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# *Atlas of the Spectrum of a Platinum/Neon Hollow-Cathode Reference Lamp in the Region 1130–4330 Å*

Volume 97

Number 1

January-February 1992

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The spectrum of a platinum hollow-cathode lamp containing neon carrier gas was recorded photographically and photoelectrically with a 10.7 m normal-incidence vacuum spectrograph. Wavelengths and intensities were determined for about 5600 lines in the region 1130–4330 Å. An atlas of the spectrum is given, with the spectral lines marked and their intensities, wavelengths, and classifications listed. Lines of impurity species are also identified. The uncertainty of the photographically measured wavelengths is estimated to be  $\pm 0.0020$  Å. The uncertainty of lines measured in the photoelectric scans is

0.01 Å for wavelengths shorter than 2030 Å and 0.02 Å for longer wavelengths. Ritz-type wavelengths are given for many of the classified lines of Pt II with uncertainties varying from  $\pm 0.0004$  to  $\pm 0.0025$  Å. The uncertainty of the relative intensities is estimated to be about 20%.

**Key words:** hollow-cathode lamp; neon; platinum; spectral atlas; spectrum; wavelength.

**Accepted:** November 21, 1991

## 1. Introduction

The deployment of the Hubble Space Telescope (HST) on April 24, 1990, launched a new era in astronomy. With the HST, stars and other astronomical objects are being observed with unprecedented clarity. The improvement over ground-based telescopes is most significant in the ultraviolet region of the spectrum, where the earth's atmosphere absorbs most of the radiation. Although the much-publicized spherical aberration in the HST's primary mirror [1] greatly reduces the quality of star images, many experiments of a spectroscopic nature are not severely affected because they do not require high spatial resolution. For example, for the Goddard High Resolution Spectrograph (GHRS), the highest resolution spectrograph on HST, the spherical aberration in the primary mirror does not degrade the spectral resolution noticeably when the small science aperture is used [2]. However, because of enlargement of the point spread function,

the exposure time must be increased by a factor of about 5 to produce the signal-to-noise ratio of prelaunch expectations [2]. Nevertheless, spectra of very high quality have been obtained [2].

The region of observation of GHRS is 1100–3200 Å. In its echelle mode it has a resolving power of 90,000 and a wavelength accuracy of a few parts in  $10^6$ . Line-of-sight velocities of stellar objects can thus be determined to an accuracy of about 1 km/s. In order to achieve this accuracy, of course, an accurate wavelength scale must be established. This is accomplished by illuminating the spectrograph with an onboard platinum/neon hollow-cathode lamp during periods in which stellar observations are not being made [3]. The use of a Pt/Ne lamp for this purpose and its space-qualified design are due to Mount, Yamasaki, Fowler, and Fastie [4], who originally suggested it for wavelength calibration of the International Ultraviolet Explorer (IUE) satellite.

To achieve the accuracy for which GHRS was designed, the calibration wavelengths must be accurate to about  $0.002 \text{ \AA}$ . However, tests carried out in our laboratory in 1983 indicated that the best available wavelengths for Pt [5] had errors ranging to about  $0.015 \text{ \AA}$ . We thus began a program to measure the spectra emitted by a Pt/Ne hollow-cathode lamp similar to the one to be used with GHRS. This work was carried out with our high resolution  $10.7 \text{ m}$  normal-incidence vacuum spectrograph at NIST. At about the same time Engleman [6] recorded the spectrum of a Pt hollow-cathode lamp with a Fourier-transform spectrometer. He obtained accurate wavelengths for 320 lines of Pt I in the region  $2200\text{--}7220 \text{ \AA}$ , optimized the energy level values, and calculated accurate Ritz-type wavelengths for 81 lines in the region  $1724\text{--}2250 \text{ \AA}$ . Many of these lines were used in calibrating our grating measurements.

Some of the results of our work have appeared in two previous papers. In the first [7] we determined accurate values for 100 energy levels of Pt II by combining our new grating measurements for over 500 Pt II lines in the ultraviolet with measurements of lines at longer wavelengths made by Engleman by Fourier transform spectroscopy. In the second [8] we reported wavelengths with accuracies of  $0.002 \text{ \AA}$  or better for some 3000 lines emitted by a Pt/Ne lamp in the region  $1032\text{--}4100 \text{ \AA}$ . In this second report we also provided relative intensities of the spectral lines of the Pt/Ne lamp that were determined by recording the spectra photoelectrically with the same spectrograph used for the wavelength measurements.

Our wavelengths for the Pt/Ne lamp are currently being used for calibration of GHRS as well as for wavelength calibration of the Faint Object Spectrograph on HST, which uses a Pt-Cr/Ne hollow-cathode lamp for both wavelength and radiometric calibration [9]. Our data are also being used for revised calibrations of spectra from the IUE satellite [10], and for calibration of spectra obtained with sounding rockets, which also use on-board Pt/Ne hollow cathode lamps [11]. In a different type of application, the data are being used to interpret the spectra of stars that contain Pt in anomalously high abundances [12].

In the present paper we present a comprehensive report of our observations of the Pt/Ne hollow-cathode lamp. For completeness we give a full account of the experimental work and data analysis. Some of this information has been given in our previous papers.

Our results are presented in the form of an atlas of the spectrum emitted by a Pt/Ne hollow-cathode lamp in the region  $1130\text{--}4330 \text{ \AA}$ . The atlas consists of plots of the spectrum accompanied by tables that include the wavelengths, wave numbers, intensities, and identifications or classifications where known for more than 5600 lines. We have attempted to provide the best available wavelength data, substituting values from the literature or calculated Ritz-type wavelengths where these are more accurate than our measurements.

The line list developed in this work was communicated to J. Blaise and J.-F. Wyart of the Laboratoire Aimé Cotton, Orsay, France, who have used it to substantially extend the energy level analysis of Pt II. Based on our measurements they have located nearly 150 new Pt II levels. Their report on the analysis appears as a companion paper in the same issue of this journal [13]. Blaise and Wyart have also located about 100 new levels of Pt I. The new line identifications for Pt I and II have been provided to us and are incorporated in the atlas.

The data included in this atlas should be of use not only for astronomical spectroscopy but also for the calibration of general laboratory spectra obtained with medium to high resolution diffraction grating spectrographs. No other source provides such a dense and complete coverage of this spectral region with lines suitable for use as reference wavelengths. The Pt/Ne hollow cathode is easy to operate and is commercially available at moderate cost.

## 2. Photographic Observations

Our observations were made with the  $10.7 \text{ m}$  normal-incidence vacuum spectrograph at the National Institute of Standards and Technology. Two different gratings were used, the first blazed at  $1200 \text{ \AA}$  in first order and the second blazed at  $3000 \text{ \AA}$  in first order. Both gratings were ruled with 1200 lines/mm. All measurements were made in the first order, the plate factor being  $0.78 \text{ \AA/mm}$ . The slit width was  $0.023 \text{ mm}$ . With this slit width the resolving limit throughout the region of observation was about  $0.020 \text{ \AA}$ . Photographic exposures were made on Kodak SWR plates.<sup>1</sup>

<sup>1</sup> Certain commercial equipment, instruments, or materials are identified in this paper to specify adequately the experimental procedure. Such identification does not imply recommendation or endorsement by the National Institute of Standards and Technology, nor does it imply that the materials or equipment identified are necessarily the best available for the purpose.

Two different light sources were used. The first was a windowless, demountable hollow-cathode lamp having a solid copper cathode containing a helical platinum wire and some chips of silicon and germanium. The general design of the lamp was similar to that of Reader and Davis [14]. In the version used in the present work the O-ring assembly at the front of the lamp was replaced by a large ball joint by which the lamp could be connected directly to the spectrograph. The lamp was operated in series with a 300  $\Omega$  ballast resistor at a dc voltage of 250 V and a current of 90 mA. The cathode was cooled with flowing water. The carrier gas consisted of flowing helium with a trace of neon at a total pressure of approximately 266 Pa (2 Torr). With this gas mixture the spectra of both Cu and Pt could be excited simultaneously. This could not be accomplished when only a single gas was used. Exposure times for this lamp were about 15 min.

The second source was a sealed hollow-cathode lamp similar to the one used by GHRS. It has a platinum hollow cathode with neon carrier gas and is sealed with a magnesium fluoride window. The lamp was manufactured by the Westinghouse Corporation (Model WL34045). It was connected to the spectrograph by a quick-disconnect flange. The cathode was located 215 mm from the slit. The lamp was operated with a 5000  $\Omega$  ballast resistor at a dc voltage of 310 V and a current of 20 mA. Exposure times ranged from 2 to 150 min.

In the first phase of the wavelength reductions of the photographic data, the spectra of Pt observed with the demountable Pt-Cu lamp were measured with respect to lines of Cu II, Si I, Si II, Ge I, Ge II, Ne I, and Ne II to determine accurate wavelengths for a select group of Pt lines. Wavelengths for Cu II were Ritz values derived from the level values of Ross [15]. Wavelengths for most Ne I and II lines above 2780  $\text{\AA}$  were taken from the Fourier-transform measurements of Palmer and Engleman [16]. Wavelengths for other Ne II lines above 2780  $\text{\AA}$  and all Ne II lines below this wavelength were Ritz values given by Persson [17]. Ne I, Si, and Ge wavelengths were taken from the compilation of reference wavelengths by Kaufman and Edlén [18]. The measurements made with the demountable Pt-Cu lamp provided accurate values for about 1500 lines of Pt I and II extending from 1032 to 2885  $\text{\AA}$ .

In the second phase of the reductions the spectra of all lines observed with the sealed Pt/Ne lamp were measured with respect to the above group of Pt lines, lines of Ne I and II, and lines of Pt I reported by Engleman [6]. In the region above

2885  $\text{\AA}$ , our reference spectra consisted solely of lines of Ne I, Ne II, and Pt I with wavelengths taken from the sources cited above.

Next, our values for lines of Pt II with known classifications were combined with values for classified lines of Pt II measured by Engleman by means of Fourier-transform spectroscopy to determine accurate values for 28 even and 72 odd energy levels of Pt II [7]. Using these level values we calculated Ritz-type wavelengths for almost all of the classified lines of Pt II. For some of these levels the energy or  $J$  value has been revised as a result of the work of Blaise and Wyart [13]. For those levels that have not been changed, the Ritz values have been substituted for the measured values in the final list of wavelengths.

### 3. Photoelectric Observations

To determine the relative intensities of lines emitted by the Pt/Ne lamp and to observe lines weaker than those recorded on the photographic plates, we recorded the spectrum by translating an exit slit and photomultiplier tube along the focal curve of the 10.7 m vacuum spectrograph. The entrance and exit slit widths were 0.050 mm. The line intensities were measured by photon counting. Signals from the photomultiplier were amplified and processed by a discriminator and logarithmic ratemeter. The analog output signal from the ratemeter was sampled at 1 Hz by a computer, which digitized and stored the data. This acquisition rate corresponded to a wavelength interval of 0.0086  $\text{\AA}$  per sample. Prior to each scan the analog response of the ratemeter was calibrated by using a pulse generator to simulate the amplified pulse signal from the photomultiplier tube. The response of the ratemeter was digitized and recorded for pulse frequencies ranging from 10/s to 10<sup>6</sup>/s by decades.

The resolution limit for the scans was about 0.07  $\text{\AA}$ . The spectrum was scanned in overlapping 650  $\text{\AA}$  segments, each segment corresponding to a different rotational setting of the grating. Each scan lasted 20 h. Two scans were made for each region above 1685  $\text{\AA}$ , the first a normal scan and the second a scan at reduced sensitivity to record very intense lines that were saturated at normal recording conditions. The sensitivity was reduced by introducing a one decade offset in the logarithmic ratemeter. In addition, for the region above 2000  $\text{\AA}$ , the source intensity was attenuated by reflecting the lamp from an uncoated glass plate.

Four different Pt/Ne lamps were used in the course of the experiments. Two lamps were used

for the photographic exposures. One of these and two additional ones were used for the photoelectric scans. The longest use of any lamp was during the photoelectric scans, where one of the lamps was run for about 250 h. After this time the cavity of the cathode had become noticeably enlarged.

The position and intensity of each spectral line in the photoelectric scans was determined by using a computer line-finding algorithm. First, the recorded signal at each point in the spectrum was converted to absolute counts/s by using the calibration information mentioned above. Then these data were scanned by the computer to locate peaks in the spectrum. The position of each peak was determined by calculating the quadratically smoothed first derivative of the data in the vicinity of the maximum intensity point and linearly interpolating the zero crossing of the derivative. The wavelength was then calculated by making a linear fit of wavelength versus position for the local spectral region, using as standards four lines accurately measured from the photographic observations on either side of the line to be determined.

The intensities derived from the raw data for each scan were adjusted to produce a consistent set of values over the whole spectral region. First, using the measured intensities for lines of moderate strength in the overlapping regions of the various scans, a set of multiplicative factors was determined to bring the separate scans onto the same relative scale. Then the spectral response of the spectrograph/detector combination as a function of wavelength was calibrated by using accurate radiance values for about 80 lines of platinum measured by Klose [19] in a similar Pt/Ne hollow-cathode lamp. All of the spectral data were corrected for this instrumental response. Thus the intensities plotted in the atlas are on a true relative scale.

The number of lines observed by photon counting was much greater than observed photographically. Whereas the weakest photographic lines produced count rates of about 500 photons/s, lines having signals as low as about 10 photons/s could be observed photoelectrically. The most intense lines produced counts of about 2,000,000 photons/s. In all scans we observed a residual background count in excess of the photomultiplier dark count. This background was only a few counts/s at low wavelengths but increased to about 60 counts/s at the highest wavelengths. This increasing background is apparent in the atlas plots. The background count has been subtracted from the measured line intensities printed in the table so

that the value reported accurately reflects the count rate due to the spectral line.

#### 4. Description of the Atlas

The atlas is a series of tables and plots that provides a comprehensive description of the spectrum of the Pt/Ne hollow-cathode lamp in the region 1128–4333 Å. Each page of plots depicts a 32 Å section of the spectrum. Every spectral line for which a wavelength and intensity have been determined is indicated with a tic mark at the bottom of the plot. The wavelengths, wave numbers, and relative intensities for these lines are listed in the table on the page facing the plot.

The wavelengths and intensities of Rowland ghosts (spurious lines caused by imperfections in the ruling of the grating) were predicted from the known properties of the gratings. Ghost lines are marked on the plots with a carat instead of a tic mark to distinguish them from true spectral lines. They are not listed in the table.

Wavelengths of lines measured on our photographic plates, taken from the literature, or calculated from optimized Pt II energy levels are given to four decimal places. Lines measured in the photoelectric data only are given to two decimal places. Wavelengths below 2000 Å are given in vacuum; wavelengths above 2000 Å are given in air. For lines originally observed in vacuum, conversion of the wavelengths from vacuum to standard air was carried out by using the three-term formula of Peck and Reeder [20] for the index of refraction of air.

Also listed in the table under the column heading CODE are the sources for wavelengths of various lines emitted by the Pt/Ne lamp that we have taken from the literature, mainly Pt I, Ne I, and Ne II. Most of these lines were used as wavelength standards. Literature values were also substituted for lines of impurity species such as H I, C I, O I, Si I, Al I, and Al II. The presence of additional impurity lines of Mg I, Mg II, Fe I, Cr I, Pd I, Rh I, Au I, Ag I, Ni I, Ca I, and Ca II were subsequently pointed out by J. Blaise. These lines are identified in the table. Literature values for their wavelengths have been substituted only for Ca II and Fe I.

The intensity of impurity lines varies greatly from lamp to lamp. For example, we did not observe the intense Al I lines at 3944 and 3961 Å on our photographic plates. However, in a lower wavelength exposure using a different lamp the normally less intense lines at 3082 and 3092 Å did appear. For this reason we have given no intensities for the impurity lines.

The energy level designations for classified lines of Pt I and II correspond to the integer parts of the level energies and are given with the even parity level first. Classifications and wavelengths for Pt I lines with CODES D and E were taken from Engleman [6]. Pt I lines with CODE N and Pt II lines with CODE K are newly classified by Blaise and Wyart [13]; the wavelengths are from the present work. Classifications for other Pt II lines were taken from Shenstone [5], with level values given by Reader, Acquista, Sansonetti, and Engleman [7]; a number given in the CODE column is the wavelength uncertainty of the Ritz wavelength in units of  $0.0001 \text{ \AA}$  (see Sec. 5).

The intensities in the atlas are a uniform set of relative values covering the entire region of observation. For lines that were blended on the photoelectric scans but resolved or nearly resolved on the photographic exposures, the intensities were estimated visually from the photographic plates by comparison with nearby well-resolved lines. In a few places a real spectral line is blended with a grating ghost. This is noted with an M in the CODE column in the table. The intensities measured for such lines are probably affected by the presence of the ghost. As mentioned, the spectral sensitivity of the spectrometer and detector combination was taken into account by using the accurate radiance values of Klose [19] for about 80 of the lines to normalize the observations. From the reproducibility of our measurements and comparisons with the data of Klose we estimate the relative intensities for a given species (element and stage of ionization) to be accurate to about 20%. A prime factor in possible variation of the relative intensities is the length of time that a particular lamp has been used. Over many hours of use the intensities of the Ne lines are observed to change relative to the Pt lines. However, for a given atom and ionization stage the relative intensities should be reliable within our estimated uncertainty. For most lines the present intensities are identical to those given by Reader, Acquista, Sansonetti, and Sansonetti [8]. The intensities of a few lines have been slightly revised in the present work.

Our relative intensities for lines emitted by the Pt/Ne lamp are potentially useful for calibration of the spectral response of spectrographic systems in other laboratories. In general, the values are sufficiently reliable to provide a good semi-quantitative calibration. Of course the accuracy that can be obtained is limited by the degree to which other Pt/Ne lamps might vary from those we used. We found only small variations in the relative intensities

of lines in our lamps, all of which were purchased separately over a 5 year period. Nevertheless, it is not certain that other lamps would exhibit identical properties. In particular, comparison of lines in the  $1130\text{--}1300 \text{ \AA}$  region with lines in higher wavelength regions could be affected by variation in the low wavelength transmission of the magnesium fluoride windows of different lamps. Since we used only a small number of lamps and did not scan each lamp over the entire spectral region, we can make no definitive statement regarding lamp to lamp variation. Further investigation would be needed to evaluate the importance of such systematic variations.

## 5. Accuracy of Wavelengths

Our estimate of the uncertainty of the photographically measured wavelengths is based on several considerations:

- The standard deviation of our polynomial fits for the Cu II reference lines in the Pt/Cu lamp was typically  $0.0010 \text{ \AA}$ .
- The standard deviation of our polynomial fits for the Pt lines used as internal standards for measurements in the Pt/Ne lamp was typically  $0.0015 \text{ \AA}$ .
- A comparison of a group of about 100 lines measured by different operators on different plates and taken with different grating rotations in the region  $1470\text{--}1520 \text{ \AA}$  showed an average deviation of  $0.0001 \text{ \AA}$  and an rms difference of  $0.0014 \text{ \AA}$ . In general, our separate measurements of the wavelengths of individual lines agreed to about this level of accuracy.
- A comparison of the wavelengths of 37 lines of Pt II in the region  $2247\text{--}3700 \text{ \AA}$  that were measured in this work and independently by Engleman [7] shows an average deviation of  $0.0003 \text{ \AA}$  and an rms difference of  $0.0019 \text{ \AA}$ .
- For the 508 lines of Pt II whose wavelengths can be calculated from the optimized level values, the rms difference between the calculated and observed wavelengths is about  $0.0015 \text{ \AA}$ .
- A comparison of our measured wavelengths for impurity lines appearing in the Pt/Ne lamp with standard wavelengths for these lines shows an average deviation of  $0.0003 \text{ \AA}$  and an rms difference of  $0.0015 \text{ \AA}$ .

Based on these comparisons we estimate an uncertainty of  $\pm 0.0020 \text{ \AA}$  for the wavelengths measured photographically.



As mentioned above, the wavelengths of classified lines of Pt II in the atlas which have numbers in the CODE column are those derived from the optimized level values. The uncertainties of these wavelengths are taken to be the square root of the sum of the squares of the uncertainties of the combining levels as given by Reader, Acquista, Sansonetti, and Engleman [7]. They are listed in the far right column under the heading CODE in units of 0.0001 Å.

The uncertainties of the photoelectrically measured lines were estimated by comparing the measured wavelengths of Pt II lines observed only in the photoelectric scans with calculated Ritz wavelengths for the same lines. The standard deviation of the differences was about 0.006 Å for lines below 2030 Å and about 0.015 Å for lines at longer wavelengths. Based on these comparisons we estimate the uncertainty to be  $\pm 0.01$  Å for lines below 2030 Å and  $\pm 0.02$  Å for lines above 2030 Å.

The uncertainties of lines whose wavelengths have been taken from the literature are discussed in some detail in the notes to the atlas. Most of these uncertainties are less than 0.001 Å and virtually all are less than 0.002 Å.

The cathodes of the lamps used in this work and with GHRS contain isotopes of Pt in their natural abundances. Some lines of Pt I and II show appreciable isotope and magnetic hyperfine structure (hfs). At the resolution of our spectrograph (and also GHRS) almost all Pt lines appear sharp and symmetric. A few lines show evidence of unresolved structure and appear wide, hazy, or asymmetric on the photographic plates. These lines are noted (W, H, L, or S) adjacent to their intensities in the atlas. Lines showing partially resolved structure are noted in the atlas as being complex (C). A few hyperfine patterns occurred in the photographic data as three fully resolved features and were measured as separate lines.

For GHRS and other instruments with resolving power of  $10^5$  or less, the existence of hfs in some lines should present no problem in using the present list of Pt lines for wavelength calibration. To achieve the highest accuracy, lines with notations indicating detectable unresolved structure should not be used. For instruments with resolving limits significantly below 0.02 Å, structure may be observed in many additional Pt lines, and our present wavelength list may not be adequate for calibration purposes. Thus, for calibration of spectrographs having much higher resolution, it may be desirable to develop calibration wavelengths based

on a lamp whose cathode contains a single even isotope of Pt.

### Acknowledgments

This investigation was undertaken at the suggestion of William C. Martin, who realized that the hollow-cathode spectrum of platinum would probably have to be newly measured in order for the Goddard High Resolution Spectrograph to meet its design goals. His encouragement and suggestions throughout the work are gratefully acknowledged. Our photoelectric scans of the Pt/Ne lamp on the 10.7 m spectrograph owe much of their success to suggestions of Richard Deslattes regarding photon counting techniques. We thank him for lending us his expertise as well as much of the equipment required to carry out the experiment. Many of the impurity lines in our list were identified by Jean Blaise. We thank him and Jean-François Wyart for making available their new classifications in Pt I and Pt II for inclusion in the atlas. This work was supported in part by the National Aeronautics and Space Administration.

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## Spectral Atlas of a Platinum/Neon Hollow-Cathode Reference Lamp

Wavelength Å		Wavelength Å	
1120.....	10	2800.....	117
1200.....	15	2900.....	123
1300.....	21	3000.....	129
1400.....	27	3100.....	135
1500.....	33	3200.....	141
1600.....	39	3300.....	147
1700.....	47	3400.....	153
1800.....	53	3500.....	159
1900.....	59	3600.....	167
2000.....	67	3700.....	173
2100.....	73	3800.....	179
2200.....	79	3900.....	185
2300.....	85	4000.....	191
2400.....	91	4100.....	197
2500.....	97	4200.....	203
2600.....	103	4300.....	209
2700.....	109		

## Explanatory Notes

Wavelengths are given in Å. Wave numbers are given in  $\text{cm}^{-1}$ . Energy level designations for the classified lines of Pt I and II correspond to the integer parts of the level energies and are given with the even parity level first. A letter appearing in the CODE column indicates the source of a literature value reported for the wavelength or a note pertaining to the line. A number appearing in the CODE column is the uncertainty of the Pt II wavelength determined from the optimized Pt II energy levels (Ritz wavelength) in units of 0.0001 Å.

The following protocols were used in substituting literature values for our measured wavelengths. For each spectrum the various literature sources are listed in order of preference. For all doubly-classified lines our experimental wavelength is given.

## Pt I

- 1) Ritz wavelength from Table 4 of R. Engleman, Jr., *J. Opt. Soc. Am. B* 2, 1934 (1985).
- 2) Measured wavelength from Table 1 of R. Engleman, Jr., *J. Opt. Soc. Am. B* 2, 1934 (1985).

## Pt II

- 1) Wavelength calculated from the optimized level values given by J. Reader, N. Acquista,

C. J. Sansonetti, and R. J. Engleman, Jr., *J. Opt. Soc. Am. B* 5, 2106 (1988) except where the energy or  $J$  value of one of the combining levels was changed by J. Blaise and J.-F. Wyart, *J. Res. Natl. Inst. Stand. Technol.* 97, 217 (1992).

## Ne I

- 1) B. A. Palmer and R. Engleman, Jr., Los Alamos National Laboratory Rep. 9615, National Technical Information Service, Springfield, VA (1983) except for a few lines that may be blended with lines of thorium.
- 2) V. Kaufman and B. Edlén, *J. Phys. Chem. Ref. Data* 3, 825 (1974).
- 3) K. Burns, K. Adams, and J. Longwell, *J. Opt. Soc. Am.* 40, 6 (1950).

## Ne II

- 1) B. A. Palmer and R. Engleman, Jr., Los Alamos National Laboratory Rep. 9615, National Technical Information Service, Springfield, VA (1983) except for a few lines that may be blended with lines of thorium.
- 2) Ritz wavelength from W. Persson, *Phys. Scr.* 3, 133 (1971).

## Fe I

- 1) R. C. M. Learner and A. P. Thorne, *J. Opt. Soc. Am. B* **5**, 2045 (1988).
- 2) T. R. O'Brian, M. E. Wickliffe, J. E. Lawler, W. Whaling, and J. W. Brault, *J. Opt. Soc. Am. B* **8**, 1185 (1991).
- 3) H. M. Crosswhite, *J. Res. Natl. Bur. Stand. (U.S.)* **79A**, 17 (1975).

Line character descriptors (appear to right of intensity):

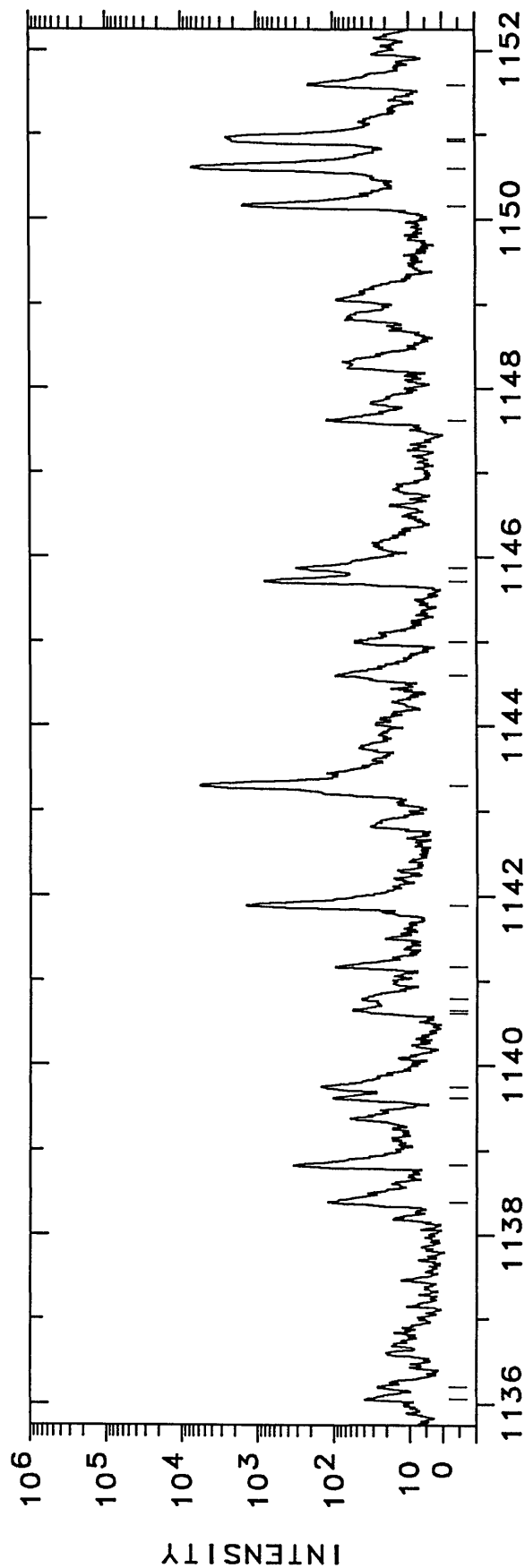
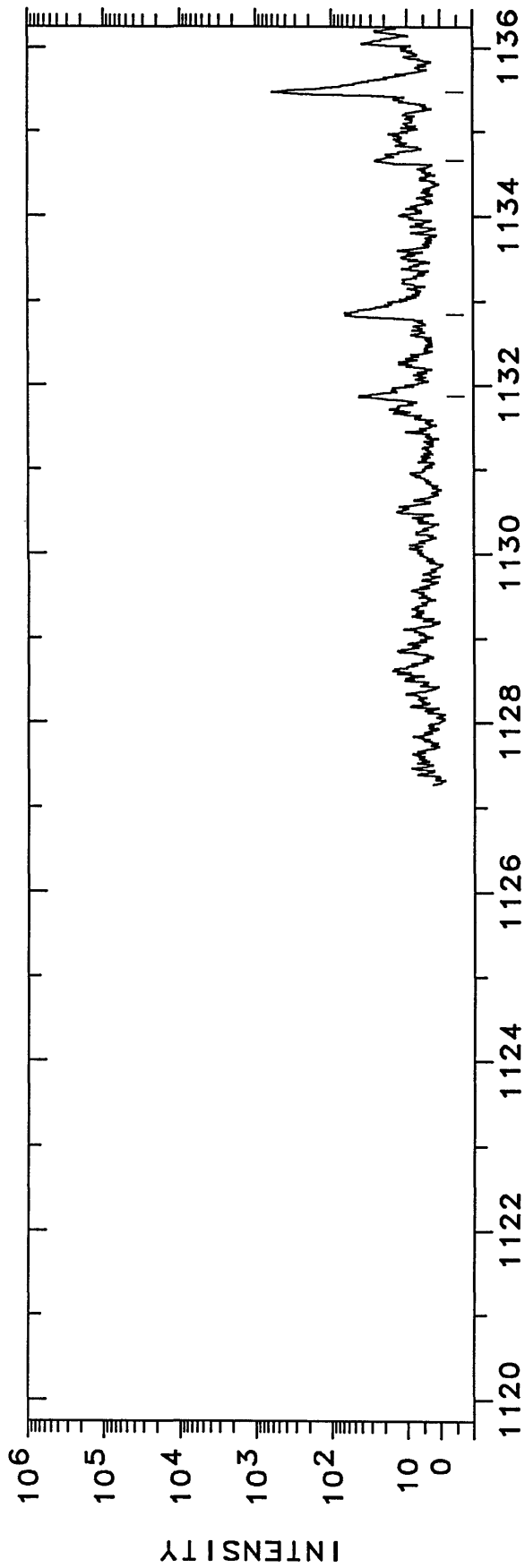
- C – Complex
- D – Double; central position of two close lines not resolved on the measuring comparator
- H – Hazy
- L – Asymmetric, tail toward longer wavelengths
- P – Perturbed by close line
- S – Asymmetric, tail toward shorter wavelengths
- U – Unresolved from close line; shoulder on stronger line
- W – Wide

## CODES:

- A – Doubly classified line. The wavelength is the present experimental value.
- B – V. Kaufman and B. Edlén, *J. Phys. Chem. Ref. Data* **3**, 825 (1974). Uncertainty is less than 0.002 Å.
- C – Value determined from optimized Ne II level values; W. Persson, *Phys. Scr.* **3**, 133 (1971). For lines below 2000 Å the uncertainty in wavelength corresponds to a wave number uncertainty of about 0.03 cm<sup>-1</sup>, which is 0.0004 Å at 1200 Å and 0.001 Å at 2000 Å. The uncertainty for lines above 2000 Å appears to be about 0.002 Å.
- D – Value determined from optimized Pt I level values; R. Engleman, Jr., *J. Opt. Soc. Am. B* **2**, 1934 (1985). The wavelength uncertainty is 0.0005 Å.
- E – R. Engleman, Jr., *J. Opt. Soc. Am. B* **2**, 1934 (1985). The wavelength uncertainty corresponds to a wave number uncertainty of 0.01 cm<sup>-1</sup>, which is 0.0005 Å at 2250 Å and 0.0017 Å at 4095 Å.
- F – Value determined from optimized Al I level values; K. B. S. Eriksson and H. B. S. Isberg, *Ark. Fys.* **23**, 527 (1963). Uncertainty is less than 0.002 Å.

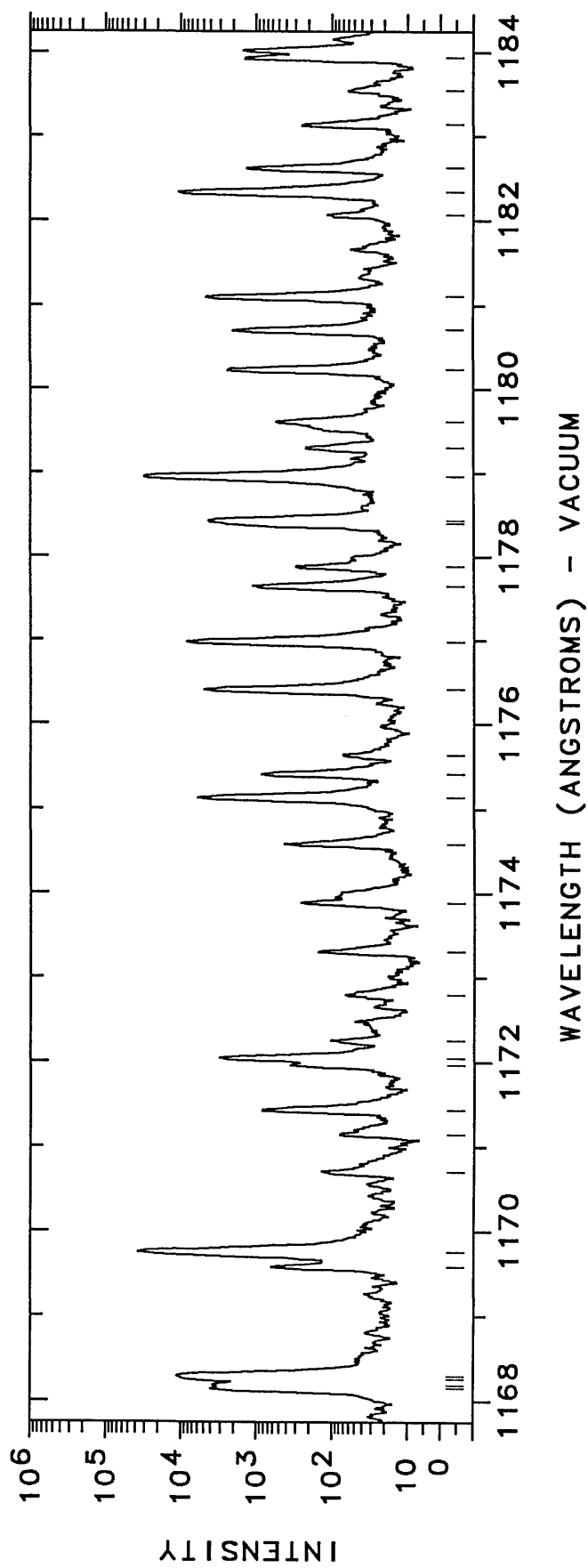
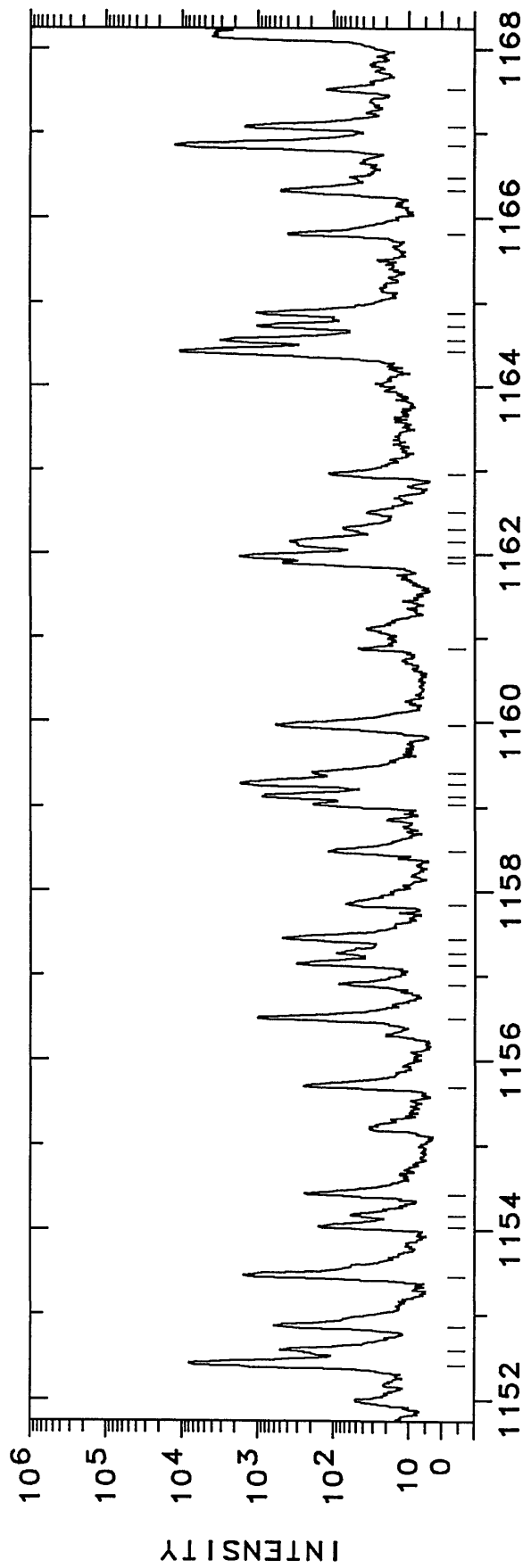
- G – B. A. Palmer and R. Engleman, Jr., Los Alamos National Laboratory Rep. 9615, National Technical Information Service, Springfield, VA (1983). The wavelength uncertainty is 0.0001 Å.
- H – Measured component of hyperfine pattern of a Pt I line.
- I – K. Burns, K. Adams, and J. Longwell, *J. Opt. Soc. Am.* **40**, 6 (1950). The wavelength uncertainty is 0.0004 Å.
- J – Measured component of the incomplete hyperfine pattern of the Pt II line 36484–61190.
- K – Newly identified Pt II line. J. Blaise and J.-F. Wyart, *J. Res. Natl. Inst. Stand. Technol.* **97**, 217 (1992). For photographically measured lines the wavelength uncertainty is ±0.002 Å. For lines found only in the photoelectric scans (two decimal digits) the uncertainty is ±0.01 Å below 2030 Å and ±0.02 Å above 2030 Å.
- L – W. Persson, C.-G. Wahlström, L. Jönsson, and H. O. DiRocco, *Phys. Rev. A* **43**, 4791 (1991). The wavelength is the experimental value from the present work.
- M – Probably blended with a grating ghost; the intensity may be affected.
- N – Newly identified Pt I line. J. Blaise, private communication (1990). For photographically measured lines the wavelength uncertainty is ±0.002 Å. For lines found only in the photoelectric scans the uncertainty is ±0.01 Å below 2030 Å and ±0.02 Å above 2030 Å.
- P – Pt II line for which a Ritz wavelength was given in J. Reader, N. Acquista, C. J. Sansonetti, and J. E. Sansonetti, *Astrophys. J. Suppl.* **72**, 831 (1990). The experimental value is given here because the energy or *J* value of a combining level was changed in the analysis of J. Blaise and J.-F. Wyart, *J. Res. Natl. Inst. Stand. Technol.* **97**, 217 (1992).
- Q – R. C. M. Learner and A. P. Thorne, *J. Opt. Soc. Am. B* **5**, 2045 (1988).
- R – T. R. O'Brian, M. E. Wickliffe, J. E. Lawler, W. Whaling, and J. W. Brault, *J. Opt. Soc. Am. B* **8**, 1185 (1991). Some additional measured wavelengths not included in this reference were communicated privately by the authors.
- S – H. M. Crosswhite, *J. Res. Natl. Bur. Stand. (U.S.)* **79A**, 17 (1975).
- T – N. E. Wagman, *U. Pitt. Bull.* **34**, 1 (1937).

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
1131.87	88349.4	41	Pt II	9356-97630 05	1141.17	87629.4	91	Pt II	15791-103421 K
1132.8322	88274.326	2300	Pt II	18097-106229 K	1141.8885	87574.227	1400	Pt II	13329-100903 06
1134.66	88132.1	22	Pt II	13329-101397 05	1143.2957	87466.439	5800	Pt II	13329-100795 06
1135.4782	88068.623	2400	Pt II	8419-96443 K	1144.60	87366.8	93		
1136.06	88023.5	35	Pt II	13329-101341 05	1145.00	87336.2	49	Pt II	16820-104158 K
1136.2004	88012.640	22	Pt II		1145.7055	87282.468	800	Pt II	13329-100611 05
1138.59	87843.4	120			1145.87	87269.9	310	Pt II	16820-104092 K
1138.83	87809.4	330			1147.62	87136.9	120	Pt II	8419-95557 K
1139.62	87748.5	99			1150.1564	86944.697	1500	Pt II	18097-105042 K
1139.75	87738.5	140			1150.6130	86910.194	7200	Pt II	13329-100239 05
1140.6146	87672.034	53	Pt II	15791-103463 07	1150.9198	86887.027	1700	Pt II	15791-102678 K
1140.65	87669.3	53			1150.9689	86883.321	1800	Pt II	4786-91669 K
1140.79	87658.6	39			1151.59	86836.5	200	Pt II	24879-111716 K



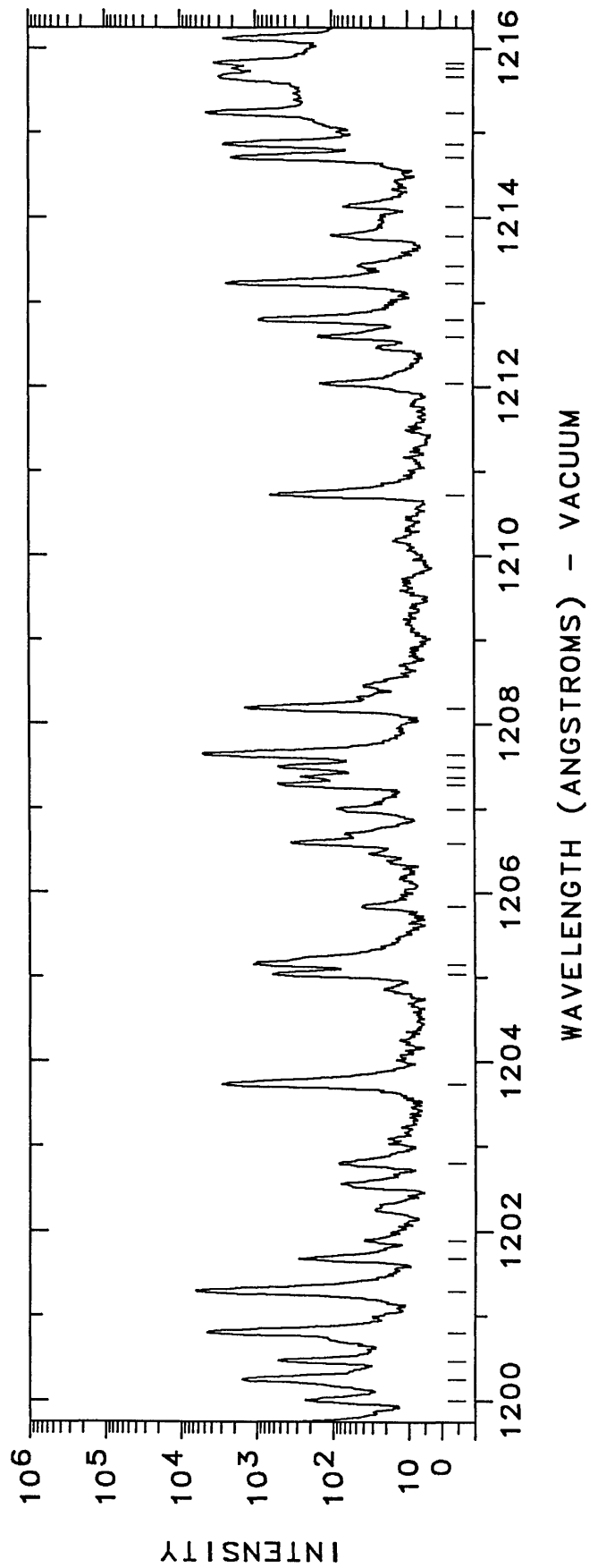
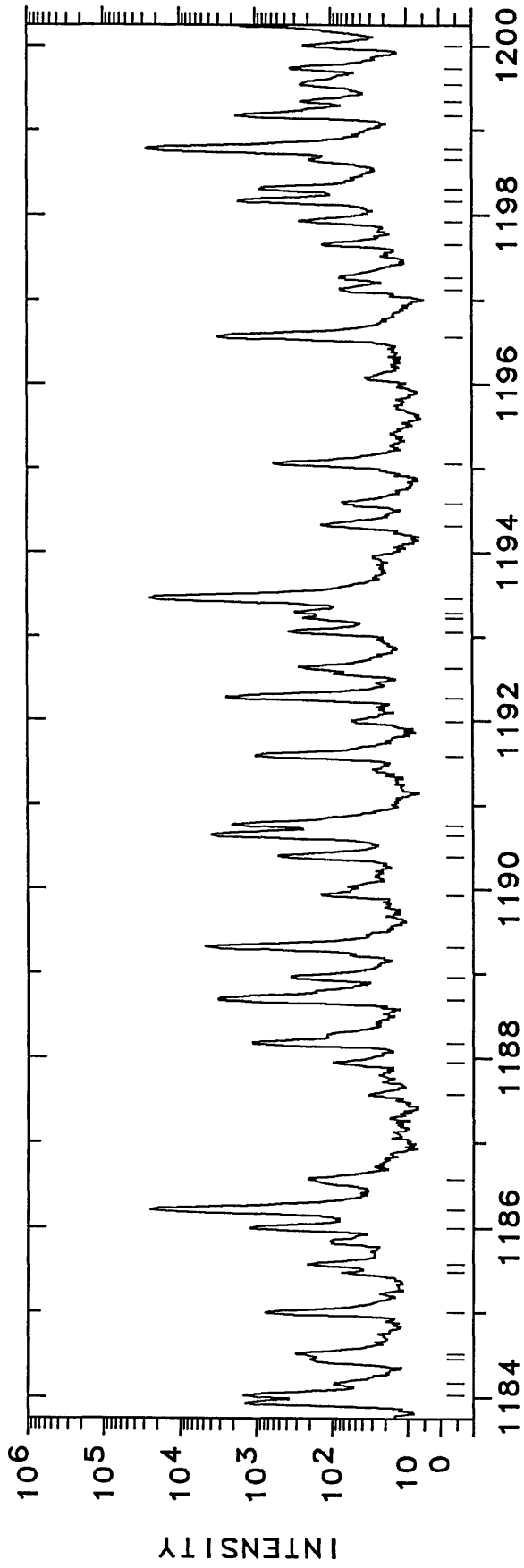
WAVELENGTH (ANGSTROMS) - VACUUM

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
1152.4079	86774.850	8100	Pt II	9356- 96131 K	1168.1346	85606.574	2400	Pt II	15791-101397 05
1152.58	86761.9	500	Pt II	23875-110638 K	1168.1882	85602.645	2100	Pt II	15791-101394 K
1152.86	86740.8	600	Pt II	23461-110202 K	1168.2621	85597.230	6000		
1153.4526	86696.238	1500	Pt II	16820-103517 08	1168.3067	85593.963	8000	Pt II	16820-102414 06
1154.03	86652.9	150			1169.58	85500.8	630		
1154.1691	86642.416	50	Pt II	16820-103463 07	1169.7477	85488.517	37000	Pt II	13329- 98817 06
1154.4201	86623.581	230	Pt II	15791-102414 06	1170.6940	85419.418	130	Pt II	18097-103517 08
1155.69	86528.4	240			1171.15	85386.2	72	Pt II	4786- 90173 K
1156.4898	86468.551	990	Pt II	13329- 99797 05	1171.4321	85365.595	840	Pt II	18097-103463 07
1156.89	86438.6	77	Pt II	21717-108155 K	1171.97	85326.4	360		
1157.13	86420.7	300			1172.0340	85321.757	3100	Pt II	15791-101113 K
1157.26	86411.0	83			1172.26	85305.3	97		
1157.43	86398.3	470	Pt II	9356- 95754 K	1172.80	85266.0	60	Pt II	23461-108727 K
1157.84	86367.7	61			1173.31	85229.0	150		
1158.48	86320.0	110	Pt II	23875-110196 AK	1173.89	85186.9	250	Pt II	24879-110066 K
1158.48	86320.0	110	Pt II	21717-108038 AK	1174.59	85136.1	430	Pt II	21717-106852 K
1159.03	86279.0	180			1175.1429	85096.036	6000	Pt II	16820-101916 06
1159.1308	86271.541	860	Pt II	23461-109733 K	1175.4112	85076.610	850	Pt II	4786- 89863 P
1159.2760	86260.735	1700	Pt II	9356- 95617 K	1175.64	85060.1	64		
1159.40	86251.5	180			1176.4098	85004.390	4900	Pt II	15791-100795 06
1159.96	86209.9	570			1176.9863	84962.756	8400	Pt II	18097-103060 K
1160.87	86142.3	39			1177.6448	84915.248	1100	Pt II	9356- 94271 K
1161.90	86065.9	450	Pt II	23875-110085 K	1177.89	84897.6	290		
1161.9681	86060.882	1700	Pt II	23461-109528 K	1178.3994	84860.871	1400	Pt II	23461-108322 K
1162.15	86047.4	360			1178.4428	84857.744	4300	Pt II	13329- 98186 06
1162.30	86036.3	66			1178.9614	84820.419	31000	Pt II	15791-100611 06
1162.50	86021.5	28			1179.30	84796.1	210	Pt II	23875-108672 K
1162.95	85988.2	110			1179.5986	84774.600	530	Pt II	18097-102872 K
1164.4184	85879.784	11000	Pt II	13329- 99209 06	1180.2490	84727.884	2400	Pt II	21168-105896 K
1164.5543	85869.762	3100	Pt II	9356- 95226 K	1180.7195	84694.121	2000	Pt II	23461-108155 K
1164.7198	85857.560	1000	Pt II	16820-102678 K	1181.1100	84666.119	4600	Pt II	9356- 94022 P
1164.8721	85846.335	1000	Pt II	23461-109307 K	1182.07	84597.4	110		
1165.81	85777.3	390			1182.3552	84576.956	11000	Pt II	16820-101397 05
1166.32	85739.8	480			1182.6276	84557.472	1300	Pt II	21168-105726 K
1166.47	85728.7	52			1183.1383	84520.973	240	Pt II	16820-101341 06
1166.8635	85699.827	12000	Pt II	16820-102520 K	1183.55	84491.6	51		
1167.0766	85684.179	1500	Pt II	21168-106852 K	1183.9423	84463.576	1400	Pt II	13329- 97792 K
1167.52	85651.6	110	Pt II	23875-109528 K					

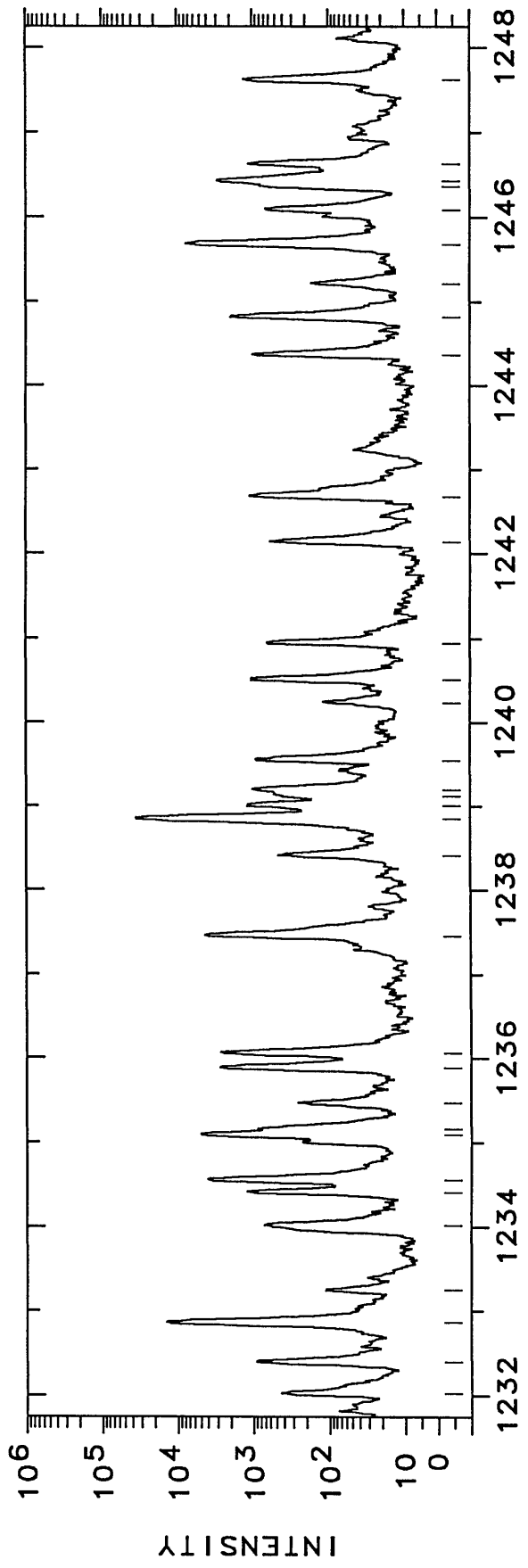
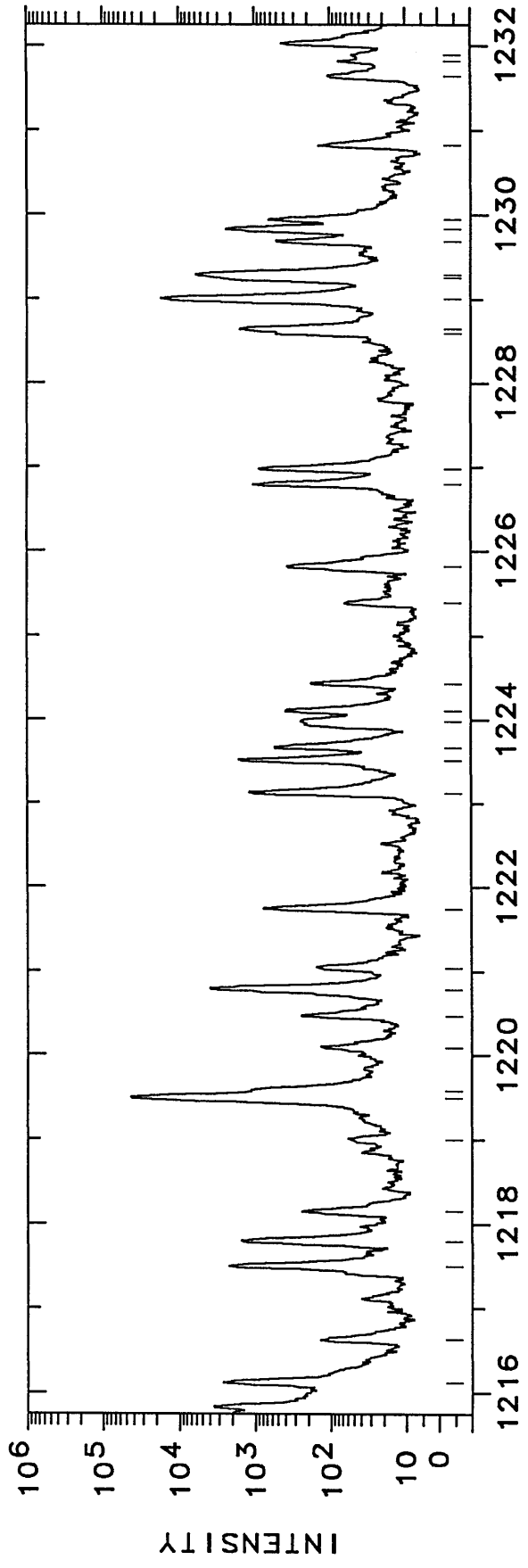




WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
1184.0298	84457.334	1500	Pt II	13329- 97786 K	1198.7745	83418.527	27000	Pt II	16820-100239 05
1184.1586	84448.145	87	Pt II	15791-100239 05	1199.1649	83391.367	1800	Pt II	23461-106852 K
1184.45	84427.4	190	Pt II		1199.34	83379.2	240	Pt II	21168-104548 K
1184.51	84423.1	300	Pt II	18097-102520 K	1199.5496	83364.623	240	N I	B
1184.9977	84388.349	740			1199.7276	83352.251	330	Pt II	0- 83352 07
1185.48	84354.0	67			1200.00	83333.3	220		
1185.57	84347.6	200	Pt II	8419- 92767 K	1200.2508	83315.920	1600	Pt II	23875-107191 K
1185.9985	84317.142	2000	Pt II	18097-102414 06	1200.4693	83300.756	520	Pt II	21717-105018 K
1186.2203	84301.373	25000	Pt II	13329- 97630 06	1200.8040	83277.537	4500	Pt II	15791- 99068 K
1186.57	84276.5	200			1201.2856	83244.152	6500	Pt II	18097-101341 06
1187.57	84205.6	25			1201.68	83216.8	270	Pt II	29030-112247 K
1187.95	84178.6	89	Pt II	21717-105896 K	1201.89	83202.3	31		
1188.1761	84162.609	1100	Pt II	23875-108038 K	1202.80	83139.3	75		
1188.6968	84125.739	3200	Pt II	9356- 93482 07	1203.7443	83074.121	2900	Pt II	13329- 96403 K
1188.95	84107.8	340			1205.0270	82985.692	610	Pt II	29261-112247 K
1189.3073	84082.560	4700	Pt II	16820-100903 06	1205.1569	82976.748	1100	Pt II	16820- 99797 A
1189.93	84038.6	130			1205.1569	82976.748	1100	Pt II	23875-106852 AK
1190.3840	84006.502	490	Pt II	15791- 99797 05	1205.84	82929.7	32	Ne III	L
1190.6418	83988.319	3800	Pt II	18097-102086 08	1206.59	82878.2	350		
1190.7595	83980.013	2000	Pt II	9356- 93336 06	1206.99	82850.7	78		
1191.5733	83922.659	980	Pt II	24879-108802 K	1207.2890	82830.209	510	Pt II	21717-104548 AK
1191.99	83893.3	45			1207.2890	82830.209	510	Pt II	27255-110085 AK
1192.2690	83873.690	2400	Pt II	21168-105042 K	1207.37	82824.7	250	Pt II	0- 82824 K
1192.62	83849.0	250	Pt II	21168-105018 AK	1207.49	82816.4	500		
1192.62	83849.0	250	Pt II	24879-108727 AK	1207.6458	82805.739	5000	Pt II	18097-100903 06
1193.05	83818.8	350	Pt II	18097-101916 K	1208.1902	82768.425	1400	Pt II	23461-106229 K
1193.22	83806.8	230			1210.6999	82596.852	630	Pt II	8419- 91016 K
1193.28	83802.6	290	Pt II	4786- 88589 K	1212.04	82505.5	130		
1193.4484	83790.801	24000	Pt II	16820-100611 06	1212.59	82468.1	140	Pt II	21168-103637 K
1194.32	83729.7	120	Pt II	23461-107191 K	1212.7905	82454.472	890	Pt II	29261-111716 K
1194.58	83711.4	63			1213.2263	82424.853	2400	Pt II	13329- 95754 P
1195.05	83678.5	560			1213.43	82411.0	36		
1196.5616	83572.797	3100			1213.78	82387.3	92		
1197.12	83533.8	68	Pt II	23461-106996 K	1214.13	82363.5	61		
1197.26	83524.0	69			1214.7092	82324.230	2100	Pt II	29030-111354 K
1197.65	83496.8	120			1214.8648	82313.686	2600	Pt II	9356- 91669 K
1197.92	83478.0	250			1215.2467	82287.819	4400	Pt II	13329- 95617 K
1198.1623	83461.147	1700			1215.6701	82259.159	H	H I	B
1198.3009	83451.494	860	Pt II	18097-101549 P	1215.7671	82252.596	2000	Pt II	21168-103421 K
1198.65	83427.2	180			1215.8369	82247.874	3500	Pt II	16820- 99068 K

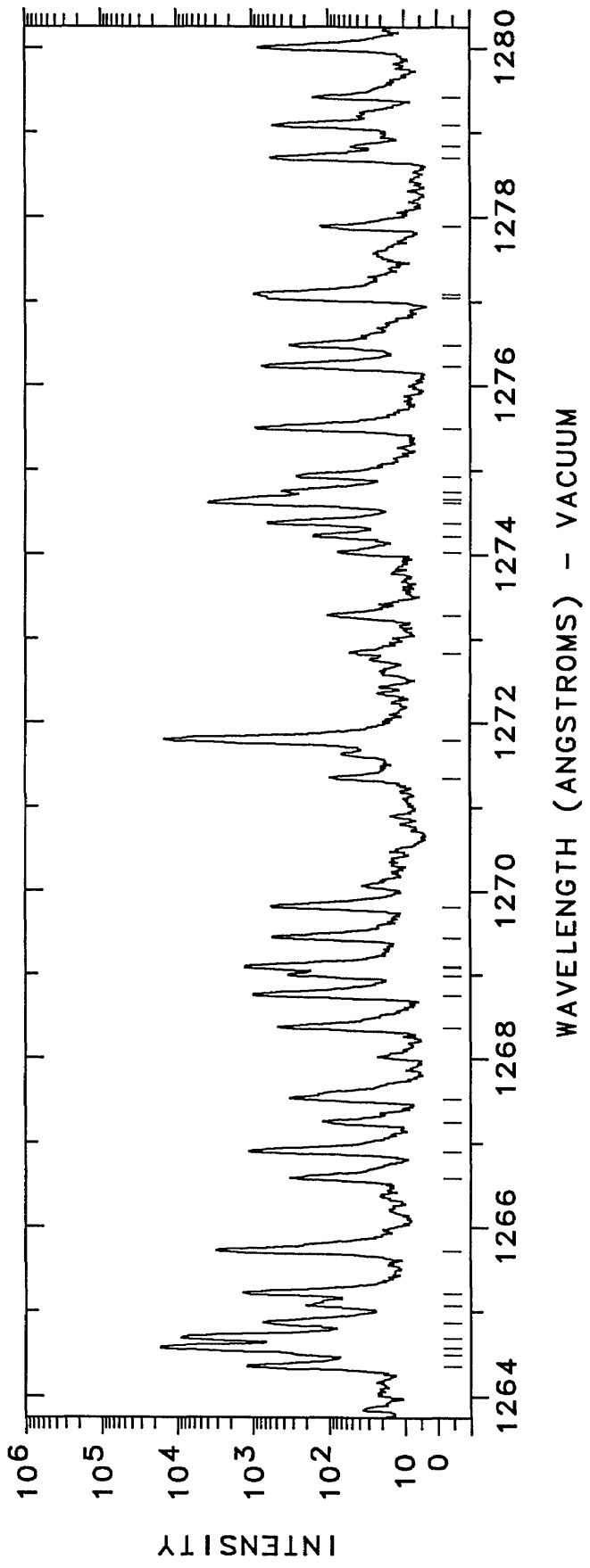
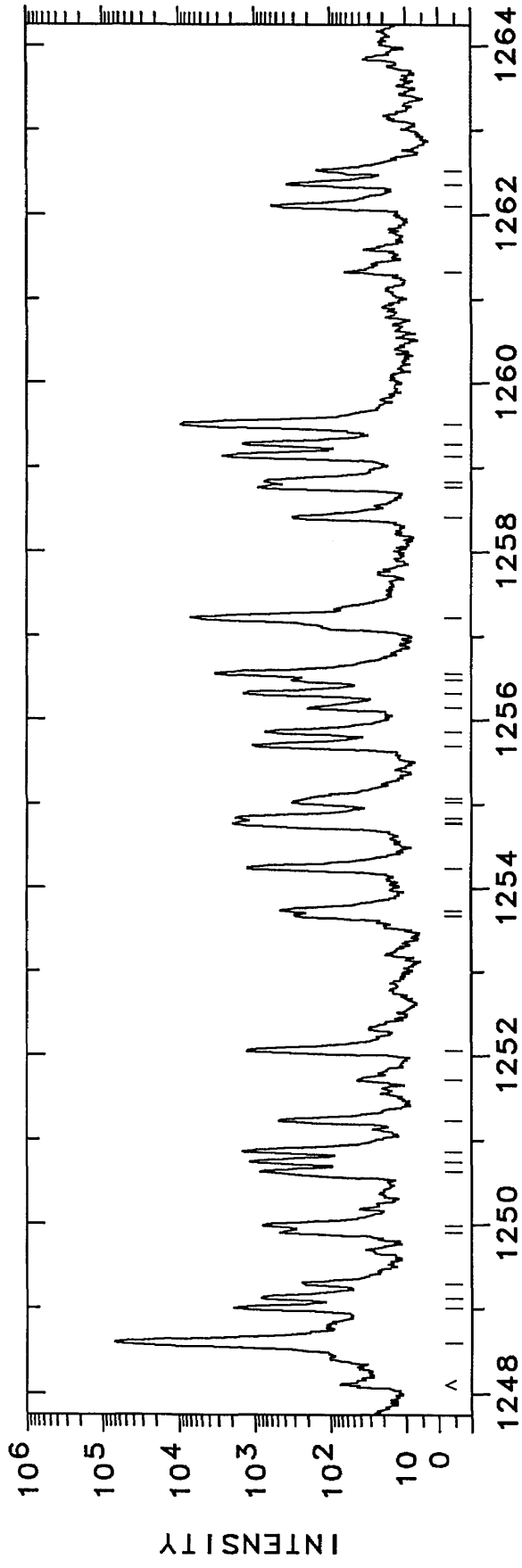


WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
1216.1236	82228.484	2600	Pt II	13329-95557	K	1231.89	81176.1	Ne III	L
1216.63	82194.3	130	Pt II	23461-105597	K	1232.0302	81166.842	Pt II	23875-105042
1217.4951	82135.854	2200	Pt II	24879-106995	K	1232.3983	81142.598	Pt II	23875-105018
1217.7927	82115.782	1500	Pt II	24879-106995	K	1232.8739	81111.296	Pt II	18097-99209
1218.15	82091.7	230	Pt II			1233.25	81086.6	Pt II	23461-104548
1219.00	82034.5	51	Pt II			1234.0154	81036.266	Pt II	29030-110066
1219.4931	82001.284	43000	Pt II	15791-97792	K	1234.4019	81010.893	Pt II	
1219.5786	81995.535	900	Pt II	15791-97786	K	1234.5580	81000.650	Pt II	
1220.09	81961.2	130	Pt II			1235.0916	80965.655	Pt II	16820-97786
1220.47	81935.6	240	Pt II			1235.1607	80961.125	Pt II	21717-102678
1220.7795	81914.875	3900	Pt II	9356-91271	K	1235.47	80940.9	Pt II	
1221.04	81897.4	150	Pt II			1235.8863	80913.592	Pt II	4786-85700
1221.7369	81850.683	760	Pt II	23875-105726	K	1236.0630	80902.025	Pt II	
1223.1214	81758.033	1200	Pt II			1237.4751	80809.706	Pt II	16820-97630
1223.5053	81732.380	1600	Pt II	29030-110762	K	1238.4170	80748.246	Pt II	21168-101916
1223.6648	81721.726	530	Pt II	23875-105597	K	1238.8499	80720.029	Pt II	18097-98817
1223.98	81700.7	240	Pt II			1239.0156	80709.23	Ne II	C
1224.1006	81692.632	380	Pt II			1239.1184	80702.538	Pt II	29030-109733
1224.43	81670.7	170	Pt II			1239.2011	80697.152	Pt II	23461-104158
1225.39	81606.7	56	Pt II	29030-110638	K	1239.5438	80674.842	Pt II	24879-105554
1225.82	81578.0	360	Pt II	29030-110609	K	1240.24	80629.6	Pt II	
1226.7936	81513.304	1000	Pt II	13329-94842	K	1240.5098	80612.019	Pt II	15791-96403
1226.9816	81500.815	860	Pt II	29261-110762	K	1240.9502	80583.411	Pt II	
1228.5930	81393.920	400	L			1242.1331	80506.670	Pt II	9356-89863
1228.6470	81390.342	1300	Pt II	9356-90746	K	1242.6815	80471.142	Pt II	29261-109733
1229.0134	81366.077	17000	Pt II	16820-98186	O6	1244.3623	80362.448	Pt II	16820-97183
1229.2515	81350.318	1500	Pt II	24879-106229	K	1244.8278	80332.396	Pt II	27255-107588
1229.3001	81347.102	4500	Pt II	29261-110609	K	1245.21	80307.7	Pt II	
1229.6873	81321.49	510	Ne II			1245.6812	80277.362	Pt II	29030-109307
1229.8367	81311.61	2400	Ne II			1246.0801	80251.662	Pt II	9356-89607
1229.9505	81304.085	630	Pt II	13329-94633	K	1246.3668	80233.203	Pt II	34647-114880
1230.8272	81246.173	130	Pt II	21168-102414	O7	1246.4295	80229.166	Pt II	21168-101397
1231.64	81192.6	97	Ne III			1246.6262	80216.508	Pt II	23875-104092
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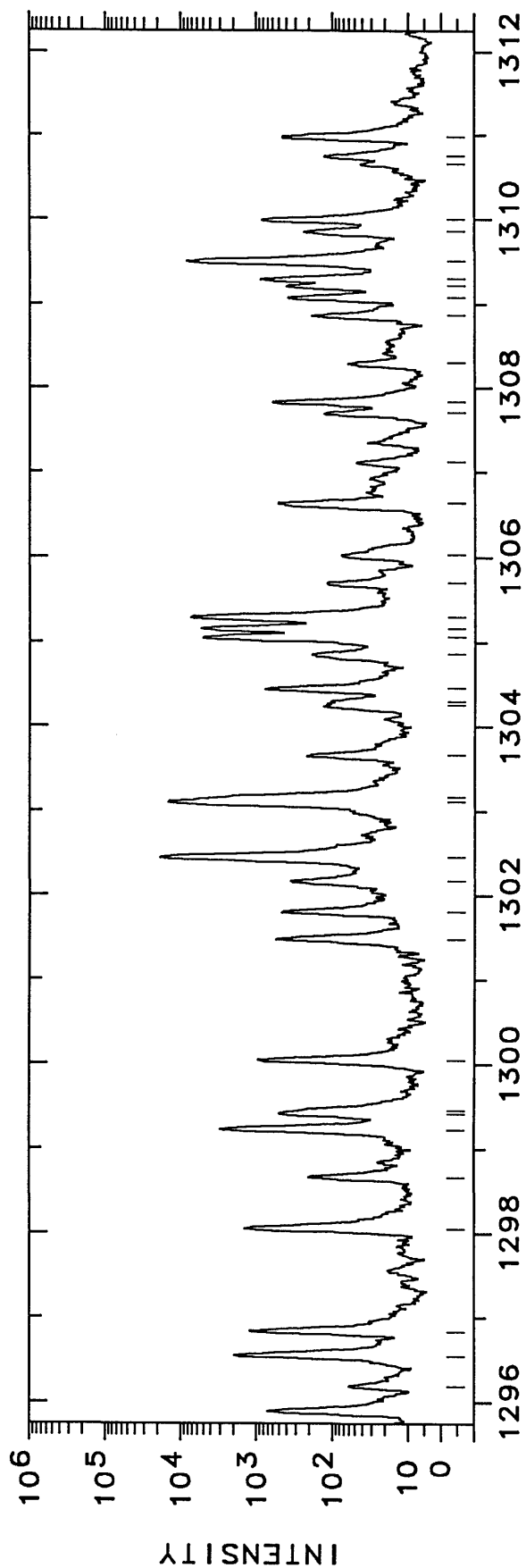
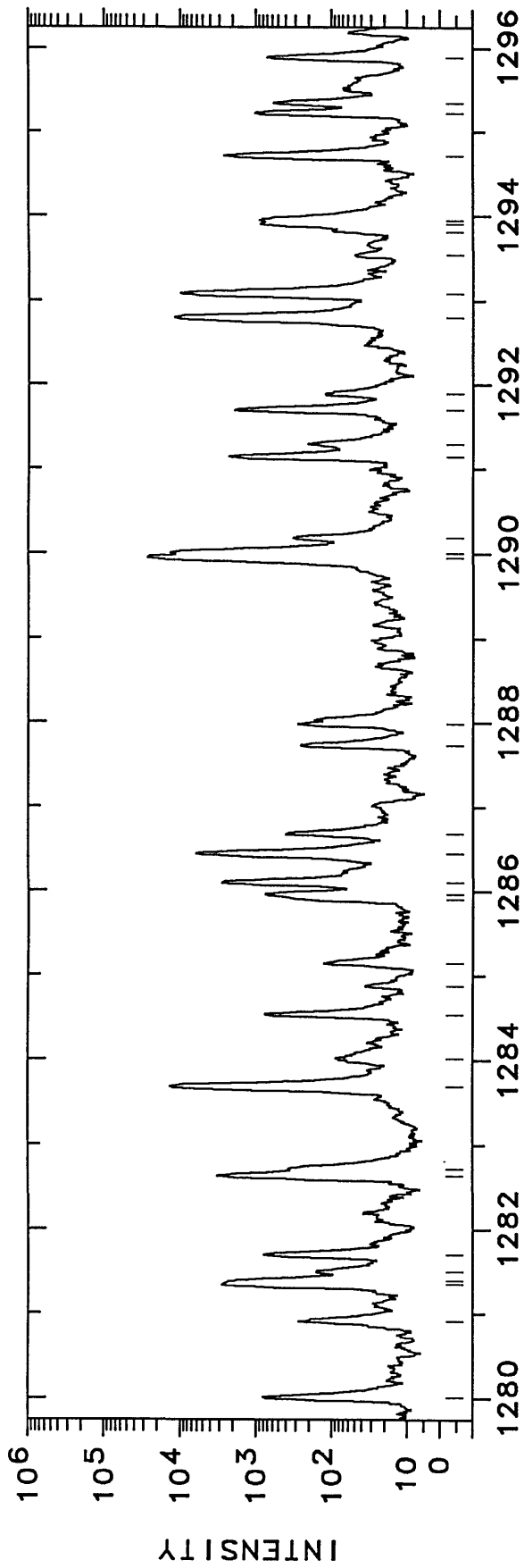


WAVELENGTH (ANGSTROMS) - VACUUM

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1249.0069	80063.609	1900				1264.5677	79078.406	Pt II	21717-100795	07
1249.1314	80055.629	810	Pt II	23461-103517	09	1264.6904	79070.737	Pt II	21168-100239	06
1249.29	80045.5	230	Pt II	29261-109307	K	1264.8691	79059.564	Pt II	23461-102520	K
1249.8897	80007.060	440	Pt II	13329-93336	06	1265.07	79047.0	190		
1249.9718	80001.807	770	Pt II	23461-103463	08	1265.2074	79038.425	1400	15791-94829	K
1250.6310	79959.636	840	Pt II	23461-103421	K	1265.7145	79006.759	3100	29030-108037	K
1250.7471	79952.214	1100	Pt II	24879-104831	K	1266.5706	78953.354	310	23461-102414	07
1250.8692	79944.410	1400	Pt II	21168-101113	K	1266.8932	78933.252	1100	16820-95754	P
1251.2230	79921.805	470				1267.25	78911.0	110		
1251.72	79890.1	37				1267.5165	78894.435	310	21717-100611	07
1252.0617	79868.269	1300	Pt II	13329-93197	K	1268.3599	78841.975	450	15791-94633	K
1253.6619	79766.323	350	Pt II	15791-95557	K	1268.7589	78817.181	970	9356-88173	K
1253.7338	79761.749	400	Pt II	23875-103637	K	1268.9912	78802.753	270	23875-102678	K
1254.2439	79729.309	1200				1269.0742	78797.599	520	32918-111716	K
1254.7526	79696.986	800	Pt II	29030-108727	K	1269.0973	78796.165	700	16820-95617	K
1254.7815	79695.150	1700	Pt II	18097-97792	K	1269.4345	78775.234	530	29261-108037	K
1254.8469	79690.997	1800				1269.8121	78751.809	540	4786-83538	K
1255.0214	79679.916	310	Ne III			1271.34	78657.2	87		
1255.0721	79676.698	150	Pt II	21717-101394	K	1271.7939	78629.094	15000	21168-99797	06
1255.6911	79637.420	1100	Ne III			1272.83	78565.1	44		
1255.8557	79626.982	710	Pt II	21168-100795	07	1273.28	78537.3	94		
1256.1477	79608.473	190	Pt II	29030-108639	K	1274.03	78491.1	66		
1256.3246	79597.263	1400	Pt II	27255-106852	K	1274.2091	78480.055	150	15791-94271	K
1256.4747	79587.757	130	Pt II	23875-103463	09	1274.3665	78470.362	620	27255-105726	K
1256.5583	79582.460	3300	Pt II	16820-96403	K	1274.6091	78455.427	3800	23461-101916	07
1257.2214	79540.485	6800	Pt II	29261-108802	K	1274.6566	78452.502	900	0-78452	K
1258.4063	79465.591	290	Pt II	29261-108727	K	1274.7362	78447.604	300	32237-110684	K
1258.7640	79443.011	880	Pt II	21168-100611	07	1274.9222	78436.159	250	32918-111354	K
1258.8332	79438.642	600	Pt II	13329-92749	K	1275.4940	78400.996	890	32237-110638	K
1259.1328	79419.740	2600	Pt II	23461-102872	K	1276.2289	78355.850	730	29030-107386	K
1259.2740	79410.835	1400	Pt II	4786-84182	A	1276.4754	78340.719	320	13329-91669	K
1259.5111	79395.886	9300	Pt II	21717-101113	AK	1277.0472	78305.641	700	18097-96403	K
1259.5111	79395.886	9300	Pt II			1277.1026	78302.245	800	21168-99471	K
1261.32	79282.0	55				1277.89	78254.0	120		
1262.0962	79233.263	590	Pt II	9356-88589	K	1278.6998	78204.439	560		
1262.3591	79216.762	370	Pt II	23461-102678	K	1278.84	78195.9	40		
1262.5104	79207.268	140				1279.0832	78180.997	510	24879-103060	K
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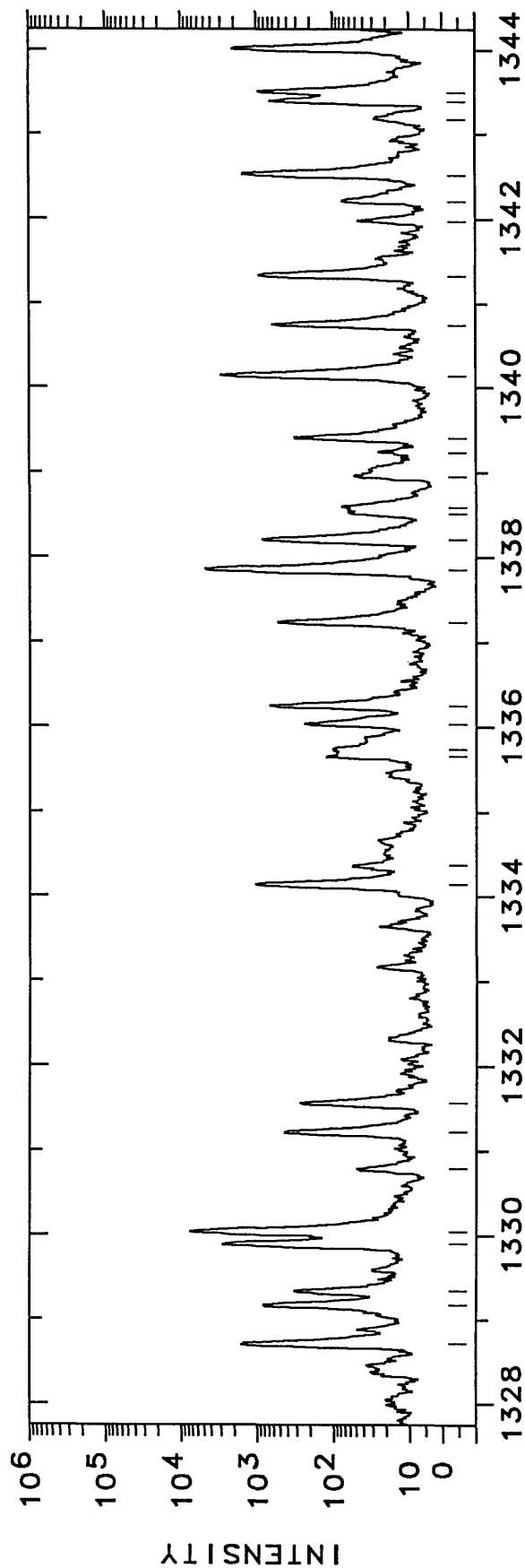
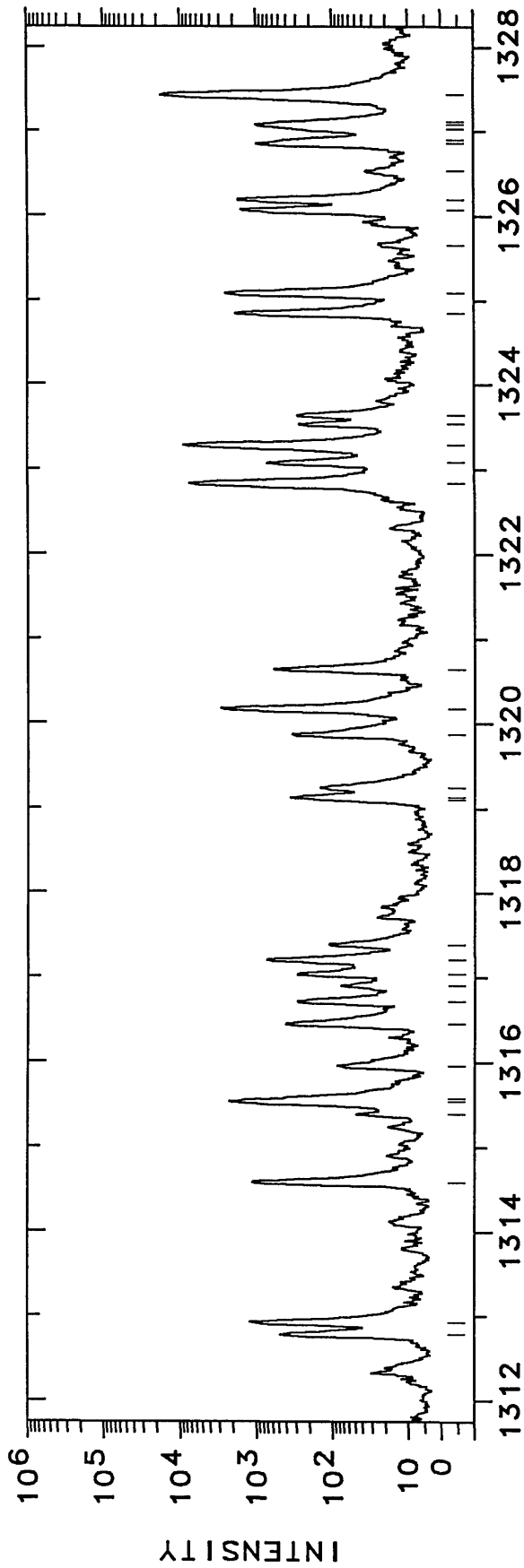
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1280.9032	78069.912	270	Pt II	8419- 86489 K	1298.0460	77038.87	1400	Ne II	
1281.3463	78042.915	2200	Pt II	0- 78043 P	1298.6562	77002.674	200	Pt II	37877-114880 K
1281.3888	78040.327	1200	Pt II	21168- 99209 07	1299.2423	76967.937	3000	Pt II	29261-106229 K
1281.5008	78033.506	450	Pt II	18097- 96131 K	1299.4141	76957.761	320	Pt II	15791- 92749 K
1281.6965	78021.591	770	Pt II	16820- 94842 K	1299.4590	76955.102	150	Pt II	23875-100795 08
1282.6318	77964.697	3200	Pt II	29030-106995 K	1300.0501	76920.113	940	Pt II	32918-109753 K
1282.7174	77959.494	400	Pt II	32237-110196 K	1301.4882	76835.118	540	Pt II	
1283.6978	77899.954	13000	Pt II	21168- 99068 K	1301.8075	76816.273	460		
1284.0207	77880.364	79	Pt II	23461-101341 07	1302.1685	76794.977		O I	
1284.5438	77848.650	750	Pt II	32237-110085 K	1302.4578	76777.918	19000	Pt II	23461-100239 06
1284.88	77828.3	28	Pt II		1303.1187	76738.979	15000	Pt II	24879-101618 14
1285.15	77811.9	120	Pt II	16820- 94633 K	1303.1669	76736.142	2300 P	Pt II	23875-100611 07
1285.9115	77765.849	400	Pt II	32918-110684 K	1303.6558	76707.364	210	Pt II	34647-111354 K
1285.9670	77762.493	700	Pt II	27255-105018 K	1304.2331	76673.411	120	Pt II	34647-111320 K
1286.1117	77753.744	2800	Pt II	21717- 99471 K	1304.2955	76669.742	100	Pt II	24879-101549 P
1286.4510	77733.237	6100	Pt II	29261-106995 K	1304.4422	76661.119	750	Pt II	16820- 93482 09
1286.6796	77719.426	390	Pt II	32918-110638 K	1304.8576	76636.715		O I	
1287.7253	77656.314	250	Pt II	18097- 95754 P	1305.0718	76624.137	5100	Pt II	21168- 97792 K
1287.9733	77641.361	270 W	Pt II	24879-102520 K	1305.1778	76617.914	5400	Pt II	21168- 97786 K
1289.9515	77522.297	27000	Pt II	32918-101397 07	1305.3118	76610.046	7400	Pt II	0- 76610 04
1290.0131	77518.593	13000	Pt II	23875-101394 AK	1305.6955	76587.535	110		
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1290.1699	77509.172	310	Pt II		1306.6087	76534.008	150 L		
1291.1450	77450.635	2300	Pt II	16820- 94271 K	1306.6389	76532.239	380		
1291.2898	77441.951	200	Pt II	23461-100903 07	1307.0999	76505.247	40		
1291.7007	77417.315	1900	Pt II	13329- 90746 K	1307.6962	76470.361	120	Pt II	9356- 85826 K
1291.89	77406.0	120	Pt II	15791- 93197 K	1307.8326	76462.387	610	Pt II	24879-101341 07
1292.7998	77351.497	12000	Pt II	21717- 99068 K	1308.3006	76435.033	54	Pt II	32237-108672 K
1293.0896	77334.163	9900	Pt II	23461-100795 07	1308.8604	76402.342	180	Pt II	32237-108639 K
1293.54	77307.2	42			1309.0824	76389.385	380	Pt II	32918-109307 K
1293.8099	77291.107	160	Pt II	32237-109528 K	1309.2150	76381.649	340	Pt II	27255-103637 K
1293.9021	77285.60	650	Ne II		1309.3000	76376.690	890	Pt II	16820- 93197 K
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1294.7073	77237.535	2600	Pt II	23875-101113 K	1309.8568	76344.223	230 D	Pt II	9356- 85700 P
1295.2268	77206.554	1000	Pt II	24879-102086 09	1309.9932	76336.275	830	Pt II	23461- 99797 06
1295.3461	77199.445	580	Pt II	29030-106229 K	1310.66	76297.4	33	Pt II	4786- 81083 K
1295.8881	77167.157	700	Pt II	32918-110085 K	1310.7472	76292.362	120	Pt II	29261-105554 K
1296.1731	77150.192	51	Pt II	23461-100611 07	1310.9818	76278.709	440	Pt II	13329- 89607 08
1296.5416	77128.262	1900	Pt II	18097- 95226 K					



WAVELENGTH (ANGSTROMS) - VACUUM

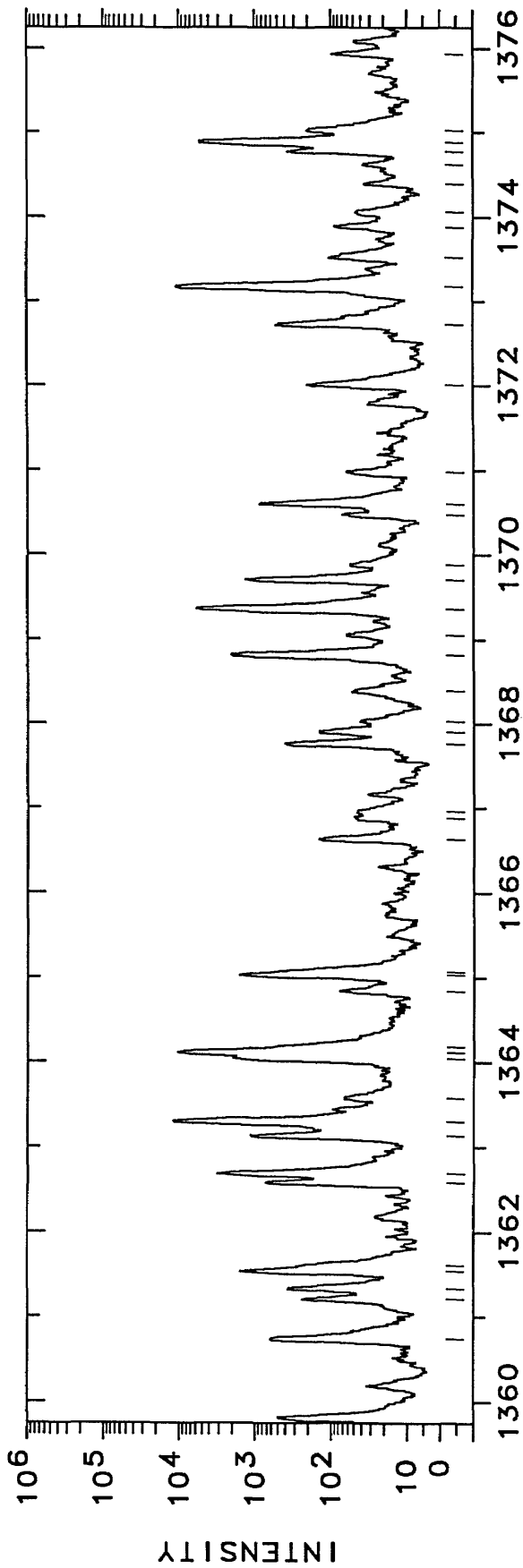
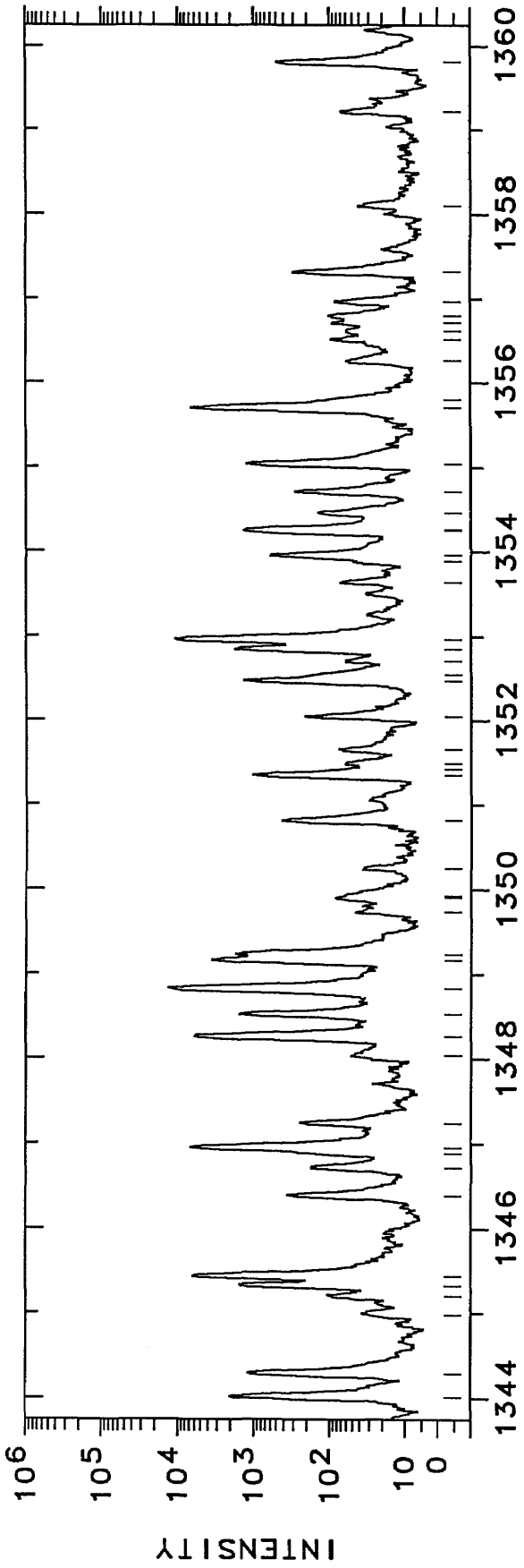


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1314.5907	76069.304	1100	Pt II	21717-97786 K	1327.4314	75333.458	18000	Pt II	23875-99209 08
1315.40	76022.5	42			1328.7227	75260.248	1600	Pt II	13329-88589 K
1315.5348	76014.713	2300	Pt II	21168-97183 K	1329.1748	75234.649	830	Pt II	21168-96403 K
1315.5810	76012.043	270 P	Pt II	29030-105042 K	1329.3385	75225.385	320	Pt II	15791-91016 K
1315.9505	75990.700	80	Pt II	34647-110638 K	1329.9067	75193.245	2900	Pt II	23875-99068 K
1316.4501	75961.861	410	Pt II	34647-110609 K	1330.0547	75184.880	7700	Pt II	0-75184 04
1316.7058	75947.110	290	Pt II	16820-92767 K	1330.79	75143.3	42		
1316.8913	75936.412	71			1331.2263	75118.708	440	Pt II	32918-108037 K
1317.0348	75928.138	290	Pt II	16820-92749 K	1331.5606	75099.849	270	Pt II	18097-93197 K
1317.2032	75918.431	740	Pt II	32237-108155 K	1334.1414	74954.574	1100	Pt II	32237-107191 K
1317.3856	75907.919	100	Pt II	37877-113785 K	1334.37	74941.7	49		
1319.1080	75808.804	84 U	Pt II	32918-108727 K	1335.6420	74870.362	120		
1319.1412	75806.896	270			1335.7277	74865.558		C II	
1319.2429	75801.052	140	Pt II	29030-104831 AK	1336.0355	74848.311	230		
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1319.8553	75765.881	340	Pt II	13329-89095 K	1337.2361	74781.110	530	Pt II	13329-88110 K
1320.1754	75747.508	3000	Pt II	23461-99209 07	1337.8657	74745.916	4900	Pt II	0-74745 05
1320.6427	75720.708	590	Pt II	32918-108639 K	1338.2103	74726.670	850	Pt II	21717-96443 K
1322.8372	75595.092	7500	Pt II	23875-99471 AK	1338.5127	74709.788	54		
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1323.0765	75581.422	710	Pt II	0-75581 06	1338.95	74685.4	46		
1323.2831	75569.619	8900	Pt II	29261-104831 K	1339.2328	74669.617	31	Pt II	32918-107588 K
1323.5388	75555.020	260	Pt II	34647-110202 K	1339.3918	74660.753	320	Pt II	34647-109307 K
1323.6402	75549.232	280	Pt II	34647-110196 K	1340.1393	74619.107	3000	Pt II	0-74619 05
1324.8562	75479.890	1900	Pt II	15791-91271 K	1340.7443	74585.437	610	Pt II	21168-95754 P
1325.0971	75466.168	2500	Pt II	21717-97183 K	1341.3300	74552.869	920	Pt II	8419-82972 P
1325.6560	75434.351	32			1341.9630	74517.703	40		
1326.0723	75410.670	1600	Pt II	4786-80197 K	1342.2101	74503.984	68		
1326.1916	75403.886	1700	Pt II	32918-108322 K	1342.5224	74486.653	1500	Pt II	29030-103517 11
1326.5362	75384.299	30	Pt II	18097-93482 09	1343.18	74450.2	21	Pt II	16820-91271 K
1326.8620	75365.788	810	Pt II	0-75365 K	1343.3742	74439.423	650	Pt II	18097-92537 K
1326.9041	75363.397	250	Pt II	29261-104625 K	1343.4932	74432.831	930	Pt II	29030-103463 09
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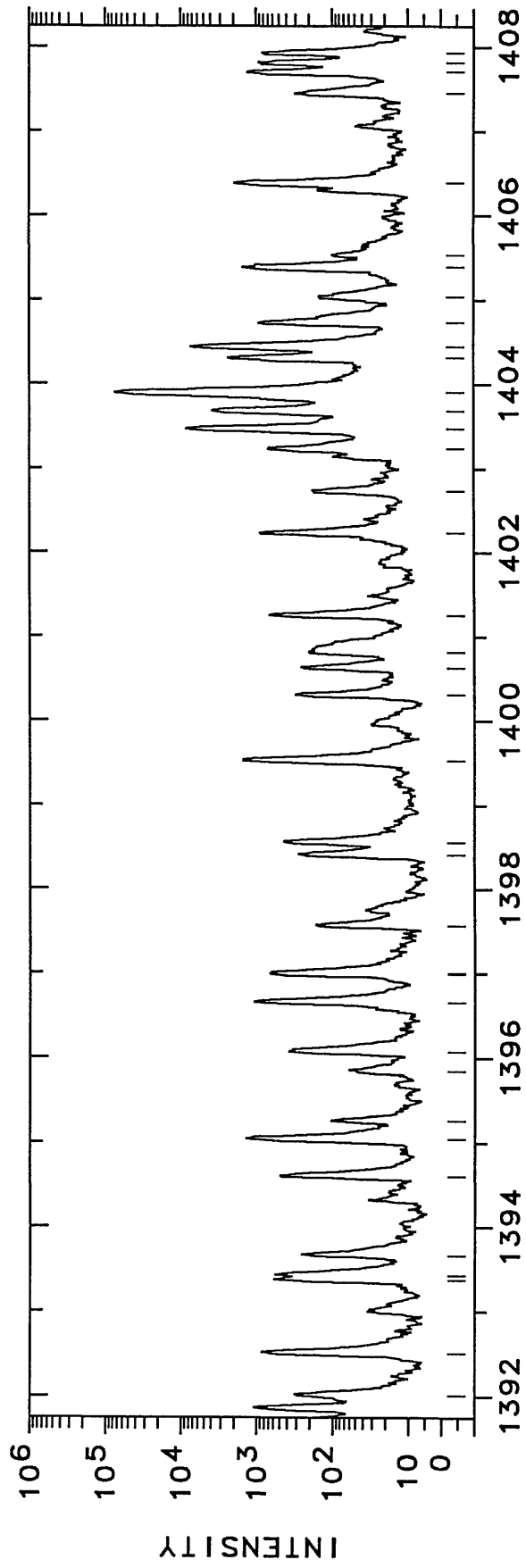
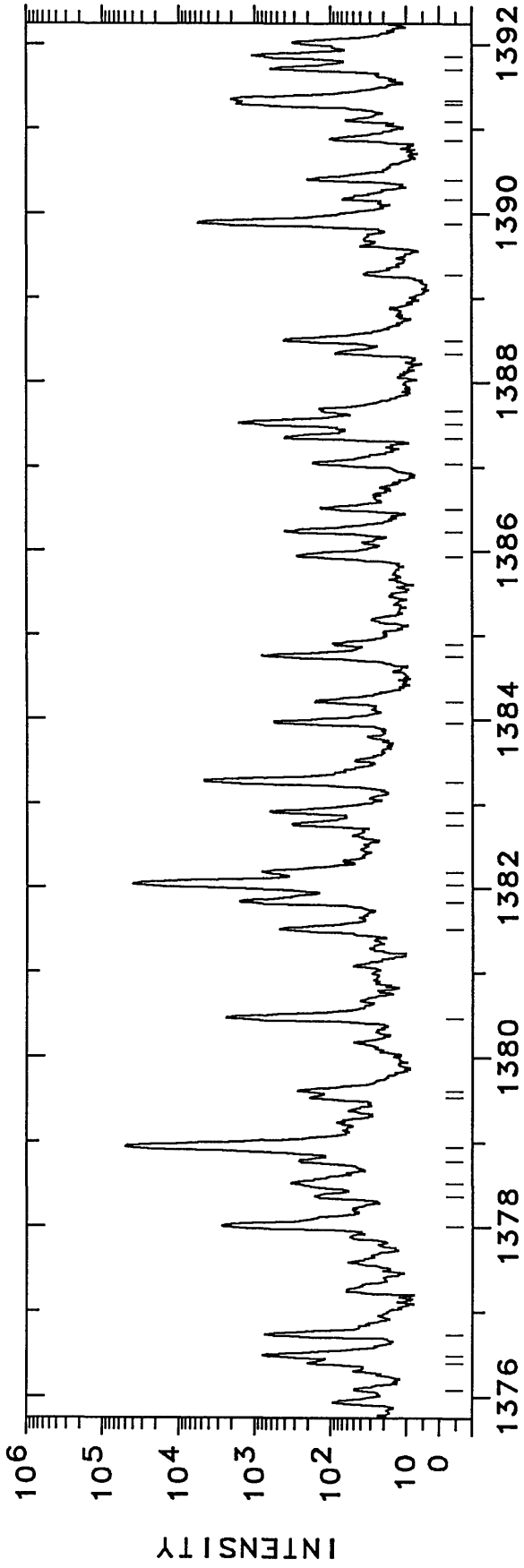
WAVELENGTH (ANGSTROMS) - VACUUM

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1344.2837	74389.059	1200	Pt II	21168- 95557	1358.10	73632.3	33	Pt II	18097- 91669
1344.9807	74350.509	41			1359.2060	73572.365	63	Pt II	27255-100795
1345.1936	74338.742	98			1359.8046	73539.979	490	Pt II	29030-102520
1345.3272	74331.360	1500	Pt II	23461- 97792	1360.7247	73490.251	400 P	Pt II	32237-105726
1345.4403	74325.111	6300	Pt II	23461- 97786	1360.7364	73489.619	250 U	Pt II	21168- 94633
1346.3867	74272.867	350	Pt II	32918-107191	1361.2009	73464.542	230	Pt II	
1346.7077	74255.165	170	Pt II	29261-103517	1361.3317	73457.483	360	Pt II	
1346.8846	74245.411	100			1361.5367	73446.423	1500	Pt II	41434-114880
1346.9559	74241.479	6800	Pt II	0- 74241	1361.6039	73442.798	240	Pt II	37877-111320
1347.2391	74225.874	240			1362.5820	73390.079	730	Pt II	34647-108037
1348.0380	74181.885	43			1362.6878	73384.378	3200	Pt II	29030-102414
1348.2704	74169.097	5900	Pt II	23461- 97630	1363.1360	73360.252	1200	Pt II	32237-105597
1348.5261	74155.035	1500	Pt II	34647-108802	1363.3059	73351.109	12000	Pt II	29261-102613
1348.8300	74138.327	14000	Pt II	27255-101394	1363.58	73336.4	59		
1349.1657	74119.881	3600	Pt II	4786- 78906	1364.0463	73311.295	2000	Pt II	32918-106229
1349.2366	74115.985	1700	Pt II	8419- 82535	1364.1171	73307.491	11000	Pt II	24879- 98186
1349.8865	74088.601	37			1364.1837	73303.911	300 U	Pt II	15791- 89095
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1350.2453	74060.617	33			1365.0223	73258.876	1300	Pt II	29261-102520
1350.8008	74030.161	29			1365.0673	73256.461	350	Pt II	4786- 78043
1351.3531	73999.904	1000	Pt II	29030-103060	1366.6169	73173.396	140	Pt II	18097- 91271
1351.4248	73995.977	33	Pt II	0- 73999	1366.88	73159.3	41		
1351.4965	73992.053	63	Pt II	9356- 83352	1366.96	73155.0	38		
1351.6578	73983.223	66			1367.7548	73112.520	390	Pt II	21717- 94829
1352.0463	73961.964	200			1367.8880	73105.400	130		
1352.4797	73938.264	1400			1368.03	73097.8	33		
1352.5501	73934.415	93			1368.39	73078.6	45		
1352.7067	73925.856	53			1368.8213	73055.555	2100	Pt II	29030-102086
1352.8623	73917.353	1800	Pt II	16820- 90746	1369.05	73043.4	53		
1352.9768	73911.097	11000	Pt II	23875- 97792	1369.3682	73026.380	5900	Pt II	0- 73026
1353.6358	73875.115	63			1369.7039	73008.480	1300		
1353.8865	73861.435	33			1369.88	72999.1	47		
1353.9613	73857.355	600			1370.47	72967.7	62		
1354.2487	73841.681	700 P	Pt II	27255-101113	1370.5971	72960.902	870		
1354.2620	73840.955	650 P	Pt II	29030-102872	1370.98	72940.5	53		
1354.4510	73830.652	130 W			1371.9971	72886.451	190	Pt II	29030-101916
1354.7077	73816.660	280			1372.7084	72848.684	520	Pt II	42031-114880
1355.0378	73798.679	1300	Pt II	15791- 89607	1373.1724	72824.067	11000	Pt II	29261-102086
1355.7164	73761.739	6600	Pt II	29261-103060	1373.52	72805.6	95	Pt II	32237-105042
1355.8015	73757.110	43			1373.88	72786.6	80		
1356.26	73732.2	51			1374.06	72777.0	38		
1356.5142	73718.358	86			1374.39	72759.6	27		
1356.6240	73712.392	50			1374.62	72747.4	28		
1356.7144	73707.480	93	Ne III	36484-110196	1374.7784	72738.996	110	Pt II	34647-107386
1356.7905	73703.346	83			1375.8896	72733.113	5300	Pt II	4786- 77519
1356.9559	73694.363	74 W	Ne III	0- 73761	1375.0230	72726.056	190	Ne III	
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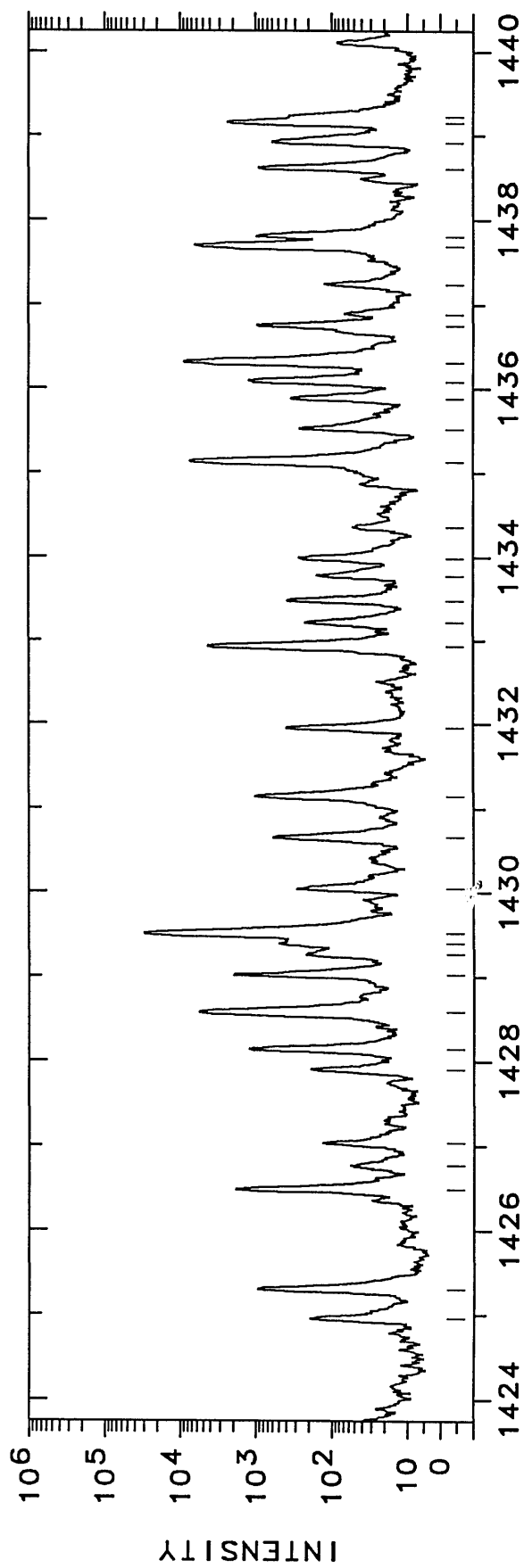
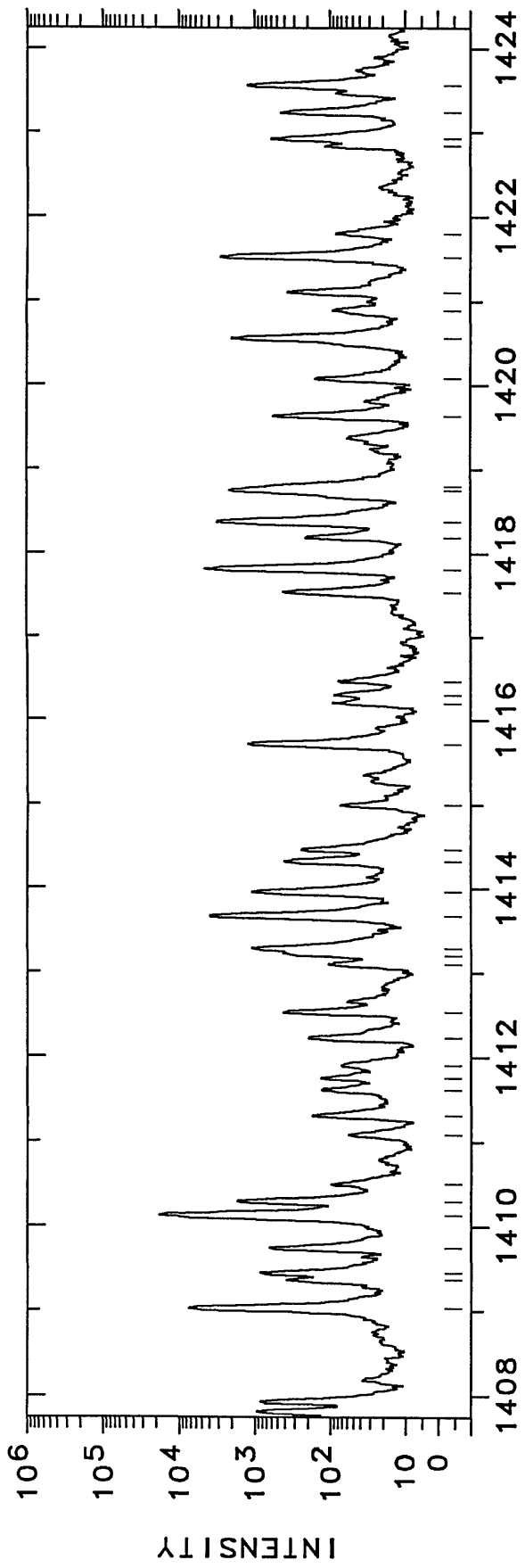
WAVELENGTH (ANGSTROMS) - VACUUM

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1376.3946	72653.584	150			1392.0143	71838.343	310	Pt II	K
1376.4844	72648.844	780	Pt II	18097- 90746 K	1392.5021	71813.177	840	Pt II	36484-108322 K
1376.7307	72635.847	730	Pt II	32918-105554 K	1393.3666	71768.621	500	Pt II	27255- 99068 K
1378.0080	72568.519	2700	Pt II	23875- 96443 K	1393.4258	71765.572	400	Pt II	16820- 88589 K
1378.36	72550.0	150	Pt II	9356- 81897 P	1393.6526	71753.893	240	Pt II	18097- 89863 P
1378.5216	72541.482	320	Pt II	23875- 95557 K	1394.6032	71704.984	480	Pt II	42031-113785 K
1378.7824	72527.761	250	Pt II	23875- 96403 K	1395.0473	71682.157	1400	Pt II	23875- 95557 K
1378.9572	72518.567	50000	Pt II	29030-101549 P	1395.26	71671.2	95	Pt II	36484-108155 K
1379.5267	72488.630	160	Pt II	8419- 80858 08	1395.8393	71641.487	51	Pt II	29261-100903 09
1379.6093	72484.290	260	Pt II	Ne II	1396.0709	71629.600	370	Pt II	32918-104548 K
1380.4782	72438.666	2400	Ne II	C	1396.6602	71599.377	1100	Pt II	21168- 92767 K
1381.5073	72384.71	470	Pt II	29030-101397 07	1396.9879	71582.581	450	Pt II	34647-106229 K
1381.8382	72367.371	1600	Pt II	29261-101618 16	1397.0043	71581.741	250	Pt II	15791- 89607 09
1382.0460	72356.492	41000	Pt II	34647-106996 K	1397.5451	71554.041	160	Pt II	9356- 80858 07
1382.1820	72349.372	800	Pt II	15791- 88110 K	1397.5451	71554.041	160	Pt II	15791- 87204 K
1382.7626	72318.994	320	Pt II	29030-101341 08	1398.4015	71510.221	270	Pt II	0- 71364 K
1382.9080	72311.388	620	Pt II	23461- 95754 P	1398.5581	71502.214	430	Pt II	0- 71314 05
1383.2676	72292.592	4700	Pt II	36484-108727 K	1399.5333	71452.39	1500	Ne II	16820- 88110 K
1383.9627	72256.283	550	Pt II	Pt II	1400.3043	71413.049	300	Ne II	8419- 79683 K
1384.2063	72243.567	150	Pt II	27255- 99471 K	1400.6222	71396.841	250	Ne II	24879- 96131 K
1384.7471	72215.353	800	Pt II	37877-110085 K	1400.8097	71387.28	200	Ne II	24879- 96109 K
1384.89	72207.9	85	Pt II	Ne II	1401.2517	71364.766	660	Pt II	29030-100239 07
1385.9355	72153.43	270	Ne II	C	1402.2375	71314.594	880	Pt II	29030-100232 K
1386.2265	72138.283	390	Pt II	32918-105042 K	1402.7326	71289.425	170	Pt II	8419- 79607 06
1386.50	72124.1	130	Pt II	23461- 95557 K	1403.2407	71263.611	680	Pt II	1500
1387.0350	72096.234	160	Pt II	29261-101341 08	1403.4752	71251.704	8400	Pt II	15791- 87204 K
1387.3493	72079.900	390	Pt II	Ne II	1403.6827	71241.17	3800	Ne II	15791- 87204 K
1387.5158	72071.25	1600	Ne II	C	1403.9006	71230.114	74000	Pt II	15791- 87204 K
1387.6616	72063.68	130	Ne II	C	1404.3180	71208.942	2300	Pt II	15791- 87204 K
1388.34	72028.5	77	Pt II	21168- 93197 K	1404.4507	71202.215	7300	Pt II	15791- 87204 K
1388.4901	72020.68	400	Ne II	C	1404.7383	71187.638	920	Pt II	15791- 87204 K
1389.27	71980.2	27	Pt II	0- 71948 05	1405.04	71172.4	140	Ne II	15791- 87204 K
1389.8750	71948.916	5400	Pt II	Pt II	1405.3752	71155.37	1500	Ne II	15791- 87204 K
1390.17	71933.6	59	Pt II	32237-104158 K	1405.53	71147.5	90	Ne II	15791- 87204 K
1390.3982	71921.842	190	Pt II	Pt II	1406.3906	71104.002	1900	Pt II	15791- 87204 K
1390.87	71897.4	91	Pt II	37877-109753 K	1407.4447	71050.749	2900	Pt II	15791- 87204 K
1391.09	71886.1	53	Pt II	29030-100903 09	1407.7103	71037.343	1300	Pt II	15791- 87204 K
1391.2877	71875.860	1300	P	Ne II	1407.8209	71031.763	910	Pt II	15791- 87204 K
1391.3435	71872.975	1600	P	C	1407.9315	71026.183	830	Pt II	15791- 87204 K
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WAVELENGTH (ANGSTROMS) - VACUUM

