

# Some Properties of Porcelains and Phase Relations in the Ternary Systems of Beryllia and Zirconia With Titania, Ceria, and Chromia

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The following physical properties were determined for some BeO-TiO<sub>2</sub>-ZrO<sub>2</sub> and BeO-CeO<sub>2</sub>-ZrO<sub>2</sub> porcelain specimens of less than 0.10 percent equivalent water absorption: Maturing range, 1,450° to 1,750° C; shrinkage, 13.9 to 18.7 percent; bulk density, 3.0 to 5.8 g/cm<sup>3</sup>; room-temperature sonic elastic properties—Young's modulus, 18.7 to 43.6×10<sup>6</sup> lb/in.<sup>2</sup>, shear modulus, 8.0 to 18.1×10<sup>6</sup> lb/in.<sup>2</sup>, Poisson's ratio, 0.17 to 0.28, and bulk modulus, 5.3 to 12.1×10<sup>6</sup> lb/in.<sup>2</sup>—for each specimen tested for transverse strength; room-temperature static strength properties—transverse, 12.0 to 23.4×10<sup>3</sup> lb/in.<sup>2</sup>, and compressive, 112 to 271×10<sup>3</sup> lb/in.<sup>2</sup>—and Young's modulus, 18.7 to 46.8×10<sup>6</sup> lb/in.<sup>2</sup>; and, at 1,800° F (982° C), static transverse strength, 9.1 to 18.1×10<sup>3</sup> lb/in.<sup>2</sup>, Young's modulus, 21.5 to 38.3×10<sup>6</sup> lb/in.<sup>2</sup>, and strain rates under various stresses. Because of the loss of chromia from the samples during preliminary heating trials, no specimens of BeO-Cr<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> mixtures were prepared for these tests. The conjecture is made that porous oxide porcelains with requisite strength properties may prove of considerable interest in the search for materials of greater thermal-shock resistance than that associated with dense, practically impervious oxide porcelains with high-strength properties.

It is proposed that the phase diagram of the BeO-TiO<sub>2</sub>-ZrO<sub>2</sub> system includes an invariant point at about 20-BeO, 35-TiO<sub>2</sub>, and 45-ZrO<sub>2</sub> (wt %) and 1,630° C; an invariant point at about 20-BeO, 55-TiO<sub>2</sub>, and 25-ZrO<sub>2</sub> (wt %) and 1,610° C; and primary crystallization fields of BeO, tetragonal ZrO<sub>2</sub> solid solution, ZrO<sub>2</sub>-TiO<sub>2</sub> solid solution, and TiO<sub>2</sub> solid solution.

The limited X-ray data indicate that the BeO-CeO<sub>2</sub>-ZrO<sub>2</sub> system is a simple one with an invariant point at approximately 40-BeO, 30-CeO<sub>2</sub>, and 30-ZrO<sub>2</sub> (wt %) and 1,845° C, and primary crystallization fields of BeO, tetragonal ZrO<sub>2</sub> solid solution, and CeO<sub>2</sub> solid solution.

Based upon extremely limited data and considerable amount of speculation, a suggested configuration of the liquidus surfaces of the BeO-Cr<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> system would be one that contains three invariant points and primary crystallization fields of BeO, tetragonal ZrO<sub>2</sub>, BeO·Cr<sub>2</sub>O<sub>3</sub>, BeO·3Cr<sub>2</sub>O<sub>3</sub>, and Cr<sub>2</sub>O<sub>3</sub>. Beryllium chromate (BeO·Cr<sub>2</sub>O<sub>3</sub>), the chromia analog of chrysoberyl, was identified; crystallographic parameters of this orthorhombic compound were tentatively determined as being  $a=10.0$  A,  $b=3.8$  A, and  $c=4.5$  A.

## 1. Introduction

Many investigations have been conducted, and many reports published, on special oxide ceramics to replace metals for high-temperature service. Although no completely acceptable ceramics have been developed for such a critical use as turbine blades, the need is so urgent that continued research is justified.

Previous work at the National Bureau of Standards [1, 2, 3, 4]<sup>2</sup> on the properties of pure oxides, singly and in combination, shows that the best ceramics for use under severe service conditions usually involve combinations of BeO and ZrO<sub>2</sub>, due in large part to the apparent thermal conductivity of beryllia and to the strength of zirconia. In order to produce impervious specimens, required to attain reproducibility of maximum strength test values, it is necessary to introduce at least a third component to beryllia-zirconia mixtures.

This report describes exploratory physical-property studies for mixtures in the systems BeO-TiO<sub>2</sub>-ZrO<sub>2</sub>, BeO-CeO<sub>2</sub>-ZrO<sub>2</sub>, and BeO-Cr<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>. In addition, a limited investigation was conducted to determine the approximate equilibrium relations that exist in these systems.

## 2. Materials, Equipment, and Procedures

Commercially available materials of high purity were used in the preparation of all specimens: *beryllia* (BeO), low-calced material of nominal 99.7 percent purity; *titania* (TiO<sub>2</sub>), TAM "Titanox A-MO", nominal titania content 98.7 percent, calcined at 1,100° C; *ceria* (CeO<sub>2</sub>), calcined material of nominal 99+ percent purity; *chromia* (Cr<sub>2</sub>O<sub>3</sub>), chemically pure reagent-grade material; and *zirconia* (ZrO<sub>2</sub>), low-calced material of nominal 99-percent purity, recalced at 1,440° C. As prepared for use, the materials were, in all instances, sufficiently finely divided to pass the No. 325 U. S. Standard Sieve.

