -0. 3	<i>a</i> ⁴ F _{2½} —61550 _{3½}	
1990. 86		12	50229. 6		<i>a</i> ⁶ D _{2½} —53422 _{1½}	
1993. 15		6	50171. 8		<i>a</i> ⁶ D _{4½} —56376 _{3½}	
1993. 53		1	50162. 3		<i>a</i> ⁴ D _{2½} —65141 _{2½}	
1993. 74		3	50156. 9		<i>a</i> ⁶ D _{2½} —53338 _{3½}	
					<i>a</i> ⁶ D _{2½} —53329 _{1½}	
1994. 21		15	50145. 1	-0. 9	<i>a</i> ⁴ F _{4½} —65003 _{4½}	
1995. 545		25	50111. 6	-0. 3	<i>a</i> ⁴ F _{4½} —64969 _{3½}	
1997. 46		6	50063. 7	-0. 3	<i>a</i> ⁴ P _{1½} —60656 _{2½}	
1998. 54		3	50036. 6	-0. 1	<i>a</i> ⁴ F _{1½} —58747 _{1½}	
1998. 99		3	50025. 2	0. 0	<i>a</i> ⁴ F _{2½} —61326 _{3½}	
Air						
1999. 83		12	49988. 1	-0. 2	<i>a</i> ⁶ D _{3½} —54704 _{2½}	
2001. 70	3	30	49941. 4	+0. 4	<i>a</i> ⁶ D _{2½} —53113 _{2½}	
2002. 59		2	49919. 2	0. 0	<i>a</i> ⁶ D _{1½} —51438 _{2½}	
2002. 73	1	3	49915. 7	+0. 4	<i>a</i> ⁴ P _{0½} —58747 _{1½}	
2005. 60		1	49844. 3	+1. 0	<i>a</i> ⁴ D _{3½} —64990 _{2½}	
2006. 07		3	49832. 6	+0. 4	<i>a</i> ⁴ P _{2½} —63266 _{3½}	
2008. 08	4	40	49782. 7	+0. 5	<i>a</i> ⁶ D _{3½} —54498 _{3½}	
2009. 37		2	49750. 8	+1. 6	<i>a</i> ⁴ D _{3½} —64896 _{3½}	
2009. 98	1	12	49735. 7	+0. 1	<i>a</i> ⁶ D _{1½} —51254 _{1½}	
2010. 24	3	15	49729. 3	+0. 1	<i>a</i> ⁶ D _{2½} —52901 _{3½}	
2010. 66	2	1	49718. 9	+1. 1	<i>a</i> ⁴ G _{4½} —66270 _{4½}	
2012. 18		5	49681. 3	0. 0	<i>a</i> ⁴ G _{3½} —66270 _{4½}	
2013. 06	4	4	49659. 6	+0. 1	<i>a</i> ⁶ D _{3½} —54375 _{2½}	
2014. 23	3	15	49630. 7	+0. 2	<i>a</i> ⁶ D _{2½} —52803 _{1½}	
2014. 43	3	10	49625. 8	+0. 1	<i>a</i> ⁴ F _{1½} —58336 _{2½}	
2015. 44	2	8	49661. 0	+1. 1	<i>a</i> ⁴ F _{2½} —60900 _{2½}	
2017. 26	—	2	49556. 2	+0. 7	<i>a</i> ⁴ P _{2½} —62989 _{2½}	
2019. 08	—	1	49511. 6	-0. 2	<i>a</i> ⁶ S _{2½} —56932 _{1½}	
2019. 55	2	5	49500. 0	+0. 5	<i>a</i> ⁴ F _{4½} —64356 _{3½}	
2021. 43		3	49454. 0	-0. 6	<i>a</i> ⁶ S _{2½} —56874 _{2½}	
2023. 25		1	49409. 5	+0. 1	<i>a</i> ⁴ G _{2½} —65644 _{3½}	
2023. 63		3	49400. 3	+0. 6	<i>a</i> ⁴ P _{1½} —59992 _{2½}	
2023. 79		3	49396. 4	+0. 4	<i>a</i> ⁴ D _{1½} —64030 _{2½}	
2025. 45	1	4	49355. 9	+0. 5	<i>a</i> ⁴ F _{2½} —60656 _{2½}	
2025. 62		2	49351. 7	+1. 4	<i>a</i> ⁴ F _{4½} —64207 _{4½}	
2026. 07	8	30	49340. 8	+0. 6	<i>a</i> ⁶ D _{3½} —54056 _{4½}	
2027. 30	1	12	49310. 8	+0. 9	<i>a</i> ⁶ D _{3½} —54026 _{2½}	
2027. 55	2	3	49304. 8	+0. 8	<i>a</i> ⁴ F _{3½} —62715 _{4½}	
2027. 87	2	5	49296. 9	+0. 6	<i>a</i> ⁴ F _{1½} —58007 _{1½}	
2029. 12	1	15	49266. 6	+0. 1	<i>a</i> ⁴ G _{5½} —66703 _{5½}	
2029. 99	5	50	49245. 5	+0. 3	<i>a</i> ⁶ D _{4½} —55392 _{4½}	
2030. 87		3	49224. 2	+0. 4	<i>a</i> ⁴ P _{1½} —59816 _{1½}	
2031. 44		12	49210. 4	+0. 7	<i>a</i> ⁴ D _{3½} —64356 _{3½}	
2032. 16		3	49192. 9	+0. 6	<i>a</i> ⁶ S _{2½} —56612 _{3½}	
2032. 92		12	49174. 5	-0. 4	<i>a</i> ⁴ P _{0½} —58007 _{1½}	
2033. 38		10	49163. 4	+0. 4	<i>a</i> ⁴ D _{3½} —64310 _{2½}	
2033. 73		8	49154. 9	+0. 4	<i>a</i> ⁶ D _{0½} —49154 _{0½}	
2034. 19		3	49143. 8	-1. 6	<i>a</i> ⁴ F _{1½} —57856 _{2½}	
2035. 02	5	25	49123. 8	-0. 2	<i>a</i> ⁶ S _{2½} —56544 _{2½}	
2035. 87	5	40	49103. 3	+0. 5	<i>a</i> ⁶ D _{2½} —52275 _{3½}	
2036. 40		2	49090. 5	-0. 4	<i>a</i> ⁴ G _{4½} —65644 _{3½}	
2037. 58	3	40	49062. 1	-0. 4	<i>a</i> ⁴ D _{2½} —64030 _{2½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2037.89	2	15	49054.6	+0.3	<i>a</i> ⁴ G _{3/2} —65644 _{3/2}	
2039.10	—	4	49025.5	+0.4	<i>a</i> ⁴ F _{3/2} —62437 _{3/2}	
2040.86	4	20	48983.3	+0.4	<i>a</i> ⁶ D _{3/2} —48982 _{3/2}	
2042.00	1	6	48956.0	+0.6	<i>a</i> ⁴ F _{2/2} —60256 _{3/2}	
2042.55		5	48942.7	+0.9	19070 _{3/2} —68012 _{3/2}	
2043.02	2	8	48931.3	+0.3	<i>a</i> ⁴ F _{4/2} —63788 _{3/2}	
2043.52	5	30	48919.6	-1.6	<i>a</i> ⁴ F _{3/2} —62333 _{3/2}	
2043.72		15	48914.7	+0.2	<i>a</i> ⁶ D _{2/2} —52087 _{3/2}	
2043.82		3	48912.3	+0.1	<i>a</i> ⁶ D _{1/2} —50430 _{3/2}	
2044.33	2	10	48900.1	+1.0	<i>a</i> ⁴ P _{2/2} —62333 _{3/2}	
2045.05	3	3	48883.0	-0.3	<i>a</i> ⁴ D _{3/2} —64030 _{3/2}	
2045.32	2	15	48876.4	+0.7	<i>a</i> ⁶ D _{4/2} —55022 _{3/2}	
2047.07	2	20	48834.8	+0.9	<i>a</i> ⁴ G _{5/2} —66270 _{3/2}	
2047.76		2	48818.2	-2.2	<i>a</i> ⁴ D _{2/2} —63788 _{3/2}	
2048.03	5	30	48811.8	+0.4	<i>a</i> ⁶ D _{4/2} —54958 _{3/2}	
2049.62	8	25	48773.9	+0.3	<i>a</i> ⁶ D _{1/2} —50292 _{3/2}	
2050.36		12	48756.3	+0.8	<i>a</i> ⁴ G _{2/2} —64990 _{3/2}	
2051.32	1?	1	48733.5	+0.4	<i>a</i> ⁴ D _{3/2} —63880 _{3/2}	
2053.10	5	15	48691.3	+0.2	<i>a</i> ⁴ F _{2/2} —59992 _{3/2}	
2053.35		3	48661.6	+0.8	<i>a</i> ⁶ D _{2/2} —51863 _{3/2}	
2054.67	10	50	48654.0	+0.2	<i>a</i> ⁴ G _{2/2} —64896 _{3/2}	
				+0.4	<i>a</i> ⁶ D _{3/2} —53369 _{3/2}	
2055.19	2	3	48641.8	+0.6	<i>a</i> ⁴ D _{3/2} —63788 _{3/2}	
2055.54	1?	3	48633.5	+0.9	<i>a</i> ⁴ F _{2/2} —59933 _{3/2}	
2055.99	2	10	48622.8	+1.0	<i>a</i> ⁶ D _{3/2} —53338 _{3/2}	
2058.30	12	15	48568.3	+0.2	<i>a</i> ⁴ F _{2/2} —59869 _{3/2}	
2059.03	1	8	48550.9	-1.0	<i>a</i> ⁴ G _{3/2} —65141 _{3/2}	
2059.45	4	8	48541.1	+0.4	<i>a</i> ⁴ F _{1/2} —57252 _{3/2}	
2060.53	3	2	48515.7	+0.5	<i>a</i> ⁴ F _{2/2} —59816 _{3/2}	
2063.34		1	48449.7	-0.4	<i>a</i> ⁴ G _{4/2} —65003 _{3/2}	
2064.76	2	6	48416.3	+0.3	<i>a</i> ⁴ G _{4/2} —64969 _{3/2}	
2065.06	6A	3	48409.4	+0.3	<i>a</i> ⁴ F _{1/2} —63266 _{3/2}	
2065.57	3	30	48397.3	+0.1	<i>a</i> ⁶ D _{3/2} —53113 _{3/2}	
2067.52	—?	30	48351.7	+0.3	<i>a</i> ⁶ D _{4/2} —54498 _{3/2}	
2067.87	—?	10	48343.5	+0.4	<i>a</i> ⁴ G _{4/2} —64896 _{3/2}	
2069.36		10	48308.8	+2.2	<i>a</i> ⁴ G _{3/2} —64896 _{3/2}	
2069.77		3	48299.1	+0.6	<i>a</i> ⁴ D _{2/2} —63266 _{3/2}	
2071.19	2	40	48265.9	+0.4	<i>a</i> ⁶ D _{2/2} —51438 _{3/2}	
2071.95		3	48248.3	+0.5	<i>a</i> ⁴ G _{5/2} —65684 _{3/2}	
2074.63		15	48185.9	+0.5	<i>a</i> ⁶ D _{3/2} —52901 _{3/2}	
2075.59	2	30	48163.8	+0.1	<i>a</i> ⁴ F _{1/2} —56874 _{3/2}	
2075.93		10	48155.9	+0.5	<i>a</i> ⁴ P _{1/2} —58747 _{3/2}	
2076.92		2	48132.9	+0.3	<i>a</i> ⁴ P _{2/2} —61566 _{3/2}	
2077.36		5	48122.6	+0.7	<i>a</i> ⁴ G _{2/2} —64356 _{3/2}	
2077.61		6	48116.9	+0.4	<i>a</i> ⁴ P _{2/2} —61550 _{3/2}	
2077.92	1	10	48109.7	+0.4	<i>a</i> ⁴ F _{4/2} —62966 _{3/2}	
2078.32	1	40	48100.3	+0.7	<i>a</i> ⁴ P _{0/2} —56932 _{3/2}	
2079.11	20	80	48082.2	+0.3	<i>a</i> ⁶ D _{2/2} —51254 _{3/2}	
2081.75		3	48021.2	+0.3	<i>a</i> ⁶ D _{4/2} —54229 _{3/2}	
2083.70	1	10	47976.4	-0.6	<i>a</i> ⁴ D _{2/2} —62989 _{3/2}	
2084.23		12	47964.1	+0.7	<i>a</i> ⁴ F _{2/2} —59276 _{3/2}	
2084.88		5	47949.1	+0.9	<i>a</i> ⁴ G _{4/2} —64516 _{3/2}	
				+0.5	<i>a</i> ⁴ F _{3/2} —61360 _{3/2}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2086.37	2	3	47914.9	+0.6	<i>a</i> ⁴ F _{3/2} —61326 _{3/2} ^{3/2}	
2086.58	5	4	47910.0	+0.6	<i>a</i> ⁶ D _{4/2} —54056 _{4/2} ^{3/2}	
2087.34	2	2	47892.6	+0.4	<i>a</i> ⁴ P _{2/2} —61326 _{3/2} ^{3/2}	
2087.46	5	4	47889.9	+0.5	<i>a</i> ⁴ G _{5/2} —65326 _{5/2} ^{3/2}	
2088.18	60	30	47873.4	+0.7	<i>a</i> ⁶ D _{2/2} —51045 _{3/2} ^{3/2}	
2089.13	40	20	47851.6	+0.8	<i>a</i> ⁶ D _{3/2} —52567 _{3/2} ^{3/2}	
2089.49		4	47843.4	+0.8	<i>a</i> ⁴ D _{3/2} —62989 _{3/2} ^{3/2}	
2091.23	2	4	47803.5	-0.1	<i>a</i> ⁴ G _{4/2} —64356 _{3/2} ^{3/2}	
2093.79	20	20	47745.1	+0.6	<i>a</i> ⁴ P _{1/2} —58336 _{3/2} ^{3/2}	
2094.72	50	25	47723.9	+0.6	<i>a</i> ⁶ D _{1/2} —49242 _{2/2} ^{3/2}	
2095.78		1	47699.8	+1.0	<i>a</i> ⁴ D _{1/2} —62333 _{2/2} ^{3/2}	
2097.76	2	3	47654.6	+0.2	<i>a</i> ⁴ G _{4/2} —64207 _{4/2} ^{3/2}	
2098.22	60A	30	47644.2	+0.4	<i>a</i> ⁴ F _{3/2} —61055 _{4/2} ^{3/2}	
2098.58	70	40	47636.2	+0.5	<i>a</i> ⁶ D _{1/2} —49154 _{0/2} ^{3/2}	
2098.69	3	—	47633.7	+0.9	19070 _{4/2} —66703 _{5/2} ^{3/2}	
2099.37	2	1	47618.3	+0.5	<i>a</i> ⁴ G _{3/2} —64207 _{4/2} ^{3/2}	
2100.06	—	1	47602.6	+0.2	<i>a</i> ⁶ S _{2/2} —55022 _{3/2} ^{3/2}	
2100.66	50	20	47589.0	+0.4	<i>a</i> ⁶ D _{0/2} —47588 _{1/2} ^{3/2}	
2101.05	—?	3	47580.1	+0.3	<i>a</i> ⁴ F _{4/2} —62437 _{4/2} ^{3/2}	
2101.66		4	47566.4	+0.2	<i>a</i> ⁴ G _{5/2} —65003 _{4/2} ^{3/2}	
2101.96	10	2	47559.6	+0.6	<i>a</i> ⁶ D _{3/2} —52275 _{3/2} ^{3/2}	
2102.21	3	1	47553.9	+0.5	<i>a</i> ⁴ G _{2/2} —63788 _{3/2} ^{3/2}	
2103.16	30	15	47532.5	+0.4	<i>a</i> ⁴ G _{5/2} —64969 _{5/2} ^{3/2}	
2105.07		3	47489.3	+0.3	<i>a</i> ⁴ F _{3/2} —60900 _{3/2} ^{3/2}	
2106.04	2		47467.4	+0.5	<i>a</i> ⁴ P _{2/2} —60900 _{3/2} ^{3/2}	
2106.17	50	30	47464.5	+0.4	<i>a</i> ⁶ D _{1/2} —48982 _{1/2} ^{3/2}	
2107.26		3	47440.0	-0.7	<i>a</i> ⁴ G _{3/2} —64030 _{3/2} ^{3/2}	
2108.38	—?	25	47414.8	-0.3	<i>a</i> ⁴ P _{1/2} —58007 _{1/2} ^{3/2}	
2108.65	—?	15	47408.6	+0.1	<i>a</i> ⁴ F _{2/2} —58709 _{3/2} ^{3/2}	
2110.33	50	30	47371.0	+0.3	<i>a</i> ⁶ D _{3/2} —52087 _{2/2} ^{3/2}	
2113.92	20	2	47290.5	{ +0.1	<i>a</i> ⁴ G _{3/2} —63880 _{3/2} ^{3/2}	
2114.16		1	47285.1	{ +0.5	<i>a</i> ⁴ D _{3/2} —62437 _{4/2} ^{3/2}	
2115.08	10	2	47264.5	+0.9	<i>a</i> ⁶ S _{2/2} —54704 _{2/2} ^{3/2}	
2115.35	20		47258.6	+0.3	<i>a</i> ⁴ P _{1/2} —57856 _{2/2} ^{3/2}	
2115.65	2		47251.8	+0.2	<i>a</i> ⁶ D _{2/2} —50430 _{1/2} ^{3/2}	
2115.91		2	47246.1	+0.2	<i>a</i> ⁴ P _{0/2} —56084 _{1/2} ^{3/2}	
2115.94	25	2	47246.1	+1.5	<i>a</i> ⁴ F _{3/2} —60656 _{2/2} ^{3/2}	
2116.94		2	47223.1	+0.3	<i>a</i> ⁶ D _{4/2} —53369 _{3/2} ^{3/2}	
2118.03	15	5	47198.8	+0.3	<i>a</i> ⁴ G _{3/2} —63788 _{3/2} ^{3/2}	
2118.34		2	47191.8	+0.9	<i>a</i> ⁶ D _{4/2} —53338 _{3/2} ^{3/2}	
2118.87	40	20	47180.1	+0.2	<i>a</i> ⁶ D _{0/2} —47179 _{1/2} ^{3/2}	
2120.38	1	1	47146.4	-0.3	<i>a</i> ⁶ D _{3/2} —51863 _{3/2} ^{3/2}	
2121.60	100	25	47119.3	-0.5	<i>a</i> ⁶ D _{2/2} —50292 _{3/2} ^{3/2}	
2123.42	15	20	47079.0	-0.4	<i>a</i> ⁴ G _{5/2} —64516 _{3/2} ^{3/2}	
2124.14		1	47063.0	+0.3	<i>a</i> ⁴ F _{3/2} —60474 _{2/2} ^{3/2}	
2125.58	4	10	47031.1	-0.4	<i>a</i> ⁴ G _{2/2} —63266 _{3/2} ^{3/2}	
2126.86	2	4	47002.8	+0.3	18000 _{3/2} —65003 _{4/2} ^{3/2}	
2127.44	12	20	46990.0	{ +0.4	18000 _{3/2} —64990 _{3/2} ^{3/2}	
2129.00	10	2	46955.6	0.0	<i>a</i> ⁴ P _{2/2} —60424 _{3/2} ^{3/2}	
2130.05	20	2	46932.4	+0.2	<i>a</i> ⁶ S _{2/2} —54374 _{3/2} ^{3/2}	
2131.73	4	3	46895.5	+0.1	<i>a</i> ⁴ D _{1/2} —61566 _{3/2} ^{3/2}	
				0.0	18000 _{3/2} —64896 _{3/2} ^{3/2}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2134. 044	25	10	46844. 61	+0. 12	$a^4F_{3/2}-60256_{3/2}^3$	
2135. 04	—	20	46822. 8	+0. 4	$a^4P_{2/2}-60256_{3/2}^3$	
2137. 135	20A	10	46776. 87	+0. 12	$a^4F_{1/2}-55488_{1/2}^1$	
2137. 636	25	6	46765. 9	+0. 2	$a^6D_{1/2}-48284_{1/2}^2$	
2138. 133	40	30	46755. 0	+0. 4	$a^6D_{3/2}-52901_{3/2}^3$	
2139. 16	30	12	46732. 6	+0. 4	$a^4F_{4/2}-61589_{3/2}^3$	
2139. 646	12	6	46722. 0	+0. 3	$a^6D_{3/2}-51438_{3/2}^3$	
2139. 86	1		46717. 3	+0. 5	$a^6S_{2/2}-54137_{1/2}^1$	
2140. 03	5	6	46713. 6	+0. 4	$a^4G_{4/2}-63266_{3/2}^3$	
2140. 94		2	46693. 7	+0. 3	$a^4F_{4/2}-61550_{3/2}^3$	
2142. 49	15	4	46660. 0	+0. 5	$a^4P_{1/2}-57252_{2/2}^2$	
2142. 736	3	1	46645. 61	+0. 26	$a^4P_{0/2}-55488_{1/2}^1$	
2143. 257	15A	3	46643. 27	+0. 35	$a^4D_{0/2}-59816_{1/2}^1$	
2144. 08	40	4	46625. 4	+0. 1	$a^6D_{0/2}-46625_{0/2}^0$	
2145. 28	6		46599. 3	+0. 4	$a^4D_{2/2}-61566_{2/2}^2$	
2146. 02	8	3	46583. 1	+0. 3	$a^4D_{2/2}-61550_{3/2}^3$	
2146. 13	25	8	46580. 8	+0. 6	$a^4F_{3/2}-59992_{2/2}^2$	
2147. 17	1		46558. 3	+0. 2	$a^4P_{2/2}-59992_{2/2}^2$	
2147. 31	35A	3	46555. 2	-0. 4	$a^4F_{2/2}-57856_{2/2}^2$	
2148. 84		8	46522. 1	+0. 4	$a^4F_{3/2}-59933_{3/2}^3$	
2149. 136		12	46515. 69	+0. 02	$18000_{3/2}-64516_{4/2}^4$	
2149. 69	3	3	46503. 7	+0. 4	$a^4F_{4/2}-61360_{4/2}^4$	
2151. 28	—	3	46469. 3	+0. 2	$a^4F_{4/2}-61326_{3/2}^3$	
2151. 83		4	46457. 4	+0. 2	$a^4F_{3/2}-59869_{3/2}^3$	
2152. 126	20	25	46451. 07	+0. 03	$a^4F_{1/2}-55162_{2/2}^2$	
2152. 85	5	—	46435. 5	+0. 5	$a^4P_{2/2}-59869_{3/2}^3$	
2153. 15	8	1	46429. 0	+0. 2	$a^4F_{2/2}-57729_{3/2}^3$	
2153. 550	40	20	46420. 36	+0. 37	$a^6D_{4/2}-52567_{4/2}^4$	
2153. 870	4	20	46413. 46	+0. 10	$a^4G_{4/2}-62966_{5/2}^5$	
2154. 31	4	3	46404. 0	+0. 4	$a^4D_{3/2}-61550_{3/2}^3$	
2155. 25	3		46383. 7	+0. 1	$a^4F_{4/2}-61240_{5/2}^5$	
2155. 31	4	2	46382. 5	+0. 3	$a^4P_{2/2}-59816_{1/2}^1$	
2156. 00		4	46367. 61	+0. 13	$19270_{0/2}-65644_{3/2}^3$	
2156. 42	4	20	46358. 6	+0. 1	$a^4D_{2/2}-61326_{3/2}^3$	
2157. 798	4	20	46328. 98	+0. 05	$a^6D_{3/2}-51045_{3/2}^3$	
2159. 96	4	8	46282. 6	+0. 1	$a^4P_{1/2}-56874_{2/2}^2$	
2160. 69	2	—	46267. 0	+0. 4	$a^4D_{1/2}-60900_{2/2}^2$	
2161. 83	2	3	46242. 6	+0. 3	$19442_{6/2}-65684_{5/2}^5$	
2162. 36		5	46231. 2	0. 0	$20039_{3/2}-66270_{4/2}^4$	6
2163. 49		3	46207. 1	+0. 3	$18000_{3/2}-64207_{4/2}^4$	
2163. 880	6	30	46198. 78	+0. 20	$a^4F_{4/2}-61055_{4/2}^4$	
2164. 800		5	46179. 15	-0. 12	$a^4D_{3/2}-61326_{3/2}^3$	
2165. 264		6	46169. 25	+0. 10	$20534_{5/2}-66703_{5/2}^5$	
2165. 56	3		46163. 0	+0. 2	$a^4G_{4/2}-62715_{4/2}^4$	
2166. 316	40	80	46146. 84	+0. 11	$a^6D_{3/2}-50863_{4/2}^4$	
2167. 185	10	20	46128. 33	+0. 21	$a^6D_{4/2}-52275_{3/2}^3$	
2167. 276		1	46126. 40	+0. 09	$a^4G_{3/2}-62715_{4/2}^4$	
2168. 590	4	10	46098. 45	+0. 09	$a^4G_{2/2}-62333_{2/2}^2$	
2169. 936	15	40	46069. 86	0. 00	$a^6D_{1/2}-47588_{1/2}^1$	
2172. 206		12	46021. 72	+0. 28	$a^6D_{2/2}-49242_{2/2}^2$	
2172. 926		6	46006. 47	-0. 43	$a^4D_{1/2}-60656_{2/2}^2$	
2173. 26	1	2	45999. 40	-0. 15	$19637_{2/2}-65644_{3/2}^3$	
				+0. 04	$18990_{1/2}-64990_{2/2}^2$	
2173. 55	25	50	45993. 27	-0. 08	$a^4F_{1/2}-54704_{2/2}^2$	
2173. 825	5	15	45987. 45	+0. 07	$a^4F_{3/2}-59399_{4/2}^4$	
2175. 494	12	8	45952. 17	+0. 17	$a^6D_{2/2}-49124_{3/2}^3$	
2175. 54		3	45951. 1	+0. 29	$a^4P_{1/2}-56544_{2/2}^2$	
2176. 424	2	12	45932. 54	+0. 2	$a^4F_{2/2}-57252_{2/2}^2$	
				+0. 02	$19070_{4/2}-65003_{4/2}^4$	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2176. 88	3	15	45922. 9	-0. 2	20780 _{4½} —66703 _{3½}	
2177. 13	3	4	45917. 65	+0. 01	<i>a</i> 6S _{2½} —53338 _{3½}	
2177. 52	4		45909. 42	+0. 14	<i>a</i> 6S _{2½} —53329 _{1½}	
2177. 546		30}	45908. 88	+0. 10	<i>a</i> 4D _{3½} —61055 _{1½}	
2178. 04	2		45898. 46	+0. 04	19070 _{4½} —64969 _{5½}	
2178. 72	10	50	45884. 14	+0. 24	<i>a</i> 4G _{4½} —62437 _{4½}	
2178. 92	10	30	45879. 9	+0. 5	18000 _{3½} —63880 _{2½}	
2179. 634		8	45864. 9	+0. 1	<i>a</i> 4F _{3½} —59276 _{3½}	
2180. 46	20	40	45847. 53	+0. 16	19276 _{2½} —65141 _{3½}	
2180. 68		8	45842. 9	+0. 2	<i>a</i> 4G _{3½} —62437 _{4½}	
2181. 49	15A	3	45825. 9	+0. 4	<i>a</i> 4F _{3½} —59276 _{3½}	
2182. 225		40	45810. 45	+0. 11	<i>a</i> 6D _{2½} —48982 _{1½}	
2183. 32		40	45787. 48	-0. 02	18000 _{3½} —63788 _{3½}	
2183. 94	2		45774. 48	+0. 14	<i>a</i> 4F _{1½} —54485 _{0½}	
2185. 42	—	50	45743. 49	-0. 04	<i>a</i> 4G _{3½} —62333 _{2½}	
2185. 75	5	40	45736. 58	-0. 02	20534 _{5½} —66270 _{1½}	
2186. 738	30	40	45715. 92	+0. 05	<i>a</i> 6D _{4½} —51863 _{3½}	
2186. 835	4	10	45713. 89	+0. 09	19276 _{2½} —64990 _{2½}	
2187. 82	3	1	45693. 3	+0. 2	<i>a</i> 6S _{2½} —53113 _{3½}	
2188. 06		2	45688. 3	-0. 4	<i>a</i> 4D _{2½} —60656 _{2½}	
2189. 19	30A	30	45664. 7	+0. 1	<i>a</i> 4F _{1½} —54375 _{3½}	
2189. 364	40	40	45661. 09	-0. 07	<i>a</i> 6D _{1½} —47179 _{1½}	
2189. 494	50	50	45658. 38	+0. 20	<i>a</i> 6D _{2½} —48830 _{3½}	
2189. 740	6	10	45653. 25	+0. 31	<i>a</i> 4P _{0½} —54485 _{0½}	
2189. 850	40	80	45650. 96	+0. 08	<i>a</i> 4G _{5½} —63087 _{6½}	
2190. 80		6	45631. 2	0. 0	<i>a</i> 4F _{2½} —56932 _{1½}	
2191. 34	4	12	45619. 9	+0. 2	19276 _{2½} —64896 _{3½}	
2192. 094	4	6	45604. 23	-0. 03	20039 _{3½} —65444 _{3½}	
2193. 440	30	40	45576. 25	+0. 24	<i>a</i> 6D _{3½} —50292 _{2½}	
2193. 542	25	40	45574. 13	+0. 22	<i>a</i> 4F _{2½} —56874 _{2½}	
2193. 88		1	45567. 1	+0. 2	<i>a</i> 4F _{1½} —60424 _{3½}	
2194. 515	70	50	45593. 92	+0. 22	<i>a</i> 6D _{0½} —45553 _{1½}	
2195. 680		2	45529. 76	+0. 28	<i>a</i> 4G _{5½} —62966 _{5½}	
2195. 816		25	45526. 94	+0. 38	19442 _{6½} —64969 _{5½}	
