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## EFFECTS OF DRYING CONDITIONS ON PROPERTIES OF TEXTILE YARNS

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#### ABSTRACT

Yarns made from raw cotton, "purified" cotton, mercerized cotton, clothing wool, carpet wool, viscose rayon, cuprammonium rayon, cellulose acetate, and degummed silk were saturated with water and then exposed for periods of ½ to 6 hours in air having temperatures of 221°, 257°, and 302° F and absolute humidities of approximately 1, 55, and 95 percent, respectively. After conditioning the dried yarns for at least 24 hours in air of 65-percent relative humidity and 70° F, measurements were made of the breaking strengths, elongations at break, and moisture contents of the yarns; the fluidities of dispersions of the cellulosic fibers in cuprammonium solution, of the silk in aqueous zinc chloride, and of the acetate in aqueous acetone; and the relative affinities of the cellulosic fibers for the dye

in aqueous acetone; and the relative affinities of the cellulosic fibers for the dye benzopurpurine 4B and of the wools for acid dyes. Heating the yarns for 6 hours at 221° F at each of the three humidities weakened all of them. The breaking strength and elongation at break of the viscose, cuprammonium, degummed silk, and cotton yarns decreased still more at higher temperatures. In comparison with heating at 1-percent absolute humidity, heating at 95-percent absolute humidity resulted in lower breaking strengths and elongations at break for all yarns except the raw cotton, higher fluidities, lower affinity of cellulosic fibers, and higher affinity of wool fibers for the dyes. Heating for ½ hour at 302° F had little effect on the properties of the yarns except the viscose and cuprammonium rayon, which were adversely affected. The damage which occurred at a given temperature and humidity increased throughout the heating period.

throughout the heating period.

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#### I. INTRODUCTION

Although it is common knowledge that textile fibers are degraded at elevated temperatures, the combined effects of heat and moisture have received little study. Therefore, particular attention was given to this subject in the course of the studies of textile drying carried out by the United States Institute for Textile Research and the National Bureau of Standards.

The materials which are dried in the various branches of the textile industry, including laundries and dry-cleaning plants, and the procedures used are so various that no one set of materials and conditions can be considered representative of all of them. By limiting the work to yarns made from the common fibers freed from the natural nonfibrous materials which would be removed from them in the course of

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manufacture, and to controlled and duplicable conditions of temperature, relative humidity, airflow, and thoroughness of exposure, it was possible to obtain data which may be considered basic to all types of textile drying. The results are given in this paper.

### **II. MATERIALS**

The characteristics of the yarns and the purification treatments they received are given below. Where treatment with water is indicated, distilled water was used.

The raw cotton yarn  $(1/24)^2$  was washed thoroughly in water. The "purified" cotton yarn was prepared from the raw cotton yarn by successive extractions with alcohol, ether, and 1-per cent NaOH solution, followed by rinsing in 5-percent acetic acid solution and then in water. The mercerized cotton yarn (2/25) was washed in a 5-percent NH4OH solution, then rinsed in water. The clothing wool yarn (2/2.3) and the carpet wool yarn (3/1.2) were extracted with alcohol and ether, and rinsed in warm water. The viscose-rayon yarn (1/30: commercial designation 150 denier, 40 filament), the cuprammoniumrayon yarn (1/30; commercial designation 150 denier, 112 filament), and the cellulose-acetate yarn (1/30; commercial designation 150 denier, 46 filament) were washed in a warm 1-percent NH4OH solution, then rinsed in warm water. The degummed silk yarn was prepared from a raw silk yarn (4/75) by degumming with an olive oil soap solution, followed by rinsing in warm water.

#### III. PROCEDURE

The equipment for this investigation is described in detail in a previous paper.<sup>3</sup> It provides means for controlling the temperature and humidity of air, for passing a stream of this air through a working chamber at a known rate, for supporting samples in this chamber so they are well exposed to the air stream, and for sampling the air in the working chamber and accurately determining its humidity by a gravimetric measurement of the moisture content. The temperature in the working chamber was maintained constant within  $\pm 1^{\circ}$  F and the humidity within  $\pm 1$  percent throughout each test. Three humidities at each temperature were studied. Hereafter, where a low, medium, and high humidity are referred to, absolute humidities of approximately 1, 55, and 95 percent, respectively, are meant. Relative humidities corresponding to these absolute humidities are also included for comparison.<sup>4</sup>

The samples for test were soaked overnight in distilled water. The following day the excess water was removed by squeezing the yarns until their weights were approximately 50 percent more than their "dry" weights (determined by heating other samples in an oven at 220° F for over 12 hours). The samples were then placed in the working chamber, which was maintained at the definite temperature