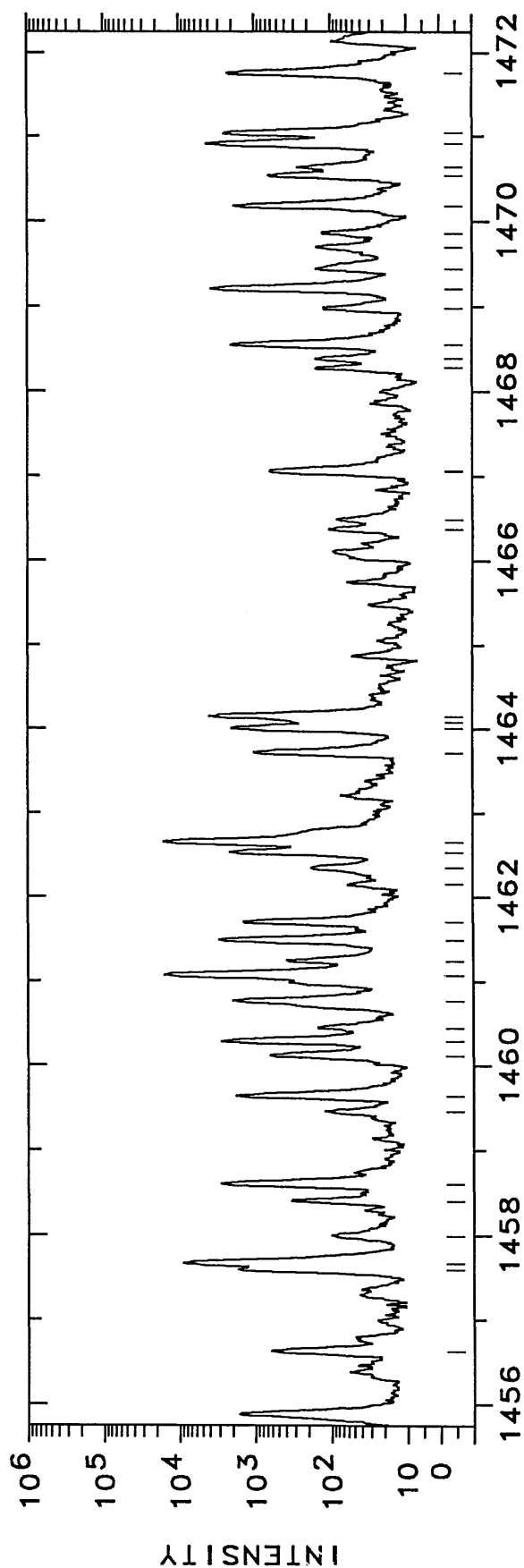
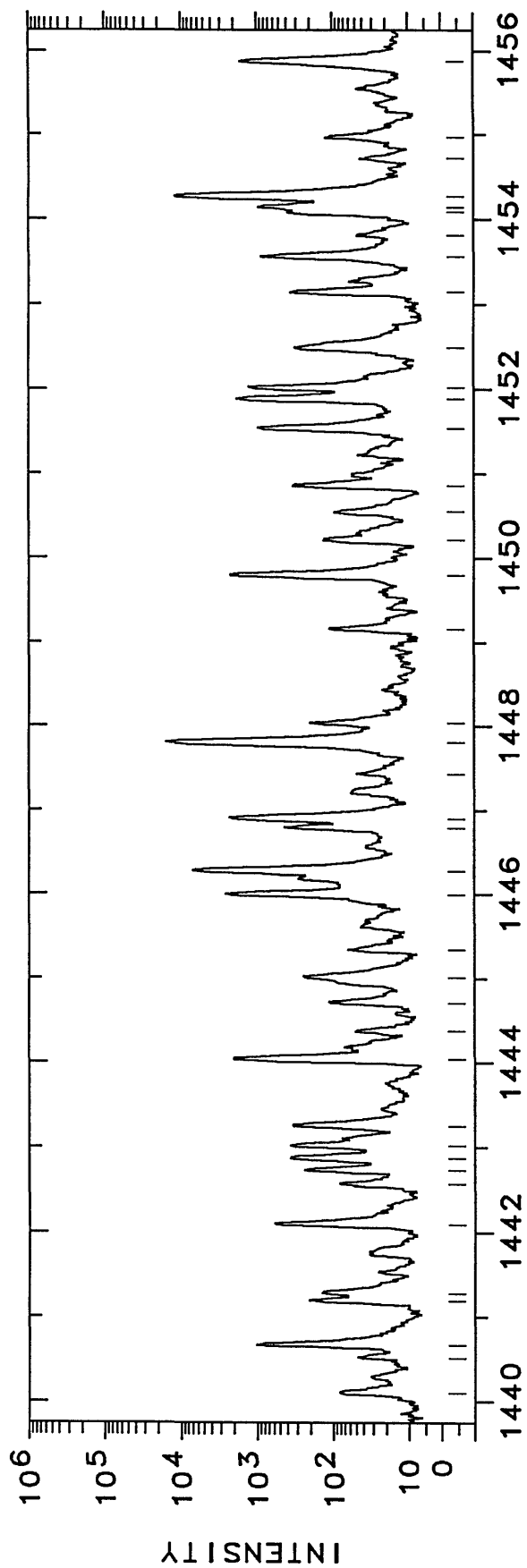
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1409.3589	70954.247	300	Pt II	23875-94829	1423.2414	70262.150	440	Ne II	
1409.4407	70950.129	840	Pt II	34647-105597	1423.5645	70246.20	1200	Pt II	32237-102414
1409.7467	70934.73	630	Ne II		1424.9510	70177.850	180	Pt II	37877-108038
1410.1346	70915.216	18000	Pt II	34647-105554	1425.3086	70160.245	950	Pt II	21168-91271
1410.2951	70907.146	1700	Pt II		1426.4824	70102.512	1800	Pt II	
1410.50	70896.8	87			1426.77	70088.4	48		
1411.09	70867.2	48			1427.04	70075.1	120		
1411.3059	70856.36	160	Ne II		1427.91	70032.4	180		
1411.62	70840.6	120	Pt II	9356-80197	1428.1530	70020.510	1200	Pt II	23461-93482
1411.76	70833.6	120	Pt II		1428.5822	69999.47	5600	Ne II	
1411.91	70826.0	62			1429.0200	69978.027	1900	Pt II	34647-104625
1412.2278	70810.106	180	Pt II	23461-94271	1429.27	69965.8	210		
1412.5350	70794.706	410	Pt II	37877-108672	1429.4024	69959.305	370	Pt II	4786-74745
1413.10	70766.4	97			1429.5248	69953.317	30000	Pt II	0-69953
1413.1988	70761.453	170	Pt II	37877-108639	1430.0503	69927.610	280	Pt II	27255-97183
1413.2736	70757.708	1100	Pt II	23875-94633	1430.6657	69897.531	570		
1413.6768	70737.526	3800	Pt II	24879-95617	1431.1564	69873.565	1000		
1413.9570	70723.51	1100	Ne II		1431.9499	69834.846	380	Pt II	8419-78254
1414.3241	70705.152	390			1432.9262	69787.265	4200	Pt II	29030-98817
1414.4573	70698.493	230	Pt II	15791-86489	1433.22	69773.0	210		
1415.00	70671.4	64			1433.4820	69760.206	370		
1415.7144	70635.71	1200	Ne II		1433.78	69745.7	140	Pt II	36484-106229
1416.20	70611.5	82			1433.9804	69735.960	250	Pt II	23461-93197
1416.30	70606.5	78			1434.36	69717.5	42		
1416.4593	70598.571	69	Pt II	32918-103517	1435.1336	69679.923	7300	Pt II	32237-101916
1417.5400	70544.749	400	Pt II	32918-103463	1435.5171	69661.309	250		
1417.8186	70530.885	4400	Pt II	27255-97786	1435.8839	69643.514	330	Pt II	13329-82972
1418.1875	70512.538	200	Pt II	36484-106996	1436.0813	69633.94	1200	Ne II	
1418.3779	70503.08	3100	Ne II		1436.3096	69622.872	8800	Pt II	4786-74409
1418.7471	70484.72	2100	Ne II		1436.7340	69602.306	950	Pt II	32918-102520
1418.7967	70482.262	300	P		1436.88	69595.2	57		
1419.6208	70441.346	550	Pt II	32237-102678	1437.24	69577.8	110	Pt II	21168-90746
1420.08	70418.6	150			1437.6951	69555.777	6300	Pt II	29261-98817
1420.5511	70395.215	2000	Pt II	34647-105042	1437.8100	69550.218	970	Pt II	9356-78906
1420.89	70378.4	82			1438.6113	69511.480	900	Pt II	34647-104158
1421.0852	70368.758	350	Pt II	36484-106852	1438.9256	69496.296	580	Pt II	32918-102414
1421.5372	70346.383	2800			1439.1596	69484.997	2300		
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WAVELENGTH (ANGSTROMS) - VACUUM

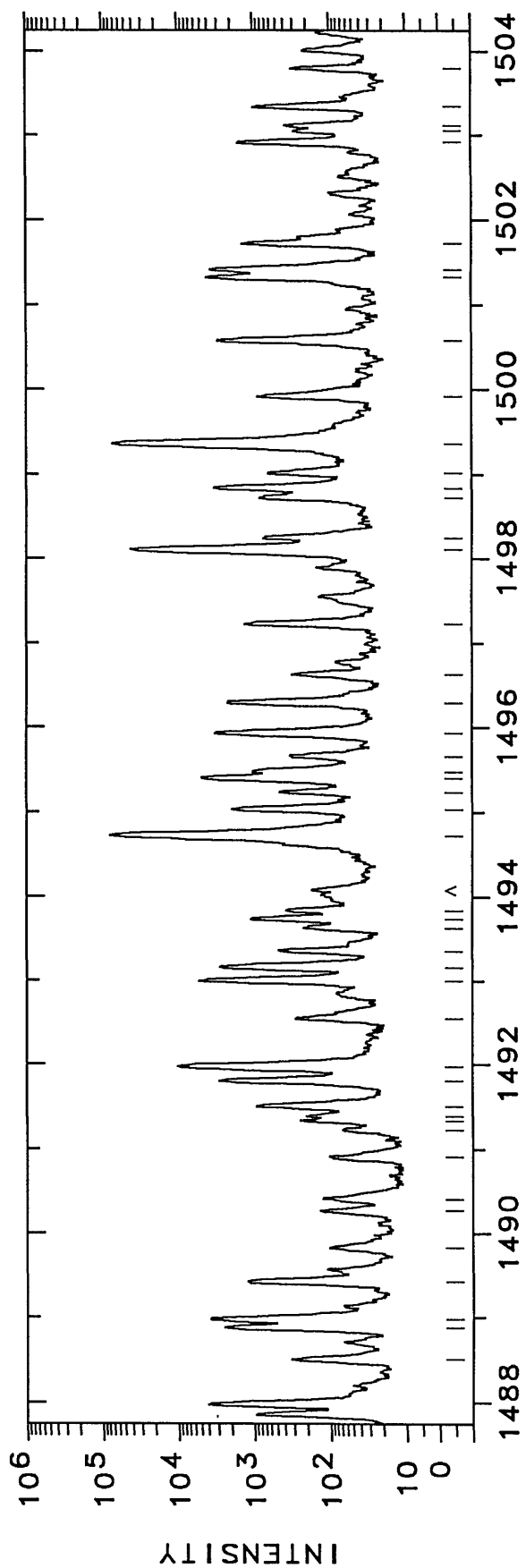
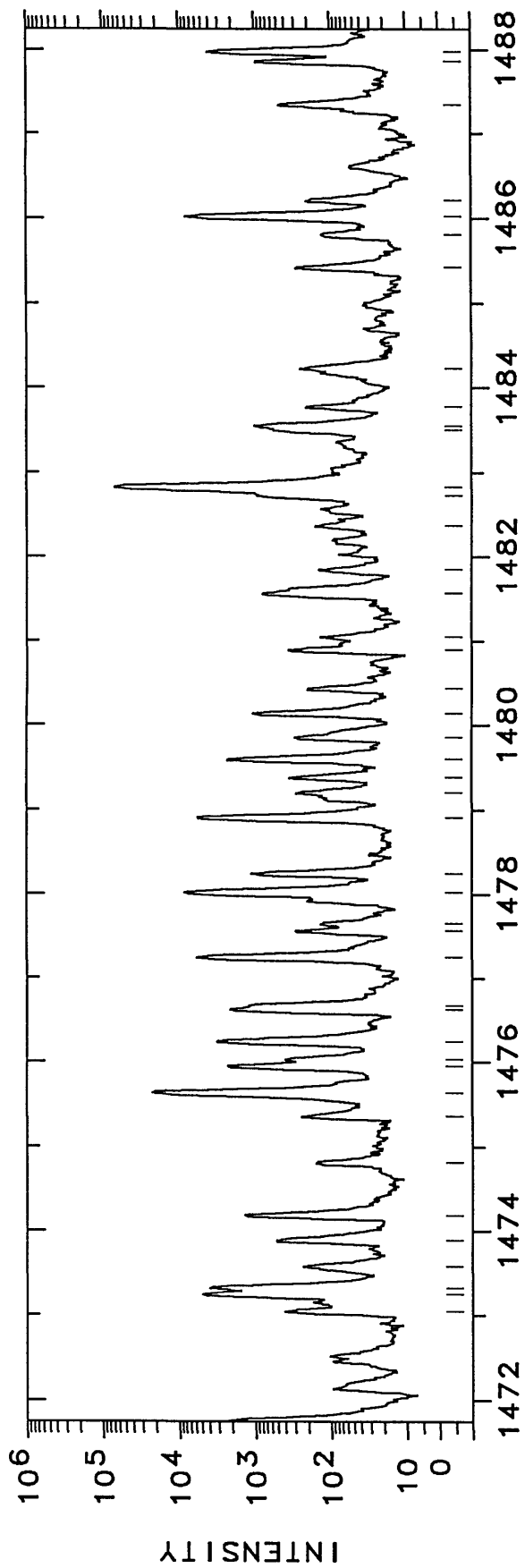


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1440.6635	69412.462	1000	Pt II	36484-105896	K	68602.533	8900	Pt II	24879-93482	11
1441.1876	69387.22	200	Ne II		1457.99	68587.6	89			
1441.28	69382.8	130			1458.3973	68568.421	330	Pt II	13329-81897	P
1442.0911	69343.747	590	Pt II	8419-77763	K	68558.659	2800	Pt II	32237-100795	09
1442.57	69320.7	71			1459.46	68518.5	110	Ne III		L
1442.7150	69313.759	230	Pt II	37877-107191	K	68510.288	1800	Pt II	43737-112247	K
1442.8676	69306.428	360	Pt II	23461-92767	K	68488.216	620	Ne III		L
1443.0133	69299.431	360	Pt II	21717-91016	K	68479.289	2800	Pt II	32918-101397	08
1443.25	69288.1	330	Pt II	23461-92749	K	68472.0	140			
1444.0351	69250.394	2100	Pt II	41434-110684	K	68456.807	1900	Pt II	24879-93336	08
1444.38	69233.9	40			1461.0786	68442.588	16000	Pt II	24879-93322	K
1444.71	69218.0	100			1461.24	68435.0	380	Ne III		L
1445.01	69203.7	240	Pt II	41434-110638	K	68423.306	3000	Pt II	32918-101341	09
1445.34	69187.9	53	Pt II	27255-96443	K	68413.290	1400	Pt II	34647-103060	K
1445.9958	69156.492	2600	Pt II	29030-98186	09	68392.0	49	Pt II	18097-86489	K
1446.2820	69142.809	6900	Pt II	24879-94022	P	68383.1	170			
1446.7921	69118.431	420	Pt II	8419-77538	K	68374.688	2100	Pt II	32237-100611	09
1446.9019	69113.186	2300	Pt II	36484-105597	K	68368.633	16000	Pt II	29261-97630	09
1447.43	69088.0	37			1462.16	68319.591	1000	Pt II	41434-109753	K
1447.8030	69070.171	16000	Pt II	36484-105554	K	68305.950	2000			
1448.04	69058.9	190			1462.5295	68302.022	350	Pt II	27255-95557	K
1449.16	69005.5	98	Pt II	16820-85826	K	68298.976	3900	Pt II	41434-109753	K
1449.8015	68974.960	2200	Pt II	4786-73761	A	68195.6	94			
1449.8015	68974.960	2200	Pt II	37877-106852	AK	68190.223	71	Pt II	8419-76610	05
1450.22	68955.1	120			1466.4859	68164.528	370	P	42031-110196	K
1450.55	68939.4	83			1467.0387	68163.450	390	P	9356-77519	05
1450.8523	68925.004	320	Pt II	29261-98186	09	68106.9	140			
1451.5382	68892.434	950	Pt II	23875-92767	K	68101.8	140			
1451.8840	68876.026	1800	Pt II	32237-101113	K	68094.142	2000	Pt II	41434-109528	K
1452.0129	68869.911	1300	Pt II	34647-103517	12	68074.4	110			
1452.49	68847.3	300			1468.98	68064.086	3800	Pt II	36484-104548	K
1453.1486	68816.089	350	Pt II	34647-103463	11	68053.1	140			
1453.5678	68796.241	870			1469.44	68041.1	140			
1453.81	68784.8	36			1469.70	68033.7	120			
1454.0865	68771.700	350			1470.1835	68018.720	1800	Pt II	37877-105896	K
1454.1586	68768.290	940	Pt II	41434-110202	K	68002.414	630	Pt II	32237-100239	08
1454.2866	68762.237	12000	Pt II	29030-97792	AK	67997.6	260			
1454.2866	68762.237	12000	Pt II	41434-110196	AK	1470.64	4300	Pt II	32918-100903	10
1454.72	68741.8	32			1470.9150	67984.893	2500	Pt II	43737-111716	K
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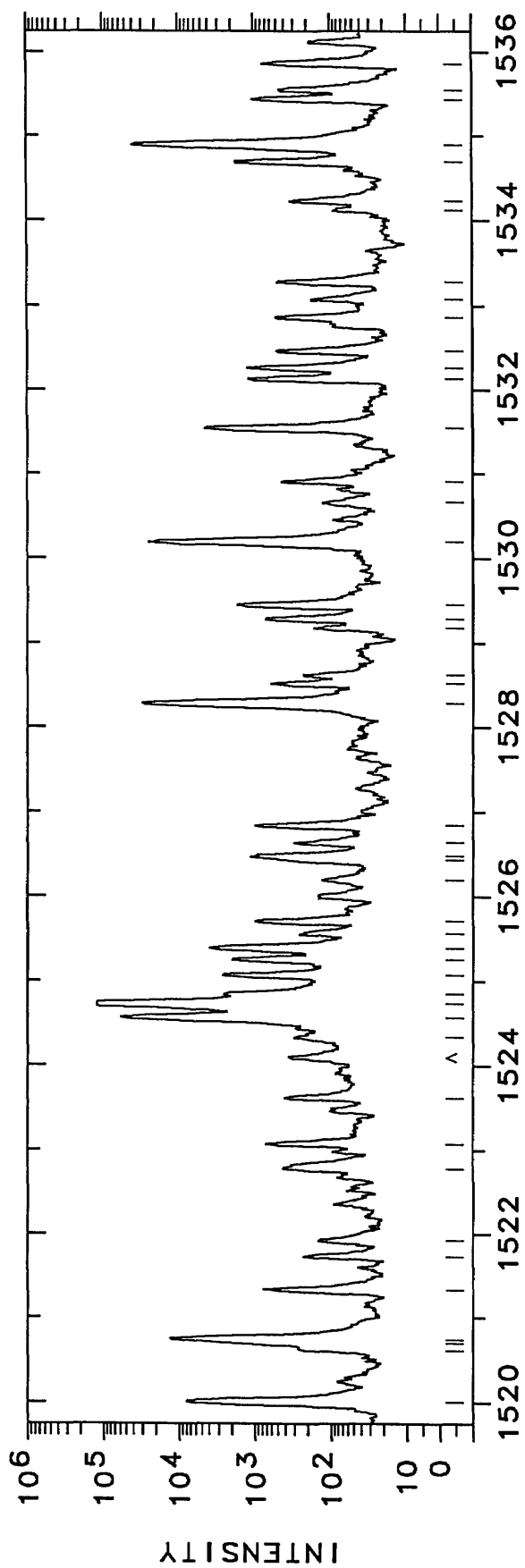
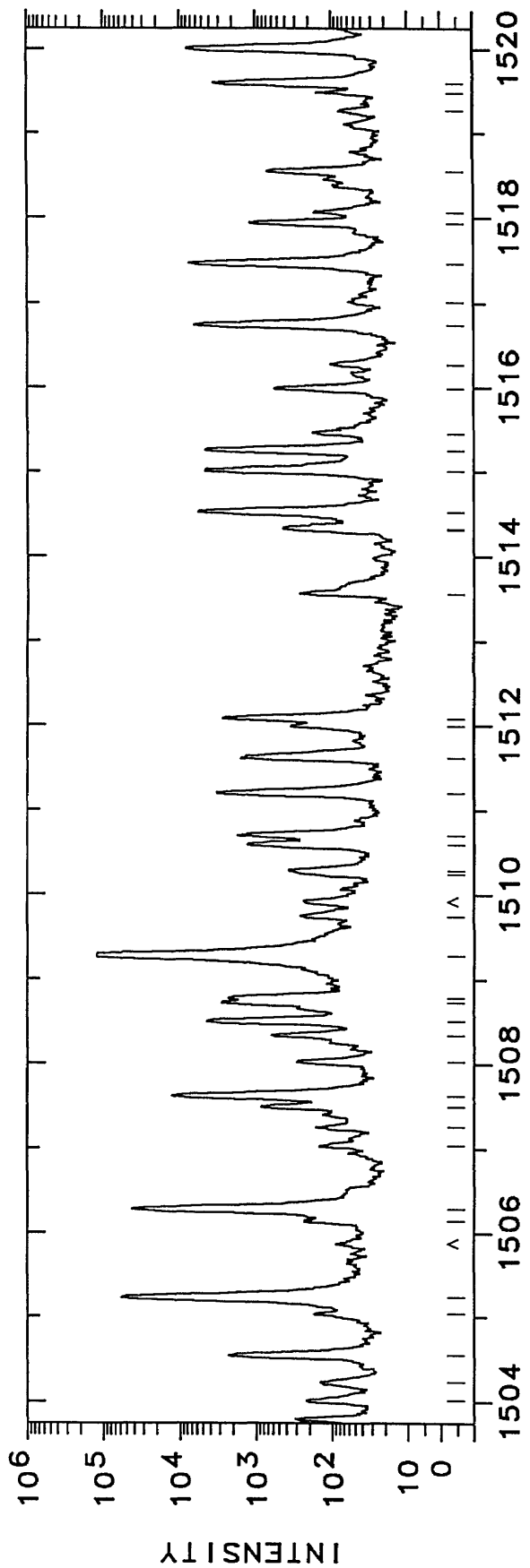
WAVELENGTH (ANGSTROMS) - VACUUM

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1473.3251	67873.683	4000	Pt II	41434-109307 AK	1489.83	67121.8	88		
1473.3251	67873.683	4000	Pt II	34647-102520 AK	1490.27	67101.9	120		
1473.5757	67862.140	220			1490.41	67095.6	110		
1473.8839	67847.949	510 L	Pt II	37877-105726 K	1490.91	67073.1	89		
1474.1931	67833.719	1300	Pt I	823- 68657 N	1491.23	67058.7	55	Ne III	L
1474.82	67804.9	150			1491.34	67053.8	230		
1475.3526	67780.407	230	Pt II	0- 67780 K	1491.39	67051.5	190		
1475.6306	67767.636	22000	Pt II	34647-102414 09	1491.5097	67046.161	910		
1475.9603	67752.50	2300	Ne II	C	1491.8030	67032.980	2900	Pt II	36484-103517 A
1476.0474	67748.502	230			1491.8030	67032.980	2900	Pt II	15791- 82824 AK
1476.2492	67739.241	3100	Pt II	46046-113785 K	1491.9735	67025.319	10000	Pt II	43737-110762 K
1476.6290	67721.818	2100	Pt II	42031-109753 K	1492.55	66999.4	270		
1476.6796	67719.497	800	Pt II	37877-105597 K	1492.9990	66979.282	5300	Pt II	36484-103463 12
1477.2547	67693.134	5700	Pt II	32918-100611 09	1493.1612	66972.004	2800	Pt II	32237- 99209 09
1477.5666	67678.844	270			1493.3508	66963.503	460		
1477.66	67674.6	120	Pt II	36484-104158 K	1493.6249	66951.214	210		
1478.0338	67657.451	8400	Pt II	24879- 92537 K	1493.7402	66946.046	1100	Pt II	8419- 75365 K
1478.2534	67647.401	1100	Pt II	24879- 92526 K	1493.8391	66941.614	360	Pt II	21168- 88110 K
1478.9117	67617.289	5700	Pt II	43737-111354 K	1494.7256	66901.912	79000	Pt II	34647-101549 P
1479.21	67603.7	270			1495.0297	66888.303	2000	Pt II	41434-108322 K
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1479.6034	67585.679	2300			1495.4014	66871.677	4900	Pt II	43737-110609 K
1479.8588	67574.015	280			1495.4796	66868.181	1000	Pt II	13329- 80197 K
1480.1489	67560.771	1000	Pt II	27255- 94829 K	1495.6544	66860.366	320		
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1479.8980	67526.595	350			1496.2958	66831.705	2200	Pt II	32237- 99068 K
1481.05	67519.7	120	Pt I	823- 68343 N	1496.63	66816.8	300		
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1481.85	67483.2	130	Ne III	L	1498.1132	66750.629	42000	Pt II	34647-101397 09
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1482.7280	67443.253	450	Pt I	823- 68266 N	1498.7213	66723.546	830	Pt II	29030- 95754 P
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1483.5530	67405.748	900			1499.3707	66694.646	73000	Pt II	34647-101341 09
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1486.0308	67293.356	8000	Pt II	41434-108727 K	1501.4245	66603.416	3600 D	Pt II	41434-108037 AK
1486.2117	67285.165	190	Pt II	23461- 90746 K	1501.7275	66589.977	1400	Pt I	823- 67413 N
1487.3425	67234.010	460	Pt II	32237- 99471 K	1502.9149	66537.367	1600		
1487.8620	67210.534	940			1503.0507	66531.357	290	Pt II	16820- 83352 09
1487.9804	67205.186	4100	Pt II	41434-108639 K	1503.1269	66527.983	300	Pt II	4786- 71314 06
1488.5058	67181.465	310	Pt II	15791- 82972 P	1503.3439	66518.380	970		
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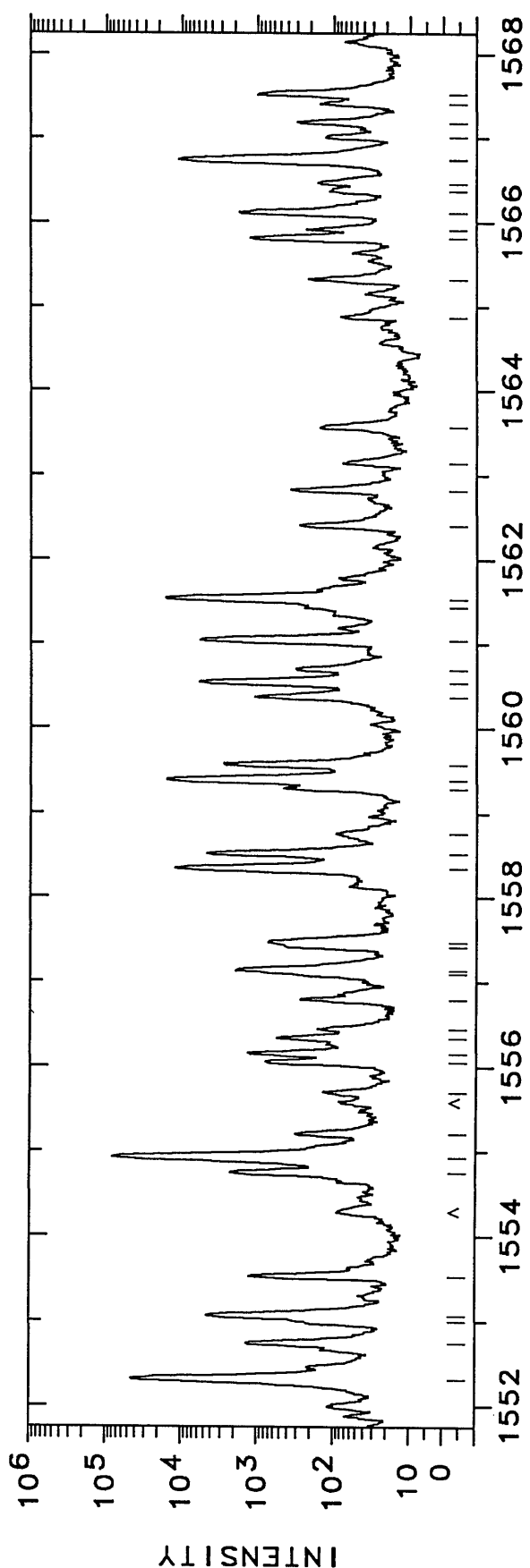
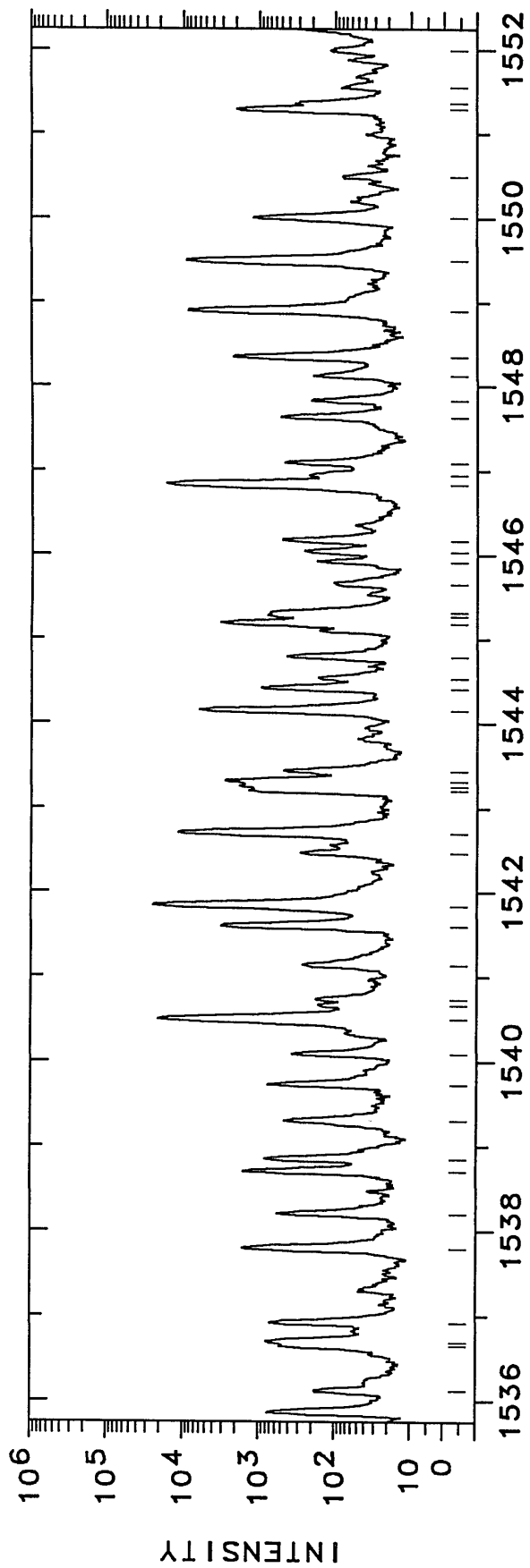
WAVELENGTH (ANGSTROMS) - VACUUM

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1504.5514	66464.994	2300	Pt II	43737-110202 K	1521.3202	65732.383	760	Pt II	23875-89607 11
1505.04	66443.4	160			1521.73	65714.7	210	Pt II	16820-82535 K
1505.2462	66434.315	58000	Pt II	0-66434 06	1521.92	65706.5	130		
1506.1480	66394.538	120			1522.7759	65669.545	410		
1506.2923	66388.177	43000	Pt II	36484-102872 K	1523.0737	65656.705	690	Pt I	775-66432 N
1507.04	66355.2	130	Pt II	29261-95617 K	1523.6106	65633.568	390	Pt II	23461-89095 K
1507.26	66345.6	150	Pt I	775-67121 N	1524.3266	65602.739	290	Pt II	29030-94633 K
1507.4998	66335.001	840	Pt II	8419-74754 08	1524.5715	65592.200	59000	Pt II	34647-100239 09
1507.6288	66329.325	13000	Pt II	43737-110066 K	1524.7295	65585.404	370000	Pt II	37877-103463 A
1508.0257	66311.867	280			1524.7295	65585.404	370000	Pt II	34647-100232 AK
1508.3427	66297.931	600	Pt I	823-67121 N	1524.8543	65580.036	2500	Pt II	8419-73999 P
1508.5129	66290.450	4400	Pt II	32918-99209 10	1525.0764	65570.486	2600	Pt II	43737-109307 K
1508.7309	66280.872	2500	Pt II	37877-104158 K	1525.2635	65562.442	2000	Pt II	41434-106996 K
1508.7910	66278.233	2300	Pt II	13329-79607 06	1525.3983	65556.648	4000 W		
1509.2920	66256.233	260000	Pt II	34647-100903 10	1525.5656	65549.459	250	Pt II	32237-97786 K
1509.75	66236.1	240			1525.7082	65543.333	980	Pt II	37877-103421 K
1510.2478	66214.299	180	Pt II	37877-104092 K	1526.20	65522.2	120		
1510.2961	66212.182	200			1526.4320	65512.253	250	Pt II	27255-92767 K
1510.5903	66199.285	1300	Pt II	8419-74619 05	1526.4791	65510.232	1100	Pt I	0-65510 N
1510.7023	66194.379	1800	Pt II	36484-102678 K	1526.64	65503.3	290		
1511.2021	66172.486	3300			1526.8391	65494.786	970		
1511.6233	66154.048	1600	Pt II	41434-107588 K	1528.2831	65432.902	31000	Pt II	36484-101916 10
1511.9871	66138.130	180			1528.5153	65422.963	600	Pt I	775-66198 N
1512.0895	66133.652	2800			1528.6138	65418.747	220	Pt II	41434-106852 K
1513.56	66069.4	250			1529.1766	65394.671	150	Pt II	4786-70181 07
1514.3107	66036.646	290 P	Pt II	36484-102520 K	1529.2942	65389.642	700	Pt II	9356-74745 04
1514.3325	66035.696	300 P	Pt II	21168-87204 K	1529.4582	65382.630	1700		
1514.5087	66028.014	5800	Pt II	0-66028 06	1530.1969	65351.069	25000	Pt II	0-65351 06
1515.0089	66006.213	4600	Pt II	42031-108038 K	1530.66	65331.3	110		
1515.2502	65995.702	4700	Pt II	43737-109733 K	1530.9006	65321.027	420	Pt II	21168-86489 K
1515.45	65987.0	170			1531.5395	65293.778	4500	Pt II	24879-90173 K
1515.9776	65964.035	560	Pt II	29261-95226 K	1532.1348	65268.410	1200	Pt II	32918-98186 10
1516.27	65951.3	90			1532.2657	65262.833	1200	Pt II	9356-74619 04
1516.7411	65930.829	6400	Pt II	36484-102414 10	1532.4605	65254.536	490	Pt II	18097-83352 10
1517.01	65919.1	46			1532.8689	65237.151	510		
1517.4695	65899.183	7500	Pt II	32918-98817 10	1533.08	65228.2	160		
1517.9314	65879.130	1200			1533.2843	65219.477	480	Pt II	23875-89095 K
1518.06	65873.5	160			1534.12	65183.9	76		
1518.5424	65852.623	690	Pt I	0-65852 N	1534.2271	65179.399	320		
1519.27	65821.1	65			1534.6947	65159.540	1700	Pt II	42031-107191 K
1519.48	65812.0	140	Pt II	29030-94842 K	1534.9063	65150.557	40000	Pt II	34647-99797 09
1519.5970	65806.921	3500			1535.4357	65128.094	1000	Pt II	23461-88589 K
1520.0051	65789.253	7800			1535.5495	65123.267	450	Pt II	13329-78452 K
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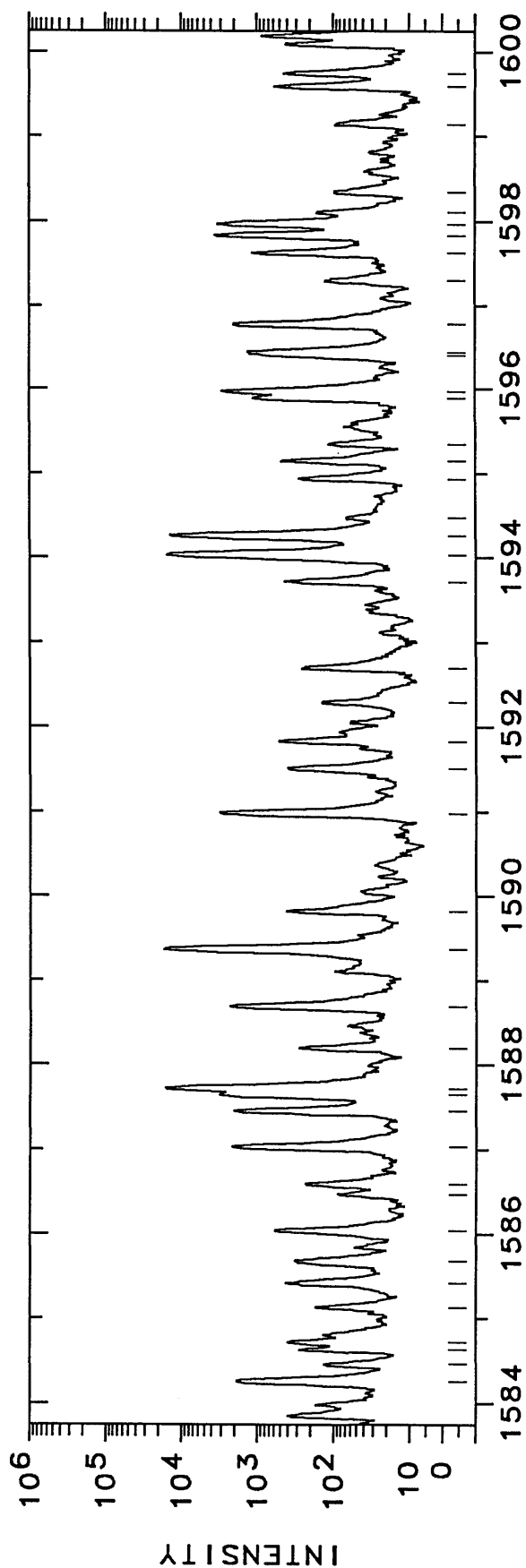
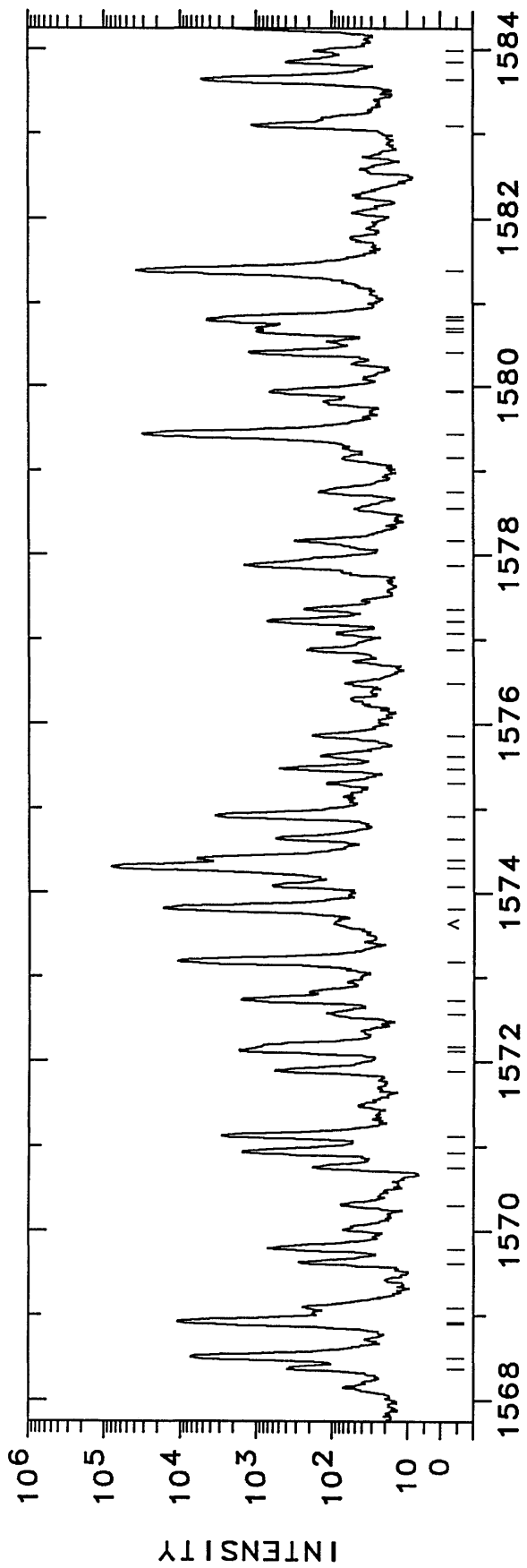
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1536.6474	65076.738	550	Pt I	775-65850 N	1552.7442	64402.108	1400	Pt II	
1536.7059	65074.261	790	Pt II	43737-108802 K	1552.9982	64391.575	180	Pt II	0-64388 07
1536.9303	65064.759	690	Pt I	823-65852 N	1553.0689	64388.642	4500	Pt I	0-64319 N
1537.7781	65028.888	1600	Pt II	43737-108727 K	1553.5288	64369.582	1300	Pt II	36484-100795 11
1538.1989	65011.098	560 W	Pt II	24879-89863 P	1554.7412	64319.586	2200	Pt II	43737-108037 K
1538.6968	64990.062	1600	Pt II	32237-97183 K	1554.9285	64311.638	80000	Pt II	
1538.8457	64983.773	810	Pt II	36484-101397 09	1555.2133	64299.862	300	Pt II	
1539.2945	64964.826	450	Pt II	0-64904 N	1555.70	64279.7	120	Pt II	32918-97183 K
1539.7316	64946.384	760	Pt II	32918-97786 K	1556.0618	64264.800	780	Pt I	0-64248 N
1540.0916	64931.203	350	Pt II	36484-101341 10	1556.1592	64260.777	1300	Pt II	23875-88110 K
1540.5040	64913.822	21000	Pt II	29261-94022 P	1556.3424	64253.213	540	Pt II	
1540.6585	64907.311	110	Pt I	775-65510 N	1556.45	64248.8	150	Pt I	0-64248 N
1540.73	64904.3	170	Pt I	775-65510 N	1556.79	64234.7	260	Pt II	23875-88110 K
1541.1327	64887.339	260	Pt II	775-65510 N	1557.0904	64222.347	180	Pt II	29261-93482 13
1541.5940	64867.922	3200	Pt II	13329-78043 P	1557.1462	64220.046	2000	Pt II	13329-77538 K
1541.8337	64857.839	25000 L	Pt II	23461-88173 K	1557.4129	64209.048	400	Pt II	32237-96443 K
1542.4651	64831.289	270	Pt II	823-65510 N	1557.4721	64206.608	450 D	Pt II	36467-98817 11
1542.7098	64821.005	12000	Pt II	41434-106229 K	1558.3479	64170.523	12000	Pt II	41434-105597 K
1543.1986	64800.474	800	Pt II	41434-106229 K	1558.5216	64163.371	4700	Pt II	
1543.2521	64798.227	1500	Pt II	41434-106229 K	1558.76	64153.6	81	Pt I	
1543.3098	64795.804	2500	Pt II	41434-106229 K	1559.2806	64132.139	280	C I	823-64904 N
1543.4274	64790.867	460 W	Pt II	29261-94022 P	1559.3893	64127.667	16000	Pt II	36484-100611 10
1544.1529	64760.426	6200	Pt II	775-65510 N	1559.5696	64120.255	2800	Pt II	41434-105554 K
1544.4116	64749.578	940	Pt I	775-65510 N	1560.3614	64087.717	1100	Pt I	
1544.53	64744.6	160	Pt I	775-65510 N	1560.5351	64080.584	6000	C I	823-64904 N
1544.7755	64734.326	420	Pt I	775-65510 N	1560.6822	64074.544	5800	Pt II	29261-93322 K
1545.1807	64717.350	3200	Pt II	13329-78043 P	1561.0312	64060.219	5800	C I	29261-93322 K
1545.2656	64713.794	600	Pt II	23461-88173 K	1561.4384	64043.513	17000	Pt II	37877-101916 A
1545.3155	64711.705	400	Pt II	823-65510 N	1561.5450	64039.141	17000	Pt II	46046-110085 AK
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1545.9171	64686.522	160	Pt I	823-65510 N	1562.3865	64004.649	360	Pt II	42031-105896 K
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1546.1695	64675.962	490	Pt II	23461-88110 K	1563.14	63973.8	64	Pt I	
1546.8248	64648.563	17000	Pt II	9356-73999 K	1563.56	63956.6	140	Pt II	
1546.9433	64643.610	200	Pt II	46046-110684 K	1564.87	63903.1	69	C I	29261-93322 K
1547.0765	64638.045	450	Pt II	8419-73026 06	1565.32	63884.7	210	Pt II	37877-101916 A
1547.6250	64615.136	520	Pt II	18097-82692 K	1565.8087	63864.762	1300	Pt II	46046-110085 AK
1547.8305	64606.558	200	Pt II	43737-108322 K	1565.91	63860.6	220	Pt I	
1548.12	64594.5	180	Pt II	37877-102414 11	1566.1156	63852.247	1800	Pt I	823-64675 N
1548.3465	64585.027	2200	Pt II	0-64515 N	1566.37	63841.9	100	Pt I	
1548.9038	64561.790	8700	Pt II	41434-105896 K	1566.46	63838.2	150	Pt I	0-63826 N
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1551.2918	64462.405	2000	Pt II	29030-93482 12	1567.1682	63809.360	290	Pt II	18097-81897 K
1551.3635	64459.426	250	Pt II	29030-93482 12	1567.41	63799.5	140	Ne II	18097-81897 K
1551.5534	64451.535	70	Pt II	29030-93482 12	1567.5248	63794.84	990	Ne II	
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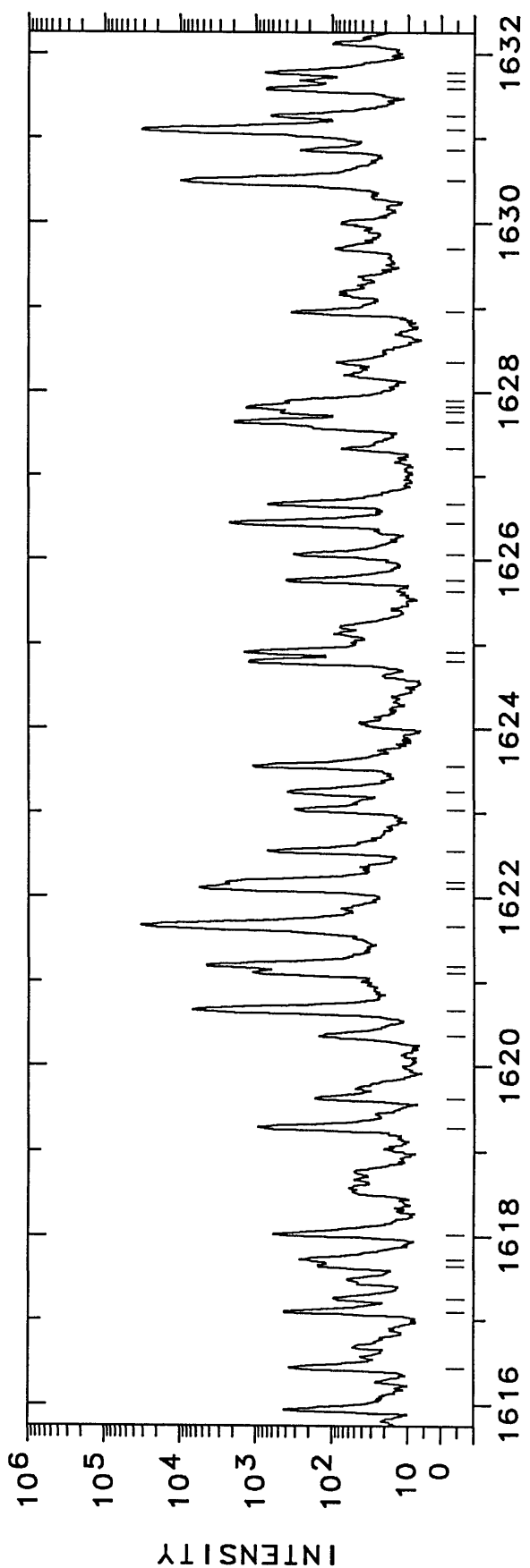
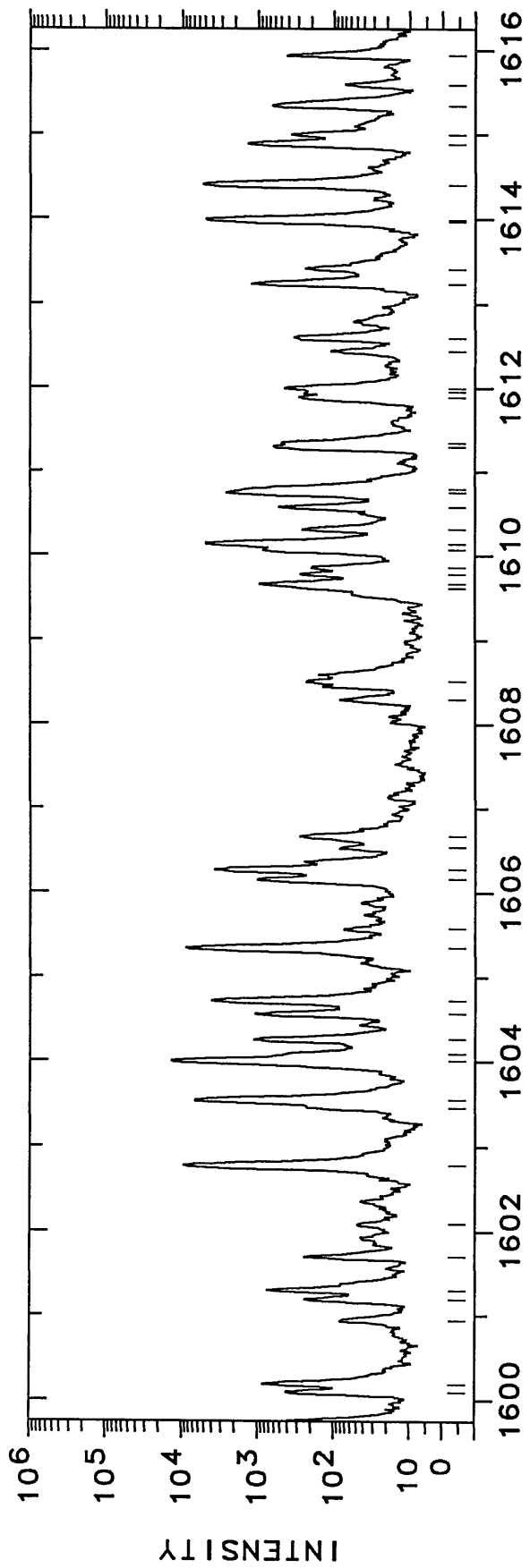


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1568.3594	63760.896	380	Pt II	27255- 91016 K	1583.8462	63137.444	380	Pt II	13329- 76461 07
1568.4948	63755.393	7200	Pt II	36484-100239 09	1583.9753	63132.298	160	Pt I	823- 63945 N
1568.9021	63738.841	11000	Pt II	0- 63738 06	1584.2474	63121.454	1900		
1568.92	63738.1	11000			1584.46	63113.0	120		
1569.09	63731.2	230			1584.6252	63106.405	280		
1569.6106	63710.069	260	Pt II	24879- 88589 K	1584.7233	63102.499	380		
1569.7820	63703.113	710			1585.13	63086.3	160		
1570.30	63682.1	64			1585.42	63074.8	410	Ne III	
1570.75	63663.9	170	Ne III		1585.68	63064.4	310	Ne III	
1570.9275	63656.661	1500	Pt II	48591-112247 K	1586.0312	63050.462	570	Pt I	775- 63826 N
1571.1196	63648.878	2900	Pt II	43737-107386 K	1586.47	63033.0	75	Ne III	
1571.8842	63617.918	570	Pt II	117493- 53875 K	1586.59	63028.3	220	Pt II	23461- 86489 K
1572.1223	63608.283	1700	Pt II	41434-105042 K	1587.0368	63010.511	200	Pt II	42031-105042 K
1572.1752	63606.143	1000			1587.4559	62993.876	2000	Pt II	4786- 67780 K
1572.56	63590.6	110	Ne III		1587.6482	62986.246	2500	Pt II	18097- 81083 AK
1572.7201	63584.105	1600	Pt II	41434-105018 K	1587.6482	62986.246	2500	Pt II	42031-105018 AK
1573.1802	63565.509	11000	Pt II	42031-105597 K	1587.7205	62983.379	16000	Pt II	34647- 97630 11
1573.8180	63539.750	17000	Pt II	34647- 98186 10	1588.1904	62964.743	270		
1574.0819	63529.094	610	Pt II	8419- 71948 06	1588.6920	62944.863	2300	Pt II	8419- 71364 K
1574.3059	63520.058	82000	Pt II	37877-101397 10	1589.3755	62917.874	17000	Pt II	37877-100795 12
1574.4002	63516.252	5500	Pt II	37877-101397 K	1589.8128	62900.487	400		
1574.6393	63506.608	540	Pt II	29030- 92537 K	1590.9851	62854.140	3100		
1574.9089	63495.736	3500	Pt I	823- 64319 N	1591.5069	62833.532	390		
1575.30	63480.0	110			1591.8192	62821.205	500		
1575.4706	63473.098	490	Pt I	775- 64248 N	1592.29	62802.6	130		
1575.62	63467.1	130			1592.6974	62786.566	250	Pt II	16820- 79607 07
1575.86	63457.4	170			1593.7073	62746.779	420		
1576.48	63432.5	55			1594.0344	62733.903	15000	Pt II	37877-100611 11
1576.88	63416.4	200			1594.2611	62724.983	14000	Pt II	36484- 99209 11
1577.07	63408.7	74			1594.47	62716.8	54		
1577.2202	63402.688	710			1594.9347	62698.492	270	Pt II	32918- 95617 K
1577.3573	63397.177	220			1595.1388	62690.469	460	Pt I	775- 63466 N
1577.8723	63376.485	1400	Pt II	16820- 80197 K	1595.34	62682.6	100		
1578.17	63364.5	300			1595.8834	62661.220	1100	Pt II	15791- 78452 K
1578.55	63349.3	37			1595.9644	62658.039	2900	Pt II	41434-104092 K
1578.75	63341.3	140			1596.3988	62640.99	450	Ne II	
1579.15	63325.2	61			1596.4379	62639.455	1100	Pt II	29030- 91669 K
1579.4357	63313.750	32000	Pt II	36484- 99797 09	1596.7767	62626.164	2000	Pt II	46046-108672 K
1579.9278	63294.032	550 P	Pt II	24879- 88173 K	1597.30	62605.6	110	Pt II	32237- 94842 K
1579.9481	63293.218	300 U			1597.6295	62592.735	1100	Pt II	9356- 71948 A
1580.4001	63275.116	1200	Pt II	29261- 92537 K	1597.6295	62592.735	1100	Pt II	32237- 94829 AK
1580.6548	63264.920	700	Pt II	29261- 92526 K	1597.8343	62584.712	3500	Pt II	36484- 99068 K
1580.7121	63262.627	1000			1597.9705	62579.38	3300	Ne II	
1580.8013	63259.057	3000 P	Pt II	43737-106996 K	1598.11	62573.9	150		
1580.8322	63257.821	1800 P	Pt II	43737-106995 K	1598.34	62564.9	82		
1581.3980	63235.188	37000	Pt II	37877-101113 K	1599.34	62533.6	80		
1583.0953	63167.391	1100	Pt I	0- 63167 N	1599.5855	62516.274	570	Pt II	42031-104548 K
1583.6406	63145.641	5200	Pt II	34647- 97792 K	1599.7339	62510.396	430	Pt I	0- 62510 N



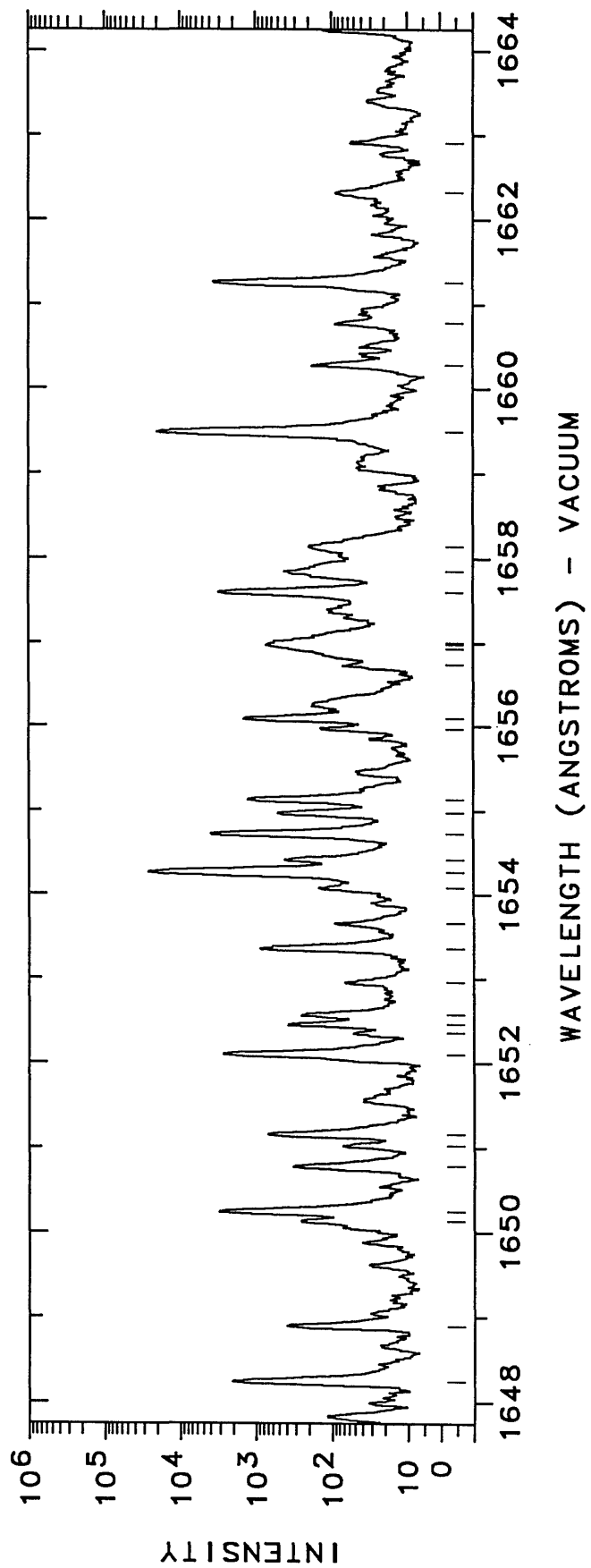
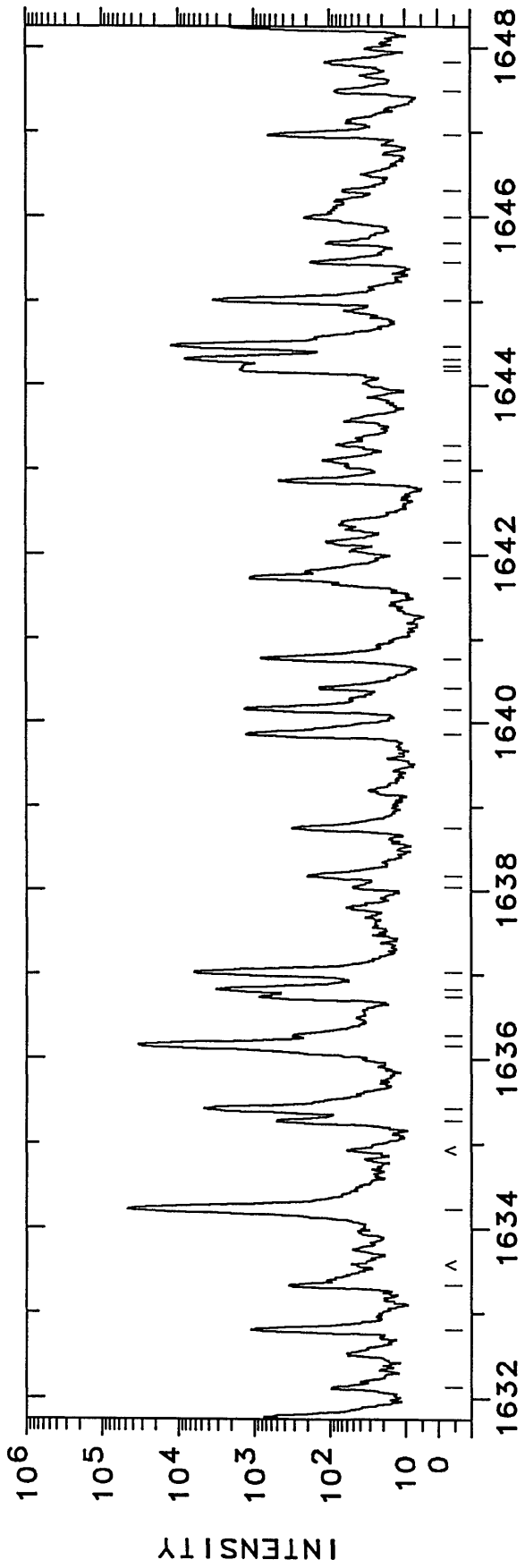
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1600.1934	62492.446	850	Pt II	43737-106229 K	1615.3211	61907.196	630		
1600.94	62463.3	73	Pt II	15791- 78254 K	1615.59	61896.9	61		
1601.1825	62453.843	230			1615.9441	61883.329	410	Pt I	775- 62659 N
1601.2962	62449.408	750			1616.43	61864.7	350		
1601.70	62433.7	230			1617.0934	61839.347	410	Pt II	27255- 89095 K
1602.09	62418.5	40			1617.25	61833.4	84		
1602.7837	62391.451	9500	Pt I	775- 63167 N	1617.64	61818.5	140		
1603.4612	62365.089	200	Pt II	23461- 85826 K	1617.7194	61815.417	250		
1603.5502	62361.629	6600	Pt II	37877-100239 10	1618.0184	61803.994	580	Pt II	21168- 82972 P
1604.0102	62343.743	14000	Ne II	A	1619.2728	61756.117	930	Pt II	34647- 96403 K
1604.0102	62343.743	14000	Pt I	823- 63167 AN	1619.62	61742.9	160		
1604.0927	62340.54	300	Ne II	C	1620.36	61714.7	140	Pt II	32918- 94633 K
1604.2682	62333.716	1100	Pt II	36484- 98817 11	1620.6682	61702.943	6800	Pt II	36484- 98186 11
1604.5702	62321.985	1100	Pt I	0- 62321 N	1621.1049	61686.323	1100 D		
1604.7337	62315.635	4100	Ne III		1621.1897	61683.096	4500	Pt II	50564-112247 K
1605.3536	62291.572	8800	Pt I	775- 63067 N	1621.6590	61665.247	33000 L	Pt II	0- 61665 A
1605.58	62282.8	63			1621.6590	61665.247	33000 L	Pt II	9356- 71021 AK
1606.1550	62260.492	1000			1622.1204	61647.704	5500	Pt II	4786- 66434 07
1606.2741	62255.875	3700			1622.1824	61645.349	2000	Pt I	0- 61645 N
1606.54	62245.6	74			1622.5440	61631.611	690	Pt II	16820- 78452 K
1606.6658	62240.698	280	Pt II	29030- 91271 K	1623.0259	61613.311	290		
1608.30	62177.5	72			1623.2360	61605.337	370	Pt II	42031-103637 K
1608.5173	62169.05	220	Ne II	C	1623.5577	61593.130	1100	Pt II	37877- 99471 K
1609.6117	62126.785	200	Pt II	42031-104158 K	1624.7988	61546.082	1200	Pt I	775- 62321 N
1609.6647	62124.739	930			1624.9144	61541.703	1400	Pt II	46046-107588 K
1609.78	62120.3	270			1625.6270	61514.726	1900	Al II	
1609.8562	62117.349	190			1625.7587	61509.745	380	Pt II	18097- 79607 07
1610.0697	62109.112	800	Pt I	46046-108155 K	1626.0619	61498.274	300	Pt I	823- 62321 N
1610.1405	62106.381	4800	Pt I	0- 62106 N	1626.4387	61484.026	2200	Pt II	34647- 96131 K
1610.3173	62099.563	250	Pt II	18097- 80197 K	1626.6610	61475.624	670	Pt II	48591-110066 K
1610.5649	62090.016	520	Pt I	6567- 68657 N	1627.33	61450.4	62		
1610.7448	62083.081	2600	Pt II	41434-103517 K	1627.6535	61438.138	1900	Pt II	41434-102872 K
1610.7907	62081.312	1900			1627.7656	61433.907	450	Pt II	16820- 78254 K
1611.2844	62062.290	600	Pt I	0- 62062 N	1627.8299	61431.480	1300	Pt II	42031-103463 K
1611.3397	62060.160	300	Pt II	42031-104092 K	1627.9003	61428.823	350		
1611.8840	62039.204	280	Pt I	6567- 68606 N	1628.36	61411.5	75		
1611.9533	62036.537	250	Pt II	13329- 75365 K	1628.9482	61389.306	320	Pt II	42031-103421 K
1612.0071	62034.466	440	Pt II	32237- 94271 K	1629.70	61361.0	79		
1612.44	62017.8	99	Pt II	48591-110609 K	1630.4910	61331.219	6200 P	Pt II	37877- 99209 12
1612.5934	62011.912	330	Pt I	823- 62835 N	1630.5063	61330.643	4600 U	Pt I	775- 62106 N
1613.2389	61987.099	1200	Pt II	41434-103421 K	1630.86	61317.3	240		
1613.41	61980.5	230			1631.0903	61308.684	32000	Pt II	36484- 97792 K
1613.9653	61959.201	800	Pt II	8419- 70379 08	1631.2626	61302.209	610		
1613.9882	61958.320	4000	Pt II	9356- 71314 04	1631.5907	61289.880	710	Pt II	13329- 74619 04
1614.4078	61942.218	5200	Pt I	0- 61942 N	1631.6826	61286.429	200	Pt I	775- 62062 N
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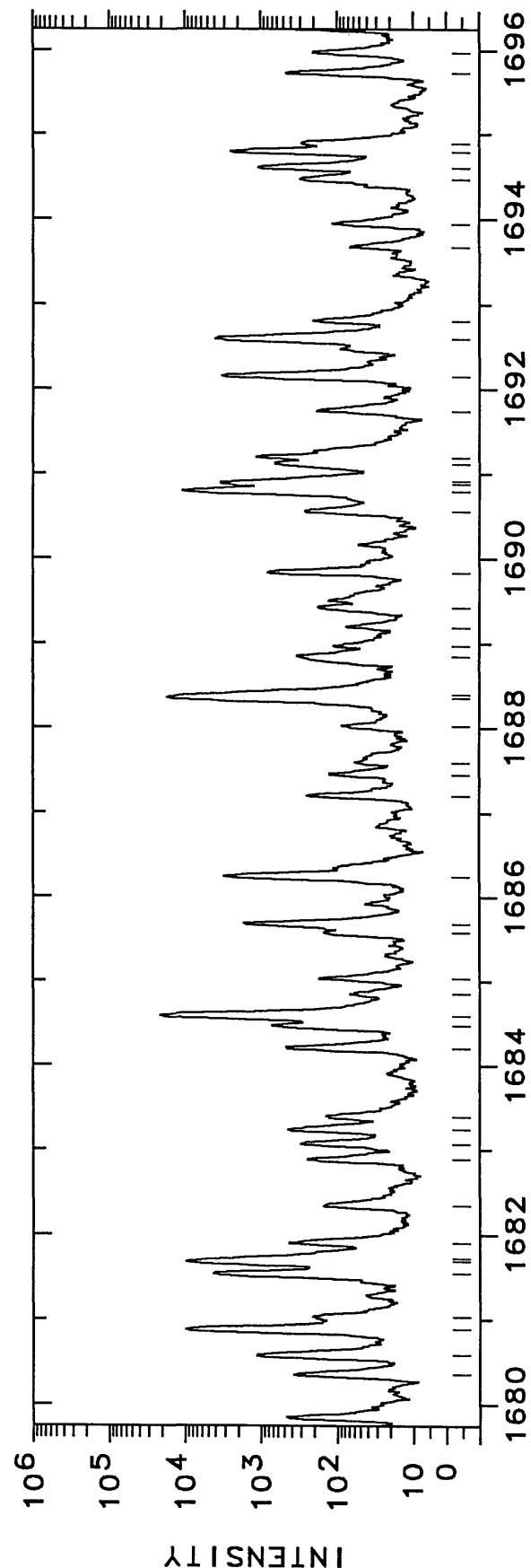
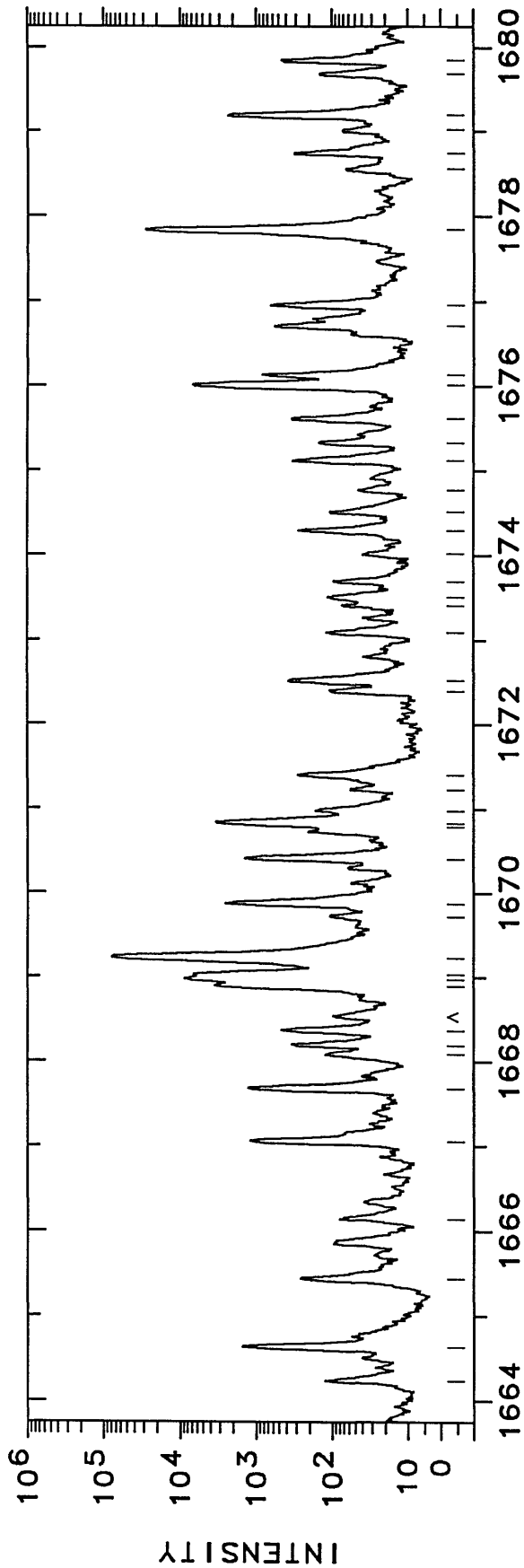


WAVELENGTH (ANGSTROMS) - VACUUM

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
1632.13	61269.6	87	Pt II	41434-102678	1648.2494	60670.430	2100	Pt II	13329-73999
1632.8049	61244.304	1100	Pt II	41434-102678	1648.9010	60646.455	390	Pt II	42031-102678
1633.3302	61224.607	340	Pt II	37877-99068	1650.1301	60601.282	250	Pt II	29261-89863
1634.2337	61190.759	46000	Pt II	50564-111716	1650.2455	60597.043	3100	Pt II	9356-69953
1635.2334	61151.854	500	Pt II	36484-97630	1650.7791	60577.457	320	Pt II	29030-89607
1635.4147	61146.572	4600	Pt II	823-61942	1651.03	60568.3	61	Pt II	32918-93482
1636.1647	61118.541	34000	Pt I	0-61097	1651.1608	60563.452	680	Pt II	823-61352
1636.28	61114.2	310	Pt I	43737-104831	1652.1112	60528.613	2700	Pt I	
1636.7302	61097.425	850	Pt II	41434-102520	1652.36	60519.5	41	Pt II	
1636.8152	61094.252	3200	Pt II	9356-70379	1652.4522	60516.123	370	Pt II	32237-92749
1637.0168	61086.728	6200	Pt II	41434-102520	1652.5631	60512.062	240	Pt II	
1638.04	61048.6	40	Ne III		1652.96	60497.5	57	Pt II	41434-101916
1638.18	61043.4	190	Pt II	9356-70379	1653.3618	60482.830	860	Pt II	
1638.7331	61022.749	310	Pt II	41434-102414	1653.66	60471.9	81	Pt II	
1639.8606	60980.793	1300	Pt II	34647-95617	1654.08	60456.6	140	Pt II	
1640.1553	60969.836	1300	Pt II	32237-93197	1654.2659	60449.774	26000	Pt II	
1640.41	60960.4	130	Pt II	24879-85826	1654.4140	60444.363	400	Pt II	
1640.7691	60947.028	790	Pt II	29261-90173	1654.7384	60432.512	3900	Pt I	13329-73761
1641.7317	60911.293	1100	Pt II	24879-85775	1654.9743	60423.899	500	Pt I	0-60423
1642.15	60895.8	99	Pt II	775-61645	1655.1434	60417.726	1300	Pt II	32918-93336
1642.8597	60869.471	450	Pt I		1655.97	60387.6	130	Pt II	
1643.11	60860.2	110	Pt II	24879-85700	1656.0959	60382.977	1400	Pt II	42031-102414
1643.29	60853.5	70	Pt II	15791-76610	1656.74	60359.5	60	Pt I	6567-66927
1644.1761	60820.736	1300	Pt II	8419-69235	1656.9283	60352.641	60	C I	
1644.2292	60818.770	1100	Pt II	823-61633	1656.9728	60351.021	400	C I	
1644.3084	60815.843	7900	Pt II	50564-111354	1657.0082	60349.732	400	C I	
1644.4634	60810.110	12000	Pt I		1657.6053	60327.992	3000	Pt I	0-60328
1645.0044	60790.111	3400	Pt II		1657.85	60319.1	400	Pt I	
1645.46	60773.3	170	Pt II		1658.14	60308.5	190	Pt II	
1645.69	60764.8	100	Pt II	16820-77538	1659.4860	60259.623	20000	Pt II	4786-65046
1645.99	60753.7	200	Pt II		1660.28	60230.8	170	Pt II	
1646.31	60741.9	56	Pt II		1660.78	60212.7	78	Pt II	
1646.9762	60717.332	640	Pt II		1661.2608	60195.245	3500	Pt II	34647-94842
1647.49	60698.4	75	Pt II		1662.32	60156.9	76	Pt II	18097-78254
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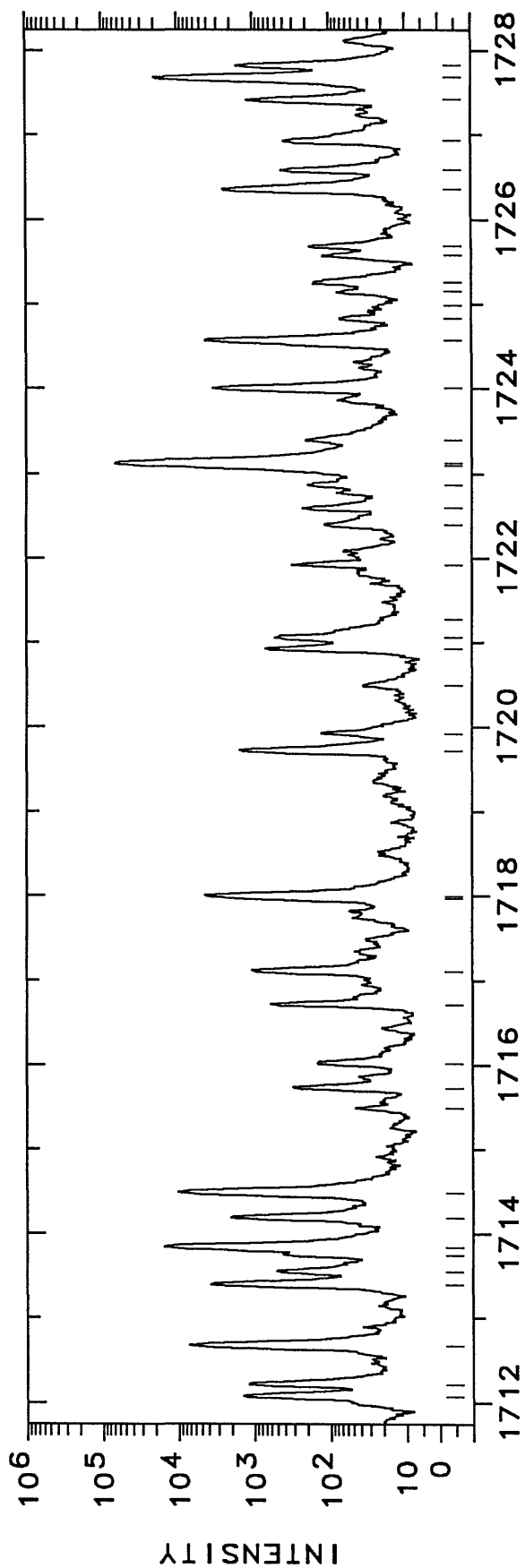
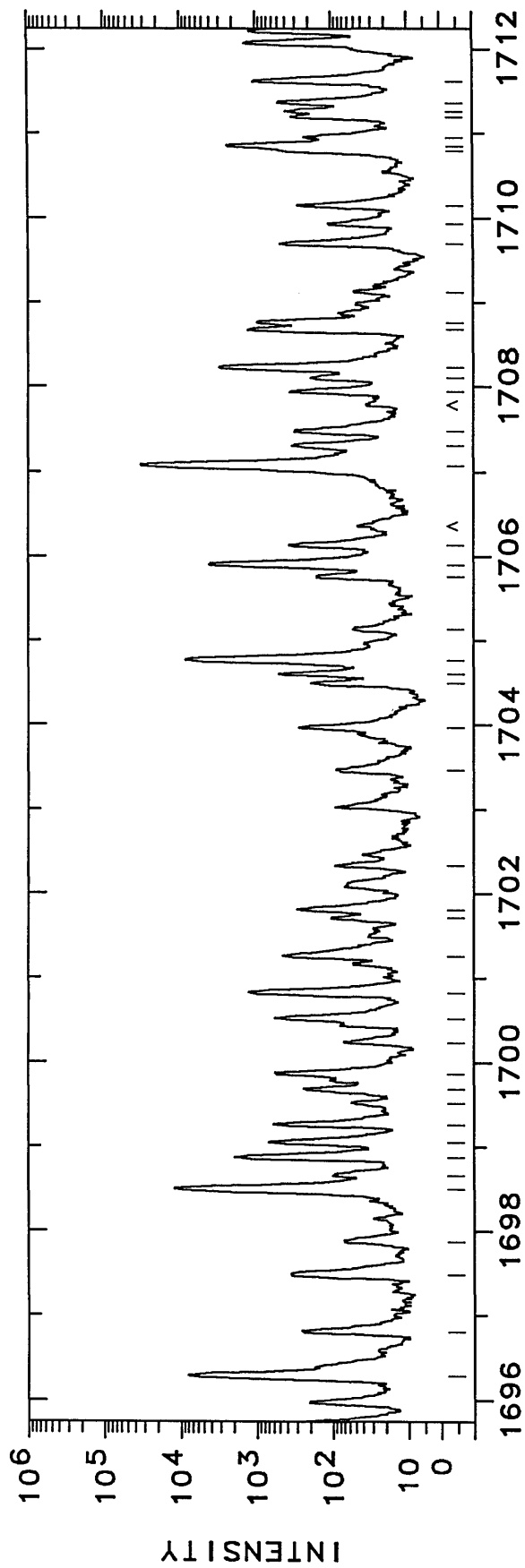
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1664.6312	60073.366	1500	Pt II	50564-110609 K	1681.5384	59469.353	4200	Pt II	41434-100903 K
1665.4292	60044.582	250	Pt II		1681.6840	59464.21	9600	Ne II	
1666.14	60019.0	70			1681.7207	59462.906	1300 U		
1667.0557	59985.998	1200	Pt II	34647- 94633 K	1681.9119	59456.146	420		
1667.6740	59963.758	1300	Pt II	41434-101397 K	1682.34	59441.0	140		
1668.09	59948.8	110	Pt II	27255- 87204 K	1682.8781	59422.010	230	Pt II	18097- 77519 06
1668.1882	59945.275	330	Pt II	18097- 78043 P	1683.07	59415.2	290		
1668.3644	59938.944	450			1683.24	59409.2	430		
1668.9014	59919.657	3500 D	Pt II	36484- 96403 AK	1683.39	59403.9	130		
1668.9014	59919.657	3500 D	Pt I	0- 59920 A	1683.39	59403.9	130		
1668.9782	59916.900	8000	Pt I	0- 59916 N	1684.2054	59375.181	460	Pt II	34647- 94022 P
1669.0350	59914.861	6000	Pt II	37877- 97792 K	1684.4637	59366.076	710	Pt II	42031-101397 K
1669.2312	59907.819	77000	Pt II	41434-101341 K	1684.5867	59361.741	21000	Pt II	41434-100795 AK
1669.7070	59890.748	98	Pt II	23461- 83352 12	1684.5867	59361.741	21000	Pt II	42031-101394 AK
1669.8647	59885.091	2500	Pt II	42031-101916 K	1684.85	59352.5	58		
1670.4235	59865.058	1400	Pt I	6567- 66432 N	1685.03	59346.1	160		
1670.7878	59852.005	1300	Al II		1685.58	59326.8	140		
1670.8423	59850.053	1300	Pt II	46046-105896 K	1685.58	59326.8	140		
1670.98	59845.1	150			1685.58	59326.8	140		
1671.23	59836.2	47	Ne III		1685.58	59326.8	140		
1671.40	59830.1	270	Ne III		1685.58	59326.8	140		
1672.39	59794.7	99			1685.58	59326.8	140		
1672.5164	59790.146	370	Pt II	15791- 75581 07	1685.58	59326.8	140		
1673.09	59769.6	110			1685.58	59326.8	140		
1673.41	59758.2	64			1685.58	59326.8	140		
1673.51	59754.6	100			1685.58	59326.8	140		
1673.69	59748.2	86			1685.58	59326.8	140		
1674.02	59736.4	29			1685.58	59326.8	140		
1674.2916	59726.75	260	Ne II		1685.58	59326.8	140		
1674.51	59719.0	97			1685.58	59326.8	140		
1674.77	59709.7	35	Pt I	6140- 65850 N	1685.58	59326.8	140		
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1675.3280	59689.804	140	Pt II	21168- 80858 10	1685.58	59326.8	140		
1675.6133	59679.641	330	Pt II	46046-105726 K	1685.58	59326.8	140		
1676.0154	59665.323	6700	Pt I	775- 60441 N	1685.58	59326.8	140		
1676.1308	59661.215	820			1685.58	59326.8	140		
1676.7093	59640.632	560	Pt II	16820- 76461 07	1685.58	59326.8	140		
1676.9604	59631.700	640	Pt II	50564-110196 K	1685.58	59326.8	140		
1677.8443	59600.286	28000	Pt I	823- 60423 N	1685.58	59326.8	140		
1678.56	59574.9	57			1685.58	59326.8	140		
1678.7493	59568.156	310			1685.58	59326.8	140		
1679.02	59558.6	62			1685.58	59326.8	140		
1679.2007	59552.143	2300	Pt I	775- 60328 N	1685.58	59326.8	140		
1679.69	59534.8	130			1685.58	59326.8	140		
1679.8544	59528.969	450			1685.58	59326.8	140		
1680.3563	59511.188	360	Pt II	23461- 82972 P	1685.58	59326.8	140		
1680.5783	59503.327	1100	Pt I	0- 59492 N	1685.58	59326.8	140		
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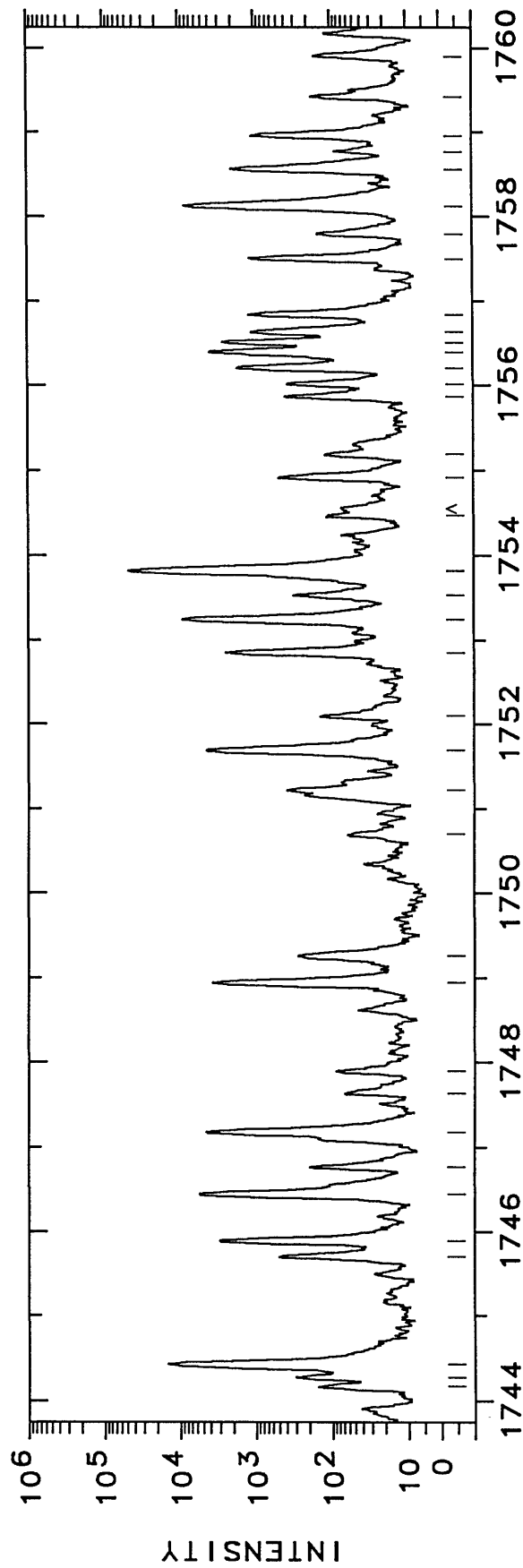
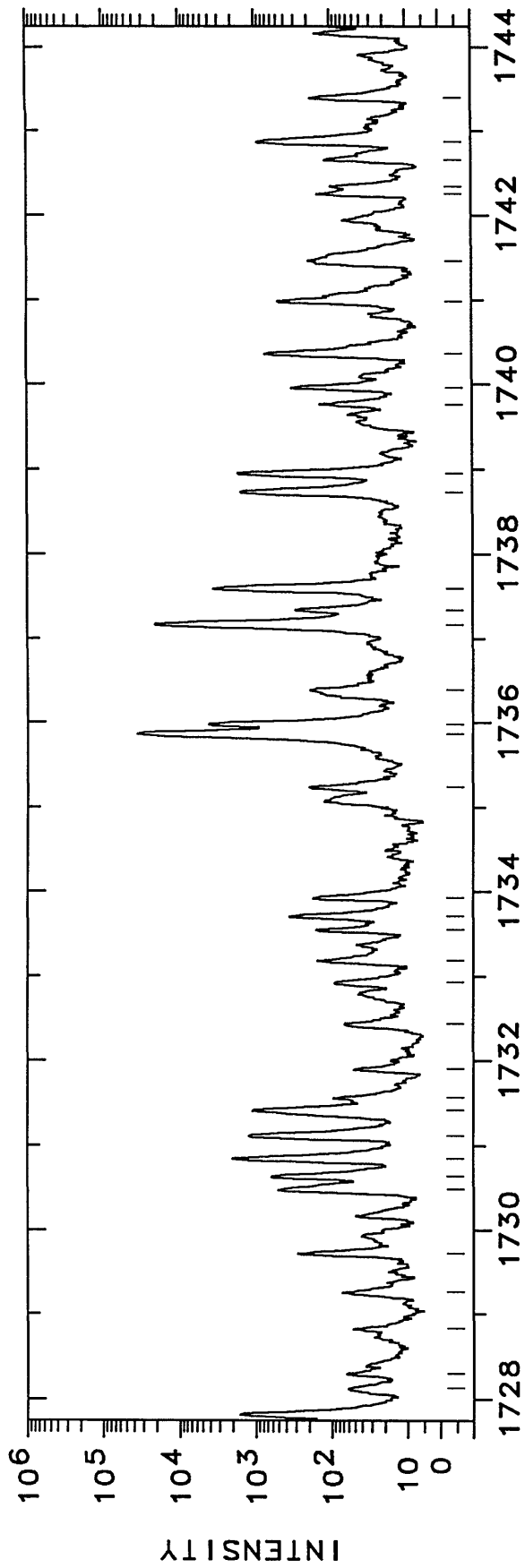
WAVELENGTH (ANGSTROMS) - VACUUM



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1696.2887	58952.230	8100	Pt II	4786- 63758 07	1711.6209	58424.152	1100	Pt II	9356- 67780 K
1696.7990	58934.500	250			1712.0665	58408.946	1400	Pt II	
1697.48	58910.9	340			1712.2098	58404.058	1200	Pt II	48591-106995 K
1697.87	58897.3	61	Ne III		1712.6670	58388.467	7300	Pt I	0- 58388 N
1698.4958	58875.624	12000	Pt II	43737-102613 K	1713.3934	58363.713	3700	Pt II	41434- 99797 AK
1698.66	58869.9	89			1713.3934	58363.713	3700	Pt II	18097- 76461 A
1698.8732	58862.545	1900	Pt I	823- 59686 N	1713.3934	58363.713	3700	Pt II	16820- 75184 AK
1699.0497	58856.430	680			1713.5477	58358.457	500	Pt II	36484- 94842 K
1699.2606	58849.125	600			1713.7421	58351.837	400	Pt I	775- 59127 N
1699.52	58840.1	47			1713.8364	58348.627	16000	Pt II	43737-102086 K
1699.6746	58834.792	230	Pt II	34647- 93482 15	1714.1842	58336.788	2100	Pt I	6567- 64904 N
1699.8757	58827.831	560	Pt II	15791- 74619 05	1714.4801	58326.720	10000	Pt I	0- 58326 N
1700.24	58815.2	61			1715.49	58292.4	37		
1700.5245	58805.386	570	Pt II	41434-100239 K	1715.7210	58284.535	300		
1700.8188	58795.211	1300	Pt II	48591-107386 K	1716.02	58274.4	140		
1701.2700	58779.618	450	Pt II	32237- 91016 K	1716.7118	58250.896	600		
1701.71	58764.4	94	Pt II	42031-100795 K	1717.1032	58237.618	1100	Pt II	50564-108802 K
1701.8227	58760.528	280	Pt II	16820- 75581 07	1717.9693	58208.258	1200 U	Pt II	15791- 73999 P
1702.33	58743.0	82			1717.9888	58207.597	4400 P	Pt II	42031-100239 K
1703.46	58704.0	79	Pt I	775- 59462 N	1719.7159	58149.140	1500	Pt II	36484- 94653 K
1703.9703	58686.469	270	Pt I	823- 59492 N	1719.92	58142.2	120		
1704.49	58668.6	180	Pt I		1720.49	58123.0	26		
1704.5981	58664.855	500			1720.9199	58108.457	680	Pt I	6567- 64675 N
1704.7667	58659.053	8400	Pt II	24879- 83538 K	1721.0604	58103.713	510 D		
1705.13	58646.6	44			1721.2723	58096.560			
1705.76	58624.9	150			1721.9209	58074.677	310	Al II	
1705.9115	58619.689	4200	Pt II	13329- 71948 05	1722.40	58058.5	110	Pt II	50564-108639 K
1706.1353	58611.999	360			1722.60	58051.8	220	Pt I	6567- 64619 N
1707.0710	58579.872	33000	Pt II	42031-100611 K	1722.87	58042.7	180	Pt II	115060- 57018 K
1707.3021	58571.942	330			1723.0983	58034.994	3500		
1707.4716	58566.128	300	Pt II	37877- 96443 K	1723.1314	58033.878	68000	Pt II	4786- 62820 07
1707.9344	58550.258	350	Pt II	34647- 93197 K	1723.3891	58025.20	190	Ne II	C
1708.10	58544.6	180	Pt II	16820- 75365 K	1723.9935	58004.859	3400	Pt I	775- 58780 N
1708.2132	58540.702	3100	Pt I	10116- 68657 N	1724.5730	57985.367	4300	Pt II	13329- 71314 05
1708.6568	58525.504	1300	Pt II	37877- 96403 K	1724.83	57976.7	63		
1708.7393	58522.678	950	Pt I	823- 59346 N	1724.9840	57971.552		Al II	
1709.12	58509.6	41	Pt II	32237- 90746 K	1725.15	57966.0	69	Pt II	21717- 79683 K
1709.6984	58489.848	470	Pt I	10116- 68606 N	1725.26	57962.3	150		
1709.93	58481.9	100	Pt I	0- 58482 N	1725.58	57951.5	110		
1710.1391	58474.776	270	Pt I	10131- 68606 N	1725.69	57947.8	170	Pt I	6567- 64515 N
1710.7964	58452.309	350			1726.3697	57925.022	2500	Pt II	16820- 74745 05
1710.8580	58450.203	2400	Pt II	15791- 74241 05	1726.5970	57917.395	420		
1710.9566	58446.836	250			1726.9376	57905.972	380		
1711.1926	58438.776	320	Pt II	21168- 79607 08	1727.4189	57889.838	1200	Pt II	34647- 92537 K
1711.2670	58436.235	350	Pt II	23461- 81897 P	1727.6799	57881.092	20000	Pt II	43737-101618 K
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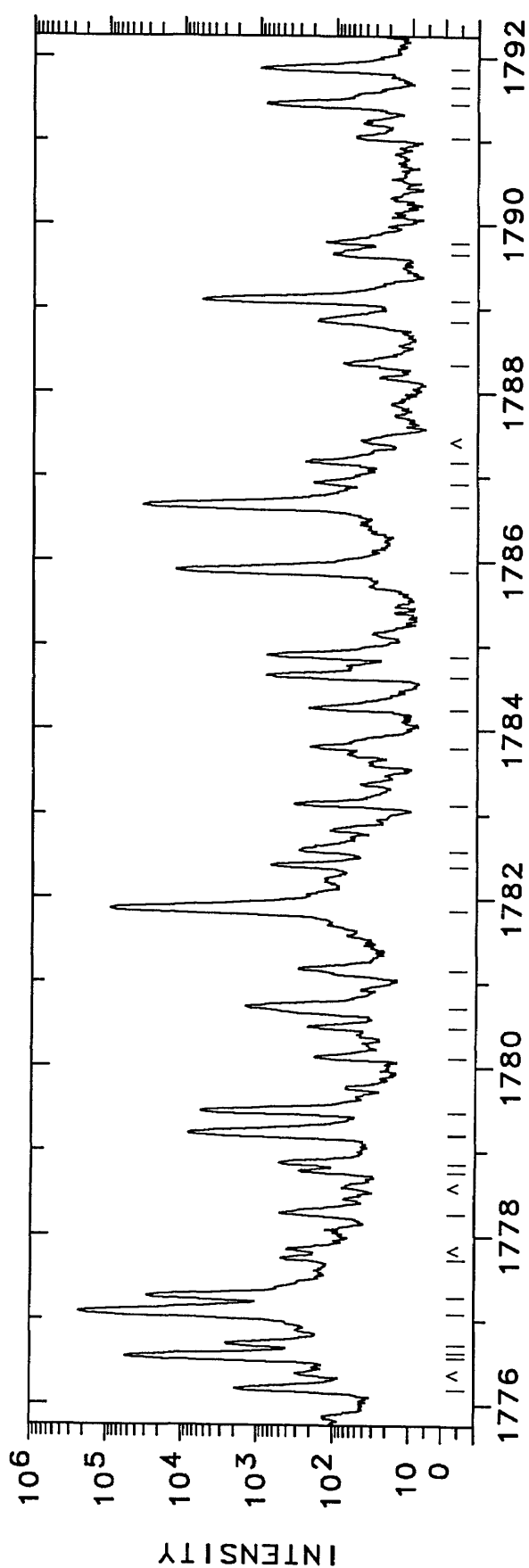
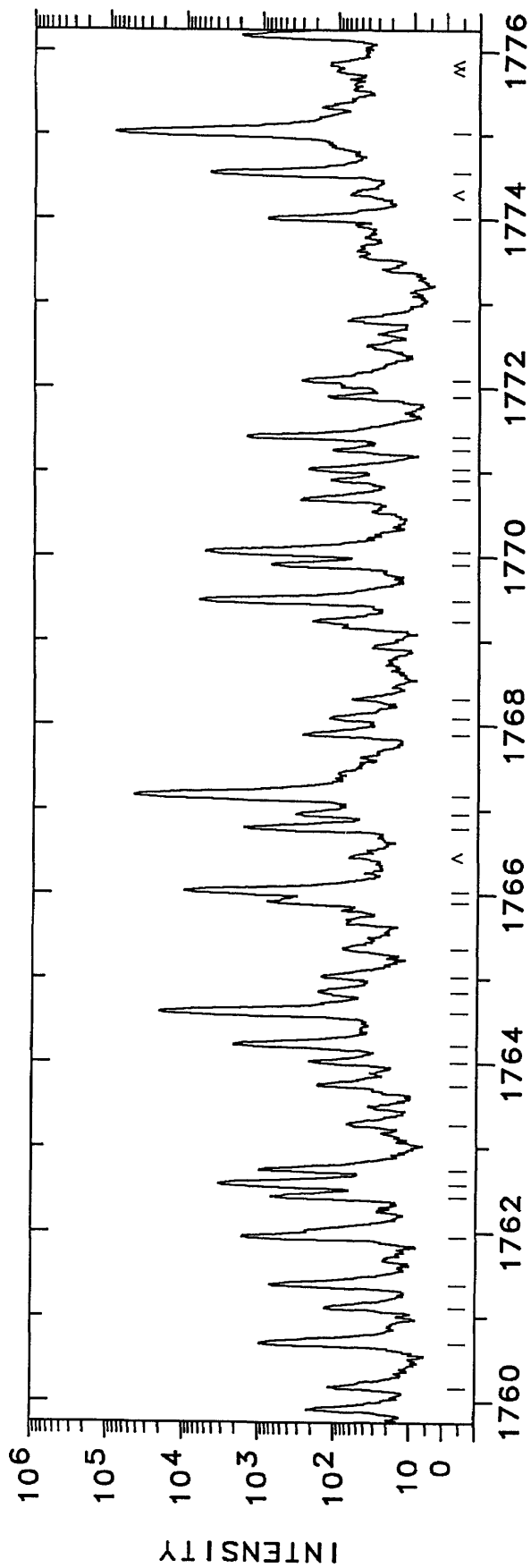


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1728.13	57866.0	52			1744.4305	57325.299	15000	Pt I	775- 58101 N
1728.30	57860.3	56			1745.6949	57283.779	490	Pt II	21168- 78452 K
1728.83	57842.6	44			1745.8874	57277.463	3000	Pt I	823- 58101 N
1729.26	57828.2	63	Pt II	32918- 90746 K	1746.4563	57258.805	5600	Pt I	6567- 63826 N
1729.7243	57812.682	270	Pt II	24879- 82692 K	1746.77	57248.5	190	Pt II	15791- 73026 06
1730.4798	57787.441	500	Pt II	36484- 94271 K	1747.1795	57235.104	4600	Pt II	
1730.6473	57781.85	620	Ne II		1747.64	57220.0	59		
1730.8544	57774.935	2000	Pt II	41434- 99209 K	1747.9003	57211.500	80	Pt I	775- 57987 D
1731.1250	57765.904	1200	Pt II	42031- 99797 K	1748.9496	57177.177	3700	Pt II	42031- 99209 K
1731.4175	57756.145	1100			1749.26	57167.0	270		
1731.57	57751.1	85			1750.70	57120.0	52		
1731.91	57739.7	42			1751.2164	57103.17	380	Ne II	
1732.44	57722.1	58			1751.7022	57087.331	4500	Pt II	18097- 75184 A
1732.93	57705.7	83	Pt I	775- 58482 N	1751.7022	57087.331	4500	Ne II	
1733.19	57697.1	150			1752.10	57074.4	130		
1733.5407	57685.407	150			1752.8546	57049.796	2500	Pt II	13329- 70379 08
1733.7099	57679.777	350			1753.2526	57036.847	9200	Pt II	42031- 99068 K
1733.93	57672.5	170	Pt II	37877- 95557 K	1753.54	57027.5	300		
1735.24	57628.9	190			1753.8286	57018.115	48000	Pt II	0- 57018 A
1735.8642	57608.192	36000	Pt II	8419- 66028 06	1753.8286	57018.115	48000	Pt II	24879- 81897 AK
1735.9774	57604.437	4100	Pt II	43737- 101341 K	1754.47	56997.3	110		
1736.39	57590.7	180	Pt II	46046- 103637 K	1754.9114	56982.935	480	Pt II	23875- 80858 12
1737.1732	57564.784	21000	Pt I	823- 58388 N	1755.19	56973.9	110		
1737.3402	57559.25	290	Ne II		1755.8673	56951.912	390	Pt II	37877- 94829 K
1737.5956	57550.790	3600	Pt I	775- 58326 N	1756.0182	56947.018	370	Pt II	54373- 111320 K
1738.7356	57513.06	1600	Ne II		1756.2086	56940.845	1700	Pt II	16820- 73761 07
1738.9433	57506.187	1700	Pt I	0- 57506 D	1756.3952	56934.795	4000	Pt II	53749- 110684 K
1739.76	57479.2	130			1756.5046	56931.247	2600	Pt II	8419- 65351 07
1739.9574	57472.672	320	Pt II	50564- 108037 K	1756.6264	56927.301	1100	Pt I	6140- 63067 N
1740.3637	57459.254	720	Pt II	29030- 86489 K	1756.8363	56920.50	1200	Ne II	
1740.9739	57439.115	480	Pt II	42031- 99471 K	1757.5047	56898.852	1200	Pt I	6567- 63466 N
1741.46	57423.1	180			1757.79	56889.6	140		
1742.2518	57396.985	140	Pt II	23461- 80858 11	1758.1220	56878.874	8400	Pt II	4786- 61665 07
1742.34	57394.1	89			1758.5549	56864.87	2000	Ne II	
1742.66	57383.5	110	Pt II	41434- 98817 K	1758.77	56857.9	76	Pt II	32237- 89095 K
1742.8712	57376.59	910	Ne II		1758.9451	56852.259	1100	Pt II	36484- 93336 12
1743.40	57359.2	170			1759.42	56836.9	160		
1744.17	57333.9	150			1759.90	56821.4	150	Pt II	50564- 107386 K
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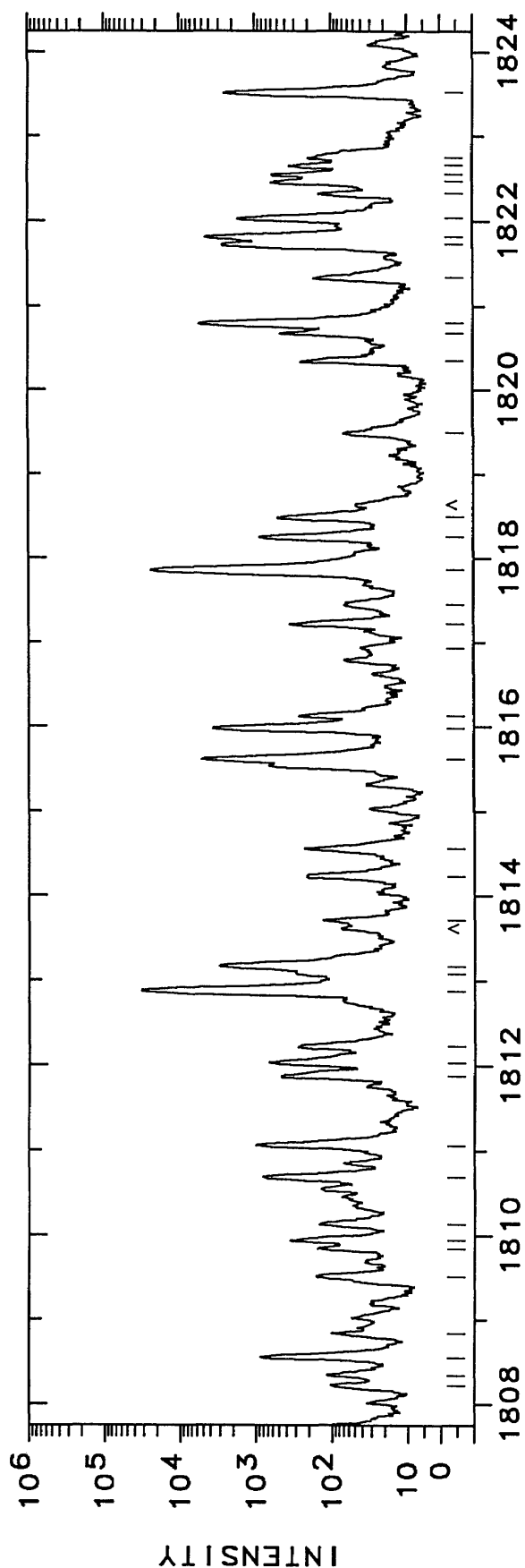
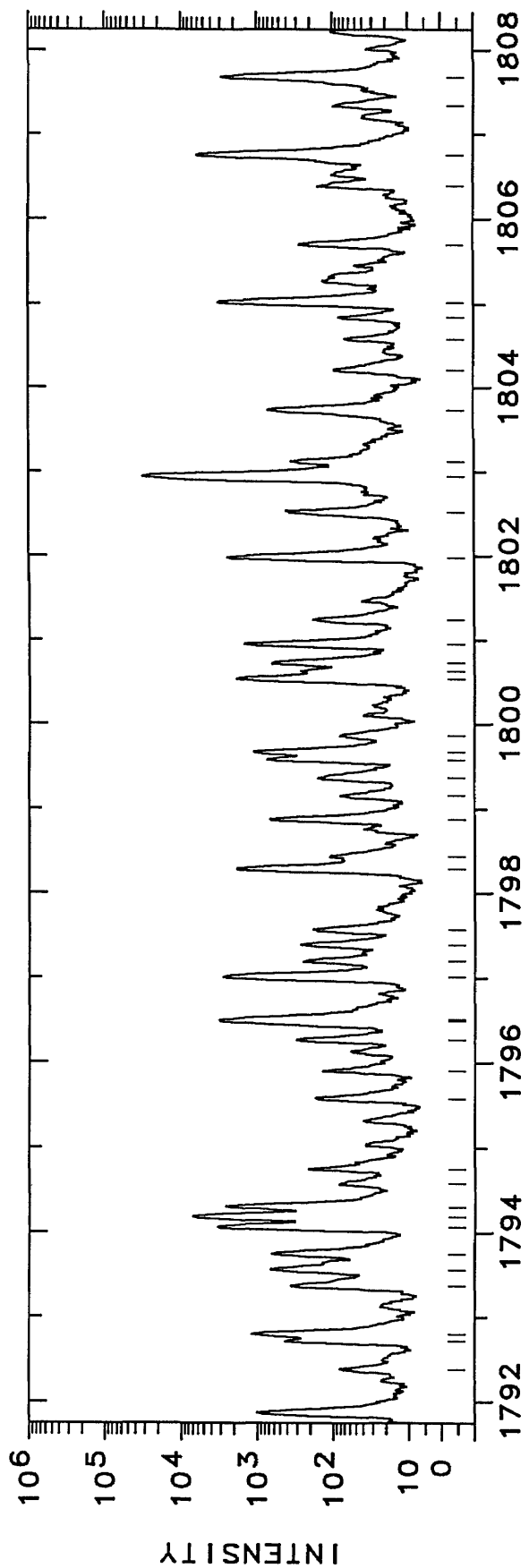
WAVELENGTH (ANGSTROMS) - VACUUM

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1760.6896	56795.928	960 D	Pt I	10131- 66927 AN	1776.1777	56300.673	1900	Pt I	10131- 66432 N
1760.6896	56795.928	960 D	Pt II	29030- 85826 AK	1776.5571	56288.650	55000	Pt I	0- 56288 N
1761.11	56782.4	120			1776.6141	56286.844	360 U		
1761.38	56773.7	710			1776.7088	56283.844	2500	Pt II	36484- 92767 K
1761.9446	56755.474	1700	Pt II	37877- 94633 K	1777.0866	56271.879	230000	Pt II	4786- 61058 07
1762.4146	56740.338	680			1777.2783	56265.808	28000	Pt I	775- 57041 N
1762.5591	56735.686	3400 D	Pt II	23461- 80197 AK	1777.72	56251.8	480		
1762.5591	56735.686	3400 D	Pt II	21717- 78452 AK	1778.2476	56235.139	490		
1762.7266	56730.295	1000	Pt I	775- 57506 D	1778.7495	56219.27	270	Ne II	C
1763.27	56712.8	61			1778.85	56216.1	510		
1763.7269	56698.12	160	Ne II	C	1779.1858	56205.486	5500	Pt II	16820- 73026 06
1764.01	56689.0	210			1779.2172	56204.493	5500	Pt II	24879- 81083 K
1764.2127	56682.509	2200	Pt I	823- 57506 D	1779.4723	56196.435	5700	Pt II	41434- 97630 K
1764.5948	56670.234	21000	Pt I	0- 56670 N	1780.11	56176.3	170		
1764.84	56662.4	160			1780.47	56164.9	210		
1765.0132	56656.80	150	Ne II	C	1780.7016	56157.640	1500	Pt II	15791- 71948 05
1765.35	56646.0	72			1781.15	56143.5	290		
1765.8981	56628.41	810	Ne II	C	1781.8617	56121.077	93000	Pt II	4786- 60907 07
1766.0328	56624.090	10000	Pt II	13329- 69953 04	1782.3858	56104.576	690		
1766.7883	56599.877	1700	Pt I	6567- 63167 N	1782.57	56098.8	280		
1766.95	56594.7	330	Pt II	21168- 77763 K	1783.1027	56082.019	340	Pt I	10116- 66198 N
1767.1612	56587.934	47000	Pt II	0- 56587 07	1783.7849	56060.57	200	Ne II	C
1767.89	56564.6	280	Pt II	29261- 85826 K	1784.24	56046.3	210	Pt II	21717- 77763 K
1768.0852	56558.36	120	Ne II	C	1784.6257	56034.159	810	Pt II	48591- 104625 K
1768.31	56551.2	55			1784.8755	56026.317	790		
1769.2416	56521.393	200	Pt II	18097- 74619 05	1785.8803	55994.795	13000	Pt II	9356- 65351 05
1769.4841	56513.647	6600	Pt II	29261- 85775 K	1786.6480	55970.734	36000	Pt I	823- 56794 N
1769.9101	56500.045	730	Pt I	6567- 63067 N	1786.92	55962.2	180		
1770.0610	56495.228	5600	Pt II	43737- 100232 K	1787.17	55954.4	240		
1770.68	56475.5	300			1788.34	55917.8	70		
1770.90	56468.5	110			1788.85	55901.8	160		
1771.03	56464.3	230			1789.0922	55894.269	5800	Pt I	775- 56670 N
1771.26	56457.0	110			1789.64	55877.2	100		
1771.4140	56452.077	1600			1789.78	55872.8	130		
1771.89	56436.9	130			1791.04	55833.5	45		
1772.0902	56430.536	290	Pt II	50564- 106995 K	1791.44	55821.0	820	Pt II	21717- 77538 K
1772.80	56407.9	65			1791.6462	55814.591	810		
1774.0082	56369.525	830	Pt II	21168- 77538 K	1791.8624	55807.857	980	Pt II	23875- 79683 K
1774.5470	56352.410	4800	Pt II	41434- 97786 K					