2196. 654		1	45509. 57	+0. 08	<i>a</i> 4D _{3½} —60656 _{3½}	
2196. 780	12	10	45506. 96	+0. 11	<i>a</i> 4D _{2½} —60474 _{2½}	
2196. 914		3	45504. 18	0. 00	19637 _{2½} —65141 _{3½}	
2197. 504	8	10	45491. 97	+0. 19	<i>a</i> 4P _{1½} —56084 _{1½}	
2197. 585	1		45490. 3	-0. 3	20780 _{4½} —66270 _{4½}	
2198. 008		6	45481. 54	+0. 23	<i>a</i> 6S _{2½} —52901 _{3½}	
2198. 676	40	60	45467. 72	+0. 19	<i>a</i> 4F _{2½} —56768 _{3½}	
2199. 166	40	20	45457. 59	+0. 57	<i>a</i> 6D _{0½} —45457 _{0½}	
2199. 742	2	8	45445. 69	0. 00	19070 _{4½} —64516 _{4½}	
2200. 696	2		45426. 0	+0. 1	<i>a</i> 4F _{1½} —54137 _{1½}	
2200. 907		12	45421. 64	+0. 15	<i>a</i> 4F _{1½} —60278 _{1½}	
2201. 984		12	45399. 42	+0. 19	<i>a</i> 4F _{4½} —60256 _{3½}	
2203. 798	10	25	45362. 06	+0. 44	<i>a</i> 4F _{1½} —60218 _{5½}	
2203. 986	20	70	45358. 19	+0. 35	<i>a</i> 4D _{1½} —59992 _{2½}	
2204. 482	100	150	45347. 98	+0. 14	<i>a</i> 6D _{4½} —z 6F _{5½}	
2205. 460	6	8	45327. 88	+0. 23	<i>a</i> 4D _{3½} —60474 _{3½}	
2205. 886	1	3	45319. 12	+0. 08	18990 _{1½} —64310 _{2½}	
2206. 060	15	15	45315. 55	-0. 21	<i>a</i> 4G _{2½} —61550 _{3½}	
2206. 134	8	12	45314. 03	+0. 19	<i>a</i> 4P _{2½} —58747 _{1½}	
2206. 237	2	—	45311. 91	+0. 25	<i>a</i> 4F _{2½} —56612 _{3½}	
2206. 588	40	80	45304. 71	+0. 17	<i>a</i> 4P _{0½} —54137 _{1½}	
2206. 922	20	30	45297. 85	+0. 25	<i>a</i> 4F _{3½} —58709 _{3½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2207. 435	—	5	45287. 33	+1. 31	19070 _{43/2} —64356 _{33/2}	
2207. 914	15	20	45277. 50	-0. 04	<i>a</i> ⁴ G _{53/2} —62714 _{63/2}	
2207. 986	30	40	45276. 02	+0. 10	<i>a</i> ⁴ F _{33/2} —58687 _{43/2}	
2208. 813		40	45259. 07	+0. 23	19637 _{23/2} —64896 _{33/2}	
2209. 564	12	6	45243. 69	+0. 37	<i>a</i> ⁴ F _{23/2} —56544 _{33/2}	
2216. 023	60	40	45111. 84	-0. 12	<i>a</i> ⁶ D _{23/2} —48284 _{33/2}	res
2216. 296	8	5	45106. 28	-0. 21	<i>a</i> ⁶ D _{13/2} —46625 _{03/2}	
2217. 582	4	3	45080. 13	-0. 05	19276 _{23/2} —64356 _{33/2}	
2217. 765	12	15	45076. 41	-0. 03	<i>a</i> ⁴ F _{43/2} —59933 _{33/2}	
2219. 588	6	12	45039. 39	+0. 01	18990 _{13/2} —64030 _{23/2}	
2219. 740	10	15	45036. 31	-0. 01	<i>a</i> ⁴ G _{43/2} —61589 _{53/2}	
2219. 882	2	2	45033. 42	-0. 06	19276 _{23/2} —64310 _{23/2}	
2220. 938	30	60	45012. 01	+0. 09	<i>a</i> ⁴ F _{43/2} —59869 _{33/2}	
2221. 525	10	15	45000. 12	+0. 10	<i>a</i> ⁴ G _{53/2} —62437 _{43/2}	
2221. 652	5	5	44997. 55	+0. 09	<i>a</i> ⁴ G _{43/2} —61550 _{33/2}	
2222. 070	10	30	44989. 08	+0. 18	18000 _{33/2} —62989 _{23/2}	
2223. 206	2	2	44966. 10	+0. 26	<i>a</i> ⁴ D _{23/2} —59933 _{33/2}	
2223. 326	4	6	44963. 67	+0. 21	20039 _{33/2} —65003 _{43/2}	
2223. 450	12	12	44961. 17	+0. 24	<i>a</i> ⁴ G _{33/2} —61550 _{33/2}	
2225. 230	15A	5	44925. 20	+0. 18	<i>a</i> ⁴ F _{33/2} —58336 _{23/2}	res
2225. 882	60	80	44912. 05	+0. 42	<i>a</i> ⁶ D _{03/2} —44911 _{13/2}	
2226. 320	12	15	44903. 21	+0. 33	<i>a</i> ⁴ P _{23/2} —58336 _{23/2}	
2226. 40	8	15	44901. 6	+0. 3	<i>a</i> ⁴ D _{23/2} —59869 _{33/2}	
2226. 56	50	60	44898. 4	+0. 3	<i>a</i> ⁶ D _{43/2} —51045 _{33/2}	
2226. 68	20	25	44895. 95	+0. 46	<i>a</i> ⁴ P _{13/2} —55488 _{13/2}	
2226. 77	20	70	44894. 14			
2228. 29	1	3	44863. 5	-0. 1	20780 _{43/2} —65644 _{33/2}	
2228. 70	5	2	44855. 26	+0. 41	<i>a</i> ⁶ S _{23/2} —52275 _{33/2}	
2228. 88	12	80	44851. 64			
2229. 026	10	6	44848. 70	+0. 22	<i>a</i> ⁴ D _{23/2} —59816 _{13/2}	
2229. 620	75	100	44836. 76	+0. 14	<i>a</i> ⁶ D _{13/2} —46355 _{23/2}	
2229. 730	8	25	44834. 54	+0. 32	<i>a</i> ⁴ D _{03/2} —58007 _{13/2}	
2231. 080	12	30	44807. 42	+0. 02	<i>a</i> ⁴ G _{43/2} —61360 _{43/2}	
2231. 84	15	5	44792. 16	+0. 11	20534 _{53/2} —65326 _{33/2}	
2232. 11	3	3	44786. 74	+0. 10	<i>a</i> ⁴ D _{33/2} —59933 _{33/2}	
2232. 284	6	4	44783. 25	+0. 03	<i>a</i> ⁴ F _{23/2} —56084 _{43/2}	
2232. 56	4	8	44777. 72	+0. 09	23234 _{43/2} —68012 _{53/2}	
2232. 80	3	2	44772. 90	-0. 25	<i>a</i> ⁴ G _{43/2} —61326 _{33/2}	
2234. 63	5?	12	44736. 24	-0. 38	<i>a</i> ⁴ G _{33/2} —61326 _{33/2}	
2235. 00	4	2	44728. 84	-0. 07	<i>a</i> ⁴ F _{13/2} —53440 _{03/2}	
2235. 48	2		44719. 24	-0. 08	19637 _{23/2} —64356 _{33/2}	
2235. 64	20	30	44716. 03	+0. 14	<i>a</i> ⁶ D _{43/2} —50863 _{43/2}	
2235. 856	8	8	44711. 71	-0. 01	<i>a</i> ⁴ F _{13/2} —53422 _{13/2}	
2237. 06	15	100	44687. 65	-0. 02	<i>a</i> ⁴ G _{43/2} —61240 _{33/2}	
2237. 84	10	4	44672. 08	-0. 54	19637 _{23/2} —64310 _{23/2}	
2238. 10	2	1	44666. 8	+0. 2	<i>a</i> ⁶ S _{23/2} —52087 _{23/2}	
2240. 53	2?		44618. 4	0. 0	<i>a</i> ⁴ F _{13/2} —53329 _{13/2}	
2241. 080	30	50	44607. 5	0. 0	<i>a</i> ⁴ P _{03/2} —53440 _{03/2}	
2241. 282	50A	10	44603. 48	-0. 10	19276 _{23/2} —63880 _{23/2}	6
2242. 71	7	7	44575. 08	+0. 12	<i>a</i> ⁴ F _{33/2} —57986 _{43/2}	
2242. 965	10	12	44570. 02	+0. 24	<i>a</i> ⁴ P _{13/2} —55162 _{23/2}	
2244. 15	10	25	44546. 48	+0. 46	20780 _{43/2} —65326 _{33/2}	
2244. 75	2	3	44534. 6	+0. 2	20455 _{13/2} —64990 _{33/2}	
2245. 19	25	40	44525. 8	0. 0	<i>a</i> ⁶ D _{33/2} —49242 _{23/2}	
2245. 90	5	3	44511. 8	+0. 1	19276 _{23/2} —63788 _{33/2}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2246.35	8	10	44502.86	+0.20	<i>a</i> ⁴ G _{4½} —61055½ _{4½}	<i>d</i>
2246.64	15	20	44497.12	+0.07	<i>a</i> ⁴ P _{0½} —53329½ _{1½}	
2247.67	6	40	44476.73	+0.10	20039 _{3½} —64516½ _{3½}	
2248.27	25	40	44464.86	+0.14	<i>a</i> ⁶ D _{3½} —49181½ _{4½}	
2248.75	60A	100	44455.37	+0.19	<i>a</i> ⁶ D _{0½} —44455½ _{0½}	
2249.28	6	5	44444.9	+0.2	<i>a</i> ⁴ F _{3½} —57856½ _{3½}	<i>res</i> 6
2249.38	15	12	44442.9	+0.3	<i>a</i> ⁶ S _{2½} —51863½ _{3½}	
2249.702	5	5	44436.56	+0.22	18000 _{3½} —62437½ _{4½}	
2249.804	20A	?	44434.54	-0.21	20534 _{5½} —64969½ _{5½}	
2250.45	1	8	44421.79	+0.12	<i>a</i> ⁴ G _{2½} —60656½ _{2½}	
2250.560	3	3	44419.62	+0.03	<i>a</i> ⁴ F _{4½} —59276½ _{3½}	
2250.730	30	50	44416.26	+0.14	<i>a</i> ⁶ D _{2½} —47588½ _{1½}	
2251.14	30	40	44408.17	-0.03	<i>a</i> ⁶ D _{3½} —49124½ _{3½}	
2251.434	18	25	44402.38	+0.12	<i>a</i> ⁴ F _{1½} —53113½ _{3½}	
2251.924	5	25	44392.71	-0.25	19637 _{2½} —64030½ _{2½}	
2254.98	10	20	44332.56	+0.06	18000 _{3½} —62333½ _{3½}	
2255.715	10A	10	44318.12	+0.16	<i>a</i> ⁴ F _{3½} —57729½ _{3½}	
2255.770	1	1	44317.04	+0.08	20039 _{3½} —64356½ _{3½}	
2256.18	2	6	44308.98	-0.01	<i>a</i> ⁴ D _{2½} —59276½ _{3½}	
2256.85	12	30	44295.8	0.0	<i>a</i> ⁴ P _{2½} —57729½ _{3½}	
2258.12	40	30	44270.9	+0.6	20039 _{3½} —64310½ _{3½}	
2259.07	10	25	44252.3	0.0	<i>a</i> ⁴ D _{3½} —59399½ _{4½}	
2259.56	10?	15	44242.7	0.0	19637 _{2½} —63880½ _{2½}	
2259.66	3	3	44240.8	0.0	<i>a</i> ⁶ D _{2½} —47413½ _{3½}	
2259.72	6	20	44239.6	-0.2	<i>a</i> ⁴ G _{2½} —60474½ _{2½}	
2260.58	4	6	44222.8	0.0	20780 _{4½} —65003½ _{4½}	
2261.946	1	25	44196.04	+0.42	19070 _{4½} —63266½ _{3½}	
2262.30	6	20	44189.13	-0.17	<i>a</i> ⁴ G _{2½} —60424½ _{3½}	
2262.406	4	4	44187.06	+0.13	<i>a</i> ⁴ F _{2½} —55488½ _{1½}	
2263.40	1	2?	44167.66	+0.12	<i>a</i> ⁴ P _{1½} —54760½ _{0½}	
				-0.10	20039 _{3½} —64207½ _{4½}	
2263.53	15	80	44165.12	-0.04	<i>a</i> ⁴ G _{5½} —61602½ _{0½}	
2264.178	8	35	44152.48	+0.04	<i>a</i> ⁴ G _{5½} —61589½ _{5½}	
2265.338	7	35	44129.87	+0.08	<i>a</i> ⁴ D _{3½} —59276½ _{3½}	
2265.67	35	20	44123.4	-0.1	23955 _{5½} —68078½ _{8½}	
2266.05	3	8?	44116.0	+0.2	20780 _{4½} —64896½ _{3½}	
2266.12	15	80	44114.6	+0.2	<i>a</i> ⁶ D _{3½} —48830½ _{3½}	
2266.25	15	80	44112.1	0.0	<i>a</i> ⁴ P _{1½} —54704½ _{2½}	
2267.30	4	4	44091.69	+0.05	<i>a</i> ⁴ F _{1½} —52803½ _{1½}	
2268.064	2	2	44076.84	-0.03	22194 _{3½} —66270½ _{4½}	
2269.08	2	4	44057.1	0.0	23955 _{5½} —68012½ _{3½}	
2270.232	25	125	44034.75	-0.17	<i>a</i> ⁶ D _{1½} —45553½ _{1½}	
2270.905	6	6	44021.70	+0.23	<i>a</i> ⁴ F _{4½} —58891½ _{5½}	
				+0.1	<i>a</i> ⁴ G _{2½} —60256½ _{3½}	
2271.105	10	12	44017.82	+0.22	<i>a</i> ⁶ S _{2½} —51438½ _{3½}	
2271.64	2	—	44007.4	0.0	<i>a</i> ⁶ D _{2½} —47179½ _{1½}	
2272.09	—	3	43998.74	+0.10	18990 _{1½} —62989½ _{2½}	
2272.510	8	25	43990.61	+0.01	20039 _{3½} —64030½ _{3½}	
2272.96	5?	15	43981.9	-0.1	20534 _{5½} —64516½ _{4½}	
2273.55	6	10	43970.49	+0.15	<i>a</i> ⁴ P _{0½} —52803½ _{1½}	
2275.22	5	?	43938.2	0.0	<i>a</i> ⁶ D _{1½} —45457½ _{0½}	
2275.98	3	2	43923.5	0.0	<i>a</i> ⁴ G _{5½} —61360½ _{4½}	
2277.416	3	4	43895.86	+0.04	19070 _{4½} —62966½ _{3½}	
2277.583	60A	20	43892.64	-0.44	<i>a</i> ⁴ P _{1½} —54485½ _{0½}	
2277.977	10	35	43885.05	+0.05	<i>a</i> ⁴ G _{3½} —60474½ _{2½}	
2278.108	25	30	43882.52	+0.06	<i>a</i> ⁴ F _{1½} —52593½ _{0½}	
2278.704	10	12	43871.05	+0.05	<i>a</i> ⁴ G _{4½} —60424½ _{3½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2279. 213	10	3	43861. 25	+0. 03	<i>a</i> ⁴ F _{2½} —55162 _{3½}	
2279. 672	1 —	—?	43852. 42	+0. 08	<i>a</i> ⁴ F _{4½} —58709 _{3½}	
2280. 300	8	30	43840. 34	-0. 02	20039 _{3½} —63880 _{3½}	
2280. 621	30	12	43834. 18	+0. 21	<i>a</i> ⁶ S _{2½} —51254 _{1½}	
2280. 802	10?	10	43830. 7	0. 0	<i>a</i> ⁴ F _{4½} —58687 _{4½}	
2282. 202	25	75	43803. 81	+0. 02	<i>a</i> ⁴ G _{5½} —61240 _{5½}	6
2283. 266	25A	5	43783. 40	+0. 10	<i>a</i> ⁴ P _{1½} —54375 _{3½}	
2283. 437	4	3	43780. 12	0. 00	<i>a</i> ⁴ D _{2½} —58747 _{1½}	
2284. 436	20	18	43760. 98	-0. 08	<i>a</i> ⁴ P _{0½} —52593 _{3½}	6
2284. 619	10	40	43757. 47	+0. 11	<i>a</i> ⁴ G _{2½} —59992 _{3½}	6
2285. 09	—?	1	43748. 45	-0. 01	20039 _{3½} —63788 _{3½}	
2285. 75	1	3	43735. 82	-0. 17	20780 _{4½} —64516 _{4½}	
2286. 28	5?	8	43725. 69	+0. 12	<i>a</i> ⁴ G _{4½} —60278 _{4½}	
2286. 476	6	4	43721. 94	+0. 16	<i>a</i> ⁴ F _{2½} —55022 _{3½}	
2286. 94	1 —	1	43713. 07	-0. 01	19276 _{2½} —62989 _{2½}	
2287. 46	8	5	43703. 13	-0. 18	<i>a</i> ⁴ G _{4½} —60256 _{3½}	
2289. 01	12A	8	43673. 5	+0. 3	20534 _{5½} —64207 _{4½}	
2289. 41	5	7	43665. 9	+0. 2	<i>a</i> ⁴ G _{4½} —60218 _{3½}	
2290. 48	2	2	43645. 5	+0. 1	19442 _{6½} —63087 _{3½}	
2290. 564	15	20	43643. 92	+0. 07	<i>a</i> ⁴ F _{1½} —52355 _{6½}	
2291. 376	4	7	43628. 45	-0. 47	19637 _{2½} —63266 _{3½}	
2291. 56	7	8	43625. 0	+0. 2	<i>a</i> ⁶ S _{2½} —51045 _{3½}	
2294. 20	—	3	43574. 7	+0. 3	20455 _{1½} —64030 _{3½}	
2294. 55	10?	35	43568. 1	-0. 1	<i>a</i> ⁶ D _{3½} —48284 _{3½}	res
2294. 84	10	20	43562. 6	+0. 1	<i>a</i> ⁴ D _{3½} —58709 _{3½}	
2295. 52	3	3	43549. 7	-0. 2	18000 _{3½} —61550 _{3½}	
2295. 78	15	20	43544. 8	+0. 1	<i>a</i> ⁴ P _{1½} —54137 _{1½}	6
2295. 985	15	25	43540. 88	+0. 02	<i>a</i> ⁴ D _{3½} —58687 _{4½}	
2296. 873	4	5	43524. 05	+0. 09	19442 _{6½} —62966 _{3½}	
2296. 956	8	6	43522. 47	+0. 02	<i>a</i> ⁴ P _{0½} —52355 _{6½}	
2297. 930	1	10	43504. 03	0. 00	22140 _{2½} —65644 _{3½}	
2298. 23	8	20	43498. 4	+0. 2	<i>a</i> ⁴ P _{2½} —56932 _{1½}	
2299. 807	6	18	43468. 53	-0. 10	23234 _{4½} —66703 _{3½}	
2300. 078	1	5	43463. 40	+0. 37	<i>a</i> ⁴ F _{3½} —56874 _{2½}	
2301. 284	3	5	43440. 63	-0. 26	<i>a</i> ⁴ P _{2½} —56874 _{3½}	
2301. 642	20	30	43433. 87	+0. 15	<i>a</i> ⁴ P _{1½} —54026 _{2½}	res
2302. 139	—	1	43424. 49	+0. 32	20455 _{1½} —63880 _{3½}	
2303. 274	25	50	43403. 10	+0. 57	<i>a</i> ⁴ G _{3½} —59992 _{2½}	
2303. 819	25	75	43392. 83	-0. 02	<i>a</i> ⁶ D _{1½} —44911 _{1½}	res
2304. 474	—	2	43380. 50	-0. 02	<i>a</i> ⁴ G _{4½} —59933 _{3½}	
2305. 219	4	8	43366. 48	+0. 12	19070 _{4½} —62437 _{4½}	
2305. 553	—	1	43360. 20	+0. 36	18000 _{3½} —61360 _{3½}	
2305. 705	—	1	43357. 34	+0. 69	<i>a</i> ⁴ F _{3½} —56768 _{3½}	
2305. 972	1	1	43352. 32	+0. 10	19637 _{2½} —62989 _{3½}	
2306. 419	2	3	43343. 92	-0. 07	<i>a</i> ⁴ G _{3½} —59933 _{3½}	
2306. 511	—?	4	43342. 19	-0. 05	18990 _{1½} —62333 _{2½}	
2306. 918	15	40	43334. 55	+0. 04	<i>a</i> ⁴ P _{2½} —56768 _{3½}	res
2307. 392	2	3	43325. 64	+0. 05	18000 _{3½} —61326 _{3½}	
2307. 930	5	10	43315. 54	-0. 46	<i>a</i> ⁴ G _{4½} —59869 _{3½}	
2309. 850	8	25	43279. 54	+0. 07	<i>a</i> ⁴ G _{3½} —59869 _{3½}	
2310. 244	4	12	43272. 16	+0. 14	19442 _{6½} —62714 _{6½}	
2312. 800	—	4	43224. 35	+0. 20	23046 _{3½} —66270 _{4½}	
2312. 907	6	20	43222. 35	+0. 01	<i>a</i> ⁴ D _{1½} —57856 _{3½}	
2314. 084	—	6	43200. 36	-0. 42	<i>a</i> ⁴ F _{3½} —56612 _{3½}	
2314. 637	10	25	43190. 04	+0. 08	<i>a</i> ⁴ D _{3½} —58336 _{3½}	
2315. 022	20	50	43182. 87	-0. 01	<i>a</i> ⁶ D _{2½} —46355 _{2½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2315. 246	3	4	43178. 69	+0. 05	<i>a</i> ⁴ P _{2½} —56612 _{3½}	
2317. 722	4	6	43132. 57	+0. 13	<i>a</i> ⁴ F _{3½} —56544 _{3½}	
2317. 88	6	10	43129. 62	-0. 08	<i>a</i> ⁴ F _{4½} —57986 _{3½}	
2318. 916	3	6	43110. 36	+0. 06	<i>a</i> ⁴ P _{2½} —56544 _{3½}	
2320. 832	6	5	43074. 76	+0. 02	<i>a</i> ⁴ F _{2½} —54375 _{3½}	
2321. 807	—	1	43056. 68	0. 00	19276 _{2½} —62333 _{3½}	
2322. 594	2	3	43042. 10	+0. 13	<i>a</i> ⁴ G _{2½} —59276 _{3½}	
2322. 720	5	8	43039. 76	-0. 02	<i>a</i> ⁴ D _{2½} —58007 _{1½}	
2323. 038	15	25	43033. 87	-0. 01	<i>a</i> ⁶ D _{4½} —49181 _{4½}	6
2324. 291	7	5	43010. 67	+0. 15	<i>a</i> ⁶ S _{2½} —50430 _{1½}	
2324. 714	1	1	43002. 84	-0. 06	<i>a</i> ⁶ D _{2½} —46175 _{3½}	
2324. 776	3	10	43001. 70	+0. 02	<i>a</i> ⁴ F _{3½} —56413 _{4½}	
2326. 091	15	60	42977. 38	+0. 11	22139 _{2½} —65141 _{3½}	
2327. 592	8A	5	42949. 67	+0. 02	<i>a</i> ⁶ D _{4½} —49124 _{3½}	
2327. 737	—	1	42947. 0	-0. 19	20039 _{3½} —62989 _{3½}	
				-0. 5	22194 _{3½} —65141 _{3½}	
2328. 314	20	35	42936. 35	-0. 05	<i>a</i> ⁶ D _{1½} —44455 _{6½}	res
2329. 691	6	15	42910. 98	+0. 06	<i>a</i> ⁴ D _{0½} —56084 _{1½}	
2330. 89	5	8	42888. 91	+0. 03	<i>a</i> ⁴ D _{2½} —57856 _{3½}	
2331. 778	3	4	42872. 57	-0. 13	<i>a</i> ⁴ F _{4½} —57729 _{3½}	
2331. 816	1	1	42871. 87	-0. 03	<i>a</i> ⁶ S _{2½} —50292 _{3½}	
2333. 146	25A	12	42847. 44	-0. 21	<i>a</i> ⁴ P _{1½} —53440 _{6½}	
2333. 462	—	1	42841. 64	-0. 05	<i>a</i> ⁴ G _{5½} —60278 _{4½}	
2333. 57	3	8	42839. 66	+0. 24	<i>a</i> ⁴ D _{3½} —57986 _{3½}	
2333. 770	15	35	42835. 98	-0. 06	<i>a</i> ⁶ D _{1½} —44354 _{3½}	res
2334. 070	5	5	42830. 48	+0. 02	<i>a</i> ⁴ P _{1½} —53422 _{1½}	
2335. 205	6	25	42809. 66	-0. 01	<i>a</i> ⁴ G _{3½} —59399 _{4½}	
2335. 548		5	42803. 38	+0. 16	25209 _{4½} —68012 _{3½}	
2335. 933	2	8	42796. 32	+0. 08	22194 _{3½} —64990 _{3½}	
2336. 716	6	15	42781. 98	+0. 16	<i>a</i> ⁴ G _{5½} —60218 _{3½}	
2337. 799	6	20	42762. 17	+0. 07	<i>a</i> ⁴ D _{2½} —57729 _{3½}	
2338. 125	—?	2	42756. 21	-0. 04	22139 _{2½} —64896 _{3½}	
2338. 582		1	42747. 86	-0. 24	23955 _{5½} —66703 _{3½}	
2339. 16	15	30	42737. 29	+0. 10	<i>a</i> ⁴ P _{1½} —53329 _{1½}	
2339. 732	10	8	42726. 84	+0. 07	<i>a</i> ⁴ F _{1½} —51438 _{2½}	
2339. 817	1	?	42725. 29	+0. 13	<i>a</i> ⁴ F _{2½} —54026 _{3½}	
2339. 904	6	20	42723. 70	+0. 03	<i>a</i> ⁴ G _{4½} —59276 _{3½}	
2340. 668	4	6	42709. 76	+0. 08	<i>a</i> ⁴ D _{3½} —57856 _{3½}	
2341. 074	4	15	42702. 35	+0. 21	22194 _{3½} —64896 _{3½}	
2341. 368	25	35	42696. 99	-0. 02	<i>a</i> ⁶ D _{3½} —47413 _{3½}	res
2341. 442	1—	2?	42695. 64	-0. 18	19637 _{2½} —62333 _{3½}	
2341. 903	1	6	42687. 24	+0. 10	<i>a</i> ⁴ G _{3½} —59276 _{3½}	
2346. 864	1	5	42597. 01	-0. 15	23046 _{3½} —65644 _{3½}	
2347. 644	1	3	42582. 86	-0. 04	<i>a</i> ⁴ D _{3½} —57729 _{3½}	
2348. 015		7	42576. 13	+0. 39	18990 _{1½} —61566 _{3½}	
2349. 262	3	20	42553. 53	-0. 02	20534 _{5½} —63087 _{6½}	
2349. 839	6	10	42543. 09	-0. 05	<i>a</i> ⁴ F _{1½} —51254 _{1½}	6
2350. 362	2	10	42533. 62	-0. 05	20455 _{1½} —62989 _{3½}	
2351. 052	2	6	42521. 14	+0. 14	<i>a</i> ⁴ P _{1½} —53113 _{3½}	
2351. 168	1—	1	42519. 04	+0. 26	19070 _{4½} —61589 _{3½}	
2351. 496	4	12	42513. 11	+0. 01	<i>a</i> ⁴ G _{2½} —58747 _{1½}	
2352. 924		4	42487. 31	+0. 07	22503 _{1½} —64990 _{3½}	
2353. 334	2	8	42479. 91	-0. 01	19070 _{4½} —61550 _{3½}	
2353. 667	1	5	42473. 90	-0. 07	18000 _{3½} —60474 _{3½}	
2354. 018		2	42467. 57	+0. 46	23803 _{3½} —66270 _{4½}	
2355. 019		4	42449. 52	-0. 41	23234 _{4½} —65684 _{3½}	
2356. 469	1	2	42423. 40	-0. 04	18000 _{3½} —60424 _{3½}	

