STANDARD SOLAR WAVE LENGTHS (3592–7148A)

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ABSTRACT

In order to determine a series of solar wave lengths in the international system to serve as standards for a new table of solar wave lengths and to find the exact corrections which should be applied to Rowland's classical table of solar spectrum wave lengths, the Bureau of Standards and the Allegheny Observatory cooperated in measuring the wave lengths corresponding to selected dark (Fraunhofer) lines in the solar spectrum. The wave lengths were compared with those of standard neon lines by the Fabry and Perot étalon-interferometer method, both spectra being photographed simultaneously. More than 11,000 observations were made on 729 solar lines in the wave-length interval (octave) from 3592.027A in the ultra-violet to 7148.159A in the red. The majority of these standard solar wave lengths have individual probable errors smaller than 1 part in 4,500,000.

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I. INTRODUCTION

The classical spectroscopic investigations of Professor Rowland culminating in his Preliminary Table of Solar Spectrum Wave Lengths,¹ formed the foundation of the so-called Rowland scale of wave lengths which has been in more or less universal use for the past 35 years. Beginning with the best available value of the wave lengths corresponding to the sodium yellow lines,² the relative wave lengths of a selected list of solar absorption lines ³ were determined by the method of overlapping spectra from diffraction gratings.

Early in the present century it was recognized that Rowland's standards were too large by approximately 1 part in 30,000, and relative errors of the order of 1 part in 100,000 were detected in different spectral regions. The International Union for Cooperation in Solar Research,⁴ later replaced by the International Astronomical

¹ Rowland, Preliminary Table of Solar Spectrum Wave Lengths, The Univ. of Chicago Press; 1896.

² Rowland, Phil. Mag. (5), 23, p. 257; 1887 and 27, p. 479; 1889.

³ Rowland, Phil. Mag. (5), 36, p. 49; 1893.

⁴ International Union for Cooperation in Solar Research, Trans. I, p. 230; 1906; II, pp. 109-174; 1908; III, p. 139; 1911; IV, p. 59; 1914.

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Union,⁵ has dealt with the situation since 1905, and as a result of recommendations a new set of standard wave lengths has been determined and adopted to form the basis of the so-called international scale. This international system consists (1) of a primary standard—viz, the wave length of cadmium red radiation which had previously been compared with the meter, and (2) several hundred secondary standards (3370-6750A) derived from the emission spectrum of the iron arc. These secondary standards were measured relative to the primary standard by means of the Fabry and Perot⁶ étalon-interferometer method. Certain neon lines which have been compared with cadmium by the same method have also been adopted as secondary standards.

This international system has gradually been displacing the older Rowland system, but there has been a tendency, especially in astrophysics, to retain the latter. The solar spectrum tables of Rowland are an almost inexhaustible mine of astrophysical study, but they could not be translated to the international scale without accurately determined corrections. On the other hand, the use of two different systems of standards caused considerable confusion in spectroscopy, and the only remedy for this double standard appeared to lie in a redetermination of solar spectrum wave lengths on the international scale. In 1922 the International Astronomical Union expressed itself as follows:⁷

It is believed that the time has arrived for the determination of a series of solar wave lengths in the international system to serve as standards for a new table of solar wave lengths. It is recommended, therefore, that efforts be made to obtain at least three independent determinations of the wave lengths of a selected list of solar lines.

In 1923 the spectroscopy section of this bureau united with the Allegheny Observatory in a cooperative program of solar wavelength determinations, and results for one octave of the spectrum (3592-7148A) were completed in 1927. These results were obtained in four overlapping spectral intervals. They were published in three installments according as the work in different spectral regions reached completion.⁸ In order that these results may be presented as a unified whole, they are republished here with the wave lengths (Table 1) in consecutive order and mean values replacing those reported twice in the slightly overlapping regions covered by the first publications. Similarly, the corrections to Rowland's wave

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⁵ International Astronomical Union, Trans. I, p. 35; 1922; II, p. 40; 1925.

⁶ Fabry and Perot, Ann de Chim, et de Phys., 25, p. 98; 1902; Astrophys. J., 15, pp. 73 and 261; 1902. ⁷ I. A. U. Transactions I, p. 36; 1922.

⁸ Burns and Meggers, Standard solar wave lengths (4073-4754A), Pub. Allegheny Observatory, 6, No. 7; 1925. Burns and Kiess, Standard solar wave lengths (5805-7142A), Pub. Allegheny Observatory, 6, No. 8; 1927. Burns, Standard solar wave lengths (3592-4107A and 4761-5892A) Pub. Allegheny Observatory, 6, No. 9; 1927.

lengths, previously reported in four sections, are now collected in one table (Table 2). A large number of additional "sun-arc" observations are included in Table 1, but the discussion of these is reserved for another paper. The main purpose of the one in hand is to present in complete and final form our observations on standard solar wave lengths. Only the essential facts relating to the method of observing, the description of the apparatus, and of the comparison sources will be given here. Further details may be found in the earlier publications.

II. METHOD OF OBSERVING

The method of observing is essentially that devised and first used by Fabry and Perot⁹ in 1902 for the measurement of 33 solar wave lengths (4643-6471A). It involves the use of a Fabry and Perot étalon interferometer combined with a prismatic or grating dispersing system, so that the orders of interference at various points in the spectrum may be compared. The method has become more or less familiar on account of its repeated use for the establishment of the international system of secondary standards in the emission spectrum of the iron arc. In the case of an absorption spectrum like that of the sun interference patterns similar to those produced by bright lines are obtained for dark (Fraunhofer) lines by a choice of order of interference and slit width such that a practical disappearance of the channeled spectrum from the continuous background is accomplished and interference fringes appear on the dark lines. The theory of interferences produced by the dark lines of the solar spectrum was discussed in some detail by Fabry and Buisson¹⁰ in 1910, but no further measurements of solar wave lengths were published until ours Similar observations have recently been made by this appeared. method at the Mount Wilson Observatory, and a portion of the results have been published.¹¹

In order that solar spectrum standards may be placed on the same footing as the international secondary standards, they must be compared with the primary standard or its equivalent. Recognizing certain advantages of neon lines for such comparisons the International Astronomical Union ¹² considers the mean of eight or more well-determined neon wave lengths as practically equivalent to the primary standard. Our method of observing was arranged so that the solar spectrum and neon comparison spectrum could be recorded simultaneously. This procedure eliminates, or reduces to a minimum, the small uncontrollable disturbances which otherwise are likely to introduce systematic errors in precise comparisons of wave lengths.

⁹ Fabry and Perot, see reference No. 6.

¹⁰ Fabry and Buisson, J. de Phys., 9, p. 197; 1910.

¹¹ Babcock, Astrophys. J., 65, p. 140, 1927.

¹² I. A. U. Transactions II, p. 47; 1925.

III. DESCRIPTION OF APPARATUS

All of the spectrograms were made at the Allegheny Observatory where the coelostat and spectrograph described by Schlesinger ¹³ were employed, but the location and mounting of the latter instrument was changed. The former vertical mounting of the spectrograph proved to be too unstable for the rather long exposures required in this work. The instrument was, therefore, mounted horizontally on concrete piers in the basement of the observatory, where ideal stability and freedom from temperature changes were obtained. A coelostat mirror reflected the sunlight down the polar axis to another mirror which sent the light into the solar telescope and interferometer. The optical arrangement from this point onward is shown diagrammatically in Figure 1. After leaving the second coelostat mirror, the beam of sunlight passed through a color filter which was placed immediately in front of the solar lens. This filter reduced the heating effect of the sun in the interferometer, and at the same time removed the part of the solar spectrum corresponding to the neon comparison source, so that the spectrum of the latter could be simultaneously recorded in an auxiliary spectrograph camera. In the interval 5,800-6,500A the two spectra were photographed superposed, higher orders than the second being removed by a yellow-glass filter.

A telescope of 40 cm focal length forms an image of the sun in the interferometer, which is of the Fabry-Perot type. A diaphragm 6 mm in diameter near the first plate of the interferometer restricts the beam of the comparison spectrum to the size of the solar image. The sunlight from the telescope passes through a diagonal mirror, which serves to reflect the light of the laterally situated neon comparison lamp into the path of the solar beam. From this point on the solar and comparison beams follow identical paths until the grating separates them into spectra. For observing the photographic region of the solar spectrum this diagonal mirror is lightly silvered, reflecting rather more light than it transmits. For the longer solar wave lengths a thinner coat of silver is used, and for the region longer than 6600A a clear-glass mirror has been used for some of the observations.

The interferometer is so mounted on a stand as to permit the necessary adjustments or to allow it to be lowered out of the path of the light so that the centering of the solar image and the comparison source on the grating may be more readily effected. The interferometer is turned 90°, in order to adjust the parallelism of the plates by means of a mercury lamp. The interferometer plates are thinly coated with silver, deposited cathodically. Some 10 to 15 images of a 40-watt lamp can be seen through a pair of plates. While a thicker

¹³ Schlesinger, Pub. Allegheny Obs., 3, p. 99; 1914.

coat would give slightly better interference, the increase in exposure time necessitated by the use of dense films more than offsets the slight gain in resolving power. The separators, or étalons, are made of invar.

A telescope of 25 cm focal length projects the ring system upon the slit of the spectrograph. The objective, of quartz and fluorite, is achromatic for the whole region of the solar spectrum observable at Allegheny Observatory. The interferometer is set at such a distance from this objective that the image of the diaphragm, 6 mm in diameter, is slightly smaller than the grating.

A gauge plate, or repère, having five fine parallel slots extending at right angles to the slit, is mounted on ways which allow it to slide almost in contact with the latter. Before the interferometer is placed in position this repère plate is slid in front of the slit. The intersections of the slit and the slots in this plate give five point-sources



FIG. 1.—Diagram of interferometer and grating spectrograph for observing solar wave lengths

of light whose images are photographed in both the solar and comparison spectra. This furnishes a means of making sure that the same scale is used in computing the ring diameters in solar and comparison spectra, a matter of considerable importance when the two spectra differ greatly in wave length, but of little consequence when both spectra are of nearly the same wave length.

The collimator and camera lenses of the spectroscope are of 19 cm aperture and 520 cm focal length. Since parallel light falls upon the grating and the rulings are only 10 cm long, only the central 10 cm of each lens is useful in connection with the interferometer. The lenses are corrected for the photographic region, having minimum focal length at 4500A, at which point in the spectrum the plate is perpendicular to the axis of the camera. The grating, by Michelson, is ruled with 500 lines per millimeter, giving a linear scale of 3.65A per mm in the first order.

To photograph the comparison spectrum, an auxiliary camera has been installed as shown in Figure 1. The lens of this camera is of 10 cm aperture and 160 cm focal length. The field is good over an angle of 5° , which is more than is required to photograph the neon spectrum in the region 5852 to 6598A. Since the solar camera is fixed with respect to the collimator, it is necessary to move the auxiliary camera as the various regions of the spectrum are brought into the solar camera. This comparison camera is arranged to rotate around an axis passing through the center of the grating; consequently the focus for the neon spectrum remains constant as the camera is rotated. For the region shorter than 6600A the comparison spectrum is observed in the first order on the side of zero opposite from that on which the solar spectrum is photographed. For the longer region it is preferable to observe the comparison and solar spectra in the first and second orders, respectively, on the same side of zero.

The greater portion of the observing has been done with the grating adjusted to photograph the solar spectrum in the second order, giving a scale of 1.82A per mm. Because of a slight astigmatism that increases with the order, the third order is less satisfactory than the second for interference purposes, and it has been used for only 10 plates. The first order gives very sharp definition of the interference rings, but the greater scale of the second order diminishes the disturbance of the solar lines by their weak neighbors. The first order was used, however, for a few of the plates from which the A. O. B. S. wave lengths were determined.

The photographic plates were either Seed 23 or Eastman 33, excepting that a few exposures in the violet were made on process plates. For use in the green and red the plates were sensitized by means of pinaverdol or pinacyanol. The exposure times varied from a few minutes to over two hours, depending on the condition of the sky, the state of the various silver coats, and the slit width.

Spectrograms were made in each portion of the solar spectrum with a variety of étalons and with two or more sets of interferometer plates. The various étalons were made of invar and had lengths of 3.75, 5, 6, 7.5, 8, 10, 12, 15, and 20 mm.

IV. COMPARISON SOURCES

The wave lengths of Table 1 were derived by simultaneous comparison with the red lines of neon, as already stated. The neon source was a lamp of the type described by Nutting.¹⁴ Its electrodes are aluminum disks 25 mm in diameter; the capillary is 10 cm long and has a bore of 2.5 mm. An exciting current of about 50 m. a. was delivered by 5,000 v. a. c. without capacity. The tube was observed exactly side on. The particular tube used in this investigation had been used previously in a comparison of neon wave lengths with the primary cadmium standard.

¹⁴ Nutting, Bull. Bureau of Standards, 4, p. 511; 1908.