WAVELENGTH (ANGSTROMS) - VACUUM

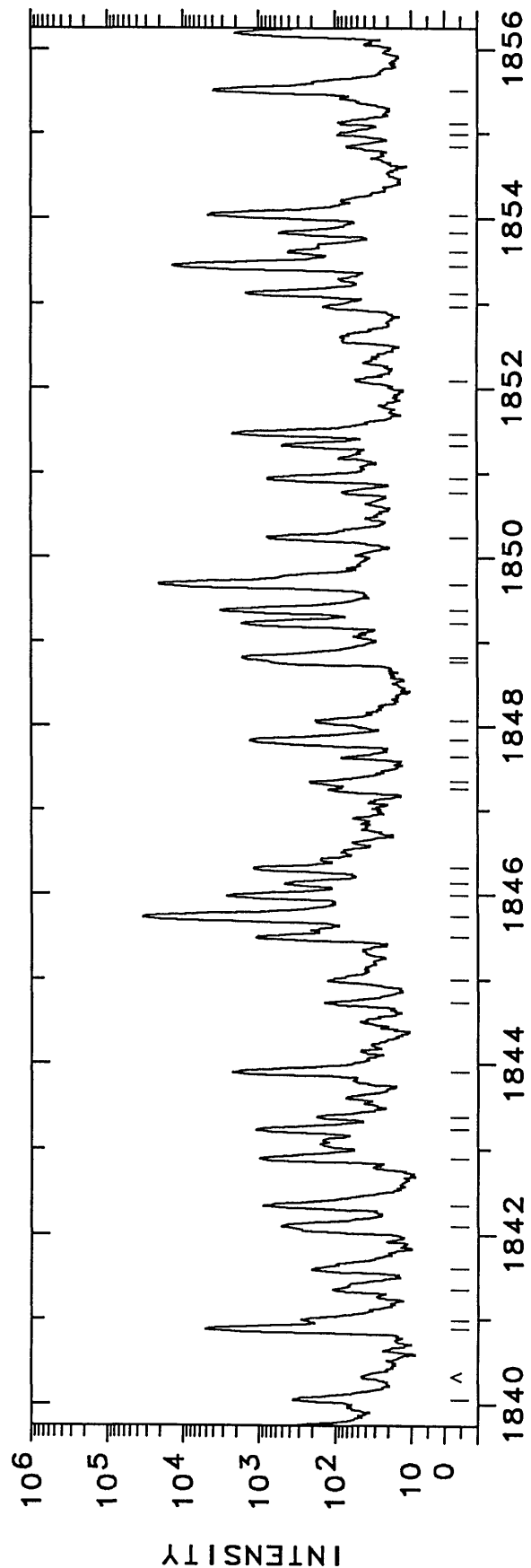
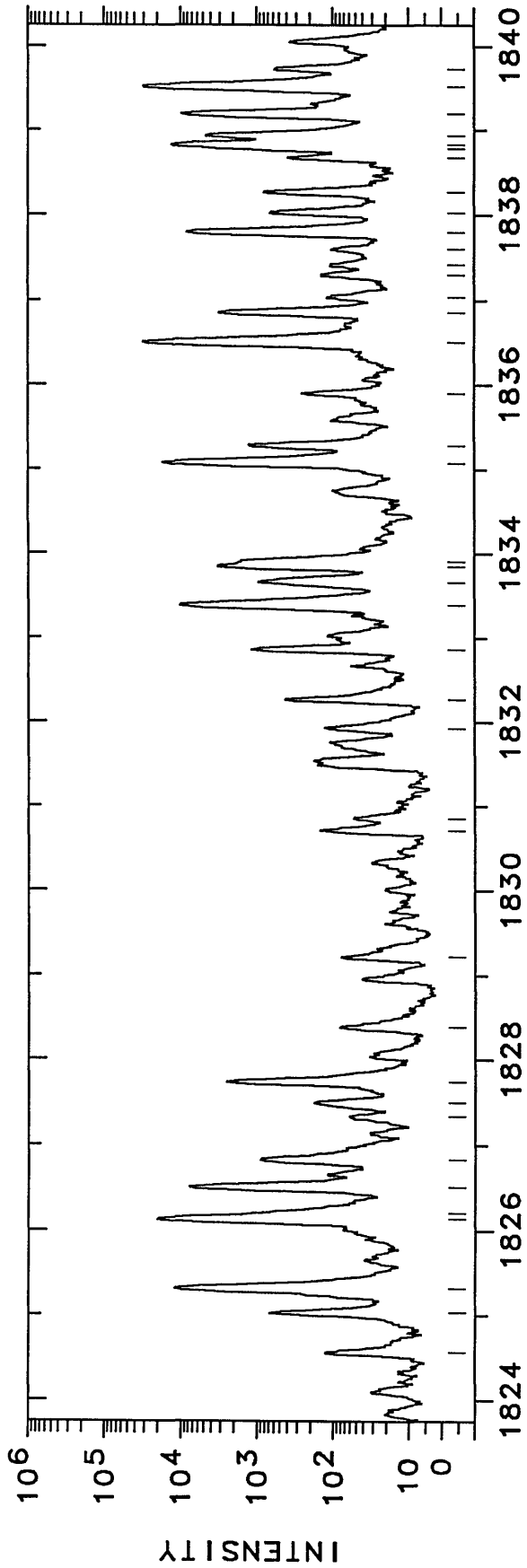
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1792.7132	55781.371	400	Pt II	116689-60907 K	1807.6755	55319.663	2900	Pt II	37877-93197 K
1792.8041	55778.543	1200	Pt II	53749-109528 K	1808.22	55303.0	95		
1793.37	55760.9	350	Pt II	42031-97792 K	1808.34	55299.3	110	Ne III	L
1793.56	55755.0	660	Pt II	42031-97786 K	1808.524	55292.842	870	Pt II	21168-76461 09
1793.75	55749.1	640	Pt II	41434-97183 K	1808.84	55284.0	93	Ne III	L
1794.0655	55739.325	3300	Pt I	10116-65852 N	1809.51	55263.6	150		
1794.1811	55735.734	7100	Pt II	23875-79607 10	1809.84	55253.5	150		
1794.3043	55731.907	2600	Pt II	58062-113785 K	1809.94	55250.5	350		
1794.58	55723.3	76	Pt I	10131-65850 N	1810.13	55244.7	140	Ne III	L
1794.75	55718.1	200	Pt I		1810.69	55227.6	800		
1795.58	55692.3	160			1811.0524	55216.514	990	Pt II	23875-79092 AK
1795.91	55682.1	130			1811.0524	55216.514	990	Pt II	34647-89863 AK
1796.27	55670.9	290	Pt II	32918-88589 K	1811.88	55191.3	460	Pt II	32918-88110 K
1796.4925	55664.024	3200	Pt II	18097-73761 08	1812.04	55186.4	670		
1796.5171	55663.26	900	Ne II		1812.23	55180.6	270	Ne III	L
1797.0175	55647.761	2800	Ne II		1812.8819	55160.791	33000	Pt I	823-55984 K
1797.1964	55642.22	240	Ne II		1813.0791	55154.792	300	Pt II	54373-109528 K
1797.39	55636.2	260			1813.1658	55152.154	3000	Pt II	29030-84182 13
1797.57	55630.7	180	Pt II	23461-79092 AK	1813.71	55135.6	120		
1797.57	55630.7	180	Pt II	116689-61058 AK	1814.23	55119.8	210		
1798.2814	55608.65	1900	Ne II		1814.56	55109.8	220		
1798.44	55603.7	100			1815.6120	55077.847	5100	Pt I	6567-61645 N
1798.8757	55590.278	670			1815.9818	55066.631	3600	Pt II	46046-101113 K
1799.16	55581.5	71			1816.13	55062.1	260		
1799.37	55575.0	150			1816.9290	55037.925		Si II	B
1799.58	55568.5	730	Pt II	27255-82824 K	1817.22	55029.1	340		
1799.6692	55565.767	1100	Pt I	10131-65697 N	1817.45	55022.1	59		
1799.87	55559.6	72			1817.8736	55009.325	24000	Pt I	0-55009 N
1800.5413	55538.854	1900	Pt I	6567-62106 N	1818.2536	54997.829	870		
1800.6249	55536.276	200	Pt I	0-55536 D	1818.49	54990.7	500	Pt II	23461-78452 K
1800.7325	55532.96	620	Ne II		1819.4814	54960.715	59	Pt II	34647-89607 15
1800.9569	55526.037	1500	Pt II	34647-90173 K	1820.35	54934.5	240	Pt II	54373-109307 K
1801.24	55517.3	170			1820.68	54924.5	460		
1801.9716	55494.770	2400	Pt I	6567-62062 N	1820.8082	54920.666	5500	Pt II	29261-84182 13
1802.52	55477.9	400			1821.34	54904.6	160		
1802.9398	55464.969	31000	Pt I	823-56288 N	1821.7330	54892.786	2700	Pt II	21717-76610 05
1803.1160	55459.55	350	Ne II		1821.8212	54890.129	4400	Pt II	37877-92767 K
1803.7301	55440.67	690	Ne II		1822.0375	54883.612	1700		
1804.21	55425.9	85			1822.33	54874.8	130		
1804.58	55414.6	59			1822.47	54870.6	590	Ne III	L
1804.84	55406.6	74			1822.55	54868.2	570	Ne III	L
1805.0193	55401.069	3200	Pt II	9356-64757 05	1822.66	54864.9	340	Ne III	L
1805.70	55380.2	260	Pt II	54373-109753 K	1822.75	54862.2	190	Ne III	L
1806.39	55359.0	150			1823.5129	54839.206	2600	Pt I	0-54839 D
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WAVELENGTH (ANGSTROMS) - VACUUM

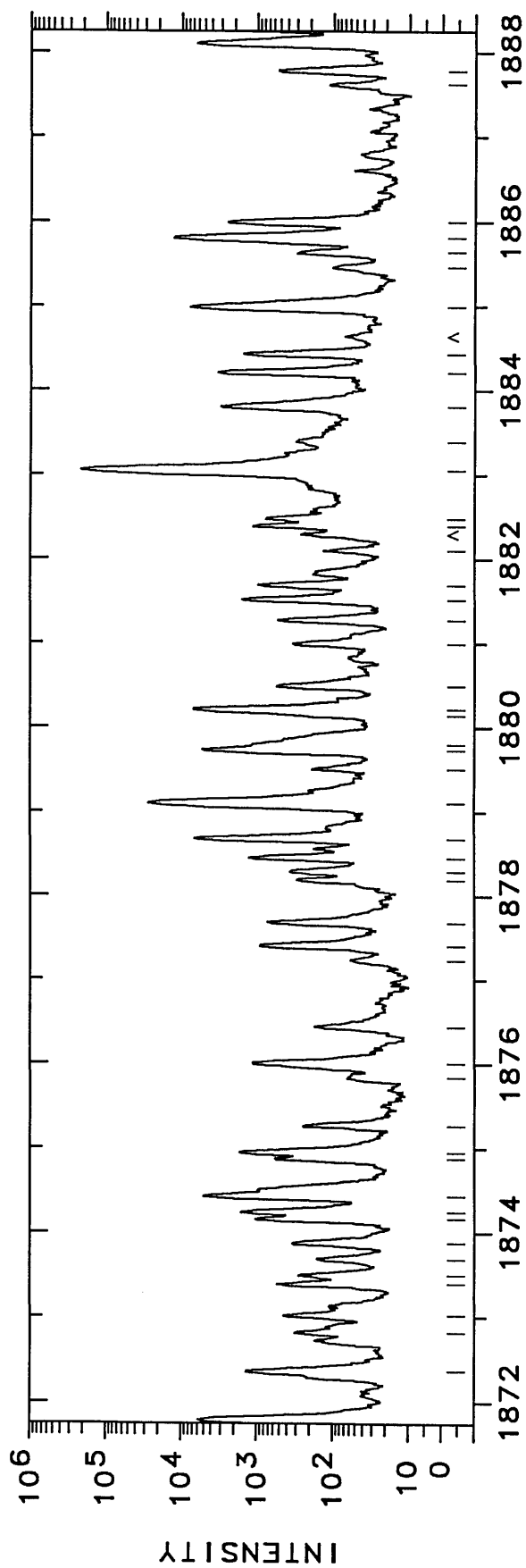
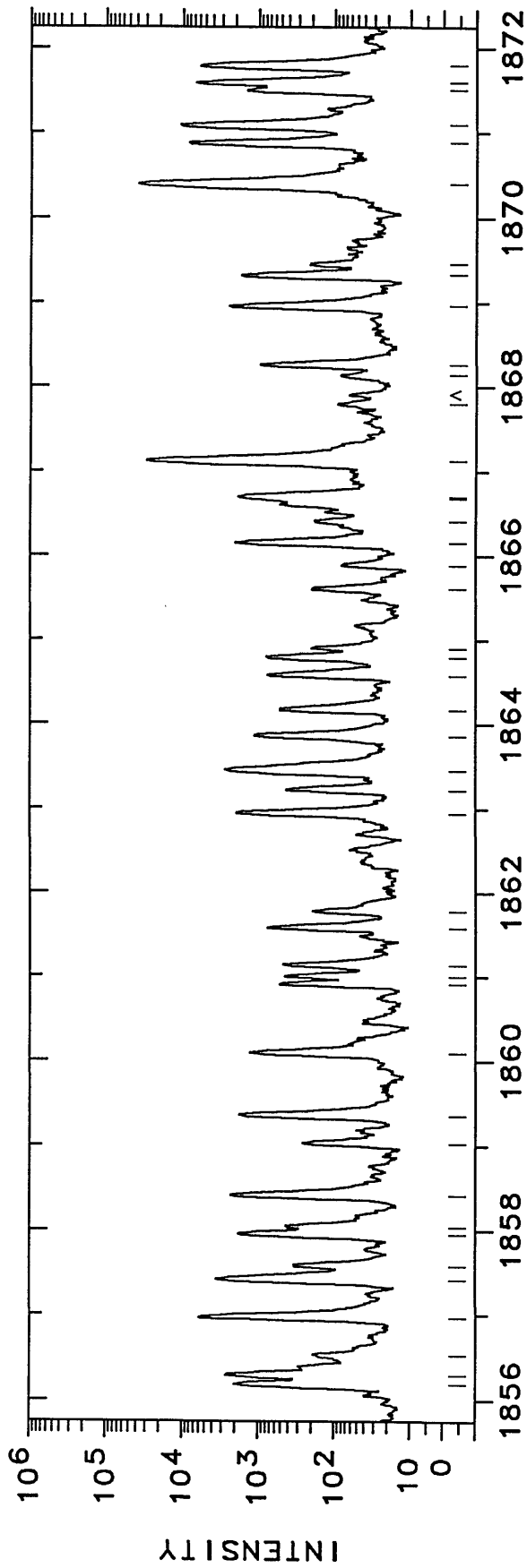


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1825.0397	54793.329	680	Pt I	6567- 61352 N	1841.60	54300.6	190	Ne III	L
1825.3262	54784.728	12000	Pt I	775- 55536 D	1842.10	54285.9	500	Pt II	32918- 87204 AK
1826.1377	54760.384	20000	Pt I	46046-100795 K	1842.10	54285.9	500	Ne III	AL
1826.2024	54758.443	700	Pt II	Ne II	1842.3413	54278.76	880	Ne II	C
1826.5063	54749.332	7800	Ne II	C	1842.8889	54262.631	970	Pt II	36484- 90746 K
1826.8324	54739.56	910	Pt II	823- 55536 D	1843.2224	54252.813	1100	Pt II	32237- 86489 K
1827.34	54724.4	52	Pt I	119057- 64388 K	1843.38	54248.2	160	Ne II	C
1827.50	54719.6	170	Pt I	23875- 78452 K	1843.9105	54232.57	2300	Ne II	C
1827.7326	54712.599	2500	Pt I	10116- 64675 N	1844.73	54208.5	130	Pt I	823- 55009 N
1828.39	54692.9	74	Pt II	16820- 71364 K	1845.00	54200.5	120	Pt I	0- 54178 N
1829.22	54668.1	140	Pt II	6567- 61097 N	1845.5046	54185.722	1100	Pt I	15791- 69953 04
1830.71	54623.6	40	Pt I	16820- 71364 K	1845.7517	54178.468	34000	Pt I	10116- 64248 N
1830.85	54619.4	45	Pt I	23875- 78452 K	1845.9968	54171.28	2600	Ne II	41434- 95557 K
1831.93	54587.2	120	Pt I	6567- 61097 N	1846.14	54167.1	450	Pt I	10131- 64248 N
1832.27	54577.1	420	Pt II	16820- 71364 K	1846.64	54162.041	1200	Pt II	29261- 83352 14
1832.8733	54559.145	1200	Pt I	10116- 64675 N	1847.34	54131.9	200	Ne II	23461- 77538 K
1833.3875	54543.843	10000	Pt II	775- 55216 D	1847.64	54123.1	74	Pt II	775- 54839 D
1833.66	54535.7	940	Pt I	21168- 75581 08	1847.8453	54117.084	1300	Pt I	24879- 78906 10
1833.8527	54530.007	3200	Pt I	53749-108155 K	1848.07	54110.5	170	Ne III	823- 54839 D
1833.9099	54528.31	1100	Ne II	10116- 64515 N	1848.77	54031.6	70	Pt II	0- 54011 D
1835.0745	54493.700	17000	Pt II	10131- 64619 N	1850.2332	54027.012	750	Pt II	53953.373
1835.2748	54487.753	1300	Pt I	48591-103060 K	1850.77	54015.528	480	Pt I	14000
1835.90	54469.2	240	Pt II	13329- 67780 K	1851.3195	54011.150	2200	Pt I	0- 53953 A
1836.5075	54451.180	30000	Pt II	775- 55216 D	1851.4696	54007.784	1700	Ne III	114861- 60907 K
1836.8531	54440.936	3100	Pt I	29030- 83352 14	1852.09	53993.1	45	Pt II	54373-108322 K
1837.04	54435.4	110	Pt I	10131- 64515 N	1852.96	53967.7	130	Ne III	34647- 88589 K
1837.30	54427.7	130	Pt I	10131- 64515 N	1853.1147	53963.20	1500	Ne II	60
1837.42	54424.1	98	Pt II	21168- 75581 08	1853.4523	53953.373	14000	Pt I	84
1837.60	54418.8	95	Pt II	53749-108155 K	1853.4523	53953.373	14000	Pt I	53908.6
1837.8050	54412.738	8100	Pt II	10116- 64515 N	1853.61	53948.8	400	Pt II	53904.9
1838.03	54406.1	660	Pt I	10131- 64515 N	1853.83	53942.4	530	Pt II	53893.161
1838.2682	54399.026	780	Pt I	10131- 64515 N	1854.0403	53936.26	4600	Ne II	4000
1838.67	54387.1	380	Pt I	10131- 64515 N	1854.84	53913.0	60	Ne III	81
1838.7836	54383.779	1200	Pt I	9356- 63738 05	1854.99	53908.6	84	Pt II	43737- 97630 K
1838.8246	54382.567	13000	Pt II	23875- 78254 K	1855.12	53904.9	81	Pt II	4000
1838.9355	54379.286	4600	Pt II	42031- 96403 K	1855.5230	53893.161	4000	Pt II	
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1839.73	54355.8	570	Ne III						
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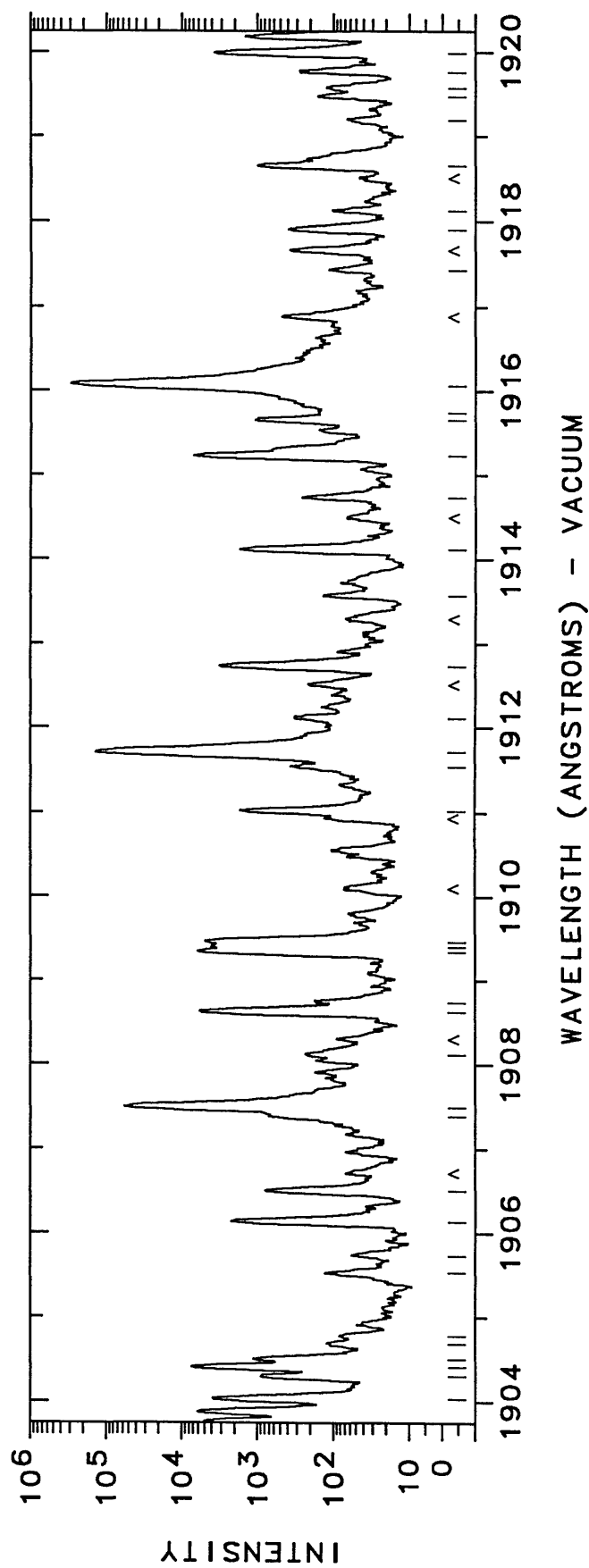
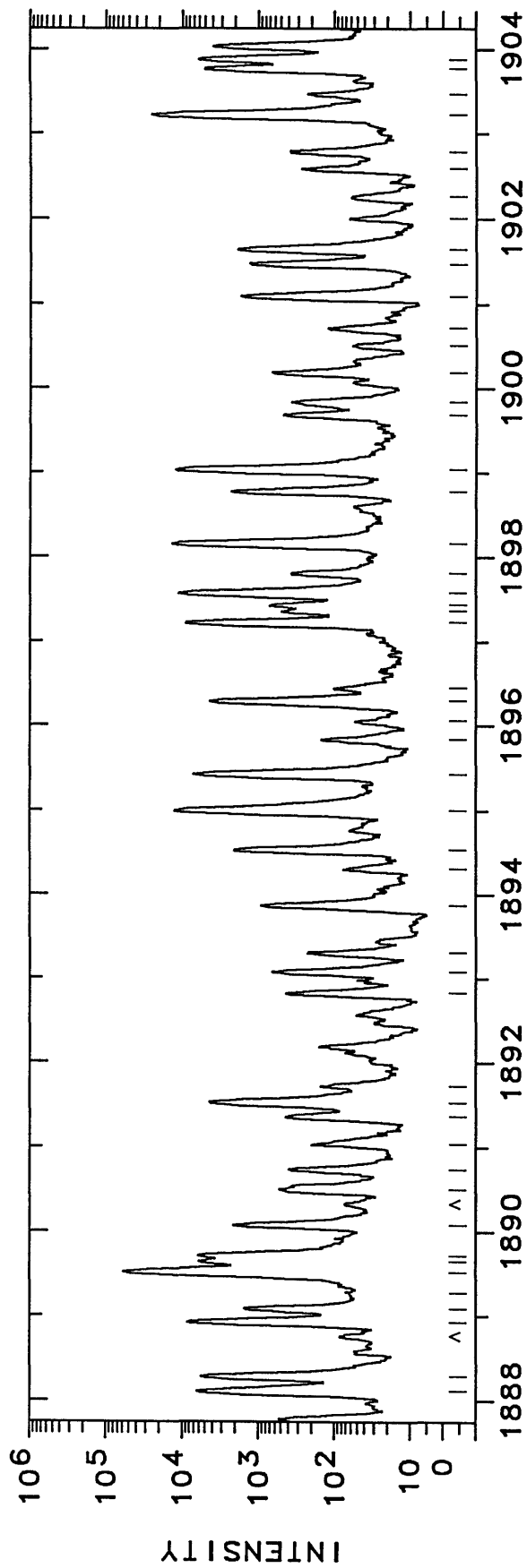
WAVELENGTH (ANGSTROMS) - VACUUM

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1856.2935	53870.791	2700	Pt II	121651- 67780 AK	1873.4903	53376.31	270	Ne II	
1856.5220	53864.162	180	Pt II	21717- 75581 09	1873.6771	53370.99	150	Ne II	
1856.9688	53851.201	6000	Pt II	18097- 71948 06	1873.8744	53365.37	330	Ne II	
1857.4069	53838.499	3500	Pt II	53749-107588 K	1874.1554	53357.368	1000	Pt I	775- 54133 N
1857.5649	53833.92	320	Ne II		1874.2481	53354.729	1600	Pt I	823- 54178 N
1857.9550	53822.68	1800	Ne II		1874.4323	53349.486	5100	Pt I	6567- 59916 N
1858.0389	53820.186	400	Pt II		1874.88	53336.7	560		
1858.4108	53809.42	2300	Ne II	110408- 56587 C	1874.9624	53334.403	1700	Pt I	10131- 63466 N
1859.03	53791.5	250			1875.27	53325.7	230		
1859.3605	53781.93	1800	Ne II		1875.84	53309.5	53	Pt I	823- 54133 N
1860.0984	53760.597	1300	Pt I	6567- 60328 N	1876.0029	53304.82	1100	Ne II	
1860.91	53737.2	510			1876.44	53292.4	160	Pt II	58062-111354 K
1861.00	53734.6	440			1877.23	53270.0	47		
1861.1355	53730.64	460	Ne II		1877.4028	53265.075	900	Pt II	114455- 61190 K
1861.5815	53717.766	740			1877.6777	53257.28	710	Ne II	
1861.78	53712.0	180			1878.19	53242.7	280		
1862.9448	53678.456	1900	Pt II	105086- 51408 K	1878.29	53239.9	350	Pt II	110258- 57018 K
1863.22	53670.5	420	Pt II	110258- 56587 K	1878.4543	53235.258	1300	Pt I	775- 54011 D
1863.4578	53663.678	2700 W	Pt II	54373-108037 K	1878.6919	53228.526	6700	Pt II	104636- 51408 K
1863.8611	53652.067	1100	Pt I	6140- 59792 N	1879.1031	53216.879	27000	Pt II	18097- 71314 06
1864.17	53643.2	510			1879.51	53205.4	170		
1864.5737	53631.562	740	Pt II	114339- 60907 K	1879.7298	53199.135	5200	Pt II	41434- 94633 K
1864.7909	53625.315	770	Pt I	13496- 67121 N	1879.7999	53197.152	930		
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1865.61	53601.8	190	Pt II	117340- 63738 K	1880.2090	53185.577	6800	Ne III	
1865.89	53593.7	69			1880.4950	53177.487	530	Pt I	775- 53953 D
1866.1542	53586.139	2000	Pt II	21168- 74754 10	1880.99	53163.5	320	Pt II	24879- 78043 K
1866.41	53578.8	170			1881.2704	53155.570	510	Pt I	15501- 68657 N
1866.6789	53571.078	500 U	Pt II	32918- 86489 K	1881.5191	53148.543	1600	Pt II	23461- 76610 05
1866.7078	53570.248	1800	Pt II	110158- 56587 K	1881.6889	53143.75	940	Ne II	
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1867.80	53538.9	82			1882.3916	53123.908	1100	Pt II	36484- 89607 16
1868.14	53529.2	73			1882.4792	53121.44	750	Ne II	
1868.2555	53525.870	940	Pt II	42031- 95557 K	1883.0587	53105.088	220000	Pt II	13329- 66434 06
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1870.4100	53464.215	38000	Pt II	9356- 62820 05	1884.4354	53066.292	1500	Pt II	114256- 61190 K
1870.8926	53450.423	8300	Pt II	21168- 74619 06	1884.9927	53050.603	7700	Pt I	10116- 63167 N
1871.1038	53444.389	11000	Pt II	15791- 69235 08	1885.4562	53037.563	91	Pt II	21717- 74754 11
1871.5054	53432.921	1400	Pt II	110020- 56587 K	1885.64	53032.4	290		
1871.5965	53430.320	6700	Pt II	29261- 82692 K	1885.8171	53027.412	13000	Pt II	48591-101618 K
1871.7979	53424.571	5900	Pt II	46046- 99471 K	1885.9970	53022.354	2500	Pt II	46046- 99068 K
1872.3638	53408.424	1400	Pt II	41434- 94842 K	1887.62	52976.8	100		
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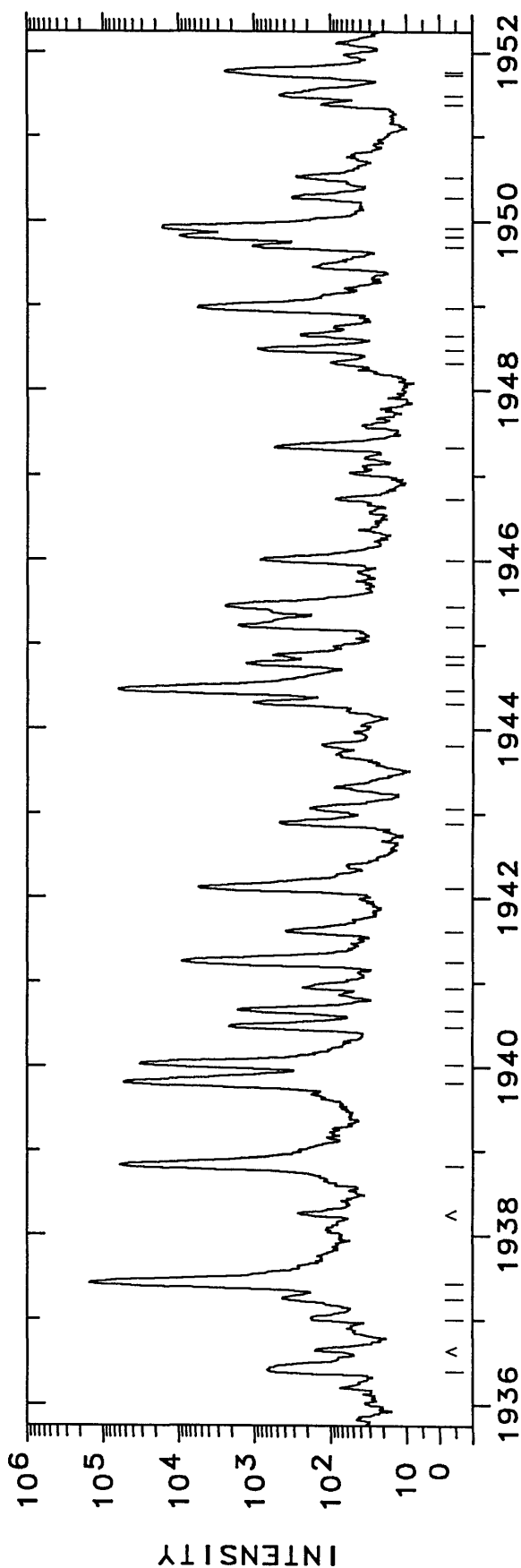
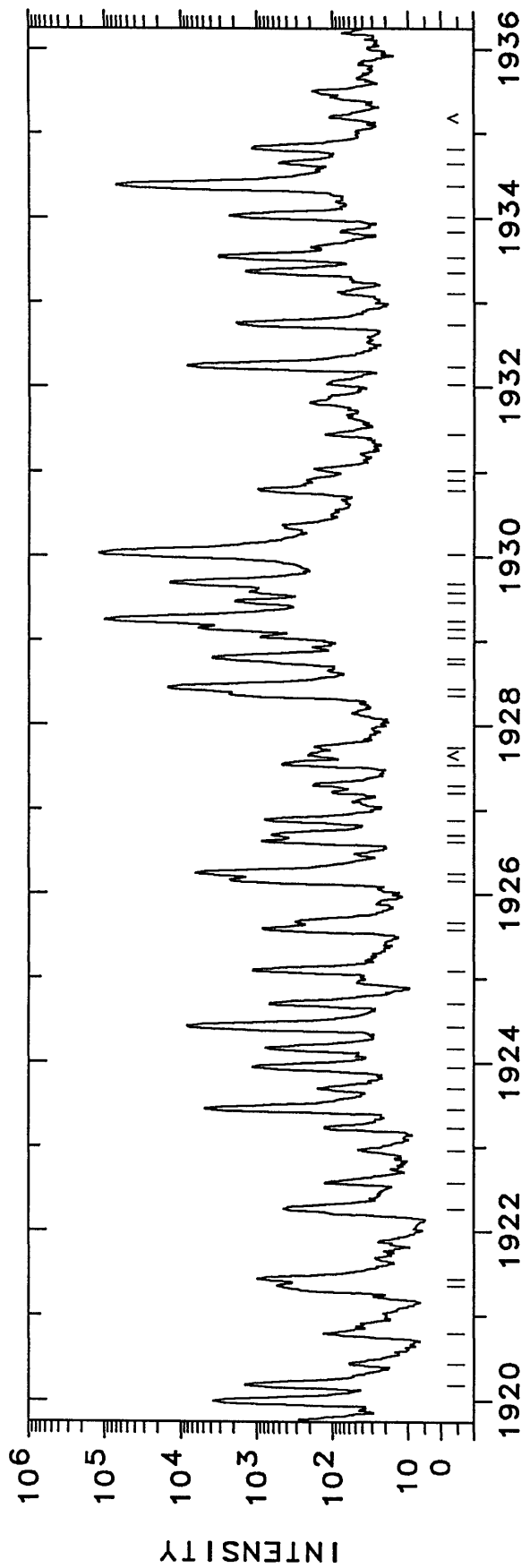


WAVELENGTH (ANGSTROMS) - VACUUM

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
1888.1064	52963.12	6400	Ne II	C	1902.59	52559.9	260	Pt I	6567- 59127 N
1888.2852	52958.102	5700	Pt II	48591-101549 K	1902.79	52554.4	370	Pt I	10116- 62659 N
1888.9330	52939.940	8500	Pt II	109527- 56587 K	1903.2186	52542.572	25000	Pt I	10131- 62659 N
1889.0888	52935.574	1500	Pt I	10131- 63067 N	1903.47	52535.6	210	Pt I	21717- 74241 07
1889.28	52930.2	59			1903.7676	52527.420	5000	Pt I	0- 52520 N
1889.5226	52923.421	58000	Pt II	18097- 71021 K	1903.8836	52524.219	6100	Pt II	109527- 57018 K
1889.6418	52920.083	6000	Pt II	109507- 56587 K	1904.0316	52520.137	3900	Pt I	Ne II
1889.7120	52918.12	6100	Ne II	C	1904.2996	52512.745	890	Pt II	Ne II
1890.0718	52908.043	2100	Pt II	32918- 85826 K	1904.4085	52509.743	7500	Ne II	C
1890.50	52896.1	510			1904.5068	52507.03	1100	Ne II	C
1890.74	52889.3	380	Pt I	775- 53665 N	1904.6890	52502.01	110	Ne II	C
1891.04	52881.0	190			1904.78	52499.5	71		
1891.3667	52871.82	420	Ne II	C	1905.53	52478.8	120		
1891.5305	52867.242	4400	Pt II	29030- 81897 P	1905.73	52473.3	46		
1891.73	52861.7	140			1906.1365	52462.140	2200	Pt II	114127- 61665 K
1892.83	52830.9	420	Pt II	21168- 73999 K	1906.4987	52452.17	770	Ne II	C
1893.08	52824.0	650			1907.3879	52427.721	500	Pt II	27255- 79683 K
1893.31	52817.6	210			1907.4940	52424.80	57000	Ne II	C
1893.8750	52801.79	900	Ne II	C	1908.12	52407.6	220		
1894.31	52789.7	65	Pt II	114455- 61665 K	1908.6190	52393.904	5700	Pt II	43737- 96131 K
1894.5483	52783.030	2000			1908.74	52390.6	160		
1895.0088	52770.204	12000	Pt II	8419- 61190 08	1909.3386	52374.157	6200		
1895.4329	52758.396	7100	Pt II	109346- 56587 K	1909.4039	52372.366	4100	Pt II	43737- 96109 K
1895.84	52747.1	140			1909.4638	52370.723	4900		
1896.06	52740.9	42			1911.0142	52328.235	1700	Pt II	109346- 57018 K
1896.2921	52734.493	4300	Pt II	23875- 76610 07	1911.54	52313.8	350		
1896.45	52730.1	91			1911.7092	52309.211	140000	Pt II	9356- 61665 04
1897.2321	52708.365	9000	Pt I	0- 52708 D	1912.11	52298.2	310		
1897.37	52704.5	480			1912.7295	52281.308	3100	Pt II	18097- 70379 10
1897.4417	52702.542	700	Pt I	13496- 66198 N	1913.57	52258.3	130		
1897.5769	52698.787	11000	Pt II	13329- 66028 04	1914.1170	52243.411	1700	Pt I	775- 53019 D
1897.8051	52692.45	360	Ne II	C	1914.7283	52226.73	250	Ne II	C
1898.1722	52682.259	14000	Pt II	104090- 51408 K	1915.2183	52213.369	6900	Pt I	6567- 58780 N
1898.7831	52665.310	2300			1915.6543	52201.485	1100	Pt I	13496- 65697 N
1899.0445	52658.060	12000	Pt II	109676- 57018 K	1915.74	52199.2	150		
1899.6717	52640.675	460	Pt I	6140- 58780 N	1916.0818	52189.84	300000	Ne II	C
1899.84	52636.0	360	Pt II	29261- 81897 K	1917.43	52153.1	100		
1900.1898	52626.32	650	Ne II	C	1917.90	52140.4	380	Pt II	58062-110202 K
1900.51	52617.5	47			1917.90	52134.4	92	Pt II	58062-110196 K
1900.72	52611.6	110			1918.12	52119.919	980	Pt II	23461- 75581 09
1901.0882	52601.452	1700	Pt II	42031- 94633 K	1918.6523	52105.3	55	Pt II	36484- 88589 K
1901.4729	52590.810	1300	Pt II	114256- 61665 K	1919.19	52097.7	150		
1901.6478	52585.973	1900	Pt II	23875- 76461 11	1919.57	52095.0	110		
1902.01	52576.0	53	Pt II	58062-110638 K	1919.76	52089.8	270		
1902.26	52569.0	50			1919.9914	52083.566	3700	Pt II	18097- 70181 08



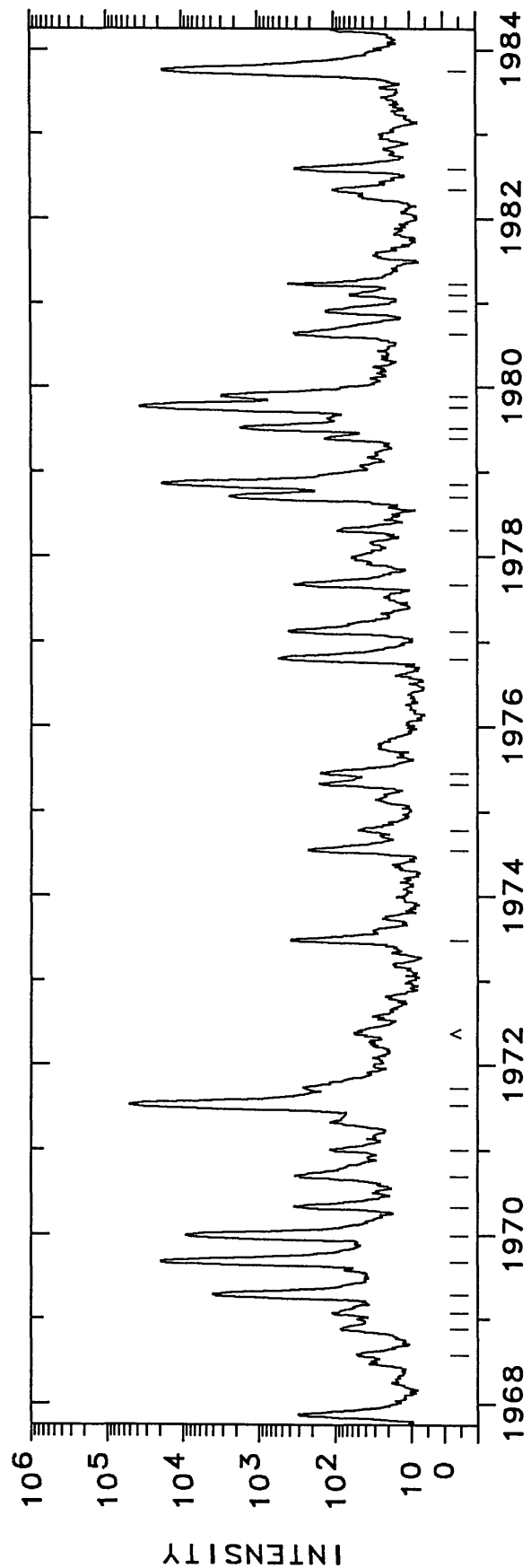
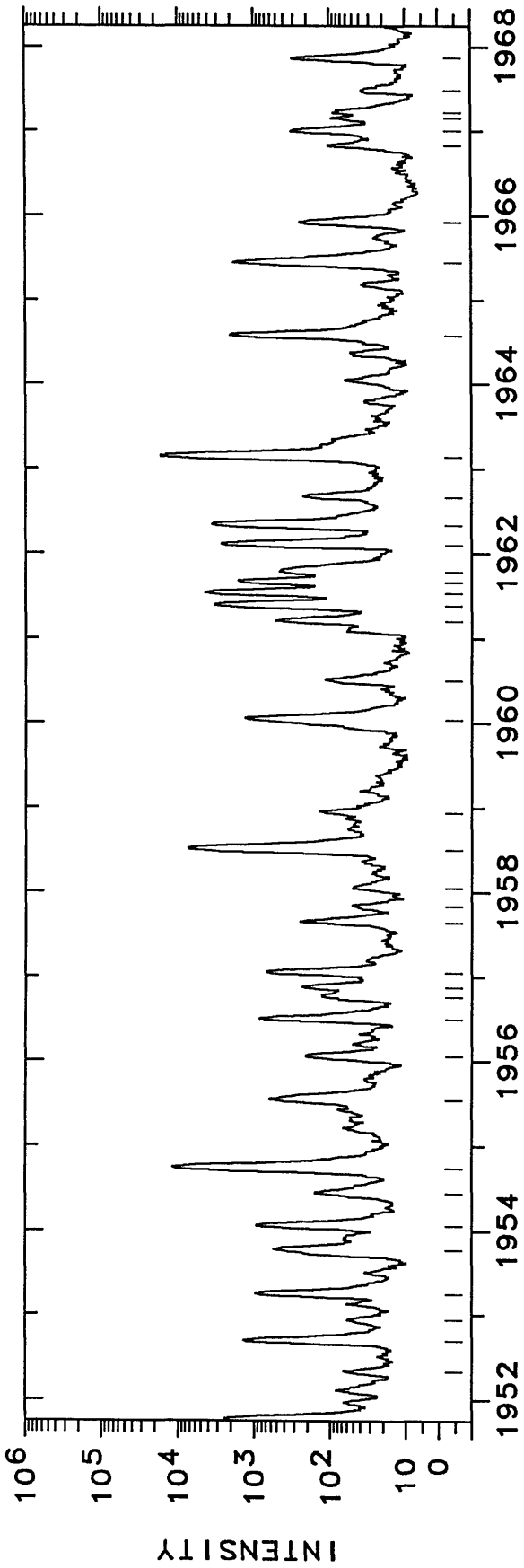
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1920.1812	52078.42	1400	Ne II	C	1933.3618	51723.377	1400	Pt II	23461- 75184	05
1920.43	52071.7	50			1933.5298	51718.88	3200	Ne II		C
1920.79	52061.9	120			1933.84	51710.6	67			
1921.35	52046.7	530			1934.0164	51705.869	2300	Pt II	23875- 75581	10
1921.43	52044.6	970			1934.3690	51696.445	70000	Pt I	823- 52520	N
1922.2695	52021.841	430	Pt II	05	1934.64	51689.2	490	Pt II	36484- 88173	K
1922.57	52013.7	120	Pt I	N	1934.8150	51684.528	1100			
1922.96	52003.2	35			1936.3772	51642.831	670	Pt II	116689- 65046	K
1923.23	51995.9	120			1937.00	51626.2	170	Pt II	36484- 88110	K
1923.4591	51989.668	4700	Pt I	N	1937.24	51619.8	410	Pt I	15501- 67121	N
1923.70	51983.2	140			1937.4245	51614.915	150000	Pt I	823- 52438	N
1923.9493	51976.422	1100	Pt II	K	1938.8269	51577.58	60000	Ne II		C
1924.1654	51970.58	740	Ne II	C	1939.8110	51551.414	53000 L			
1924.4245	51963.587	8200			1940.0319	51545.544	32000	Pt I	9356- 60907	05
1924.70	51956.1	670	Pt II	K	1940.4766	51533.732	2100	Pt I	0- 51545	D
1925.0910	51945.596	1100	Pt I	N	1940.6664	51528.691	1600	Pt I	6567- 58101	N
1925.5775	51932.473	820	Pt I	D	1940.93	51521.7	220	Pt II	10116- 61645	N
1925.66	51930.2	300	Pt I	N	1941.2409	51513.442	8900 L			
1926.1535	51916.942	2300			1941.60	51503.9	380			
1926.2370	51914.692	6400	Pt I	N	1942.1105	51490.376	5500	Pt II	23875- 75365	K
1926.6198	51904.377	840	Pt II	K	1942.8811	51469.954	460	Pt II	121651- 70181	K
1926.70	51902.2	620	Pt II	K	1943.06	51465.2	180			
1926.88	51897.4	770			1943.81	51445.4	120			
1927.20	51888.8	91			1944.3026	51432.323	1000			
1927.29	51886.3	170			1944.4617	51428.116	63000	Pt II	13329- 64757	05
1927.53	51879.9	450	Pt II	K	1944.7712	51419.931	1300	Pt I	6567- 57987	D
1927.74	51874.2	160			1944.8719	51417.27	560	Ne II		C
1928.3541	51857.696	1100	Pt II	07	1945.2210	51408.041	1600	Pt I	13496- 64904	N
1928.4320	51855.602	15000	Pt II	05	1945.4550	51401.857	2400	Ne II		A
1928.7297	51847.597	740	Pt II	K	1945.4550	51401.857	2400	Ne III		AL
1928.7866	51846.07	3800	Ne II	C	1946.0018	51387.414	840	Ne III		L
1929.04	51839.3	880			1946.72	51368.5	76			
1929.1426	51836.500	5900	Pt II	K	1947.33	51352.4	540	Pt II	50564-101916	K
1929.2449	51833.752	100000	Pt II	05	1948.32	51326.3	88			
1929.4586	51828.009	1900	Pt II	14	1948.4820	51322.004	890	Pt II	115060- 63738	K
1929.5799	51824.752	750			1948.64	51317.8	240			
1929.6829	51821.986	14000	Pt II	K	1948.9713	51309.120	5600	Pt II	21717- 73026	07
1930.0345	51812.55	120000	Ne II	C	1949.6947	51290.08	1000	Ne II		C
1930.7617	51793.031	960 D			1949.8139	51286.946	9700	Pt I	0- 51286	D
1930.9056	51789.171		C I	B	1949.9102	51284.413	16000	Pt II	23461- 74745	06
1931.02	51786.1	170	Ne III	L	1950.2777	51274.75	300	Ne II		C
1931.44	51774.8	120	Ne III	L	1950.51	51268.6	270	Pt II	53749-105018	K
1932.03	51759.0	110	Pt I	N	1951.37	51246.0	120	Pt II	58062-109307	K
1932.2433	51753.317	8200	Pt I	D	1951.4743	51243.309	450	Pt II	112433- 61190	K
1932.7391	51740.041	1900	Pt II	K	1951.7297	51236.60	400 U	Ne II		C
1933.1089	51730.144	75	Pt II	18	1951.7701	51235.543	2400	Pt I	10116- 61352	N



WAVELENGTH (ANGSTROMS) - VACUUM

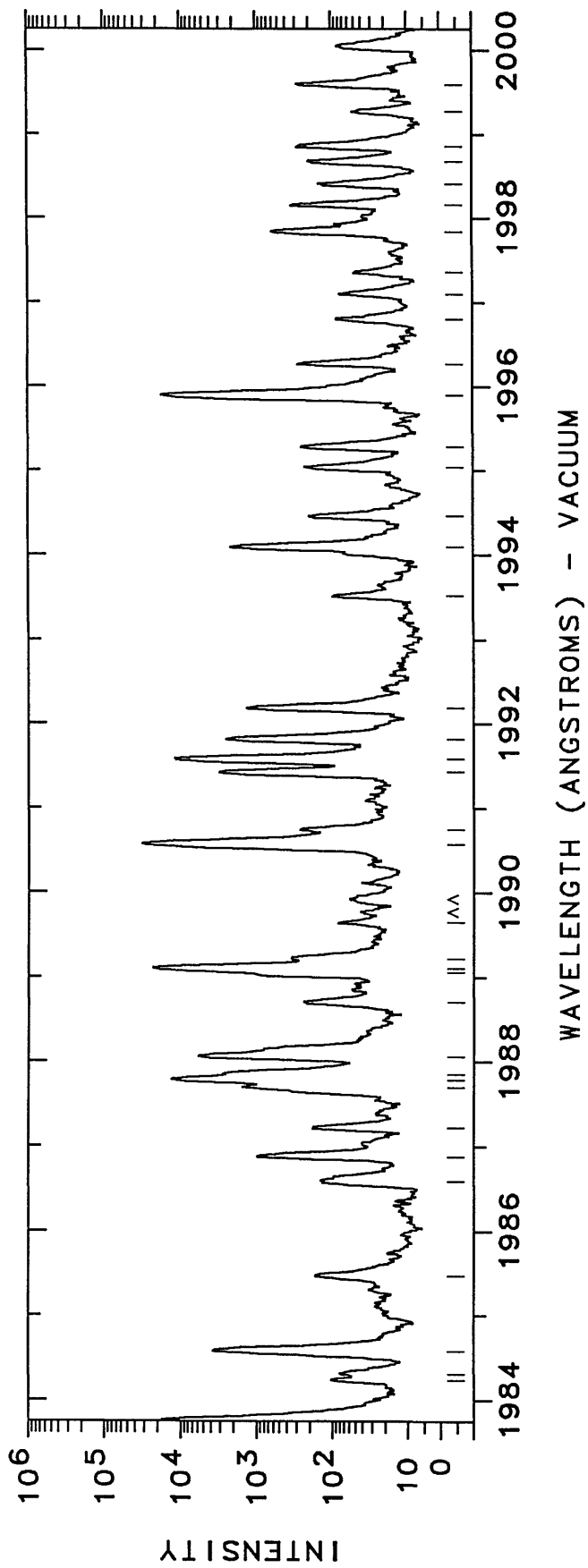


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1952.33	51220.8	59	Ne III	L	1967.22	50833.2	80	Pt II	50564-101397 K
1952.6940	51211.301	1400	Pt II	105086- 53875 K	1967.48	50826.4	29		
1952.94	51204.9	50			1967.87	50816.4	300	Pt II	58491-109307 K
1953.2467	51196.810	940	Pt II	27255- 78452 K	1968.57	50798.3	43	Pt II	53749-104548 K
1953.77	51183.1	540			1968.88	50790.3	74		
1954.0479	51175.82	920	Ne II	C	1969.07	50785.4	100		
1954.44	51165.6	150	Pt II	42031- 93197 K	1969.2802	50779.976	4000	Pt II	23461- 74241 07
1954.7436	51157.604	12000	Pt II	23461- 74619 06	1969.6807	50769.651	20000	Pt I	775- 51545 D
1955.54	51136.8	620	Pt II	46046- 97183 K	1970.0007	50761.403	9200	Pt II	104636- 53875 P
1956.06	51123.2	200	Pt I	13496- 64619 N	1970.33	50752.9	340	Pt I	13496- 64248 N
1956.4950	51111.810	840			1970.6936	50743.554	320	Pt II	23875- 74619 08
1956.76	51104.9	120	Ne III	L	1971.00	50735.7	110	Pt II	32237- 82972 K
1956.87	51102.0	220			1971.5374	50721.838	51000	Pt I	823- 51545 N
1957.0418	51097.529	680	Pt I	0- 51097 D	1971.73	50716.9	250	Pt II	42031- 92749 K
1957.64	51081.9	240	Ne III	L	1973.4663	50672.261	370	Pt II	115060- 64388 K
1957.8427	51076.626	41	Fe I	S	1974.54	50644.7	210	Pt II	54373-105018 K
1958.05	51071.2	7400	Ne III	L	1974.78	50638.6	41	Ne III	
1958.5027	51059.415	1300	Pt II	13329- 64388 08	1975.32	50624.7	150		
1958.94	51048.0	130			1975.45	50621.4	150		
1960.0384	51019.409	1300	Pt I	13496- 64515 N	1976.7900	50587.063	540	Pt II	32237- 82824 K
1960.50	51007.4	110			1977.12	50578.6	400		
1961.20	50989.2	510			1977.6654	50564.67	330	Ne II	
1961.3804	50984.501	3300	Pt II	50564-101549 K	1978.31	50548.2	82		
1961.5244	50980.758	4400	Pt I	10116- 61097 N	1978.6960	50538.334	2400	Pt II	23461- 73999 P
1961.6527	50977.424	1600	Pt I	775- 51753 D	1978.8444	50534.544	19000	Pt II	104410- 53875 K
1961.7910	50973.83	460	Ne II	C	1979.39	50520.6	130		
1962.1105	50965.529	2700	Pt I	10131- 61097 N	1979.5138	50517.455	1700	Pt II	114256- 63738 K
1962.3409	50959.545	3500	Pt II	16820- 67780 K	1979.7647	50511.054	37000	Pt I	775- 51286 D
1962.66	50951.3	220			1979.8876	50507.918	3100	Pt II	27255- 77763 K
1963.1429	50938.726	17000	Pt I	6567- 57506 D	1980.63	50489.0	330		
1964.5758	50901.574	2000	Pt I	6140- 57041 N	1980.90	50482.1	120		
1965.4370	50879.270	1800	Pt II	23875- 74754 12	1981.09	50477.3	53		
1965.92	50866.8	240			1981.2072	50474.277	390	Pt I	6567- 57041 N
1966.83	50843.2	96	Ne III	L	1982.34	50445.4	95		
1967.00	50838.8	310			1982.5759	50439.43	310	Ne II	
1967.15	50835.0	85			1983.7486	50409.614	18000	Pt II	13329- 63738 05

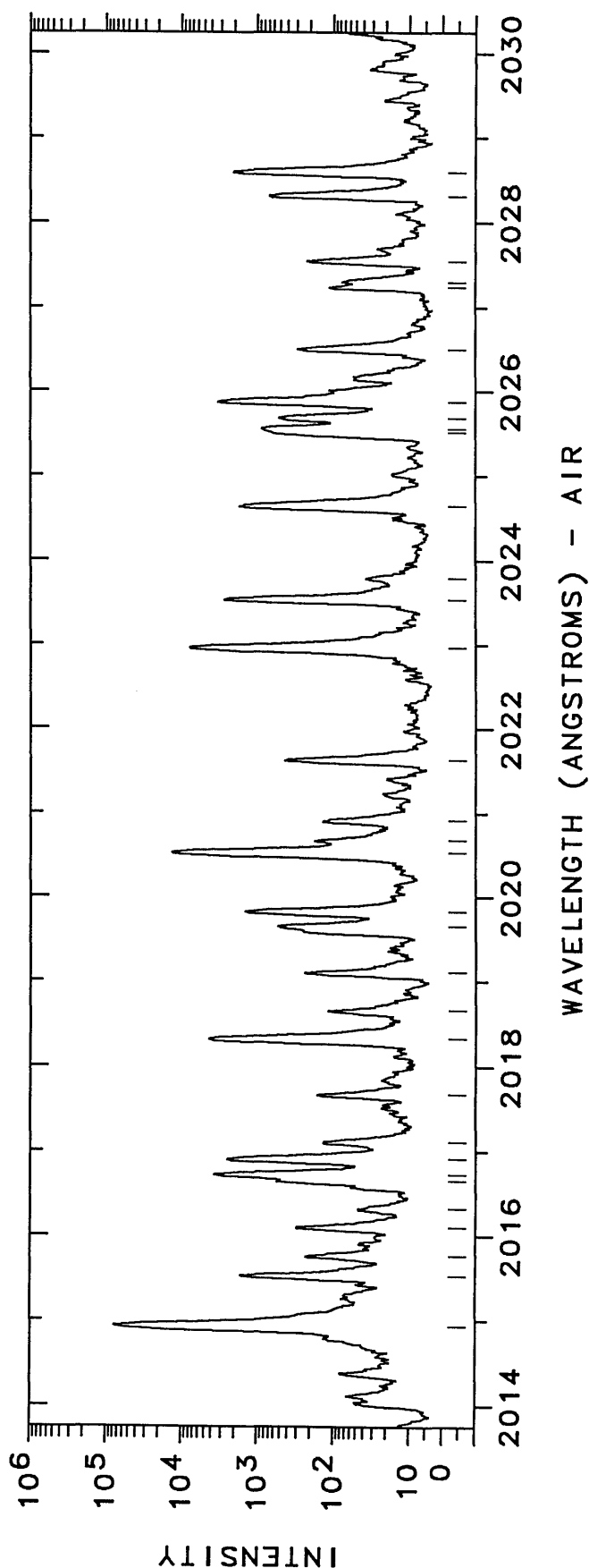
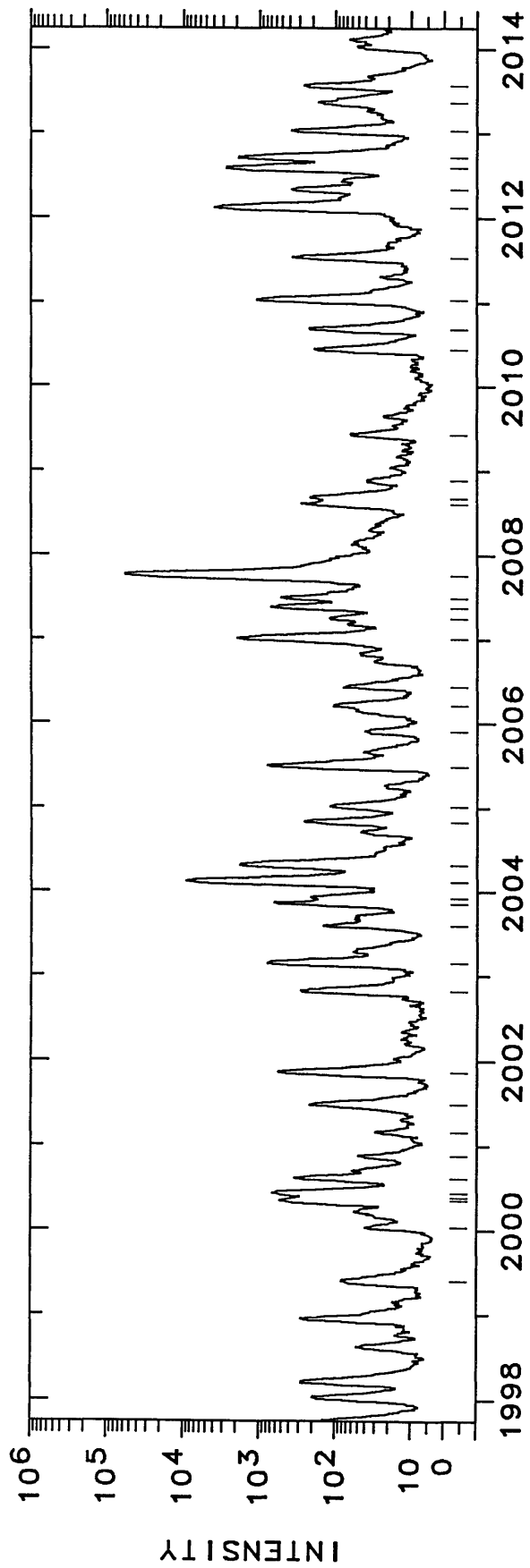


WAVELENGTH (ANGSTROMS) - VACUUM

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
1984.23	50397.4	96	Pt II	46046- 96443 K	1991.8236	50205.249	2500		
1984.31	50395.4	71			1992.1936	50195.924	1300	Pt I	15501- 65697 AN
1984.5698	50388.754	3700	Pt II	114127- 63738 K	1992.1936	50195.924	1300	Pt II	21168- 71364 AK
1985.4693	50365.926	160	Pt II	23875- 74241 09	1993.52	50162.5	91		
1986.59	50337.5	130	Pt II	113119- 62781 K	1994.0957	50148.05	2200	Ne II	C
1986.8846	50330.049	970	Pt I	13496- 63826 N	1994.46	50138.9	190		
1987.2168	50321.637	170	Pt I	775- 51097 D	1995.04	50124.3	220	Pt II	23875- 73999 K
1987.6987	50309.436	1500	Pt I	10131- 60441 N	1995.2792	50118.30	240	Ne II	C
1987.7868	50307.206	13000	Pt I	10116- 60423 N	1995.8991	50102.733	17000	Pt I	6567- 56670 N
1987.8582	50305.400	2200	Pt II	24879- 75184 05	1996.27	50093.4	270	Pt II	58062-108155 K
1988.0622	50300.236	5900	Pt II	23461- 73761 10	1996.80	50080.1	77		
1988.71	50283.9	230			1997.10	50072.6	70		
1989.0626	50274.939	1000 U	Ne II		1997.36	50066.1	42		
1989.0626	50274.939	U	Si I		1997.8371	50054.131	590	Pt II	32918- 82972 P
1989.1056	50273.852	23000	Pt I	823- 51097 D	1998.16	50046.0	330		
1989.2257	50270.816	200			1998.41	50039.8	140	Pt I	18566- 68606 N
1989.65	50260.1	75	Pt II	58062-108322 K	1998.6681	50033.32	190	Ne II	C
1990.5751	50236.738	32000	Pt II	15791- 66028 05	1998.86	50028.5	270		
1990.75	50232.3	260	Pt II	37877- 88110 K	1999.28	50018.0	44		
1991.4283	50215.215	3100	Pt II	104090- 53875 K	1999.5947	50010.135	280	Pt I	0- 50010 N
1991.5830	50211.314	12000	Pt I	10116- 60328 N					

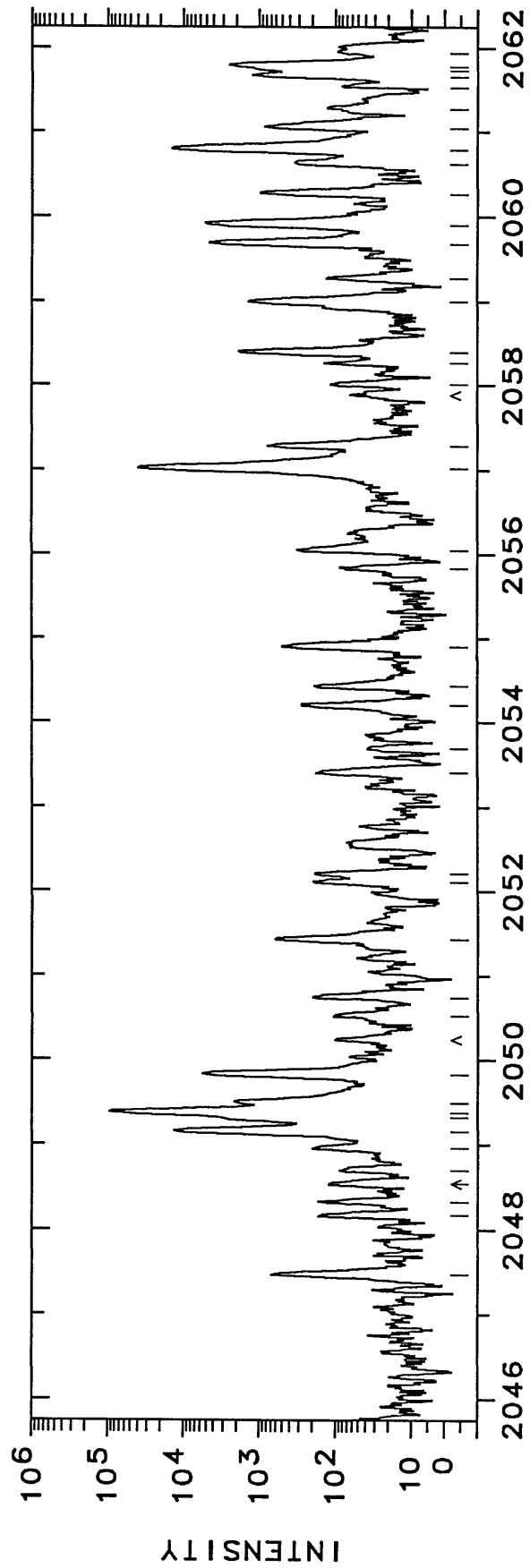
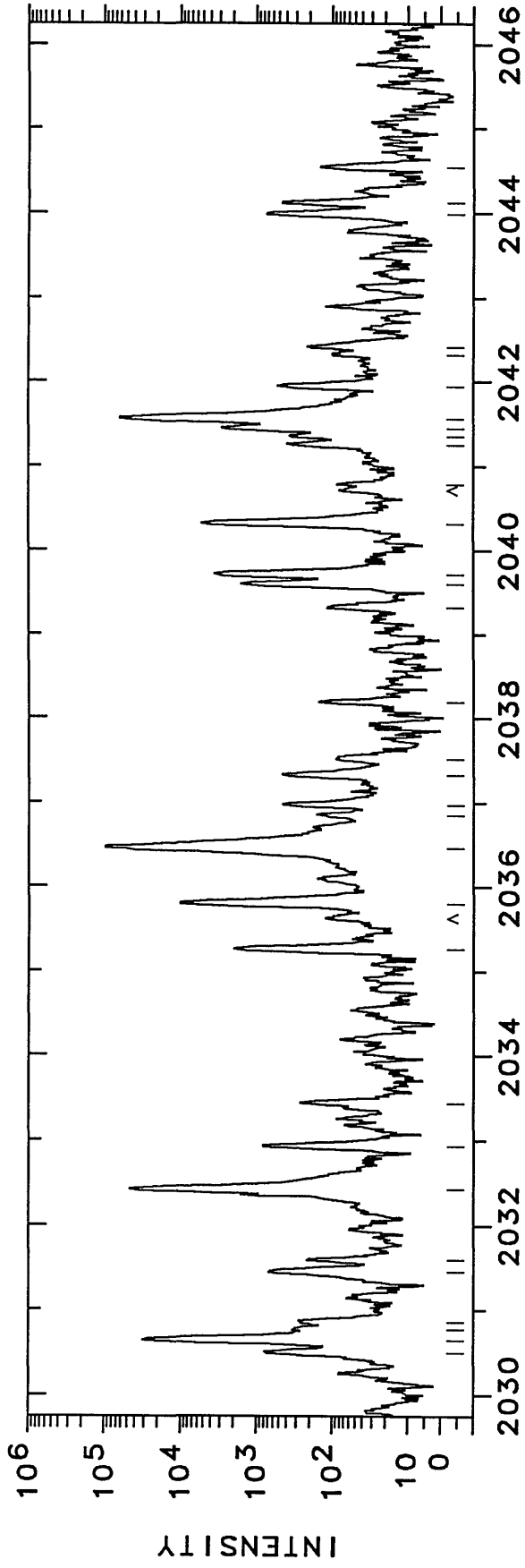


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1999.40	49998.8	76	Ne III	L	2012.5939	49671.076	2700	Pt I	13496- 63167 N
2000.03	49983.1	33	Pt II	58062-108037 K	2012.7156	49668.071	1900	Pt II	50564-100232 K
2000.3426	49975.245	450	Pt II	111162- 61190 K	2013.0290	49660.341	370	Pt I	10131- 59792 N
2000.3826	49974.246	550	Pt II		2013.36	49652.2	160	Pt II	21717- 71364 K
2000.4449	49972.690	660			2013.56	49647.2	250	Pt II	16820- 66434 07
2000.61	49968.6	340			2014.9330	49613.421	78000	Pt II	43737- 93336 K
2000.88	49961.8	43			2015.5192	49598.992	1700	Pt II	
2001.16	49954.8	23	Ne III	L	2015.76	49593.1	220	Pt II	
2001.49	49946.6	210	Ne II	C	2016.10	49584.7	300	Pt II	43737- 93322 K
2001.8736	49937.03	570	Ne III	L	2016.32	49579.3	41	Pt I	13496- 63067 N
2002.82	49913.4	280	Pt II	32918- 82824 K	2016.6483	49571.226	250	Pt I	10116- 59686 N
2003.1419	49905.417	790	Pt II	53749-103637 K	2016.7207	49569.447	3700	Pt I	23461- 73026 08
2003.59	49894.3	140	Pt II	0- 49880 D	2016.9067	49564.877	2500	Pt II	15791- 65351 05
2003.8556	49887.646	630	Pt I	29030- 78906 12	2017.1136	49559.793	130	Pt II	58491-108037 K
2003.92	49886.0	210	Pt II		2017.68	49545.9	160	Pt II	24879- 74409 K
2004.1273	49880.883	9300	Pt I		2018.3288	49529.958	4400	Pt II	46046- 95557 K
2004.3230	49876.013	1800	Pt II		2018.66	49521.8	110	Pt II	11162- 61665 K
2004.83	49863.4	250	Pt II	106434- 56587 K	2019.11	49510.8	230	Pt II	114539- 65046 K
2005.01	49858.9	110	Pt II	41434- 91271 K	2019.6648	49497.200	530	Pt I	823- 50299 N
2005.4895	49847.007	790	Pt II		2019.8361	49493.004	1400	Pt II	
2005.90	49836.8	35	Pt II		2020.5434	49475.679	14000	Pt I	
2006.21	49829.1	100			2020.68	49472.3	170		
2006.43	49823.6	72			2020.92	49466.5	130		
2007.0084	49809.29	2000	Ne II	C	2021.6302	49449.085	430	Pt I	16983- 66432 N
2007.25	49803.3	110	Pt I	10116- 59920 N	2022.9516	49416.791	7800	Pt II	106434- 57018 P
2007.3725	49800.256	690	Pt I	10116- 59916 N	2023.5420	49402.375	2700	Pt I	15501- 64904 N
2007.4809	49797.568	510	Pt II		2023.79	49396.3	31		
2007.7572	49790.715	58000	Pt II	101199- 51408 03	2024.6363	49375.677	1700	Pt I	10116- 59492 N
2008.60	49769.8	280			2025.5109	49354.359	250	Pt II	27255- 76610 08
2008.67	49768.1	210			2025.5585	49353.20	700	Ne II	C
2008.88	49762.9	32			2025.6856	49350.104	510		
2009.42	49749.5	56			2025.8727	49345.547	3300	Pt I	10116- 59462 N
2010.44	49724.3	180			2026.50	49330.3	290	Pt I	10131- 59462 N
2010.68	49718.3	220			2027.24	49312.3	110	Pt II	41434- 90746 K
2011.0252	49709.814	1100	Pt II	115060- 65351 K	2027.30	49310.8	70		
2011.53	49697.3	360			2027.54	49305.0	220		
2012.1226	49682.706	3900	Pt II	18097- 67780 K	2028.3159	49286.116	690	Pt I	0- 49286 D
2012.3291	49677.610	370			2028.5916	49279.420	2100	Pt I	775- 50055 D



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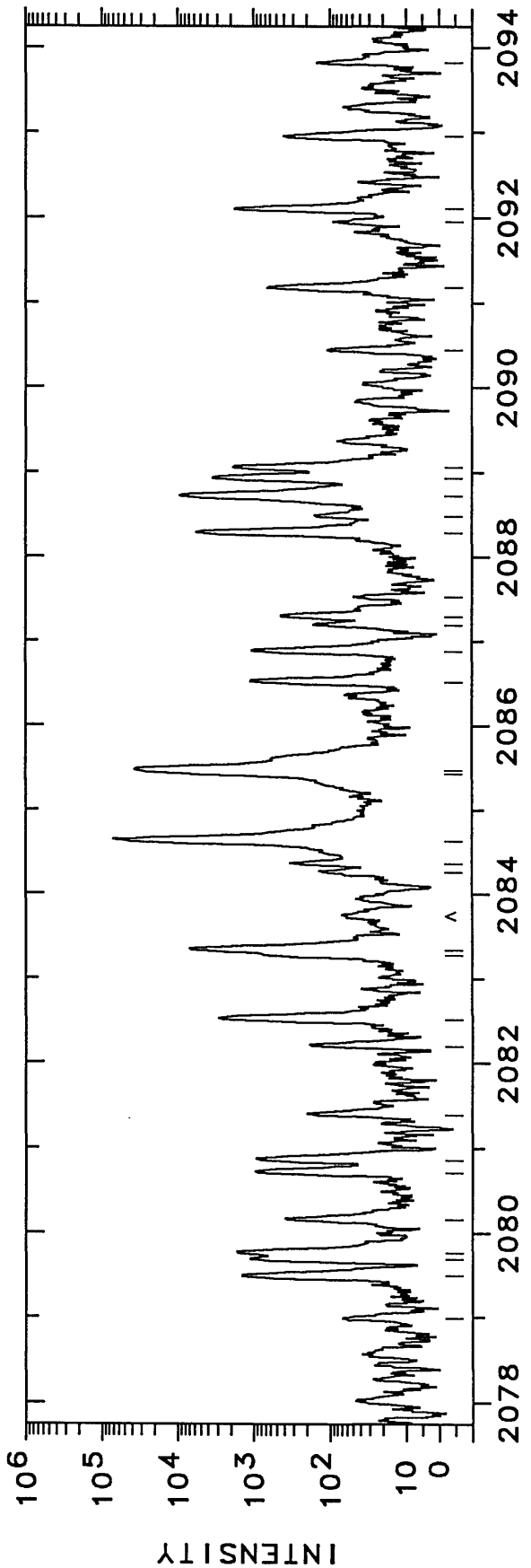
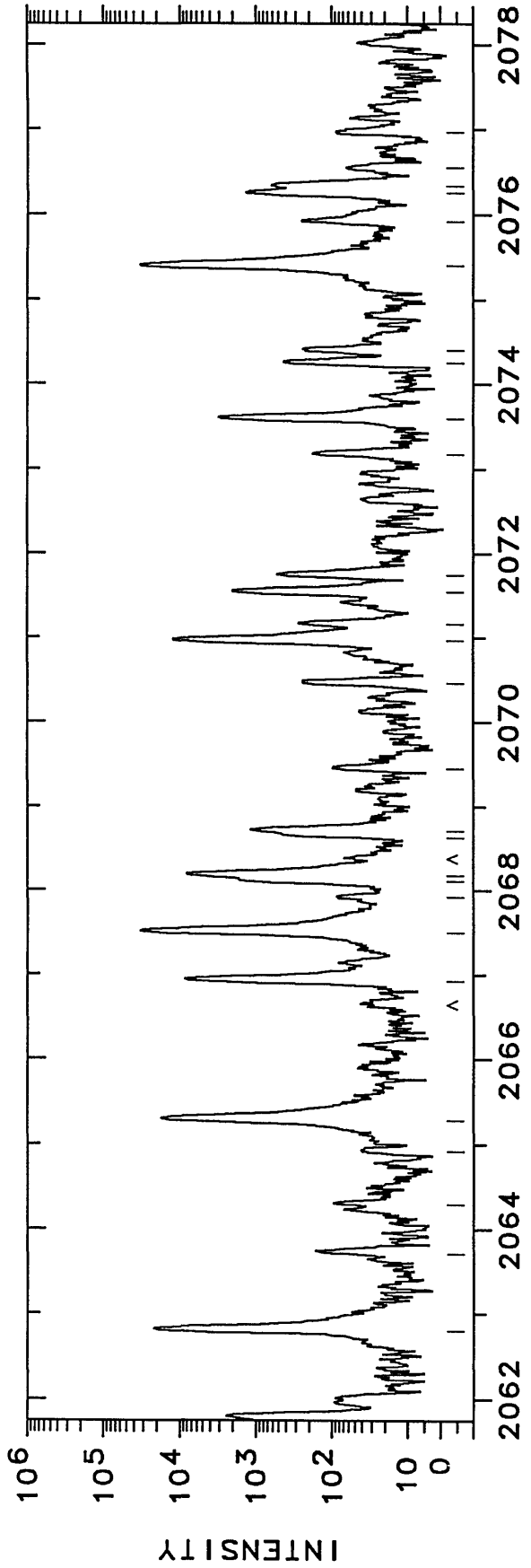
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2030.6456	49229.579	31000	Pt I	10116- 59346 N	2049.3255	48780.907	1400 P	Pt II	29261- 78043 K
2030.77	49226.6	330			2049.3915	48779.336	94000	Pt I	0- 48779 D
2030.86	49224.4	270	Pt II	29030- 78254 K	2049.5141	48776.419	2100	Pt II	105794- 57018 K
2031.4397	49210.339	680	Pt II	21168- 70379 12	2049.8396	48768.673	5600	Pt I	775- 49544 D
2031.59	49206.7	210			2050.52	48752.5	100		
2032.4256	49186.471	46000	Pt I	823- 50010 N	2050.74	48747.3	190	Pt I	15501- 64248 N
2032.9392	49174.046	820	Pt I	15501- 64675 N	2051.4224	48731.051	610	Pt II	113119- 64388 K
2033.44	49161.9	260			2052.11	48714.7	190	Pt II	42031- 90746 K
2035.2685	49117.776	2000	Pt I	15501- 64619 N	2052.21	48712.4	180		
2035.7985	49104.991	10000	Pt I	775- 49880 D	2053.41	48683.9	170		
2036.4666	49088.882	98000	Pt II	4786- 53875 09	2053.69	48677.3	32		
2036.85	49079.6	160			2054.1900	48665.405	270	Pt II	53749-102414 K
2036.9743	49076.649	450	Pt I	6140- 55216 D	2054.43	48659.7	180		
2037.3229	49068.253	450 S	Pt II	110258- 61190 K	2054.8678	48649.354	480	Pt I	6567- 55216 AN
2037.52	49063.5	83			2054.8678	48649.354	480	Pt I	10131- 58780 AN
2038.19	49047.4	150	Pt II	54373-103421 K	2055.83	48626.6	81	Pt II	115060- 66434 K
2039.32	49020.2	110	Ne III		2056.0459	48621.481	310	Pt II	32237- 80858 16
2039.5871	49013.789	1600	Pt I	15501- 64515 N	2057.0265	48598.308	39000	Pt II	8419- 57018 08
2039.7039	49010.983	3500	Pt I	10116- 59127 N	2057.2923	48592.029	770	Pt II	110257- 61665 K
2040.3346	48995.833	5200	Pt I	10131- 59127 N	2058.01	48575.1	110		
2040.78	48985.1	80	Pt II	42031- 91016 K	2058.26	48569.2	130	Ne III	
2041.25	48973.9	390			2058.3942	48566.020	1800	Pt I	13496- 62062 N
2041.3668	48971.064	360			2058.9944	48551.866	1400	Pt II	24879- 73431 15
2041.4605	48968.815	2900	Pt I	6567- 55536 D	2059.27	48545.4	120		
2041.5751	48966.067	62000	Pt II	15791- 64757 05	2059.6847	48535.596	4500	Pt I	0- 48535 D
2041.9609	48956.818	520	Pt II	110146- 61190 K	2059.9148	48530.175	5100	Pt II	16820- 65351 05
2042.32	48948.2	95			2060.2705	48521.796	970		
2042.41	48946.1	210			2060.62	48513.6	340		
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2044.1155	48905.222	460	Pt II	114256- 65351 K	2061.0173	48504.217	840	Pt II	58491-106995 K
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2047.4477	48825.638	690	Pt I	13496- 62321 N	2061.53	48492.2	77		
2048.17	48808.4	160			2061.6538	48489.245	1200	Pt II	29030- 77519 10
2048.33	48804.6	160			2061.7317	48487.413	1000	Pt II	23461- 71948 07
2048.54	48799.6	120	Pt II	43737- 92537 KM	2061.7824	48486.221	2500	Pt II	109676- 61190 K
2048.70	48795.8	83			2061.94	48482.5	88		
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WAVELENGTH (ANGSTROMS) - AIR

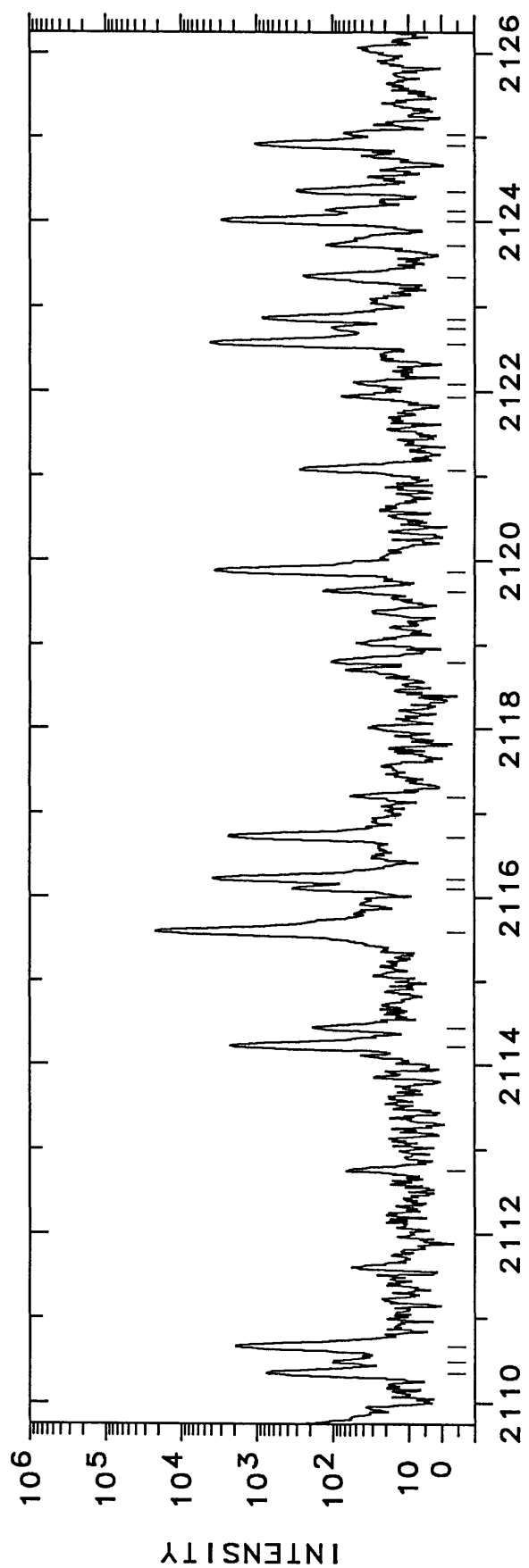
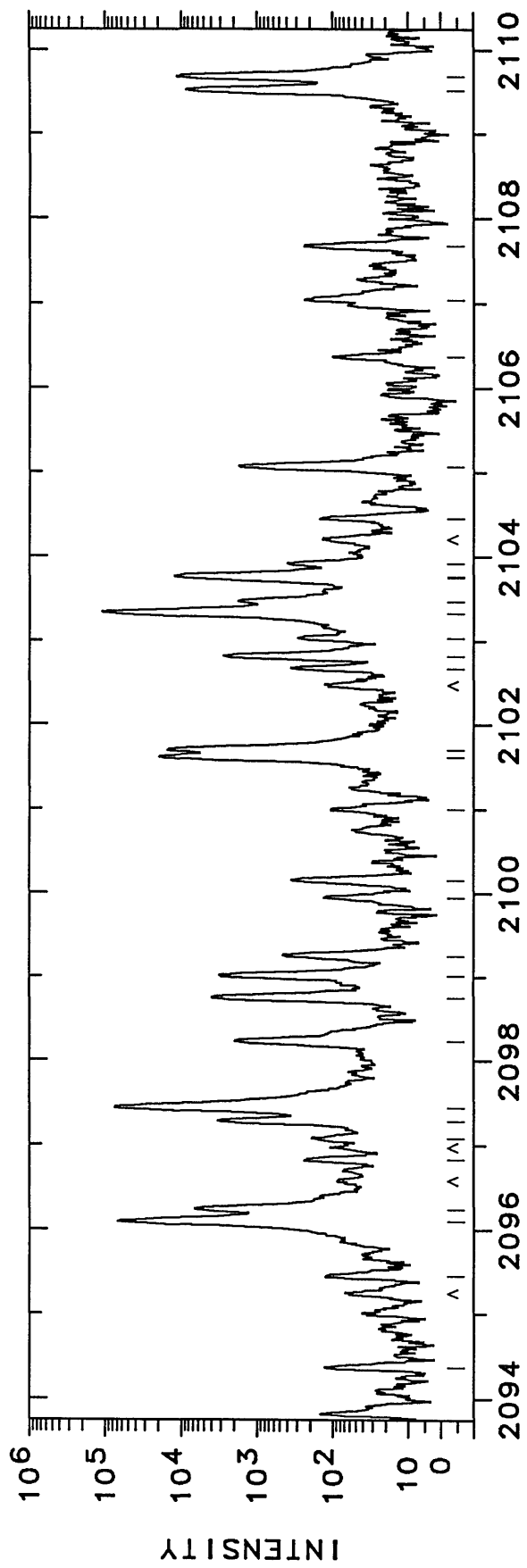


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2063.71	48440.9	160	Pt II		2079.7676	48066.981	1700	Pt II	21168- 69235 11
2064.29	48427.3	90	Pt II	114455- 66028 AK	2080.16	48057.9	380		
2064.29	48427.3	90	Pt II	114861- 66434 AK	2080.7324	48044.696	950	Pt II	112433- 64388 K
2064.92	48412.6	37	Ne III		2080.8762	48041.375	910	Pt II	54373-102414 K
2065.3084	48403.453	17000	Ne III		2081.39	48029.5	190		
2066.9329	48365.416	8500	Pt I	10116- 58482 N	2082.20	48010.8	180	Pt II	109676- 61665 K
2067.5105	48351.906	33000	Pt I	0- 48351 D	2082.5207	48003.444	2900	Pt I	775- 48779 D
2067.92	48342.3	81	Pt II	104930- 56587 K	2083.2782	47985.992	1000		
2068.1114	48337.859	1200	Pt II	109527- 61190 K	2083.3453	47984.445	6900	Pt I	10116- 58101 N
2068.1799	48336.258	8000	Pt II	13329- 61665 04	2084.26	47963.4	130		
2068.6303	48325.735	300	Pt II	27255- 75581 12	2084.36	47961.1	320		
2068.6854	48324.447	1200	Pt I	15501- 63826 N	2084.5960	47955.659	70000	Pt I	823- 48779 D
2069.45	48306.6	92			2085.4315	47936.449	6900 U	Pt II	16820- 64757 05
2070.46	48283.0	240			2085.4628	47935.73	37000	Ne II	
2070.9443	48271.745	12000	Pt I	6567- 54839 A	2086.4898	47912.138	1100	Pt II	104930- 57018 K
2070.9443	48271.745	12000	Pt I	10116- 58388 AN	2086.8804	47903.173	1000	Pt II	23461- 71364 K
2071.16	48266.7	270			2087.19	47896.1	160		
2071.5446	48257.757	2000	Pt II	29261- 77519 10	2087.29	47893.8	430		
2071.7423	48253.154	510	Pt II	50564- 98817 K	2087.52	47888.5	43	Pt II	34647- 82535 K
2073.17	48219.9	170	Pt II	121651- 73431 K	2088.2978	47870.663	5600	Pt I	10116- 57987 D
2073.5962	48210.018	3100	Pt I	10116- 58326 N	2088.48	47866.5	150	Pt I	18566- 66432 N
2074.2473	48194.887	420	Pt I	10131- 58326 N	2088.7282	47860.799	9300	Pt II	13329- 61190 05
2074.40	48191.3	230			2088.9388	47855.976	3400	Pt I	13496- 61352 N
2075.4004	48168.112	33000	Pt II	8419- 56587 09	2089.0647	47853.091	1800	Pt II	23461- 71314 07
2075.92	48156.1	240			2090.44	47821.6	100		
2076.2219	48149.056	1300	Pt I	13496- 61645 N	2091.1788	47804.719	650		
2076.2963	48147.332	550	Pt II	54373-102520 K	2091.95	47787.1	86		
2076.55	48141.5	58			2092.0837	47784.046	1800		
2076.97	48131.7	81			2092.9456	47764.370	400		
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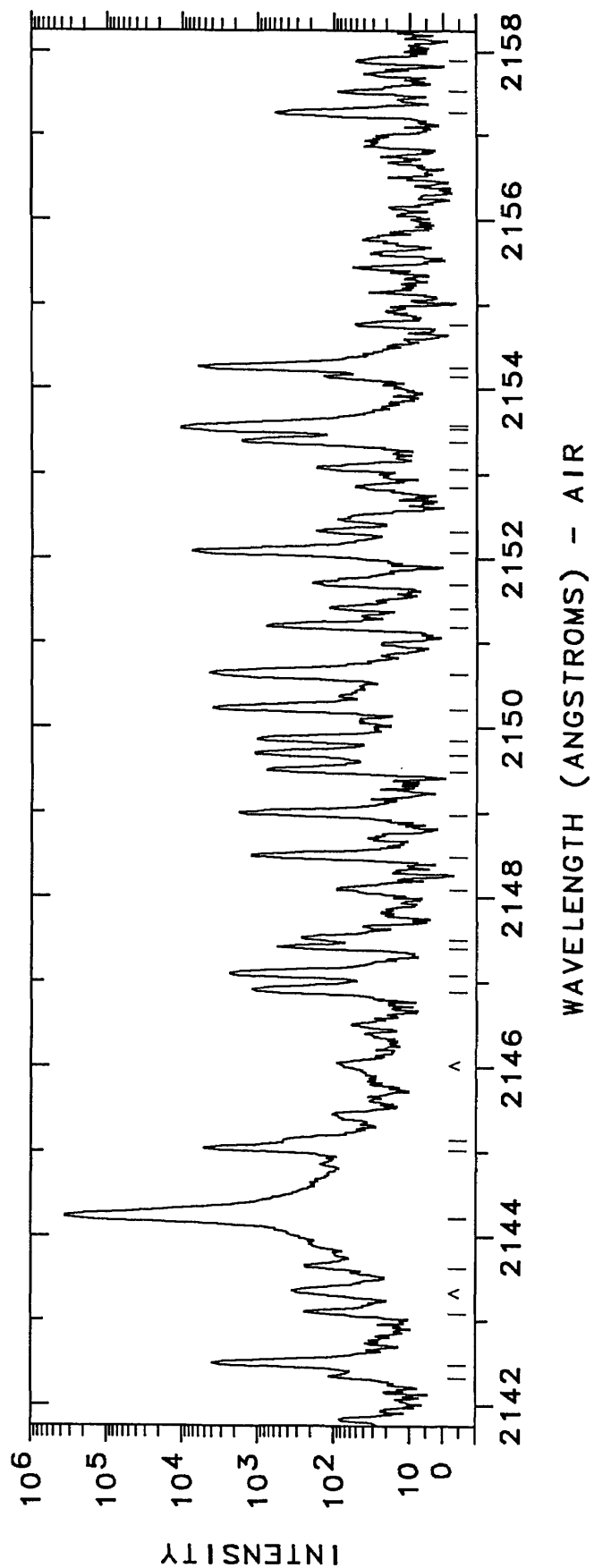
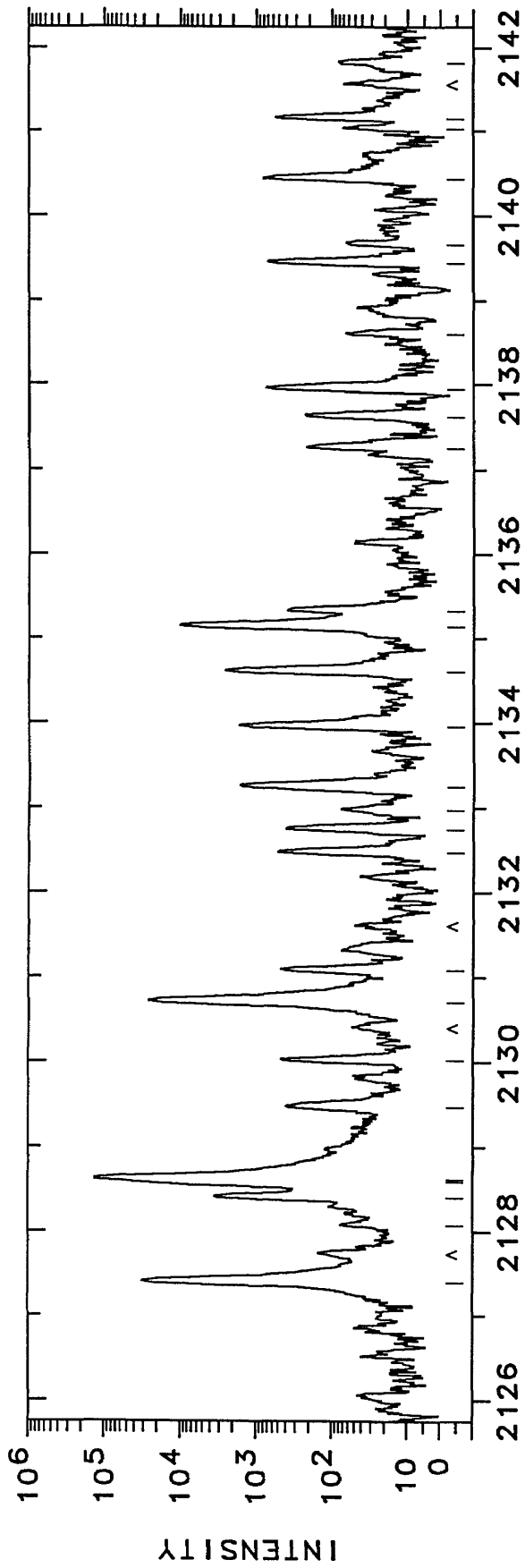
WAVELENGTH (ANGSTROMS) - AIR

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2095.45	47707.3	120	Ne II	C	2107.6556	47431.047	230	Pt I	10116- 57506
2096.1065	47692.35	69000	Ne II	C	2109.5055	47389.458	8600	Pt I	6567- 53953
2096.2538	47689.00	6600	Ne II	C	2109.6631	47385.919	12000	Pt II	32237- 79607
2096.83	47675.9	230	Pt II	112433- 64757	2110.3519	47370.453	730	Pt II	53749-101113
2097.08	47670.2	180	Pt II	15501- 63167	2110.48	47367.6	94	Pt II	64003-111320
2097.2881	47665.483	3300	Pt I	9356- 57018	2110.6657	47363.412	1900	Pt II	18566- 65850
2097.4478	47661.856	74000	Pt II	53749-101394	2112.75	47316.7	60	Pt I	32918- 80197
2098.2127	47644.483	1900	Pt II	18566- 66198	2114.2307	47283.557	2200	Pt II	18097- 65351
2098.7493	47632.303	3900	Pt I	110408- 62781	2114.44	47278.9	180	Pt II	121651- 74409
2099.0111	47626.362	3100	Pt II	13496- 61097	2115.5823	47253.354	22000	Pt II	110020- 62781
2099.25	47620.9	450	Ne III	L	2116.1050	47241.683	330	Pt II	50564- 97792
2099.95	47605.1	130	Pt I	16820- 64388	2116.2173	47239.175	3700	Pt II	
2100.1196	47601.227	340	Pt I	15501- 63067	2116.7102	47228.176	2300	Pt II	
2101.00	47581.3	100	Pt II	6567- 54133	2117.19	47217.5	53		
2101.5979	47567.748	19000	Pt II	54373-101916	2118.79	47181.8	97		
2101.6839	47565.801	15000	Pt I	48591- 96131	2119.63	47163.1	130		
2101.6839	47565.801	15000	Pt I	117493- 69953	2119.8880	47157.388	3600	Pt I	15501- 62659
2102.67	47543.5	350	Pt II	823- 48351	2121.0700	47131.113	270	Pt I	18566- 65697
2102.8167	47540.181	2800	Pt II	6140- 53665	2121.93	47112.0	71		
2102.8167	47540.181	2800	Pt II	58062-105597	2122.09	47108.5	47	Pt II	119057- 71948
2103.03	47535.4	290	Pt II	21717- 69235	2122.5713	47097.781	4100	Pt I	6567- 53665
2103.3449	47528.242	110000	Pt I	48591- 96109	2122.74	47094.0	97		
2103.4852	47525.072	1800	Pt I	21717- 69235	2122.8504	47091.588	830	Pt II	113119- 66028
2103.7536	47519.011	1900	Pt II	48591- 96109	2123.34	47080.7	240	Pt II	114861- 67780
2103.7804	47518.405	12000	Pt II		2123.71	47072.5	120	Pt II	104090- 57018
2103.7804	47518.405	12000	Pt II		2124.0062	47065.967	2900	Pt II	50564- 97630
2103.92	47515.3	390	Pt II		2124.12	47063.4	120	Pt II	42031- 89095
2104.45	47503.3	140	Pt II		2124.35	47058.3	290		
2105.0776	47489.126	1700	Pt II	23875- 71364	2124.9015	47046.138	1000	Pt II	53749-100795
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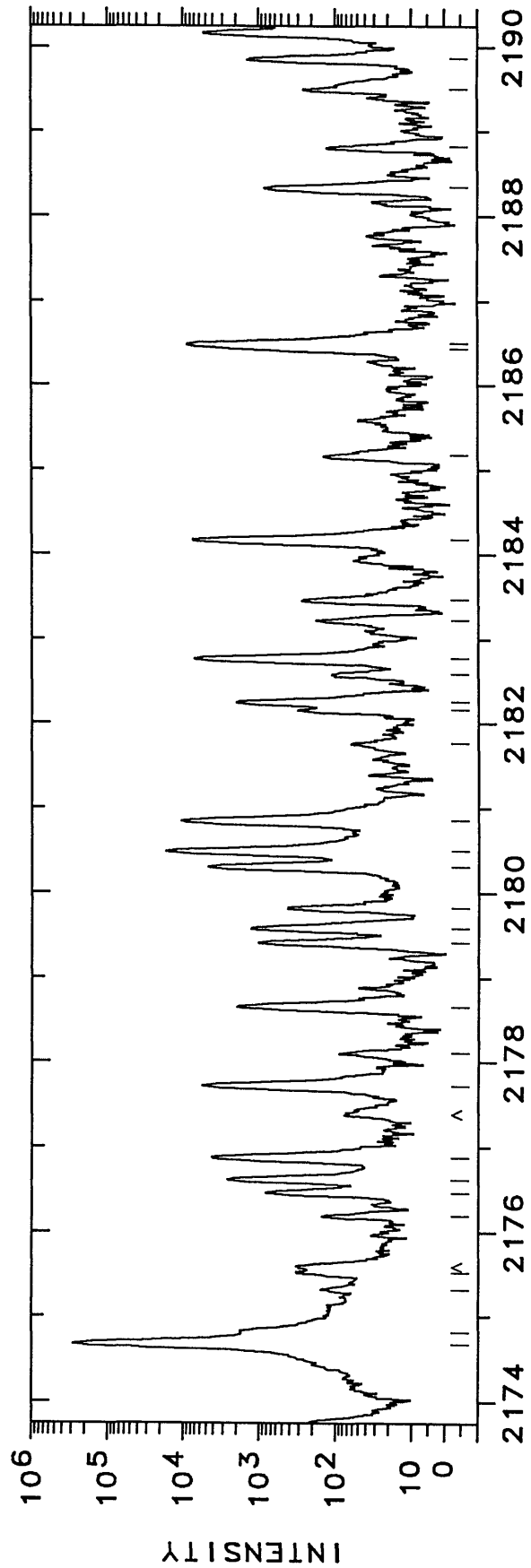
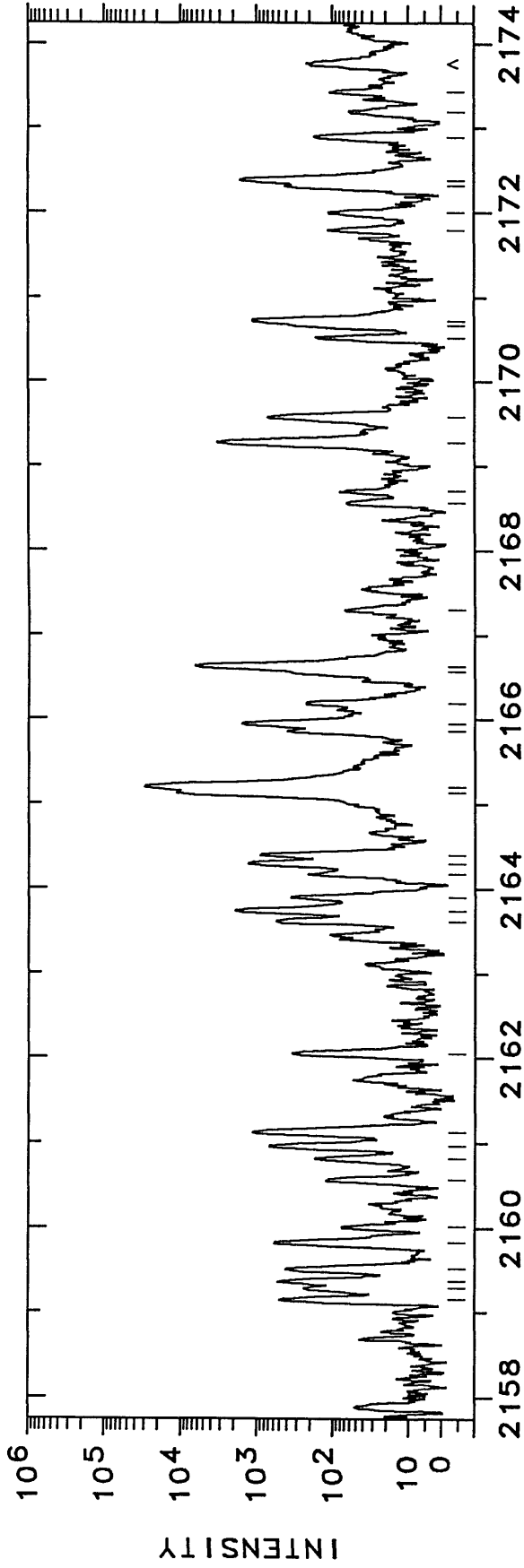


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2128.4205	46968.364	3500	Pt II	54373-101341	K	2146.8767	46564.634	1200	Pt II	109346- 62781	K
2128.5878	46964.673	40000 P	Pt I	775- 47740	D	2147.0706	46560.428	2400	Pt I	15501- 62062	N
2128.6340	46963.654	130000	Pt I	0- 46963	N	2147.3909	46553.485	560	Pt I	10116- 56670	N
2129.47	46945.2	400	Pt I	13496- 60441	N	2147.50	46551.1	260			
2130.02	46933.1	460				2148.09	46538.3	88	Pt I	10131- 56670	N
2130.7079	46917.947	26000	Pt II	16820- 63738	05	2148.4748	46530.002	1200	Pt II	54373-100903	K
2131.0749	46909.869	470	Pt I	10131- 57041	N	2148.9998	46518.636	1800	Pt II	110257- 63738	K
2132.4727	46879.123	520	Pt I	6140- 53019	D	2149.5030	46507.747	780	Pt II	116689- 70181	K
2132.7460	46873.116	400				2149.7007	46503.470	1100	Pt II	23875- 70379	14
2132.9687	46868.223	70	Pt II	36484- 83352	19	2149.8689	46499.832	1000	Ne III		L
2133.2486	46862.073	1700	Pt II	53749-100611	K	2150.2397	46491.814	4000	Pt II	23461- 69953	06
2133.9737	46846.153	1700	Pt II	112433- 65587	K	2150.6274	46483.433	850 U	Ne III		L
2134.6307	46831.737	2600	Pt I	13496- 60328	N	2150.6567	46482.800	4200 P	Pt I	16983- 63466	N
2135.1631	46820.061	10000	Pt I	15501- 62321	N	2151.2003	46471.055	790	Ne III		L
2135.3443	46816.087	390				2151.40	46466.7	110	Pt II	121651- 75184	K
2137.25	46774.3	210	Pt II	111162- 64388	K	2151.69	46460.5	190	Ne III		L
2137.62	46766.3	220				2152.0902	46451.842	7500	Pt I	6567- 53019	D
2137.9562	46758.900	740	Pt II	64003-110762	K	2152.32	46446.9	170			
2138.59	46745.0	61				2152.8656	46435.114	47	Pt II	24879- 71314	07
2139.4476	46726.308	700	Pt II	109507- 62781	K	2153.06	46430.9	170	Ne III		L
2139.66	46721.7	59	Pt II	46046- 92767	K	2153.3933	46423.736	1600	Pt I	13496- 59920	N
2140.4367	46704.718	800				2153.5394	46420.587	7500 P	Pt I	13496- 59916	N
2141.02	46692.0	65				2153.5684	46419.962	6500 U	Pt I	0- 46419	D
2141.1620	46688.899	550	Pt II	32918- 79607	12	2154.14	46407.6	130	Pt II	110146- 63738	K
2141.81	46674.8	77	Pt II	114455- 67780	K	2154.2472	46405.336	6200	Pt II	112433- 66028	AK
2142.32	46663.7	110				2154.2472	46405.336	6200	Pt II	111162- 64757	AK
2142.5054	46659.628	3900	Pt II	18097- 64757	06	2154.76	46394.3	48			
2143.08	46647.1	230				2157.2670	46340.384	580	Pt II	58491-104831	K
2143.62	46635.4	230	Pt II	48591- 95226	K	2157.52	46335.0	82			
2144.2123	46622.489	200000 U	Pt I	0- 46622	D	2157.89	46327.0	46			
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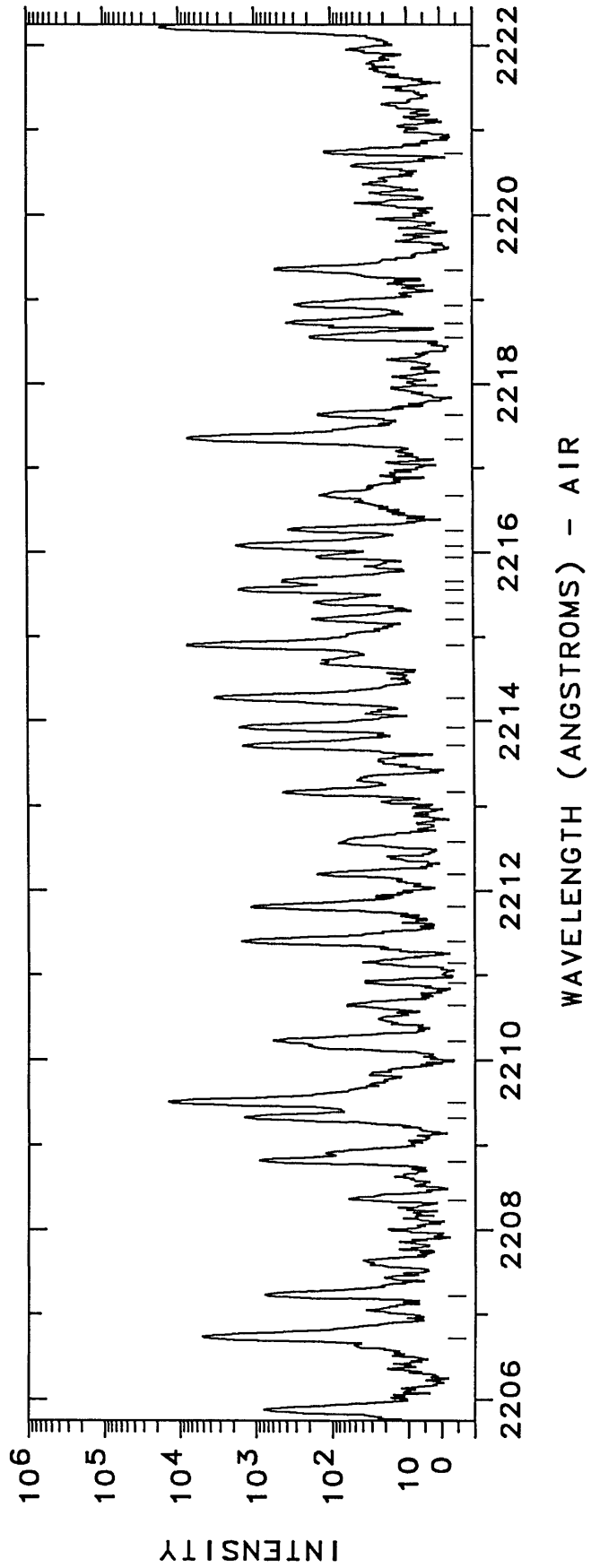
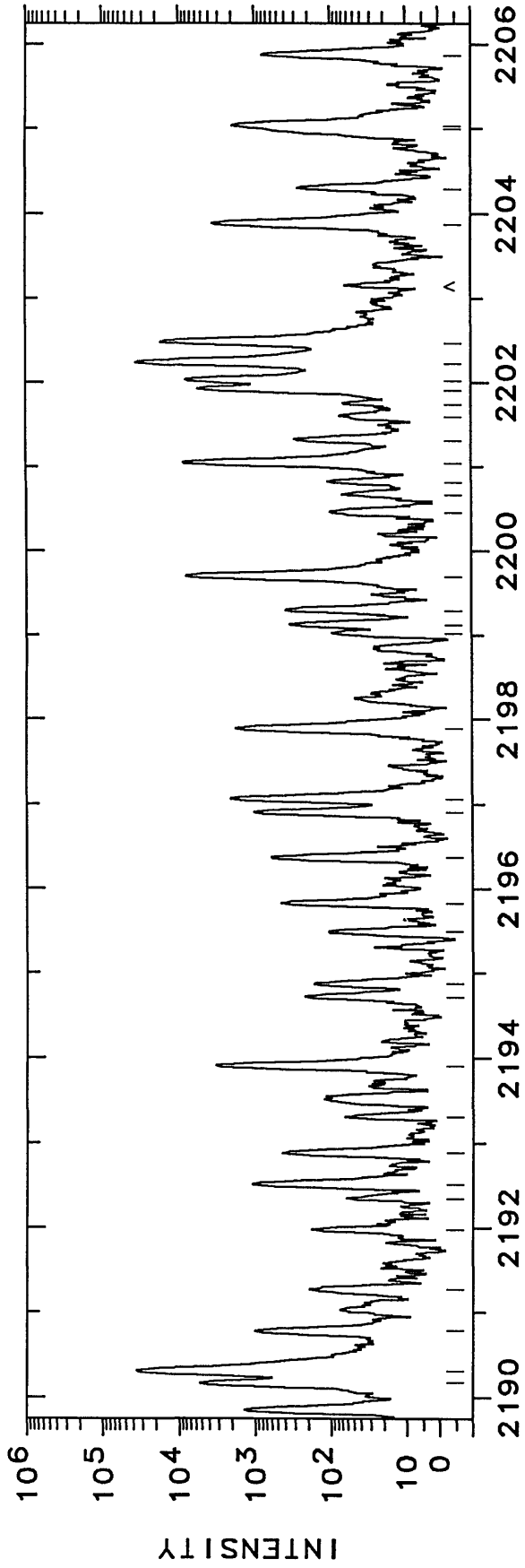
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2159.29	46297.0	240	Ne III		2173.19	46000.9	57		
2159.3719	46295.216	530	Ne III		2173.43	45995.8	110		
2159.5153	46292.143	420	Ne III		2174.6853	45969.257	290000	Pt I	823- 46792 N
2159.8289	46285.424	590			2174.8392	45966.005	1000	Pt I	13496- 59462 N
2160.02	46281.3	74			2175.32	45955.8	150		
2160.57	46269.5	120			2175.52	45951.6	330		
2160.82	46264.2	170	Ne III		2176.19	45937.5	150	Pt II	109676- 63738 K
2160.9675	46261.037	690	Ne III		2176.4730	45931.504	820	Pt I	6140- 52071 D
2161.1343	46257.468	1200	Ne III		2176.6289	45928.214	2600	Ne III	
2162.05	46237.9	340			2176.8802	45922.913	4200	Pt II	29261- 75184 L
2163.6119	46204.503	550	Ne III		2177.6988	45905.652	5700	Ne III	
2163.7345	46201.886	2000	Ne III		2178.1182	45896.809		Fe I	
2163.8965	46198.426	360	Pt II	64003-110202 K	2178.6549	45885.508	2000	Ne III	
2164.18	46192.4	210	Pt II	64003-110196 K	2179.4123	45869.563	1000	Pt II	110258- 64388 K
2164.2949	46189.923	1300	Pt I	13496- 59686 N	2179.5832	45865.967	1300	Pt II	54373-100239 K
2164.3955	46187.776	910			2179.83	45860.8	430		
2165.1407	46171.882	8000 P	Pt I	10116- 56288 N	2180.3229	45850.408	4800	Pt I	15501- 61352 N
2165.2108	46170.386	30000 P	Pt I	0- 46170 D	2180.5042	45846.596	17000	Pt I	775- 46622 D
2165.8714	46156.306	400			2180.8613	45839.090	11000	Ne III	
2165.9608	46154.401	1600	Pt II	29030- 75184 07	2181.7748	45819.90	60	Ne II	
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2166.5655	46141.521	300 U	Pt II	24879- 71021 K	2182.2632	45809.645	2000	Pt II	
2166.6376	46139.986	6500	Pt I	823- 46963 N	2182.59	45802.8	110	Ne III	
2167.30	46125.9	68	Pt II	43737- 89863 K	2182.7795	45798.811	7200	Pt I	823- 46622 D
2168.56	46099.1	63			2183.23	45789.4	180	Pt II	109527- 63738 K
2168.70	46096.1	79			2183.47	45784.3	270	Pt II	111371- 65587 K
2169.2711	46083.977	3300	Pt I	16983- 63067 N	2184.1755	45769.542	7500	Pt II	110158- 64388 K
2169.5637	46077.764	710	Pt II	23875- 69953 09	2185.17	45748.7	140		
2170.5112	46057.65	160	Ne II		2186.4314	45722.325	600 P		
2170.6696	46054.29	300 U	Ne II		2186.4768	45721.375	8900 L	Pt II	53749- 99471 K
2170.7267	46053.079	1100	Pt I	18566- 64619 N	2188.3437	45682.374	840	Pt I	18566- 64248 N
2171.79	46030.5	110	Pt II	119057- 73026 K	2188.82	45672.4	120		
2172.00	46026.1	110	Pt II	117340- 71314 K	2189.50	45658.3	250		
2172.3162	46019.385	420	Pt II	110408- 64388 K	2189.8625	45650.694	1400	Pt II	110408- 64757 K
2172.3937	46017.744	1600	Pt II	32237- 78254 K					



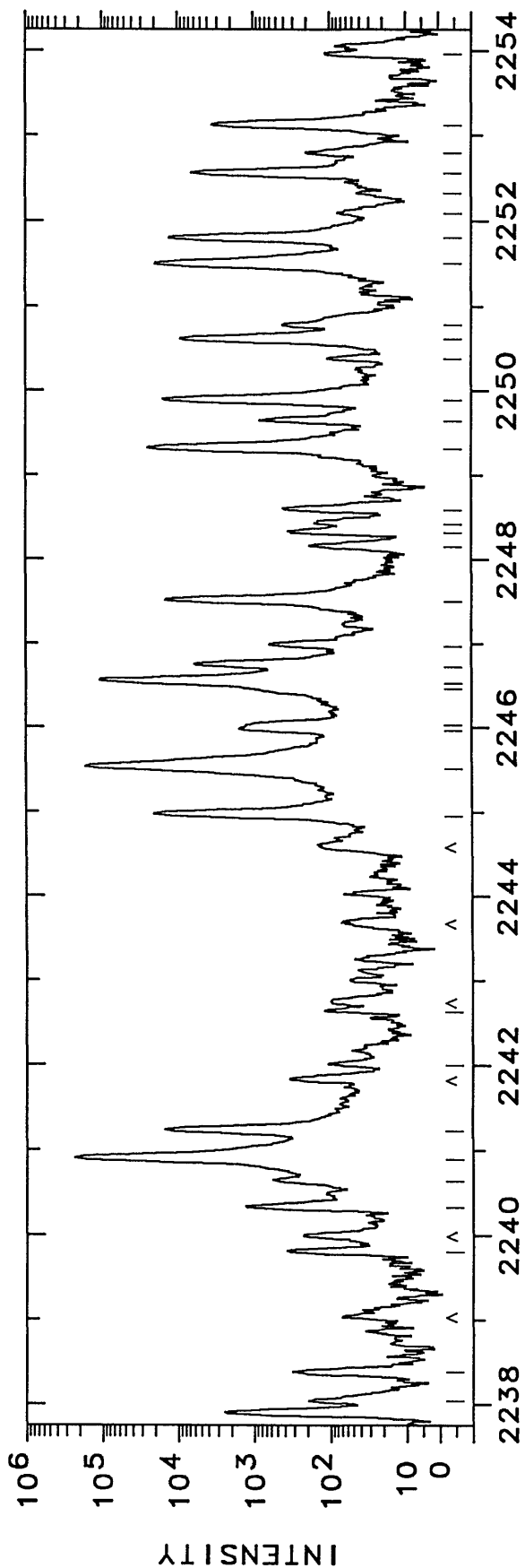
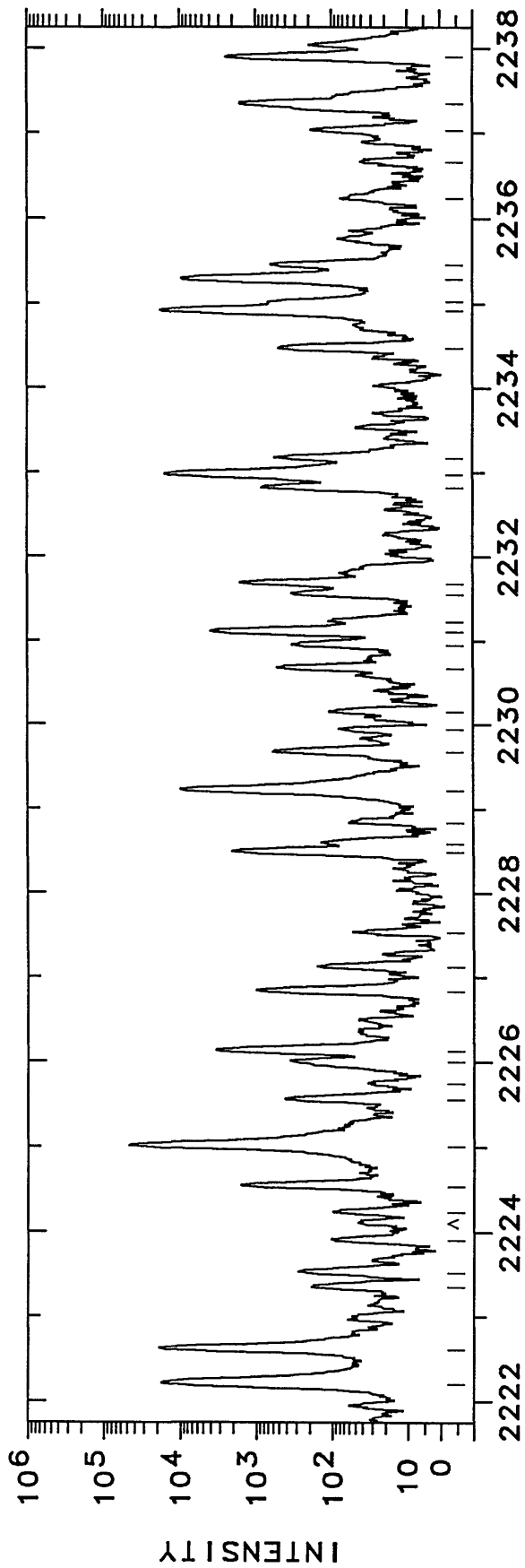
WAVELENGTH (ANGSTROMS) - AIR