TABLE 3. Classified lines of W II—Continued

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2357. 268	1	5	42409. 02	-0. 11	23234 _{4/2} —65644 _{3/2}	res
2357. 931		1	42397. 10	-0. 20	20039 _{3/2} —62437 _{1/2}	
2358. 816	12	18	42381. 19	+0. 01	a ⁶ D _{2/2} —45553 _{1/2}	
2361. 194	12A	10	42338. 51	-0. 09	a ⁴ G _{4/2} —58891 _{3/2}	
2362. 108	3	15	42322. 13	-0. 16	22194 _{3/2} —64516 _{1/2}	
2362. 484	1	10	42315. 40	-0. 15	23955 _{5/2} —66270 _{3/2}	
2362. 528	1	4?	42314. 61	-0. 02	a ⁴ D _{0/2} —55488 _{1/2}	
2363. 464	8	14	42297. 85	-0. 06	a ⁴ D _{1/2} —56932 _{1/2}	
2363. 721		1	42293. 25	-0. 21	20039 _{3/2} —62333 _{2/2}	
2363. 910	6	30	42289. 87	+0. 01	19070 _{4/2} —61360 _{1/2}	
2364. 225	10	50	42284. 24	+0. 06	a ⁴ D _{2/2} —57252 _{3/2}	
2364. 577	3	1	42277. 94	-0. 07	18000 _{3/2} —60278 _{1/2}	
2365. 832		7	42255. 52	-0. 09	19070 _{4/2} —61326 _{3/2}	
2366. 684	4	6	42240. 31	-0. 32	a ⁴ D _{1/2} —56874 _{2/2}	
2367. 132	1	3	42232. 32	+0. 08	a ⁴ F _{4/2} —57089 _{1/2}	
2368. 021		2	42216. 46	-0. 27	22139 _{2/2} —64356 _{3/2}	
2368. 36	8	14	42210. 42	-0. 06	a ⁴ P _{1/2} —52803 _{1/2}	
2369. 755	6	8	42185. 57	0. 00	a ⁶ D _{4/2} —48332 _{3/2}	
2370. 056	10	45	42180. 22	+0. 01	20534 _{5/2} —62714 _{6/2}	
2370. 624	5	12	42170. 11	-0. 02	19070 _{4/2} —61240 _{5/2}	
2371. 058	1	7	42162. 40	-0. 22	22194 _{3/2} —64356 _{3/2}	
2371. 218	2	5	42159. 55	-0. 09	19442 _{6/2} —61602 _{3/2}	
2371. 936	5	20	42146. 79	-0. 13	19442 _{6/2} —61589 _{3/2}	
2372. 610	5	30	42134. 82	+0. 08	a ⁴ G _{4/2} —58687 _{1/2}	
2373. 305		1	42122. 48	+0. 58	a ⁴ F _{2/2} —53422 _{1/2}	
2373. 462		4	42119. 69	-0. 20	a ⁴ G _{3/2} —58709 _{3/2}	
2373. 679	1	3	42115. 84	-0. 08	22194 _{3/2} —64310 _{3/2}	
2374. 454	5?	35	42102. 10	-0. 04	a ⁴ G _{2/2} —58336 _{3/2}	
2375. 044	4	20	42091. 64	+0. 11	23234 _{4/2} —65326 _{3/2}	
2377. 172	6	12	42053. 96	+0. 05	a ⁴ P _{2/2} —55488 _{1/2}	
2377. 393	6	8	42050. 06	+0. 29	19276 _{2/2} —61326 _{3/2}	
2378. 130	8	15	42037. 02	+0. 03	a ⁴ F _{2/2} —53338 _{3/2}	
2378. 603	10	15	42028. 67	+0. 04	a ⁴ F _{2/2} —53329 _{1/2}	
2379. 466	1	2	42013. 42	0. 00	22194 _{3/2} —64207 _{1/2}	
2380. 159	4	9	42001. 19	-0. 01	a ⁴ P _{1/2} —52593 _{0/2}	
2380. 708	3	5	41991. 51	+0. 01	18000 _{3/2} —59992 _{3/2}	
2381. 065	1	2	41985. 22	+0. 10	19070 _{4/2} —61055 _{1/2}	
2381. 333	6	8	41980. 47	+0. 06	a ⁴ F _{3/2} —55392 _{4/2}	
2382. 243	2	2	41964. 45	0. 00	a ⁴ D _{2/2} —56932 _{1/2}	
2382. 364	7	20	41962. 32	0. 00	a ⁴ G _{5/2} —59399 _{1/2}	
2382. 700		25	41956. 40	0. 00	23046 _{3/2} —65003 _{4/2}	
2383. 500	2	3	41942. 32	-0. 12	a ⁴ D _{3/2} —57089 _{1/2}	
2383. 884	1—	1	41935. 57	-0. 03	20780 _{4/2} —62715 _{1/2}	
2384. 033	3	6	41932. 95	-0. 01	18000 _{3/2} —59933 _{3/2}	
2385. 253	7	15	41911. 48	+0. 09	a ⁴ F _{4/2} —56768 _{3/2}	
2385. 335	5	7	41910. 04	0. 00	a ⁴ D _{1/2} —56544 _{2/2}	
2385. 500	8	12	41907. 14	-0. 03	a ⁴ D _{2/2} —56874 _{3/2}	
2386. 447	2	9	41890. 51	+0. 14	22139 _{2/2} —64030 _{2/2}	
2387. 708	2	5	41868. 39	-0. 05	18000 _{3/2} —59869 _{3/2}	
2388. 536	2	8	41853. 88	+0. 12	26158 _{4/2} —68012 _{3/2}	
2388. 798	2	8	41849. 28	-0. 14	23046 _{3/2} —64896 _{3/2}	
2389. 541		1	41836. 28	+0. 02	22194 _{3/2} —64030 _{3/2}	
2390. 371	25	75	41821. 75	+0. 08	a ⁸ S _{2/2} —49242 _{2/2}	
2390. 890	4	30	41812. 68	+0. 24	a ⁴ F _{2/2} —53113 _{3/2}	
2391. 218	1	3	41806. 94	0. 00	22503 _{1/2} —64310 _{3/2}	
2391. 574	2	3	41800. 71	-0. 08	a ⁴ D _{2/2} —56768 _{3/2}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2391. 717	4	8	41798. 22	-0. 05	19442 _{0½} —61240 _{5½}	res
2392. 932	20	60	41777. 00	-0. 11	a ⁶ D _{3½} —z ⁶ F _{4½}	
2393. 171	4	10	41772. 83	+0. 07	a ⁴ G _{3½} —58007 _{1½}	
2393. 768	1	3	41762. 41	-0. 18	a ⁴ F _{1½} —52355 _{0½}	
2394. 162	7	25	41755. 54	+0. 02	a ⁴ F _{4½} —56612 _{3½}	
2394. 444	12	7	41750. 62	+0. 28	a ⁴ F _{3½} —55162 _{2½}	res
2394. 636	1	7	41747. 27	-0. 04	a ⁴ G _{3½} —58336 _{3½}	
2395. 036	1	5	41740. 30	+0. 17	22139 _{2½} —63880 _{2½}	
2395. 104	9	10	41739. 12	+0. 01	a ⁶ D _{2½} —44911 _{1½}	
2395. 384	—	1	41734. 24	+0. 01	23234 _{4½} —64969 _{3½}	
2395. 664	1	3	41729. 36	-0. 04	23955 _{5½} —65684 _{5½}	res
2395. 730	5	8	41728. 21	+0. 01	a ⁴ P _{2½} —55162 _{2½}	
2396. 221	7	10	41719. 66	+0. 24	a ⁴ D _{3½} —56874 _{2½}	
2397. 097	—	200	41704. 42	-0. 03	a ⁴ F _{1½} —50430 _{1½}	
2397. 997	—	15	41688. 77	-0. 24	a ⁶ D _{2½} —z ⁶ F _{3½}	
2398. 149	—	7	41688. 77	-0. 14	19637 _{2½} —61326 _{3½}	res
2399. 332	4	12	41686. 12	+0. 10	22194 _{3½} —63880 _{3½}	
2399. 574	1	4	41665. 57	+0. 02	18990 _{1½} —60656 _{3½}	
2400. 358	1	6	41661. 37	+0. 02	23234 _{4½} —64896 _{3½}	
2400. 519	5	8	41647. 76	-0. 47	22139 _{2½} —63788 _{3½}	
2400. 866	4	2	41644. 97	+0. 05	a ⁴ D _{2½} —56612 _{3½}	res
2401. 863	5	12	41638. 95	-0. 13	a ⁶ D _{3½} —46355 _{2½}	
2402. 480	2	7	41621. 67	+0. 08	a ⁴ D _{3½} —56768 _{3½}	
2403. 074	5	10	41610. 98	+0. 08	a ⁴ F _{3½} —55022 _{3½}	
2403. 222	10	15	41600. 69	+0. 03	a ⁴ F _{2½} —52901 _{3½}	
2403. 455	4	10	41598. 13	-0. 16	a ⁴ P _{0½} —50430 _{1½}	res
2403. 762	1	2	41594. 10	-0. 02	22194 _{3½} —63788 _{3½}	
2405. 280	—?	8	41588. 79	+0. 03	a ⁴ P _{2½} —55022 _{3½}	
2405. 631	—?	1	41562. 54	+0. 11	a ⁶ S _{2½} —48982 _{1½}	
2406. 576	1—	1	41556. 48	+0. 06	a ⁴ F _{4½} —56413 _{4½}	
2407. 286	1	6	41540. 16	+0. 34	23450 _{2½} —64990 _{3½}	res
2407. 787	5	12	41527. 92	+0. 64	22503 _{1½} —64030 _{3½}	
2408. 282	12A	15	41519. 27	+0. 04	a ⁴ F _{4½} —56376 _{3½}	
2409. 226	5	20	41510. 73	-0. 13	20039 _{3½} —61550 _{3½}	
2409. 474	3	18	41494. 48	-0. 02	a ⁴ P _{1½} —52087 _{3½}	
2409. 827	—	4	41490. 21	+0. 42	18990 _{1½} —60474 _{2½}	res
2410. 694	1	2	41484. 13	-0. 36	23046 _{3½} —64516 _{4½}	
2410. 854	1	1	41469. 21	+0. 18	24804 _{3½} —66270 _{1½}	
2411. 287	7	3	41466. 46	-0. 09	a ⁴ D _{3½} —46175 _{3½}	
2411. 538	6	20	41459. 01	-0. 02	a ⁴ G _{5½} —58891 _{5½}	
2411. 820	10	25	41454. 70	-0. 08	a ⁴ D _{1½} —56084 _{1½}	4
2412. 064	2	2	41449. 86	-0. 06	23450 _{2½} —64896 _{3½}	
2412. 76	5	8	41445. 66	-0. 06	a ⁴ G _{4½} —57986 _{1½}	
2414. 118	4	7	41433. 72	+0. 13	a ⁶ S _{2½} —48830 _{3½}	
2414. 806	6	25	41410. 40	-0. 04	18000 _{3½} —59399 _{1½}	
2414. 888	3	3	41398. 60	-0. 05	a ⁴ G _{3½} —57986 _{1½}	4
2416. 063	1	3	41397. 20	+0. 02	22503 _{1½} —63880 _{3½}	
2416. 416	—	1	41377. 06	+0. 02	23955 _{5½} —65326 _{3½}	
2417. 430	2	4	41371. 02	+0. 02	19070 _{1½} —60424 _{3½}	
2419. 350	8	35	41353. 67	+0. 21	20039 _{3½} —61360 _{4½}	
2419. 848	4	5	41320. 85	+0. 05	a ⁴ D _{0½} —54485 _{0½}	4
2419. 987	3	8	41312. 34	+0. 12	23046 _{3½} —64356 _{3½}	
2420. 990	12	35	41309. 98	+0. 08	a ⁴ F _{3½} —54704 _{2½}	
2421. 358	1	3	41292. 86	+0. 21	20039 _{3½} —61326 _{3½}	
2421. 662	3	12	41286. 59	+0. 04	23234 _{4½} —64516 _{4½}	
			41281. 40	-0. 10		