For convenience, the test procedures employed [2, 3, 4] are given briefly. Carbon tetrachloride was used for absorption determinations, and the results were converted to equivalent water-absorption values. Matured bodies were considered to be those having less than 0.1 percent of equivalent water absorption. Shrinkage values were calculated from micrometer measurements before and after heating. Apparent density values were obtained by calculations based upon the volume as determined by a mercury volumeter and the dry weight of the specimen. A few calculated bulk density values were obtained from the dry weight of the samples by measuring the length, width, and breadth of specimens specifically prepared for transverse-strength tests. The ends

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<sup>2</sup> Figures in brackets indicate the literature references at the end of this paper.

of the 1/2-in.-diameter specimens for the compressive-strength tests were ground parallel, so that the height-to-diameter ratio was approximately 2. The test pieces were placed between graphite-oil lubricated, cold-rolled steel blocks, and the compressive stress was applied at about 31,250 lb/in.<sup>2</sup>/min by a 75,000-lb-capacity hydraulic press.

Transverse moduli of rupture and of elasticity were determined statically at room temperature and at 1,800° F (982° C), using a specially designed transverse-strength test furnace [3]. The specimens were stressed at 2-min intervals at calculated increments of 1,500 lb/in.<sup>2</sup>. When it was noted, during the 1,800° F tests, that the deflection following loading continued after the first minute, it was assumed that permanent deformation, or "plastic flow," had occurred. This deformation could be verified when the test pieces were examined for permanent curvature following rupture. In order to investigate the relative magnitude of the deformation, some bars were subjected to a short-time (1 hr) stress-strain test at 1,800° F. Beginning at 6,000-lb/in.<sup>2</sup> calculated stress, stress increments of 1,500 lb/in.<sup>2</sup> were added to the bars at hourly intervals, or until rupture occurred, during which time the deflection was measured at prescribed intervals.

This paper is believed to be the first in which the room temperature elastic properties, Young's modulus, shear modulus, Poisson's ratio, and bulk modulus, are reported for each of a series of porcelain-type specimens. The prepared transverse-test specimens and equipment recently developed [5] were used for these tests. Young's modulus values were calculated, using the flexural vibration frequencies determined along the width and depth of the bars and, in a few instances, longitudinally through the length. In most cases, the values obtained for sound bars were within one-half percent of each other and were always within 1 percent. Where internal flaws, such as cracks, were present, the variations obtained were large. Shear modulus values were calculated, using the determined torsional vibration frequencies. Poisson's ratio and the bulk modulus were calculated for each specimen by the formulas:

$$\sigma = \frac{E}{2G} - 1 \quad (1)$$

$$K = \frac{E}{3(1 + \sigma)} \quad (2)$$

where  $\sigma$  is Poisson's ratio,  $E$  is Young's modulus,  $G$  is the shear modulus, and  $K$  is the bulk modulus.

The reported phase relations for the three systems were determined mainly by interpreting X-ray diffraction patterns of the interiors of some of the maturing range and transverse-strength test specimens. Liquidus surface configurations were obtained by isothermal tests of mixtures at various temperature levels. A few melting-point and softening-range determinations were made. It was assumed that the published equilibrium relations of the various subordinate binary systems were correct. Because of the nature of the investigation, it was

not deemed advisable to determine any phase relations in anything more than an approximate manner.

Assignment of mole ratios to the various mixtures<sup>3</sup> is used solely because a compound will nearly always correspond to an integral molecular ratio. If sufficient mole-ratio mixtures are heated, the chances of missing a compound are minimized, regardless of the investigational procedure employed.

### 3. The System BeO-TiO<sub>2</sub>-ZrO<sub>2</sub>

#### 3.1. Phase Relations

##### a. The System BeO-TiO<sub>2</sub>

The equilibria were described by von Wartenberg et al. [6] as including two compounds, 3BeO·TiO<sub>2</sub> and BeO·TiO<sub>2</sub>, melting congruently at 1,800° and 1,720° C, respectively. In the work at NBS [4] no evidence was found of a compound in this system. A single eutectic exists at about 85 weight percent of TiO<sub>2</sub> and 1,670° C, and a narrow region of TiO<sub>2</sub>-BeO solid solution extends from just beyond the eutectic at about 90 weight percent of TiO<sub>2</sub> to pure TiO<sub>2</sub>. The absence of compound formation is supported by the results of a limited study at Pennsylvania State College [7], which also indicate that a solid solution may exist at high temperatures.

##### b. The System BeO-ZrO<sub>2</sub>

It was first proposed [8] that this is a simple system with one eutectic at about 2,180° C and 65 weight percent of ZrO<sub>2</sub>. The compound 3BeO·2ZrO<sub>2</sub>, melting at 2,550° C, and two eutectics were then reported [9]; but later [10], the system was shown as a simple one with the eutectic at about 75 weight percent of ZrO<sub>2</sub> and 2,240° C. Similar data, placing the eutectic at 2,210° C, were published the same year [11], and a diagram again showing the 3B·2Z compound was published in 1933 [12]. In 1937 von Wartenberg et al. [6] reported a single, sharp eutectic at about 66 mole percent of BeO and 2,200° C. Mixtures of ZrO<sub>2</sub> and BeO for use in crucibles were discussed by Ryschkewitsch [13]. In the work at NBS, Geller et al. [1] found no evidence of a compound between BeO and ZrO<sub>2</sub>.

##### c. The System TiO<sub>2</sub>-ZrO<sub>2</sub>

The melting relations were reported by von Wartenberg and Gurr [10] as indicating one eutectic at about 20 mole (27.8 wt) percent of ZrO<sub>2</sub> and 1,760° C. Vaporization was insignificant, but they reported considerable reduction of TiO<sub>2</sub>, so that the diagram obtained was not strictly that between ZrO<sub>2</sub> and TiO<sub>2</sub>. A limited study by Bussem, Schusterius, and Ungewiss [14] indicated no compound formation but some solid-solution development. They showed that 10 weight percent of zirconia at 1,460°, and 16 weight percent at 1,520° C, may dissolve in the rutile structure without change. The system was found by Sowman and Andrews [15] to be one of partial solid solutions with no inter-

<sup>3</sup> The short form of indicating the mole compositions of mixtures is used throughout the text. The code is B=BeO, Ti=TiO<sub>2</sub>, Ce=CeO<sub>2</sub>, Cr=Cr<sub>2</sub>O<sub>3</sub>, and Z=ZrO<sub>2</sub>. The short form, i. e., 1B:2Ti:3Z, then reads: 1 mole of BeO plus 2 moles of TiO<sub>2</sub> plus 3 moles of ZrO<sub>2</sub> and does not indicate a compound.