<sup>&</sup>lt;sup>2</sup> The typp system for designating sizes of yarns is employed. The first number (1 in the case of the raw cotton yarn) indicates the number of units of which the yarn is composed, that is, the ply. The second number (24 in the case of the raw cotton yarn) indicates the number of thousands of yards of the finished

number (24 in the case of the raw contain yair) instance the analysis of the point, yarn in 1 pound. 3 J. G. Wiegerink, Equipment for conditioning materials at constant humidities and at elevated temperatures, J. Research NBS 24, 639 (1940) RP1303. 4 The term "relative humidity" as used in this report is the ratio of the actual pressure of water vapor to the maximum possible pressure of water vapor in the atmosphere at the same temperature, expressed as a percentage. The term "absolute humidity" as used in this report is the actual percentage by volume of water vapor in the system.

and humidity of the test. The samples were kept in the chamber for different intervals of time ranging from  $\frac{1}{2}$  to 6 hours. All samples came to practically constant weight before removal from the working chamber and consequently contained an amount of moisture con-sistent with the relative humidity and temperature of the test. These equilibrium values at the various relative humidities and temperatures are reported in a previous paper.<sup>5</sup> It should be noted that all samples were placed in the working chamber wet, and that during evaporation of the moisture the textile was at a lower temperature than that indicated by the dry-bulb temperature in the working chamber. Thus, where a ½- to 1-hour heat treatment at a certain dry-bulb temperature is indicated, the samples, although dried to equilibrium before being taken from the working chamber, may have been at the dry-bulb temperature for less than 15 minutes during the ½-hour exposure and less than ½ hour during the 1-hour exposure.

The samples were removed from the working chamber and conditioned for at least 24 hours in an atmosphere of 65-percent relative humidity at 70° F. They were tested in this atmosphere, using a pendulum single-strand tester. The distance between the jaws of the testing machine at the start of each test was 10 inches, and the speed of separation of the jaws was 12 inches per minute. The breaking strength and elongation at break were observed.

The fluidities of dispersions in cuprammonium solution of the dried raw cotton, the purified cotton, and the viscose rayon were measured with the method described by Mease.<sup>6</sup> These dispersions contained 0.5 g of the cotton, or 2.5 g of the viscose rayon, dry basis (calculated from the moisture content determined on a duplicate sample) for 100 ml of dispersion. Measurements were made of the fluidity of the dried degummed silk in aqueous zinc chloride solution, density 1.67 at 70° F, 2.5 g of the silk, dry basis, being used for 100 ml of solvent. The weighed amount of the silk, cut into small pieces, was introduced into a small flask, and the required volume of zinc chloride solution added. The flask was then stoppered and placed in an oven at 113° F for 3 hours, with occasional swirling of the flask to ensure mixing of the contents. The solution was then cooled to 70° F, transferred to a viscosimeter, and the viscosity measured at 70° F.7

The fluidity of the dried cellulose acetate was measured in aqueous acetone, density 0.81 at  $70^{\circ}$  F, 2.5 g of the acetate, dry basis, being used for 100 ml of solvent. The weighed amount of acetate was dissolved in the required volume of acetone, and kept at  $70^{\circ}$  F overnight. In the morning the solution was transferred to a viscosimeter and the viscosity at  $70^{\circ}$  F measured. The fluidities of the original samples, not dried, were measured for comparison with the dried samples.

The moisture contents of the heat-treated yarns, after conditioning them for 24 hours or more in an atmosphere of 65-percent relative humidity and 70° F, were determined in the usual manner.

The heat-treated cellulosic yarns, namely viscose rayon, cupram-

<sup>&</sup>lt;sup>5</sup> J. G. Wiegerink, The moisture relations of textile fibers at elevated temperatures, J. Research NBS 24, 645

 <sup>&</sup>lt;sup>6</sup> J. G. Wiegerink, The moisture relations of lexitle fibers at elevated temperatures, J. Research NBS 24, 645 (1940) RP1804.
 <sup>6</sup> R. T. Messe, Measurement of the apparent fluidity of dispersions of cellulose in cuprammonium solution, J. Research NBS 22, 3 (1939) RP1179.
 <sup>7</sup> A. S. Tweedie, A study of the viscosity method for the determination of damage in silk, Can. J. Research 16B, 134-150 (1938).

monium rayon, purified cotton, and mercerized cotton, were dyed with a solution containing 0.5 percent of benzopurpurine 4B and 10 percent of NaCl, based on the weight of the yarn. The heat-treated clothing and carpet wools were dyed with a solution containing 0.3 percent of alizarine astrole B, 0.1 percent of fast light yellow 2G, 0.25 percent of neolan red 3B, 20 percent of Glauber's salt, and 5 percent of sodium bisulfate. The dyed yarns were wound on dark cardboard and their spectral reflectances relative to magnesium oxide were determined at a wavelength of 501 millimicrons. This wavelength was chosen after a study of the complete reflectance curves (400 to 740  $\lambda$ ) for typical samples.

The cystine contents of the heat-treated samples of clothing wool were determined by the Sullivan method.<sup>8</sup>

#### IV. RESULTS AND CONCLUSIONS

Tables 1 to 9 give the breaking strengths, elongations at break, and "quality indices" of the yarns, after being heated at different humidities for various periods of time and then exposed to the standard conditions of 65-percent relative humidity and 70° F for at least 24 hours. Each value is the average of 25 tests. The "quality index" is the percentage of the original breaking strength after drying, multiplied by the percentage of the original elongation after drying. It appears to be useful in analyzing the results.