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2421. 974	5	12	41276. 09	-0. 02	18000 _{3/2} —59276 _{3/2}	
2422. 292	30.A	20	41270. 67	+0. 16	<i>a</i> ⁴ P _{2/2} —54704 _{3/2}	
2422. 529	8	25	41266. 63	+0. 01	<i>a</i> ⁴ D _{1/2} —56413 _{3/2}	
2422. 726	1	4	41263. 28	+0. 08	23046 _{3/2} —64310 _{3/2}	
2425. 975	10.A	6	41208. 02	-0. 01	19070 _{4/2} —60278 _{3/2}	
2426. 482	1	4	41199. 42	+0. 06	23803 _{3/2} —65003 _{3/2}	
2426. 558	4	10	41198. 13	-0. 02	19276 _{2/2} —60474 _{3/2}	6
2427. 493	10	40	41182. 26	-0. 04	<i>a</i> ⁶ D _{2/2} —44354 _{3/2}	6 res
2427. 807	4	6	41176. 93	+0. 15	<i>a</i> ⁴ G _{1/2} —57729 _{3/2}	
2428. 758	4	10	41160. 80	+0. 10	23046 _{3/2} —64207 _{3/2}	
2429. 396	4	10	41149. 99	+0. 43	26929 _{5/2} —68078 _{6/2}	
2429. 489	4	6	41148. 42	+0. 26	19070 _{1/2} —60218 _{3/2}	
2429. 528	3	8	41147. 76	+0. 14	19276 _{2/2} —60424 _{3/2}	
2429. 971	1	6	41140. 26	+0. 01	<i>a</i> ⁴ G _{3/2} —57729 _{3/2}	6
2430. 788	3	10	41126. 44	+0. 11	22139 _{2/2} —63266 _{3/2}	
2431. 373	5	18	41116. 54	+0. 06	<i>a</i> ⁴ D _{2/2} —56084 _{1/2}	
2431. 714	5	12	41110. 78	+0. 01	20455 _{1/2} —61566 _{3/2}	
2432. 797		6	41092. 47	+0. 09	23803 _{1/2} —64896 _{3/2}	
2433. 139	5	8	41086. 70	+0. 09	<i>a</i> ⁴ F _{3/2} —54498 _{3/2}	6 res
2433. 982	25.A	20	41072. 47	+0. 25	22194 _{1/2} —63266 _{3/2}	
2434. 254	10.A	12	41067. 88	+0. 05	20534 _{5/2} —61602 _{6/2}	
2434. 453	5	8	41064. 53	+0. 06	<i>a</i> ⁴ P _{2/2} —54498 _{3/2}	
2435. 008	10	50	41055. 17	+0. 06	20534 _{5/2} —61589 _{5/2}	
2435. 445	4	20	41047. 80	0. 00	23955 _{5/2} —65003 _{3/2}	
2437. 155	1—	1	41019. 00	-0. 13	19637 _{2/2} —60656 _{3/2}	
2437. 332	3	6	41016. 02	-0. 04	20039 _{3/2} —61055 _{3/2}	
2437. 471	4	15	41013. 68	-0. 02	23955 _{5/2} —64969 _{3/2}	6
2439. 473	4	12	40980. 03	+0. 10	19276 _{2/2} —60256 _{3/2}	
2439. 808	2	7	40974. 40	+0. 20	<i>a</i> ⁴ F _{2/2} —52275 _{3/2}	
2439. 913	2	7	40972. 64	+0. 01	23234 _{4/2} —64207 _{3/2}	
2440. 432	10	20	40963. 93	+0. 11	<i>a</i> ⁴ D _{0/2} —54137 _{1/2}	
2441. 612	7	12	40944. 13			6
2441. 790		7	40941. 14	-0. 58	<i>a</i> ⁴ P _{2/2} —54375 _{3/2}	
2443. 858		2	40906. 51	+0. 31	23450 _{2/2} —64356 _{3/2}	
2446. 394	25	120	40864. 10	+0. 05	<i>a</i> ⁶ S _{2/2} —48284 _{2/2}	6
2446. 570	1	1	40861. 16	-0. 07	20039 _{3/2} —60900 _{3/2}	
2447. 255	4	12	40849. 73	+0. 10	22139 _{2/2} —62989 _{2/2}	
2447. 52		1	40845. 3	-0. 2	<i>a</i> ⁴ P _{1/2} —51438 _{3/2}	
2448. 00	5	15	40837. 3	0. 0	19637 _{2/2} —60474 _{3/2}	
2448. 237	4	50	40833. 34	+0. 04	23046 _{3/2} —63880 _{2/2}	
2448. 662	4	8	40826. 26	+0. 07	20534 _{5/2} —61360 _{3/2}	
2448. 719	3	4	40825. 31	-0. 03	18990 _{1/2} —59816 _{1/2}	
2449. 694	4	20	40809. 06	-0. 02	20780 _{4/2} —61589 _{5/2}	
2450. 324	2	7	40798. 57	+0. 11	19070 _{4/2} —59869 _{3/2}	
2451. 032	3	7	40786. 78	+0. 02	19637 _{2/2} —60424 _{3/2}	
2451. 468		50	40779. 53	+0. 11	<i>a</i> ⁶ D _{1/2} —42298 _{1/2}	
2451. 660		1	40776. 33	+0. 03	19442 _{3/2} —60218 _{3/2}	
2453. 760	3	10	40741. 44	0. 04	23046 _{3/2} —63783 _{3/2}	
2455. 506	40.A	10	40712. 48	-0. 05	23803 _{3/2} —64516 _{3/2}	
2455. 722	2	5	40708. 90	+0. 04	18000 _{3/2} —58709 _{3/2}	
2455. 866	6	35	40706. 51	+0. 05	20534 _{5/2} —61240 _{5/2}	6
2456. 072	4	8	40703. 09	-0. 01	<i>a</i> ⁴ P _{2/2} —54137 _{1/2}	
2457. 043	1	3	40687. 01	-0. 17	18000 _{3/2} —58687 _{4/2}	
2458. 529	3	4?	40662. 42	+0. 09	<i>a</i> ⁴ G _{3/2} —57252 _{3/2}	
2458. 564	5	30	40661. 84	-0. 04	<i>a</i> ⁴ P _{1/2} —51254 _{1/2}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2458. 838	3	20	40657. 31	+0. 17	19276 _{2½} —59933 _{3½}	6
2459. 602	20	10	40644. 68	+0. 10	<i>a</i> ⁴ F _{3½} —54056 _{4½}	
2459. 876	4	30	40640. 15	0. 00	<i>a</i> ⁴ G _{2½} —56874 _{2½}	
2461. 148	5	20	40619. 15	+0. 08	19637 _{2½} —60256 _{3½}	
2461. 294	3	8	40616. 74	-0. 03	20039 _{3½} —60656 _{3½}	
2461. 442	5	15	40614. 30	+0. 02	<i>a</i> ⁴ F _{3½} —54026 _{3½}	
2464. 616	15	40	40562. 00	+0. 05	<i>a</i> ⁴ F _{2½} —51863 _{3½}	7
2464. 70	1	4	40560. 6	-0. 4	23955 _{5½} —64516 _{4½}	
2465. 148		15	40553. 25	-0. 08	23234 _{4½} —63788 _{3½}	
2465. 598	2	7	40545. 85	-0. 06	20780 _{4½} —61326 _{3½}	
2465. 667	2	20	40544. 72	-0. 04	26158 _{4½} —66703 _{5½}	
2465. 962	4	30	40539. 87	+0. 09	19276 _{2½} —59816 _{1½}	
2466. 176	2	5	40536. 35	+0. 03	<i>a</i> ⁴ G _{4½} —57089 _{4½}	res
2466. 330	5	10	40533. 82	+0. 05	<i>a</i> ⁴ G _{2½} —56768 _{3½}	
2466. 522	35	80	40530. 66	+0. 01	<i>a</i> ⁶ D _{1½} — <i>z</i> ⁶ F _{3½}	
				-0. 18	<i>a</i> ⁴ F _{1½} —49242 _{2½}	
2467. 078	3	9	40521. 53	+0. 08	20534 _{5½} —61055 _{4½}	
2468. 006	2	10	40506. 29	+0. 13	23803 _{3½} —64310 _{3½}	
2468. 404	6	15	40499. 76	-0. 03	<i>a</i> ⁴ G _{3½} —57089 _{4½}	4
2469. 206	2	6	40486. 61	+0. 07	22503 _{1½} —62989 _{3½}	
2469. 873	3	25	40475. 67	+0. 15	25209 _{4½} —65684 _{5½}	
2470. 804	8	70	40460. 43	0. 00	20780 _{4½} —61240 _{5½}	
2471. 740	15	40	40445. 11	+0. 07	20455 _{1½} —60900 _{3½}	
2472. 380	1	3	40434. 64	-0. 29	20039 _{3½} —60474 _{2½}	
2473. 752		1	40412. 21	-0. 01	19404 _{0½} —59816 _{1½}	res
2474. 278		2	40403. 62	-0. 04	23803 _{3½} —64207 _{4½}	
2475. 474	1	3	40384. 43	+0. 03	20039 _{3½} —60424 _{3½}	
2475. 588	3	50	40382. 24			
2475. 844	4	10	40378. 07	+0. 17	<i>a</i> ⁴ G _{2½} —56612 _{3½}	
2477. 284	3	15	40354. 60	-0. 22	19637 _{2½} —59992 _{2½}	
2477. 796	30	200	40346. 26	-0. 01	<i>a</i> ⁶ D _{4½} — <i>z</i> ⁶ F _{4½}	6
2478. 313	2	20	40337. 84	+0. 14	23450 _{2½} —63788 _{3½}	
2478. 402	2	6	40336. 40	+0. 12	18000 _{3½} —58336 _{3½}	
2478. 874	4	10	40328. 72	+0. 06	19070 _{4½} —59399 _{4½}	
2480. 041	3	4	40309. 74	+0. 18	<i>a</i> ⁴ G _{2½} —56544 _{2½}	
2480. 867	3	6	40296. 32	+0. 04	19637 _{2½} —59933 _{3½}	
2481. 546	10	30	40285. 30	-0. 02	<i>a</i> ⁴ G _{3½} —56874 _{2½}	res
2482. 154		3	40275. 43	+0. 01	20780 _{4½} —61055 _{4½}	
2482. 390	3	2	40271. 60	0. 00	<i>a</i> ⁴ F _{1½} —48982 _{1½}	
2482. 688	3	4	40266. 77	-0. 02	<i>a</i> ⁴ D _{0½} —53440 _{0½}	
2483. 592	4	12	40252. 11	+0. 01	23955 _{5½} —64207 _{4½}	
2483. 744	5	7	40249. 64	+0. 04	<i>a</i> ⁴ D _{0½} —53422 _{0½}	
2484. 008	7	20	40245. 37	+0. 02	<i>a</i> ⁴ D _{3½} —55392 _{4½}	7
2484. 404	7	40	40238. 95	-0. 02	20039 _{3½} —60278 _{3½}	
2484. 848	2	4	40231. 76	0. 00	19637 _{2½} —59869 _{3½}	
2485. 160	1	2	40226. 71	+0. 21	23803 _{3½} —64030 _{3½}	
2485. 606	1	3	40219. 50	0. 00	23046 _{3½} —63266 _{3½}	
2485. 779	5	15	40216. 70	-0. 01	20039 _{3½} —60256 _{3½}	
2486. 429	6	18	40206. 18	+0. 05	19070 _{4½} —59276 _{3½}	4
2486. 776	3	6	40200. 57	-0. 01	20455 _{1½} —60656 _{3½}	
2487. 155	2	1	40194. 45	-0. 03	<i>a</i> ⁴ D _{2½} —55162 _{2½}	
2487. 231	3	5	40193. 22	-0. 01	22139 _{2½} —62333 _{3½}	
2488. 120	8	30	40178. 86	+0. 08	<i>a</i> ⁴ G _{3½} —56768 _{3½}	
				-0. 06	19637 _{2½} —59816 _{1½}	
2488. 780	30	120	40168. 21	0. 00	<i>a</i> ⁶ S _{2½} —47588 _{1½}	res
2488. 932	15	7	40165. 76	+0. 12	<i>a</i> ⁴ F _{4½} —55022 _{3½}	
2489. 231	40	200	40160. 93	+0. 07	<i>a</i> ⁶ D _{3½} — <i>z</i> ⁶ F _{3½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	<i>O-C</i>		
Air						
2489. 514	5	12	40156. 37	+0. 04	<i>a</i> ⁴ D _{3/2} —53329 _{1/2} ¹	
2489. 900	5	10	40150. 14	-0. 06	<i>a</i> ⁴ P _{0/2} —48982 _{1/2} ¹	
2490. 586	4	15	40139. 08	-0. 04	22194 _{3/2} —62333 _{3/2} ³	
2490. 718	12	25	40136. 95	0. 00	<i>a</i> ⁴ F _{2/2} —51438 _{2/2} ²	
2492. 252	4	14	40112. 25	+0. 04	26158 _{4/2} —66270 _{4/2} ⁴	
2492. 928	8	80	40101. 38	+0. 02	<i>a</i> ⁴ F _{4/2} —54958 _{3/2} ³	
2493. 54	3	7	40091. 54	-0. 01	24804 _{3/2} —64896 _{3/2} ³	
2494. 738		2	40072. 29	+0. 07	24918 _{1/2} —64990 _{3/2} ³	
2494. 872		7	40070. 14	-0. 11	<i>a</i> ⁴ D _{1/2} —54704 _{2/2} ²	
2495. 522	5	10	40059. 70	+0. 10	<i>a</i> ⁴ G _{4/2} —56612 _{3/2} ³	
2496. 648	50	120	40041. 63	-0. 15	<i>a</i> ⁶ D _{3/2} —44758 _{3/2} ³	5
2497. 480	35	75	40028. 29	+0. 03	<i>a</i> ⁶ D _{4/2} —46175 _{3/2} ³	5
2498. 076	2	3	40018. 74	0. 00	20455 _{1/2} —60474 _{2/2} ³	
2499. 223	8	16	40000. 38	+0. 09	19276 _{2/2} —59276 _{3/2} ³	
2499. 330	2	4	39998. 67	-0. 09	24991 _{1/2} —64990 _{2/2} ³	
2499. 692	15	100	39992. 88	-0. 02	<i>a</i> ⁶ S _{2/2} —47413 _{2/2} ²	
2499. 934	3	4	39989. 00	+0. 12	<i>a</i> ⁴ P _{2/2} —53422 _{1/2} ¹	
2500. 11	12	30	39986. 19	-0. 03	18000 _{3/2} —57986 _{4/2} ⁴	
2500. 217	1	3	39984. 48	+0. 12	23803 _{3/2} —63788 _{3/2} ³	
2501. 020	1	10	39971. 64	-0. 05	25169 _{1/2} —65141 _{2/2} ²	res
2501. 877		10	39957. 95	-0. 06	<i>a</i> ⁴ F _{3/2} —53369 _{4/2} ⁴	
2502. 072	2	10	39954. 84	+0. 11	<i>a</i> ⁴ G _{3/2} —56544 _{3/2} ³	
2502. 162	3	4?	39953. 40	+0. 08	<i>a</i> ⁴ F _{2/2} —51254 _{1/2} ¹	
2502. 836	1	3	39942. 64	-0. 16	23046 _{3/2} —62989 _{3/2} ³	
2505. 264		1	39903. 93	-0. 04	<i>a</i> ⁴ P _{2/2} —53338 _{3/2} ³	
2505. 790	3	5	39895. 56	-0. 05	<i>a</i> ⁴ P _{2/2} —53329 _{1/2} ¹	
2506. 048	—?	80	39891. 45	+0. 15	28187 _{6/2} —68078 _{6/2} ⁶	6
2507. 994	12	30	39860. 50	0. 00	<i>a</i> ⁴ G _{4/2} —56413 _{3/2} ³	6
2508. 274	2	3	39856. 05	+0. 05	18000 _{3/2} —57856 _{3/2} ³	
2508. 582	1	3	39851. 16	-0. 08	<i>a</i> ⁴ D _{1/2} —54485 _{0/2} ⁰	
2508. 690	—?	4	39849. 44	-0. 02	<i>a</i> ⁴ G _{2/2} —56084 _{1/2} ¹	
2509. 386	2	3	39838. 39	-0. 04	<i>a</i> ⁴ P _{1/2} —50430 _{1/2} ¹	
2509. 955	6	40	39829. 35	-0. 05	20039 _{3/2} —59869 _{3/2} ³	7
2510. 246		3	39824. 74	-0. 16	28187 _{6/2} —68012 _{3/2} ³	
2510. 348	—?	2	39823. 12	-0. 19	<i>a</i> ⁴ G _{4/2} —56376 _{3/2} ³	
2510. 482	8	80	39821. 00	-0. 06	19070 _{4/2} —58891 _{3/2} ³	
2510. 799		3	39815. 97	+0. 17	23450 _{2/2} —63266 _{3/2} ³	
2512. 186	2	4	39793. 99	+0. 07	25209 _{4/2} —65003 _{4/2} ⁴	
2513. 435	1	30	39774. 22	+0. 06	26929 _{5/2} —66703 _{5/2} ⁵	6
2514. 358	2	4	39759. 62	+0. 11	<i>a</i> ⁶ S _{2/2} —47179 _{1/2} ¹	
2514. 526	3	20	39756. 96	-0. 02	18990 _{1/2} —58747 _{1/2} ¹	res
2515. 324	3	30	39744. 35	+0. 18	<i>a</i> ⁴ F _{2/2} —51045 _{3/2} ³	
2515. 508	5	8	39741. 44	-0. 01	20534 _{5/2} —60278 _{4/2} ⁴	
2515. 806	2	10	39736. 73	-0. 02	<i>a</i> ⁴ D _{1/2} —54375 _{3/2} ³	
2516. 138		10	39731. 49	-0. 06	<i>a</i> ⁴ D _{2/2} —54704 _{2/2} ²	
				-0. 14	23234 _{4/2} —62966 _{5/2} ⁵	
2516. 284	1	3	39729. 18	-0. 04	18000 _{3/2} —57729 _{3/2} ³	
2517. 406	1	25	39711. 48	-0. 22	24804 _{3/2} —64516 _{4/2} ⁴	5
2518. 144	6	50	39699. 84	+0. 03	<i>a</i> ⁴ P _{1/2} —50292 _{2/2} ²	
2518. 973		4	39686. 78	-0. 16	25209 _{4/2} —64896 _{3/2} ³	
2519. 126	4	7	39684. 37	-0. 12	20534 _{5/2} —60218 _{3/2} ³	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2519.444	8	30	39679.36	-0.06	<i>a</i> ⁴ P _{2½} —53113 _{2½}	res
2520.10	1	3	39669.0	-0.2	23040 _{3½} —62715 _{4½}	
2521.156	3	10	39652.42	-0.02	<i>a</i> ⁴ G _{5½} —57089 _{4½}	
2521.686	3A	3	39644.09	+0.33	20780 _{4½} —60424 _{3½}	
2521.853	3	3	39641.46	+0.11	<i>a</i> ⁴ F _{4½} —54498 _{3½}	
2522.039	30	60	39638.54	+0.04	<i>a</i> ⁶ D _{3½} —44354 _{2½}	
2522.270	3	8	39634.91	+0.21	28377 _{5½} —68012 _{5½}	
2526.208	4	10	39573.12	-0.10	<i>a</i> ⁴ F _{1½} —48284 _{3½}	res
2527.200	2	15	39557.59	0.00	<i>a</i> ⁴ D _{3½} —54704 _{2½}	
2527.552	2	10	39552.08	+0.05	24804 _{3½} —64356 _{3½}	
2528.560	—?	8	39536.32	+0.05	20455 _{1½} —59992 _{2½}	
2528.913	5	20	39530.80	+0.05	<i>a</i> ⁴ D _{2½} —54498 _{3½}	res
2529.209	2	8	39526.17	+0.11	26158 _{4½} —65684 _{5½}	
2530.54	1	4	39505.38	+0.05	24804 _{3½} —64310 _{2½}	
2530.70	10	8	39502.88	+0.04	<i>a</i> ⁴ D _{1½} —54137 _{1½}	
2530.986	5	50	39498.42	+0.09	20780 _{1½} —60278 _{1½}	
2532.085	1	1	39481.28	+0.17	23234 _{4½} —62715 _{4½}	
2532.414	4	7	39476.15	+0.08	20780 _{4½} —60256 _{3½}	
2532.711	2	5	39471.52	+0.10	19276 _{2½} —58747 _{1½}	
2532.842	2	3	39469.48	+0.08	25672 _{2½} —65141 _{2½}	
2532.960	6	15	39467.64	0.00	<i>a</i> ⁴ P _{2½} —52901 _{3½}	
2533.278	2	7	39462.69	+0.23	23803 _{3½} —63266 _{3½}	
2534.140	5	30	39449.27	+0.07	19442 _{0½} —58891 _{5½}	7
2534.829	5	50	39438.55	+0.09	20780 _{0½} —60218 _{5½}	7
2535.178		3	39433.12	+0.08	19276 _{2½} —58709 _{3½}	
2535.573	1	10	39426.98	+0.25	22139 _{2½} —61566 _{2½}	4
2536.000	6	40	39420.34	0.00	<i>a</i> ⁴ D _{0½} —52593 _{0½}	
2536.622	2	25	39410.67	+0.04	22139 _{2½} —61550 _{3½}	
2536.789	1	1	39408.07	+0.07	<i>a</i> ⁴ D _{2½} —54375 _{2½}	
2537.133	1	30	39402.73	-0.10	24804 _{3½} —64207 _{1½}	7
2539.313	7	35	39368.91	+0.01	<i>a</i> ⁴ P _{2½} —52803 _{1½}	
2539.869	1	8	39360.29	-0.08	20455 _{1½} —59816 _{1½}	
2539.919	3	20	39359.52	-0.08	20039 _{3½} —59399 _{4½}	4
2540.101	1		39356.70	+0.18	22194 _{3½} —61550 _{3½}	
2540.431	1	4	39351.58	+0.03	<i>a</i> ⁴ D _{3½} —54498 _{3½}	
2540.807		2	39345.76	-0.26	18990 _{1½} —58336 _{2½}	
2540.925	10A	4	39343.93	+0.07	19404 _{0½} —58747 _{1½}	
2541.063	6	20	39341.80	+0.19	26929 _{5½} —66270 _{4½}	
2542.598	1	30	39318.05	-0.11	25672 _{2½} —64990 _{2½}	6
2543.308	2	25	39307.07	-0.02	25209 _{4½} —64516 _{1½}	6
2544.658		1	39286.22	-0.18	23046 _{3½} —62333 _{2½}	
2546.283	3	30	39261.15			
2546.790	1	15	39253.33	+0.16	<i>a</i> ⁴ G _{2½} —55488 _{1½}	res
2546.912	1	2	39251.45	+0.15	18000 _{3½} —57252 _{2½}	
2547.838		5	39237.19	+0.12	20039 _{3½} —59276 _{3½}	
2548.378	6	20	39228.88	+0.08	<i>a</i> ⁴ D _{3½} —54375 _{2½}	
2548.690	1	6	39224.08	+0.02	25672 _{2½} —64896 _{3½}	
2549.096	5	15	39217.83	+0.08	<i>a</i> ⁶ D _{2½} —42390 _{3½}	res
2550.10		4	39202.38	+0.21	23235 _{4½} —62437 _{4½}	
2550.295	5	8	39199.39	+0.07	<i>a</i> ⁴ F _{4½} —54056 _{4½}	
2551.157	1	10	39186.15	-0.17	22139 _{2½} —61326 _{3½}	
2551.450		15	39181.65	-0.08	<i>a</i> ⁴ D _{0½} —52355 _{0½}	res
2552.249	5	5	39169.38	0.00	<i>a</i> ⁴ D _{2½} —54137 _{1½}	
2552.362	4	40	39167.65	-0.01	26158 _{4½} —65326 _{5½}	7
2553.168	70A	50	39155.29	+0.10	<i>a</i> ⁴ F _{3½} —52567 _{4½}	res