TABLE 1. *Maturing-range studies and compressive-strength results of some BeO-TiO<sub>2</sub>-ZrO<sub>2</sub> porcelains*

| Composition |                  |                  |             |                          |                          | Results of maturing-range studies <sup>a</sup> |                        |                   |                     |                                    | Properties of compressive-strength specimens <sup>b</sup> |                   |                     |                                    |                        |  |
|-------------|------------------|------------------|-------------|--------------------------|--------------------------|--|------------------------|-------------------|---------------------|------------------------------------|---|-------------------|---------------------|------------------------------------|------------------------|--|
| Molecular   |                  |                  | Weight      |                          |                          | Maturing <sup>c</sup> range                    | Properties at maturity |                   |                     |                                    | Firing temperature  | Shrinkage (±0.05) | Absorption (±0.005) | Bulk <sup>d</sup> density (±0.005) | Height; diameter ratio | Strength <sup>e</sup> at room temperature (±5,000) |
| BeO         | TiO <sub>2</sub> | ZrO <sub>2</sub> | BeO (±0.01) | TiO <sub>2</sub> (±0.01) | ZrO <sub>2</sub> (±0.01) |  | Firing temperature     | Shrinkage (±0.05) | Absorption (±0.005) | Bulk <sup>d</sup> density (±0.005) |   |                   |                     |                                    |                        |  |
|             |                  |                  | %           | %                        | %                        | ° C.   | ° C.                   | %                 | %                   | g/cm <sup>3</sup>                  | ° C.  | %                 | %                   | g/cm <sup>3</sup>                  |                        | lb/in. <sup>2</sup>                                |
| 1           | 1                | 1                | 10.97       | 35.02                    | 54.01                    | O. F. 1,550                                    | -----                  | -----             | -----               | -----                              | -----   | -----             | -----               | -----                              | -----                  | -----  |
| 1           | 2                | 1                | 8.12        | 51.88                    | 40.00                    | O. F. 1,500                                    | -----                  | -----             | -----               | -----                              | -----   | -----             | -----               | -----                              | -----                  | -----  |
| 2           | 1                | 4                | 8.03        | 12.83                    | 79.14                    | O. F. 1,550                                    | -----                  | -----             | -----               | -----                              | -----   | -----             | -----               | -----                              | -----                  | -----  |
| 4           | 1                | 1                | 33.01       | 26.35                    | 40.64                    | 1,500 to 1,550                                 | 1,550                  | 15.6              | 0.00                | 3.82                               | 1,525   | 17.5              | 0.01                | 3.87                               | 1.98                   | 203×10 <sup>3</sup>                                |
| 4           | 2                | 1                | 26.12       | 41.71                    | 32.17                    | 1,500 to 1,550                                 | 1,550                  | 16.7              | .00                 | 3.96                               | 1,525   | 18.7              | .01                 | 4.02                               | 1.97                   | 244  |
| 4           | 4                | 1                | 18.43       | 58.87                    | 22.70                    | 1,500 to 1,550                                 | 1,550                  | 16.8              | .00                 | 3.92                               | 1,550   | 18.3              | .01                 | 3.95                               | 1.95                   | 233  |
| 5           | 10               | 1                | 11.94       | 76.29                    | 11.77                    | 1,500 to 1,550                                 | 1,550                  | 16.8              | .00                 | 3.85                               | 1,550   | 18.1              | .01                 | 3.90                               | 1.97                   | 239  |
| 6           | 1                | 4                | 20.77       | 11.05                    | 68.18                    | O. F. 1,550                                    | -----                  | -----             | -----               | -----                              | -----   | -----             | -----               | -----                              | -----                  | -----  |
| 9           | 1                | 1                | 52.58       | 18.65                    | 28.77                    | 1,500 to 1,550                                 | 1,550                  | 16.3              | .01                 | 3.43                               | 1,525   | 17.8              | .00                 | 3.42                               | 2.02                   | 227  |
| 9           | 1                | 2                | 40.83       | 14.49                    | 44.68                    | O. F. 1,650                                    | -----                  | -----             | -----               | -----                              | -----   | -----             | -----               | -----                              | -----                  | -----  |
| 12          | 4                | 1                | 40.41       | 43.01                    | 16.58                    | 1,500 to 1,600                                 | 1,500                  | 17.8              | .00                 | 3.63                               | 1,525   | 21.4              | .01                 | 3.63                               | 2.05                   | 271  |
| 15          | 1                | 5                | 35.03       | 7.46                     | 57.51                    | O. F. 1,550                                    | -----                  | -----             | -----               | -----                              | -----   | -----             | -----               | -----                              | -----                  | -----  |
| 30          | 1                | 2                | 69.70       | 7.42                     | 22.88                    | O. F. 1,500                                    | -----                  | -----             | -----               | -----                              | -----   | -----             | -----               | -----                              | -----                  | -----  |
| 30          | 1                | 4                | 56.72       | 6.04                     | 37.24                    | O. F. 1,550                                    | -----                  | -----             | -----               | -----                              | -----   | -----             | -----               | -----                              | -----                  | -----  |
| 36          | 4                | 1                | 67.04       | 23.79                    | 9.17                     | 1,450 to 1,550                                 | 1,500                  | 18.7              | .00                 | 3.27                               | 1,525   | 20.4              | .01                 | 3.27                               | 1.98                   | 241  |
| 40          | 10               | 1                | 52.26       | 41.30                    | 6.44                     | 1,450 to 1,600                                 | 1,550                  | 18.3              | .00                 | 3.41                               | 1,550   | 20.5              | .01                 | 3.39                               | 1.99                   | 250  |
| 60          | 2                | 1                | 84.14       | 8.95                     | 6.91                     | 1,550 to 1,600                                 | 1,550                  | 18.1              | .00                 | 3.00                               | 1,550   | 20.0              | .01                 | 2.96                               | 1.94                   | 221  |

<sup>a</sup> All specimens for this determination were heated in an electrically heated furnace (ThO<sub>2</sub> resistor-type) for 1 hr. at the temperatures indicated.

