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**DEPARTMENT OF COMMERCE**  
**BUREAU OF STANDARDS**  
**George K. Burgess, Director**

**RELATIONS BETWEEN THE  
TEMPERATURES, PRESSURES,  
AND DENSITIES OF GASES**

**CIRCULAR OF THE BUREAU OF STANDARDS, No. 279**

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THE TEMPERATURES, PRESSURES, AND  
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# RELATIONS BETWEEN THE TEMPERATURES PRESSURES, AND DENSITIES OF GASES<sup>1</sup>

## ABSTRACT

The attempt has been made, in discussing the relations between the temperatures, pressures, volumes, and weights of gases, to derive the formulas in a simple manner with the minimum requirements of theoretical knowledge on the part of the reader. The experimental data involving high pressures are presented in such a form that problems of this nature can be easily solved by introducing factors taken directly from curves. The significance of the equations of state of van der Waals, of Dieterici, and of Berthelot are discussed, and the manner in which these equations may be used to predict compressibilities is explained in detail. Comparisons of the calculated values with the experimental data for various gases are shown by means of a series of curves. There is included a rather extensive bibliography of the literature pertaining to the subjects herein discussed, together with a number of tables of conversion factors and equivalents.

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<sup>1</sup> Prepared by S. F. Pickering, associate chemist, Bureau of Standards of the Department of Commerce, Washington.

## I. INTRODUCTION

That the calculations of the relations involving the temperatures, pressures, and volumes of gases, particularly where high pressures are concerned, are not without their difficulties is apparent from the large number of requests for such information which have been received by this bureau. These difficulties, no doubt, find their explanation, to a large extent, in the comparative lack of simple yet complete discussions of the subject. This is especially true with regard to compressed gases, for, although many data upon them have been published, they have been presented by so many different observers in so many different forms that the application of the results by the average user has been rendered especially difficult.

The primary purpose of this circular, therefore, is to show in as simple a manner as possible the methods by which these relations may be computed and to present the necessary experimental data in such a way that they can be directly and easily used for solving practical problems.

A survey of the literature revealed that information is lacking for several important gases under high pressures, which fact suggested the question as to how accurate are various equations of state for predicting compressibilities. A complete discussion of this subject, of course, would be of prohibitive length, but it did seem feasible to compare with existing data several of the best known equations in order that some idea of their reliability in this respect could be obtained. While these equations have been considered in detail in many textbooks, there have been very few discussions in which it is shown how to use them in making actual calculations.

For several of the important gases charts have been prepared showing the volumes of gases delivered from cylinders of the compressed gas when the gauge pressure and temperature are known.

Miscellaneous tables of constants and conversion factors, together with a bibliography, complete this paper, which, it is hoped, will be of service to many who have had difficulty with the subjects herein discussed.

The author is indebted to E. R. Weaver for his many valuable suggestions.

## II. CALCULATIONS INVOLVING THE RELATIONS BETWEEN THE TEMPERATURES, PRESSURES, VOLUMES, AND WEIGHTS OF GASES

### 1. SIMPLE LAWS

Unlike a solid or liquid, any amount of gas completely fills the space in which it is confined, and the pressure which it exerts upon the confining walls depends upon the temperature. A quantity of gas can not, therefore, be specified in terms of volume only; all

three factors—volume, temperature, and pressure—are of equal importance and must always be stated unless those not stated are certainly understood.

The relations between these three factors are expressed by means of the following equation,

$$pv = kT \quad (1)$$

in which  $p$ ,  $v$ , and  $T$  represent simultaneous values of the pressure, volume, and absolute temperature of any definite quantity of gas, while  $k$  is a constant, the numerical value of which depends upon the quantity of gas considered and the units in which pressure, volume, and temperature are measured. This equation means that whatever one does to two of the three conditions—volume, temperature, and pressure—the third condition automatically varies in such a way that the equation is still true.

The significance of the absolute temperature is as follows: When the pressure remains constant, the volume of the gas varies directly as the temperature measured from a certain point called the absolute zero. This absolute zero is  $-273.1^{\circ}$  C. (or  $-459.6^{\circ}$  F.). In other words, if the temperature of a gas is changed from  $0^{\circ}$  C. to  $1^{\circ}$  C., its volume is increased by one two-hundred and seventy-third of its volume at  $0^{\circ}$  C. (If the increase in temperature is from  $0^{\circ}$  F. to  $1^{\circ}$  F., the increase in volume is one four-hundred and sixtieth of its volume at  $0^{\circ}$  F.). Similarly, if the temperature of the gas is increased from  $100$  to  $101^{\circ}$  C., the volume is increased by one three-hundred and seventy-third of its volume at  $100^{\circ}$  C.

Since zero points on the centigrade scale and on the Fahrenheit scale are  $273.1^{\circ}$  C. and  $459.6^{\circ}$  F., respectively, above the fixed absolute zero point (which is the same for both scales), the corresponding absolute temperatures are obtained by adding  $273.1^{\circ}$  to the temperature measured in degrees centigrade, or  $459.6^{\circ}$  to the temperature measured in degrees Fahrenheit. Inasmuch as the volumes and absolute temperatures are directly proportional, the ratio of the volumes of a definite quantity of a gas at constant pressure is equal to the ratio of the absolute temperatures of the gas. Similarly, the ratio of the absolute temperatures is equal to the ratio of the pressures at constant volume.

While the behavior of gases at atmospheric pressure closely approximates that represented by equation (1), the relation is not exact. The expansion of air, for example, is nearer one two-hundred and seventy-second of its volume at  $0^{\circ}$  C. per degree. For most practical purposes, however, such errors may be neglected.

For several reasons, it is generally convenient to make measurements or comparisons of quantities of gas in terms of the volume occupied under definite conditions of temperature and pressure

rather than to fix the volume and measure quantity in units of pressure or temperature; when it is not possible to measure the volume under the chosen conditions, it is necessary to make corrections to determine what volume would be occupied under those conditions.

Ordinarily, "standard conditions" of temperature and pressure are chosen for the measurement of gas volume; for scientific work in which the metric system is employed the standard conditions generally chosen are 0° C. and 760 mm (29.92 inches) of mercury (at 0° C.)<sup>2</sup> pressure,<sup>3</sup> which is called 1 atmosphere.

In the manufactured fuel-gas industry 60° F. and 30 inches (762.0 mm) of mercury pressure are usually chosen. In other commercial and engineering work in this country 68 and 70° F. are in general use as standard temperatures, with a growing tendency to agree upon 68° F. (20° C.), which is also coming into use in scientific work.

From equation (1) it follows that

$$\frac{p_1 v_1}{T_1} = k = \frac{p_2 v_2}{T_2}$$

where  $p_1$ ,  $v_1$ ,  $T_1$ , and  $p_2$ ,  $v_2$ ,  $T_2$ , represent two sets of conditions of pressure, volume, and absolute temperature of the same quantity of gas. Hence

$$v_2 = v_1 \frac{p_1 T_2}{p_2 T_1} \quad (2)$$

If the temperatures are measured in degrees centigrade, equation (2) becomes

$$v_2 = v_1 \frac{p_1 (273.1 + t_2)}{p_2 (273.1 + t_1)} \quad (3)$$

If measured in degrees Fahrenheit, it becomes

$$v_2 = v_1 \frac{p_1 (459.6 + t_2)}{p_2 (459.6 + t_1)} \quad (4)$$

In these equations and subsequently throughout this circular,  $T$ , with or without subscript, is used to denote absolute temperature (on the centigrade scale unless otherwise stated), while  $t$  denotes temperature measured from the centigrade or Fahrenheit zero.

The foregoing equations are sufficient for making the usual conversions of volumes from one set of conditions to another, but do not show the relations connecting volumes and weights of gases.

<sup>2</sup> In this paper the height of a mercury column when used to indicate a pressure will always refer to the height at 0° C.

<sup>3</sup> An exact definition of pressure must include the value of the acceleration of gravity, which is slightly different at different places on the earth's surface. In this paper the value 980.665 cm per second per second agreed upon by the International Conference on Weights and Measures for the acceleration of gravity is used. (Trav. et Mem. Bur. Int. Third Gen. Conference p. 66; 1902.) In commercial work with gases and in all except the most exact scientific work the differences in the acceleration of gravity at different places are negligible.

If now we consider weights of different gases proportional to their respective molecular weights, a new relation of the greatest importance develops: *The value of the constant in equation (1) is the same for each gas.* In scientific work it is customary to use, as the unit of quantity, the number of grams of gas equal to the molecular weight. This unit is called the mol; and when 1 mol is the quantity of gas considered, the resulting value of  $k$  is given the special designation  $R$ . The constant  $R$  so defined is one of the most important constants employed in physical and chemical science. It is commonly called "the gas constant," and will be used very frequently in this circular.

TABLE 1.—Values of "the gas constant  $R$ " corresponding to different systems of units of temperature, pressure, and volume

[ $R$  is defined by the equation  $pv = NRT$ , in which the mol is the unit of quantity of gas]

Units employed			Numerical value of $R$
Absolute temperature	Pressure	Volume	
°C. +273.1	Atmosphere	Liter	0.08206
°C. +273.1	mm of mercury	do	62.37
°C. +273.1	Gram per cm <sup>2</sup>	do	84.79
°C. +273.1	Megabar	do	.08315
°C. +273.1	Atmosphere	Cubic feet	.002898
°C. +273.1	mm of mercury	do	2.2024
°C. +273.1	Inches of mercury	do	.08671
°C. +273.1	Pounds per in. <sup>2</sup>	do	.04259
°F. +459.6	Atmosphere	Liter	.04559
°F. +459.6	do	Cubic feet	.001610
°F. +459.6	mm of mercury	do	1.2236
°F. +459.6	Inches of mercury	do	<del>.0457</del> 0.4217
°F. +459.6	Pounds per in. <sup>2</sup>	do	.02366

When the mol is employed as the unit of quantity, equation (1) becomes

$$pv = NRT \tag{5}$$

in which  $N$  represents the number of mols in the quantity of gas under consideration. The numerical value of  $R$  depends upon the units in which pressure, volume, and temperature are expressed. Table 1 gives values of  $R$  in the different systems of units in common use in both scientific and commercial work. (The cubic centimeter and the cubic meter in which volumes of gas are frequently measured are respectively, one one-thousandth of and one thousand times the liter.)

By the use of equation (5), Table 1, and a table of molecular weights which will be found on page 60, the solution of any problem involving volumes, temperatures, pressures, and weights of gases is very simple, including problems requiring conversion from one set of

units to another. For the purpose of solving various types of problems equation (5) may be put in the following forms:

$$v = \frac{NR T}{p} \quad (6)$$

$$N = \frac{pv}{RT} \quad (7)$$

$$\frac{p_1 v_1}{R_1 T_1} = \frac{p_2 v_2}{R_2 T_2} \text{ or } v_2 = v_1 \frac{p_1 R_2 T_2}{p_2 R_1 T_1} \quad (8)$$

In equation (8),  $v_1$  represents the volume of any definite quantity of gas at pressure  $p_1$ , and absolute temperature  $T_1$ ;  $v_2$  represents the volume of the same quantity of gas at pressure  $p_2$  and absolute temperature  $T_2$ , as in equation (2); and  $R_1$  and  $R_2$  represent the numerical values of the gas constant corresponding to the respective systems of units employed. If the same system of units is used in both gas measurements,  $R_1$  and  $R_2$  are identical and are eliminated from the equation which becomes identical with equation (2)

$$\frac{p_1 v_1}{T_1} = \frac{p_2 v_2}{T_2} \text{ or } v_2 = v_1 \frac{p_1 T_2}{p_2 T_1}$$

The use of these equations is illustrated by the following problems:

**PROBLEM 1.**—What volume in cubic feet will 900 g of oxygen occupy at a temperature of 82° F. and a pressure of 23 pounds per square inch?

*Solution.*—The molecular weight of oxygen is 32. The value of  $N$  is, therefore,  $\frac{900}{32}$ ; the value of  $R$  for the system of units chosen is 0.02366 and we can, therefore, substitute at once in equation (6)

$$v = \frac{900}{32} \times \frac{0.02366 (82 + 459.6)}{23} = 15.76 \text{ cubic feet}$$

**PROBLEM 2.**—What would be the weight in pounds of 85 cubic meters of nitrogen at 27° C. and 740 mm pressure?

*Solution.*—Substituting in equation (7)

$$N = \frac{740 \times 85 \text{ 000}}{62.37 \times (27 + 273.1)} = 3358 \text{ mols}$$

The molecular weight of nitrogen is 28, and 1 pound corresponds to 453.6 g, hence the weight in pounds,  $w$ , of 3358 mols of nitrogen is

$$w = \frac{28 \times 3358}{453.6} = 207 \text{ pounds}$$

**PROBLEM 3.**—A certain quantity of hydrogen at 80° F. and 150 lbs./in.<sup>2</sup> occupies 1.3 cubic feet. What will be its volume in liters at 15° C. and a pressure of 1.8 atmospheres?

*Solution.*—Substitute in equation (8)

$$v_2 = 1.3 \times \frac{150 \times 0.08206 (15 + 273.1)}{1.8 \times 0.02366 (80 + 459.6)} = 201 \text{ liters}$$

**PROBLEM 4.**—A quantity of gas occupies 8,800 cubic feet at 55° F. and a pressure of 28 inches of mercury. What volume will it occupy at 60° F. and 30 inches of mercury?

*Solution.*—Substitute in equation (2).

$$v_2 = 8,800 \times \frac{28 (60 + 459.6)}{30 (55 + 459.6)} = 8,300 \text{ cubic feet}$$

## 2. MIXTURES OF GASES; VAPOR PRESSURE AND THE EFFECT OF VAPOR PRESSURE UPON THE MEASUREMENT OF GAS

It was pointed out on page 2 that any quantity of gas completely fills the space in which it is confined and exerts a pressure upon the confining walls. If an additional quantity of the same gas is added, it has been shown in the discussion of the simple gas laws that the pressure is increased in direct proportion to the quantity added. The simplest way to look at this fact is to regard the pressure exerted by each portion of the total quantity of gas as independent of the presence of the remainder. This relation is equally true in case the second portion of gas introduced into the space has a different chemical composition from the first (Dalton's law) provided, of course, the two gases do not react chemically.

If a volatile liquid is introduced into a confined space, a portion of it evaporates (becomes gas) and exerts a pressure on the confining walls just as any other portion of gas does. The amount which evaporates and the pressure which it exerts are independent of the presence of any other gas in the space. If there is enough liquid present so that it does not all evaporate and if enough time is allowed for equilibrium to be reached, the pressure exerted is independent of the volume of space occupied and of the amount of liquid left unevaporated; but it does depend upon the temperature. For each volatile liquid there is therefore a definite saturation pressure or vapor pressure (both terms are widely used in technical literature) corresponding to every temperature. The phenomenon of vapor pressure is not confined to liquids. Many solids have appreciable vapor pressures at ordinary temperatures (witness naphthalene, which causes so much trouble for the gas companies), and almost all substances at sufficiently high temperatures have vapor pressures which

can be detected. By a volatile substance we mean one which has an appreciable vapor pressure at the temperature considered.

When any quantity of gas is in contact with a volatile substance, the measured pressure is the sum of the pressure exerted by the gas and the vapor pressure of the volatile material. Assuming no change of temperature, this vapor pressure remains constant no matter how we change the total pressure. Hence for purposes of volume conversion the saturated gas may be considered as a dry gas, the pressure of which is the partial pressure of the gas, or its equivalent, the difference between the total pressure and the saturated vapor pressure of the volatile material.

If, for example, a gas is in contact with water at 30° C., the partial pressure of the water vapor is 31.86 mm of mercury or 0.0419 atmosphere; and assuming the total pressure to be 1 atmosphere, the partial pressure of the gas would be 0.9581 atmosphere. Upon being compressed to 2 atmospheres (the temperature remaining constant), half of the water vapor would be condensed (neglecting any deviations from the simple gas law), thus maintaining the partial pressure of the water vapor at 0.0419 atmosphere, while the partial pressure of the gas would become 1.9581 atmospheres. Upon expansion at constant temperature (still in contact with the water) water would evaporate until the partial pressure of the water vapor became equal to 0.0419 atmosphere, as before.

Whatever changes of pressure, temperature, and volume take place, the gas (as distinguished from the vapor which varies in quantity) behaves in accordance with the simple gas laws already stated, and these laws may be accordingly modified to include vapors by making the simple substitution

$$P = w + p \quad \text{or} \quad p = P - w$$

in which  $P$  is the total pressure exerted on the walls of the confining space,  $p$  is the partial pressure of the gas, and  $w$  is the vapor pressure of the liquid.

Replacing  $p_1$  in equations (2), (3), and (4) by the value for its partial pressure, namely,  $P_1 - w_1$ , gives the corresponding equations, which can be used for converting from the saturated to the standard dry basis. These equations are

$$v_2 = v_1 \frac{(P_1 - w_1) T_2}{p_2 T_1} \quad (9)$$

$$v_2 = v_1 \frac{(P_1 - w_1) (273.1 + t_2)}{p_2 (273.1 + t_1)} \quad (10)$$

$$v_2 = v_1 \frac{(P_1 - w_1) (459.6 + t_2)}{p_2 (459.6 + t_1)} \quad (11)$$

where  $w_1$  is the saturated pressure of the vapor at temperature  $t_1$ .

For conversions to a standard saturated basis the term  $p_2$  in the above equations is replaced by the value for its partial pressure, namely,  $P_2 - w_2$ , where  $w_2$  is the saturated pressure of the vapor at temperature  $t_2$ . The equations then become

$$v_2 = v_1 \frac{(P_1 - w_1) T_2}{(P_2 - w_2) T_1} \tag{12}$$

$$v_2 = v_1 \frac{(P_1 - w_1) (273.1 + t_2)}{(P_2 - w_2) (273.1 + t_1)} \tag{13}$$

$$v_2 = v_1 \frac{(P_1 - w_1) (459.6 + t_2)}{(P_2 - w_2) (459.6 + t_1)} \tag{14}$$

The following problems illustrate the use of the above equations:

**PROBLEM 1.**—The volume of a gas saturated with water vapor measured at a pressure of 741.6 mm of mercury and at 25° C. is 74.69 liters. What would be the volume of the dry gas at 760.0 mm and at 0° C.?

*Solution.*—From table 12, page 58, the vapor pressure of water at 25° C. is 23.8 mm.

Substituting in equation (10)

$$v_2 = 74.69 \frac{(741.6 - 23.8) (273.1 + 0.0)}{760.0 (273.1 + 25.0)} = 64.61 \text{ liters.}$$

**PROBLEM 2.**—The volume of a gas measured with a wet meter is 432.7 cubic feet. The pressure is 29.67 inches of mercury and the temperature is 86° F. What volume would the saturated gas occupy at a pressure of 30 inches and 68° F.?

*Solution.*—From the table the vapor pressure of water is found to be 1.25 inches at 86° F. and 0.69 inch at 68° F.

Substituting in equation (14)

$$v_2 = 432.7 \frac{(29.67 - 1.25) (459.6 + 68.0)}{(30.00 - 0.69) (459.6 + 86.0)} = 405.8 \text{ cubic feet.}$$

Equations (6), (7), and (8) may likewise be modified by substituting  $P_1 - w_1$  and  $P_2 - w_2$  for  $p_1$  and  $p_2$ .

### 3. VOLUME CONVERSIONS INVOLVING HIGH PRESSURES

In the measurement of gases at high pressures, for example, compressed oxygen or hydrogen as they are ordinarily sold on the market, the foregoing equations are inadequate; for such a pressure range (2,000 lbs./in.<sup>2</sup>) the quantity  $pv$  is no longer constant at constant temperature, but varies with the pressure by amounts which differ for each gas. Consequently the relation

$$\frac{p_1 v_1}{T_1} = \frac{p_2 v_2}{T_2}$$

is no longer true.

In Figures 1 to 8 the values of  $\frac{273.1}{T} pv$  are plotted against the pressure. These figures contain nearly all of the published data in this range of temperature and pressure, and the isothermals are drawn according to what appear to be the most probable values. This quantity  $\frac{273.1}{T} pv$  is called the factor ( $F$ ) and is discussed in the following paragraphs.

Let us consider for the time being the  $0^\circ$  C. isothermals only. These are plotted on the basis of  $pv$  at  $0^\circ$  C. and 1 atmosphere as being unity. Hence, the value of the factor for any pressure as given by the curve will represent the ratio of the value of  $pv$  at this pressure to the value of  $pv$  at 1 atmosphere; that is,

$$\frac{(pv)_n}{(pv)_1} = F_n$$

where  $F_n$  is the factor from the curve for  $n$  atmospheres. This relation, of course, holds for all pressures, therefore,

$$\frac{(pv)_n}{(pv)_m} = \frac{F_n}{F_m}$$

$$v_m = v_n \frac{P_n}{P_m} \frac{F_m}{F_n}$$

In other words, the corrections are made as though the substance behaved as a perfect gas, and the result is then multiplied by the ratio of the factor at the desired pressure to the factor at the measured pressure.

Suppose, for example, a cylinder whose volume is 1.372 cubic feet contains oxygen at 120 atmospheres ( $0^\circ$  C.) and it is desired to calculate the volume occupied by the gas at 30 atmospheres ( $0^\circ$  C.).

From Figure 8,

$$F_{120} = 0.9140 \text{ and } F_{30} = 0.9735$$

Hence,

$$v_{30 \text{ atm.}} = 1.372 \frac{120}{30} \frac{0.9735}{0.9140} = 5.85$$

The desired volume is, therefore, 5.85 cubic feet.

The volume occupied by the gas at 1 atmosphere ( $0^\circ$  C.) would be

$$v_{1 \text{ atm.}} = 1.372 \frac{120}{1} \frac{1.0000}{0.9140} = 180.2 \text{ cubic feet.}$$

Inasmuch as the volume varies directly with the absolute temperature at a constant pressure of 1 atmosphere, the value for  $pv$  at  $100^\circ$  C. and 1 atmosphere would be 1.366 (approximately). If this isothermal were to be placed on the same chart with the  $0^\circ$  C. isothermal,

the large range covered by  $pv$  ordinate would make it difficult to read variations in the values of  $pv$  for a given temperature with any degree of accuracy. By multiplying the  $pv$  values at each temperature  $T$  ( $^{\circ}\text{C. absolute}$ ) by  $\frac{273.1}{T}$ , however, this major temperature effect is eliminated, leaving only the deviations from the simple gas law.

Since

$$F = pv \frac{273.1}{T}$$

then

$$pv = F \frac{T}{273.1}$$

Hence, the value of  $pv$  for any temperature can be obtained by multiplying the factor obtained from the curve by the quotient of the absolute temperature divided by  $273.1^{\circ}$ .

In order to use the factors directly in computing the pressure, volume, and temperature relations an equation may be derived as follows:

$$\begin{aligned} F_1 &= (p_1 v_1) \frac{273.1}{T_1} \\ F_2 &= (p_2 v_2) \frac{273.1}{T_2} \\ \frac{F_1}{F_2} &= \frac{(p_1 v_1)}{(p_2 v_2)} \frac{T_2}{T_1} \\ \therefore v_2 &= v_1 \frac{p_1}{p_2} \frac{T_2}{T_1} \frac{F_2}{F_1} = v_1 \frac{p_1 (273.1 + t_2)}{p_2 (273.1 + t_1)} \frac{F_2}{F_1} \end{aligned} \tag{15}$$

This is the general equation for converting volumes at high pressures.