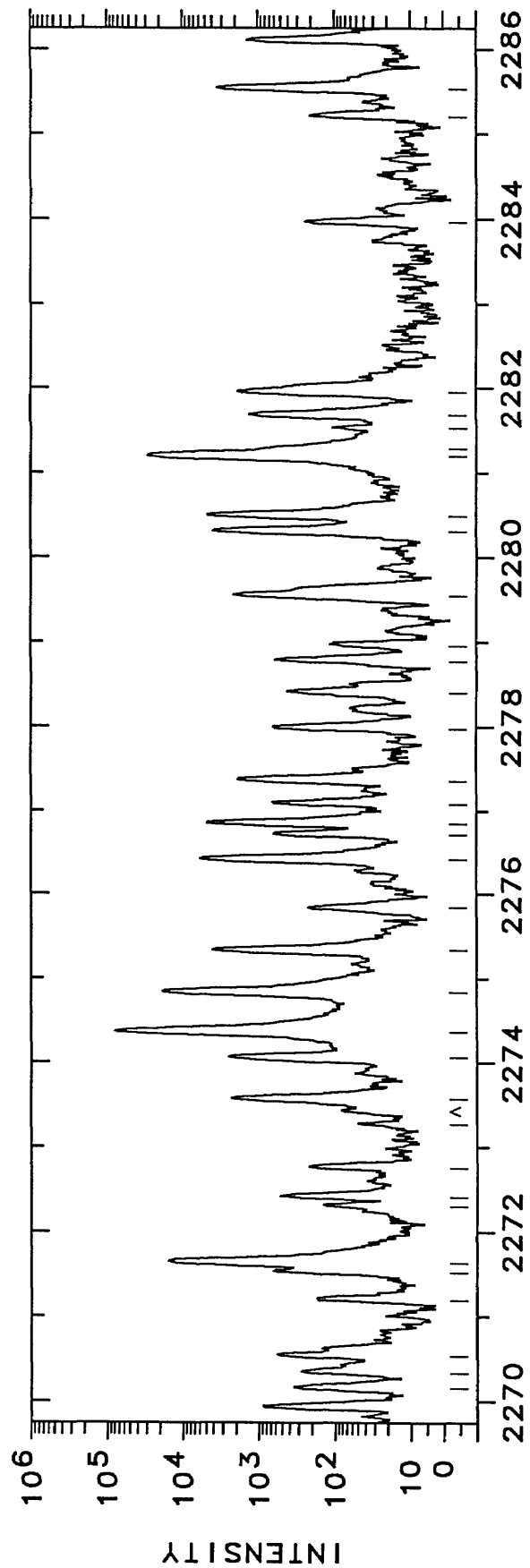
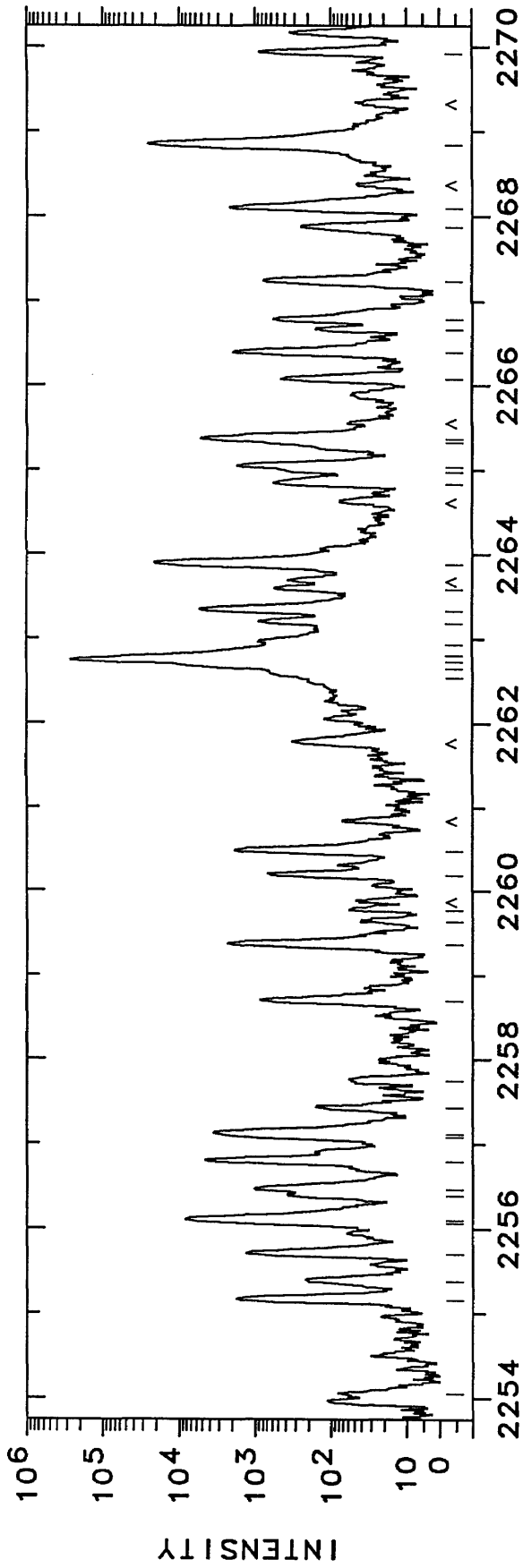
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2190.3216	45641.126	40000	Pt II	18097- 63738 06	2206.7295	45301.801	5100	Pt II	24879- 70181 10
2190.7859	45631.455	1000	Pt I	13496- 59127 N	2207.2323	45291.482	770	Ne III	
2191.27	45621.4	190			2208.35	45268.6	57		
2191.98	45606.6	180			2208.7801	45259.748	910	Pt I	18566- 63826 N
2192.34	45599.1	60			2209.3139	45248.814	1400	Ne III	
2192.5064	45595.650	1100	Pt I	15501- 61097 N	2209.5043	45244.913	14000	Pt II	106434- 61190 P
2192.8441	45588.628	450	Pt II	29030- 74619 08	2210.2121	45230.427	590		
2193.31	45578.9	64			2210.64	45221.7	61		
2193.9016	45566.656	3300	Pt II	50564- 96131 K	2210.8919	45216.522		Si I	
2194.71	45549.9	220	Pt II	34647- 80197 K	2211.14	45211.4	36	Pt II	110257- 65046 K
2194.87	45546.6	170	Ne III		2211.4074	45205.982	1500	Pt II	96614- 51408 05
2195.49	45533.7	100	Pt II	32918- 78452 K	2211.8204	45197.542	1200	Ne III	
2195.8322	45526.598	450	Pt II	32237- 77763 K	2212.20	45189.8	150	Pt II	50564- 95754 K
2196.3763	45515.321	610			2212.58	45182.0	78	Ne III	
2196.9120	45504.223	1000	Pt I	6567- 52071 D	2213.17	45170.0	430		
2197.0743	45500.863	2100	Pt II	110258- 64757 K	2213.7165	45158.833	1500	Ne III	
2197.8914	45483.949	1800	Pt II	29261- 74745 08	2213.9314	45154.449	1600	Pt I	21967- 67121 N
2199.02	45460.6	92			2214.2720	45147.503	3400	Pt II	29261- 74409 K
2199.12	45458.5	340			2214.9014	45134.676	7800	Pt II	111162- 66028 K
2199.29	45455.0	380			2215.21	45128.4	170		
2199.7010	45446.535	8000	Pt I	58062-103517 K	2215.40	45124.5	160	Pt II	32918- 78043 K
2200.45	45431.1	98	Pt II	21967- 67413 N	2215.5540	45121.384	1600	Pt II	109507- 64388 K
2200.66	45426.7	66			2215.6525	45119.378	430		
2200.81	45423.6	100			2215.94	45113.5	150	Ne III	
2201.0082	45419.547	8500	Pt I	10116- 55536 D	2215.94	45111.511	1700		
2201.31	45413.3	290	Pt II	36484- 81897 K	2216.26	45107.0	350		
2201.59	45407.5	71			2216.6688	45098.692		Si I	
2201.74	45404.5	64			2217.3450	45084.941	7500	Pt I	10131- 55216 D
2201.9153	45400.836	5500	Pt II	110158- 64757 K	2217.63	45079.1	140		
2202.0165	45398.750	7900	Pt II	15791- 61190 06	2218.55	45060.5	180		
2202.2230	45394.494	42000	Pt I	775- 46170 D	2218.72	45057.0	370	Pt II	119057- 73999 AK
2202.4664	45389.478	17000	Pt II	110146- 64757 K	2218.72	45057.0	370	Pt II	110408- 65351 AK
2203.8924	45360.112	3500	Pt II	23875- 69235 14	2218.93	45052.7	290		
2204.29	45351.9	260			2219.35	45044.2	520		
2204.9955	45337.422	750	Ne III		2220.73	45016.2	120		
2205.0541	45336.218	1900	Pt II	32918- 78254 K					



WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
2222.2053	44986.344	18000	Pt I	6567- 51545 D	2237.3520	44681.818	1600	Pt II	115060- 70379 K
2222.6134	44978.083	19000	Pt I		2237.8916	44671.046	2400	Pt II	110258- 65587 K
2223.35	44963.2	180			2238.04	44668.1	190		
2223.52	44959.7	280			2238.38	44661.3	310	Pt II	50564- 95226 K
2223.90	44952.1	99			2239.80	44633.0	370		
2224.23	44945.4	93			2240.3222	44622.586	1300	Pt I	775- 45398 D
2224.5247	44939.443	1600	Pt I	15501- 60441 N	2240.6434	44616.189	560	Pt II	58062-102678 K
2225.0094	44929.655	48000	Pt II	101517- 56587 K	2240.8965	44611.151	240000	Pt II	101199- 56587 04
2225.56	44918.5	420			2241.2288	44604.537	15000	Pt II	105794- 61190 K
2225.75	44914.7	28			2242.00	44589.2	100	Pt II	109346- 64757 K
2226.00	44909.7	350	Pt II	60986-105896 K	2242.63	44576.7	110		
2226.1261	44907.118	3400	Pt II	110258- 65351 K	2244.9773	44530.068	21000	Pt I	6567- 51097 D
2226.8442	44892.639	990	Pt I	10116- 55009 N	2245.5244	44519.219	170000	Pt II	9356- 53875 06
2227.12	44887.1	150	Pt II	105794- 60907 K	2245.9752	44510.284	650		
2227.53	44878.8	49			2246.0273	44509.252	650		
2228.4978	44859.330	2100	Pt II	21168- 66028 07	2246.4630	44500.620	600 U	Pt I	18566- 63067 N
2228.59	44857.5	130			2246.5216	44499.460	110000	Pt II	101517- 57018 K
2228.84	44852.4	54	Pt II	43737- 88589 K	2246.7172	44495.585	5900		
2229.2303	44844.591	9700	Pt II	16820- 61665 04	2246.9427	44491.121	600	Pt I	13496- 57987 D
2229.67	44835.7	590	Pt II	54373- 99209 K	2247.4822	44480.442	15000	Pt II	105388- 60907 11
2229.94	44830.3	75	Pt I	13496- 58326 N	2248.15	44467.2	180		
2230.15	44826.1	100	Pt I	15501- 60328 N	2248.32	44463.9	340		
2230.67	44815.7	520	Pt II	119057- 74241 K	2248.42	44461.9	150		
2230.9447	44810.133	320	Pt II	58062-102872 K	2248.59	44458.5	400	Pt II	58062-102520 K
2231.0958	44807.099	3900	Pt II	110158- 65351 K	2249.3075	44444.350	24000	Pt I	0- 44444 A
2231.23	44804.4	110			2249.3075	44444.350	24000	Pt II	54373- 98817 AK
2231.55	44798.0	330	Pt II	64003-108802 K	2249.6320	44437.939	800	Pt II	119057- 74619 K
2231.6623	44795.727	1600	Pt II	110146- 65351 K	2249.8994	44432.659	16000	Pt I	0- 44432 E
2232.8199	44772.504	830	Pt II	105962- 61190 K	2250.38	44423.2	99		
2232.9725	44769.445	15000	Pt II	106434- 61665 P	2250.6201	44418.431	9000	Pt II	21168- 65587 12
2233.1579	44765.727	550			2250.7883	44415.113	410	Pt I	15501- 59916 N
2234.47	44739.4	490	Pt II	60986-105726 K	2251.5105	44400.867	19000	Pt II	29030- 73431 18
2234.9262	44730.313	18000	Pt I	0- 44730 D	2251.8084	44394.993	13000	Pt II	95803- 51408 05
2235.0229	44728.376	600	Pt II	111162- 66434 K	2252.09	44389.4	72		
2235.3029	44722.774	9300	Pt II	18097- 62820 06	2252.32	44384.9	38		
2235.4674	44719.485	620	Pt I	6567- 51286 D	2252.5690	44380.005	6400	Pt II	110408- 66028 K
2236.2508	44703.82	71	Ne II		2252.8022	44375.41	200	Ne II	
2236.66	44695.6	36	Pt II	54373- 99068 K	2253.1210	44369.132	3500	Pt II	16820- 61190 05
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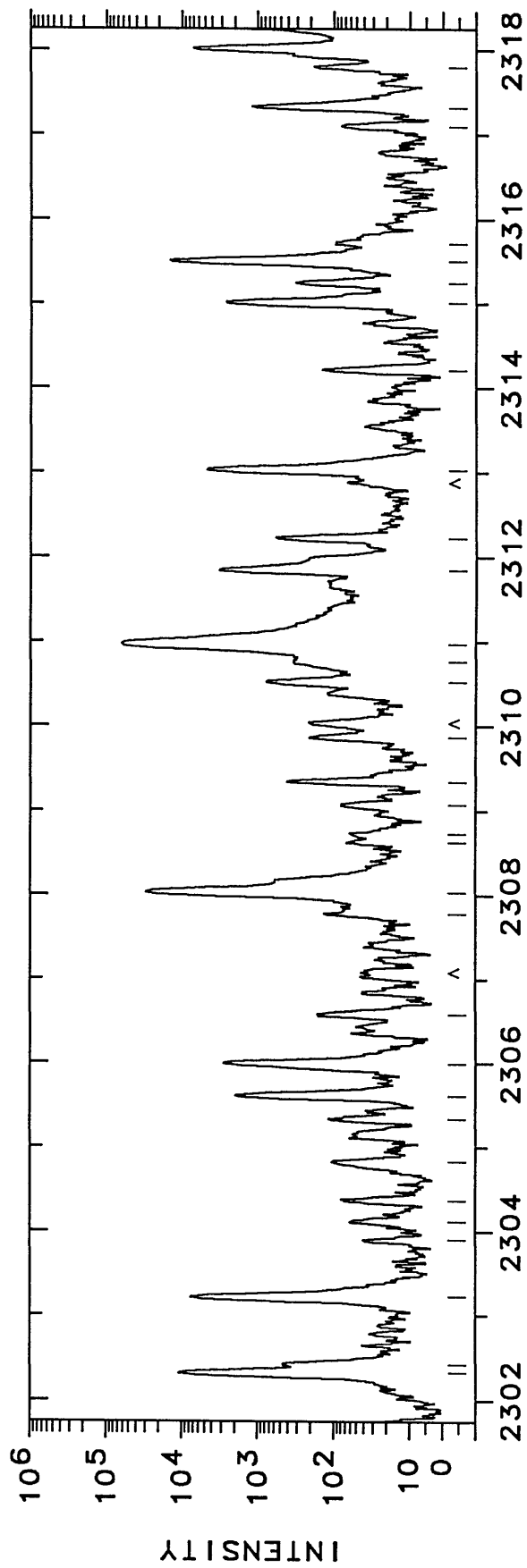
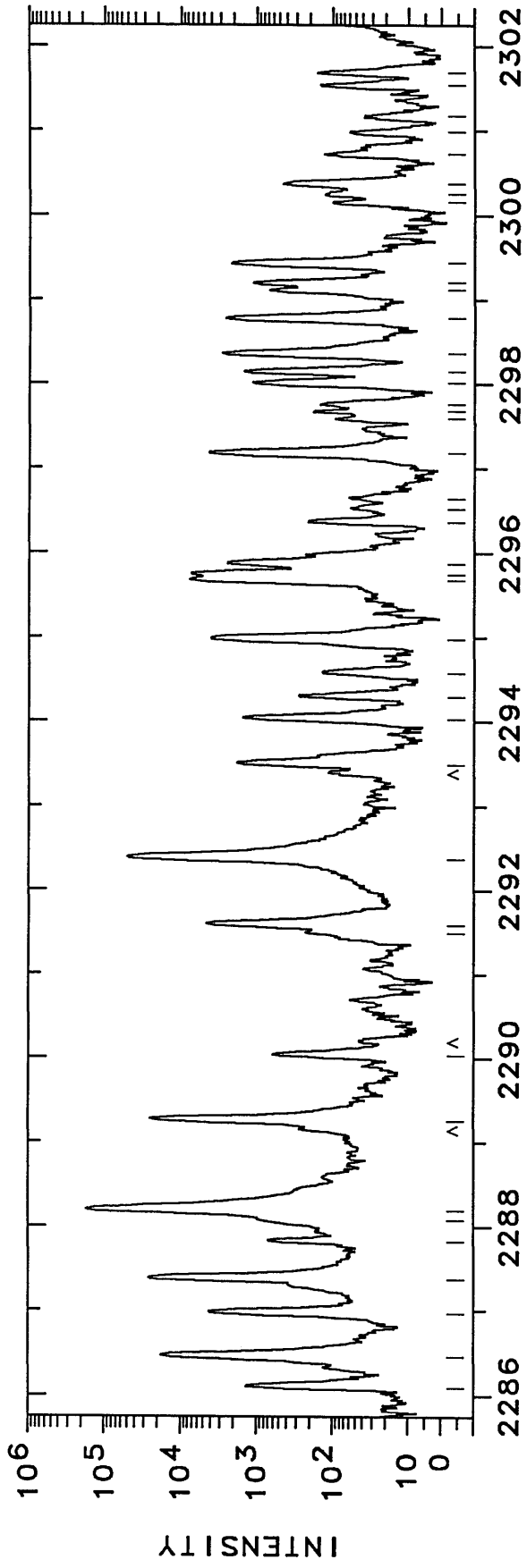


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2255.1285	44359.640	1800	Pt II	109676- 65351 K	2268.8384	44061.794	25000	Pt I	101116- 54178 N
2255.38	44364.7	210	Pt II	109676- 65351 K	2269.8986	44041.215	870	Pt II	53749- 97786 K
2255.6725	44318.949	1300	Pt II	23461- 67780 K	2270.15	44036.3	340	Pt II	64003-108037 K
2256.0645	44311.249	600 U	Pt II	119057- 74745 K	2270.33	44032.8	270	Pt II	58491-102520 K
2256.0897	44310.754	8200 P	Pt II	21717- 66028 07	2270.53	44029.0	560	Pt I	10116- 54133 N
2256.3955	44304.75	380	Ne II		2271.1694	44016.576	170	Pt I	13496- 57506 N
2256.4402	44303.873	1000	Pt II	105962- 61665 K	2271.5067	44010.040	500	Pt I	105066- 61058 11
2256.7868	44297.069	4500 P	Pt II	15501- 59792 N	2271.6194	44007.857	15000	Pt II	
2257.0841	44291.234	1000 P	Pt I	15501- 59792 N	2272.30	43994.7	140	Pt II	
2257.1283	44290.367	3500 P	Pt I	15501- 59792 N	2272.3928	43992.880	510	Pt II	110020- 66028 K
2257.43	44284.4	150	Pt II	50564- 94842 K	2272.75	43986.0	210		
2257.75	44278.2	53	Pt II	34647- 78906 16	2273.27	43975.9	43		
2258.7143	44259.271	840	Pt II		2273.5812	43969.886	2300	Ne III	
2259.3776	44246.278	2300	Pt II		2274.0682	43960.471	2500	Pt I	15501- 59462 N
2259.63	44241.3	35			2274.3816	43954.415	78000	Pt I	775- 44730 E
2259.77	44238.6	53			2274.8409	43945.541	18000	Pt I	0- 43945 E
2260.1994	44230.191	670	Pt II	110258- 66028 K	2275.3406	43935.891	4000	Pt II	48591- 92526 K
2260.4894	44224.519	1800	Pt II	32237- 76461 13	2275.84	43926.3	220		
2262.5437	44184.367	400	Pt I	15501- 59686 N	2276.4229	43915.004	5800	Pt I	6140- 50055 E
2262.6453	44182.385	8200	Pt II	21168- 65351 07	2276.7069	43909.527	630	Pt II	117340- 73431 K
2262.7185	44180.955	260000	Pt II	101199- 57018 04	2276.8553	43906.665	4700	Pt I	823- 44730 E
2262.8033	44179.300	1000 P	Pt II	105086- 60907 K	2277.0957	43902.030	640		
2262.9279	44176.868	890	Pt II	109527- 65351 K	2277.3650	43896.838	1900	Pt II	105086- 61190 K
2263.1646	44172.247	870	Ne III		2277.9574	43885.424	630	Pt I	21967- 65852 N
2263.3116	44169.379	5300	Pt II	29261- 73431 18	2278.3772	43877.339	410	Pt II	114256- 70379 K
2263.5635	44164.463	540			2278.7659	43869.855	590	Pt II	21717- 65587 12
2263.8611	44158.659	21000	Pt II	105066- 60907 11	2278.95	43866.3	110	Ne III	
2264.8318	44139.733	570	Ne III		2279.5408	43854.944	2100	Pt II	58062-101916 K
2264.9735	44136.973	300 P			2280.3080	43840.190	3900	Pt II	114861- 71021 K
2265.0364	44135.747	1700			2280.4916	43836.661	4600	Pt I	10116- 53953 E
2265.3238	44130.148	400 P	Pt II	110158- 66028 K	2281.1942	43823.161	29000	Pt II	110257- 66434 K
2265.3794	44129.065	5200	Pt II	105794- 61665 K	2281.2798	43821.517	400	Pt I	10131- 53953 N
2266.0799	44115.426	450	Ne III		2281.52	43816.9	99		
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2266.66	44104.1	160			2281.9613	43808.430	1900		
2266.7928	44101.552	580			2283.96	43770.1	230		
2267.2445	44092.766	760	Pt I	18566- 62659 N	2285.20	43746.3	200	Pt II	115060- 71314 K
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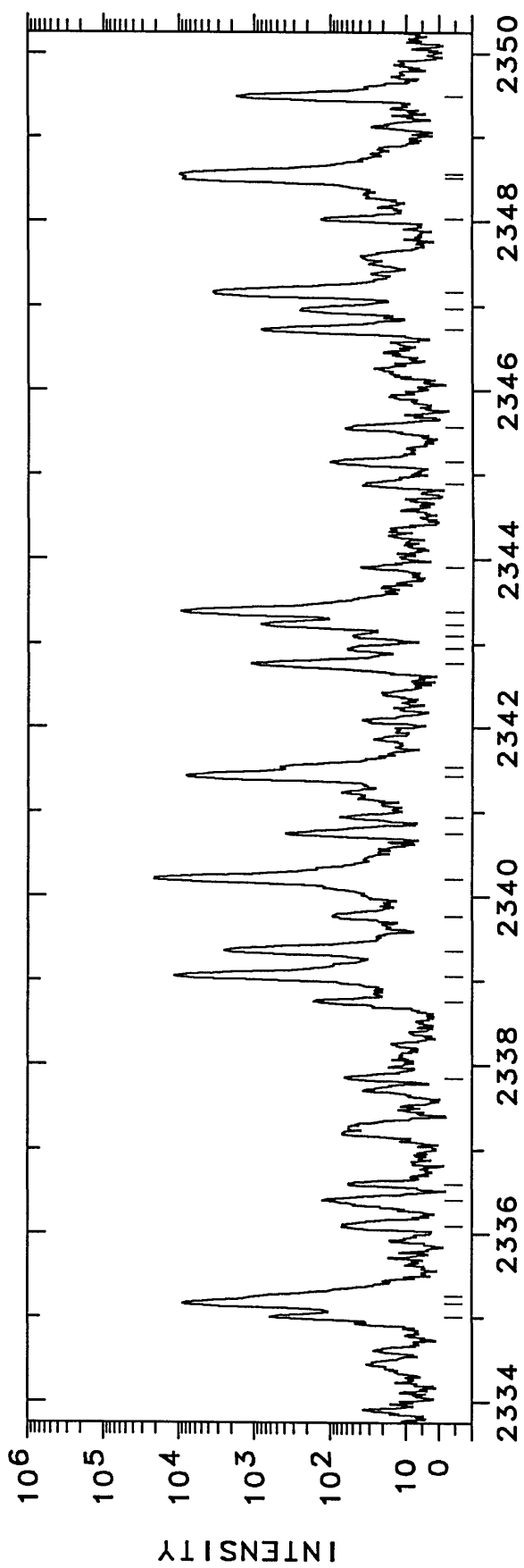
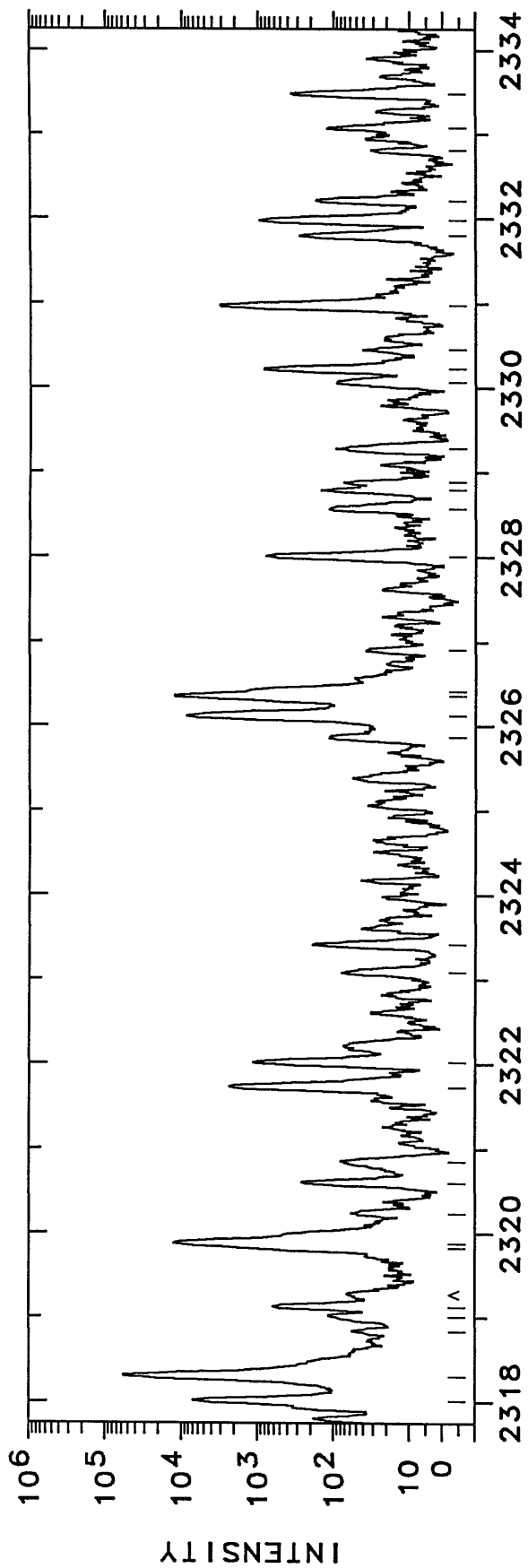
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2286.9707	43712.480	4200	Pt II	110146- 66434 K	2301.175	43442.68			
2287.3643	43704.959	26000	Pt II	104763- 61058 K	2301.54	43435.8	140		
2287.8248	43696.164	680	Pt II	115060- 71364 K	2301.69	43433.0	160	Pt II	53749- 97183 K
2288.0770	43691.348	250 P	Pt II	32918- 76610 A	2302.3068	43421.330	11000	Pt II	105086- 61665 K
2288.0770	43691.348	250 P	Pt II	119057- 75365 AK	2302.42	43419.2	460	Pt II	54373- 97792 K
2288.2050	43688.903	180000	Pt II	13329- 57018 05	2303.2065	43404.369	7600	Pt I	6140- 49544 E
2289.2765	43668.457	25000	Pt I	775- 44444 E	2303.90	43391.3	34	Ne III	L
2290.0616	43653.488	610			2304.12	43387.2	54		
2291.5144	43625.813	250	Pt I	15501- 59127 N	2304.37	43382.5	72	Pt II	64003- 107386 AK
2291.6058	43624.073	4500			2304.37	43382.5	72	Pt II	111162- 67780 AK
2292.3987	43608.986	90000	Pt I	823- 44432 E	2304.83	43373.8	99	Ne III	L
2293.4678	43588.659	1800	Pt II	21168- 64757 07	2305.34	43364.2	110	Pt I	21967- 65331 N
2294.0059	43578.436	1500	Pt II	104636- 61058 P	2305.6355	43358.646	1900		
2294.29	43573.0	280			2306.0122	43351.565	2800	Pt II	104410- 61058 K
2294.5676	43567.770	130	Pt II	18097- 61665 05	2306.58	43340.9	160	Ne III	L
2294.9724	43560.086	4000			2307.78	43318.4	130	Pt II	109346- 66028 K
2295.6764	43546.728	6400	Pt II	114861- 71314 K	2308.0437	43313.411	35000	Pt I	6567- 49880 E
2295.7435	43545.455	6000	Pt I	13496- 57041 N	2308.63	43302.4	61	Ne III	L
2295.8748	43542.965	2400	Pt II	32918- 76461 14	2308.73	43300.5	55		
2296.3797	43533.393	210	Pt I	10131- 53665 N	2309.07	43294.2	74		
2296.52	43530.7	53	Pd II		2309.3225	43289.427	400		
2296.64	43528.5	57			2309.87	43279.2	200		
2297.1873	43518.089	4300	Pt II	114539- 71021 K	2310.5009	43267.351	770		
2297.59	43510.5	88			2310.76	43262.5	340		
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2297.7869	43506.735		Fe I		2311.8636	43241.850	3200	Pt II	109676- 66434 K
2298.0163	43502.392	1100	Pt II	104410- 60907 K	2312.2207	43235.172	570	Pt II	114256- 71021 K
2298.1494	43499.873	1500	Pt II	109527- 66028 K	2313.0347	43219.958	4700	Pt II	21168- 64388 12
2298.3680	43495.735	2900	Pt I	18566- 62062 N	2314.21	43198.0	140	Pt II	112433- 69235 K
2298.7859	43487.830	2600	Pt I	6567- 50055 N	2315.0140	43183.009	2600	Pt II	104090- 60907 K
2299.1162	43481.583	680			2315.24	43178.8	310		
2299.2020	43479.960	1100	Pt II	109507- 66028 K	2315.5024	43173.902	14000	Pt I	13496- 56670 N
2299.4324	43475.603	2200	Pt II	119057- 75581 K	2315.71	43170.0	90		
2300.1421	43462.191		Fe I		2317.10	43144.1	74		
2300.2469	43460.21	120	Ne II		2317.2977	43140.456	1200	Pt II	114455- 71314 K
2300.38	43457.7	450	Pt I	16983- 60441 AN	2317.80	43131.1	180		
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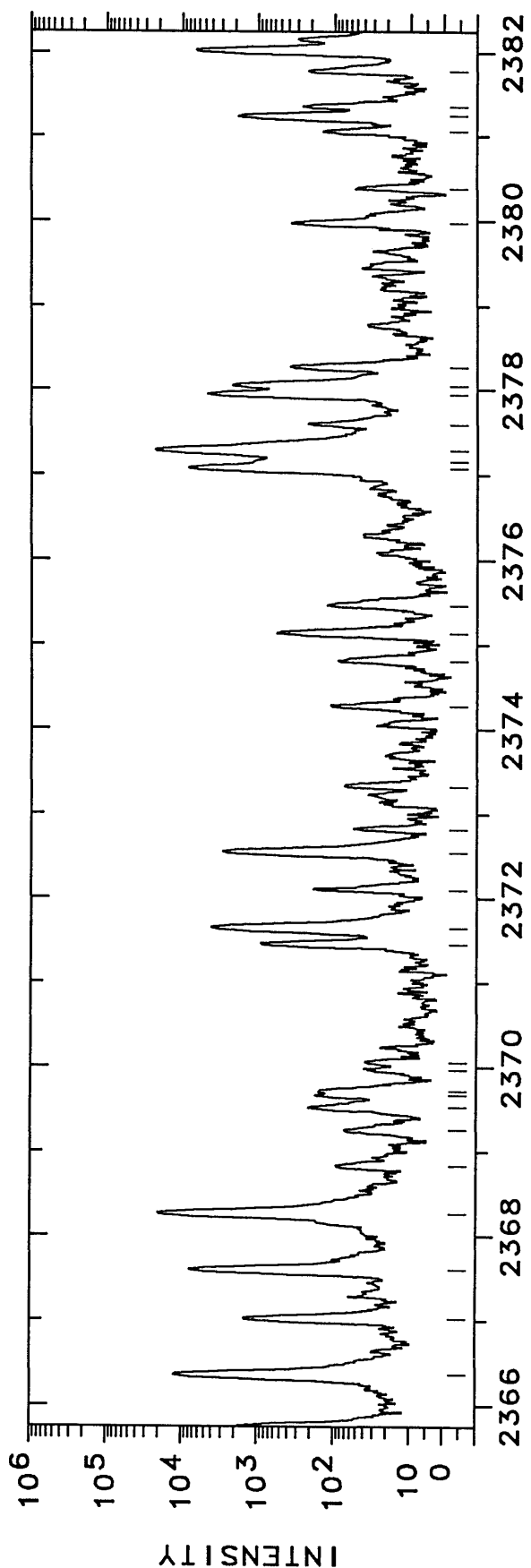
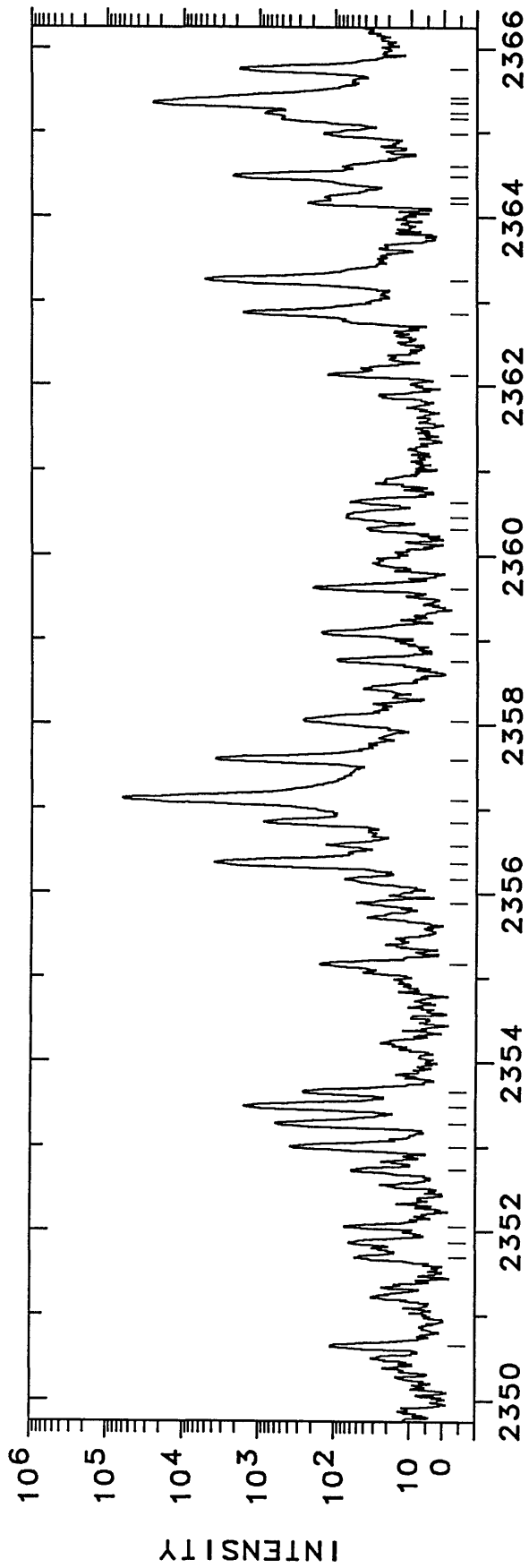


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2318.83	43112.0	54	Pt II	115060- 71948 K	2335.1888	42809.963	8800	Pt II	54373- 97183 AK
2319.01	43108.6	110	Pt II		2335.2555	42808.740	1000	Pt I	16983- 59792 N
2319.1251	43106.466	620	Pt II	114127- 71021 K	2336.09	42793.4	66		
2319.8215	43093.526	750	Pt II	109527- 66434 K	2336.40	42787.8	120		
2319.8869	43092.311	12000	Pt II	18097- 61190 06	2336.59	42784.3	53		
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2320.6133	43078.823	250	Pt I	18566- 61645 N	2338.75	42744.8	160	Pt II	121651- 78906 K
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2321.7422	43057.879	2400	Pt II	58491-101549 K	2339.3589	42733.657	2500	Pt II	58062-100795 K
2322.0304	43052.535	1100			2339.77	42728.1	90		
2323.09	43032.9	75			2340.1805	42718.654	21000	Pt I	6567- 49286 E
2323.42	43026.8	190			2340.7195	42708.819	380	Pt I	21967- 64675 N
2325.87	42981.5	110			2340.94	42704.8	72		
2326.1053	42977.122	8600	Pt I	6567- 49544 E	2341.4178	42696.082	7900	Pt II	106434- 63738 P
2326.3386	42972.812	13000	Pt II	23461- 66434 10	2341.53	42694.0	450	Pt II	53749- 96443 K
2326.4148	42971.406	750	Pt II	104636- 61665 K	2342.7732	42671.382	1100	Pt II	21717- 64388 13
2326.91	42962.3	35			2342.95	42668.2	56		
2328.0220	42941.741	780	Pt II	114256- 71314 K	2343.10	42665.4	48		
2328.57	42931.6	110	Pt II	117340- 74409 K	2343.2412	42662.861	830	Pt II	32918- 75581 13
2328.79	42927.6	150	Pt II	116689- 73761 K	2343.3952	42660.057	9500	Pt I	0- 42660 E
2328.88	42925.9	71			2343.91	42650.7	38	Pt II	60986-103637 K
2329.2862	42918.437	92	Pt II	29030- 71948 09	2344.89	42632.9	35	Pt II	50564- 93197 K
2330.07	42904.0	89			2345.15	42628.1	99		
2330.2360	42900.945	830	Pt II	24879- 67780 K	2345.56	42620.7	60		
2330.46	42896.8	38			2346.7367	42599.318	810	Pt I	15501- 58101 N
2330.9705	42887.428	3200	Pt I	10131- 53019 E	2346.97	42595.1	250	Pt II	117340- 74745 K
2331.7820	42872.503	280	Pt II	34647- 77519 13	2347.1600	42591.638	3600	Pt I	10116- 52708 N
2331.9574	42869.279	950			2348.03	42575.9	130		
2332.21	42864.6	170			2348.4833	42567.641	6000	Pt II	105388- 62820 12
2332.7994	42853.808	120	Fe II	s	2348.5456	42566.511	6600	Pt II	23461- 66028 07
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2333.48	42841.3		Pt II	58062-100903 K					



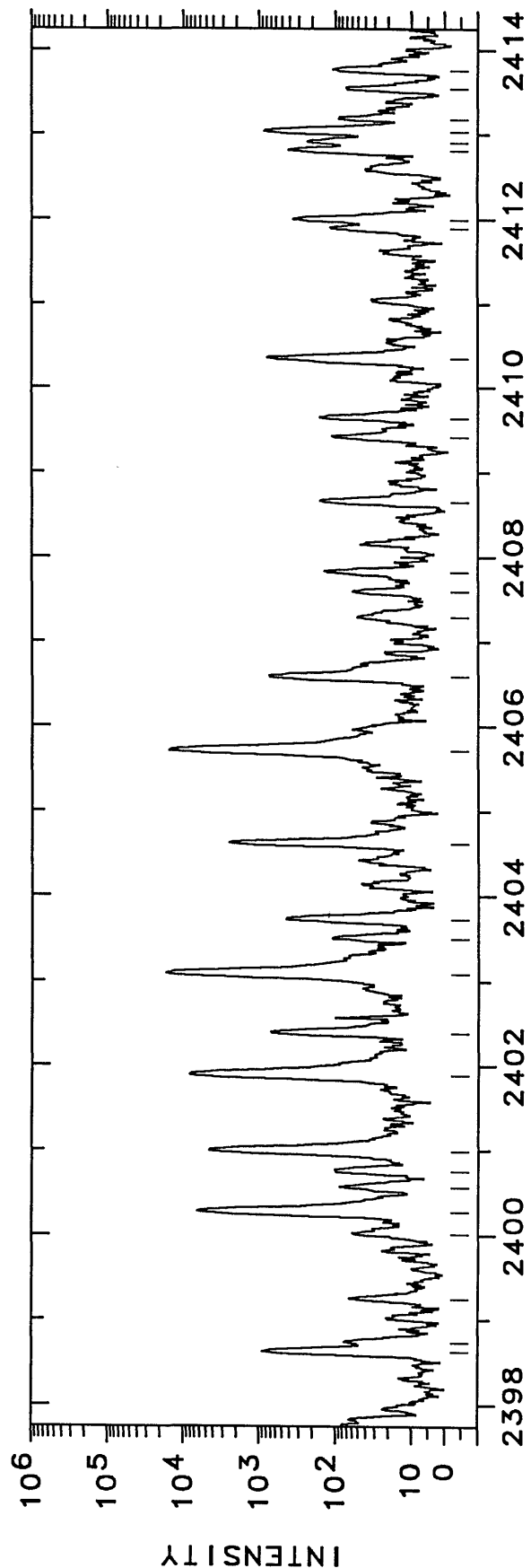
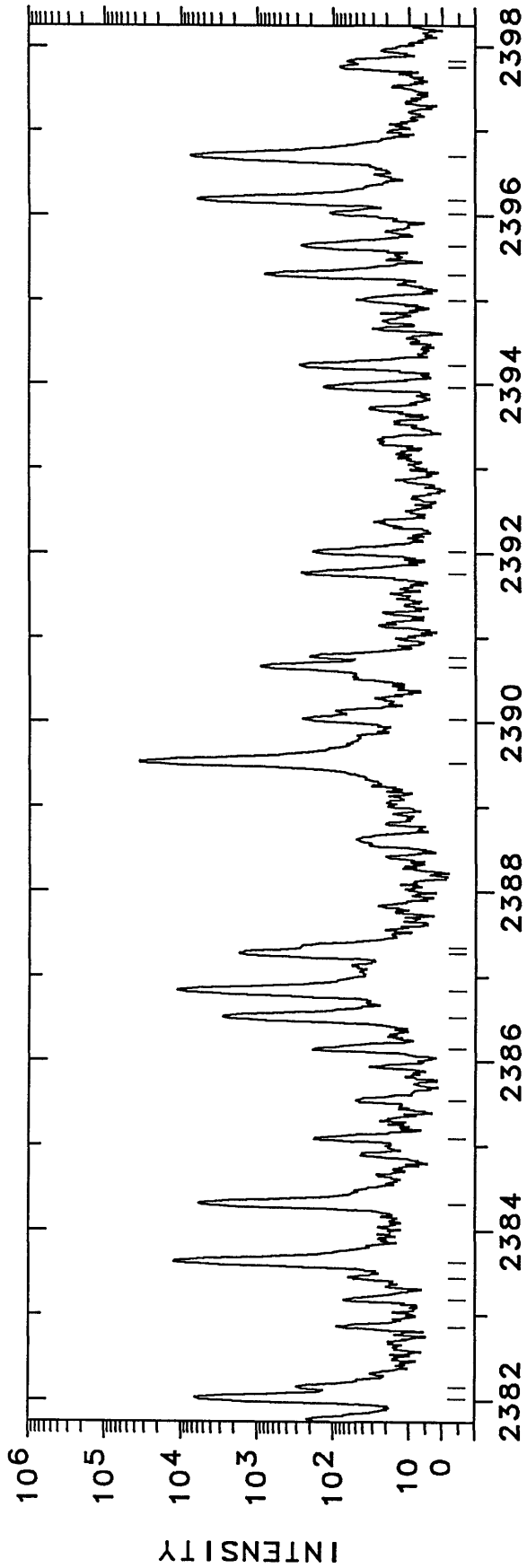
WAVELENGTH (ANGSTROMS) - AIR

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2351.69	42509.6	50			2366.3729	42245.858	13000	Pt II	105066- 62820 13
2351.86	42506.5	59			2367.0394	42233.964	1500	Ne III	L
2352.05	42503.1	69			2367.6160	42223.680	7800	Pt II	105962- 63738 K
2352.73	42490.8	56			2368.2781	42211.876	21000	Pt I	6567- 48779 E
2353.0213	42485.551	380	Pt I	15501- 57987 N	2368.83	42202.0	89		
2353.2883	42480.732	590			2369.26	42194.4	68		
2353.4916	42477.062	1600	Pt II	110257- 67780 K	2369.53	42189.6	210		
2353.65	42474.2	260			2369.67	42187.1	170		
2355.16	42447.0	160	Pt II	32918- 75365 AK	2369.72	42186.2	160		
2355.16	42447.0	160	Pt II	119057- 76610 AK	2369.97	42181.7	37		
2355.89	42433.8	49			2370.06	42180.1	35		
2356.17	42428.8	72			2371.4185	42155.980	920	Pt II	117340- 75184 K
2356.3384	42425.748	3900 L			2371.6165	42152.461	4200	Pt II	23875- 66028 11
2356.57	42421.6	130			2372.10	42143.9	180		
2356.8505	42416.531	880			2372.5390	42136.073	2900	Pt II	111371- 69235 K
2357.1047	42411.956	64000	Pt I	775- 43187 E	2372.82	42131.1	53		
2357.5804	42403.399	3800	Pt I	10116- 52520 N	2373.32	42122.2	70		
2358.04	42395.1	260			2374.27	42105.4	110		
2358.7653	42382.100	92	Pt II	32237- 74619 09	2374.8090	42095.80	86	Ne II	C
2359.08	42376.4	150			2375.13	42090.1	570		
2359.61	42366.9	200			2375.46	42084.3	120		
2360.31	42354.4	35			2377.0752	42055.671	8400	Pt II	105794- 63738 K
2360.45	42351.9	69	Pt I	21967- 64319 N	2377.1539	42054.277	900	Pt II	112433- 70379 K
2360.63	42348.6	61			2377.2773	42052.096	23000	Pt II	9356- 51408 07
2362.12	42321.9	120			2377.58	42046.7	220	Pt II	106434- 64388 K
2362.8646	42308.578	1600	Pt II	117493- 75184 K	2377.9606	42040.012	4700	Pt I	13496- 55536 E
2363.2297	42302.043	5200	Ne III		2378.0597	42038.260	2200	Pt II	43737- 85775 K
2364.16	42285.4	230			2378.2731	42034.490	380	Pt II	115060- 73026 K
2364.2318	42284.115	140	Pt II	29030- 71314 09	2379.9758	42004.419	370	Pt I	15501- 57506 A
2364.4860	42279.569	2200	Pt II	116689- 74409 K	2379.9758	42004.419	370	Pt II	32237- 74241 A
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2365.2273	42266.319	850	Pt II	32918- 75184 A	2381.2324	41982.254	1900		
2365.2273	42266.319	850	Pt II	105086- 62820 AK	2381.78	41979.978	260	Pt II	27255- 69235 15
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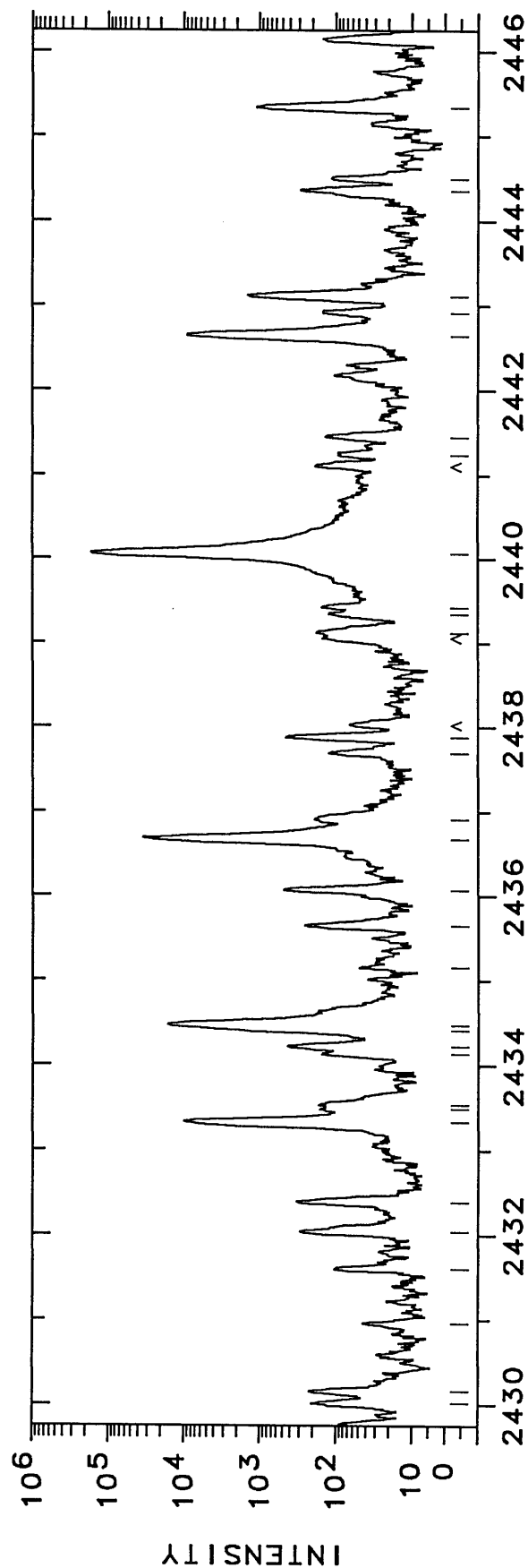
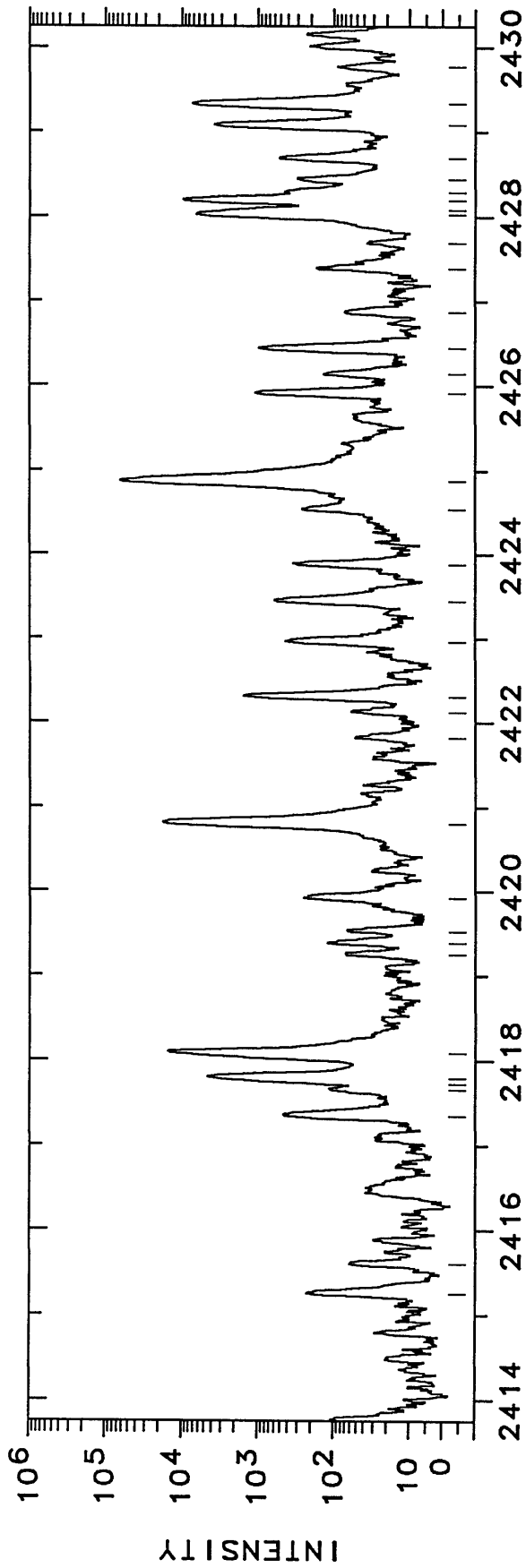
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2382.0330	41968.145	6500	Pt I	26638- 68606 AN	2399.2413	41667.158	57	Pt II	13
2382.15	41966.1	300			2400.01	41653.8	6500	Pt II	L
2382.86	41953.6	87			2400.2707	41649.289	85	Ne III	
2383.18	41947.9	69			2400.56	41644.3	100		
2383.44	41943.4	61	Pt II	116689- 74745 K	2400.75	41641.0	4700	Pt I	51753 E
2383.6432	41939.797	12000	Pt I	10131- 52071 E	2401.0033	41636.581	8500	Pt I	51753 E
2384.3213	41927.870	5900	Pt II	95803- 53875 06	2401.8773	41621.432	700	Pt II	21168- 62781 09
2385.09	41914.4	180			2402.3655	41612.974	17000	Pt I	6140- 47740 E
2385.54	41906.5	47			2403.0918	41600.398	110		
2386.15	41895.7	190	Pt II	109676- 67780 K	2403.50	41593.3	450	Pt II	104410- 62820 K
2386.5017	41889.566	2900	Pt II	23461- 65351 07	2403.7227	41589.480	2500	Pt II	105962- 64388 K
2386.8089	41884.176	11000	Pt I	775- 42660 E	2404.6239	41573.895	15000	Pt II	24879- 66434 10
2387.2596	41876.270	1700			2405.7269	41554.835	740	Pt I	15501- 57041 N
2387.3456	41874.760	250	Pt I	18566- 60441 N	2406.5926	41539.889	49		
2389.5358	41836.382	36000	Pt I	823- 42660 E	2407.29	41527.9	57		
2390.0515	41827.355	260	Pt II	32918- 74745 09	2407.59	41522.7	140		
2390.6758	41816.434	920	Pt II	104636- 62820 P	2407.82	41518.7	160	Pt II	116689- 75184 K
2390.7975	41814.305	200	Pt II	34647- 76461 15	2408.65	41504.4	110		
2391.76	41797.5	260	Pt I	16983- 58780 N	2409.41	41491.3	160		
2392.02	41792.9	180			2409.63	41487.5	780	Pt II	23875- 65351 11
2393.96	41759.1	130	Pt II	29261- 71021 K	2410.3280	41475.516	110		
2394.22	41754.5	270			2411.89	41448.7	360		
2395.00	41740.9	46			2411.99	41446.9	410	Ne III	L
2395.2985	41735.738	800	Pt II	58062- 99797 K	2412.8173	41432.731	230	Ne III	L
2395.6470	41729.668	260	Pt II	37877- 79607 17	2412.90	41431.3	850	Pt I	10116- 51545 A
2396.02	41723.2	110			2413.0462	41428.800	850	Pt II	114455- 73026 AK
2396.1705	41720.552	6000	Pt I	13496- 55216 E	2413.0462	41428.800	86	Ne III	L
2396.6869	41711.562	7400	Pt II	23875- 65587 15	2413.18	41426.5	68	Ne III	L
2397.76	41692.9	79			2413.54	41420.3	100	Ne III	L
2397.83	41691.7	62	Pt II	60986- 102678 K	2413.76	41416.5			
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WAVELENGTH (ANGSTROMS) - AIR

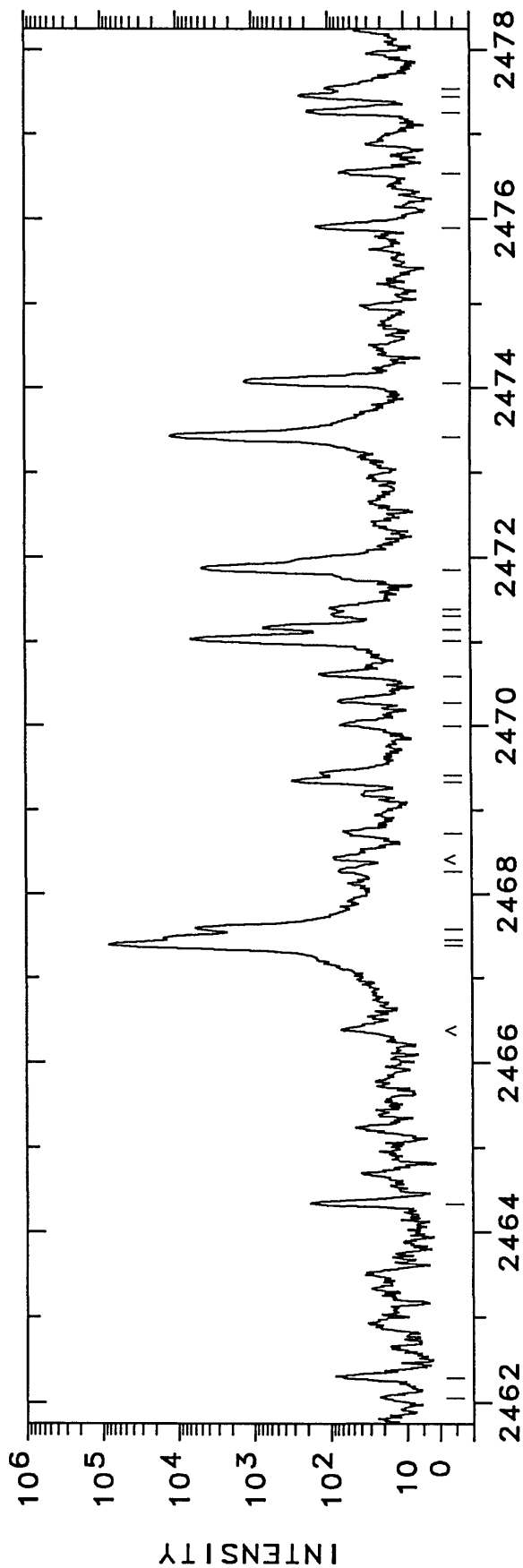
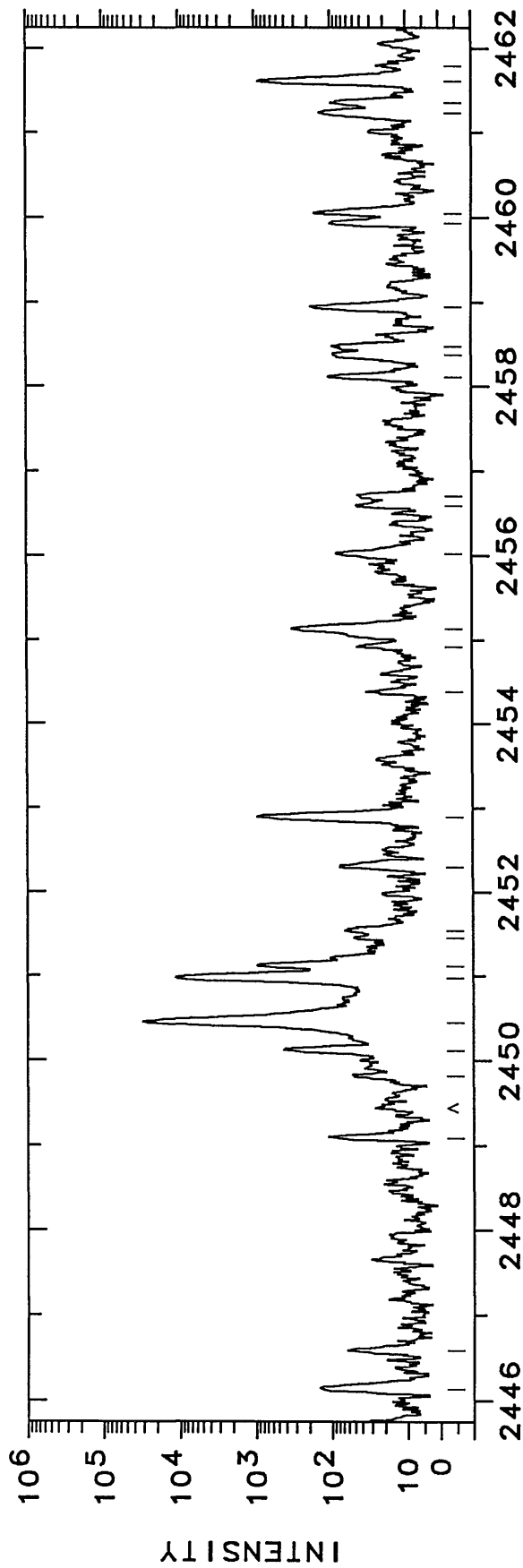
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2415.60	41385.0	57			2430.0176	41139.48	200	Ne II	C
2417.3375	41355.26	450	Ne II	C	2430.1647	41136.99	220	Ne II	C
2417.66	41349.7	110			2430.96	41123.5	37		
2417.7302	41348.544	910 U	Pt II	29030- 70379 16	2431.60	41112.7	98		
2417.7630	41347.982	4600 P	Pt II	105086- 63738 K	2432.04	41105.3	290	Pt II	50564- 91669 K
2418.0583	41342.934	15000	Pt I	13496- 54839 E	2432.39	41099.4	320	Pt II	114861- 73761 K
2419.2297	41322.918	64	Pt II	32918- 74241 10	2433.3064	41083.882	10000	Pt II	106434- 65351 P
2419.38	41320.3	120			2433.49	41080.8	160	Pt II	32918- 73999 AK
2419.52	41318.0	61			2433.49	41080.8	160	Ne II	A
2419.92	41311.1	240			2433.54	41079.9	160	Pt II	53749- 94829 K
2420.8161	41295.840	18000	Pt II	23461- 64757 08	2434.14	41069.8	150		
2421.82	41278.7	46			2434.2105	41068.624	430	Pt II	112433- 71364 K
2422.12	41273.6	53			2434.4128	41065.210	1000 P		
2422.3192	41270.216	1500	Pt II	104090- 62850 K	2434.4610	41064.398	16000	Pt II	21717- 62781 09
2422.9672	41259.18	420	Ne II	C	2435.1545	41052.705	250	Si I	B
2423.4495	41250.97	600	Ne II	C	2435.6448	41044.44	480	Ne II	C
2423.88	41243.6	340	Pt II	54373- 95617 K	2436.0764	41037.169	480	Pt II	105794- 64757 K
2424.5504	41232.24	250	Ne II	C	2436.6887	41026.858	35000	Pt I	775- 41802 E
2424.8672	41226.854	64000	Pt II	15791- 57018 05	2436.91	41023.1	180		
2425.8955	41209.380	1100	Pt II	111162- 69953 K	2437.69	41010.0	120		
2426.14	41205.2	130	Pt II	105962- 64757 K	2437.8887	41006.664	440	Pt II	58062- 99068 K
2426.4352	41200.215	950	Pt I	21967- 63167 N	2439.1180	40986.00	170	Ne II	C
2426.87	41192.8	66	Ne III		2439.34	40982.3	120		
2427.39	41184.0	160	Pt II	54373- 95557 K	2439.42	40980.9	150	Pt I	10116- 51097 N
2427.69	41178.9	30			2440.0608	40970.165	170000	Pt I	0- 40970 E
2428.0333	41173.099	6400	Pt I	6567- 47740 E	2441.24	40950.4	87		
2428.0806	41172.297	950 P	Pt II	110408- 69235 K	2441.4347	40947.11	130	Ne II	C
2428.2031	41170.220	9600	Pt I	10116- 51286 E	2442.6261	40927.139	9100	Pt II	23461- 64388 13
2428.3122	41168.370	440	Pt I	15501- 56670 N	2442.91	40922.4	140	Pt II	110158- 69235 K
2428.4520	41166.00	290	Ne II	C	2443.0933	40919.314	1400	Pt II	29261- 70181 13
2428.7069	41161.68	510	Ne II	C	2444.36	40898.1	280	Pt II	104636- 63738 K
2429.0969	41155.073	3700	Pt I	10131- 51286 E	2444.50	40895.8	110	Pt I	18566- 59462 N
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WAVELENGTH (ANGSTROMS) - AIR

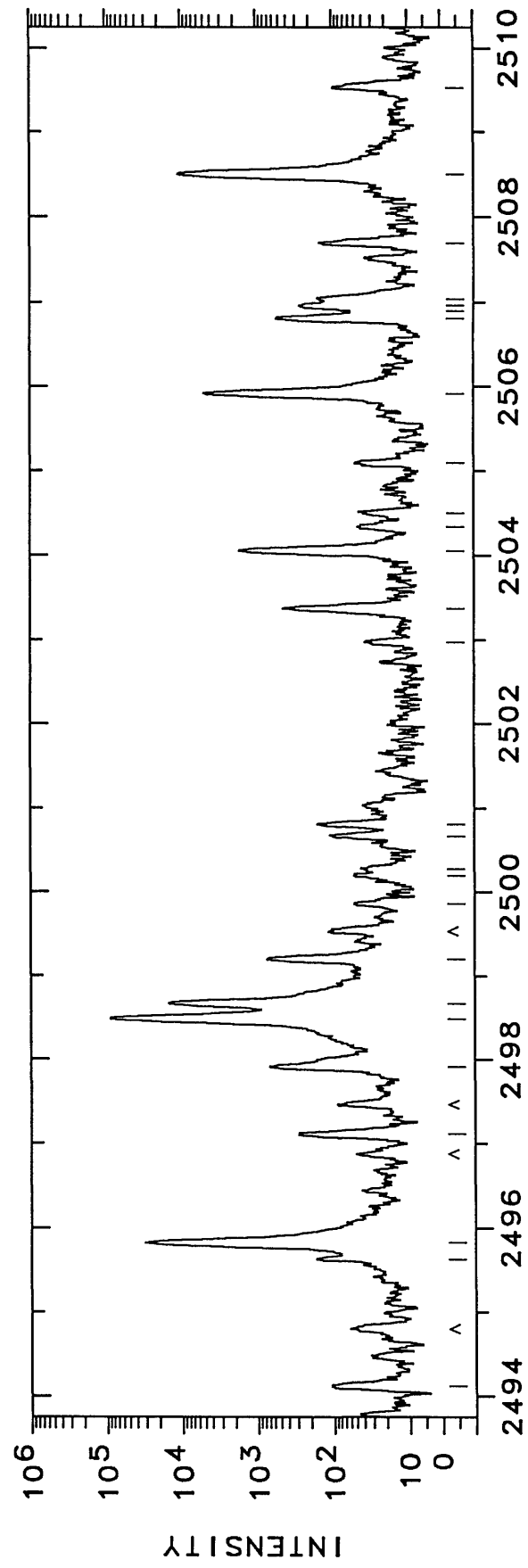
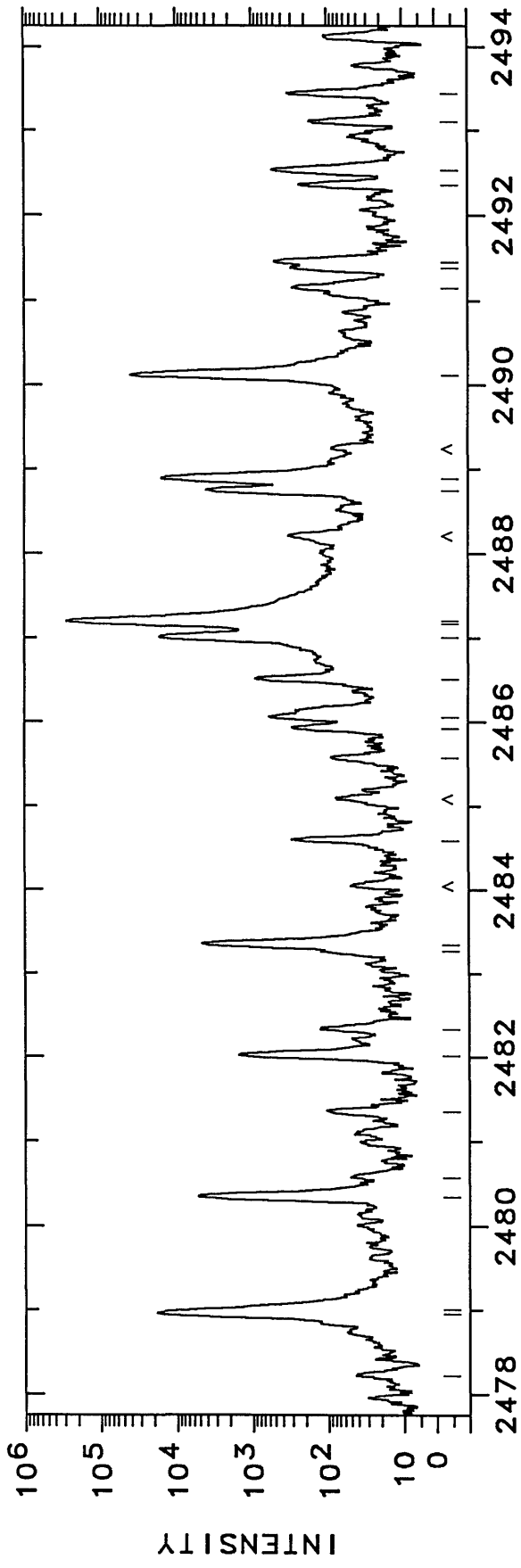


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2446.58	40861.0	57			2462.05	40604.3	16		
2449.09	40819.1	110	Pt II	115060- 74241 K	2462.29	40600.3	81	Ne III	L
2449.82	40807.0	47			2464.33	40566.7	180		
2450.12	40802.0	420			2467.4003	40516.236	80000 P	Pt I	0- 40516 E
2450.4390	40796.658	30000	Pt II	15791- 56587 06	2467.4824	40514.888	15000 P	Pt I	13496- 54011 E
2450.9670	40787.870	11000 C	Pt I	0- 40787 E	2467.5920	40513.089	5800	Pt II	23875- 64388 16
2451.1276	40785.198	940	Pt II	110020- 69235 K	2468.27	40502.0	69		
2451.45	40779.8	45			2468.72	40494.6	60	Pt II	114256- 73761 K
2451.54	40778.3	61			2469.33	40484.6	300	Pt II	112433- 71948 K
2452.30	40765.7	71			2469.41	40483.3	120	Pt I	26638- 67121 N
2452.9005	40755.722	940	Pt II	58062- 98817 K	2470.0003	40473.59	63	Ne II	
2454.38	40731.2	28			2470.27	40469.2	69	Pt II	54373- 94842 K
2454.92	40722.2	39	Ne III		2470.59	40463.9	130	Pt II	41434- 81897 K
2455.1380	40718.582	320	Pt II	34647- 75365 K	2471.0073	40457.098	6400	Pt I	13496- 53953 E
2456.02	40704.0	78			2471.1551	40454.678	700	Pt II	110408- 69953 K
2456.59	40694.5	39			2471.31	40452.1	83	Pt II	114861- 74409 K
2456.70	40692.7	38			2471.39	40450.8	88		
2458.11	40669.4	99			2471.8422	40443.433	4600	Pt II	105794- 65351 K
2458.37	40665.1	84			2473.3856	40418.199	12000	Ne III	L
2458.47	40663.4	87			2474.0576	40407.221	1300 L	Pt II	60986-101394 K
2458.94	40655.6	170			2475.89	40377.3	130	Pt II	37877- 78254 K
2459.93	40639.3	94			2476.53	40366.9	64		
2460.05	40637.3	160	Pt I	13496- 54133 N	2477.2734	40354.772	180	Pt I	21967- 62321 N
2461.2423	40617.60	130	Ne II		2477.44	40352.1	230	Pt II	104090- 63738 K
2461.35	40615.8	90			2477.5449	40350.35	100	Ne II	
2461.6167	40611.423	880	Pt II	105962- 65351 K					



WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
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2479.0091	40326.519	550 P	Pt II	58491- 98817 K	2495.63	40058.0	160	Pt I	16983- 57041 N
2480.3415	40304.858	5200	Pt II	110258- 69953 K	2495.8126	40055.032	31000	Pt I	6567- 46622 E
2480.57	40301.1	45			2497.0968	40034.434	280	Pt I	15501- 55536 N
2481.35	40288.5	100			2497.9137	40021.342	680	Pt II	21168- 61190 08
2482.0363	40277.338	1500	Pt II	23461- 63738 08	2498.4996	40011.958	89000	Pt I	775- 40787 E
2482.33	40272.6	120	Pt II	109507- 69235 K	2498.6806	40009.059	15000	Pt II	101199- 61190 07
2483.2714	40257.306		Fe I		2499.2092	40000.598	730	Pt II	106434- 66434 P
2483.3675	40255.750	4600	Pt I	10131- 50387 N	2499.86	39990.2	46		
2484.59	40235.9	290			2500.20	39984.7	47		
2485.57	40220.1	83			2500.28	39983.5	36		
2485.9312	40214.237	290	Pt I	18566- 58780 N	2500.67	39977.2	100		
2486.0694	40212.001	580			2500.81	39975.0	150	Pt I	21967- 61942 N
2486.5135	40204.819	890	Pt II	110158- 69953 K	2502.97	39940.5	31		
2486.9827	40197.236	17000	Pt II	16820- 57018 05	2503.3469	39934.487	440	Pt II	105962- 66028 K
2487.1685	40194.232	280000	Pt I	775- 40970 E	2504.0404	39923.427	1700	Pt I	10131- 50055 E
2487.1685	40194.232	280000	Pt I	0- 40194 E	2504.34	39918.7	39		
2488.7321	40168.981	4000	Pt I	13496- 53665 N	2504.50	39916.1	38		
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2491.1651	40129.754	280	Pt II	114539- 74409 K	2506.8216	39879.138	540	Pt II	110258- 70379 K
2491.38	40126.3	300	Pt II	60986- 10113 AK	2506.8973	39877.934		Si I	
2491.38	40126.3	300	Pt II	36484- 76610 A	2506.96	39876.9	260		
2491.4659	40124.909	490	Pt II	58062- 98186 K	2507.04	39875.7	150	Ne III	
2492.35	40110.7	230	Pt II	109346- 69235 K	2507.69	39865.3	140		
2492.5276	40107.819	520	Pt II	32918- 73026 12	2508.4973	39852.500	11000	Pt I	6567- 46419 E
2493.0948	40098.695	160	Pt II	34647- 74745 11	2509.53	39836.1	89	Pt II	114455- 74619 K



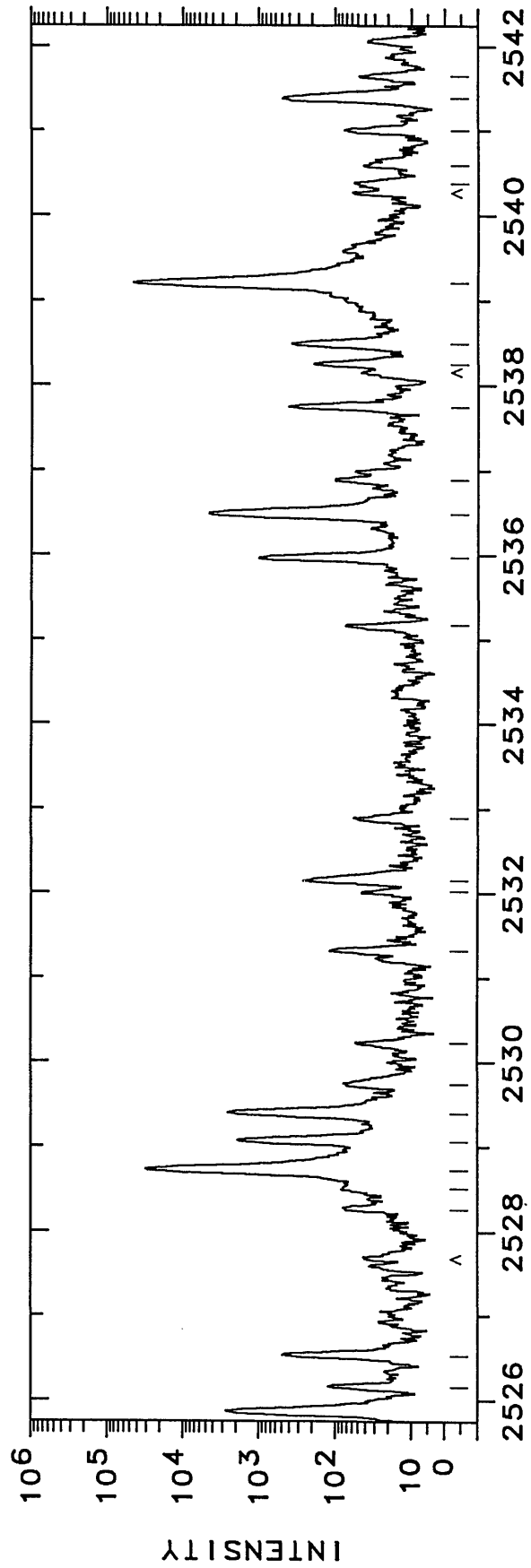
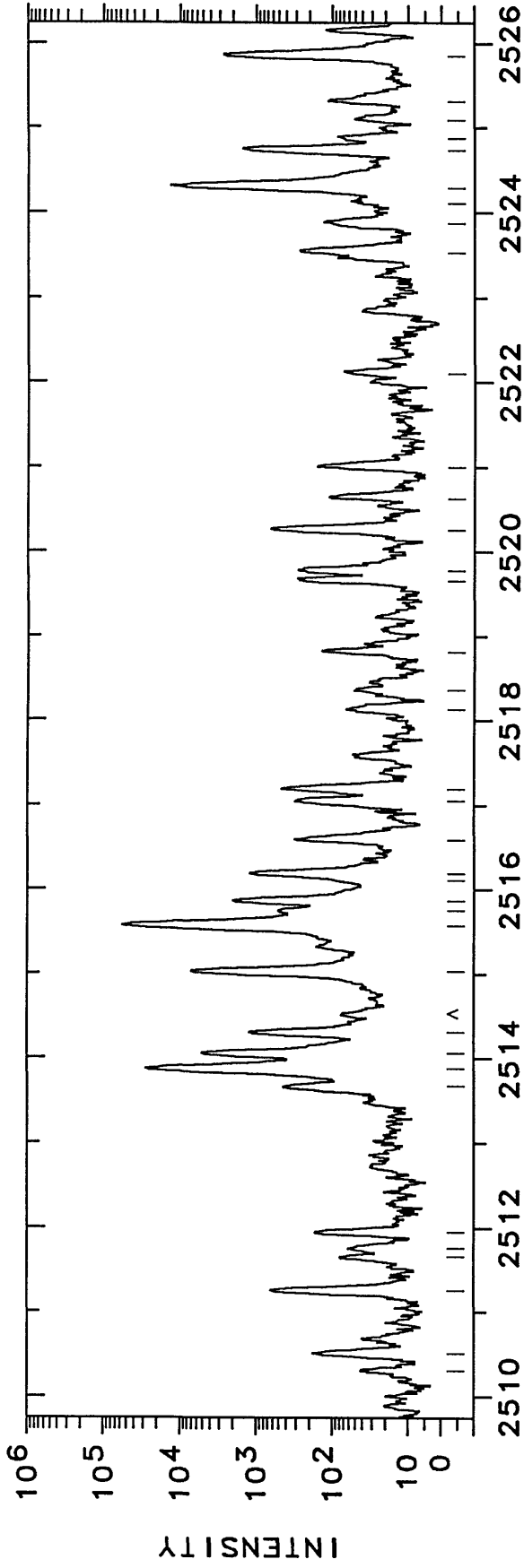
WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH INTENSITY CLASSIFICATION CODE

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2515.0305	7000	Pt I	10131- 49880 E
2515.5770	56000	Pt I	775- 40516 E
2515.7517	450		
2515.8665	2000	Pt II	105086- 65351 K
2516.1125	1200	Si I	
2516.1835	39730.770	Pt II	58062- 97792 K
2516.59	310	Pt II	58062- 97786 K
2517.05	300	Pt II	104763- 65046 K
2517.1843	450	Pt I	15501- 55216 N
2518.1079	58	Ne II	
2518.36	44		
2518.81	130		
2519.66	280		
2519.78	280		
2520.2494	630	Pt I	21967- 61633 N
2520.63	100	Pt II	37877- 77538 K
2521.00	150		
2522.10	64	Pt II	114256- 74619 K
2523.53	260	Pt II	43757- 83352 K
2523.87	120		
2524.1079	13000	Si I	
2524.3065	1500	Pt I	6567- 46170 E
2524.7341		Pt II	96614- 57018 05

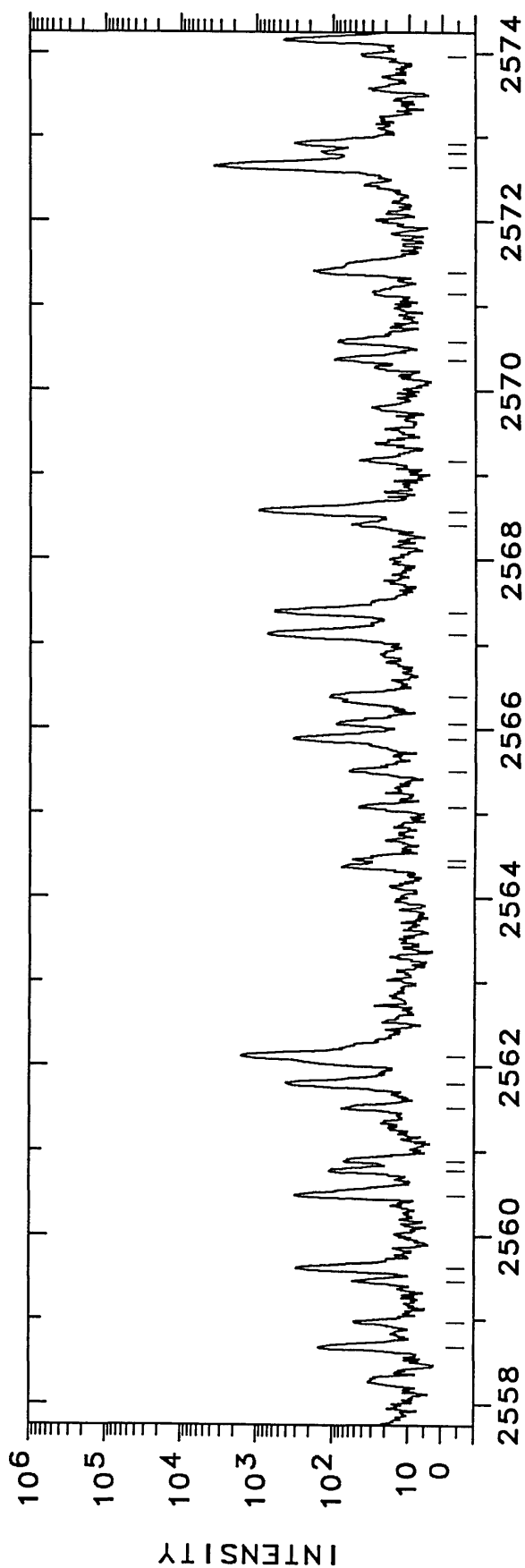
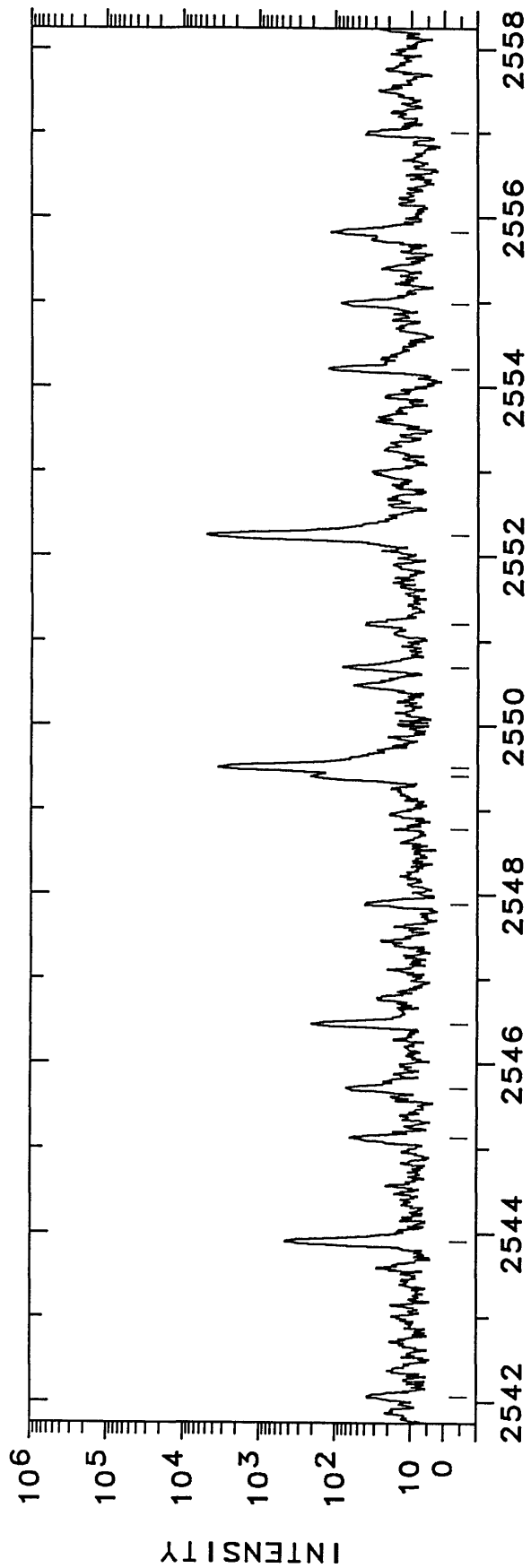
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2524.8688	78	Ne II	
2525.09	43	Pt II	104636- 65046 K
2525.31	110		
2525.8211	2700	Pt II	104930- 65351 K
2526.15	110	Pt II	109527- 69953 K
2526.5031	480	Pt II	58062- 97630 K
2528.26	71		
2528.5086	39541.0	Si I	
2528.7336	39537.117	Pt II	101199- 61665 B
2529.0806	30000	Pt II	105962- 66434 05
2529.4100	1900	Pt II	105962- 66434 K
2529.74	2500	Pt I	13496- 53019 E
2530.23	69		
2530.23	46	Ne II	
2531.32	46	Pt II	114256- 74745 AK
2532.02	110		
2532.1535	37		
2532.89	260	Ne II	
2535.17	50		
2535.9677	67		
2536.4932	1000	Pt I	18566- 57987 E
2536.89	4500	Pt I	10131- 49544 E
2537.7612	93		
2538.25	410	Pt II	109346- 69953 K
2538.5033	180	Pt I	21967- 61352 N
2538.5033	360	Pt II	114127- 74745 AK
2539.2067	360	Ne II	
2540.38	46000	Pt I	823- 40194 E
2540.59	49	Pt II	34647- 73999 K
2541.00	36		
2541.00	69	Pt II	104930- 65587 K
2541.3494	480	Pt I	15501- 54839 N
2541.65	42		



WAVELENGTH (ANGSTROMS) - AIR

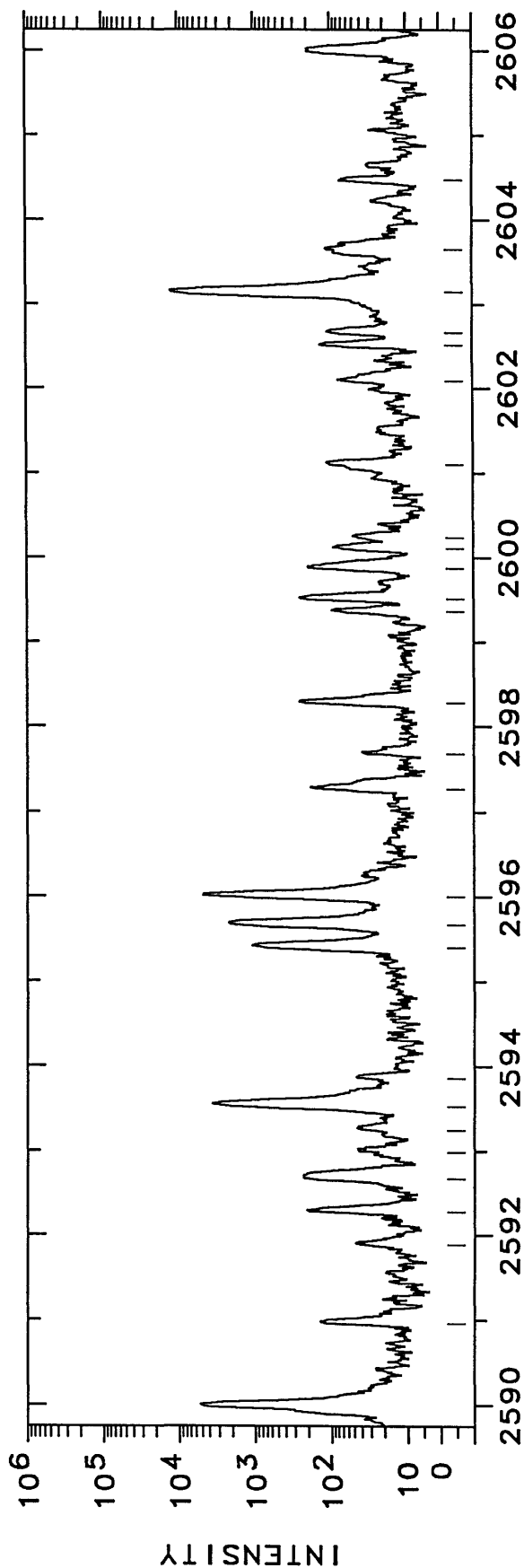
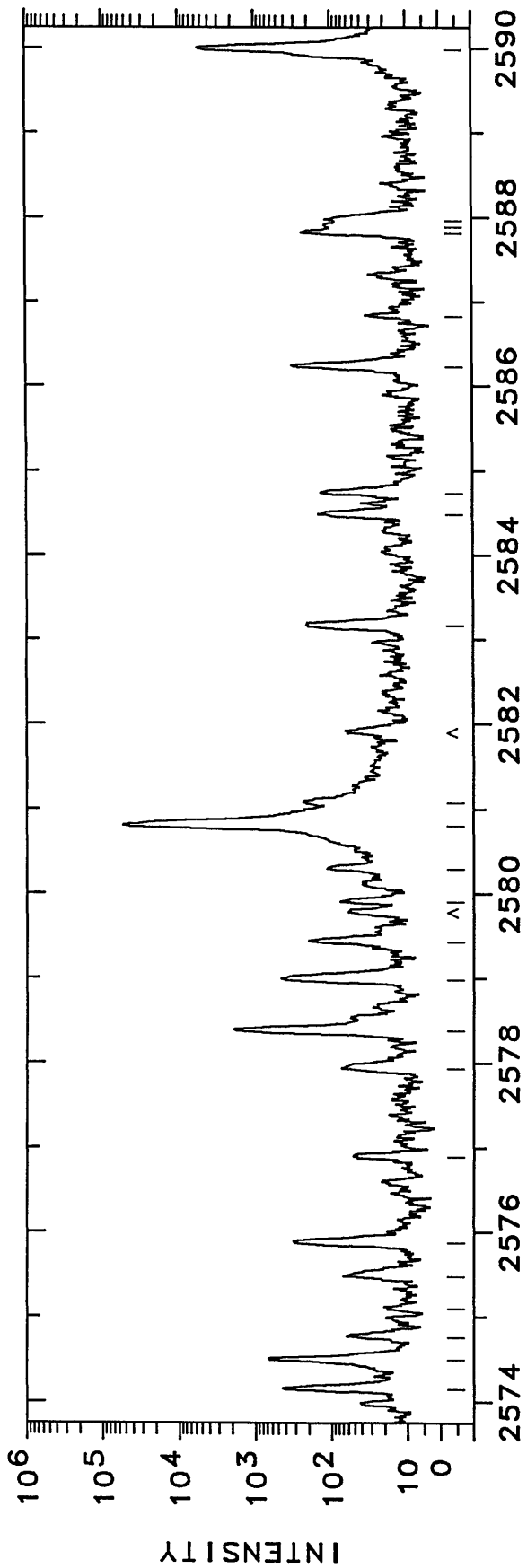
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2542.06	39326.4	30	Pt II	117340- 78043 K	2560.88	39037.4	61		
2543.9076	39297.803	440			2561.51	39027.8	67		
2545.13	39278.9	56			2561.7989	39023.37	390	Ne II	C
2545.71	39270.0	63	Pt II	114455- 75184 K	2562.1226	39018.44	1600	Ne II	C
2546.4674	39258.302	200	Pt I	6140- 45398 N	2564.37	38984.2	69		
2547.89	39236.4	34	Pt II	110257- 71021 K	2564.45	38983.0	47		
2548.78	39222.7	10			2565.07	38973.6	39		
2549.40	39213.1	210			2565.50	38967.1	54	Pt II	109346- 70379 K
2549.4688	39212.088	3500	Pt I	13496- 52708 A	2565.8574	38961.65	330	Ne II	C
2549.4688	39212.088	3500	Pt I	26638- 65850 AN	2566.06	38958.6	84	Pt II	121651- 82692 K
2550.69	39193.3	75			2566.3736	38953.814	100	Pt II	105388- 66434 17
2551.20	39185.5	34			2567.1244	38942.422	720	Ne II	
2552.2488	39169.380	5000	Pt I	10116- 49286 E	2567.3836	38938.49	590	Ne II	C
2554.21	39139.3	120	Pt II	58491- 97630 K	2568.40	38923.1	50		
2554.98	39127.5	79	Pt II	32237- 71364 K	2568.5760	38920.415	950	Pt II	18097- 57018 06
2555.8288	39114.518	110	Pt II	34647- 73761 16	2569.16	38911.6	38		
2557.00	39096.6	33			2570.36	38893.4	90	Pt II	110258- 71364 K
2558.67	39071.1	140	Pt II	114256- 75184 K	2570.57	38890.2	79	Pt II	114256- 75365 K
2558.97	39066.5	44			2571.14	38881.6	23	Pt II	36484- 75365 K
2559.45	39059.2	46	Pt I	26638- 65697 N	2571.39	38877.8	170	Pt II	113119- 74241 K
2559.61	39056.7	290	Pt II	64003-103060 K	2572.6119	38859.361	3700	Pt II	24879- 63738 08
2560.4897	39043.322	300	Pt II	110408- 71364 AK	2572.81	38856.4	140		
2560.4897	39043.322	300	Pt II	50564- 89607 AK	2572.9020	38854.98	310	Ne II	C
2560.77	39039.0	100			2573.96	38839.0	35		



WAVELENGTH (ANGSTROMS) - AIR

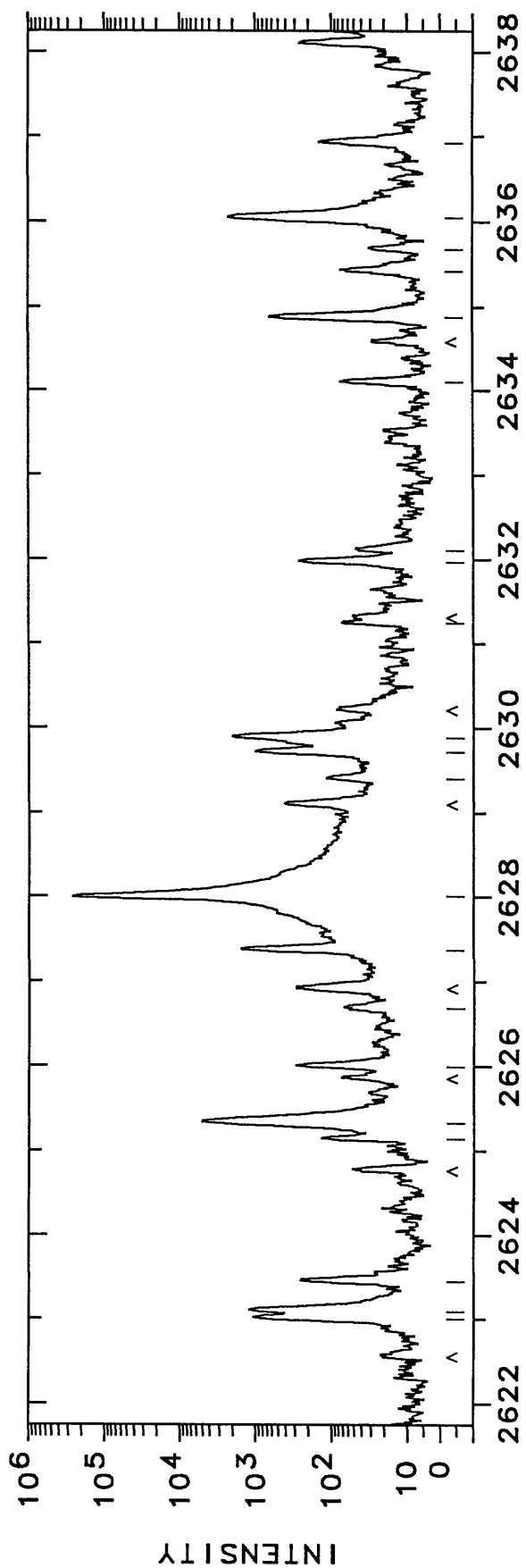
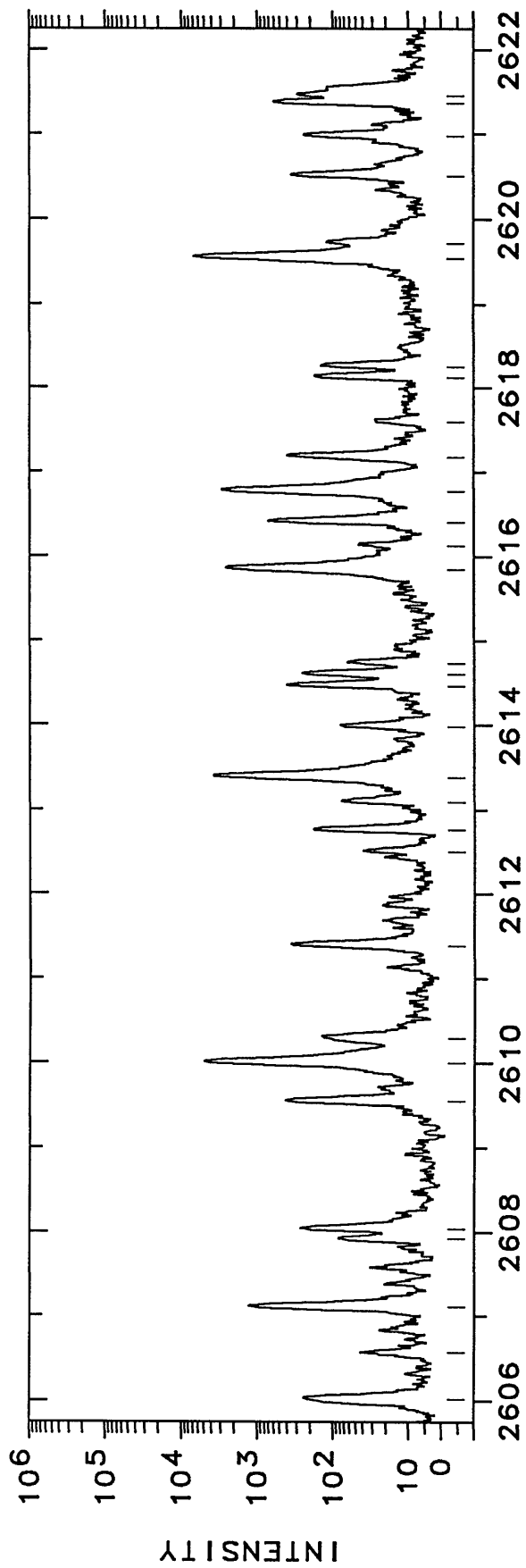


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2574.4904	38831.008	680	Pt I	6567- 45398	2592.27	38564.7	200		
2574.76	38826.9	58	Pt II	42031- 80858	2592.67	38558.7	230		
2575.0945	38821.900		Al I		2592.99	38554.0	38		
2575.47	38816.2	63	Pt I	0- 38815	2593.25	38550.1	38		
2575.87	38810.2	320			2593.5555	38545.581	3700	Ne III	L
2576.89	38794.9	46			2593.86	38541.1	40		
2577.9221	38779.32	67	Ne II		2595.3814	38518.466	1100	Pt II	29261- 67780
2578.3871	38772.327	1900	Pt II	27255- 66028	2595.6498	38514.483	2300	Ne III	L
2578.9887	38763.284	460	Pt II	41434- 80197	2595.9986	38509.308	4900	Pt I	15501- 54011
2579.4082	38756.98	190	Ne II		2597.27	38490.5	180	Ne III	L
2579.90	38749.6	70	Pt II	29030- 67780	2597.68	38484.4	32	Pt II	60986- 99471
2580.29	38743.7	110			2598.3020	38475.172	260	Pt I	18566- 57041
2580.8102	38735.926	55000	Pt II	101517- 62781	2599.36	38459.5	90	Pt II	110408- 71948
2581.0549	38732.254	230	Pt II	37877- 76610	2599.5423	38456.816	250	Pt I	21967- 60423
2583.1494	38700.852	210	Pt II	36484- 75184	2599.9043	38451.461	200	Pt I	15501- 53953
2584.48	38680.9	140			2600.11	38448.4	86		
2584.73	38677.2	130			2600.24	38446.5	44	Pt II	32918- 71364
2586.22	38654.9	320	Pt II	109676- 71021	2601.10	38433.8	110	Pt II	112433- 73999
2586.82	38645.9	27	Pt I	116689- 78043	2602.09	38419.2	73	Pt I	10116- 48535
2587.7936	38631.401	230	Pt I	15501- 54133	2602.51	38413.0	130		
2587.886	38630.02	110	Ne II		2602.66	38410.8	100		
2587.960	38628.92	110	Ne II		2603.1374	38403.708	13000	Pt I	10131- 48535
2589.9962	38598.550	5400	Ne III		2603.6578	38396.032	110	Pt II	32918- 71314
2590.96	38584.2	130			2604.47	38384.1	67		



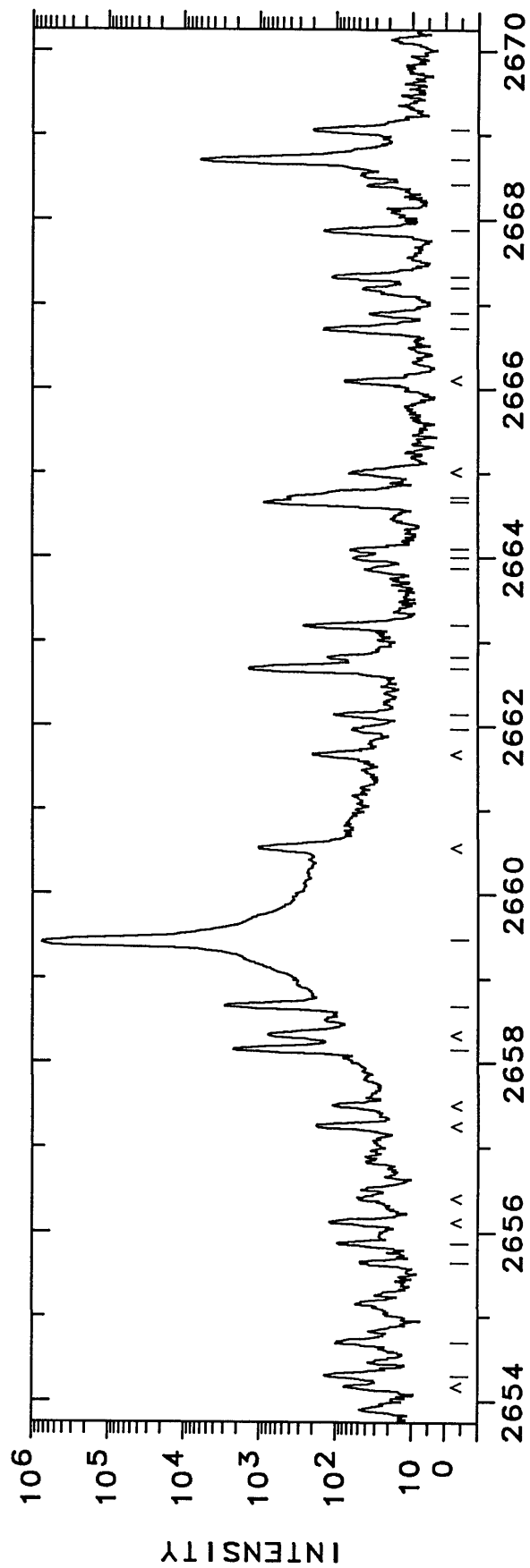
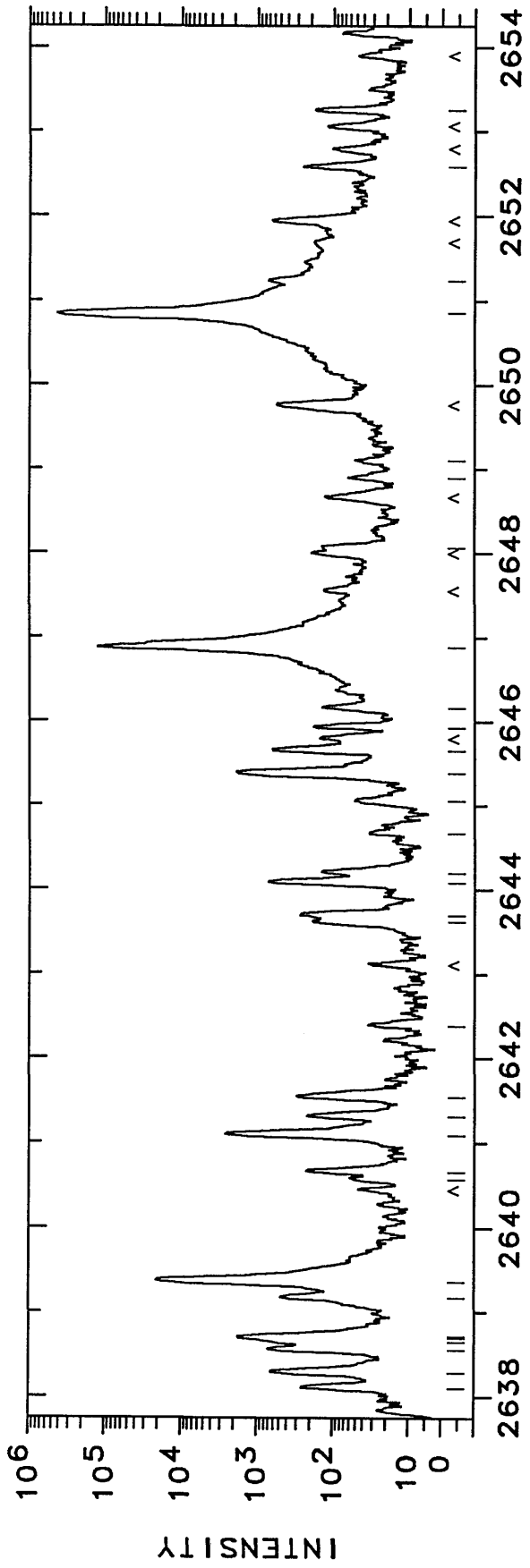
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WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
2606.02	38361.2	240	Pt I	21967- 60328 N	2619.5674	38162.854	6700	Pt I	6567- 44730 E
2606.57	38353.1	38			2619.72	38160.6	110	Pt II	43737- 81897 K
2607.1001	38345.339	1300	Pt II	111371- 73026 K	2620.5386	38148.71	350	Ne II	
2607.92	38333.3	80			2620.9986	38142.016	230	Pt II	32237- 70379 19
2608.0449	38331.449	260	Pt II	27255- 65587 A	2621.3906	38136.312	600	Pt II	111162- 73026 K
2608.0449	38331.449	260	Ne II		2621.4754	38135.079	290	Pt II	36484- 74619 11
2609.5560	38309.253	420	Pt II	110258- 71948 K	2623.0193	38112.633	1100	Pt II	121651- 83538 K
2610.0069	38302.636	5000	Ne III		2623.1070	38111.36	1200	Ne II	
2610.3051	38298.26	140	Ne II		2623.4567	38106.28	250	Ne II	
2611.4088	38282.075	360	Ne III		2625.14	38081.8	130	Pt II	64003-102086 AK
2612.50	38266.1	35	Pt I	26638- 64904 N	2625.14	38081.8	130	Pt II	60986- 99068 AK
2612.76	38262.3	180			2625.3264	38079.143	5100	Pt II	13329- 51408 06
2613.09	38257.4	72	Pt I	13496- 51753 N	2625.9859	38069.58	290	Ne II	
2613.4164	38252.669	3700	Ne III		2626.68	38059.5	64		
2613.98	38244.4	75			2627.3883	38049.262	1600	Pt I	13496- 51545 E
2614.4727	38237.215	410	Ne III		2628.0269	38040.016	270000	Pt I	775- 38815 E
2614.60	38235.4	250	Pt I	10116- 48551 N	2629.40	38020.2	110		
2614.73	38233.5	60	Pt I	16983- 55216 N	2629.7211	38015.51	1000	Ne II	
2615.8502	38217.080	2600	Ne III		2629.8858	38013.13	2000	Ne II	
2616.13	38213.0	40	Pt II	109527- 71314 K	2631.24	37993.6	68	Pt II	114455- 76461 K
2616.3865	38209.247	710	Pt II	110158- 71948 K	2631.9686	37983.05	260	Ne II	
2616.7471	38203.982	2900	Pt II	23461- 61665 07	2632.11	37981.0	43	Pt I	26638- 64619 N
2617.17	38197.8	400	Pt II	110146- 71948 K	2634.10	37952.3	69		
2617.59	38191.7	22	Pt II	112433- 74241 K	2634.8852	37941.009	640	Pt II	24879- 62820 08
2618.12	38183.9	170			2635.42	37933.3	69		
2618.25	38182.1	140	Pt II	105962- 67780 K	2635.68	37929.6	26	Ne III	
2619.5353	38163.322	600	Pt I	1501- 53665 AN	2636.0734	37923.907	2200 S	Ne II	
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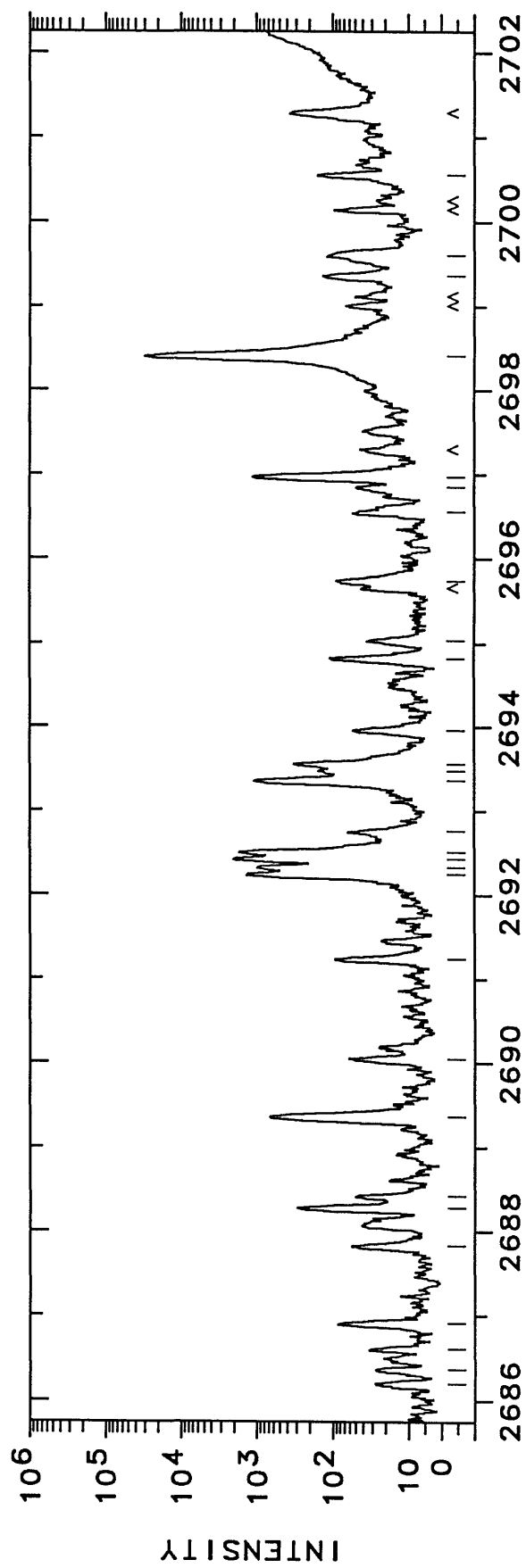
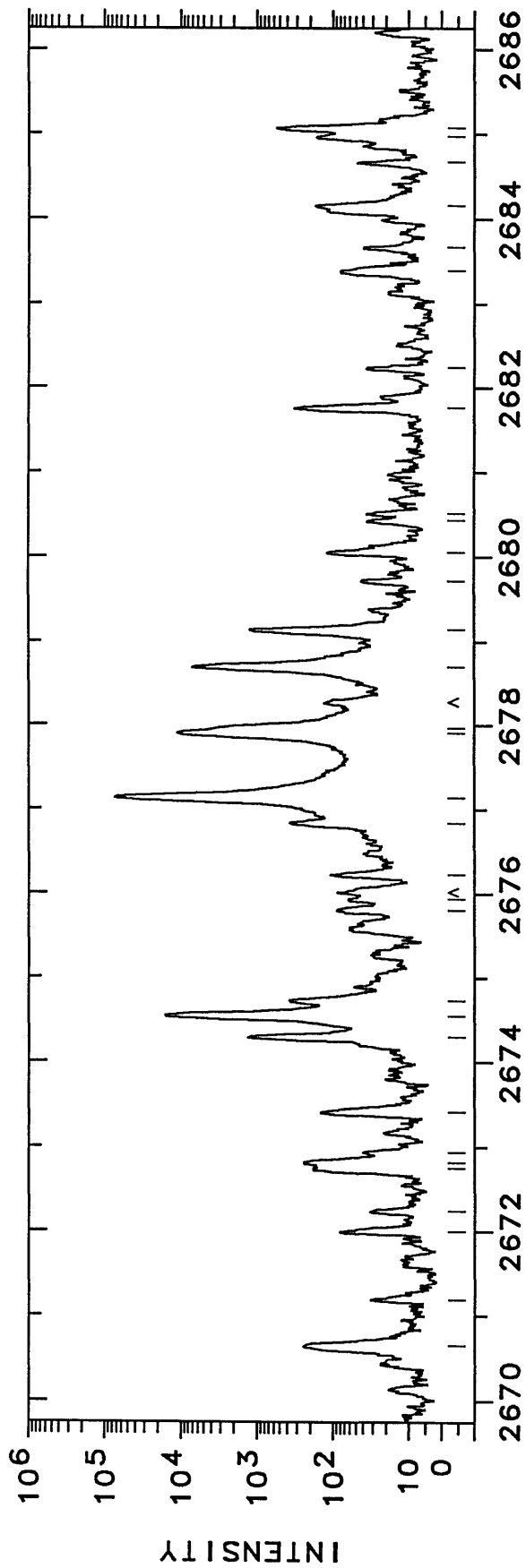
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2638.0969	37894.82	260	Ne II	C	2649.10	37737.4	47	Pt I	823- 38536 E
2638.2912	37892.03	650	Ne II	C	2650.8524	37712.487	430000	Ne II	
2638.5593	37888.180	710	Ne II		2651.2572	37706.73	720	Ne II	
2638.6418	37886.995	480			2652.5953	37687.71	250	Ne II	
2638.6949	37886.233	710 U			2653.25	37678.4	170	Pt II	112433- 74754 K
2638.7081	37886.044	1100 P	Pt II	117493- 79607 AK	2654.3075	37663.40	130	Ne II	
2638.7081	37886.044	1100 P	Ne III	AL	2654.69	37658.0	94	Pt II	41434- 79092 K
2639.1678	37879.445	480	Ne III	L	2655.64	37644.5	42		
2639.3454	37876.896	26000	Pt I	6567- 44444 A	2655.87	37641.2	88		
2639.3454	37876.896	26000	Pt I	26638- 64515 A	2658.1694	37608.684	2200	Pt I	10131- 47740 E
2640.57	37859.3	56	Ne III	L	2658.6943	37601.260	2900	Pt I	13496- 51097 E
2640.6629	37858.00	220	Ne II	C	2659.4503	37590.571	770000	Pt I	0- 37590 E
2641.0821	37851.990	2600	Ne III	L	2661.97	37555.0	56		
2641.31	37848.7	220			2662.14	37552.6	99		
2641.5274	37845.61	300	Ne II	C	2662.6599	37545.262	1400	Pt II	64003-101549 K
2642.39	37833.3	29	Ne III	L	2662.82	37543.0	120		
2643.6259	37815.57	190	Ne II	C	2663.20	37537.6	260		
2643.69	37814.7	270	Pt II		2663.87	37528.2	36		
2643.69	37814.7	270	Ne II	112433- 74619 AK	2664.00	37526.4	54		
2644.0965	37808.84	710	Ne II	A	2664.10	37525.0	59	Pt I	21967- 59492 N
2644.20	37807.4	140		C	2664.6346	37517.439	870	Pt I	15501- 53019 E
2644.67	37800.6	28			2664.6996	37516.525	300		
2645.05	37795.2	46	Pt II	114256- 76461 K	2666.72	37488.1	140	Pt II	37877- 75365 K
2645.3682	37790.666	1900	Pt I	13496- 51286 E	2666.72	37485.40	31	Ne II	
2645.6438	37786.729	620	Ne II		2667.20	37481.4	39		
2645.93	37782.6	180	Pt II	116689- 78906 K	2667.33	37479.5	110		
2646.1739	37779.16	140	Ne II	C	2667.8866	37471.71	140	Ne II	
2646.8804	37769.077	130000	Pt I	0- 37769 E	2668.42	37464.2	34		
2648.06	37752.3	130			2668.7033	37460.244	6100	Pt II	101199- 63738 08
2648.89	37740.4	58			2669.0563	37455.29	190	Ne II	C