<sup>b</sup> All specimens for this determination were heated in a gas-fired furnace for 1 hr. at the temperatures indicated.

<sup>c</sup> Maturing range is defined as that temperature interval resulting in an equivalent water-absorption value of 0.10 percent or less. "O. F. 1,500° C." indicates that a specimen had overfired at 1,500° C. and that at the next lower temperature of heating, a 50-deg-C. interval, a specimen had not reached a matured condition.

<sup>d</sup> Values calculated from the dry weight of the specimens and from the volume determined, using a mercury volumeter.

<sup>e</sup> The numerical average of three test values.

and used for the compressive-strength tests (about 1¼ in. high). Although both were made in the same manner, it should be noted that shrinkage and bulk density values obtained for the larger specimens fired in the gas-heated furnace were higher than those for the smaller specimens fired in the electrically heated furnace at the same apparent temperatures. The area of the ternary diagram (fig. 1) between the heavy dash-line and the BeO-TiO<sub>2</sub> join indicates the mixtures that could be matured to an impervious condition.

Table 2 gives the maturing data, the flexural strength, and elasticity both at room temperature and at 1,800° F (982° C) determined statically, and

Young's modulus, shear modulus, Poisson's ratio, and bulk modulus determined sonically at room temperature. It should be noted that the value of Poisson's ratio for BeO-TiO<sub>2</sub>-ZrO<sub>2</sub> porcelains ranges between 0.17 and 0.24.

When the bars for these tests were first made, it was found that those that did not contain at least 70 weight percent of BeO had cracked during the maturing treatment. Unfortunately, these cracks were all internal, and they were not found until the specimens had been ground to size for the transverse-strength tests. Another set of specimens was made, which behaved identically. When a third set of specimens was made in which 2 weight percent

TABLE 2. *Flexural strength and elasticity of some BeO-TiO<sub>2</sub>-ZrO<sub>2</sub> porcelains*

| Mole <sup>a</sup> composition | Number of specimens <sup>b</sup> | Maturing data <sup>c</sup> |            |                           |                   | Room temperature <sup>e</sup> |                     |                 |                     | Strength in bending (flexural) at — t |                     |                     |                     |                     |                     |                     |
|-------------------------------|----------------------------------|----------------------------|------------|---------------------------|-------------------|-------------------------------|---------------------|-----------------|---------------------|---------------------------------------|---------------------|---------------------|---------------------|---------------------|---------------------|---------------------|
|                               |                                  | Firing temperature         | Absorption | Bulk density <sup>d</sup> |                   | Sonic elastic properties      |                     |                 |                     | Room temperature                      |                     |                     | 1,800° F (982° C)   |                     |                     |                     |
|                               |                                  |                            |            | Calculated                | Mercury           | Young's modulus               | Shear modulus       | Poisson's ratio | Bulk modulus        | Number of specimens                   | Transverse strength | Young's modulus     | Number of specimens | Transverse strength | Young's modulus     |                     |
| 4:4:1C                        | 3                                | ° C                        | %          | g/cm <sup>3</sup>         | g/cm <sup>3</sup> | lb/in. <sup>2</sup>           | lb/in. <sup>2</sup> |                 |                     |                                       |                     |                     |                     |                     |                     |                     |
|                               |                                  | 1,550                      | 0.99       | 3.66                      | 3.68              | 18.7×10 <sup>6</sup>          | 8.0×10 <sup>6</sup> | 0.17            | 5.3×10 <sup>6</sup> | 1                                     | lb/in. <sup>2</sup> | lb/in. <sup>2</sup> | 2                   | lb/in. <sup>2</sup> | lb/in. <sup>2</sup> | lb/in. <sup>2</sup> |
| 5:10:1C                       | 1                                | 1,550                      | .80        | 3.58                      | 3.60              | 20.4                          | 8.6                 | .18             | 5.8                 |                                       |                     |                     | 1                   | 9.1                 | 23.5                |                     |
| 9:1:1                         | 6                                | 1,525                      | .01        | 3.55                      | 3.55              | 36.4                          | 14.8                | .23             | 9.9                 | 2                                     | 12.0                | 39.5                | 3                   | 15.0                | 29.0                |                     |
| 12:4:1                        | 4                                | 1,525                      | .02        | 3.51                      | 3.52              | 37.0                          | 14.9                | .24             | 9.9                 | 2                                     | 14.3                | 38.3                | 1                   | 16.5                | 31.8                |                     |
| 12:4:1                        | 4                                | 1,525                      | .01        | 3.56                      | 3.57              | 38.8                          | 15.7                | .24             | 10.4                | 1                                     | 18.1                | 36.9                | 2                   | 15.1                | 26.7                |                     |
| 36:4:1                        | 4                                | 1,500                      | .01        | 3.24                      | 3.24              | 43.6                          | 18.1                | .20             | 12.1                | 2                                     | 16.6                | 44.6                | 1                   | 16.5                | 38.3                |                     |
| 36:4:1C                       | 6                                | 1,500                      | .36        | 3.09                      | 3.11              | 40.6                          | 16.7                | .22             | 11.1                | 2                                     | 15.1                | 38.1                | 4                   | 11.5                | 30.8                |                     |
| 40:10:1                       | 2                                | 1,550                      | .01        | 3.36                      | 3.36              | 43.0                          | 17.7                | .22             | 11.8                | 1                                     | 18.9                | 41.9                | 1                   | 12.1                | 31.1                |                     |
| 60:2:1                        | 7                                | 1,550                      | .35        | 2.96                      | 2.99              | 41.2                          | 17.3                | .19             | 11.5                | 2                                     | 14.5                | 46.8                | 4                   | 10.8                | 29.2                |                     |

<sup>a</sup> The weight compositions of these molar mixtures are given in table 1. Those marked "C", i. e., 4:4:1C, indicate an admixture of 2 weight percent of CaO to the base composition.