Temperature (°F)	Relative humidity <sup>1</sup>	Absolute humidity <sup>1</sup>	Time of exposure	Breaking strength (as % of original)	Elonga- tion at break (as % of original)	Quality index
221	% 1	% 1	$ \begin{cases} hr \\ 1 \\ 1^{\frac{1}{2}} \\ 6 \end{cases} $	95 94 90	97 97 89	92 91 80
221	48	57	$\left\{\begin{array}{cc} 1\frac{1}{2}\\ 3\\ 6\end{array}\right.$	99 100 97	93 91 84	92 91 81
221	79	94	$\left\{\begin{array}{c}1\frac{1}{2}\\4\\6\end{array}\right.$	96 97 90	97 91 83	93 88 75
257	0. 5	1	$\left\{\begin{array}{c} 1^{\frac{1}{2}} \\ 1^{\frac{1}{2}} \\ 6 \end{array}\right.$	92 85 72	91 79 67	84 67 48
257	24	55	$\begin{cases} & \frac{34}{134} \\ & 6 \end{cases}$	96 85 72	86 72 56	82 61 40
257	42	96	$\left\{\begin{array}{c} 1^{\frac{1}{2}} \\ 1^{\frac{1}{2}} \\ 6 \end{array}\right.$	99 90 68	93 82 57	92 74 38
302	0. 2	0.5	$\left\{\begin{array}{c} 1^{\frac{1}{2}} \\ 1^{\frac{1}{2}} \\ 6 \end{array}\right.$	73 67 50	$\begin{array}{c} 61\\58\\42\end{array}$	45 39 21
302	12	56	$\left\{\begin{array}{c} 1 \\ 1 \\ 1 \\ 6 \end{array}\right.$	69 57 45	54 38 23	37 22 10
302	20	96	$\left\{\begin{array}{c} 1 \\ 1 \\ 1 \\ 6 \end{array}\right.$	83 60 43	70 50 27	58 30 11

TABLE 1.-Viscose rayon yarn

<sup>1</sup> See footnote 4 of text.

8 M. X. Sullivan, Public Health Reports 86 (1930).

Temperature (°F)	Relative humidity	Absolute humidity	Time of exposure	Breaking strength (as % of original)	Elongation at break (as % of original)	Quality index
221	% 1	% 1	$\left\{\begin{array}{c}hr\\1\\2\\6\end{array}\right.$	100 100 100	94 94 94	94 94 94
221	48	57	$\left\{\begin{array}{cc}1^{1}_{2}\\3\\6\end{array}\right.$	97 94 86	85 76 67	82 71 58
221	79	94	$\left\{\begin{array}{c} 2\\ 4\\ 6\end{array}\right.$	98 96 92	79 61 58	77 59 53
257	0.5	1	$\left\{\begin{array}{c} 1 & 1 \\ 1 & 1 \\ 1 & 1 \\ 6 & 1 \\ \end{array}\right.$	100 96 96	97 91 85	97 87 82
257	24	55	$\left\{\begin{array}{c} 34 \\ 134 \\ 6 \end{array}\right.$	97 89 77	85 70 55	82 62 42
257	42	96	$\left\{\begin{array}{cc} 1\\ 2\\ 6\end{array}\right.$	98 87 76	79 58 45	77 50 34
302	0.2	0.5	$\left\{\begin{array}{c} 1^{\frac{1}{2}} \\ 1^{\frac{1}{2}} \\ 6 \end{array}\right.$	94 93 76	79 73 55	74 68 42
302	12	56	$\left\{\begin{array}{c} 1 \\ 1 \\ 1 \\ 6 \\ \end{array}\right.$	89 79 65	73 60 36	65 47 23
302	20	96	$\left\{\begin{array}{c} 1^{\frac{1}{2}} \\ 1^{\frac{1}{2}} \\ 6 \end{array}\right.$	86 71 56	67 42 24	58 30 13