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The maximum pressure in the solar reversing layer where the Fraunhofer lines originate has been demonstrated to be so low that for spectroscopic purposes it may be regarded comparable with laboratory vacuum sources. For comparison of solar with terrestrial wave lengths we have employed the very convenient type of vacuum arc designed and built by Curtis.¹⁵ Using currents of 6 amp. or less, this arc operates without a cooling system and is in other respects so simple to manipulate that it would seem that this or a similar type of source should become a standard piece of laboratory equipment wherever wave lengths of a high order of accuracy are being deter-This arc was used as the source for all the sun-arc comparimined. sons listed in Table 1. It was usually operated at pressures corresponding to 1 to 6 cm of mercury. All the vacuum arc wave lengths were derived from the neon standards by simultaneous comparison exactly in the same manner as the solar wave lengths.

V. MEASUREMENT AND REDUCTION

The diameters of two or, more often, three innermost fringes were measured for each of the wave lengths on a number of spectrograms ranging from 2 to 33. In addition to the solar and neon spectra, each plate had on it the images of the slots in the repére plate at the slit, measurement of which furnished the scale factor used in the reductions.

The method of reduction employed by Buisson and Fabry ¹⁶ was followed for about half of the plates, the remainder being reduced by the method described by Childs.¹⁷ In the former method the fractional order of interference at the center of the interference pattern is derived from measurements of the repère images and ring diameters, while in the latter it is deduced from ring diameters alone when three or more are available. Practically the same results are obtained from both methods, but the latter has the advantage of involving considerably less labor.

The order of interference was invariably obtained with the aid of the neon interferences,¹⁸ and the thickness of the interferometer, or double separation of the plates, was computed from each of six or more neon lines, the mean optical distance thus found being used to derive the solar wave lengths from their measured orders of interference. The values used for the neon lines were those compared with the primary cadmium standard; ¹⁹ their mean value is regarded as practically equivalent to the primary standard itself.

Corrections for dispersion of phase upon reflection in the interferometer surfaces were made by the well-known device of comparing

¹⁵ Curtis, J. Opt. Soc. Am., 8, p. 697; 1924.

¹⁶ Buisson and Fabry, J. de Phys., 7, p. 169; 1908, Astrophys. J., 28, p. 169; 1908.

¹⁷ Childs, J. Sci. Inst., 3, pp. 97 and 129; 1926.

¹⁸ Meggers, Bull. Bureau of Standards, 12, p. 203; 1915.

¹⁹ Burns, Meggers, and Merrill, Bull. Bureau of Standards, 14, p. 765; 1918. I. A. U. Trans. I., p. 40, 1922. II, p. 44, 1925.

wave lengths first with low orders of interference and then with high values in which the differential phase change plays a proportionately smaller part.²⁰ For this purpose wave lengths of the iron arc in vacuo were compared with neon standards by means of interferometers of 3.75, 6, 10, and 20 mm separation.

Observations made under conditions of temperature and pressure of air which deviated from normal were corrected to their values at 15° C. and 760 mm Hg by the tables of Meggers and Peters.²¹

The proper corrections for motion of the earth relative to the sun were made for each spectrogram.

VI. RESULTS

The first column of Table 1 contains the wave lengths of solar lines compared with red neon standards by means of simultaneous exposures as described above. The second column indicates the probable error of measurement. These probable errors are expressed in parts per million; thus "A" denotes a probable error of 1 part in 6,000,000; "B," 1 part in 4,500,000; "C," 1 part in 3,000,000; and "D" probable errors greater than 1 part 3,000,000. The number of independent comparisons of each line with the neon standards is indicated in column 3. The fourth, fifth, and sixth columns contain Rowland's wave length, chemical identification, and intensity for each line. An "s" attached to Rowland's wave length means that it was one of his standards. Column 7 shows the wave-length difference between Rowland and A. O. B. S. for the individual lines. and the next column gives the value of this difference interpolated from Table 2. In the ninth column are shown the differences between the wave lengths in the solar spectrum and the laboratory vacuum-arc values for the same lines, the unit being 0.001A. The final column gives the temperature class according to King and the pressure class to which the line belongs. The A. O. B. S. wavelength values are for air at 15° C. and 760 mm Hg pressure, while those of Rowland apply to air at 20° C. and normal pressure. In both cases the source was integrated solar light.

In Table 2 are listed the corrections which must be applied to Rowland's wave lengths to reduce them to the international scale. These are taken from a smooth curve drawn through the plotted values of column 7 in Table 1. The differences, Rowland minus A. O. B. S., run smoothly for the most part, but there are several marked discontinuities, notably at 4142A, at 5220A, and at 6870A. The smaller irregularity near 5800A may not be real, as the observations between 5740 and 5850A are of slightly inferior quality.

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²⁰ Meggers, Bull. Bureau of Standards, 12, p. 199; 1915.

²¹ Meggers and Peters, Bull. Bureau of Standards, 14, p. 724; 1918.

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A most encouraging feature of this comparison is an entire lack of an intensity equation. The values of the differences, Rowland minus A. O. B. S., are quite independent of the intensity of the solar line. After applying the interpolated corrections to Rowland's values, the mean of the residuals, Rowland minus A. O. B. S., is only ± 0.0015 A.

TABLE 1.—A. O. B. S. solar wave lengths

[3592-7148A]

A.O.B.S.λ	Proba- ble error	No.		Rowland		Correction to Rowland		Sun-arc	Tempera- ture and	
	error	ODS.	λ	Iden.	Int.	Obs.	Mean		classes	
$\begin{array}{c} 3592.\ 027\\ 3600.\ 736\\ 15.\ 661\\ 35.\ 470\\ 50.\ 539 \end{array}$	000000000000000000000000000000000000000	3 3 3 3 3 3 3	. 169 . 880 . 802 . 608 s . 681	V? V Fe Ti, Fe	$\begin{array}{c}2\\3\\3\\4\\2\end{array}$	$142 \\ 144 \\ 141 \\ 138 \\ 142$	141 141 141 141 141 141		VE	
$\begin{array}{c} 61.\ 366\\ 72.\ 712\\ 81.\ 648\\ 3695.\ 056\\ 3710.\ 291 \end{array}$	C C B B A	6 6 8 6 10	. 506 . 851 . 787 . 194 s . 431	Fe Fe Fe Fe Y	80 80 80 80	$ \begin{array}{r} 140 \\ 139 \\ 139 \\ 138 \\ 140 \end{array} $	$ \begin{array}{r} 140 \\ 140 \\ 140 \\ 140 \\ 140 \\ 140 \end{array} $	+6	IV IV IV	
$\begin{array}{c} 25.\ 495\\ 41.\ 064\\ 52.\ 419\\ 60.\ 537\\ 69.\ 993 \end{array}$	A A A A A	$ \begin{array}{c} 10 \\ 10 \\ 7 \\ 10 \\ 9 \end{array} $. 638 . 205 . 556 . 679 0. 132 s	Ti Fe Fe Fe	3 4 3 4 4	$ \begin{array}{c c} 143 \\ 141 \\ 137 \\ 142 \\ 139 \\ \end{array} $	$140 \\ 100 \\ 100 $	+5 +6	I III IV	
$\begin{array}{c} 81.\ 190\\ 3793.\ 877\\ 3802.\ 285\\ 04.\ 014\\ 21.\ 187\end{array}$	A A B A A	10 10 10 9 9	. 330 s 4. 016 s . 424 . 151 s . 328 s	Fe Fe Fe Fe Fe	3 2 2 3 4	$ \begin{array}{r} 140 \\ 139 \\ 139 \\ 137 \\ 141 \end{array} $	$ 140 \\ 140 \\ 140 \\ 140 \\ 140 \\ 140 $		IV IV IV	
$\begin{array}{c} 36.\ 090\\ 43.\ 264\\ 59.\ 219\\ 64.\ 302\\ 73.\ 764 \end{array}$	A B C B B	10 9 8 8 8	. 229 s . 404 s . 355 . 438 s . 903	Fe Fe C Fe	2 4 3 3 4	$ \begin{array}{r} 139 \\ 139 \\ 136 \\ 136 \\ 139 \\ 139 \end{array} $	$ 140 \\ 140 \\ 140 \\ 140 \\ 140 \\ 140 $	+7 +3	IV III IV	
$\begin{array}{r} 85.\ 516\\ 3897.\ 458\\ 3906.\ 751\\ 16.\ 736\\ 37.\ 336\end{array}$	A A A A A	14 14 17 18 9	. 657 . 596 s . 890 . 879 s . 479 s	Fe Fe Fe Fe	4 2 4 5 3	$141 \\ 138 \\ 139 \\ 141 \\ 143$	$140 \\ 140 \\ 140 \\ 140 \\ 140 \\ 140$	+2 +5 +8	III b IV b IV b	
49. 958 53. 859 58. 739 60. 283 63. 690	A A B A A	18 19 6 17 14	0. 102 s 4. 002 s .877 .422 s .831	Fe Fe Fe Cr	5 3 1 4 3	$ \begin{array}{r} 144 \\ 143 \\ 138 \\ 139 \\ 141 \end{array} $	$141 \\ 142 \\ 142 \\ 142 \\ 142 \\ 143$	+5	III b	
$\begin{array}{c} 76.\ 866\\ 77.\ 747\\ 78.\ 658\\ 81.\ 770\\ 87.\ 609 \end{array}$	B C A A A	8 16 9 11 9	7.009 .891 .809 .917 .755	Fe Fe Co, Cr Ti Ti?	$2 \\ 6 \\ 3 \\ 4 \\ 2$	$ 143 \\ 144 \\ 151 \\ 147 \\ 146 $	$145 \\ 145 \\ 145 \\ 146 \\ 147$	+6 +9	III b4 II	
$\begin{array}{c} 91.\ 120\\ 3993.\ 099\\ 4000.\ 253\\ 00.\ 460\\ 03.\ 768\end{array}$	A A C C A	$ \begin{array}{c} 13 \\ 8 \\ 5 \\ 6 \\ 11 \end{array} $. 333 . 246 . 403 . 611 . 912 s	Cr, Zn Fe Fe Co, Fe, Ti	3 2 2 2 3	$ 147 \\ 150 \\ 151 \\ 144 $	$147 \\ 148 \\ 149 \\ 149 \\ 150$	±0	b	
$\begin{array}{c} 10.\ 174\\ 11.\ 713\\ 16.\ 421\\ 22.\ 736\\ 29.\ 639 \end{array}$	C B A A A	5 8 11 8 10	.327 .865 .574 .893 .796	Fe Fe Fe Fe, Zn	$\begin{array}{c}1\\2\\2\\2\\5\end{array}$	$ 153 \\ 152 \\ 153 \\ 156 \\ 157 $	$151 \\ 151 \\ 151 \\ 152 \\ 154$			
$\begin{array}{c} 4030.187\\ 31.962\\ 37.119\\ 47.306\\ 49.327 \end{array}$	A A B A B	$ \begin{array}{c} 12 \\ 6 \\ 5 \\ 7 \\ 7 \\ 7 \end{array} $	$\begin{array}{r} .339\\ 2.117\\ .268\\ .461\\ .482\end{array}$	Fe Fe Fe	2 2 2 2 2	$152 \\ 155 \\ 149 \\ 155 $	$154 \\ 154 \\ 154 \\ 155 $	-1		