<sup>b</sup> Because of cracking, only a limited number of specimens were obtained.

<sup>c</sup> All specimens were heated in a gas-fired furnace for 1 hr at the temperatures indicated.

<sup>d</sup> These values were calculated from the dry weight and the measured dimensions, and from the volumes determined, using a mercury volumeter.

<sup>e</sup> Young's modulus and the shear modulus were calculated by using the various flexural and the torsional vibration frequencies, respectively. Poisson's ratio and the bulk modulus were calculated from these moduli.

<sup>f</sup> These values were determined statically.



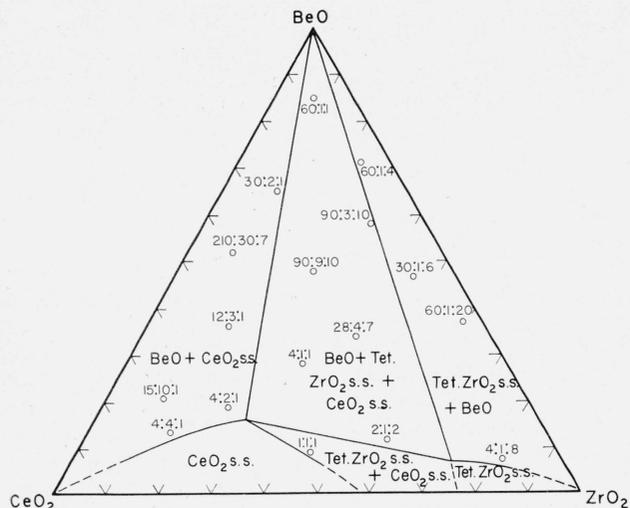


FIGURE 3. Isothermal section of the system BeO-CeO<sub>2</sub>-ZrO<sub>2</sub> at 1,750° C.

The compositions of the mixtures are indicated on the figure in molar ratios, but are placed graphically according to weight percentages. Mixture 4:1:8 indicates it to be the molecular ratio 4BeO:1CeO<sub>2</sub>:8ZrO<sub>2</sub> and is not intended to infer a compound formulation.

range tests. Each sample was sectioned so that an interior surface could be used to prepare the X-ray diffraction patterns. The data indicate that this is a system of partial solid solutions with no binary or ternary compounds. Although BeO has not been reported as forming solid solutions with either CeO<sub>2</sub> or ZrO<sub>2</sub>, it is apparent that it did enter both of the CeO-ZrO<sub>2</sub> solid solutions. For example, after being heated at 1,750° C, mixture 1B:1Ce:1Z contains no free BeO but only tetragonal ZrO<sub>2</sub> and cubic CeO<sub>2</sub> solid solutions. Similarly, mixture 4B:4Ce:1Z is

almost a single-phase cubic CeO<sub>2</sub> solid solution containing only a very small amount of free BeO. It seems likely, therefore, that BeO should form a solid solution with CeO<sub>2</sub> in the binary as well as it does in the ternary system.

For the specimens used in this study, the phases identified at room temperature were the same as those shown at the 1,750° C isothermal section, with the following exceptions: Mixtures 4B:1Ce:8Z, 30B:1Ce:6Z, 60B:1Ce:4Z, and 60B:1Ce:20Z. At room temperature, mixture 60B:1Ce:20Z is composed of monoclinic ZrO<sub>2</sub> solid solution and BeO. The effect of a larger CeO<sub>2</sub> content (as in the other three mixtures) is that BeO and both monoclinic and tetragonal ZrO<sub>2</sub> solid solutions are present. With these data and that from other investigations [12, 23, 24], showing the 1,000° C transformation of tetragonal to monoclinic ZrO<sub>2</sub> solid solution, it is likely that at 1,750° C the four mixtures contain only tetragonal ZrO<sub>2</sub> solid solution and BeO.

When ternary mixtures were heated successively at 1,750°, 1,800°, and at 1,845° C for periods of 30 min at each temperature, the only liquid formation that could be determined by visual examination at room temperature had occurred in mixture 90B:9Ce:10Z, which had been heated at 1,845° C. From the data determined for the solid-state reactions at 1,750° C, it is evident that this is a simple ternary system. If the ternary eutectic were to be located at the 90B:9Ce:10Z composition, it would violate the laws of the phase rule, assuming that the phase diagrams of the binary systems, as previously published, are correct. However, it has been shown in this investigation that a solid solution probably exists at the CeO<sub>2</sub> side of the BeO-CeO<sub>2</sub> system. If this is true, it seems reasonable to assume that the reported