TABLE 2.—Cuprammonium rayon yarn

TABLE 3.—Clothing wool yarn

Temperature (°F)	Relative humidity	Absolute humidity	Time of exposure	Breaking strength (as % of original)	Elongation at break (as % of original)	Quality index	Cystine content (original =11.5)
	%	%	hr [ 1	102	100	102	%
221	1	1	$\left\{\begin{array}{cc} 1\\ 2\\ 6\end{array}\right $	99 95	100 93	99 88	11.3
221	48	57	$\left\{\begin{array}{cc} 1^{1} \sqrt{2} \\ 3 \\ 6 \end{array}\right.$	95 91 91	97 91 91	92 83 83	11. 2
221	79	94	$\left\{\begin{array}{cc} 2\\ 4\\ 6\end{array}\right.$	100 97 95	100 89 86	$     \begin{array}{r}       100 \\       86 \\       82     \end{array} $	9.6
257	0.5	1	$ \begin{cases} & \frac{1_2}{11_2} \\ & 6 \end{cases} $	100 91 91	100 93 93	$     \begin{array}{r}       100 \\       85 \\       85     \end{array} $	11. 3
257	24	55	$\left\{\begin{array}{cc} & \frac{3}{4} \\ & 1\frac{3}{4} \\ & 6 \end{array}\right.$	105 97 95	98 97 93	103 94 88	11.1
257	42	96	$\left\{\begin{array}{cc} 1\\ 2\\ 6\end{array}\right.$	$     \begin{array}{r}       100 \\       98 \\       94     \end{array} $	98 93 89	98 91 84	9.5
302	0. 2	0.5	$\left\{\begin{array}{cc} & \frac{1_{2}}{11_{2}} \\ & & 1\frac{1_{2}}{6} \end{array}\right.$	99 92 91	100 97 93	99 89 85	10.3
302	12	56	$\left\{\begin{array}{c} 1 \\ 1 \\ 1 \\ 6 \\ \end{array}\right.$	107 93 91	93 91 91	100 85 83	10.3
302	20	96	$\left\{\begin{array}{c} 1 \\ 1 \\ 1 \\ 6 \\ \end{array}\right.$	100 96 90	97 93 85	97 89 77	8.8

Temperature (°F)	Relative humidity	Absolute humidity	Time of exposure	Breaking strength (as % of original)	Elongation at break (as % of original)	Quality index
H	%	%	hr	92	100	92
221	1	1	$\left\{\begin{array}{cc}1\\2\\6\end{array}\right.$	87 87	95 85	83 74
221	48	57	$\left\{\begin{array}{cc} 1^{1} 1^{1} \\ 3 \\ 6 \end{array}\right.$	89 87 87	90 85 85	80 74 74
221	79	94	$\left\{\begin{array}{cc} 2\\ 4\\ 6\end{array}\right.$	78 78 78	90 85 77	70 66 60
257	0.5	1	$\left\{\begin{array}{c} 1 \\ 1 \\ 1 \\ 6 \\ \end{array}\right.$	95 91 89	100 90 85	95 82 76
257	24	55	$\left\{\begin{array}{c} & \frac{3}{4} \\ & 1\frac{3}{4} \\ & 6 \end{array}\right.$	84 81 86	85 80 85	71 65 73
257	42	96	$\left\{\begin{array}{c}1\\2\\6\end{array}\right.$	81 84 82	90 80 80	73 67 66
302	0.2	0.5	$\left\{\begin{array}{c} 1 \\ 1 \\ 1 \\ 6 \\ \end{array}\right.$	94 89 86	$     \begin{array}{r}       100 \\       90 \\       85     \end{array} $	94 80 73
302	12	56	$\left\{\begin{array}{c}1\\1\\1\\2\\6\end{array}\right\}$	87 84 81	90 90 85	78 76 69
302	20	96	$\left\{\begin{array}{c} 1 \\ 1 \\ 1 \\ 6 \\ \end{array}\right.$	89 83 81	85 75 75	76 62 61

TABLE 4.—Carpet wool yarn

TABLE 5.—"Purified" cotton yarn

Temperature (°F)	Relative humidity	Absolute humidity			Breaking strength (as % of original)	Elongation at break (as % of original)	Quality index
221	%1	%1	hr {		99 95	97 97	96 92
221	48	57	{		100 93	98 91	98 85
221	79	94	{		91 87	94 89	86 77
257	0. 5	1	{		100 92	102 93	102 86
257	24	55	{		93 85	89 87	83 74
257	42	96	{		87 78	90 81	78 63
302	0.2	0.5	{		98 94 84	95 93 82	93 87 69
302	12	56	{		92 79 68	90 80 67	8 <b>3</b> 63 46
302	20	96	{		96 82 58	100 85 69	96 70 40

Temperature (°F)	Relative humidity	Absolute humidity	Time of exposure	Breaking strength (as % of original)	Elongation at break (as % of original)	Quality index
221	% 1	% 1	$\begin{cases} hr \\ 1\frac{1}{2} \\ 6 \end{cases}$	95 94	94 93	89 87
221	48	57	$\left\{ \begin{array}{cc} 1^{1}/2 \\ 6 \end{array} \right.$	89 92	100 95	89 87
221	79	94	$\left\{ \begin{array}{cc} 1^{1}_{2} \\ 6 \end{array} \right.$	93 95	95 92	88 87
257	0.5	1	$\left\{ \begin{array}{cc} 1^{1}_{2} \\ 6 \end{array} \right.$	89 88	90 90	80 79
257	24	55	$\left\{ \begin{array}{cc} 1^{1}_{1/2} \\ 6 \end{array} \right.$	98 93	95 90	93 84
257	42	96	$\left\{ \begin{array}{cc} 11/2 \\ 6 \end{array} \right.$	90 92	90 88	81 81
302	0.2	0.5	$\left\{\begin{array}{c} 1 \\ 1 \\ 1 \\ 6 \\ \end{array}\right.$	96 94 89	90 90 84	86 85 75
302	12	56	$\left\{\begin{array}{c} 1 \\ 1 \\ 1 \\ 6 \\ \end{array}\right.$	94 91 89	90 85 80	85 77 71
302	20	96	$\left\{\begin{array}{c} 1 \\ 1 \\ 1 \\ 6 \\ \end{array}\right.$	85 89 84	90 86 83	77 77 70