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A .Ο.Β.S.λ	Proba-	No.		Rowland		Correc Row	etion to vland	Gun and	Tempera- ture and
A. U. D. S. A	error	obs.	λ	Iden.	Int.	Obs.	Mean	Sun-are	pressure classes
4050. 675 53. 824 59. 718 62. 446 66. 585	A A A A A		.830 .981 .872 .599 s .742	Fe Fe, Ti Fe Fe Fe	2 3 2 5 2	$155 \\ 157 \\ 154 \\ 153 \\ 157$	$ 155 \\ 155 \\ 155 \\ 155 \\ 155 \\ 155 $	+6	шь
73. 766 79. 841 80. 879 82. 941 84. 499	A A A A A	$31 \\ 41 \\ 35 \\ 25 \\ 25 \\ 25$. 921 s . 966 1. 033 3. 095 . 647	Fe Fe Mn Fe	4 3 2 4 5	$155 \\ 155 \\ 154 \\ 154 \\ 148$	$ 155 \\ 155 \\ 155 \\ 155 \\ 155 \\ 155 $	+6 +3 +4 +8	IV b
85.007 91.556 94.938 4098.179 4100.744	A A B A	28 38 22 26 32	$.161 \\ .711 \\ 5.094 \\ .335 \\ .901$	Fe Fe Ca? Fe Fe	4 3 4 5 4	$154 \\ 155 \\ 156 \\ 156 \\ 157$	$ 155 \\ 156 \\ 156 \\ 156 \\ 156 \\ 156 $	+3 +5	IV b IV b IIA
$\begin{array}{c} 01.\ 267\\ 06.\ 260\ ^1\\ 06.\ 431\ 1\\ 07.\ 492\\ 12.\ 321\\ \end{array}$	A A B A B	10 10 10 25 20	$\begin{array}{r} .421 \\ .420 \\ .583 \\ .649 \\ .478 \end{array}$	Fe Fe Fe Ce-Fe-Zr Fe	2 2 2 5 2	$154 \\ 160 \\ 152 \\ 157 \\ 157 \\ 157$	156 15 15	$ \begin{array}{c c} \pm 0 \\ \pm 9 \\ + 9 \\ + 4 \end{array} $	d III b
$14.\ 450\\20.\ 212\\-\ 26.\ 190\\36.\ 527\\37.\ 000$	B C B A C	17 13 17 20 18	. 606 s . 368 . 344 . 678 . 156	Fe Fe Fe Fe Fe	4 4 4 4 6	$156 \\ 156 \\ 154 \\ 151 \\ 156$	156 155 154 152 152 152 152 1	+5 +6 +7 +3	IV b IV b IV b d IV b
$\begin{array}{c} 39.\ 936\\ 43.\ 876\\ 47.\ 675\\ 49.\ 371\\ 54.\ 505 \end{array}$	A C C A C	$23 \\ 6 \\ 13 \\ 7 \\ 12$	$\begin{array}{c} 0.089\\ 4.038\\ \cdot836\\ \cdot533\\ \cdot667\end{array}$	Fe Fe Fe Fe	$\begin{array}{c} 6\\ 15\\ 4\\ 4\\ 4\\ 4\\ 4\end{array}$	$153 \\ 162 \\ 161 \\ 162 \\ 162 \\ 162$	$ \begin{array}{r} 152 \\ 163 \\ 163 \\ 163 \\ 164 \end{array} $	$ \begin{array}{c c} +9 \\ +9 \\ +6 \\ +6 \\ +6 \\ +6 \end{array} $	IIA a b1 III b V e III b
$54.\ 814\\58.\ 794\\63.\ 651\\68.\ 619\\78.\ 858$	A B C C B	17 19 11 8 13	.976 .959 .818 .784 9.025	Fe Fe Ti, Cr —	4 5 4 2 3	$162 \\ 165 \\ 167 \\ 165 \\ 167 \\ 167 \\ 167 \\ 167 \\ 167 \\ 167 \\ 167 \\ 167 \\ 167 \\ 167 \\ 100 $	$ \begin{array}{r} 164 \\ 164 \\ 164 \\ 163 \\ 162 \end{array} $	+8 +1	IV d V d
82. 387 84. 898 87. 046 91. 683 4198. 639	A B C C C	$25 \\ 12 \\ 8 \\ 11 \\ 16$.548 5.058 s .204 .843 .800	Fe Fe, Cr Fe Fe Fe	34633 3	$161 \\ 160 \\ 158 \\ 160 \\ 161$	$ \begin{array}{c c} 162 \\ 162 \\ 162 \\ 161 \\ 161 \\ 161 \end{array} $	+6 +8	IV b III b III d e? V d
$\begin{array}{c} 4202.\ 041\\ 07.\ 132\\ 08.\ 608\\ 13.\ 651\\ 20.\ 348 \end{array}$	C B B B B B	8 26 20 26 30	.198.291.766.812.509	Fe Fe Fe Fe	80 m m m m	157 159 158 161 161	$ \begin{array}{r} 160 \\ 160 \\ 160 \\ 160 \\ 159 \end{array} $	+12 +3 +4 +8	$\begin{matrix} \mathbf{I} & \mathbf{b1} \\ \mathbf{IV} & \mathbf{b} \\ \mathbf{V} & \mathbf{b} \\ \mathbf{IV} & \mathbf{b} \\ \mathbf{IV} & \mathbf{b} \\ \mathbf{IV} & \mathbf{b} \end{matrix}$
$\begin{array}{c} 22.\ 219\\ 24.\ 175\\ 25.\ 461\\ 25.\ 961\\ 26.\ 742 \end{array}$	B C C B C	$22 \\ 9 \\ 16 \\ 16 \\ 6$.382 s .337 .619 6.116 .904 sg	Fe Fe Fe Ca	5 4 3 2 20d?	$ \begin{array}{r} 163 \\ 162 \\ 158 \\ 155 \\ 160 \end{array} $	159 15 15	+7 +4 +7 +13	III d IV e IV d IV b I
$\begin{array}{c} 27.\ 432\ ^2\\ 31.\ 023\\ 32.\ 731\\ 33.\ 612\\ 35.\ 947\end{array}$	C C B C C B C C	9 11 17 13 10	$\begin{array}{r} .\ 606\\ .\ 183\\ .\ 887\\ .\ 772\\ 6.\ 112 \end{array}$	Fe Ni Fe Fe Fe	${}^{4}_{2}$ 4N 2 6 8	$174 \\ 160 \\ 156 \\ 160 \\ 165$	159 159 159 159 159 159	+6 +6 +10 +10	III d IA III d5 III d5
4238.025 41.121 43.815 ³ 46.838 4248.233 ⁴	D B D B B	$5 \\ 25 \\ 4 \\ 10 \\ 11$.188 .285 .981 .996 .384	Fe Fe-Zr Y? Fe	3 2 2 5 2	$163 \\ 164 \\ 166 \\ 158 \\ 151$	$ \begin{array}{c ccccc} 159 \\ 159 \\ 159 \\ 158 $	+3	IV d? IV b

TABLE 1.—A. O. B. S. solar wave lengths—Continued

¹4106.2 and 4106.4. These lines are too close together for the most accurate measurement with moderate resolution. The mean wave length of these two lines is probably quite correct. ²4227.4. The A. O. B. S. and laboratory values of this wave length agree. This is a line of much greater solar intensity than 4, the figure in Rowland's table. Perhaps there is a typographical error in Rowland's value of the wave length. ³4243.8. A close companion renders the interference measurements of this line rather uncertain. ⁴4248.2. The laboratory value of this line agrees with Rowland.

Standard Solar Wave Lengths TABLE 1.—A. O. B. S. solar wave lengths—Continued

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ning pilot (Proba- ble			Rowland	and a training	Correc	etion to vland		Tempera-
A.Ο.Β.S.λ	ble error	obs.	λ	Iden.	Int.	Obs.	Mean	_ Sun—arc	pressure classes
$\begin{array}{r} 4250.\ 129\\ 54.\ 347\\ 57.\ 660\\ 60.\ 488\\ 65.\ 264\end{array}$	C C A C B	7 5 11 7 20	.287 .505 s .815 .640 s .418	Fe Cr Mn Fe Fe Fe	8 8 2 10 2	158 158 155 152 154 154	158 15 15	+10 +10 +14	III c5 II II III c2
$\begin{array}{c} 66.\ 967\\ 68.\ 754\\ 71.\ 160\\ 71.\ 774\\ 76.\ 678 \end{array}$	C A C C B	11 17 7 7 13	7.122 .915 .325 .934 s .836	Fe Fe Fe Zr	$3 \\ 2 \\ 6 \\ 15 \\ 2$	$155 \\ 161 \\ 165 \\ 160 \\ 158$	$ 158 \\ 158 \\ 158 \\ 158 \\ 158 \\ 158 $	$^{+2}_{+10}_{+7}_{+14}$	IV b IV b III d II b1
$\begin{array}{r} 82.411\\ 90.384\\ 4291.471\\ 4318.658\\ 21.797\end{array}$	B C B B B B	$ \begin{array}{r} 19 \\ 7 \\ 26 \\ 12 \\ 9 \end{array} $.565 .542 .630 .817 .961	Fe Fe Ca, Mn? Fe	$5\\1\\2\\4\\2$	$154 \\ 158 \\ 159 \\ 159 \\ 164$	158 158 158 160 161	+8 +7	III b1 IA a3
$\begin{array}{c} 25.773\\ 26.758\\ 27.110\\ 31.649\\ 37.055 \end{array}$	D B A B C	5 14 18 18 20	.939 s .923 .274 .811 .216	Fe Fe Fe Ni Fe	8 2 3 2 5	166 165 164 162 161	$ \begin{array}{r} 161 \\ 161 \\ 161 \\ 162 \\ 162 \end{array} $	+12	II b1 V b II II b3
$\begin{array}{c} 37.927\\ 38.265\\ 43.703\\ 46.557\\ 47.238\end{array}$	A C B C B	17 17 18 13 17	$\begin{array}{r} 8.084 \\ .430 \\ .861 \\ .725 \\ .403 \end{array}$	Ti Fe Fe Fe Fe	$\begin{array}{c}4\\1\\2\\2\\1\end{array}$	$ 157 \\ 165 \\ 158 \\ 168 \\ 165 $	$ \begin{array}{r} 162 \\ 162 \\ 162 \\ 162 \\ 162 \end{array} $	+11 +2 +4 +5	VE
$\begin{array}{c} 48.946\\ 51.548\\ 58.504\\ 59.621\\ 60.799 \end{array}$	B B D A	$ \begin{array}{r} 16 \\ 12 \\ 13 \\ 6 \\ 11 \end{array} $	9. 107 .711 .670 .748 s .958	Fe Fe Cr Fe, Zr	2 2 3 1	$ \begin{array}{r} 161 \\ 163 \\ 166 \\ 163 \\ 159 \end{array} $	$162 \\ 162 \\ 161 \\ 161 \\ 161 \\ 161$	$^{+10}_{+6}_{+4}$	IV b IV b I
65.903 67.910 69.779 73.564 75.947	B A C B C	$28 \\ 24 \\ 16 \\ 18 \\ 25$	6.061 8.071 .941 s .727 6.107 s	Fe Fe Fe Fe	2 2 4 2 6	$ 158 \\ 161 \\ 162 \\ 163 \\ 160 $	$ \begin{array}{r} 161 \\ 161 \\ 161 \\ 161 \\ 160 \\ 160 \\ \end{array} $	+4 +7 +1 +17	IIIA a III b3 I a3
77.79379.24183.56387.89788.414	B D C C C C	$ \begin{array}{c} 18 \\ 5 \\ 9 \\ 22 \\ 7 \end{array} $.948 .396 .720 s 8.057 .571	Fe V Fe Fe, Co Fe	$ \begin{array}{c} 1 \\ 4 \\ 15 \\ 2 \\ 3 \end{array} $	$155 \\ 155 \\ 157 \\ 160 \\ 157$	$160 \\ 159 \\ 159 \\ 159 \\ 159 \\ 159 \\ 159 $	+19 +7	II b1 IV b IV d?
$\begin{array}{c} 89.252\\ 94.066\\ 98.020\\ 4399.775\\ 4404.767\end{array}$	A A B A C	18 10 16 15 9	.413 .225 .178 .935 .927 s	Fe- Ti? Ti, Cr Fe	$2 \\ 2 \\ 1 \\ 3 \\ 10$	$ \begin{array}{r} 161 \\ 159 \\ 158 \\ 160 \\ 160 \end{array} $	$ 159 \\ 159 \\ 150 \\ 160 \\ 160 $	+17	IIA a II b1
$\begin{array}{r} 08.204 \\ 15.144^{5} \\ 16.829 \\ 22.572 \\ 4425.445 \end{array}$	B B B B B	$14 \\ 13 \\ 17 \\ 16 \\ 19$.364 .263 s .985 .741 .608 s	V Fe Fe, Y Ca	2 8 2 3 4	$ \begin{array}{r} 160 \\ 149 \\ 156 \\ 169 \\ 163 \end{array} $	$ \begin{array}{r} 160 \\ 161 \\ 161 \\ 161 \\ 161 \end{array} $	+22 +3	II b1 III b3 I
$\begin{array}{c} 27.323\\ 30.195\\ 30.621\\ 32.572\\ 33.230 \end{array}$	B D B B C	$ \begin{array}{r} 16 \\ 6 \\ 29 \\ 16 \\ 16 \\ 16 \end{array} $.482 .356 .785 .736 .390	Fe Fe Fe Fe	5 1 3 1 3	$159 \\ 161 \\ 164 \\ 164 \\ 160$	$ \begin{array}{r} 162 \\ 162 \\ 162 \\ 162 \\ 162 \end{array} $	+13 +7 +10	I a3 IV III c4 IV e
$\begin{array}{r} 33.783\\ 35.157\\ 35.688\\ 39.888\\ 4442.353\end{array}$	C D B A B	75152420	.948 .321 .851 s 0.054 .510	Fe Fe Ca Fe Fe	$ \begin{array}{c} 1 \\ 2 \\ 4 \\ 1 \\ 6 \end{array} $	$ \begin{array}{r} 165 \\ 164 \\ 163 \\ 166 \\ 157 \end{array} $	$ \begin{array}{c c} 162 \\ 162 \\ 162 \\ 163 \\ 163 \\ 163 \\ \end{array} $	+1 +9 +13	d IIA a I IV IV c4

 $^{\rm 5}$ 4415.1. The wave length of this line is no doubt affected by close companions. The laboratory value agrees with Rowland.