If the volume at 1 atmosphere is to be calculated,  $p_2$  and  $F_2$  become equal to unity and equation (15) is reduced to

$$v_2 = v_1 p_1 \frac{(273.1 + t_2)}{(273.1 + t_1)} \frac{F_1}{F_1} \tag{16}$$

The values of  $F_1$  for temperatures intermediate between those represented by the isothermals can be approximately found by interpolation from the values of the two isothermals above and below the temperature in question, but a more accurate method consists of plotting the values at different temperatures (pressure constant) and interpolating from the curve.

The following problems will illustrate the use of equations (15) and (16):

A cylinder whose volume is 1.528 cubic feet contains hydrogen at 2,000 lbs./in.<sup>2</sup> gauge pressure, the temperature being  $87^{\circ}\text{ F.}$  What is the volume of the hydrogen at 1,400 lbs./in.<sup>2</sup> and at  $50^{\circ}\text{ F.}$ ?

For convenience in obtaining  $F_1$  and  $F_2$  it is best to convert the pressures and temperatures to atmospheres and ° C. These equivalents can be found in Tables 13 and 14.

$$2,000 \text{ lbs./in.}^2 = 137.0 \text{ atms. abs.}$$

$$1,400 \text{ lbs./in.}^2 = 96.25 \text{ atms. abs.}$$

$$87^\circ \text{ F.} = 30.6^\circ \text{ C.}$$

$$50^\circ \text{ F.} = 10^\circ \text{ C.}$$

$$F_2(96.25 \text{ atms. and } 10^\circ \text{ C.}) = 1.060.$$

$$F_1(137.0 \text{ atms. and } 30.6^\circ \text{ C.}) = 1.082.$$

Substituting in equation (15) gives

$$v_2 = 1.528 \frac{137.0}{96.25} \frac{283.1}{303.7} \frac{1.060}{1.082} = 1.988.$$

$$v_2 = 1.988 \text{ cu. ft.}$$

To find the volume at 1 atmosphere and 68° F.

$$p_2 = 1 \quad F_2 = 1 \quad 68^\circ \text{ F.} = 20^\circ \text{ C.}$$

From equation (16)

$$v_2 = 1.528 \frac{137.0}{1} \frac{293.1}{303.7} \frac{1}{1.082} = 187.0.$$

$$v_2 = 187.0 \text{ cu. ft.}$$

The volume of hydrogen delivered from the cylinder, if the final pressure in the cylinder became one atmosphere, would, of course, be 1.5 cubic feet less than the above figure because this much gas would remain in the cylinder.

The volume delivered by the cylinder would therefore be 185.5 cubic feet.

#### 4. SUMMARY OF IMPORTANT EQUATIONS.

Symbols:

$p_1, v_1, T_1$ , and  $p_2, v_2, T_2$  represent two sets of conditions of pressure, volume, and *absolute* temperature (on either the centigrade or Fahrenheit scale).

$t_1$  and  $t_2$  represent the corresponding temperatures measured in degrees centigrade or degrees Fahrenheit.

$R_1$  and  $R_2$  represent the values for the gas constant expressed in the same units as the corresponding pressure, volume, and temperature. The values for these constants can be obtained from Table 1, page 5.

$P$  is the total pressure of a mixture of gas and vapor.

$w$  is the vapor pressure of the liquid (or solid) in contact with the gas.

$F_1$  and  $F_2$  represent factors for conversions involving high pressures. These factors are obtained from Figures 1 to 8.

$$v_2 = v_1 \frac{p_1 T_2}{p_2 T_1} \quad \text{Equation (2)}$$

$$v_2 = v_1 \frac{p_1(273.1 + t_2)}{p_2(273.1 + t_1)} \quad \text{Equation (3)}$$

$t_1$  and  $t_2$  expressed in degrees centigrade

$$v_2 = v_1 \frac{p_1(459.6 + t_2)}{p_2(459.6 + t_1)} \quad \text{Equation (4)}$$

$t_1$  and  $t_2$  expressed in degrees Fahrenheit

$$N = \frac{pv}{RT} \quad \text{Equation (6)}$$

$$v_2 = v_1 \frac{p_1 R_2 T_2}{p_2 R_1 T_1} \quad \text{Equation (8)}$$

$$v_2 = v_1 \frac{(P_1 - w_1) T_2}{p_2 T_1} \quad \text{Equation (9)}$$

$$v_2 = v_1 \frac{(P_1 - w_1) T_2}{(P_2 - w_2) T_1} \quad \text{Equation (12)}$$

$$v_2 = v_1 \frac{p_1 T_2 F_2}{p_2 T_1 F_1} \quad \text{Equation (15)}$$

If  $v_2$  is to be measured at 1 atmosphere, the equation becomes

$$v_2 = v_1 p_1 \frac{T_2}{T_1 F_1} \quad \text{Equation (16)}$$

**5. CURVES SHOWING THE COMPRESSIBILITIES OF GASES (0 TO 200 ATM.)**

In Figures 1 to 8 the values of  $\frac{273.1}{T} pv$  are plotted against the pressure. These charts contain nearly all of the published data covering this range of temperature and pressure, and the curves are drawn according to what appear to be the most probable values.

**6. CHARTS SHOWING THE VOLUMES OF SEVERAL GASES DELIVERED FROM CYLINDERS CONTAINING THE GASES AT HIGH PRESSURES**

Figures 9 to 13 show the volume (measured at 68° F. and 1 atmosphere) of gas delivered from a cylinder if the pressure and temperature of the gas in the cylinder are known.

In each case the volume of the cylinder is assumed to be 1.528 cubic feet, which is the volume of the so-called "200-foot" cylinder. For a cylinder of any other capacity the volume delivered would be proportional to the volume of the cylinder. In other words, the figure obtained from the chart should be multiplied by  $\frac{V}{1.528}$  where  $V$  is the volume (in cubic feet) of the cylinder in question.

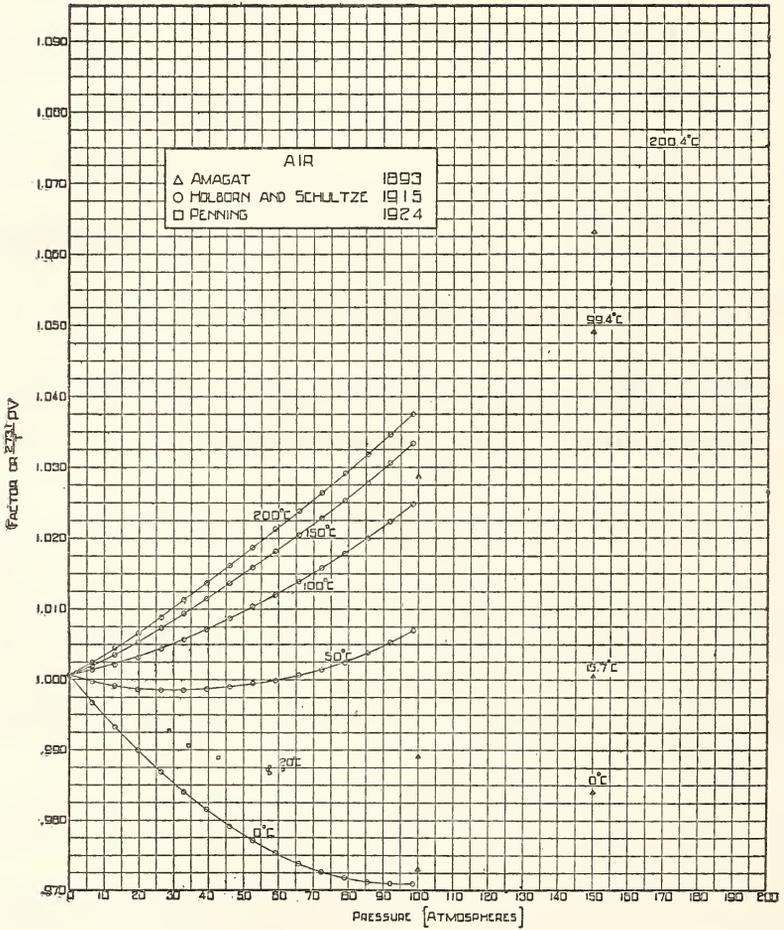


FIG. 1.—The compressibility factors for air

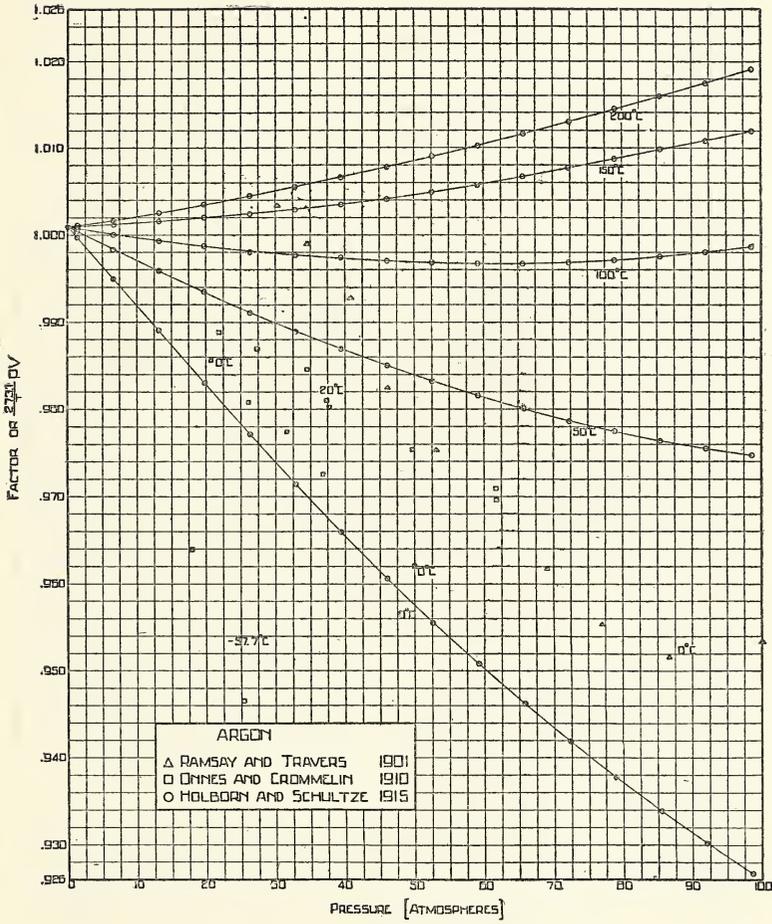


FIG. 2.—The compressibility factors for argon

53852°—26†—2

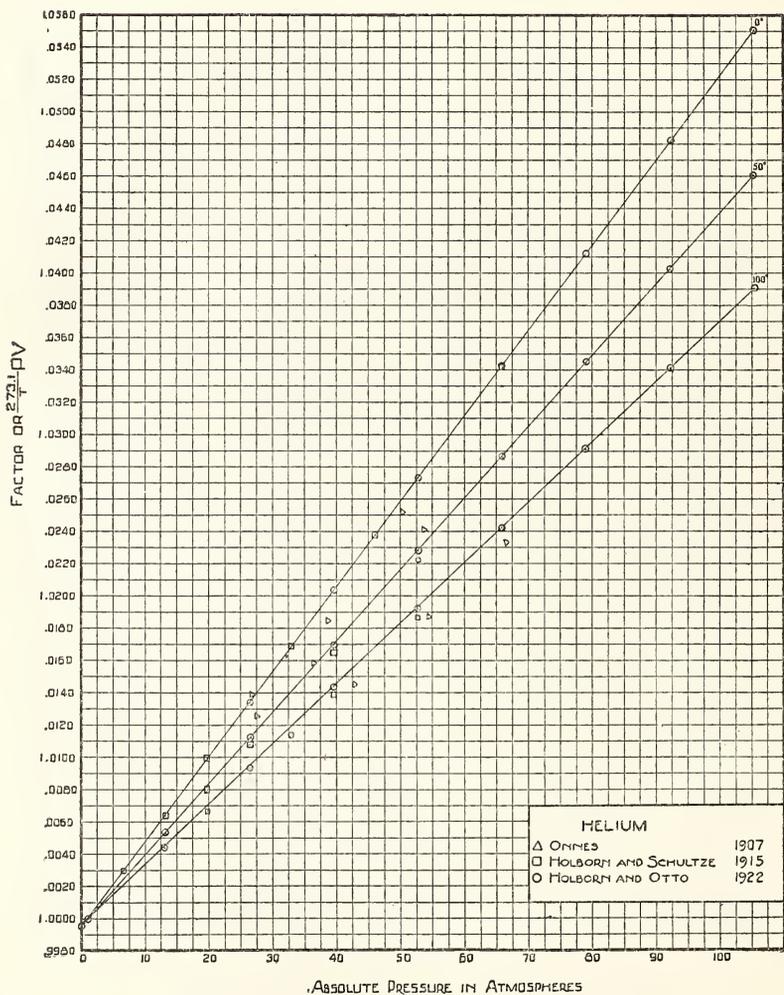


FIG. 3.—The compressibility factors for helium

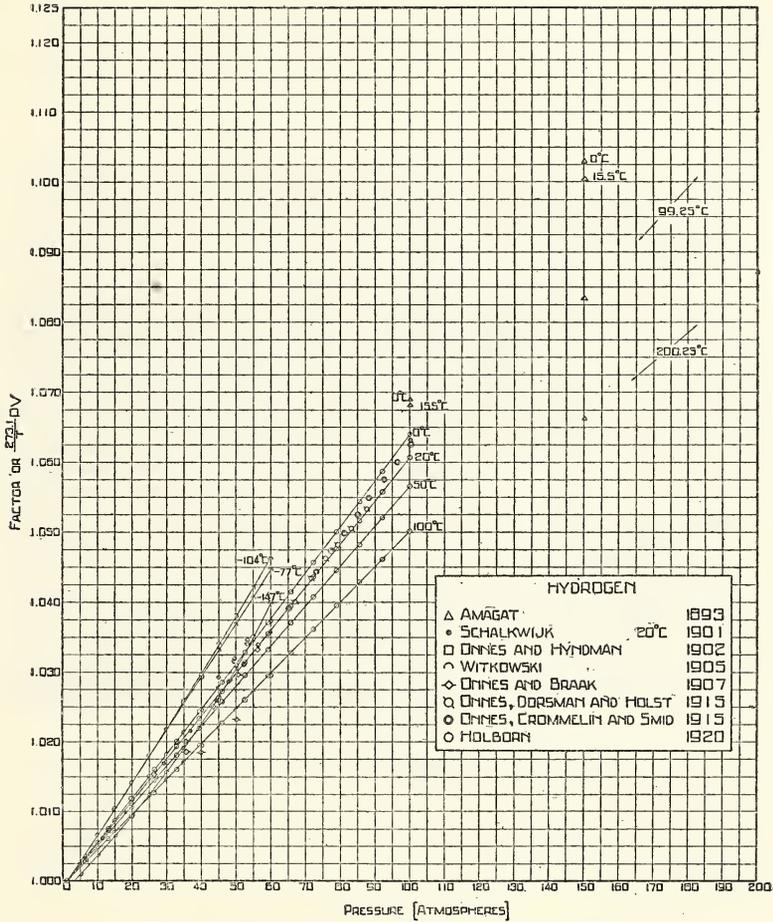


FIG. 4.—The compressibility factors for hydrogen

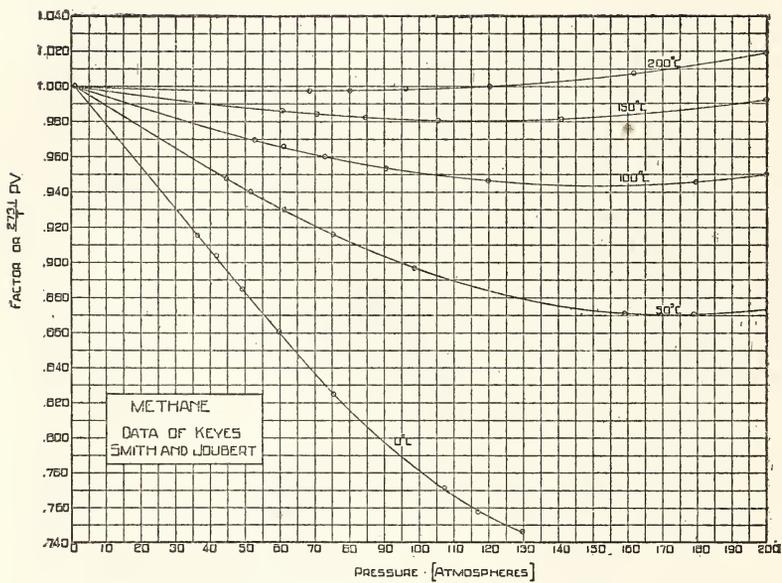


FIG. 5.—The compressibility factors for methane

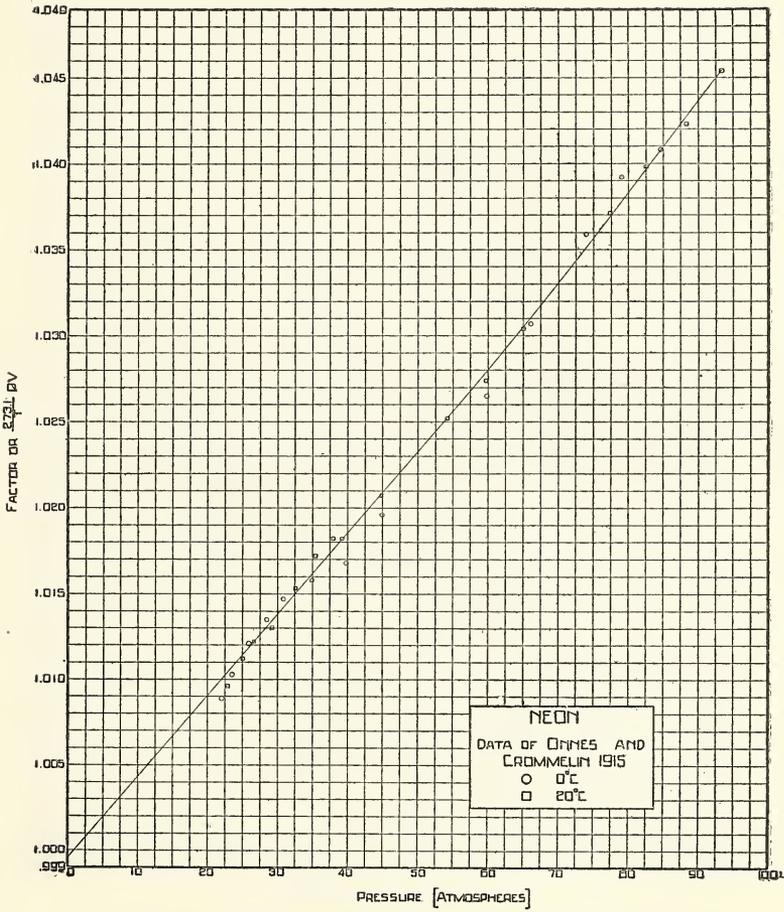


FIG. 6.—The compressibility factors for neon

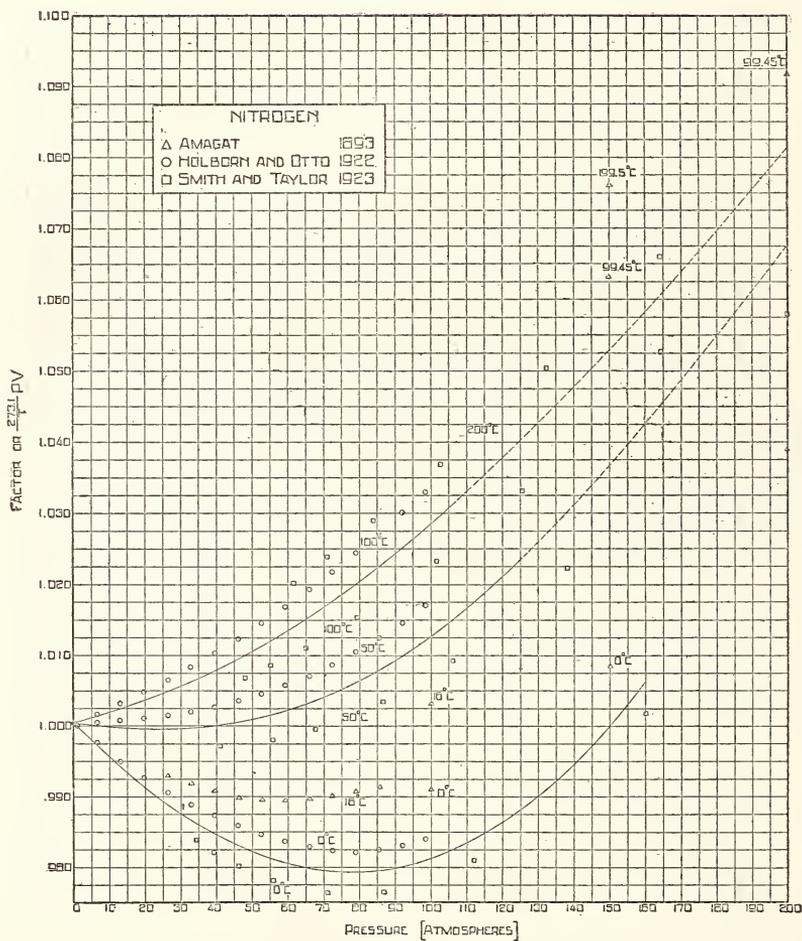


FIG. 7.—The compressibility factors for nitrogen

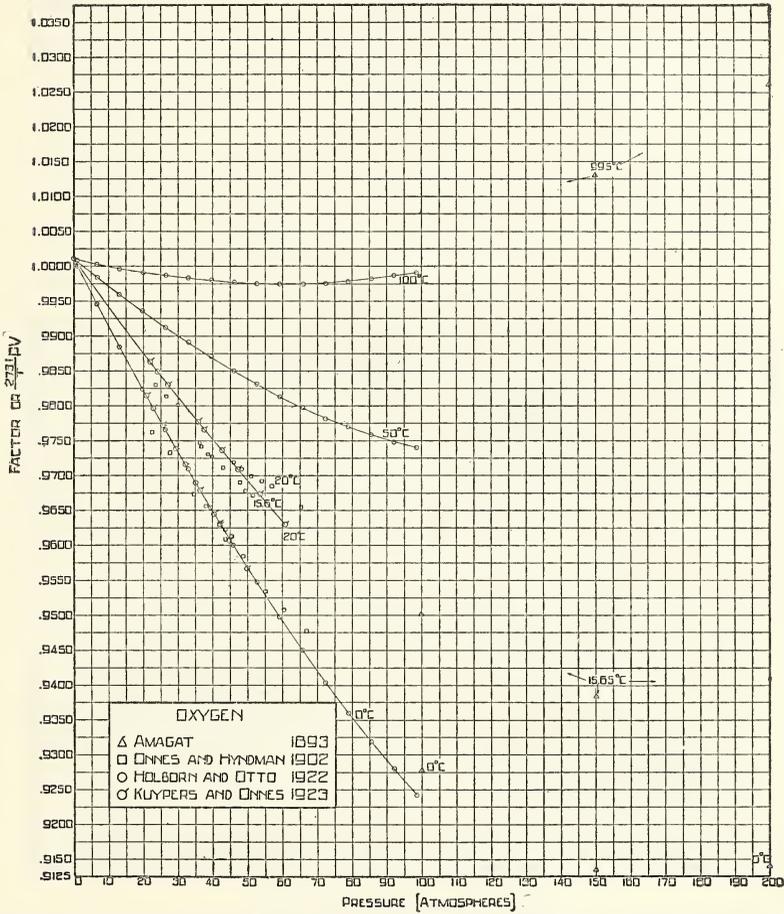


FIG. 8.—The compressibility factors for oxygen

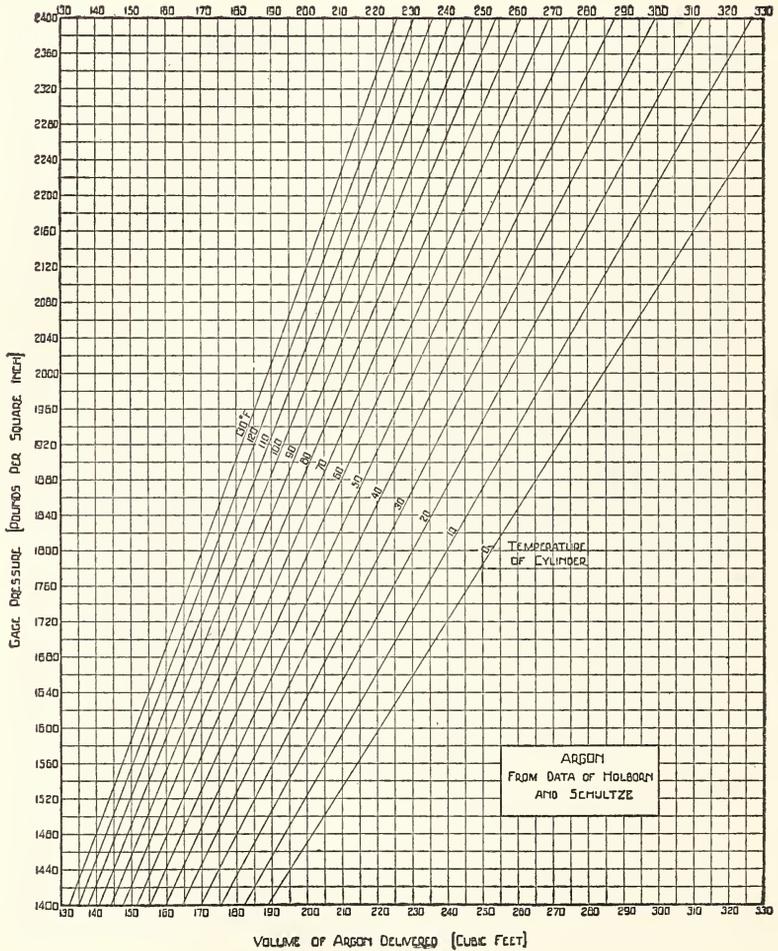


FIG. 9.—Chart showing volume of argon (measured at 1 atm. and 68° F.) delivered from a cylinder whose volume is 1.528 cubic feet