TABLE 6.—Raw cotton yarn

## TABLE 7.—Mercerized cotton yarn

Temperature (°F)	Relative humidity	Absolute humidity	Time of exposure	Breaking strength (as % of original)	Elongation at break (as % of original)	Quality index
a here	%	%	hr	91	90	82
221	1	1	$\left\{\begin{array}{cc} 1\\ 2\\ 6\end{array}\right.$	91 92 108	90 95 105	82 87 113
221	48	57	$\left\{\begin{array}{cc} 1\frac{1}{2}\\ 3\\ 6\end{array}\right.$	92 98 105	95 96 97	87 94 102
221	79	94	$\left\{\begin{array}{cc} 2\\ 4\\ 6\end{array}\right.$	92 97 94	94 95 93	86 92 87
257	0.5	1	$\left\{\begin{array}{cc} 1_{2}'\\ 1_{2}''\\ 6\end{array}\right.$	96 92 99	96 94 96	92 86 95
257	24	55	$\left\{\begin{array}{c} & \frac{3}{4} \\ & 1\frac{3}{4} \\ & 6 \end{array}\right.$	$97\\ 88\\ 100$	96 90 98	93 79 98
257	42	96	$\left\{ egin{array}{c} 1 \\ 2 \\ 6 \end{array}  ight.$	87 92 88	92 90 89	80 83 78
302	0.2	0. 5	$\left\{\begin{array}{cc} & \frac{1}{2} \\ & 1\frac{1}{2} \\ & 6 \end{array}\right.$	94 90 92	93 91 95	87 82 87
302	12	56	$\left\{\begin{array}{cc} & \frac{1/2}{11/2} \\ & & 0 \\ & & 6 \end{array}\right.$	97 87 91	95 89 93	92 77 85
302	20	96	$\left\{\begin{array}{c} 1 \\ 1 \\ 1 \\ 6 \end{array}\right.$	93 88 89	90 89 89	84 78 79

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Temperature (°F)	Relative humidity	Absolute humidity	Time of exposure	Breaking strength (as % of original)	Elongation at break (as % of original)	Quality index
	%	%	hr		100	
221	1	1	$\left\{\begin{array}{cc}1\\2\\6\end{array}\right.$	96 96 96	$     \begin{array}{r}       100 \\       100 \\       100     \end{array} $	96 96 96
221	48	57	$\left\{\begin{array}{cc} 1^{1} \sqrt{2} \\ 3 \\ 6 \end{array}\right.$	100 98 93	92 88 90	92 86 84
221	79	94	$\left\{\begin{array}{cc} 2\\ 4\\ 6\end{array}\right.$	99 99 99	92 92 90	91 91 89
257	0.5	1	$\left\{\begin{array}{cc} 1_{2}'\\ 1_{2}'\\ 6'\end{array}\right.$	99 96 93	99 93 88	98 89 82
257	24	55	$\begin{cases} & \frac{3}{4} \\ & 1\frac{3}{4} \\ & 6 \end{cases}$	94 91 89	85 84 81	80 76 72
257	42	96	$\left\{ egin{array}{c} 1 \\ 2 \\ 6 \end{array}  ight\}$	100 99 89	86 84 78	86 83 69
302	0.2	0.5	$\left\{\begin{array}{c} 1^{1/2} \\ 1^{1/2} \\ 6 \end{array}\right.$	90 88 74	89 84 75	80 74 56
302	12	56	$\left\{\begin{array}{c} 1_{2} \\ 1_{2} \\ 1_{2} \\ 6 \end{array}\right.$	93 92 76	98 85 74	91 78 56
302	20	96	$\left\{\begin{array}{c} 1_{2} \\ 1_{1/2}^{1/2} \\ 6 \end{array}\right.$	96 95 76	91 89 74	87 85 56