A.O.B.S.λ	Proba- ble error	No.		Rowland	and the second	Correc	etion to vland	Sun-oro	Tempera- ture and
A. U. D. S. A	error	obs.	λ	Iden	Int.	Obs.	Mean	_ sun-arc	pressure classes
4443. 202 43. 812 45. 476 47. 737 ⁶ 51. 588	B B A B	$13 \\ 15 \\ 13 \\ 16 \\ 16 \\ 16$. 365 . 976 . 641 . 892 s . 752	Fe Ti Fe Fe Mn	$\begin{array}{c}3\\5\\1\\6\\3\end{array}$	163 164 165 155 164	$ \begin{array}{r} 163 \\ 163 \\ 163 \\ 163 \\ 163 \end{array} $	$ \begin{array}{c} +8 \\ +10 \\ +6 \\ +20 \end{array} $	III b3 VE IA III c4 II
$54.388 \\ 56.332 \\ 59.756 \\ 61.661 \\ 66.566$	A B A B B	$30 \\ 10 \\ 15 \\ 24 \\ 22$.552 .497 .922 .818 .727	Fe Fe Fe Fe	3 1 1 4 5	$ \begin{array}{r} 164 \\ 165 \\ 166 \\ 157 \\ 161 \end{array} $	$163 \\ 163 $	+7 +8 +14	III b3 I a3 II b4
$\begin{array}{c} 70.\ 136\\ 70.\ 486\\ 81.\ 617\\ 84.\ 229\\ 85.\ 682 \end{array}$	D A A A A		.300 .648 .782 .392 .846	Mn Ni-Zr Fe Fe Fe	$ \begin{array}{c} 1 \\ 2 \\ 1 \\ 4 \\ 3 \end{array} $	$ \begin{array}{r} 164 \\ 162 \\ 165 \\ 163 \\ 164 \end{array} $	$163 \\ 163 \\ 163 \\ 163 \\ 163 \\ 163$	+9 +6	III IV d IV e?
91. 410 94. 575 4496. 864 4501. 280 02. 220	B A B A A	$16 \\ 14 \\ 17 \\ 16 \\ 15$.570 .738 s 7.023 s .448 s .388	Fe Cr Ti- Mn	2 6 3 5 2	$ \begin{array}{r} 160 \\ 163 \\ 159 \\ 168 \\ 168 \end{array} $	$ 164 \\ 164 \\ 165 \\ 165 165 $	+12	III c4
$\begin{array}{c} 04.834\\ 08.290\\ 12.741\\ 17.536\\ 25.149 \end{array}$	B A A A A	$16 \\ 23 \\ 22 \\ 17 \\ 16$	$5.003 \\ .455 \text{ s} \\ .906 \\ .702 \\ .314$	Fe Fe?— Ti Fe Fe	1 4 3 3 5	$ \begin{array}{r} 169 \\ 165 \\ 165 \\ 166 \\ 165 \end{array} $	$ \begin{array}{r} 165 \\ 165 \\ 166 \\ 167 \end{array} $	+6 +7 +12 +11	d II IV d?
$\begin{array}{c} 26.\ 934\\ 28.\ 631\\ 31.\ 631\\ 34.\ 785\\ 41.\ 524 \end{array}$	B A A A	$15 \\ 13 \\ 21 \\ 17 \\ 22$	$7.101 \\ .798 \\ .801 \\ .953 \\ .690$	Ca? Fe Fe Ti Cr	3 8 2 4 2	$ \begin{array}{r} 167 \\ 167 \\ 170 \\ 168 \\ 166 \end{array} $	$ 167 \\ 167 \\ 167 \\ 167 \\ 168 $	+17	II c4 II b3
$\begin{array}{r} 47.\ 855\\ 48.\ 772\\ 50.\ 775\\ 54.\ 042\\ 58.\ 653\end{array}$	A A B A	$17 \\ 16 \\ 15 \\ 8 \\ 7$	8.024 .938 .942 .211 s .827	Fe Ti Fe? Ba Cr?	3 2 2 8 3	$ \begin{array}{c c} 169 \\ 166 \\ 167 \\ 169 \\ 174 \end{array} $	168 168 168 169 16 1 16 16 16 1	+8 +8 +8 +5	ы п ш п
$\begin{array}{c} 60.\ 094\\ 63.\ 769\\ 71.\ 103\\ 71.\ 983\\ 74.\ 727 \end{array}$	B B A A B	$10 \\ 20 \\ 20 \\ 15 \\ 10$. 266 . 939 s . 275 s . 156 s . 899	Fe Ti Mg Ti- Fe	$\begin{array}{c} 2\\ 4\\ 5\\ 6\\ 2\end{array}$	$ \begin{array}{c c} 172 \\ 170 \\ 172 \\ 173 \\ 172 \end{array} $	$ 170 \\ 171 \\ 172 \\ 172 \\ 172 \\ 172 172 $	+7 +8	VE IA
$76.\ 340\\78.\ 560\\4587.\ 135\\88.\ 207\\89.\ 955$	A A B A A	$15 \\ 17 \\ 20 \\ 16 \\ 15$.512 .732 s .308 .381 s 0.126 s	Ca Fe	2 3 2 3 3	$ \begin{array}{c c} 172\\172\\173\\174\\171\end{array} $	$ \begin{array}{r} 172 \\ 172 \\ 172 \\ 173 \\ 173 \end{array} $	+7	п
$\begin{array}{r} 95.367\\ 4598.127\\ 4602.008\\ 02.951\\ 07.657\end{array}$	A A A A A	$21 \\ 14 \\ 17 \\ 17 \\ 23$.540 .303 .183 s 3.126 .831	Fe Fe Fe Fe	2 3 6 4	$ 173 \\ 176 \\ 175 \\ 175 \\ 174 $	$ 173 \\ 174 \\ 174 \\ 174 \\ 174 \\ 174 174 $	$ \begin{array}{c c} +9 \\ +10 \\ +7 \\ +10 \\ +11 \end{array} $	d IB V
$\begin{array}{c} 16.\ 133\\ 17.\ 277\\ 20.\ 520\\ 25.\ 055\\ 30.\ 128 \end{array}$	A A A A A	$17 \\ 16 \\ 21 \\ 19 \\ 17$.305 .452 .693 .227 .306	Cr Ti Fe Fe Fe	$ \begin{array}{c} 4 \\ 3 \\ 1 \\ 5 \\ 4 \end{array} $	$ \begin{array}{c c} 172 \\ 175 \\ 173 \\ 172 \\ 178 \\ \end{array} $	$ 174 \\ 174 \\ 174 \\ 174 \\ 174 \\ 174 174 $	+8 +10 +8	I II d
$\begin{array}{c} 35.855\\ 37.511\\ 38.019\\ 43.472\\ 47.443\end{array}$	A C A A C	$ \begin{array}{r} 15 \\ 7 \\ 16 \\ 23 \\ 7 \end{array} $	6.027 .685 s .193 s .645 s .617	Fe Fe Fe Fe	2 5 4 4 4	$ 172 \\ 174 \\ 174 \\ 173 \\ 174 $	173 173 173 173 173 173	+8 +6 +11 +8 +9	IV d IV b IV b
$\begin{array}{r} 48.\ 660\\ 52.\ 170\\ 56.\ 475\\ 64.\ 795\\ 4673.\ 174\end{array}$	B A A B C	$ \begin{array}{r} 10 \\ 16 \\ 22 \\ 17 \\ 7 \end{array} $.835 s .343 .644 .965 .347	Ni Cr Ti Cr Fe	$\begin{array}{c} 4\\ 5\\ 3\\ 3\\ 4\end{array}$	175 173 169 170 173	$ 173 \\ 172 \\ 172 \\ 172 \\ 172 \\ 173 $	+7	III I I III

TABLE 1.—A. O. B. S. solar wave lengths—Continued

⁶ 4447.7. One series of measurements gives .730 for the fractional part of this wave length. The results from many other plates are in good agreement and give the value tabulated. A companion affects the wave length as measured by the interferometer.

Standard Solar Wave Lengths

A .O.B.S.λ	Proba- ble error	No.		Rowland	north off	Correc Row	tion to	Sun-are	Tempera- ture and
A. U. B. S. A	error	obs.	λ	Iden.	Int.	Obs.	Mean		pressure classes
$\begin{array}{r} 4678.171\\78.855\\83.567\\86.221\\4690.146\end{array}$	B B A A A	17 19 22 20 22	.347 s 9.027 s .745 s .395 s .317 s	Cd Fe Fe Ni Fe?	3N 6 3 3 4	176 172 178 174 173 173	$ 173 \\ 173 \\ 173 \\ 173 \\ 173 \\ 173 173 $	$+9 \\ +4 \\ +8$	V III
$\begin{array}{c} 4700.\ 164\\ 03.\ 006\\ 03.\ 817\\ 04.\ 956\\ 09.\ 718 \end{array}$	A B C A A	$15 \\ 11 \\ 11 \\ 20 \\ 13$.337 .177 s .994 s 5.131 .896	(Fe) Mg Ni Fe Mn	$ \begin{array}{c} 4 \\ 10 \\ 3 \\ 4 \\ 2 \end{array} $	$ 173 \\ 171 \\ 177 \\ 175 \\ 178 \\ 178 $	$174 \\ 174 \\ 174 \\ 174 \\ 174 \\ 175$	+7 +9	v d III
$15.774 \\ 18.428 \\ 21.001 \\ 22.166 \\ 28.554$	B B C A B	$13 \\ 13 \\ 5 \\ 22 \\ 11$. 946 . 601 . 179 . 342 s . 732	Ni Cr Fe? Zn Fe	4 3 2 3 4	$ \begin{array}{c c} 172 \\ 173 \\ 178 \\ 176 \\ 178 \\ 178 \\ \end{array} $	$ 175 \\ 175 \\ 175 \\ 176 \\ 176 \\ 176 $	+7	II III IV
$\begin{array}{c} 33.\ 602\\ 36.\ 785\\ 41.\ 537\\ 45.\ 808\\ 52.\ 431 \end{array}$	A C A B C	19 14 18 17 8	.779 .963 .718 .992 .613	Fe Fe Fe Ni	$ \begin{array}{c} 4 \\ 6 \\ 3 \\ 4 \\ 3 \end{array} $	177 178 181 184 182 182	177 178 179 180 181	$+11 \\ +12 \\ +6 \\ +7 \\ +7 \\ +7 \\ +7 \\ +7 \\ +7 \\ +7$	$\begin{matrix} IB & a \\ II & d \\ V & b \\ V & b \\ V & b \end{matrix}$
$54.047 \\ 4761.534 \\ 66.430 \\ 72.826 \\ 79.985$	C B B C C	$ \begin{array}{c} 12 \\ 9 \\ 9 \\ 8 \\ 10 \end{array} $. 225 s .718 .621 3.007 .169	Mn Mn Fe Co	$\begin{array}{c} 7\\ 3\\ 4\\ 4\\ 2\end{array}$	178 184 181 181 184	$ 182 \\ 183 \\ 183 \\ 183 \\ 184 $	+10	I III III III b III
$\begin{array}{r} 86.820 \\ 88.766 \\ 4789.659 \\ 4802.888 \\ 10.539 \end{array}$	C A C A B		7.003 .952 .849 3.072 .724 s	Fe Fe Fe Zn	2 3 3 2 3	$ 183 \\ 186 \\ 190 \\ 184 \\ 185 $	185 185 185 185 185 185	+14 +9 +9 +9 +6	IV? b V
$\begin{array}{c} 23.\ 516\\ 24.\ 145\\ 32.\ 718\\ 39.\ 551\\ 48.\ 257\end{array}$	B D B B D	7 8 9 9	. 697 s . 325 s . 905 . 734 . 438	Mn Fe Fe Fe	5 3 3 3 2	181 180 187 183 181	184 184 183 182 181	+7+6	I
$54.875 \\ 59.751 \\ 70.824 \\ 82.154 \\ 85.437$	A B D D	6 5 7 9 7	5.059 .928 s .996 .336 .620	Fe Fe Ni, Cr Fe Fe	$\begin{array}{c}1\\4\\3\\3\\3\end{array}$	184 177 172 182 183	179 179 177 176 175	+10 +9 +7	III c5 d V
$\begin{array}{r} 4892.867\\ 4904.424\\ 17.239\\ 24.784\\ 38.184 \end{array}$	B C A A A		3. 030 . 597 . 410 . 956 s . 350	Fe Fe Fe	$\begin{array}{c}1\\3\\2\\3\\2\end{array}$	$ \begin{array}{r} 163 \\ 173 \\ 171 \\ 172 \\ 166 \end{array} $	$ 175 \\ 173 \\ 172 \\ 171 \\ 171 \\ 171 $	$+11 \\ +10$	V b
$\begin{array}{c} 38.825\\ 39.697\\ 46.401\\ 50.117\\ 53.217\end{array}$	D B B B C	7 13 10 13 8	. 997 . 868 . 568 . 291 . 392	Fe Fe Fe Ni	4 3 3 2 2	$ 172 \\ 171 \\ 167 \\ 174 \\ 175 $	$ \begin{array}{c} 171\\ 171\\ 171\\ 171\\ 171\\ 171\\ 171 \end{array} $	$ \begin{array}{c} +13 \\ +11 \\ +14 \\ +11 \end{array}$	$ \begin{array}{c c} IV & d \\ IB & a \\ IV & d \\ V? \\ \end{array} $
$\begin{array}{c} 62.583\\ 66.102\\ 67.909\\ 73.110\\ 83.262\end{array}$	B B C C B	$12 \\ 12 \\ 14 \\ 12 \\ 14 \\ 12 \\ 14$.751 .270 8.080 .281 s .433	Fe Fe Ti, Fe Fe	$2 \\ 4 \\ 3 \\ 4 \\ 3 \\ 3$	168 168 171 171 171 171	171 171 171 171 171 171	+13 +10 +14	V d e V d
$\begin{array}{c} 4994.140\\ 5001.876\\ 02.802\\ 14.954\\ 28.135\end{array}$	B C A C A	$16 \\ 15 \\ 19 \\ 14 \\ 17$.316 s 2.044 .976 5.123 .308	Fe Fe Fe Fe	3 5 2 3 2	176 168 174 169 173	171 171 171 171 171 171	+10 +12 +10 +12 +12 +8	IB a V d V d
$\begin{array}{r} 39.968 \\ 48.448 \\ 49.834 \\ 60.080 \\ 5067.160 \end{array}$	B A B A B	$20 \\ 13 \\ 13 \\ 21 \\ 20$	0. 138 . 612 0. 008 s . 258 s . 336	Ti Fe Fe Fe	3 3 6 3 3	170 164 174 178 176	171 171 171 170 170	+ 9 +15	I a III a