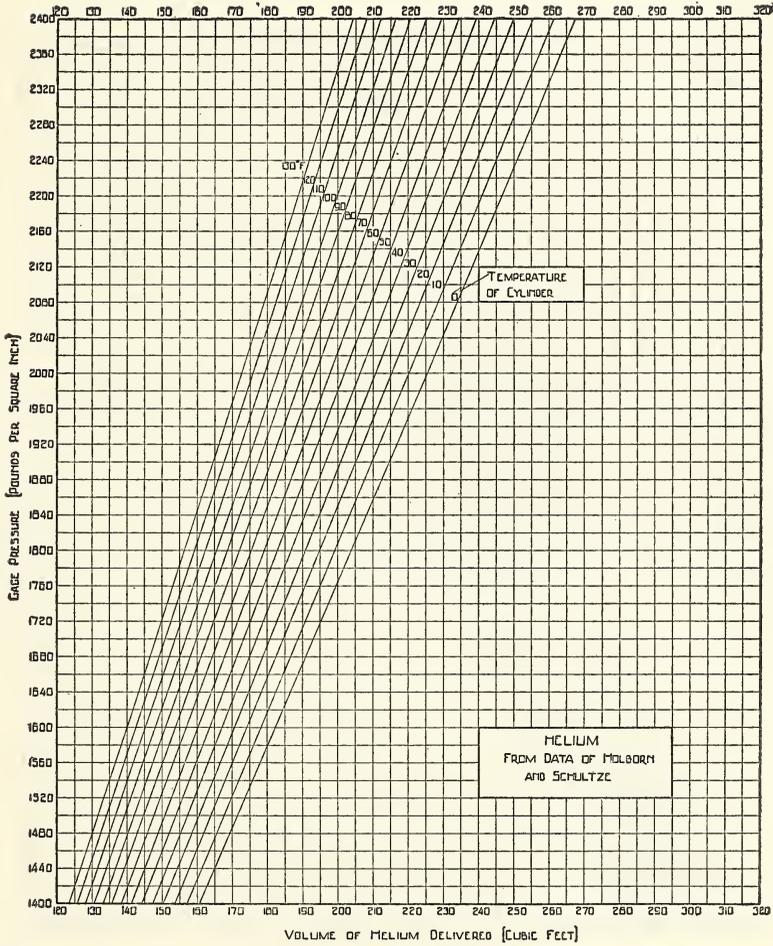


Fig. 10.—Chart showing volume of helium (measured at 1 atm. and 68° F.) delivered from a cylinder whose volume is 1.528 cubic feet

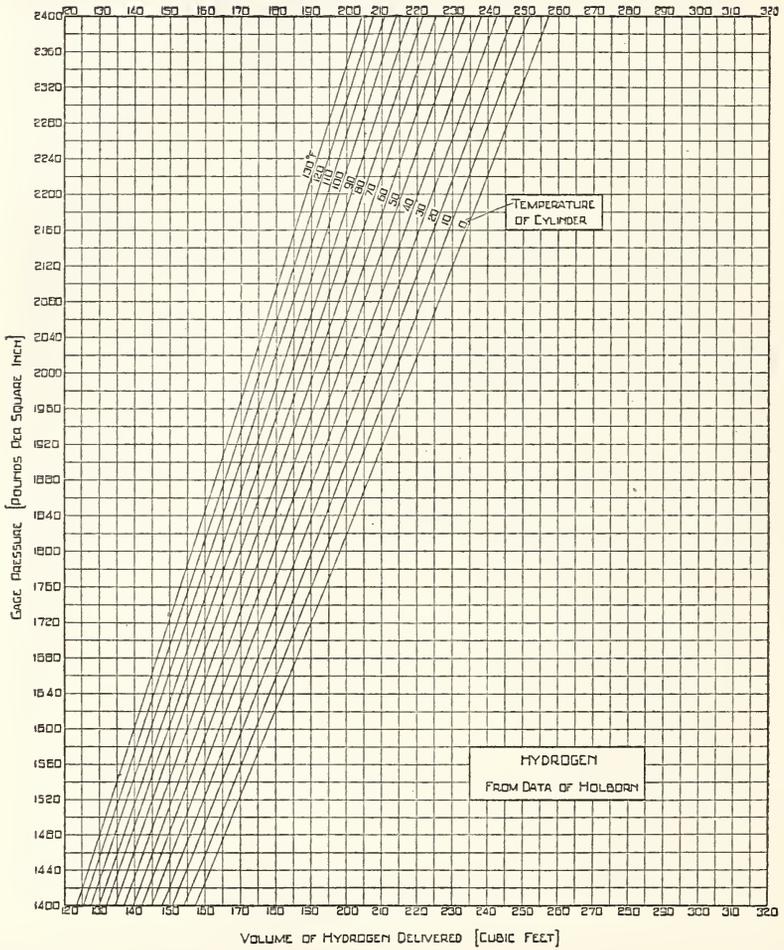


FIG. 11.—Chart showing the volume of hydrogen (measured at 1 atm. and 68° F.) delivered from a cylinder whose volume is 1.523 cubic feet

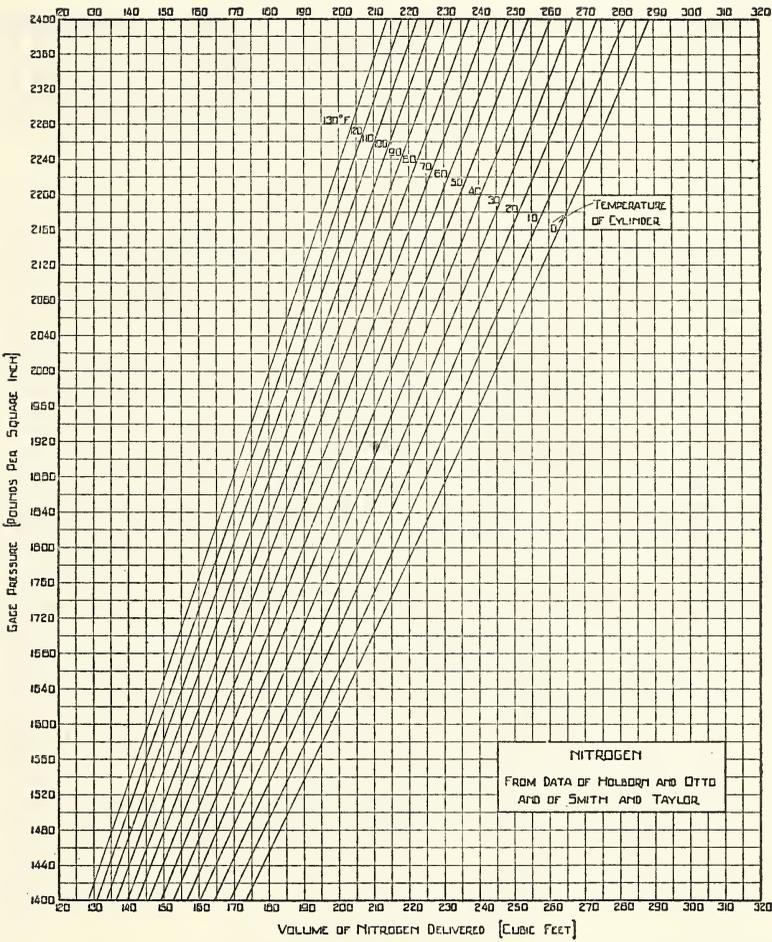


FIG. 12.—Chart showing volume of nitrogen (measured at 1 atm. and 68° F.) delivered from a cylinder whose volume is 1.528 cubic feet

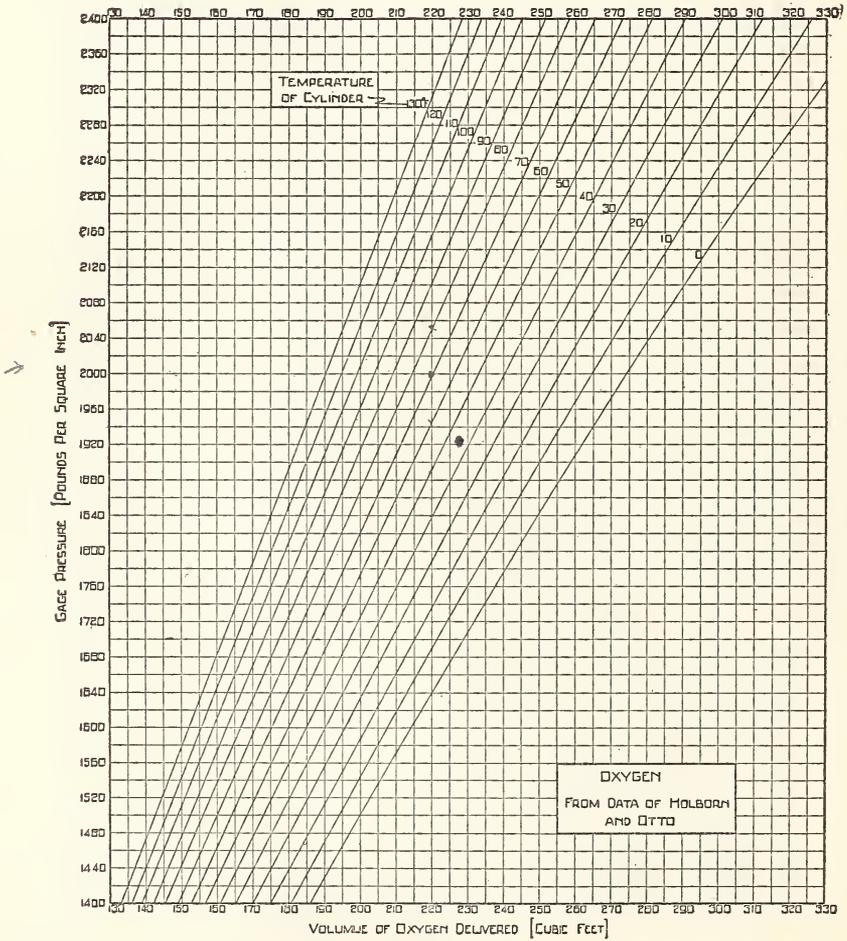


FIG. 13.—Chart showing volume of oxygen (measured at 1 atm. and 68° F.) delivered from a cylinder whose volume is 1.528 cubic feet

## III. EQUATIONS OF STATE

## 1. SIMPLE LAWS

The pressure exerted by a gas on the walls of a container is explained by the kinetic theory as being due to the bombardment of the walls by the moving molecules of the gas. The velocities with which these molecules move are very large (the average velocity of the hydrogen molecules at 0° C. is about 1 mile per second) and become greater as the temperature is increased.

The general relations involving the temperature, pressure, and volume of a gas are expressed in the following well-known gas law:

$$pv = NRT \quad (17)$$

where  $p$ ,  $v$ , and  $T$  represent the pressure, volume, and absolute temperature, respectively;  $R$  stands for a constant, which is the same for all gases; and  $N$  is the number of gram molecules of gas under consideration. A weight of a gas in grams numerically equal to the molecular weight is called a gram molecule of the gas (or mol). The derivation of the above relation can be found in most textbooks of physical chemistry and hence is not included in this paper.

This law is taken as part of the criteria of a perfect gas. The product of the pressure and volume of such a gas at constant temperature would be a constant at all pressures, while the expansion at either constant volume or constant pressure would be directly proportional to the temperature.

None of the actual gases, however, obey this law; although for most practical purposes nearly all of the common gases may be considered as ideal at or below atmospheric pressure and at temperatures reasonably higher than the condensation temperature. Ordinary corrections for temperature and pressure, for instance those which arise in measuring volumes of gases at normal room conditions, can be made without appreciable error. Such means of correction, however, can not be used when it is desired to know the volume of gas contained in a cylinder where the pressure may be around 1,800 lbs/in.<sup>2</sup> or more. In such a case the product  $pv$  is no longer constant at different pressures, but may vary by 8 or 10 per cent.

It, therefore, becomes necessary either to use experimental data for making such calculations or to apply some equation which will predict with reasonable accuracy the behavior of a gas for which no compressibility data have been obtained.

The ideal gas law as derived involves the assumptions that there are no attractive forces between the molecules, and that the molecules themselves are mere points having no real volume. Since both of these assumptions are erroneous, it could hardly be expected that an equation based upon them would be accurate.

Over 100 equations of state, theoretical and empirical, have been devised to include these factors; but so far no satisfactory equation of general application has been presented whose constants are not empirical, thus requiring experimental data which it was desired to predict.

Fairly good approximations, however, are given by a few of the general equations, three of which will be considered here, namely, those of van der Waals, Dieterici, and Berthelot.

## 2. EQUATION OF VAN DER WAALS

Van der Waals, in taking into account the cohesive force between molecules, assumed that this force is proportional to the product of the masses of each volume element, this product being in turn proportional to the product of the densities. In the case of a pure gas the force would be proportional to the square of the densities or inversely proportional to the square of the volume. Inasmuch as this cohesive force diminishes the actual measured pressure, the theoretical pressure  $P$  in equation (17) is replaced by the term  $\left(p + \frac{a}{v^2}\right)$ .

The actual free space for expansion of the gas would be the total volume less the volume of the molecules themselves, represented by  $(b)$  so that the term  $v$  in equation (17) is replaced by the term  $(v-b)$ .

The equation of van der Waals, then, is

$$\left(p + \frac{a}{v^2}\right)(v-b) = NRT \quad (18)$$

where  $(a)$  and  $(b)$  are constants which are characteristic of each gas.

These constants can be evaluated in terms of the critical constants of the gas by introducing certain existing conditions at the critical point.<sup>4</sup> These relations are as follows:

$$a = \frac{27 N^2 R^2 T_c^2}{64 P_c} \quad (19)$$

$$b = \frac{NRT_c}{8P_c} \quad (20)$$

or

$$a = \frac{27 NRT_c}{8} b \quad (21)$$

In these equations  $T_c$  and  $P_c$  represent critical temperature and pressure, respectively.

These relations have been derived with the elimination of the critical volume, for there is difficulty in accurately determining this quantity.

<sup>4</sup> This derivation is given in many textbooks of physical chemistry, such as that of W. C. McC. Lewis, 1, p. 75.

Equation (18) can be more easily used for such computations by changing its form somewhat. Transposing, the equation gives

$$p = \frac{NRT}{v-b} - \frac{a}{v^2} \tag{22}$$

multiplying both sides by  $v$

$$pv = \frac{NRT}{1 - \frac{b}{v}} - \frac{a}{v}$$

Perhaps the most confusing difficulty connected with the use of the equations of state is the selection of proper units for the various terms in the equation. In some cases the values of ( $a$ ) and ( $b$ ) are given in tables of constants without indicating the units used. The empirical values for these constants are obtained by choosing two points on an isotherm and solving for the constants, and it is obvious that the shape of the curve obtained will depend upon the particular fixed points chosen.

In computing the curves of the three equations of state as shown in Figures 14 to 22, the value of  $pv$  at 0 atmosphere pressure and 0° C. is taken as unity. Since  $v$  becomes infinite

$$p_0 v_\infty = \frac{NRT_0}{1 - \frac{b}{\infty}} - \frac{a}{\infty} = NRT_0 = 1$$

that is, the gas acts as a perfect gas when

$$p = 0$$

It follows that when  $p_0 v_\infty = 1$

$$NR = \frac{1}{T_0} = \frac{1}{273.1}$$

and equations (20) and (19) become

$$b = \frac{T_0}{(273.1)8P_c}, a = \frac{27T_c^2}{(273.1)^2 64 P_c}$$

This is the value of  $NR$  used to calculate ( $a$ ) and ( $b$ ), and naturally all three terms must be expressed in the same system of units. Since

$$NR = \frac{1}{273.1}$$

it follows that the values of  $T_c$  used for evaluating ( $a$ ) and ( $b$ ) must be expressed in ° C. absolute. For convenience  $p_c$  is expressed in atmospheres, thereby necessitating the use of this unit for all subsequent computations involving ( $p$ ).

Substituting  $\frac{1}{273.1}$  for  $NR$  in equation (22) gives

$$p = \frac{T}{273.1 (v-b)} - \frac{a}{v^2} \tag{23}$$

which is a convenient form for calculating  $pv$  for all temperatures.

Inasmuch as the equation of van der Waals is a cubic with respect to  $v$ , it is simpler to assume values for  $v$  and calculate ( $p$ ) by means of equation (23).

It will be seen from Figures 14 to 22 that this equation, while indicating qualitatively the  $pv$  relations, is very inaccurate quantitatively except in the case of the gas, neon. In reality, however, the quantities ( $a$ ) and ( $b$ ) are not constants, but are generally accepted as being functions of both temperature and pressure.<sup>5</sup> Calculations involving the corrections of these "constants" are too involved for use in practical calculations and will, therefore, be left out of consideration. Hence the discussions of these equations of state, apply only in so far as the constants ( $a$ ) and ( $b$ ) are calculated directly from the critical constants and are considered as invariants.

It is quite evident that while this equation has been of great service in the study of liquids and gases and is quite valuable in a general way, it is not particularly useful for the present purpose.

### 3. EQUATION OF DIETERICI

Referring to equation (22)

$$p = \frac{NRT}{v-b} - \frac{a}{v^2}$$

it is seen that the pressure is, according to van der Waals' term  $\frac{NRT}{v-b}$ , diminished, because of the attractive forces between the molecules, by the quantity  $\frac{a}{v^2}$ .

Dieterici,<sup>6</sup> instead of subtracting a term from  $\frac{NRT}{v-b}$ , multiplies it by a quantity which at any pressure is never greater than unity.

The term which he introduced is  $e^{-\frac{A}{RTv}}$  where  $e$  is the base of the natural logarithms (2.7183),  $A$  the constant involving the cohesive effect of the molecules, and  $R$ ,  $T$ , and  $v$  have their usual significance.

The equation thus becomes

$$p = \frac{NRT}{v-b} e^{-\frac{A}{RTv}} \quad (24)$$

a revised form being

$$p = \frac{NRT}{v-b} e^{-\frac{a}{T^{1.25}v}} \quad (25)$$

This equation was derived by assuming that since in the interior of the gas the cohesive forces are effective in all directions they are

<sup>5</sup> F. H. MacDougal, J. Am. Chem. Soc., 33, p. 528; 1916. T. H. Richards, J. Am. Chem. Soc., 36, p. 617; 1914.

<sup>6</sup> Dieterici, Ann. Physik u. Chem., 11, p. 700; 1899; Ann. Physik, 5, p. 51; 1901.

neutralized, and hence do not affect the molecules. At the surface of the gas, however, the molecules are pulled toward the interior and the effective pressure would be reduced. This equation is fully discussed in a paper by F. H. MacDougal.<sup>7</sup>

The relations between  $a$  and  $b$  and the critical constants are as follows:

$$a = 4b T_c^{1.27} \tag{26}$$

$$b = \frac{NR T_c}{P_c e^2} \tag{27}$$

Multiplying equation (25) by  $v$  gives

$$pv = \frac{NRT}{1 - \frac{a}{v}} e^{-\frac{a}{T^{1.27} v}}$$

and when  $p = 0$  and  $v = \infty$

$$pv = \frac{NRT_c}{1 - \frac{\infty}{\infty}} e^{-\frac{x}{T_c^{1.27} \infty}} = NRT_c$$

$$NR = \frac{1}{T_c} = \frac{1}{273.1}$$

as before

Substituting this value for  $NR$  in equation (27) gives

$$b = \frac{T_c}{273.1 P_c e^2}$$

The same substitution in equation (25) gives

$$p = \frac{T}{273.1 (v - b)} e^{-\frac{a}{T^{1.27} v}} \tag{28}$$

where

$$b = \frac{T_c}{273.1 P_c e^2} \text{ and } a = 4b T_c^{1.27}$$

For computing  $p$  at different volumes by means of equation (25)

the values of  $e^{-\frac{a}{T^{1.27} v}}$  can be conveniently obtained from mathematical tables after the exponent has been calculated.

From the accompanying figures it can be seen that Dieterici's equation, while not particularly applicable to gases at temperatures considerably above their critical temperatures, reproduces quite well the experimental data for gases in the neighborhood of their critical temperatures.

<sup>7</sup> F. H. MacDougal, J. Am. Chem. Soc., 38, p. 528; 1916.