WAVELENGTH (ANGSTROMS) - AIR

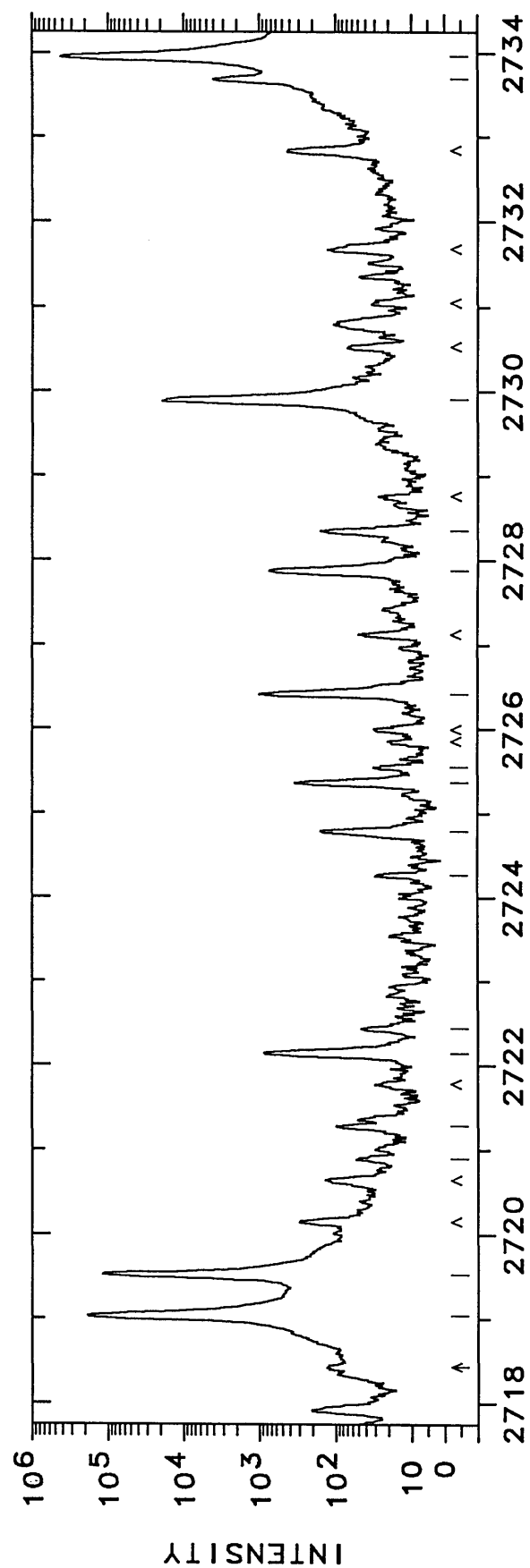
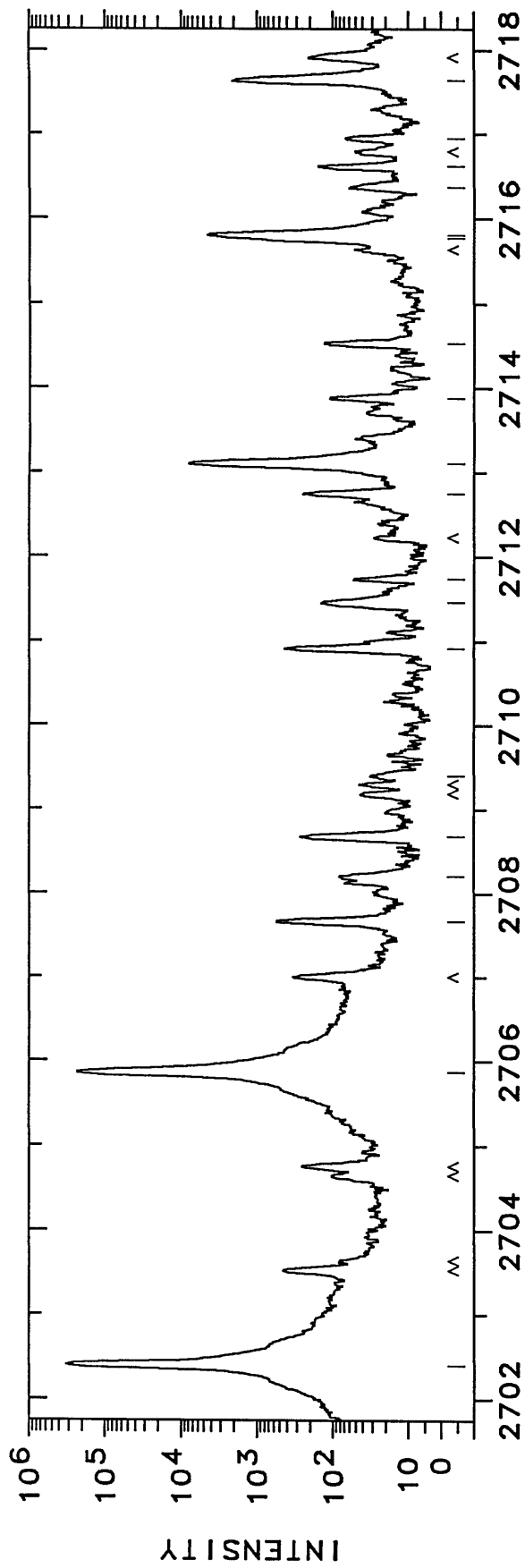
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2671.19	37425.4	27			2686.20	37216.3	23		
2672.00	37414.0	76			2686.37	37213.9	22		
2672.24	37410.7	28			2686.61	37210.6	28		
2672.7281	37403.837	180	Pt II	29030- 66434 13	2686.91	37206.4	79	Pt I	15501- 52708 N
2672.82	37402.6	230			2687.83	37193.7	51		
2672.94	37400.9	35	Pt II	111162- 73761 AK	2688.28	37187.5	290	Pt I	26638- 63826 N
2673.42	37394.2	140	Ne II	A	2688.42	37185.5	45		
2673.42	37394.2	140	Ne II	A	2689.3733	37172.348	670 L	Pt II	29261- 66434 13
2674.3124	37381.680	1300	Pt II	64003-101397 K	2690.05	37163.0	56	Pt II	111162- 73999 K
2674.5700	37378.079	13000	Pt I	110408- 73026 K	2691.24	37146.6	88		
2674.7524	37375.53	370	Ne II	6567- 43945 E	2692.2265	37132.955	1400	Pt II	27255- 64388 18
2675.81	37360.8	84		C	2692.3116	37131.781	980	Pt II	110158- 73026 K
2675.94	37358.9				2692.4255	37130.211	2000 L	Pt II	111371- 74241 AK
2676.2411	37354.74	100	Au I		2692.4255	37130.211	2000 L	Ne II	
2676.84	37346.4	360	Ne II	43737- 81083 K	2692.5154	37128.971	1700	Pt II	101517- 64388 K
2677.1477	37342.092	73000	Pt I	0- 37342 E	2692.76	37125.6	57		
2677.9046	37331.537	11000	Ne III	L	2693.3555	37117.39	1100	Ne II	C
2677.9694	37330.634	2300	Ne III	L	2693.48	37115.7	150		
2678.6908	37320.581	6900	Ne III	L	2693.5391	37114.86	320	Ne II	C
2679.1293	37314.473	1200	Pt II	23875- 61190 13	2693.96	37109.1	48	Pt II	48591- 85700 K
2679.72	37306.2	37	Pt II	105086- 67780 K	2694.8186	37097.24	100	Ne II	C
2680.0471	37301.695	110	Pt II	34647- 71948 13	2695.04	37094.2	30		
2680.43	37296.4	30	Pt II	54373- 91669 K	2695.7211	37084.82	82	Ne II	C
2680.51	37295.3	31			2696.55	37073.4	49		
2681.7715	37277.711	310	Pt II	36484- 73761 18	2696.85	37069.3	43		
2682.24	37271.2	31			2696.9844	37067.450	1100	Pt II	112433- 75365 K
2683.3985	37255.11	75	Ne II	C	2698.4248	37047.665	30000	Pt I	6140- 43187 E
2683.67	37251.3	34			2699.3655	37034.756	130	Pt II	32918- 69953 10
2684.1572	37244.58	170	Ne II	C	2699.61	37031.4	110	Ne III	L
2684.67	37237.5	42			2700.56	37018.4	150	Pt II	41434- 78452 K
2684.9769	37233.21	160	Ne II	C					



WAVELENGTH (ANGSTROMS) - AIR

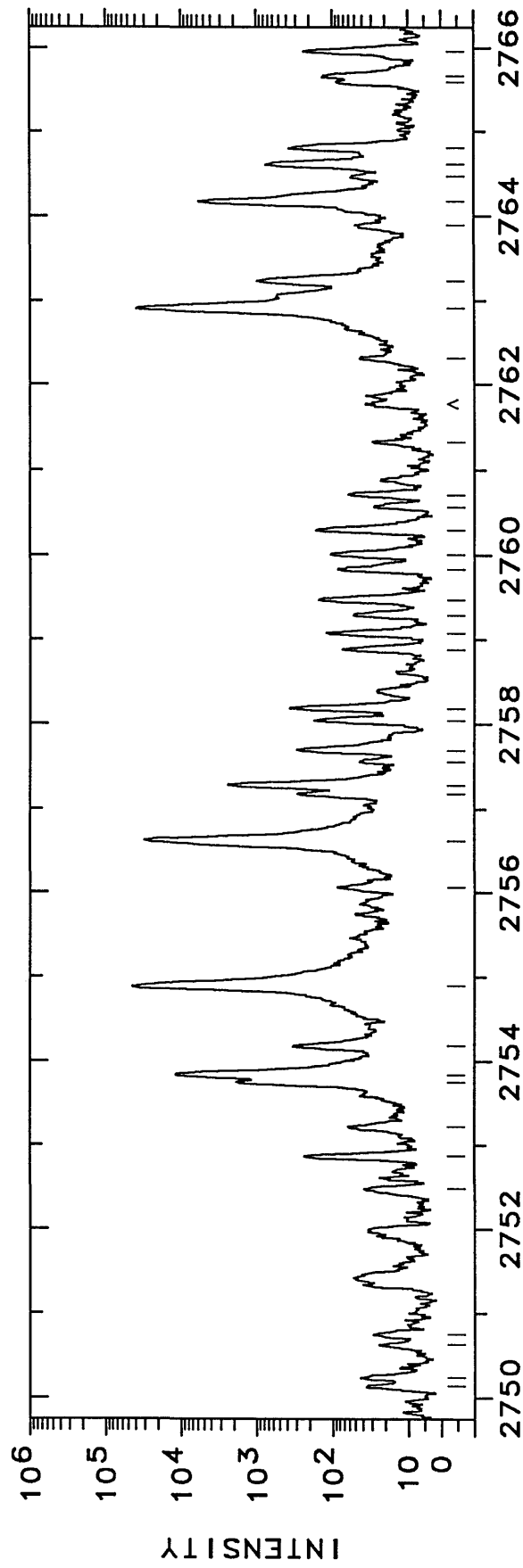
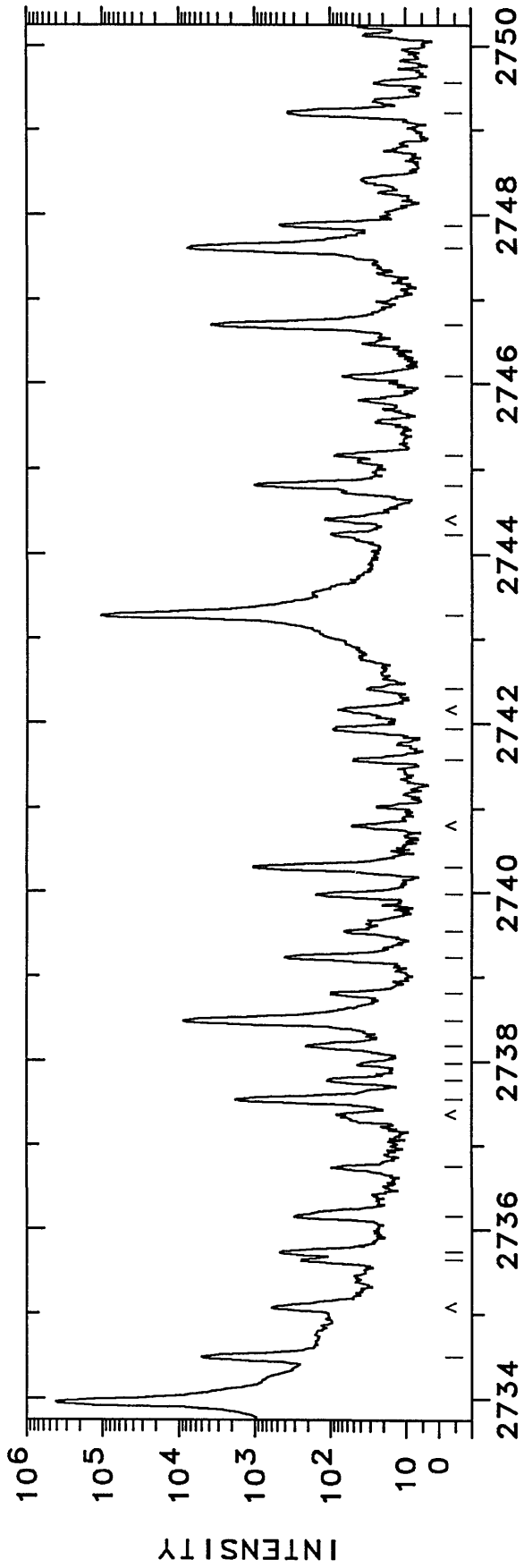


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2702.3995	36993.178	330000	Pt I	775- 37769	E	2717.6199	36786.005	Pt II	24879- 61665	06
2705.8951	36945.391	240000	Pt I	823- 37769	E	2718.4363	36774.958	Fe I		MR
2707.6694	36921.183	550	Pt II	111162- 74241	K	2719.0333	36766.883	Pt I	823- 37590	E
2708.21	36913.8	76				2719.5239	36760.251	Pt II	101517- 64757	K
2708.68	36907.4	260				2720.9024	36741.628	Fe I		R
2709.40	36897.6	27	Pt II	54373- 91271	K	2721.29	36736.4	Pt II	114256- 77519	K
2710.9114	36877.031	420	W	37877- 74754	23	2722.1611	36724.64	Ne II		C
2711.4534	36869.66	140			C	2722.44	36720.9			
2711.7322	36865.87	48	Ne II		C	2724.27	36696.2			
2712.75	36852.0	240	Pt II	112433- 75581	K	2724.79	36689.2			
2713.1254	36846.940	7900	Pt I	10116- 46963	N	2725.37	36681.4			
2713.8944	36836.50	110	Ne II		C	2725.55	36679.0	Pt I	16983- 53665	N
2714.53	36827.9	130	Pt I	26638- 63466	N	2726.4128	36667.373			
2715.7683	36811.084	800	P	6967- 30156	N	2727.8956	36647.444	Pt II	34647- 71314	13
2715.8156	36810.443	4500		101199- 64388	16	2728.35	36641.3			
2716.37	36802.9	56				2729.9123	36620.372	Pt I	6567- 43187	E
2716.62	36799.5	150		60986- 97786	K	2733.6855	36569.829	Pt I	15501- 52071	E
2716.95	36795.1	64				2733.9567	36566.201	Pt I	775- 37342	E



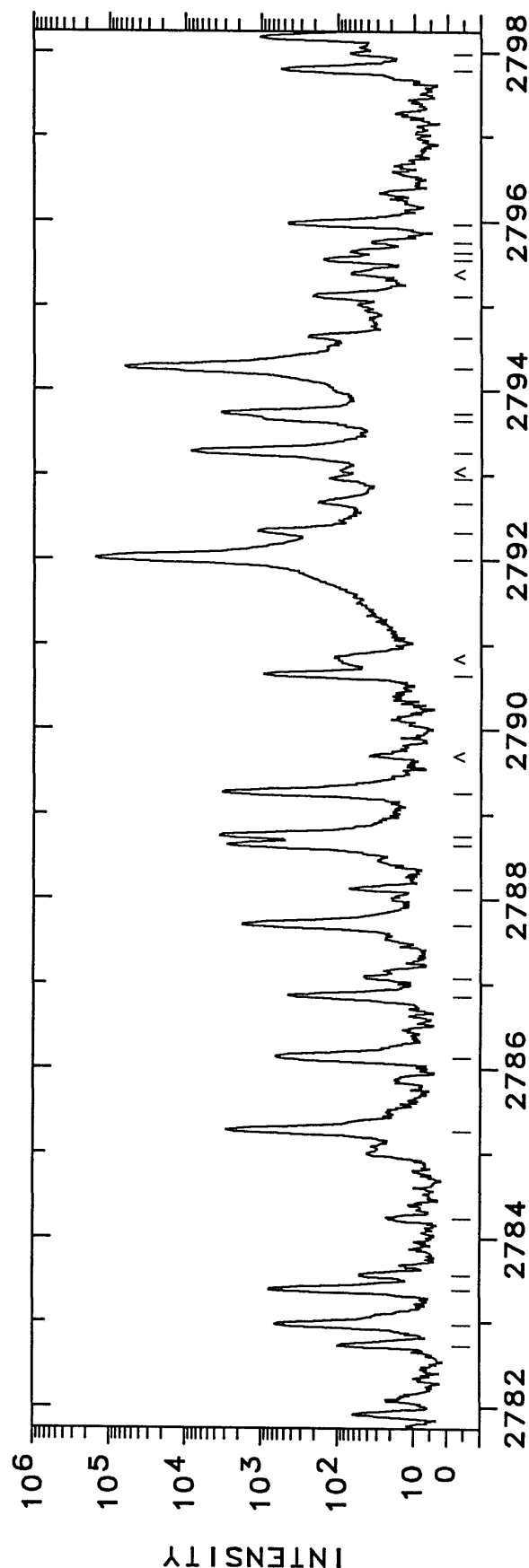
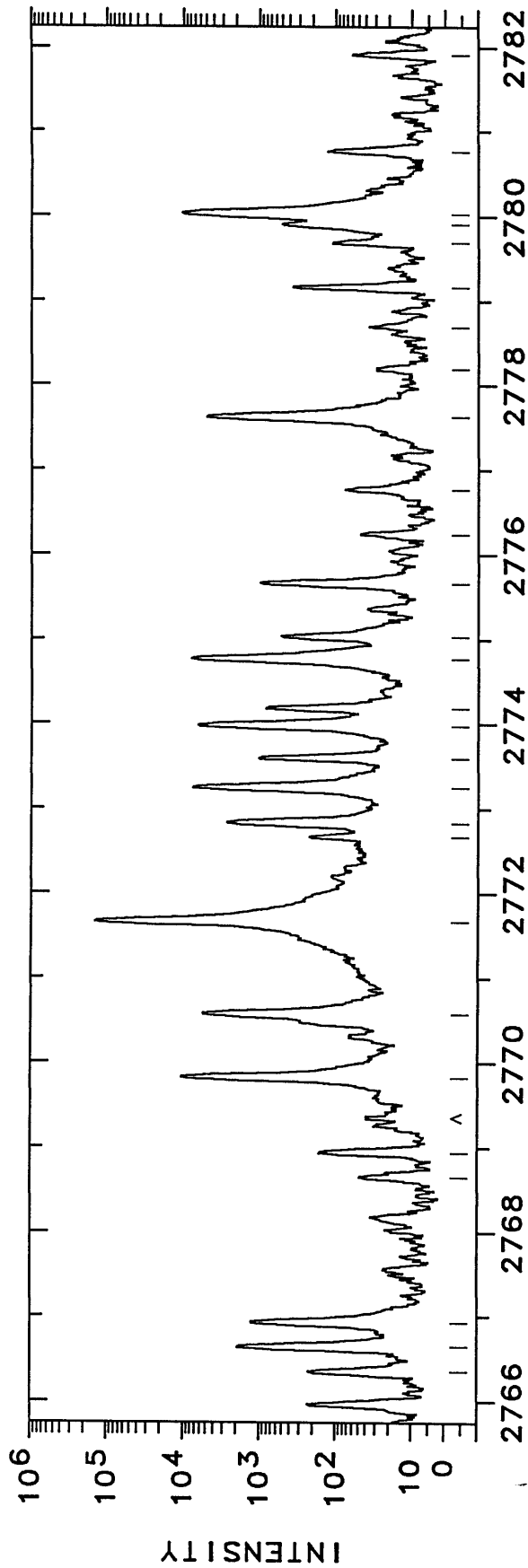
WAVELENGTH (ANGSTROMS) - AIR

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2734.4930	36559.030	5000	Pt I	13496- 50055 E	2753.22	36310.4	57	Pt II	104090- 67780 K
2735.64	36543.7	240	Pt II	111162- 74619 K	2753.7613	36303.237	1800	Pt I	10116- 46419 E
2735.7411	36542.352	470	Pt II	36484- 73026 14	2753.8531	36302.027	12000	Pt I	10131- 46433 E
2736.16	36536.8	300	Ne I		2754.19	36297.6	330		
2736.75	36528.9	92	Pt I	26638- 63167 N	2754.9122	36288.071	45000	Pt I	10131- 46419 E
2737.5573	36518.109	1800			2756.06	36273.0	81		
2737.78	36515.1	110	Pt I	21967- 58482 N	2756.6186	36265.61	31000	Ne II	
2737.98	36512.5	39	Ne III		2757.18	36258.2	290	Pt II	110258- 73999 K
2738.19	36509.7	210	Pt II	113119- 76610 K	2757.69	36256.929	2400	Pt II	117340- 81083 K
2738.4831	36505.764	8700	Pt I	10116- 46622 E	2757.56	36253.2	39		
2738.81	36501.4	94	Pt II	109527- 73026 K	2757.69	36251.5	290	Pt I	15501- 51753 N
2739.23	36495.8	400	Pt II	110257- 73761 K	2758.04	36246.9	170		
2739.54	36491.7	60	Pt II	116689- 80197 K	2758.1983	36244.840	360	Pt II	109676- 73431 K
2739.98	36485.8	150			2758.88	36235.9	69	Pt II	64003-100239 K
2740.2940	36481.642	1000	Pt II	106434- 69953 AK	2759.07	36233.4	120		
2740.2940	36481.642	1000	Pt II	109507- 73026 AK	2759.29	36230.5	48		
2741.58	36464.5	46	Ne III		2759.47	36228.1	150		
2741.94	36459.7	89	Pt II	43737- 80197 AK	2759.83	36223.4	80		
2741.94	36459.7	89	Ne II		2760.01	36221.1	99		
2742.4055	36453.554		Fe I		2760.30	36217.2	160		
2743.2944	36441.742	110000	Pt II	101199- 64757 09	2760.57	36213.7	23		
2744.24	36429.2	93	Pt I	26638- 63067 N	2760.71	36211.9	57		
2744.8285	36421.377	1000	Pt I	21967- 58388 N	2761.32	36203.9	24		
2745.16	36417.0	84	Pt II	111162- 74745 K	2762.31	36190.9	38		
2746.09	36404.6	64	Ne III		2762.9217	36182.88	39000	Ne II	
2746.7095	36396.436	3700	Pt II	110158- 73761 K	2763.2173	36179.010	980 H	Pt II	24879- 61058 08
2747.6023	36384.609	7600	Pt I	13496- 49880 E	2763.89	36170.2	44		
2747.8517	36381.507	460			2764.1709	36166.530	5800	Pt II	110408- 74241 AK
2749.1833	36363.687	360	Pt II	37877- 74241 16	2764.1709	36166.530	5800	Pt II	101517- 65351 AK
2749.56	36358.7	21			2764.47	36162.6	51		
2750.1408	36351.027		Fe I		2764.6067	36160.829	740	Ne III	
2750.24	36349.7	37			2764.81	36158.2	370	Pt II	110158- 73999 K
2750.63	36344.6	19			2765.59	36148.0	83		
2750.75	36343.0	24			2765.66	36147.1	130	Pt II	110146- 73999 K
2752.48	36320.1	34	Pt II	109346- 73026 K	2765.96	36143.1	230	Ne III	
2752.87	36315.0	230							



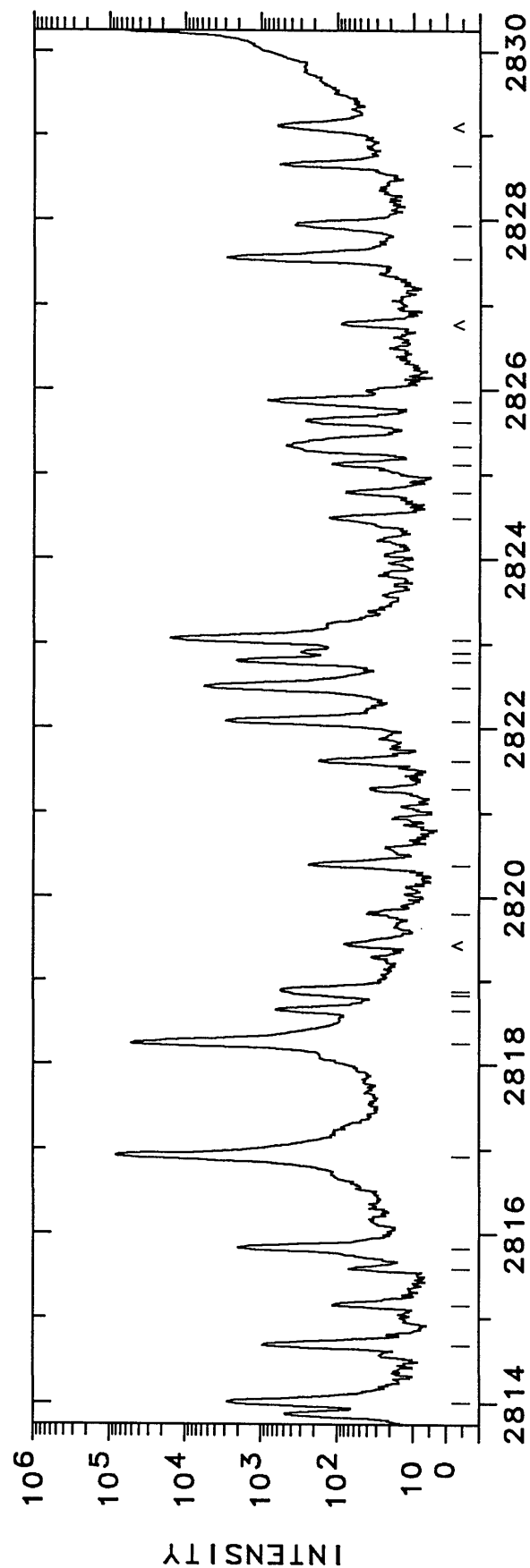
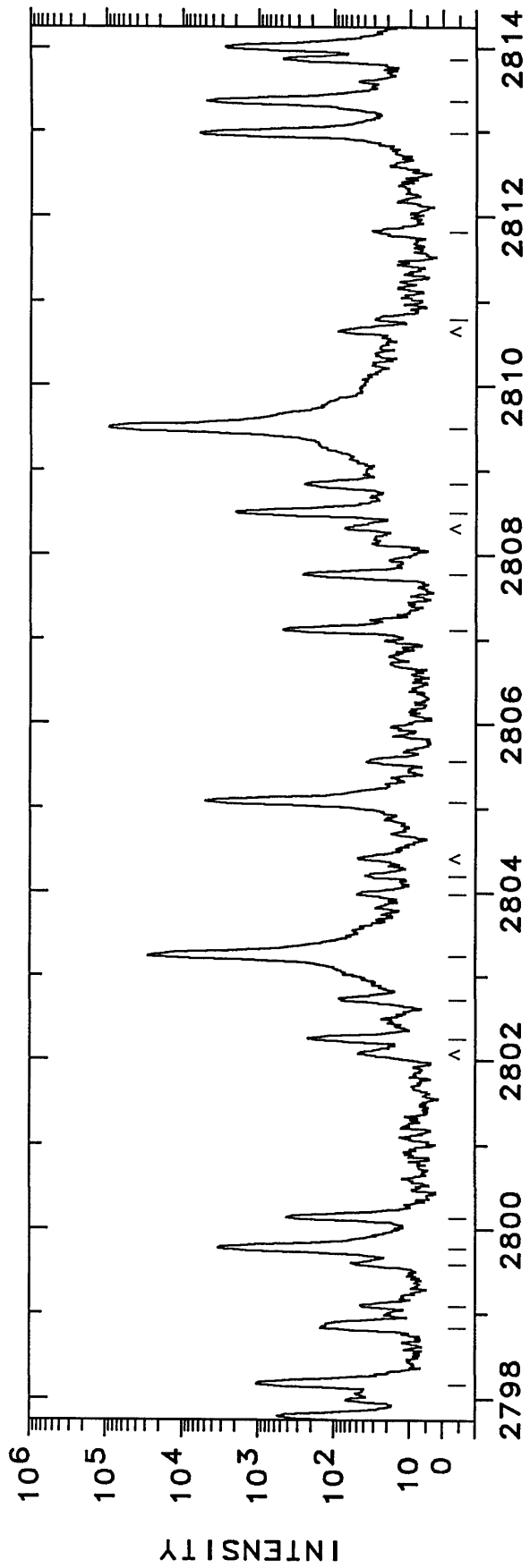
WAVELENGTH (ANGSTROMS) - AIR

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2766.6534	36134.080	1900	Ne III		2783.56	35914.6	45	Pt II	109676- 73761
2766.9444	36130.279	1300			2784.23	35906.0	17		
2768.65	36108.0	43			2785.2734	35892.529	2900	Ne III	
2768.94	36104.2	160	Pt II	41434- 77538	2786.1247	35881.563	650	Ne III	
2769.8332	36092.599	11000	Pt I	6567- 42660	2786.85	35872.2	440	Ne III	
2770.5747	36082.94	5500	Ne II		2787.07	35869.4	40		
2771.6594	36068.819	150000	Pt I	775- 36844	2787.6892	35861.426	1800	Ne III	
2772.67	36055.7	220	Pt II	106434- 70379	2788.1048	35856.082		Fe I	
2772.8253	36053.654	2700	Pt I	10116- 46170	2788.6209	35849.446	2800	H	21168- 57018
2773.2372	36048.299	7600	Pt I	13496- 49544	2788.7317	35848.022	3600	Pt II	101199- 65351
2773.5903	36043.710	1000	Pt I	15501- 51545	2788.7317	35848.022	3600	Pt II	110257- 74409
2773.9918	36038.494	6500	Pt I	10131- 46170	2789.2620	35841.206	3300	Pt II	105794- 69953
2774.1959	36035.843	840	Pt I	16983- 53019	2790.6578	35823.281	940	Pt II	112433- 76610
2774.7838	36028.208	7900	Pt II	24879- 60907	2792.0165	35805.849	150000	Ne II	
2775.0515	36024.733	520	Ne I		2792.3180	35801.983	1100	Ne I	
2775.6679	36016.734	1000	Pt II	110258- 74241	2792.66	35797.6	180	Ne I	
2776.24	36009.3	43	Pt II	105962- 69953	2792.95	35793.9	130	Pt II	64003- 99797
2776.76	36002.6	72	Pt II	114455- 78452	2793.2647	35789.849	8600	Pt I	13496- 49286
2777.6274	35991.326	5000	Ne III		2793.6347	35785.109	940	Pt I	15501- 51286
2778.2204	35983.645		Fe I		2793.7012	35784.258	3400	Pt II	29261- 65046
2778.69	35977.6	32	Pt II	111162- 75184	2794.2192	35777.625	64000	Ne II	
2779.16	35971.5	370	Pt II	112433- 76461	2794.62	35772.5	240		
2779.69	35964.6	110			2795.11	35766.2	210	Pt II	109527- 73761
2779.9025	35961.872	500	Ne III		2795.54	35760.7		Mg II	
2780.0249	35960.289	11000	Ne II		2795.63	35759.6	64		
2780.76	35950.8	130	Pt II	121651- 85700	2795.75	35758.0	31		
2781.91	35935.9	56			2795.9565	35755.394	450	Ne I	
2782.72	35925.5	92	Pt II	50564- 86489	2797.8027	35731.802	550	Pt II	34647- 70379
2782.9913	35921.961	640	Ne III		2797.98	35729.5		Mg II	



WAVELENGTH (ANGSTROMS) - AIR

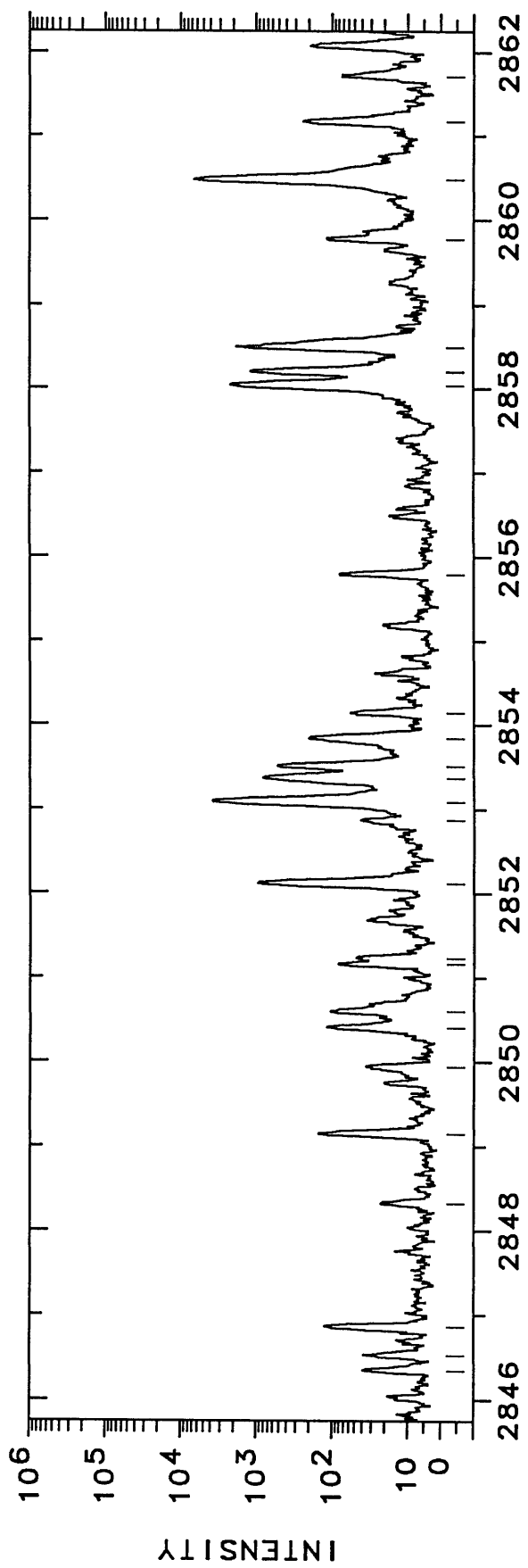
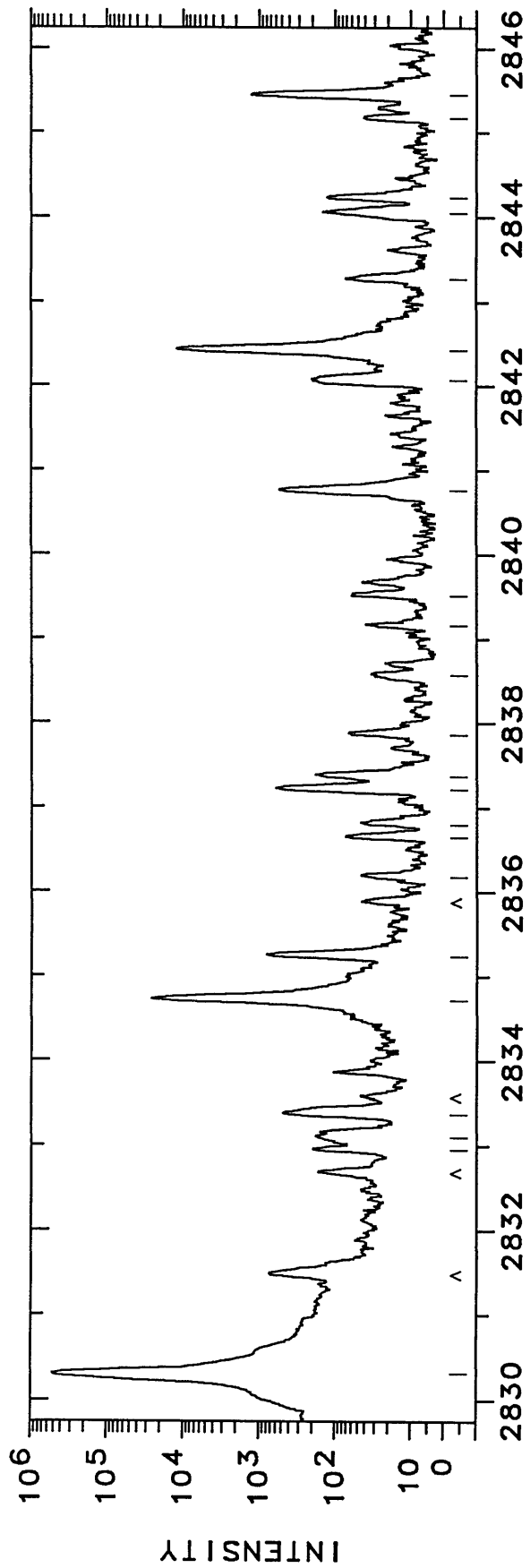
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2798.1894	35726.864	1000	Pt II	29030- 64757 10	2815.15	35511.6	110	Pt II	110257- 74745 K
2798.83	35718.7	140	Ne III		2815.58	35506.2	64	Pt II	42031- 77538 K
2799.09	35715.4	39			2815.8103	35503.302	2000	Pt II	110258- 74754 K
2799.58	35709.1	54			2816.9021	35489.542	81000	Pt II	101517- 66028 K
2799.7725	35706.664	3400	Pt II	96614- 60907 10	2818.2450	35472.632	51000	Pt I	823- 36296 E
2800.13	35702.1	420	Ne III		2818.6341	35467.736	630	Pt I	26638- 62106 N
2802.25	35675.1	210	Ne III		2818.8232	35465.356	350	Ne III	
2802.72	35669.1		Mg II		2818.8604	35464.888	400	Pt II	36484- 71948 L
2803.2357	35662.553	28000	Pt I	6140- 41802 E	2819.81	35452.9	35		
2803.98	35653.1	45	Pt II	110408- 74754 K	2820.38	35445.8	230	Ne III	
2804.20	35650.3	34	Ne III		2821.28	35434.5	31		
2805.0833	35639.064	4900	Pt II	110258- 74619 K	2821.61	35430.3	160	Ne III	
2805.56	35633.0	32	Pt II	114539- 78906 K	2822.0882	35424.326	2900	Pt II	96614- 61190 09
2807.11	35613.3	470	Pt II	105794- 70181 K	2822.4927	35419.250	5600	Pt II	21168- 56587 09
2807.77	35605.0	250	Pt II	116689- 81083 K	2822.7941	35415.469	2100	Pt II	105794- 70379 K
2808.5026	35595.677	2000	Pt I	15501- 51097 E	2822.89	35414.3	300	Ne III	
2808.84	35591.4	240	Pt II	48591- 84182 K	2823.0513	35412.242	16000	Pt II	110158- 74745 K
2809.4835	35583.249	92000	Ne II		2824.48	35394.3	120	Ne III	
2810.79	35566.7	24			2824.78	35390.6	72	Ne III	
2811.82	35553.7	27			2825.11	35386.4	110		
2812.9789	35539.036	6000	Pt I	21967- 57506 A	2825.33	35383.7	470	Ne III	
2812.9789	35539.036	6000	Pt II	110158- 74619 AK	2825.62	35380.1	260	Ne III	
2813.3728	35534.060	4900	Pt II	34647- 70181 18	2825.8440	35377.247	820	Ne III	
2813.8769	35527.694	470	Pt II	110146- 74619 K	2827.5379	35356.054	2900	Pt II	113119- 77763 K
2814.0134	35525.971	2800	Pt II	27255- 62781 15	2827.93	35351.2	360	Ne III	
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WAVELENGTH (ANGSTROMS) - AIR



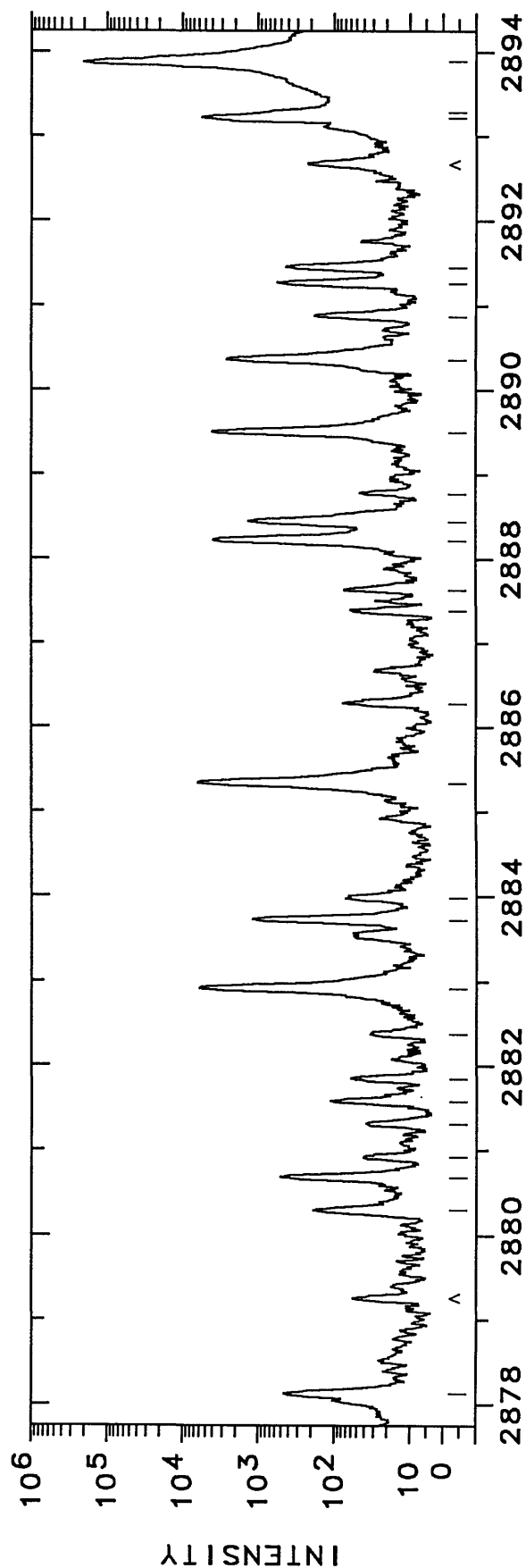
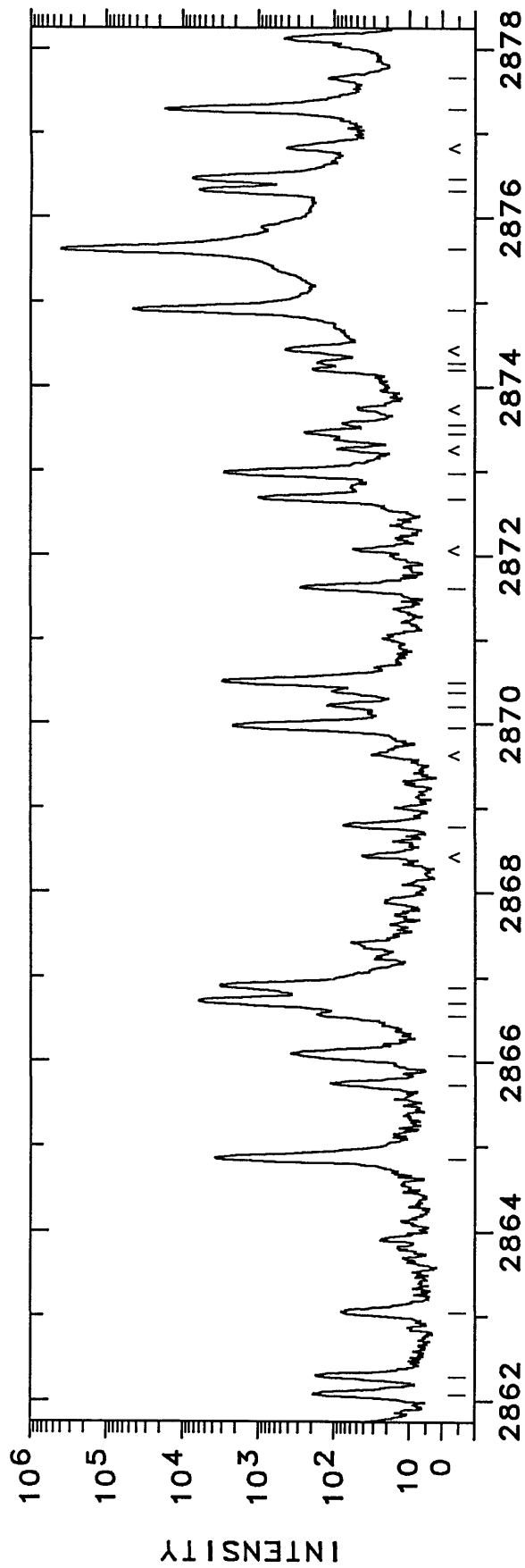
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2832.95	35288.5	190			2848.32	35098.1	18		
2833.10	35286.6	180	Pt II	109527- 74241 K	2849.15	35087.9	150	Pt I	16983- 52071 N
2833.37	35283.3	490	Pt I	13496- 48779 N	2849.94	35078.1	31	Pt II	110257- 75184 K
2834.7107	35266.596	26000	Pt I	10131- 45398 E	2850.41	35072.4	110	Pt II	106434- 71364 K
2835.2370	35260.049	800	Ne I		2850.60	35070.0	100	Pt II	
2836.18	35248.3	41			2851.16	35063.1	78	Ne III	
2836.65	35242.5	68			2851.23	35062.3	43		
2836.80	35240.6	41	Ne III		2852.1238	35051.293		Mg I	
2837.2284	35235.302	610	Pt I	6567- 41802 N	2852.87	35042.1	37	Pt II	110408- 75365 K
2837.37	35233.5	180	Ne III		2853.0972	35039.335	3800	Pt I	13496- 48535 E
2837.86	35227.5	62			2853.3729	35035.950	810	Pt I	68716- 33680 N
2838.57	35218.6	29			2853.5092	35034.275	510		
2839.16	35211.3	35			2853.84	35030.2	190		
2839.5216	35206.848	55	Pt II	105388- 70181 23	2854.14	35026.5	52		
2840.76	35191.5	540	Ne III		2855.79	35006.3	74		
2842.07	35175.3	200			2858.0244	34978.931	2200	Ne II	
2842.4101	35171.071	12000	Pt II	101199- 66028 09	2858.1879	34976.930	810 P	Pt II	104930- 69953 K
2843.27	35160.4	67			2858.2026	34976.750	650 U		
2844.05	35150.8	140	Pt I	68831- 33680 N	2858.4846	34975.299	1800	Pt II	110158- 75184 K
2844.2284	35148.588	120	Pt II	37877- 73026 18	2859.77	34957.6	110	Pt II	117493- 82535 K
2845.17	35137.0	37			2860.4830	34948.867	6600	Pt II	96614- 61665 08
2845.4468	35133.538	1300	Pt II	105086- 69953 K	2861.17	34940.5	230		
2846.34	35122.5	34			2861.71	34933.9	68		
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WAVELENGTH (ANGSTROMS) - AIR

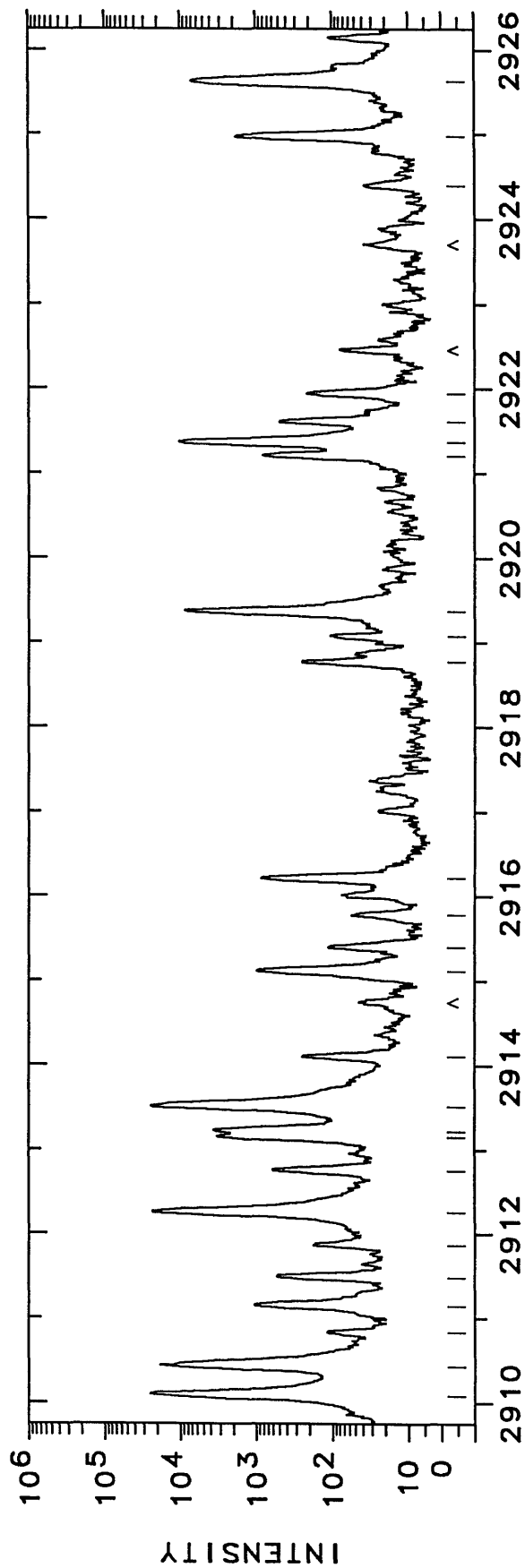
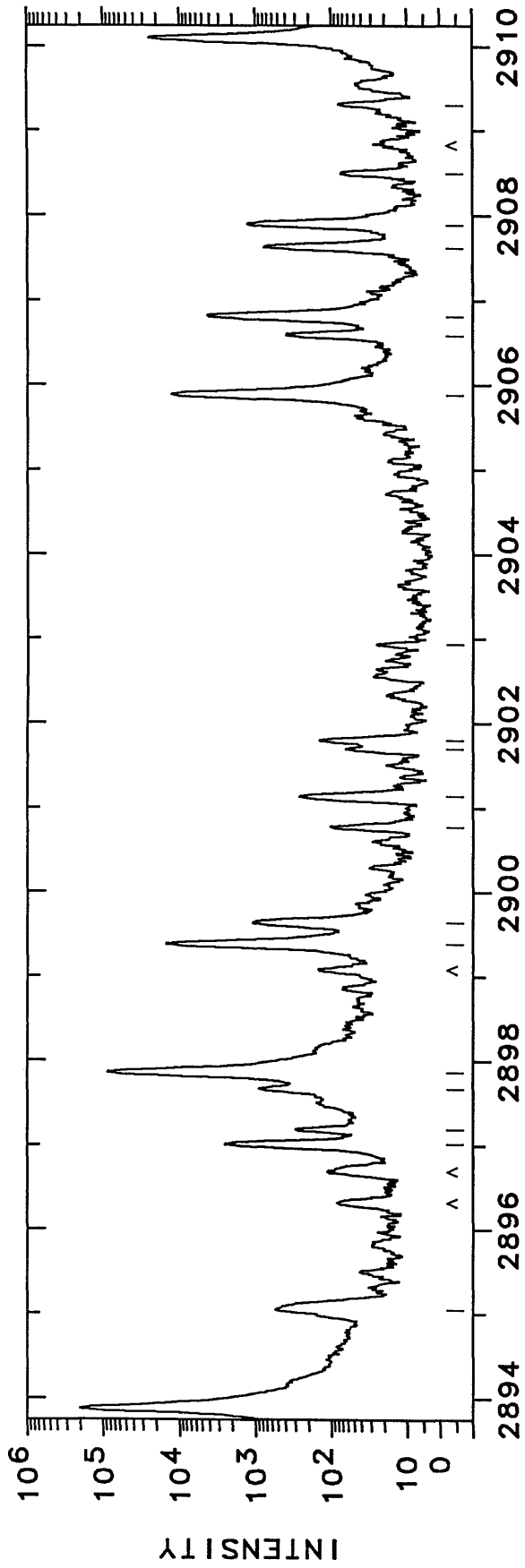
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2880.68	34703.8	510		
2880.92	34701.0	37	Pt II	K
2881.31	34696.3	32	Ne I	
2881.5792	34693.016		Si I	B
2881.85	34689.8	55	Ne I	
2882.38	34683.4	28		
2882.9326	34676.731	6000	Pt II	K
2883.7321	34667.117	1200	Pt II	K
2883.98	34664.1	66	Pt II	K
2885.3275	34647.949	6300	Pt II	K
2886.28	34636.5	71	Pt I	N
2887.38	34623.3	55		
2887.63	34620.3	68		
2888.1924	34613.582	3900	Pt I	E
2888.4162	34610.90	1300	Ne II	C
2888.77	34606.7	40		
2889.5096	34597.805	4000	Pt II	K
2890.3725	34587.476	2600	Pt II	07
2890.87	34581.5	180	Pt I	N
2891.26	34576.9	560	Pt II	K
2891.4581	34574.49	430	Ne II	C
2893.2175	34553.466	5600	Pt I	E
2893.2881	34552.623	600 P	Pt II	K
2893.8630	34545.759	200000	Pt I	E

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
34929.5		180	Ne I	
34926.9		170		
34917.7		75		
34895.675		3700	Pt II	11
34885.066		110	Pt II	23
34880.6		360	Pt II	K
34874.9		160		
34872.851		6100	Ne III	L
34870.674		3200 L	Pt II	10
34847.8		69	Pt II	K
34833.520		2100	Ne II	G
34830.565		120	Pt II	13
34828.5		100		
34827.338		3000	Pt I	N
34813.5		270		
34800.695		970	Ne I	G
34797.118		2800	Ne II	G
34791.3		240	Pt II	K
34790.0		72	Pt I	N
34782.1		180	Pt II	K
34781.1		160	Pt II	K
34773.378		44000	Pt II	14
34764.770		400000	Pt II	G
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34754.667		7400	Ne II	G
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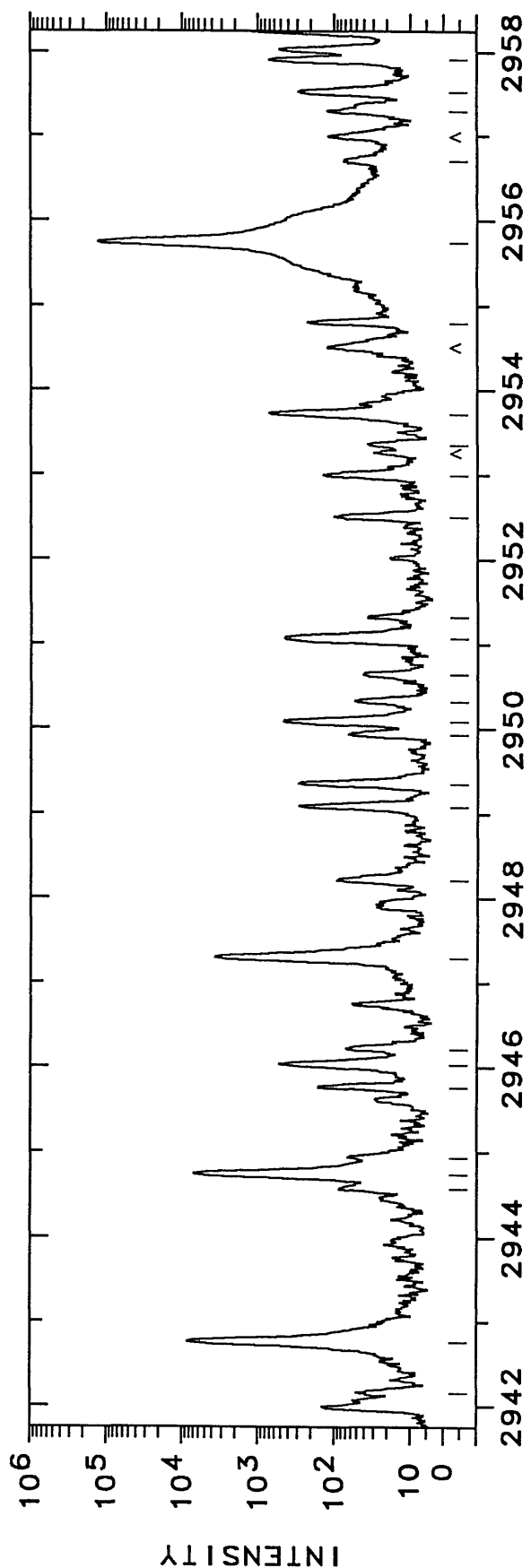
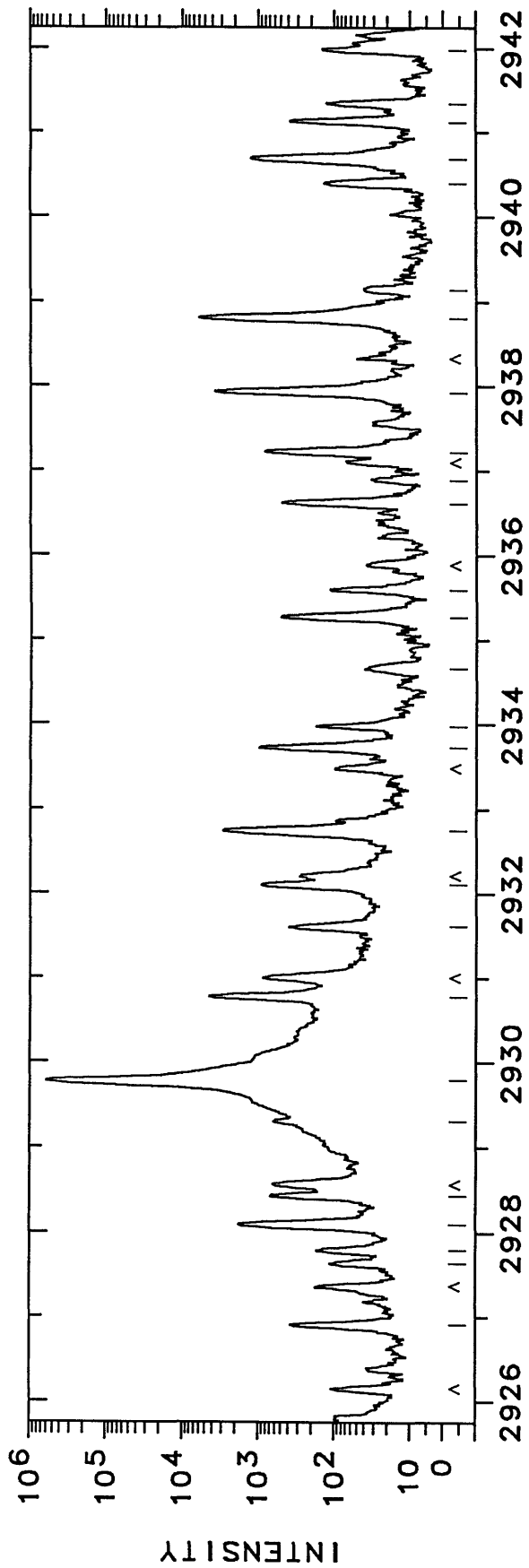
WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
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2897.0028	34508.32	2500	Ne II	C	2911.48	34336.7	530	Ne II	C
2897.2001	34505.97	290	Ne II	C	2911.8588	34332.27	170	Ne II	C
2897.6782	34500.277	890	Ne II	G	2912.2515	34327.641	23000	Pt I	10116- 44444
2897.8715	34497.976	88000	Pt I	E	2912.7692	34321.540	600	Pt I	21967- 56288
2899.3861	34479.955	15000	Pt II	K	2913.1735	34316.777	3200	Ne I	
2899.6452	34476.874	1100 L	Pt II	11	2913.2445	34315.940	3600	Pt I	10116- 44432
2900.78	34463.4	98			2913.5386	34312.477	24000	Pt I	10131- 44444
2901.14	34459.1	260	Pt I	N	2914.11	34305.7	240	Pt II	43737- 78043
2901.70	34452.5	58	Pt I	N	2915.1200	34293.864	980	Ne II	
2901.80	34451.3	140	Ne III	L	2915.40	34290.6	110	Ne III	
2902.93	34437.9	19	Ne III	L	2915.78	34286.1	49	Ne III	
2905.8974	34402.699	12000	Pt I	A	2916.2029	34281.13	850	Ne II	
2905.8974	34402.699	12000	Ne III	AL	2918.7487	34251.23	240	Ne II	
2906.5918	34394.48	390	Ne II	C	2919.07	34247.5	100	Ne II	
2906.8152	34391.837	4300	Ne II	G	2919.3402	34244.291	8800	Pt I	13496- 47740
2907.6288	34382.214	760	Ne III	L	2921.2203	34222.252	800	Pt I	64379- 30156
2907.8960	34379.055	1300	Pt I	E	2921.3792	34220.391	10000	Pt I	6567- 40787
2908.49	34372.0	69	Ne III	L	2921.6217	34217.55	490	Ne II	
2909.30	34362.5	73			2921.9574	34213.62	210	Ne II	
2910.0599	34353.493	25000	Ne II	G	2924.39	34185.2	32	Ne III	
2910.4075	34349.389	20000	Ne II	G	2924.9582	34178.520	1800	Pt II	112433- 78254
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WAVELENGTH (ANGSTROMS) - AIR

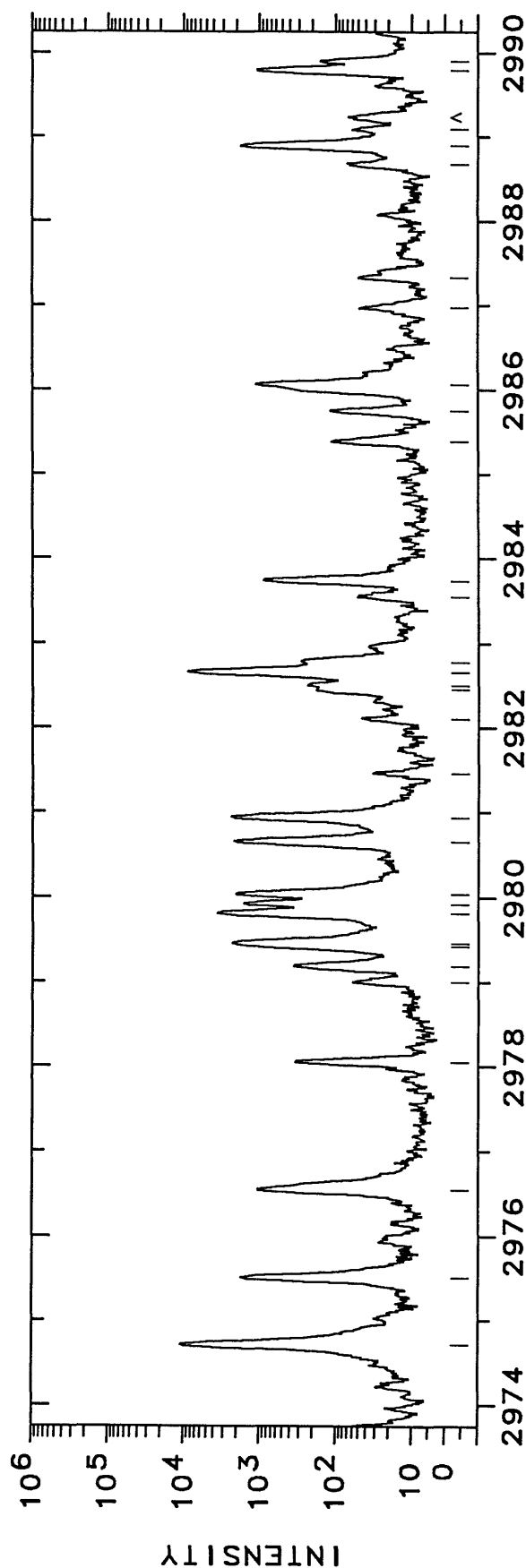
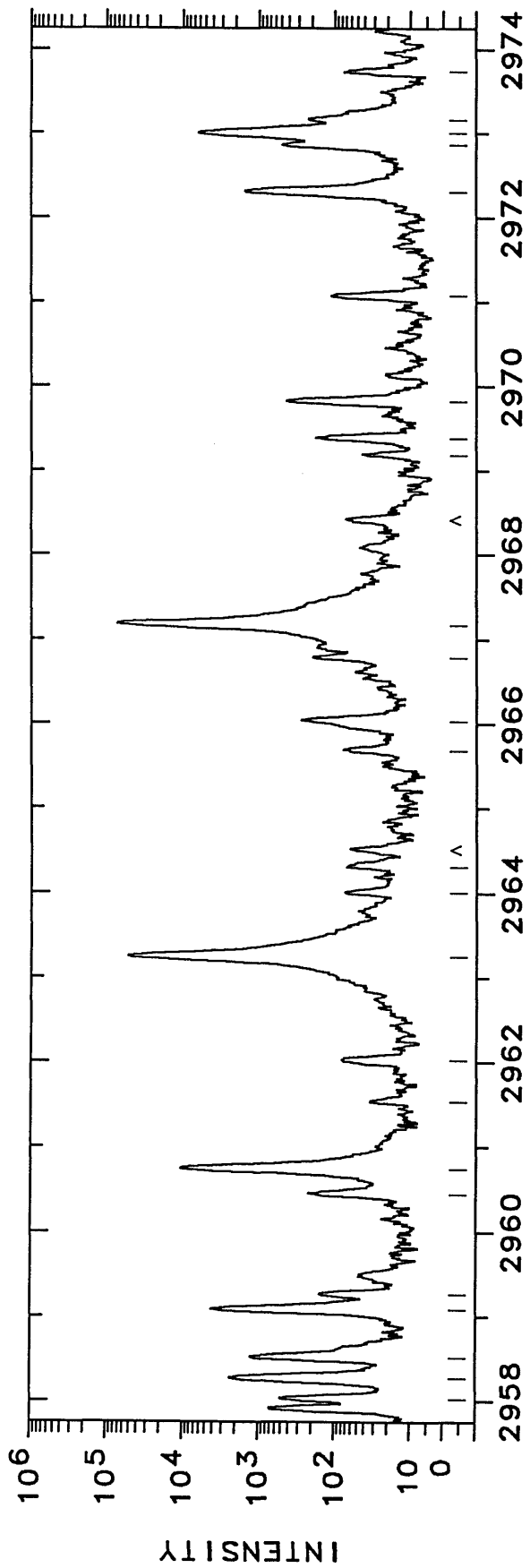
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2926.91	34155.7	370	Pt I	64312- 30156 N	2942.7514	33971.871	8400	Pt I	64128- 30156 E
2927.64	34147.2	110	Pt II	41434- 75581 K	2944.57	33950.9	80	Pt I	6567- 40516 E
2927.7843	34145.53	170	Ne II		2944.7525	33948.786	7100	Pt I	110408- 76461 AK
2928.1044	34141.798	1800	Pt I	18566- 52708 E	2944.93	33946.7	61	Pt II	109527- 75581 AK
2928.4406	34137.878	690	Pt II	95803- 61665 09	2944.93	33946.7	61	Pt II	
2929.3257	34127.564	620	Ne I		2945.76	33937.2	160	Ne II	
2929.7894	34122.163	610000	Pt I	0- 34122 E	2946.0435	33933.91	520	Ne II	
2930.7847	34110.576	4400	Pt I	64267- 30156 N	2946.21	33932.0	64	Pt II	41434- 75365 K
2931.61	34101.0	400	Pt II	48591- 82692 K	2947.3010	33919.432	3700	Ne I	
2932.1079	34095.182	900	Ne II		2948.21	33909.0	88		
2932.7252	34088.006	2900	Ne I		2949.08	33899.0	290		
2933.7138	34076.52	970	Ne II		2949.35	33895.9	290		
2933.9707	34073.536	170	Pt II	105388- 71314 21	2949.93	33889.2	60	Ne III	
2934.66	34065.5	34	Pt II	105086- 71021 K	2950.08	33887.5	470		
2935.2626	34058.54	510	Ne II		2950.32	33884.7	49	Pt I	68006- 34122 N
2935.59	34054.7	110			2950.64	33881.1	36	Ne III	
2936.61	34042.9	490	Pt I	15501- 49544 N	2951.0485	33876.36	450	Ne II	
2936.9037	34039.510		Fe I		2951.32	33873.2	31		
2937.21	34036.0	840	Pt II	58491- 92526 K	2952.50	33859.7	94		
2937.9421	34027.479	3800	Pt II	113119- 79092 K	2953.0047	33853.92	140	Ne II	
2938.8101	34017.430	6000	Pt I	21967- 55984 N	2953.35	33850.0	31		
2939.14	34013.6	35	Pt II	105962- 71948 K	2953.71	33845.8	720	Pt II	105794- 71948 K
2940.39	33999.2	130	Pt I	68121- 34122 N	2954.79	33833.5	220	Pt II	111371- 77538 K
2940.6481	33996.168	1300	Ne II		2955.7255	33822.759	130000	Ne II	
2941.12	33990.7	380			2956.70	33811.6	69		
2941.34	33988.2	120	Pt II	117340- 83352 K	2957.29	33804.9	120		
2941.98	33980.8	140	Pt II	112433- 78452 K	2957.52	33802.2	290	Pt II	117340- 83538 K
2942.15	33978.8	44			2957.91	33797.8	710	Pt II	110408- 76610 K



WAVELENGTH (ANGSTROMS) - AIR

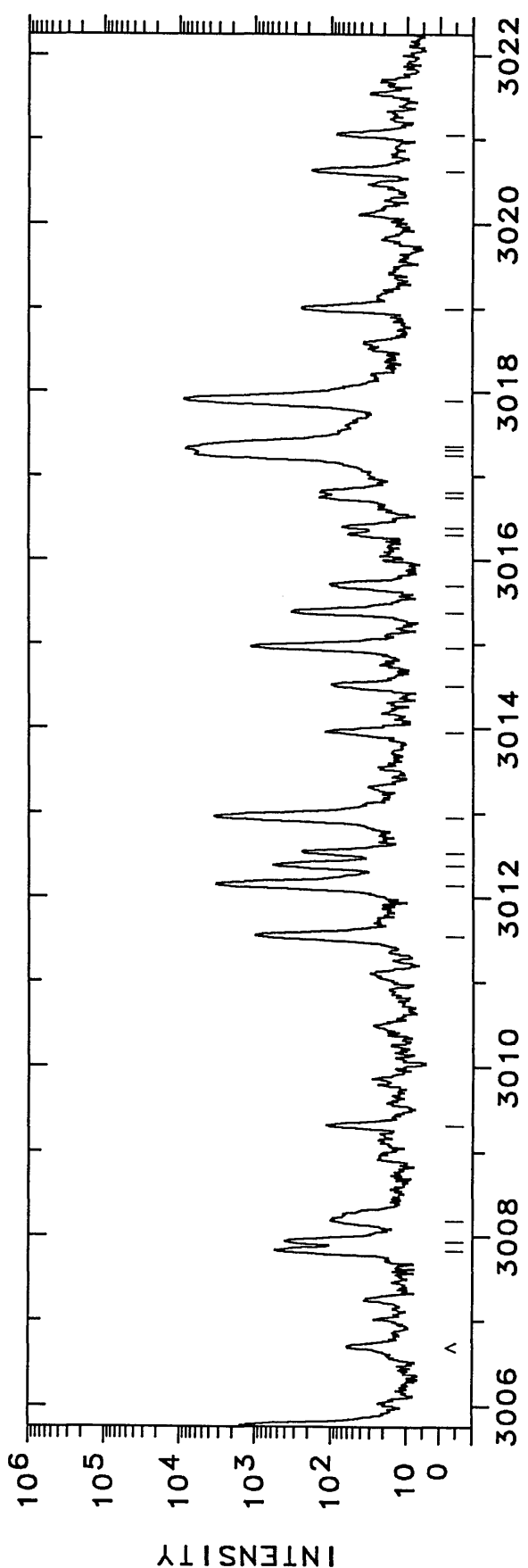
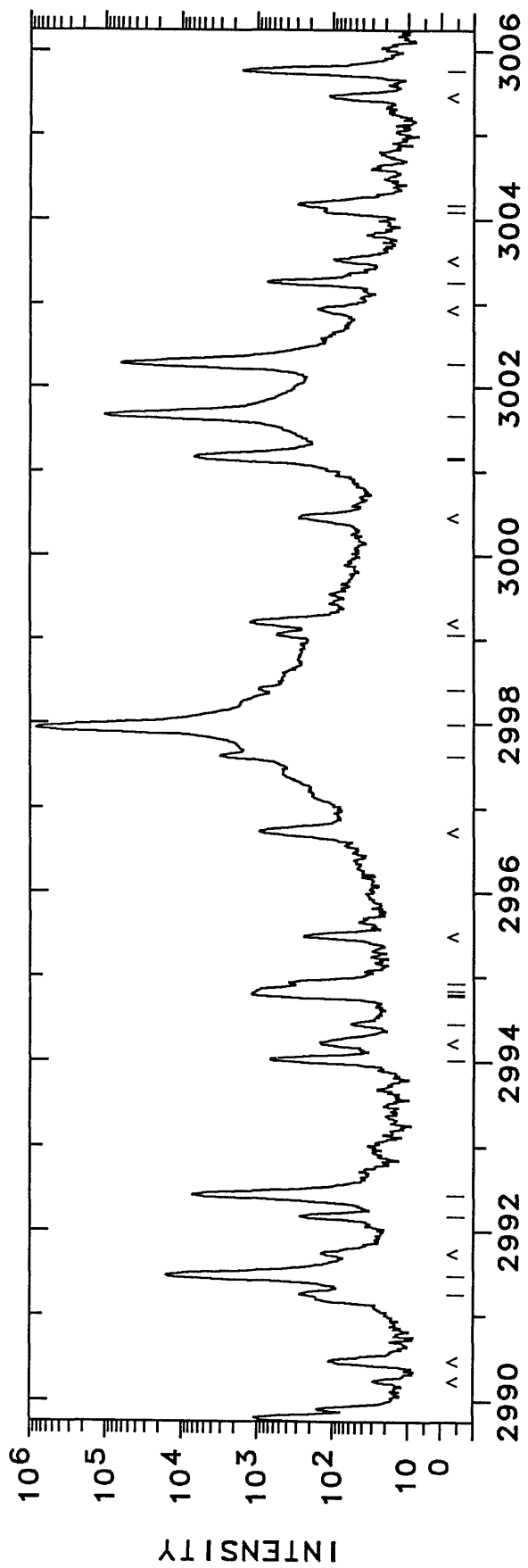


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2958.02	33796.5	510	Pt II	110258- 76461 K	2978.05	33569.2	330	Pt I	21967- 55536 N
2958.2529	33793.863	2300	Pt II	96614- 62820 11	2978.9996	33558.522	54	Pt II	29261- 62820 11
2958.5030	33791.007	1200	Pt II	32237- 66028 11	2979.1679	33556.627	350	Pt II	23461- 57018 08
2959.0936	33784.263	4100	Pt I	15501- 49286 E	2979.4223	33553.761	1430 P		
2959.26	33782.4	150	Pt II	43737- 77519 K	2979.4585	33553.353	2100 P	Ne II	G
2960.4556	33768.72	220	Ne II		2979.8086	33549.411	3600	Ne I	G
2960.7494	33765.369	11000	Pt I	63922- 30156 N	2979.9237	33548.116	1600	Pt II	110158- 76610 K
2961.53	33756.5	28			2980.0375	33546.834	2100	Ne II	G
2962.02	33750.9	74	Pt II	41434- 75184 K	2980.0375	33546.834	2100	Ne II	G
2963.2351	33737.046	53000	Ne II		2980.6453	33539.994	2200	Ne I	G
2964.01	33728.2	68			2980.9252	33536.845	2400	Ne I	G
2964.31	33724.8	64			2981.4453	33530.995		Fe I	R
2965.68	33709.2	70			33523.6	33523.6	39		
2966.03	33705.3	270			2982.45	33519.7	180		
2966.78	33696.7	190			2982.50	33519.1	230		
2967.1827	33692.164	74000	Pt II	110158- 76461 K	2982.6696	33517.233	8800	Ne I	G
2969.18	33669.5	38	Ne II		2982.8011	33515.754	280	Pt II	32918- 66434 16
2969.3909	33667.11	170	Ne II		2983.5700	33507.118		Fe I	R
2969.82	33662.2	430			2983.7465	33505.136	890	Pt I	18566- 52071 E
2971.07	33648.1	110	Pt II	110258- 76610 K	2985.39	33486.7	110	Pt II	37877- 71364 K
2972.2799	33634.388	1500	Ne II		2985.75	33482.7	110	Ne II	G
2972.8560	33627.87	490 W	Ne II		2986.0615	33479.162	1100	Ne II	G
2972.9959	33626.287	6200	Ne II		2986.9423	33469.289	42	Pt II	36484- 69953 12
2973.16	33624.4	220	Pt II	111162- 77538 K	2987.33	33464.9	43		
2973.74	33617.9	69	Pt II	50564- 84182 K	2988.67	33449.9	64		
2974.7189	33606.812	11000	Ne I		2988.8832	33447.556	1800	Ne II	G
2975.5233	33597.726	1800	Ne I		2989.09	33445.2	54		
2976.5553	33586.079	1100	Ne II		2989.7940	33437.367	1100	Pt I	68759- 35321 N
					2989.90	33436.2	150	Pt II	113119- 79683 K



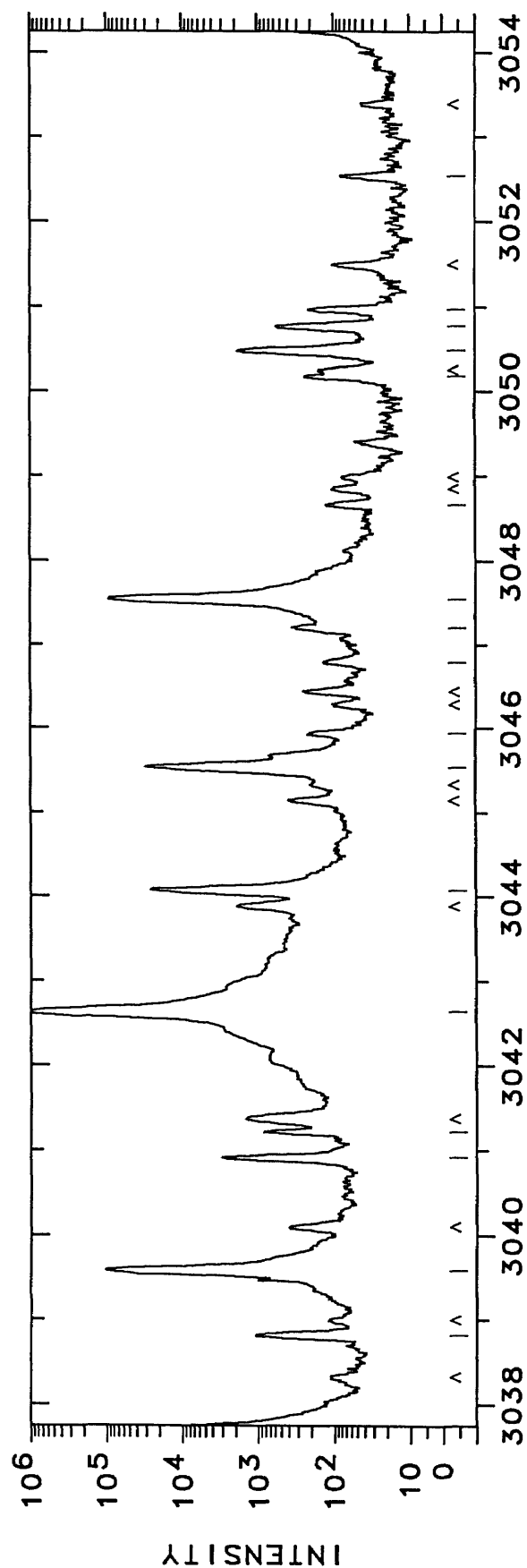
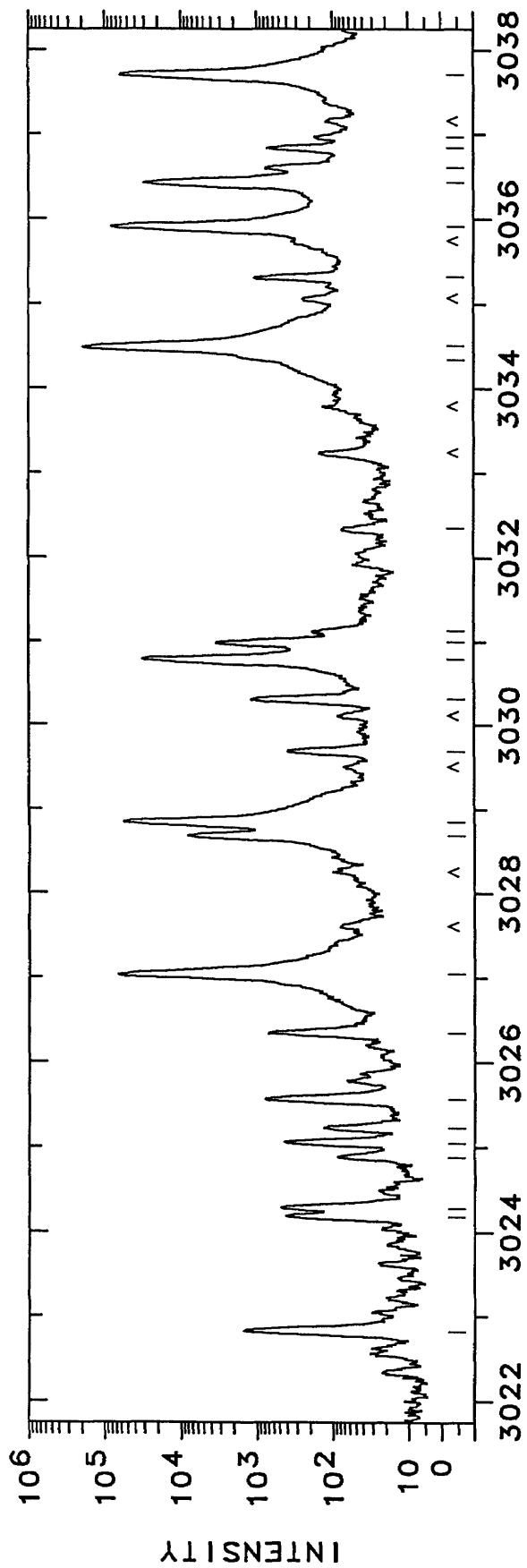
WAVELENGTH (ANGSTROMS) - AIR

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2991.25	33421.1	260			3008.18	33233.0	95		
2991.4665	33418.674	24000	Pt II	101199- 67780 K	3009.31	33220.5	110		
2992.17	33410.8	270	Pt II	110020- 76610 K	3011.5305	33196.035	1000		
2992.4296	33407.918	7100	Ne I		3012.1354	33189.368	3300	Ne I	18566- 51753 N
2994.0230	33390.14	660	Ne II		3012.38	33186.7	570	Pt I	41434- 74619 K
2994.44	33385.5	50			3012.53	33185.0	240	Pt II	
2994.7722	33381.787	850	Pt I	68703- 35321 N	3012.9576	33180.311	3500	Ne I	
2994.79	33381.6	1200			3013.9706	33169.16	110	Ne II	
2994.8285	33381.159	500	Ne II		3014.50	33163.3	90	Pt II	115060- 81897 K
2994.9101	33380.25	380	Ne II		3014.9700	33158.165	1100	Pt II	117340- 84182 K
2997.6170	33350.108	3100	Pt II	32237- 65587 20	3015.37	33153.8	320	Pt I	26638- 59792 N
2997.9622	33346.268	840000 C	Pt I	775- 34122 E	3015.69	33150.2	95		
2998.40	33341.4	940	Pt II	112433- 79092 K	3016.30	33143.5	51		
2999.05	33334.2	540	Pt II	42031- 75365 K	3016.30	33142.577	63	Pt II	23875- 57018 15
3001.1410	33310.950	900 U	Pt II	117493- 84182 K	3016.74	33138.7	130		
3001.1675	33310.655	6800 D	Pt II	18097- 51408 08	3016.80	33138.1	130	Pt II	105086- 71948 K
3001.6685	33305.096	110000	Ne II		3017.2399	33133.222	6200	Pt II	34647- 67780 K
3002.2641	33298.489	63000	Pt I	823- 34122 E	3017.3093	33132.459	8000	Ne II	
3003.2488	33287.572	730	Pt I	66967- 33680 N	3017.3498	33132.014	1300	Ne I	
3004.09	33278.3	130	Pt I	26638- 59916 N	3017.8714	33126.289	8800	Pt I	13496- 46622 E
3004.17	33277.4	290	Pt I	15501- 48779 N	3018.9858	33114.062	230	Pt II	32237- 65351 11
3005.7717	33259.632	1600			3020.6390	33095.939		Fe I	
3007.8321	33236.85	530	Ne II		3021.05	33091.4	77		
3007.9335	33235.73	400	Ne II						



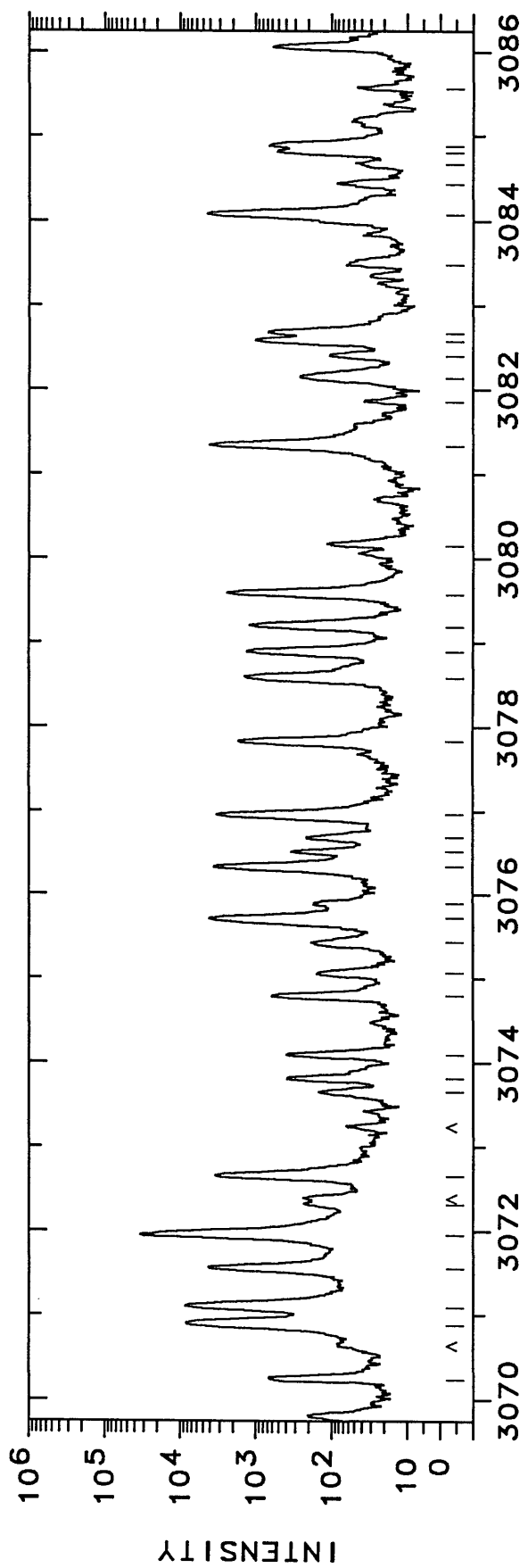
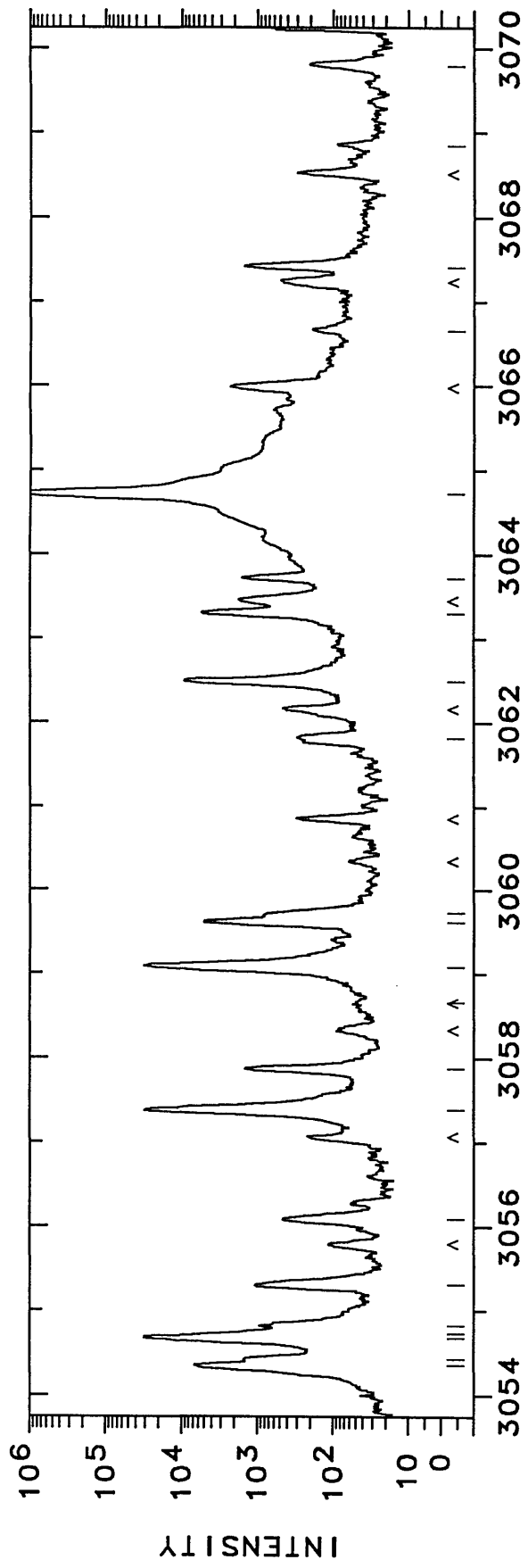
WAVELENGTH (ANGSTROMS) - AIR

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3022.8401	33071.841	1500	Pt I	16983- 50055 N	3036.6237	32921.73	750	Ne II	C
3024.18	33057.2	410			3036.84	32919.4	710	Pt II	111371- 78452 K
3024.2929	33055.954	480	Pt I	10131- 43187 E	3036.97	32918.0	160	Pt II	109527- 76610 K
3024.88	33049.5	80			3037.7192	32909.858	62000	Ne II	G
3025.05	33047.7	430	Pt I	26638- 59686 N	3038.8196	32897.941	1100	Pt II	109507- 76610 K
3025.23	33045.7	130	Pt II	46046- 79092 K	3039.5855	32889.651	100000	Ne II	G
3025.5458	33042.266	790	Pt I	21967- 55009 N	3040.8930	32875.511	3000	Pt II	96614- 63738 11
3026.3266	33033.742	710	Pt I	15501- 48535 E	3041.2085	32872.100	830	Pt I	21967- 54839 E
3027.0151	33026.228	68000	Ne II		3042.6318	32856.724	1200000 C	Pt I	823- 33680 E
3028.7000	33007.856	8100	Ne II	G	3044.0878	32841.009	26000	Ne II	G
3028.8633	33006.076	57000	Ne II	G	3045.5563	32825.174	30000	Ne II	G
3029.7112	32996.84	380	Ne II	C	3045.94	32821.0	210	Ne I	
3030.3209	32990.201	1200	Ne I		3046.79	32811.9	130		
3030.7876	32985.122	31000	Ne II	G	3047.21	32807.4	340	Pt II	41434- 74241 K
3030.9941	32982.874	3400	Pt II	95803- 62820 12	3047.5569	32803.627	91000	Ne II	G
3031.13	32981.4	180	Pt II	104930- 71948 K	3048.66	32791.8	120		
3032.35	32968.1	67			3050.18	32775.4	230		
3034.3397	32946.51	1100 U	Ne II	C	3050.4724	32772.276	1800	Ne II	G
3034.4609	32945.193	190000	Ne II	G	3050.7662	32769.12	560	Ne II	C
3035.32	32935.9	1100	Pt II	105962- 73026 K	3050.97	32766.9	200	Pt I	65387- 32620 N
3035.9216	32929.343	81000	Ne II		3052.54	32750.1	72	Pt II	112433- 79683 K
3036.4425	32923.694	30000	Pt I	13496- 46419 E					



WAVELENGTH (ANGSTROMS) - AIR

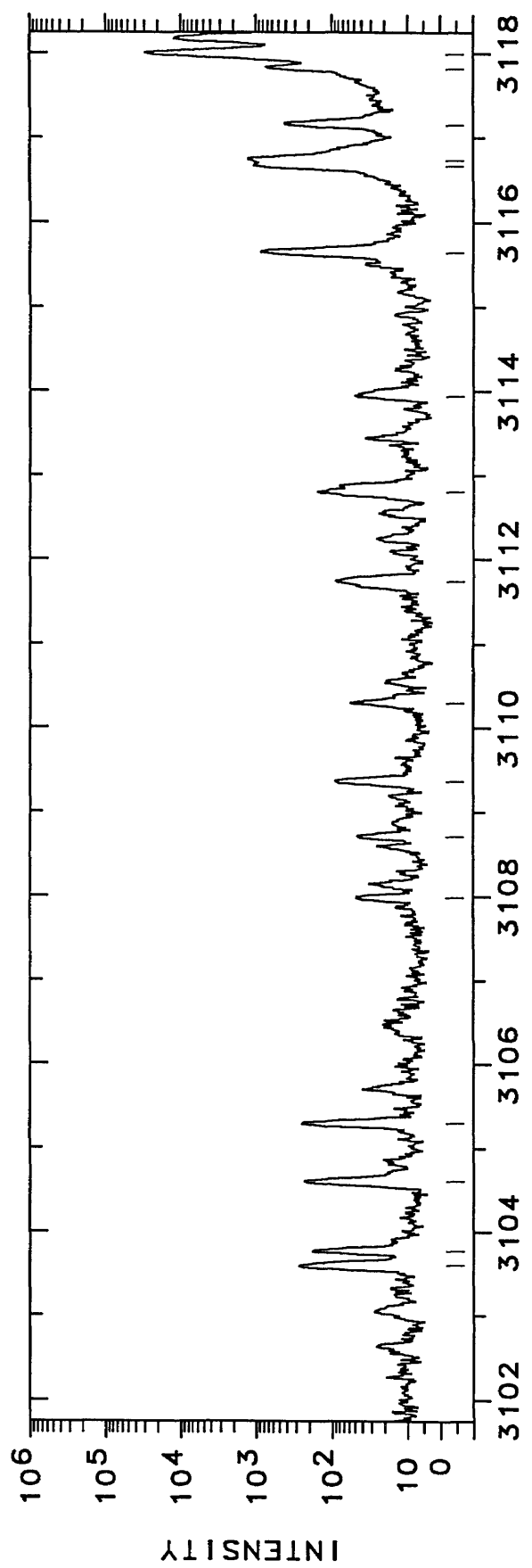
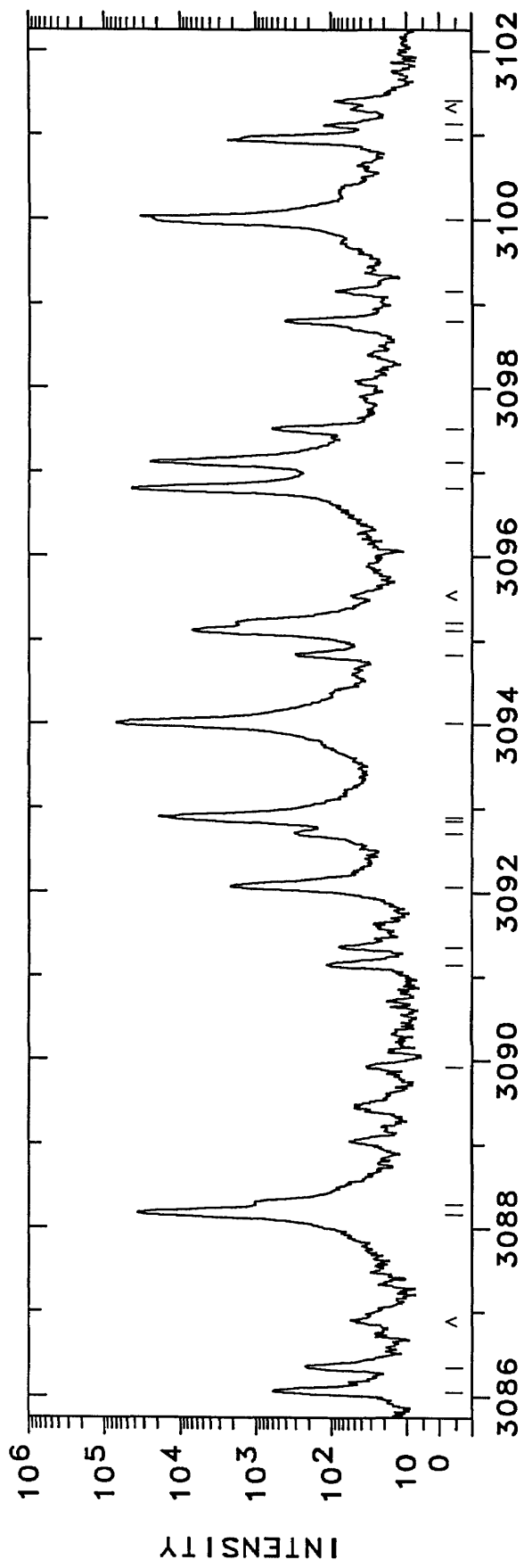




WAVELENGTH (ANGSTROMS) - AIR

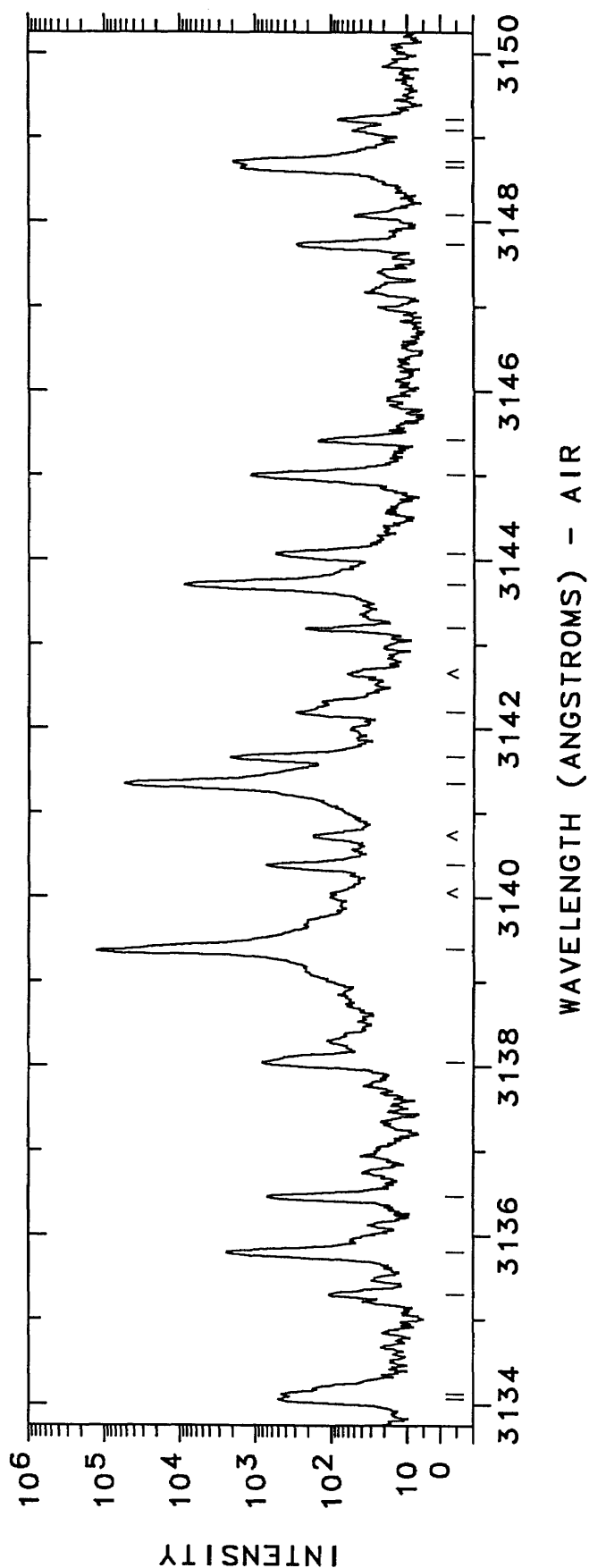
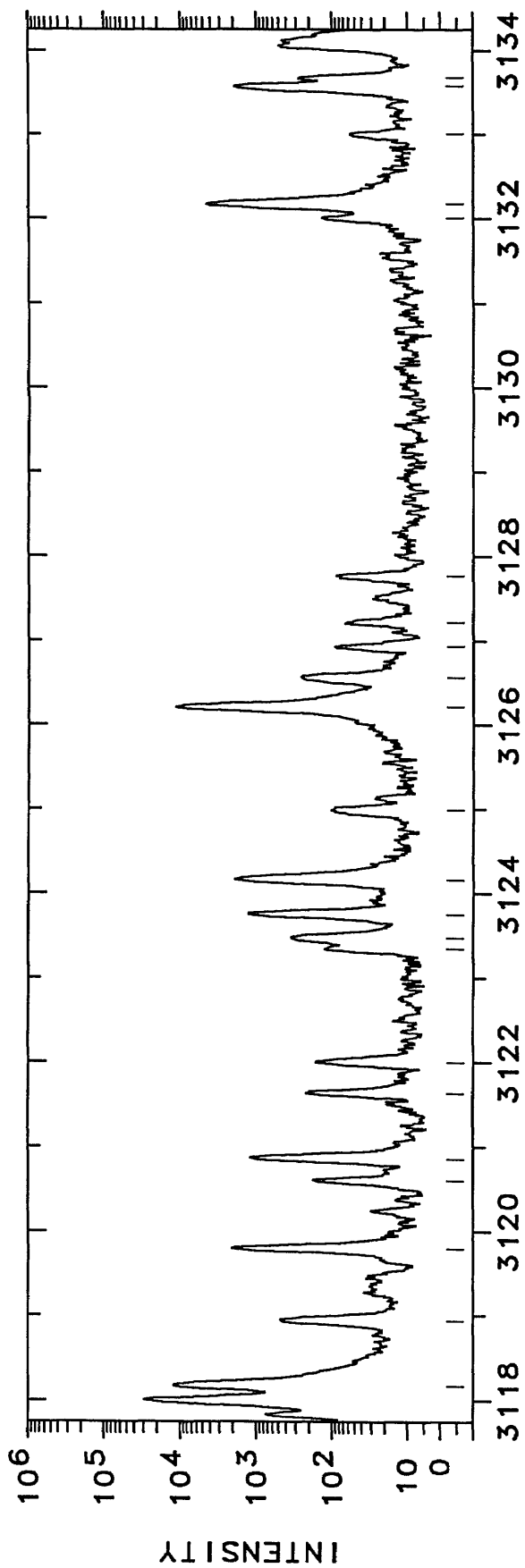


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3086.0810	32394.15	580	Ne II	C	3100.9598	32238.725	2300	Pt I	15501- 47740 E
3086.34	32391.4	210			3101.13	32237.0	120	Pt II	115060- 82824 K
3088.1641	32372.300	36000	Ne II	G	3101.41	32234.0	81		
3088.2852	32371.03	1000	Ne II	C	3103.60	32211.3	260	Pt I	21967- 54178 N
3089.92	32353.9	27			3103.77	32209.5	170	Pt II	42031- 74241 K
3091.14	32341.1	110			3104.61	32200.8	220	Pt II	105962- 73761 K
3091.35	32338.9	72			3105.30	32193.7	240	Pt II	106434- 74241 K
3092.0940	32331.158	2100	Ne II	G	3107.99	32165.8	39		
3092.7101	32324.717		Al I	F	3108.71	32158.4	38		
3092.8520	32323.233		Al I	F	3109.3597	32151.635	82	Pt II	32237- 64388 21
3092.9020	32322.711	19000	Ne II	G	3110.30	32141.9	49	Pt I	26638- 58780 AN
3094.0059	32311.179	69000	Ne II	G	3110.50	32141.9	49	Pt II	104090- 71948 AK
3094.83	32302.6	290			3111.74	32127.0	82	Pt II	64003- 96131 K
3095.1034	32299.723	6900	Ne II	G	3112.80	32116.1	150	Pt II	54373- 86489 K
3095.1843	32298.879	1500 P	Ne II	G	3113.94	32104.3	42		
3096.8104	32281.920	44000	Pt II	K	3115.64	32086.8	850	Ne II	C
3097.1318	32278.569	25000	Ne II	G	3116.684	32076.08	1100	Ne II	C
3097.5425	32274.29	600	Ne II	C	3116.7380	32075.525	1300	Pt II	37877- 69953 17
3098.8282	32260.90	410	Ne II	C	3117.155	32071.24	410	Ne II	C
3099.15	32257.6	79	Pt II	K	3117.8076	32064.522	730	Pt II	95803- 63738 12
3100.0252	32248.444	34000	Pt I	E	3117.9807	32062.742	29000	Ne II	G

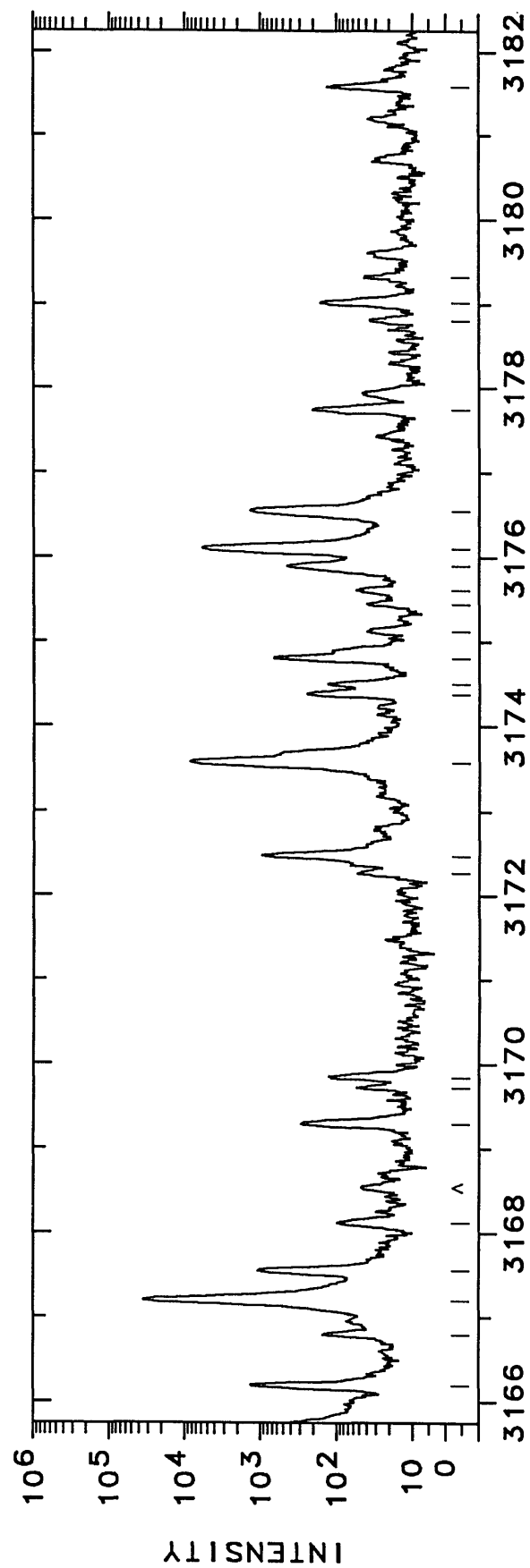
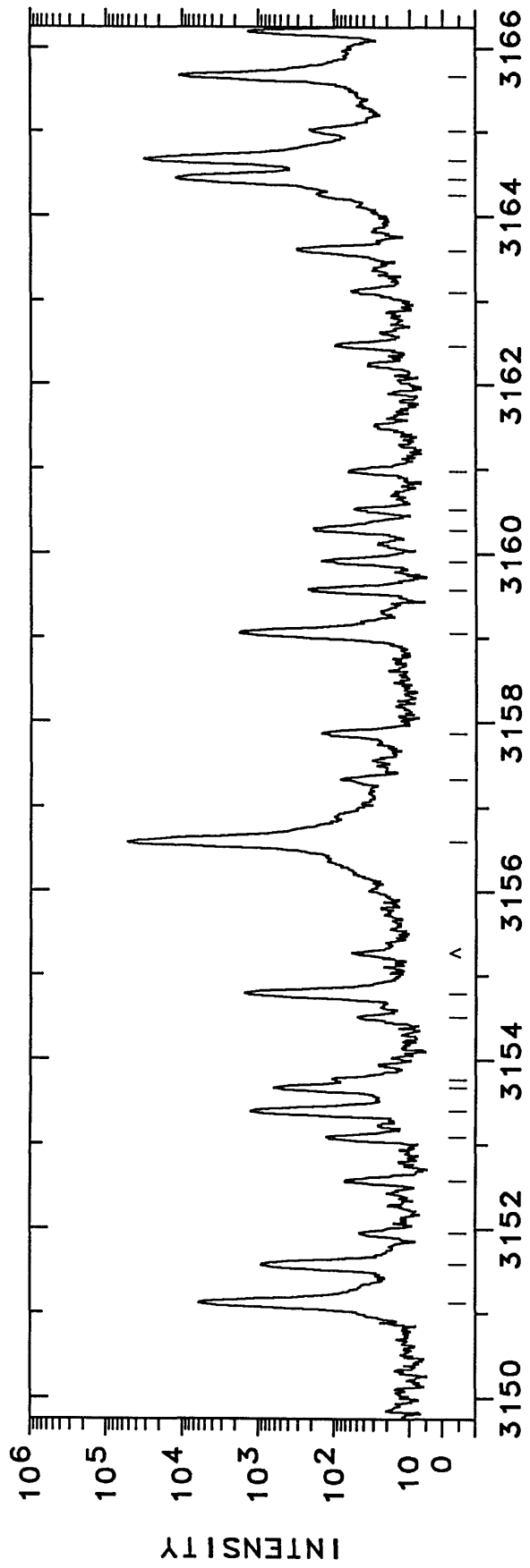


WAVELENGTH (ANGSTROMS) - AIR

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3118.1600	32060.898	12000	Ne II	G	3134.065	31898.20	490	Ne II	C
3118.94	32052.9	470			3134.134	31897.50	450	Ne II	C
3119.8001	32044.044	2100	Pt I	21967- 54011 E	3135.30	31885.6	99	Pt I	64505- 32620 N
3120.60	32035.8	170			3135.8153	31880.395	2400	Ne II	G
3120.86	32033.2	1200	Pt II	105794- 73761 K	3136.476	31873.68	680	Ne II	C
3121.64	32025.2	210			3138.056	31857.63	810	Ne II	C
3122.00	32021.5	160			3139.3870	31844.126	130000	Pt I	E
3123.365	32007.47	120	Ne II	C	3140.358	31834.28	710	Ne II	C
3123.461	32006.49	330	Ne II	C	3141.3320	31824.410	54000 S	Ne II	G
3123.7644	32003.380	1200	Pt II	110258- 78254 K	3141.6559	31821.150	2100	Pt I	18566- 50387 N
3124.1846	31999.074	1900	Ne II	G	3142.20	31815.6	280	Pt II	106434- 74619 K
3124.99	31990.8	96			3143.20	31805.5	210	Pt II	110258- 78452 K
3126.1965	31978.483	12000	Ne I	G	3143.7204	31800.233	8900	Ne II	G
3126.57	31974.7	250			3144.0872	31796.523	540	Pt II	29261- 61058 11
3126.94	31970.9	85			3145.0199	31787.094	1100	Pt II	34647- 66434 19
3127.22	31968.0	59			3145.433	31782.92	140	Ne II	C
3127.77	31962.4	80	Pt II	42031- 73999 K	3147.73	31759.7	280		
3132.01	31919.1	130	Pt II	114455- 82535 K	3148.08	31756.2	42		
3132.1882	31917.312	4400	Ne II	G	3148.6107	31750.844	1500	Ne I	I
3133.01	31908.9	50			3148.6805	31750.140	2000	Ne II	G
3133.5572	31903.368	1900	Pt II	110158- 78254 K	3149.09	31746.0	44		
3133.6714	31902.206	260	Pt I	13496- 45398 E	3149.22	31744.7	73	Pt II	109507- 77763 K