TABLE 4. Maturing-range studies and compressive-strength results of some BeO-CeO<sub>2</sub>-ZrO<sub>2</sub> porcelains

| Composition |                  |                  |             |                          |                          | Results of maturing-range studies <sup>a</sup> |                        |                   |                     |                                    | Properties of compressive-strength specimens <sup>b</sup> |                   |                     |                                    |                        |                                       |                     |
|-------------|------------------|------------------|-------------|--------------------------|--------------------------|--|------------------------|-------------------|---------------------|------------------------------------|---|-------------------|---------------------|------------------------------------|------------------------|---------------------------------------|---------------------|
| Molecular   |                  |                  | Weight      |                          |                          | Maturing <sup>c</sup> range                    | Properties at maturity |                   |                     |                                    | Firing temperatures                                       | Shrinkage (±0.05) | Absorption (±0.005) | Bulk <sup>d</sup> density (±0.005) | Height: diameter ratio | Strength at room temperature (±5,000) | Number of specimens |
| BeO         | CeO <sub>2</sub> | ZrO <sub>2</sub> | BeO (±0.01) | CeO <sub>2</sub> (±0.01) | ZrO <sub>2</sub> (±0.01) |  | Firing temperature     | Shrinkage (±0.05) | Absorption (±0.005) | Bulk <sup>d</sup> density (±0.005) |   |                   |                     |                                    |                        |                                       |                     |
|             |                  |                  | %           | %                        | %                        | ° C  | ° C                    | %                 | %                   | g/cm <sup>3</sup>                  | ° C   | %                 | %                   | g/cm <sup>3</sup>                  | lb/in. <sup>2</sup>    |                                       |                     |
| 1           | 1                | 1                | 7.81        | 53.73                    | 38.46                    | O.F. 1,750                                     |                        |                   |                     |                                    | 1,750   | 14.9              | 0.36                | 5.33                               | 1.84                   | 3                                     |                     |
| 2           | 1                | 2                | 10.68       | 36.73                    | 52.59                    | O.F. 1,700                                     |                        |                   |                     |                                    | 1,750   | 12.0              | 2.6                 | 4.71                               | 1.80                   | 2                                     |                     |
| 4           | 1                | 1                | 25.31       | 43.53                    | 31.16                    | 1,600 to 1,750                                 | 1,750                  | 15.6              | 0.00                | 4.90                               | 1,750   | 16.6              | 0.06                | 4.63                               | 1.89                   | 3                                     |                     |
| 4           | 1                | 8                | 7.96        | 13.68                    | 78.36                    | 1,600 to 1,750                                 | 1,700                  | 13.9              | .01                 | 5.14                               | 1,700   | 17.1              | .06                 | 5.25                               | 1.89                   | 1                                     |                     |
| 4           | 2                | 1                | 17.63       | 60.66                    | 21.71                    | 1,600 to 1,700                                 | 1,650                  | 14.7              | .01                 | 5.37                               | 1,700   | 17.1              | .06                 | 5.25                               | 1.89                   | 1                                     |                     |
| 4           | 4                | 1                | 10.98       | 75.51                    | 13.51                    | 1,600 to 1,750                                 | 1,750                  | 14.4              | .01                 | 5.80                               | 1,750   | 18.4              | .04                 | 5.87                               | 1.83                   | 4                                     |                     |
| 12          | 3                | 1                | 31.95       | 54.94                    | 13.11                    | 1,550 to 1,750                                 | 1,700                  | 15.9              | .00                 | 4.71                               |   |                   |                     |                                    |                        |                                       |                     |
| 15          | 10               | 1                | 16.91       | 77.54                    | 5.55                     | 1,650 to 1,750                                 | 1,750                  | 14.4              | .00                 | 5.48                               |   |                   |                     |                                    |                        |                                       |                     |
| 28          | 4                | 7                | 31.11       | 30.58                    | 38.31                    | 1,550 to 1,750                                 | 1,700                  | 15.6              | .01                 | 4.53                               |   |                   |                     |                                    |                        |                                       |                     |
| 30          | 1                | 6                | 45.16       | 10.36                    | 44.48                    | 1,550 to 1,700                                 | 1,650                  | 17.2              | .00                 | 3.99                               | 1,650   | 17.7              | .07                 | 3.92                               | 2.03                   | 1                                     |                     |
| 30          | 2                | 1                | 61.62       | 28.26                    | 10.12                    | 1,550 to 1,700                                 | 1,700                  | 18.0              | .00                 | 3.67                               |   |                   |                     |                                    |                        |                                       |                     |
| 60          | 1                | 1                | 83.56       | 9.58                     | 6.86                     | 1,550 to 1,700                                 | 1,700                  | 18.1              | .00                 | 3.14                               | 1,650   | 17.9              | 1.8                 | 2.89                               | 1.88                   | 1                                     |                     |
| 60          | 1                | 4                | 69.30       | 7.95                     | 22.75                    | 1,550 to 1,700                                 | 1,700                  | 18.0              | .01                 | 3.42                               | 1,650   | 18.4              | 0.23                | 3.24                               | 1.86                   | 1                                     |                     |
| 60          | 1                | 20               | 36.28       | 4.16                     | 59.56                    | O.F. 1,700                                     |                        |                   |                     |                                    |   |                   |                     |                                    |                        |                                       |                     |
| 90          | 3                | 10               | 56.29       | 12.91                    | 30.80                    | 1,550 to 1,750                                 | 1,750                  | 17.6              | .01                 | 3.74                               |   |                   |                     |                                    |                        |                                       |                     |
| 90          | 9                | 10               | 44.74       | 30.78                    | 24.48                    | 1,550 to 1,750                                 | 1,750                  | 16.8              | .00                 | 4.13                               | 1,700   | 17.1              | .09                 | 3.85                               | 1.87                   | 1                                     |                     |
| 210         | 30               | 7                | 46.58       | 45.78                    | 7.64                     | 1,550 to 1,700                                 | 1,700                  | 16.7              | .00                 | 4.15                               |   |                   |                     |                                    |                        |                                       |                     |

<sup>a</sup> All specimens for this determination were heated in an electrically heated furnace (ThO<sub>2</sub> resistor-type) for 1 hr at the temperatures indicated.

<sup>b</sup> All specimens for this determination were heated in a gas-fired furnace for 1 hr at the temperatures indicated. At least three of each mixture were heated originally, some had cracked during heating.