## 4. EQUATION OF BERTHELOT

The equation of Berthelot<sup>8</sup> was derived from van der Waals's equation by replacing the quantities (*a*) and (*b*) with their equivalent values in terms of the critical constants and by introducing an experimental relation in the place of a relation deduced from van der Waals's equation.<sup>9</sup>

Berthelot's equation may be stated as follows:

$$\left[ \frac{p}{P_c} + \frac{16}{3} \frac{T_c}{T} \frac{V_c^2}{v^2} \right] - \left[ \frac{v}{V_c} - \frac{1}{4} \right] = \frac{32}{9} \frac{T}{T_c} \quad (29)$$

The equation of Berthelot as sometimes given in textbooks

$$pv = NRT \left[ 1 + \frac{9pT_c}{128P_cT} \left( 1 - 6 \frac{T_c^2}{T^2} \right) \right]$$

is a simplification of equation (29) and involves an assumption which is true only for small pressures. It can be seen from this equation that *pv* is a linear function of the pressure; that is, the isothermals would be straight lines. This equation, however, was derived for use in molecular weight determinations based upon the densities of gases and is to be used only over a pressure range of 0 to 1 atmosphere.

It is obvious that equation (29) does not hold at the critical point for then *p*, *T*, and *v* are replaced by *P<sub>c</sub>*, *T<sub>c</sub>*, and *V<sub>c</sub>*, respectively, and the equation becomes

$$\left[ 1 + \frac{16}{3} \right] \left[ 1 - \frac{1}{4} \right] = \frac{32}{9}$$

or

$$\frac{171}{36} = \frac{128}{36}$$

Furthermore, the equation contains the undesirable term *V<sub>c</sub>*. Upon solving the equation for *pv* and setting this term equal to unity when *p* = 0, *v* = ∞, and *T* = 273.1, there is obtained a relation between *V<sub>c</sub>*, *P<sub>c</sub>*, and *T<sub>c</sub>* by means of which *V<sub>c</sub>* can be eliminated from the original equation. The selection of 273.1° for the temperature at which *p<sub>0</sub>v<sub>∞</sub>* equals unity is purely arbitrary and the relation of *V<sub>c</sub>* to *P<sub>c</sub>* and *T<sub>c</sub>* would be different if some other temperature were used.

In any case, however, *V<sub>c</sub>* would always be proportional to  $\frac{T_c}{P_c}$  and since the value of *p<sub>0</sub>v<sub>∞</sub>* (when *T* = 273.1°) is the unit the final results would be the same.

Transposing equation (29)

$$p = \frac{32}{9} \frac{TP_c}{T_c} \left( \frac{4V_c}{4v - V_c} \right) - \frac{16}{3} \frac{T_c}{T} \frac{V_c^2 P_c}{v^2} \quad (30)$$

$$pv = \frac{32}{9} \frac{T}{T_c} P_c \left( \frac{4V_c}{4 - \frac{V_c}{v}} \right) - \frac{16}{3} \frac{T_c}{T} \frac{V_c^2 P_c}{v}$$

<sup>8</sup> Berthelot Trav. et Mem. Bur. intern. Poids. et Mes., p. 113; 1903.

<sup>9</sup> Jellinck, Lehrbuch der Physikalischen Chemie, 2, p. 167.

setting  $pv=1$ , when  $p=0$ ,  $v=\infty$  and  $T=273.1$

$$1 = \frac{32}{9} \frac{(273.1) P_c V_c}{T_c}$$

or

$$V_c = \frac{9 T_c}{32 (273.1) P_c} = \frac{0.001030 T_c}{P_c}$$

substituting in (30)

$$p = \frac{32}{9} \frac{TP_c}{T_c} \frac{4 (9 T_c)}{32 (273.1) P_c \left( 4V - \frac{0.001030 T_c}{P_c} \right)} - \frac{16 T_c}{3 T} \frac{0.0000010605 T_c^2 P_c}{P_c^2 v^2}$$

$$p = \frac{T}{273.1 \left( v - \frac{0.0002575 T_c}{P_c} \right)} - \frac{0.000005656 T_c^3}{TP_c v^2} \quad (31)$$

For the 0° C. isothermal

$$p = \frac{1}{v - \frac{0.0002575 T_c}{P_c}} - \frac{0.00000002070 T_c^3}{P_c v^2} \quad (32)$$

Equation (31) can be put in the following form:

$$p = \frac{T}{273.1(v-b)} - \frac{a}{Tv^2} \quad (33)$$

in which

$$b = \frac{0.0002575 T_c}{P_c}$$

$$a = \frac{0.000005656 T_c^3}{P_c}$$

This equation is seen to be similar to that of van der Waals, equation (23), excepting that the term  $T$  is introduced into the denominator of van der Waals' term  $\frac{a}{v^2}$ , and the constants ( $a$ ) and ( $b$ ) are different functions of the critical constants.

In most cases, however, this equation appears to fit better than the others the experimental data of gases at temperatures considerably above the critical. For gases such as ethylene and carbon dioxide at 0° C., however, that of Dieterici is to be preferred.

Table 2 indicates which of the three equations would probably give the best results for each of the various gases at ordinary temperatures, and gives for each gas the values of the constants ( $a$ ) and ( $b$ ). The evaluation of these constants necessitates a knowledge of the

critical constants of the various gases, and because of the importance of these properties and the lack of recent reliable tables a critical review of the work in this field has been prepared from which the values given in Table 2 have been selected. This review will appear in a forthcoming publication of the Bureau of Standards.

TABLE 2

Gas	Critical temperature (° C. abs.)	Pressure range, atmospheres	Equation for 0° C. isothermal	Values of constants	
				$p_0 v_\infty = RT = 1$	
				<i>a</i>	<i>b</i>
Helium.....	5.2	Total.....	Berthelot.....	0.00035	0.00058
Hydrogen.....	33.2	do.....	do.....	.0162	.000668
Neon.....	44.4	do.....	Van der Waals.....	.000414	.000756
Nitrogen.....	126.0	0-200.....	Berthelot.....	.3377	.00969
Do.....		200-600.....	Van der Waals.....	.002677	.001720
Do.....		Above 600.....	Dieterici.....	3.467	.001865
Carbon monoxide.....	134.4	0-200.....	Berthelot.....	.3969	.001000
Do.....		200-600.....	Van der Waals.....	.002952	.001778
Do.....		Above 600.....	Dieterici.....	3.887	.001925
Argon.....	151	0-200.....	Berthelot.....	.406	.000810
Oxygen.....	154.3	0-200.....	do.....	.4181	.000800
Do.....		200-600.....	Van der Waals.....	.002710	.001421
Do.....		Above 600.....	Dieterici.....	3.700	.001538
Nitric oxide.....	179	0-200.....	Berthelot.....	.4646	.000653
Methane.....	190.6	0-100.....	do.....	.8570	.001074
Do.....		100-300.....	Van der Waals.....	.00450	.00191
Do.....		0-100.....	Dieterici.....	14.32	.00276
Ethylene.....	282.8			11.79	.00207
Carbon dioxide.....	304.1			17.73	.00310
Ethane.....	305.2			14.4	.00247
Acetylene.....	309			12.46	.00214
Nitrous oxide.....	309.6			12.18	.00197
Hydrogen chloride.....	324.5			28.8	.0042
Propane.....	368.7			14.78	.00180
Ammonia.....	405.5			23.13	.00272
Chlorine.....	417.1				

Van der Waals's equation—equation (23).

Dieterici's equation—equation (28).

Berthelot's equation—equation (33).

5. CURVES COMPARING EQUATIONS OF STATE WITH EXPERIMENTAL DATA

In Figures 14 to 22 the experimental data on the compressibilities of various gases for pressures up to 1,000 atmospheres are compared with the data calculated from the equations of state of van der Waals, of Dieterici, and of Berthelot.

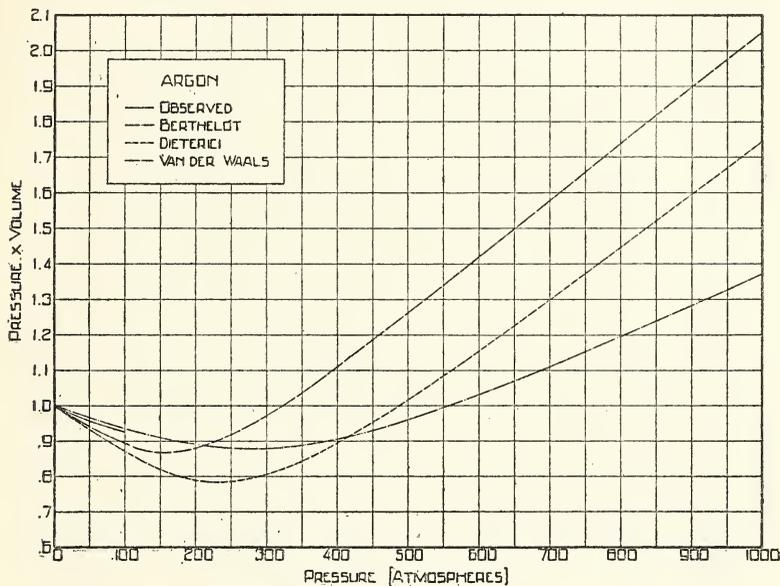


FIG. 14.—Comparison of the experimental data on the compressibility of argon at 0° C. with those calculated from the equation of Berthelot, of Dieterici, and of van der Waals

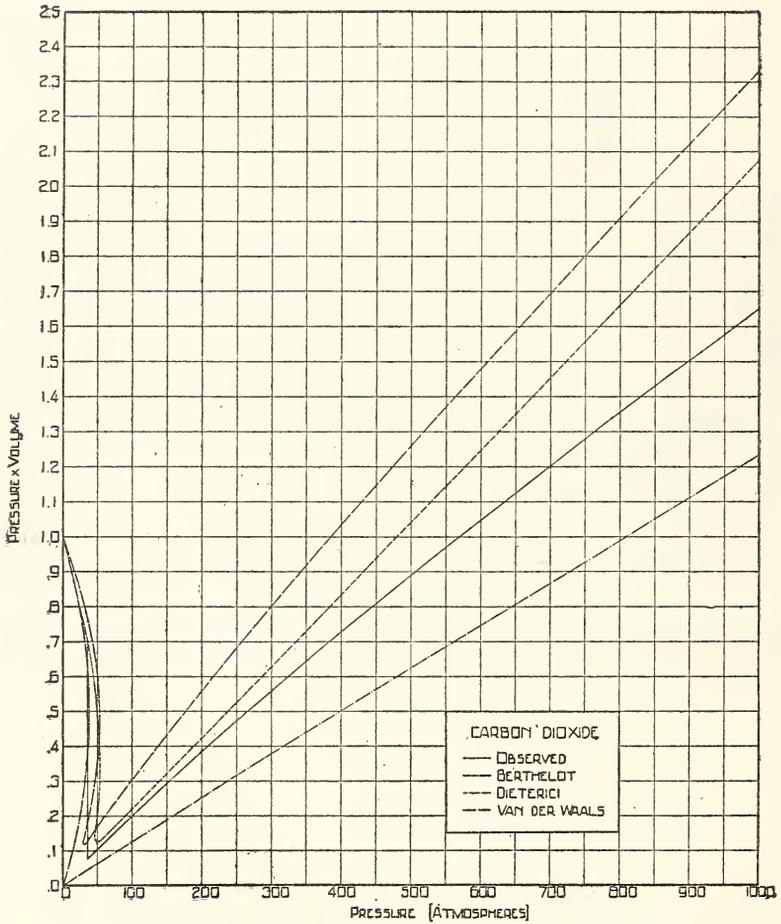


FIG. 15.—Comparison of the experimental data on the compressibility of carbon dioxide at  $0^{\circ}$  C. with those calculated from the equation of Berthelot, of Dieterici, and of van der Waals

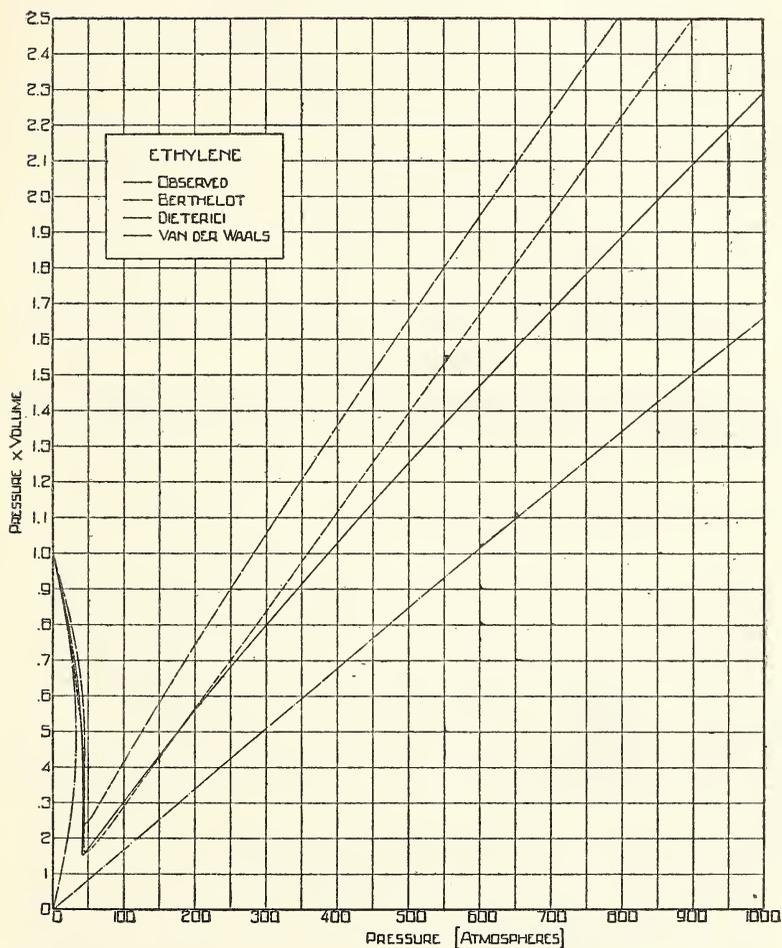


FIG. 16.—Comparison of the experimental data on the compressibility of ethylene at 0° C. with those calculated from the equation of Berthelot, of Dieterici, and of van der Waals

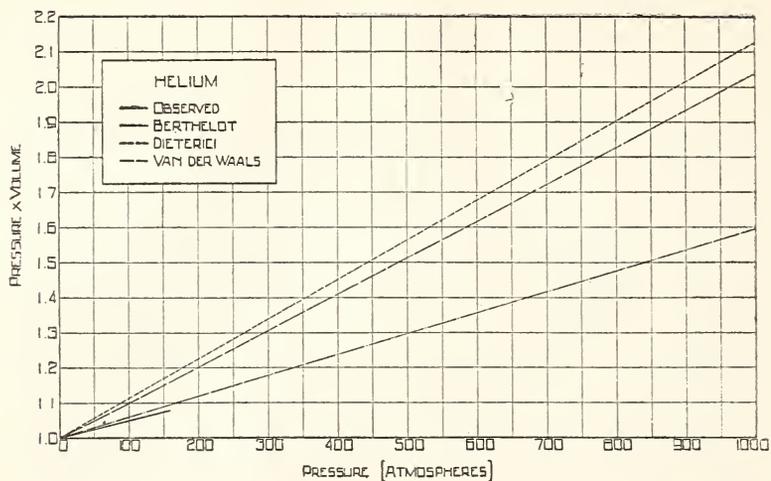


FIG. 17.—Comparison of the experimental data on the compressibility of helium at 0° C. with those calculated from the equation of Berthelot, of Dieterici, and of van der Waals

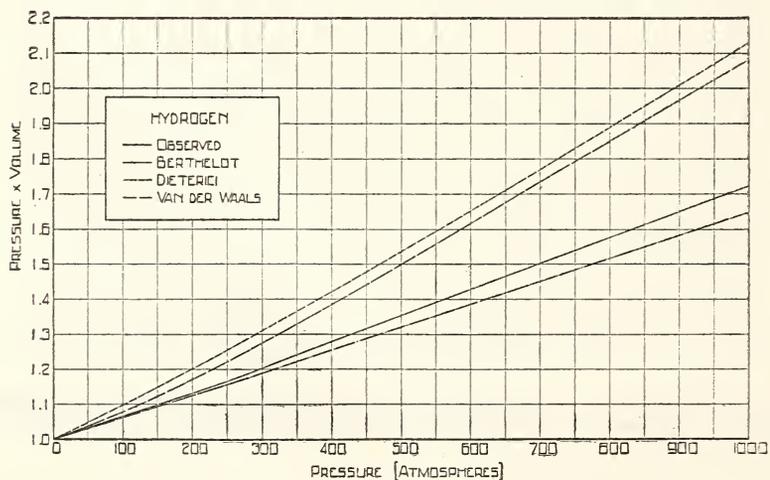


FIG. 18.—Comparison of the experimental data on the compressibility of hydrogen at 0° C. with those calculated from the equation of Berthelot, of Dieterici, and of van der Waals

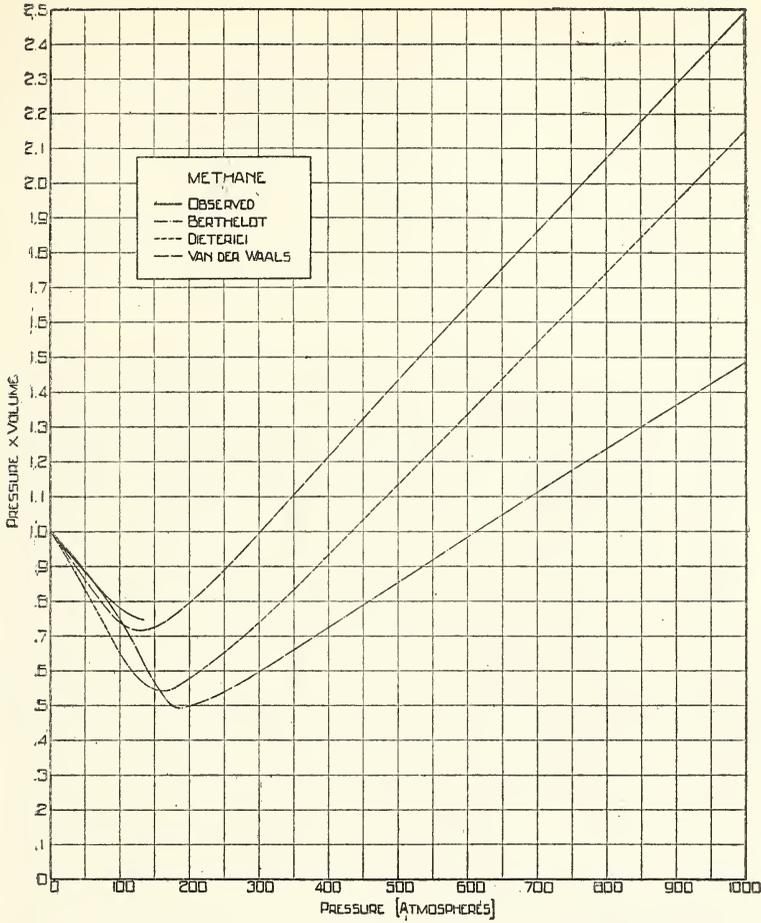


FIG. 19.—Comparison of the experimental data on the compressibility of methane at  $0^{\circ}$  C. with those calculated from the equation of Berthelot, of Dieterici, and of van der Waals

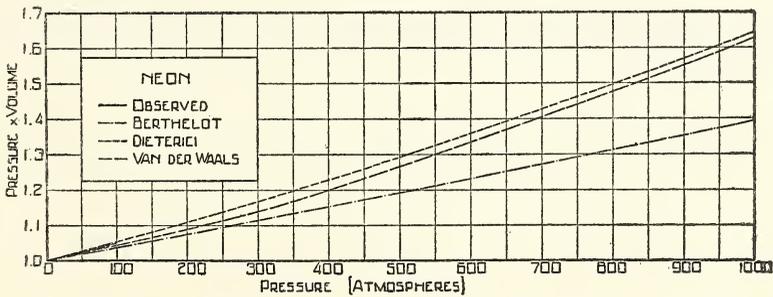


FIG. 20.—Comparison of the experimental data on the compressibility of neon at  $0^{\circ}$  C. with those calculated from the equation of Berthelot, of Dieterici, and of van der Waals

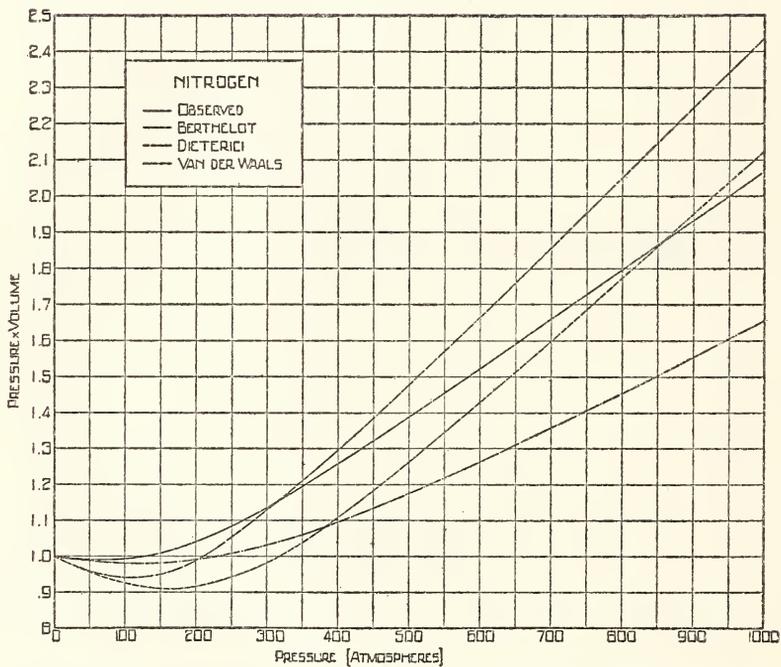


FIG. 21.—Comparison of the experimental data on the compressibility of nitrogen at 0° C. with those calculated from the equation of Berthelot, of Dieterici, and of van der Waals

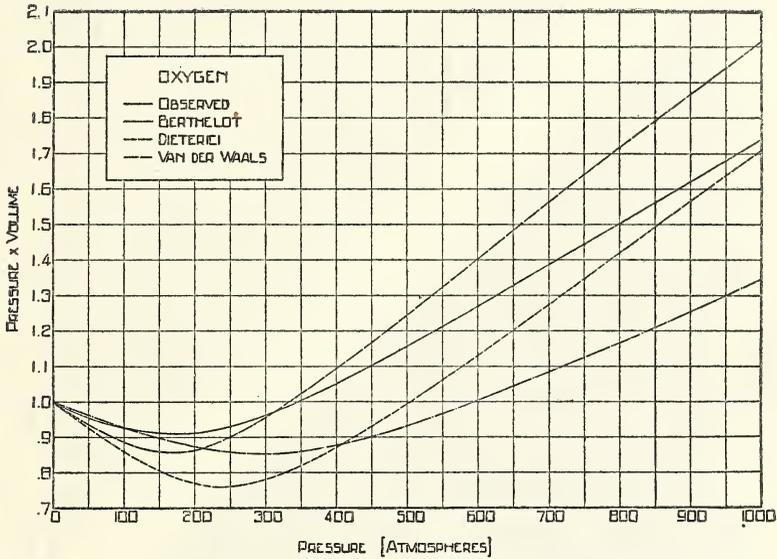


FIG. 22.—Comparison of the experimental data on the compressibility of oxygen at 0° C. with those calculated from the equation of Berthelot, of Dieterici, and of van der Waals