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2553. 308	1	7	39153. 14	-0. 14	20780 _{4½} —59933 _{3½}	
2553. 693		1	39147. 24	-0. 18	25209 _{4½} —64356 _{3½}	
2554. 665	15	70	39132. 34	-0. 16	23955 _{5½} —63087 _{6½}	
2554. 864	40	60	39129. 30	+0. 13	22194 _{3½} —61326 _{3½}	
2555. 106	40	100	39125. 59	-0. 11	<i>a</i> ⁶ D _{0½} — <i>z</i> ⁶ F _{1½}	
				-0. 09	<i>a</i> ⁶ D _{2½} —42298 _{1½}	
2556. 092		6	39110. 50	-0. 06	19637 _{2½} —58747 _{1½}	
2557. 511		2	39088. 80	+0. 04	18000 _{3½} —57089 _{4½}	
2558. 582		12	39072. 44	+0. 26	19637 _{2½} —58709 _{3½}	
2559. 170		1	39063. 46	-0. 18	22503 _{1½} —61566 _{2½}	
2559. 500	7	40	39058. 43	+0. 01	<i>a</i> ⁴ D _{2½} —54026 _{3½}	6
2560. 788		9	39038. 78	0. 00	24991 _{1½} —64030 _{3½}	
2562. 244	1	9	39016. 60	-0. 04	18990 _{1½} —58007 _{1½}	6
2562. 594	1	8	39011. 27	+0. 17	23955 _{5½} —62966 _{5½}	
2563. 166	20	200	39002. 57	-0. 01	<i>a</i> ⁴ G _{5½} —56439 _{6½}	4
2563. 432		5	38998. 52	+0. 30	25209 _{4½} —64207 _{4½}	
2563. 534	1	4	38996. 97	-0. 12	27273 _{3½} —66270 _{3½}	
2563. 914	12	30	38991. 19	-0. 06	<i>a</i> ⁴ F _{2½} —50292 _{2½}	6 res
2564. 424		8	38983. 43	-0. 10	24804 _{3½} —63788 _{3½}	7
2565. 834		7	38962. 01	+0. 01	24918 _{1½} —63880 _{3½}	
2567. 320		1	38939. 46	+0. 03	<i>a</i> ⁴ G _{5½} —56376 _{5½}	
2567. 620	10	30	38934. 92	-0. 05	<i>a</i> ⁶ S _{2½} —46355 _{3½}	6 res
2568. 108	2	10	38927. 52	+0. 06	<i>a</i> ⁴ G _{2½} —55162 _{2½}	
2568. 850	10	30	38916. 28	+0. 03	19070 _{4½} —57986 _{4½}	6
2569. 123	1	3	38912. 14	0. 00	23803 _{3½} —62715 _{4½}	
2569. 298	8	80	38909. 49	-0. 03	<i>a</i> ⁴ D _{3½} —54056 _{4½}	5
2570. 701		2	38888. 26	-0. 28	24991 _{1½} —63880 _{3½}	
2571. 459	50	150	38876. 79	-0. 14	<i>a</i> ⁶ D _{2½} — <i>z</i> ⁶ F _{3½}	res
2571. 632	3	15	38874. 18	-0. 11	18000 _{3½} —56874 _{3½}	
2572. 240	8	45	38864. 99	0. 00	20534 _{5½} —59399 _{4½}	
2572. 366	8	30	38863. 08	-0. 24	<i>a</i> ⁴ F _{3½} —52275 _{3½}	
2572. 572		25	38859. 97	-0. 50	25169 _{1½} —64030 _{3½}	
2573. 605		9	38844. 38	-0. 08	26158 _{4½} —65003 _{3½}	
2573. 820	3	12	38841. 13	-0. 05	<i>a</i> ⁴ P _{2½} —52275 _{3½}	
2573. 952	15A	7	38839. 14	-0. 09	<i>a</i> ⁴ G _{4½} —55392 _{4½}	
2576. 168	7	30	38805. 73	-0. 08	<i>a</i> ⁴ D _{1½} —53440 _{0½}	
2576. 372	8	40	38802. 66	-0. 04	<i>a</i> ⁴ G _{3½} —55392 _{4½}	
2577. 308		5	38788. 57	-0. 05	<i>a</i> ⁴ D _{1½} —53422 _{1½}	
2578. 695	8	3	38767. 71	-0. 20	18000 _{3½} —56768 _{3½}	
2579. 266	20	70	38759. 13	-0. 03	23955 _{5½} —62714 _{6½}	7
				-0. 32	<i>a</i> ⁴ P _{0½} —47588 _{1½}	
2579. 497		20	38755. 66	+0. 20	26929 _{5½} —65684 _{5½}	
2579. 542	20	100	38754. 98	-0. 01	<i>a</i> ⁶ S _{2½} —46175 _{3½}	res
2581. 140	2	8	38730. 99	-0. 09	19276 _{2½} —58007 _{1½}	
2581. 206	18	30	38730. 00	-0. 02	<i>a</i> ⁶ D _{4½} — <i>z</i> ⁶ F _{3½}	
2582. 527	1	5	38710. 19	-0. 04	25169 _{1½} —63880 _{3½}	
2582. 746	1	4	38706. 90	+0. 01	22194 _{3½} —60900 _{2½}	
2583. 520	3	5	38695. 31	-0. 04	<i>a</i> ⁴ D _{1½} —53329 _{1½}	6
2584. 236	12A	5	38684. 59	+0. 05	25672 _{2½} —64356 _{3½}	
2585. 146		4	38670. 97	+0. 03	29341 _{4½} —68012 _{5½}	
2585. 934	6	30	38659. 18	-0. 06	19070 _{4½} —57729 _{3½}	
2586. 350	8	25	38652. 97	+0. 05	<i>a</i> ⁴ P _{2½} —52087 _{2½}	6
2586. 586	1	5	38649. 44	-0. 14	<i>a</i> ⁴ P _{1½} —49242 _{2½}	
2587. 367		6	38637. 78	-0. 06	25672 _{2½} —64310 _{3½}	
2587. 676	2	9	38633. 17	-0. 03	23803 _{3½} —62437 _{4½}	
2589. 171	30	90	38610. 86	-0. 08	<i>a</i> ⁶ D _{4½} —44758 _{4½}	
2589. 661	4	9	38603. 56	+0. 04	19404 _{0½} —58007 _{1½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2591. 229		2	38580. 20	+0. 02	19276 _{2½} —57856 _{2½}	
2591. 492	14	12	38576. 28	-0. 04	<i>a</i> ⁶ D _{0½} — <i>z</i> ² S _{0½}	
2591. 738	1	4	38572. 62	-0. 01	<i>a</i> ⁴ G _{3½} —55162 _{2½}	
2592. 458	3	3	38561. 91	-0. 07	<i>a</i> ⁴ P _{1½} —49154 _{0½}	
2593. 686	1	2	38543. 65	-0. 05	18000 _{3½} —56544 _{2½}	
2594. 645		2	38529. 41	+0. 05	23803 _{3½} —62333 _{2½}	
2595. 506	2	7	38516. 63	+0. 09	22139 _{2½} —60656 _{2½}	7
2595. 580	5	5	38515. 53	-0. 37	28187 _{6½} —66703 _{5½}	
2595. 764	3	8	38512. 80	+0. 05	<i>a</i> ⁴ F _{4½} —53369 _{4½}	6
2596. 867	3	15	38496. 44	+0. 01	20780 _{4½} —59276 _{3½}	7
2597. 866	2	25	38481. 64	0. 00	23955 _{5½} —62437 _{4½}	7
2598. 672	7A	7	38469. 71	-0. 06	<i>a</i> ⁴ G _{2½} —54704 _{2½}	
2598. 748	20	35	38468. 58	-0. 01	<i>a</i> ⁴ G _{4½} —55022 _{3½}	
2599. 174	1—	1	38462. 27	-0. 10	<i>a</i> ⁴ F _{4½} —47179 _{1½}	
2599. 652	3	7	38455. 20	-0. 16	22194 _{3½} —60656 _{2½}	
				+0. 04	<i>a</i> ⁴ D _{2½} —53422 _{1½}	
2599. 772	4	20	38453. 42	+0. 02	19276 _{2½} —57729 _{3½}	res
2601. 141	1	6	38433. 19	0. 00	<i>a</i> ⁴ G _{3½} —55022 _{3½}	res
2601. 430	8	30	38428. 92	-0. 01	<i>a</i> ⁴ P _{2½} —51863 _{3½}	
2602. 166	2	1	38418. 06	-0. 01	<i>a</i> ⁶ D _{1½} —39936 _{2½}	
2602. 516	12	75	38412. 89	+0. 03	<i>a</i> ⁶ D _{1½} —39936 _{2½}	
				-0. 05	18000 _{3½} —56413 _{4½}	
2603. 018	20	120	38405. 48	+0. 04	<i>a</i> ⁴ G _{4½} —54958 _{3½}	7
2603. 609		3	38396. 76	-0. 30	26929 _{3½} —65326 _{3½}	
2604. 042	2	6	38390. 38	+0. 04	<i>a</i> ⁴ P _{1½} —48982 _{1½}	6
2605. 410	—?	5	38370. 23	-0. 02	<i>a</i> ⁴ D _{3½} —53338 _{3½}	
2605. 973	7	15	38361. 94	+0. 01	19637 _{2½} —58007 _{1½}	
				+0. 05	<i>a</i> ⁴ D _{2½} —53329 _{1½}	res
2606. 227		2?	38358. 20	+0. 02	25672 _{2½} —64030 _{3½}	
2606. 273	2	20	38357. 52	-0. 11	26158 _{4½} —64516 _{4½}	
				+0. 13	20534 _{5½} —58891 _{5½}	
2606. 472	4	40	38354. 59	0. 00	23234 _{4½} —61589 _{5½}	
2606. 974	4	12	38347. 21	-0. 07	<i>a</i> ⁴ P _{0½} —47179 _{1½}	
2607. 822		20	38334. 74	+0. 04	22139 _{2½} —60474 _{2½}	7
2608. 440		5	38325. 66	-0. 04	28377 _{5½} —66703 _{5½}	
2609. 116	2	7	38315. 72	-0. 01	23234 _{4½} —61550 _{3½}	
2609. 250	4	40	38313. 76	+0. 02	23046 _{3½} —61360 _{4½}	5
2610. 370	1	3	38297. 32	-0. 08	20039 _{3½} —58336 _{2½}	
2611. 264	1	8	38284. 21	+0. 04	22139 _{2½} —60424 _{3½}	
2611. 510		1	38280. 60	+0. 01	22194 _{3½} —60474 _{2½}	
2611. 592	1	6	38279. 40	-0. 09	23046 _{3½} —61326 _{3½}	6
2612. 667	4	15	38263. 65	-0. 08	<i>a</i> ⁴ G _{2½} —54498 _{3½}	
2612. 848		2	38261. 00	-0. 04	18990 _{1½} —57252 _{2½}	
2614. 956		2	38230. 16	+0. 10	22194 _{3½} —60424 _{3½}	
2615. 446	20	80	38223. 00	+0. 05	<i>a</i> ⁴ D _{3½} —53369 _{4½}	
2615. 701	3	15	38219. 27	-0. 05	19637 _{2½} —57856 _{2½}	
2617. 162	1	2	38197. 94	-0. 02	26158 _{4½} —64356 _{3½}	
2617. 636		5	38191. 02	-0. 03	<i>a</i> ⁴ D _{3½} —53338 _{3½}	6
2618. 072	1	7	38184. 66	-0. 27	24804 _{3½} —62989 _{3½}	
2619. 18	40A	15	38168. 50	-0. 14	<i>a</i> ⁴ D _{1½} —52803 _{1½}	
2620. 215	50A	60	38153. 43	-0. 02	22503 _{1½} —60656 _{2½}	4
2620. 757	7	30	38145. 54	-0. 16	<i>a</i> ⁴ D _{2½} —53113 _{2½}	res
2621. 074		2	38140. 93	-0. 05	<i>a</i> ⁴ G _{2½} —54375 _{2½}	
2621. 601	5	12	38133. 26	-0. 01	<i>a</i> ⁶ S _{2½} —45553 _{1½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2621. 826		1	38129. 99	+0. 29	26227 _{2½} —64356 _{3½}	
2622. 778	1	5	38116. 15	-0. 05	23450 _{2½} —61566 _{2½}	
2622. 873	1	2	38114. 77	-0. 17	<i>a</i> ⁴ G _{3½} —54704 _{3½}	
2623. 114	6	50	38111. 27	-0. 09	20780 _{4½} —58891 _{3½}	
2623. 890	2	8	38100. 00	-0. 10	23450 _{2½} —61550 _{3½}	res
2624. 401		3	38092. 58	+0. 04	19637 _{2½} —57729 _{3½}	
2624. 488	2	15	38091. 32	-0. 10	23234 _{4½} —61326 _{3½}	
2624. 952		4	38084. 59	-0. 04	22194 _{3½} —60278 _{4½}	
2625. 058		3	38083. 05	+0. 05	26227 _{2½} —64310 _{3½}	
2625. 863		4	38071. 38	-0. 12	24918 _{1½} —62989 _{3½}	
2626. 486		12	38062. 35	-0. 02	22194 _{3½} —60256 _{3½}	6
2626. 851		3	38057. 06	+0. 04	25209 _{4½} —63266 _{3½}	
2627. 722	4	10	38044. 44	-0. 08	<i>a</i> ⁴ F _{4½} —52901 _{3½}	
2628. 045	1	8	38039. 76	0. 00	26929 _{5½} —64969 _{3½}	
2628. 996	7	35	38026. 00	-0. 07	<i>a</i> ⁴ F _{3½} —51438 _{2½}	4
2629. 496	1	5	38018. 78	0. 00	19070 _{4½} —57089 _{4½}	6
2630. 177	3	7	38008. 93	-0. 07	23046 _{3½} —61055 _{4½}	7
2630. 384	3	20	38005. 94	0. 00	23234 _{4½} —61240 _{3½}	
2630. 534	6	9	38003. 78	-0. 15	<i>a</i> ⁴ P _{2½} —51438 _{3½}	res
2630. 946		2	37997. 83	-0. 21	24991 _{1½} —62989 _{2½}	
2632. 485	35A	7	37975. 61	+0. 13	19276 _{2½} —57252 _{3½}	
2632. 768	7?	7	37971. 53	-0. 08	22503 _{1½} —60474 _{2½}	
2633. 886	4	25	37955. 41	+0. 06	<i>a</i> ⁴ G _{5½} —55392 _{4½}	
2634. 578	6	35	37945. 45	+0. 02	<i>a</i> ⁴ G _{4½} —54498 _{3½}	
2635. 379	6	30	37933. 91	-0. 01	<i>a</i> ⁴ D _{2½} —52901 _{3½}	
2635. 723		1	37928. 96	-0. 22	20780 _{4½} —58709 _{3½}	
2636. 772	1	2	37913. 87	-0. 14	<i>a</i> ⁴ F _{1½} —46625 _{0½}	
2636. 953	1	20	37911. 27	-0. 04	24804 _{3½} —62715 _{4½}	
2637. 209	—?	10	37907. 59	+0. 09	20780 _{4½} —58687 _{4½}	
2637. 576	15A	25	37902. 32	-0. 04	<i>a</i> ⁴ G _{2½} —54137 _{1½}	res
2638. 220		7	37893. 06	-0. 09	28377 _{5½} —66270 _{4½}	
2638. 870		1	37883. 73	-0. 30	18990 _{1½} —56874 _{3½}	
2639. 052	1	3	37881. 12	+0. 07	20455 _{1½} —58336 _{2½}	
2639. 432		1	37875. 67	-0. 12	23450 _{2½} —61326 _{3½}	
2641. 076	2	8	37852. 09	-0. 14	22139 _{2½} —59992 _{3½}	6
2643. 086	—?	10	37823. 31	-0. 13	<i>a</i> ⁴ F _{2½} —49124 _{3½}	
2643. 253	1	10	37820. 92	-0. 01	23234 _{4½} —61055 _{4½}	
2643. 296	4	30	37820. 31	+0. 01	<i>a</i> ⁴ P _{2½} —51254 _{1½}	
2645. 692	25A	7	37786. 06	-0. 09	<i>a</i> ⁴ G _{3½} —54375 _{2½}	
2647. 309	1	4	37762. 98	+0. 12	23803 _{3½} —61566 _{2½}	
2647. 726	7	70	37757. 03	-0. 19	25209 _{4½} —62966 _{3½}	4
2647. 894	1	2	37754. 63	-0. 09	<i>a</i> ⁴ D _{3½} —52901 _{3½}	
2648. 453		2	37746. 67	-0. 09	23803 _{3½} —61550 _{3½}	
2648. 958		2	37739. 47	-0. 11	22194 _{3½} —59933 _{3½}	
2649. 682	1	10	37729. 16	-0. 01	22139 _{2½} —59869 _{3½}	
2650. 276	3	7	37720. 70	-0. 05	<i>a</i> ⁴ D _{1½} —52355 _{0½}	
2650. 580	1	3	37716. 38	-0. 08	27273 _{3½} —64990 _{2½}	
2651. 035	1	8	37709. 90	-0. 03	<i>a</i> ⁴ F _{4½} —52567 _{1½}	6
2651. 881	4	30	37697. 87	-0. 06	19070 _{4½} —56768 _{3½}	
2542. 298	1	3	37691. 95	-0. 01	<i>a</i> ⁴ F _{1½} —48284 _{2½}	
2652. 433		4	37690. 03	-0. 15	20039 _{3½} —57729 _{3½}	
2653. 015	10A	8	37681. 76	-0. 02	<i>a</i> ⁴ F _{2½} —48982 _{1½}	
2653. 424	7	35	37675. 96	+0. 04	<i>a</i> ⁴ G _{4½} —54229 _{3½}	
2653. 568	10	35	37673. 91	-0. 04	<i>a</i> ⁶ D _{3½} —42390 _{3½}	
2654. 841	1	5	37655. 84	+0. 09	19276 _{2½} —56932 _{1½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2655. 485	3	25	37646. 71	-0. 07	23955 _{5/2} -61602 _{3/2}	
2655. 667	15	20	37644. 13	-0. 01	a ⁴ F _{1/2} -46355 _{3/2}	
2656. 027	—?	10	27639. 03	-0. 06	28631 _{3/2} -66270 _{1/2}	
2656. 435	—?	8	37633. 25	-0. 04	a ⁴ F _{3/2} -51045 _{3/2}	
2656. 706	—?	10	37629. 41	-0. 05	26158 _{4/2} -63788 _{3/2}	
2657. 745	1	6	37614. 71	+0. 09	19637 _{2/2} -57252 _{3/2}	
2658. 036	25	100	37610. 59	-0. 04	a ⁶ D _{1/2} -z ⁶ F _{1/2}	res
2659. 171	1?	10	37594. 53	+0. 39	25672 _{3/2} -63266 _{3/2}	
2659. 703	1	15	37587. 02	-0. 01	26929 _{5/2} -64516 _{4/2}	
2661. 852	1	20	37556. 67	-0. 03	23803 _{3/2} -61360 _{1/2}	
2662. 214	3	30	37551. 57	-0. 10	20455 _{1/2} -58007 _{1/2}	res
2663. 874	2	15	37528. 17	-0. 02	19404 _{0/2} -56932 _{1/2}	
2664. 346	80	200	37521. 52	-0. 04	a ⁴ G _{5/2} -54958 _{3/2}	
2665. 644	2	8	27503. 25	-0. 15	a ⁴ G _{4/2} -54056 _{3/2}	
2666. 086	1	40	37497. 03	-0. 17	28187 _{6/2} -65684 _{3/2}	
2666. 446	8	?	37491. 97	-0. 12	19276 _{2/2} -56768 _{3/2}	
2666. 493	20	60	37491. 31	+0. 11	a ⁶ S _{2/2} -44911 _{1/2}	
2668. 245	1	5	37466. 69	-0. 18	a ⁴ G _{3/2} -54056 _{3/2}	
2668. 961	5	5	37456. 64	-0. 11	a ⁶ S _{2/2} -z ⁶ F _{3/2}	
2669. 250	10	25	37452. 59	-0. 07	a ⁴ D _{1/2} -52087 _{3/2}	
2669. 371	5	30	37450. 89	-0. 20	a ⁴ F _{3/2} -50863 _{4/2}	
2670. 395	10	50	37436. 52	-0. 04	a ⁴ G _{3/2} -54026 _{3/2}	
2671. 040	—?	2	37427. 49	-0. 38	23046 _{3/2} -60474 _{3/2}	
2671. 580	8	18	37419. 92	-0. 21	a ⁴ D _{3/2} -52567 _{4/2}	
2672. 647	—?	15	37404. 98	-0. 16	23955 _{5/2} -61360 _{4/2}	
2672. 956	1	3	37400. 66	-0. 11	20455 _{1/2} -57856 _{2/2}	
2673. 608	20	60	37391. 54	-0. 13	18000 _{3/2} -55392 _{4/2}	res
2674. 471	—?	4	37379. 48	0. 00	30633 _{4/2} -68012 _{3/2}	
2674. 628	—?	10	37377. 29	-0. 05	23046 _{0/2} -60424 _{3/2}	
2675. 734	1	20	37361. 84	-0. 10	29341 _{4/2} -66703 _{3/2}	
2677. 579	3	6	37336. 10	-0. 12	19276 _{2/2} -56612 _{3/2}	
2677. 796	20	60	37333. 07	-0. 06	a ⁶ D _{3/2} -z ⁶ F _{3/2}	
2679. 638	20	70	37307. 41	-0. 05	a ⁴ D _{2/2} -52275 _{3/2}	
2679. 758	3	18	37305. 74	-0. 03	19070 _{4/2} -56376 _{3/2}	
2680. 546	—?	10	37294. 77	-0. 12	19637 _{2/2} -56932 _{1/2}	
2681. 568	—?	2	37280. 55	+0. 05	22535 _{0/2} -59816 _{1/2}	
2681. 730	—?	1	37278. 30	+0. 14	26929 _{5/2} -64207 _{4/2}	
2683. 226	8	80	37257. 52	-0. 05	a ⁴ D _{0/2} -50430 _{1/2}	
2683. 512	1	35	37253. 56	—	—	
2683. 632	4	30	37251. 89	-0. 07	23803 _{3/2} -61055 _{4/2}	
2684. 301	12	20	37242. 60	+0. 09	27273 _{3/2} -64516 _{3/2}	
2685. 068	12	25	37231. 96	+0. 05	23046 _{3/2} -60278 _{4/2}	
2685. 366	6	12	37227. 84	+0. 08	25209 _{4/2} -62437 _{4/2}	
2686. 946	4	100	37205. 95	-0. 06	23450 _{2/2} -60656 _{3/2}	res
2687. 000	5	70	37205. 20	-0. 06	22194 _{3/2} -59399 _{4/2}	
2688. 230	7	35	37188. 17	+0. 03	a ⁴ G _{2/2} -53422 _{1/2}	
2690. 036	—?	2	37163. 21	-0. 12	25169 _{1/2} -62333 _{2/2}	
2690. 153	—?	1	37161. 59	-0. 01	18000 _{3/2} -55162 _{2/2}	
2690. 710	2	35	37153. 90	—	—	
2691. 952	2	5	37136. 74	-0. 10	22139 _{2/2} -59276 _{3/2}	
2692. 358	4	18	37131. 14	-0. 09	19637 _{2/2} -56768 _{3/2}	
2693. 228	—?	1	37119. 14	-0. 06	a ⁴ D _{2/2} -52087 _{2/2}	
2694. 080	—?	4?	37107. 40	-0. 16	26158 _{4/2} -63266 _{3/2}	
2694. 382	20	60	37103. 24	+0. 01	a ⁴ G _{2/2} -53338 _{3/2}	
2694. 594	6	70	37100. 32	-0. 08	23955 _{5/2} -61055 _{4/2}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2694. 828	2	6	37097. 10	-0. 03	23803 _{3/2} —60900 _{3/2}	6
2694. 994	6	30	37094. 82	-0. 05	<i>a</i> ⁴ G _{2/2} —53329 _{1/2}	
2695. 111		1	37093. 21	-0. 13	18990 _{1/2} —56084 _{1/2}	
2695. 874	3	10	37082. 72	-0. 01	22194 _{3/2} —59276 _{3/2}	
2696. 914	2	35	37068. 41			
2697. 714	80	160	37057. 42	-0. 12	<i>a</i> ⁶ D _{1/2} — <i>z</i> ² S _{0/2}	res
2698. 265	1	1?	37049. 86	+0. 14	20039 _{3/2} —57089 _{4/2}	
2698. 706	1	3	37043. 80	-0. 04	23234 _{4/2} —60278 _{4/2}	6
2699. 041	8	12	37039. 21	-0. 09	26227 _{2/2} —63266 _{3/2}	
2699. 270	1	10	37036. 06	-0. 08	27273 _{3/2} —64310 _{2/2}	
2700. 320	3	50	37021. 67	+0. 09	23234 _{4/2} —60256 _{3/2}	
2701. 036	8A	10	37011. 85	-0. 29	28631 _{3/2} —65644 _{3/2}	
2701. 485	20	60	37005. 70	-0. 11	<i>a</i> ⁴ F _{4/2} —51863 _{3/2}	6
2702. 115	25	250	36997. 07	+0. 01	19442 _{6/2} —56439 _{6/2}	
2702. 188	4	?	36996. 07	-0. 05	<i>a</i> ⁴ P _{1/2} —47588 _{1/2}	5
2703. 066	8	60	36984. 05	+0. 08	23234 _{4/2} —60218 _{5/2}	
2703. 118	8	10	36983. 36	-0. 04	<i>a</i> ⁴ F _{2/2} —48284 _{2/2}	
2703. 467	12	120	36978. 57	+0. 13	31100 _{5/2} —68078 _{6/2}	
2703. 698	1	5	36975. 41	+0. 05	19637 _{2/2} —56612 _{3/2}	
2703. 829		1	36973. 62	-0. 02	23450 _{2/2} —60424 _{3/2}	6
2705. 599	10	35	36949. 43	-0. 11	20780 _{4/2} —57729 _{3/2}	
2705. 895		12	36945. 40	0. 00	23046 _{3/2} —59992 _{2/2}	
2706. 702	6	?	36934. 38	-0. 01	<i>a</i> ⁶ S _{2/2} —44354 _{2/2}	
2706. 733		50	36933. 95	+0. 04	19442 _{6/2} —56376 _{5/2}	
2707. 067		25	36929. 40	+0. 01	29341 _{4/2} —66270 _{1/2}	6
2708. 360	4A	2	36911. 77	-0. 27	31100 _{5/2} —68012 _{5/2}	
2709. 582	20	80	36895. 12	-0. 09	<i>a</i> ⁴ D _{2/2} —51863 _{3/2}	6 res
2710. 678	2	1	36880. 20	-0. 17	<i>a</i> ⁴ F _{3/2} —50292 _{2/2}	
2710. 792	5	40	36878. 65	-0. 03	<i>a</i> ⁴ G _{2/2} —53113 _{2/2}	
2711. 336		3	36871. 26	-0. 16	28118 _{2/2} —64990 _{3/2}	
2712. 704	5	50	36852. 66	-0. 01	23803 _{3/2} —60656 _{2/2}	
2713. 478	4	2	36842. 15	-0. 29	<i>a</i> ⁴ F _{1/2} —45553 _{1/2}	6
2714. 016		1	36834. 85	-0. 40	20039 _{3/2} —56874 _{2/2}	
2714. 950	1	5	36822. 18	-0. 16	23046 _{3/2} —59869 _{3/2}	
2715. 346	25	80	36816. 81	-0. 02	<i>a</i> ⁴ G _{4/2} —53369 _{1/2}	
2716. 020	2	3	36807. 67	-0. 11 -0. 09	19276 _{2/2} —56084 _{1/2} 26158 _{4/2} —62966 _{5/2}	
2716. 147	3	15	36805. 95	0. 00	23450 _{2/2} —60256 _{3/2}	6 res
2716. 322	30	80	36803. 58	-0. 09	<i>a</i> ⁴ D _{1/2} —51438 _{2/2}	
2716. 890	35A	35	36795. 90	-0. 17	20455 _{1/2} —57252 _{3/2}	
2717. 180	10	40	36791. 96	-0. 08	<i>a</i> ⁴ G _{5/2} —54229 _{3/2}	
2717. 702	3	18	36784. 90	-0. 03	<i>a</i> ⁴ G _{4/2} —53338 _{3/2}	
2718. 044	30	120	36780. 26	-0. 04	<i>a</i> ⁴ G _{3/2} —53369 _{1/2}	4
2718. 257		2	36777. 38	+0. 06	28118 _{2/2} —64896 _{3/2}	
2719. 232	8	3	36764. 20	-0. 09	<i>a</i> ⁶ D _{2/2} —39936 _{2/2}	6
2719. 392		10	36762. 03	0. 00	24804 _{3/2} —61566 _{3/2}	
2719. 798		1	36756. 54	+0. 06	27273 _{3/2} —64030 _{2/2}	
2720. 404	6	30	36748. 36	-0. 04	<i>a</i> ⁴ G _{3/2} —53338 _{3/2}	
2720. 594		40	36745. 80	+0. 04	<i>a</i> ⁴ F _{1/2} —45457 _{0/2}	
2721. 850	4	15	36728. 83	-0. 04	20039 _{3/2} —56768 _{3/2}	6
2722. 805	20	70	36715. 95	-0. 06	<i>a</i> ⁴ D _{3/2} —51863 _{3/2}	
2723. 704	3	5	36703. 84	-0. 07	18000 _{3/2} —54704 _{2/2}	
2724. 081	5	60	36698. 75	-0. 04	23234 _{4/2} —59933 _{3/2}	6
2725. 457		8	36680. 23	+0. 01	19404 _{0/2} —56084 _{1/2}	
2726. 445	3	4	36666. 94	+0. 04	<i>a</i> ⁴ G _{2/2} —52901 _{3/2}	6
2728. 880	1	6	36634. 22	-0. 05	23234 _{4/2} —59869 _{3/2}	
2729. 532	1	6	36625. 48	+0. 08	28377 _{3/2} —65003 _{4/2}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2729. 620	25	75	36624. 30	-0. 06	<i>a</i> ⁴ P _{0½} — <i>45457</i> _{0½}	res
2729. 936	5	30	36620. 06	+0. 02	<i>a</i> ⁴ D _{1½} — <i>51254</i> _{1½}	
2730. 846	3	8	36607. 86	-0. 11	22139 _{2½} — <i>58747</i> _{1½}	
2732. 078	2	8	36591. 35	+0. 05	28377 _{5½} — <i>64969</i> _{5½}	6
2732. 378	4	4	36587. 33	-0. 09	<i>a</i> ⁴ P _{1½} — <i>47179</i> _{1½}	6
2733. 448	5	35	36573. 01	+0. 01	20039 _{3½} — <i>56612</i> _{3½}	6
2733. 704		3	36569. 58	-0. 01	22139 _{2½} — <i>58709</i> _{3½}	
2734. 627		3	36557. 24	0. 00	26158 _{4½} — <i>62715</i> _{4½}	
2734. 737	5	40	36555. 77	-0. 10	24804 _{3½} — <i>61360</i> _{4½}	
2735. 784	2	10	36541. 78	+0. 08	23450 _{2½} — <i>59992</i> _{2½}	6
2737. 135	1	3	36523. 74	-0. 11	<i>a</i> ⁴ G _{3½} — <i>53113</i> _{2½}	
2737. 756	2	5	36515. 46	-0. 02	22194 _{3½} — <i>58709</i> _{3½}	
2737. 840		3	36514. 34	0. 00	27273 _{3½} — <i>63788</i> _{3½}	
2738. 962	1	5	36499. 38	+0. 06	28491 _{1½} — <i>64990</i> _{2½}	7
2739. 080	4	4	36497. 81	-0. 06	18000 _{3½} — <i>54498</i> _{3½}	
2739. 140	4	15	36497. 01	-0. 04	18990 _{1½} — <i>55488</i> _{1½}	7
2739. 384	6	30	36493. 76	-0. 04	22194 _{3½} — <i>58687</i> _{4½}	
2740. 187	6	20	36483. 06	-0. 10	23450 _{2½} — <i>59933</i> _{3½}	
2740. 801	20	200	36474. 90	+0. 03	23803 _{3½} — <i>60278</i> _{4½}	4
2742. 471	15	30	36452. 68	+0. 07	23803 _{3½} — <i>60256</i> _{3½}	6 res
2742. 903	8	40	36446. 94	+0. 02	19637 _{2½} — <i>56084</i> _{1½}	
2745. 036	2	30	36418. 62	-0. 02	23450 _{2½} — <i>59869</i> _{3½}	4 res
2748. 312	20	15	36375. 21	+0. 09	18000 _{3½} — <i>54375</i> _{2½}	res
2748. 418	2	12	36373. 82	-0. 08	20039 _{3½} — <i>56413</i> _{4½}	
2750. 023	1	9	36352. 61	+0. 07	23046 _{3½} — <i>59399</i> _{4½}	
2750. 325	10	20	36348. 60	0. 00	<i>a</i> ⁴ G _{4½} — <i>52901</i> _{3½}	res
2750. 728	2	15	36343. 28	+0. 04	29341 _{4½} — <i>65684</i> _{5½}	
2750. 880	3	12	36341. 28	-0. 04	25209 _{4½} — <i>61550</i> _{3½}	
2752. 242	5	30	36323. 28	-0. 03	23955 _{5½} — <i>60278</i> _{4½}	7
2752. 360	1?	2	36321. 72	+0. 03	19070 _{4½} — <i>55392</i> _{4½}	
2753. 094		6	36312. 03	-0. 04	<i>a</i> ⁴ G _{3½} — <i>52901</i> _{3½}	
2753. 320	6	25	36309. 05	-0. 03	20780 _{4½} — <i>57089</i> _{4½}	7
2753. 826		6	36302. 37	-0. 07	29341 _{4½} — <i>65644</i> _{3½}	
2754. 695	1	2	36290. 93	-0. 08	<i>a</i> ⁴ D _{3½} — <i>51438</i> _{2½}	
2755. 036	1	3	36286. 44	-0. 14	<i>a</i> ⁴ D _{2½} — <i>51254</i> _{1½}	
2755. 661		6	36278. 21	-0. 09	26158 _{4½} — <i>62437</i> _{4½}	
2756. 776	2	20	36263. 54	+0. 10	23955 _{5½} — <i>60218</i> _{5½}	6
2757. 710		6	36251. 26	+0. 13	24804 _{3½} — <i>61055</i> _{4½}	
2758. 182		4	36245. 05	+0. 17	22503 _{1½} — <i>58747</i> _{1½}	
2758. 333	18	20	36234. 07	-0. 04	<i>a</i> ⁶ D _{4½} — <i>42390</i> _{3½}	res
2759. 338	1	10	36229. 87	-0. 14	23046 _{3½} — <i>59276</i> _{3½}	7
2760. 691	3	15	36212. 11	-0. 03	22535 _{0½} — <i>58747</i> _{1½}	6
2760. 742	12.A	10	36211. 44	-0. 05	19276 _{2½} — <i>55488</i> _{1½}	
2761. 587	40	100	36200. 37	0. 00	<i>a</i> ⁴ F _{1½} — <i>44911</i> _{1½}	res
2761. 837	2	6	36197. 09	+0. 08	22139 _{2½} — <i>58336</i> _{2½}	
2762. 499	6	15	36188. 42	+0. 06	23803 _{3½} — <i>59992</i> _{2½}	
2764. 263	200	400	36165. 33	-0. 02	<i>a</i> ⁶ D _{0½} — <i>z</i> ⁶ F _{0½}	
2764. 768	8	50	36158. 72	+0. 16	26929 _{5½} — <i>63087</i> _{6½}	5
2765. 340	2	10	36151. 24	-0. 02	25209 _{4½} — <i>61360</i> _{4½}	6
2765. 986		1	36142. 80	-0. 10	22194 _{3½} — <i>58336</i> _{2½}	
2766. 318	1	35	36138. 46	-0. 11	28377 _{5½} — <i>64516</i> _{4½}	7
2766. 981	4	35	36129. 80	-0. 02	23803 _{3½} — <i>59933</i> _{3½}	6
2767. 967	4	25	36116. 93	-0. 08	25209 _{4½} — <i>61326</i> _{3½}	
2768. 326	30	50	36112. 25	0. 00	<i>a</i> ⁴ F _{2½} — <i>47113</i> _{2½}	6
2770. 496	2	5	36083. 96	+0. 03	19404 _{0½} — <i>55488</i> _{1½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2771. 005	5	20	36077. 34	-0. 09	<i>a</i> ⁴ D _{3/2} -51045 ³ / ₂	
2771. 531	5	3	36070. 50	+0. 02	30633 _{1/2} -66703 ³ / ₂	
2771. 927	2	6	36065. 34	+0. 04	23803 _{3/2} -59869 ³ / ₂	
2772. 658	2	8	36055. 83	-0. 01	18000 _{3/2} -54056 ⁴ / ₂	
2773. 849	5	25	36040. 35	-0. 09	<i>a</i> ⁴ G _{2/2} -52275 ³ / ₂	
2774. 092	?	30	36037. 20	+0. 04	26929 _{3/2} -62966 ³ / ₂	
2774. 433		10?	36032. 76	+0. 01	<i>a</i> ⁴ P _{1/2} -46625 ⁰ / ₂	
2774. 988	6	20	36025. 56	+0. 02	18000 _{3/2} -54026 ³ / ₂	
2775. 878	1	5	36014. 01	0. 00	<i>a</i> ⁴ G _{4/2} -52567 ⁴ / ₂	
2776. 509	20	100	36005. 84	+0. 01	<i>a</i> ⁴ F _{4/2} -50863 ³ / ₂	6
2777. 536	2	10	35992. 51	+0. 07	27273 _{3/2} -63266 ³ / ₂	
2777. 870	8	30	35988. 18	-0. 05	20780 _{1/2} -56768 ³ / ₂	
2778. 124		2	35984. 90	+0. 06	29341 _{1/2} -65326 ³ / ₂	
2778. 281		3	35982. 86	-0. 01	24918 _{1/2} -60900 ³ / ₂	
2778. 429	5	6	35980. 95	-0. 17	<i>a</i> ⁴ D _{0/2} -49154 ⁰ / ₂	
2778. 694	20	80	35977. 51	+0. 03	<i>a</i> ⁴ G _{3/2} -52567 ⁴ / ₂	res
2780. 285	60A	40	35956. 94	+0. 05	<i>a</i> ⁶ D _{2/2} -z ⁶ F _{1/2}	res
2782. 142	20	80	35932. 93	-0. 02	<i>a</i> ⁴ G _{5/2} -53369 ³ / ₂	
2783. 979	2	6	35909. 22	-0. 19	24991 _{1/2} -60900 ³ / ₂	
2784. 290	2	15	35905. 21	-0. 04	20534 _{3/2} -56439 ⁰ / ₂	
2785. 126	1	3	35894. 43	-0. 11	25672 _{3/2} -61566 ³ / ₂	
2785. 634	12	50	35887. 90	0. 00	19070 _{1/2} -54958 ³ / ₂	7
2786. 300	4	20	35879. 31	+0. 02	20534 _{3/2} -56413 ³ / ₂	
2786. 340	3		35878. 80	-0. 06	<i>a</i> ⁴ F _{2/2} -47179 ¹ / ₂	
2788. 403		2	35852. 25	+0. 07	<i>a</i> ⁴ G _{2/2} -52087 ³ / ₂	
2788. 536	4	6	35850. 54	-0. 09	19637 _{3/2} -55488 ¹ / ₂	
2789. 197	10	20	35842. 04	-0. 06	20534 _{3/2} -56376 ³ / ₂	7
2790. 160	2	18	35829. 67	-0. 03	28377 _{3/2} -64207 ³ / ₂	
2790. 433	5	50	35826. 17	-0. 14	23450 _{3/2} -59276 ³ / ₂	res
2790. 998	3	3	35818. 92	-0. 08	28491 _{1/2} -64310 ³ / ₂	
2791. 740	2	5	35809. 40	-0. 08	<i>a</i> ⁴ D _{0/2} -48982 ¹ / ₂	
2791. 850	—?	1	35807. 98	-0. 02	<i>a</i> ⁴ P _{2/2} -49242 ³ / ₂	
2793. 622	1	4	35785. 28	+0. 06	26929 _{3/2} -62714 ⁰ / ₂	
2796. 674	1	3	35746. 23	-0. 11	19276 _{3/2} -55022 ³ / ₂	
2796. 866	3	6	35743. 77	-0. 15	<i>a</i> ⁴ F _{1/2} -44455 ⁰ / ₂	res
2797. 298		2	35738. 25	-0. 16	24918 _{1/2} -60656 ³ / ₂	
2797. 879		1	35730. 83	-0. 27	25169 _{1/2} -60900 ³ / ₂	
2798. 353		3	35724. 78	-0. 06	28631 _{3/2} -64356 ³ / ₂	
2799. 042	20	100	35715. 98	-0. 05	<i>a</i> ⁴ D _{3/2} -50863 ³ / ₂	5
2799. 248	1		35713. 36	-0. 29	18990 _{1/2} -54704 ³ / ₂	
2799. 312	1		35712. 54	-0. 02	<i>a</i> ⁴ F _{3/2} -49124 ³ / ₂	
2801. 058	4	30	35690. 28	-0. 14	<i>a</i> ⁴ P _{2/2} -49124 ³ / ₂	
2801. 430		10	35685. 54	-0. 07	<i>a</i> ⁴ G _{3/2} -52275 ³ / ₂	
3802. 705		3	35669. 31	+0. 01	28118 _{2/2} -63788 ³ / ₂	
2803. 068		4	35664. 70	-0. 25	24991 _{1/2} -60656 ³ / ₂	6_res
2803. 233	4	10	35662. 60	-0. 02	22194 _{3/2} -57856 ³ / ₂	
2803. 302	1	3	35661. 71	+0. 07	29341 _{1/2} -65003 ³ / ₂	
2803. 604	8	25	35657. 87	-0. 10	<i>a</i> ⁴ D _{1/2} -50292 ³ / ₂	res
2803. 682		3	35656. 88	+0. 01	23234 _{1/2} -58891 ³ / ₂	
2803. 909		5	35654. 00	-0. 13	25672 _{3/2} -61326 ³ / ₂	
2804. 922	3	12	35641. 12	+0. 04	23046 _{3/2} -58687 ³ / ₂	
2805. 177	2	15	35637. 88	-0. 05	30633 _{1/2} -66270 ³ / ₂	6
2805. 546		7	35633. 20	-0. 06	20780 _{1/2} -56415 ³ / ₂	6
2805. 936	20	120	35628. 24	-0. 13	20455 _{1/2} -56084 ¹ / ₂	
2806. 392	3	4	35622. 45	+0. 05	<i>a</i> ⁴ G _{2/2} -51863 ³ / ₂	
				-0. 07	<i>a</i> ⁴ P _{0/2} -44455 ⁰ / ₂	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2806. 626	3	10	35619. 48	+0. 01	24804 _{3/2} —60424 _{3/2}	6
2808. 474	4	40	35596. 04	-0. 03	20780 _{4/2} —56376 _{3/2}	res
2808. 956	3	50	35589. 93	-0. 02	22139 _{2/2} —57729 _{3/2}	res
2810. 085		3	35575. 64	0. 00	28631 _{3/2} —64207 _{1/2}	
2811. 743	1	6	35554. 65	-0. 01	29341 _{4/2} —64896 _{3/2}	
2812. 210	8	50	35548. 76	0. 00	<i>a</i> 4P _{2/2} —48982 _{1/2}	res
2813. 228	3	15	35535. 90	+0. 06	22194 _{3/2} —57729 _{3/2}	
2814. 106		2	35524. 81	-0. 11	19637 _{2/2} —55162 _{3/2}	
2814. 798	4	30	35516. 07	+0. 03	19442 _{6/2} —54958 _{3/2}	5
2815. 720		2	35504. 44	-0. 10	22503 _{1/2} —58007 _{1/2}	
2816. 283	6	10	35497. 35	0. 00	<i>a</i> 4G _{3/2} —52087 _{3/2}	
2816. 478		2	35494. 90	+0. 26	18990 _{1/2} —54485 _{6/2}	
2817. 422	1	3	35483. 00	-0. 11	24991 _{1/2} —60474 _{3/2}	
2819. 002	4	12	35463. 11	-0. 02	<i>a</i> 4D _{2/2} —50430 _{1/2}	7
2819. 897	4	20	35451. 85	+0. 07	24804 _{3/2} —60256 _{3/2}	res
2820. 532	3	8	35443. 87	-0. 07	23955 _{5/2} —59399 _{4/2}	
2821. 800	5	35	35427. 95	-0. 14	19276 _{2/2} —54704 _{2/2}	res
2822. 542	25	125	35418. 64	-0. 10	<i>a</i> 4F _{3/2} —48830 _{3/2}	res
2824. 144		4	35398. 54	+0. 06	28631 _{3/2} —64030 _{3/2}	
2824. 306	4	4	35396. 52	-0. 08	<i>a</i> 4P _{2/2} —48830 _{3/2}	
2824. 680	2	6	35391. 83	-0. 03	26158 _{4/2} —61550 _{3/2}	
2824. 896	1	7	35389. 12	+0. 02	28491 _{1/2} —63880 _{3/2}	
2825. 188	1	6	35385. 47	-0. 01	19637 _{2/2} —55022 _{3/2}	
2826. 482	3	15	35369. 27	0. 00	18000 _{3/2} —53369 _{4/2}	7
2827. 542		8	35356. 00	+0. 02	19404 _{0/2} —54760 _{6/2}	
2830. 064	12	80	35324. 50	-0. 01	<i>a</i> 4D _{2/2} —50292 _{3/2}	6
2831. 236	7	35	35309. 88	-0. 01	<i>a</i> 4G _{4/2} —51863 _{3/2}	
2831. 643	1	2	35304. 80	0. 00	25169 _{1/2} —60474 _{3/2}	
2832. 215		3	35297. 67	+0. 23	23450 _{2/2} —58747 _{1/2}	
2832. 848		1	35289. 80	-0. 38	23046 _{3/2} —58336 _{3/2}	
2834. 208		50	35272. 85	-0. 51	<i>a</i> 4G _{3/2} —51863 _{3/2}	6
2835. 334	8A	5	35258. 85	-0. 21	23450 _{2/2} —58709 _{3/2}	
2838. 422	5	4	35220. 50	-0. 01	<i>a</i> 6D _{3/2} —39936 _{3/2}	
2839. 820	3	10	35203. 15	-0. 04	<i>a</i> 4G _{2/2} —51438 _{3/2}	
2839. 936	1	10	35201. 71	-0. 09	26158 _{4/2} —61360 _{3/2}	
2841. 080	2	6	35187. 54	+0. 01	24804 _{3/2} —59992 _{3/2}	
2842. 460		6	35170. 46	-0. 03	31100 _{5/2} —66270 _{4/2}	
2842. 700	2	15	35167. 50	-0. 05	26158 _{4/2} —61326 _{3/2}	
2843. 045	2	2	35163. 22	+0. 04	27273 _{3/2} —62437 _{3/2}	
2843. 449	2	5	35158. 23	-0. 15	19070 _{4/2} —54229 _{3/2}	
2843. 603	1	12	35156. 32	-0. 02	28631 _{3/2} —63788 _{3/2}	6
2844. 426		1	35146. 15	-0. 09	18990 _{1/2} —54137 _{1/2}	
2844. 500	2	8	35145. 24	-0. 07	<i>a</i> 4D _{3/2} —50292 _{3/2}	res
2845. 725	3	10	35130. 11	-0. 02	<i>a</i> 4G _{5/2} —52567 _{4/2}	res
2846. 357		1	35122. 31	-0. 25	20039 _{3/2} —55162 _{3/2}	
2847. 140	3	18	35112. 65	-0. 17	18000 _{3/2} —53113 _{3/2}	res
2848. 234	2	5	35099. 16	-0. 14	19276 _{2/2} —54375 _{3/2}	
2849. 678		1	35081. 38	-0. 13	26227 _{2/2} —61326 _{3/2}	
2850. 808	35A	8	35067. 48	-0. 04	19404 _{0/2} —54485 _{6/2}	
2851. 068		4	35064. 28	+0. 25	19637 _{2/2} —54704 _{2/2}	
				-0. 19	24804 _{3/2} —59869 _{3/2}	
2851. 554	3	3	35058. 30	+0. 38	22194 _{3/2} —57252 _{3/2}	
2852. 083	3	70	35051. 80	+0. 02	30633 _{4/2} —65684 _{5/2}	5
2852. 460		1	35047. 17	0. 00	25209 _{4/2} —60256 _{3/2}	
2853. 440	3	20	35035. 13	-0. 15	18990 _{1/2} —54026 _{3/2}	res
2853. 694		4	35032. 02	-0. 06	20455 _{1/2} —55488 _{1/2}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2854. 719	3	4	35019. 44	-0. 12	$a^4G_{2\frac{1}{2}}-51254\frac{1}{2}$	
2855. 524		25	35009. 56	0. 00	$25209_{4\frac{1}{2}}-60218\frac{3}{2}$	
2856. 256		2	35000. 60	-0. 04	$24991_{1\frac{1}{2}}-59992\frac{3}{2}$	
2857. 470		1	34985. 72	-0. 14	$19070_{4\frac{1}{2}}-54056\frac{3}{2}$	
2857. 695	2	6	34982. 97	-0. 15	$20039_{3\frac{1}{2}}-55022\frac{3}{2}$	6
2859. 484	8	30	34961. 08	-0. 10	$a^4P_{1\frac{1}{2}}-45553\frac{1}{2}$	res
2860. 898		12	34943. 80			
2861. 058	2	6	34941. 85	-0. 01	$a^4G_{4\frac{1}{2}}-z^6F_{5\frac{1}{2}}$	
2861. 21	2	10	34939. 99	-0. 13	$23046_{3\frac{1}{2}}-57986\frac{3}{2}$	
2861. 518		2	34936. 23	-0. 11	$23955_{5\frac{1}{2}}-58891\frac{5}{2}$	
2864. 036		2	34905. 52	-0. 20	$23803_{3\frac{1}{2}}-58709\frac{3}{2}$	
2864. 395	1		34901. 14	+0. 10	$18000_{3\frac{1}{2}}-52901\frac{3}{2}$	
2864. 473	2	15	34900. 20	-0. 10	$28187_{6\frac{1}{2}}-63087\frac{6}{2}$	6
2864. 744	1	8	34896. 90	-0. 16	$26158_{4\frac{1}{2}}-61055\frac{3}{2}$	7
2864. 858	3	10	34895. 51	+0. 13	$22194_{3\frac{1}{2}}-57089\frac{3}{2}$	
2865. 603		6	34886. 43	-0. 05	$23450_{2\frac{1}{2}}-58336\frac{3}{2}$	6
2865. 804	3	20	34884. 00	-0. 04	$23803_{3\frac{1}{2}}-58687\frac{1}{2}$	
2866. 322	8	10	34877. 68	-0. 09	$a^6S_{2\frac{1}{2}}-42298\frac{1}{2}$	
2866. 600	4	8	34874. 30	-0. 04	$a^4F_{2\frac{1}{2}}-46175\frac{3}{2}$	
2866. 751	6	20	34872. 46	-0. 06	$a^4F_{3\frac{1}{2}}-48284\frac{2}{2}$	res
2866. 910		1	34870. 53	-0. 17	$28118_{2\frac{1}{2}}-62989\frac{3}{2}$	
2867. 409	6	15	34864. 46	-0. 04	$a^4P_{1\frac{1}{2}}-45457\frac{6}{2}$	res
2867. 697	4	3	34860. 96	-0. 23	$19637_{2\frac{1}{2}}-54498\frac{3}{2}$	
2867. 934	4	20	34858. 08	+0. 28	$19276_{2\frac{1}{2}}-54137\frac{1}{2}$	
2868. 736	8	80	34848. 33	+0. 06	$20534_{3\frac{1}{2}}-55392\frac{4}{2}$	
				-0. 03	$a^4G_{3\frac{1}{2}}-51438\frac{3}{2}$	
2870. 906	18A	10	34822. 00	-0. 33	$25169_{1\frac{1}{2}}-59992\frac{3}{2}$	
2871. 902	2	12	34809. 92	+0. 02	$23046_{3\frac{1}{2}}-57856\frac{3}{2}$	res
2873. 352	2?	10	34792. 35	+0. 05	$22139_{2\frac{1}{2}}-56932\frac{1}{2}$	
2873. 836	2	12	34786. 50	-0. 02	$19442_{6\frac{1}{2}}-54229\frac{3}{2}$	
2874. 478		12	34778. 72	-0. 18	$28187_{6\frac{1}{2}}-62966\frac{3}{2}$	
2875. 110		4	34771. 08	-0. 02	$25045_{0\frac{1}{2}}-59816\frac{1}{2}$	
2876. 684	1-	2	34752. 06	+0. 08	$25672_{2\frac{1}{2}}-60424\frac{3}{2}$	
2876. 934	20A	10	34749. 01	+0. 07	$22503_{1\frac{1}{2}}-57252\frac{3}{2}$	6
2877. 827		2	34738. 26	-0. 18	$19637_{2\frac{1}{2}}-54375\frac{2}{2}$	
2878. 083	10A	8	34735. 16	+0. 14	$22139_{2\frac{1}{2}}-56874\frac{3}{2}$	6
2878. 316	2	40	34732. 35	-0. 13	$23955_{5\frac{1}{2}}-58687\frac{1}{2}$	
2880. 164	1-	8	34710. 07	-0. 03	$28377_{5\frac{1}{2}}-63087\frac{6}{2}$	
2881. 538		8	34693. 52	+0. 14	$30633_{4\frac{1}{2}}-65326\frac{3}{2}$	
2882. 400	3	20	34683. 14	+0. 02	$23046_{3\frac{1}{2}}-57729\frac{3}{2}$	6
2883. 152	3	3	34674. 10	+0. 13	$26227_{2\frac{1}{2}}-60900\frac{3}{2}$	
2883. 247	6	4	34672. 95	+0. 11	$26929_{5\frac{1}{2}}-61602\frac{6}{2}$	
2883. 915		2	34664. 92	+0. 05	$20039_{3\frac{1}{2}}-54704\frac{2}{2}$	
2884. 310	2	20	34660. 18	+0. 06	$26929_{5\frac{1}{2}}-61589\frac{5}{2}$	6
2885. 463	1	2	34646. 33	-0. 24	$a^6D_{1\frac{1}{2}}-z^6F_{6\frac{1}{2}}$	
2886. 464		6	34634. 31	-0. 13	$28631_{3\frac{1}{2}}-63266\frac{3}{2}$	
2886. 896	5		34629. 13	+0. 11	$a^6S_{2\frac{1}{2}}-z^6F_{5\frac{1}{2}}$	
2886. 923		35}	34628. 81	+0. 17	$22139_{2\frac{1}{2}}-56768\frac{3}{2}$	
2888. 318	15A	8	34612. 08	+0. 09	$20780_{4\frac{1}{2}}-55392\frac{4}{2}$	d
2888. 699		4	34607. 52	-0. 22	$a^4D_{1\frac{1}{2}}-49242\frac{3}{2}$	
2889. 780	4	50	34594. 58	-0. 09	$24804_{3\frac{1}{2}}-59399\frac{4}{2}$	
2890. 634	2	25	34584. 35	+0. 01	$31100_{5\frac{1}{2}}-65684\frac{5}{2}$	6
2891. 456	3	20	34574. 52	-0. 01	$22194_{3\frac{1}{2}}-56768\frac{3}{2}$	6
2892. 912	2	10	34557. 12	+0. 02	$23450_{2\frac{1}{2}}-58007\frac{1}{2}$	res
2894. 924	2	10	34533. 10	-0. 04	$23803_{3\frac{1}{2}}-58336\frac{3}{2}$	
2895. 441	2	10	34526. 94	-0. 02	$28187_{6\frac{1}{2}}-62714\frac{6}{2}$	6