<sup>c</sup> Maturing range is defined as that temperature interval resulting in an equivalent water-absorption value of 0.10 percent or less. "O.F. 1,750° C" indicates that a specimen had overfired at 1,750° C and that at the next lower firing temperature, a 50-deg-C interval, a specimen had not reached a matured condition.

<sup>d</sup> Values calculated from the dry weight of the specimens and from the volume determined, using a mercury volumeter.





When heated at 1,800° C only two mixtures, 60B:1Cr:1Z and 12B:1Cr:1Z, were found to have matured. Because of the volatilization of the chromia, it was not considered practical to attempt either further heatings at that temperature or higher temperature heatings. The time allotted to the project permitted only one attempt at reducing the maturing temperature. A series of mixtures were prepared that contained an admixture of 2 weight percent of CaO. When the first trials showed that the maturing temperatures were reduced by less than 50 deg C, and that the chromia loss remained appreciable, further work in this system was discontinued.

## 6. Discussion

The principal factors limiting the use of ceramics under stress conditions at temperatures above the useful temperature range for metals are their poor thermal-shock resistance and impact strengths. From a theoretical viewpoint, the resistance to thermal shock may be expressed in the general form

$$W \sim \frac{\sigma_t}{\alpha E} \cdot F \left( \frac{Kt}{\rho Cl^2} \right),$$

where  $\sigma_t$  is the tensile strength,  $E$  is Young's modulus,  $\alpha$  is the coefficient of linear thermal expansion,  $F$  is an unknown function,  $K$  is the thermal conductivity,  $t$  is the time at which maximum stress is developed,  $\rho$  is the density,  $C$  is the specific heat, and  $l^2$  is the dimensional area.

Considering two specimens of the same material and size, one practically impervious and one slightly porous, it can be assumed that the coefficient of linear thermal expansion, Poisson's ratio, and the specific heat will be the same for both, and that for the porous specimen the tensile strength, the thermal conductivity, and the density will be lower. A reduction in Young's modulus with increased porosity is probable for a given body, as shown by the following values for the 1BeO:1CeO<sub>2</sub>:1ZrO<sub>2</sub> mixture:

| Specimen | Absorption | Bulk density      | Young's modulus        |
|----------|------------|-------------------|------------------------|
|          | %          | g/cm <sup>3</sup> | lb./in. <sup>2</sup>   |
| 1        | 0.00       | 5.64              | 25.7 × 10 <sup>3</sup> |
| 2        | .23        | 5.49              | 23.6                   |
| 3        | 1.63       | 5.33              | 22.2                   |
| 4        | 1.83       | 5.28              | 22.5                   |

It seems reasonable to expect that the value of the function,  $F$ , will not be appreciably different for a porous specimen and for a practically impervious specimen. Therefore, the expression  $\sigma_t/\alpha E$  is the dominant consideration. The conjecture is made that porous oxide porcelains with requisite strength properties may prove of considerable interest in the search for materials of greater thermal-shock resistance than that associated with dense, practically impervious porcelains with high strength properties.

Although most of the mixtures studied in this investigation have fairly good strength properties, both at room temperature and at 1,800° F; addi-

tional work would be required if a considerable number of specimens of any one mixture are desired, all with nearly identical properties. This is illustrated by the variations shown by specimens of mixture 12B:4Ti:1Z, given in table 2, when similar samples were fired in the same furnace, at the same apparent temperature, but on different days.

## 7. Summary

### 7.1. The System BeO-TiO<sub>2</sub>-ZrO<sub>2</sub>

The configuration of the liquidus surfaces indicates the phase equilibrium relations to be those of a simple eutectic system with primary crystallization fields for BeO, tetragonal ZrO<sub>2</sub>, ZrO<sub>2</sub>·TiO<sub>2</sub>, and TiO<sub>2</sub> solid solutions. The lowest melting ternary mixture studied occurs at about mole ratio 4BeO:4TiO<sub>2</sub>:1ZrO<sub>2</sub> and 1,615° ± 10 deg. C.

Those mixtures whose compositions are within the triangular area bounded by BeO, ZrO<sub>2</sub>·TiO<sub>2</sub>, and TiO<sub>2</sub>, and which contain at least 15 to 20 weight percent of BeO, could be matured to imperviousness, but only when the sample size was small (5/8 in. in diameter by 1/2 in. high). Considerable difficulty was encountered in fabricating large, usable samples (6 in. long by 3/4 in. wide by 5/16 in. thick) probably because of the length change, parallel to the  $c$ -axis, that occurs during the crystallographic transformation of ZrO<sub>2</sub>·TiO<sub>2</sub> between 800° and 1,200° C. Some usable test specimens could be made when 2 weight percent of CaO was added to the base mixtures. The range of physical property values for the BeO-TiO<sub>2</sub>-ZrO<sub>2</sub> porcelains investigated is given in table 7.

### 7.2. The system BeO-CeO<sub>2</sub>-ZrO<sub>2</sub>

The limited data available indicates this to be a simple system with primary crystallization fields of BeO, tetragonal ZrO<sub>2</sub> solid solution, and CeO<sub>2</sub> solid solution. No liquidus surface equilibrium diagram is given because the lowest melting invariant point was not located at a composition consistent with the phase rule. The data indicate that the invariant point temperature is at least as high as 1,845° C.

All of the mixtures studied, except those few near the reported BeO-ZrO<sub>2</sub> and the CeO<sub>2</sub>-ZrO<sub>2</sub> eutectic compositions, could be matured to imperviousness, but only when a small specimen was used. Large, strength-test samples were difficult to obtain in usable form probably because of the large expansion of tetragonal zirconia and, for some samples, because of the crystallographic transformation of tetragonal zirconia to the monoclinic form during cooling. The range of physical property values for the BeO-CeO<sub>2</sub>-ZrO<sub>2</sub> porcelains investigated is given in table 7.