TABLE 8.—Degummed silk yarn

## TABLE 9.—Acetate yarn

Temperature (°F)	Relative humidity	Absolute humidity	Time of exposure	Breaking strength (as % of original)	Elongation at break (as % of original)	Quality index
221	% 1	% 1	$\begin{cases} hr \\ 1 \\ 2 \\ 6 \end{cases}$	100 94 94	98 95 95	98 89 89
221	48	57	$\left\{\begin{array}{c}1\frac{1}{2}\\3\\6\end{array}\right.$	98 98 98	90 93 93	88 91 91
221	79	94	$\left\{\begin{array}{cc} 2\\ 4\\ 6\end{array}\right.$	82 83 82	84 85 84	69 70 69
257	0.5	1	$\left\{\begin{array}{cc} & \frac{1_{2}}{1} \\ & 1_{2}^{1_{2}} \\ & 6 \end{array}\right.$	99 96 95	95 91 95	94 87 90
257	24	55	$\begin{cases} & \frac{3/4}{13/4} \\ & 6 \end{cases}$	99 98 93	95 95 92	94 93 86
257	42	96	$\left\{ egin{array}{c} 1 \\ 2 \\ 6 \end{array}  ight\}$	100 99 100	87 84 86	87 83 86
302	0.2	0.5	$ \left\{ \begin{array}{c} & \frac{1_{2}}{11_{2}} \\ & 1_{2}^{1_{2}} \\ & 6 \end{array} \right. $	98 100 100	95 95 92	93 95 92
302	12	56	$\left\{\begin{array}{cc} & \frac{1_{2}}{11_{2}} \\ & 1\frac{1_{2}}{6} \end{array}\right.$	100 98 96	91 91 88	91 89 84
302	20	96	$\left\{\begin{array}{c} 1_{2} \\ 1_{1_{2}}^{1_{2}} \\ 6 \end{array}\right.$	$103 \\ 102 \\ 96$	87 85 84	90 87 81

The relationships between temperature and humidity of drying, on the one hand, and quality index, fluidity, moisture content, and affinity for dyes of the dried conditioned fibers, on the other hand, are shown in figures 1 to 4, respectively. The data are for the 6-hour treatment, the maximum time of exposure used in the experiments. The solid lines in the figures indicate the averages of the values for the different humidities at constant temperature. These lines show in a general way the effects of heat, while the departures of the points show the effects of humidity. It should be emphasized that the results and conclusions based on them apply only to the samples examined. Further work is necessary to determine what variation is to be expected in different lots of the same fiber, or when the fibers contain oils, sizing materials, and dyes.

Figure 1 shows that the quality indices of all of the yarns were adversely affected by the temperatures at which the yarns were heated. All were decreased by heating for 6 hours at 221° F, and the lowering of the quality indices for the viscose and cuprammonium rayons, the degummed silk, and the cotton yarns was greater as the temperature was increased. Heating in air of an absolute humidity of approximately 95 percent tended to give lower quality indices for all of the yarns, except the raw cotton, than heating in air of an absolute humidity of approximately 1 percent. The greatest effect of humidity was obtained with the cuprammonium rayon, whose behavior was in marked contrast to that of the viscose rayon in this respect. Indeed, the effect of the humidity of the air on the quality index of cuprammonium rayon was as great as that of the change in temperature from  $221^{\circ}$  to  $302^{\circ}$  F.

The effects of heat on the clothing and carpet wool yarns were less than the effects of humidity as measured by the quality index, the average line being nearly horizontal. This is particularly true of the carpet wool yarn, which shows the greatest degradation at the high humidity. The results also indicate that the carpet wool is less resistant to heat and humidity than the corresponding clothing wool yarn.

Figure 1 indicates that heat had a greater effect on the quality indices of the purified and the raw cotton yarns than on the wool yarns. The purified cotton yarn was less resistant to heat treatment than the raw cotton yarn. The high humidity had a more degrading effect at constant temperature on the purified cotton yarn than the low humidity, but the raw cotton yarn was scarcely affected. This difference in behavior between the raw and the purified cotton yarns may be attributed to a protective action of the natural waxes in the raw cotton, which are removed by the caustic purification. It appears from the results for the mercerized cotton and the ace-

It appears from the results for the mercerized cotton and the acetate yarns that the effect of humidity, particularly the high humidity, which had the greatest degrading effect, was relatively more important than the effect of heat. In fact, the high humidity at 221° F gave the lowest quality index for the acetate yarn. This low quality index for the acetate yarn dried at 221° F at the

This low quality index for the acetate yarn dried at 221° F at the high humidity may be explained by the data given in table 9. The breaking strength of the acetate yarn was found to decrease only when the yarn was heated at 221° F at the high humidity. At any of the other conditions studied there was no significant decrease in the breaking strength. On the other hand, there were appreciable variations in the elongation, which was lower at a high humidity at each temperature than at a low humidity. The yarns dried at the high humidity were more brittle than the yarns dried at the low

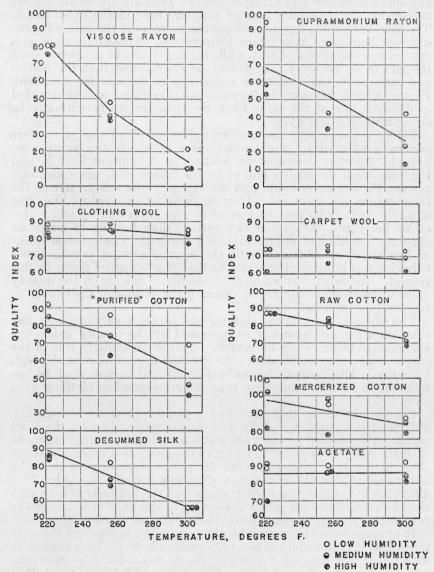


FIGURE 1.—Relationship between quality index and temperature of drying at different humidities for 6-hour time of exposure.