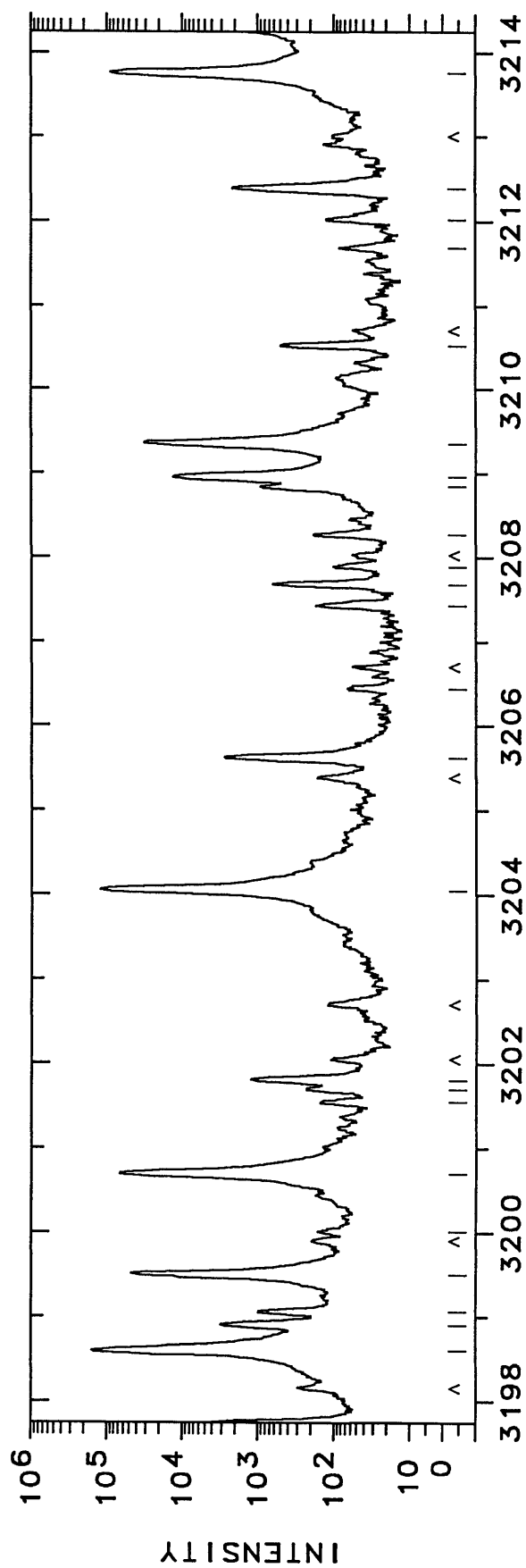
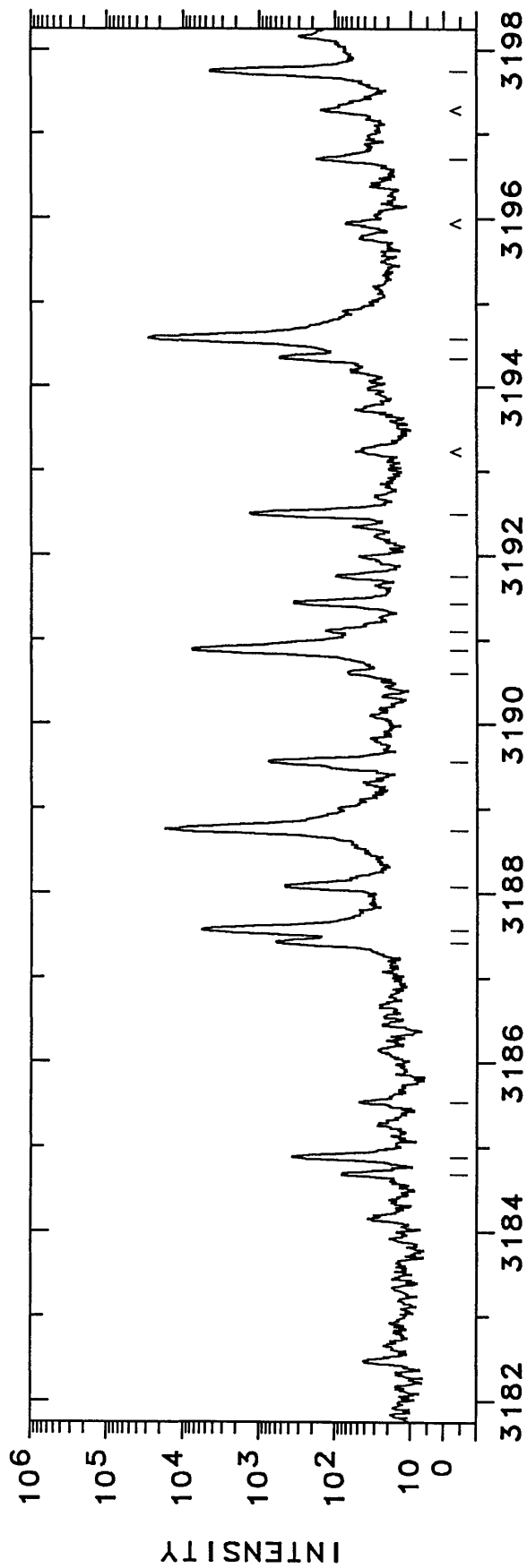


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3151.1364	31725.396	6000	Ne II	G	3165.01	31586.3	200	Ne III	L
3151.58	31720.9	900	Pt II	74241 AK	3165.6479	31579.971	11000	Ne II	G
3151.58	31720.9	900	Ne II	A	3166.180	31574.66	1300	Ne II	C
3151.58	31720.9	900	Pt II	114256- 82535 AK	3166.79	31568.6	140	Pt II	110020- 78452 K
3151.95	31717.2	38	Pt II	46046- 77763 K	3167.2244	31566.252	35000	Pt II	101517- 69953 K
3152.57	31711.0	63	Pt I	68006- 36296 N	3167.55	31561.0	1100	Ne I	
3153.09	31705.7	120	Pt II	110158- 78452 K	3168.12	31555.3	90	Pt II	111162- 79607 K
3153.4107	31702.516	1300	Ne I	I	3169.304	31543.54	290	Ne II	C
3153.678	31699.83	620	Ne II	C	3169.72	31539.4	47		
3153.77	31698.9	100			3169.84	31538.2	120		
3154.51	31691.5	42			3172.27	31514.0	45	Pt II	117340- 85826 K
3154.794	31688.62	1500	Ne II	C	3172.474	31512.03	960	Ne II	C
3156.5625	31670.862	53000	Pt I	10131- 41802 E	3173.5726	31501.115	8600	Ne II	G
3157.33	31663.2	76			3174.37	31493.2	240		
3157.87	31657.7	140			3174.49	31492.0	120	Pt II	46046- 77538 K
3159.0704	31645.721	1800	Pt II	29261- 60907 13	3174.8232	31488.707	660	Pt I	18566- 50055 E
3159.57	31640.7	210	Pt II	117340- 85700 K	3175.12	31485.8	32	Ne III	L
3159.91	31637.3	140	Ne II	A	3175.44	31482.6	31	Pt II	114455- 82972 K
3159.91	31637.3	140	Ne III	AL	3175.61	31480.9	46	Ne III	L
3160.28	31633.6	180			3175.90	31478.0	440	Pt II	121651- 90173 K
3160.52	31631.2	46	Pt II	114455- 82824 K	3176.1199	31475.852	5900	Ne II	G
3161.0013	31626.390	56	Pt II	105388- 73761 30	3176.548	31471.61	1400	Ne II	C
3162.46	31611.8	89			3177.745	31459.76	200	Ne II	C
3163.10	31605.4	51	Pt I	68947- 37342 N	3178.80	31449.3	29		
3163.578	31600.63	300	Ne II	C	3179.02	31447.1	150	Ca II	
3164.231	31594.11	160	Ne II	C	3179.32	31444.2			
3164.4295	31592.129	12000	Ne II	G	3181.58	31421.8	120		
3164.6618	31589.810	31000	Ne II	G					



WAVELENGTH (ANGSTROMS) - AIR

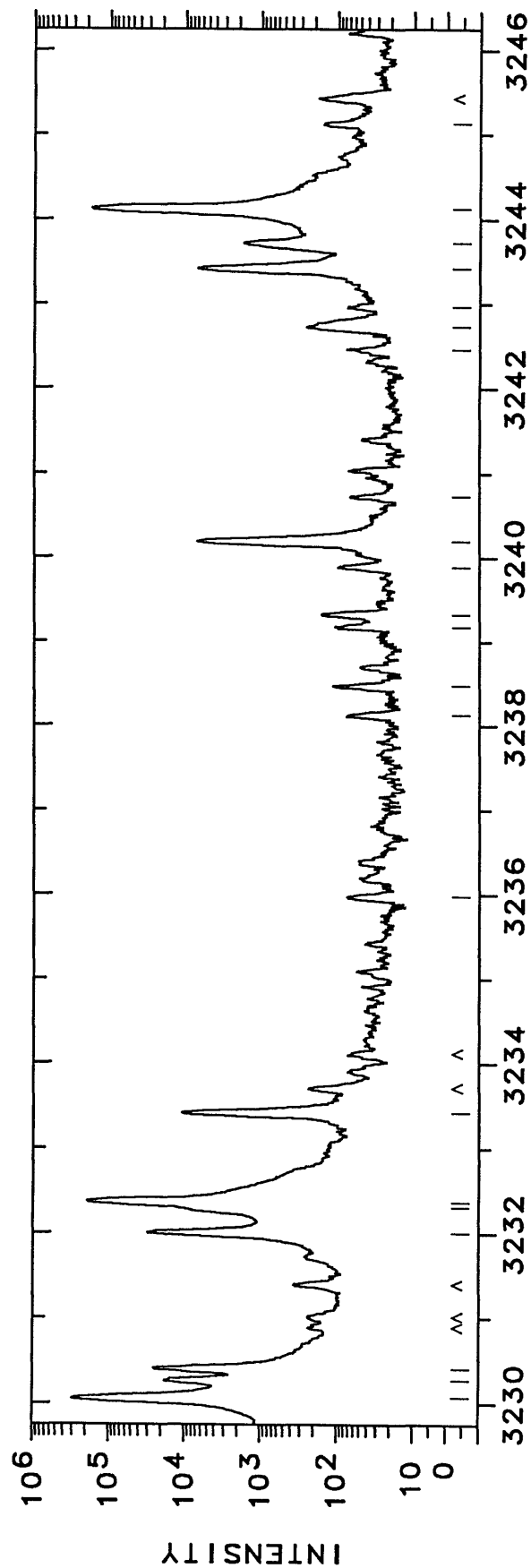
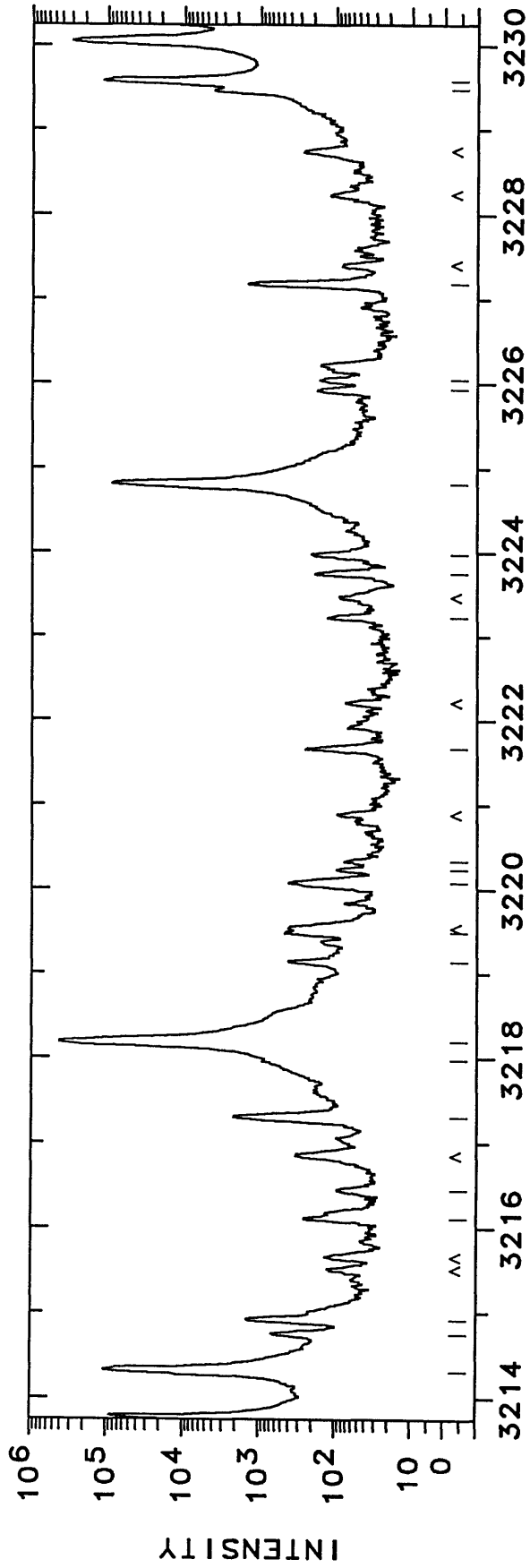
WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3184.68	31391.3	72			3199.06	31250.2	970	Pt II	106434- 75184 AK
3184.88	31389.3	360			3199.5087	31245.768	48000	Pt II	101199- 69953 13
3185.53	31382.9	38			3200.01	31240.9	150	Pt I	68831- 37590 N
3187.42	31364.3	600			3200.7097	31234.044	67000	Pt I	13496- 44730 E
3187.5763	31362.729	5700 L	Ne II	G	3201.55	31225.8	140		
3188.0700	31357.873	450	Pt II	37877- 69235 27	3201.70	31224.4	220		
3188.7410	31351.275	17000	Ne II	G	3201.81	31223.3	1200		
3189.55	31343.3	750	Pt II	105962- 74619 K	3201.615	31201.615	120000	Pt I	6567- 37769 E
3190.60	31333.0	59	Pt II	50564- 81897 K	3205.6023	31186.374	2800	Pt I	65308- 34122 N
3190.8630	31330.426	7600	Ne II	G	3206.44	31178.2	57	Pt I	68947- 37769 N
3191.10	31328.1	120			3207.43	31168.6	160	Pt I	68759- 37590 N
3191.43	31324.9	340	Pt II	105086- 73761 AK	3207.68	31166.2	620	Pt II	110258- 79092 K
3191.43	31324.9	340	Pt I	68169- 36844 AN	3207.89	31164.1	91		
3191.75	31321.7	89	Pt I	68912- 37590 N	3208.27	31160.4	170		
3192.5031	31314.331	1300	Pt I	18566- 49880 E	3208.84	31154.9	920		
3194.34	31296.3	520	Pt II	36484- 67780 K	3208.9647	31153.697	17000	Ne II	G
3194.5754	31294.018	28000	Ne II		3209.3554	31149.905	32000	Ne II	G
3196.70	31273.2	160	Pt II	109527- 78254 K	3210.52	31138.6	490	Pt II	101517- 70379 K
3197.7161	31263.283	4400	Pt II	96614- 65351 12	3211.69	31127.3	73		
3198.5862	31254.779	160000	Ne II	G	3211.994	31124.32	110	Ne II	C
3198.916	31251.56	3100	Ne II	C	3212.3775	31120.602	2100	Pt I	15501- 46622 E
3199.06	31250.2	970	Pt I	68094- 36844 AN	3213.7348	31107.459	88000	Ne II	G



WAVELENGTH (ANGSTROMS) - AIR

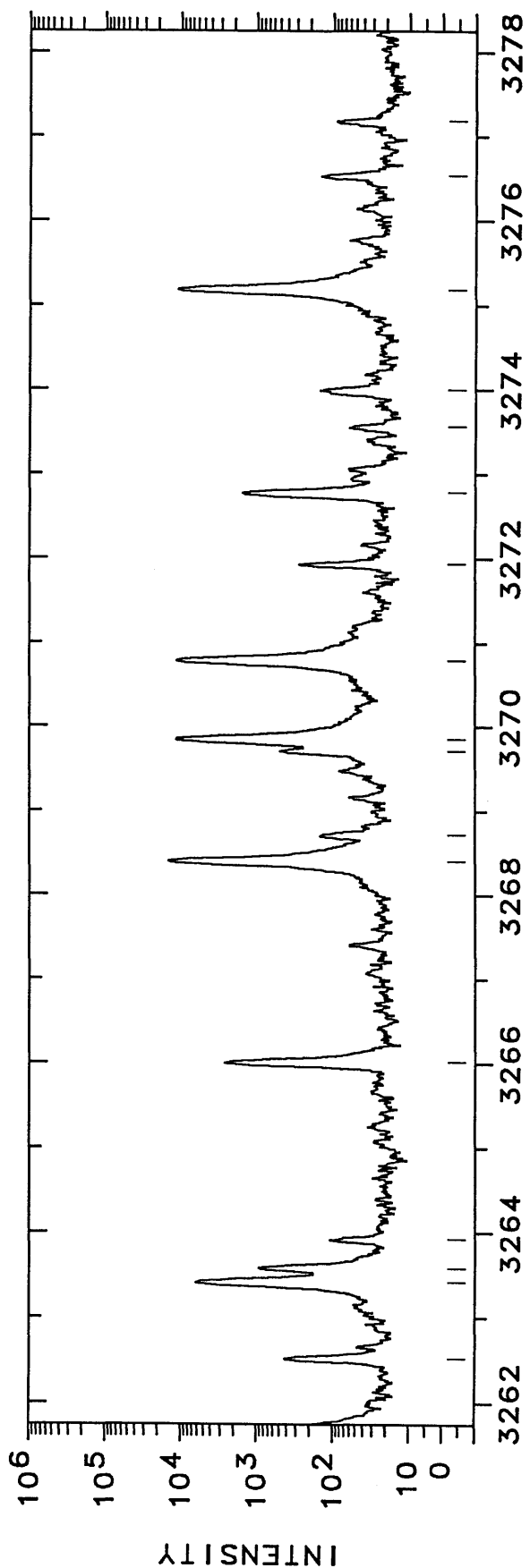
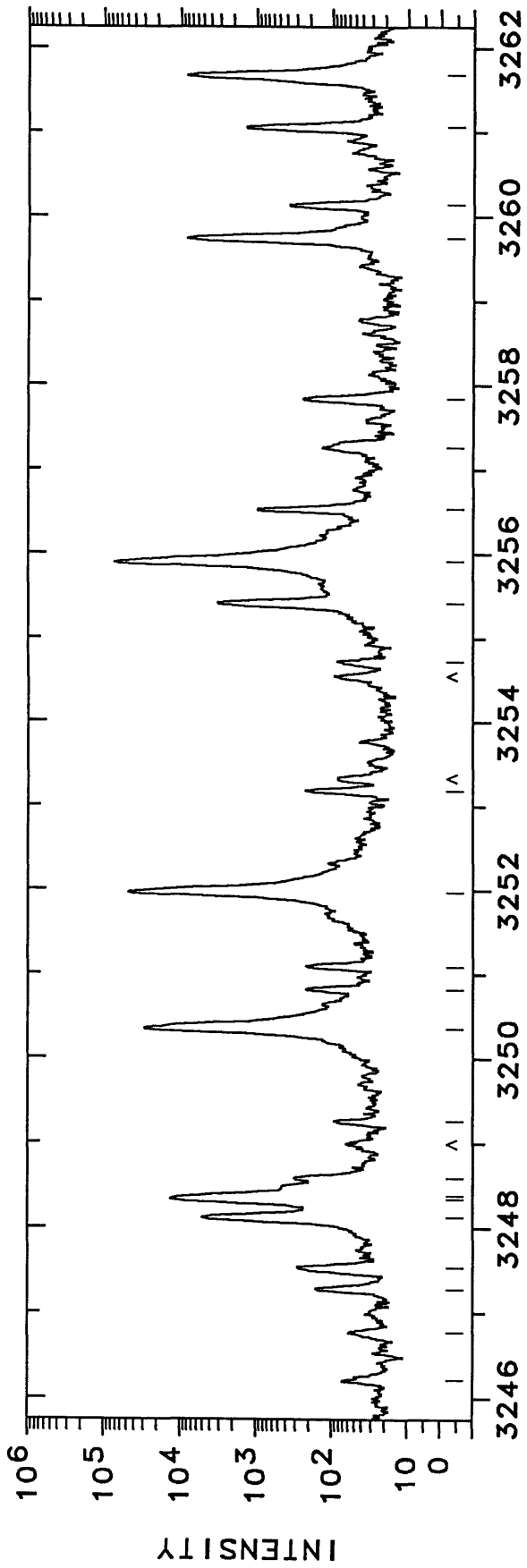


WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3214.3262	31101.735	110000	Ne II	G	3230.0698	30950.148	300000	Ne II	G
3214.756	31097.58	660	Ne II	C	3230.2837	30948.099	18000	Pt I	13496- 44444 E
3214.926	31095.93	1400	Ne II	C	3230.4209	30946.784	26000	Ne II	G
3216.11	31084.5	240			3232.0240	30931.436	31000	Ne II	G
3216.45	31081.2	80			3232.3096	30928.703	5000 U	Pt II	110020- 79092 K
3217.31	31072.9	2200			3232.3731	30928.095	200000 P	Ne II	G
3217.98	31066.4	890			3233.4167	30918.113	11000	Pt I	15501- 46419 E
3218.1925	31064.371	430000	Ne II	G	3235.98	30893.6	59	Pt II	109346- 78452 K
3219.14	31055.2	410	Pt II	109507- 78452 K	3238.13	30873.1	60		
3219.49	31051.9	450			3238.48	30869.8	98		
3220.08	31046.2	400			3239.17	30863.2	92		
3220.24	31044.6	82			3239.32	30861.8	140		
3220.34	31043.7	61			3239.89	30856.3	82		
3221.67	31030.8	230			3240.1957	30853.430	7000	Pt I	10116- 40970 E
3223.23	31015.8	110			3240.73	30848.3	52		
3223.75	31010.8	170	Pt I	65132- 34122 N	3242.46	30831.9	59		
3223.98	31008.6	200	Pt II	43737- 74745 K	3242.73	30829.3	240	Pd I	
3224.8174	31000.556	87000	Ne II	G	3242.96	30827.1	58	Pt I	68169- 37342 N
3225.93	30989.9	160	Pt I	68759- 37769 N	3243.3963	30822.985	6900	Ne II	G
3226.05	30988.7	150	Pt II	116689- 85700 K	3243.7039	30820.062	1700	Pt II	101199- 70379 28
3227.1645	30978.011	1400	Pt I	18566- 49544 E	3244.0942	30816.354	170000	Ne II	G
3229.457	30956.02	4000	Ne II	C	3245.13	30806.5	140		
3229.5717	30954.921	120000	Ne II	G					



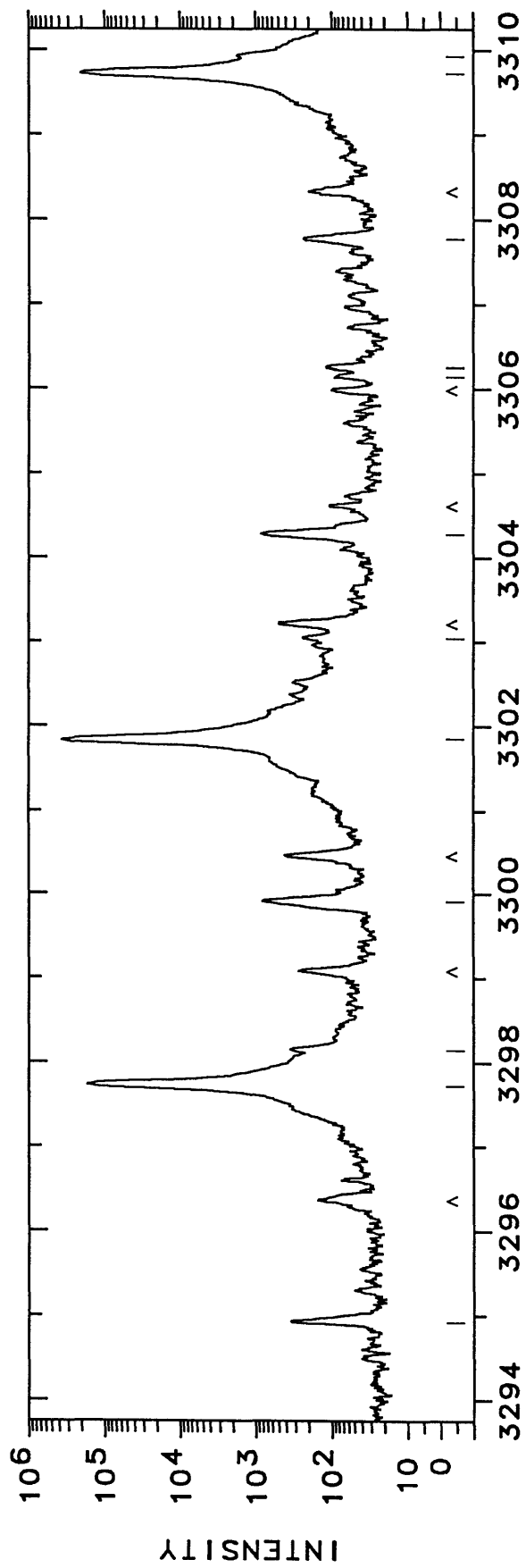
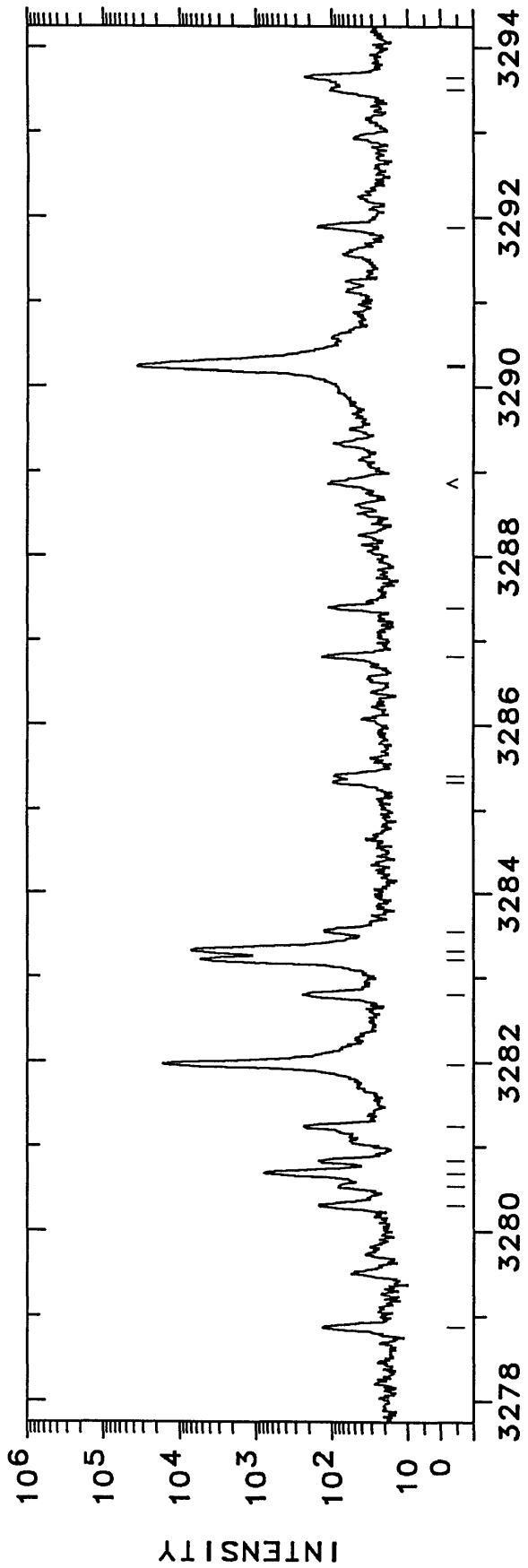
WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3246.21	30796.3	57			3260.14	30664.7	350	Pt I	68006- 37342 N
3246.77	30791.0	44			3261.0683	30655.958	1300	Pt I	10131- 40787 E
3247.28	30786.1	150			3261.6887	30650.127	8200	Pt I	64330- 33680 N
3247.53	30783.8		Cu I		3262.5311	30642.213	410	Pt II	105388- 74745 26
3248.1314	30778.053	5000	Ne II	G	3263.4128	30633.935	6400	Ne II	
3248.3449	30776.030	13000	Ne II	G	3263.58	30632.4	920	Pt I	64312- 33680 N
3248.3787	30775.710	3100	Ne II	G	3263.92	30629.2	94	Pt II	64003- 94633 K
3248.59	30773.7	290			3266.02	30609.5	2600	Pt II	105794- 75184 K
3249.26	30767.4	76			3268.4170	30587.034	15000	Pt I	64267- 33680 N
3250.3571	30756.978	29000	Ne II	G	3268.72	30584.2	130		
3250.82	30752.6	200	Pt I	68094- 37342 N	3269.71	30574.9	470	Pt II	110258- 79683 K
3251.09	30750.0	200			3269.8705	30573.438	12000	Ne II	G
3251.9787	30741.642	47000	Pt I	10131- 40873 E	3270.8010	30564.741	11000	Ne II	G
3253.18	30730.3	200	Pt I	68072- 37342 N	3271.94	30554.1	260		
3254.72	30715.8	69			3272.78	30546.3	1600	Pt I	64668- 34122 N
3255.4223	30709.124	3100	Ne II	G	3273.56	30539.0	46	Pt II	110146- 79607 K
3255.9088	30704.536	72000	Pt I	6140- 36844 E	3274.00	30534.9	130	Cu I	
3256.53	30698.7	930	Pt I	64379- 33680 N	3275.1810	30523.866	11000	Ne II	G
3257.26	30691.8	120			3276.54	30511.2	130		
3257.84	30686.3	230			3277.19	30505.2	76		
3259.7308	30668.536	8200	Pt I	15501- 46170 E					



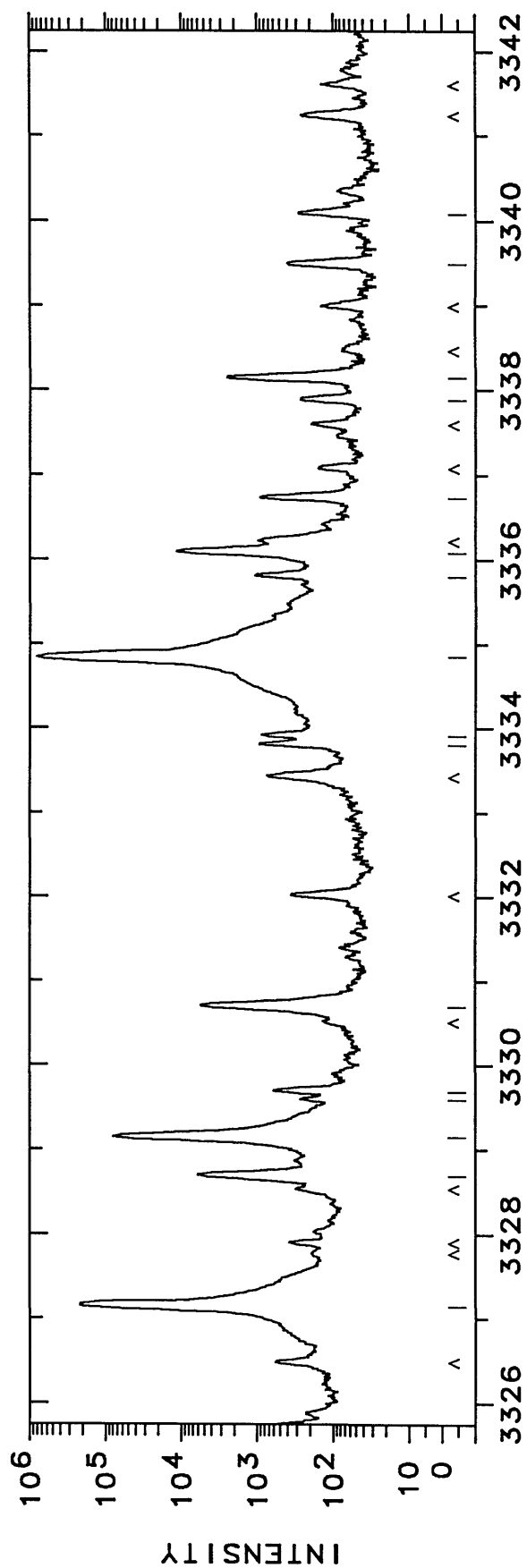
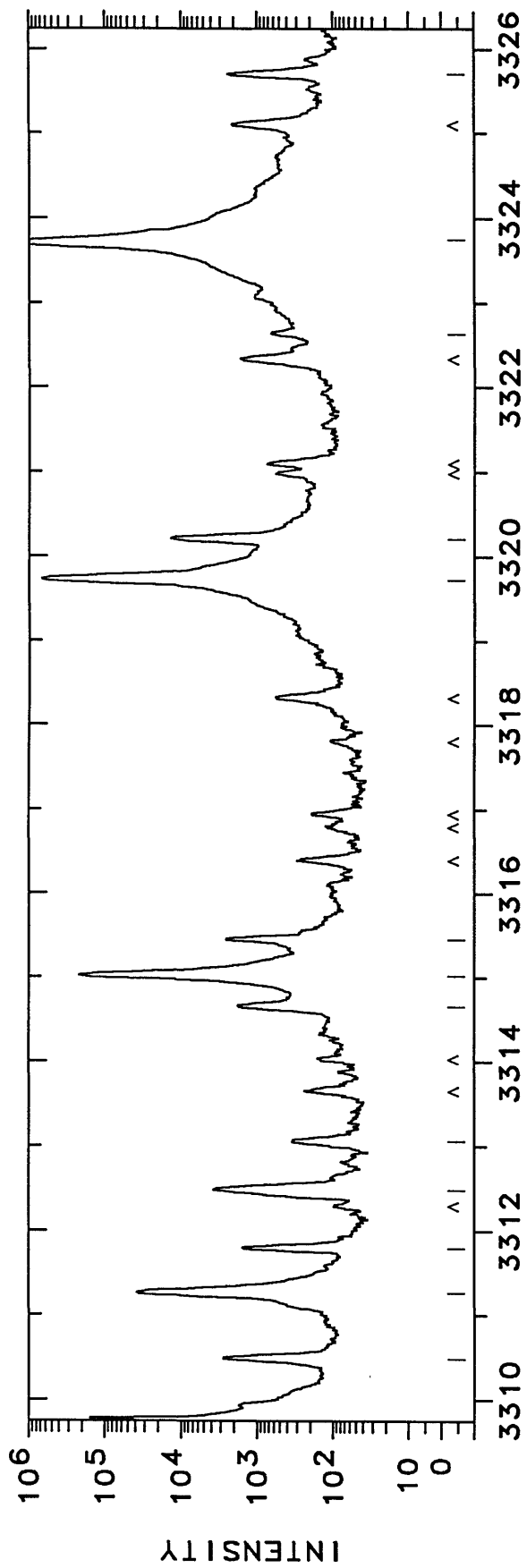
WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3278.87	30489.5	120			3290.2517	30384.060	6000 U		
3280.30	30476.2	130			3291.88	30369.0	140		
3280.53	30474.1		Rh I		3293.50	30354.1	90	Pt II	104763- 74409 K
3280.68	30472.7		Ag I		3293.64	30352.8	210	Pt I	68121- 37769 N
3280.83	30471.3	130	Pt I	21967- 52438 N	3294.92	30341.0	330	Pt II	105086- 74745 K
3281.24	30467.5	220	Pt II	105086- 74619 AK	3297.7252	30315.203	170000	Ne II	
3281.24	30467.5	220	Pt II	119057- 88589 AK	3298.15	30311.3	330	Pt II	104930- 74619 K
3281.9670	30460.756	17000	Pt I	64141- 33680 E	3299.91	30295.1	790	Pt I	68831- 38536 N
3282.80	30453.0	230			3301.8596	30277.246	370000	Pt I	6567- 36844 E
3283.2046	30449.274	5300	Pt I	13496- 43945 E	3303.04	30266.4	230		
3283.3086	30448.310	7000	Pt I	64128- 33680 E	3304.28	30255.1	820		
3283.54	30446.2		Rh I		3306.14	30238.0	76	Pt I	68006- 37769 N
3285.33	30429.6	80			3306.25	30237.0	100		
3285.40	30428.9	77	Pt II	105794- 75365 K	3307.77	30223.1	220	Pt I	68759- 38536 N
3286.81	30415.9	120	Pt II	109507- 79092 K	3309.7398	30205.161	210000	Ne II	
3287.39	30410.5	94			3309.9493	30203.250	1700	Pt II	105388- 75184 26
3290.2196	30384.356	36000	Pt I	10131- 40516 E					



WAVELENGTH (ANGSTROMS) - AIR

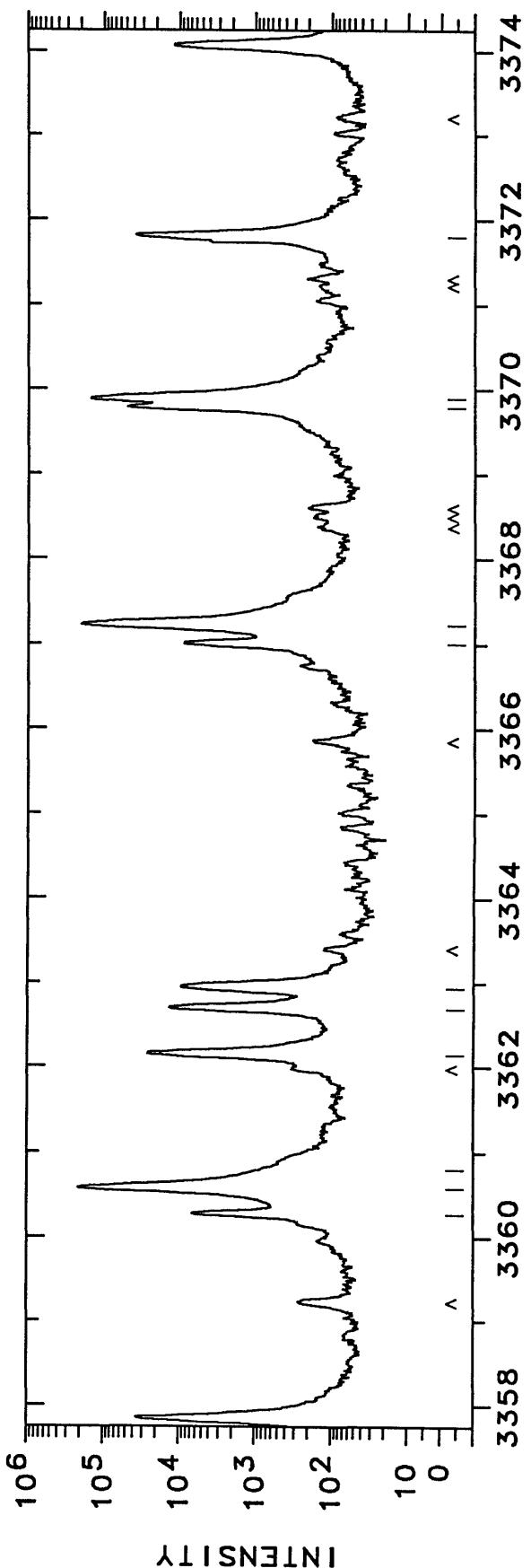
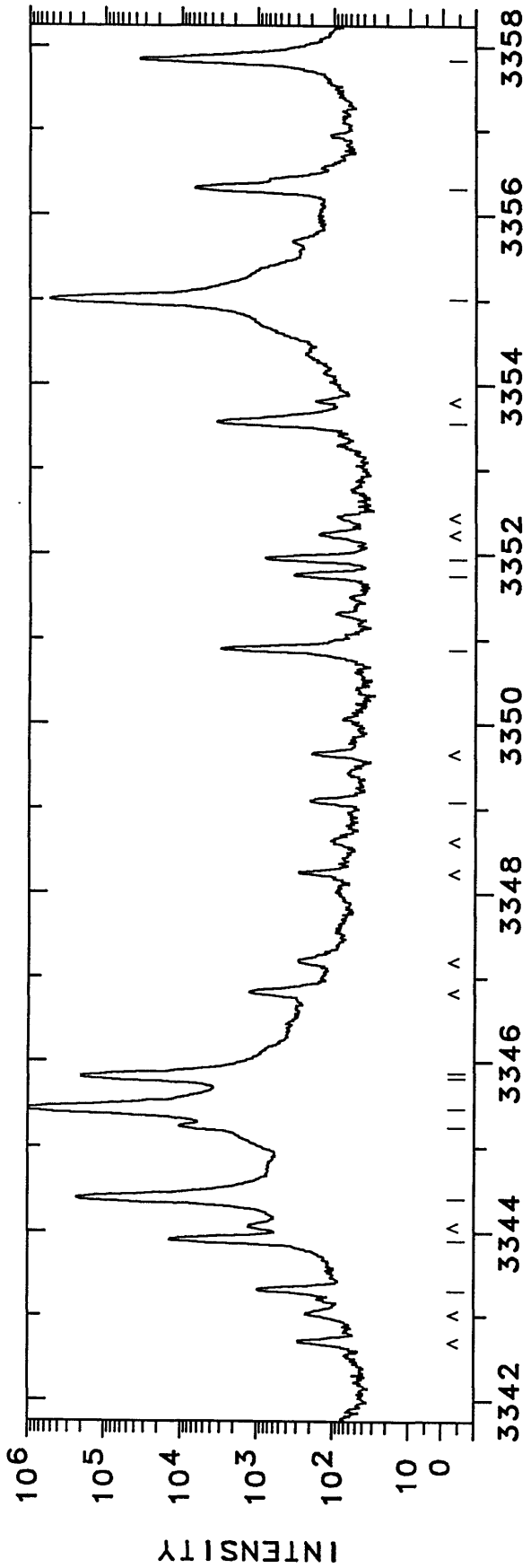
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3310.499	30198.24	2800	Ne II	C	3328.6977	30033.140	6000	Ne III	L
3311.2711	30191.193	37000	Ne II	G	3329.1575	30028.992	80000	Ne II	G
3311.7986	30186.385	1500	Pt I	66967- 36781	3329.59	30025.1	260		
3312.4818	30180.159	3700	Pt I	68716- 38536 AN	3329.69	30024.2	590	Pt II	43737- 73761 K
3312.4818	30180.159	3700	Pt II	96614- 66434 A	3330.7335	30014.784	5500	Ne II	G
3313.06	30174.9	330			3333.80	29987.2	920		
3314.674	30160.20	1800	Ne II	C	3333.91	29986.2	860		
3315.0419	30156.852	220000	Pt I	0- 30156 E	3334.8368	29977.853	820000	Ne II	G
3315.45	30153.1	2500	Pt II	101517- 71364 K	3335.8163	29969.051	1100	Pt I	18566- 48535 E
3319.7246	30114.315	680000	Ne II	G	3336.0922	29966.572	11000	Ne II	G
3320.1973	30110.028	14000	Ne II	G	3336.73	29960.8	900	Pt II	110158- 80197 K
3322.63	30088.0	640			3337.9063	29950.287	250	Pt II	36484- 66434 20
3323.7350	30077.980	1900000	Ne II	G	3338.14	29948.2	2500	Pt I	62567- 32620 N
3325.70	30060.2	2400	Pt I	64182- 34122 N	3339.49	29936.1	390		
3325.70	30060.2	2400	Pt II	110257- 80197 K	3340.08	29930.8	270	Pt II	41434- 71364 K
3327.1534	30047.079	220000	Ne II	G					



WAVELENGTH (ANGSTROMS) - AIR



WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3343.30	29902.0	960	Pt II	105086- 75184	3357.8190	29772.680	36000	Ne II	G
3343.8961	29896.640	14000	Pt I	15501- 45398	3360.2707	29750.958	6600	Ne II	G
3344.3956	29892.175	230000	Ne II		3360.5977	29748.063	210000	Ne II	G
3345.2555	29884.491	10000	Pt II	101199- 71314	3360.8058	29746.222	1000	Ne II	G
3345.4544	29882.715	1200000	Ne II		3362.1623	29734.220	26000	Ne II	G
3345.8304	29879.356	210000	Ne II		3362.7067	29729.407	14000	Ne II	G
3345.8678	29879.023	15000 U			3362.9378	29727.363	9400 L	Ne II	G
3349.08	29850.4	190			3366.9903	29691.585	8900	Pt I	13496- 43187
3350.88	29834.3	3000	Pt II	101199- 71364	3366.9903	29691.585	8900	Ne II	A
3351.7492	29826.595	320	Ne I		3366.9903	29691.585	8900	Ne II	A
3351.94	29824.9	800	Pt II	106434- 76610	3367.2164	29689.592	200000	Ne II	G
3353.567	29810.43	3400	Ne II		3369.8073	29666.766	49000	Ne I	G
3355.0176	29797.539	550000	Ne II		3369.9068	29665.890	150000	Ne I	G
3356.3078	29786.084	6800	Ne II		3371.797	29649.26	39000	Ne II	C

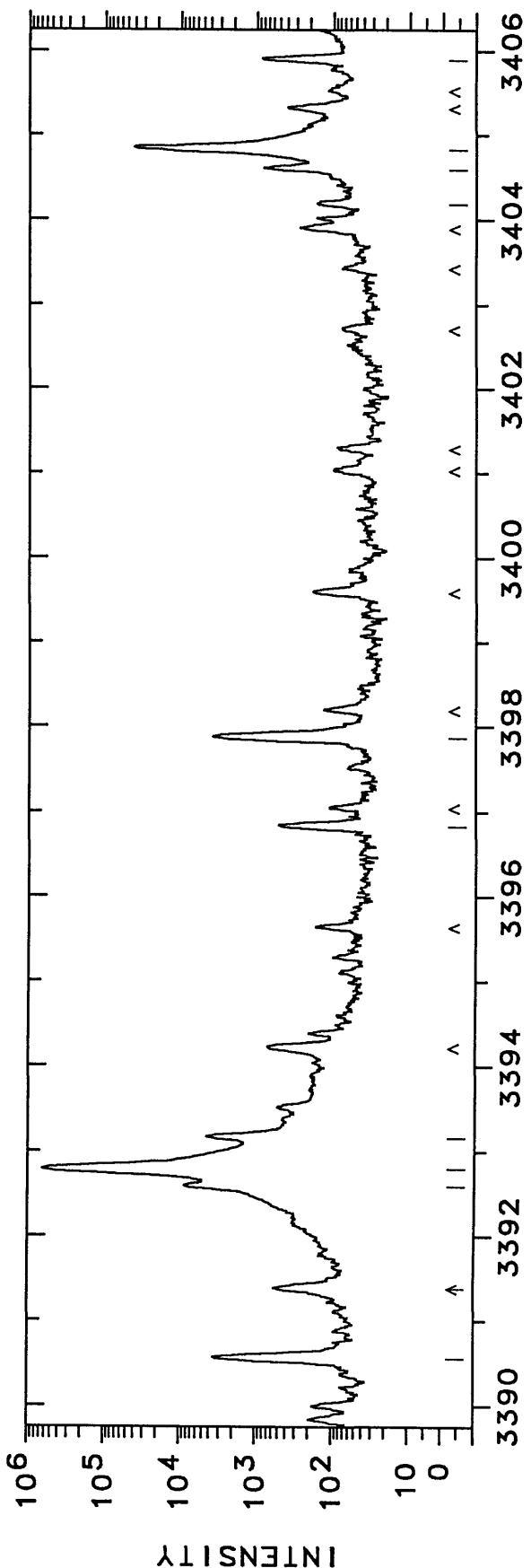
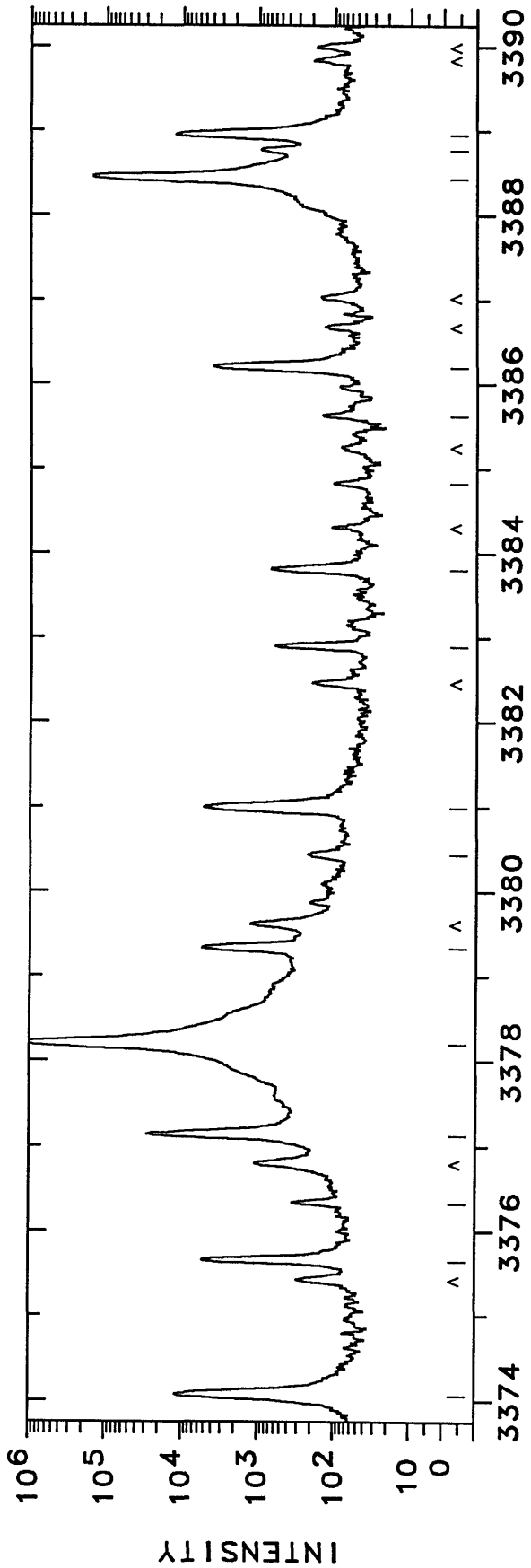


WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3374.0607	29629.368	12000	Ne II	G
3375.6490	29615.427	5300	Ne I	B
3376.33	29609.5	330	Pt II	112433- 82824 K
3377.1543	29602.228	28000	Ne II	G
3378.2193	29592.895	1200000	Ne II	G
3379.3209	29583.249	5500	Ne II	G
3380.44	29573.5	200		
3380.99	29568.6	5200	Pt II	101517- 71948 K
3382.89	29552.0		Ag I	
3383.8121	29543.986	670	Pt II	36484- 66028 15
3384.82	29535.2	83	Pt II	46046- 75581 K
3385.62	29528.2	130		
3386.202	29523.13	4000	Ne II	C
3388.4169	29503.837	150000	Ne II	G

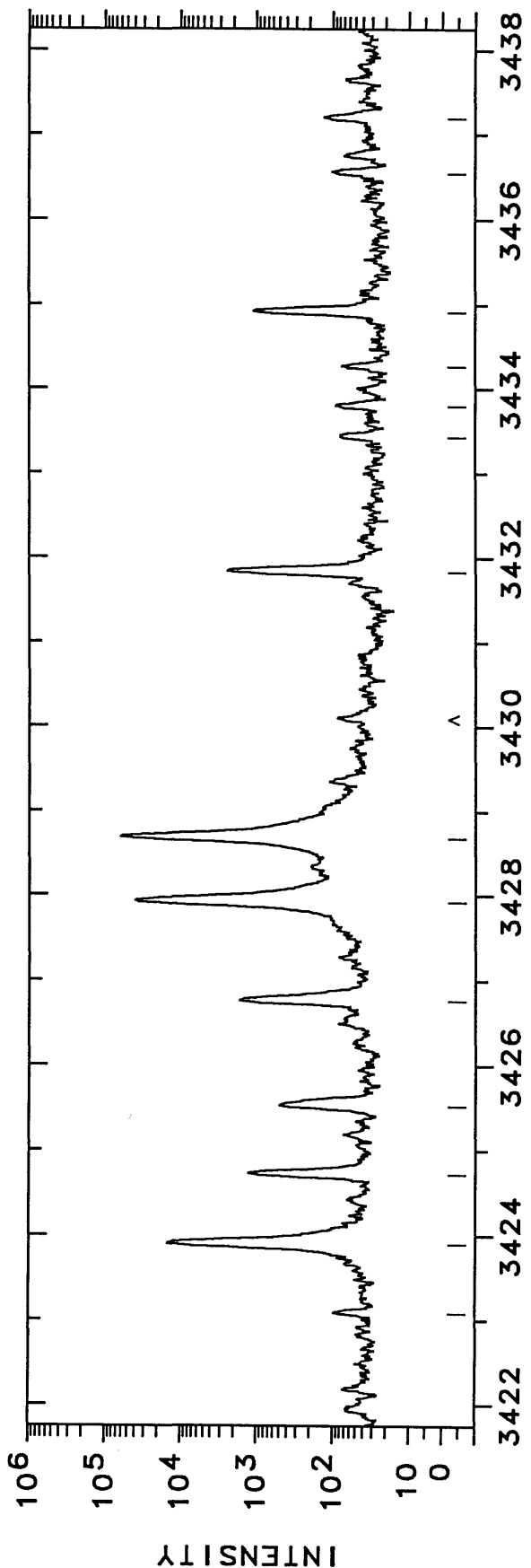
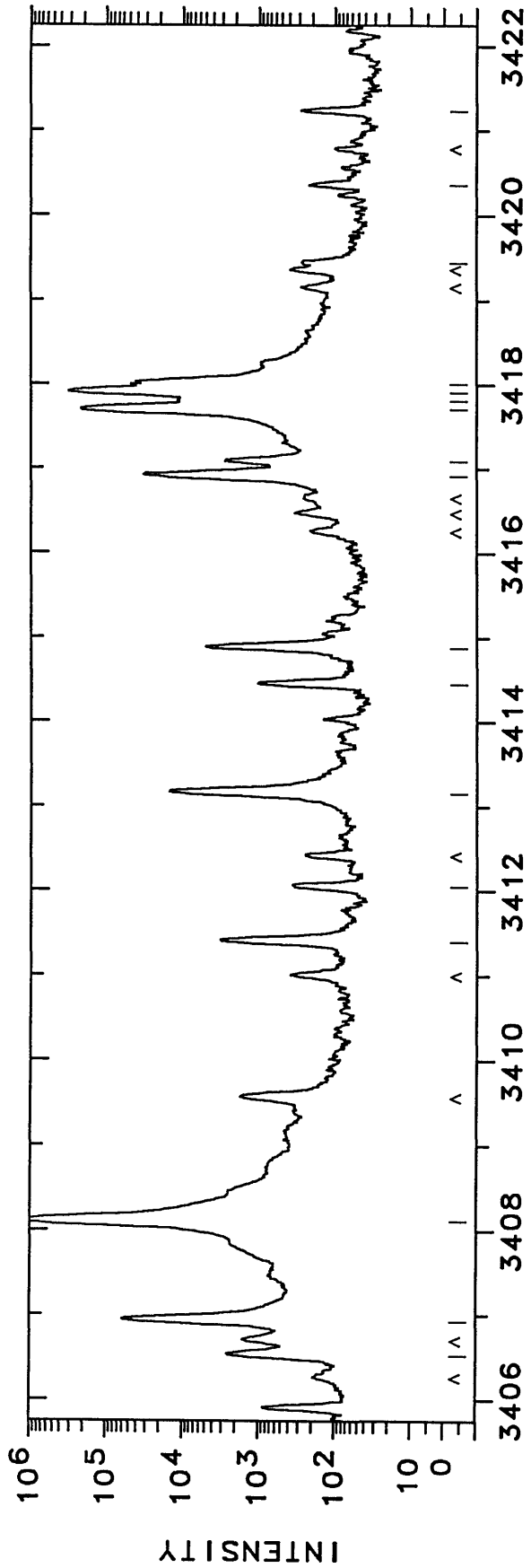
  

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3388.77	29500.8	920	Pt II	105962- 76461 K
3388.9431	29499.256	12000	Ne II	G
3390.552	29485.26	3500	Ne II	C
3391.38	29478.1	550	Pt II	64003- 93482 KM
3392.606	29467.41	8700	Ne II	C
3392.8006	29465.717	650000	Ne II	G
3393.1812	29462.412	4400	Ne II	G
3396.83	29430.8		Rh I	
3397.866	29421.79	3800	Ne II	C
3404.18	29367.2	140		
3404.59	29363.7		Pd I	
3404.8208	29361.696	42000	Ne II	G
3405.89	29352.5	830	Pt II	105962- 76610 K



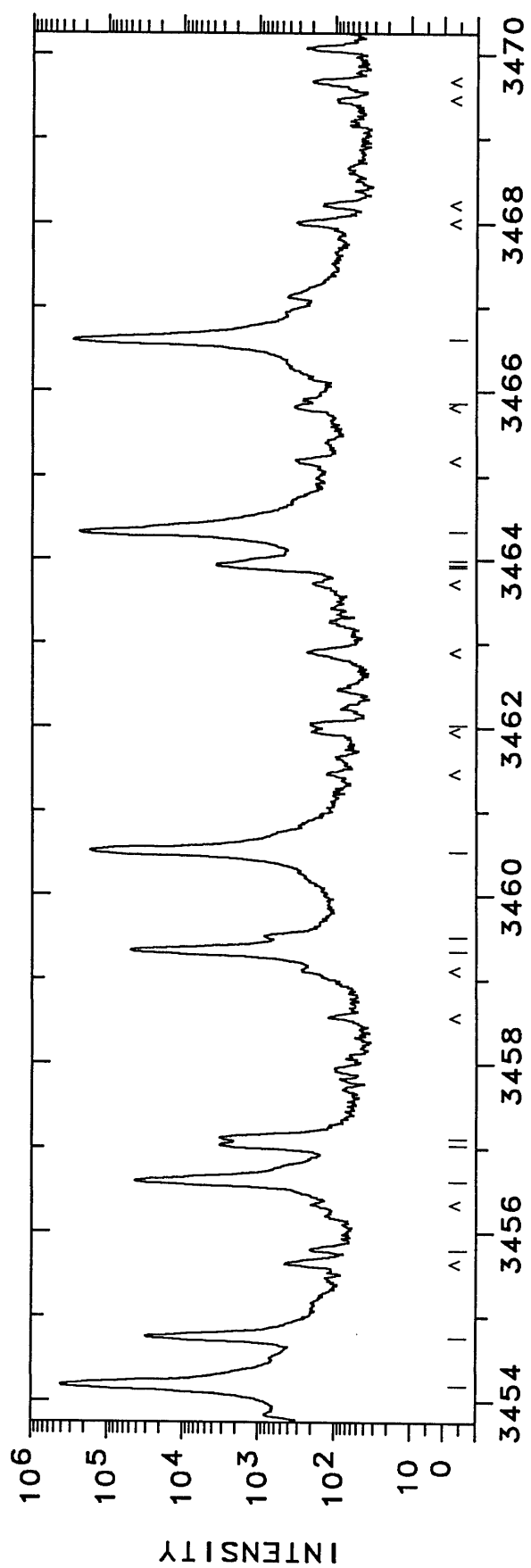
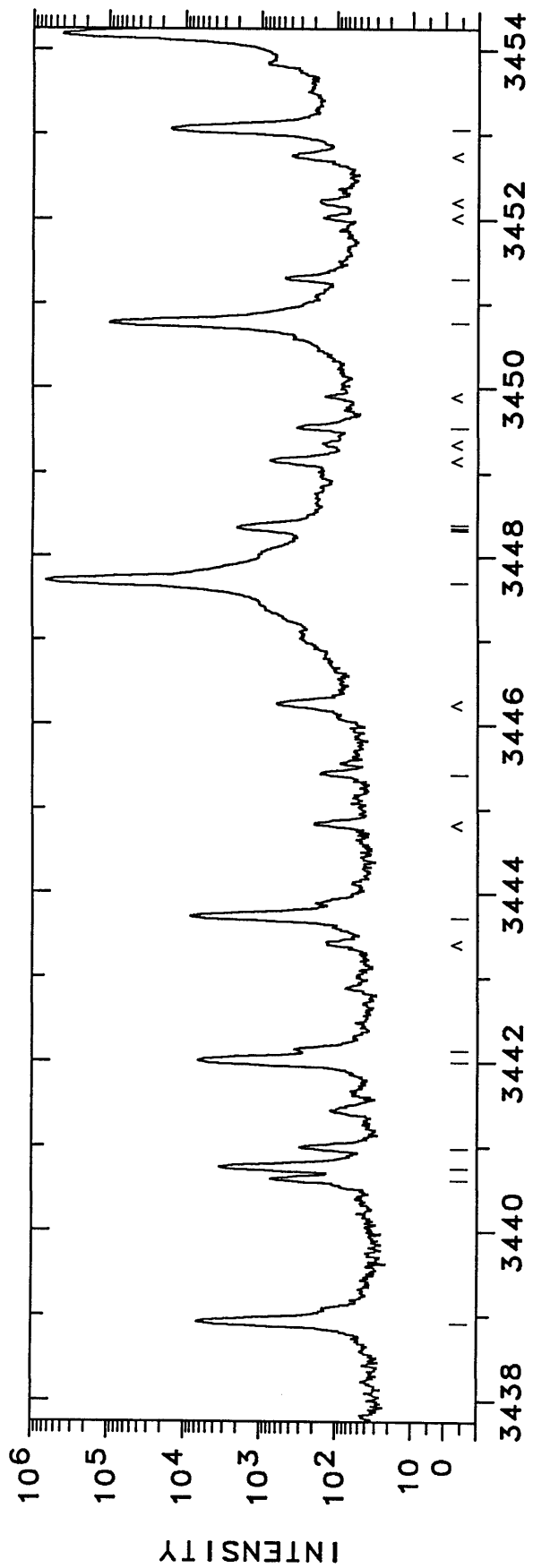
WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3406.52	29347.1	2500	Pt I	64668-35321	3421.2218	29220.943	260	Pd I	
3406.9451	29343.389	60000	Ne II		3423.08	29205.1	74		
3408.1308	29333.181	1300000 C	Pt I	823-30156	3423.9126	29197.981	15000	Ne I	B
3411.3604	29305.412	3200	Ne II		3424.7283	29191.027	1300	Pt I	68006-38815
3412.0248	29299.705	350	Pt II	110158-80858	3425.5299	29184.195	480	Pt I	64505-35321
3413.1453	29290.087	15000	Ne II		3426.7263	29174.006	1600 L	Pt I	18566-47740
3414.4564	29278.841	1000	Pt I	68094-38815	3427.9268	29163.790	40000	Pt I	13496-42660
3414.8886	29275.135	5000	Ne II		3428.6850	29157.340	62000	Ne II	
3416.9126	29257.794	33000	Ne II		3431.8551	29130.408	2400	Pt I	21967-51097
3417.0828	29256.337	2800	Pt I	68072-38815	3433.42	29117.1	57		
3417.6870	29251.165	220000	Ne II		3433.79	29114.0	70	Pt II	121651-92537
3417.8034	29250.169	12000 P	Pt II	101199-71948	3434.26	29110.0	54		
3417.9029	29249.318	320000	Ne I		3434.8865	29104.701		Rh I	
3418.0052	29248.441	35000 P	Ne I		3436.54	29090.7	79	Pt I	65387-36296
3419.44	29236.2	250			3437.19	29085.2	110		
3420.3407	29228.471	200	Pt I	15501-44730					



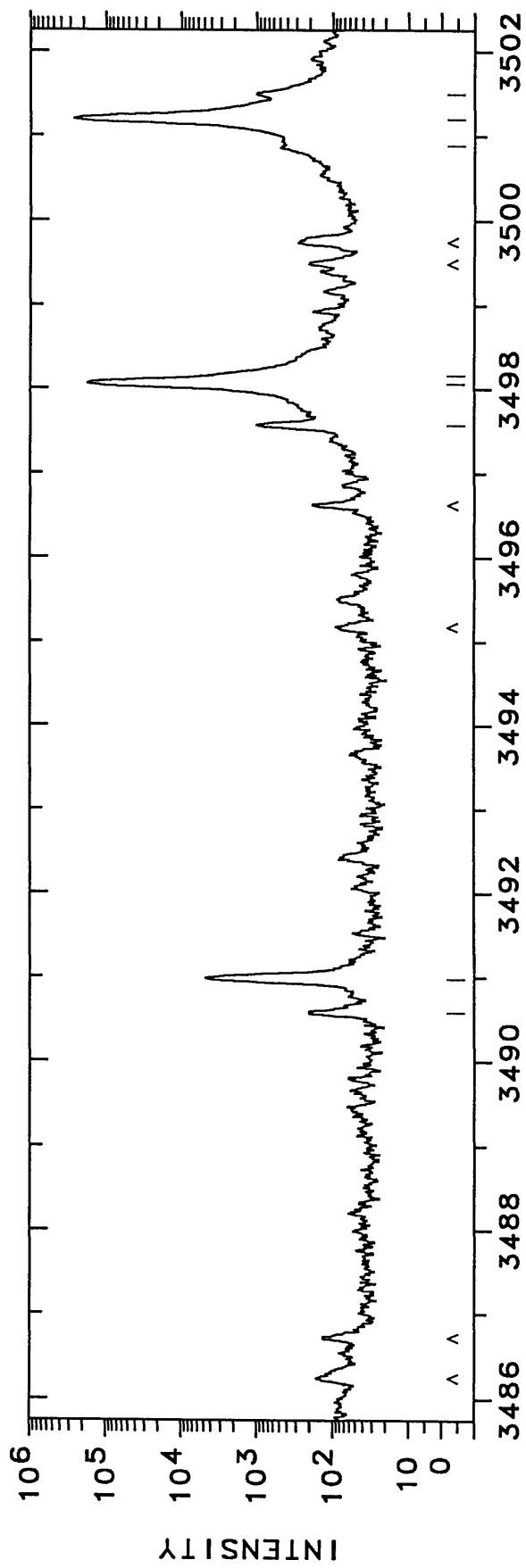
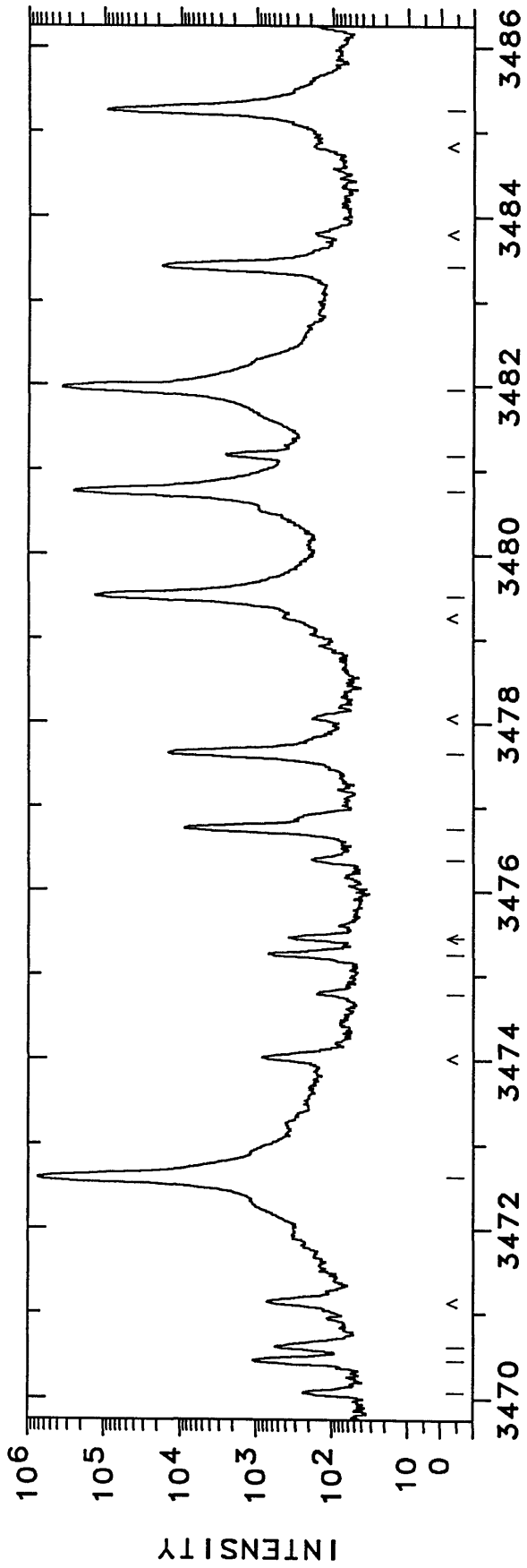
WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3438.9331	29070.453	6600	Ne II	G	3454.1940	28942.022	410000	Ne I	G
3440.6059	29056.320		Fe I	R	3454.7720	28937.180	30000	Ne II	G
3440.7474	29055.125	3400	Ne II	G	3455.7881	28928.672	190	Pt II	48591-77519 K
3440.9887	29053.088		Fe I	R	3456.6081	28921.809	43000	Ne II	G
3441.9762	29044.753	6500	Ne II	G	3457.0079	28918.464	3300	Ne II	G
3442.1028	29043.685	330			3457.084	28917.83	3300	Ne II	C
3443.7065	29030.159	8200	Ne II	G	3459.3197	28899.140	50000	Ne II	G
3445.41	29015.8	140			3459.4946	28897.679	820	Pt I	E
3447.7022	28996.516	660000	Ne I	G	3460.5233	28889.089	170000	Ne I	G
3448.3169	28991.348	700 U	Pt I	H	3462.03	28876.5		Rh I	
3448.3424	28991.133	2000	Pt I	64312-35321 H	3463.9094	28860.849	1200 U	Pt I	64182-35321 H
3448.3817	28990.803	600 P	Pt I	64312-35321 H	3463.9340	28860.644	3600 P	Pt I	64182-35321 H
3449.5082	28981.336	310			3463.9873	28860.200	1000	Pt I	64182-35321 H
3450.7642	28970.788	97000	Ne I	G	3464.3377	28857.281	240000	Ne I	G
3451.2854	28966.413	460			3465.8607	28844.601		Fe I	R
3453.0685	28951.455	15000	Ne II	G	3466.5778	28838.634	290000	Ne I	G



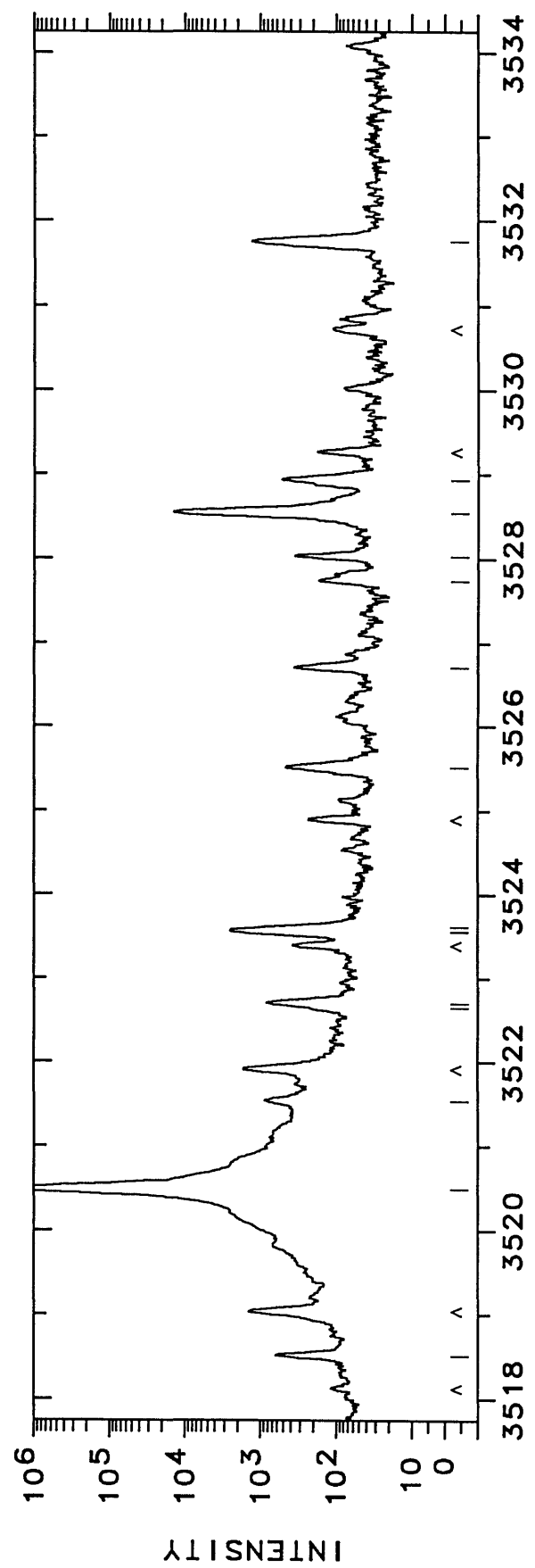
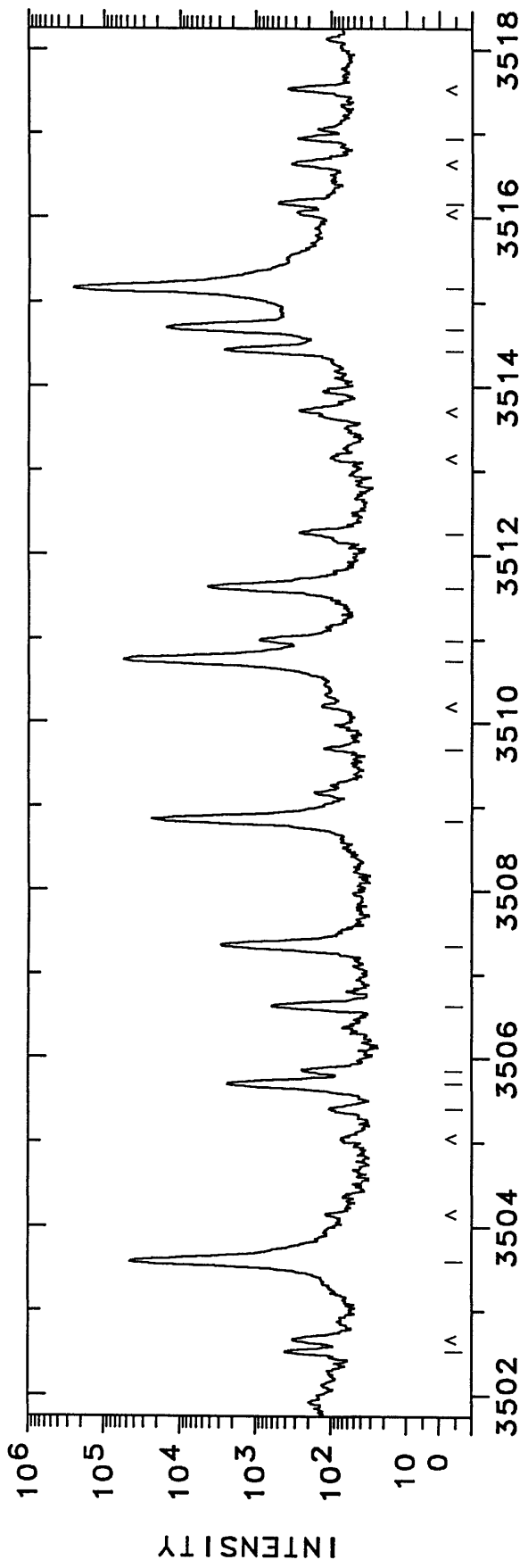


WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3470.07	28809.6	210			3481.1429	28717.977		Pd I	A
3470.4444	28806.505	1100			3481.9337	28711.455	360000	Ne II	G
3470.6071	28805.154	530			3483.4231	28699.179	18000	Pt I	10116- 38815
3472.5701	28788.871	750000	Ne I	G	3485.2641	28684.020	92000	Pt I	10131- 38815
3474.78	28770.6		Rh I		3490.5739	28640.388		Fe I	R
3475.241	28766.75	670	Ne II	C	3490.9998	28636.894	4700 C	Pt I	68831- 40194
3475.4502	28765.015		Fe I	MR	3497.5624	28583.163	980	Pt I	62705- 34122
3476.37	28757.4	160			3498.0635	28579.068	180000	Ne I	G
3476.7600	28754.179	8800	Pt I	6567- 35321	3498.1646	28578.243	2300 P	Ne I	26638- 55216
3477.6466	28746.848	14000	Ne II	G	3500.8873	28556.017	600 P	Pt II	114256- 85700
3479.5193	28731.377	130000	Ne II	G	3501.2158	28553.338	270000	Ne I	G
3480.7181	28721.482	250000	Ne II	G	3501.4968	28551.047	980	Pt I	65395- 36844
3481.1429	28717.977	2500	Pt I	68912- 40194					N



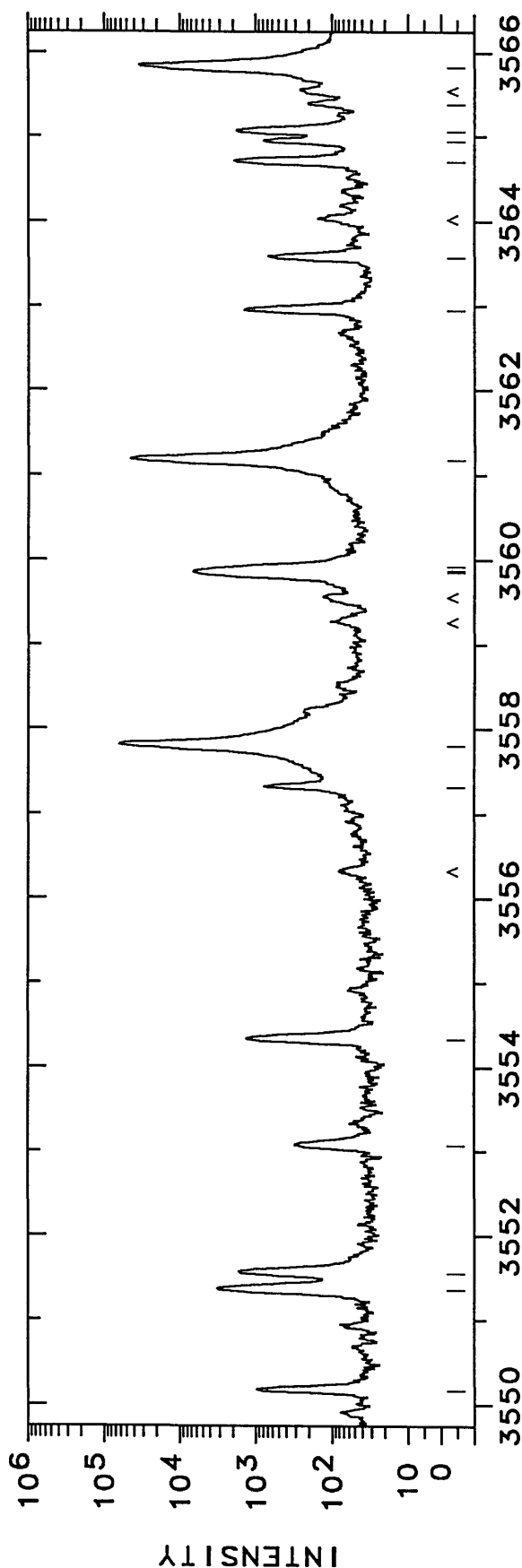
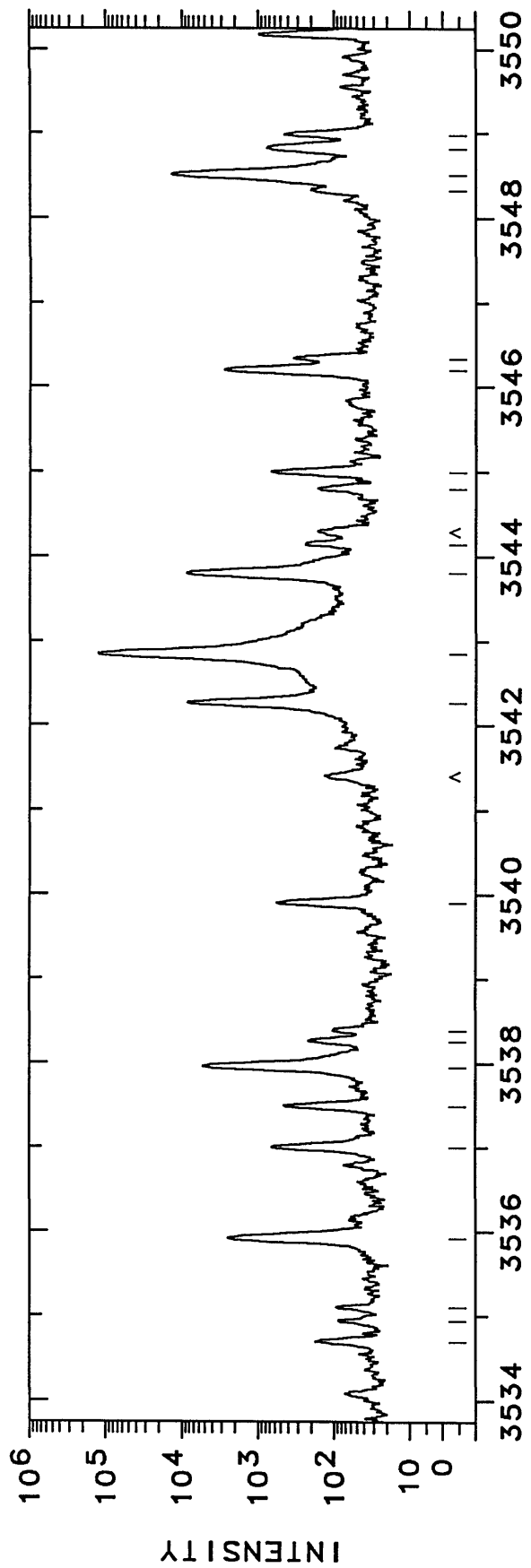
WAVELENGTH (ANGSTROMS) - AIR

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3502.5154	28542.744		Rh I		3516.9422	28425.663		Pd I	
3503.5820	28534.055	45000	Ne II	G	3518.4850	28413.199	600	Ne I	G
3505.40	28519.3	80	Pt II	41434- 69953	3520.4707	28397.172	1700000	Ne I	
3505.6874	28516.919	2300 C	Pt I	65361- 36844	3521.54	28388.6	850		
3505.85	28515.6	220	Pt II	116689- 88173	3522.6501	28379.604	350	Ne II	C
3506.6335	28509.226	580	Pt I	68703- 40194	3522.724	28379.01	550	Pt I	64668- 36296
3507.364	28503.29	2800	Ne II	101517- 73026	3523.5520	28372.341	400 U	Pt I	64668- 36296
3508.8500	28491.217	24000	Pt II		3523.5736	28372.167	2000 P	Pt I	64668- 36296
3509.68	28484.5	98			3523.6105	28371.870	350 P	Pt I	64668- 36296
3510.7214	28476.029	54000	Ne I	G	3525.51	28356.6	430		
3510.9507	28474.170	860			3526.71	28346.9	330	Pt II	42031- 70379
3511.5797	28469.07	4200	Ne II	C	3527.74	28338.7	150	Pt II	111162- 82824
3512.25	28463.6	240			3528.03	28336.3		Rh I	
3514.4480	28445.835	2600	Pt I	62567- 34122	3528.5348	28332.276	14000	Pt I	21967- 50299
3514.7134	28443.688	15000	Pt I	15501- 43945	3528.9426	28329.002	500	Pt II	121651- 93322
3515.1899	28439.832	260000	Ne I	G	3531.7516	28306.471	1300 L	Pt I	13496- 41802
3516.1820	28431.808	480	Pt I	66967- 38536					



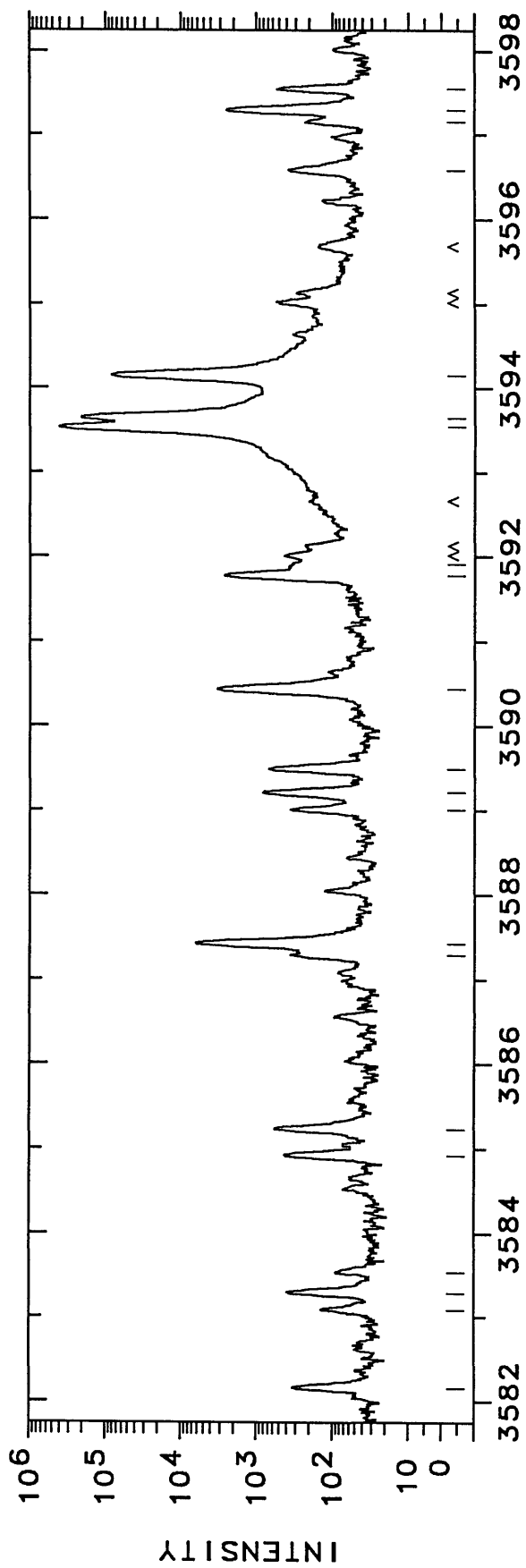
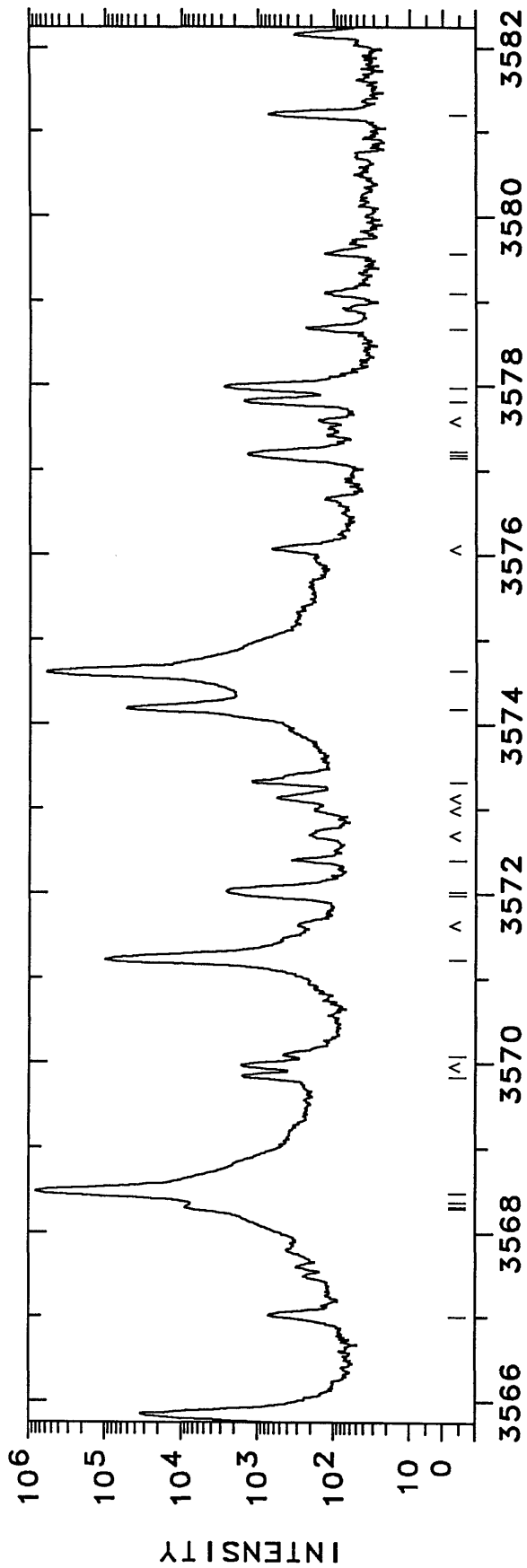
WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	
3534.69	28282.9	150			3548.9635	28169.193	430	Pt II	121651- 93482	K
3534.94	28280.9	62			3550.1696	28159.624	950	Pt I	68947- 40787	N
3535.10	28279.7	68			3551.3553	28150.222	3200	L	37877- 66028	22
3535.8934	28273.315	2500	L	16	3551.557	28148.62	1600	H		C
3537.002	28264.45	630		C	3553.07	28136.6		Pd I		
3537.5014	28260.463	430		K	3554.3563	28126.455	1300			
3537.9757	28256.674	5300		G	3557.313	28103.08	750	Ne II		C
3538.26	28254.4	190			3557.8055	28099.188	64000	Ne II		G
3538.39	28253.4	78			3559.8455	28083.086	2500	P		
3539.897	28241.34	550		C	3559.8455	28083.086	2500	P	64379- 36296	AH
3542.2406	28222.654	8500		G	3559.8748	28082.855	3500	P	64379- 36296	H
3542.8452	28217.838	130000		G	3559.9178	28082.515	1000	P	64379- 36296	H
3543.7907	28210.310	8700		G	3561.1990	28072.413	46000	Ne II		G
3544.14	28207.5	210			3562.9541	28058.584	1400	Ne I		B
3544.815	28202.16	140		C	3563.5851	28053.617	660	Pt I	65395- 37342	N
3545.0094	28200.612	650		E	3564.6881	28044.936	1900	Pt I	65387- 37342	N
3546.2099	28191.065	2700		G	3564.9264	28043.062	760	Pt I	21967- 50010	N
3546.33	28190.1	320		K	3565.0472	28042.111	1800			
3548.32	28174.3	180			3565.3790	28039.502		Fe I		R
3548.5211	28172.705	14000		23	3565.8232	28036.008	34000	Ne II		G
3548.8143	28170.377	740		E						



WAVELENGTH (ANGSTROMS) - AIR

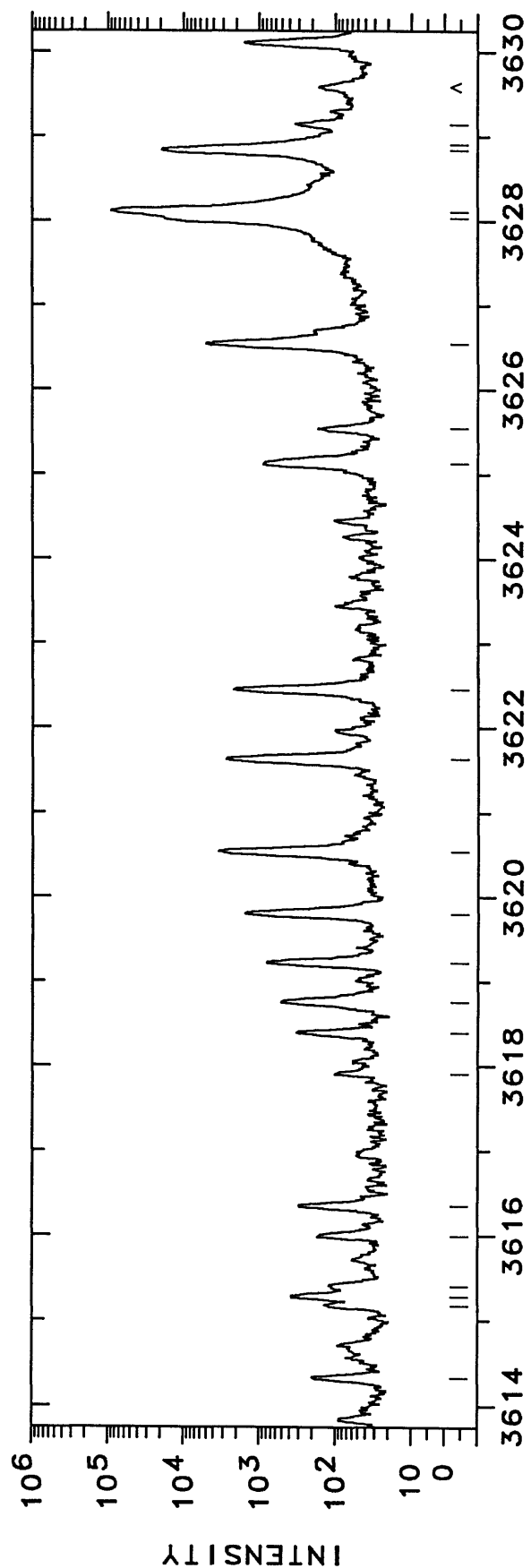
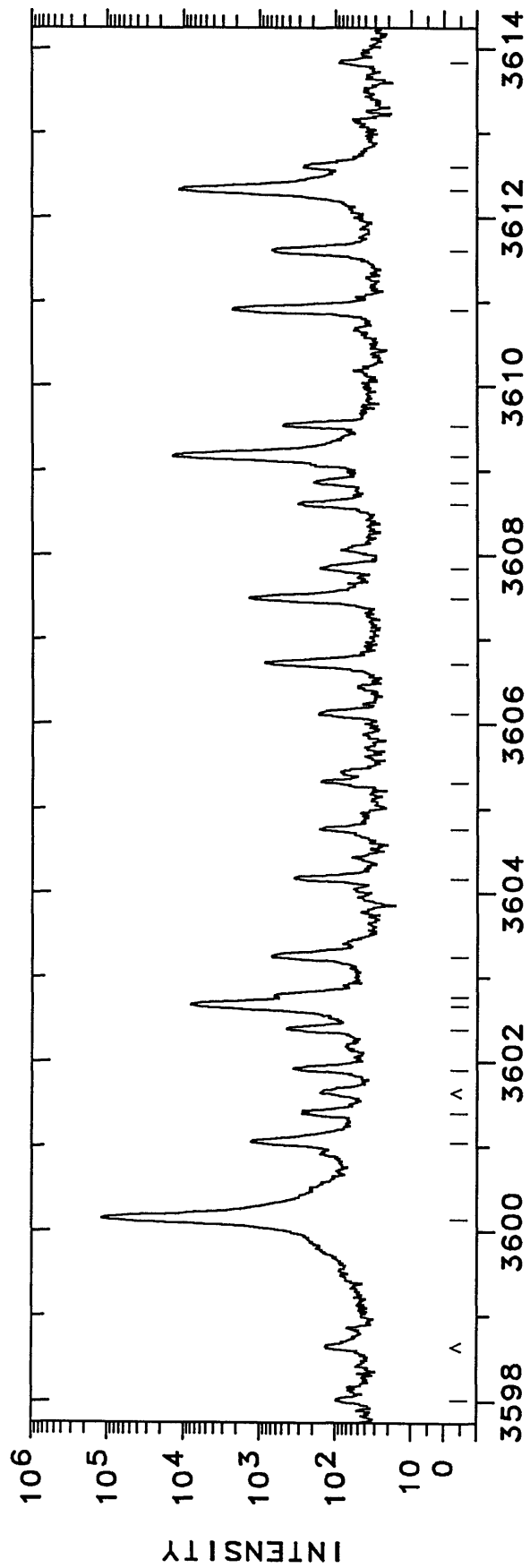
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3567.00	28026.8	690	Pt I	64312- 36296	3581.1928	27915.689	310	Fe I	R
3568.2840	28016.675	3000 U	Pt I	64312- 36296	3582.146	27908.26		Ne II	C
3568.3094	28016.476	4500 P	Pt I	64312- 36296	3583.08	27901.0		Rh I	
3568.3594	28016.083	3000 P	Pt I	64312- 36296	3583.3024	27899.254	360		
3568.5022	28014.962	820000	Ne II		3583.53	27897.5	64		
3569.8461	28004.416	1600			3584.932	27886.57	400	Ne II	C
3570.0985	28002.436		Fe I		3585.241	27884.17	540	Ne II	C
3571.2311	27993.555	100000	Ne II		3587.2691	27868.405	330	Pt II	105388- 77519
3571.9845	27987.651	1500 C	Pt II	29030- 57018	3587.4045	27867.353	6300	Pt I	18566- 46433
3572.026	27987.33	1200 P	Ne II		3588.9941	27855.011	330		
3572.378	27984.57	330	Ne II		3589.1981	27853.428	810	Pt I	18566- 46419
3573.3068	27977.295	1200	Pt I	68947- 40970	3589.4879	27851.179	650	Ne II	
3574.1826	27970.440	53000	Ne II		3590.450	27843.72	3300	Ne II	C
3574.6122	27967.078	610000	Ne II		3591.796	27833.28	2700	Ne II	C
3577.1483	27947.251	250 P	Pt II	23461- 51408	3591.9077	27832.417	300	Pt I	64128- 36296
3577.1960	27946.878	900 P	Pt II	23461- 51408			410000	Ne I	G
3577.2202	27946.689	500 U	Pt II	23461- 51408	3593.5252	27819.889	210000	Ne I	G
3577.8151	27942.042	1500	Pt I	68912- 40970	3593.6385	27819.012	83000	Ne II	G
3577.9772	27940.776	2800	Ne II		3594.1582	27814.990	350	Pt I	65387- 37590
3578.6866	27935.238		Cr I		3596.5531	27796.469		Rh I	
3579.09	27932.1	110			3597.15	27791.9	2400	Pt I	65132- 37342
3579.56	27928.4	110			3597.2858	27790.807	510	Pt I	68759- 40970



WAVELENGTH (ANGSTROMS) - AIR

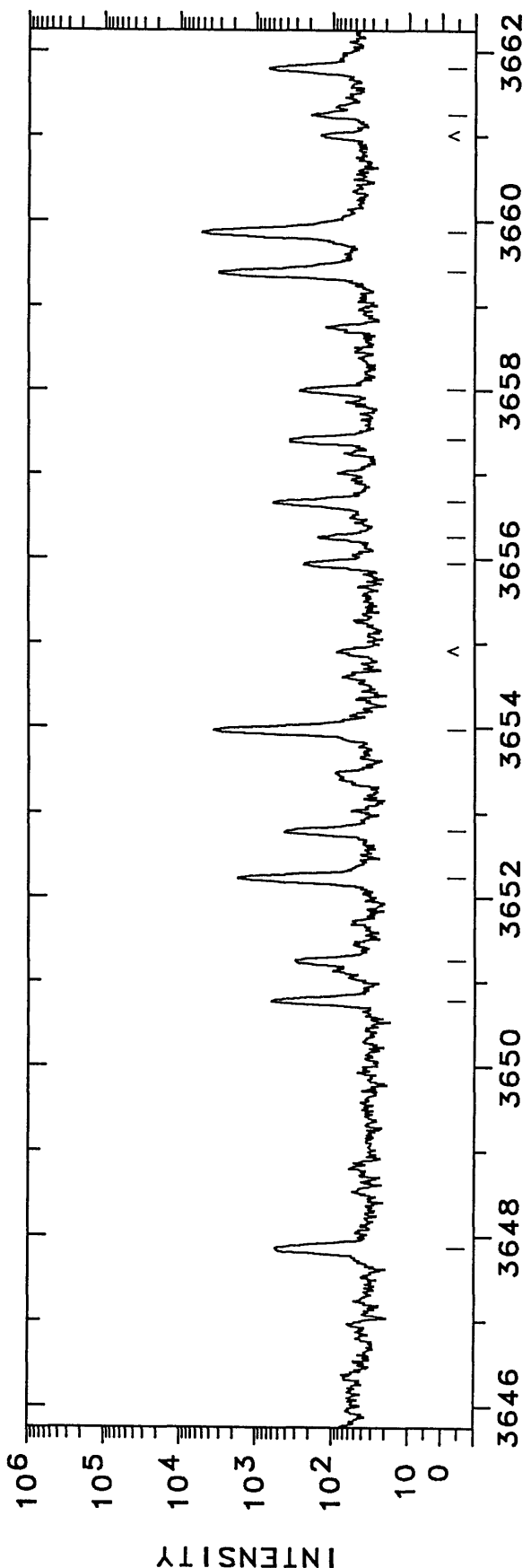
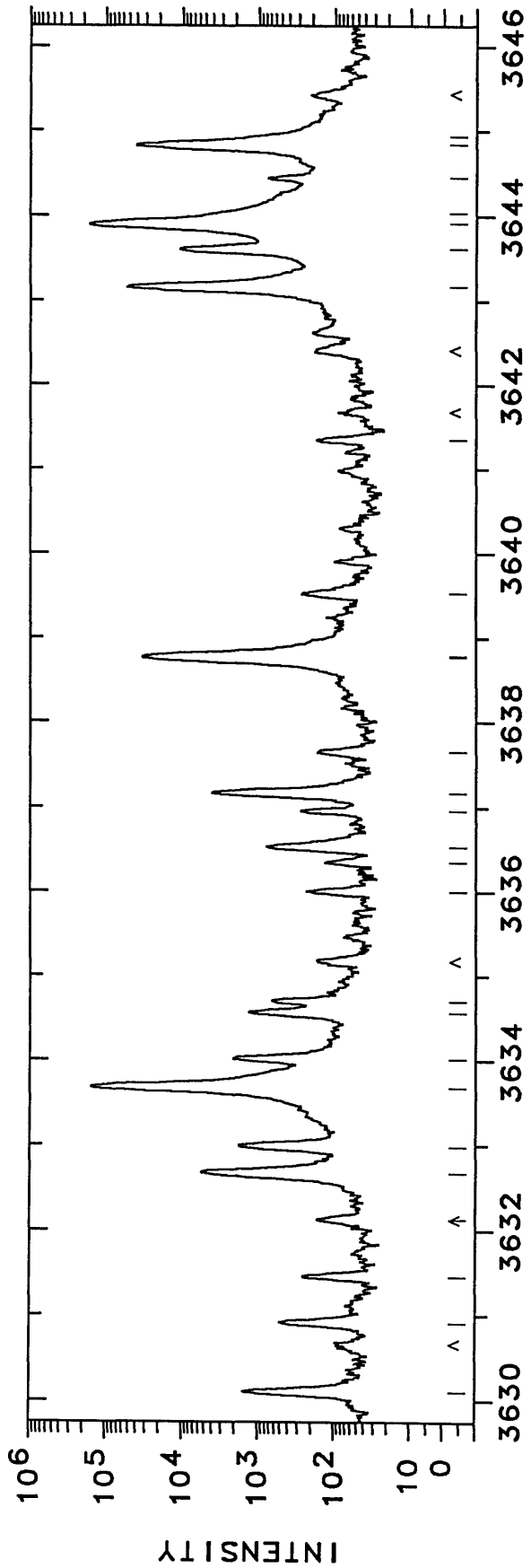


WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3598.02	27785.1	71			3613.84	27663.5	65		
3600.1682	27768.557	120000	Ne I	G	3614.33	27659.8	180	Pt I	68169- 40516 N
3601.056	27761.71	1300	Ne II	C	3615.17	27653.3	110	Pt I	10116- 37769 N
3601.4005	27759.057	250	Pt I	68275- 40516 N	3615.28	27652.5	350		
3601.9340	27754.945	330 L			3615.40	27651.6	95		
3602.3841	27751.477	420 L	Pt II	105794- 78043 K	3615.99	27647.1	150		
3602.6582	27749.366	8100			3616.348	27644.32	270	Ne II	C
3602.771	27748.50	630	Ne II	C	3617.91	27632.4	78		
3603.236	27744.92	680	Ne II	C	3618.3806	27628.794	300	Pt II	121651- 94022 K
3604.1641	27737.772	330	Pt I	60357- 32620 E	3618.7603	27625.895	500	Ne II	A
3604.76	27733.2	140	Pt I	68703- 40970 N	3618.7603	27625.895		Fe I	A
3605.31	27729.0		Cr I		3619.2212	27622.377	780	Pt II	110158- 82535 K
3606.12	27722.7	150			3619.8007	27617.955	1500	Pt I	65387- 37769 N
3606.7395	27717.966	840	Pt I	65308- 37590 N	3620.5414	27612.305	3500		
3607.504	27712.09	1400	Ne II	C	3621.6546	27603.818	2800	Pt I	18566- 46170 E
3607.8646	27709.323	140	Pt II	37877- 65587 33	3622.4709	27597.598	2200	Pt I	64379- 36781 N
3608.605	27703.64	290	Ne II	C	3625.1223	27577.413	870 L		
3608.8592	27701.686		Fe I	R	3625.54	27574.2	140		
3609.1783	27699.236	14000	Ne I	G	3626.5363	27566.661	5000	Ne II	G
3609.5443	27696.428		Pd I		3628.0329	27555.290	15000	Ne II	G
3610.9063	27685.982	2300	Pt I	15501- 43187 E	3628.1107	27554.699	91000	Pt I	6567- 34122 E
3611.599	27680.67	650	Ne II	C	3628.8660	27548.965	20000	Pt I	64330- 36781 N
3612.326	27675.10	11000	Ne II	C	3628.9097	27548.632	400 U		
3612.606	27672.96	240	Ne II	C	3629.1744	27546.623	310 W	Pt II	105066- 77519 38



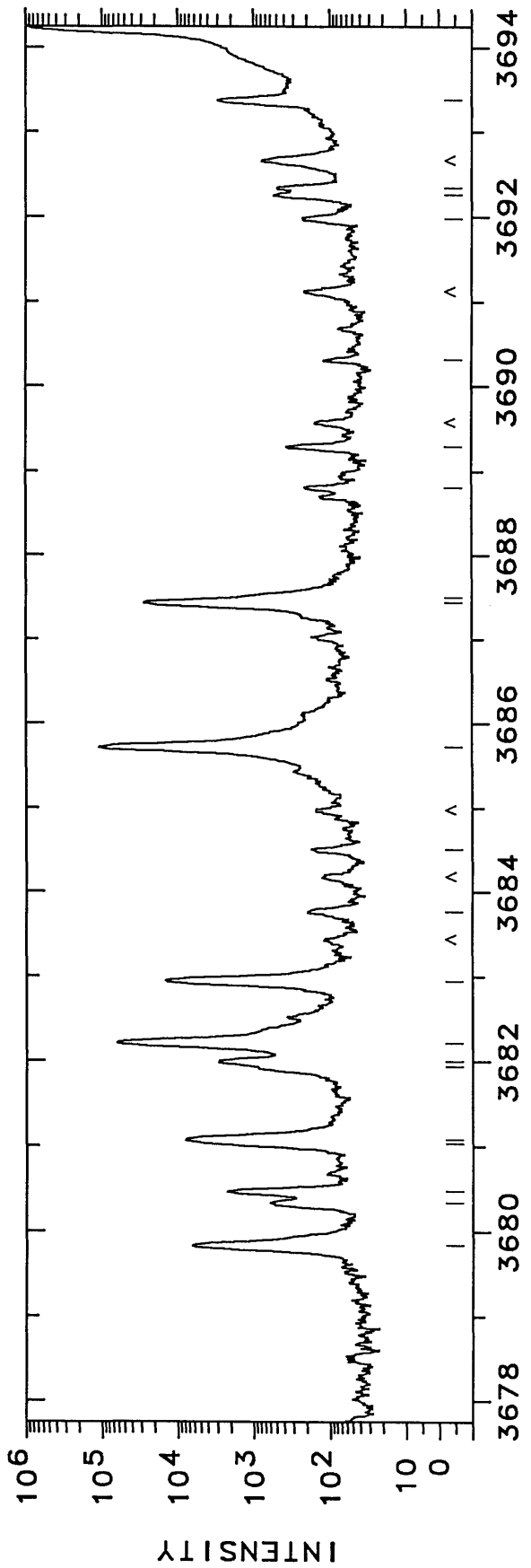
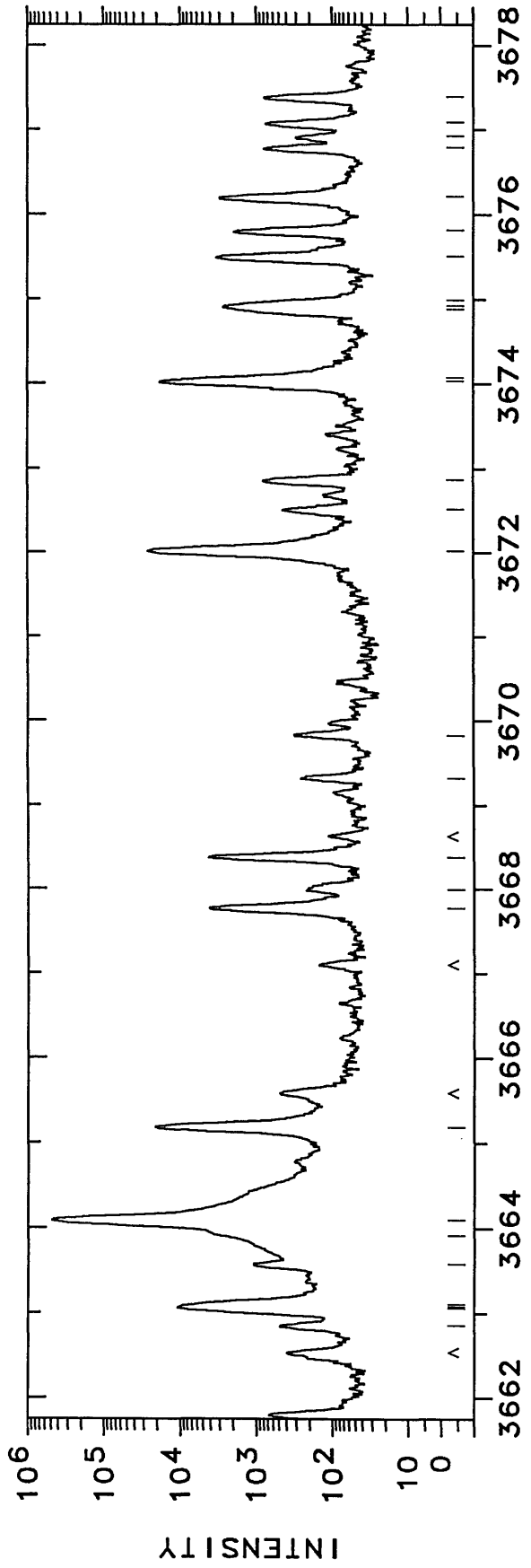
WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3630.1180	27539.463	1500	Pt I	65308-37769 N	3643.9291	27435.087	170000	Ne II	G
3630.9299	27533.305	480	Ne II		3644.0403	27434.249	1000 P	Pt II	82824 K
3631.4632	27529.262		Fe I	R	3644.4680	27431.030	730		
3632.13	27524.2	140	Pt II	54373-81897 KM	3644.8566	27428.105	39000	Ne II	G
3632.6804	27520.038	5500	Ne II		3644.9425	27427.459	550 U		
3632.9823	27517.751	1800 H	Pt II	101517-73999 K	3647.8477	27405.616	520 W	Fe I	A
3633.6637	27512.591	160000	Ne I	G	3647.8477	27405.616	610	Ne II	A
3634.0023	27510.027	2100	Pt II	105962-78452 K	3650.7680	27383.695	280	Pt I	62705-35321 N
3634.568	27505.75	1300	Ne II	C	3651.266	27379.96	1700	Ne II	C
3634.6874	27504.843		Pd I		3652.2552	27372.544	400	Pt I	26638-54011 E
3636.01	27494.8	210	Pt I	26638-54133 N	3652.812	27368.37	400	Ne II	C
3636.36	27492.2	110			3653.9828	27359.603	3600	Pt I	64141-36781 E
3636.5559	27490.711	750	Pt I	68006-40516 N	3655.95	27344.9	210	Pt II	105388-78043 K
3636.9875	27487.449	250	Pt I	68275-40787 N	3656.26	27342.6	120	Pt II	106434-79092 K
3637.1933	27485.893	4000	Pt I	64267-36781 N	3656.651	27339.64	570	Ne II	C
3637.66	27482.4	140			3657.41	27334.0	330	Pt II	110158-82824 K
3638.7879	27473.848	34000	Pt I	13496-40970 E	3658.01	27329.5		Rh I	
3638.7879	27473.848	34000	Pt I	10116-37590 E	3659.4131	27319.004	3100	Pt I	21967-49286 E
3639.54	27468.2	240			3659.8921	27315.429	5200	Ne II	G
3641.35	27454.5	150	Pt II	110146-82692 K	3661.25	27305.3	160	Pt I	68275-40970 N
3643.1667	27440.828	53000	Pt I	64222-36781 N	3661.809	27301.13	650	Ne II	C
3643.6290	27437.346	11000	Pt II	101199-73761 32					



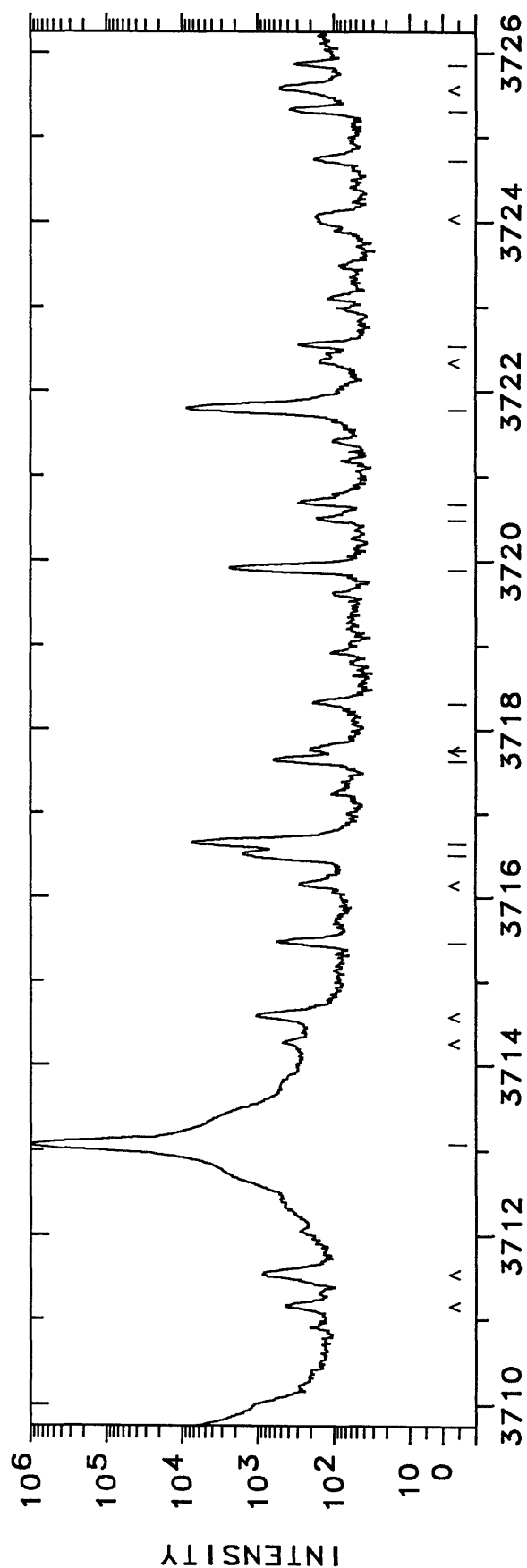
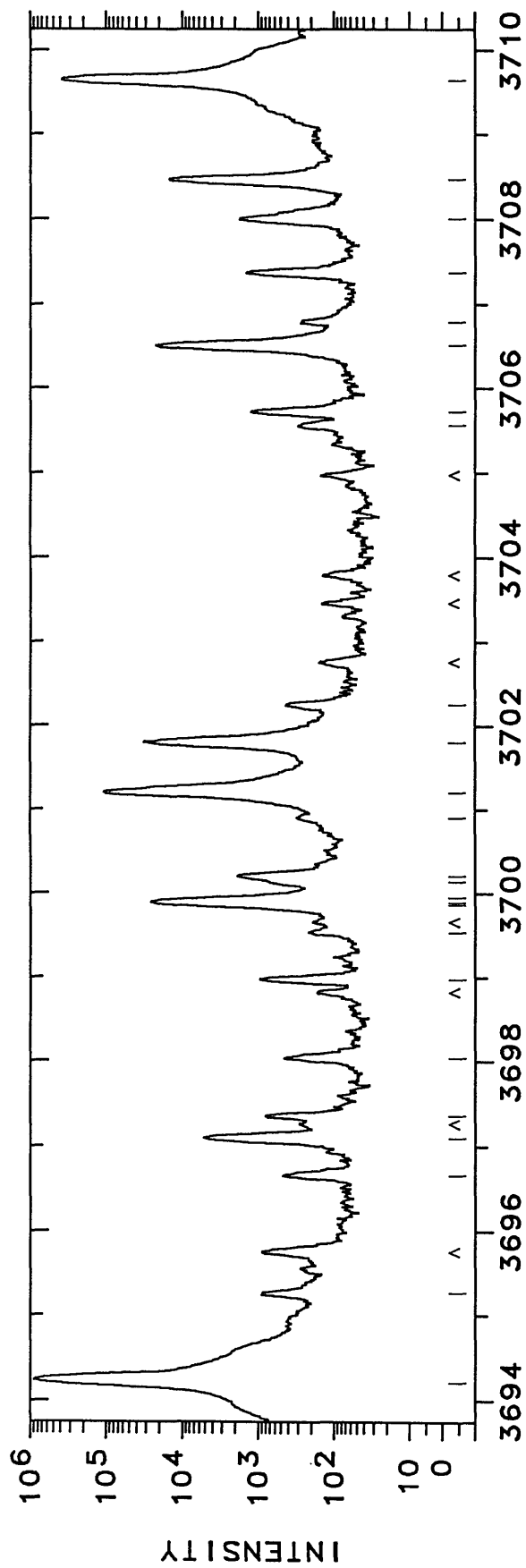
WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3662.8761	27293.177	460	Pt I	13496- 40787	3676.804	27189.79	750	Ne II	C
3663.0602	27291.805	2500 U	Pt I	13496- 40787	3676.93	27188.9	270	Ne II	C
3663.0952	27291.544	5000	Pt I	13496- 40787	3677.090	27187.68	700	Ne II	C
3663.1071	27291.455	4400 U	Pt I	13496- 40787	3677.3943	27185.427	730	Pt II	110158- 82972
3663.5492	27288.162	1100	Pt I	59908- 32620	3679.8160	27167.536	6500	Ne II	K
3663.9192	27285.407	4000 P	Pt II	110258- 82972	3680.3319	27163.729	580	Pt I	64505- 37342
3664.0740	27284.254	490000	Ne II	101517- 74241	3680.4520	27162.842	2200	Pt I	59782- 32620
3665.1680	27276.110	21000	Pt II	101517- 74241	3681.0364	27158.530	2500 U	Ne II	G
3667.7969	27256.560	4100	Ne II	36484- 63738	3681.0798	27158.210	7500 P	Pt I	15501- 42660
3668.0321	27254.813	190	Pt II	59872- 32620	3681.941	27151.86	600 P	Ne II	C
3668.3939	27252.125	4100	Pt I	59872- 32620	3682.0226	27151.256	2900	Ne II	G
3669.32	27245.2	230			3682.2418	27149.640	64000	Ne I	G
3669.83	27241.5	280			3682.9727	27144.252	15000	Pt I	59764- 32620
3671.9990	27225.370	23000	Pt I	10116- 37342	3683.77	27138.4	170		
3672.5042	27221.625	420			3684.51	27132.9	150		
3672.8450	27219.099	760	Pt I	68006- 40787	3685.7349	27123.910	110000	Ne I	G
3674.0449	27210.210	18000 P	Pt I	10131- 37342	3687.4152	27111.550	28000	Pt I	59731- 32620
3674.0738	27209.996	2500 U			3687.497	27110.95	350 U	Ne II	C
3674.8829	27204.005	500	Pt II	42031- 69235	3688.81	27101.3	180		
3674.8829	27204.005	500	Pt I	60884- 33680	3689.316	27097.58	330	Ne II	C
3674.9388	27203.591	2700	Pt I	60884- 33680	3690.32	27090.2	87	Pd I	
3674.9872	27203.233	500	Pt I	60884- 33680	3691.98	27078.0	200	Pt I	64668- 37590
3675.5230	27199.268	3300	Pt II	101199- 73999	3692.272	27075.89	500	Ne II	C
3675.5230	27199.268	3300	Pt I	68169- 40970	3692.5525	27075.299		Rh I	
3675.8238	27197.042	1900			3693.389	27067.70	2900	Ne II	C
3676.226	27194.07	3000	Ne II						