### 7.3. The system BeO-Cr<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>

Although the binary system BeO-Cr<sub>2</sub>O<sub>3</sub> was not studied, beryllium chromate (BeO·Cr<sub>2</sub>O<sub>3</sub>), the chromia analog of chrysoberyl, was identified in all of the ternary mixtures. The crystallographic parameters of this orthorhombic compound are tentatively given as being  $a=10.0$  Å,  $b=5.8$  Å, and  $c=4.5$  Å. The compositions studied are located within

TABLE 7. Summary and comparison of the physical properties of some BeO-TiO<sub>2</sub>-ZrO<sub>2</sub> and BeO-CeO<sub>2</sub>-ZrO<sub>2</sub> porcelains

| Physical properties               | Units               | BeO-TiO <sub>2</sub> -ZrO <sub>2</sub> porcelains | BeO-CeO <sub>2</sub> -ZrO <sub>2</sub> porcelains |
|-----------------------------------|---------------------|---|---|
| Maturing range                    | °C                  | 1,450 to 1,600                                    | 1550 to 1,750                                     |
| Matured specimens:                |                     |   |   |
| Temperature                       | °C                  | 1,500 to 1,550                                    | 1,650 to 1,750                                    |
| Shrinkage                         | %                   | 16.3 to 18.7                                      | 13.9 to 18.1                                      |
| Absorption                        | %                   | 0.00 to 0.01                                      | 0.00 to 0.01                                      |
| Density, bulk                     | g/cm <sup>3</sup>   | 3.00 to 3.96                                      | 3.14 to 5.80                                      |
| Room-temperature properties:      |                     |   |   |
| Statically tested:                |                     |   |   |
| Compressive strength              | lb/in. <sup>2</sup> | 203 to 271×10 <sup>3</sup>                        | 112 to 247×10 <sup>3</sup>                        |
| Transverse strength               | lb/in. <sup>2</sup> | 12.0 to 18.9×10 <sup>3</sup>                      | 12.0 to 23.4×10 <sup>3</sup>                      |
| Young's modulus                   | lb/in. <sup>2</sup> | 18.7 to 46.8×10 <sup>6</sup>                      | 22.4 to 38.4×10 <sup>6</sup>                      |
| Sonically tested:                 |                     |   |   |
| Young's modulus                   | lb/in. <sup>2</sup> | 18.7 to 43.6×10 <sup>6</sup>                      | 22.2 to 38.2×10 <sup>6</sup>                      |
| Shear modulus                     | lb/in. <sup>2</sup> | 8.0 to 18.1×10 <sup>6</sup>                       | 8.7 to 15.2×10 <sup>6</sup>                       |
| Poisson's ratio                   |                     | 0.17 to 0.24                                      | 0.21 to 0.28                                      |
| Bulk modulus                      | lb/in. <sup>2</sup> | 5.3 to 12.1×10 <sup>6</sup>                       | 5.8 to 10.2×10 <sup>6</sup>                       |
| 1,800° F properties:              |                     |   |   |
| Statically tested:                |                     |   |   |
| Transverse strength               | lb/in. <sup>2</sup> | 9.1 to 16.5×10 <sup>3</sup>                       | 12.0 to 18.1×10 <sup>3</sup>                      |
| Young's modulus                   | lb/in. <sup>2</sup> | 21.5 to 38.3×10 <sup>6</sup>                      | 17.9 to 28.9×10 <sup>6</sup>                      |
| Strain rates under—               |                     |   |   |
| 6,000-lb/in. <sup>2</sup> stress  | (in./in.)/min       | 1.0 to 2.8×10 <sup>-6</sup>                       | 0.8 to 1.5×10 <sup>-6</sup>                       |
| 12,000-lb/in. <sup>2</sup> stress | (in./in.)/min       | 1.2 to 3.2×10 <sup>-6</sup>                       | 0.7 to 1.2×10 <sup>-6</sup>                       |
| 15,000-lb/in. <sup>2</sup> stress | (in./in.)/min       |   | 0.7 to 1.3×10 <sup>-6</sup>                       |

the subordinate ternary system BeO-BeO·Cr<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub>.

Based upon extremely limited data and a considerable amount of speculation, it is suggested that the BeO-Cr<sub>2</sub>O<sub>3</sub>-ZrO<sub>2</sub> equilibrium diagram should contain three invariant points, each above 2,000° C, with primary crystallization fields for BeO, tetragonal ZrO<sub>2</sub>, BeO·Cr<sub>2</sub>O<sub>3</sub>, BeO·3Cr<sub>2</sub>O<sub>3</sub>, and Cr<sub>2</sub>O<sub>3</sub>.

Only two ternary mixtures attained an impervious structure when heated as high as 1,800° C for 1 hour. An admixture of 2 weight percent of lime, CaO, to some of these resulted in only a slight lowering of the maturing temperatures and no noticeable reduction of the chromia losses. Because of these appreciable chromia losses, no work was done to fabricate test specimens.

#### 7.4. General Considerations

Of possible interest to the designers of high-temperature components are the room-temperature elastic properties (Young's modulus, shear modulus, Poisson's ratio, and bulk modulus) that are presented, it is believed for the first time, for a series of porcelain-type ceramics. It should be noted that the commonly accepted value of Poisson's ratio (0.30) for oxide porcelains is considerably higher than those determined for the BeO-TiO<sub>2</sub>-ZrO<sub>2</sub> and BeO-CeO<sub>2</sub>-ZrO<sub>2</sub> porcelains.

One of the more interesting sidelights of the investigation is the suggestion that porous oxide porcelains with requisite strength properties may prove of considerable interest in the search for materials of greater thermal-shock resistance than that associated with dense, practically impervious oxide porcelains with high-strength properties.

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