humidity, even after conditioning them. The fact that there was a decrease in breaking strength of the yarns heated at  $221^{\circ}$  F at the high humidity may indicate that this particular condition aids hydrolysis. The water in the acetate yarn before drying would be evaporated more slowly at  $221^{\circ}$  F at the high humidity than at any

Wiegerink]

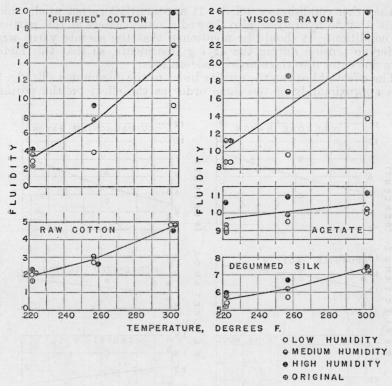


FIGURE 2.—Relationship between fluidity and temperature of drying at different humidities for 6-hour time of exposure.

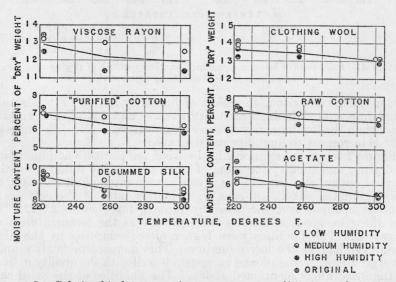


FIGURE 3.—Relationship between moisture content on conditioning and temperature of drying at different humidities for 6-hour time of exposure.

of the other conditions studied. It appears that carpet wool, which lends itself to hydrolysis, also showed a similar effect at this particular condition. It should be mentioned that the acetate yarns were under no tension during the drying treatments, so that this factor does not enter into the above considerations.

The effect of heat on the quality index of the degummed silk (fig. 1) was approximately of the same order as the effect on the purified

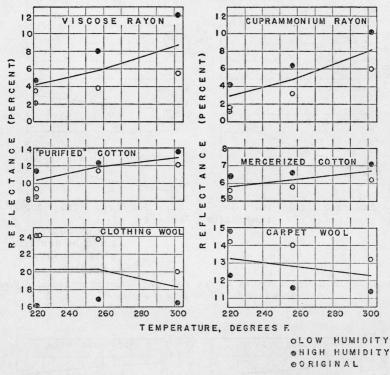


FIGURE 4.—Relationship between reflectance and temperature of drying at different humidities for 6-hour time of exposure.

cotton yarn. However, the effect of humidity at  $302^{\circ}$  F was somewhat different. The high humidity at  $221^{\circ}$  and  $257^{\circ}$  F had greater effect than the low humidity at these temperatures. No differences at  $302^{\circ}$  F in respect to humidity are indicated.

Figure 2 shows the relationships between temperature and humidity of drying, and fluidity for some of the yarns. The fluidities of the purified cotton and the viscose rayon in cuprammonium solution, of the degummed silk in aqueous zinc chloride, and of the acetate in aqueous acetone were increased by heating for 6 hours at 221° F, and these increases in fluidity were greater as the temperature was increased. The fluidities were higher after treatment at the high humidity than at the low humidity. This increase in fluidity indicates greater degradation and corresponds well with the quality indices of the dried fibers mentioned above. The fluidities of the dried raw cotton in cuprammonium solution, however, did not change with change in humidity at constant temperature, an effect which was also found to be true for the quality indices.

Although the viscose rayon gave lower values of quality index for the high humidity at a given temperature, the differences were small. However, figure 2 indicates that the effect of humidity is important. The fluidities are much higher at the high humidity than at the low humidity, which indicates that at the temperatures studied the high humidity has a greater degrading effect than a low humidity.

Figure 3 shows the effects of heat and humidity on the moisture contents of the various textile materials when conditioned in an atmosphere of 65-percent relative humidity and 70° F. These values are given for the 6-hour treatment.

Each of the dried yarns failed to regain the amount of moisture it held originally. Yarns heated at the high humidity had a lower moisture content on conditioning than those heated at the low humidity, with the exception of the acetate yarn. The moisture contents of the acetate yarns on conditioning show little effect with respect to humidity, but the effect of heat is important. For example, yarns heated at  $302^{\circ}$  F for 6 hours had a moisture content of only 5.3 percent on conditioning at 65-percent relative humidity,  $70^{\circ}$  F, as compared with the 7.3 percent moisture content of the original sample for the same conditions.

Figure 4 shows the effects of the 6-hour treatments on the affinities of the various textile materials for dyes, as measured by changes in their spectral reflectances relative to MgO. An examination of figure 4 shows that the affinity of the dried cellulosic fibers for the dye benzopurpurine 4B decreased, as indicated by the higher reflectance values. Also, the fibers heated at the high humidity for a given temperature adsorbed less of this dye than when heated at the low humidity. This is in agreement with the physical and chemical data given above.