WAVELENGTH (ANGSTROMS) - AIR

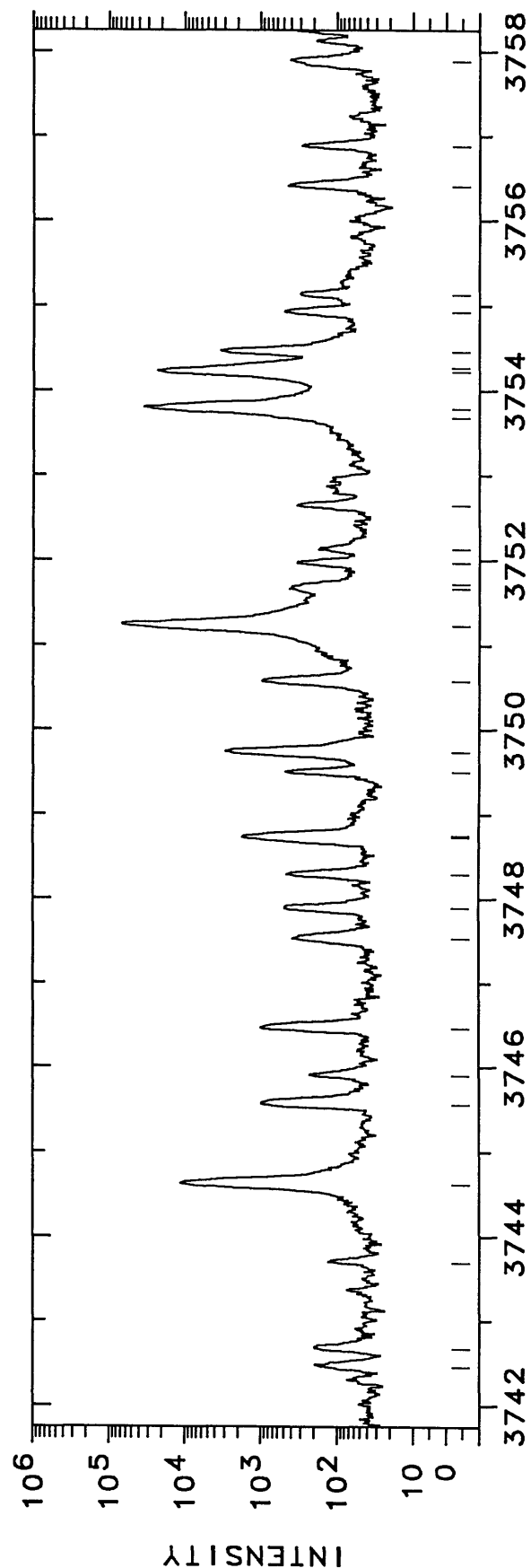
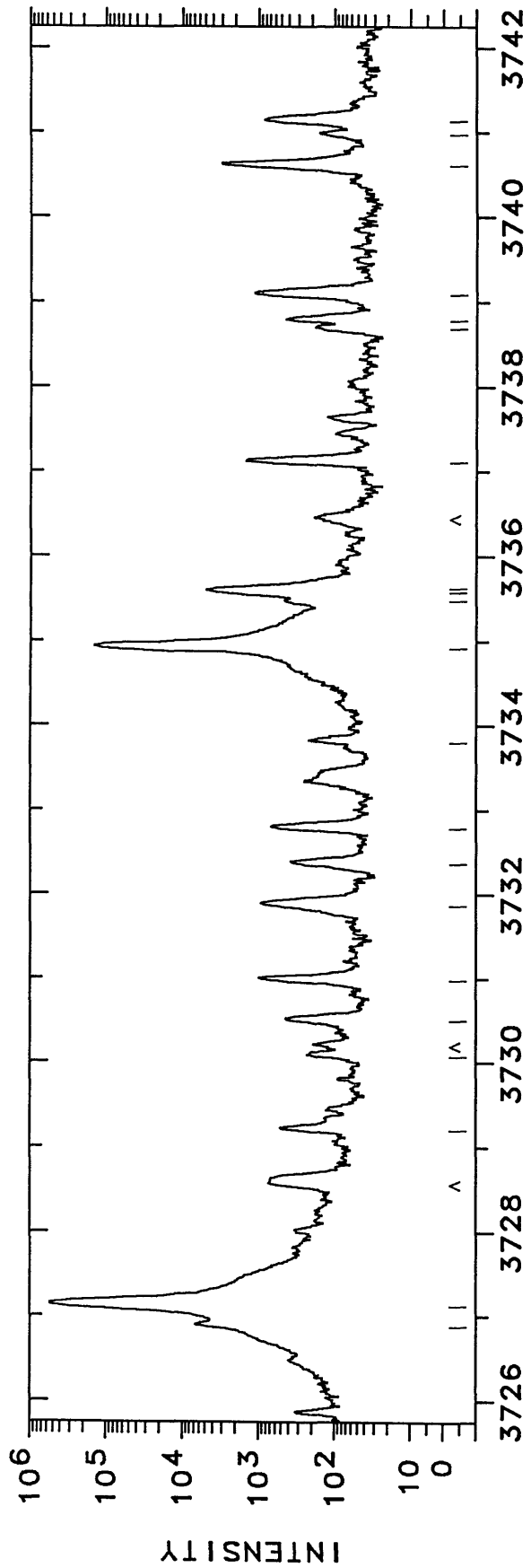
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3694.2145	27061.652	910000	Ne II	G	3706.79	26969.8	230	Ne II	C
3695.247	27054.09	860	Ne II	C	3707.386	26965.51	1400	Ne II	C
3696.6518	27043.810	430	Pt II	105086- 78043	3707.998	26961.06	1700	Ne II	C
3697.1234	27040.360	5100	Ne II	G	3708.4731	26957.606	15000	Pt II	101199- 74241
3697.3787	27038.493	760	Ne II	C	3709.6222	26949.256	380000	Ne II	G
3698.067	27033.46	420	Ne II	C	3713.0826	26924.141	1000000	Ne II	G
3698.9960	27026.671	920	Pt I	26638- 53665	3715.458	26906.93	520	Ne II	C
3699.54	27022.7	180	Pt I	13496- 40516	3716.5006	26899.380	1500 C	Pt I	64668- 37769
3699.8649	27020.325	300 U	Pt I	13496- 40516	3716.5265	26898.469	7300	Pt II	101517- 74619
3699.9126	27019.976	21000	Pt I	13496- 40516	3717.6207	26891.276	570	Pt II	104410- 77519
3699.9539	27019.675	350 U	Pt I	13496- 40516	3717.75	26890.3	170	Pt II	104410- 77519
3700.1471	27018.264	450 W	Pt II	34647- 61665	3718.31	26886.3	150	Fe I	R
3700.219	27017.74	1900	Ne II	C	3719.9346	26874.549	130	Pt II	105962- 79092
3700.9064	27012.721	270	Ne I	G	3720.48	26870.6	250	Ne II	C
3701.2242	27010.401	110000	Ne II	G	3720.717	26868.90	8700	Ne II	C
3701.7769	27006.368	31000	Ne II	G	3721.819	26860.94	250	Ne II	C
3702.2305	27003.060	400	Fe I	R	3722.53	26855.8	150	Pt I	64182- 37342
3705.5660	26978.754	1200	Ne II	C	3724.72	26840.0	340	Pt I	18566- 45398
3705.744	26977.46	22000	Pt I	59591- 32620	3725.2851	26835.951	290	Pt I	
3706.5217	26971.798				3725.85	26831.9			



WAVELENGTH (ANGSTROMS) - AIR

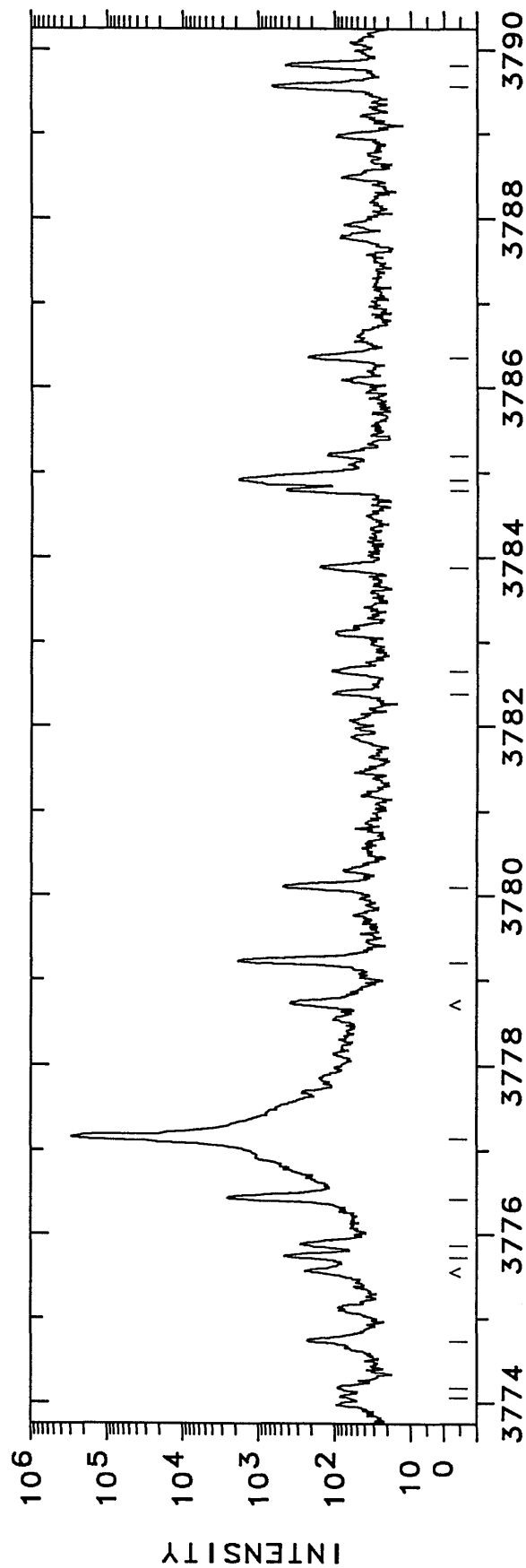
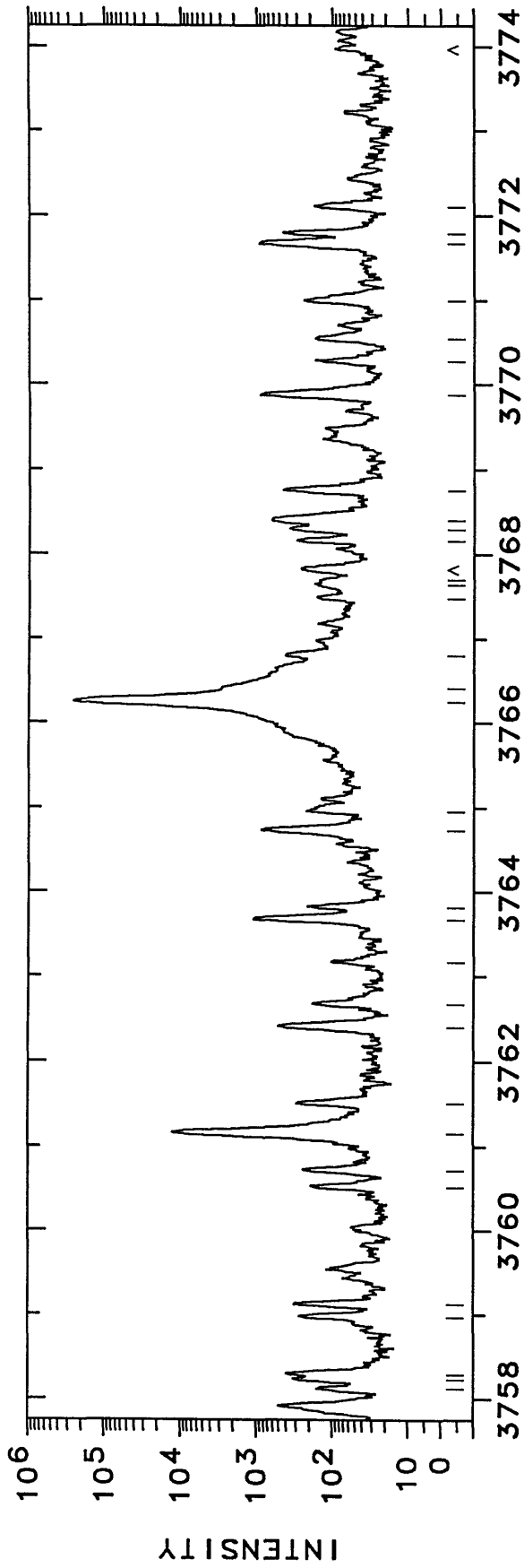


WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3726.871	26824.53	6800 P	Ne II	C	3745.8995	26688.271		Fe I	R
3727.1081	26822.825	550000	Ne II	G	3746.4653	26684.241	950	Ne II	
3729.20	26807.8	480			3747.53	26676.7	350	Pt I	64267- 37590 N
3730.07	26801.5	200			3747.849	26674.39	450	Ne II	C
3730.50	26798.4	410			3748.2622	26671.449		Fe I	R
3730.981	26794.98	950	Ne II	C	3748.7156	26668.223	1700	Pt I	60790- 34122 E
3731.8721	26788.585	900 S	Pt I	N	3748.7469	26668.000	400 U		
3732.346	26785.18	350	Ne II	C	3749.4853	26662.749		Fe I	R
3732.777	26782.09	650	Ne II	C	3749.7263	26661.035	2900	Pt II	96614- 69953 18
3733.8023	26774.737	190			3750.588	26654.91	920 W	Ne II	C
3734.9388	26766.589	150000	Ne II	G	3751.2459	26650.235	68000	Ne II	G
3735.4749	26762.749	420	Pt II	K	3751.6678	26647.238	310		
3735.5740	26762.039	1200 U	Pt I	H	3751.7200	26646.868	250		
3735.6027	26761.833	3500 P	Pt I	H	3751.9754	26645.054	300		
3735.6221	26761.694	1300 U	Pt I	H	3752.1269	26643.978	140		
3737.1313	26750.887		Fe I	R	3752.6447	26640.301	300		
3738.688	26739.75	150	Ne II	C	3753.6755	26632.986	310		
3738.78	26739.1	420			3753.7792	26632.250	35000	Ne II	G
3739.1037	26736.776	1100 S	Pt I	E	3754.2143	26629.163	23000	Ne I	G
3740.5987	26726.090	3000	Ne II	G	3754.2685	26628.779	1000 P		
3740.967	26723.46	130	Ne II	C	3754.4527	26627.473	3400	Pt I	56784- 30156 E
3741.1392	26722.229	800	Pt I	N	3754.92	26624.2	460		
3742.4511	26712.862	160	Pt I	E	3755.0849	26622.990	280		
3742.67	26711.3	170			3756.393	26613.72	410	Ne II	C
3743.69	26704.0	100	Pt II	K	3756.88	26610.3	260		
3744.6245	26697.358	11000	Ne II	G	3757.8940	26603.090	480		
3745.5613	26690.681		Fe I	R					



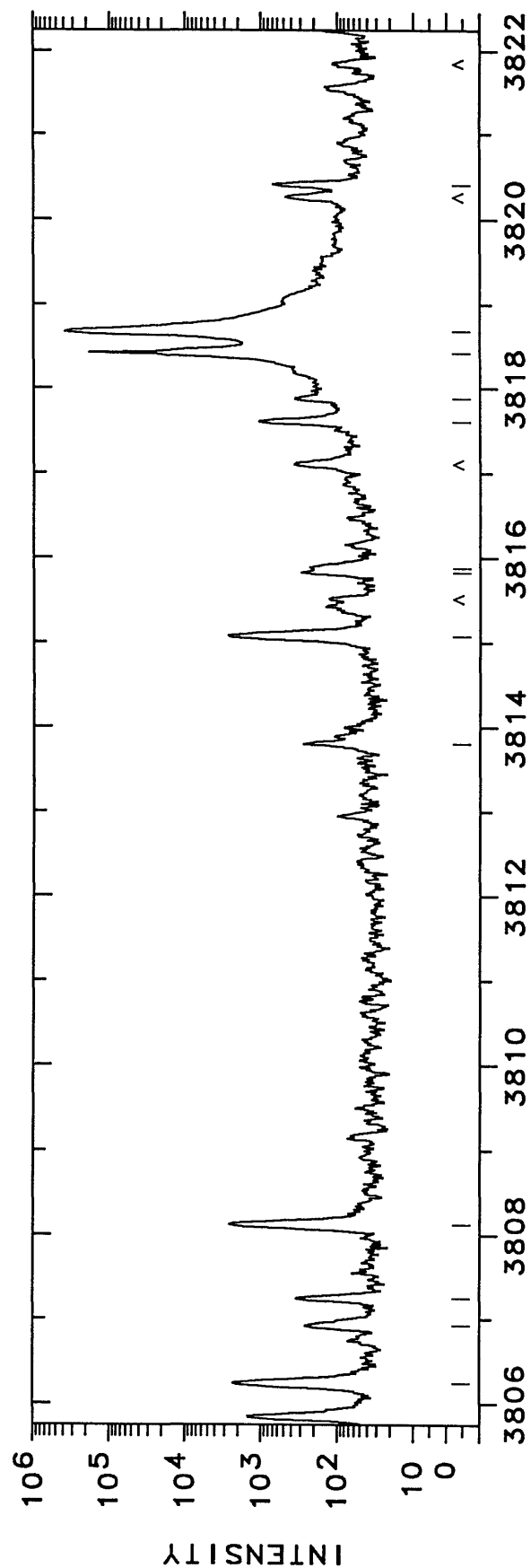
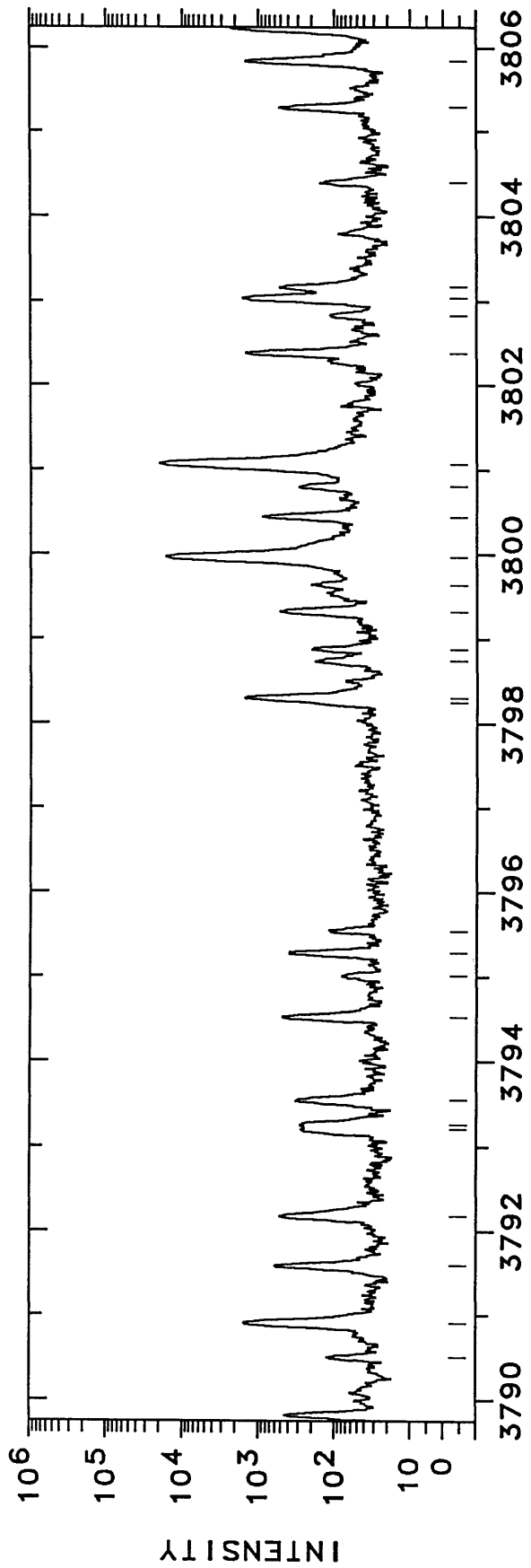
WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3758.12	26601.5	140	Fe I	R	3769.8806	26518.505	890	Pt I	60640- 34122 E
3758.2330	26600.690				3770.27	26515.8	150	Pt II	116689- 90173 K
3758.29	26600.3	380			3770.54	26513.9	150		
3758.97	26595.5	240			3770.9691	26510.851	220	Pt II	37877- 64388 36
3759.12	26594.4	290			3771.6504	26506.062	900	Ne III	L
3760.51	26584.6	160			3771.7806	26505.147	430		
3760.71	26583.2	220			3772.10	26502.9	150		
3761.1616	26579.978	12000	Pt II	101199- 74619 22	3774.06	26489.1	60		
3761.51	26577.5	270			3774.17	26488.4	66		
3762.40	26571.2	490	Pt I	65387- 38815 N	3774.73	26484.4	200		
3762.67	26569.3	160			3775.7464	26477.308	430		
3763.16	26565.9	80			3775.86	26476.5	250		
3763.646	26562.43	1100	Ne II	C	3776.4251	26472.550	2500	Pt I	68275- 41802 N
3763.7891	26561.423		Fe I	R	3777.1359	26467.568	290000	Ne II	G
3764.708	26554.94	840 H	Ne II	C	3779.1920	26453.169	1800	Pt II	101199- 74745 22
3764.9789	26553.029	200			3780.0762	26446.981	450		
3766.260	26544.00	260000	Ne II	C	3782.38	26430.9	83	Ne III	L
3766.4078	26542.956	2500 U			3782.65	26429.0	85		
3766.810	26540.12	390	Ne II	C	3783.88	26420.4	130	Ne III	L
3767.4986	26535.271	140	Pt II	109507- 82972 K	3784.7698	26414.184	410		
3767.6446	26534.242	150			3784.9106	26413.201	1800 S	Pt I	64182- 37769 N
3767.6959	26533.881	120			3785.19	26411.3	100		
3768.1727	26530.524	270			3786.35	26403.2	200	Ne III	L
3768.29	26529.7	340			3789.5705	26380.723	640	Pt I	26638- 53019 E
3768.4048	26528.890	610 C	Pt II	24879- 51408 12	3789.8282	26378.930	420		
3768.7573	26526.409	430 W							



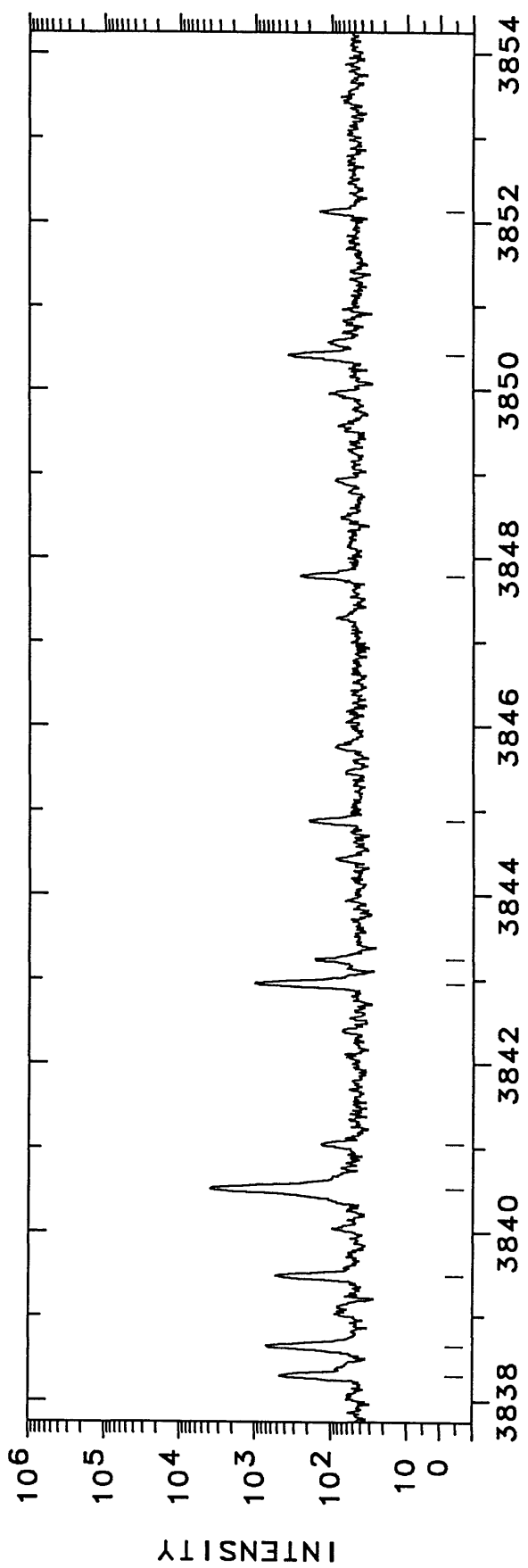
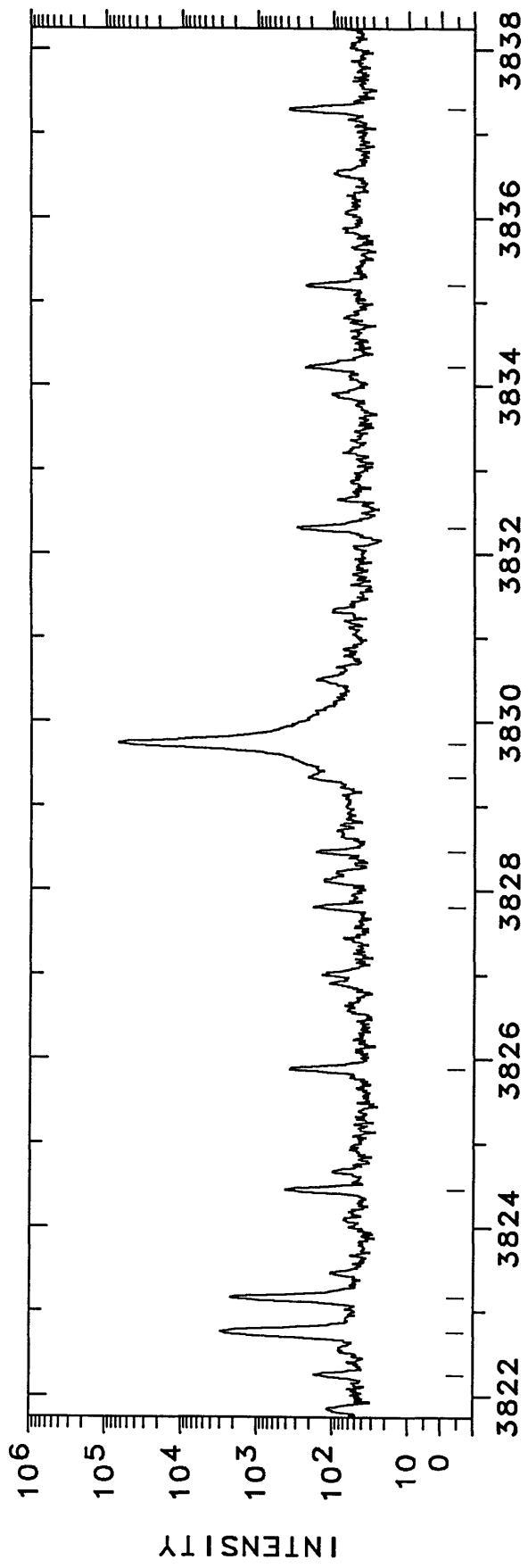
WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3790.50	26374.3	98			3802.3589	26291.999	1400	Pt I	68094- 41802 N
3790.918	26371.35	1500	Ne II	C	3802.83	26288.7	90		
3791.59	26366.7	580	Pt I	68169- 41802 N	3803.0226	26287.412	1600	Pt I	68947- 42660 N
3792.161	26362.70	500	Ne II	C	3803.17	26286.4	510		
3793.2055	26355.443		Rh I		3804.40	26277.9	130		
3793.26	26355.1	260	Pt II	105962- 79607 K	3805.2973	26271.698	500	Pt I	62567- 36296 N
3793.55	26353.0	300			3805.8569	26267.835	1500		
3794.5166	26346.337	460	Pt II	41434- 67780 K	3806.249	26265.13	2300	Ne II	
3795.01	26342.9	55			3806.9248	26260.467	240	Pt II	34647- 60907 C
3795.2677	26341.123	370			3807.2422	26258.278	320		
3795.54	26339.2	95			3808.1298	26252.157	2600	Pt I	68912- 42660 N
3798.2534	26320.418	1000			3813.8174	26213.008	250		
3798.3227	26319.937	1500	Ne II	G	3815.0673	26204.420	2700 L	Pt I	16983- 43187 N
3798.74	26317.0	160	Pt I	65132- 38815 N	3815.8403	26199.112		Fe I	
3798.88	26316.1	180			3815.88	26198.8	200		
3799.32	26313.0		Rh I		3817.5962	26187.062	1000	Pt II	105794- 79607 K
3799.64	26310.8	180			3817.8859	26185.075	330		
3799.9645	26308.566	17000	Ne II	G	3818.4236	26181.388	34000	Ne II	
3800.456	26305.16	870	Ne II	C	3818.6874	26179.579	380000	Pt I	10116- 36296 E
3800.80	26302.8	270			3820.4254	26167.670		Fe I	
3801.0723	26300.899	20000 D	Pt I	15501- 41802 E					



WAVELENGTH (ANGSTROMS) - AIR

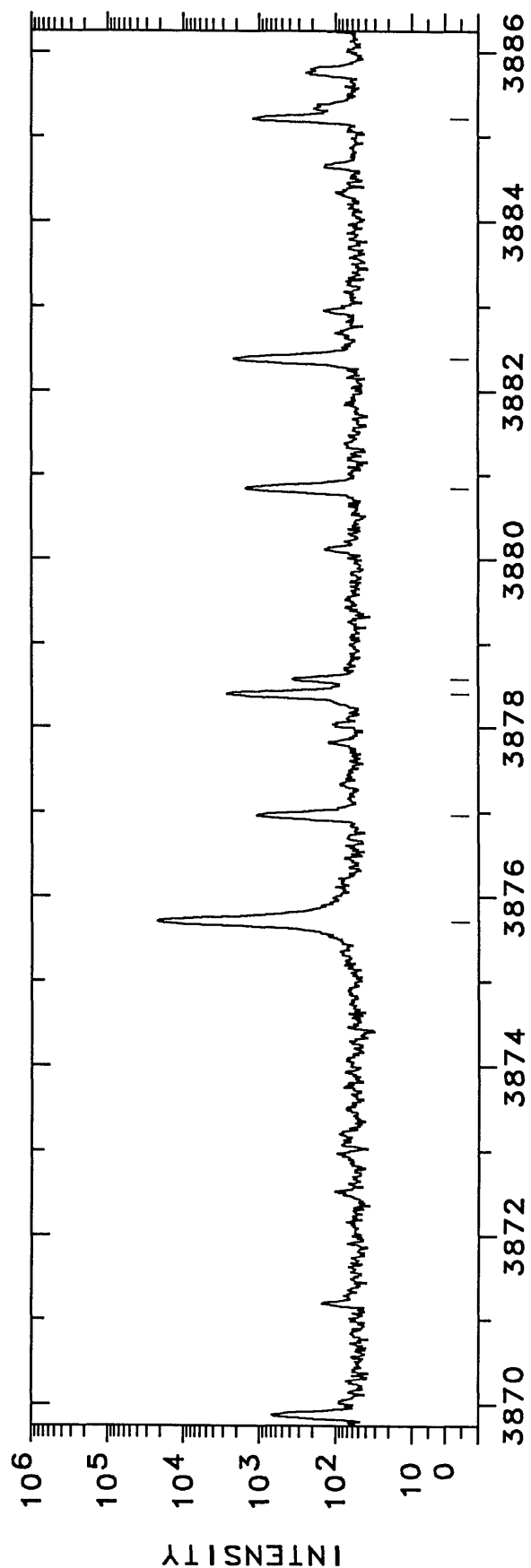
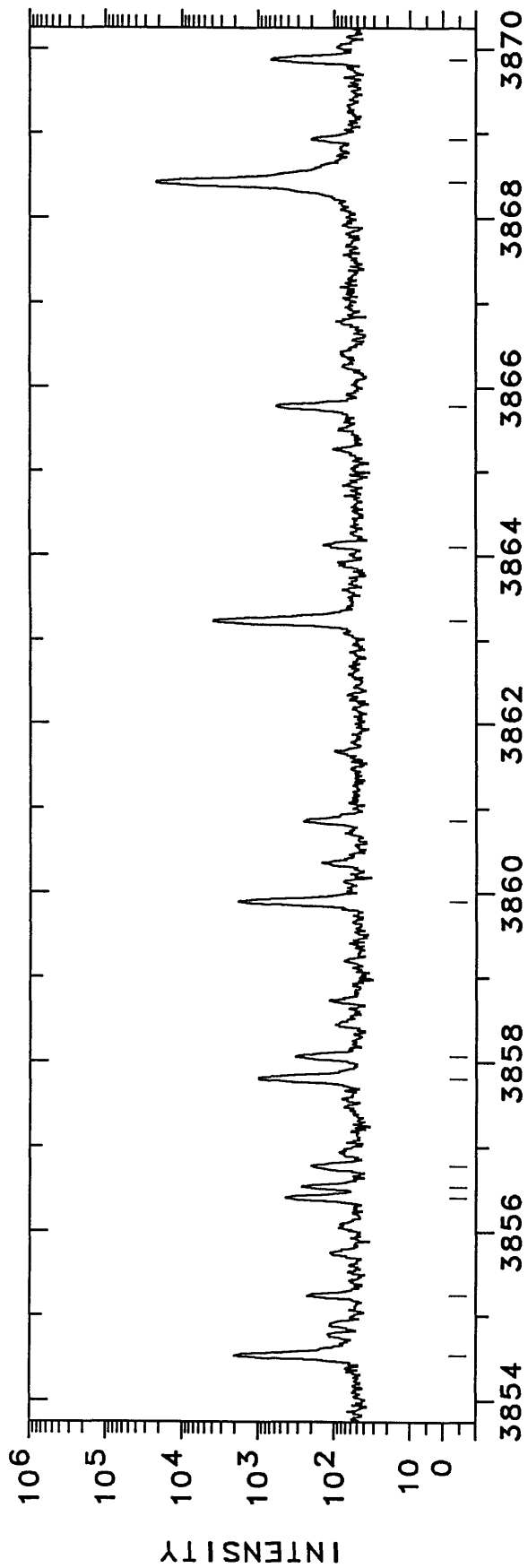
WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3822.25	26155.2		Rh I		3837.29	26052.7	350	Pt I	6567- 32620 N
3822.7531	26151.736	2900 L	Pt II	101517- 75365 K	3838.2891	26045.886		Mg I	
3823.152	26149.01	2200	Ne II		3838.6561	26043.596	670	Pt I	68703- 42660 N
3824.4436	26140.177		Fe I		3839.4742	26037.847	500		
3825.8814	26130.354		Fe I		3840.4953	26030.924	3900	Ne II	
3827.8227	26117.102		Fe I		3841.0480	26027.179		Fe I	
3828.46	26112.8		Rh I		3842.9636	26014.205	980	Pt II	101199- 75184 20
3829.34	26106.8	180			3843.24	26012.3	130	Ne III	
3829.7503	26103.957	69000	Ne II		3844.88	26001.2	160	Ne III	
3832.31	26086.5		Mg I	G	3847.78	25981.6	220	Ne III	
3834.2224	26073.511		Fe I		3850.41	25963.9	340	Pt II	110146- 84182 K
3835.20	26066.9	190			3852.13	25952.3	110		



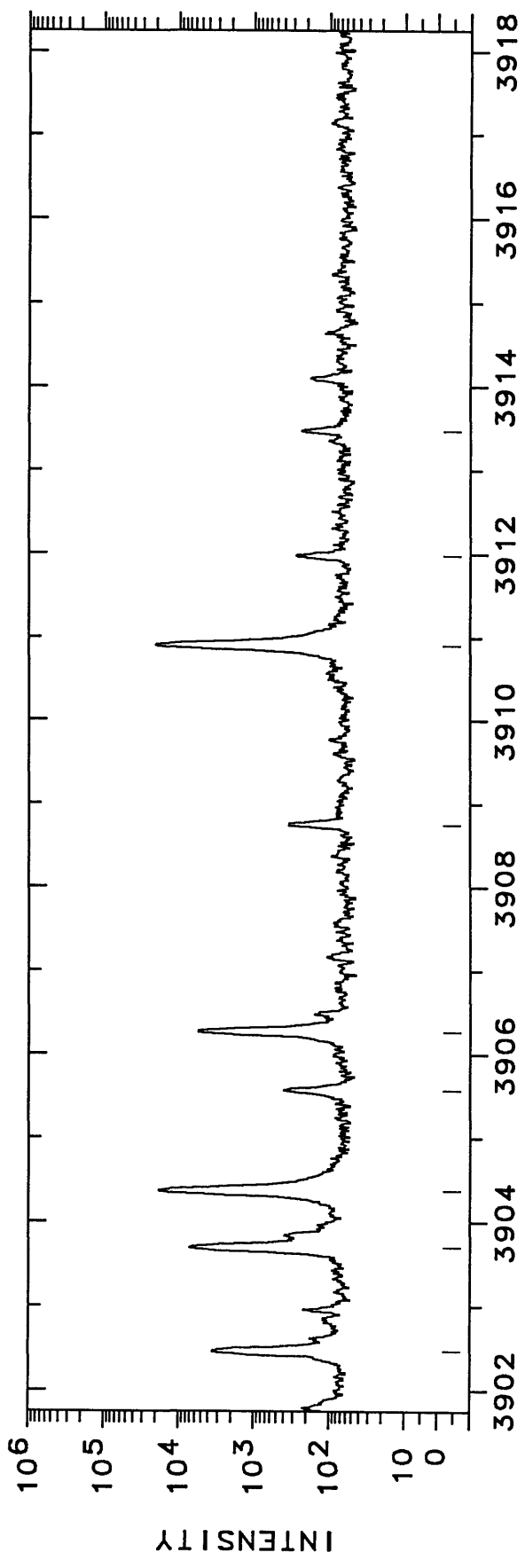
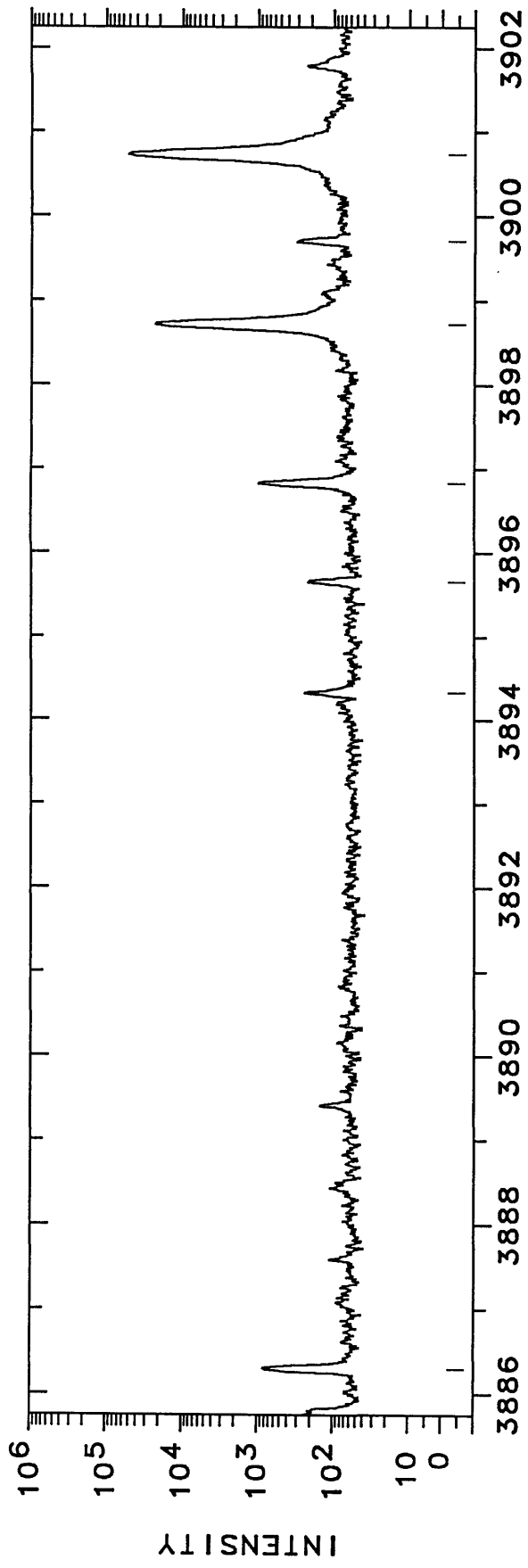
WAVELENGTH (ANGSTROMS) - AIR



WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3854.5252	25936.178	2000	Pt II	101517- 75581	3865.7875	25860.619	530	Pt I	62705- 36844
3855.24	25931.4	180	Fe I		3868.4209	25843.015	22000	Pt I	64379- 38536
3856.3716	25923.760		Rh I		3868.93	25839.6	160		
3856.53	25922.7				3869.8816	25833.261	640	Pt II	101199- 75365
3856.78	25921.0	160			3875.7150	25794.380	22000	Pt I	64330- 38536
3857.817	25914.05	960	Ne II	C	3876.9749	25785.997	1000	Pt I	59908- 34122
3858.07	25912.3	280			3878.3549	25776.823	2600		
3859.9115	25899.986		Fe I	R	3878.5733	25775.371		Fe I	
3860.86	25893.6	210			3880.8488	25760.258	1500	Pt I	59882- 34122
3863.2223	25877.790	3900	Pt I	18566- 44444	3882.3976	25749.982	2100	Pt I	59872- 34122
3864.1005	25871.909	94			3885.2172	25731.295	1200	Pt I	64267- 38536

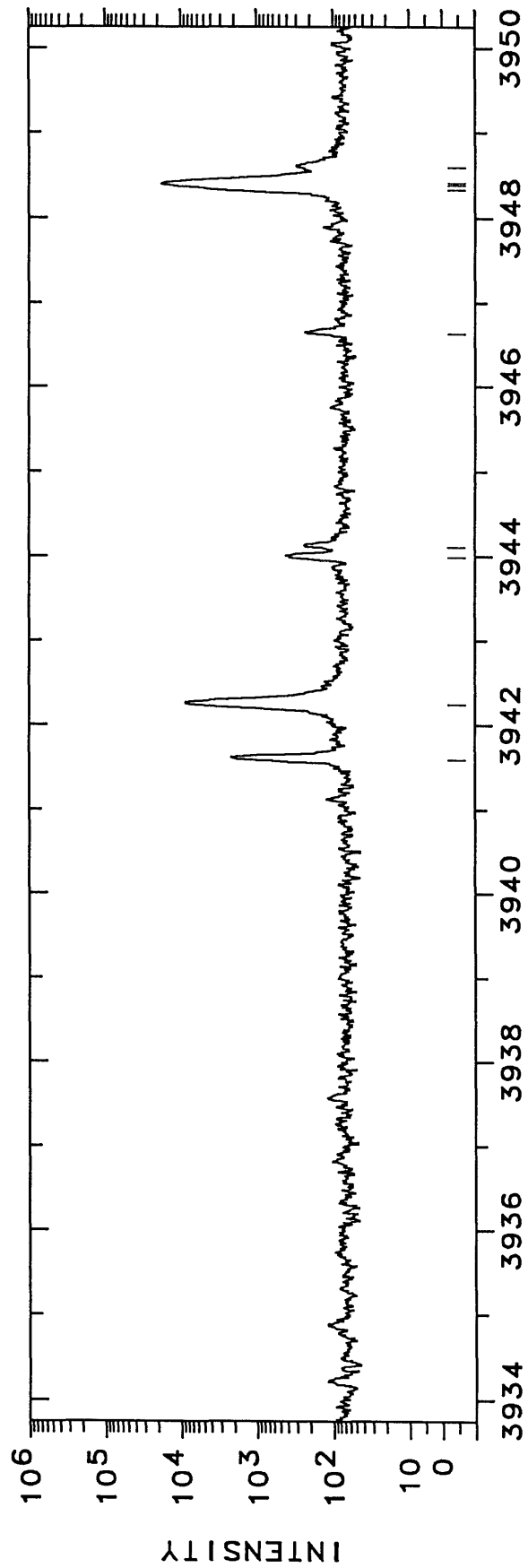
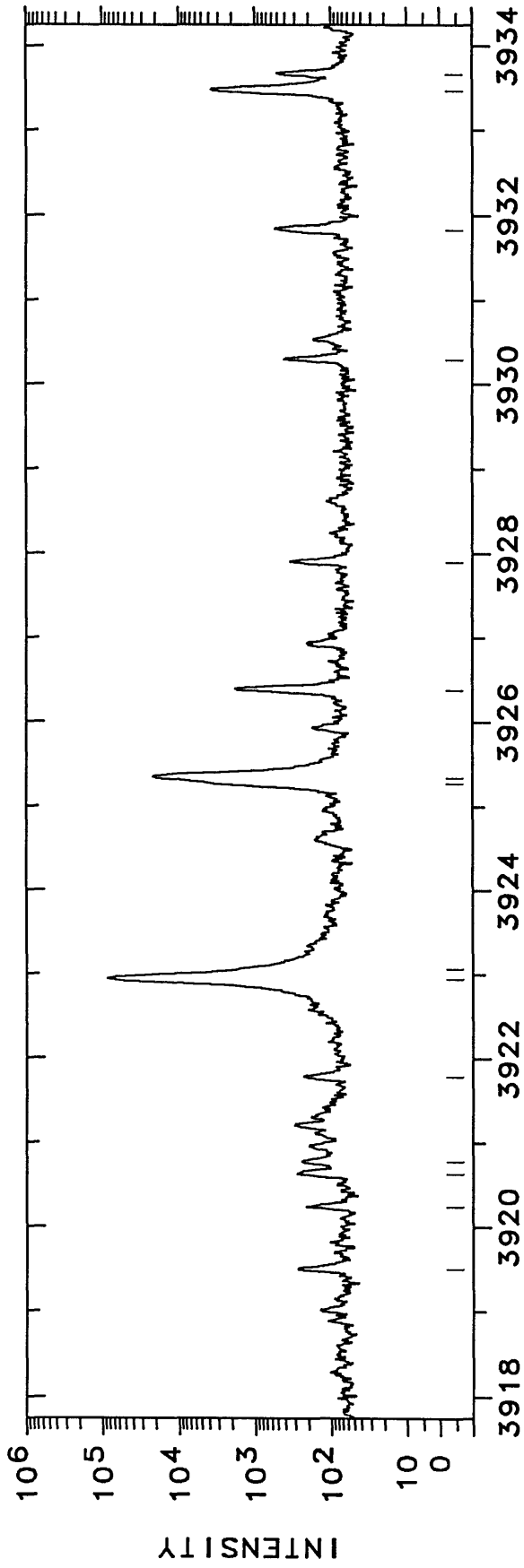


WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3886.2823	25724.243		Fe I	Q	3903.7085	25609.412	7100	Pt I	59731- 34122
3894.33	25671.1	190	Pt II	K	3904.3823	25604.993	18000	Pt I	64141- 38536
3895.6564	25662.344		Fe I	Q	3905.57	25597.2	350	Pt II	105794- 80197
3896.846	25654.51	940	Ne II	C	3906.2788	25592.562	5500	Pt I	64128- 38536
3898.7316	25642.103	23000 s	Pt I	E	3908.75	25576.4	300	Pt II	106434- 80858
3899.7074	25635.687		Fe I	Q	3910.8955	25562.351	20000	Pt I	60884- 35321
3900.7228	25629.014	51000 s	Pt I	E	3911.98	25555.3	230		
3902.4512	25617.663	3400	Pt II	36	3913.47	25545.5	180		



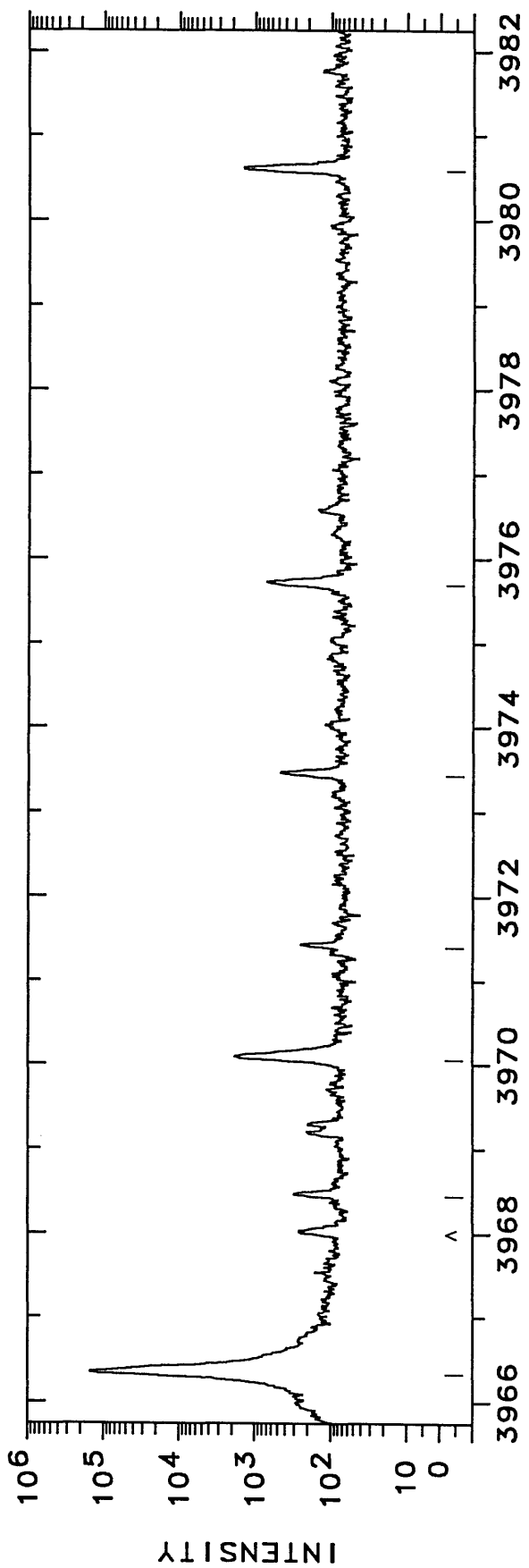
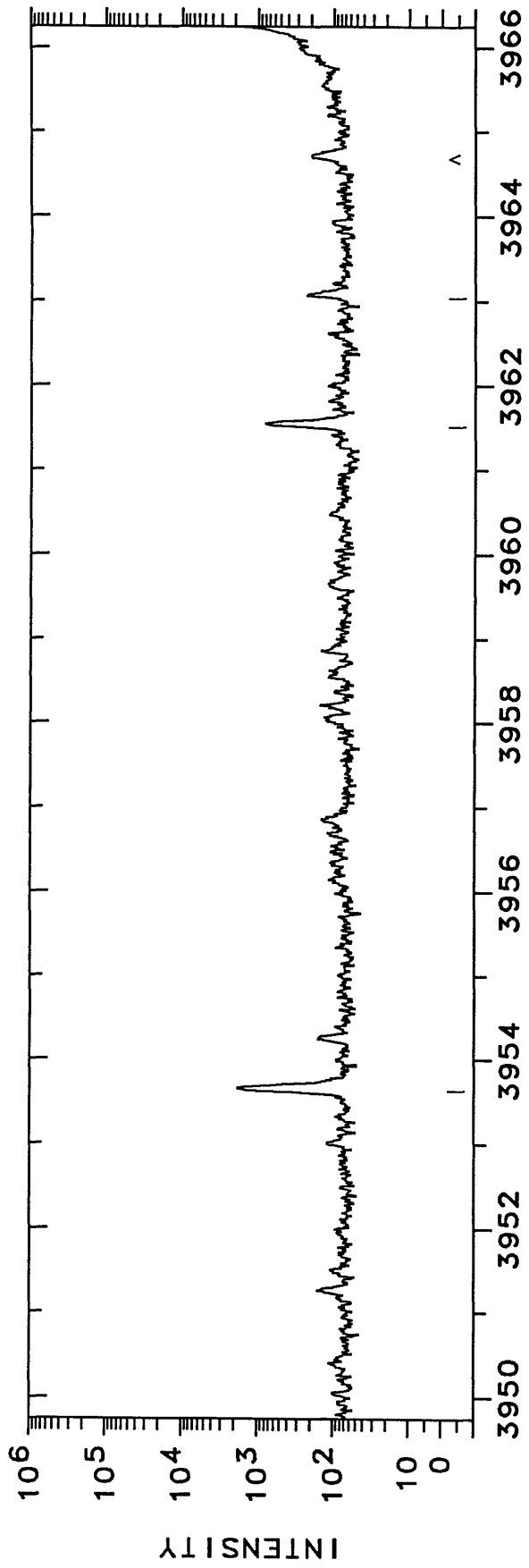
WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3919.50	25506.2	210	Fe I	Q	3931.83	25426.3	480		
3920.2580	25501.304				3933.465	25415.68	3700	Ne II	C
3920.63	25498.9	220			3933.66	25414.4		Ca II	
3920.78	25497.9	190			3941.5998	25363.230	2100	Pt I	62705- 37342 N
3921.79	25491.3	170			3942.262	25358.97	8600	Ne II	C
3922.9559	25483.766	86000 C	Pt I	55640- 30156 E	3943.99	25347.9		Al I	
3923.0660	25483.051	370 U			3944.11	25347.1	180	Pt I	68006- 42660 N
3925.2718	25468.731	3500	Pt I	60790- 35321 E	3946.63	25330.9	170		
3925.3359	25468.315	22000	Pt I	15501- 40970 E	3948.3325	25319.981	3000 P	Pt I	13496- 38815 H
3926.3831	25461.523	1700	Pt I	68121- 42660 N	3948.3881	25319.625	14000 P	Pt I	13496- 38815 H
3927.9199	25451.562		Fe I	Q	3948.4117	25319.474	4000 U	Pt I	13496- 38815 H
3930.2967	25436.170		Fe I	Q	3948.59	25318.3	240	Pt II	46046- 71364 K



WAVELENGTH (ANGSTROMS) - AIR

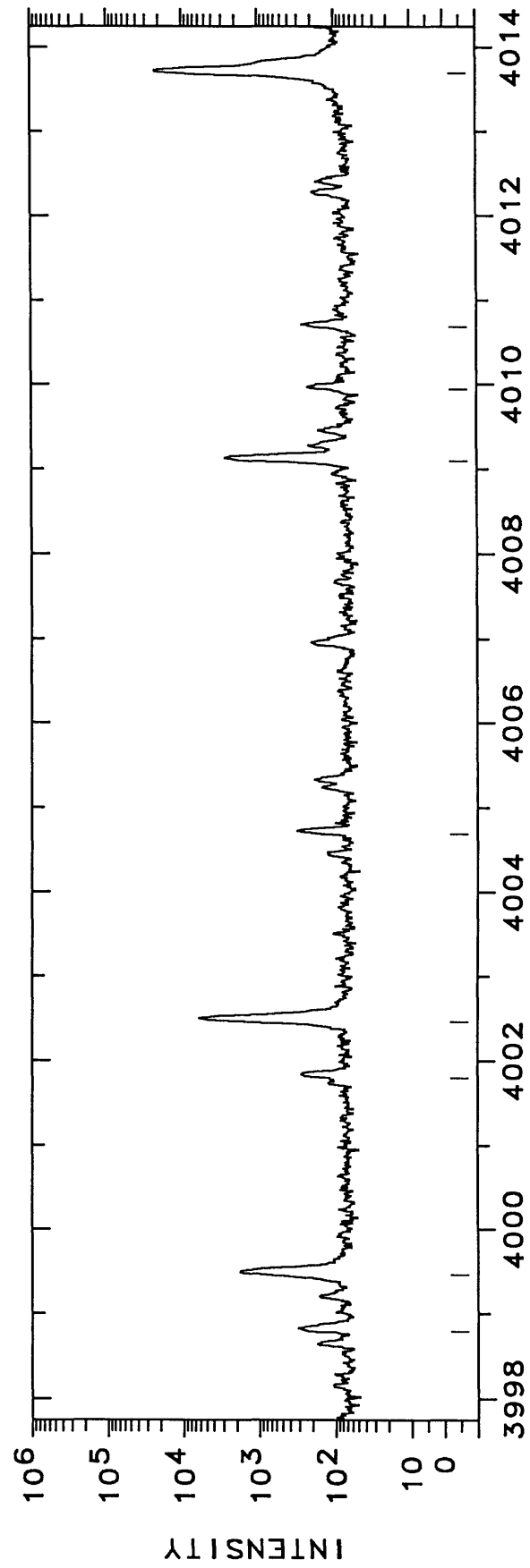
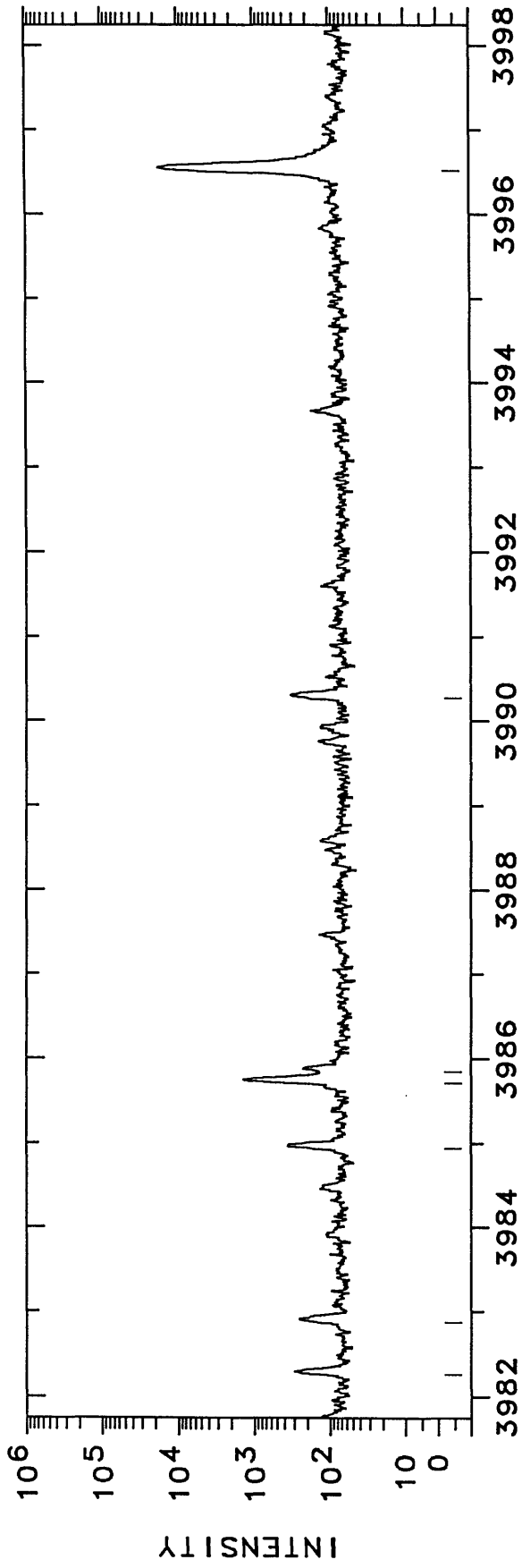
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3953.6375	25286.008	1800	Pt I	15501- 40787	E	3970.0530	25181.457	Pt II	36484- 61665	16
3961.51	25235.8		Al I			3971.40	25172.9			190
3963.04	25226.0	170	Pt I	62567- 37342	N	3973.458	25159.88	Ne II		C
3966.3570	25204.921	150000	Pt I	10116- 35321	E	3975.69	25145.8			640
3968.44	25191.7		Ca II			3980.6010	25114.731	Pt I	26638- 51753	E



WAVELENGTH (ANGSTROMS) - AIR

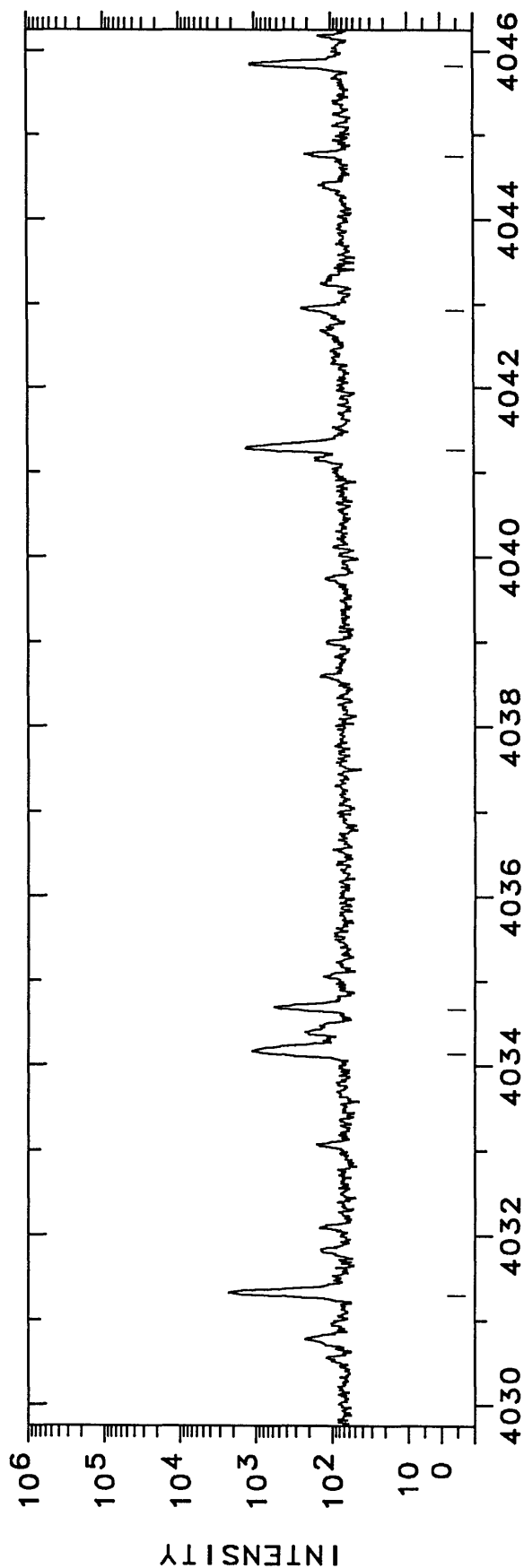
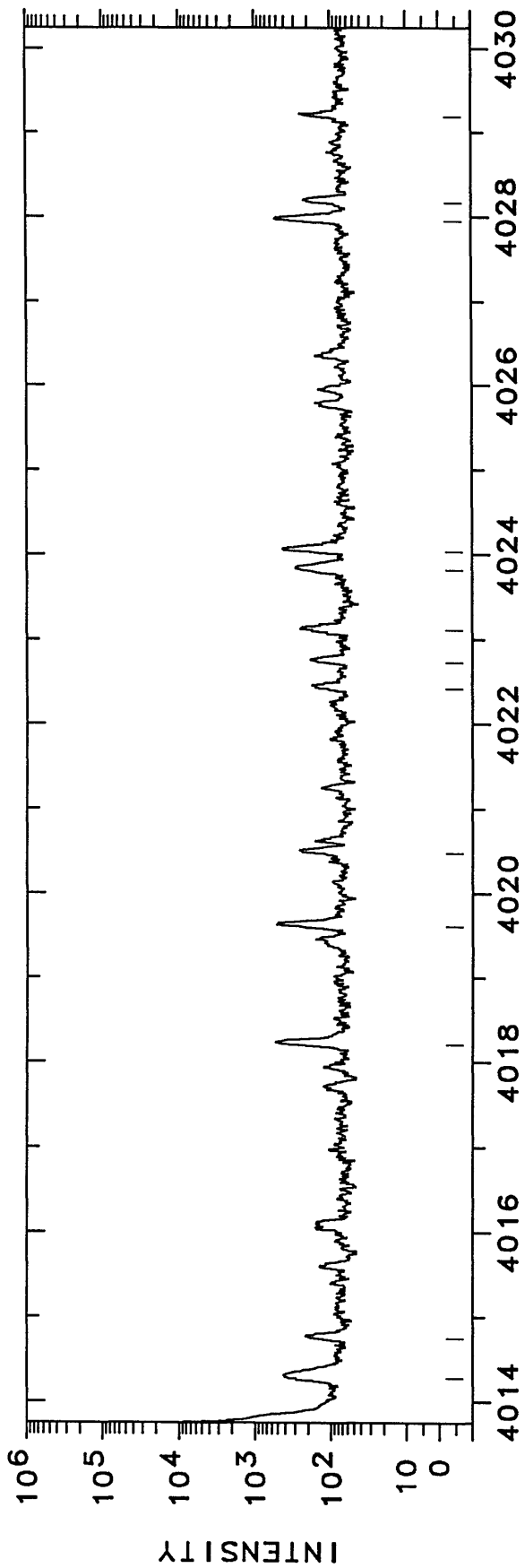


WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
3982.26	25104.3	230	Pt II	105962- 80858	3999.468	24996.26	1700	Ne II	C
3982.87	25100.4	200			4001.80	24981.7	220	Pt I	68169- 43187
3984.94	25087.4	300	Pt I	68275- 43187	4002.4834	24977.427	6100	Pt I	62567- 37590
3985.723	25082.46	1300	Ne II		4004.69	24963.7	260		
3985.85	25081.7	170			4009.0950	24936.236	2700	Pt I	62705- 37769
3990.27	25053.9	270			4009.94	24931.0	160		
3996.5674	25014.399	17000	Pt I	15501- 40516	4010.68	24926.4	210		
3998.79	25000.5	250	Pt II	41434- 66434	4013.7145	24907.536	23000	Pt II	101517- 76610



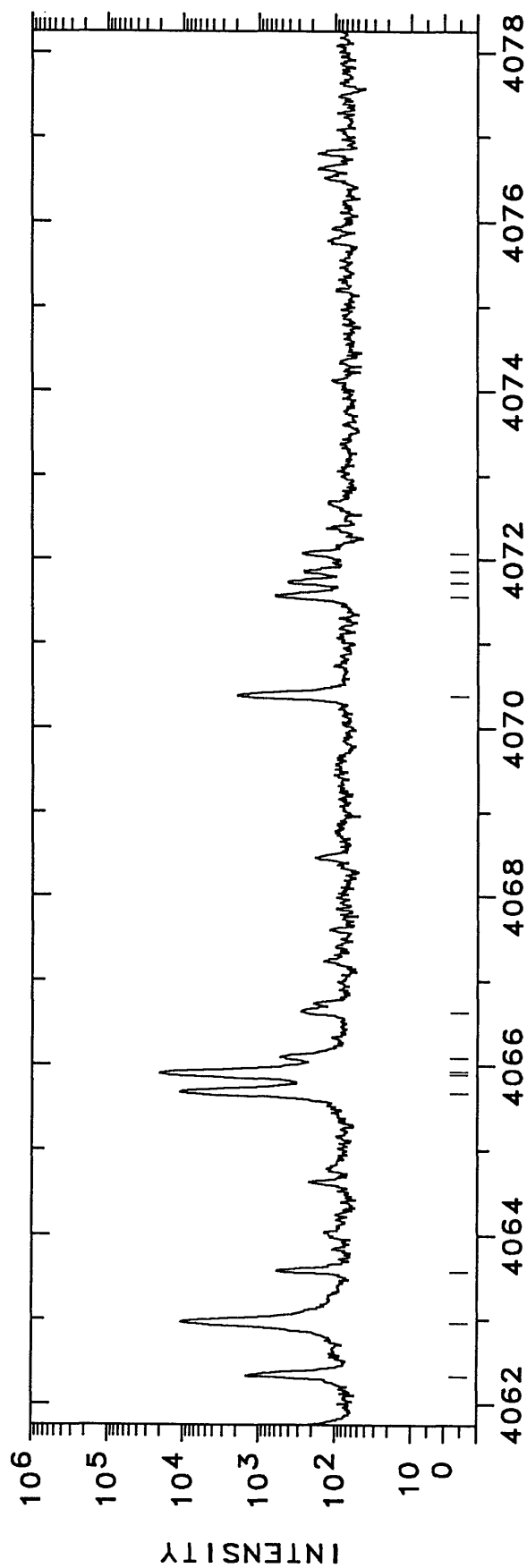
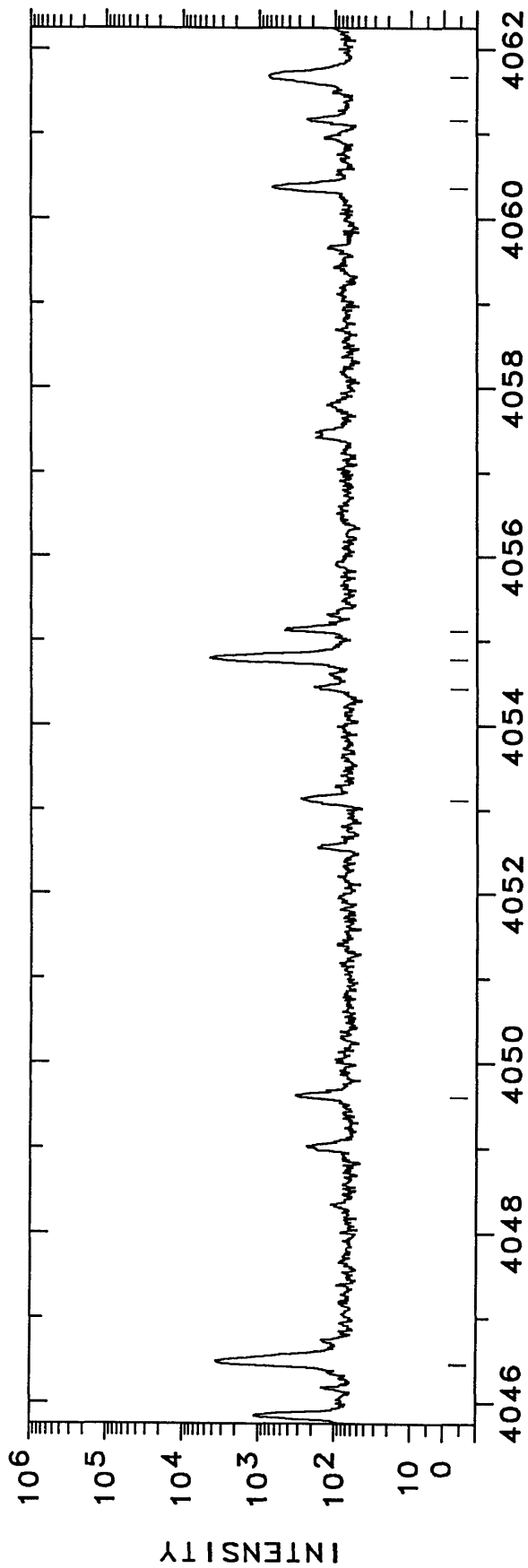
WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	
4014.3061	24903.866	360	Pt II	37877- 62781	30	4027.95	24819.5	Pt I	16983- 41802	N
4014.75	24901.1	160				4028.17	24818.2			
4018.21	24879.7	480	Pt I	65395- 40516	N	4029.19	24811.9			
4019.61	24871.0	460	Pt I	65387- 40516	N	4031.2981	24798.898	Pt I	62567- 37769	N
4020.48	24865.6	200				4034.14	24781.4			
4022.42	24853.6	110				4034.66	24778.2			
4022.73	24851.7	130				4041.2943	24737.559	Pt II	101199- 76461	42
4023.11	24849.4	190				4042.92	24727.6			
4023.8153	24845.014	230	Pt II	29030- 53875	17	4044.75	24716.4			
4024.041	24843.62	370	Ne II		C	4045.8124	24709.934	Fe I		Q

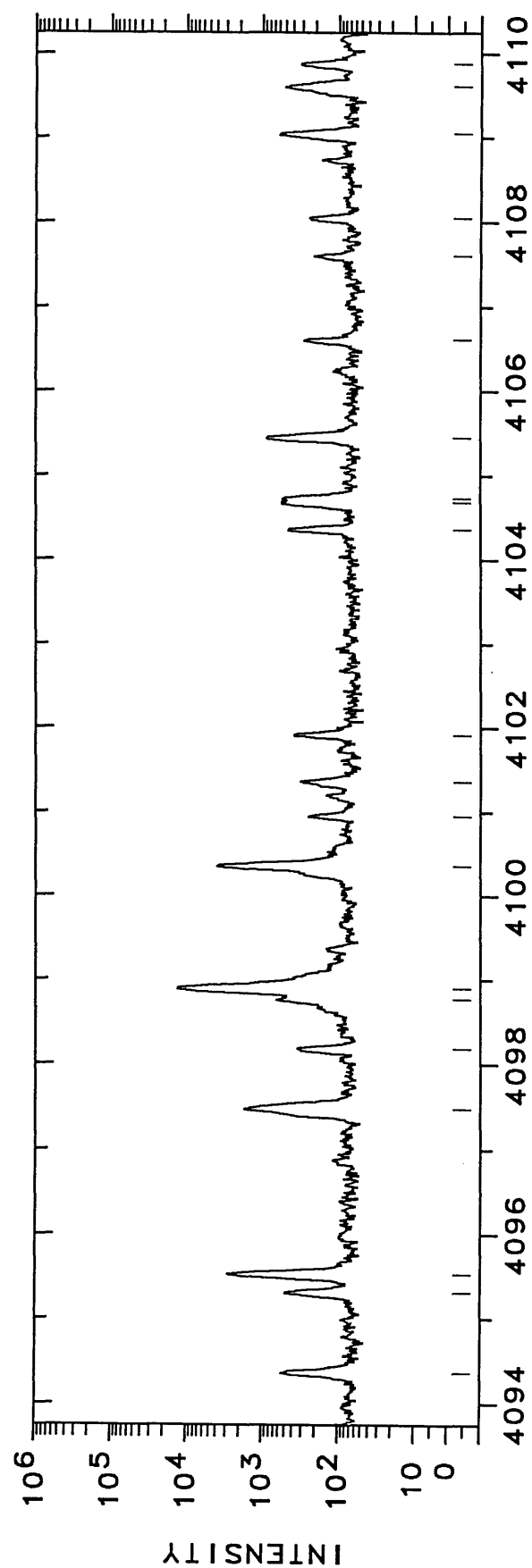
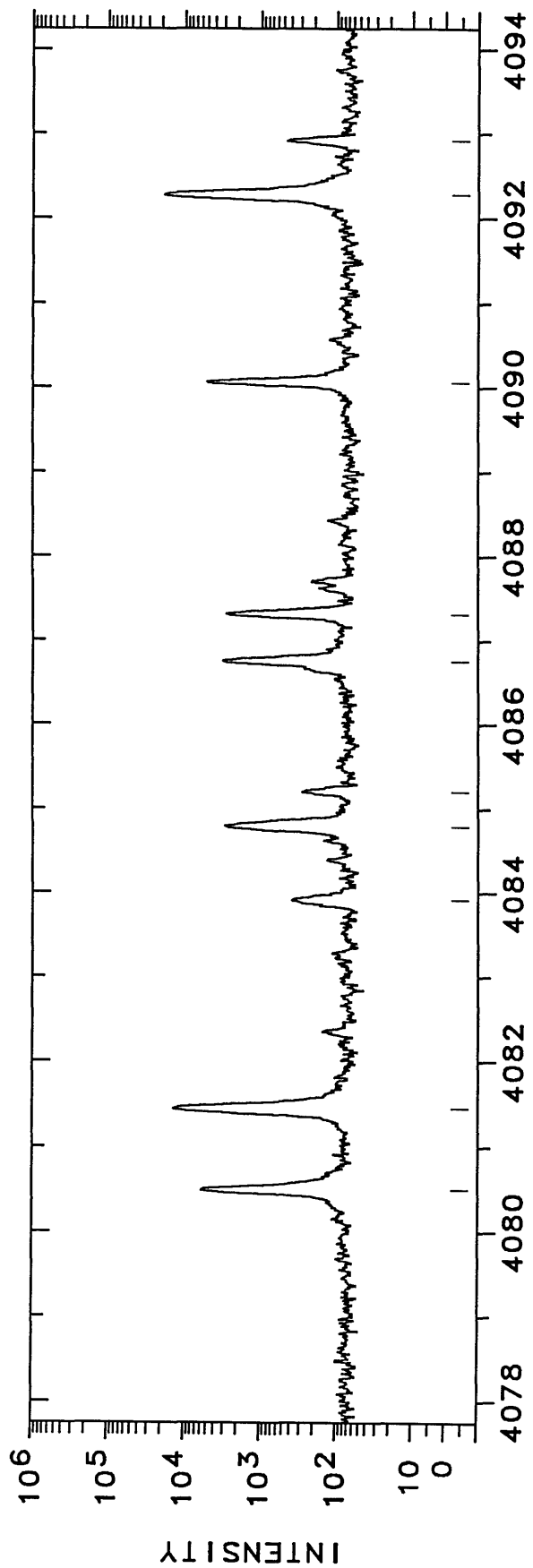


WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
4046.4498	24706.042	2100 P	Pt II	36484- 61190 J	4063.5940	24601.810		Fe I	q
4046.4749	24705.889	1800 U	Pt II	36484- 61190 J	4065.7046	24589.039	11000	Pt II	101199- 76610 22
4049.60	24686.8	270			4065.8895	24587.921	6000 U	Pt I	60884- 36296 H
4053.1114	24665.436	220	Pt II	96614- 71948 27	4065.9283	24587.686	16000 P	Pt I	60884- 36296 H
4054.43	24657.4	130			4066.09	24586.7	460	Pt I	59908- 35321 N
4054.7658	24655.373	4400	Pt I	21967- 46622 E	4066.63	24583.4	220		
4055.11	24653.3	400			4070.3844	24560.769	1900	Pt I	59882- 35321 E
4060.36	24621.4	610	Pt I	18566- 43187 N	4071.55	24553.7	560		
4061.16	24616.6	170	Pt I	65132- 40516 N	4071.7379	24552.605		Fe I	q
4061.6597	24613.526	690	Pt II	29261- 53875 18	4071.85	24551.9	200		
4062.33	24609.5	1400			4072.1002	24550.420	210	Pt I	59872- 35321 N
4062.9730	24605.570	11000	Ne II	G					



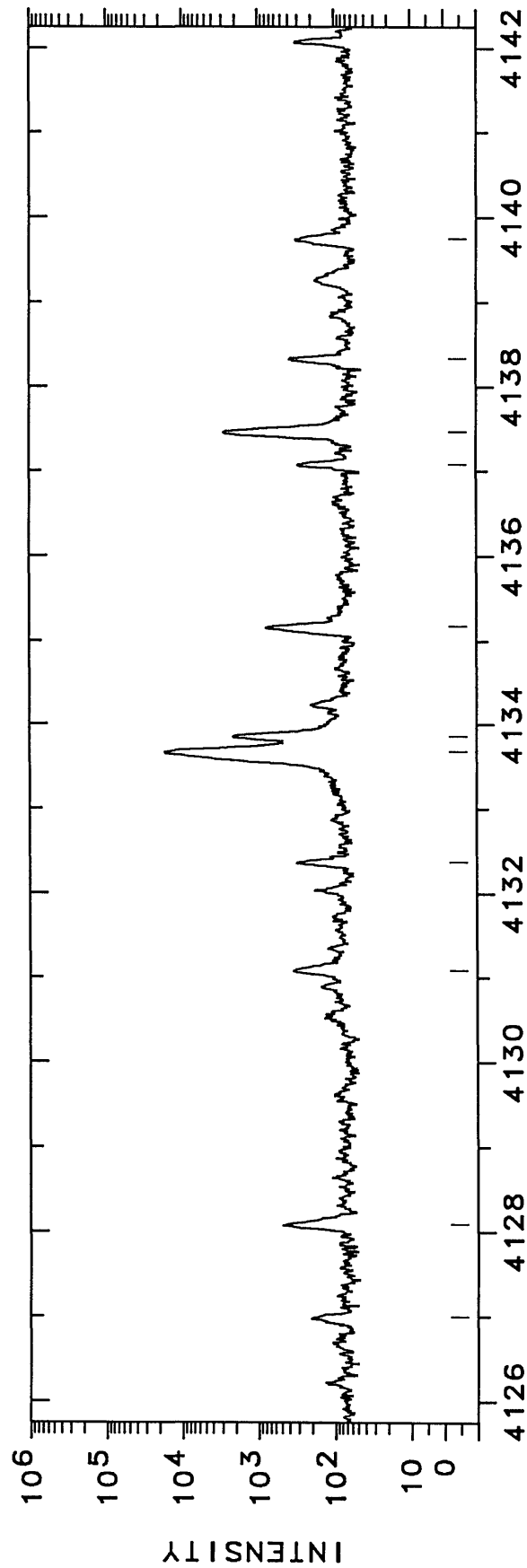
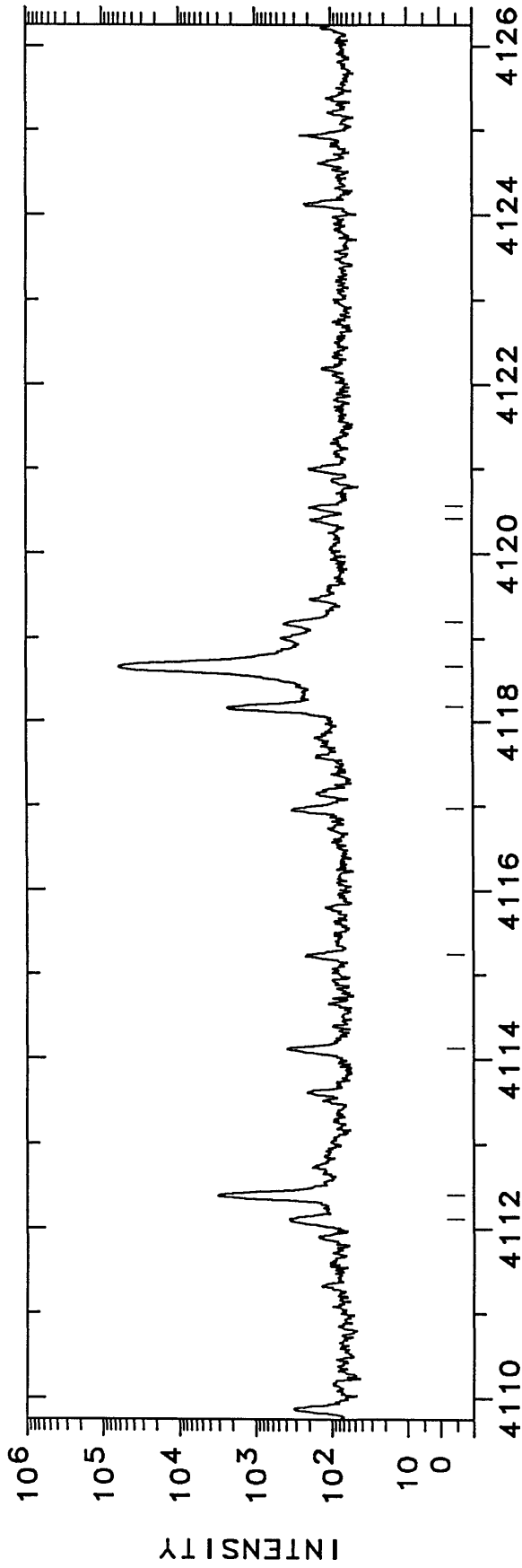
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4080.516	24499.79	5900	Ne II	C	4098.864	24390.12	13000	Ne II	C
4081.4669	24494.080	14000 C	Pt I	60790-36296 E	4100.354	24381.26	3900	Ne II	C
4083.9285	24479.316	330			4100.95	24377.7	190		
4084.7775	24474.229	2900	Pt I	64668-40194 N	4101.36	24375.3	260		
4085.21	24471.6	220			4101.928	24371.90	320	Ne II	C
4086.769	24462.30	3100	Ne II	C	4104.36	24357.5	400		
4087.3313	24458.937	2800	Pt I	26638-51097 E	4104.68	24355.6	490		
4090.0628	24442.603	5100	Pt I	59764-35321 E	4104.73	24355.3	490		
4092.2522	24429.526	19000	Pt I	59751-35321 E	4105.4613	24350.927	820	Pt II	32237-56587 16
4092.92	24425.5	400	Pt I	65395-40970 N	4106.61	24344.1	220		
4094.36	24416.9	490	Pt I	65387-40970 N	4107.60	24338.2	150	Pt I	65308-40970 N
4095.31	24411.3	430			4108.05	24335.6	180		
4095.5370	24409.933	2800	Pt I	59731-35321 E	4109.05	24329.7	550	Pt I	68275-43945 N
4097.48	24398.4	1700	Pt I	68831-44432 N	4109.61	24326.3	450	Pt I	68759-44432 N
4098.1807	24394.187	280			4109.88	24324.7	250		
4098.77	24390.7	590							



WAVELENGTH (ANGSTROMS) - AIR



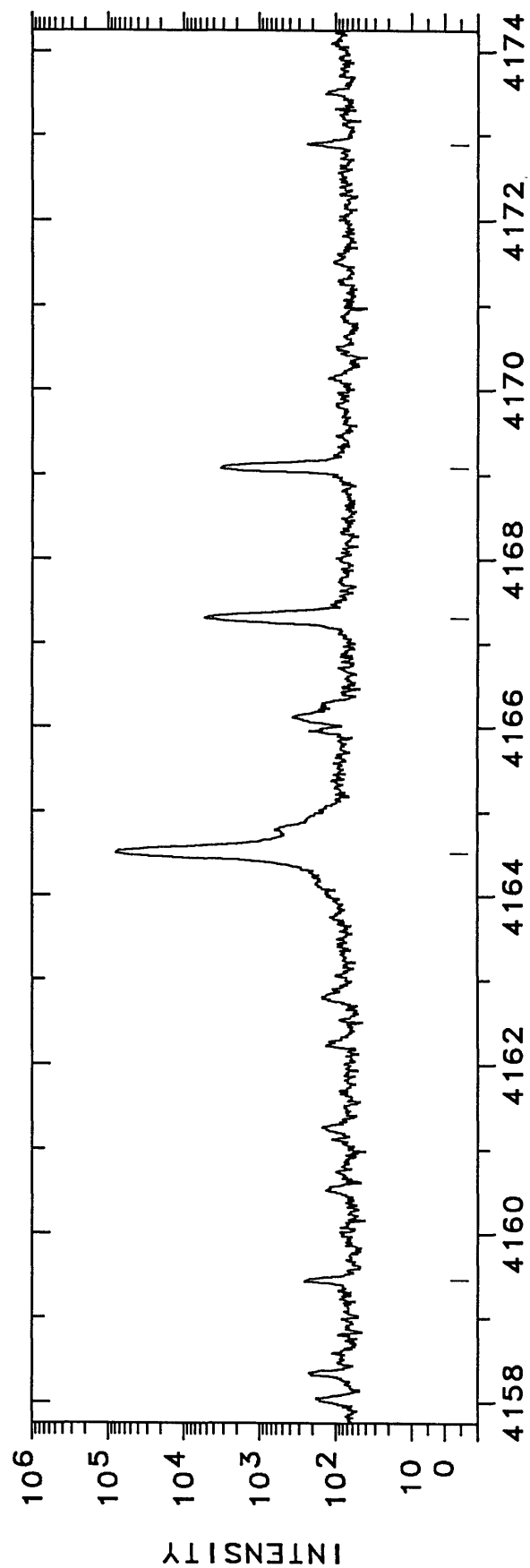
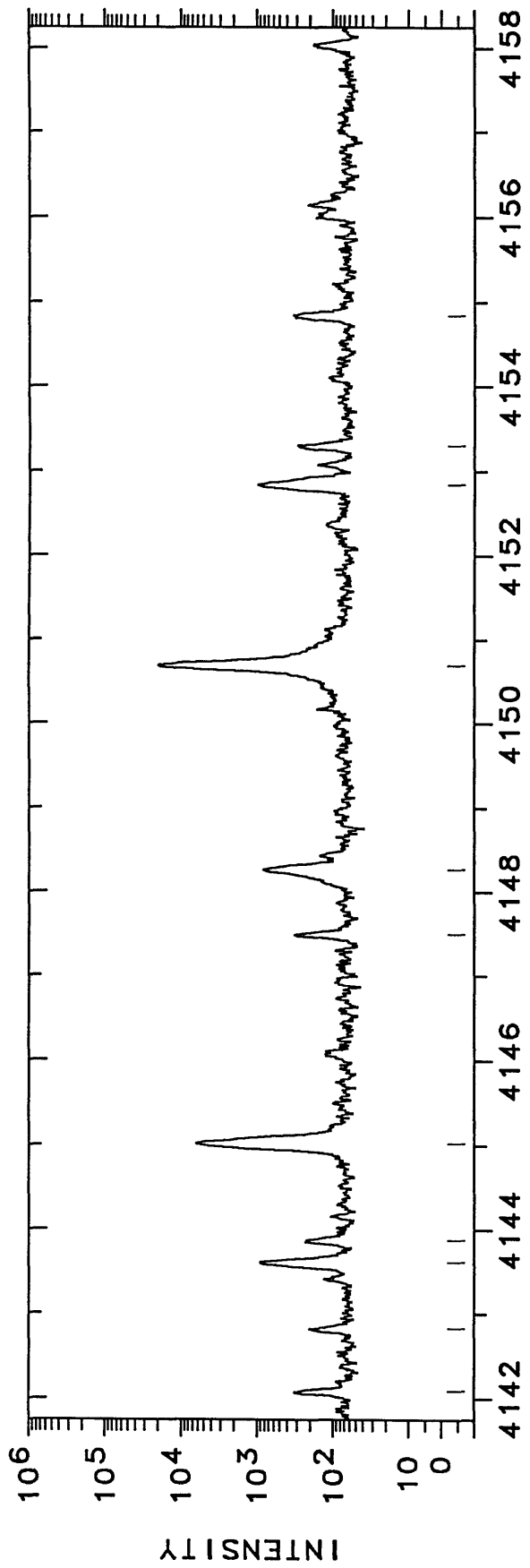
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4112.12	24311.5	300	Pt I	64505- 40194	4128.09	24217.4	420		
4112.395	24309.87	3000	Ne II		4131.09	24199.9	280		
4114.13	24299.6	330			4132.38	24192.3	250		
4115.24	24293.1	160			4133.691	24184.63	17000	Ne II	C
4116.97	24282.9	270			4133.871	24183.58	2000	Ne II	C
4118.199	24275.61	2200	Ne II		4135.18	24175.9	710	Pt I	68121- 43945
4118.6745	24272.808	89000	Pt I	13496- 37769	4137.08	24164.8	230	Pt I	65132- 40970
4119.20	24269.7	350			4137.47	24162.5	2700		
4120.41	24262.6	120			4138.34	24157.5	320		
4120.56	24261.7	130			4139.75	24149.2	250	Pt I	68094- 43945
4127.00	24223.8	140	Pt I	68169- 43945					



WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
4152.84	24073.1	920	Pt I	64267- 40194 N
4153.30	24070.5	240		
4154.84	24061.5	270	Pt I	68006- 43945 N
4159.45	24034.9	200		
4164.5491	24005.436	78000	Pt I	10116- 34122 E
4167.30	23989.6	5300	Pt I	64505- 40516 N
4169.08	23979.3	3100	Pt II	101517- 77538 K
4172.89	23957.5	180		

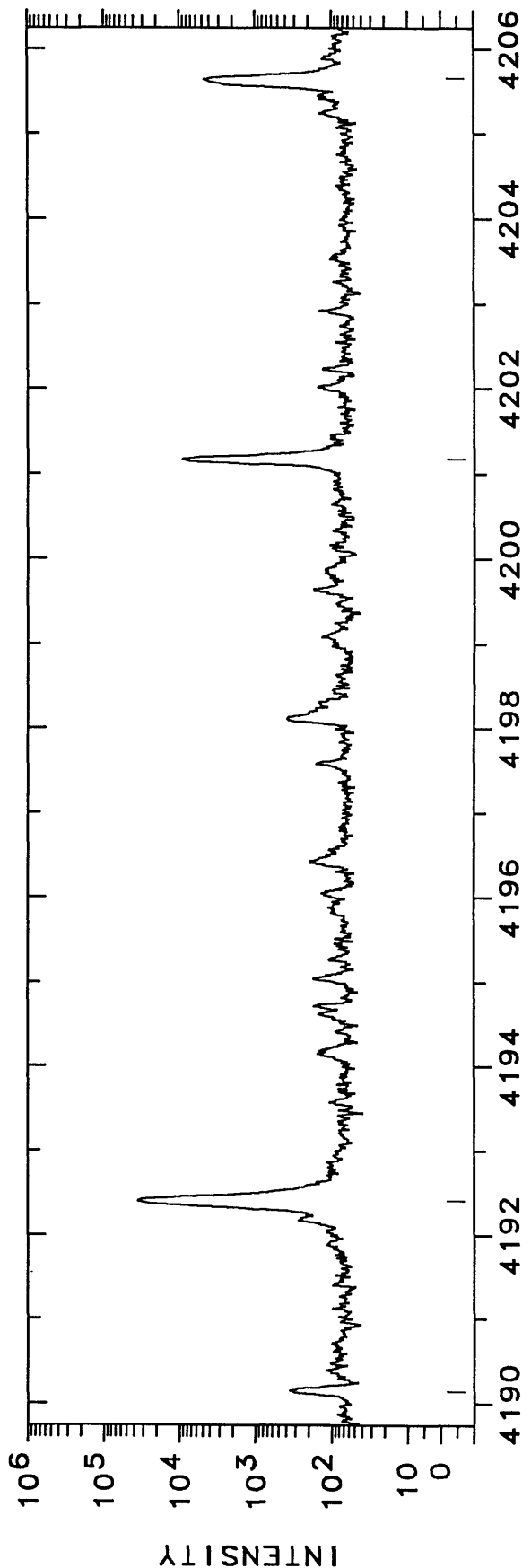
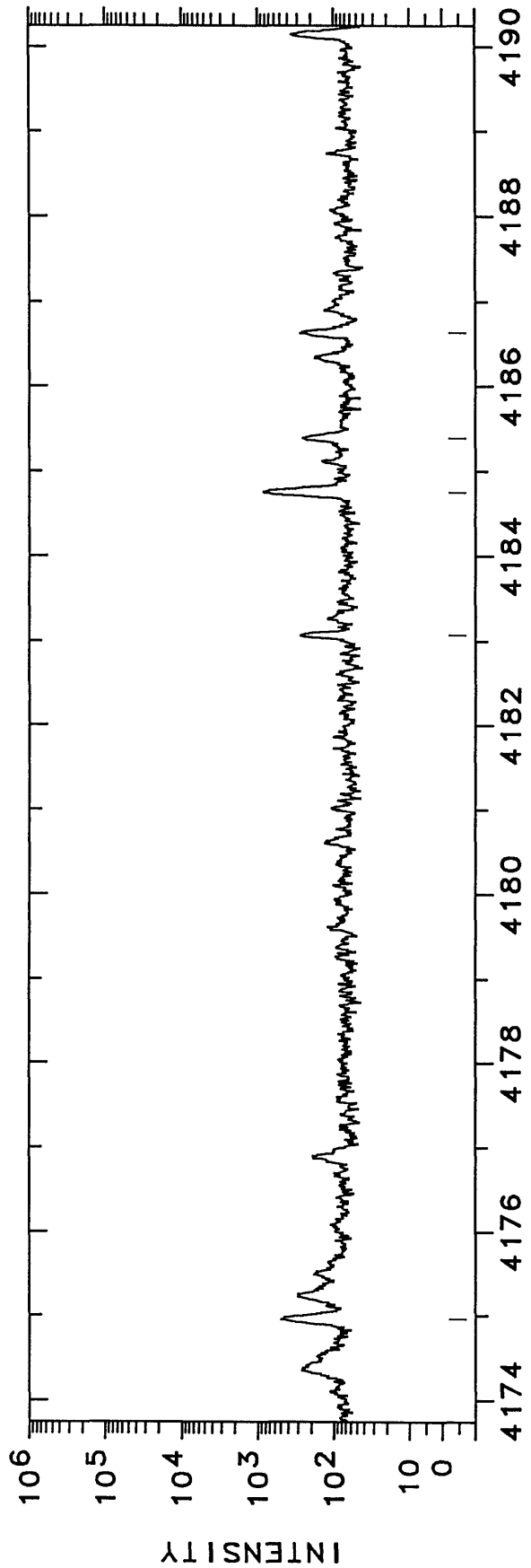
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4142.09	24135.6	260		
4142.83	24131.3	150		
4143.61	24126.7	840	Pt I	68072- 43945 N
4143.8680	24125.240		Fe I	Q
4145.03	24118.5	6300	Pt I	64312- 40194 N
4147.50	24104.1	260		
4148.2820	24099.569	770	Pt II	32918- 57018 16
4150.6893	24085.592	20000	Ne II	G



WAVELENGTH (ANGSTROMS) - AIR

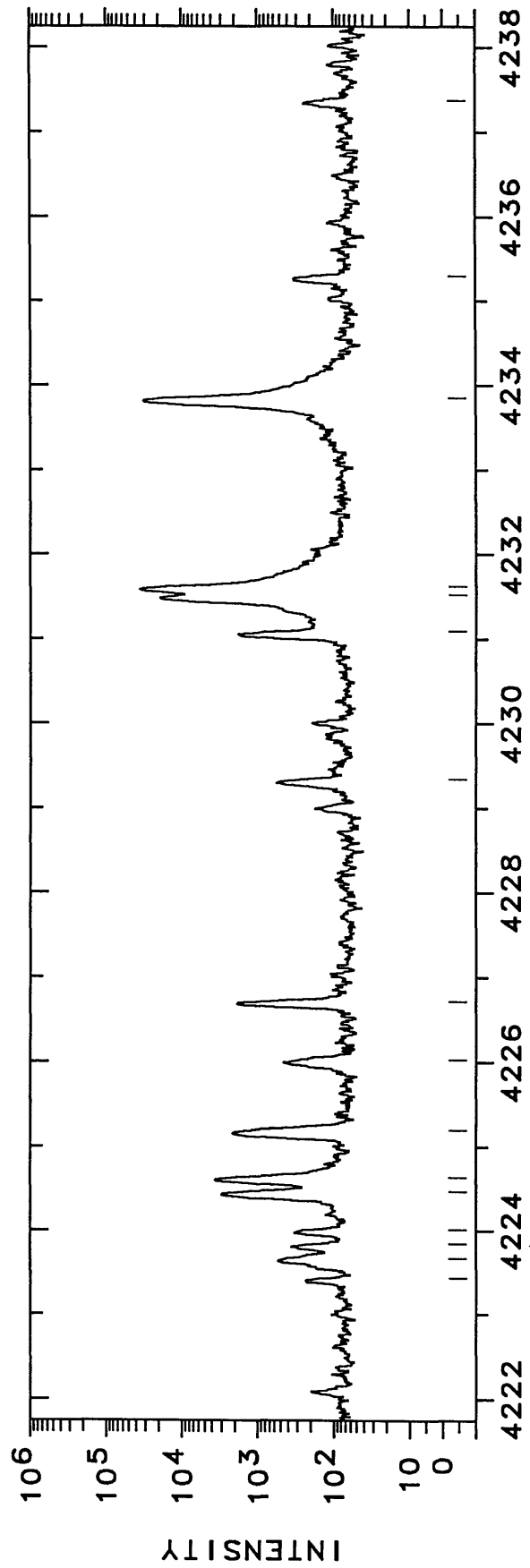
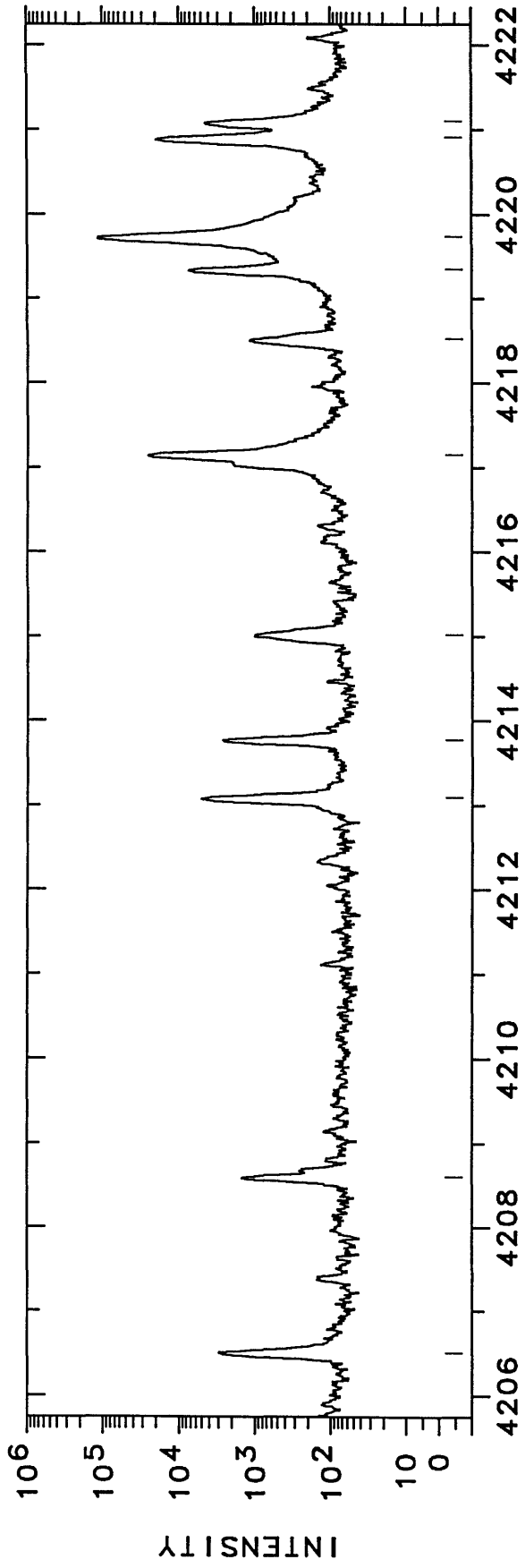
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4190.14	23858.8	300	Pt II	117340- 93482 K
4192.4231	23845.835	35000	Pt I	13496- 37342 E
4201.2102	23795.961	9200	Pt I	60640- 36844 E
4205.5937	23771.159	4700	Ne II	

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
4174.96	23945.6	440	Pt II	106434- 82535 K
4183.07	23899.2	220	Pt I	62705- 38815 N
4184.75	23889.6	780		
4185.39	23885.9	200		
4186.662	23878.65	230	Ne II	C



WAVELENGTH (ANGSTROMS) - AIR

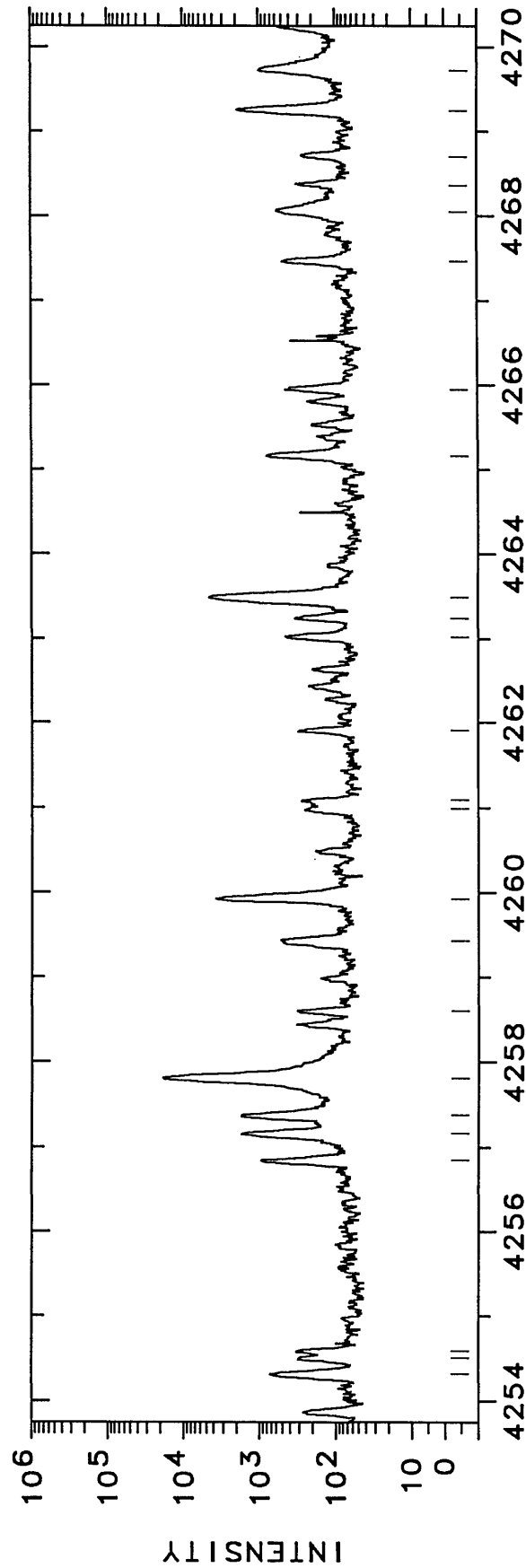
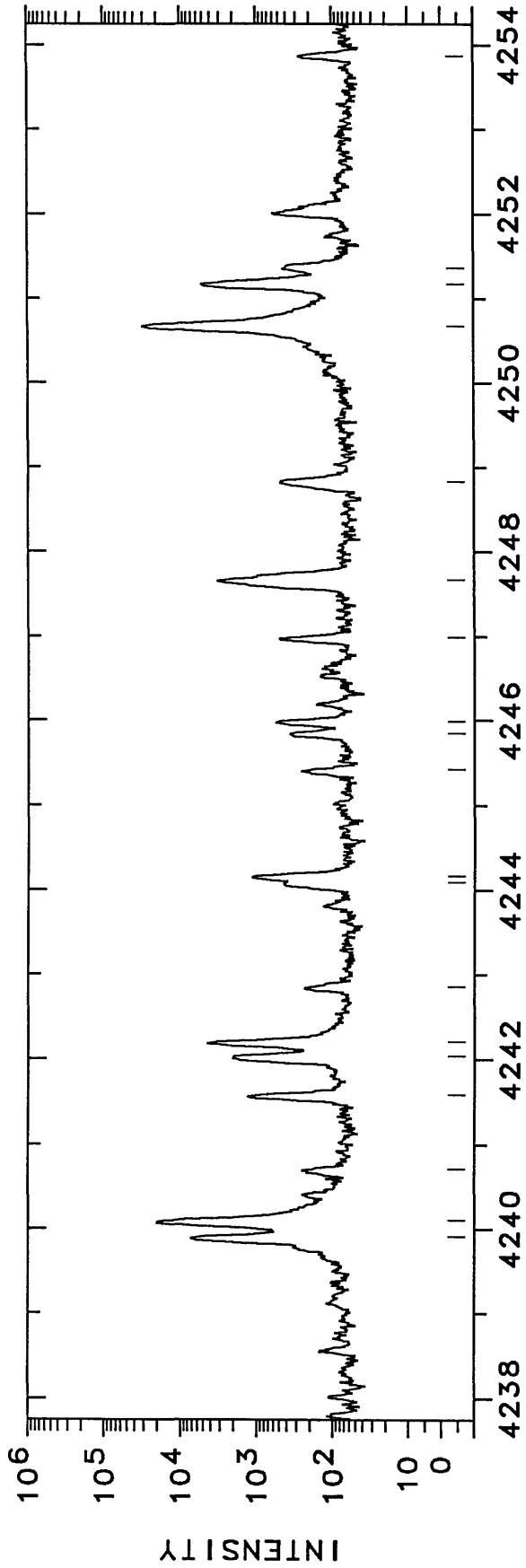




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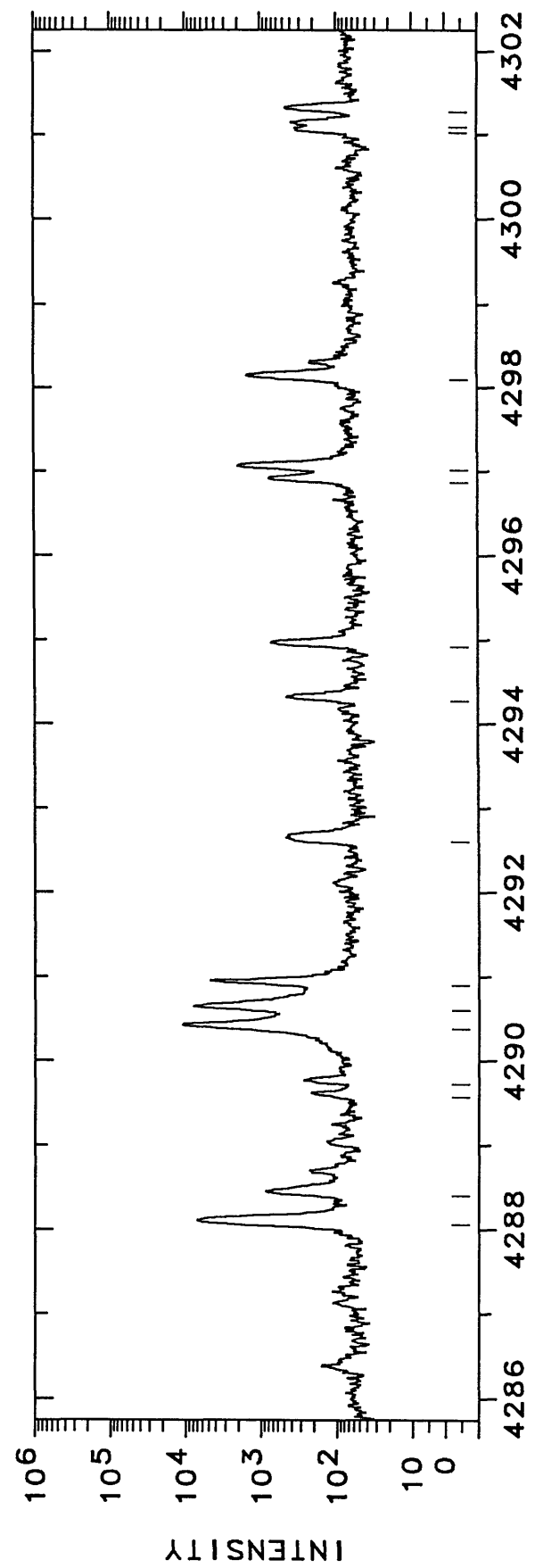
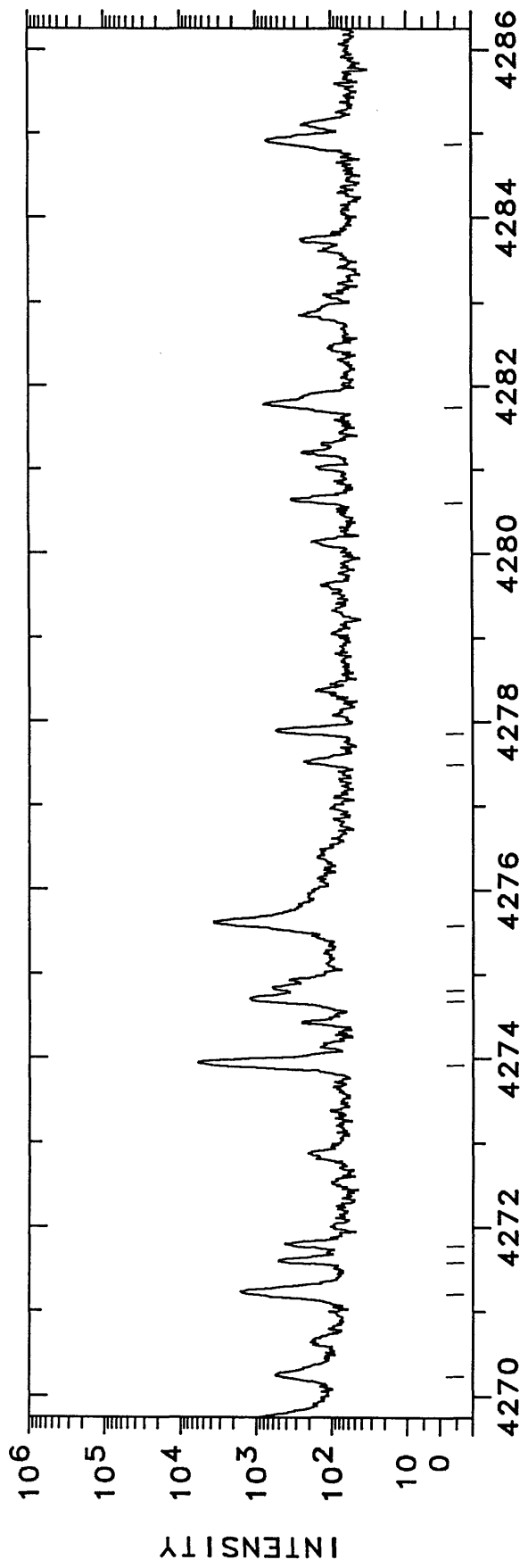


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4239.9190	23578.717	7300	Ne II	G	4256.85	23484.9	900		
4240.1049	23577.683	21000	Ne II	G	4257.180	23483.12	1700	Ne II	C
4240.72	23574.3	190	Pt I	68006-44432	4257.395	23481.93	1700	Ne II	C
4241.59	23569.4	1200	Ne II		4257.8028	23479.683	19000	Ne II	G
4242.040	23566.93	2100	Ne II	C	4258.60	23475.3	270		
4242.2094	23565.987	4400	Ne II	G	4259.43	23470.7	470		
4242.86	23562.4	180	Pt I	68006-44444	4259.9310	23467.953	3800	Pt I	59764-36296
4244.10	23555.5	390	Ne II		4260.99	23462.1	200	Pt II	106434-82972
4244.17	23555.1	1100	Pt II	42031-65587	4261.09	23461.6	220		
4245.42	23548.2	200	Pt I		4261.91	23457.1	250	Ne III	L
4245.85	23545.8	310	Pt I		4263.02	23450.9	400		
4245.99	23545.0	500	Pt I	68275-44730	4263.24	23449.7	290		
4246.99	23539.5	450	Pt I		4263.5022	23448.296	4600	Pt I	60790-37342
4247.6735	23535.673	3200	Pt I	64505-40970	4265.16	23439.2	750	Ne III	AL
4248.83	23529.3	430	Ne II		4265.16	23439.2	750	Pt I	68169-44730
4250.6462	23519.214	31000	Pt I		4265.95	23434.8	400		
4251.17	23516.3	5100	Pt I	59812-36296	4267.46	23426.5	440	Pt II	105962-82535
4251.36	23515.3	390	Cr I		4268.05	23423.3	520	Ne III	L
4253.87	23501.4	210			4268.36	23421.6	260		
4254.32	23498.9	250			4268.70	23419.7	220		
4254.51	23497.9	270			4269.2490	23416.733	1900	Pt I	26638-50055
4254.59	23497.4				4269.72	23414.1	930		



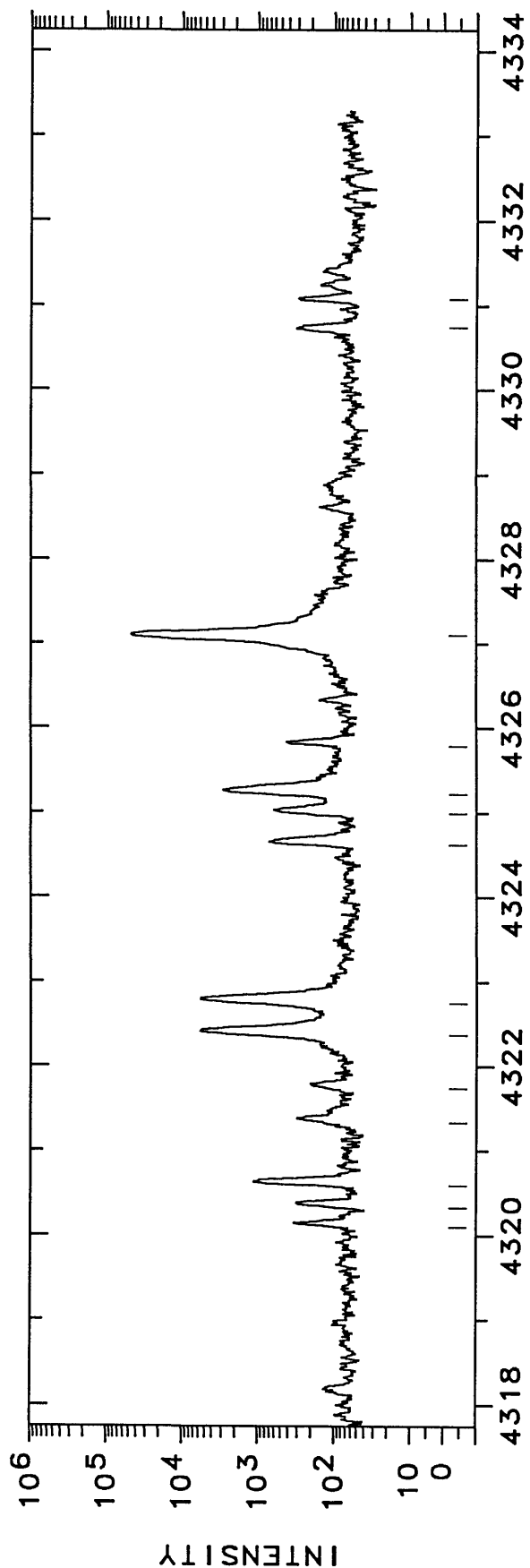
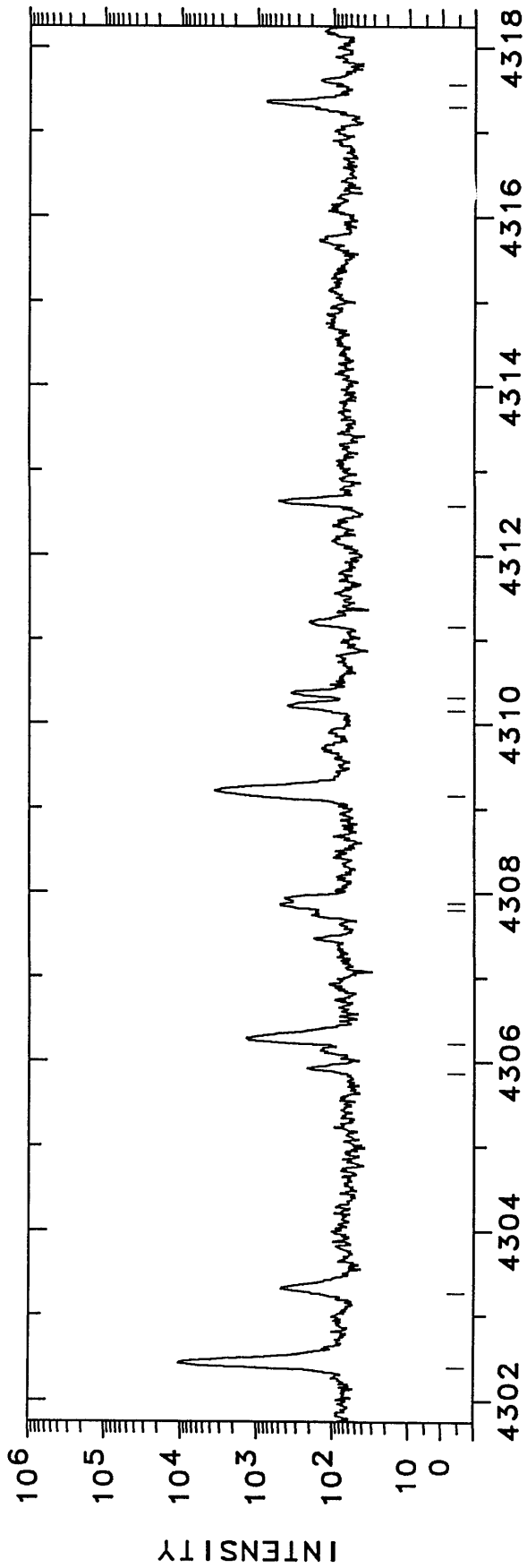
WAVELENGTH (ANGSTROMS) - AIR

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4270.23	23411.4	510	Ne I		4289.57	23305.8	170		
4271.20	23406.0	1600	Pt I	63922- 40516 N	4289.73	23304.9		Cr I	
4271.58	23404.0	460			4290.574	23301.44	11000	Ne II	C
4271.7604	23402.966		Fe I		4290.602	23300.20	8000	Ne II	C
4273.92	23391.1	5800	Pt I	68121- 44730 N	4290.8991	23298.584	4700	Pt I	60640- 37342 E
4274.68	23387.0	1200			4292.60	23289.4	410		
4274.81	23386.3		Cr I		4294.27	23280.3	400		
4275.58	23382.1	3600	Ne I		4294.92	23276.8	670	Pt I	68006- 44730 N
4277.49	23371.6	180			4296.86	23266.3	710		
4277.86	23369.6	500			4297.01	23265.5	1900		
4280.60	23354.6	280			4298.096	23259.57	1500	Ne II	C
4281.7393	23348.425	710	Pt I	13496- 36844 E	4301.02	23243.8	290		
4284.87	23331.4	660			4301.09	23243.4	320		
4288.0507	23314.060	7100	Pt I	15501- 38815 E	4301.27	23242.4	400	Pt I	26638- 49880 N
4288.3866	23312.234	810	Pt II	37877- 61190 31					



WAVELENGTH (ANGSTROMS) - AIR

WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE	WAVELENGTH	WAVE NUMBER	INTENSITY	CLASSIFICATION	CODE
4302.4207	23236.193	430	Pt I	18566- 41802 E	4320.10	23141.1	280		
4303.26	23231.7	430			4320.33	23139.9	260		
4305.87	23217.6	160			4320.59	23138.5	1100	Pt II	105962- 82824 K
4306.22	23215.7	1300	Ne I		4321.33	23134.5	250	Pt I	63922- 40787 N
4307.80	23207.2	440	Pt II	116689- 93482 K	4321.74	23132.3	150		
4307.9021	23206.628		Fe I		4322.3727	23128.937	5800	Ne II	
4309.1759	23199.768	3600	Pt I	60790- 37590 E	4322.7409	23126.967	5700	Ne II	
4310.16	23194.5	340			4324.62	23116.9	650		
4310.31	23193.7	300			4324.99	23114.9	560	Pt I	60884- 37769 N
4311.15	23189.1	150	Pt II	46046- 69235 AK	4325.235	23113.63	2900	Ne II	
4311.15	23189.1	150	Pt II	105086- 81897 AK	4325.7618	23110.816		Fe I	
4312.59	23181.4	470			4327.0533	23103.919	17000	Pt I	56784- 33680 E
4317.30	23156.1	720	Pt II	101199- 78043 K	4330.74	23084.3	70		
4317.56	23154.7	91			4331.08	23082.4	65	Pt II	106434- 83352 K



WAVELENGTH (ANGSTROMS) - AIR

# *Energy Levels of Neutral Platinum*

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Volume 97

Number 1

January–February 1992

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All known energy levels of neutral platinum (Pt I) are presented, including 119 new levels based on analysis of recent comprehensive observations of the spectrum. These results are taken from a detailed analysis of the spectrum to be published in *Journal de Physique II*.