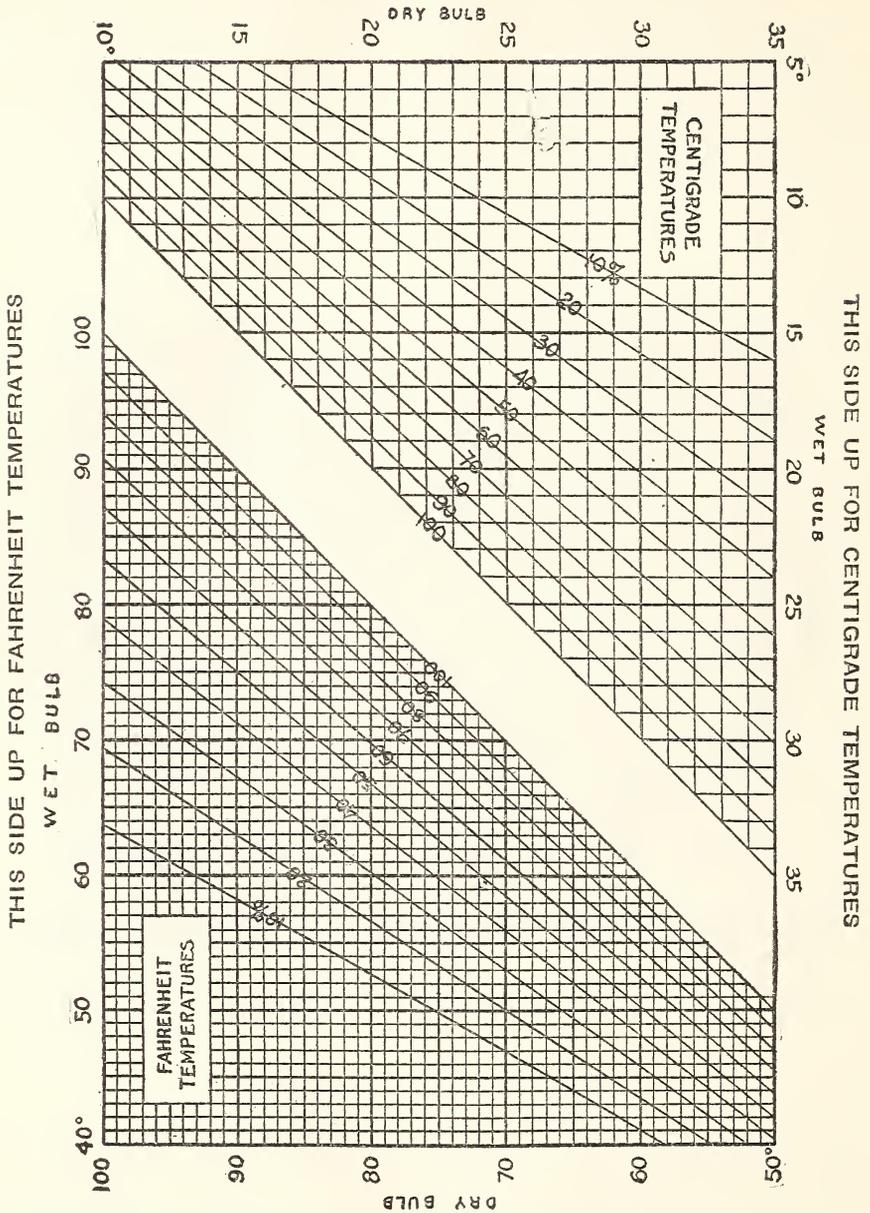


FIG. 23.—Relative humidity from wet and dry bulb thermometer readings for psychrometer with rapid ventilation

[Calculated for a barometer height of 755 mm. At altitudes of 6,000 feet or over the reduction in barometric pressure will cause an error of 5 per cent or over at very low humidities]

6. GAS CONSTANT  $R$  AND THE VOLUME OF A GRAM MOLECULE OF A PERFECT GAS

It is easy to obtain the value of the gas constant  $R$  and of the volume of a gram molecule of a perfect gas if the volume of a gram molecule of a particular gas at a given temperature and pressure is known, together with the value for the change in the product  $pv$  between the given pressure and zero pressure. The weights of a normal liter of the gases are given in Table 8 and the value of  $\frac{p_0v_0}{p_1v_1}$  at  $0^\circ$  C. have been measured rather accurately for several of the gases so that the above-mentioned quantities can be calculated without introducing any considerations of the theoretical equations of state.

It might be of interest to compare the values of these constants as obtained from data on various gases.

$$\frac{M}{L_n} = V_0 \text{ for the particular gas at 1 atmosphere and } 0^\circ \text{ C.}$$

where  $M$  = molecular weight

$L_n$  = weight of 1 liter of gas at  $0^\circ$  C. and 760 mm (at  $0^\circ$  C.)  
 where the acceleration of gravity is 980.665 cm per second per second.

$V_0$  = volume of 1 g molecule.

If  $p_0v_0$  = value of  $pv$  of an actual gas at zero pressure  $0^\circ$  C., then, since an actual gas at zero pressure behaves as a perfect gas  $p_0v_0$  = value of  $pv$  of perfect gas at 1 atmosphere (760 mm)  $0^\circ$  C.

Let  $p_1v_1$  = value of  $pv$  of an actual gas at 1 atmosphere (760 mm)  $0^\circ$  C.; then  $\frac{M}{L_n} \frac{p_0v_0}{p_1v_1} = V_0$  for a perfect gas at 1 atmosphere and  $0^\circ$  C.

Since  $pv = NR T$  for a perfect gas, and since  $v = V_0$  when  $N = 1$  and  $p = p_1 = 1$

$$p_1 V_0 = RT$$

$$R = \frac{p_1 V_0}{T} = \frac{1}{273.1} \frac{M}{L_n} \frac{p_0 v_0}{p_1 v_1}$$

In Table 3 are given the values for  $R$  and for the gram molecular volume of a perfect gas at 1 atmosphere and  $0^\circ$  C. calculated from data on the gases hydrogen, nitrogen, oxygen, and carbon dioxide for which the most accurate figures have been obtained.

TABLE 3.— $0^{\circ}$  C. =  $273.1^{\circ}$ , absolute

Gas	Weight of a normal liter in grams	Molecular weight <sup>1</sup>	$\frac{p_0 v_0}{p v_1}$	Gram molecular volume (in liters) of perfect gas at 1 atmosphere and $0^{\circ}$ C.	$R$ , liters per gram molecular atmosphere
Hydrogen.....	0.08988	2.016	<sup>2, 3, 4, 5</sup> 0.99939	22.416	0.08208
Nitrogen.....	1.2506	28.016	<sup>4, 6, 7, 8</sup> 1.00052	22.414	.08207
Oxygen.....	1.4290	32.000	<sup>3, 6, 7, 9, 10</sup> 1.00094	22.414	.08207
Carbon dioxide.....	1.9769	44.000	<sup>2</sup> 1.00706	22.415	.08208
Means.....				22.415	.08208

<sup>1</sup> From International Atomic Weights for 1925.

<sup>2</sup> Holborn, Ann. Physik, 63, p. 674; 1920.

<sup>3</sup> Guye and Batuecas, J. chim. phys., 20, p. 308; 1923.

<sup>4</sup> Henning and Heuse, Z. Physik, 5, p., 285; 1921.

<sup>5</sup> Onnes and Braak, Proc. Acad. Sci., Amsterdam, 10, p. 413; 1908. Comm. Leyden, 100a; 1908.

<sup>6</sup> Holborn and Otto, Z. Physik, 10, p. 367; 1922.

<sup>7</sup> Maverick, Thesis Univ. of Geneva; 1923.

<sup>8</sup> Smith and Taylor, J. Am. Chem. Soc., 45, p. 2107; 1923.

<sup>9</sup> Jaqueroed and Scheuer, Compt. rend. 140, p. 1384; 1905.

<sup>10</sup> Kuypers and Onnes, Comm. Leyden, 165e; 1923.

Inasmuch, however, as the molecular weights of these gases are subject to change, it seems best to calculate these constants from the data on oxygen only as proposed by Henning <sup>10</sup> because this gas is the standard from which molecular weights are computed. The value for the  $G. M. V.$  of a perfect gas at 1 atmosphere and  $0^{\circ}$  C. then becomes

$$G. M. V. = 22.414$$

and

$$R = 0.08207$$

Berthelot,<sup>11</sup> by calculating from experimental data on the density and compressibility of several gases, obtained

$$G. M. V. = 22.412$$

Henning,<sup>10</sup> using 1.4291 g/L for  $L_n$  and 1.00099 for the coefficient of compressibility of oxygen, found

$$G. M. V. = 22.414$$

Keyes,<sup>12</sup> by means of his equation of state, the densities and molecular weights of several gases, found

$$G. M. V. = 22.413$$

The values for  $R$  given by these investigators are

Berthelot.....	$R$ 0.08207	Absolutes using $0^{\circ}$ C. = 273.09
Henning.....	.08204	using $0^{\circ}$ C. = 273.2
Keyes.....	.08206	using $0^{\circ}$ C. = 273.134

The values adopted for use in the new International Critical Tables are

$$G. M. V. = 22.4115$$

$$R = 0.08206$$

<sup>10</sup> Henning. Z. Physik, 6, p. 69; 1921.

<sup>11</sup> Berthelot. Z. Elektrochemie, 10, p. 621; 1904.

<sup>12</sup> Keyes. J. Am. Soc. Refrig. Eng., 8, p. 505; 1922.

IV. SUPPLEMENTARY TABLES

TABLE 4.—Relative volumes occupied by a given quantity of gas, dry and saturated, under various conditions of temperature and pressure

	0° C., 760 mm, dry	0° C., 760 mm, saturated	20° C., 760 mm, dry	20° C., 760 mm, saturated	60° F., 30 inches, dry	60° F., 30 inches, saturated	68° F., 30 inches, dry	68° F., 30 inches, saturated	68° F., 15 pounds per square inch, dry	68° F., 15 pounds per square inch, saturated	70° F., 30 inches, dry	70° F., 30 inches, saturated
0° C., 760 mm, dry-----	1.0000	1.0061	1.0735	1.0989	1.0543	1.0730	1.0797	1.0960	1.0521	1.0769	1.0747	1.1019
0° C., 760 mm, saturated---	.9940	1.0000	1.0671	1.0923	1.0480	1.0666	1.0642	1.0894	1.0457	1.0704	1.0682	1.0953
20° C., 760 mm, dry-----	.9316	.9372	1.0000	1.0236	.9822	.9996	.9973	1.0209	.9800	1.0032	1.0011	1.0265
20° C., 760 mm, saturated---	.9100	.9156	.9769	1.0000	.9535	.9765	.9743	.9973	.9574	.9800	.9780	1.0027
60° F., 30 inches, dry-----	.9485	.9542	1.0181	1.0422	1.0000	1.0177	1.0154	1.0394	.9973	1.0214	1.0192	1.0451
60° F., 30 inches, saturated---	.9319	.9376	1.0004	1.0240	.9826	1.0000	.9977	1.0213	.9804	1.0035	1.0015	1.0265
68° F., 30 inches, dry-----	.9341	.9397	1.0027	1.0264	.9848	1.0023	1.0000	1.0236	.9826	1.0058	1.0038	1.0292
68° F., 30 inches, saturated---	.9125	.9180	.9795	1.0027	.9621	.9791	.9769	1.0000	.9599	.9826	.9806	1.0054
68° F., 15 pounds per square inch, dry-----	.9506	.9563	1.0204	1.0445	1.0022	1.0200	1.0177	1.0417	1.0000	1.0236	1.0215	1.0474
68° F., 15 pounds per square inch, saturated---	.9286	.9343	.9968	1.0204	.9791	.9965	.9942	1.0177	.9769	1.0000	.9979	1.0232
70° F., 30 inches, dry-----	.9306	.9362	.9989	1.0225	.9811	.9985	.9963	1.0198	.9789	1.0021	1.0000	1.0254
70° F., 30 inches, saturated---	.9076	.9131	.9742	.9973	.9569	.9739	.9716	.9946	.9547	.9773	.9753	1.0000

TABLE 5.—Correction

[Multiply observed volumes of saturated gas by factor to correct to

Temperature (° C.)	Total gas pressure—millimeters of mercury														
	716	718	720	722	724	726	728	730	732	734	736	738	740	742	
5	0.917	0.919	0.922	0.924	0.927	0.930	0.932	0.935	0.937	0.940	0.943	0.945	0.948	0.950	
6	.913	.915	.918	.920	.923	.926	.928	.931	.933	.936	.939	.941	.944	.946	
7	.909	.911	.914	.917	.919	.922	.924	.927	.930	.932	.935	.937	.940	.942	
8	.905	.908	.910	.913	.915	.918	.920	.923	.926	.928	.931	.933	.936	.938	
9	.901	.904	.906	.909	.911	.914	.916	.919	.921	.924	.926	.929	.932	.934	
10	.897	.900	.902	.905	.907	.910	.912	.915	.917	.920	.922	.925	.928	.930	
11	.893	.896	.898	.901	.903	.906	.908	.911	.913	.916	.918	.921	.924	.926	
12	.889	.892	.894	.897	.899	.902	.904	.907	.909	.912	.914	.917	.919	.922	
13	.885	.888	.890	.893	.895	.898	.900	.903	.905	.908	.910	.913	.915	.918	
14	.881	.884	.886	.887	.891	.894	.896	.899	.901	.904	.906	.909	.911	.914	
15	.877	.880	.882	.885	.887	.890	.892	.895	.897	.900	.902	.904	.907	.910	
16	.873	.876	.878	.880	.883	.885	.888	.890	.893	.895	.898	.900	.903	.905	
17	.869	.871	.874	.876	.879	.881	.884	.886	.889	.891	.894	.896	.898	.901	
18	.865	.867	.870	.872	.874	.877	.880	.882	.884	.887	.889	.892	.894	.897	
19	.860	.863	.865	.868	.870	.873	.875	.878	.880	.883	.885	.888	.890	.892	
20	.856	.859	.861	.864	.866	.869	.871	.874	.876	.878	.881	.883	.886	.889	
21	.852	.854	.857	.859	.862	.864	.867	.869	.872	.874	.876	.879	.881	.884	
22	.848	.850	.853	.855	.857	.860	.862	.865	.867	.870	.872	.874	.877	.879	
23	.843	.846	.848	.851	.853	.856	.858	.860	.863	.865	.868	.870	.872	.875	
24	.839	.841	.844	.846	.848	.851	.853	.856	.858	.861	.863	.866	.868	.870	
25	.834	.837	.839	.842	.844	.846	.849	.851	.854	.856	.858	.861	.863	.866	
26	.830	.832	.835	.837	.840	.842	.844	.847	.847	.852	.854	.856	.859	.861	
27	.825	.828	.830	.833	.835	.837	.840	.842	.842	.847	.847	.852	.854	.856	
28	.821	.823	.825	.828	.830	.833	.835	.837	.839	.842	.844	.847	.849	.852	
29	.816	.818	.821	.823	.825	.828	.830	.832	.835	.837	.840	.842	.844	.847	
30	.811	.813	.816	.818	.821	.823	.825	.828	.830	.832	.835	.837	.840	.842	
31	.806	.809	.811	.813	.816	.818	.820	.823	.825	.828	.830	.832	.835	.837	
32	.801	.804	.806	.808	.811	.814	.815	.818	.820	.822	.825	.827	.830	.832	
33	.796	.798	.801	.803	.806	.809	.810	.813	.815	.817	.820	.822	.824	.827	
34	.791	.793	.796	.798	.800	.803	.805	.807	.810	.812	.814	.817	.819	.822	
35	.786	.788	.790	.793	.795	.797	.800	.802	.804	.807	.809	.811	.814	.816	
36	.781	.783	.785	.787	.790	.792	.794	.797	.799	.801	.804	.806	.808	.811	
37	.775	.777	.780	.782	.784	.787	.789	.791	.794	.796	.798	.801	.803	.805	
38	.770	.772	.774	.776	.779	.781	.783	.786	.788	.790	.793	.795	.796	.799	
39	.764	.766	.768	.771	.773	.775	.778	.780	.782	.784	.787	.789	.790	.794	
40	.758	.760	.763	.765	.767	.770	.772	.774	.776	.779	.781	.783	.786	.788	
41	.752	.755	.757	.759	.761	.764	.766	.768	.771	.773	.775	.777	.780	.782	
42	.746	.748	.751	.753	.755	.758	.760	.762	.764	.767	.769	.771	.774	.776	
43	.740	.742	.745	.747	.749	.751	.754	.756	.758	.761	.763	.765	.767	.770	
44	.734	.736	.738	.741	.743	.745	.747	.750	.752	.754	.756	.759	.761	.763	
45	.727	.730	.732	.733	.736	.739	.741	.743	.745	.748	.750	.752	.754	.757	
46	.721	.723	.725	.728	.730	.732	.734	.737	.739	.741	.743	.746	.748	.750	
47	.714	.716	.719	.721	.723	.725	.728	.730	.732	.734	.737	.739	.741	.743	
48	.707	.710	.712	.714	.716	.718	.721	.723	.725	.727	.730	.732	.734	.736	
49	.701	.703	.705	.707	.709	.712	.714	.716	.718	.720	.723	.725	.727	.729	

*factors for gas volume*

volume of dry gas at 760 mm of mercury pressure (0° C.) and 0° C.]

Total gas pressure—millimeters of mercury—Continued													
744	746	748	750	752	754	756	758	760	762	764	766	768	770
0.953	0.956	0.958	0.961	0.963	0.966	0.968	0.971	0.974	0.976	0.979	0.981	0.984	0.986
.949	.952	.954	.957	.959	.962	.964	.967	.970	.972	.975	.977	.980	.982
.945	.948	.950	.952	.955	.958	.960	.963	.965	.968	.971	.973	.976	.978
.941	.943	.946	.948	.951	.954	.956	.959	.961	.964	.966	.969	.972	.974
.937	.939	.942	.944	.947	.950	.952	.954	.957	.960	.962	.965	.967	.970
.933	.935	.938	.940	.943	.945	.948	.950	.953	.956	.958	.961	.963	.966
.929	.931	.934	.936	.939	.941	.944	.946	.949	.951	.954	.956	.959	.962
.924	.927	.930	.932	.934	.937	.940	.942	.945	.947	.950	.952	.955	.957
.920	.923	.925	.928	.930	.933	.935	.938	.940	.943	.946	.948	.950	.953
.916	.919	.921	.924	.926	.929	.931	.934	.936	.939	.941	.944	.946	.949
.912	.914	.917	.920	.922	.924	.927	.929	.932	.934	.937	.940	.942	.944
.908	.910	.913	.915	.918	.920	.923	.925	.928	.930	.933	.935	.938	.940
.904	.906	.908	.911	.913	.916	.918	.921	.923	.926	.928	.931	.933	.936
.899	.902	.904	.907	.909	.912	.914	.916	.919	.922	.924	.925	.929	.931
.895	.897	.900	.902	.905	.907	.910	.912	.915	.917	.920	.921	.924	.927
.891	.893	.896	.898	.900	.903	.905	.908	.910	.913	.915	.918	.920	.922
.886	.889	.891	.894	.896	.898	.901	.903	.906	.908	.911	.913	.916	.918
.882	.884	.887	.888	.892	.894	.895	.899	.901	.904	.906	.909	.911	.913
.877	.880	.882	.885	.887	.889	.892	.894	.897	.899	.902	.904	.906	.909
.873	.875	.878	.880	.882	.885	.887	.890	.892	.895	.897	.899	.902	.904
.868	.871	.873	.875	.878	.880	.883	.885	.888	.890	.892	.895	.897	.899
.864	.866	.868	.871	.873	.876	.878	.880	.883	.885	.888	.890	.892	.895
.859	.861	.864	.866	.868	.871	.873	.876	.878	.880	.883	.885	.888	.890
.854	.856	.859	.861	.864	.866	.868	.871	.873	.876	.878	.880	.883	.885
.849	.852	.854	.856	.859	.861	.864	.866	.868	.870	.873	.875	.878	.880
.844	.847	.849	.851	.854	.856	.858	.861	.863	.865	.868	.870	.873	.875
.839	.842	.844	.846	.849	.851	.854	.856	.858	.860	.863	.865	.868	.870
.834	.836	.839	.841	.844	.846	.848	.851	.853	.855	.858	.860	.862	.865
.829	.831	.834	.836	.838	.841	.843	.845	.848	.850	.852	.855	.857	.860
.824	.826	.828	.831	.833	.836	.838	.840	.842	.845	.847	.850	.852	.854
.818	.821	.823	.825	.829	.830	.832	.835	.837	.839	.842	.844	.846	.849
.813	.815	.818	.820	.823	.825	.827	.829	.832	.834	.835	.839	.841	.843
.808	.810	.812	.814	.817	.819	.821	.824	.826	.828	.831	.833	.835	.838
.802	.804	.806	.809	.811	.813	.816	.818	.820	.823	.825	.827	.830	.832
.796	.798	.801	.803	.805	.808	.810	.812	.814	.817	.819	.821	.824	.826
.790	.793	.795	.797	.799	.802	.804	.806	.809	.811	.813	.816	.818	.820
.784	.786	.789	.791	.793	.796	.798	.800	.803	.805	.807	.809	.812	.814
.778	.780	.783	.785	.787	.790	.792	.794	.796	.799	.801	.803	.806	.808
.772	.774	.777	.779	.781	.783	.786	.788	.790	.792	.795	.797	.799	.802
.766	.768	.770	.772	.775	.777	.779	.781	.784	.786	.788	.791	.793	.795
.759	.761	.764	.766	.768	.770	.773	.775	.777	.779	.783	.784	.786	.788
.752	.755	.757	.759	.762	.764	.766	.768	.770	.773	.775	.777	.780	.782
.746	.748	.750	.752	.755	.757	.759	.761	.764	.766	.768	.770	.773	.775
.739	.741	.743	.745	.748	.750	.752	.754	.756	.759	.761	.763	.766	.768
.732	.734	.736	.738	.741	.743	.745	.747	.750	.752	.754	.756	.758	.761