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A.O.B.S.λ	Proba- ble error	No.		Rowland	an a	Correc Row	tion to land	Sun-are	Tempera- ture and
n. 0. D . 5. k	error	obs.	λ	Iden.	Int.	Obs.	Mean	. Sun uro	pressure classes
5068.77974.76276.27879.24179.749	C C B C B	$15 \\ 15 \\ 15 \\ 14 \\ 15$.944 s .932 .450 .409 .921	Fe Fe Fe Fe	5 5 3 4 4	165 170 172 168 172 172	169 169 169 169 169	+13 +14 + 8	V d V e IV b IB a
$\begin{array}{r} 83.351\\ 90.787\\ 5099.941\\ 5109.661\\ 15.401\end{array}$	A A B B	21 18 21 17 16	. 518 s . 954 s 0. 108 . 827 s . 566	Fe Fe Ni Fe Ni	4 5 2 2 2 2	$167 \\ 167 \\ 167 \\ 166 \\ 165$	$168 \\ 168 \\ 167 \\ 167 \\ 166 \\$	+13 +12	IB a V
$\begin{array}{c} 26.204\\ 37.394\\ 50.852\\ 59.067\\ 73.752 \end{array}$	C B C B A	18 16 17 19 21	.371 s .588 1.020 s .231 s .917 s	Fe, Co Fe Fe Fe Ti	2 3 4 2 2	$167 \\ 164 \\ 168 \\ 164 \\ 165$	$166 \\ 165 \\ 165 \\ 165 \\ 165 \\ 164$	+12 +12 +12 +10	V d IB a I
$\begin{array}{r} 85.911\\ 5198.723\\ 5210.396\\ 17.403\\ 25.537\end{array}$	A B A B A	20 21 23 21 23 23	6.073 .888 s .555 s .552 s .695 s	Ti Fe Ti Fe Fe	2 3 3 3 2	$162 \\ 165 \\ 169 \\ 149 \\ 158 $	$163 \\ 162 \\ 161 \\ 155$	$+11 \\ +10 \\ +15$	IV a I a V d IA
$\begin{array}{r} 42.502 \\ 53.471 \\ 63.318 \\ 73.391 \\ 5288,536 \end{array}$	A A C A	$22 \\ 24 \\ 23 \\ 14 \\ 24$. 658 s . 633 s . 486 . 558 s . 705 s	Fe Fe Fe, Cr Fe	$2 \\ 2 \\ 4 \\ 2 \\ 2 \\ 2$	$156 \\ 162 \\ 168 \\ 167 \\ 169$	$159 \\ 162 \\ 165 \\ 167 \\ 170$	+12 +13	IV a V d
$5300.753 \\ 07.370 \\ 22.051 \\ 32.909 \\ 48.327$	A A A A A	$22 \\ 23 \\ 14 \\ 13 \\ 16$.929 s .541 s .227 3.089 s .511	Cr Fe Fe Fe Cr	$2 \\ 3 \\ 3 \\ 4 \\ 4$	$176 \\ 171 \\ 176 \\ 180 \\ 184$	$172 \\ 173 \\ 177 \\ 179 \\ 183$	+10 +8	I III? a IB? a4 I
65. 409 79. 583 89. 487 5398. 290 5409. 799	A A A A A	$16 \\ 14 \\ 14 \\ 14 \\ 14 \\ 14 \\ 14$.596 .775 s .683 s .486 0.000 s	Fe Fe Fe Cr	. 3 3 3 4	187 192 196 196 201	187 192 195 197 201	+7	V a a I
$\begin{array}{r} 15.215\\5432\ 956\\45.055\\62.971\\73.909\end{array}$	C B A A A	$11 \\ 14 \\ 16 \\ 15 \\ 18$. 416 s 3. 160 . 259 3. 174 s 4. 113	Fe, V Fe Fe Fe Fe	5 2 4 3 3	$201 \\ 204 \\ 204 \\ 203 \\ 204$	$202 \\ 203 \\ 204 \\ 204 \\ 204 \\ 204$	+13	V e e d
$5487.754 \\ 5501.477 \\ 12.989 \\ 25.552 \\ 34.848$	B A B A A	19 18 18 17 22	. 959 s . 683 s 3. 198 s . 765 5. 061 s	Fe Fe Fe Fe	3 5 4 2 2	$205 \\ 206 \\ 209 \\ 213 \\ 213 \\ 213$	$205 \\ 206 \\ 209 \\ 212 \\ 214$	+ 7 +11	IB a3 III
$\begin{array}{r} 46.516\\ 60.217\\ 76.104\\ 5590.125\\ 5601.286\end{array}$	B A A A A	20 24 24 24 24 22	. 732 434 . 320 s . 343 s . 505 s	Fe Fe Ca Ca	2 2 4 3 3	216 217 216 218 217	$216 \\ 216 \\ 217 $		IV d5 III III ,
$\begin{array}{c} 18.\ 640\\ 24.\ 558\\ 41.\ 447\\ 55.\ 499\\ 67.\ 525\end{array}$	A A B B	$19 \\ 20 \\ 18 \\ 18 \\ 15 $.858 .769 s .667 s .715 s .739	Fe Fe, V Fe Fe Fe	$\begin{array}{c}1\\4\\2\\2\\2\\2\end{array}$	$218 \\ 211 \\ 220 \\ 216 \\ 214$	218 218 218 217 216		IV V
$\begin{array}{c} 79.032 \\ 5690.433 \\ 5701.557 \\ 17.839 \\ 31.772 \end{array}$	A A A A A	$17 \\ 15 \\ 17 \\ 16 \\ 14$. 249 s . 646 . 772 s 8. 055 . 984 s	Fe Si Fe Fe Fe	3 3 4 4 4	$217 \\ 213 \\ 215 \\ 216 \\ 212$	$216 \\ 215 \\ 214 \\ 214 \\ 213$	+ 9	111?
$\begin{array}{r} 41.856\\ 52.042\\ 60.841\\ 72.156\\ 5783.871\end{array}$	C C B C C	9 13 10 10 11	2.068 s .254 s 1.052 .364 s 4.080 s	Fe Fe Ni Si Cr	$ \begin{array}{c} 2 \\ 4 \\ 2 \\ 3 \\ 3 \end{array} $	$\begin{array}{c} 212 \\ 212 \\ 211 \\ 208 \\ 209 \end{array}$	$212 \\ 211 \\ 211 \\ 210 \\ 209$		IV III

TABLE 1.—A. O. B. S. solar wave lengths—Continued

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Standard Solar Wave Lengths

A.O.B.S.λ	Proba-	No.		Rowland		Correc	etion to rland	Sup	Tempera- ture and
A. U. B. S.A	èrror	obs.	λ	Iden.	Int.	Obs.	Mean	_ Sun—are	pressure classes
5797.8705805.22606.73809.22716.379	B C D B C	9 6 6 19 6	8.077 s .441 s .950 s .439 s .601 s	Ni Fe Fe Fe	3 4 5 4 5	207 215 212 212 212 222	$\begin{array}{r} 209 \\ 214 \\ 214 \\ 214 \\ 214 \\ 214 \end{array}$	±0	v
$\begin{array}{r} 47.012\\ 48.129\\ 52.235\\ 53.688\\ 55.087\end{array}$	D C D A D	4 14 7 17 4	. 221 . 342 . 443 . 902 s . 300	Ni Fe Ba Fe	$ \begin{array}{c} 1 \\ 3 \\ 3 \\ 5 \\ 1 \end{array} $	209 213 208 214 213	$\begin{array}{c c} 213 \\ 213 \\ 213 \\ 213 \\ 213 \\ 213 \\ 213 \end{array}$	+9	ш
$56.101 \\ 57.459 \\ 57.762 \\ 59.596 \\ 62.368$	B B C A B		.312 .674 s .976 .809 s .582 s	Fe Ca Ni Fe Fe	2 8 3 5 6	$\begin{array}{c} 211\\ 215\\ 214\\ 213\\ 214\\ 214\\ \end{array}$	$213 \\ 213 \\ 213 \\ 213 \\ 213 \\ 213 \\ 213$	+8 +3 +11	III IV V V
$\begin{array}{c} 66.\ 461 \\ 67.\ 573 \\ 85.\ 978 \\ 87.\ 217 \\ 91.\ 656 \end{array}$	A B D C B	$23 \\ 6 \\ 7 \\ 4 \\ 4 \\ 4$.675 .785 6.193 .445 .878	Ti Ca Air Air Air	3 2 5 5 4	$214 \\ 212 \\ 215 \\ 228 \\ 222$	$213 \\ 213 \\ 215 \\ 215 \\ 215 \\ 215 \\ 215$	+8	п
92. 884 98. 166 5899. 007 5901. 462 05. 681	B B C B A	$ \begin{array}{r} 19 \\ 8 \\ 2 \\ 12 \\ 17 \\ 17 \end{array} $	3.097 s .378 s .215 .682 s .895 s	Ni Air Air Air Fe	$\begin{array}{c c} 4\\ 4\\ 2\\ 6\\ 4 \end{array}$	$213 \\ 212 \\ 208 \\ 220 \\ 214$	$215 \\ 216 \\ 216 \\ 216 \\ 216 \\ 216 \\ 216 \\$	+6+8	II V
$\begin{array}{c} 08.999\\ 16.257\\ 18.441\\ 19.052\\ 19.645 \end{array}$	C B D C B	$2 \\ 17 \\ 4 \\ 8 \\ 13$	9. 213 . 475 s . 635 . 276 . 860 s	Air Fe Air Air Air	3 3 4 5 7	$214 \\ 218 \\ 194 \\ 224 \\ 215$	$216 \\ 216 \\ 216 \\ 216 \\ 216 \\ 216 \\ 216$		
$\begin{array}{c} 24.268\\ 27.797\\ 29.689\\ 30.192\\ 32.092 \end{array}$	D B C A C	$5 \\ 15 \\ 12 \\ 16 \\ 10$. 490 8. 013 . 898 . 406 s . 306	Air Fe Fe Fe Air		$222 \\ 216 \\ 209 \\ 214 \\ 214 \\ 214$	$216 \\ 216 \\ 216 \\ 216 \\ 216 \\ 216 \\ 216 \\$	+11	v
$\begin{array}{c} 34.\ 665\\ 41.\ 074\\ 42.\ 568\\ 46.\ 005\\ 47.\ 057\end{array}$	A C C C D	$ \begin{array}{r} 18 \\ 4 \\ 3 \\ 11 \\ 2 \end{array} $. 881 s . 290 . 789 . 223 . 283	Fe Air Air Air Air	5 5 3 3 2	$216 \\ 216 \\ 221 \\ 218 \\ 226$	$216 \\ 217 $	+7	V
$\begin{array}{c} 48.544\\ 52.726\\ 53.170\\ 56.706\\ 75.357\end{array}$	B A C B C	$ \begin{array}{r} 14 \\ 18 \\ 6 \\ 17 \\ 9 \end{array} $. 765 s . 943 . 386 . 923 s . 575 s	Si Fe Fe Fe	$\begin{array}{c} 6\\ 4\\ 1\\ 4\\ 3\end{array}$	221 217 216 217 218	$217 \\ 217 \\ 217 \\ 217 \\ 217 \\ 218 \\$	+8	V II V b4
$76.788 \\78.564 \\83.689 \\84.826 \\87.067$	B C B B A	17 3 18 19 18	7.007 s .768 .908 5.040 s .290 s	Fe Ti Fe Fe Fe	4 1 5 6 5	219 204 219 214 223	218 218 218 218 218 218 218	+9 +5 +9 -3	V II V IV V
$\begin{array}{c} 91.382 \\ 5997.786 \\ 6003.023 \\ 05.552 \\ 07.321 \end{array}$	C C B D D	$9 \\ 11 \\ 19 \\ 6 \\ 7$.600 8.002 .239 s .770 .540	Fe Fe Fe	$ \begin{array}{c} 2 \\ 2 \\ 6 \\ 1 \\ 1 \end{array} $	218 216 216 218 218 219	218 217 217 217 217 217	+10	v
$\begin{array}{c} 07.965\\ 08.565\\ 13.497\\ 16.646\\ 21.800 \end{array}$	A A B A	22 21 21 21 21 22	8. 186 s .785 s .715 s .861 s 2. 016 s	Fe Fe Mn Mn Mn	$\begin{array}{c} 4\\ 6\\ 6\\ 6\\ 6\\ 6\end{array}$	221 220 218 215 216	$217 \\ 217 \\ 216 \\ 216 \\ 216 \\ 216$	+6 +7 +7 +7 +3	V III III
$\begin{array}{c} 24.069\\ 27.058\\ 42.104\\ 56.005\\ 6065.495\end{array}$	A A B B A	24 26 24 27 28	.281 s .274 s .315 s .227 s .709 s	Fe Fe Fe Fe	7 [4 3 5 7	$\begin{array}{c} 212 \\ 216 \\ 211 \\ 222 \\ 214 \end{array}$	$\begin{array}{c c} 212 \\ 215 \\ 215 \\ 214 \\ 214 \\ 214 \end{array}$	$\begin{array}{c c} +9 \\ +10 \\ +13 \\ +1 \\ +12 \end{array}$	$\begin{array}{ccc} V & b4 \\ V & e \\ V \\ III & b4 \end{array}$