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2897. 726	2	3	34499. 71	-0. 11	19637 _{2½} -54137 _{1½}	
2898. 102		2	34495. 24	+0. 19	23234 _{4½} -57729 _{3½}	
2898. 360		1	34492. 17	+0. 06	<i>a</i> ⁴ G _{4½} -51045 _{3½}	
2901. 174	2	25	34458. 71	-0. 12	20039 _{3½} -54498 _{3½}	
2901. 448		3	34455. 46	-0. 12	<i>a</i> ⁴ G _{3½} -51045 _{3½}	
2902. 201	30A	20	34446. 52	-0. 12	29341 _{4½} -63788 _{3½}	
2903. 500		50	34431. 11	-0. 09	26929 _{5½} -61360 _{4½}	
2904. 081	8	80	34424. 22	-0. 01	20534 _{5½} -54958 _{3½}	6
2904. 556	2	8	34418. 58	-0. 08	22194 _{3½} -56612 _{3½}	6
2904. 843	—?	5	34415. 18	-0. 08	<i>a</i> ⁴ D _{0½} -47588 _{1½}	
2905. 602	8A	12	34406. 20	0. 00	23450 _{2½} -57856 _{3½}	6
2906. 416	2	12	34396. 57	+0. 10	22535 _{0½} -56932 _{1½}	
2908. 504	3	25	34371. 87	-0. 06	22503 _{1½} -56874 _{3½}	
2910. 332	2	10	34350. 30	-0. 02	22194 _{3½} -56544 _{3½}	
2911. 542	2	20	34336. 01	{ -0. 07 -0. 07	20039 _{3½} -54375 _{3½} 30633 _{4½} -64969 _{5½}	
2912. 464	2	25	34325. 15			
2912. 584	3	5	34323. 73	-0. 09	<i>a</i> ⁴ F _{4½} -49181 _{4½}	
2912. 986	1		34319. 00	-0. 11	<i>a</i> ⁴ P _{1½} -44911 _{1½}	
2913. 614		2	34311. 60	+0. 13	26929 _{5½} -61240 _{3½}	
2913. 748	12	30	34310. 02	+0. 11	<i>a</i> ⁴ G _{4½} -50863 _{4½}	6
2914. 272		30	34303. 85	-0. 28	20455 _{1½} -54760 _{0½}	
2914. 655	2	15	34299. 34	+0. 05	19070 _{4½} -53369 _{4½}	6
2916. 347		5	34279. 44	+0. 02	23450 _{2½} -57729 _{3½}	
2916. 584	3	8	34276. 66	-0. 08	27273 _{3½} -61550 _{3½}	
2916. 768	3	10	34274. 50	{ +0. 22 -0. 08	<i>a</i> ⁴ D _{2½} -49242 _{2½} 18000 _{3½} -52275 _{3½}	
2916. 896	2	12	34273. 00	-0. 38	<i>a</i> ⁴ G _{3½} -50863 _{4½}	
2917. 389	3	5	34267. 20	-0. 10	<i>a</i> ⁴ F _{4½} -49124 _{3½}	
2917. 540	1	5	34265. 42	+0. 02	26158 _{4½} -60424 _{3½}	
2917. 895		3	34261. 25	-0. 25	25672 _{2½} -59933 _{3½}	
2918. 633	25	100	34252. 58	-0. 04	<i>a</i> ⁴ F _{2½} -45553 _{1½}	7
2918. 976	2	10	34248. 57	-0. 11	20455 _{1½} -54704 _{3½}	
2919. 508	2	12	34242. 33	-0. 15	20780 _{4½} -55022 _{3½}	
2920. 903	—	6	34225. 98	+0. 04	31100 _{5½} -65326 _{5½}	
2921. 908	10A	12	34214. 21	-0. 09	28118 _{2½} -62533 _{2½}	<i>d</i>
2922. 674	—	5	34205. 24	+0. 04	23046 _{3½} -57252 _{2½}	
2923. 382	5A	10	34196. 95	-0. 03	25672 _{2½} -59869 _{3½}	
2923. 451	1	10	34196. 15	+0. 04	<i>a</i> ⁴ G _{2½} -50430 _{1½}	
2923. 980	3	12	34189. 96	-0. 10	25209 _{4½} -59399 _{3½}	6
2924. 996	4	40	34178. 08	-0. 12	20780 _{4½} -54958 _{3½}	5
2925. 834	5	125	34168. 30	-0. 04	33910 _{5½} -68078 _{5½}	5
2926. 836	3	15	34156. 60	-0. 10	<i>a</i> ⁴ D _{2½} -49124 _{3½}	res
2926. 990	40A	10	34154. 80	+0. 26	<i>a</i> ⁴ P _{2½} -47588 _{1½}	
2927. 710	3	20	34146. 40	-0. 06	19276 _{2½} -53422 _{1½}	7
2929. 984	3	20	34119. 90	-0. 07	26158 _{4½} -60278 _{3½}	6
2931. 530	2	20	34101. 90	-0. 04	33910 _{5½} -68012 _{3½}	6
2931. 895	5	35	34097. 65	-0. 06	26158 _{4½} -60256 _{3½}	res
2932. 864	3	20	34086. 39	+0. 07	18000 _{3½} -52087 _{2½}	res
2933. 068	1	1	34083. 80	-0. 32	28631 _{3½} -62715 _{4½}	
2935. 201	2	6	34059. 25	+0. 01	28377 _{5½} -62437 _{4½}	
2935. 358	8	25	34057. 43	-0. 06	<i>a</i> ⁴ G _{2½} -50292 _{2½}	6
2935. 726	2	10	34053. 16	-0. 03	19276 _{2½} -53329 _{1½}	
2935. 806	—	4	34052. 23	-0. 20	27273 _{3½} -61326 _{3½}	
2936. 61	40A	125	34042. 92	+0. 26	23046 _{3½} -57089 _{4½}	
2937. 200	8?	15	34036. 07	-0. 02	19404 _{0½} -53440 _{0½}	6
2937. 61	10A	12	34031. 33	-0. 19	23955 _{5½} -57986 _{4½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2937. 774	2	4	34029. 42	-0. 03	26227 _{2½} —60256 _{3½}	
2938. 685	?	4	34018. 87	-0. 03	19404 _{0½} —53422 _{1½}	
2938. 872	2	12	34016. 71	-0. 09	20039 _{3½} —54056 _{4½}	
2939. 757	6	35	34006. 47	-0. 09	<i>a</i> ⁴ D _{0½} —47179 _{1½}	
2940. 204	8	60	34001. 30	-0. 07	<i>a</i> ⁴ F _{3½} —47413 _{3½}	
2941. 476	4	5	33986. 60	+0. 10	20039 _{3½} —54026 _{2½}	
2942. 128	12 <i>A</i>	10	33979. 07	-0. 16	<i>a</i> ⁴ P _{2½} —47413 _{3½}	
2942. 263	2	10	33977. 49	-0. 01	<i>a</i> ⁴ D _{3½} —49124 _{3½}	
2942. 618	3	10	33973. 41	-0. 07	<i>a</i> ⁴ F _{1½} —48830 _{3½}	
2945. 137	—	6	33944. 35	+0. 02	22139 _{2½} —56084 _{1½}	
2946. 454	—	25	33929. 18			
2947. 136	—?	2	33921. 33	-0. 15	34091 _{4½} —68012 _{5½}	
2950. 453	4	40	33883. 20	-0. 01	24804 _{3½} —58687 _{1½}	res
2952. 262	75 <i>A</i>	100	33862. 44	-0. 22	<i>a</i> ⁴ P _{1½} —44455 _{0½}	<i>d</i>
2952. 974	4 <i>A</i>	4	33854. 27	+0. 11	18000 _{3½} —51863 _{3½}	
				-0. 32	23234 _{4½} —57089 _{1½}	
2954. 070	4 <i>A</i>	3	33841. 71	-0. 49	28491 _{1½} —62333 _{2½}	
2954. 482	4	15	33836. 99	-0. 01	19276 _{2½} —53113 _{2½}	6 res
2955. 007	8	15	33830. 98	-0. 08	19070 _{4½} —52901 _{3½}	
2955. 256	2	10	33828. 13	-0. 06	23046 _{3½} —56874 _{3½}	
2956. 67	20 <i>A</i>	10	33811. 96	-0. 08	18990 _{1½} —52803 _{1½}	
2957. 266	1	12	33805. 12	-0. 06	28631 _{3½} —62437 _{4½}	
2957. 590	1		33801. 43	-0. 07	23450 _{2½} —57252 _{2½}	
2958. 972	—	4	33785. 65	+0. 05	19637 _{2½} —53422 _{1½}	
2959. 312	—	2	33781. 77	-0. 17	27273 _{3½} —61055 _{4½}	
2959. 910	—	10	33774. 94	+0. 02	26158 _{4½} —59933 _{3½}	
2960. 771	—	1	33765. 12	-0. 08	26227 _{2½} —59992 _{2½}	
2961. 020	12	50	33762. 28	-0. 02	<i>a</i> ⁴ P _{1½} —44354 _{2½}	
2961. 558	—	2	33756. 15	-0. 23	24991 _{1½} —58747 _{1½}	
2964. 412	—	1	33723. 65	-0. 03	30633 _{4½} —64356 _{3½}	
2964. 898	2	20	33718. 12	-0. 07	20780 _{4½} —54498 _{3½}	res
2965. 589	2	15	33710. 27	-0. 13	26158 _{4½} —59869 _{3½}	
2966. 417	4 <i>A</i>	2	33700. 86	+0. 17	19637 _{2½} —53338 _{3½}	
2967. 926	4	20	33683. 73	+0. 05	<i>a</i> ⁴ D _{3½} —48830 _{3½}	6
2970. 908	2	5	33649. 92	-0. 20	<i>a</i> ⁴ D _{1½} —48284 _{2½}	
2973. 092	—	3	33625. 24	+0. 02	19276 _{2½} —52901 _{3½}	
2974. 377	20	35	33610. 67	+0. 12	<i>a</i> ⁴ F _{2½} —44911 _{1½}	res
2975. 078	3	10	33602. 75	-0. 01	18990 _{1½} —52593 _{0½}	
2976. 476	15	50	33586. 97	+0. 03	<i>a</i> ⁴ F _{1½} —42298 _{1½}	res
2976. 985	—	2	33581. 23	-0. 01	22503 _{1½} —56084 _{1½}	
2977. 442	—	3	33576. 08	-0. 02	<i>a</i> ⁴ F _{2½} — <i>z</i> ⁶ F _{3½}	
2977. 580	4	40	33574. 52	+0. 04	30633 _{4½} —64207 _{4½}	6
2977. 950	3	20	33570. 35	+0. 04	20445 _{1½} —54026 _{2½}	
2978. 332	1	6	33566. 05	+0. 11	23046 _{3½} —56612 _{3½}	
2981. 319	1		33532. 41	+0. 10	24804 _{3½} —58336 _{2½}	
2982. 219	2	25	33522. 29	+0. 10	20534 _{5½} —54056 _{4½}	
2984. 426		6	33497. 50	-0. 10	23046 _{3½} —56544 _{2½}	
2985. 830		6	33481. 75	-0. 02	23450 _{2½} —56932 _{1½}	
2986. 103	5	25	33478. 69	+0. 09	25209 _{4½} —58687 _{4½}	6
2986. 382	3	20	33475. 57	+0. 06	<i>a</i> ⁴ F _{4½} —48332 _{3½}	res
2987. 294	15	60	33465. 35	-0. 19	<i>a</i> ⁴ P _{0½} —42298 _{1½}	res
2988. 502	4	12	33451. 82	-0. 07	<i>a</i> ⁴ D _{0½} —46625 _{0½}	res
2988. 771		12	33448. 81	+0. 13	20780 _{4½} —54229 _{5½}	
2990. 850		12	33425. 56	-0. 47	<i>a</i> ⁴ G _{5½} —50863 _{4½}	
2991. 470		4	33418. 63	-0. 25	24918 _{1½} —58336 _{2½}	
2991. 855		3	33414. 33	-0. 25	28187 _{6½} —61602 _{6½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
2992. 043		18	33412. 23			
2994. 700	3	60	33382. 59	-0. 06	27273 _{3/2} —60656 _{3/2}	
2995. 129		6	33377. 81	-0. 06	23234 _{4/2} —56612 _{3/2}	
2997. 685		8	33349. 35	-0. 02	26929 _{1/2} —60278 _{4/2}	
2998. 050		5	33345. 29	-0. 13	24991 _{1/2} —58336 _{3/2}	
2998. 693	15	50	33338. 14	-0. 05	<i>a</i> 4F _{1/2} — <i>z</i> 6F _{2/2}	res
3000. 499		3	33318. 07	-0. 04	23450 _{2/2} —56768 _{3/2}	
3000. 624	5	50	33316. 69	+0. 03	<i>a</i> 4D _{2/2} —48284 _{2/2}	res
3002. 287	2	40	33298. 23	-0. 10	20039 _{3/2} —53338 _{3/2}	6 res
3003. 070	4	10	33289. 55	+0. 05	26929 _{5/2} —60218 _{5/2}	6
3003. 435		15	33285. 51	-0. 11	23803 _{3/2} —57089 _{4/2}	
3004. 284		5	33276. 10	-0. 06	20780 _{1/2} —54056 _{1/2}	
3007. 511		4?	33240. 40	-0. 20	26158 _{4/2} —59399 _{4/2}	
3008. 946	2	25	33224. 55	+0. 17	28377 _{5/2} —61602 _{5/2}	7
3010. 131		3	33211. 47	-0. 19	28377 _{3/2} —61589 _{5/2}	
3010. 750	4	80	33204. 64	+0. 04	19070 _{4/2} —52275 _{3/2}	res
3011. 102		2	33200. 76	-0. 05	27273 _{3/2} —60474 _{2/2}	
3011. 327		4	33198. 27	-0. 02	22194 _{3/2} —55392 _{4/2}	
3012. 102	2	15	33189. 74	+0. 10	19404 _{0/2} —52593 _{0/2}	res
3013. 093		1	33178. 82	+0. 05	23234 _{4/2} —56413 _{3/2}	
3014. 200	6A	3	33166. 63	-0. 48	25169 _{1/2} —58336 _{2/2}	
3014. 606	2	25	33162. 17	-0. 07	23450 _{2/2} —56612 _{3/2}	res
3015. 694	1	8	33150. 20	-0. 08	27273 _{3/2} —60424 _{3/2}	6
3017. 148	2	25	33134. 23	+0. 17	23955 _{5/2} —57089 _{4/2}	
3018. 624	1	20	33118. 03	-0. 04	26158 _{4/2} —59276 _{3/2}	5
3019. 628		3	33107. 08	+0. 04	31100 _{5/2} —64207 _{4/2}	
3020. 630	4	20	33096. 04	-0. 02	18990 _{1/2} —52087 _{2/2}	
3021. 982	20	80	33081. 23	-0. 24	<i>a</i> 4F _{3/2} — <i>z</i> 6F _{4/2}	
3022. 482		20	33075. 76	-0. 02	25672 _{2/2} —58747 _{1/2}	
3022. 672	3	30	33073. 68	+0. 06	28491 _{1/2} —61566 _{3/2}	
				-0. 10	20039 _{3/2} —53113 _{3/2}	
3022. 906	2	6	33071. 12	-0. 03	23803 _{3/2} —56874 _{2/2}	
3024. 502	25	250	33053. 67	-0. 07	<i>a</i> 4F _{2/2} —44354 _{3/2}	res
3025. 993		1	33037. 38	-0. 02	25672 _{2/2} —58709 _{3/2}	
3027. 369		6	33022. 33	0. 00	22139 _{2/2} —55162 _{2/2}	
3028. 750		10	33007. 31	+0. 05	<i>a</i> 4G _{2/2} —49242 _{2/2}	
3028. 975		8	33004. 86	+0. 01	27273 _{3/2} —60278 _{4/2}	
3029. 524		4	32998. 88	+0. 12	19276 _{2/2} —52275 _{3/2}	
3030. 793		2	32985. 06	+0. 11	22503 _{1/2} —55488 _{1/2}	
3031. 000		25	32982. 81	+0. 07	28377 _{5/2} —61360 _{4/2}	
3032. 450	3	15	32967. 04	-0. 01	20455 _{1/2} —53422 _{1/2}	res
3032. 660		8	32964. 76	-0. 01	23803 _{3/2} —56768 _{3/2}	
3033. 626		30	32954. 26	-0. 02	<i>a</i> 4D _{1/2} —47588 _{1/2}	res
3033. 790		2	32952. 48	+0. 27	22535 _{0/2} —55488 _{1/2}	
3033. 913	4	20	32951. 14	+0. 11	19404 _{0/2} —52355 _{0/2}	
3036. 311		1	32925. 11	-0. 14	24804 _{3/2} —57729 _{3/2}	
3036. 670	5	50	32921. 23	-0. 07	<i>a</i> 4P _{2/2} —46355 _{2/2}	
3039. 578	3	20	32889. 73	+0. 05	<i>a</i> 4G _{2/2} —49124 _{3/2}	
3044. 400		10	32837. 64	-0. 09	25169 _{1/2} —58007 _{1/2}	res
3044. 564		1	32835. 88	+0. 26	20534 _{5/2} —53369 _{4/2}	6
3045. 216		15	32828. 85	+0. 07	22194 _{3/2} —55022 _{3/2}	
3046. 911	1	5	32810. 57	+0. 07	19276 _{2/2} —52087 _{2/2}	
3047. 060	1	15	32808. 97	+0. 07	23803 _{3/2} —56612 _{3/2}	
3048. 604	4	40	32792. 36	+0. 01	19070 _{4/2} —51863 _{3/2}	res
3049. 563	—?	3	32782. 03	-0. 04	28118 _{2/2} —60900 _{2/2}	
3049. 850	5	50	32778. 96	-0. 01	<i>a</i> 4D _{1/2} —47413 _{2/2}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
3051. 29	25	250	32763. 49	+0. 03	<i>a</i> ⁴ F _{3½} —46175 _{3½}	res
3053. 354	6	?)	32741. 34	+0. 02	<i>a</i> ⁴ P _{2½} —46175 _{3½}	
3053. 420		20)	32740. 64	+0. 08	23803 _{3½} —56544 _{2½}	
3054. 129		1	32733. 03	+0. 03	26158 _{4½} —58891 _{5½}	
3058. 452	1	20	32686. 79	-0. 04	25169 _{1½} —57856 _{2½}	res
3059. 268		3	32678. 06	+0. 06	28377 _{5½} —61055 _{4½}	
3061. 027		10	32659. 28	+0. 04	22503 _{1½} —55162 _{3½}	
3061. 678	6	15	32652. 35	-0. 08	<i>a</i> ⁴ G _{3½} —49242 _{2½}	res
3063. 422		8	32633. 74	-0. 06	23450 _{2½} —56084 _{1½}	
3063. 972	4	30	32627. 89	-0. 01	<i>a</i> ⁴ G _{4½} —49181 _{1½}	res
3064. 635		3	32620. 83	+0. 01	<i>a</i> ⁴ D _{2½} —47588 _{1½}	
3066. 976	6	60	32595. 93	+0. 07	<i>a</i> ⁴ G _{2½} —48830 _{3½}	7
3067. 410	3	6	32591. 32	-0. 05	<i>a</i> ⁴ G _{3½} —49181 _{1½}	
3067. 572	5	50	32589. 61	+0. 02	20780 _{4½} —53369 _{4½}	6
3067. 856	6	60	32586. 59	+0. 08	19276 _{2½} —51863 _{3½}	7
3069. 288	8	80	32571. 38	0. 00	<i>a</i> ⁴ G _{4½} —49124 _{3½}	res
3071. 234	1	15	32550. 74	-0. 08	26158 _{4½} —58709 _{3½}	res
3071. 730	5	50	32545. 48	-0. 10	<i>a</i> ⁴ D _{1½} —47179 _{1½}	res
3072. 740	4	30	32534. 78	-0. 07	<i>a</i> ⁴ G _{3½} —49124 _{3½}	res
3073. 403		4	32527. 77	+0. 36	20039 _{3½} —52567 _{4½}	
3075. 963		8	32500. 70			
3077. 520	30	300	32484. 26	+0. 06	23955 _{5½} —56439 _{6½}	5
3078. 868	?	15	32470. 03	+0. 03	26929 _{5½} —59399 _{4½}	res
3079. 992		20	32458. 19	-0. 05	23955 _{5½} —56413 _{4½}	4
3080. 787		2	32449. 81	+0. 17	19637 _{2½} —52087 _{2½}	
3081. 042	4	40	32447. 13	+0. 06	18990 _{1½} —51438 _{2½}	res
3081. 215	1	3	32445. 30	-0. 21	<i>a</i> ⁴ D _{2½} —47413 _{2½}	
3083. 520	2	20	32421. 05	0. 00	23955 _{5½} —56376 _{3½}	6
3087. 394	10	50	32380. 37	+0. 05	<i>a</i> ⁴ D _{0½} —45553 _{1½}	res
3089. 742		6	32355. 77	0. 00	28118 _{2½} —60474 _{2½}	
3090. 712	2	2	32345. 62	+0. 07	23046 _{3½} —55392 _{4½}	
3091. 870		3	32333. 49	+0. 01	30633 _{4½} —62966 _{5½}	
3094. 629		4	32304. 67	+0. 18	22194 _{3½} —54498 _{3½}	
3095. 870	5	50	32291. 73	+0. 10	18000 _{3½} —50292 _{2½}	res
3098. 031		2	32269. 20	+0. 09	28631 _{3½} —60900 _{2½}	
3098. 300	2	12	32266. 40	+0. 09	<i>a</i> ⁴ D _{3½} —47413 _{2½}	
3098. 580	—	12	32263. 48	+0. 04	18990 _{1½} —51254 _{1½}	
3098. 870	—	8	32260. 47	+0. 03	24991 _{1½} —57252 _{2½}	
3100. 074		5	32247. 93	+0. 03	29341 _{4½} —61589 _{3½}	
3100. 736	5	50	32241. 05	+0. 02	<i>a</i> ⁴ G _{3½} —48830 _{3½}	res
3101. 224		4	32235. 98	+0. 13	22139 _{2½} —54375 _{2½}	
3102. 204	5	50	32225. 79	+0. 14	19637 _{2½} —51863 _{3½}	res
3103. 517	2	12	32212. 16	+0. 04	<i>a</i> ⁴ D _{2½} —47179 _{1½}	
3104. 534		3	32201. 61	+0. 06	22503 _{1½} —54704 _{2½}	
3106. 180		8	32184. 55	+0. 01	25672 _{2½} —57856 _{2½}	
3106. 632		20	32179. 86	-0. 07	34091 _{4½} —66270 _{4½}	
3108. 386		3	32161. 71	+0. 20	19404 _{2½} —51438 _{2½}	6
3108. 778	6	60	32157. 65	+0. 15	23234 _{4½} —55392 _{4½}	res
3110. 690	4	40	32137. 89	+0. 10	20455 _{1½} —52593 _{0½}	res
3111. 887	1	4	32125. 52	+0. 04	27273 _{3½} —59399 _{4½}	
3112. 463	1	4	32119. 58	-0. 02	<i>a</i> ⁴ P _{2½} —45553 _{1½}	
3112. 860	20	50	32115. 48	-0. 02	23046 _{3½} —55162 _{3½}	res
3113. 384		12	32110. 08	+0. 10	26227 _{2½} —58337 _{2½}	6
3116. 100		3	32082. 09	-0. 04	25169 _{1½} —57252 _{2½}	
3117. 263		1	32070. 12	-0. 20	24804 _{3½} —56874 _{2½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
3118. 475		5	32057. 66	-0. 10	25672 _{2½} —57729 _{3½}	
3118. 981		1	32052. 46	0. 00	19442 _{6½} —z ⁶ F _{5½}	
3119. 237	5	12	32049. 83	+0. 19	a ⁴ G _{2½} —48284 _{2½}	
3121. 032		10	32031. 40	+0. 16	28187 _{6½} —60218 _{3½}	
3125. 700	1	2	31983. 59	-0. 08	28491 _{1½} —60474 _{3½}	
3125. 790	1	8	31982. 64	+0. 10	22503 _{1½} —54485 _{0½}	
3126. 420	4	40	31976. 20	+0. 14	23046 _{3½} —55022 _{3½}	6 res
3127. 750	1	50	31962. 60	+0. 20	26929 _{5½} —58891 _{3½}	6 res
3128. 982	2	40	31950. 01	+0. 21	22535 _{0½} —54485 _{0½}	res
3129. 682	1	25	31942. 87			
3129. 907	3	2	31940. 57	-0. 14	24991 _{1½} —56932 _{1½}	
3133. 780		3	31901. 10	+0. 19	28377 _{5½} —60278 _{3½}	
3133. 965		20	31899. 22	-0. 03	29341 _{4½} —61240 _{5½}	
3135. 156		4	31887. 10	+0. 04	20455 _{1½} —52355 _{0½}	
3135. 238		4	31886. 27	+0. 03	25045 _{0½} —56932 _{1½}	
3135. 838	1	12	31880. 17	0. 00	22139 _{2½} —54026 _{2½}	
3137. 224	4	8	31866. 08	-0. 01	25209 _{4½} —57089 _{1½}	6
3137. 57		2	31862. 56	+0. 04	31100 _{5½} —62966 _{5½}	
3138. 770		6	31850. 39	+0. 10	22194 _{3½} —54056 _{1½}	res
3139. 517	1	12	31842. 81	+0. 07	19404 _{0½} —51254 _{1½}	
3140. 577	2	2	31832. 06	0. 00	28631 _{3½} —60474 _{3½}	
3140. 96		2	31828. 18	-0. 10	22194 _{3½} —54026 _{2½}	
3142. 928		3	31808. 25	0. 00	26158 _{4½} —57986 _{3½}	
3143. 348	4	20	31804. 00	+0. 18	24804 _{3½} —56612 _{3½}	6
3143. 670		4	31800. 74	-0. 02	30633 _{4½} —62437 _{4½}	res
3144. 493		25	31792. 42	+0. 09	19637 _{2½} —51438 _{2½}	
3145. 768	20	200	31779. 53	+0. 05	19070 _{4½} —50863 _{1½}	5
3146. 292	—?	20	31774. 24	+0. 14	28631 _{3½} —60424 _{3½}	7
3146. 836	2	4	31768. 75	-0. 06	a ⁴ G _{4½} —48332 _{3½}	
3147. 474	—	3	31762. 31	0. 00	33910 _{5½} —65684 _{3½}	
3147. 825		15	31758. 77	+0. 02	19276 _{2½} —51045 _{3½}	
3148. 678	1	10	31750. 17	-0. 09	25169 _{1½} —56932 _{1½}	
3149. 856	30	300	31738. 29	+0. 23	26929 _{5½} —58687 _{1½}	res
3151. 304	5	125	31723. 71	-0. 07	28118 _{2½} —59869 _{3½}	res
3151. 568	5	20	31721. 05	+0. 04	a ⁴ D _{0½} —44911 _{1½}	5
3152. 238		4	31714. 31	0. 00	23234 _{4½} —54958 _{3½}	
3152. 484	25	100	31711. 84	+0. 01	a ⁴ D _{1½} —46355 _{2½}	
3152. 749	5	6	31709. 17	+0. 07	29341 _{4½} —61055 _{1½}	6
3153. 134		2	31705. 30	+0. 04	23450 _{2½} —55162 _{3½}	
3153. 934		2	31697. 28	+0. 19	a ⁶ S _{2½} —z ⁶ F _{1½}	
3154. 172	5	10	31694. 87	+0. 18	25169 _{1½} —56874 _{2½}	
3158. 925	1	2	31647. 18	-0. 12	28118 _{2½} —59816 _{1½}	
3160. 026	20	200	31636. 15	+0. 06	a ⁴ G _{3½} —48284 _{2½}	6
3160. 673	1	4	31629. 68	+0. 33	28631 _{3½} —60278 _{3½}	6
3161. 942		10	31616. 98	-0. 06	a ⁴ F _{4½} —z ⁶ F _{4½}	6
3162. 225		15	31614. 15	-0. 02	26227 _{2½} —57856 _{3½}	res
3164. 262		10	31593. 80	-0. 04	19637 _{2½} —51254 _{1½}	
3164. 794	1	30	31588. 49	+0. 05	31100 _{5½} —62714 _{0½}	
3165. 657		4	31579. 88	+0. 02	34091 _{4½} —65684 _{3½}	
3166. 534		12	31571. 13	-0. 04	23803 _{3½} —55392 _{3½}	
3167. 736	1	6	31559. 16	+0. 04	25672 _{2½} —57252 _{2½}	
3168. 372		2	31552. 82	-0. 05	26158 _{4½} —57729 _{3½}	
3171. 355	1	6	31523. 14	-0. 17	25209 _{4½} —56768 _{3½}	
3173. 564		8	31501. 20	-0. 02	24991 _{1½} —56544 _{3½}	
3174. 221		1	31494. 68	-0. 04	22503 _{1½} —54026 _{3½}	7
				0. 00	28491 _{1½} —59992 _{3½}	
				-0. 22	20780 _{4½} —52275 _{3½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
3175. 958	20	200	31477. 46	-0. 07	$a^4P_{2\frac{1}{2}}-44911\frac{1}{2}$	res
3177. 200	30	120	31465. 15	-0. 07	$a^4F_{3\frac{1}{2}}-z^6F_{3\frac{1}{2}}$	6
3178. 036	6	60	31456. 88	-0. 05	$a^4P_{1\frac{1}{2}}-z^6F_{2\frac{1}{2}}$	res
3178. 672		8	31450. 58			
3179. 436	15	120	31443. 02	-0. 06	$a^4P_{2\frac{1}{2}}-z^6F_{3\frac{1}{2}}$	res
3180. 060	2	60	31436. 85	-0. 12	$23955_{5\frac{1}{2}}-55392_{4\frac{1}{2}}$	res
3182. 194		30	31415. 77	-0. 07	$33910_{5\frac{1}{2}}-65326_{3\frac{1}{2}}$	
3183. 000		2	31407. 82	-0. 05	$19637_{2\frac{1}{2}}-51045_{3\frac{1}{2}}$	
3183. 441		12	31403. 47	+0. 01	$25209_{4\frac{1}{2}}-56612_{3\frac{1}{2}}$	
3183. 965	3	10	31398. 30	+0. 01	$20039_{3\frac{1}{2}}-51438_{3\frac{1}{2}}$	
3185. 057	2	20	31387. 54	-0. 04	$a^4D_{2\frac{1}{2}}-46355_{3\frac{1}{2}}$	6
3186. 396	2	15	31374. 35	-0. 18	$25169_{1\frac{1}{2}}-56544_{3\frac{1}{2}}$	7
3187. 116	1	80	31367. 26			
3188. 016		6	31358. 40	-0. 06	$23803_{3\frac{1}{2}}-55162_{3\frac{1}{2}}$	
3188. 495	1	10	31353. 69	-0. 11	$a^4G_{2\frac{1}{2}}-47588_{1\frac{1}{2}}$	
3189. 238	50A	100	31346. 39	-0. 02	$a^4D_{3\frac{1}{2}}-z^6F_{4\frac{1}{2}}$	
				+0. 25	$a^4F_{3\frac{1}{2}}-44758_{3\frac{1}{2}}$	
3191. 016	2	20	31328. 92	-0. 10	$23046_{3\frac{1}{2}}-54375_{3\frac{1}{2}}$	res
3192. 117		8	31318. 12	-0. 08	$a^4F_{4\frac{1}{2}}-46175_{3\frac{1}{2}}$	
3193. 825		25	31301. 37	0. 00	$18990_{1\frac{1}{2}}-50292_{3\frac{1}{2}}$	
3195. 708	2	5	31282. 93	-0. 08	$22139_{2\frac{1}{2}}-53422_{1\frac{1}{2}}$	
3200. 380		6	31237. 26	-0. 02	$28631_{3\frac{1}{2}}-59869_{3\frac{1}{2}}$	
3200. 565		6	31235. 46	+0. 08	$34091_{4\frac{1}{2}}-65326_{3\frac{1}{2}}$	
3201. 583	20	60	31225. 53	-0. 02	$a^4F_{1\frac{1}{2}}-39936_{2\frac{1}{2}}$	res
3202. 254		10	31218. 98	-0. 04	$23803_{3\frac{1}{2}}-55022_{3\frac{1}{2}}$	6
3203. 343	12	60	31208. 37	-0. 01	$a^4D_{3\frac{1}{2}}-46355_{3\frac{1}{2}}$	res
3203. 433	6	30	31207. 49	-0. 11	$a^4D_{2\frac{1}{2}}-46175_{3\frac{1}{2}}$	
3203. 752		10	31204. 39	+0. 03	$25209_{4\frac{1}{2}}-56413_{3\frac{1}{2}}$	
3203. 909	2	2	31202. 86	+0. 03	$25672_{2\frac{1}{2}}-56874_{3\frac{1}{2}}$	
3204. 400	2	30	31198. 07	-0. 03	$22139_{2\frac{1}{2}}-53338_{3\frac{1}{2}}$	
3205. 262		5	31189. 69	-0. 05	$22139_{2\frac{1}{2}}-53329_{1\frac{1}{2}}$	res
3206. 420	6	60	31178. 42	-0. 07	$a^4G_{2\frac{1}{2}}-47413_{3\frac{1}{2}}$	res
3206. 680	—?	12	31175. 89	0. 00	$22194_{3\frac{1}{2}}-53369_{3\frac{1}{2}}$	
3207. 580		8	31167. 15	-0. 02	$25209_{4\frac{1}{2}}-56376_{3\frac{1}{2}}$	
3207. 671		6	31166. 26	+0. 06	$24918_{1\frac{1}{2}}-56084_{1\frac{1}{2}}$	
3209. 968	4	80	31143. 96	-0. 03	$22194_{3\frac{1}{2}}-53338_{3\frac{1}{2}}$	res
3215. 275	2	40	31092. 56	-0. 08	$33910_{5\frac{1}{2}}-65003_{4\frac{1}{2}}$	
3215. 648	?	30	31088. 95	-0. 18	$24991_{1\frac{1}{2}}-56084_{1\frac{1}{2}}$	
3216. 308	2	30	31082. 57	-0. 24	$a^4F_{2\frac{1}{2}}-42390_{3\frac{1}{2}}$	
3218. 806		6	31058. 45	-0. 08	$20780_{4\frac{1}{2}}-51863_{3\frac{1}{2}}$	
				-0. 01	$29341_{4\frac{1}{2}}-60424_{3\frac{1}{2}}$	
				-0. 09	$33910_{5\frac{1}{2}}-64969_{5\frac{1}{2}}$	
3219. 890		5	31048. 00	-0. 07	$23450_{2\frac{1}{2}}-54498_{3\frac{1}{2}}$	
3221. 914	60A	20	31028. 49	+0. 09	$a^4D_{3\frac{1}{2}}-46175_{3\frac{1}{2}}$	
3222. 274		3	31025. 03	+0. 03	$26227_{2\frac{1}{2}}-57252_{2\frac{1}{2}}$	
3222. 646		20	31021. 45	-0. 09	$28377_{5\frac{1}{2}}-59399_{4\frac{1}{2}}$	
3223. 22		2	31015. 90	+0. 09	$19276_{2\frac{1}{2}}-50292_{2\frac{1}{2}}$	
3223. 900		8	31009. 38	-0. 36	$23046_{3\frac{1}{2}}-54056_{4\frac{1}{2}}$	
3224. 320	3	4	31005. 34	-0. 17	$20039_{3\frac{1}{2}}-51045_{3\frac{1}{2}}$	
3224. 550	6	15	31003. 13	-0. 05	$23955_{5\frac{1}{2}}-54958_{3\frac{1}{2}}$	6
3225. 170	1	2	30997. 17	+0. 05	$a^4F_{2\frac{1}{2}}-42298_{3\frac{1}{2}}$	
3225. 480	2	20	30994. 19	0. 00	$23234_{4\frac{1}{2}}-54229_{5\frac{1}{2}}$	res
3226. 750		5	30981. 99	-0. 11	$20455_{1\frac{1}{2}}-51438_{3\frac{1}{2}}$	
3227. 020	1	6	30979. 40	-0. 04	$23046_{3\frac{1}{2}}-54026_{3\frac{1}{2}}$	
3228. 990	3	15	30960. 50	-0. 15	$20534_{5\frac{1}{2}}-z^6F_{3\frac{1}{2}}$	res
3229. 422		8	30956. 36	-0. 08	$30633_{4\frac{1}{2}}-61589_{3\frac{1}{2}}$	
3230. 604	4	20	30945. 03	-0. 07	$a^4G_{2\frac{1}{2}}-47179_{1\frac{1}{2}}$	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
3230. 846	8	12	30942. 71	-0. 15	$a\ ^4F_{3\frac{1}{2}}-44354\frac{3}{2}$	res
3231. 053		4	30940. 73	+0. 15	$25672\frac{2}{2}-56612\frac{3}{2}$	
3231. 442		1	30937. 01	-0. 10	$22503\frac{1}{2}-53440\frac{0}{2}$	
3232. 132	15A	6	30930. 40	-0. 32	$26158\frac{4}{2}-57089\frac{4}{2}$	
3233. 140	3	8	30920. 76	+0. 04	$a\ ^4P_{2\frac{1}{2}}-44354\frac{3}{2}$	
3233. 286		20	30919. 36	{ -0. 08	$22194\frac{3}{2}-53113\frac{3}{2}$	
3233. 46		1	30917. 70	+0. 02	$a\ ^4D_{1\frac{1}{2}}-45553\frac{1}{2}$	
3233. 820		2	30914. 25	+0. 12	$30633\frac{4}{2}-61550\frac{3}{2}$	
3234. 50		4	30904. 40	-0. 18	$25169\frac{1}{2}-56084\frac{1}{2}$	
3235. 774	1-	8	30895. 59	+0. 03	$22535\frac{0}{2}-53440\frac{0}{2}$	7
				-0. 12	$a\ ^4G_{5\frac{1}{2}}-48332\frac{5}{2}$	6
3236. 644	3	25	30887. 29	+0. 11	$22535\frac{0}{2}-53422\frac{1}{2}$	
3236. 744		6	30886. 33			
3237. 684	1	30	30877. 37	+0. 09	$29341\frac{4}{2}-60218\frac{5}{2}$	
3238. 220		2	30872. 25	+0. 01	$25672\frac{2}{2}-56544\frac{3}{2}$	
3243. 008	5	40	30826. 67	+0. 02	$22503\frac{1}{2}-53329\frac{1}{2}$	res
3243. 334	15	100	30823. 58	-0. 08	$a\ ^4G_{3\frac{1}{2}}-47413\frac{3}{2}$	5