TABLE 6.—Correction

[Multiply observed volume of saturated gas by factor to correct to

Temperature (° F.)	Total gas pressure—inches of mercury											
	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	29.0	29.1
55	0.928	0.931	0.935	0.939	0.942	0.944	0.947	0.951	0.954	0.958	0.961	0.965
56	.926	.929	.933	.936	.939	.942	.945	.948	.952	.955	.959	.962
57	.923	.927	.930	.933	.937	.940	.943	.946	.949	.953	.956	.960
58	.921	.924	.928	.931	.935	.938	.941	.944	.947	.951	.954	.957
59	.919	.922	.925	.929	.932	.936	.939	.942	.945	.948	.952	.955
60	.916	.920	.923	.926	.930	.933	.937	.940	.942	.946	.949	.952
61	.914	.917	.920	.924	.927	.931	.934	.937	.940	.944	.947	.950
62	.911	.915	.918	.921	.925	.928	.932	.935	.938	.942	.944	.947
63	.909	.912	.916	.919	.922	.926	.929	.932	.936	.939	.942	.945
64	.906	.910	.913	.916	.920	.923	.927	.930	.933	.937	.940	.942
65	.904	.907	.911	.914	.917	.921	.924	.928	.931	.934	.938	.940
66	.901	.905	.908	.912	.915	.918	.922	.925	.928	.932	.935	.938
67	.899	.902	.906	.909	.912	.916	.919	.922	.926	.929	.932	.936
68	.896	.900	.903	.906	.910	.913	.916	.920	.923	.926	.930	.933
69	.894	.897	.901	.904	.907	.911	.914	.917	.921	.924	.927	.931
70	.891	.895	.898	.901	.905	.908	.911	.915	.918	.921	.925	.928
71	.889	.892	.896	.899	.902	.906	.909	.912	.915	.919	.922	.925
72	.886	.890	.894	.896	.900	.903	.906	.910	.913	.916	.920	.923
73	.884	.887	.890	.894	.897	.900	.904	.907	.910	.914	.917	.920
74	.882	.885	.888	.891	.894	.898	.901	.904	.908	.911	.914	.917
75	.879	.883	.885	.888	.892	.895	.898	.902	.905	.908	.912	.915
76	.877	.880	.883	.886	.889	.892	.896	.899	.902	.905	.909	.912
77	.874	.877	.881	.884	.886	.890	.893	.896	.900	.903	.906	.909
78	.872	.875	.878	.881	.884	.887	.890	.894	.897	.900	.903	.907
79	.869	.872	.875	.879	.882	.884	.888	.891	.894	.897	.900	.904
80	.866	.869	.873	.876	.879	.882	.885	.888	.891	.894	.898	.901
81	.863	.867	.870	.873	.876	.880	.883	.885	.888	.892	.895	.898
82	.861	.864	.867	.870	.874	.877	.880	.883	.886	.889	.892	.895
83	.858	.861	.864	.868	.871	.874	.877	.881	.884	.886	.889	.893
84	.855	.858	.861	.865	.868	.871	.875	.878	.881	.884	.886	.890
85	.852	.855	.859	.862	.865	.868	.872	.875	.878	.881	.884	.887
86	.849	.853	.856	.859	.862	.865	.869	.872	.875	.878	.882	.884
87	.846	.850	.853	.856	.858	.863	.866	.869	.872	.875	.879	.882
88	.844	.847	.850	.853	.857	.860	.863	.866	.869	.873	.876	.879
89	.841	.844	.847	.850	.853	.857	.860	.863	.866	.870	.873	.876
90	.838	.841	.844	.847	.851	.854	.857	.860	.863	.867	.870	.873
91	.835	.838	.841	.844	.847	.851	.854	.857	.860	.863	.867	.870
92	.832	.835	.838	.841	.845	.848	.851	.854	.857	.860	.864	.867
93	.829	.832	.835	.838	.841	.845	.848	.851	.854	.857	.861	.864
94	.826	.829	.832	.835	.838	.841	.845	.848	.851	.854	.857	.861
95	.823	.826	.829	.832	.835	.838	.841	.845	.848	.851	.854	.857
96	.820	.823	.826	.829	.832	.835	.838	.841	.845	.848	.851	.854
97	.817	.820	.823	.826	.829	.832	.835	.838	.841	.845	.848	.851
98	.814	.817	.820	.823	.826	.829	.832	.835	.838	.841	.845	.848
99	.811	.814	.817	.820	.823	.825	.829	.832	.835	.838	.841	.844
100	.807	.810	.813	.816	.819	.822	.826	.828	.831	.834	.837	.840
101	.803	.807	.810	.813	.816	.819	.823	.826	.828	.831	.834	.836
102	.800	.803	.806	.810	.812	.815	.819	.822	.825	.828	.830	.833
103	.797	.800	.803	.805	.809	.812	.816	.819	.822	.825	.827	.830
104	.793	.796	.800	.803	.806	.809	.812	.815	.818	.821	.824	.827
105	.790	.793	.796	.799	.802	.805	.809	.812	.815	.818	.821	.824
106	.786	.789	.792	.796	.799	.802	.805	.808	.811	.814	.818	.821
107	.783	.785	.789	.792	.795	.798	.801	.804	.807	.811	.814	.817
108	.779	.782	.785	.788	.791	.795	.798	.801	.804	.807	.810	.813
109	.775	.778	.781	.784	.787	.791	.794	.797	.800	.803	.806	.809

*factors for gas volume*

volume of dry gas at 30 inches of mercury pressure (32° F.) and 60° F.]

Total gas pressure—inches of mercury—Continued													
29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	30.0	30.1	30.2	30.3	30.4	30.5
0.968	0.971	0.975	0.978	0.982	0.985	0.988	0.992	0.995	0.999	1.001	1.005	1.008	1.011
.965	.969	.972	.976	.980	.983	.986	.990	.993	.996	.999	1.002	1.005	1.008
.963	.967	.970	.973	.977	.980	.984	.987	.990	.994	.997	1.000	1.003	1.006
.961	.964	.968	.971	.975	.978	.981	.985	.988	.992	.995	.998	1.001	1.004
.958	.962	.965	.969	.972	.975	.979	.983	.985	.989	.992	.995	.998	1.001
.956	.959	.963	.966	.969	.973	.976	.980	.983	.986	.990	.993	.996	.999
.953	.957	.960	.963	.967	.970	.974	.977	.980	.984	.987	.991	.994	.997
.951	.954	.958	.961	.964	.968	.971	.975	.978	.981	.985	.988	.991	.995
.948	.952	.955	.958	.962	.965	.969	.972	.975	.979	.982	.985	.989	.992
.946	.949	.953	.956	.959	.963	.966	.969	.973	.976	.979	.983	.986	.990
.943	.947	.950	.953	.957	.960	.963	.967	.970	.973	.977	.980	.984	.987
.941	.944	.947	.951	.954	.957	.961	.964	.967	.971	.974	.978	.981	.984
.939	.942	.945	.948	.951	.955	.958	.962	.965	.968	.972	.975	.978	.982
.936	.940	.942	.945	.949	.952	.956	.959	.962	.966	.969	.972	.976	.979
.934	.937	.940	.943	.946	.950	.953	.956	.960	.963	.966	.970	.973	.976
.931	.935	.938	.941	.944	.947	.950	.954	.957	.960	.964	.967	.970	.974
.929	.932	.935	.939	.942	.944	.949	.951	.954	.958	.961	.964	.968	.971
.926	.929	.933	.936	.939	.942	.945	.948	.952	.955	.958	.961	.965	.968
.923	.927	.930	.933	.937	.940	.942	.946	.949	.952	.955	.959	.962	.966
.921	.924	.927	.931	.934	.937	.940	.943	.946	.949	.953	.956	.959	.963
.918	.921	.925	.928	.931	.934	.938	.941	.943	.947	.950	.953	.957	.960
.915	.919	.922	.925	.928	.932	.935	.938	.941	.944	.947	.951	.954	.957
.913	.916	.919	.922	.926	.929	.932	.936	.939	.941	.944	.948	.951	.954
.910	.913	.916	.920	.923	.926	.930	.933	.936	.939	.942	.945	.948	.951
.907	.910	.914	.917	.920	.924	.927	.930	.933	.936	.940	.942	.945	.949
.904	.908	.911	.914	.917	.921	.924	.927	.930	.934	.937	.940	.943	.946
.902	.905	.908	.911	.914	.918	.921	.924	.928	.931	.934	.937	.941	.943
.899	.902	.905	.908	.912	.915	.918	.921	.925	.928	.931	.934	.938	.941
.896	.899	.902	.906	.909	.912	.915	.918	.922	.925	.928	.932	.935	.938
.893	.896	.899	.903	.906	.909	.912	.916	.919	.922	.925	.929	.932	.935
.890	.893	.896	.900	.903	.906	.909	.913	.916	.919	.922	.926	.929	.932
.887	.890	.894	.897	.900	.903	.906	.910	.913	.916	.919	.923	.926	.929
.884	.887	.891	.894	.897	.900	.903	.907	.910	.913	.916	.920	.923	.926
.882	.884	.888	.891	.894	.897	.900	.904	.907	.910	.913	.917	.920	.923
.879	.882	.885	.888	.891	.894	.898	.901	.904	.907	.910	.914	.917	.920
.876	.879	.882	.885	.888	.891	.894	.898	.901	.904	.907	.910	.914	.917
.873	.876	.879	.883	.885	.888	.891	.894	.898	.901	.904	.907	.911	.914
.870	.873	.876	.880	.883	.885	.888	.891	.895	.898	.901	.904	.907	.911
.867	.870	.873	.877	.880	.883	.885	.888	.892	.895	.898	.901	.904	.907
.864	.867	.870	.873	.877	.880	.883	.885	.888	.891	.895	.898	.901	.904
.861	.864	.867	.870	.873	.877	.880	.883	.885	.888	.891	.895	.898	.901
.857	.861	.864	.867	.870	.873	.876	.880	.883	.885	.888	.891	.894	.898
.854	.857	.861	.864	.867	.870	.873	.876	.879	.883	.885	.888	.891	.894
.851	.854	.857	.860	.864	.867	.870	.873	.876	.879	.883	.885	.888	.891
.848	.851	.854	.857	.860	.863	.867	.870	.873	.876	.879	.882	.884	.888
.844	.847	.850	.853	.856	.859	.862	.865	.868	.871	.875	.878	.881	.884
.840	.843	.847	.850	.853	.856	.859	.862	.865	.868	.872	.875	.878	.881
.836	.839	.843	.846	.849	.852	.855	.858	.861	.864	.868	.871	.874	.877
.833	.836	.840	.843	.846	.849	.852	.855	.858	.861	.865	.868	.871	.874
.830	.833	.836	.839	.843	.846	.849	.852	.855	.858	.861	.864	.867	.871
.827	.830	.833	.836	.839	.842	.845	.848	.851	.854	.857	.860	.864	.867
.824	.827	.829	.831	.836	.838	.841	.844	.847	.850	.853	.856	.860	.863
.820	.823	.826	.828	.832	.835	.838	.841	.844	.847	.849	.853	.856	.860
.816	.819	.822	.825	.828	.831	.834	.837	.840	.843	.845	.849	.853	.856
.812	.815	.818	.822	.825	.827	.830	.833	.836	.839	.842	.845	.849	.852

TABLE 7.—Correction

[Multiply observed volume of saturated gas by factor to correct to

Temperature (° F.)	Total gas pressure—inches of mercury											
	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	29.0	29.1
55	0.944	0.947	0.951	0.954	0.958	0.961	0.964	0.968	0.971	0.975	0.978	0.982
56	.942	.945	.949	.952	.955	.959	.962	.965	.969	.972	.976	.979
57	.939	.943	.946	.949	.953	.956	.960	.963	.966	.970	.973	.977
58	.937	.940	.944	.947	.951	.954	.957	.961	.964	.968	.971	.974
59	.935	.938	.941	.945	.948	.952	.955	.958	.962	.965	.969	.972
60	.932	.936	.939	.942	.946	.949	.953	.956	.959	.963	.966	.969
61	.930	.933	.936	.940	.943	.947	.950	.953	.957	.960	.964	.967
62	.927	.931	.934	.937	.941	.944	.948	.951	.954	.958	.961	.964
63	.925	.928	.932	.935	.938	.942	.945	.948	.952	.955	.959	.962
64	.922	.926	.929	.932	.936	.939	.943	.946	.949	.953	.955	.959
65	.920	.923	.927	.930	.933	.937	.940	.944	.947	.950	.954	.957
66	.917	.921	.924	.928	.931	.934	.938	.941	.944	.948	.951	.954
67	.915	.918	.922	.925	.928	.932	.935	.938	.942	.945	.948	.952
68	.912	.916	.919	.922	.926	.929	.932	.936	.939	.942	.946	.949
69	.910	.913	.917	.920	.923	.927	.930	.933	.937	.940	.943	.947
70	.907	.911	.914	.917	.921	.924	.927	.931	.934	.937	.941	.944
71	.905	.908	.912	.915	.918	.922	.925	.928	.931	.935	.938	.941
72	.902	.906	.909	.912	.916	.919	.922	.926	.929	.932	.936	.939
73	.900	.903	.906	.910	.913	.916	.920	.923	.926	.930	.933	.936
74	.897	.900	.904	.907	.910	.914	.917	.920	.924	.927	.930	.933
75	.894	.898	.901	.904	.908	.911	.914	.918	.921	.924	.928	.931
76	.892	.895	.898	.902	.905	.908	.912	.915	.918	.921	.925	.928
77	.889	.892	.896	.899	.902	.906	.909	.912	.916	.919	.922	.925
78	.887	.890	.893	.896	.900	.903	.906	.910	.913	.916	.919	.923
79	.884	.887	.890	.894	.897	.900	.904	.907	.910	.913	.916	.920
80	.881	.884	.888	.891	.894	.897	.901	.904	.907	.910	.914	.917
81	.878	.882	.885	.888	.891	.895	.898	.901	.904	.908	.911	.914
82	.876	.879	.882	.885	.889	.892	.895	.898	.902	.905	.908	.911
83	.873	.876	.879	.883	.886	.889	.892	.896	.899	.902	.905	.909
84	.870	.873	.876	.880	.883	.886	.890	.893	.896	.899	.902	.906
85	.867	.870	.874	.877	.880	.883	.887	.890	.893	.896	.900	.903
86	.864	.868	.871	.874	.877	.880	.884	.887	.890	.893	.897	.900
87	.861	.865	.868	.871	.874	.878	.881	.884	.887	.890	.894	.897
88	.859	.862	.865	.868	.872	.875	.878	.881	.884	.888	.891	.894
89	.856	.859	.862	.865	.868	.872	.875	.878	.881	.885	.888	.891
90	.853	.856	.859	.862	.866	.869	.872	.875	.878	.882	.885	.888
91	.850	.853	.856	.859	.862	.866	.869	.872	.875	.878	.882	.885
92	.847	.850	.853	.856	.860	.863	.866	.869	.872	.875	.879	.882
93	.844	.847	.850	.853	.856	.860	.863	.866	.869	.872	.876	.879
94	.841	.844	.847	.850	.853	.856	.860	.863	.866	.869	.872	.876
95	.837	.841	.844	.847	.850	.853	.856	.860	.863	.866	.869	.872
96	.834	.838	.841	.844	.847	.850	.853	.856	.860	.863	.866	.869
97	.831	.834	.838	.841	.844	.847	.850	.853	.856	.860	.863	.866
98	.828	.831	.834	.838	.841	.844	.847	.850	.853	.856	.860	.863
99	.825	.828	.831	.834	.837	.840	.844	.847	.850	.853	.856	.859
100	.821	.824	.827	.830	.833	.836	.840	.843	.846	.849	.852	.855
101	.818	.821	.824	.827	.830	.833	.837	.840	.843	.846	.849	.851
102	.814	.817	.820	.824	.826	.829	.833	.836	.839	.842	.845	.848
103	.811	.814	.817	.820	.823	.826	.830	.833	.836	.839	.842	.845
104	.807	.810	.814	.817	.820	.823	.825	.829	.832	.835	.839	.842
105	.804	.807	.810	.813	.816	.819	.823	.826	.829	.832	.835	.838
106	.800	.803	.806	.810	.813	.816	.819	.822	.825	.828	.832	.835
107	.797	.799	.803	.806	.809	.812	.815	.818	.821	.825	.828	.831
108	.793	.796	.799	.802	.805	.809	.812	.815	.818	.821	.824	.827
109	.789	.792	.795	.798	.801	.805	.808	.811	.814	.817	.820	.823

*factors for gas volume*

volume of saturated gas at 30 inches of mercury pressure (32° F.) and 60° F.]

Total gas pressure—inches of mercury—Continued													
29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	30.0	30.1	30.2	30.3	30.4	30.5
0.985	0.988	0.992	0.995	0.999	1.002	1.006	1.009	1.012	1.016	1.019	1.023	1.026	1.029
.982	.986	.989	.993	.997	1.000	1.003	1.007	1.010	1.013	1.016	1.020	1.023	1.026
.980	.984	.987	.990	.994	.997	1.001	1.004	1.007	1.011	1.014	1.018	1.021	1.024
.978	.981	.985	.988	.992	.995	.998	1.002	1.005	1.009	1.012	1.015	1.019	1.022
.975	.979	.982	.986	.989	.992	.996	.999	1.003	1.006	1.009	1.013	1.016	1.019
.973	.976	.980	.983	.986	.990	.993	.997	1.000	1.003	1.007	1.010	1.014	1.017
.970	.974	.977	.980	.984	.987	.991	.994	.997	1.001	1.004	1.008	1.011	1.014
.968	.971	.975	.978	.981	.985	.988	.992	.995	.998	1.002	1.005	1.008	1.012
.965	.969	.972	.975	.979	.982	.986	.989	.992	.996	.999	1.002	1.006	1.009
.963	.966	.970	.973	.976	.980	.983	.986	.990	.993	.996	1.000	1.003	1.007
.960	.964	.967	.970	.974	.977	.980	.984	.987	.990	.994	.997	1.001	1.004
.958	.961	.964	.968	.971	.974	.978	.981	.984	.988	.991	.995	.998	1.001
.955	.958	.962	.965	.968	.972	.975	.979	.982	.985	.989	.992	.995	.999
.952	.956	.959	.962	.966	.969	.973	.976	.979	.983	.986	.989	.993	.996
.950	.953	.957	.960	.963	.967	.970	.973	.977	.980	.983	.987	.990	.993
.947	.951	.954	.957	.961	.964	.967	.971	.974	.977	.981	.984	.987	.991
.945	.948	.951	.955	.958	.961	.965	.968	.971	.975	.978	.981	.985	.988
.942	.945	.949	.952	.955	.959	.962	.965	.969	.972	.975	.978	.982	.985
.939	.943	.946	.949	.953	.956	.959	.963	.966	.969	.972	.976	.979	.982
.937	.940	.943	.947	.950	.953	.957	.960	.963	.966	.970	.973	.976	.980
.934	.937	.941	.944	.947	.950	.954	.957	.960	.964	.967	.970	.974	.977
.931	.935	.938	.941	.944	.948	.951	.954	.958	.961	.964	.968	.971	.974
.929	.932	.935	.938	.942	.945	.948	.952	.955	.958	.961	.965	.968	.971
.926	.929	.932	.936	.939	.942	.946	.949	.952	.955	.959	.962	.965	.968
.923	.926	.930	.933	.936	.940	.943	.946	.949	.952	.956	.959	.962	.966
.920	.924	.927	.930	.933	.937	.940	.943	.946	.950	.953	.956	.960	.963
.918	.921	.924	.927	.930	.934	.937	.940	.944	.947	.950	.953	.957	.960
.915	.918	.921	.924	.928	.931	.934	.937	.941	.944	.947	.950	.954	.957
.912	.915	.918	.922	.925	.928	.931	.934	.938	.941	.944	.948	.951	.954
.909	.912	.915	.919	.922	.925	.928	.932	.935	.938	.941	.945	.948	.951
.906	.909	.912	.916	.919	.922	.925	.929	.932	.935	.938	.942	.945	.948
.903	.906	.910	.913	.916	.919	.922	.926	.929	.932	.935	.939	.942	.945
.900	.903	.907	.910	.913	.916	.920	.923	.926	.929	.932	.936	.939	.942
.897	.900	.904	.907	.910	.913	.916	.920	.923	.926	.929	.933	.936	.939
.894	.897	.901	.904	.907	.910	.914	.917	.920	.923	.926	.930	.933	.936
.891	.894	.898	.901	.904	.907	.910	.914	.917	.920	.923	.926	.930	.933
.888	.891	.894	.898	.901	.904	.907	.910	.914	.917	.920	.923	.926	.930
.885	.888	.891	.895	.898	.901	.904	.907	.911	.914	.917	.920	.923	.927
.882	.885	.888	.892	.895	.898	.901	.904	.908	.911	.914	.917	.920	.923
.879	.882	.885	.888	.892	.895	.898	.901	.904	.907	.911	.914	.917	.920
.876	.879	.882	.885	.888	.892	.895	.898	.901	.904	.907	.911	.914	.917
.872	.876	.879	.882	.885	.888	.891	.895	.898	.901	.904	.907	.910	.914
.869	.872	.876	.879	.882	.885	.888	.891	.894	.898	.901	.904	.907	.910
.866	.869	.872	.875	.879	.882	.885	.888	.891	.894	.898	.901	.904	.907
.863	.866	.869	.872	.875	.878	.882	.885	.888	.891	.894	.897	.900	.904
.859	.862	.865	.868	.871	.874	.878	.881	.884	.887	.890	.893	.896	.899
.855	.858	.862	.865	.868	.871	.874	.877	.880	.883	.887	.890	.893	.896
.851	.854	.858	.861	.864	.867	.870	.873	.876	.879	.883	.886	.889	.892
.848	.851	.855	.858	.861	.864	.867	.870	.873	.876	.880	.883	.886	.889
.845	.848	.851	.854	.858	.861	.864	.867	.870	.873	.876	.879	.882	.886
.841	.844	.848	.851	.854	.857	.860	.863	.866	.869	.872	.875	.879	.882
.838	.841	.844	.846	.851	.853	.856	.859	.862	.865	.868	.871	.875	.878
.834	.837	.840	.843	.847	.850	.853	.856	.859	.862	.864	.868	.871	.875
.830	.833	.836	.839	.843	.846	.849	.852	.855	.858	.860	.864	.868	.871
.826	.829	.832	.836	.839	.842	.845	.848	.851	.854	.857	.860	.864	.867