A. O. B. S.λ	Proba-	No.		Rowland		Correc Row	tion to land	Sun-are	Tempera- ture and
	error	obs.	λ	Iden.	Int.	Obs.	Mean		classes
$\begin{array}{c} 6078.\ 499\\79.\ 016\\82.\ 717\\84.\ 121\\85.\ 255\end{array}$	A A C D C	26 23 17 3 20	. 710 s . 227 s . 930 . 325 . 470	Fe Fe Fe Fe-Ti	$\begin{array}{c} 5\\ 2\\ 1\\ 0\\ 2\end{array}$	$211 \\ 211 \\ 213 \\ 204 \\ 215$	213 213 213 213 213 213	+3	v
86. 287 89. 572 90. 215 93. 649 6096. 673	B C C B B	$17 \\ 18 \\ 12 \\ 12 \\ 12 \\ 17 $.500 .787 .429 .864 .880	Ni Fe Fe Fe	$\begin{array}{c}1\\1\\2\\2\\3\end{array}$	$213 \\ 215 \\ 214 \\ 215 \\ 207$	212 212 212 212 212 212 212		v
6102. 182 02. 726 03. 207 08. 120 11. 078	A A C A C	$26 \\ 22 \\ 12 \\ 26 \\ 15$. 392 s . 937 s . 400 s . 334 s . 290 s	Fe Ca Fe Ni Ni	$\begin{vmatrix} 6\\9\\4\\6\\2 \end{vmatrix}$	$210 \\ 211 \\ 193 \\ 214 \\ 212$	$\begin{array}{c c} 212 \\ 212 \\ 212 \\ 212 \\ 211 \\ 211 \\ 211 \end{array}$	$ \begin{vmatrix} +7 \\ +6 \\ +13 \\ -1 \end{vmatrix} $	V II V II
$\begin{array}{c} 16.197\\ 22.226\\ 25.021\\ 26.228\\ 27.912 \end{array}$	B C B B	$ \begin{array}{c} 17 \\ 21 \\ 8 \\ 8 \\ 22 \end{array} $	$\begin{array}{r} .397 \text{ s} \\ .434 \text{ s} \\ .236 \\ .435 \\ 8.124 \end{array}$	Ni Ca Ti Fe		$200 \\ 208 \\ 215 \\ 207 \\ 212$	$\begin{array}{c c} 211 \\ 211 \\ 211 \\ 210 \\ 210 \\ 210 \end{array}$	+10 +11	V II II b
$\begin{array}{c} 28,983\\ 36,621\\ 37,000\\ 37,701\\ 41,729 \end{array}$	C B A A A	9 21 24 21 21 24	9. 190 . 829 s 7. 210 . 915 . 938 s	Ni Fe Fe Fe-Ba	1 8 3 7 7	$\begin{array}{c} 207 \\ 208 \\ 210 \\ 214 \\ 209 \end{array}$	210 210 210 210 210 210	+4 +7	III b4 b III b4 V
$\begin{array}{c} 45.021\\ 49.248\\ 51.623\\ 54.229\\ 55.142\end{array}$	B B A B	$14 \\ 17 \\ 24 \\ 12 \\ 16$. 228 . 458 . 834 . 438 s . 350	Fe Na	2 2 4 2 7	$\begin{array}{c} 207 \\ 210 \\ 211 \\ 209 \\ 208 \end{array}$	210 210 210 210 210 210		
$57.733 \\ 60.750 \\ 61.294 \\ 62.181 \\ 63.759$	B A B C C	$25 \\ 23 \\ 21 \\ 16 \\ 4$. 945 . 956 s . 503 . 390 s . 968	Fe Na Ca Ca Ca	$5 \\ 3 \\ 4 \\ 15 \\ 3$	212 206 209 209 209 209	210 210 210 210 210 210	+1 +9	V b4
$\begin{array}{c} 65,363\\ 66,440\\ 69,040\\ 69,563\\ 70,517\end{array}$	B A A B	24 25 25 23 21	.577 .651 .249 s .778 s .730	Fe Ca Ca Ca Fe-Ni	3 5 6 7 6	$214 \\ 211 \\ 209 \\ 215 \\ 213$	$\begin{array}{c c} 210 \\ 211 \\ 211 \\ 211 \\ 211 \\ 211 \\ 211 \end{array}$	+9 +7	b III III V
$\begin{array}{c} 73.339\\ 6175.370\\ 76.816\\ 80.208\\ 86.717\end{array}$	A A A C	27 23 27 26 13	. 553 s . 584 7. 027 s . 420 s . 928	Fe Ni Fe Ni	53552	214 214 211 212 211	$\begin{array}{c c} 211 \\ 211 \\ 212 \\ 212 \\ 212 \\ 212 \end{array}$	+3	V III b4
87. 994 91. 181 6191. 570 6200. 320 04. 619	A A A D	$ \begin{array}{r} 18 \\ 26 \\ 20 \\ 25 \\ 3 \end{array} $	8. 210 . 393 s . 779 s . 527 s . 825	Fe Ni Fe Ni		216 212 209 207 206	$\begin{array}{c c} 212 \\ 211 \\ 211 \\ 210 \\ 210 \\ 210 \end{array}$	+11	I II b4 IV b4 III
$\begin{array}{c} 13.\ 436\\ 15.\ 147\\ 16.\ 359\\ 19.\ 286\\ 23.\ 986\end{array}$	B A B A C	$26 \\ 16 \\ 12 \\ 28 \\ 10$. 644 s . 360 . 567 . 494 s 4. 198	Fe Fe V? Fe Ni		208 213 208 208 212	209 209 209 209 209 209	+3 ±0	III b4 b4 III b4 V
$\begin{array}{c} 26.\ 740\\ 29.\ 229\\ 30.\ 736\\ 32.\ 645\\ 37.\ 322 \end{array}$	B B A C	12 19 25 27 16	. 951 . 437 . 943 s . 856 . 534 s	Fe Fe V-Fe Fe	1 1 8 3 3	211 208 207 211 212	209 210 210 210 210 210	+1 .	III b4 V
$\begin{array}{c} 38.387\\ 40.652\\ 43.114\\ 43.813\\ 6244.476\end{array}$	B B D C C	$ \begin{array}{r} 14 \\ 20 \\ 6 \\ 12 \\ 12 \end{array} $. 598 . 863 . 320 4. 033 . 686	Fe V	2 3 1 2 2	$\begin{array}{c} 211 \\ 211 \\ 216 \\ 213 \\ 210 \end{array}$	210 210 210 210 210 210	. 1	

Standard Solar Wave Lengths

A . Ο. Β. S.λ	Proba- ble error	Proba- ble error	Proba- ble error	Proba- ble error	No.		Rowland	in the off	Correc	etion to vland	Sup	Tempera- ture and
A. U. B. S. A	error	obs.	λ	Iden.	Int.	Obs.	Mean	sun_are	pressure classes			
6245. 621 46. 328 47. 558 52. 562 54. 254	A B B A B	11 22 20 22 20	. 832 . 535 s . 774 . 773 s . 456 s	Fe V Fe Fe	1 8 2 7 5	$211 \\ 207 \\ 216 \\ 211 \\ 202$	210 210 210 210 210 210	+10 +6	V III b4 III b4			
$56.\ 366 \\ 58.\ 110 \\ 58.\ 712 \\ 61.\ 103 \\ 65.\ 138$	A B B A A	22 20 19 19 19	. 572 s . 322 . 927 . 316 s . 348 s	Ni-Fe Ti Ti Ti Fe	6 2 3 1 5	206 212 215 213 210	210 210 210 210 210 209	+4 +6 +2 +8	III b II II II b4			
70. 231 71. 280 78. 093 78. 881 79. 102	A C B A A	20 7 23 8 9	. 442 . 486 . 303 9. 084 . 308	Fe Fe Air Air Air	3 0 4 2 3	$211 \\ 206 \\ 210 \\ 203 \\ 206$	209 209 208 208 208		III b			
79. 897 80. 393 80. 623 81. 178 81. 955	A A C A A	2 9 6 14 15	0. 108 . 598 . 833 . 387 2. 164	Air Air Fe Air Air	2 2 3 1 2	$211 \\ 205 \\ 210 \\ 209 \\ 209 \\ 209$	208 208 208 208 208 208		IA a			
82. 730 83. 797 87. 750 89. 398 90. 220	A A A C A	3 8 3 10 26	$\begin{array}{r} .933\\ 4.002\\ .953\\ .606\\ .427\end{array}$	Air Air Air Air Air	$2 \\ 1 \\ 1 \\ 1 \\ 2$	203 205 203 208 207	208 208 208 208 208 208					
90. 967 92. 161 92. 959 95. 178 95. 959	C A A A A	13 26 26 23 26	1. 184 . 373 3. 170 . 389 6. 170	Fe Air Air Air Air	4 2 3 3 3	$217 \\ 212 \\ 211 \\ 211 \\ 211 \\ 211$	208 208 208 209 209		e?			
97.797 6298.453 6299.227 6301.505 01.998	A A A A A	19 26 26 18 21	8.007 .666 .436 .718 .209	Fe Air Air Fe Air	5 2 3 7 2	$210 \\ 213 \\ 209 \\ 213 \\ 211$	209 210 210 211 211	+7+4	III b4 IV			
$\begin{array}{c} 02.497 \\ 02.764 \\ 05.810 \\ 06.564 \\ 09.887 \end{array}$	B A A A A	14 16 20 20 18	.709 .975 *6.024 .780 0.101	Fe Air Air Air Air	5 2 2 2 2 2	$212 \\ 211 \\ 214 \\ 216 \\ 214$	$211 \\ 211 \\ 212 \\ 212 \\ 212 \\ 213$	+4	v			
$\begin{array}{c} 10.663 \\ 14.663 \\ 15.314 \\ 15.814 \\ 18.025 \end{array}$	A B C B	$12 \\ 16 \\ 13 \\ 8 \\ 17$.848 .876 .517 6.028 .239	Air Ni Fe Fe Fe	$ \begin{array}{c} 1 \\ 4 \\ 2 \\ 1 \\ 6 \end{array} $	$215 \\ 213 \\ 203 \\ 214 \\ 214 \\ 214$	213 213 213 213 213 214	-3 +7	II b III b4			
$\begin{array}{c} 18.710 \\ 22.693 \\ 27.604 \\ 30.098 \\ 30.852 \end{array}$	A B C B C	4 19 13 12 11	.919 .907 .820 .316 1.067	Fe Ni Cr Fe	1 4 2 1 2	209 214 216 218 215	214 214 215 215 215 215	+5	III b II IA			
35.337 36.830 38.874 39.115 44.157	A A B D A	20 20 5 5 19	.554 7.048 9.096 .335 .371	Fe Fe Fe Fe	6 7 2 2 4	217 218 212 220 214	215 215 215 215 215 215	+12 +6	III b4 V b4			
$\begin{array}{r} 47.087\\ 55.036\\ 58.685\\ 62.869\\ 78.256\end{array}$	D B B B C	10 20 18 7 11	.310 .246 .898 3.090 .468	Fe Fe Cr-Fe Ni	2 4 6 2 2	223 210 213 221 212	215 215 214 214 214 211	+5	III b IA IV			
$\begin{array}{r} 80.751 \\ 6393.611 \\ 6400.005 \\ 00.326 \\ 6408.026 \end{array}$	C B B C B	19 19 17 13	.958 .820 s .217 s .538 s	Fe Fe Fe	4 7 8 2 5	207 209 212 212 212	211 211 211 211 211 211	+5 +10 +3 +8	V b III b4 III			