3245. 273		6	30805. 16	-0. 04	$34091\frac{4}{2}-64896\frac{3}{2}$	
3245. 937		2	30798. 86	+0. 39	$20455\frac{1}{2}-51254\frac{1}{2}$	
3246. 413		1	30794. 35	+0. 44	$22535\frac{0}{2}-53329\frac{1}{2}$	
3246. 498	1	12	30793. 54	-0. 03	$19637\frac{2}{2}-50430\frac{1}{2}$	res
3249. 848	10	30	30761. 80	+0. 03	$22139\frac{2}{2}-52901\frac{3}{2}$	res
3251. 262	40A	40	30748. 42	+0. 05	$a\ ^4F_{2\frac{1}{2}}-z\ ^6F_{2\frac{1}{2}}$	res
3254. 848	1	4	30714. 54	-0. 08	$20780\frac{4}{2}-z\ ^6F_{5\frac{1}{2}}$	
3255. 012		30	30713. 00	-0. 05	$27273\frac{3}{2}-57986\frac{4}{2}$	5
3255. 582		20	30707. 62	-0. 04	$22194\frac{3}{2}-52901\frac{3}{2}$	
3255. 824		1	30705. 33	+0. 06	$26227\frac{2}{2}-56932\frac{1}{2}$	
3255. 957	60A	20	30704. 08	-0. 06	$28187\frac{6}{2}-58891\frac{3}{2}$	
3257. 815		12	30686. 57	-0. 13	$23450\frac{2}{2}-54137\frac{1}{2}$	
3260. 32		3	30663. 00	-0. 03	$22139\frac{2}{2}-52803\frac{1}{2}$	
3261. 937		8	30647. 79	-0. 20	$26227\frac{2}{2}-56874\frac{3}{2}$	
3262. 244	3	60	30644. 91	-0. 04	$28631\frac{3}{2}-59276\frac{3}{2}$	6
3265. 988	2	12	30609. 78	-0. 09	$26158\frac{4}{2}-56768\frac{3}{2}$	
3267. 430		40	30596. 27			
3268. 353	—?	30	30587. 63	-0. 07	$24804\frac{3}{2}-55392\frac{4}{2}$	res
3268. 882		4	30582. 68	-0. 16	$27273\frac{3}{2}-57856\frac{3}{2}$	
3269. 622	50A	10	30575. 76	+0. 02	$23450\frac{2}{2}-54026\frac{2}{2}$	
3270. 049		3	30571. 77	-0. 21	$23803\frac{3}{2}-54375\frac{2}{2}$	
3273. 300	1	8	30541. 41	-0. 20	$26227\frac{2}{2}-56768\frac{3}{2}$	
3274. 788	1	12	30527. 53	-0. 05	$29341\frac{4}{2}-59869\frac{3}{2}$	
3277. 608	3	3	30501. 27	-0. 45	$31100\frac{5}{2}-61602\frac{6}{2}$	
3278. 148		15	30496. 24	-0. 21	$24991\frac{1}{2}-55488\frac{1}{2}$	7
3278. 924	12A	20	30489. 02	+0. 02	$31100\frac{5}{2}-61589\frac{5}{2}$	
3282. 478		4	30456. 01	-0. 05	$27273\frac{3}{2}-57729\frac{3}{2}$	
3282. 693	—?	5	30454. 02	+0. 02	$26158\frac{4}{2}-56612\frac{3}{2}$	
3283. 765		20	30444. 08			
3285. 820	1	15	30425. 04	-0. 31	$34091\frac{4}{2}-64516\frac{4}{2}$	
3286. 566	25	75	30418. 13	-0. 02	$a\ ^4F_{1\frac{1}{2}}-z\ ^6F_{1\frac{1}{2}}$	res
3290. 10		1	30385. 46	-0. 28	$26227\frac{2}{2}-56612\frac{3}{2}$	
3291. 45		3	30373. 00	-0. 07	$22194\frac{3}{2}-52567\frac{4}{2}$	
3293. 138	2	25	30357. 43	-0. 20	$24804\frac{3}{2}-55162\frac{2}{2}$	
3297. 418		4	30318. 03	-0. 11	$25169\frac{1}{2}-55488\frac{1}{2}$	
3297. 497		4	30317. 30	-0. 10	$26227\frac{2}{2}-56544\frac{2}{2}$	
3298. 284		40	30310. 07	-0. 01	$28377\frac{5}{2}-58687\frac{4}{2}$	
3299. 39		4	30299. 91	-0. 03	$22503\frac{1}{2}-52803\frac{1}{2}$	
3299. 741	6	25	30296. 69	-0. 06	$a\ ^4P_{0\frac{1}{2}}-z\ ^6F_{1\frac{1}{2}}$	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
3300.344	5	12	30291.15	-0.12	23046 _{3/2} —53338 _{3/2}	6
3301.870		8	30277.15	-0.12	<i>a</i> ⁴ D _{1/2} —44911 _{1/2}	
3303.216		6	30264.81	-0.06	20780 _{1/2} —51045 _{3/2}	
3303.736		2	30260.05	-0.03	31100 _{3/2} —61360 _{1/2}	
3304.324	4A	3	30254.66	-0.24	26158 _{4/2} —56413 _{4/2}	
3304.548		80	30252.62	{ -0.08 +0.03	23803 _{3/2} —54056 _{1/2} 20039 _{3/2} —50292 _{2/2}	7
3305.46	1	1	30244.27	+0.07	24918 _{1/2} —55162 _{3/2}	
3308.358	3	60	30217.77	+0.06	26158 _{4/2} —56376 _{3/2}	5
3310.190		20	30201.05			
3312.163	1—	4	30183.06	-0.03	25209 _{4/2} —55392 _{4/2}	
3313.532		4	30170.59	-0.15	24991 _{1/2} —55162 _{3/2}	
3314.323		8	30163.39	-0.15	18990 _{1/2} —49154 _{0/2}	
3316.820		3	30140.68	+0.33	31100 _{3/2} —61240 _{3/2}	
3317.412	2	15	30135.31	{ 0.00 +0.21	22139 _{2/2} —52275 _{3/2} 23234 _{4/2} —53369 _{4/2}	
3319.488	1	10	30116.47	-0.01	34091 _{4/2} —64207 _{4/2}	6
3320.944		10	30103.26	+0.06	23234 _{4/2} —53338 _{3/2}	
3322.345		6	30090.57	-0.09	22503 _{1/2} —52593 _{0/2}	
3323.414	15	10	30080.89	-0.31	22194 _{3/2} —52275 _{3/2}	6
3325.980	2	8	30057.68	-0.10	29341 _{4/2} —59399 _{4/2}	
3333.280	1	8	29991.85	-0.05	18990 _{1/2} —48982 _{1/2}	
3334.806		5	29978.13	-0.01	27273 _{3/2} —57252 _{2/2}	7
3335.404		3	29972.75	+0.27	23450 _{2/2} —53422 _{1/2}	
3336.170		2	29965.87	+0.29	19276 _{2/2} —49242 _{2/2}	
3337.352		3	29955.26	-0.08	31100 _{3/2} —61055 _{4/2}	
3338.276	1	12	29946.97	-0.08	22139 _{2/2} —52087 _{2/2}	
3338.632	5	25	29943.78	-0.03	<i>a</i> ⁴ D _{2/2} —44911 _{1/2}	res
3339.036	5	30	29940.15	-0.14	<i>a</i> ⁴ C _{4/2} — <i>z</i> ⁶ F _{4/2}	res
3339.590		8	29935.19	-0.06	29341 _{4/2} —59276 _{3/2}	
3342.468	25	120	29909.41	+0.05	<i>a</i> ⁴ D _{2/2} — <i>z</i> ⁶ F _{3/2}	res
3343.095	12	60	29903.80	+0.04	<i>a</i> ⁴ C _{3/2} — <i>z</i> ⁶ F _{4/2}	res
3343.410	15	80	29900.99	+0.11	<i>a</i> ⁴ F _{4/2} —44758 _{4/2}	6
3344.898	3	25	29887.69	+0.12	23450 _{2/2} —53338 _{3/2}	
3345.858	100A	80	29879.11	-0.10	23450 _{2/2} —53329 _{1/2}	7
3347.458	1	2	29864.83	-0.23	<i>a</i> ⁴ F _{1/2} — <i>z</i> ² S _{0/2}	
3348.296	4	80	29857.36	+0.06	26227 _{2/2} —56084 _{1/2}	7
3348.876	4	40	29852.18	+0.13	22503 _{1/2} —52355 _{0/2}	6 res
3349.323	3	8	29848.20	+0.20	19276 _{2/2} —49124 _{3/2}	
3350.634	12	30	29836.52	+0.12	20455 _{1/2} —50292 _{2/2}	res
3352.388	3	10	29820.91	+0.09	<i>a</i> ⁴ D _{1/2} —44455 _{0/2}	
3352.954	20A	15	29815.88	+0.03	25672 _{2/2} —55488 _{1/2}	<i>d</i>
3356.241	4A	2	29786.68	+0.17	24918 _{1/2} —54704 _{2/2}	
3358.292		5	29768.49	-0.01	24991 _{1/2} —54760 _{0/2}	
3358.608	50	200	29765.69	-0.04	<i>a</i> ⁴ C _{3/2} —46355 _{2/2}	4
3359.274		10	29759.79	-0.23	19070 _{1/2} —48830 _{3/2}	
3360.326	3	30	29750.47	+0.05	19404 _{0/2} —49154 _{0/2}	res
3361.104	40A	100	29743.58	-0.08	<i>a</i> ⁴ P _{0/2} — <i>z</i> ² S _{0/2}	res
3361.748		6	29737.89	+0.09	28118 _{2/2} —57856 _{2/2}	
3362.595		3	29730.39	+0.23	<i>a</i> ⁴ D _{3/2} — <i>z</i> ⁶ F _{3/2}	
3363.721	10	30	29720.44	-0.02	<i>a</i> ⁴ D _{1/2} —44354 _{3/2}	res
3364.351		4	29714.88	+0.02	25045 _{0/2} —54760 _{0/2}	
3364.588	1	3	29712.79	-0.26	24991 _{1/2} —54704 _{3/2}	
3366.718	2	30	29693.99	+0.09	24804 _{3/2} —54498 _{3/2}	res
3369.561		3	29668.93	-0.02	22194 _{3/2} —51863 _{3/2}	
3369.795	1	4	29666.87	0.00	23234 _{4/2} —52901 _{3/2}	
3370.240		3	29662.96	-0.06	23450 _{2/2} —53113 _{2/2}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
3372. 202	2	15	29645. 70	+0. 01	30633 _{4½} —60278 _{3½}	6
3374. 866	3	30	29622. 30	+0. 02	<i>a</i> ⁴ G _{4½} —46175 _{3½}	res
3376. 146	30	300	29611. 07	-0. 01	<i>a</i> ⁴ D _{3½} —44758 _{4½}	res
3379. 028	4	40	29585. 81	+0. 06	<i>a</i> ⁴ G _{3½} —46175 _{3½}	res
3379. 825		2	29578. 84	+0. 06	19404 _{0½} —48982 _{1½}	
3380. 681	1	8	29571. 35	+0. 20	24804 _{3½} —54375 _{2½}	
3382. 598	50A	40	29554. 59	+0. 41	19276 _{2½} —48830 _{3½}	
3383. 091	2	50	29550. 28	+0. 10	29341 _{4½} —58891 _{5½}	
3384. 888	25	20	29534. 60	-0. 14	25169 _{1½} —54704 _{2½}	
3386. 502	4	20	29520. 52	+0. 17	23046 _{3½} —52567 _{3½}	
3386. 933		3	29516. 76	+0. 16	28491 _{1½} —58007 _{1½}	
3387. 634	1	15	29510. 66	+0. 40	26929 _{5½} —56439 _{5½}	
3389. 544		2	29494. 03	-0. 01	24991 _{1½} —54485 _{0½}	
3389. 985		1	29490. 19	+0. 05	25672 _{2½} —55162 _{2½}	
3390. 324	1	20	29487. 24	+0. 10	19637 _{2½} —49124 _{3½}	res
3394. 450	2	15	29451. 40	+0. 16	23450 _{2½} —52901 _{3½}	
3394. 907	1	3	29447. 44	+0. 33	26929 _{5½} —56376 _{3½}	
3395. 712		2	29440. 45	+0. 05	25045 _{0½} —54485 _{0½}	
3398. 690		1	29414. 66	+0. 09	23955 _{5½} —53369 _{4½}	
3398. 922	15	120	29412. 65	+0. 02	18000 _{3½} —47413 _{2½}	7
3401. 884	30	300	29387. 04	+0. 04	<i>a</i> ⁴ D _{2½} —44354 _{2½}	res
3402. 194		40?	29384. 37	+0. 11	24991 _{1½} —54375 _{2½}	
3404. 082		1	29368. 07	+0. 07	29341 _{4½} —58709 _{3½}	
3406. 086	2	12	29350. 79	+0. 09	25672 _{2½} —55022 _{3½}	
3406. 588	1	20	29346. 47	+0. 15	29341 _{4½} —58687 _{4½}	
3406. 824	30A	40	29344. 43	+0. 14	<i>a</i> ⁴ P _{1½} —39936 _{2½}	
3407. 450	2	10	29339. 04	+0. 16	27273 _{3½} —56612 _{3½}	
3408. 214	2	5	29332. 47	+0. 19	23234 _{4½} —52567 _{3½}	
3410. 170	1	25	29315. 64	-0. 09	25169 _{1½} —54485 _{0½}	
3412. 736	3	30	29293. 60	+0. 08	18990 _{1½} —48284 _{2½}	res
3415. 406	4	6	29270. 70	+0. 16	27273 _{3½} —56544 _{2½}	
3416. 370		2	29262. 44	+0. 39	19070 _{4½} —48332 _{5½}	
3416. 623	20	100	29260. 27			
3417. 620		3	29251. 74	-0. 13	24804 _{3½} —54056 _{3½}	
3419. 720		5	29233. 77	+0. 14	26158 _{4½} —55392 _{4½}	
3421. 134	4	40	29221. 69	+0. 12	24804 _{3½} —54026 _{2½}	4
3421. 430		5	29219. 17	+0. 07	24918 _{1½} —54137 _{1½}	
3422. 742	1	6	29207. 97	+0. 17	<i>a</i> ⁴ D _{3½} —44354 _{2½}	
3424. 436	5	50	29193. 52	+0. 20	19637 _{2½} —48830 _{3½}	res
3426. 20		4	29178. 5	+0. 3	31100 _{5½} —60278 _{4½}	
3430. 558		1	29141. 42	+0. 12	20039 _{3½} —49181 _{3½}	
3430. 739	1—	8	29139. 89	+0. 11	27273 _{3½} —56413 _{4½}	
3435. 636		4	29098. 35	+0. 29	28631 _{3½} —57729 _{3½}	
3435. 710	30A	6	29097. 73	-0. 17	23803 _{3½} —52901 _{3½}	<i>d</i>
3437. 233	3	20?	29084. 83	+0. 05	20039 _{3½} —49124 _{3½}	res
3440. 583	4	20	29056. 51	+0. 10	<i>a</i> ⁴ G _{5½} — <i>z</i> ⁶ F _{4½}	
3440. 644		200	29056. 00	+0. 06	33910 _{5½} —62966 _{5½}	
3442. 493	2	20	29040. 40	+0. 18	23046 _{3½} —52087 _{2½}	res
3443. 167		2	29034. 71	+0. 03	24991 _{1½} —54026 _{2½}	
3444. 934		2	29019. 82	+0. 04	25209 _{4½} —54229 _{5½}	
3449. 862	10	100	28978. 36	+0. 05	<i>a</i> ⁴ F _{3½} —42390 _{3½}	6
3451. 166		10	28967. 41	+0. 08	25169 _{1½} —54137 _{1½}	7
3452. 494	8	30	28956. 27	+0. 10	<i>a</i> ⁴ P _{2½} —42390 _{3½}	res
3454. 962	} 1 <i>d</i>	} 30 <i>d</i>	28935. 54	+0. 24	26227 _{2½} —55162 _{2½}	} 5
3455. 015			28935. 14	+0. 17	22503 _{1½} —51438 _{2½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
3460.377	1	10	28890.31	+0.12	19442 _{6½} —48332 _{3½}	
3463.510	20	150	28864.18	+0.08	<i>a</i> 4P _{2½} —42298 _{1½}	7
3464.446	1	20	28856.38	+0.01	25169 _{1½} —54026 _{3½}	res
3465.062	1	10	28851.25	+0.08	22194 _{3½} —51045 _{3½}	6
3468.225	4	6	28824.94	+0.16	23450 _{2½} —52275 _{3½}	
3469.266	2	25	28816.29	+0.60	23046 _{3½} —51863 _{3½}	6
3470.746		1	28804.00	0.00	33910 _{3½} —62714 _{6½}	
3471.230	1	6	28799.99	+0.15	26158 _{4½} —54958 _{5½}	
3471.698		3	28796.10	+0.24	26227 _{2½} —55022 _{3½}	
3472.310	1	10	28791.03	+0.07	20039 _{3½} —48850 _{3½}	
3472.896		4	28786.17	0.00	20455 _{1½} —49242 _{3½}	
3475.288	2	80	28766.36	+0.04	30633 _{4½} —59399 _{4½}	res
3475.936	1	10	28761.00	0.00	28491 _{1½} —57252 _{3½}	
3476.496	30A	8	28756.36	+0.27	28118 _{2½} —56874 _{3½}	7
3477.092	1	4	28751.43	+0.09	22503 _{1½} —51254 _{1½}	6
3481.910	—?	10	28711.65	-0.01	28377 _{5½} —57089 _{4½}	
3483.490		3	28698.63	+0.06	20455 _{1½} —49154 _{6½}	
3486.122	10	50	28676.96	+0.17	<i>a</i> 4G _{2½} —44911 _{1½}	res
3487.080		3	28669.08	+0.11	22194 _{3½} —50863 _{3½}	
3489.42		3	28649.86	+0.15	28118 _{2½} —56768 _{3½}	
3489.785	1	3	28646.86	+0.17	20534 _{3½} —49181 _{4½}	
3490.313	8	40	28642.53	+0.19	<i>a</i> 4G _{2½} —z 6F _{3½}	res
3490.912	12	50	28637.61	+0.12	<i>a</i> 4F _{3½} —z 6F _{2½}	4
3491.127	8	25	28635.85	+0.12	<i>a</i> 4F _{2½} —39936 _{3½}	6 res
3492.056	3	40	28628.23	+0.07	23234 _{4½} —51863 _{3½}	
3492.46	1	3	28624.92	-0.04	34091 _{4½} —62715 _{4½}	
3493.62	1—		28615.42	+0.07	<i>a</i> 4P _{2½} —z 6F _{3½}	
3498.134	1	5	28578.49			
3503.22		3	28537.00	+0.11	<i>a</i> 4P _{1½} —z 6F _{1½}	
3503.656		30	28533.45	+0.05	24804 _{3½} —53338 _{3½}	
3505.05		2	28522.1	0.0	24918 _{1½} —53440 _{6½}	
3507.17		2	28504.87	-0.01	24918 _{1½} —53422 _{1½}	
3508.54	1	3	28493.73	-0.11	28118 _{2½} —56612 _{3½}	
3508.664		50	28492.73	0.00	18000 _{3½} —z 6F _{4½}	
3511.269	2	15	28471.59	+0.15	23803 _{3½} —52279 _{3½}	
3512.077	1	20	28465.04	0.00	25672 _{2½} —54137 _{1½}	res
3512.98		3	28457.72	+0.12	28631 _{3½} —57089 _{4½}	
3514.106		20	28448.60	-0.01	24991 _{1½} —53440 _{6½}	
3514.990	1	4	28441.45	+0.18	28491 _{1½} —56932 _{1½}	
3516.234		15	28431.39	-0.03	24991 _{1½} —53422 _{1½}	
3517.39		3	28422.04	-0.33	18990 _{1½} —47413 _{3½}	
3518.56	1	2	28412.60	+0.07	23450 _{2½} —51863 _{3½}	
3521.57		2	28388.31	-0.05	29341 _{4½} —57729 _{3½}	
3522.102	1	10	28384.02	+0.03	28491 _{1½} —56874 _{2½}	
3523.133		8	28375.71			
3525.733	3	30	28354.79	+0.09	18000 _{3½} —46355 _{3½}	res
3526.817	—	50	28346.08	+0.06	34091 _{4½} —62437 _{4½}	6
3527.040	—?	30	28344.28	+0.14	20780 _{4½} —49124 _{3½}	
3529.546	10	100	28324.16	+0.12	<i>a</i> 4G _{4½} —z 6F _{3½}	res
3531.440	2	5	28308.97	+0.12	24804 _{3½} —53113 _{2½}	
3532.680		3	28299.03	+0.15	31100 _{5½} —59399 _{4½}	
3534.12		5	28287.50	-0.01	<i>a</i> 4G _{3½} —z 6F _{3½}	
3534.498	3	25	28284.48	-0.03	25045 _{0½} —53329 _{1½}	6?
3536.12		5	28271.50	-0.07	26227 _{2½} —54498 _{3½}	
3536.268	4	80	28270.32	+0.02	25169 _{1½} —53440 _{6½}	6?
3538.40		2	28253.29	+0.18	25169 _{1½} —53422 _{1½}	
3538.55	(—?)	3	28252.09	+0.09	28187 _{6½} —56439 _{6½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
3539.455	3A	4	28244.87	+0.13	20039 _{3/2} —48284 _{2/2}	res
3544.460	5	25	28204.98	+0.02	<i>a</i> ⁴ G _{3/2} —44758 _{4/2}	res
3546.474	3A	3	28188.97	-0.01	18990 _{1/2} —47179 _{1/2}	
3547.00	1	1	28184.79	+0.23	19404 _{0/2} —47588 _{1/2}	
3548.258	15A	12	28174.79	+0.07	18000 _{3/2} —46175 _{3/2}	<i>d</i>
3549.052	25	150	28168.49	+0.06	<i>a</i> ⁴ G _{3/2} —44758 _{4/2}	res
3550.14		3	28159.86	+0.02	25169 _{1/2} —53329 _{1/2}	
3551.528		10	28148.85	+0.03	26227 _{2/2} —54375 _{2/2}	
3553.020		5	28137.03	+0.22	19276 _{2/2} —47413 _{2/2}	
3554.068	1	3	28128.74	-0.05	25209 _{4/2} —53338 _{3/2}	
3554.93		2	28121.92	-0.04	24991 _{1/2} —53113 _{2/2}	
3555.166	12	120	28120.05	+0.07	<i>a</i> ⁴ G _{2/2} —44354 _{2/2}	res
3557.914	5	30	28098.33	+0.08	22194 _{3/2} —50292 _{3/2}	
3560.67		2	28076.58	+0.04	30633 _{1/2} —58709 _{3/2}	
3561.456		5	28070.39	+0.07	26158 _{4/2} —54229 _{5/2}	
3562.508	1	5	28062.10	+0.30	28377 _{3/2} —56439 _{0/2}	4
3563.59		3	28053.6	+0.2	28491 _{1/2} —56544 _{2/2}	
3563.998	1	2	28050.37	+0.05	20780 _{1/2} —48830 _{3/2}	
3565.834	1	3	28035.92	+0.08	28377 _{3/2} —56413 _{1/2}	
3566.73		3	28028.9	-0.3	26929 _{3/2} —54958 _{5/2}	
3571.972	3	8	27987.75	+0.22	23450 _{3/2} —51438 _{2/2}	
3572.474	60	200	27983.82	+0.02	<i>a</i> ⁴ P _{1/2} — <i>z</i> ² S _{0/2}	res
3572.830	1	5	27981.03	+0.15	28631 _{3/2} —56612 _{3/2}	6
3574.82		2	27965.4	0.0	28118 _{2/2} —56084 _{1/2}	
3577.59		2	27943.8	+0.2	25169 _{1/2} —53113 _{2/2}	
3579.64		3	27927.8	-0.1	22503 _{1/2} —50430 _{1/2}	
3581.876	2	6	27910.36	+0.16	26227 _{2/2} —54137 _{1/2}	res
3582.75	1	2	27903.56	+0.14	19276 _{2/2} —47179 _{1/2}	
3583.458	1	8	27898.04	+0.24	26158 _{4/2} —54056 _{1/2}	6
3584.68		3	27888.53	+0.09	27273 _{3/2} —55162 _{2/2}	
3592.418	50	150	27828.46	{ -0.09	20455 _{1/2} —48284 _{2/2}	5 res
3596.171	2	30	27799.42	{ +0.13	<i>a</i> ⁴ F _{2/2} — <i>z</i> ⁶ F _{1/2}	4
3597.48	—?	2	27789.31	+0.18	26227 _{2/2} —54026 _{2/2}	
3598.45	2	20	27781.8	+0.04	22503 _{3/2} —50292 _{3/2}	
3600.594		1	27765.27	0.0	28631 _{3/2} —56413 _{4/2}	7
				+0.12	<i>a</i> ⁴ G _{3/2} —44354 _{2/2}	
3600.933	1	6	27762.66	+0.18	24804 _{3/2} —52567 _{4/2}	
3601.55		1	27757.90	+0.10	25045 _{0/2} —52803 _{1/2}	
3602.455	3	8	27750.93	+0.11	25672 _{2/2} —53422 _{1/2}	
3602.700	—?	1	27749.04	+0.04	27273 _{3/2} —55022 _{3/2}	
3608.280		10	27706.13			
3610.044	1	20	27692.59	+0.13	25209 _{4/2} —52901 _{3/2}	res
3611.826	1	20	27678.92	+0.02	33910 _{3/2} —61589 _{5/2}	6
3613.530		4	27665.88	-0.03	25672 _{2/2} —53338 _{3/2}	
3613.785	30	150	27663.93	+0.09	<i>a</i> ⁴ D _{1/2} —42298 _{1/2}	res
3614.606	1	8	27657.64	+0.09	25672 _{2/2} —53329 _{1/2}	
3617.652		4	27634.36	{ +0.05	18990 _{1/2} —46625 _{0/2}	
3618.434	1	25	27628.39	{ +0.17	23803 _{3/2} —51438 _{2/2}	
3628.413	3	30	27552.40	+0.21	23234 _{4/2} —50863 _{4/2}	
3628.924	2	25	27548.52	+0.05	20780 _{4/2} —48332 _{3/2}	res
3630.080	2	3	27539.75	0.00	25045 _{0/2} —52593 _{0/2}	res
				0.15	23955 _{3/2} — <i>z</i> ⁶ F _{5/2}	
3630.950		8	27533.15	+0.10	<i>a</i> ⁴ F _{4/2} —42390 _{3/2}	
3639.213		1	27470.64	+0.03	24804 _{3/2} —52275 _{3/2}	
3641.403	60	120	27454.12	+0.03	<i>a</i> ⁴ F _{1/2} — <i>z</i> ⁶ F _{0/2}	7
3645.594	10	100	27422.56	+0.11	<i>a</i> ⁴ D _{2/2} —42390 _{3/2}	res
3646.577	10	50	27415.16	+0.07	<i>a</i> ⁴ D _{1/2} — <i>z</i> ⁶ F _{2/2}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
3652. 114	10	20	27373. 60	+0. 01	20039 _{3/2} —47413 _{3/2}	
3653. 324	2	10	27364. 54	+0. 10	18990 _{1/2} —46355 _{3/2}	
3654. 74		10	27353. 94	+0. 04	30633 _{1/2} —57986 _{3/2}	
3657. 583	40	120	27332. 67	-0. 02	<i>a</i> ⁴ P _{0/2} — <i>z</i> ⁶ F _{0/2}	
3657. 871	10	40	27330. 52	+0. 14	<i>a</i> ⁴ D _{2/2} —42298 _{1/2}	res
3660. 604	30.A	8	27310. 12	+0. 21	25045 _{0/2} —52355 _{0/2}	
3670. 65		1?	27235. 37	+0. 10	34091 _{4/2} —61326 _{3/2}	
3672. 547	5	25	27221. 31	+0. 12	19404 _{0/2} —46625 _{0/2}	6
3677. 405	1	8	27185. 35	+0. 11	25169 _{1/2} —52355 _{0/2}	
3678. 210	1	10	27179. 40	+0. 07	26158 _{4/2} —53338 _{3/2}	res
3687. 510		2	27110. 85	-0. 22	26227 _{2/2} —53338 _{3/2}	
3689. 596		10	27095. 52	+0. 06	24991 _{1/2} —52087 _{3/2}	
3691. 463	1	2	27081. 82	+0. 19	<i>a</i> ⁴ D _{2/2} — <i>z</i> ⁶ F _{3/2}	
3691. 846	4	40	27079. 01	+0. 13	19276 _{2/2} —46355 _{3/2}	res
3692. 864		2	27071. 55	-0. 53	29341 _{4/2} —56413 _{3/2}	
3694. 525	40.A	40	27059. 38	+0. 17	23803 _{3/2} —50863 _{3/2}	5
3705. 310	1	4	26980. 62	+0. 17	23450 _{2/2} —50430 _{1/2}	
3707. 478	3	2	26964. 84	+0. 06	34091 _{4/2} —61055 _{3/2}	
3708. 494	8	60	26957. 45	+0. 05	20455 _{1/2} —47413 _{3/2}	
3712. 202	3	12	26930. 53	+0. 09	22194 _{3/2} —49124 _{3/2}	
3714. 033		2	26917. 25	+0. 10	25169 _{1/2} —52087 _{3/2}	
3715. 832	3	8	26904. 22	+0. 26	28118 _{2/2} —55022 _{3/2}	
3716. 062	10	50	26902. 55	+0. 12	<i>a</i> ⁴ D _{3/2} — <i>z</i> ⁶ F _{3/2}	res
3716. 550	2	2	26899. 02	+0. 12	19276 _{2/2} —46175 _{3/2}	
3719. 66		3	26876. 53	+0. 05	18000 _{3/2} — <i>z</i> ⁶ F _{3/2}	
3721. 102		10	26866. 12			
3732. 684	2	2	26782. 76	+0. 08	27273 _{3/2} —54056 _{3/2}	
3736. 213	12	60	26757. 46	+0. 06	18000 _{3/2} —44758 _{3/2}	res
3736. 91		2	26752. 5	+0. 1	27273 _{3/2} —54026 _{3/2}	
3741. 706	30.A	12	26718. 18	+0. 16	19637 _{2/2} —46355 _{3/2}	6
3745. 530	4	40	26690. 90	+0. 17	22139 _{2/2} —48830 _{3/2}	7
3750. 744	1	8	26653. 80	+0. 05	25209 _{4/2} —51863 _{3/2}	
3753. 162		3	26636. 63	+0. 01	22194 _{3/2} —48830 _{3/2}	
3753. 620		10	26633. 38	+0. 02	24804 _{3/2} —51438 _{3/2}	
3760. 364	2	20	26585. 61	-0. 10	28118 _{2/2} —54704 _{2/2}	
3763. 616	2	2	26562. 64	-0. 10	18990 _{1/2} —45553 _{1/2}	
3768. 97		4	26524. 91	+0. 06	<i>a</i> ⁴ F _{3/2} —39936 _{3/2}	
3772. 05	8.A	3	26503. 25	+0. 54	<i>a</i> ⁴ P _{2/2} —39936 _{3/2}	
3774. 14	—	20	26488. 58	+0. 09	23803 _{3/2} —50292 _{3/2}	
3777. 35	1	10	26466. 07	+0. 01	18990 _{1/2} —45457 _{0/2}	
3778. 686	30.A	8	26456. 71	+0. 27	30633 _{4/2} —57089 _{3/2}	
3785. 58		20	26408. 5	+0. 1	26158 _{4/2} —52567 _{3/2}	
3789. 726		20	26379. 64	-0. 03	28118 _{2/2} —54498 _{3/2}	
3804. 481	1	2	26277. 3	+0. 1	19276 _{2/2} —45553 _{1/2}	
3814. 418	5	6	26208. 88	-0. 32	25045 _{0/2} —51254 _{1/2}	
3822. 198	2	4	26155. 53	+0. 10	<i>a</i> ⁴ G _{2/2} —42390 _{3/2}	
3823. 062	3	10	26149. 62	0. 00	19404 _{0/2} —45553 _{1/2}	res
3827. 89		4	26116. 6	+0. 1	26158 _{4/2} —52275 _{3/2}	
3833. 61	2		26077. 7	0. 0	23046 _{3/2} —49124 _{3/2}	
3837. 238	4	10	26053. 02	+0. 08	19404 _{0/2} —45457 _{0/2}	
3846. 688	2		25989. 02	+0. 02	31100 _{3/2} —57089 _{3/2}	
3851. 131	—?	2	25959. 03	-0. 05	20534 _{3/2} — <i>z</i> ⁶ F _{1/2}	
3851. 570	12	60	25956. 07	+0. 04	<i>a</i> ⁴ D _{0/2} — <i>z</i> ⁶ F _{1/2}	res
3856. 828	3	6	25920. 69	+0. 02	18990 _{1/2} —44911 _{1/2}	6
3859. 986	2	6	25899. 48	+0. 01	20455 _{1/2} —46355 _{3/2}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
3872. 656	4	10	25814. 75	+0. 14	<i>a</i> ⁴ G _{2½} — <i>z</i> ⁶ F _{3½}	6
3877. 29	2	15	25783. 9	0. 0	23046 _{3½} —48830 _{3½}	
3877. 65	1		25781. 5	+0. 1	22503 _{1½} —48284 _{2½}	
3883. 336	2	3	25743. 76	-0. 20	28631 _{3½} —54375 _{2½}	
3887. 951	1	3	25713. 20	+0. 15	20780 _{4½} — <i>z</i> ⁶ F _{3½}	
3890. 658	—?	2	25695. 31	0. 00	<i>a</i> ⁴ P _{2½} — <i>z</i> ⁶ F _{1½}	6
3891. 83	1	1	25687. 57	+0. 15	19070 _{4½} —44758 _{4½}	
3896. 930	3	20	25653. 95	+0. 18	25209 _{4½} —50863 _{4½}	
3899. 782	2	3	25635. 19	+0. 08	19276 _{2½} —44911 _{1½}	
3900. 879	2	8	25627. 98	+0. 10	27273 _{3½} —52901 _{3½}	
3905. 79	1	3	25595. 8	0. 0	23234 _{4½} —48830 _{3½}	
3909. 276	2	2	25572. 94	+0. 11	<i>a</i> ⁴ P _{1½} — <i>z</i> ⁶ F _{0½}	
3915. 456	2	5	25532. 57	+0. 21	23450 _{3½} —48982 _{1½}	
3935. 43	4	10	25403. 0	+0. 1	<i>a</i> ⁴ D _{0½} — <i>z</i> ² S _{0½}	
3936. 653	1	5	25395. 10	+0. 06	20780 _{4½} —46175 _{3½}	
3936. 782	1		25394. 27	-0. 11	28631 _{3½} —54026 _{2½}	
3938. 10		1	25385. 8	0. 0	25045 _{0½} —50430 _{1½}	
3939. 43	8	3	25377. 2	0. 0	23803 _{3½} —49181 _{4½}	
3951. 067	3	6	25302. 45	0. 00	<i>a</i> ⁴ D _{1½} — <i>z</i> ³ S _{0½}	
3955. 606	1	1	25273. 42	+0. 06	22139 _{2½} —47413 _{2½}	
3960. 87	2	6	25239. 83	+0. 03	19637 _{2½} — <i>z</i> ⁶ F _{3½}	6, <i>d</i>
3691. 192	—?	3	25237. 78	+0. 10	23046 _{3½} —48284 _{2½}	
3964. 096	—?	6	25219. 29	+0. 04	22194 _{3½} —47413 _{2½}	
3983. 292	50A	5	25097. 76	-0. 01	20455 _{1½} —45553 _{1½}	
3986. 38		1	25078. 3	0. 0	19276 _{2½} —44354 _{2½}	
3990. 42		2	25052. 9	+0. 1	22535 _{0½} —47588 _{1½}	6
3994. 56	2		25027. 0	+0. 1	23803 _{3½} —48830 _{3½}	
4000. 10	1	1	24992. 3	+0. 1	28377 _{5½} —53369 _{4½}	
4001. 883	1	4	24981. 17	-0. 01	33910 _{0½} —58891 _{5½}	
4060. 166	1	2	24622. 58	+0. 06	28491 _{1½} —53113 _{2½}	
4069. 61	1		24565. 4	-0. 3	26929 _{5½} — <i>z</i> ⁶ F _{5½}	6
4081. 294	4	10	24495. 12	+0. 07	<i>a</i> ⁴ D _{1½} — <i>z</i> ⁶ F _{1½}	
4114. 19	1	2	24299. 3	-0. 08	22194 _{3½} — <i>z</i> ⁶ F _{1½}	
4144. 41	1		24122. 1	-0. 1	22503 _{1½} —46625 _{0½}	
4146. 62	—?	1	24109. 2	-0. 1	25045 _{0½} —49154 _{0½}	
4157. 030	2	5	24048. 86	+0. 11	18000 _{3½} — <i>z</i> ⁶ F _{3½}	
4165. 60	1	2	23999. 4	+0. 2	20455 _{1½} —44455 _{0½}	
4175. 58	5	5	23942. 0	0. 0	<i>a</i> ⁴ D _{1½} — <i>z</i> ² S _{0½}	
4257. 82	1		23479. 6	-0. 2	24804 _{3½} —48284 _{2½}	
4262. 75	1		23452. 4	0. 0	25672 _{2½} —49124 _{3½}	
4263. 81	1		23446. 6	0. 0	23046 _{3½} — <i>z</i> ⁶ F _{4½}	}
4289. 28	2	2	23307. 4	0. 0	28187 _{6½} — <i>z</i> ⁶ F _{5½}	
				+0. 2	18990 _{1½} —42298 _{1½}	
4298. 26	1		23258. 7	+0. 1	23234 _{4½} — <i>z</i> ⁶ F _{1½}	
4323. 392	1	6	23123. 49	+0. 04	25209 _{4½} —48332 _{3½}	
4335. 58	1?	6	23058. 5	0. 0	18990 _{1½} — <i>z</i> ⁶ F _{2½}	
4342. 40		2	23022. 3	0. 0	26158 _{0½} —49181 _{4½}	res res
4343. 20	2	5	23018. 0	+0. 1	22535 _{0½} —45553 _{1½}	
4348. 108	20A	25	22992. 05	+0. 08	<i>a</i> ⁴ D _{0½} — <i>z</i> ⁶ F _{0½}	
4361. 534	8A	3	22921. 28	+0. 06	22535 _{0½} —45457 _{0½}	
4393. 80	1	2	22753. 0	+0. 1	19637 _{2½} —42390 _{3½}	