**Key words:** atomic spectroscopy; electronic configurations; energy levels; platinum.

**Accepted:** December 30, 1991

and

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## 1. Introduction

An extensive analysis of the energy levels of neutral platinum (Pt I) based on new spectra recorded at the National Institute of Standards and Technology [1], at Kitt Peak National Observatory [2], and at Laboratoire Aimé Cotton has recently been prepared for publication elsewhere [3]. For complete-

ness of the present special issue of the Journal of Research of the National Institute of Standards and Technology we list in Tables 1 and 2 the values of the Pt I energy levels. Full details of the analysis are given in Ref. [3].

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<sup>1</sup> In association with Université Paris-Sud.

**Table 1.** Even energy levels of Pt I. The leading components of the eigenfunctions are derived from theoretical studies of the configuration groups ( $5d + 6s$ )<sup>10</sup>,  $5d^9 6d$ ,  $5d^9 7s$ ,  $5d^9 7d$ , and  $5d^9 8s$ . Where other configurations are indicated, the designations are empirical

Energy (cm <sup>-1</sup> )	<i>J</i>	Leading component	Energy (cm <sup>-1</sup> )	<i>J</i>	Leading component
0.	3	$5d^9 6s^3 D$	63922.22	3	
775.892	2	$5d^9 6s^1 D$	64128.722	5,4	
823.678	4	$5d^8 6s^2^3 F$	64141.155	6	$5d^8 6s 6d (^3F_4, ^3D)$
6140.180	0	$5d^{10} 1S$	64182.29	2	
6567.461	2	$5d^9 6s^3 D$	64222.379	7	$5d^8 6s 6d (^3F_4, ^3D_3)$
10116.729	3	$5d^8 6s^2^3 F$	64267.43	5	$5d^8 6s 6d (^3F_4, ^3D)$
10131.887	1	$5d^9 6s^3 D$	64312.78	4	$5d^8 6s 6d (^3F_4, ^3D)$
13496.271	2	$5d^9 6s^1 D$	64330.53	6	$5d^8 6s 6d (^3F_4)$
15501.845	2	$5d^8 6s^2^3 F$	64379.155	5	$5d^8 6s 6d (^3F_4)$
16983.492	0	$5d^8 6s^2^3 P$	64505.839	3	$5d^8 6s 7s (^3F_3, ^3S_1)$
18566.558	1	$5d^8 6s^2^3 P$	64668.46	4	$5d^8 6s 6d (^3F_4, ^3D)$
21967.111	4	$5d^8 6s^2^1 G$	65132.91	2	$5d^9 7d^3 P$
26638.591	2	$5d^8 6s^2^1 D$	65308.53	4	$5d^9 7d^3 G$
52379.375	3	$5d^9 7s^3 D$	65339.93	5	$5d^9 7d^3 G$
52667.213	2	$5d^9 7s^1 D$	65346.52	3	$5d^9 7d^3 F$
55640.623	5	$5d^8 6s 7s (^3F_4, ^3S_1)$	65361.63	1	$5d^9 7d^1 P$
56784.325	4	$5d^8 6s 7s (^3F_4, ^3S_1)$	65381.38	4	$5d^9 7d^3 F$
59591.82	1	$5d^9 6d^3 S$	65387.03	3	$5d^9 7d^3 D$
59731.571	2	$5d^9 6d^3 P$	65395.72	2	$5d^9 7d^1 D$
59751.177	4	$5d^9 6d^3 G$	66967.965	5	$5d^8 6s 8s (^3F_4, ^3S_1)$
59764.266	3	$5d^9 6d^3 D$	67342.66	4	$5d^8 6s 8s (^3F_4, ^3S_1)$
59782.853	1	$5d^9 6d^1 P$	68006.95	3	$5d^9 6d^3 G$
59812.72	5	$5d^9 6d^3 G$	68072.245	3	$5d^9 6d^3 F$
59872.140	3	$5d^9 6d^1 F$	68094.74	2	$5d^9 6d^3 F$
59882.421	4	$5d^9 6d^3 F$	68121.56	4	$5d^9 6d^3 G$
59908.170	2	$5d^9 6d^1 D$	68169.42	2	$5d^9 6d^1 D$
60357.804	1	$5d^9 7s^3 D$	68275.31	2	
60573.69	0	$5d^9 6d^1 S$	68703.45	4	
60640.669	2	$5d^9 7s^3 D$	68716.32	6	$5d^8 6s 6d (^3F_4, ^1D_2)$
60790.393	3	$5d^8 6s 7s (^3F_4, ^3S_1)$	68759.01	4	
60884.001	4	$5d^8 6s 7s (^3F_4, ^1S_0)$	68831.115	5	
62567.995	3	$5d^9 8s^3 D$	68912.21	4	
62705.33	2	$5d^9 8s^1 D$	68947.47	3	



**Table 2.** Odd energy levels of Pt I. The leading components of the eigenfunctions are derived from theoretical studies of the mixed group of configurations  $5d^9 6p + 5d^8 6s 6p + 5d^7 6s^2 6p + 5d^9 7p$ . Where other configurations are indicated, the designations are empirical

Energy ( $\text{cm}^{-1}$ )	<i>J</i>	Leading component	Energy ( $\text{cm}^{-1}$ )	<i>J</i>	Leading component
30156.854	4	$5d^8 6s 6p$ ( $^4F$ ) $^5D$	54839.206	3	$5d^8 6s 6p$ ( $^4P$ ) $^3D$
32620.018	2	$5d^9 6p$ $^3P$	55009.37	4	$5d^8 6s 6p$ ( $^2G$ ) $^3H$
33680.402	5	$5d^8 6s 6p$ ( $^4F$ ) $^5F$	55216.828	1	$5d^9 6p$ $^3D$
34122.165	3	$5d^9 6p$ $^3F$	55536.276	3	$5d^8 6s 6p$ ( $^2P$ ) $^3D$
35321.653	3	$5d^8 6s 6p$ ( $^4F$ ) $^5D$	55984.51	5	$5d^8 6s 6p$ ( $^2G$ ) $^3H$
36296.310	4	$5d^8 6s 6p$ ( $^4F$ ) $^5G$	56288.65	4	$5d^8 6s 6p$ ( $^2G$ ) $^3F$
36781.551	6	$5d^8 6s 6p$ ( $^4F$ ) $^5G$	56670.20	2	$5d^8 6s 6p$ ( $^4P$ ) $^3P$
36844.710	1	$5d^9 6p$ $^3P$	56794.43	5	$5d^7 6s^2 6p$ $^4F^*3G$
37342.101	2	$5d^9 6p$ $^3P$	57041.73	1	$5d^8 6s 6p$ ( $^4P$ ) $^3P$
37590.569	4	$5d^9 6p$ $^3F$	57506.187	3	$5d^8 6s 6p$ ( $^2G$ ) $^3F$
37769.073	3	$5d^9 6p$ $^3D$	57987.392	2	$5d^9 7p$ $^3P$
38536.160	5	$5d^8 6s 6p$ ( $^4F$ ) $^5F$	58101.17	3	$5d^9 7p$ $^3F$
38815.908	2	$5d^8 6s 6p$ ( $^2D$ ) $^3F$	58326.75	2	$5d^8 6s 6p$ ( $^2P$ ) $^3D$
40194.228	4	$5d^8 6s 6p$ ( $^4F$ ) $^5F$	58388.47	4	$5d^7 6s^2 6p$ $^4F^*5G$
40516.243	2	$5d^8 6s 6p$ ( $^4F$ ) $^5D$	58482.14	3	$5d^9 7p$ $^1F$
40787.857	2	$5d^8 6s 6p$ ( $^4P$ ) $^5P$	58780.80	1	$5d^9 7p$ $^1P$
40873.529	0	$5d^8 6s 6p$ ( $^2D$ ) $^3P$	59127.72	2	$5d^8 6s 6p$ ( $^2D$ ) $^3F$
40970.165	3	$5d^8 6s 6p$ ( $^4F$ ) $^5G$	59346.33	4	$5d^9 7p$ $^3F$
41802.744	1	$5d^8 6s 6p$ ( $^2D$ ) $^3D$	59462.28	2	$5d^9 7p$ $^1D$
42660.058	3	$5d^8 6s 6p$ ( $^4F$ ) $^5D$	59492.41	4	$5d^9 7p$ $^3F$
43187.836	1	$5d^8 6s 6p$ ( $^4F$ ) $^5D$	59686.20	3	$5d^7 6s^2 6p$ $^4F^*5G$
43945.543	3	$5d^8 6s 6p$ ( $^4P$ ) $^5P$	59792.23	1	$5d^8 6s 6p$ ( $^4P$ ) $^3S$
44432.663	4	$5d^8 6s 6p$ ( $^4F$ ) $^5G$	59916.97	2	$5d^9 7p$ $^1D$
44444.364	2	$5d^8 6s 6p$ ( $^4F$ ) $^5F$	59920.03	3	$5d^9 7p$ $^3D$
44730.313	3	$5d^8 6s 6p$ ( $^2F$ ) $^3D$	60328.02	3	$5d^8 6s 6p$ ( $^4F$ ) $^3F$
45398.478	1	$5d^8 6s 6p$ ( $^4P$ ) $^5P$	60423.93	4	$5d^8 6s 6p$ ( $^2G$ ) $^3G$
46170.386	2	$5d^9 6p$ $^3F$	60441.30	1	$5d^9 7p$ $^1P$
46419.962	2	$5d^8 6s 6p$ ( $^4P$ ) $^5D$	61097.48	2	$5d^8 6s 6p$ ( $^2G$ ) $^3F$
46433.912	0	$5d^8 6s 6p$ ( $^4P$ ) $^5D$	61352.25	3	$5d^8 6s 6p$ ( $^2G$ ) $^3F$
46622.489	3	$5d^8 6s 6p$ ( $^2F$ ) $^3D$	61633.79	5	$5d^8 6s 6p$ ( $^2G$ ) $^3G$
46792.965	5	$5d^8 6s 6p$ ( $^4F$ ) $^3G$	61645.33	2	$5d^8 6s 6p$ ( $^2G$ ) $^3F$
46963.670	4	$5d^8 6s 6p$ ( $^4P$ ) $^5D$	61942.22	4	$5d^8(^3F_4)6s 7p$ ( $^3P_0$ )
47740.565	1	$5d^9 6p$ $^1P$	62062.29	2	$5d^7 6s^2 6p$ $^4F^*5G$
48351.94	4	$5d^8 6s 6p$ ( $^4F$ ) $^3F$	62106.38	3	$5d^8 6s 6p$ ( $^4P$ ) $^3D$
48535.596	2	$5d^8 6s 6p$ ( $^4F$ ) $^5G$	62321.92	3	$5d^8 6s 6p$ ( $^2D$ ) $^3F$
48779.337	3	$5d^8 6s 6p$ ( $^4F$ ) $^3D$	62510.36	4	$5d^8(^3F_4)6s 7p$ ( $^3P_1$ )
49286.116	3	$5d^8 6s 6p$ ( $^4P$ ) $^5P$	62659.30	2	$5d^8 6s 6p$ ( $^4P$ ) $^3D$
49544.565	1	$5d^9 6p$ $^3D$	62835.58	5	$5d^8(^3F_4)6s 7p$ ( $^3P_1$ )
49880.883	2	$5d^9 6p$ $^3D$	63067.47	1	$5d^8 6s 6p$ ( $^2D$ ) $^3D$
50010.155	4	$5d^8 6s 6p$ ( $^2F$ ) $^3F$	63167.33	3	$5d^8(^3F_4)6s 7p$ ( $^3P_1$ )
50055.313	1	$5d^8 6s 6p$ ( $^4F$ ) $^5F$	63352.91	6	$5d^8(^3F_4)6s 7p$ ( $^3P_2$ )
50299.385	5	$5d^7 6s^2 6p$ $^4F^*3G$	63466.29	1	$5d^8 6s 6p$ ( $^2P$ ) $^3P$
50387.66	0	$5d^9 6p$ $^3P$	63826.31	2	$5d^7 6s^2 6p$ $^4F^*5G$
51097.529	3	$5d^8 6s 6p$ ( $^4P$ ) $^5D$	63945.05	5	$5d^8(^3F_4)6s 7p$ ( $^3P_2$ )
51286.946	2	$5d^8 6s 6p$ ( $^2F$ ) $^1D$	64248.95	2	$5d^8 6s 6p$ ( $^2D$ ) $^3D$
51545.544	3	$5d^8 6s 6p$ ( $^4F$ ) $^3D$	64319.385	4	$5d^8(^3F_4)6s 7p$ ( $^3P_2$ )
51753.317	2	$5d^8 6s 6p$ ( $^2F$ ) $^3F$	64515.68	2	$5d^7 6s^2 6p$ $^4F^*5G$
52071.684	1	$5d^8 6s 6p$ ( $^4P$ ) $^5D$	64619.64	1	$5d^8 6s 6p$ ( $^4P$ ) $^3D$
52438.59	5	$5d^8 6s 6p$ ( $^2F$ ) $^3G$	64675.92	3	$5d^7 6s^2 6p$ $^4P^*5D$
52520.13	4	$5d^8 6s 6p$ ( $^2F$ ) $^3F$	64904.25	3	$5d^8(^3F_4)6s 7p$ ( $^3P_2$ )
52708.365	2	$5d^8 6s 6p$ ( $^4P$ ) $^5D$	65306.80	1	$5d^9 5f$
53019.303	1	$5d^8 6s 6p$ ( $^2F$ ) $^3D$	65315.89	2	$5d^9 5f$
53665.25	1	$5d^8 6s 6p$ ( $^2P$ ) $^3D$	65318.95	6	$5d^9 5f$
53953.379	2	$5d^8 6s 6p$ ( $^2P$ ) $^3P$	65325.49	2	$5d^9 5f$
54011.150	3	$5d^8 6s 6p$ ( $^4P$ ) $^5P$	65331.20	3	$5d^9 5f$
54133.26	2	$5d^8 6s 6p$ ( $^4P$ ) $^5S$	65332.43	1	$5d^9 5f$
54178.47	4	$5d^8 6s 6p$ ( $^4P$ ) $^5D$	65333.25	4	$5d^9 5f$

**Table 2.** Odd energy levels of Pt I. The leading components of the eigenfunctions are derived from theoretical studies of the mixed group of configurations  $5d^96p + 5d^86s6p + 5d^76s^26p + 5d^97p$ . Where other configurations are indicated, the designations are empirical – Continued

Energy ( $\text{cm}^{-1}$ )	$J$	Leading component	Energy ( $\text{cm}^{-1}$ )	$J$	Leading component
65336.49	3	$5d^95f$	67303.64	3,4	$5d^86s7p$
65339.66	4	$5d^95f$	67413.65	5,4	$5d^86s7p$
65341.92	5	$5d^95f$	68266.90	5	$5d^86s7p$
65510.22	3		68343.55	3,4	$5d^86s7p$
65697.70	2,1		68606.62	2	
65850.11	1		68657.42	3	
65852.56	4		70087.93	7	$5d^8(^3F_4)6s5f$
66198.85	2		70088.64	5,6	$5d^8(^3F_4)6s5f$
66432.56	1		70095.52	6	$5d^8(^3F_4)6s5f$
66927.43	2	$5d^97p(^2D_{3/2}, ^2P_{1/2})$	70099.57	5	$5d^8(^3F_4)6s5f$
67121.58	3	$5d^97p(^2D_{3/2}, ^2P_{3/2})$			

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# Energy Levels of Singly-Ionized Platinum

Volume 97

Number 1

January–February 1992

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The analysis of Pt II is extended by using accurate wavelength measurements by Sansonetti et al. Forty-three new even and 104 new odd levels have been found. The Slater-Condon parametric method is used for the interpretation of the  $5d^9$ ,  $5d^86s$ , and  $5d^76s^2$  low even configurations and the  $5d^8(7s+6d)$  high even configurations with root mean square deviations smaller than  $80\text{ cm}^{-1}$ .

The importance of the  $5d^8-5d^76s$  core interaction in interpreting the even-parity levels is stressed.

**Key words:** atomic spectroscopy; electronic configurations; energy levels; platinum.

**Accepted:** November 21, 1991

## 1. Introduction

The spectrum of platinum emitted by a hollow cathode lamp has been recently observed and measured [1]. The improved wavelengths of the classified lines led Reader et al. [2] to determine accurate energies for the known levels. The extensive line list comprised many unclassified lines. Their interpretation has been undertaken at Laboratoire Aimé Cotton in order to improve the knowledge of excited levels at the end of the  $5d$ -period.

The strong unclassified lines have been interpreted in the present work with the support of theoretical energy level predictions and a computer program to search for recurring energy differences in the list of observed wave numbers. The measured wave numbers of classified lines deviate from the differences between their initial and final levels by less than  $0.050\text{ cm}^{-1}$  if the lines are not blended with other transitions. The energy levels are reported in Tables 2, 3, and 5, in which the 3-digit

values are taken from Ref. [2]. The  $J$ -values of some levels have been changed and the newly classified lines led to slight modifications of their energies. The uncertainty of the levels depends on the intensities and spectral regions of their transitions. It ranges from  $0.050$  to  $0.100\text{ cm}^{-1}$ . The classified lines are reported in Ref. [1].

## 2. Interpretation of the Low Even-Parity Configurations $5d^9$ , $5d^86s$ , and $5d^76s^2$

In 1977 [3], a systematic description of the even configurations  $(5d+6s)^N$  was performed in the framework of the Slater-Condon parametric method. It was shown that configuration mixing was very important within these groups and led to the revision and limited extension of some analyses. In the absence of definite configuration assignments for many levels, the sum of the squared amplitudes represented 53% of all  $5d^N$  levels from Lu II to Au II, 56% for  $5d^{N-1}6s$  and only 27% for

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$5d^{N-2}6s^2$ . In Pt II, all 21 levels found by Shenstone [4] were supported by the theoretical calculation, but six of his empirical  $LS$  designations did not correspond to the leading component of the eigenfunction. The  $5d^76s^2$ -configuration was limited to four known levels and the relevant energy parameters needed to be fixed or constrained. The present analysis was guided by the results of [3] and the number of levels of the  $(5d+6s)^9$  group has been brought from 21 to 33. The present interpretation of the three configurations  $5d^9$ ,  $5d^86s$  and  $5d^76s^2$  leads to improved parameter values, a number of constraints in the least-squares fitting process being now removed. The present set of parameters includes: a constant energy for all three configurations,  $A$ , the energy differences between configurations,  $S(d^9-d^7s^2)$  and  $S(d^8s-d^7s^2)$ , all Slater integrals describing the electrostatic interactions within the studied group, the effective electrostatic

parameters  $\alpha_0$  and  $\beta_0$  as defined in the formalism of orthogonal operators [5], and finally, the usual spin-orbit parameters. These 18 parameters have been reduced to 13 adjustable ones by means of constraints detailed in Table 1. These constraints were derived from earlier studies of  $(5d+6s)^N$  groups. The root mean square deviation is  $73 \text{ cm}^{-1}$ . The comparison of experimental and theoretical energies is given in Table 2. The theoretical data are limited to the theoretical energy  $E_{th}$ , the first component of the eigenfunction and the percentage of the components of the 3 configurations (squared amplitudes) in the eigenfunctions. The coefficients of the interaction parameter  $R^2(5d^2,5d6s)$  in intermediate coupling show that  $5d^86s \ ^2P_{1/2}$  and  $5d^76s^2 \ ^2P_{1/2}$  which are distant by  $33700 \text{ cm}^{-1}$  have a mutual repulsion of  $7000 \text{ cm}^{-1}$  and that four other levels of  $5d^86s$  are shifted to lower energies by more than  $2000 \text{ cm}^{-1}$ .

**Table 1.** Fitted energy parameters ( $\text{cm}^{-1}$ ) of the even configurations of Pt II. Standard deviations of the parameters are given in parentheses

Parameter	$5d^76s^2$	$5d^86s$	$5d^9$	$5d^86d$	$5d^87s$
$A$	58028 (65)			121854 (119)	112271 (66)
$S(5d^86s - 5d^76s^2)$		-30621 (94)			
$S(5d^9 - 5d^76s^2)$			-51804 (117)		
$F^2(5d,5d)$	52391 (219)	50566 (202)		46155 (235)	46155 <sup>g</sup>
$F^4(5d,5d)$	39365 (318)	38754 (35)		39579 (541)	39579 <sup>g</sup>
$F^2(5d,6d)$				3544 (369)	
$F^4(5d,6d)$				1252 (405)	
$G^0(5d,6d)$				767 (46)	
$G^2(5d,6d)$				1256 (227)	
$G^4(5d,6d)$				1256 <sup>e</sup>	
$G^2(5d,6s)$		15354 (180)			
$G^2(5d,7s)$					1879 (247)
$R^2(5d^2,6s^2)$		16889 <sup>b</sup>			
$R^2(5d^2,5d6s)$	-20905 (242)h	-20277 <sup>c</sup>			
$R^2(5d6d,5d7s)$				2568	(302)
$R^2(5d6d,7s5d)$				942	(657)
$\alpha_0$	15.1 <sup>a</sup>	15.1 (4.5)		115 (6.5)	115 <sup>g</sup>
$\beta_0$	-204 <sup>a</sup>	-204 (50)		-204 <sup>f</sup>	-204 <sup>f</sup>
$\zeta_{5d}$	4607.1 (19)	4349.5 (21)	4092.0 <sup>d</sup>	4378 (18)	4335 (27)
$\zeta_{6d}$				228 (17)	

<sup>a</sup> Parameters constrained to be equal in  $5d^76s^2$  and  $5d^86s$ .

<sup>b</sup> The parameter  $R^2(5d^2,6s^2)$  of the  $5d^76s^2-5d^9$  interaction is held in a constant ratio with the  $G^2(5d,6s)$  of  $5d^86s$ .

<sup>c</sup> Slater parameters  $R^{(2)}(5d^2,5d6s)$  for  $5d^86s-5d^9$  and  $5d^86s-5d^76s^2$  interactions are held in a constant ratio.

<sup>d</sup>  $\zeta(5d^76s^2) + \zeta(5d^9) = 2\zeta(5d^86s)$ .

<sup>e</sup>  $G^2(5d,6d) = G^4(5d,6d)$ .

<sup>f</sup> Held fixed to the fitted value of the lowest configurations.

<sup>g</sup> Held equal to the same parameter in  $5d^86d$ .

<sup>h</sup> Parameter for the  $5d^76s^2-5d^86s$  interaction.

**Table 2.** Low even energy levels of Pt II. The theoretical energies  $E_{th}$  are those of the mixed configurations  $5d^9, 5d^8 6s$  and  $5d^7 6s^2$  (designated A, B, and C in the first components of the eigenfunction)

$E_{exp}$ ( $cm^{-1}$ )	$J$	$E_{th}$ ( $cm^{-1}$ )	First comp. %	$5d^9$ %	$5d^8 6s$ %	$5d^7 6s^2$ %
0	5/2	16	A <sup>2</sup> D 90.7	90.7	7.6	1.7
4786.611	9/2	4862	B <sup>4</sup> F 96.6	0	100.	0
8419.822	3/2	8475	A <sup>2</sup> D 62.9	62.9	34.5	2.6
9356.274	7/2	9234	B <sup>4</sup> F 67.5	0	99.6	0.4
13329.227	5/2	13345	B <sup>4</sup> P 36.2	5.5	94.1	0.4
15791.276	3/2	15639	A <sup>2</sup> D 32.3	32.3	65.1	2.6
16820.894	5/2	16770	B <sup>4</sup> F 60.0	0.4	99.3	0.3
18097.715	7/2	18171	B <sup>2</sup> F 63.8	0	98.8	1.2
21168.684	3/2	21146	B <sup>4</sup> F 39.5	0.1	94.1	5.8
21717.260	1/2	21774	B <sup>4</sup> P 87.4	0	99.8	0.2
23461.503	5/2	23542	B <sup>2</sup> F 48.3	1.2	95.8	3.0
23875.553	3/2	23886	B <sup>4</sup> P 56.3	0.3	87.4	12.3
24879.480	9/2	24846	C <sup>4</sup> F 67.7	0	13.6	86.4
27255.687	1/2	27207	B <sup>2</sup> P 77.8	0	84.7	15.3
29030.479	7/2	28968	B <sup>2</sup> G 88.0	0	94.5	5.5
29261.967	9/2	29341	B <sup>2</sup> G 78.6	0	81.3	18.7
32237.007	3/2	32182	B <sup>2</sup> D 53.3	3.4	85.6	11.0
32918.561	5/2	32981	B <sup>2</sup> D 36.2	1.4	87.3	11.3
34647.221	7/2	34624	C <sup>4</sup> F 95.2	0	1.5	98.5
36484.028	5/2	36555	C <sup>4</sup> F 55.6	0.1	9.4	90.5
37877.792	3/2	37895	C <sup>4</sup> F 43.7	0.1	12.9	87.0
N 41434.11	5/2	41433	C <sup>4</sup> P 76.1	0.1	0	99.9
N 42031.85	3/2	41986	C <sup>4</sup> P 50.1	0	11.9	88.1
N 43737.40	9/2	43774	C <sup>2</sup> G 52.7	0	4.5	95.5
N 46046.43	1/2	46086	C <sup>4</sup> P 76.6	0	9.0	91.0
N 48591.04	11/2	48524	C <sup>2</sup> H 100.	0	0	100.
N 50564.60	7/2	50607	C <sup>2</sup> G 79.8	0	4.2	95.8
	1/2	53204	B <sup>2</sup> S 76.6	0	86.6	13.4
N 53749.63	3/2	53722	C <sup>4</sup> P 50.1	0	3.8	96.2
N 54373.47	5/2	54333	C <sup>3</sup> D 53.5	0.1	2.5	97.4
N 58062.04	5/2	58072	C <sup>2</sup> F 81.7	0.1	3.9	96.1
N 58491.21	9/2	58518	C <sup>2</sup> H 68.1	0	0.6	99.4
N 60986.75	1/2	60939	C <sup>2</sup> P 65.8	0	20.0	80.0
N 64003.90	7/2	64001	C <sup>2</sup> F 83.7	0	1.3	98.7
	3/2	65221	C <sup>3</sup> D 50.8	0.2	4.3	95.5
	3/2	77750	C <sup>3</sup> D 88.5	0.9	0.4	98.7
	5/2	79860	C <sup>3</sup> D 67.0	0.5	0.1	99.4

Note: N—new energy level.

### 3. The Predicted Low Configurations of Pt III

The spectrum of Pt III is still unknown but, for application to Pt II, its low energy levels can be predicted by means of the Slater-Condon method. By comparing the lowest energy levels of  $5d^N$ ,  $5d^{N-1}6s$  and  $5d^{N-2}6s^2$  in Hf III ( $N=2$ ) [6], W III ( $N=4$ ) [7], Au III ( $N=9$ ) [8] and Hg III ( $N=10$ ) [9], one can reasonably assume that the excitation energies of  $5d^7 6s^2$  <sup>5</sup>F<sub>5</sub> and  $5d^6 6s^2$  <sup>5</sup>F<sub>5</sub> and  $5d^6 6s^2$  <sup>5</sup>D<sub>4</sub> levels above the ground level  $5d^8$  <sup>3</sup>F<sub>4</sub> are about 20000 and 60000  $cm^{-1}$ , respectively. All other parameters needed for describing  $(5d+6s)^8$  in Pt III may be obtained

[3] and in third spectra. The results of this preliminary study are summarized below.

For all  $J$ -values, the configuration  $5d^8$  does not overlap the energy range of the  $5d^7 6s$  and  $5d^6 6s^2$  configurations, but this does not prevent configuration mixing. The effect of  $5d^6 6s^2$  is a constant shift of about  $-800 cm^{-1}$  for all levels of  $5d^8$  except <sup>3</sup>P<sub>0</sub> and <sup>1</sup>S<sub>0</sub>, both shifted by  $-1400 cm^{-1}$ . The effect of the  $5d^7 6s-5d^8$  mixing is more selective and is reported in the last column of Table 3. These shifts mean that the  $5d^8$  parameters would certainly differ if fitted in the approximation of *isolated* configurations or in mixed groups  $(5d+6s)^N$ . The  $LS$  names are well defined except for the  $J=2$  levels, for which <sup>3</sup>P<sub>2</sub> is nowhere the leading component of

**Table 3.** Energy levels of Pt III  $5d^8$  predicted in the parametric study of  $(5d + 6s)^8$ 

$J$	Energy $\text{cm}^{-1}$	$5d^8$ purity %	First comp. %	Second comp. %	Third comp. %	Shift ( $\text{cm}^{-1}$ ) $d^7s - d^8$
4	0	98.8	$^3F$ 94.7	$^1G$ 4.0		– 800
2	5547	94.4	$^1D$ 41.1	$^3P$ 37.7	$^3F$ 16.3	– 3350
3	9859	98.4	$^3F$ 98.4	$(^2F)^3F$ 1.1		– 1000
2	14249	93.2	$^3F$ 47.6	$^3P$ 40.6	$^1D$ 5.1	– 3050
0	15127	93.4	$^3P$ 81.5	$^1S$ 11.9	$(^2P)^3P$ 5.5	– 3800
1	16700	89.7	$^3P$ 89.7	$(^2P)^3P$ 8.4		– 4950
4	21675	89.8	$^1G$ 86.0	$(^2G)^1G$ 5.8	$^3F$ 3.9	– 2850
2	24760	92.5	$^1D$ 48.0	$^3F$ 33.9	$^3P$ 10.7	– 3200
0	46301	60.3	$^1S$ 58.3	$(^2P)^3P$ 28.0	$(^4P)^3P$ 10.6	– 1350

the eigenfunction. Since the second and third  $J=2$  levels have respectively dominant  $^3F_2$  and  $^1D_2$  characters, the lowest  $J=2$  level has been given the designation  $^3P_2$  for identification purposes in the next step of the work.

#### 4. Interpretation of the Upper Even Configurations

Nine high even levels were identified by Shenstone [4] as  $5d^87s$  and  $5d^86d$ . One of these levels has now been rejected and the  $J$ -values of two revised. The three levels of  $5d^88s$  and  $5d^87d$  have not been confirmed. Thirty-two levels have been found between 101500 and 121700  $\text{cm}^{-1}$ . The intensity of their transitions and some relatively large deviations  $E_{\text{exp}} - E_{\text{th}}$  in the separate studies of these configurations led us to evaluate their mixing. The 21 integrals needed to describe the levels of  $5d^87s + 5d^86d$  were reduced to 15 adjustable parameters by means of constraints given in Table 1. The mixing of the lowest  $J=1/2$  levels leads to a well-defined value for the interaction parameter  $R^2(5d7s, 5d6d)$  and the final rms deviation is 79  $\text{cm}^{-1}$ . As shown in Table 1, the values of the parameters  $F^2(5d, 5d)$  and  $\alpha$  for  $5d^8(6d + 7s)$  differ significantly from those for  $5d^76s^2$  and  $5d^86s$ ; however, the parameters are well-defined in the least-squares fit. We consider this to be an effect of truncation problems discussed in Sec. 3. It seems likely that these inconsistencies would be corrected if all six configurations  $(5d + 6s)^87s + (5d + 6s)^86d$  were studied together. This extended parametric study has not been undertaken because  $5d^66s^27s$ ,  $5d^66s^26d$  and  $5d^76s6d$  are totally unknown and only two levels of  $5d^76s7s$  are located so far. The predictions of our restricted study might well be unreliable and the theoretical energies of unknown levels have therefore not been reported here.

#### 5. Odd Levels of Pt II

The lowest odd levels were attributed to  $5d^86p$  by Shenstone [4]. This configuration is also known in other ions of the isoelectronic sequence through Bi VII [9–11]. The approximation of an *isolated*  $5d^86p$  configuration, if valid, has been used for the theoretical study of Au III–Bi VII spectra. It does not hold for Pt II. In second spectra, the overlap of  $5d^N6p$ ,  $5d^{N-1}6s6p$  and  $5d^{N-2}6s^26p$  requires a multi-configurational treatment. In Hf II, Ta II, W II, Au II and Hg II [12], these low odd configurations had been interpreted with rms deviations smaller than 200  $\text{cm}^{-1}$ . For unclear reasons, the rms deviation for Pt II is larger than 500  $\text{cm}^{-1}$  and the designations reported in Table 4 are carefully limited to the lowest levels. Some of them might well be revised with further advances in the parametric interpretation. The  $5d^76s6p$  configuration starts with the 62820 level, for which we explain the absence of decay to  $5d^76s^2\ ^4F_{9/2}$  by the selection rule on the strongly forbidden transition  $6s6p\ ^3P_0 - 6s^2\ ^1S_0$ . Most of the levels without designation belong to  $5d^76s6p$  with some admixture of  $5d^66s^26p$  for the highest energies.

#### 6. Conclusion

The strongest unclassified lines of Pt II have been interpreted by extending the early analysis of Shenstone with the help of accurate wavelength measurements and parametric calculations of the main configurations. The number of levels has been brought from 29 to 72 in the even parity and from 71 to 174 in the odd parity. The theoretical study stresses the importance of the  $5d^8 - 5d^76s$  interaction and, although somewhat preliminary, the parametric interpretation of the low odd levels indicates that all levels with  $J=3/2$  through  $11/2$  below 79000  $\text{cm}^{-1}$  have been found.

**Table 4.** Upper even levels of Pt II. The theoretical energies  $E_{th}$  are from the parametric study of  $5d^86d + 5d^87s$ . The core term of  $5d^8$  is indicated in parenthesis for  $5d^86d$  only

$E_{exp}$ ( $cm^{-1}$ )	$J$	$E_{th}$ ( $cm^{-1}$ )	Designation	$5d^87s$ %	$5d^86d$ %	Leading $LS$ comp. %
95803.363	9/2	95837	( <sup>3</sup> F <sub>4</sub> )7s <sub>1/2</sub>	99.8	0.2	7s <sup>4</sup> F 95
96614.352	7/2	96630	( <sup>3</sup> F <sub>4</sub> )7s <sub>1/2</sub>	99.9	0.1	7s <sup>2</sup> F 66
101199.085	5/2	101199	( <sup>3</sup> P <sub>2</sub> )7s <sub>1/2</sub>	97.6	2.4	7s <sup>2</sup> D 43
N 101517.59	3/2	101500	( <sup>3</sup> P <sub>2</sub> )7s <sub>1/2</sub>	99.5	0.5	7s <sup>2</sup> D 46
N 104090.70	7/2	104210	( <sup>3</sup> F <sub>4</sub> )6d <sub>3/2</sub>	0.9	99.1	6d ( <sup>3</sup> F) <sup>4</sup> D 62
N 104410.05	11/2	104405	( <sup>3</sup> F <sub>4</sub> )6d <sub>3/2</sub>	0	100.	6d ( <sup>3</sup> F) <sup>2</sup> H 46
J 104636.905	9/2	104612	( <sup>3</sup> F <sub>4</sub> )6d <sub>3/2</sub>	0.1	99.9	6d ( <sup>3</sup> F) <sup>4</sup> F 36
104763.45	13/2	104698	( <sup>3</sup> F <sub>4</sub> )6d <sub>5/2</sub>	0	100.	6d ( <sup>3</sup> F) <sup>4</sup> H 95
N 104930.26	3/2	105955	( <sup>3</sup> F <sub>4</sub> )6d <sub>5/2</sub>	0.7	99.3	6d ( <sup>3</sup> F) <sup>2</sup> P 58
105066.347	11/2	105029	( <sup>3</sup> F <sub>4</sub> )6d <sub>5/2</sub>	0	100.	6d ( <sup>3</sup> F) <sup>4</sup> G 72
N 105086.83	7/2	105046	( <sup>3</sup> F <sub>4</sub> )6d <sub>5/2</sub>	0.1	99.9	6d ( <sup>3</sup> F) <sup>2</sup> F 61
105388.130	9/2	105413	( <sup>3</sup> F <sub>4</sub> )6d <sub>5/2</sub>	0	100.	6d ( <sup>3</sup> F) <sup>2</sup> G 48
N 105794.53	7/2	105739	( <sup>3</sup> F <sub>3</sub> )7s <sub>1/2</sub>	98.9	1.1	7s <sup>4</sup> F 69
N 105962.52	5/2	105880	( <sup>3</sup> F <sub>3</sub> )7s <sub>1/2</sub>	99.0	1.0	7s <sup>4</sup> F 59
J 106434.92	5/2	106430	( <sup>3</sup> F <sub>4</sub> )6d <sub>5/2</sub>	1.1	98.9	6d ( <sup>3</sup> F) <sup>2</sup> D 39
N 109346.33	3/2	109412	( <sup>3</sup> P <sub>2</sub> )6d <sub>3/2</sub>	3.5	96.5	6d ( <sup>1</sup> D) <sup>2</sup> D 37
N 109507.99	1/2	109472	( <sup>3</sup> P <sub>2</sub> )6d <sub>3/2</sub>	43.8	56.2	7s <sup>4</sup> F 32
N 109527.87	5/2	109446	( <sup>3</sup> P <sub>2</sub> )6d <sub>3/2</sub>	3.3	96.7	6d ( <sup>1</sup> D) <sup>2</sup> F 37
N 109676.18	7/2	109676	( <sup>3</sup> P <sub>2</sub> )6d <sub>3/2</sub>	0.2	99.8	6d ( <sup>1</sup> D) <sup>2</sup> G 24
N 110020.85	1/2	110077	( <sup>3</sup> P <sub>2</sub> )6d <sub>5/2</sub>	10.7	89.3	6d ( <sup>1</sup> D) <sup>2</sup> P 40
N 110146.80	7/2	110061	( <sup>3</sup> P <sub>2</sub> )6d <sub>5/2</sub>	0	100.	6d ( <sup>1</sup> D) <sup>2</sup> F 23
N 110158.16	5/2	110261	( <sup>3</sup> F <sub>2</sub> )7s <sub>1/2</sub>	94.6	5.6	7s <sup>4</sup> P 44
N 110257.49	9/2	110313	( <sup>3</sup> P <sub>2</sub> )6d <sub>5/2</sub>	0.1	99.9	6d ( <sup>1</sup> D) <sup>2</sup> G 45
N 110258.18	3/2	110356	( <sup>3</sup> F <sub>2</sub> )7s <sub>1/2</sub>	93.9	6.1	7s <sup>4</sup> F 42
N 110408.02	3/2	110530	( <sup>3</sup> F <sub>2</sub> )6d <sub>5/2</sub>	2.1	97.9	6d ( <sup>1</sup> D) <sup>2</sup> P 39
N 111162.69	5/2	111075	( <sup>3</sup> P <sub>2</sub> )6d <sub>5/2</sub>	1.6	98.4	6d ( <sup>1</sup> D) <sup>2</sup> D 32
N 111371.71	1/2	111309	( <sup>3</sup> P <sub>0</sub> )7s <sub>1/2</sub>	45.6	54.4	7s <sup>4</sup> P 33
N 112433.31	3/2	112371	( <sup>3</sup> P <sub>1</sub> )7s <sub>1/2</sub>	90.9	9.1	7s <sup>4</sup> P 65
N 113119.61	1/2	113112	( <sup>3</sup> P <sub>1</sub> )7s <sub>1/2</sub>	93.1	6.9	7s <sup>2</sup> P 76
N 114127.60	9/2	114088	( <sup>3</sup> F <sub>3</sub> )6d <sub>3/2</sub>	0.1	99.9	6d ( <sup>3</sup> F) <sup>4</sup> H 58
N 114256.30	7/2	114179	( <sup>3</sup> F <sub>3</sub> )6d <sub>3/2</sub>	0	100.	6d ( <sup>3</sup> F) <sup>4</sup> G 48
N 114455.05	5/2	114530	( <sup>3</sup> F <sub>3</sub> )6d <sub>3/2</sub>	0.3	99.7	6d ( <sup>3</sup> F) <sup>4</sup> D 40
N 114539.25	11/2	114549	( <sup>3</sup> F <sub>3</sub> )6d <sub>5/2</sub>	0	100.	6d ( <sup>3</sup> F) <sup>4</sup> H 63
N 114861.32	9/2	114823	( <sup>3</sup> F <sub>3</sub> )6d <sub>5/2</sub>	0.1	99.9	6d ( <sup>3</sup> F) <sup>4</sup> G 54
N 115060.84	5/2	115144	( <sup>3</sup> F <sub>3</sub> )6d <sub>5/2</sub>	0.2	99.8	6d ( <sup>3</sup> F) <sup>2</sup> D 31
N 116689.04	9/2		5d <sup>7</sup> 6s 7s			
N 117340.84	9/2	117404	( <sup>1</sup> G <sub>4</sub> )7s <sub>1/2</sub>	98.7	1.3	7s <sup>2</sup> G 94
N 117493.46	7/2	117437	( <sup>1</sup> G <sub>4</sub> )7s <sub>1/2</sub>	96.6	3.4	7s <sup>2</sup> G 92
N 119057.05	5/2	*				
N 121651.19	9/2		5d <sup>7</sup> 6s 7s			

\* Undetermined identification; theoretical  $J = 5/2$  levels are calculated at 119011 and 119177  $cm^{-1}$ .

Notes: N—new energy level.

J—revised  $J$ -value.

Table 5. Odd energy levels of Pt II

$E$ (cm <sup>-1</sup> )	$J$	Configuration	Designation	$E$ (cm <sup>-1</sup> )	$J$	Configuration	Designation
51408.370	7/2	$5d^8 6p$	( <sup>3</sup> F <sub>4</sub> ) $6p_{1/2}$	N 83538.53	11/2	$5d^7 6s 6p$	
53875.493	9/2	$5d^8 6p$	( <sup>3</sup> F <sub>4</sub> ) $6p_{1/2}$	84182.633	9/2		
56587.934	3/2	$5d^8 6p$	( <sup>3</sup> P <sub>2</sub> ) $6p_{1/2}$	E,J 85700.27	9/2	$5d^7 6s 6p$	
57018.130	5/2	$5d^8 6p$	( <sup>3</sup> P <sub>2</sub> ) $6p_{1/2}$	N 85775.64	11/2		
60907.688	9/2	$5d^8 6p$	( <sup>3</sup> F <sub>4</sub> ) $6p_{3/2}$	N 85826.57	7/2		
61058.490	11/2	$5d^8 6p$	( <sup>3</sup> F <sub>4</sub> ) $6p_{3/2}$	N 86489.76	5/2		
61190.026	5/2	$5d^8 6p$	( <sup>3</sup> F <sub>4</sub> ) $6p_{3/2}^a$	N 87204.35	3/2		
61665.485	7/2	$5d^8 6p$	( <sup>3</sup> F <sub>4</sub> ) $6p_{3/2}$	N 88110.30	3/2,(5/2)		
62781.658	1/2	$5d^8 6p$	( <sup>3</sup> P <sub>2</sub> ) $6p_{3/2}$	N 88173.46	7/2		
62820.489	9/2	$5d^7 6s 6p$	( <sup>4</sup> F <sub>9/2</sub> , <sup>3</sup> P <sub>0</sub> )	N 88589.53	7/2		
63738.841	7/2	$5d^8 6p$	( <sup>3</sup> F <sub>3</sub> ) $6p_{1/2}$	N 89095.05	3/2		
64388.642	3/2	$5d^8 6p$	( <sup>3</sup> F <sub>2</sub> ) $6p_{1/2}$	N 89607.936	5/2		
64757.343	5/2	$5d^8 6p$	( <sup>3</sup> F <sub>3</sub> ) $6p_{1/2}^a$	E 89863.27	9/2		
N 65046.23	11/2	$5d^7 6s 6p$	( <sup>4</sup> F <sub>9/2</sub> , <sup>3</sup> P <sub>1</sub> )	N 90173.25	7/2,9/2		
65351.069	5/2	$5d^8 6p$	( <sup>3</sup> P <sub>2</sub> ) $6p_{3/2}$	N 90746.64	5/2		
65587.115	1/2	$5d^8 6p$	( <sup>3</sup> P <sub>0</sub> ) $6p_{1/2}$	N 91016.64	1/2,3/2		
66028.014	3/2	$5d^8 6p$	( <sup>3</sup> P <sub>2</sub> ) $6p_{3/2}$	N 91271.16	5/2		
66434.315	7/2	$5d^8 6p$	( <sup>3</sup> P <sub>2</sub> ) $6p_{3/2}$	N 91669.95	7/2		
N 67780.44	7/2	$5d^7 6s 6p$	( <sup>4</sup> F <sub>9/2</sub> , <sup>3</sup> P <sub>1</sub> )	N 92526.90	11/2	$5d^7 6s 6p$	
J 69235.665	3/2	$5d^8 6p$	( <sup>3</sup> P <sub>1</sub> ) $6p_{1/2}$	N 92537.08	9/2		
69953.317	5/2	$5d^8 6p$	( <sup>3</sup> F <sub>3</sub> ) $6p_{3/2}$	N 92749.02	3/2		
70181.281	9/2	$5d^7 6s 6p$	( <sup>4</sup> F <sub>9/2</sub> , <sup>3</sup> P <sub>1</sub> )	N 92767.97	3/2		
70379.023	5/2	$5d^8 6p$	( <sup>3</sup> P <sub>1</sub> ) $6p_{3/2}$	N 93197.46	5/2		
N 71021.13	9/2	$5d^8 6p$	( <sup>3</sup> F <sub>3</sub> ) $6p_{3/2}$	N 93322.18	11/2	$5d^7 6s 6p$	
J 71314.594	7/2	$5d^8 6p$	( <sup>3</sup> F <sub>3</sub> ) $6p_{3/2}$	93336.287	7/2		
N 71364.68	3/2	$5d^8 6p$	( <sup>3</sup> F <sub>3</sub> ) $6p_{3/2}$	93482.013	7/2		
71948.916	5/2	$5d^7 6s 6p$		E 94022.39	9/2		
73026.380	3/2	$5d^8 6p$	( <sup>3</sup> F <sub>2</sub> ) $6p_{3/2}$	N 94271.53	5/2		
73431.346	9/2	$5d^8 6p$	( <sup>1</sup> G <sub>4</sub> ) $6p_{1/2}$	N 94633.25	5/2		
73761.739	7/2			N 94829.73	1/2,3/2		
E,J 73999.85	5/2			N 94842.49	5/2		
74241.479	3/2	$5d^8 6p$		N 95226.00	9/2		
N 74409.47	11/2	$5d^7 6s 6p$	( <sup>4</sup> F <sub>9/2</sub> , <sup>3</sup> P <sub>2</sub> )	N 95557.71	3/2		
74619.107	5/2			N 95617.03	7/2		
74745.916	7/2			E 95754.07	5/2		
74754.823	1/2	$5d^8 6p$	( <sup>3</sup> F <sub>2</sub> ) $6p_{3/2}$	N 96109.73	11/2		
75184.880	7/2	$5d^8 6p$	( <sup>1</sup> G <sub>4</sub> ) $6p_{1/2}$	N 96131.24	9/2		
N 75365.84	5/2			N 96403.32	5/2		
75581.422	3/2			N 96443.92	1/2		
76461.526	5/2			N 97183.40	3/2		
76610.046	3/2			97630.600	7/2		
77519.724	9/2			N 97786.55	3/2		
N 77538.25	3/2			N 97792.75	5/2		
N 77763.58	1/2			J 98186.971	7/2		
E,J 78043.02	7/2			98817.744	7/2		
N 78254.80	5/2			N 99068.74	3/2		
N 78452.50	3/2			99209.011	5/2		
78906.492	9/2	$5d^7 6s 6p$	( <sup>4</sup> F <sub>9/2</sub> , <sup>3</sup> P <sub>2</sub> )	N 99471.02	1/2		
N 79092.09	3/2			99797.778	5/2		
79607.460	5/2			N 100232.63	9/2		
N 79683.41	1/2			100239.421	5/2		
N 80197.33	7/2	$5d^8 6p$	( <sup>1</sup> G <sub>4</sub> ) $6p_{3/2}$	100611.695	3/2		
80858.488	5/2			100795.666	3/2		
N 81083.95	9/2	$5d^8 6p$	( <sup>1</sup> G <sub>4</sub> ) $6p_{3/2}$	100903.454	7/2		
E 81897.71	7/2			N 101113.06	1/2		
E,J 82535.79	5/2			101341.867	7/2		
N 82692.28	9/2	$5d^7 6s 6p$		N 101394.01	1/2		
E 82824.00	3/2			101397.850	5/2		
E,J 82972.72	3/2			J 101549.10	9/2		
83352.251	7/2			101618.459	11/2		



Table 5. Odd energy levels of Pt II—Continued

$E$ (cm <sup>-1</sup> )	$J$	Configuration	Designation	$E$ (cm <sup>-1</sup> )	$J$	Configuration	Designation
101916.930	5/2			N 107386.26	9/2		
102086.034	9/2			N 107588.13	3/2		
102414.857	5/2			N 108037.26	7/2		
N 102520.80	7/2			N 108038.05	3/2		
N 102613.05	11/2			N 108155.51	3/2		
N 102678.30	3/2			N 108322.40	7/2		
N 102872.20	7/2			N 108639.24	5/2		
N 103060.55	9/2			N 108672.51	1/2,3/2		
N 103421.16	3/2			N 108727.50	7/2		
103463.310	5/2			N 108802.20	7/2,9/2		
103517.132	7/2			N 109307.89	7/2		
N 103637.26	1/2,3/2			N 109528.23	3/2,5/2		
N 104092.10	3/2,5/2			N 109733.10	7/2		
N 104158.64	5/2			N 109753.67	5/2		
N 104548.13	3/2			N 110066.71	9/2		
N 104625.27	9/2			N 110085.70	3/2		
N 104831.58	9/2			N 110196.40	5/2		
N 105018.17	3/2			N 110202.39	7/2		
N 105042.36	5/2			N 110609.08	9/2		
N 105554.33	7/2			N 110638.00	5/2		
N 105597.33	5/2			N 110684.45	3/2		
N 105726.12	1/2			N 110762.77	7/2,9/2		
N 105896.50	3/2			N 111320.57	5/2		
N 106229.90	7/2			N 111354.67	7/2		
N 106852.84	3/2			N 111716.41	7/2,9/2		
N 106995.20	9/2			N 112247.69	9/2		
N 106996.55	7/2			N 113785.71	3/2,(1/2)		
N 107191.45	3/2,5/2			N 114880.48	5/2		

<sup>a</sup> These  $J$ - $j$  characters are equally shared by the levels 61190 and 64757.

Notes: N—new energy level.

J—revised  $J$ -value.

E—revised energy value.

## Acknowledgments

We are grateful to Dr. J. Reader and his coworkers for sending us several line lists of platinum as soon as they were completed. The theoretical calculations have been performed by means of the chain of programs written and maintained at Laboratoire Aimé Cotton by A. Bachelier and J. Sinzelle.

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# News Briefs

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## General Developments

*Inquiries about News Briefs, where no contact person is identified, should be referred to the Managing Editor, Journal of Research, National Institute of Standards and Technology, Administration Building, A635, Gaithersburg, MD 20899; telephone: 301/975-3572.*

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### **NIST DEVELOPS TEST CHIP FOR MEASUREMENTS OF MMIC PACKAGES AND INTERCONNECTS**

NIST scientists have invented a method for measuring the effect of a monolithic microwave/millimeter-wave integrated-circuit (MMIC) package or interconnect on microwave signals passing through it. This information is needed by MMIC designers to separate the effects of the package or interconnect from measurements intended to characterize a MMIC chip. The test vehicle is itself a microchip carrying a coplanar transmission line with a beam-lead diode that can be biased at different levels. To make measurements of packages or interconnects, this test chip replaces a MMIC chip. For example, to characterize a package designed to house and protect a single MMIC chip, the test chip would be mounted in a specimen of the package and connections made to it in, as nearly as possible, the same way that connections would be made to the MMIC chip. The bias for the diode would be applied directly through the radiofrequency connections of the package. Scattering parameter measurements would then be made at the coaxial connections of the package. The package effects then could be determined from the results of these measurements and a prior characterization of the diode.

The term interconnect as used here refers to a structure that transduces a microwave signal from one transmission medium to another. Examples

include coaxial to coplanar waveguide, coaxial to microstrip, and microstrip to coplanar waveguide.

### **FIIA SYSTEM FIELD-TESTED FOR THEOPHYLLINE IN SERUM AT NIST**

A new concept for the measurement of a wide variety of clinical analytes in blood serum, flow injection immunoassay (FIIA), has been recently developed by researchers at NIST. FIIA promises to improve measurements in three ways: by allowing the reuse of expensive antibody reagents, by increasing the assay sensitivities, and by providing the opportunity for automation. The FIIA system was successfully tested for the determination of serum theophylline, a drug which is administered for the treatment of asthma. The performance of the theophylline FIIA for a large number of samples was compared to a fluorescence-polarization immunoassay and to liquid chromatographic determination. There was excellent agreement among the three techniques.

The primary component of the FIIA system is a regenerable reactor column that has the antibody reagent bound to a bed of silica particles. This immobilization provides a site in the flowing system for the specific reaction with the antigen and stabilizes the expensive antibody component for hundreds of measurement cycles. Detection of the immunochemical interaction between the analyte and antibody is achieved by use of theophylline-tagged liposomes, submicroscopic particles capable of encapsulating thousands of fluorescent markers which can be released for detection in the flow system. This provides a very sensitive test that requires much smaller blood volumes than currently used assays, a definite advantage for monitoring therapy in small children. All steps in the assay sequence are automated using a flow injection system under computer control.

**NON-METHANE ORGANIC COMPOUND (NMOC) GAS STANDARDS DEVELOPED TO SUPPORT ATMOSPHERIC MEASUREMENTS OF AUTO EMISSIONS**

Scientists at NIST have developed a series of gas mixtures consisting of trace level concentrations of 15 different organic compounds in nitrogen. The compounds are constituents of automobile exhaust and have been identified as reactants in the formation of ozone. The standards are difficult to produce since some of the reference compounds are gases, while others are liquids under normal conditions. Because of the low concentration levels, approximately 5 parts per billion (ppb), special procedures had to be developed to accurately produce the mixtures and preconcentrate the organic constituents to allow detection for analysis.

These standards are required to better understand and follow the complex atmospheric chemistry of ozone formation. Ozone at high altitudes is essential to regulating the Earth's atmosphere. However, ozone at ground level is a pollutant that adversely affects human health and is a major contributor to plant and crop damage. Ground-level ozone is formed by complex interactions involving hydrocarbons, oxygen, and sunlight, and is one of the constituents of photochemical smog. Current concern with high pollution levels has caused environmental agencies to embark on studies to determine sources and levels of pollutants so that they might recommend remediation steps and then measure whether these steps are effective. The standards developed at NIST contain the hydrocarbon compounds involved in the reactions to form ozone and will be used to calibrate instruments for accurately measuring these components in the atmosphere.

**TWO NEW NIST PRECISION MEASUREMENT GRANTS AWARDED FOR FY 92**

Two new \$30,000 NIST precision measurement grants have been awarded for fiscal year 1992. The recipients, Daniel J. Heinzen of the University of Texas at Austin and Carol E. Tanner of the University of Notre Dame, were selected from an initial group of 42 candidates. NIST Sponsors these grants to promote fundamental research in measurement science in U.S. universities and to foster contacts between NIST scientists and researchers in the academic community actively engaged in such work.

Heinzen's project, "Quantum-Limited Cooling and Detection with Stored Ions," involves new ion

trapping and cooling experiments with the aim of extending recently developed quantum-limited cooling and detection techniques to a wider variety of ions and to protons and electrons. The ultimate goal is to increase the accuracy of mass ratio and electron and positron  $g$ -factor measurements to unprecedented parts in  $10^{11}$ - $10^{12}$  range.

Tanner's project, "Absolute Calibration of Atomic Parity Nonconservation Measurements," will focus on measuring the transition probability or strength of a particular transition in the cesium atom with an accuracy never before achieved. This will allow the detailed interpretation of new atomic parity non-conservation experiments in cesium, experiments that, because of their high accuracy and low-interaction energy, will probe the standard model of the weak interaction or force at a level that can test it critically and search for new physical effects.

**SILICON PHOTODIODES OPERATE OVER 14 DECADES OF DYNAMIC RANGE**

The improvements in commercial silicon photodiodes and operational amplifiers over the past several years permit optical power measurements over a wider dynamic range. In a recently published study, scientists at NIST analyzed in detail the origin of noise and drift in certain photodetector circuits and showed that, with the careful selection of components, a simple detector can operate over a dynamic range of 14 orders of magnitude. With a measurement time of 400 s, the electrical noise can be reduced to an equivalent photocurrent of 0.1 fA (fewer than 800 photons/s). At the other extreme, the same sensor without attenuation can measure mW of power.

This wide range of operation is important because the primary NIST radiometric standards have a much narrower range of operation and there is an operational need to transfer primary calibrations to other instruments with different sensitivities. The 14-decade detectors are well suited for this purpose. For example, laser-based facilities may be compared to lamp- and monochromator-based facilities. In one project, the 14-decade detectors facilitated the calibration of night-vision equipment against NIST incandescent lamp standards.

There are a large number of other applications where such a silicon photodiode circuit could replace large and expensive photomultiplier tubes, or inspire new, better, or less expensive products. There is an increasing demand for sensitive radiant

power measurements in such diverse fields as chemiluminescence and bioluminescence, materials science (optical density and surface scatter), and optical communication.

#### **X-RAY DIFFRACTION IMAGING OF ARTIFICIAL DIAMOND SINGLE CRYSTALS**

Diamond single crystals possess many remarkable properties, such as the highest thermal conductivity and the highest hardness of any material. These properties make diamonds an attractive material for high technology applications such as laser and x-ray windows and high temperature electronic devices. Natural diamonds are recognizable individuals, each with its own set of defects. Since electronic properties are influenced by crystalline perfection, the properties of one crystal are not necessarily the same as those of another crystal. Therefore, the intrinsic properties of diamonds are difficult to determine by analysis of natural crystals.

The high temperature/high pressure process for growing single crystal diamond that was invented by a well known U.S. industrial firm in 1970 has improved to the point where single crystals can be grown that exceed the quality of naturally occurring crystals. These crystals may provide the best opportunity to establish the intrinsic properties of diamonds. In collaboration with this firm, scientists at NIST have been investigating the quality of artificial diamonds by x-ray diffraction imaging, and in particular the influence of isotopic concentration on crystal quality. Using the MSEL beamline at the National Synchrotron Light Source at Brookhaven National Laboratories, NIST scientists examined several natural type IIa (lowest nitrogen concentration) diamonds and several artificial type IIa and IIb (boron doped) diamonds with varying carbon-<sup>12</sup> and carbon-<sup>13</sup> isotope concentration. The results indicate that diamonds grown from pure <sup>12</sup>C stock can have a higher degree of crystallographic perfection than comparable crystals with isotopic concentrations identified to natural crystals.

#### **SENSORS IDENTIFIED FOR POLYMER COMPOSITE PROCESSING**

The driving force for process control sensors is the need for the U.S. polymer composites industry to improve the efficiency and reliability of fabrication to increase competitiveness. The most promising on-line sensor techniques are ultrasonic, dielectric, spectroscopic, and optical. NIST researchers identified and analyzed these process control methods

in a report, Assessment of the State-of-the-Art for Monitoring Sensors for Polymer Composites (NISTIR 4514). Each sensor technique was evaluated for measurement speed, sampling geometry, sensitivity to different resins, effects of fiber type, interpretation of the data, and sensitivity to the manufacturing environment. The future for process control is very bright, but the major short-term needs are to build more rugged and reliable equipment that can withstand the harsh manufacturing environment and to develop better relationships between sensor data and the information needed for process control.

#### **DAMAGE IDENTIFICATION IN CYCLICALLY LOADED PZT TRANSDUCERS**

Catastrophic failure limits the application of brittle, ceramic materials; consequently, their fracture behavior has been intensely investigated. There exist a number of applications of ceramics, however, in which components are subjected to cyclic, rather than static or monotonically increasing, loads. One such application is the use of piezoelectric ceramics as transducers, in which the material undergoes large cyclic strains, often at resonance frequency. NIST investigations of lead zirconate titanate (PZT), a commercial transducer material, have shown that microcracks are generated during cyclic loading. These cracks do not link up at lower temperatures (e.g., at  $T \sim 80^\circ\text{C}$ ) but, at higher temperatures, may cause hundreds of micrometers of crack extension, which can eventually lead to mechanical failure. If the temperature of the specimen under load is allowed to rise above  $\sim 100^\circ\text{C}$ , the material fails catastrophically. While these results explain the lower strengths of PZT driven at resonance frequency, the fracture process is not yet understood. This understanding will be critical for the design of reliable, higher power devices.

#### **NIST PARTICIPATES IN THE UNITED NATIONS ASSESSMENT OF THE INTERNATIONAL CFC TREATY**

A NIST scientist was a principal author of a technology review report for the United Nations. This report assessed the impact of the planned phase-down of environmentally unacceptable chlorofluorocarbons (CFC) on chilled water systems for commercial building air conditioning. The Contracting Parties of the Montreal Protocol, signed in September 1988 and updated in London in 1990, will meet in Copenhagen in 1992. At that time, the group will likely make decisions for an

accelerated phase-out of CFCs and new plans to phase-out partially halogenated compounds (HCFCs). This decision will be based on an extensive number of reports summarizing all current knowledge on ozone sciences effects, technology, and economics. The NIST scientist and representatives of the three largest air conditioning manufacturers assessed the technology of large building air conditioning. They concluded that: (1) no substitute is currently known for HCFC-22 or HCFC-123, and (2) currently used HCFCs and HFC-134a must be available until 2020 AD (the generation of current equipment lifetime) if alternatives exhibiting equal or better performance and acceptable system cannot be found.

#### **NEW PUBLICATION FOCUSES ON MICROCOMPUTER-BASED EXPERT SYSTEM BUILDING TOOLS (ESBTs)**

Recent years have seen substantial growth in the number of expert systems being developed and fielded in the microcomputer environment. To a great extent, this growth is due to the advent of ESBTs designed for use on microcomputers. Sometimes known as expert system shells, ESBTs are special-purpose software packages that are used to develop expert systems. NIST Special Publication 500-188, Guide to Expert System Building Tools for Microcomputers, provides system managers, planners, and potential expert system developers with a description of ESBTs for the microcomputer environment, identifying specific tool features and the capabilities they support.

#### **GAMS TO BECOME COMPONENT OF HPCC DISTRIBUTED INFORMATION SYSTEM**

NIST has been invited to participate in the High Performance Computing and Communications (HPCC) Distributed Information System project being organized by NASA. The system will integrate several software libraries and information systems, NIST's contribution being its Guide to Available Mathematical Software (GAMS) system. As part of this project, an X-window interface to the GAMS on-line software catalog will be developed, and data describing the net-lib software collection of Oak Ridge National Laboratories will be added to the GAMS database. The NIST scientist who leads the GAMS project, will also coordinate planning for ongoing user support for the integrated information system. A number of other organizations are also participating.

#### **INDUSTRY/NIST TO DEVELOP AXLE INSPECTION SENSOR**

An automobile manufacturer and NIST are working to produce a nondestructive evaluation (NDE) sensor for inspecting case hardened steel drive axles. Under a 2 year cooperative research and development agreement, an automobile industry engineer will collaborate with NIST scientists to develop electrical eddy current sensing technology to measure "case depth," or how deeply steel axles have been case hardened. Case hardening is a heat-treating process that carburizes metals by making the outer surface harder than the core. The NDE sensor will allow all axles to be tested, possibly replacing current destructive testing of a small fraction of axles produced. The cooperative effort is under the sponsorship of NIST's Office of Intelligent Processing of Materials, an agency-wide program for upgrading the quality of engineering materials and confirming their reliability in service. For information, contact Arnold Kahn, A163 Materials Building, NIST, Gaithersburg, MD 20899, 301/975-6146.

#### **COMPUTER SECURITY BBS USER'S GUIDE PUBLISHED**

The Computer Security Bulletin Board System User's Guide (IR4667), a 38-page manual offering step-by-step instructions for using the NIST Computer Security Division's electronic bulletin board system (BBS), is now available. The BBS offers federal agencies and the general public access to a variety of computer security information. Included are software reviews, publications, bibliographies, lists of organizations, an events calendar, and other government BBS numbers. To use the BBS, you need a modem and personal computer with communication software. Access the BBS by dialing 301/948-5717 (300-2400/8/N/1 or 300-2400/7/E/1) or 301/948-5140 (9600/8/N/1). If you can't access the BBS after verifying your communications hardware and software are operating correctly, call the voice line, 301/975-3359, and ask for the BBS system operator. The user's guide is for sale by the National Technical Information Service, Springfield, VA 22161. Order by PB 92-112390; price \$17.

#### **AMINO ACID, ION INTERACTIONS PROBED**

A new basic chemistry project is spinning off useful tools for clinical laboratories and may eventually shed light on how living cells communicate. The project's long-term goal is the development of a standard reference database on the thermodynamic properties of amino acids, polypeptides, and

proteins. A more immediate benefit is the creation of a set of Standard Reference Materials for pH buffer solutions. These are used by medical laboratories to assess the accuracy of blood chemistry analyses. Buffer solutions for pH 6.8 and 7.4 developed at NIST are more accurate than previous standards. Nearly ready is a third buffer of pH 7.8 that will complete the normal physiologic range for cells. The project next calls for determining the electrical conductivity and potential measurements of the essential amino acid glycine, as well as a simple polypeptide, glycylglycine. Completion of the long-term goal—an electrochemical database for amino acids, polypeptides, and proteins—could help biologists understand and model how nerve impulses travel throughout the body.

#### **FIRST COMPILATION OF HIGH $T_c$ PHASE DIAGRAMS**

Under a cooperative program between NIST and industry, the American Ceramic Society (ACerS) has published Phase Diagrams for High  $T_c$  Superconductors. The volume, which contains 231 ceramic phase diagrams, was compiled by a team of experts under a NIST chemist and an ACerS guest scientist. Chemical systems are divided into two parts: alkaline earth, rare earth, copper, and oxygen diagrams; and alkaline earth, bismuth/lead, and copper oxygen diagrams. Often described as “road maps,” the diagrams save individual producers from having to conduct research on the combination of two or more ceramic materials in various relationships and conditions. Data evaluations were conducted in the Phase Diagrams for Ceramists Data Center at NIST, one of 22 centers making up the National Standard Reference Data System. The volume is available for \$70 (\$62 for ACerS members) from the American Ceramic Society, 735 Ceramic Place, Westerville, OH 43081, 614/890-4700.

#### **BULLETIN SURVEYS ELECTRONICS/ELECTRICAL ABSTRACTS**

Measurement programs in semiconductor microelectronics, signals and systems, electrical systems, and electromagnetic interference are among those described in the Technical Progress Bulletin, available now from NIST. The Bulletin covers programs that provide national reference standards, measurement methods, supporting theory and data, and traceability to national standards. It features abstracts of papers and other published works arranged by topic (with phone numbers of contacts). Semiconductor topics covered include silicon materials, insulators and interfaces, integrated circuit

test structures, and photodetectors. Also in the Bulletin are sections on waveform, cryoelectronic, antenna, electromagnetic, and laser metrology. To receive the most recent issue, or to be placed on the Bulletin mailing list, write or call (stating professional affiliation or technical interest) EEEL, B358 Metrology Building, NIST, Gaithersburg, MD 20899, 301/975-2220.

#### **NIST—INDUSTRY COLLABORATION DEMONSTRATES POTENTIAL FOR USE OF GARNET IN HIGH-FREQUENCY MAGNETIC FIELD SENSORS**

A NIST scientist and a team of industry scientists have demonstrated that certain iron garnets possess a Faraday effect response at much higher frequencies than anticipated. The work grows out of measurements carried out and reported by NIST last year that showed the existence of a Faraday response for pure yttrium-iron-garnet (YIG) at frequencies as high as 700 MHz. The industry team had developed a theoretical model for domain wall movement in ferrimagnetic films and the relationship of this movement to Faraday frequency response. On learning of the NIST result, the industry team reported to NIST that the model suggested that other materials introduced into pure YIG should affect the frequency response. The industry team then arranged to provide NIST with selected iron garnet thick films for determination of their Faraday response with frequency. The results of NIST's transmission-line measurements showed reasonable agreement with the predictions of the theoretical model. The material properties that affect the frequency response are the saturation magnetization, the magneto-crystalline energy, and the damping constant associated with ferrimagnetic resonance. It appears that all of these may be adjusted (although not necessarily independently) by varying the composition of the garnet. The large Faraday rotation of the iron garnets makes them good candidates for compact, sensitive magnetic sensors. This work opens up a new range of applications for them. A publication describing this work is in preparation.

#### **NEW CALCULATIONS OF DEMAGNETIZING FACTORS PUBLISHED**

A former NIST guest researcher and two NIST scientists have completed a comprehensive study of the demagnetizing factors of circular cylinders, including a review of the literature. The results of this work have appeared in the July 1991 issue of the IEEE Transactions on Magnetics and constitute

the first across-the-board update of material published some 50 years ago. The subject is important to researchers and engineers concerned with ferromagnetic and ferroelectric materials. Demagnetizing factors are used to correct experimental magnetic measurements on finite-sized samples to give data characteristic of the actual material. The demagnetizing factors for cylinders depend on both the cylinder's aspect ratio and the material's magnetic susceptibility. In contrast to earlier specialized treatments, the NIST work covers the entire range of susceptibilities, including infinite susceptibility (for ferromagnetic materials), zero susceptibility (for paramagnetic and diamagnetic materials), and negative susceptibilities (applicable to superconductors). Factors are reported to four significant figures with an accuracy of 1 percent.

#### **NIST PUBLISHES CRITERIA FOR THE OPERATION OF SECONDARY CALIBRATION LABORATORIES FOR IONIZING RADIATION**

NIST recently published Special Publication 812, Criteria for the Operation of Federally-Owned Secondary Calibration Laboratories (Ionizing Radiation). These criteria, for laboratories that calibrate instrumentation used to measure ionizing radiation, may be used for accreditation of a particular laboratory. They were developed by a group of 47 representatives of federally owned laboratories that perform instrument calibrations, and represent a consensus of those experts with regard to the conditions necessary for the assurance of quality. NIST actively supports the development of secondary calibration laboratories for ionizing radiation measurements through the Office of Radiation Measurement. This office serves as the coordinator between the NIST technical staff and the NIST accrediting body, the National Voluntary Laboratory Accreditation Program. This program is expected to accredit about eight laboratories within the next 2 years in such areas as calibration of survey instruments and irradiation of personnel dosimeters with alpha, beta, gamma, and x rays. These laboratories can then provide a high-quality link between the physical measurement standards maintained by NIST and those who make routine measurements at the field level.

#### **NIST REFEREES AND PROVIDES STANDARDS FOR AN INTERNATIONAL INTERCOMPARISON OF ATMOSPHERIC RADON MEASUREMENTS**

An international intercomparison of instruments used to measure trace atmospheric concentrations

of radon was recently conducted at the Bermuda Biological Research Station. Measurements of radon in remote marine environments are used to obtain information on the temporal and spatial distributions which are in turn used to test and validate global models that simulate the transport and removal of trace atmospheric species. Unlike other chemical species, radon is an excellent tracer for such studies because it has a well-characterized source (large land masses) and only one principal "sink" (radioactive decay). NIST's radioactivity group participated and served as the referee for the intercomparison, and was responsible for providing standardized additions of radon concentration to the sampling tower used by the various participants for simultaneous measurements. The intercomparison included radon activity concentrations ranging from less than 50 atoms per L (at typical ambient levels) to over several hundred thousand atoms per L (0.001 Bq/L to 0.4 Bq/L). The participants were the U.S. DOE Environmental Measurements Laboratory; Centre des Faibles Radioactivités, Laboratoire CARS-CEA, France; the Australian Nuclear Science and Technology Organization; and Drexel University (U.S.A.). This exercise was the first such intercomparison of instruments used in different worldwide locations and will provide a common reference and intercalibration for data obtained from various world locations.

#### **TECHNOLOGY TRANSFER PROGRAM BETWEEN NIST AND SEMATECH YIELDS NEW STANDARDS AND IMPROVES U.S. COMPETITIVENESS**

NIST recently completed a joint development contract with Sematech to establish calibration procedures for ultraviolet (uv) light intensity measurements. NIST now provides a service for calibrating I-line (the 365 nm mercury line) radiometers used as detectors in photolithography systems. A direct benefit of this program was to demonstrate that the U.S.-manufactured, GCA I-line system, performs equivalently to its competitors. GCA can now offer its customers better control of their semiconductor production as a result of uv measurements that are traceable to a NIST standard. The weaknesses and strengths of I-line radiometers and the techniques used to calibrate them are identified in the Sematech technology transfer publication #91040516A-ENG.

**NEW EDDY CURRENT INVERSION THEORY**

A NIST scientist, in collaboration with the University of Surrey Physics Department, U.K., has developed a general theory of flaw reconstruction from eddy-current measurements. Based on this theory, multifrequency and variable probe-position impedance data can be processed to determine the three-dimensional geometry of discrete flaws—cracks or voids—in metals. The theory also permits the determination of an unknown continuous distribution of electrical conductivity. Thus far, reconstructions based on simulated multifrequency impedance data have verified the theory for a layered conductor, in which the thicknesses and conductivities of the individual layers were successfully predicted. Other potential applications of the inversion methodology include the nondestructive characterization of composite materials and the determination of the thickness of metallic coatings.

**FLOW THROUGH POROUS MEDIA**

NIST scientists have developed a method for measuring the permeabilities of fiber preforms which minimizes edge effects and maximizes the accuracy of flow and pressure measurements. The permeability to resin flow of fiber preforms, the reinforcement fabrics of polymer composite parts, is needed to accurately model mold filling in resin transfer molding. The NIST method uses saturated fabrics in one-dimensional flow geometries, and data are collected for flow in at least three directions in the case of an anisotropic fabric. From such measurements the in-plane permeability tensor is determined and flow in any in-plane direction through the fabric can be calculated. This method is currently being extended to measure the complete three-dimensional permeability tensor.

Collaborative work with a private company was undertaken to compare permeability data obtained by the NIST method with values measured in unsaturated radial flow experiments. The excellent agreement between the NIST predictions of the shape and progress of elliptical flow fronts in radial flow experiments and the experimental observations at the company indicated that the radial and one-dimensional flow experiments are geometrically consistent, and, therefore, can be combined in characterization studies to maximize efficiency.

**CIB WORKSHOP ON FIRE MODEL VERIFICATION, SELECTION, AND ACCEPTANCE HELD AT NIST**

The Committee on Fire (W14) of the International Council for Building Research Studies and Docu-

mentation (CIB) recently held a Workshop on Fire Model Verification, Selection, and Acceptance at NIST.

The workshop was designed to provide strategic guidance to the research community on knowledge needed for the verification of fire models and their international acceptance for use in fire safety engineering. The sessions covered: model quality and validity, supporting infrastructure needed, guidance for selection and use of models, and criteria and strategy for model acceptance.

The workshop attendees agreed that guide documents on model validation and on model documentation developed by ASTM should be reviewed by CIB for submission to ISO as bases for international standards. They also recognized the need for an internationally accepted method for organizing input data and large-scale test data for convenient use by fire model developers and users. The method should be developed for electronic distribution. The fire data management system conceived in the NIST fire program is a candidate. It was agreed that CIB should develop a 5 year coordinated program of research on the validation and use of fire models.

**NORTH AMERICAN INTEGRATED SERVICES DIGITAL NETWORK (ISDN) USERS' FORUM (NIU-FORUM) RESULTS PUBLISHED**

Two new publications document the work of the NIU-Forum, a NIST/industry collaboration established in 1988 to create a strong user voice in the implementation of ISDN technology. NIST Special Publication 500-194, ISDN Conformance Testing, Layer 1—Physical Layer, Part 1—Basic Rate S/T Interface, User Side, describes a set of test specifications, developed by NIU-Forum members, which test conformance of Terminal Equipment and Network Termination (NTs) to the ISDN Physical Layer at the S/T reference point, as defined in American National Standard (ANS) T1.605-1989. NIST Special Publication 500-195, North American ISDN Users' Forum Agreements on Integrated Services Digital Network, compiles the existing NIU-Forum agreements as of November 1990.

**GLOSSARY OF COMPUTER SECURITY TERMINOLOGY PUBLISHED**

NISTIR 4659, Glossary of Computer Security Terminology, presents a collection of terms and definitions used by various federal departments and agencies in their policies, standards, and other publications. Developed under the auspices of the National Security Telecommunications and Information Systems Security Committee and published



by NIST as part of its efforts to disseminate federally sponsored work, the document provides multiple definitions to reflect the variations in use of these frequently encountered computer and communications security terms among the federal community.

#### **SMALLEST ANTENNAS IMITATE INSECT COMMUNICATION**

Using tools developed for fabricating electronic integrated circuits, NIST scientists have produced microantennas the size of a grain of sand and only 60  $\mu\text{m}$  across (about the diameter of a human hair). At this tiny size, these "world's smallest" antennas can capture the extremely short (about 3 to 30  $\mu\text{m}$ ) wavelengths of infrared radiation. Their development paves the way for novel infrared detectors that rely on antennas to "see" images of heat radiating from all warm objects such as people, animals, and buildings. Such detectors have many applications, including satellite observation of Earth, astronomy, medicine, and national defense. There is evidence that insects evolved microantennas, similar to the NIST devices, to enhance their infrared pickup, allow them to see in darkness, and give them a survival advantage. The NIST work proves that such tiny insect structures can function efficiently for infrared wavelengths.

#### **NEW OFFICE TO SPEED ROCKY MOUNTAIN TECH TRANSFER**

To coordinate and intensify the commercialization of government-developed technology to industry in the Rocky Mountain region, NIST has established an Office of Research and Technology Applications (ORTA) at the U.S. Commerce Department's Boulder, CO Laboratories. The office will support the technology transfer efforts of scientists and engineers at the three laboratories—NIST, the National Oceanic and Atmospheric Administration's Environmental Research Laboratories (NOAA/ERL), and the National Telecommunications and Information Administration (NTIA)—by coordinating common on-site services, providing training in commercialization procedures, helping create Cooperative Research and Development Agreements (CRDAs), licensing federal patents, and improving dissemination of research results to the private sector.

#### **NEW PUBLICATION ISSUED ON SECURITY IN ISDN**

In this decade, Integrated Services Digital Network (ISDN) standards will provide worldwide digital communications service and play a key role in the transition to electronic documents and business transactions. Government and businesses are increasingly concerned with security in ISDN. Security in ISDN (NIST Special Publication 500-189), covers the standards needed to implement user security. ISDN security standards should take advantage of, and be compatible with, emerging standards for Open Systems Interconnection security, including confidentiality, access control, authentication, data integrity, and nonrepudiation. The challenge of ISDN security is to extend these concepts to all ISDN applications, including voice use of the public network. The 76-page publication provides a broad discussion of user security needs and suggests possible solutions. Available from the National Technical Information Service, Springfield, VA 22161 for \$19 prepaid. Order by PB 92-116391.

#### **CASE STUDY ON SOFTWARE RE-ENGINEERING**

Software re-engineering involves the use of existing software and documentation to specify requirements, design, documentation, and production of software for a new computing platform. Software Reengineering: A Case Study and Lessons Learned (NIST Special Publication 500-193) targets managers and technical personnel in government and industry who need to understand concepts and issues of software re-engineering, the use of Computer-Aided Software Engineering (CASE) tools in the re-engineering process, and the application of this technology to organizational problems. A case study conducted by NIST and the Internal Revenue Service indicates that software re-engineering can be a cost-effective, viable solution for extending the lifetime of an application system. Technical information on the 39-page publication is available from Mary K. Ruhl at 301/975-2983. The publication is for sale by the National Technical Information Service, Springfield, VA 2161 for \$17 (hard copy) and \$9 (microfiche) prepaid. Order by PB 92-116417/AS.

**MAGNETIC FIELD FACILITIES IN JAPAN EVALUATED**

Japanese high magnetic field facilities for research on superconducting materials are capable of producing fields (both direct current and pulsed) comparable to the highest in the world, says a NIST researcher in a study prepared under the Japanese Technical Literature Act of 1986 (P.L. 99-382). Further, a concerted effort by Japan will result in a new magnetic facility capable of creating the world's highest dc field, 40 T, by 1993 (current highest is the U.S. limit at 31.8 T). The United States will not reach 45 T until new facilities are completed by 1995 or later, so research in this area must currently be performed in either Japan or Europe. The NIST report says most research on superconducting materials does not require the highest magnetic fields. However, critical properties such as current density and temperature must be perfected at such levels before promising new materials can be used. High Magnetic Field Facilities in Japan Related to Superconductivity Research (NISTIR 4593), is available for \$17 prepaid from the National Technical Information Service, Springfield, VA 22161. Order by PB 91-240762.

**TRAPPED ION EXPERIMENTS HIGHLIGHTED**

Researchers in the field of trapped and stored atoms and ions will be interested in a new paper from the NIST ion storage group in Boulder, CO. The paper summarizes recent work in developing techniques for high-resolution spectroscopy using stored ions. Topics covered in the paper include beryllium hyperfine pressure shift, linear Paul traps, Penning trap density limitations, theory of Sisyphus cooling for a bound atom, observation of "atomic projection" noise, and subharmonic excitation of a single electron. For a copy of paper 49-91, Recent Experiments on Trapped Ions at the National Institute of Standards and Technology, contact Jo Emery, Div. 104, NIST, Boulder, CO 80303, 303/497-3237.

**"MEETING THE CHALLENGE" NOW AVAILABLE ON VHS**

A new videotape describing how NIST helps strengthen U.S. industry's competitiveness, advance science, and improve safety, health, and the environment was recently released. The 11 minute tape, "Meeting the Challenge," highlights research in biotechnology, precision

measurement of atoms, intelligent processing of materials, automated manufacturing, the Integrated Services Digital Network, and the Malcolm Baldrige National Quality Award. Also featured are cooperative programs with the Ray Watson Co., Du Pont, and Hewlett-Packard. VHS copies are \$12 (shipping included) and may be purchased from Video Transfer, Inc., 5709-B Arundel Ave., Rockville, MD 20852, 301/881-0270.

**HIGH-PERFORMANCE COMPUTING ACT OF 1991 (S. 272) BECOMES LAW**

On Dec. 9, the President signed into law S. 272, the High-Performance Computing Act of 1991—P.L. 102-194. NIST's responsibilities under the act include: developing and proposing standards and guidelines and developing measurement techniques and test methods for the interoperability of high-performance computing systems in networks and for common user interfaces to systems; developing benchmark tests and standards for high-performance computing and software; and developing and proposing standards and guidelines for assuring cost-effective security and privacy for sensitive information in federal computer systems.

**NIST WORK PROMPTS INCREASED INTEREST IN ADVANCED PARTIAL DISCHARGE MEASUREMENT SYSTEMS AS DIAGNOSTIC TOOLS**

The electric power industry is becoming increasingly interested in applying to practical diagnostic issues the results of the research on partial discharge measurements carried out by NIST scientists. It recently has sought sensors for physical parameters to be incorporated in its largest, most expensive high-voltage transformers to be able to operate the resulting "smart" devices as close to their limits as possible for the sake of efficiency. Conventional sensors develop limited data useful for predicting failure. The NIST research has demonstrated that partial discharge measurement systems can provide data for failure prediction, and the electric power industry is renewing its interest in these systems. A major contribution of the NIST work has been to uncover the basis for the nonstationary behavior of partial discharge phenomena, which frustrated previous attempts at reliable pattern recognition using conventional pulse-height analysis techniques.

### PROTEIN MAPPING TECHNIQUES ADVANCE CANCER RESEARCH

A method based on two-dimensional electrophoresis and computerized image processing has been developed to map and characterize subtle changes in the protein composition of cancer cells when they are treated with chemotherapy drugs. This research was featured in a recent issue of Genetic Engineering News, one of the most widely read biotechnology news magazines. NIST scientists collaborated with researchers at the John Wayne Cancer Institute at St. John's Hospital in Santa Monica, CA, in this research, which is being used to identify specific proteins associated with the disease state. When the protein maps of untreated cells of skin cancer (melanoma) patients were compared with the maps of cells treated with chemotherapy drugs (e.g., interferon or tumor necrosis factor), it was discovered that the cells slowed down or stopped production of certain proteins and increased or began making other proteins in response to treatment. Attempts are being made to correlate the genetic expression of these proteins with the tumor gene products and the tumor suppressor gene products. This approach will prove valuable in monitoring the effects of drugs on tumor cells as well as providing insight into the molecular mechanisms of tumor growth and suppression.

### ULTRACOLD ATOMIC COLLISIONS

Collisions of laser cooled and trapped atoms exhibit new and unusual effects at temperatures below 1 mK. Recent studies at NIST show that these collisions can be modeled by considering the relative motion of two atoms in a laser field and allowing this energy to dissipate by spontaneous photon emission. The equations of motion, called the optical Bloch equations and widely used in quantum optics, are normally not used to describe collisions. This theoretical formulation offers new insight into the novel mechanisms of ultracold collisions, treats intense laser modification of the collision dynamics, and provides a predictive tool for analyzing experiments. Good agreement is found between theory and current experiments on both Cs and metastable He traps. It is expected that predictions for other traps will soon be tested by experiments at NIST and other laboratories.

### A MULTINATIONAL VIEW OF THE ACTIVE SUN

On Aug. 30, a major x-ray imaging and spectroscopic spacecraft was launched from the Kagoshima

Space Center in Sagami-hara, Japan. As reported Nov. 8 in Science, the satellite, now dubbed Yohkoh, has begun sending back spectacular pictures of solar activity viewed with unprecedented angular resolution and spectroscopic refinement. Developed by the Japanese space science agency, the spacecraft's principal instrumentation is a multinational project involving U.S., U.K., and Japanese research organizations.

Spectacular early results from the mission include remarkable high-resolution spectra being recorded and sent to Earth from a group of four Bragg crystal spectrometers (BCS) on Yokoh. These instruments, three trained on the He-like resonance lines of S, Ca, and Fe and one on H-like Fe, were developed jointly by the Naval Research Laboratory and NIST in collaboration with the Rutherford Appleton Research Laboratory and Imperial College in the United Kingdom.

The BCS instrument required both improved sensitivity and improved resolution in a package severely constrained in volume, mass, footprint, and power consumption in comparison with previous NASA missions. The overall design of BCS was a joint undertaking, with NIST responsible for the design, fabrication, testing, and alignment of the four large, 4 × 18 cm, germanium diffraction crystals, each bent to a particular radius of curvature between 5 and 15 m. The technology needed, the result of more than 2 decades of development for a wide range of applications, was fully exploited in preparing the crystals now in orbit.

Results already in hand indicate that the efforts were fully successful. Both the spectroscopic detail resolved and the instrumental sensitivity are in accord with expectations. Of particular note in this regard is that there is already evidence of rapid outward motion of flare material in the period of time before the flare manifests itself to the telescope.

### QUALITY CONTROL IN RADIATION THERAPY

NIST and the U.S. Nuclear Regulatory Commission recently co-sponsored a workshop at NIST to examine calibration issues for the high-dose-rate (HDR) iridium-192 radioactive sources used in cancer therapy. Over 100 of these computer-controller source-insertion devices are now used in the United States for the treatment of approximately 6,000 patients per year. A national strategy is needed for calibrating these sources to allow uniform specification of source strength by source manufacturers, instrument manufacturers,

secondary calibration laboratories, and hospital medical physicists. The sources have activities more than 100 times higher than the low-dose-rate iridium-192 seeds for which NIST offers calibrations. The goal of the workshop was to define the requirements for NIST and the secondary calibration laboratories, and to explore the standardization methods and transfer instruments appropriate to each level. Based on discussions held at the workshop, NIST will begin to develop an appropriate national primary dosimetry standard. The workshop provided the medical physics community, the health-care industry, and regulators with a snapshot of quality control and standards-related issues in HDR iridium-192 cancer therapy.

#### **MERGED-BEAMS TECHNIQUE FOR ABSOLUTE ELECTRON-ION EXCITATION MEASUREMENTS DEMONSTRATED**

The combination of a merged-beams and an electron-energy-loss technique has permitted ground-breaking absolute measurements of a cross section for electron-impact excitation of a multiply-charged atomic ion. Highly charged atomic ions are pervasive and critical elements in high-temperature plasmas (fusion, astrophysical, laser, and others). Their structure, dynamics, and interactions with other particles are, despite the crying need for data as well as fundamental understanding, generally not well known. Experimental information on electron-impact excitation of multiply-charged ions is particularly scarce—almost all past measurements involved singly-charged ions and a very restricted set of transitions for which fluorescence from excited states could be used as the detector. This new collisions technology, combined with the availability of abundant ions from advanced ion sources, permits greatly enhanced signals (merged rather than crossed beams) and detection efficiencies (all electrons involved rather than just some photons) compared with that attainable with traditional ion sources and crossed-beams collision geometries. The first measurements that demonstrated the power of this new technique involved the third ionic stage of silicon, but an entirely new spectrum of measurements has now been proven feasible. A key element in the new technique is a real-time charged-particle beam probe that can be used both as a beam diagnostic and to quantitatively determine the beam density distribution in all three dimensions.

#### **NEW PUBLICATION FOCUSES ON COMPUTER SECURITY INCIDENT RESPONSE**

Increased threats to computer security have prompted government agencies and industry organizations to augment their computer security efforts. NIST Special Publication 800-3, Establishing a Computer Security Incident Response Capability (CSIRC), provides advice and assistance on initiating an efficient and timely response to computer security-related incidents such as computer viruses, unauthorized user activity, and serious software vulnerabilities. The guide discusses some of the considerations in establishing a CSIRC and the organizational, technical, and legal issues connected with a CSIRC operation. Efficient and cost-effective, a CSIRC is a proactive approach to computer security, one that combines reactive capabilities with active steps to prevent future incidents.

#### **NIST COLLABORATION ON FRICTION CHARACTERIZATION OF ULTRA-LOW SPEED TURNING MACHINES**

Two mechanical engineers from a major U.S. university recently completed a 3 month research project at NIST in collaboration with a NIST statistician. The project goal was to improve the precision of high-performance grinding where a machining defect called sub-surface damage is a major problem. The basic hypothesis is that this damage occurs due to impact type chip removal in the machining process. Such impact chip removal is avoided by machining in the ductile regime, which translates to a very slow and well-regulated speed control problem. Such low speeds accentuate the effect of friction and its unpredictable nature. To study this problem, off-line statistically designed experiments involving factors affecting friction were conducted. The data collected were analyzed to understand the friction characterizations and develop appropriate model structures for on-line control. Details of this collaborative research will appear as a NIST internal report.

#### **A CATALYST PACKAGE FOR LUBRICANT OXIDATION (ASTM SEQUENCE IIIE ENGINE TEST)**

The Standard Reference Materials Program announces the availability of RM 8501, a Catalyst Package for Lubricant Oxidation. The material is intended for use in a modified thin-film uptake test developed for use with oils for the ASTM Sequence IIIE Engine Test.

The thin-film oxygen uptake test identified in ASTM D4742 was originally developed to evaluate

the oxidation stability of automotive crankcase lubricants under conditions similar to ASTM engine sequence 111D test. The test used fuel fractions and mixed metal catalysts to simulate the chemical environment in an operating automotive engine. Recently, ASTM Sequence 111E test was developed to replace the 111D test. The 111E test defines a new oil category having improved performance and requires an increased oxidation severity. This is achieved by using a smaller oil charge and increased blow-by to oil charge ratio.

The oxidation induction times for seven IIE oils were determined by both the modified thin-film oxygen uptake test and differential scanning calorimetry using RM 8501. The test conditions for the correlation between the two measurements are given in the Report of Investigation.

The RM includes five ampoules each of four components: an oxidized/nitrated fuel fraction; a nitroparaffin model compound; a metal naphthenates mixture containing lead, iron manganese, and tin in a 20:2:1:1 weight ratio; and distilled water. Each is contained in a sealed ampoule, which should be thoroughly shaken before opening and sampled immediately after opening in order to maintain the RM integrity.

#### **REFERENCE MATERIALS 8589 AND 8590— FLUID CRACKING CATALYSTS (8589) AND HIGH SULFUR GAS OIL FEED (8590)**

The Standard Reference Materials Program announces the availability of two reference materials (RMs), 8589 and 8590, intended for use in determining the activity of Fluid Cracking Catalysts (FCC) as specified in the American Society for Testing and Materials Microactivity Test D3907-87. RM 8589 consists of six 50 g units of equilibrium FCCs, one each of RR1 through RR6, while RM 8590 consists of 946 mL of the High Sulfur Gas Oil Feed (Amoco Oil No. FCC 893).

These RMs are intended for use primarily by the petroleum refining industry and catalyst suppliers to this industry. They were prepared and characterized through a cooperative program between NIST and the ASTM Committee D32 on Catalysts. The six FCCs comprising RM 8589 are characterized for the weight percent conversion of gas oil, RM 8590, in a microactivity unit. Results given are the consensus values from an interlaboratory study after modification for nonuniform data according to ASTM Standard Practice E 691.

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## **Calibration Services**

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### **NEW HUMIDITY MEASUREMENTS PUBLICATION AVAILABLE**

The National Weather Service, the semiconductor industry, and food processors all keep a watchful eye on humidity with a variety of sophisticated instruments. When these instruments need calibration, industry and government scientists turn to a specially designed lab at NIST that compares the instruments' performance against the most accurate humidity standards available. A new 61-page publication describing NIST calibration services for humidity measurements has been compiled. The new document is a combined and condensed version of earlier reports on NIST's primary and secondary standards for humidity measurement. The two-part document covers NIST's standard hygrometer and two-pressure humidity generator. NIST Calibration Services for Humidity Measurement is available from the National Technical Information Service, Springfield, VA 22161. Order by PB 92-112499; price is \$19 in print or \$9 on microfiche.

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## **Standard Reference Materials**

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### **STANDARD REFERENCE MATERIAL 1414— LEAD-SILICA GLASS HIGH-TEMPERATURE RESISTIVITY**

The Standard Reference Materials Program announces the availability of SRM 1414, Lead-Silica Glass for High-Temperature Resistivity. SRM 1414 is intended for use in glass resistivity measurements. The SRM is a lead-silica glass (4×4×12 cm bar) certified for resistivity at a series of temperatures in the molten range of 950-1300 °C. Additional information is also given on the glass composition, refractive index, and dispersion.

### **STANDARD REFERENCE MATERIAL 2695— FLUORIDE IN VEGETATION**

The Standard Reference Materials Program announces the availability of SRM 2695, Fluoride in Vegetation (timothy grass). This SRM is intended for use in monitoring fluoride in vegetation

used as cattle forage, for which there are annual, bimonthly, and monthly regulatory limits in the range of 40-80 parts per million (ppm). Animals normally ingest small amounts of fluoride in their rations with no harmful effects. However, excessive fluoride ingestion can cause specific dental and skeletal lesions, and in severe cases, adversely influence the productive performance of domestic animals. Uncontaminated plant material typically contains less than 5 ppm.

The SRM is supplied as 25 g each of a low and high level sample. The low-level concentration of 64.0 ppm is in the range of the regulatory limits, which varies somewhat between states, while the high-level concentration of 277 ppm exceeds all regulatory limits.

Certification measurements were made using a number of methods, including the Association of Official Analytical Chemists (AOAC) and Intersociety method for the semi-automated determination of fluoride based on calorimetric alizarin measurement following fusion and microdistillation.

#### **STANDARD REFERENCE MATERIAL 885—REFINED COPPER**

The Standard Reference Materials Program announces the availability of SRM 885, Refined Copper. The intended use of this SRM is for calibration of instruments and the evaluation of methods used in determining sulfur and oxygen in pure copper or related materials. SRM 885 will be used primarily by copper producers employing a continuous casting process in producing high purity copper rod or wire products. It is certified for sulfur and oxygen contents of 0.0018 percent and 0.013 percent, respectively, and has been analyzed for trace element impurities such as antimony, arsenic, bismuth, iron, lead, nickel, silver, tin and zinc.

The SRM is in the form of pins approximately 13 mm long and 3 mm in diameter, having a mass just under 1 g.

#### **AROMATIC HYDROCARBONS IN TOLUENE (NOMINAL CONCENTRATION 60 µg/mL)**

The Standard Reference Materials Program announces the availability of SRM 2260, Aromatic Hydrocarbons in Toluene. The SRM is intended primarily for use in calibrating chromatographic instrumentation and for use in evaluating analytical methods used to determine aromatic hydrocarbons

(AHs). The SRM consists of five 2 mL ampoules, each containing approximately 1.2 mL of the AHs in toluene solution. Because of the volatility of toluene, certified values are not applicable to material, unless analysis is initiated immediately (under 5 min) after opening the ampoule.

SRM 2260 is certified for the actual concentrations of 23 AHs, all present in the toluene at a nominal concentration of 60 µg/mL. The concentration of one additional AH is not certified but is given for information. The actual concentrations were determined both gravimetrically in preparing the solution and chromatographically on the prepared solution.

#### **TWO NEW SRMs FOR OPIATES IN URINE CERTIFIED**

NIST has an ongoing program, in cooperation with the College of American Pathologists, to provide the drugs-of-abuse testing community with urine-based reference materials. Scientists at NIST recently have completed work on two new SRMs for drugs of abuse in urine. SRM 2381 is a freeze-dried human urine material with certified concentrations of free morphine and codeine at three levels. Certification was accomplished by use of two independent methods. One was a gas chromatography/mass spectrometry (GC/MS) procedure, similar to the procedures used in drug testing laboratories to confirm and quantify these analytes in samples that test positive in preliminary screening analyses. The other involved liquid chromatography/mass spectrometry (LC/MS) with a different sample preparation procedure. The certified concentrations bracket the cutoff concentration level set by the National Institute of Drug Abuse for determining both morphine and codeine abuse and thus permit laboratories to validate the accuracy of their methods in this critical concentration range.

The second material, SRM 2382, has three certified levels of morphine glucuronide in freeze-dried human urine. Much of the morphine excreted by opiate users is in the form of the glucuronide. Laboratories testing urine specimens for opiates must release the morphine from the morphine glucuronide prior to accurately measuring the morphine present. The quantitative release of morphine has been identified as a major problem area in accurate drug analysis. This SRM will allow laboratories to test their methods for releasing the morphine on samples with known concentrations. Certification of SRM 2382 required the use of a

different procedure for releasing morphine for each of the analytical techniques used for the measurements. Enzymatic hydrolysis was used with the GC/MS method and acid hydrolysis was used with LC/MS. Careful studies at NIST found the two hydrolysis procedures to provide comparable results.

#### **STANDARD REFERENCE MATERIAL 1048, CUP FURNACE SMOKE TOXICITY STANDARD**

The Standard Reference Materials Program announces the availability of SRM 1048, Cup Furnace Smoke Toxicity Method Standard. The SRM is intended for use in calibrating the NIST Cup Furnace Smoke Toxicity Method for assessing the acute inhalation toxicity of combustion products. The SRM consists of eight sheets of acrylonitrile-butadiene-styrene (ABS) copolymer, each approximately 254 mm square and 0.76 mm thick. The quantity is sufficient for calibration of the test method four times.

Certified values for  $LC_{50}$  and N-gas in flaming and nonflaming modes are provided at 30 min and 30 min plus 14 d post exposure periods. The values are based on three separate series of tests and statistical evaluation of the resultant data.

#### **STANDARD REFERENCE MATERIALS 1271 AND 2171 LOW-ALLOY STEEL (Ni-Cr-Cu-Mo) (HSLA 100)**

The Standard Reference Materials Program announces the availability of SRMs 1271 and 2171, Low-Alloy Steel issued in both disk and chip forms. The steel is identified as HSLA 100 (Ni-Cr-Cu-Mo) and is primarily intended for use in optical emission and x-ray spectrometric analyses (disk) or in chemical methods (chip). SRM 1271 is issued in the form of a disk approximately 35 mm in diameter by 19 mm thick, while SRM 2171 is issued as 150 g of chips, sized between 0.50 and 1.18 mm (or between 16 and 35 mesh).

Certification was performed in cooperation with ASTM. In addition to Ni, Cr, Cu, and Mo, the SRMs are certified for C, Mn, P, S, Si, V, Al and Nb.

#### **STANDARD REFERENCE MATERIAL 2193, CALCIUM CARBONATE pH STANDARD**

The Standard Reference Materials Program announces the availability of SRM 2193, Calcium Carbonate pH Standard. This commercially available calcium carbonate, selected specifically for its extremely low level of metal impurities, is certified only with respect to pH values and not for compo-

sition. The SRM is supplied as a 30 g unit of finely powdered material. It is intended for calibration of pH measuring systems at pHs above 11.0.

The SRM is used to prepare a freshly filtered saturated solution (0.0202 molal) of calcium hydroxide as instructed on the certificate. The pHs of the resulting solution are certified at 12 temperatures from 0 to 50 °C, based on EMF measurements of cells without liquid junction, using hydrogen gas and AgCl/Ag electrodes. Two-point calibration is recommended for high alkalinity measurements and is accomplished using SRM 2193 in conjunction with SRM 187 (borax).

#### **STANDARD REFERENCE MATERIALS 862 AND 1242, HIGH-TEMPERATURE ALLOY L 605**

The Standard Reference Materials Program announces the availability of SRMs 862 and 1242, the chip and disk forms of High-Temperature Alloy L 605. The chips are intended primarily for use in chemical methods of analysis, while the disks are for use in optical emission and x-ray spectrometric methods. SRM 862 is issued as a unit of 100 g of chips sized between 0.35 and 0.85 mm (or between 46 and 20 mesh). SRM 1242 is issued as a disk approximately 35 mm in diameter and 19 mm thick.

SRMs 862 and 1242 are certified for 13 elements: the primary constituents Co, Cr, W, Ni, Fe, and Mn, and the trace constituents C, P, S, Si, Cu, V, and N. Certification was performed in cooperation with ASTM.

#### **STANDARD REFERENCE MATERIAL 1976, INSTRUMENT SENSITIVITY STANDARD FOR X-RAY POWDER DIFFRACTION**

The Standard Reference Materials Program announces the availability of SRM 1976 for use in calibration of powder x-ray diffraction intensity as a function of 2 angle (instrument sensitivity) and to provide comparability of measurements between laboratories. The SRM consists of a sintered high-purity alumina plate approximately 45 mm on a side and 1.6 mm thick. The material was selected for consistency of microstructure.

The SRM is certified for the absolute variation of intensity of the [104] reflection, 12 relative intensities determined throughout the 2 range of x-ray diffraction goniometers, and the lattice parameters. Proper use of the SRM requires measurement of test equipment intensities according to one of the two procedures used for certification of the SRM.

**STANDARD REFERENCE MATERIAL 2261,  
CHLORINATED PESTICIDES IN HEXANE  
(NOMINAL CONCENTRATION 2 µg/mL)**

The Standard Reference Materials Program announces the availability of SRM 2261, a solution of 15 chlorinated pesticides in hexane. It is intended primarily for use in research and in health and environmental monitoring. This SRM is one of a series of pesticide and PCB SRMs produced and/or characterized in cooperation with other U.S. government agencies, including NOAA and the EPA. Certified pesticide values are based on the equally weighted means of the gravimetric concentration from the preparation of the solution and the measured concentration from the chromatographic analysis of the solution. The following pesticide compounds are present in the solution at a nominal concentration of 2 g/mL: hexachlorobenzene, gamma-HCH, heptachlor, aldrin, heptachlor epoxide, cis-chlordane, trans-nonachlor, dieldrin, mirex; 2,4'-DDE; 4,4'-DDE; 2,4'-DDD; 4,4'-DDD; 2,4'-DDT; 4,4'-DDT. The SRM is supplied as a unit of five 2 mL ampoules, each containing approximately 1.2 mL of solution.

**BROCHURES OFFER QUICK GLIMPSE OF  
CHEMISTRY SRMs**

A series of NIST brochures offers easy-to-read descriptions of Standard Reference Materials (SRMs) for verifying the accuracy of hundreds of chemical measurements. The set of eight brochures lists SRMs for agriculture and food science, clinical laboratories, environmental laboratories, gases, industrial hygiene, marine science, microprobe and scanning electron microscope measurements, and spectrometric analysis. Examples of how these measurements can be used include: food manufacturers measuring cholesterol, minerals, and trace elements in their products; environmental regulators monitoring air, water, and soil pollution; and medical labs measuring drugs of abuse or verifying the accuracy of blood chemistry analyses. The eight chemistry SRM brochures, part of a series of 16 on select SRMs, are available singly or as a set from the Standard Reference Materials Program, Building 202, Rm. 204, NIST, Gaithersburg, MD 20899, 301/975-6776.

**STANDARD REFERENCE MATERIAL 131e—  
LOW CARBON SILICON STEEL**

The Standard Reference Materials Program announces the availability of a low-alloy steel, Standard Reference Material (SRM) 131e, which

is certified for carbon and sulfur. SRM 131e was developed in cooperation with the American Society for Testing and Materials.

The SRM is intended primarily for use in calibrating or verifying accuracy of analyses performed using carbon/sulfur analyzers. The SRM is in chip form, with the chips sized between 0.5 and 1.0 mm sieve openings. The certified concentrations of carbon and sulfur are 0.0035 and 0.0004 weight percent, respectively.

**STANDARD REFERENCE MATERIAL (SRM)  
FOR MAGNETIC TAPE CARTRIDGE DRIVES  
AND MEDIA NOW AVAILABLE**

SRM 3202 is now available for public sale. The SRM will be used by manufacturers of 12.7 mm (1/2 in), 972 ft/mm (24,689 ft/in) magnetic tape cartridge drives and media as specified in interchange standards x3.180 and ISO 9661. SRM 3202 will provide the manufacturers with a reference for several magnetic properties including output signal amplitude, typical field, overwrite, and resolution.



# Calendar

March 2-6, 1992

## IEEE P1157 MEDICAL DATA INTERCHANGE (MEDIX)

Location: National Institute of Standards and Technology  
Gaithersburg, MD

**Purpose:** To specify and establish a robust and flexible communications standard for exchange of data between heterogeneous healthcare information systems.

**Topics:** User requirements, framework, information model methods, clinical laboratory information model, registration/ADT information model, pharmacy information model, finance/statistics information model, communication model methods, mapping, OSI profiles, executive committee, education/publicity.

**Format:** Workshop.

**Audience:** Individuals with an interest in the following areas: User requirements for healthcare data interchange, healthcare information modeling, data interchange formats for healthcare data, OSI in healthcare, Semantics and knowledge representation as applied to the electronic patient record, prototype development of MEDIX systems.

**Sponsors:** NIST and the Institute of Electrical and Electronics Engineers.

**Contact:** Jack Harrington, Hewlett-Packard Company, 175 Wyman St., Waltham, MA 02254-9030, 617/290-3517.

March 2-6, 1992

## IEEE P1073 MEDICAL INFORMATION BUS (MIB)

Location: National Institute of Standards and Technology  
Gaithersburg, MD

**Purpose:** To provide an international standard for open systems communication in healthcare applica-

tions primarily between bedside medical devices and clinical information systems, optimized for the acute care setting.

**Topics:** Progression of the individual MIB documents.

**Format:** Workshop.

**Audience:** Individuals with an interest in the following areas: User requirements for medical data interchange, medical device information modeling, data interchange language for healthcare data, OSI in healthcare, prototype development of MIB systems.

**Sponsors:** NIST, and the Institute of Electrical and Electronics Engineers.

**Contact:** Jack Harrington, Hewlett-Packard Company, 175 Wyman St., Waltham, MA 02254-9030, 617/290-3517.

March 4-6, 1992

## NIST WORKSHOP ON THE ELECTRONIC EXCHANGE OF FINGERPRINT IMAGES

Location: Holiday Inn Hotel  
Gaithersburg, MD

**Purpose:** To finalize the text for the draft of the forthcoming American National Standards Institute (ANSI) standard Data Format for the Interchange of Fingerprint Information.

**Topics:** Review of past workshops, current status of the draft standard, finalization of the draft text, current status of the FBI's ITN and IAFIS systems.

**Format:** Workshop.

**Audience:** Law enforcement agencies, vendors, consultants.

**Sponsors:** NIST.

**Contact:** Dana Grubb, A61 Technology Building, NIST, Gaithersburg, MD 20899, 301/975-2915.