TABLE 8.—Correction

[Multiply observed volume of saturated gas by factor to correct to

Temperature (° F.)	Total gas pressure—inches of mercury											
	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	29.0	29.1
55	0.942	0.945	0.949	0.952	0.956	0.959	0.963	0.966	0.969	0.973	0.976	0.980
56	.940	.943	.947	.950	.953	.957	.960	.963	.967	.970	.974	.977
57	.937	.941	.944	.947	.951	.954	.958	.961	.964	.968	.971	.975
58	.935	.938	.942	.945	.949	.952	.955	.959	.962	.966	.969	.972
59	.933	.936	.939	.943	.946	.950	.953	.956	.960	.963	.967	.970
60	.930	.934	.937	.940	.944	.947	.951	.954	.957	.961	.964	.967
61	.928	.931	.934	.938	.941	.945	.948	.951	.955	.958	.962	.965
62	.925	.929	.932	.935	.939	.942	.946	.949	.952	.956	.959	.962
63	.923	.926	.930	.933	.936	.940	.943	.946	.950	.953	.957	.960
64	.920	.924	.927	.930	.934	.937	.941	.944	.947	.951	.954	.957
65	.918	.921	.925	.928	.931	.935	.938	.942	.945	.948	.952	.955
66	.915	.919	.922	.926	.929	.932	.936	.939	.942	.946	.949	.952
67	.913	.916	.920	.923	.926	.930	.933	.936	.940	.943	.946	.950
68	.910	.914	.917	.920	.924	.927	.930	.934	.937	.940	.944	.947
69	.908	.910	.915	.918	.921	.925	.928	.931	.935	.938	.941	.945
70	.905	.909	.912	.915	.919	.922	.925	.929	.932	.935	.939	.942
71	.903	.906	.910	.913	.916	.920	.923	.926	.929	.933	.936	.939
72	.900	.904	.907	.910	.914	.917	.920	.924	.927	.930	.934	.937
73	.898	.901	.904	.908	.911	.914	.918	.921	.924	.928	.931	.934
74	.895	.898	.902	.905	.908	.912	.915	.918	.922	.925	.928	.931
75	.892	.896	.899	.902	.906	.909	.912	.916	.919	.922	.926	.929
76	.890	.893	.896	.900	.903	.906	.910	.913	.916	.919	.923	.926
77	.887	.890	.894	.897	.900	.904	.907	.910	.914	.917	.920	.923
78	.885	.888	.891	.894	.898	.901	.904	.908	.911	.914	.917	.921
79	.882	.885	.888	.892	.895	.898	.902	.905	.908	.911	.914	.918
80	.879	.882	.886	.889	.892	.895	.899	.902	.905	.908	.912	.915
81	.876	.880	.883	.886	.889	.893	.896	.899	.902	.906	.909	.912
82	.874	.877	.880	.883	.887	.890	.893	.896	.900	.903	.906	.909
83	.871	.874	.877	.881	.884	.887	.890	.894	.897	.900	.903	.907
84	.868	.871	.874	.878	.881	.884	.888	.891	.894	.897	.900	.904
85	.865	.868	.872	.875	.878	.881	.885	.888	.891	.894	.898	.901
86	.862	.866	.869	.872	.875	.878	.882	.885	.888	.891	.895	.898
87	.859	.863	.866	.869	.872	.876	.879	.882	.885	.888	.892	.895
88	.857	.860	.863	.866	.870	.873	.876	.879	.882	.886	.889	.892
89	.854	.857	.860	.863	.866	.870	.873	.876	.879	.883	.886	.889
90	.851	.854	.857	.860	.864	.867	.870	.873	.876	.880	.883	.886
91	.848	.851	.854	.857	.862	.864	.867	.870	.873	.876	.880	.883
92	.845	.848	.851	.854	.858	.861	.864	.867	.870	.873	.877	.880
93	.842	.845	.848	.851	.854	.858	.861	.864	.867	.870	.874	.877
94	.839	.842	.845	.848	.851	.854	.858	.861	.864	.867	.870	.874
95	.835	.839	.842	.845	.848	.851	.854	.858	.861	.864	.867	.870
96	.832	.836	.839	.842	.845	.848	.851	.854	.858	.861	.864	.867
97	.829	.832	.836	.839	.842	.845	.848	.851	.854	.858	.861	.864
98	.826	.829	.832	.836	.839	.842	.845	.848	.851	.854	.858	.861
99	.823	.826	.829	.832	.835	.838	.842	.845	.848	.851	.854	.857
100	.819	.822	.825	.828	.831	.834	.838	.841	.844	.847	.850	.853
101	.816	.819	.822	.825	.828	.831	.835	.838	.841	.844	.847	.849
102	.812	.815	.818	.822	.824	.827	.831	.834	.837	.840	.843	.846
103	.809	.812	.815	.818	.821	.824	.828	.831	.834	.837	.840	.843
104	.805	.808	.812	.815	.818	.821	.824	.827	.830	.833	.837	.840
105	.802	.805	.808	.811	.814	.817	.821	.824	.827	.830	.833	.836
106	.798	.801	.804	.808	.811	.814	.817	.820	.823	.826	.830	.833
107	.795	.797	.801	.804	.807	.810	.813	.816	.819	.823	.826	.829
108	.791	.794	.797	.800	.803	.807	.810	.813	.816	.819	.822	.825
109	.787	.790	.793	.796	.799	.803	.806	.809	.812	.815	.818	.820

factors for gas volume

volume of dry gas at 30 inches of mercury pressure (32° F.) and (68° F.)]

Total gas pressure — inches of mercury—Continued													
29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	30.0	30.1	30.2	30.3	30.4	30.5
0.983	0.986	0.990	0.993	0.997	1.000	1.004	1.007	1.010	1.014	1.017	1.021	1.024	1.027
.980	.984	.987	.991	.995	.998	1.001	1.005	1.008	1.011	1.014	1.018	1.021	1.024
.978	.982	.985	.988	.992	.995	.999	1.002	1.005	1.009	1.012	1.016	1.019	1.022
.976	.979	.983	.986	.990	.993	.996	1.000	1.003	1.007	1.010	1.013	1.017	1.020
.973	.977	.980	.984	.987	.990	.994	.997	1.001	1.004	1.007	1.011	1.014	1.017
.971	.974	.978	.981	.984	.988	.991	.995	.998	1.001	1.005	1.008	1.012	1.015
.968	.972	.975	.978	.982	.985	.989	.992	.995	.999	1.002	1.006	1.009	1.012
.966	.969	.973	.976	.979	.983	.986	.990	.993	.996	1.000	1.003	1.006	1.010
.963	.967	.970	.973	.977	.980	.984	.987	.990	.994	.997	1.000	1.004	1.007
.961	.964	.968	.971	.974	.978	.981	.984	.988	.991	.994	.998	1.001	1.005
.958	.962	.965	.968	.972	.975	.978	.982	.985	.988	.992	.995	.999	1.002
.956	.959	.962	.966	.969	.972	.976	.979	.982	.986	.989	.993	.996	.999
.953	.956	.960	.963	.966	.970	.973	.977	.980	.983	.987	.990	.993	.997
.950	.954	.957	.960	.964	.967	.971	.974	.977	.981	.984	.987	.991	.994
.948	.951	.955	.958	.961	.965	.968	.971	.975	.978	.981	.985	.988	.991
.945	.949	.952	.955	.959	.962	.965	.969	.972	.975	.979	.982	.985	.989
.943	.946	.949	.953	.956	.959	.963	.966	.969	.973	.976	.979	.983	.986
.940	.943	.947	.950	.953	.957	.960	.963	.967	.970	.973	.976	.980	.983
.937	.941	.944	.947	.951	.954	.957	.961	.964	.967	.970	.974	.977	.980
.935	.938	.941	.945	.948	.951	.955	.958	.961	.964	.968	.971	.974	.978
.932	.935	.939	.942	.945	.948	.952	.955	.958	.962	.965	.968	.972	.975
.929	.933	.936	.939	.942	.946	.949	.952	.956	.959	.962	.966	.969	.972
.927	.930	.933	.936	.940	.943	.946	.950	.953	.956	.959	.963	.966	.969
.924	.927	.930	.934	.937	.940	.944	.947	.950	.953	.957	.960	.963	.966
.921	.924	.928	.931	.934	.938	.941	.944	.947	.950	.955	.960	.966	.964
.918	.922	.925	.928	.931	.935	.938	.941	.944	.948	.951	.954	.958	.961
.916	.919	.922	.925	.928	.932	.935	.938	.942	.945	.948	.951	.955	.958
.913	.916	.919	.922	.926	.929	.932	.935	.939	.942	.945	.948	.952	.955
.910	.913	.916	.920	.923	.926	.929	.932	.936	.939	.942	.945	.949	.952
.907	.910	.913	.917	.920	.923	.926	.930	.933	.936	.939	.943	.946	.949
.904	.907	.910	.914	.917	.920	.923	.927	.930	.933	.936	.940	.943	.946
.901	.904	.908	.911	.914	.917	.920	.924	.927	.930	.933	.937	.940	.943
.898	.901	.905	.908	.911	.914	.918	.921	.924	.927	.930	.934	.937	.940
.895	.898	.902	.905	.908	.911	.914	.918	.921	.924	.927	.931	.934	.937
.892	.895	.899	.902	.905	.908	.912	.915	.918	.921	.924	.928	.931	.934
.889	.892	.896	.899	.902	.905	.908	.912	.915	.918	.921	.924	.928	.931
.886	.889	.892	.896	.899	.902	.905	.908	.912	.915	.918	.921	.924	.928
.883	.886	.889	.893	.896	.899	.902	.905	.909	.912	.915	.918	.921	.925
.880	.883	.886	.890	.893	.896	.899	.902	.906	.909	.912	.915	.918	.921
.877	.880	.883	.886	.890	.893	.896	.899	.902	.905	.909	.912	.915	.918
.874	.877	.880	.883	.886	.890	.893	.896	.899	.902	.905	.909	.912	.915
.870	.874	.877	.880	.883	.886	.889	.893	.896	.899	.902	.905	.908	.912
.867	.870	.874	.877	.880	.883	.886	.889	.892	.896	.899	.902	.905	.908
.864	.867	.870	.873	.877	.880	.883	.886	.889	.892	.896	.899	.902	.905
.861	.864	.867	.870	.873	.876	.880	.883	.886	.889	.892	.895	.898	.902
.857	.860	.863	.866	.869	.872	.876	.879	.881	.884	.888	.891	.894	.897
.853	.856	.860	.863	.866	.869	.872	.875	.878	.881	.885	.888	.891	.894
.849	.852	.856	.859	.862	.865	.868	.871	.874	.877	.881	.884	.887	.890
.846	.849	.853	.856	.859	.862	.865	.868	.871	.874	.878	.881	.884	.887
.843	.846	.849	.852	.856	.859	.862	.865	.868	.871	.874	.877	.880	.884
.839	.842	.846	.849	.852	.855	.858	.861	.864	.867	.870	.873	.877	.880
.836	.839	.842	.844	.849	.851	.854	.857	.860	.863	.866	.869	.873	.876
.832	.835	.838	.841	.845	.848	.851	.854	.857	.860	.862	.866	.869	.873
.828	.831	.834	.837	.841	.844	.847	.850	.853	.856	.858	.862	.866	.869
.824	.827	.830	.834	.837	.840	.843	.846	.849	.852	.855	.858	.862	.865

TABLE 9.—Correction

[Multiply observed volume of saturated gas by factor to correct to

Temperature (° F.)	Total gas pressure—Inches of mercury											
	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	29.0	29.1
55	0.964	0.968	0.971	0.975	0.978	0.982	0.985	0.989	0.992	0.996	0.999	1.003
56	.962	.965	.969	.972	.975	.980	.983	.986	.990	.993	.997	1.000
57	.959	.963	.966	.969	.973	.976	.981	.984	.987	.991	.994	.998
58	.957	.960	.964	.967	.971	.974	.977	.982	.985	.989	.992	.995
59	.955	.958	.961	.965	.968	.972	.975	.979	.983	.986	.990	.993
60	.952	.956	.959	.962	.966	.969	.973	.976	.980	.984	.987	.990
61	.950	.953	.956	.960	.963	.967	.970	.973	.977	.981	.985	.988
62	.947	.951	.954	.957	.961	.964	.968	.971	.974	.979	.982	.985
63	.945	.948	.952	.955	.958	.962	.965	.968	.972	.975	.980	.983
64	.942	.946	.949	.952	.956	.959	.963	.966	.969	.973	.977	.980
65	.940	.943	.947	.950	.953	.957	.960	.964	.967	.970	.974	.977
66	.937	.941	.944	.948	.951	.954	.958	.961	.964	.968	.971	.974
67	.935	.938	.942	.945	.948	.952	.955	.958	.962	.965	.968	.972
68	.932	.936	.939	.942	.946	.949	.952	.956	.959	.962	.966	.969
69	.929	.933	.937	.940	.943	.947	.950	.953	.957	.960	.963	.967
70	.926	.930	.934	.937	.941	.944	.947	.951	.954	.957	.961	.964
71	.924	.927	.932	.935	.938	.942	.945	.948	.951	.955	.958	.961
72	.921	.925	.928	.932	.936	.939	.942	.946	.949	.952	.956	.959
73	.919	.922	.925	.929	.933	.936	.940	.943	.946	.950	.953	.956
74	.916	.919	.923	.926	.930	.934	.937	.940	.944	.947	.950	.953
75	.913	.917	.920	.923	.927	.930	.934	.938	.941	.944	.948	.951
76	.911	.914	.917	.921	.924	.927	.932	.935	.938	.941	.945	.948
77	.908	.911	.915	.918	.921	.925	.928	.932	.936	.939	.942	.945
78	.906	.909	.912	.915	.919	.922	.925	.929	.933	.936	.939	.943
79	.904	.906	.909	.913	.916	.919	.923	.926	.929	.933	.936	.940
80	.900	.903	.907	.910	.913	.916	.920	.923	.926	.929	.934	.937
81	.897	.901	.904	.907	.910	.914	.917	.920	.923	.927	.930	.934
82	.895	.898	.901	.904	.908	.911	.914	.917	.921	.924	.927	.931
83	.892	.895	.898	.902	.905	.908	.911	.915	.918	.921	.924	.928
84	.889	.892	.895	.899	.902	.905	.909	.912	.915	.918	.921	.925
85	.886	.889	.893	.896	.899	.902	.906	.909	.912	.915	.919	.922
86	.883	.887	.890	.893	.896	.899	.903	.906	.909	.912	.916	.919
87	.879	.884	.887	.890	.893	.897	.900	.903	.906	.909	.913	.916
88	.877	.880	.884	.887	.891	.894	.897	.900	.903	.907	.910	.913
89	.874	.877	.880	.884	.887	.891	.894	.897	.900	.904	.907	.910
90	.871	.874	.877	.880	.885	.888	.891	.894	.897	.901	.904	.907
91	.868	.871	.874	.877	.881	.885	.888	.891	.894	.897	.901	.904
92	.865	.868	.871	.874	.878	.881	.885	.888	.891	.894	.898	.901
93	.862	.865	.868	.871	.874	.878	.881	.885	.888	.891	.895	.898
94	.859	.862	.865	.868	.871	.875	.878	.881	.885	.888	.891	.895
95	.855	.859	.862	.865	.868	.871	.874	.878	.881	.885	.888	.891
96	.852	.856	.859	.862	.865	.868	.871	.874	.878	.881	.885	.888
97	.849	.852	.856	.859	.862	.865	.868	.871	.874	.878	.881	.885
98	.846	.849	.852	.856	.859	.862	.865	.868	.871	.874	.878	.881
99	.843	.846	.849	.852	.855	.858	.862	.865	.868	.871	.874	.877
100	.839	.842	.845	.848	.851	.854	.858	.861	.864	.867	.870	.874
101	.836	.839	.842	.845	.848	.851	.855	.858	.861	.864	.867	.870
102	.831	.835	.838	.842	.844	.847	.851	.854	.857	.860	.863	.867
103	.828	.831	.835	.838	.841	.844	.848	.851	.854	.857	.860	.863
104	.824	.828	.831	.835	.838	.841	.844	.847	.850	.853	.857	.860
105	.821	.824	.827	.831	.834	.837	.841	.844	.847	.850	.853	.856
106	.817	.821	.823	.827	.830	.834	.837	.840	.843	.846	.850	.853
107	.814	.817	.820	.823	.826	.829	.833	.836	.839	.843	.846	.849
108	.810	.813	.816	.819	.822	.826	.829	.833	.836	.839	.842	.845
109	.806	.810	.813	.816	.819	.822	.825	.828	.832	.835	.838	.841

*factors for gas volume*

volume of saturated gas at 30 inches of mercury pressure (32° F.) and (68° F.)]

Total gas pressure -- inches of mercury--Continued													
29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	30.0	30.1	30.2	30.3	30.4	30.5
1.006	1.009	1.013	1.016	1.020	1.023	1.027	1.031	1.034	1.038	1.041	1.045	1.048	1.051
1.003	1.007	1.010	1.014	1.018	1.021	1.024	1.029	1.032	1.035	1.038	1.042	1.045	1.048
1.001	1.005	1.008	1.011	1.015	1.018	1.022	1.026	1.029	1.033	1.036	1.040	1.043	1.046
.999	1.002	1.006	1.009	1.013	1.016	1.019	1.023	1.027	1.031	1.034	1.037	1.041	1.044
.996	1.000	1.003	1.007	1.010	1.013	1.017	1.020	1.024	1.028	1.031	1.035	1.038	1.041
.994	.997	1.001	1.004	1.007	1.011	1.014	1.018	1.021	1.025	1.029	1.032	1.036	1.039
.991	.995	.998	1.001	1.005	1.008	1.012	1.015	1.018	1.022	1.026	1.030	1.033	1.036
.989	.992	.996	.999	1.002	1.006	1.009	1.013	1.016	1.019	1.023	1.027	1.030	1.034
.986	.990	.993	.996	1.000	1.003	1.007	1.010	1.013	1.017	1.020	1.024	1.028	1.031
.984	.987	.991	.994	.997	1.001	1.004	1.007	1.011	1.014	1.017	1.021	1.025	1.029
.981	.985	.988	.991	.995	.998	1.001	1.005	1.008	1.011	1.015	1.018	1.022	1.026
.979	.982	.985	.989	.992	.995	.999	1.002	1.005	1.009	1.012	1.016	1.019	1.023
.976	.979	.983	.986	.989	.993	.996	1.000	1.003	1.006	1.010	1.013	1.016	1.020
.973	.977	.980	.983	.987	.990	.994	.997	1.000	1.004	1.007	1.010	1.014	1.017
.970	.974	.978	.981	.984	.988	.991	.994	.998	1.001	1.004	1.008	1.011	1.014
.967	.971	.974	.978	.982	.985	.988	.992	.995	.998	1.002	1.005	1.008	1.012
.965	.968	.972	.976	.979	.982	.986	.989	.992	.996	.999	1.002	1.006	1.009
.962	.965	.969	.973	.976	.980	.983	.986	.990	.993	.996	.999	1.003	1.006
.959	.963	.966	.970	.973	.977	.980	.984	.987	.990	.993	.997	1.000	1.003
.957	.960	.963	.967	.970	.974	.978	.981	.984	.987	.991	.994	.997	1.001
.954	.957	.961	.964	.967	.971	.974	.978	.981	.985	.988	.991	.995	.998
.951	.955	.958	.961	.964	.968	.971	.975	.979	.982	.985	.989	.992	.995
.949	.952	.955	.958	.962	.965	.968	.972	.976	.979	.982	.986	.989	.992
.946	.949	.952	.956	.959	.962	.966	.969	.973	.976	.980	.983	.986	.989
.943	.946	.950	.953	.956	.960	.963	.966	.970	.973	.977	.980	.983	.987
.940	.944	.947	.950	.953	.957	.960	.963	.966	.970	.973	.977	.980	.984
.938	.941	.944	.947	.950	.954	.957	.960	.964	.967	.970	.973	.977	.981
.935	.938	.941	.944	.948	.951	.954	.957	.961	.964	.967	.970	.974	.978
.932	.935	.938	.942	.945	.948	.951	.954	.958	.961	.964	.968	.971	.974
.928	.932	.935	.939	.942	.945	.948	.952	.955	.958	.961	.965	.968	.971
.925	.928	.932	.936	.939	.942	.945	.949	.952	.955	.958	.962	.965	.968
.922	.925	.930	.933	.936	.939	.942	.946	.949	.952	.955	.959	.962	.965
.919	.922	.926	.930	.933	.936	.939	.943	.946	.949	.952	.956	.959	.962
.916	.919	.923	.927	.930	.933	.936	.940	.943	.946	.949	.953	.956	.959
.913	.916	.920	.923	.926	.930	.933	.937	.940	.943	.946	.950	.953	.956
.910	.913	.917	.920	.923	.926	.930	.934	.937	.940	.943	.946	.950	.953
.907	.910	.913	.917	.920	.923	.926	.930	.934	.937	.940	.943	.946	.950
.904	.907	.910	.914	.917	.920	.923	.927	.931	.934	.937	.940	.943	.947
.901	.904	.907	.911	.914	.917	.920	.923	.927	.931	.934	.937	.940	.943
.898	.901	.904	.907	.911	.914	.917	.920	.923	.927	.931	.934	.937	.940
.895	.898	.901	.904	.907	.911	.914	.917	.920	.923	.927	.931	.934	.937
.891	.895	.898	.901	.904	.907	.910	.914	.917	.920	.923	.927	.930	.934
.888	.891	.895	.898	.901	.904	.907	.910	.913	.917	.920	.923	.926	.930
.885	.888	.891	.894	.898	.901	.904	.907	.910	.913	.917	.920	.923	.926
.882	.885	.888	.891	.894	.897	.901	.904	.907	.910	.913	.916	.919	.923
.878	.881	.884	.887	.890	.893	.896	.900	.903	.906	.909	.912	.915	.918
.874	.876	.880	.884	.887	.890	.893	.896	.899	.902	.906	.909	.912	.915
.870	.872	.876	.880	.883	.886	.889	.892	.895	.898	.902	.905	.908	.911
.866	.869	.873	.876	.879	.883	.886	.889	.892	.895	.899	.902	.905	.908
.863	.866	.869	.872	.876	.880	.883	.886	.889	.892	.895	.898	.901	.905
.859	.862	.866	.869	.872	.876	.878	.882	.885	.888	.891	.894	.898	.901
.856	.859	.862	.864	.869	.872	.874	.878	.881	.884	.887	.890	.894	.897
.852	.855	.858	.861	.865	.869	.871	.874	.877	.880	.883	.887	.890	.894
.848	.851	.854	.857	.861	.865	.867	.870	.873	.876	.880	.883	.887	.891
.844	.848	.851	.854	.857	.860	.863	.866	.870	.873	.876	.879	.882	.886

TABLE 10.—Inches to millimeters

Inches	0.00	0.01	0.02	0.03	0.04	0.05	0.06	0.07	0.08	0.09
27.0	685.8	686.1	686.3	686.6	686.8	687.1	687.3	687.6	687.8	688.1
27.1	688.3	688.6	688.8	689.1	689.4	689.6	689.9	690.1	690.4	690.6
27.2	690.9	691.1	691.4	691.6	691.9	692.2	692.4	692.7	692.9	693.2
27.3	693.4	693.7	693.9	694.2	694.4	694.7	694.9	695.2	695.5	695.7
27.4	696.0	696.2	696.5	696.7	697.0	697.2	697.5	697.7	698.0	698.2
27.5	698.5	698.8	699.0	699.3	699.5	699.8	700.0	700.3	700.5	700.8
27.6	701.0	701.3	701.5	701.8	702.1	702.3	702.6	702.8	703.1	703.3
27.7	703.6	703.8	704.1	704.3	704.6	704.9	705.1	705.4	705.6	705.9
27.8	706.1	706.4	706.6	706.9	707.1	707.4	707.6	707.9	708.2	708.4
27.9	708.7	708.9	709.2	709.4	709.7	709.9	710.2	710.4	710.7	710.9
28.0	711.2	711.5	711.7	712.0	712.2	712.5	712.7	713.0	713.2	713.5
28.1	713.7	714.0	714.2	714.5	714.8	715.0	715.3	715.5	715.8	716.0
28.2	716.3	716.5	716.8	717.0	717.3	717.6	717.8	718.1	718.3	718.6
28.3	718.8	719.1	719.3	719.6	719.8	720.1	720.3	720.6	720.9	721.1
28.4	721.4	721.6	721.9	722.1	722.4	722.6	722.9	723.1	723.4	723.6
28.5	723.9	724.2	724.4	724.7	724.9	725.2	725.4	725.7	725.9	726.2
28.6	726.4	726.7	727.0	727.2	727.5	727.7	728.0	728.2	728.5	728.7
28.7	729.0	729.2	729.5	729.7	730.0	730.2	730.5	730.7	731.0	731.2
28.8	731.5	731.8	732.0	732.3	732.5	732.8	733.0	733.3	733.5	733.8
28.9	734.0	734.3	734.5	734.8	735.0	735.3	735.5	735.8	736.0	736.3
29.0	736.5	736.8	737.1	737.3	737.6	737.8	738.1	738.3	738.5	738.8
29.1	739.0	739.3	739.5	739.8	740.0	740.3	740.6	740.8	741.1	741.4
29.2	741.6	741.8	742.1	742.3	742.6	742.8	743.1	743.4	743.6	743.9
29.3	744.1	744.4	744.6	744.9	745.2	745.4	745.7	745.9	746.2	746.4
29.4	746.7	746.9	747.2	747.5	747.7	748.0	748.2	748.5	748.7	749.0
29.5	749.3	749.5	749.8	750.0	750.3	750.5	750.8	751.0	751.3	751.5
29.6	751.8	752.0	752.3	752.6	752.8	753.1	753.3	753.6	753.8	754.1
29.7	754.3	754.6	754.8	755.1	755.4	755.6	755.9	756.1	756.4	756.6
29.8	756.9	757.1	757.4	757.7	757.9	758.2	758.4	758.7	758.9	759.2
29.9	759.4	759.7	759.9	760.2	760.4	760.7	760.9	761.2	761.5	761.7
30.0	762.0	762.2	762.5	762.7	763.0	763.2	763.5	763.7	764.0	764.2
30.1	764.5	764.7	765.0	765.3	765.5	765.8	766.0	766.3	766.5	766.8
30.2	767.0	767.3	767.6	767.8	768.1	768.4	768.6	768.9	769.1	769.4
30.3	769.6	769.9	770.1	770.4	770.6	770.9	771.1	771.4	771.7	771.9
30.4	772.2	772.4	772.7	772.9	773.2	773.4	773.7	773.9	774.2	774.4
30.5	774.7	775.0	775.2	775.5	775.7	776.0	776.2	776.5	776.7	777.0