The wool yarns, on the other hand, when degraded by heat and humidity treatments adsorbed more of the acid dyes. The wool yarns heated at the high humidity at a given temperature adsorbed more of the acid dyes than when heated at the low humidity, as indicated by the lower reflectance values. In fact, there is little difference in the reflectance at a low humidity for any of the temperatures investigated, but a high humidity even at the lowest temperature investigated, 221° F, gave low reflectance compared with the original. This difference in affinity of the dried clothing wool yarn for dyes corresponds to the difference in the cystine content (see table 3). Figure 5 shows the relationship between breaking strength and

Figure 5 shows the relationship between breaking strength and fluidity of the dried and conditioned textile materials. The curves for the viscose rayon, the purified cotton, and the degummed silk indicate linear relations between fluidity and breaking strength, provided the humidity is taken into consideration. Little relationship was found between breaking strength and fluidity for the raw cotton. The changes in breaking strength and fluidity are small compared with those of the viscose-rayon and the purified-cotton yarns. The sharp break upward in the curve for the raw cotton yarn does indicate that the fluidity is more sensitive to changes in the fiber than the breaking strength of the yarn.

The acetate yarn is peculiar in that no relationship was found between breaking strength and fluidity. However, elongation plotted

against the corresponding fluidity gave an approximate linear relationship. This indicates that breaking strength is the least sensitive of the criteria used for judging degradation in the acetate yarn.

Figure 6 shows a definite relationship between the reflectance and the chemical and physical properties. The reflectances of the purified cotton and the viscose-rayon yarns change more rapidly than the fluidities in the first stages of apparent degradation. This may indi-

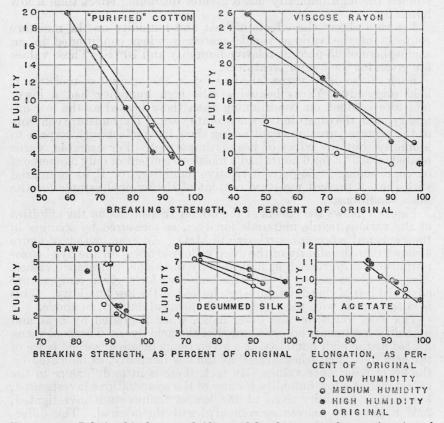


FIGURE 5.—Relationship between fluidity and breaking strength as a function of humidity.

cate merely that the dye test measures surface changes in the yarns, and that the fluidity measures mainly chemical changes.

The time of heating the yarns is also important. The conclusions mentioned above were drawn on the basis of the data for the 6-hour treatment. The tables give the results for short intervals of time as well as for the 6-hour period. An examination of tables 1 to 9 shows that for the shorter periods studied, ½, ¾, and 1 hour, most of the materials underwent very little decrease in breaking strength. A slightly greater effect on elongation at break is indicated. Several exceptions, however, are noted. There was some lowering in breaking strength and elongation at break of the carpet wool and acetate yarns when heated for a 2-hour period at 221° F at the high humidity. The viscose- and cuprammonium-rayon yarns, which were the least resistant to heat of all the materials studied, showed a decrease in breaking strength and elongation if heated for only  $\frac{1}{2}$  hour at 302° F. The purified cotton yarn showed a small decrease in quality index on heating for  $\frac{1}{2}$  hour at 302° F.

There was an increase in fluidity of the viscose-rayon yarn after heating it for a short period at 257° F at the high humidity, and for

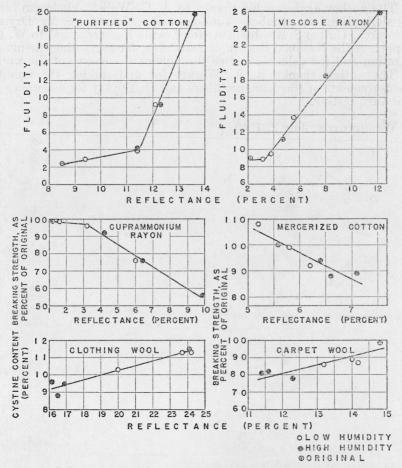


FIGURE 6.—Relationship between reflectance and the physical and chemical data as a function of humidity.

a short period at  $302^{\circ}$  F at all three humidities. The fluidity of the purified cotton yarn was approximately 4.0 rhes after  $\frac{1}{2}$ -hour treatment at  $302^{\circ}$  F at all humidities, 9.1 rhes after  $\frac{1}{2}$  hour at  $302^{\circ}$  F at the high humidity, as compared with the original sample with a fluidity of 2.4 rhes.

There was an increase in reflectance of dyeings of the viscose rayon, cuprammonium rayon, and purified cotton heated for only short periods of time, indicating a decrease in affinity for the dye. For example, dyeings were prepared after heating the yarns at  $302^{\circ}$  F for  $1\frac{1}{2}$  hours at the low humidity and at the high humidity. The

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reflectances of the untreated yarns, yarns heated at the low humidity, and yarns heated at the high humidity, respectively, were: viscose rayon, 2.1, 4.4, and 5.7 percent; cuprammonium rayon, 1.2, 1.7, and 4.3 percent; purified cotton, 8.5, 10.8, and 10.7 percent.

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