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A.O.B.S.λ	Proba- ble error	No.	nasion F ado R	Rowland	protor I	Correc	etion to rland	Sun_oro	Tempera- ture and
A. U. B. S. A	error	obs.	λ	Iden.	Int.	Obs.	Mean	- sun-arc	pressure classes
$\begin{array}{r} 6411.656\\ 14.995\\ 16.930\\ 19.954\\ 21.360 \end{array}$	B C C A B	20 9 11 20 21	.865 s 5.199 7.133 0.169 s .570 s	Fe Fe Fe Fe	7 1 1 4 7	$209 \\ 204 \\ 203 \\ 215 \\ 210$	211 211 211 211 211 211 211	+8 +5 +10	IV V III b
$\begin{array}{c} 30.854\\ 32.686\\ 39.085\\ 49.820\\ 55.605\end{array}$	B A B B	21 13 22 23 23	1.066 s .895 .293 s 0.033 s .820	Fe Fe Ca Ca Ca	$5\\1\\8\\6\\2$	$212 \\ 209 \\ 208 \\ 213 \\ 215$	$211 \\ 211 \\ 211 \\ 212 \\ 212 \\ 213$	+10 +13 +10 +7	III b4 II II II
$\begin{array}{c} 56.391 \\ 62.559 \\ 62.733 \\ 69.189 \\ 71.668 \end{array}$	B D B A	22 3 3 15 23	.603 .784 s .965 .408 .885 s	Fe Ca Fe Fe Ca	3 5 3 2 5	$212 \\ 225 \\ 232 \\ 219 \\ 217$	$\begin{array}{c c} 213 \\ 214 \\ 214 \\ 216 \\ 216 \\ 216 \end{array}$	$\begin{vmatrix} -6\\+8\\+8\\+8 \end{vmatrix}$	II b II
75.632 80.057 81.875 82.810 83.239	D A B B A	7 22 25 13 8	.846 .285 s 2.098 3.027 .468	Fe Air Fe Ni Air	$2 \\ 1 \\ 3 \\ 1 \\ 1 \\ 1$	$214 \\ 218 \\ 223 \\ 217 \\ 229$	217 218 218 219 219		IV b IV V
$\begin{array}{r} 86.777\\6490.790\\91.574\\92.903\\93.789\end{array}$	C A C A A	3 29 13 13 31	7.005 1.015 .800 3.130 4.004 s	Air Air Air Air Ca	0 1 1 1 6	$228 \\ 225 \\ 226 \\ 227 \\ 215$	219 220 220 221 221	+9	п
94. 995 96. 469 96. 911 98. 945 6499. 654	B A A A A	31 22 33 28 32	. 213 s . 688 7. 128 9. 168 . 880 s	Fe Fe Fe Ca	8 2 4 1 4	$218 \\ 219 \\ 217 \\ 223 \\ 226$	221 222 222 222 222 222	+14 +5 +6	II b4 II
$\begin{array}{c} 6504.\ 193\\ 08.\ 596\\ 14.\ 730\\ 16.\ 084\\ 18.\ 374 \end{array}$	D D A A B	3 5 28 20 20	. 415 . 826 . 956 . 311 s . 599 s	Air Air Air Fe Fe	$ \begin{array}{c} 0 \\ 0 \\ 2 \\ 2 \\ 2 \end{array} $	222 230 226 227 225	223 224 226 226 226 227		b
$\begin{array}{c} 23.839\\ 32.352\\ 33.946\\ 43.904\\ 46.247\end{array}$	B C C A A	$12 \\ 13 \\ 15 \\ 26 \\ 28$	4. 080 . 595 s 4. 172 s 4. 140 . 479 s	Air Air Air Air Ti-Fe	$\begin{array}{c}1\\1\\2\\2\\6\end{array}$	241 243 226 236 232	229 232 232 235 235	+8	III b
47. 692 48. 619 52. 626 55. 463 64. 197	B B B C C	$10 \\ 15 \\ 20 \\ 8 \\ 5$. 945 . 855 . 865 s . 700 . 450	Air Air Air Air	0 1 1 1 0	253 236 239 237 253	235 236 236 236 236 237	20 H H	8191.04 5191.54 \$15.71 \$15.71 \$15.74 \$10.84
69. 223 72. 083 72. 786 74. 234 75. 022	A C B C C	$28 \\ 11 \\ 15 \\ 13 \\ 12$. 460 s . 330 3. 030 . 468 s . 270 s	Fe Air Ca Fe Fe	5 1 1 1 2	237 247 244 234 234 248	238 238 238 238 238 238	+9	V IA b
$\begin{array}{r} 86.\ 317\\ 92.\ 926\\ 93.\ 881\\ 6597.\ 561\\ 6604.\ 594 \end{array}$	C A B B	13 29 29 19 17	. 550 3. 161 s 4. 121 s . 807 . 837	Ni Fe Fe Cr? Fe? Fe	$ \begin{array}{c} 1 \\ 6 \\ 4 \\ 1 \\ 1 \\ 1 \end{array} $	$233 \\ 235 \\ 240 \\ 246 \\ 243$	239 240 240 240 240 240	+13 +6	II III b
09. 118 27. 551 33. 753 43. 638 63. 451	A C A A A	27 12 27 31 30	. 360 s . 797 . 995 s . 876 s . 701 s	Fe Fe Ni Fe	3 0 2 5 3	$242 \\ 246 \\ 242 \\ 238 \\ 250$	$241 \\ 242 \\ 243 \\ 243 \\ 243 \\ 245$	$^{+1}_{-3}$	IV b V I IV b
$\begin{array}{c} 6677.\ 996\\ 6703.\ 569\\ 05.\ 108\\ 15.\ 387\\ 6717.\ 686\end{array}$	B C C D B	$31 \\ 17 \\ 19 \\ 4 \\ 20$	8. 235 s . 820 s . 352 s . 635 . 940 s	Fe Fe Cr? Fe? Ca	$5 \\ 1 \\ 1 \\ 1 \\ 5 \\ 5$	$239 \\ 251 \\ 244 \\ 248 \\ 254$	246 248 248 248 248 249	+9	III b4

TABLE 1.—A. O. B. S. solar wave lengths—Continued

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TABLE	1A.	0.	<i>B</i> . <i>S</i> .	solar	wave	lengths-	-Continued
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AOBSA	Proba-	Pa- No. or obs.	10140. 570.)	Rowland .		Correc	Correction to Rowland		Tempera- ture and
A. 0, D. S. A	error		λ	Iden.	Int.	Obs.	Mean	Jun-art	pressure classes
6721. 849 26. 667 33. 157 50. 161 52. 708	C C C B C	10 14 9 21 11	2. 096 s . 925 s . 410 . 407 s . 965 s	- Fe Fe Fe Fe	$\begin{array}{c}2\\2\\1\\3\\1\end{array}$	247 258 253 246 257	249 249 249 250 250	+10	IV b
$\begin{array}{c} 67.\ 781\\ 6772.\ 325\\ 6806.\ 849\\ 10.\ 268\\ 20.\ 375\end{array}$	B C C B B	23 17 10 21 13	8. 028 s . 568 s 7. 103 s . 519 s . 630 s	Ni Ni Fe Fe Fe	4 2 1 3 2	247 243 254 251 255	250 251 252 252 252 252	+3	I V
$\begin{array}{c} 28.\ 600\\ 6839.\ 826\\ 41.\ 344\\ 42.\ 690\\ 43.\ 658\end{array}$	В С А С В	21 8 23 9 21	. 850 s . 086 . 598 s . 945 . 913 s	Fe Fe Fe Fe	$2 \\ 1 \\ 3 \\ 1 \\ 3$	$250 \\ 250 \\ 254 \\ 255 \\ 255$	253 253 253 253 253 253		v v v
55, 169 57, 250 58, 154 62, 496 67, 221	B D A D A	$24 \\ 4 \\ 24 \\ 4 \\ 26$. 419 s . 515 . 415 . 760 . 457 s	Fe Fe Fe Air	3. 0 2 1 6	$250 \\ 265 \\ 261 \\ 264 \\ 236$	$254 \\ 254 \\ 254 \\ 254 \\ 254 \\ 254 $	+10	V
67. 545 69. 936 70. 945 71. 289 72. 247	A C A A A A	29 4 17 18 31	. 800 s . 116 1. 180 s . 532 s . 486 s	Air Air Air Air Air Air	5 7 8 10 11	255 180 235 243 239	$254 \\ 254 \\ 242 $		
72. 843 73. 795 74. 652 75. 592 76. 718	A A A A A	31 31 31 31 31 31	3. 080 s 4. 037 s . 899 s . 830 s . 958 s	Air Air Air Air Air Air	$ \begin{array}{c} 12 \\ 12 \\ 13 \\ 13 \\ 13 \\ 13 \end{array} $	$237 \\ 242 \\ 247 \\ 248 \\ 240$	243 243 243 243 243 243	0.4000	010, 20 08 <u>6</u> , 137 10, 10 19, 10 19, 10 19, 10 10 10 10 10 10 10 10 10 10 10 10 10 1
77. 637 79. 044 79. 929 83. 833 85. 756	A A A A A	30 31 34 31 31 31	. 882 s . 288 s 0. 172 s 4. 076 s 6. 000 s	Air Air Air Air Air Air	$ \begin{array}{c c} 12 \\ 12 \\ 6 \\ 10 \\ 11 \end{array} $	$245 \\ 244 \\ 243 \\ 243 \\ 243 \\ 244$	243 243 243 244 244 244		882 <u>55</u> 8 27 82 97 82 97 93 - 2917
86. 744 88. 948 89. 903 92. 372 93. 310	B A A A A	31 31 31 31 31 31	. 990 s 9. 192 s 0. 151 s . 618 s . 560 s	Air Air Air Air Air Air	12 13 14 14 15	$246 \\ 244 \\ 248 \\ 246 \\ 250$	$244 \\ 245 \\ 245 \\ 245 \\ 245 \\ 245 \\ 245$	ana Taan Marina Marina	s an an a
96. 040 96. 965 6899. 955 6900. 869 04. 118	A A A A A	30 31 31 31 31 31	. 289 s 7. 208 s 0. 199 s 1. 117 s . 362 s	Air Air Air Air Air Air	14 15 14 15 14	249 243 244 248 248 244	$246 \\ 246 \\ 246 \\ 246 \\ 246 \\ 246$	1779) 1810 1812 1819	
05. 025 08. 535 09. 432 13. 201 14. 092	A A A A A X	31 30 31 33 32	. 271 s . 783 s . 676 s . 448 s . 337 s	Air Air Air Air Air Air	14 13 13 11 11	246 248 244 247 245	246 247 247 247 247 247		
$\begin{array}{c} 14.\ 573\\ 16.\ 686\\ 18.\ 121\\ 19.\ 002\\ 23.\ 302 \end{array}$	B B A A A	20 21 33 33 33 31	. 823 s . 948 s . 370 s 9. 250 s . 553 s	Ni Fe Air Air Air	4 2 9 9 9 9	$250 \\ 262 \\ 249 \\ 248 \\ 251$	247 248 248 248 248 249	·	4001 -3004 -2004 -2004 -2004
$\begin{array}{c} 24.\ 173\\ 28.\ 729\\ 29.\ 595\\ 33.\ 615\\ 33.\ 804 \end{array}$	A A B C D	$31 \\ 21 \\ 13 \\ 5 \\ 7$. 427 s . 977 s . 840 s . 887 4. 075	Air Air Air Fe Air	9 4 4 2 2	254 248 245 272 271	249 249 249 250 250		
34. 422 35. 280 37. 703 39. 618 6940. 190	B B B B B B	$13 \\ 14 \\ 19 \\ 13 \\ 6$. 670 s . 530 s . 957 . 875 . 436	Air Air Air Air Air	2 2 2 2 2 2	248 250 254 257 246	250 250 251 251 251 251	114	

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Α .Ο.Β.S.λ	Proba- ble error	oba- ole obs.	Rowland			Correction to Rowland		Sun-are	Tempera- ture and
			λ	Iden.	Int.	Obs.	Mean		classes
6942. 152 43. 802 45. 214 47. 534 51. 248	A B B B B	$5 \\ 15 \\ 17 \\ 14 \\ 13$. 402 4. 060 . 477 . 782 s . 518	Air Air Fe Air-Fe Fe	2 3 5 5 1	250 258 263 248 270	$251 \\ 251 \\ 252 $	+10	IV
56. 426 59. 452 61. 260 78. 403 78. 862	C A A C B	7 16 16 3 13	. 660 s . 704 s . 515 s . 670 s 9. 120	Air Air Air Cr Fe	4 3 4 1 2	234 252 255 267 258	253 253 254 257 257	+4	IV
86. 580 88. 518 88. 986 90. 373 93. 517	C D B C C	14 4 14 7 10	. 833 s . 805 9. 237 s . 632 . 776	Air Fe Air Air Air Air	$3 \\ 0 \\ 3 \\ 1 \\ 2$	253 287 251 259 259	259 259 259 259 259 260		2012 201 2010 201 2010 2010 2010 2010 2010 2010 2010 2010
94. 107 98. 963 6999. 882 7003. 574 04. 747	D C C C C C C C	7 12 9 4 12	. 360 9. 223 0. 155 s . 837 . 995	Air Air Fe Si? Air	$2 \\ 2 \\ 1 \\ 1 \\ 2 \\ 2$	253 260 273 263 248	260 261 261 262 262	D S C	141 44 161 233 162 757 162 434 164 53
11. 330 22. 956 23. 504 27. 479 34. 909	D B C B C	11 8 10 10 8	. 590 s 3. 230 s . 770 s . 740 s 5. 170 s	Air Fe Air Air	2 2 2 2 2 2	260 274 266 261 261	263 265 266 266 267		
38. 219 39. 796 50. 858 56. 999 7084. 981	C B D C C	9 11 6 4 4	. 500 s . 053 s 1. 115 7. 260 5. 265	Fe Air Air Air Co	$ \begin{array}{c} 1 \\ 1 \\ 0 \\ 0 \\ 2 \end{array} $	281 267 257 261 284	267 268 269 269 271		
$\begin{array}{c} 7122,\ 206\\ 30,\ 928\\ 32,\ 988\\ 7148,\ 159 \end{array}$	D D D D	5 5 5 5	. 484 1. 204 3. 263 . 435	Ni Fe Fe Ca	4 3 1 3	278 276 275 276	275 276 276 277	±0 +14	IV II