TABLE 11.—*The equivalent of inches of water pressure in inches of mercury and ounces per square inch*

Inches of water	Inches of mercury	Ounces per square inch	Inches of water	Inches of mercury	Ounces per square inch	Inches of water	Inches of mercury	Ounces per square inch	Inches of water	Inches of mercury	Ounces per square inch
0.0			3.5	.258	2.023	7.0	0.515	4.05	10.5	0.772	6.07
0.1	0.007	0.058	3.6	.265	2.081	7.1	.522	4.10	10.6	.780	6.13
0.2	.015	.116	3.7	.272	2.138	7.2	.530	4.16	10.7	.787	6.18
0.3	.022	.173	3.8	.280	2.196	7.3	.537	4.22	10.8	.794	6.24
0.4	.029	.231	3.9	.287	2.254	7.4	.544	4.28	10.9	.802	6.30
0.5	.037	.289	4.0	.294	2.312	7.5	.552	4.33	11.0	.809	6.36
0.6	.044	.347	4.1	.302	2.370	7.6	.559	4.39	11.1	.816	6.41
0.7	.052	.404	4.2	.309	2.427	7.7	.566	4.45	11.2	.824	6.47
0.8	.059	.462	4.3	.316	2.485	7.8	.574	4.51	11.3	.831	6.53
0.9	.066	.520	4.4	.324	2.543	7.9	.581	4.57	11.4	.838	6.59
1.0	.074	.578	4.5	.331	2.601	8.0	.588	4.62	11.5	.846	6.65
1.1	.081	.636	4.6	.338	2.659	8.1	.596	4.68	11.6	.853	6.70
1.2	.088	.693	4.7	.346	2.716	8.2	.603	4.74	11.7	.861	6.76
1.3	.096	.751	4.8	.353	2.774	8.3	.611	4.80	11.8	.868	6.82
1.4	.103	.809	4.9	.360	2.832	8.4	.618	4.85	11.9	.875	6.88
1.5	.110	.867	5.0	.368	2.890	8.5	.625	4.91	12.0	.883	6.94
1.6	.118	.925	5.1	.375	2.948	8.6	.633	4.97	12.1	.890	6.99
1.7	.125	.982	5.2	.383	3.00	8.7	.640	5.03	12.2	.897	7.05
1.8	.132	1.040	5.3	.390	3.06	8.8	.647	5.09	12.3	.905	7.11
1.9	.140	1.098	5.4	.397	3.12	8.9	.655	5.14	12.4	.912	7.17
2.0	.147	1.156	5.5	.405	3.18	9.0	.662	5.20	12.5	.920	7.22
2.1	.154	1.214	5.6	.412	3.24	9.1	.669	5.26	12.6	.927	7.28
2.2	.162	1.271	5.7	.419	3.29	9.2	.677	5.32	12.7	.934	7.34
2.3	.169	1.329	5.8	.427	3.35	9.3	.684	5.37	12.8	.941	7.40
2.4	.177	1.387	5.9	.434	3.41	9.4	.691	5.43	12.9	.949	7.45
2.5	.184	1.445	6.0	.442	3.47	9.5	.699	5.49	13.0	.956	7.51
2.6	.191	1.503	6.1	.449	3.53	9.6	.706	5.55	13.1	.964	7.57
2.7	.199	1.560	6.2	.456	3.58	9.7	.713	5.61	13.2	.971	7.63
2.8	.206	1.618	6.3	.464	3.64	9.8	.721	5.66	13.3	.978	7.69
2.9	.213	1.676	6.4	.471	3.70	9.9	.728	5.72	13.4	.986	7.74
3.0	.221	1.734	6.5	.478	3.76	10.0	.736	5.78	13.5	.993	7.80
3.1	.228	1.792	6.6	.486	3.81	10.1	.743	5.84	13.6	1.000	7.86
3.2	.235	1.849	6.7	.493	3.87	10.2	.750	5.89	13.7	1.008	7.92
3.3	.243	1.907	6.8	.500	3.93	10.3	.758	5.95	13.8	1.015	7.98
3.4	.250	1.965	6.9	.508	3.99	10.4	.765	6.01	13.9	1.022	8.03

TABLE 12.—*The vapor pressure of water*<sup>1</sup>

Temperature (°F.)	Pressure		Temperature (°F.)	Pressure		Temperature (°F.)	Pressure	
	Inches of mercury	mm of mercury		Inches of mercury	mm of mercury		Inches of mercury	mm of mercury
32	0.180	4.580	58	0.486	12.35 <sup>2</sup>	83	1.139	28.93
33	.188	4.766	59	.504	12.79	84	1.176	29.88
34	.195	4.964	60	.522	13.25	85	1.215	30.86
35	.203	5.166	61	.541	13.74	86	1.254	31.86
36	.212	5.376	62	.560	14.23	87	1.295	32.89
37	.220	5.592	63	.581	14.75	88	1.337	33.95
38	.229	5.818	64	.601	15.26	89	1.379	35.04
39	.238	6.052	65	.622	15.81	90	1.423	36.15
40	.248	6.290	66	.644	16.37	91	1.469	37.31
41	.258	6.541	67	.667	16.95	92	1.515	38.49
42	.268	6.799	68	.691	17.55	93	1.563	39.70
43	.278	7.066	69	.715	18.15	94	1.612	40.94
44	.289	7.343	70	.740	18.79	95	1.663	42.23
45	.300	7.627	71	.765	19.43	96	1.715	43.56
46	.312	7.923	72	.792	20.11	97	1.767	44.88
47	.324	8.230	73	.819	20.81	98	1.822	46.28
48	.336	8.546	74	.847	21.51	99	1.878	47.69
49	.349	8.868	75	.876	22.25	100	1.935	49.16
50	.363	9.21	76	.906	23.00	101	1.994	50.66
51	.376	9.56	77	.936	23.78	102	2.055	52.20
52	.391	9.92	78	.966	24.57	103	2.117	53.77
53	.405	10.29	79	1.000	25.40	104	2.181	55.40
54	.420	10.67	80	1.033	26.24	105	2.246	57.04
55	.436	11.08	81	1.067	27.11	106	2.313	58.76
56	.452	11.48	82	1.103	28.02	107	2.382	60.51
57	.469	11.90						

<sup>1</sup> Smithsonian Meteorological Tables, 4th ed., 1918.TABLE 13.—*Gauge pressure (pounds per square inch) to atmospheres (absolute)*

Pounds per square inch	0	10	20	30	40	50	60	70	80	90
0	1.00	1.68	2.36	3.04	3.72	4.40	5.08	5.76	6.44	7.12
100	7.80	8.48	9.17	9.85	10.53	11.21	11.89	12.57	13.25	13.93
200	14.61	15.29	15.97	16.65	17.33	18.01	18.69	19.37	20.05	20.73
300	21.41	22.09	22.77	23.45	24.14	24.82	25.50	26.18	26.86	27.54
400	28.22	28.90	29.58	30.26	30.94	31.62	32.30	32.98	33.66	34.34
500	35.02	35.70	36.38	37.06	37.74	38.42	39.11	39.79	40.47	41.15
600	41.83	42.51	43.19	43.87	44.55	45.23	45.91	46.59	47.27	47.95
700	48.63	49.31	49.99	50.67	51.35	52.03	52.71	53.39	54.08	54.76
800	55.44	56.12	56.80	57.48	58.16	58.84	59.52	60.20	60.88	61.56
900	62.24	62.92	63.60	64.28	64.96	65.64	66.32	67.00	67.68	68.36
1,000	69.04	69.73	70.41	71.09	71.77	72.45	73.13	73.81	74.49	75.17
1,100	75.85	76.53	77.21	77.89	78.57	79.25	79.93	80.61	81.29	81.97
1,200	82.65	83.34	84.01	84.70	85.38	86.06	86.74	87.42	88.10	88.78
1,300	89.46	90.14	90.82	91.50	92.18	92.86	93.54	94.22	94.90	95.58
1,400	96.27	96.95	97.63	98.31	98.98	99.67	100.3	101.0	101.7	102.4
1,500	103.0	103.7	104.4	105.1	105.8	106.5	107.1	107.8	108.5	109.2
1,600	109.9	110.6	111.3	111.9	112.6	113.3	114.0	114.6	115.3	116.0
1,700	116.7	117.4	118.0	118.7	119.4	120.1	120.8	121.4	122.1	122.8
1,800	123.5	124.1	124.8	125.5	126.2	126.9	127.6	128.2	128.9	129.6
1,900	130.3	131.0	131.6	132.3	133.0	133.7	134.4	135.0	135.7	136.4
2,000	137.1	137.8	138.4	139.1	139.8	140.5	141.2	141.9	142.5	143.2
2,100	143.9	144.6	145.2	145.9	146.6	147.3	148.0	148.7	149.3	150.0
2,200	150.7	151.4	152.1	152.7	153.4	154.1	154.8	155.5	156.1	156.8
2,300	157.5	158.2	158.9	159.5	160.2	160.9	161.6	162.3	162.9	163.6
2,400	164.3	165.0	165.7	166.3	167.0	167.7	168.4	169.1	169.8	170.4
2,500	171.1	171.8	172.5	173.2	173.8	174.5	175.2	175.9	176.6	177.2
2,600	177.9	178.6	179.3	180.0	180.6	181.3	182.0	182.7	183.4	184.0
2,700	184.7	185.4	186.1	186.8	187.4	188.1	188.8	189.5	190.2	190.8
2,800	191.5	192.2	192.9	193.6	194.2	194.9	195.6	196.3	197.0	197.7
2,900	198.3	199.0	199.7	200.4	201.1	201.7	202.4	203.1	203.8	204.4

TABLE 14.—Table of equivalent temperatures on the centigrade and Fahrenheit scales

° F.	° C.														
55.0	12.8	60.0	15.6	65.0	18.3	70.0	21.1	75.0	23.9	80.0	26.7	85.0	29.4	90.0	32.2
.1	.8	.1	.6	.1	.4	.1	.2	.1	.9	.1	.7	.1	.5	.1	.3
.2	.9	.2	.7	.2	.4	.2	.2	.2	24.0	.2	.8	.2	.6	.2	.3
.3	.9	.3	.7	.5	.5	.3	.3	.3	.0	.3	.8	.3	.6	.3	.4
.4	13.0	.4	.8	.4	.6	.4	.3	.4	.1	.4	.9	.4	.7	.4	.4
.5	.1	.5	.8	.5	.6	.5	.4	.5	.2	.5	.9	.5	.7	.5	.5
.6	.1	.6	.9	.6	.7	.6	.4	.6	.2	.6	27.0	.6	.8	.6	.6
.7	.2	.7	.9	.7	.7	.7	.5	.7	.3	.7	.0	.7	.8	.7	.6
.8	.2	.8	16.0	.8	.8	.8	.6	.8	.3	.8	.1	.8	.9	.8	.7
.9	.3	.9	.0	.9	.8	.9	.6	.9	.4	.9	.2	.9	.9	.9	.7
56.0	.3	61.0	.1	66.0	.9	71.0	.7	76.0	.4	81.0	.2	86.0	30.0	91.0	.8
.1	.4	.1	.2	.1	.9	.1	.7	.1	.5	.1	.3	.1	.0	.1	.8
.2	.4	.2	.2	.2	19.0	.2	.8	.2	.6	.2	.3	.2	.1	.2	.9
.3	.5	.3	.3	.3	.0	.3	.8	.3	.6	.3	.4	.3	.2	.3	.9
.4	.6	.4	.3	.4	.1	.4	.9	.4	.7	.4	.4	.4	.2	.4	33.0
.5	.6	.5	.4	.5	.2	.5	.9	.5	.7	.5	.5	.5	.3	.5	.0
.6	.7	.6	.4	.6	.2	.6	22.0	.6	.8	.6	.6	.6	.3	.6	.1
.7	.7	.7	.5	.7	.3	.7	.0	.7	.8	.7	.6	.7	.4	.7	.2
.8	.8	.8	.5	.8	.3	.8	.1	.8	.9	.8	.7	.8	.4	.8	.2
.9	.8	.9	.6	.9	.4	.9	.2	.9	.9	.9	.7	.9	.5	.9	.3
57.0	.9	62.0	.7	67.0	.4	72.0	.2	77.0	25.0	82.0	.8	87.0	.6	92.0	.3
.1	.9	.1	.7	.1	.5	.1	.3	.1	.0	.1	.8	.1	.6	.1	.4
.2	14.0	.2	.8	.2	.6	.2	.3	.2	.1	.2	.9	.2	.7	.2	.4
.3	.0	.3	.8	.3	.6	.3	.4	.3	.2	.3	.9	.3	.7	.3	.5
.4	.1	.4	.9	.4	.7	.4	.4	.4	.2	.4	28.0	.4	.8	.4	.6
.5	.2	.5	.9	.5	.7	.5	.5	.5	.3	.5	.0	.5	.8	.5	.6
.6	.2	.6	17.0	.6	.8	.6	.6	.6	.3	.6	.1	.6	.9	.6	.7
.7	.3	.7	.0	.7	.8	.7	.6	.7	.4	.7	.2	.7	.9	.7	.7
.8	.3	.8	.1	.8	.9	.8	.7	.8	.4	.8	.2	.8	31.0	.8	.8
.9	.4	.9	.2	.9	.9	.9	.7	.9	.5	.9	.3	.9	.0	.9	.8
58.0	.4	63.0	.2	68.0	20.0	73.0	.8	78.0	.6	83.0	.3	88.0	.1	93.0	.9
.1	.5	.1	.3	.1	.0	.1	.8	.1	.6	.1	.4	.1	.2	.1	.9
.2	.6	.2	.3	.2	.1	.2	.9	.2	.7	.2	.4	.2	.2	.2	34.0
.3	.6	.3	.4	.3	.2	.3	.9	.3	.7	.3	.5	.3	.3	.3	.0
.4	.7	.4	.4	.4	.2	.4	23.0	.4	.8	.4	.6	.4	.3	.4	.1
.5	.7	.5	.5	.5	.3	.5	.0	.5	.8	.5	.6	.5	.4	.5	.2
.6	.8	.6	.5	.6	.3	.6	.1	.6	.9	.6	.7	.6	.4	.6	.2
.7	.8	.7	.6	.7	.4	.7	.2	.7	.9	.7	.7	.7	.5	.7	.3
.8	.9	.8	.7	.8	.4	.8	.2	.8	26.0	.8	.8	.8	.6	.8	.3
.9	.9	.9	.7	.9	.5	.9	.3	.9	.0	.9	.8	.9	.6	.9	.4
59.0	15.0	64.0	.8	69.0	.6	74.0	.3	79.0	.1	84.0	.9	89.0	.7	94.0	.4
.1	.0	.1	.8	.1	.6	.1	.4	.1	.2	.1	.9	.1	.7	.1	.5
.2	.1	.2	.9	.2	.7	.2	.4	.2	.2	.2	29.0	.2	.8	.2	.6
.3	.2	.3	.9	.3	.7	.3	.5	.3	.3	.3	.0	.3	.8	.3	.6
.4	.2	.4	18.0	.4	.8	.4	.6	.4	.3	.4	.1	.4	.9	.4	.7
.5	.3	.5	.0	.5	.8	.5	.6	.5	.4	.5	.2	.5	.9	.5	.7
.6	.3	.6	.1	.6	.9	.6	.7	.6	.4	.6	.2	.6	32.0	.6	.8
.7	.4	.7	.1	.7	.9	.7	.7	.7	.5	.7	.3	.7	.0	.7	.8
.8	.4	.8	.2	.8	21.0	.8	.8	.8	.6	.8	.3	.8	.1	.8	.9
.9	.5	.9	.3	.9	.0	.9	.9	.9	.6	.9	.4	.9	.2	.9	.9

TABLE 15.—Weights of a normal liter of various gases

[In selecting these values an extensive critical review of the literature has been made. This review will appear in a later publication of this bureau]

$L_n$  = Weight in grams of a normal liter of gas at 0° C. and at a pressure of 760 mm of mercury (at 0° C.), the acceleration of gravity being taken as 980.665 cm per second per second.

Gas	Formula	Molecular weight <sup>1</sup>	$L_n$	Specific gravity, air=1
Acetylene	C <sub>2</sub> H <sub>2</sub>	26.016	1.179	0.912
Air			1.2929	1.0000
Ammonia	NH <sub>3</sub>	17.032	.7710	.5963
Argon	A	39.91	1.7825	1.3787
Arsene	AsH <sub>3</sub>	77.98	3.48	2.69
Iso-Butane	C <sub>4</sub> H <sub>10</sub>	58.08	2.873	2.067
Carbon dioxide	CO <sub>2</sub>	44.000	1.9769	1.5290
Carbon monoxide	CO	28.000	1.2504	.9671
Carbon oxysulphide	COS	60.064	2.72	2.10
Chlorine	Cl <sub>2</sub>	70.914	3.214	2.486
Chlorine monoxide	Cl <sub>2</sub> O	86.914	3.89	3.01
Ethane	C <sub>2</sub> H <sub>6</sub>	30.048	1.3566	1.0493
Ethylene	C <sub>2</sub> H <sub>4</sub>	28.032	1.2604	.9749
Fluorine	F <sub>2</sub>	38.00	1.695	1.311
Helium	He	4.00	.1785	.1381
Hydrogen	H <sub>2</sub>	2.016	.08983	.06952
Hydrogen bromide	HBr	80.924	3.6445	2.8189
Hydrogen chloride	HCl	36.465	1.6392	1.2678
Hydrogen iodide	HI	127.940	5.79	4.48
Hydrogen selenide	H <sub>2</sub> Se	81.2	3.670	2.839
Hydrogen sulphide	H <sub>2</sub> S	34.080	1.539	1.130
Krypton	Kr	82.9	3.708	2.868
Methane	CH <sub>4</sub>	16.032	.7168	.5544
Methyl chloride	CH <sub>3</sub> Cl	50.481	2.3046	1.7825
di-Methyl ether	(CH <sub>3</sub> ) <sub>2</sub> O	46.048	2.1098	1.6318
Methyl fluoride	CH <sub>3</sub> F	34.02	1.5452	1.1951
Neon	Ne	20.2	.9002	.6963
Nitric oxide	NO	30.008	1.3402	1.0366
Nitrogen (chem.)	N <sub>2</sub>	28.016	1.25057	.96724
Nitrogen (atm.)			1.2569	.9722
Nitrosyl chloride	NOCl	65.465	2.992	2.314
Nitrous oxide	N <sub>2</sub> O	44.016	1.9778	1.5297
Oxygen	O <sub>2</sub>	32.000	1.42904	1.10527
Phosphine	PH <sub>3</sub>	34.051	1.5294	1.1829
Propane	C <sub>3</sub> H <sub>8</sub>	44.064	2.020	1.562
mono-Silane	SiH <sub>4</sub>	32.09	1.44	1.11
Silicon tetrafluoride	SiF <sub>4</sub>	104.06	4.684	3.623
Sulphur dioxide	SO <sub>2</sub>	64.064	2.9269	2.2638
Xenon	X	130.2	5.851	4.525

<sup>1</sup> From International Table of Atomic Weights for 1925.

TABLE 16.—Critical constants of substances

[In selecting these figures an extensive critical review of the literature has been made. This review will appear in a later publication of this bureau]

Substance	Critical ° C.	Tem- perature ° C. ab- solute <sup>1</sup>	Critical pressure atmos- phere	Critical density g/cc
Acetylene.....	36	309	62	0.231
Air.....	-140.7	132.4	37.2	{ <sup>2</sup> .35 <sup>3</sup> .31
Allylene.....	128	401		
Ammonia.....	132.4	405.5	111.5	.235
Argon.....	-122	151	48	.53
iso-Butane.....	134	407	37	
n-Butane.....	153	426	36	
Carbon dioxide.....	31.0	304.1	72.9	.460
Carbon monoxide.....	-138.7	134.4	34.6	.311
Carbon oxysulphide.....	105	378	61	
Chlorine.....	144	417	76	.573
Cyanogen.....	128	401	59	
Ethane.....	32.1	305.2	48.8	.21
Ethyl chloride.....	187.2	460.3	52	
Ethylene.....	9.7	282.8	50.9	.22
Helium.....	-267.9	5.2	2.3	.066
Hydrogen.....	-239.9	33.2	12.8	.0310
Hydrogen bromide.....	90	363	84	
Hydrogen chloride.....	51.4	324.5	81.6	
Hydrogen iodide.....	151	424	82	
Hydrogen sulphide.....	100.4	373.5	88.9	
Krypton.....	-63?	210?	54?	.78?
Methane.....	-82.5	190.6	45.8	.162
Methyl chloride.....	143.1	416.2	65.8	.37?
Neon.....	-228.7	44.4	25.9	.484
Nitric oxide.....	-94?	179?	65?	
Nitrogen.....	-147.1	126.0	33.5	.3110
Nitrous oxide.....	36.5	309.6	71.7	.45?
Oxygen.....	-118.8	154.3	49.7	.430
Ozone.....	-5?	268?	92?	
Phosgene.....	183?	456?		
Phosphine.....	52	325	65	
Propane.....	95.6	368.7	43	
Propylene.....	92.3	365.4	45.0	
Silicon tetrafluoride.....	-1	272	50	
Sulphur dioxide.....	157.2	430.3	77.7	.52?
Xenon.....	17	290	58	1.155

<sup>1</sup> The absolute zero is taken as -273.1° C.

<sup>2</sup> "Plait point."

<sup>3</sup> "Critical point of contact."

NOTE.—Doubtful values are indicated by question marks.

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