TABLE 3. *Classified lines of W II—Continued*

Wavelength (Å)	Intensity		Wave number (cm ⁻¹)		Combination	Zeeman effect
	Arc	Spark	Observed	O-C		
Air						
4396. 88	2	2	22737. 0	{ -0. 2 0. 0	22139 _{2½} —z ⁶ F _{3½} 30633 _{1½} —53369 _{4½}	
4421. 836	15A	3	22608. 69	+ 0. 03	24804 _{3½} —47413 _{2½}	
4438. 92		2	22521. 7	0. 0	34091 _{1½} —56612 _{3½}	
4468. 72		1	22371. 5	-0. 1	23803 _{3½} —46175 _{3½}	
4508. 50		2	22174. 1	+0. 1	26158 _{1½} —48332 _{3½}	
4542. 144	1	2	22009. 86	{ -0. 21 +0. 15	25169 _{1½} —47179 _{1½} 20039 _{3½} —z ⁶ F _{2½}	
4554. 045	1	2	21952. 35	+0. 23	22503 _{1½} —44455 _{0½}	
4604. 576	1	3	21711. 44	+0. 14	23046 _{3½} —44758 _{1½}	
4658. 24	2	2	21461. 3	+0. 19	23450 _{2½} —44911 _{1½}	
4665. 76	4A	3	21426. 74	+0. 06	23450 _{2½} —z ⁶ F _{3½}	
4691. 74	1	2	21308. 1	+0. 1	23046 _{3½} —44354 _{2½}	
4718. 91	1	3	21185. 4	-0. 1	25169 _{1½} —46355 _{2½}	
4768. 25	1	2	20966. 2	+0. 1	25209 _{1½} —46175 _{3½}	
4782. 35	1	1	20904. 4	+0. 1	23450 _{2½} —44354 _{2½}	
4864. 565	2	3	20551. 08	+0. 10	23803 _{3½} —44354 _{2½}	
4959. 33	3	2	20158. 4	+0. 2	22139 _{2½} —42298 _{1½}	
5021. 324	5	2	19909. 51	+0. 03	22139 _{2½} —z ⁶ F _{2½}	
5104. 427	6	6	19585. 37	+0. 01	18990 _{1½} —z ² S _{0½}	
5114. 59	3	3	19546. 46	+0. 07	22503 _{1½} —z ⁶ F _{2½}	
5131. 83	2	2	19480. 8	-0. 1	20455 _{1½} —39936 _{3½}	
5214. 41	2	?	19172. 3	+0. 1	19404 _{0½} —z ² S _{0½}	
5219. 04	3	?	19155. 3	-0. 1	23234 _{1½} —42390 _{3½}	
5260. 92	4	4	19002. 8	+0. 2	23046 _{3½} —z ⁶ F _{2½}	
5278. 38	8	2	18939. 9	+0. 1	23450 _{2½} —42390 _{3½}	
5304. 17	10	4	18847. 8	+0. 1	23450 _{2½} —42298 _{1½}	
5353. 677	5	3	18673. 54	+0. 06	20455 _{1½} —z ⁶ F _{1½}	
5375. 103	3	2	18599. 12	{ -0. 24 +0. 17	26158 _{1½} —44758 _{4½} 23450 _{2½} —z ⁶ F _{2½}	
5410. 89	2	2	18476. 12	-0. 01	34091 _{1½} —52567 _{4½}	
5597. 056	3	3	17861. 63	+0. 06	28631 _{3½} —z ⁶ F _{4½}	
5698. 47	1	1	17543. 7	+0. 1	28631 _{3½} —46175 _{3½}	
5821. 00	4A	1	17174. 42	+0. 03	18990 _{1½} —z ⁶ F _{0½}	
5884. 32	2	2	16989. 6	+0. 2	22139 _{2½} —z ⁶ F _{1½}	
5964. 48	3	5	16761. 28	+0. 01	19404 _{0½} —z ⁶ F _{0½}	
6024. 64	2	5	16593. 91	+0. 30	22535 _{0½} —z ⁶ F _{1½}	
6219. 77	2	8	16073. 32	+0. 06	22503 _{1½} —z ² S _{0½}	

I gratefully acknowledge the assistance of Dr. C. C. Kiess, who supplied most of the spectrograms, and of Mrs. Isabel Murray, who carefully prepared press-copy of the tables.

4. References

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Publications of the National Bureau of Standards*

Selected Abstracts

Gaussian wave functions for polyatomic molecules: integral formulas, M. Krauss, *J. Res.* **68B** (*Math. and Math. Phys.*), No. 1, 35–41 (Jan.–Mar. 1894).

Explicit formulas are given for the molecular coulomb integrals that arise for all Gaussian basis functions. These results should expedite computational efforts with these basis functions.

A Fabry-Perot spectrometer for high-resolution spectroscopy and laser work, K. D. Mielenz, R. B. Stephens, and K. F. Nefflen, *J. Res.* **68C** (*Eng. and Instr.*), No. 1, 1–6 (Jan.–Mar. 1964).

A Fabry-Perot spectrometer with a piezoelectric spacer was constructed to record with a recorder, or display with an oculoscope, the fine structure of the Haidinger fringes. The spectrometer is of the fixed spacer design, which provides great stability of adjustment. It was used to record the Zeeman splitting of the green line of Hg 198, as well as to exhibit, on the oscilloscope screen, the multimode output signal of a He-Ne gas laser.

A laser with a multihole diaphragm, T. Morokuma, *J. Res.* **68C** (*Eng. and Instr.*), No. 1, 25–34 (Jan.–Mar. 1964).

The properties of a laser with a multihole diaphragm were both theoretically and experimentally examined. This laser may be called a multibeam laser. Laser action was observed in the optical paths which were defined by the position of the holes and the cavity configuration. Interference fringes were observed on one of the cavity mirrors. A wavelength dependent interaction among the beams was observed. It is believed that the wavelength of a beam can be stabilized by the intensities of the other beams. A possible method will be proposed for the stabilization.

Principles of cryometric impurity determination as applied to samples of small sizes, C. P. Saylor and G. S. Ross, *J. Res.* **68C** (*Eng. and Instr.*), No. 1, 35–39 (Jan.–Mar. 1964).

A consideration of the factors that tend to prevent attainment of thermal and thermodynamic equilibrium during thermometric methods of purity analysis suggests that the problems largely originate from spontaneously introduced inequalities in composition. During either a freezing or melting cycle, the solid phase settles in the liquid. This results in a greater average purity in the bottom than in the upper part of the vessel. The effects would be particularly strong during a melting sequence where the liquid released by melting of the solid would provide the compositional environment for the establishment of final temperature. This hypothesis has been tested by the design of a new cell for small samples. The design incorporates use of small gold pans to hold solid and liquid in close contact. The results are comparable in precision to those from conventional time-temperature curves with much larger samples, a condition not ordinarily possible with small samples.

Reference tables for thermocouples of iridium-rhodium alloys versus iridium, G. F. Blackburn and F. R. Caldwell, *J. Res.* **68C** (*Eng. and Instr.*), No. 1, 41–59 (Jan.–Mar. 1964).

The program at the National Bureau of Standards to establish reference tables of temperature versus emf for thermocouples of iridium-rhodium alloys versus iridium has been extended to cover all three of the currently used thermocouples of this type. In addition to the values published in 1962 for the 40 Ir-60 Rh versus Ir thermocouples, tables now are available for thermocouples of 60 Ir-40 Rh and 50 Ir-50 Rh versus Ir. These tables give emfs for temperatures in degrees

Celsius from 0 to 2150 °C and in degrees Fahrenheit from 32 to 3900 °F, and temperatures in these units with emf in millivolts as the argument.

In addition to the reference tables for these thermocouples, temperature-emf relationships are presented for other alloys containing 10, 25, 75, and 90 percent iridium versus iridium. It appears from the information obtained on all of the alloy versus iridium combinations tested that the 50 Ir-50 Rh alloy versus iridium gives about the maximum thermal emf (12.2 mv at 2150 °C), and as a result may provide the optimum thermocouple combination of this type.

A simplified theory of diffraction at an interface separating two dielectrics, J. Kane and S. N. Karp, *Radio Sci. J. Res.* **NBS/USNC-URSI 68D** No. 3, 303–310 (Mar. 1964).

Many electromagnetic problems involving more than one dielectric medium are not susceptible of an exact solution, when appropriate boundary conditions are considered. The purpose of the present paper is to formulate a new boundary condition, which is capable of leading to mathematically tractable problems, with limited sacrifices in accuracy.

Propagation of plasma waves in a "spoke-wheel" magnetic field, R. L. Liboff, *Radio Sci. J. Res.* **NBS/USNC-URSI 68D** No. 3, 325–331 (Mar. 1964).

A study of the cold plasma cylindrical waves that may propagate in a specific type of two-dimensional magnetic field is initiated in this paper. The plasma is assumed to be of uniform density and collisionless, and a "spoke-wheel" magnetic field is considered which is both anisotropic and inhomogeneous (varying as the inverse radius), as defined in the text. Perturbation series solutions are obtained for the first Fourier component of the electric field for the four extreme cases: large and small magnetic field; large and small plasma densities.

Compilation of the melting points of the metal oxides, S. J. Schneider, *NBS Mono. 68* (Oct. 10, 1963), 25 cents.

A compilation has been made of the melting points of 70 metal oxides published prior to January 1963. Both the original melting point and the equivalent value based on the International Practical Temperature Scale of 1948 are presented. Included in the survey is information on pertinent experimental details such as the method of temperature measurement, purity, furnace type, and environmental conditions.

Calibration and test services of the National Bureau of Standards, *NBS Misc. Publ. 250* (Nov. 22, 1963), 70 cents.

This publication is a listing of the numerous calibration and testing services provided to science and industry by the National Bureau of Standards. The Bureau promotes accuracy and uniformity of measurement through its program of measurement services, including the calibration and testing of standards and standard instruments. An up-to-date listing of the Bureau's calibration and test fee schedules was printed in recent issues of the Federal Register, with a large proportion of the fees being changed at that time. This publication contains all of this material, but in larger, more legible type, and fully indexed. Besides listing all NBS calibration services and their cost, the publication includes a statement of the Bureau's statutory functions, testing policy, and routine for securing the Bureau's calibration and test services—from original request to the reporting and use of test results.

A comparison of two melting-pressure equations constrained to the triple point using data for eleven gases and three metals, R. D. Goodwin and L. A. Weber, *NBS Tech. Note 184* (Oct. 9, 1963), 25 cents.

Parameters have been determined by a least-squares method for the reduced Simon equation and for a new, empirical melting equation using data for H_2 , D_2 , T_2 , Ne, Ar, Kr, Xe, N_2 , O_2 , CO_2 , H_2O , Na, K, and Hg. The new equation, $(P - P^3)/(T - T^3) = A \exp(-\alpha/T) + BT$, represents experimental data with essentially the same accuracy as the Simon equation. It provides a sensitive difference method for graphical examination of data.

Carbon resistors for cryogenic liquid level measurements, R. C. Muhlenhaupt and P. Smelser, *NBS Tech. Note 200* (Oct. 8, 1963), 25 cents.

Data are shown in graphical form. One set of plots presents resistance ratio R_0/R_L as a function of "warming up" time at various levels of constant power dissipation. A second set of plots presents resistance ratio R_L/R_0 as a function of nominal resistance at various levels of constant power dissipation.

The use of the data and the design of a practical liquid level indicator are discussed in the appendix.

Absolute calibration of the National Bureau of Standards photoneutron source: III. Absorption in a heavy water solution of manganous sulfate, R. H. Noyce, E. R. Mosburg, Jr., S. B. Garfinkel, and R. S. Caswell, *J. Nucl. Eng.* **17**, No. 7, 313-318 (1963).

The neutron emission rate for the National Bureau of Standards radium-beryllium (γ, n) standard source (NBS-I) has been redetermined by a relative comparison to an antimony-beryllium source which had been calibrated absolutely in a heavy water manganous sulfate solution through an indirect method involving $4\pi\beta-\gamma$ coincidence counting of the induced Mn^{55} activity. Correction was made for absorption of neutrons by other elements present in the bath. The emission rate of NBS-I was found to be 1.252×10^6 neutrons per second, as of June 1961 with an uncertainty of 1 percent. This measurement, when suitably averaged with previous determinations (DeJuren, Padgett, and Curtiss, 1955; and DeJuren and Chin, 1955), yields the best value 1.257×10^6 neutrons per second with an uncertainty of 1 percent.

Heating rate as a test of adiabatic calorimeters and the heat capacity of α -alumina, E. D. West, *Trans. Faraday Soc.* **59**, No. 489, pt. 9, 2200-2203 (Sept. 1963).

The constancy of heat capacities measured in an adiabatic calorimeter at different heating rates does not demonstrate the absence of heat leak errors due to departures of the surface temperature from the "isothermal" condition. On the contrary, the total heat exchange between the calorimeter and its shield is virtually independent of the heating rate. The test tends to obscure a real source of error due to the variation in the total heat exchange between experiments with the empty and the full calorimeter.

A new standard of spectral irradiance, R. Stair, W. E. Schneider, and J. K. Jackson, *Appl. Opt.* **2**, No. 11, 1151-1154 (Nov. 1963).

The National Bureau of Standards has made available a new standard of spectral irradiance in the form of a 200-watt quartz-iodine lamp with a coiled-coil tungsten filament operating at about 3000° K and calibrated over the spectral range of 0.25 to 2.6 microns. The calibration of this standard is based upon the radiance of a blackbody as defined by the Planck law of radiation since it was done by comparisons with the NBS standards of spectral radiance, of luminous intensity, and of total irradiance, each of which was established through the use of blackbodies. This standard is used without auxiliary optics. Because of its small physical size and high operating temperature, relatively high spectral irradiances may be obtained through its use.

Intercomparisons of the standard thermal-neutron flux density of the National Bureau of Standards, W. M. Murphey and J. Chin, (*Proc. Symp. Neutron Detection, Dosimetry and Standardization, International Atomic Energy Agency, Atomic Energy Research Establishment, Harwell, England, Dec. 10-14, 1962*). Book, *Neutron Dosimetry II*, 513-521 (*International Atomic Energy Agency, Vienna, 1963*).

The standard thermal neutron flux maintained at the Na-

tional Bureau of Standards since 1951 consists of two radium-beryllium (α, n) sources in a geometry of lead, paraffin and carbon. The flux has been absolutely measured twice by NBS; once in terms of the absorption cross section of boron, and once in terms of the absorption cross section of gold (1,2). A neutron flux with a cadmium ratio of about 7 (for 40 mg/cm² gold foils and 0.040 inch cadmium covers) and a conventional thermal neutron flux density of 4231 (Apr. 62) neutrons per cm² per second was obtained. It has also been absolutely measured twice through the intercomparison program; once by NPL, UK and once by PTB, Federal Republic of Germany.

The agreement between most laboratories at present is about 1.5%. This is in addition to the uncertainty in the absolute measurement which is about 1.5% or more for each laboratory. Intercomparisons of NBS with CEA, France; Oak Ridge National Laboratory, USA; Electrotechnical Laboratory, Japan; National Physical Laboratory, UK; and Physikalisch-Technische Bundesanstalt, Federal Republic of Germany will be shown.

Interpretation of pH measurements in alcohol-water solvents, R. G. Bates, M. Paabo, and R. A. Robinson, *J. Phys. Chem.* **67**, 1833-1838 (1963).

The operational pH numbers for solutions in alcohol-water solvents obtained from the e.m.f. of the cell with hydrogen (or glass) electrode, salt bridge, and calomel reference electrode, standardized with aqueous buffer standards, are subject to no simple interpretation. Because of the indeterminate potential at the junction Soln. X (alc.-H₂O)|KCl bridge (aq.), they do not lie on a conventional scale of hydrogen ion activity referred either to the aqueous standard state (pa_H^*) or to the standard state in the alcoholic medium ($pa_H^{\#}$).

Values of $\bar{E}_j + \log m\gamma_{Cl}$ (where \bar{E}_j is the liquid-junction potential expressed in pH units and $m\gamma_{Cl}$ is the primary medium effect of chloride ion) were found to be as constant for different buffer solutions in alcoholic solvents of fixed composition as for the strictly aqueous medium. Inasmuch as $m\gamma_{Cl}$ at a given temperature is dependent only on solvent composition, the liquid-junction potential must therefore also be nearly constant for a given solvent medium. Correction terms $\bar{E}_j - \log m\gamma_H = \delta$ have been calculated, and it is shown that $pH - \delta$ closely approximates pa_H^* under optimum conditions of measurement. An operational scale of pH^* (which is related to pa_H^* in the same way that pH is related to $pa_H^{\#}$) is described. Values of pa_H^* were obtained for 12 solutions in methanol-water solvents (0 to 68.1 wt. % MeOH) and for 3 solutions in ethanol-water solvents (0 to 100 % EtOH).

Short-duration visible afterglow in helium, A. L. Schmeltekopf, Jr., and H. P. Broida, *J. Chem. Phys.* **39**, 1261-1268 (Sept. 1963).

A bright, reproducible afterglow which consists of helium atomic and molecular emissions has been observed in the products of an electrical discharge in a deLaval nozzle clearly separated from the discharge. This afterglow has been observed at pressures from 0.4 to 20 mm Hg and with flows from 10 to 1000 cm³/sec NTP. At the low pressure the existence of the afterglow is extremely sensitive to small changes in pressure. Metastable He atom concentration decreases after the discharge and then increases in the region of afterglow emission. The afterglow is very sensitive to impurities greater than a few parts in 10⁵ and emission intensity is reduced by the presence of an rf field, possibly because heating the electrons retards recombination.

Infrared transmission of the atmosphere to solar radiation, D. M. Gates and W. J. Harrop, *Appl. Opt.* **2**, 887-898 (Sept. 1963).

Infrared solar spectrum observations taken on 12 January 1955 in Denver, Colorado, with a double pass NaCl prism spectrometer have been analyzed for transmission coefficients for the "selective" absorption and for the "continuum" extinction. The analysis was performed over the range 1.0 to 12.5 μ . The goodness of fit for the average transmission for a random band model and for a regular band model is given for each of 203 data points distributed throughout the spectrum.

Some topics in quantum statistics. The Wigner function and transport theory, H. Mori, I. Oppenheim, and J. Ross, *Book, Studies in Statistical Mechanics, ed. DeBoer and Uhlenbeck, I, Pt. C, 218-298* (North Holland Publ. Co., Amsterdam, the Netherlands, 1962).

This article is devoted to a discussion of Wigner functions and their application in quantum statistical mechanics, as well as some recent work in the theory of non-equilibrium systems. An analysis of these systems also requires the inclusion of some other topics: scattering theory, representative ensembles, and factors influencing the derivation of a transport equation for irreversible phenomena. We begin with the description of a quantum mechanical system. In Section I we first present some definitions and then discuss scattering theory. The description of equilibrium systems is given in Section II with primary emphasis on the construction of ensembles. A basis for the discussion of non-equilibrium systems is given in Section III and the construction of ensembles are treated in some detail. In Section IV, a derivation of a transport equation for non-uniform systems (the Maxwell-Boltzmann equation) is outlined. Section V is devoted to an alternative approach to transport theory for gases and liquids (the correlation function method).

Thermodynamic study of the thorium phosphide with a mass spectrometer, J. Efimenko and K. A. Gingerich, *Proc. Symp. Thermodynamics of Nuclear Materials, Vienna, May 21-25, 1963, pp. 477-486* (International Atomic Energy Agency, Vienna, Austria, Sept. 1962).

For the thorium-phosphorous system the ion intensity variation with temperature over the range 1100°-2250°K and composition range $\text{ThP}_{1.3}$ - $\text{ThP}_{0.5}$ has been obtained for the phosphorus vapor species. No molecules containing both thorium and phosphorus have been observed in the vapor below 2245°K. With the aid of a silver calibration the ion intensities have been related to the partial pressures of the effusing phosphorus vapor species, P , P_2 , and P_4 . From these data the "apparent" molar free energies of formation have been obtained with reference to gaseous P_2 for different compositions of the solid and the dissociation energy for P_2 has been computed. The vaporization of the thorium phosphides occurs incongruently by decomposition into gaseous phosphorus and a condensed phase of lower phosphorus content. The rate of phosphorus loss from the Th_3P_4 phase appears to be diffusion controlled. There is a marked increase of thermodynamic stability with decreasing phosphorus content within the homogeneity range of the lower phosphide. The phase boundaries of the lower phosphide have been estimated to correspond to $\text{ThP}_{0.7}$ and $\text{ThP}_{0.9}$. The thermodynamic stability of the thorium phosphides is compared with that of selected lower phosphides of transition metals.

Low energy levels of neutral cerium (Ce I), W. C. Martin, *J. Opt. Soc. Am.* **53**, No. 9, 1047-1050 (Sept. 1963). The first results of a continuing analysis of the Ce I spectrum show the ground level to be $4f5d6s^2 \ ^1G_1$, with $g_J=0.945$. Of twelve other low odd levels for which the energies, J- and g-values are given, six have been assigned to $4f5d6s$ and three to $4f5d^26s$.

A study of stress relaxation with finite strain, B. Bernstein, E. A. Kearsley, and L. J. Zapas, *Trans. Soc. Rheology* **VII**, 391-410 (1963).

Two simple types of constitutive equations appropriate to materials exhibiting elasticity are presented, one of a basic solid nature and one of a basic fluid nature. The predictions of the equations for a stress relaxation experiment are worked out and compared to the data from some experiments on various elastomers. The fluid theory is shown to be most appropriate in a certain sense.

Measurement of weak magnetic fields by optical pumping methods, P. L. Bender, *Bull. Ampere* **9**, Pt. II, 261-628 (1960).

Three new types of magnetometer, the dc alkali vapor magnetometer, the self-oscillating alkali vapor magnetometer, and the helium magnetometer, all based on optical pumping, are compared. Practical limitations and performance in various environmental circumstances are considered.

Three-body bound state in He⁴, J. M. Blatt, J. N. Lyness, and S. Y. Larsen, *Phys. Rev.* **131**, No. 5, 2131-2132 (Sept. 1, 1963).

The binding energy of three He⁴ atoms, subject to pair forces, is investigated numerically for a number of proposed intermolecular potentials and for a series of square wells. For some potentials a 3-body bound state is found, for others not. However, a direct correlation is found between 2-body and 3-body binding. The need for more accurate experimental data is discussed.

Momentum autocorrelation functions and energy transport in harmonic crystals containing isotopic defects, R. J. Rubin, *Phys. Rev.* **131**, 964 (1963).

In this paper we review and extend the investigation of the effect of isotopic impurities on two statistical dynamical properties of harmonic crystals: the decay of the momentum autocorrelation function and the transport of energy. A spectral representation is obtained for the momentum autocorrelation functions. The spectral density is directly related to the normal mode frequency distribution of the crystal; the recent investigations of the classical momentum autocorrelation function in a perfect one-dimensional crystal and a one-defect crystal are discussed as special cases of this general Wiener-Khinchin formula. The corresponding quantum mechanical autocorrelation function is also treated. A formal relation involving the average momentum autocorrelation function of an isotopically disordered crystal and the frequency spectrum of the crystal is derived. The energy transport property is studied in terms of the time-dependent dispersion of the momentum of a lattice particle when the crystal is characterized initially by a spatially nonuniform temperature. The local temperature, which is related to the momentum dispersion, is studied analytically in the case of the perfect one-dimensional crystal and the one-defect one-dimensional crystal. The local temperature is studied numerically with the aid of an IBM 7090 for several isotopically disordered one-dimensional crystals.

Galvanostalometry, a new technique based on the negative pressure of liquids, for investigating electrochemical phenomena at an electrode, J. Sligh and A. Brenner, *J. Electrochem. Soc.* **110**, No. 11, 1136-1142 (Nov. 1963).

A procedure based on the negative pressure of water has been used as a sensitive indicator for the study of electrochemical phenomena. The apparatus consisted of a vertical glass tube, closed at the upper end, which was evacuated and filled with an electrolyte. The latter remained suspended in the column in a metastable state of tension. The column of electrolyte was dropped by producing a minute amount of electrolysis between an indicator electrode sealed in the top of the column and a companion electrode which could also be at the top or in the reservoir at the bottom of the column. The time or current required to drop the column was used for making the following experiments and/or observations: (A) The decomposition potential of water was determined by observing the lowest applied voltage required to drop the column. (B) The time required to drop the column (on passage of a constant current) was proportional to the concentration of iodide ion in the electrolyte. (C) The current required to drop the column was proportional to the area of the indicator electrode, regardless of the irregularity of its shape. (D) The formation of the gas required to drop the column occurred in less than 15 μsec after closing the circuit.

Electrical resistance-strain characteristics of thin evaporated metal films, R. L. Parker and A. Krinsky, *J. Appl. Phys.* **34**, No. 9, 2700-2708 (Sept. 1963).

The electrical resistance-strain coefficients of thin evaporated films of Aluminum, Gold, Cobalt, Nickel, Palladium, Platinum, Antimony, and Tellurium have been measured. The coefficients (strain-sensitivity coefficient or "gauge-factor" γ) depend on the specific resistance R_s of the films. For relatively thick films (small R_s), γ tends to approach the bulk value γ_b ; for relatively thin films (large R_s), γ may be many times greater than γ_b ; for films of intermediate thickness γ has a minimum value. The resistance change was found to be proportional to strain for all the above films except those of Ni and Sb. Some possible mechanisms

for the observed behavior are discussed; it was found that free-path effects are predominant in films of intermediate thickness, and that the tunnelling conduction mechanism plays an important role in producing the high strain-sensitivity of very thin (high R_s) films of separated particles.

Other NBS Publications

J. Res. NBS 68B (Math. and Math. Phys.), No. 1 (Jan.-Mar. 1964) 75 cents.

- A note on a generalized elliptic integral. G. H. Weiss.
An asymptotic expansion for the multivariate normal distribution and Mills' ratio. H. Ruben.
Calculation of certain multiple generating functions. G. H. Weiss.
Some infinite sums involving zeros of $J_0(x)$. L. F. Epstein.
Optimal matchings and degree-constrained subgraphs. A. J. Goldman.
Effects of a distribution on gap acceptance functions on pedestrian queues. G. H. Weiss.
Gaussian wave functions for polyatomic molecules: integral formulas. M. Krauss. (See above abstracts.)

J. Res. NBS 68C (Eng. and Instr.), No. 1 (Jan.-Mar. 1964) 75 cents.

- A Fabry-Perot spectrometer for high-resolution spectroscopy and laser work. K. D. Mielenz, R. B. Stephens, and K. F. Nefflen.
Variable impedance power meter, and adjustable reflection coefficient standard. G. F. Engen.
A laser with a multihole diaphragm. T. Morokuma.
Principles of cryometric impurity determination as applied to samples of small sizes. C. P. Saylor and G. S. Ross.
Reference tables for thermocouples of iridium-rhodium alloys versus iridium. G. F. Blackburn and F. R. Caldwell.

Radio Sci. J. Res. NBS/USNC-URSI, Vol. 68D, No. 3 (Mar. 1964). \$1.00.

- An interpretation of rapid changes in the phase of horizontally polarized VLF waves recorded at night over a short path in the southwestern United States. E. E. Gossard and M. R. Paulson.
Precise phase and amplitude measurements on VLF signals propagated through the Arctic zone. F. H. Reeder, C. J. Abom, and G. M. R. Winkler.
On the long term phase stability of the 19.8 kc/s signal transmitted from Hawaii, and received at Boulder, Colorado. A. H. Brady.
Oblique propagation of groundwaves across a coastline. Part III. J. R. Wait.
Impedance of a monopole antenna with a radial-wire ground system on an imperfectly conducting half space, Part III. S. W. Maley and R. J. King.
A simplified theory of diffraction at an interface separating two dielectrics. J. Kane and S. N. Karp. (See above abstract.)
Variational solution for the admittance of long cylindrical antenna. R. A. Hurd.
Admittance of annular slot antennas radiating into a plasma layer. J. Galejs.
Propagation of plasma waves in a "spoke-wheel" magnetic field. R. L. Liboff. (See above abstract.)
An experimental investigation of signal strength in the area around a transmitter's antipode. R. M. Pipp and J. B. Webster.
Relationship between simultaneous geomagnetic and ionospheric oscillations. H. Rishbeth and O. K. Garriott.

- Bibliography on ignition and spark-ignition systems, G. F. Blackburn, NBS Misc. Publ. 251 (Nov. 22, 1963), 15 cents. (Supersedes NBS Circular 580.)
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Lunar occultations of two discrete radio sources in 1963-1964, J. A. Eddy, NBS Tech. Note 184 (Oct. 11, 1963), 20 cents.

- Expanded vinyl fabrics for apparel use, CS 258-63 (Sept. 19, 1963), 10 cents.
Steel spirals for reinforced concrete columns, SPR 53-63, (Oct. 1, 1963), 10 cents.
Determination of differential X-ray photon flux and total beam energy, H. W. Koch and J. S. Pruitt, Ed. L. C. Yugan and C. Wu, Nuclear Physics, **5**, ch. 2.8.2, 508-553 (1963).
Metallurgical microanalysis with the electron probe, J. R. Cuthill, L. L. Wyman, and H. Yakowitz, J. Metals AIME **15**, No. 10, 763-768 (Oct. 1963).
Large longitudinal retarded elastic deformation of rubberlike network polymers. II. Application of a general formulation of nonlinear response, H. Leaderman, F. L. McCrackin, and O. Nakada, Trans. Soc. Rheology **VII**, 111-123 (1963).
The error rate in a multiple-frequency shift system and the output signal/noise ratio in a frequency modulation and a pulse-code-modulation/frequency-shift system, H. Akima, Intern. Conf. Satellite Communication, London, Nov. 22-28, 1963, pp. 305-309 (Programme and Conference Digest, London, England, 1963.)
Synoptic variations and vertical profiles of large-scale ionospheric irregularities, R. G. Merrill, R. S. Lawrence, and N. J. Roper, J. Geophys. Res. **68**, No. 19, 5453-5459 (Oct. 1, 1963).
Excitation of the red and green coronal lines, C. Pecker and R. N. Thomas, Ann. Astrophys. **25**, No. 2, 100-108 (1962).
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