TABLE 1.-A. O. B. S. solar wave lengths-Continued

TABLE 2.—Corrections to Rowland's wave lengths (3590-7142)

Wave length	Correction	Wave length	Correction	Wave length	Correction
3590-3650 3651-3940 3941-3952 3953-3960	-0. 141A . 140 . 141 . 142	$\begin{array}{r} 4165 - 4176 \\ 4177 - 4187 \\ 4188 - 4199 \\ 4200 - 4213 \end{array}$	$\begin{array}{r} .163\\ .162\\ .161\\ .160\end{array}$	$\begin{array}{r} 4567 - 4587 \\ 4588 - 4597 \\ 4598 - 4634 \\ 4635 - 4648 \end{array}$.172 .173 .174 .174 .173
3961-3970	.143	4214-4244	. 159	4649-4671	. 172
3971–3975 3976–3978 3979–3985 3986–3992 3993–3997	. 144 . 145 . 146 . 147 . 148	$\begin{array}{r} 4245 - 4295 \\ 4296 - 4310 \\ 4311 - 4320 \\ 4321 - 4330 \\ 4331 - 4357 \end{array}$	$\begin{array}{c} .158\\ .159\\ .160\\ .161\\ .162\end{array}$	$\begin{array}{c} 4672 - 4690 \\ 4691 - 4708 \\ 4709 - 4721 \\ 4722 - 4729 \\ 4730 - 4734 \end{array}$. 173 . 174 . 175 . 176 . 177
3998–4000 4001–4007 4008–4018 4019–4024 4025–4028	$\begin{array}{r} .149 \\ .150 \\ .151 \\ .152 \\ .153 \end{array}$	$\begin{array}{r} 4358-4373\\ 4374-4378\\ 4379-4397\\ 4398-4414\\ 4415-4426\end{array}$	$\begin{array}{r} .161 \\ .160 \\ .159 \\ .160 \\ .161 \end{array}$	$\begin{array}{r} 4735{-}4738\\ 4739{-}4744\\ 4745{-}4749\\ 4750{-}4753\\ 4754{-}4760\end{array}$. 178 . 179 . 180 . 181 . 182
$\begin{array}{r} 4029 - 4037 \\ 4038 - 4090 \\ 4091 - 4116 \\ 4117 - 4123 \\ 4124 - 4129 \end{array}$.154 .155 .156 .155 .155 .154	$\begin{array}{r} 4427-4435\\ 4436-4488\\ 4489-4500\\ 4501-4514\\ 4515-4523\end{array}$.162 .163 .164 .165 .166	$\begin{array}{r} 4761-\!$. 183 . 184 . 185 . 184 . 183
$\begin{array}{r} 4130 - 4135 \\ 4136 - 4141 \\ 4142 \\ 4143 - 4152 \\ 4153 - 4164 \end{array}$.153 .152 (1) .163 .164	$\begin{array}{r} 4524-4535\\ 4536-4550\\ 4551-4558\\ 4559-4562\\ 4563-4566\end{array}$.167 .168 .169 .170 .171	$\begin{array}{r} 4836 - 4842 \\ 4843 - 4848 \\ 4849 - 4853 \\ 4854 - 4860 \end{array}$. 182 . 181 . 180 . 179

¹ Discontinuity.

TABLE 2.—Corrections to Rowland's wave lengths (3590-7142)—Continued

Wave length	Correction	Wave length	Correction	Wave length	Correction
4861-4865 4866-4877 4878-4884 4885-4892 4893-4900	$-0.178 \\ .177 \\ .176 \\ .175 \\ .175 \\ .174$	5497-5502 5503-5506 5507-5511 5512-5515 5516-5519	. 206 . 207 . 208 . 209 . 210	$\begin{array}{c} 6513-6516\\ 6517-6519\\ 6520-6522\\ 6523-6524\\ 6525-6524\\ \end{array}$. 226 . 227 . 228 . 229 . 230
$\begin{array}{r} 4901-4907\\ 4908-4920\\ 4921-5050\\ 5051-5067\\ 5068-5080\end{array}$.173 .172 .171 .170 .169	5520-5524 5525-5528 5529-5532 5533-5537 5538-5543	$\begin{array}{r} .211\\ .212\\ .213\\ .213\\ .214\\ .215\end{array}$	$\begin{array}{c} 6529{-}6531\\ 6532{-}6534\\ 6535{-}6537\\ 6538{-}6541\\ 6542{-}6547\end{array}$. 231 . 232 . 233 . 234 . 235
$\begin{array}{c} 5081{-}5095\\ 5096{-}5110\\ 5111{-}5130\\ 5131{-}5160\\ 5161{-}5175\end{array}$.168 .167 .166 .165 .164	$\begin{array}{c} 5544{-}5565\\ 5566{-}5604\\ 5605{-}5650\\ 5651{-}5660\\ 5661{-}5681\end{array}$	$\begin{array}{r} .216\\ .217\\ .218\\ .218\\ .217\\ .216\end{array}$	$\begin{array}{c} 6548 - 6553 \\ 6554 - 6566 \\ 6567 - 6581 \\ 6582 - 6592 \\ 6593 - 6604 \end{array}$. 236 . 237 . 238 . 239 . 240
$5176-5188 \\ 5189-5200 \\ 5201-5212 \\ 5218 \\ 5224-5225$.163 .162 .161 $(^1)$.155	$\begin{array}{c} 5682{-}5700\\ 5701{-}5725\\ 5726{-}5737\\ 5738{-}5748\\ 5749{-}5762\end{array}$	$\begin{array}{r} .\ 215\\ .\ 214\\ .\ 213\\ .\ 212.\\ .\ 211\end{array}$	$\begin{array}{c} 6605-6617\\ 6618-6631\\ 6632-6643\\ 6644-6656\\ 6657-6669\end{array}$	$\begin{array}{c} . 241 \\ . 242 \\ . 243 \\ . 244 \\ . 245 \end{array}$
$\begin{array}{c} 5226-5230\\ 5231-5234\\ 5235-5238\\ 5239-5242\\ 5243-5246\end{array}$.156 .157 .158 .159 .160	5763-5772 5773-5795 5805-5819 5820-5870 5871-5882	$\begin{array}{r} .\ 210\\ .\ 209\\ .\ 214\\ .\ 213\\ .\ 214\end{array}$	$\begin{array}{c} 6670-6681\\ 6682-6695\\ 6696-6718\\ 6719-6738\\ 6739-6767\end{array}$	$\begin{array}{c} . 246 \\ . 247 \\ . 248 \\ . 249 \\ . 250 \end{array}$
$\begin{array}{c} 5247 - 5250 \\ 5251 - 5254 \\ 5255 - 5258 \\ 5259 - 5262 \\ 5263 - 5266 \end{array}$.161 .162 .163 .164 .165	5883-5894 5895-5937 5938-5972 5973-5991 5992-6007	$\begin{array}{r} .\ 215\\ .\ 216\\ .\ 217\\ .\ 218\\ .\ 217\end{array}$	$\begin{array}{c} 6768-6794\\ 6795-6822\\ 6823-6847\\ 6848-6869\\ 6870\\ \end{array}$	$\begin{array}{c} . 251 \\ . 252 \\ . 253 \\ . 254 \\ (1) \end{array}$
5267-5271 5272-5275 5276-5280 5281-5286 5287-5291	.166 .167 .168 .169 .170	$\begin{array}{c} 6008-6024\\ 6025-6044\\ 6045-6066\\ 6067-6084\\ 6085-6104 \end{array}$	$\begin{array}{r} .\ 216\\ .\ 215\\ .\ 214\\ .\ 213\\ .\ 212\end{array}$	$\begin{array}{r} 6870-6872\\ 6873-6879\\ 6880-6886\\ 6887-6895\\ 6896-6907\end{array}$	242 243 244 244 245 245 246
$\begin{array}{c} 5292 - 5297 \\ 5298 - 5302 \\ 5303 - 5307 \\ 5308 - 5311 \\ 5312 - 5316 \end{array}$	$\begin{array}{r} .171\\ .172\\ .173\\ .173\\ .174\\ .175\end{array}$	$\begin{array}{c} 6105-6123\\ 6124-6162\\ 6163-6176\\ 6177-6189\\ 6190-6196\end{array}$	$\begin{array}{r} .211\\ .210\\ .211\\ .212\\ .212\\ .211\end{array}$	$\begin{array}{c} 6908-6913\\ 6914-6920\\ 6921-6929\\ 6930-6937\\ 6938-6943\\ \end{array}$	$\begin{array}{c} . 247 \\ . 248 \\ . 249 \\ . 250 \\ . 251 \end{array}$
5317 - 5320 5321 - 5324 5325 - 5329 5330 - 5333 5334 - 5338	.176 .177 .178 .179 .180	$\begin{array}{c} 6197 - 6203 \\ 6204 - 6240 \\ 6241 - 6263 \\ 6264 - 6272 \\ 6273 - 6292 \end{array}$	$\begin{array}{r} . 210 \\ . 209 \\ . 210 \\ . 209 \\ . 209 \\ . 208 \end{array}$	6944-6952 6953-6959 6960-6964 6965-6969 6970-6974	$\begin{array}{r} .\ 252 \\ .\ 253 \\ .\ 254 \\ .\ 255 \\ .\ 256 \end{array}$
5339-5342 5343-5346 5347-5350 5351-5354 5355-5358	$\begin{array}{c} .181\\ .182\\ .183\\ .183\\ .184\\ .185\end{array}$	$\begin{array}{c} 6293-6297\\ 6298-6300\\ 6301-6303\\ 6304-6307\\ 6308-6315\end{array}$	$\begin{array}{c} .\ 209\\ .\ 210\\ .\ 211\\ .\ 212\\ .\ 213\end{array}$	6975–6980 6981–6985 6986–6990 6991–6996 6997–7001	257 258 259 260 261
$\begin{array}{c} 5359{-}5361\\ 5362{-}5365\\ 5366{-}5369\\ 5370{-}5373\\ 5374{-}5376\end{array}$.186 .187 .188 .189 .190	$\begin{array}{c} 6316 - 6327 \\ 6328 - 6355 \\ 6356 - 6361 \\ 6362 - 6368 \\ 6369 - 6375 \end{array}$	$\begin{array}{r} . 214 \\ . 215 \\ . 214 \\ . 213 \\ . 212 \end{array}$	7002-7006 7007-7010 7011-7016 7017-7022 7023-7028	262 263 264 265 265 266
5377-5379 5380-5383 5384-5386 5387-5389 5390-5393	.191 .192 .193 .194 .195	$\begin{array}{c} 6376-6444\\ 6445-6453\\ 6454-6459\\ 6460-6463\\ 6460-6463\\ 6464-6467\end{array}$	$\begin{array}{r} . 211 \\ . 212 \\ . 213 \\ . 214 \\ . 215 \end{array}$	7029–7036 7037–7049 7050–7061 7062–7073 7074–7085	$ \begin{array}{r} 267 \\ 268 \\ 269 \\ 270 \\ 271 \end{array} $
$\begin{array}{c} 5394-5396\\ 5397-5399\\ 5400-5402\\ 5403-5405\\ 5406-5408\end{array}$.196 .197 .198 .199 .200	$\begin{array}{c} 6468-6473\\ 6474-6477\\ 6478-6482\\ 6483-6486\\ 6487-6490\\ \end{array}$	$\begin{array}{r} .\ 216\\ .\ 217\\ .\ 218\\ .\ 219\\ .\ 220\end{array}$	7086–7096 7097–7107 7108–7118 7119–7129 7130–7141	. 272 . 273 . 274 . 275 . 276
5409–5412 5413–5422 5423–5438 5439–5487 5488–5406	201 202 203 204 205	$\begin{array}{r} 6491-6495\\ 6496-6499\\ 6500-6504\\ 6505-6508\\ 6509-6512\end{array}$	$\begin{array}{c} . 221 \\ . 222 \\ . 223 \\ . 224 \\ . 225 \end{array}$	7142	. 277

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¹ Discontinuity.

WASHINGTON, May 23, 1928.

Standard Solar Ways Lendis

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